

TITLE. Calcoli preliminari di dimensionamento strutture

AVAILABLE LANGUAGE: IT

CALCOLI PRELIMINARI DI DIMENSIONAMENTO DELLE STRUTTURE

Progetto di un impianto agrivoltaico denominato “Masala”, di potenza pari a 48,76 MWp, e delle relative opere di connessione.

Da realizzarsi nei comuni di Ploaghe (SS) e Codrongianos (SS).



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UTILIZATION SCOPE Basic Design

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1.0 INDICAZIONI GENERALI

1.1 Struttura

Legge 5 novembre 1971 N. 1086 - Norme per la disciplina delle opere in conglomerato cementizio armato normale e precompresso ed a struttura metallica.

Decreto Ministeriale 17/01/2018 – Aggiornamento delle Norme tecniche per le Costruzioni.

Circolare Esplicativa 21/01/2019 – Istruzioni per l'applicazione dell'aggiornamento delle Norme tecniche per le Costruzioni D.M. 17/01/2018.

1.2 Norme di cui è consentita l'applicazione ai sensi del cap. 12 del D.M. 17/01/2018

UNI EN 1990: 2006 - Eurocodice 1 – Criteri generali di progettazione strutturale.

UNI ENV 1991-1-1: 2010; -1-2; 1-3; 1-4; 1.5; Azioni sulla struttura.

Eurocodice 2 - Progettazione delle strutture in calcestruzzo.

UNI ENV 1992-1-1 Parte 1-1: Regole generali e regole per gli edifici.

Eurocodice 3 – Progettazione delle strutture in acciaio.

UNI ENV 1993-1-1 - Parte 1-1: Regole generali e regole per gli edifici.

UNI EN 206:2016 - Calcestruzzo. Specificazioni, prestazioni, produzione e conformità.

Servizio Tecnico Centrale del Ministero dei Lavori Pubblici – “Linee Guida sul calcestruzzo strutturale”

Circ. MIN.LL.PP. N.11951 del 14 febbraio 1992 - Circolare illustrativa della legge N. 1086.

1.3 Carichi e sovraccarichi

Decreto Ministeriale 17/01/2018 – Aggiornamento delle Norme tecniche per le Costruzioni.

Circolare Esplicativa 21/01/2019 – Istruzioni per l'applicazione dell'aggiornamento delle Norme tecniche per le Costruzioni D.M. 17/01/2018.

1.4 Terreni e fondazione

Decreto Ministeriale 17/01/2018 – Aggiornamento delle Norme tecniche per le Costruzioni.

Circolare Esplicativa 21/01/2019 – Istruzioni per l'applicazione dell'aggiornamento delle Norme tecniche per le Costruzioni D.M. 17/01/2018.

D.M. 11 marzo 1988 – Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione ed il collaudo delle opere di sostegno delle terre e delle opere di fondazione.

Circ. MIN.LL.PP. N.30483 del 24 settembre 1988 - Istruzioni riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione ed il collaudo delle opere di sostegno delle terre.

1.5 Norme generali di riferimento

"Linee guida in materia di impianti agrivoltaici", Ministero della Transizione Ecologica - Dipartimento per l'energia.

LEGGE 29 luglio 2021, n. 108 *"Conversione in legge, con modificazioni, del decreto-legge 31 maggio 2021, n. 77, recante governance del Piano nazionale di ripresa e resilienza e prime misure di rafforzamento delle strutture amministrative e di accelerazione e snellimento delle procedure"*.

"Consultazione pubblica Misura PNRR Sviluppo Agrivoltaico: Piano di Ripresa e Resilienza, Missione 2 (Rivoluzione verde e Transizione ecologica), Componente 2 (Energia rinnovabile, idrogeno, rete e mobilità sostenibile), Investimento 1.1 (Sviluppo Agrovoltico)".

"Piano Nazionale Integrato per l'Energia e il Clima 2030 (PNIEC)", Ministero dello Sviluppo Economico ([PNIEC_finale_17012020.pdf \(mise.gov.it\)](#)).

D.Lgs. 8 novembre 2021, n. 199, di recepimento della direttiva UE 2018/2001 del Parlamento europeo e del Consiglio sulla promozione dell'uso dell'energia da fonti rinnovabili (*Direttiva RED II*).

2.0 DESCRIZIONE GENERALE DEL PROGETTO

2.1 Generalità

La seguente relazione illustra il dimensionamento strutturale delle strutture tracker del progetto proposto da Lightsource Renewable Energy Italy SPV 23 S.R.L., che prevede la realizzazione di un impianto agrivoltaico denominato "Masala", localizzato nel comune di Codrogianos (SS) e Ploaghe (SS). L'impianto, installato a terra, con potenza nominale massima pari a 48,76 MW_p, verrà collegato in antenna a 36 kV con un futuro ampliamento della Stazione Elettrica (SE) di Trasformazione 380/220/150 kV della RTN "Codrongianos".

I criteri generali adottati per lo sviluppo del presente progetto sono in linea con le prescrizioni contenute nel quadro normativo di riferimento per tali interventi.

Inoltre, la presente relazione tecnica ha carattere di preliminare e rimanda ad approfondimenti successivi per la profondità di infissione delle strutture portamoduli. Si rimanda, inoltre, al produttore delle strutture portamoduli, scelto in fase successiva, per le caratteristiche delle stesse.

Il calcolo, pertanto, fornisce un'indicazione per caratterizzare le proprietà meccaniche dei sostegni fissi dei moduli fotovoltaici, le assunzioni ed ipotesi alla base della progettazione dovranno essere verificate nelle successive fasi di ingegneria con quanto dichiarato dai produttori/fornitori delle strutture stesse.

In linea generale, si prevede l'infissione delle strutture porta-moduli nel terreno mediante battipalo, per una profondità non inferiore ai 2,5 m, tale lunghezza sarà definita nelle successive fasi di progettazione (ingegneria di dettaglio), a seguito della definizione finale delle caratteristiche tecniche e geometriche della struttura e dell'esecuzione di specifiche prove di campo (pull-out test).

Si specifica, inoltre, che l'eventuale posizionamento di manufatti prefabbricati e di container sarà previsto su magrone in CLS gettato in opera e/o platea in CLS debolmente armata; le relative fondazioni saranno di tipo prefabbricato e pertanto il dimensionamento sarà a cura ed onere del fornitore degli elementi prefabbricati.

In riferimento all'altezza minima dei moduli fotovoltaici rispetto al suolo, ossia misurata con i moduli collocati alla massima inclinazione tecnicamente raggiungibile, essa non sarà inferiore a 60 cm; sarà compresa tra 60 cm e 130 cm, da definire nella fase successiva di ingegneria.

In via cautelativa, le verifiche di seguito riportate hanno considerato un'altezza minima di 130 cm.

Si riportano in sintesi le caratteristiche generali inserite nel codice di calcolo:

Intestazione del lavoro	Masala
Tipo di struttura	Nello Spazio
Tipo di analisi	Statica e Sismica
Tipo di soluzione	Lineare
Unita' di misura delle forze	daN - kg
Unita' di misura delle lunghezze	cm - m
Normativa	NTC 2018

2.2 Descrizione delle strutture

Nel seguito si riporta una breve descrizione delle strutture progettate.

2.2.1 Struttura tracker 2x14

La struttura sarà caratterizzata dai seguenti elementi (Vedi Figura 1 e Figura 2):

- 1) Telaio Principale, composto da:
 - a. Montante – sezione HEA 280;
 - b. Trave principale – sezione 300x300x10;
- 2) Travi secondarie porta pannelli – sezione 150x100x10.

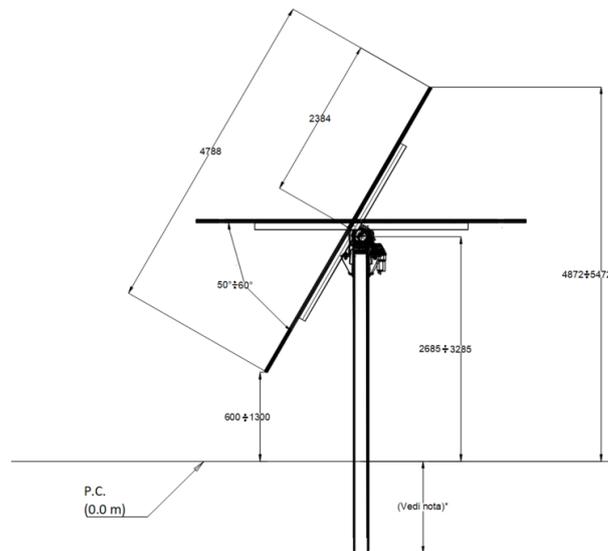


Figure 1: Telaio trasversale Tracker 2x14

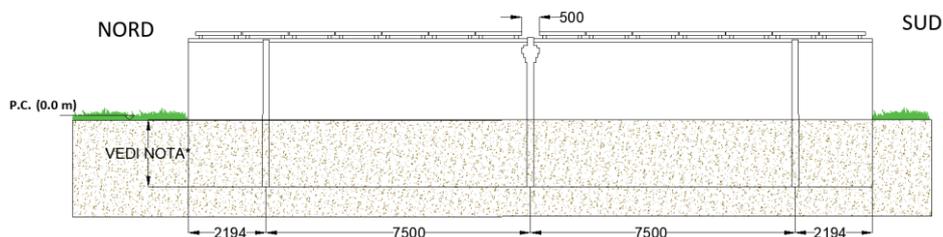


Figure 2: Vista Longitudinale Tracker 2x14

Note* Le dimensioni indicate saranno validate in una fase successiva del progetto (ingegneria di dettaglio) dopo aver definito le caratteristiche geometriche e meccaniche delle strutture porta moduli (scelta delle sezioni e del fornitore/produttore), i parametri geotecnici dei terreni ed eseguito le prove di campo (pull-out test ecc.).

MODELLI DI CALCOLO

Si è analizzato la struttura nelle due configurazioni tipo:

- Configurazione a riposo: inclinazione pannelli 0°;
- Configurazione in esercizio: inclinazione pannelli a 60°.

Nei calcoli si è considerato che le strutture siano dotate di sensori tali che nella configurazione di esercizio una volta raggiunta la velocità limite del vento di 15 m/s la struttura tracker si posizionerà automaticamente in configurazione di riposo.

Tale valore della velocità del vento dovrà essere validato e confermato dal produttore/fornitore scelto per le strutture tracker nelle successive fasi.

Nel seguito si riportano le immagini dei due modelli di calcolo analizzati.

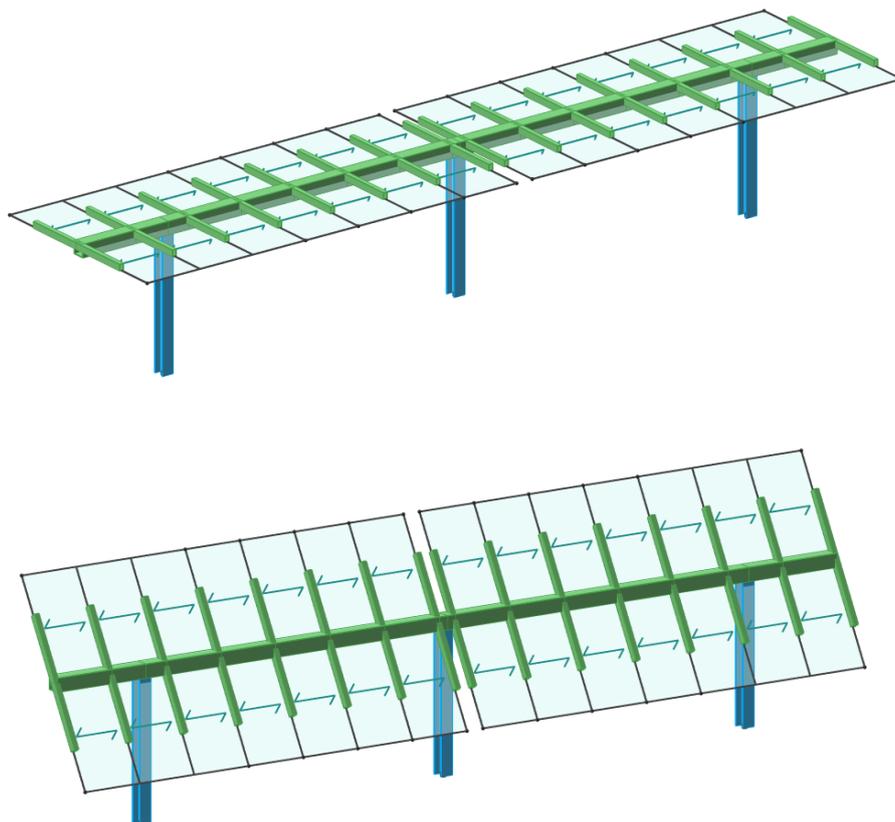


Figure 3: Vista modellazione strutturale: in alto configurazione di riposo, in basso configurazione di esercizio
Tutti gli elementi saranno realizzati con acciaio del tipo S355 (FE 510).

LISTA MATERIALI UTILIZZATI

Materiale acciaio:

Modulo elastico – $E = 2.100.000 \text{ daN/cm}^2$

Coefficiente di Poisson – $\nu = 0,30$

Peso specifico – $\gamma = 7.850 \text{ daN/m}^3$

2.2.2 Struttura tracker 2x28

La struttura sarà caratterizzata dai seguenti elementi (Vedi Figura 4 e Figura 5):

- 1) Telaio Principale, composto da:
 - a. Montante – sezione HEA 280;
 - b. Trave principale – sezione 300x300x10;
- 2) Travi secondarie porta pannelli – sezione 150x100x10.

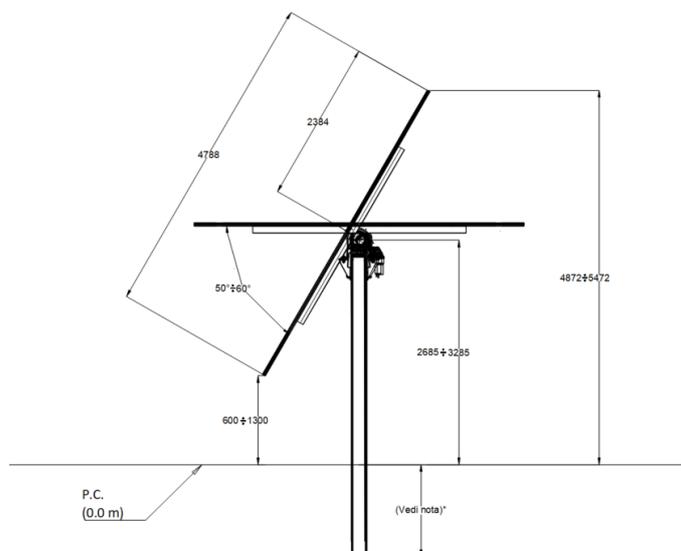


Figure 4: Telaio trasversale Tracker 2x28

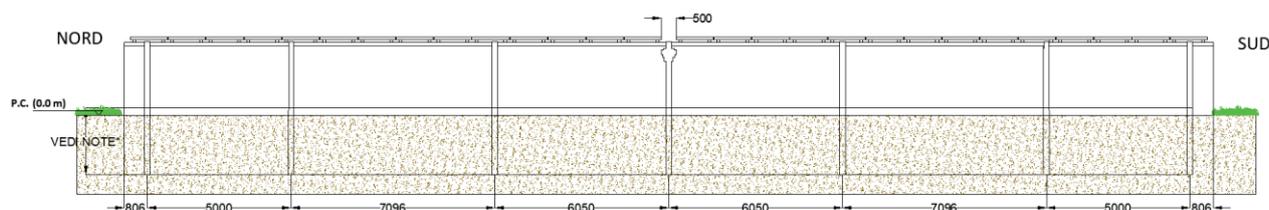


Figure 5: Vista Longitudinale Tracker 2x28

Note* Le dimensioni indicate saranno validate in una fase successiva del progetto (ingegneria di dettaglio) dopo aver definito le caratteristiche geometriche e meccaniche delle strutture porta moduli (scelta delle sezioni e del fornitore/produttore), i parametri geotecnici dei terreni ed eseguito le prove di campo (pull-out test ecc.).

MODELLI DI CALCOLO

Si è analizzato la struttura nelle due configurazioni tipo:

- Configurazione a riposo: inclinazione pannelli 0°;
- Configurazione in esercizio: inclinazione pannelli a 60°.

Nei calcoli si è considerato che le strutture siano dotate di sensori tali che nella configurazione di esercizio una volta raggiunta la velocità limite di 15 m/s la struttura tracker si posizionerà automaticamente in configurazione di riposo.

Tale valore della velocità del vento dovrà essere validato e confermato dal produttore/fornitore scelto per le strutture tracker nelle successive fasi.

Nel seguito si riportano le immagini dei due modelli di calcolo analizzati.

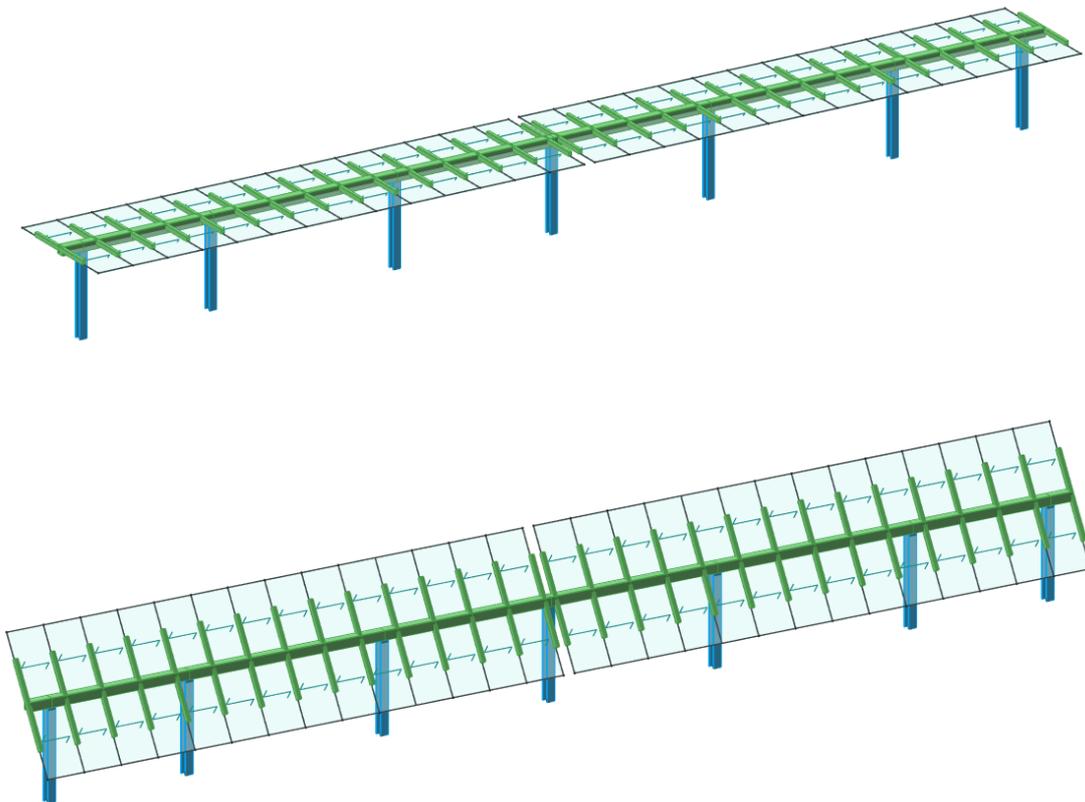


Figure 6: Vista modellazione strutturale: in alto configurazione di riposo, in basso configurazione di esercizio
Tutti gli elementi saranno realizzati con acciaio del tipo S355 (FE 430) o superiori.

LISTA MATERIALI UTILIZZATI

Materiale acciaio:

Modulo elastico - $E = 2.100.000 \text{ daN/cm}^2$

Coefficiente di Poisson - $\nu = 0,30$

Peso specifico - $\gamma = 7.850 \text{ daN/m}^3$

3.0 CARICHI DI PROGETTO

3.1 Generalità

I carichi considerati per la progettazione delle strutture tracker sono:

Carichi permanenti (G):

- Peso Strutture (Carico Permanente Strutturale - G1)
- Peso Moduli (Carico Permanente non Strutturale - G2)

Carichi Variabili (Q):

- Neve
- Vento
- Sisma

3.2 Carichi permanenti strutturale

I pesi propri degli elementi strutturali, quali travi e pilastri, sono stati considerati in automatico dal programma di calcolo.

Si assume il seguente valore per il peso del materiale utilizzato:

- Peso Strutture in acciaio: 7850 daN/m³
- Peso Strutture in cemento armato: 2500 daN/m³

3.3 Carichi permanenti non strutturali

Nel seguito si riportano i valori dei carichi permanenti non strutturali assunti nel calcolo delle strutture oggetto della presente progettazione.

Per le strutture tracker i carichi permanenti non strutturali assumono i seguenti valori:

- Peso Moduli: 35 daN

3.4 Carichi da neve

Il carico provocato dalla presenza della neve agisce in direzione verticale ed è riferito alla proiezione orizzontale della superficie della copertura. Esso è valutato con la seguente espressione:

$$q_s = \mu_i \cdot q_{sk} \cdot C_E \cdot C_t$$

Provincia : Masala (SS)

Zona : III Costiera e Isole

Altitudine : 550 m s.l.m.

Valore caratteristico neve al suolo : $q_{sk} = 118 \text{ kg/m}^2$

Coefficiente di esposizione C_E : 0,9

Coefficiente termico C_t : 1

Tipo di copertura: ad una falda

Si assume che la neve non sia impedita di scivolare.

Se l'estremità più bassa della falda termina con un parapetto, una barriera od altre ostruzioni, allora il coefficiente di forma non potrà essere assunto inferiore a 0,8 indipendentemente dall'angolo α .

La struttura del tracker può essere assimilata ad una pensilina ad una falda, per tale motivo si può considerare la condizione di carico riportata nella figura, la quale deve essere utilizzata per entrambi i casi di carico, con o senza vento.

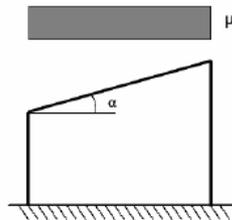


Figure 7: Carico neve per copertura ad una falda

Carico da neve :

Per $\alpha = 0^\circ$ configurazione di riposo

$$q_s(\mu_i=0,8) = 84,7 \text{ kg/m}^2$$

Si assume un carico pari a **85 kg/m²**.

Per $\alpha = 60^\circ$ configurazione di esercizio

$$q_s(\mu_i=0,0) = 0,0 \text{ kg/m}^2$$

Si assume un carico pari a **5 kg/m²**.

3.5 Carichi da vento

La pressione del vento è calcolata secondo l'espressione:

$$p = q_b \cdot c_e \cdot c_p \cdot c_d$$

Provincia: Masala (SS)

Zona: 6

Altitudine: 550 m s.l.m

Tempo di ritorno T_r : 50 anni;

Distanza dalla costa: entro 30 km dalla costa

Classe di rugosità del terreno: D

Categoria di esposizione del sito: II

Coefficiente topografico c_t : 1

Coefficiente dinamico c_d : 1

Per la configurazione di riposo:

Velocità di riferimento $v_b(T_r)$: 28 m/s

Altezza della costruzione h : 3,28 m

Pressione cinetica di riferimento q_b : 52,7 Kg/m²

Coefficiente di esposizione $c_e(z)$: $c_e = 1,8$

Si assume il seguente valore della pressione del vento:

$p = 94,8 \text{ daN/m}^2$

Il riferimento è il p.to C3.3.8.2.1 della Circolare n. 7 del 21.01.2019 per cui risulta (vedi anche figura seguente):

$\alpha = 0^\circ$

$\varphi = 0$

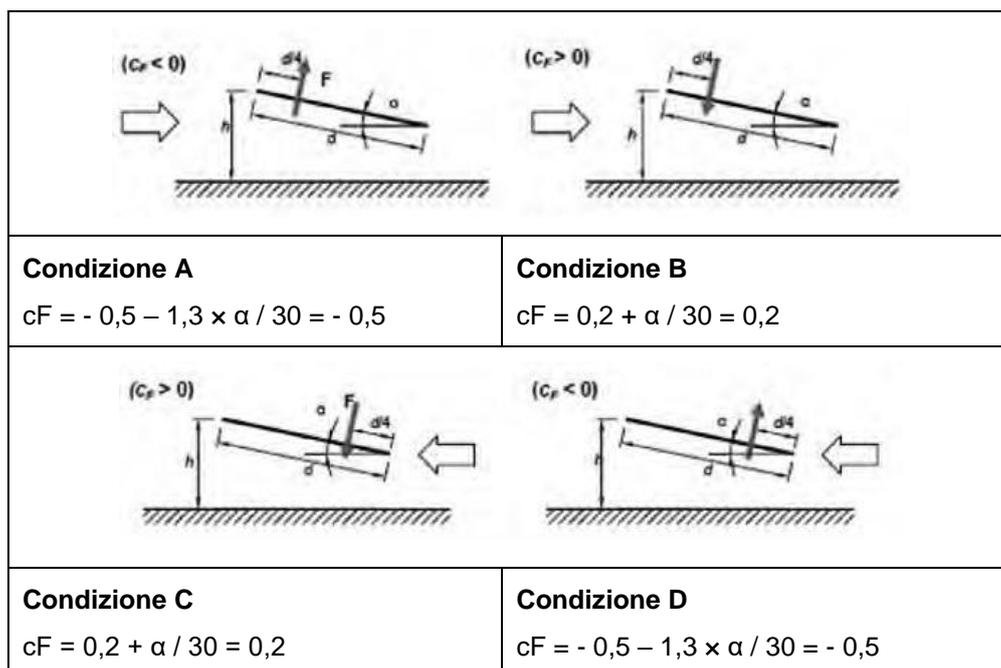


Figure 8: Casistiche carico vento per tettoia ad una falda – condizioni di riposo

Per la configurazione di esercizio:

Velocità di riferimento $v_b(Tr)$: 15 m/s

Altezza della costruzione h : 5,45 m

Pressione cinetica di riferimento q_b : 15,1 Kg/m²

Coefficiente di esposizione $c_e(z)$: $c_e = 1,98$

Si assume il seguente valore della pressione del vento:

$p = 29,9 \text{ daN/m}^2$

Il riferimento è il p.to C3.3.8.2.1 della Circolare n. 7 del 21.01.2019 per cui risulta (vedi anche figura seguente):

$\alpha = 60^\circ$

$\varphi = 0$

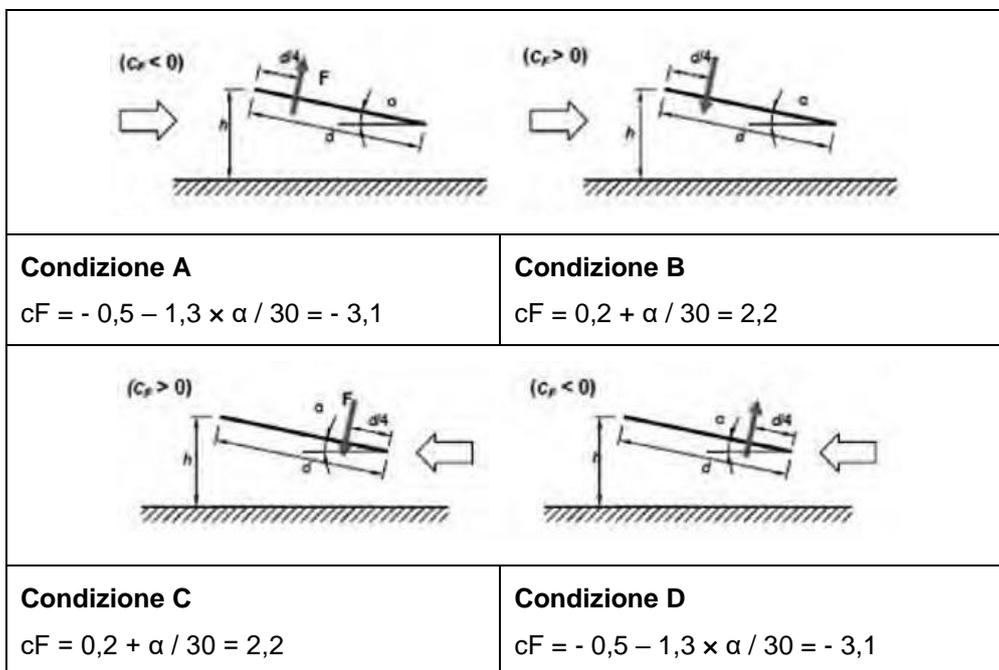


Figure 9: Casistiche carico vento per tettoia ad una falda – condizioni di esercizio

3.6 Azione sismica

Lo spettro di risposta di progetto in accelerazione, a meno del coefficiente γ_{Rd} , è stato determinato nelle seguenti ipotesi:

- Costruzione di tipo 2 - opere ordinarie con vita nominale $VN = 50$ anni;
- Classe d'uso costruzione II per cui periodo di riferimento per l'azione sismica $VR = VN \times CU = 50 \times 1,0 = 50$ anni;
- Categoria di sottosuolo D;
- Categoria topografica T1 per cui $ST = 1,0$;
- Struttura a comportamento non dissipativo

Si riportano di seguito i valori relativi alle azioni sismiche caratteristiche di sito:

Stato limite	ag/g	F0	TC* [s]	q
SLV	0,0395	2,77	0,295	A seconda del tipo di struttura
SLD	0,022	2,628	0,1874	A seconda del tipo di struttura

Essendo:

- ag l'accelerazione orizzontale massima al sito;
- g l'accelerazione di gravità;
- F0 il valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;
- TC* il valore di riferimento per la determinazione del periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;
- q il fattore di comportamento.

4.0 CRITERI DI VERIFICA

4.1 DI OPERE IN ACCIAIO CON IL METODO DELLE NTC 2018 E DELL'EUROCODICE 3

Il tabulato riporta una legenda dei parametri di calcolo e di progetto richiamati nel tabulato stesso, le caratteristiche delle sezioni e dei materiali utilizzate e successivamente, in sequenza per ogni asta, le verifiche svolte nelle quali sono riportati:

- numero combinazione di carico;
- sollecitazioni di calcolo a seconda della verifica condotta;
- classe della sezione; non viene riportata se agisce la trazione;
- parametri di calcolo utilizzati nella verifica;
- Verifica svolta con indice di sfruttamento ottenuto come rapporto fra la sollecitazione esterna e la resistenza di progetto.

Se è abilitata la verifica di stabilità per aste consecutive (membrature) viene riportato un ulteriore tabulato riguardante la verifica globale delle aste che costituiscono la membratura; la sola differenza con il precedente riguarda l'indicazione, nel prospetto, della lunghezza totale che influisce sul valore di snellezza e quindi sul risultato finale della verifica.

5.0 RISULTATI STRUTTURE TRACKER

5.1 Tracker 2x14 - configurazione a riposo ($\alpha = 0^\circ$)

5.1.1 Diagrammi tassi di sfruttamento

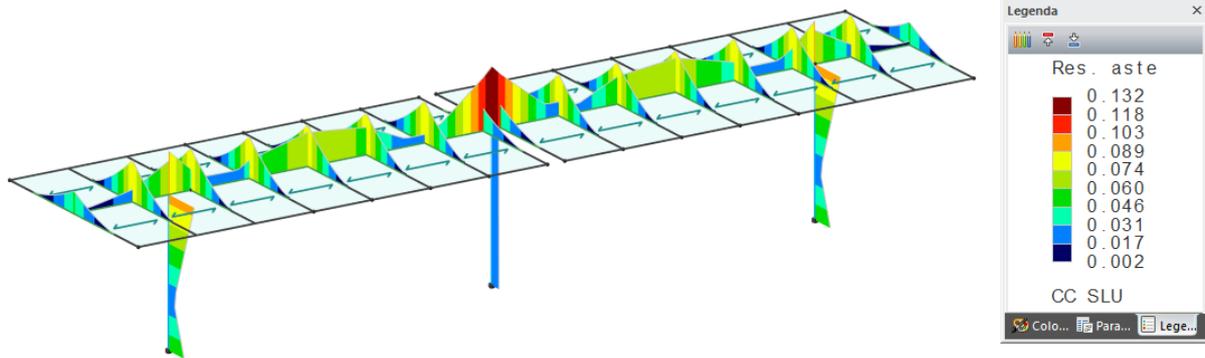


Diagramma tassi di sfruttamento resistenza aste combo SLU con valore massimo pari a 0,132

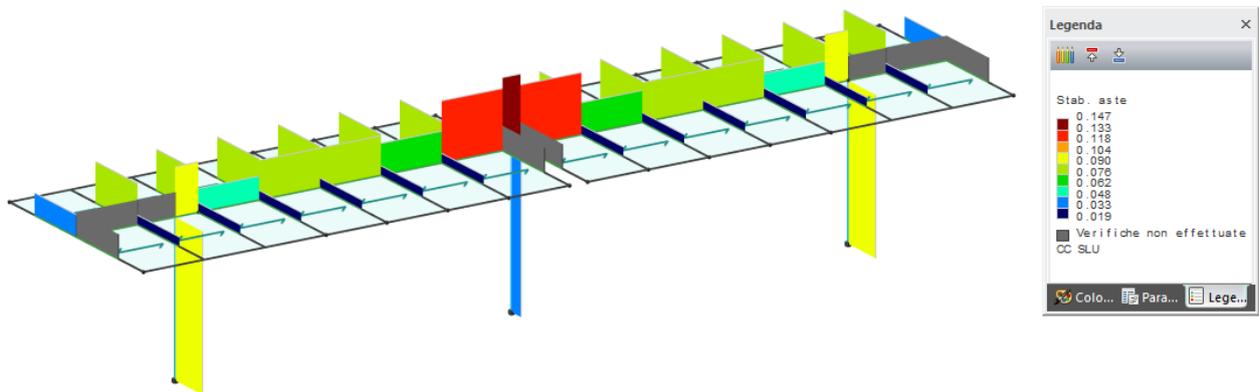


Diagramma tassi di sfruttamento stabilità aste combo SLU con valore massimo pari a 0,147

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

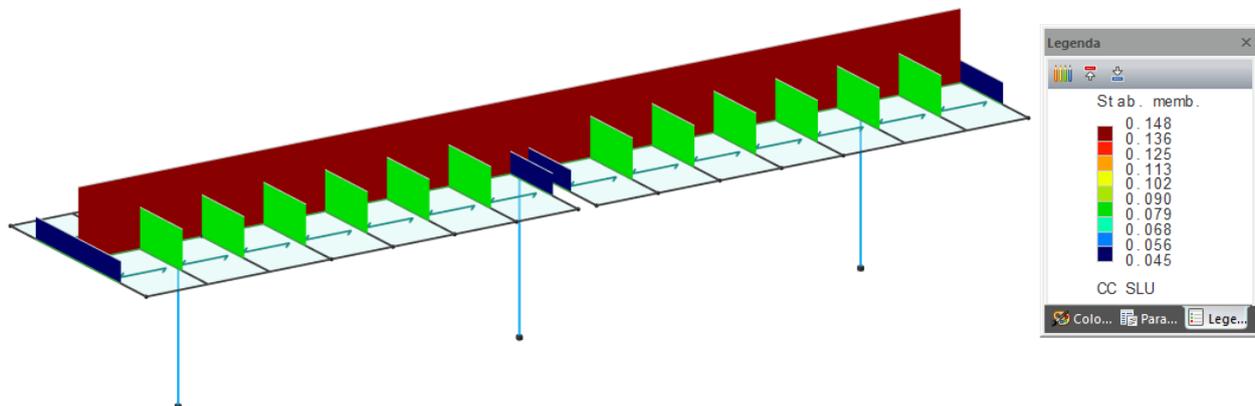


Diagramma tassi di sfruttamento stabilità membrane combo SLU con valore massimo pari a 0,148

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

Figure 10: Tassi di sfruttamento SLU (Stato limite ultimo)

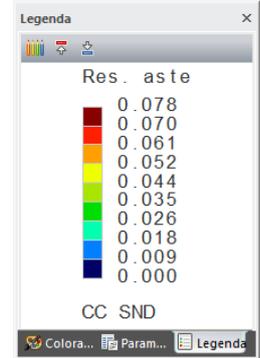
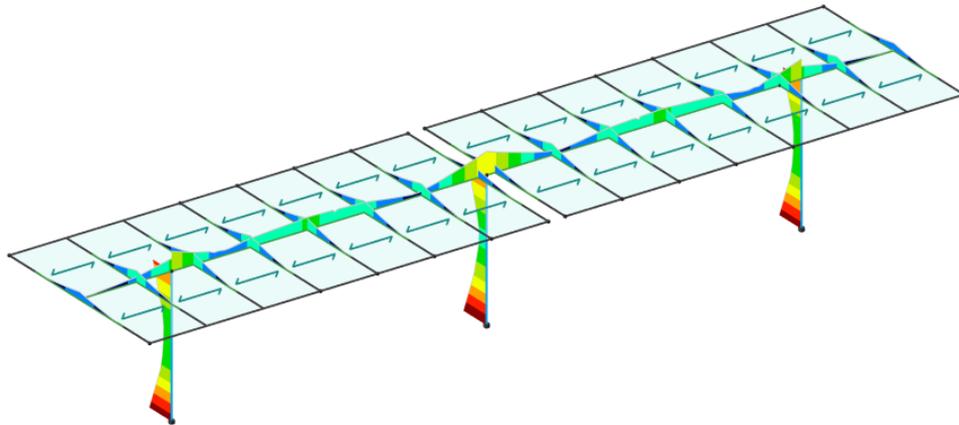


Diagramma tassi di sfruttamento resistenza aste combo SND con valore massimo pari a 0,078

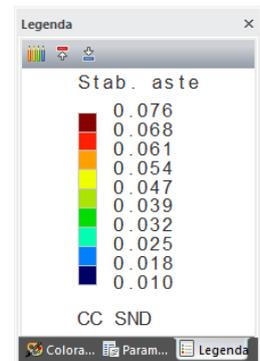
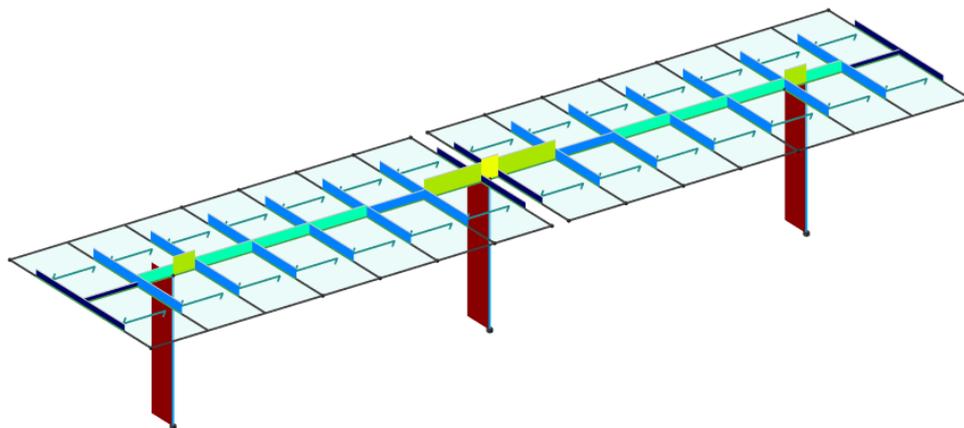


Diagramma tassi di sfruttamento stabilità aste combo SND con valore massimo pari a 0,076

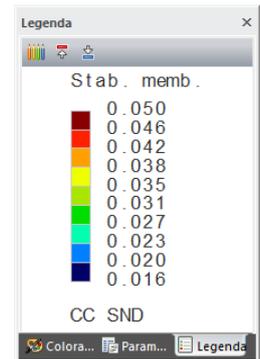
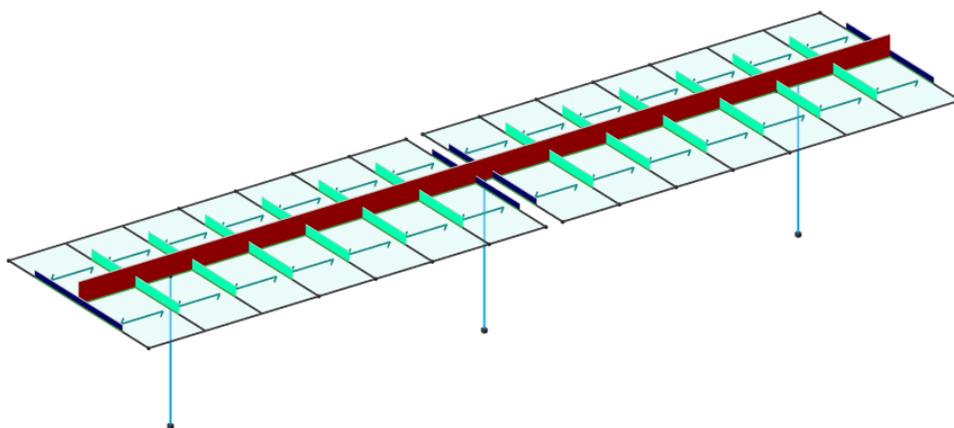


Diagramma tassi di sfruttamento stabilità membrature combo SND con valore massimo pari a 0,050

Figure 11: Tassi di sfruttamento SND (Stato limite di vita non dissipativo)

5.1.2 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:

ModeSt ver. 8.31, licenza n. 7429, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:

Xfinest ver. 9.6.2, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18

Tipo di calcolo: sismica statica

Vincoli esterni: Considera sempre vincoli assegnati in modellazione

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Tipo di analisi: Lineare
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Non sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

Opzioni generali:

- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Si
- Check sequenza di Sturm: Si
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

- Tipo di elemento bidimensionale: QF46

- Calcolo sforzo nei nodi: No

Opzioni per analisi P-Delta:

- Numero massimo di iterazioni: 15
- Valore della norma euclidea degli spostamenti: 1.0000E-04

Opzioni per analisi pushover:

- Esegui analisi in regime di piccoli spostamenti: Si

Opzioni per analisi pushover murature:

- Interrompi analisi nel caso di plasticizzazione per carichi statici: Si
- Utilizza sforzo normale medio: Si

Metodo di convergenza:

- Forze e momenti residui (F)
Valore della norma euclidea delle forze: 1.0000E-03
Valore della norma euclidea dei momenti: 1.0000E-02

- Opzioni aggiuntive per analisi non lineari in presenza di elementi bidimensionali con comportamento Drucker-Prager:

OPTION PARAM AUTO_INCREMENT=YES
OPTION PARAM LINE_SEARCHES=YES
OPTION PARAM BGINCRS=1.0
OPTION PARAM AVINCRS=1.0

Dati struttura

- Sito di costruzione: PP5J+MV Ploaghe SS, Italia LON. 8.73219 LAT. 40.70920
Contenuto tra ID reticolo: 26271 26049 26272 26050

Simbologia

- Ag =Accelerazione orizzontale massima al sito
- C_c =Coefficiente funzione della categoria del suolo
- F_o =Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
- S_s =Coefficiente di amplificazione stratigrafica
- T_r =Periodo di ritorno <anni>
- TCC =Tipo di combinazione di carico
 - SLU = Stato limite ultimo
 - SLE R = Stato limite d'esercizio, combinazione rara
 - SLE F = Stato limite d'esercizio, combinazione frequente
 - SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 - SLD = Stato limite di danno
 - SND = Stato limite di salvaguardia della vita (non dissipativo)
- Tc* =Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

TCC	T _r	Ag <g>	F _o	Tc*	S _s	C _c
SLD	50	0.0217	2.63	0.19	1.80	2.89
SLV	475	0.0395	2.77	0.29	1.80	2.30

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale V_N: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 3.29 <m>
- Altezza della struttura: 3.29 <m>
- Numero piani edificio: 0
- Coefficiente θ: 0.00
- Edificio regolare in altezza: Si
- Edificio regolare in pianta: Si
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di calcolo

- Categoria del suolo di fondazione: D
- Tipologia strutturale: acciaio a mensola o a pendolo inverso

Periodo T ₁	0.20741
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovrarresistenza (α _u /α ₁)	1.00
Valore di riferimento del fattore di comportamento (q ₀)	2.00
Fattore riduttivo (K _w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di comportamento dissipativo (q)	2.00
Fattore di comportamento non dissipativo (qND)	1.33
Fattore di comportamento per SLD (qD)	1.33

- Categoria topografica: T2 - Pendii con inclinazione media i > 15°
- Coeff. amplificazione topografica S_T: 1.20
- Accelerazione di picco del terreno AgS: 0.0853 <g>
- Fattore di comportamento per sisma verticale (q_v): 1.50
- Smorzamento spettro: 5.00%

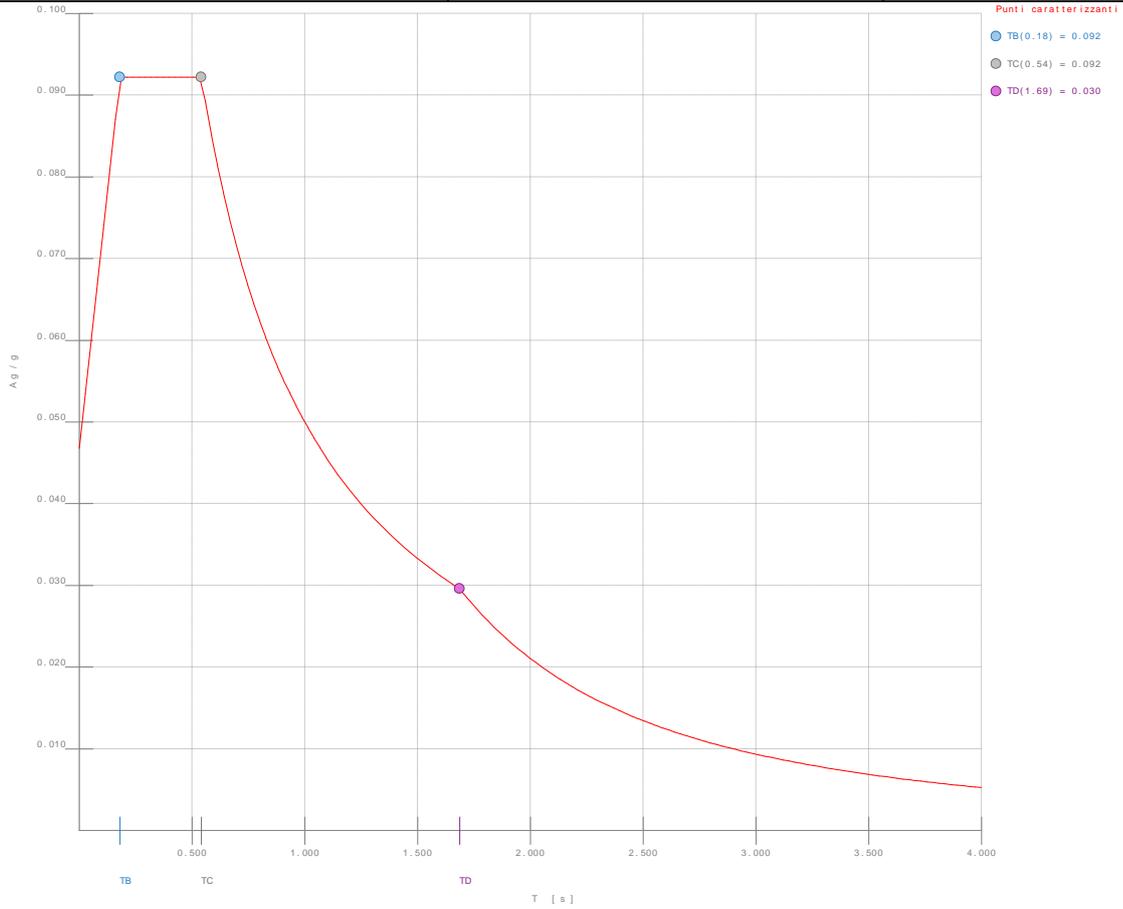


Figura numero 1: Spettro SLD

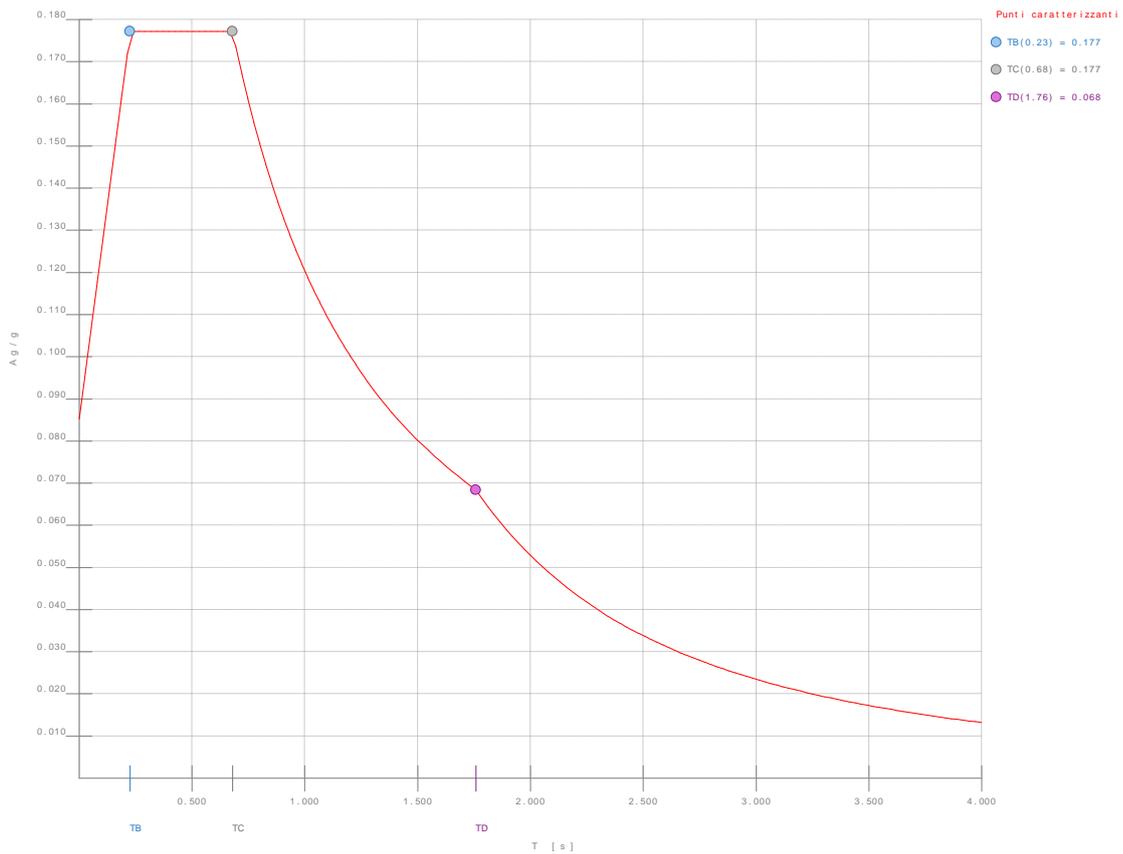


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>
- Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

- N = Numero
- Comm. = Commento
- 1 = G1 - Peso Proprio
- 2 = G2 - Permanenti non strutturali
- 3 = Q - Variabili neve
- 4 = Vento da retro - Cond. A
- 5 = Vento da retro - Cond. B
- 6 = Vento da fronte - Cond. C
- 7 = Vento da fronte - Cond. D
- F = azioni orizzontali convenzionali
- SLU = Stato limite ultimo
- SLR = Stato limite per combinazioni rare
- SLF = Stato limite per combinazioni frequenti
- SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
- S = Si
- N = No

N	Comm.	1	2	3	4	5	6	7	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	S	S	S	N	N	N	N	S	N	N	N	N
2	Calcolo statico	S	S	N	N	N	N	N	S	S	S	S	S
3	Vento cond A	S	S	S	N	N	N	N	S	S	S	S	S
4	Vento cond B	S	S	S	N	N	N	N	S	S	S	S	S
5	Vento cond C	S	S	N	N	N	N	N	S	S	S	S	S
6	Vento cond D	S	S	N	N	N	N	N	S	S	S	S	S

Elenco combinazioni di carico simboliche

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	1	2	3	4	5	6	7	S
1	Amb. 1 (Sisma)	SLU S	1	1	ψ_2	-----	-----	-----	-----	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	-----	-----
3	Amb. 2 (SLE R)	SLE R	1	1	ψ_1	-----	-----	-----	-----	-----
4	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	-----	-----	-----	-----	-----
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	-----	-----	-----	-----	-----
6	Amb. 3 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	γ max	-----	-----	-----	-----
7	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	-----
8	Amb. 3 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
9	Amb. 3 (SLE R)	SLE R	1	1	1	ψ_0	-----	-----	-----	-----
10	Amb. 3 (SLE F)	SLE F	1	1	ψ_2	ψ_1	-----	-----	-----	-----
11	Amb. 3 (SLE F)	SLE F	1	1	ψ_1	ψ_2	-----	-----	-----	-----
12	Amb. 3 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	-----	-----	-----	-----
13	Amb. 4 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
14	Amb. 4 (SLU)	SLU	γ max	γ max	γ max	-----	$\psi_0 * \gamma$ max	-----	-----	-----
15	Amb. 4 (SLE R)	SLE R	1	1	ψ_0	-----	1	-----	-----	-----
16	Amb. 4 (SLE R)	SLE R	1	1	1	-----	ψ_0	-----	-----	-----
17	Amb. 4 (SLE F)	SLE F	1	1	ψ_2	-----	ψ_1	-----	-----	-----
18	Amb. 4 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_2	-----	-----	-----
19	Amb. 4 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	-----	-----	-----
20	Amb. 5 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	γ max	-----	-----
21	Amb. 5 (SLU)	SLU	γ max	γ max	γ max	-----	-----	$\psi_0 * \gamma$ max	-----	-----
22	Amb. 5 (SLE R)	SLE R	1	1	ψ_0	-----	-----	1	-----	-----
23	Amb. 5 (SLE R)	SLE R	1	1	1	-----	-----	ψ_0	-----	-----
24	Amb. 5 (SLE F)	SLE F	1	1	ψ_2	-----	-----	ψ_1	-----	-----
25	Amb. 5 (SLE F)	SLE F	1	1	ψ_1	-----	-----	ψ_2	-----	-----
26	Amb. 5 (SLE Q)	SLE Q	1	1	ψ_2	-----	-----	ψ_2	-----	-----
27	Amb. 6 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	γ max	-----

28	Amb. 6 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	$\Psi_0 * \gamma$ max	-----
29	Amb. 6 (SLE R)	SLE R	1	1	Ψ_0	-----	-----	-----	1	-----
30	Amb. 6 (SLE F)	SLE R	1	1	1	-----	-----	-----	Ψ_0	-----
31	Amb. 6 (SLE F)	SLE F	1	1	Ψ_2	-----	-----	-----	Ψ_1	-----
32	Amb. 6 (SLE F)	SLE F	1	1	Ψ_1	-----	-----	-----	Ψ_2	-----
33	Amb. 6 (SLE Q)	SLE Q	1	1	Ψ_2	-----	-----	-----	Ψ_2	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: Si

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

An. = Tipo di analisi
 L = Lineare
 NL = Non lineare
 PD = P-Delta

Bk = Buckling
 S = Si
 N = No

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	S X	S Y
1	Amb. 1 (SLU S) S +X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
2	Amb. 1 (SLE) S +X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
3	Amb. 1 (SLU S) S +X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
4	Amb. 1 (SLE) S +X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
5	Amb. 1 (SLU S) S -X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
6	Amb. 1 (SLE) S -X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
7	Amb. 1 (SLU S) S -X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
8	Amb. 1 (SLE) S -X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
9	Amb. 1 (SLU S) S +0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
10	Amb. 1 (SLE) S +0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
11	Amb. 1 (SLU S) S -0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
12	Amb. 1 (SLE) S -0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
13	Amb. 1 (SLU S) S +0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
14	Amb. 1 (SLE) S +0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
15	Amb. 1 (SLU S) S -0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
16	Amb. 1 (SLE) S -0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
17	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.00	0.00	0.00
18	Amb. 2 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
19	Amb. 2 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
20	Amb. 2 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	0.75	1.50	0.00	0.00	0.00	0.00	0.00
22	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
23	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	0.50	1.00	0.00	0.00	0.00	0.00	0.00
24	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
25	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.20	0.00	0.00	0.00	0.00	0.00
26	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
27	Amb. 3 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	1.50	0.00	0.00	0.00	0.00
29	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.90	0.00	0.00	0.00	0.00
30	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	1.00	0.00	0.00	0.00	0.00
31	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.60	0.00	0.00	0.00	0.00
32	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.20	0.00	0.00	0.00	0.00
33	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
34	Amb. 4 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	1.50	0.00	0.00	0.00
36	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.90	0.00	0.00	0.00
37	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00
38	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00
39	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00
40	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
41	Amb. 5 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	0.00	1.50	0.00	0.00
43	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.90	0.00	0.00
44	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00

45	Amb. 6 (SLE R)	SLE R L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00
46	Amb. 6 (SLE F)	SLE F L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.20	0.00	0.00
47	Amb. 6 (SLE F)	SLE F L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
48	Amb. 6 (SLE Q)	SLE Q L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Elenco masse nodi

Simbologia

Mo =Massa orizzontale

Nodo =Numero del nodo

Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo
<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>
-81	84.43	-80	84.43	-79	84.43	-78	84.43	-77	194.07	-76	84.43	-75	84.43	-74	84.43	-73	84.43
-71	56.02	-70	56.02	-69	56.02	-68	56.02	-66	84.43	-65	84.43	-64	84.43	-63	84.43	-62	84.43
-61	84.43	-60	84.43	-59	84.43	-58	56.02	-57	56.02	-56	56.02	-55	56.02	-54	84.43	-53	84.43
-52	84.43	-51	84.43	-50	84.43	-49	84.43	-48	84.43	-47	84.43	-45	184.29	-29	208.89	-26	208.89
-18	144.09	-15	232.96	-14	232.96	-13	232.96	-12	232.96	-11	153.37	-10	153.37	-9	232.96	-8	232.96
-7	232.96	-6	232.96	-3	144.09	201	194.08	202	139.90	203	184.29						

Totali masse nodi

Mo
<kg>
6247.42

Elenco forze sismiche nodali allo SLD

Simbologia

Fx =Forza in dir. X

Fy =Forza in dir. Y

Nodo =Numero del nodo

cx =Coeff. c in dir. X

cy =Coeff. c in dir. Y

Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy
<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>
-81	0.01	0.01	7.64	7.64	-80	0.01	0.01	7.64	7.64	-79	0.01	0.01	7.64	7.64	-78	0.01	0.01	7.64	7.64
-77	0.03	0.03	17.56	17.56	-76	0.01	0.01	7.64	7.64	-75	0.01	0.01	7.64	7.64	-74	0.01	0.01	7.64	7.64
-73	0.01	0.01	7.64	7.64	-71	0.01	0.01	5.07	5.07	-70	0.01	0.01	5.07	5.07	-69	0.01	0.01	5.07	5.07
-68	0.01	0.01	5.07	5.07	-66	0.01	0.01	7.64	7.64	-65	0.01	0.01	7.64	7.64	-64	0.01	0.01	7.64	7.64
-63	0.01	0.01	7.64	7.64	-62	0.01	0.01	7.64	7.64	-61	0.01	0.01	7.64	7.64	-60	0.01	0.01	7.64	7.64
-59	0.01	0.01	7.64	7.64	-58	0.01	0.01	5.07	5.07	-57	0.01	0.01	5.07	5.07	-56	0.01	0.01	5.07	5.07
-55	0.01	0.01	5.07	5.07	-54	0.01	0.01	7.64	7.64	-53	0.01	0.01	7.64	7.64	-52	0.01	0.01	7.64	7.64
-51	0.01	0.01	7.64	7.64	-50	0.01	0.01	7.64	7.64	-49	0.01	0.01	7.64	7.64	-48	0.01	0.01	7.64	7.64
-47	0.01	0.01	7.64	7.64	-45	0.03	0.03	16.67	16.67	-29	0.03	0.03	18.90	18.90	-26	0.03	0.03	18.90	18.90
-18	0.02	0.02	13.04	13.04	-15	0.04	0.04	21.08	21.08	-14	0.04	0.04	21.08	21.08	-13	0.04	0.04	21.08	21.08
-12	0.04	0.04	21.08	21.08	-11	0.02	0.02	13.88	13.88	-10	0.02	0.02	13.88	13.88	-9	0.04	0.04	21.08	21.08
-8	0.04	0.04	21.08	21.08	-7	0.04	0.04	21.08	21.08	-6	0.04	0.04	21.08	21.08	-3	0.02	0.02	13.04	13.04
201	0.03	0.03	17.56	17.56	202	0.02	0.02	12.66	12.66	203	0.03	0.03	16.67	16.67					

Totali forze sismiche

Fx	Fy
<daN>	<daN>
565.20	565.20

Elenco forze sismiche nodali allo SND

Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy
<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>
-81	0.01	0.01	14.04	14.04	-80	0.01	0.01	14.04	14.04	-79	0.01	0.01	14.04	14.04	-78	0.01	0.01	14.04	14.04
-77	0.03	0.03	32.27	32.27	-76	0.01	0.01	14.04	14.04	-75	0.01	0.01	14.04	14.04	-74	0.01	0.01	14.04	14.04
-73	0.01	0.01	14.04	14.04	-71	0.01	0.01	9.32	9.32	-70	0.01	0.01	9.32	9.32	-69	0.01	0.01	9.32	9.32
-68	0.01	0.01	9.32	9.32	-66	0.01	0.01	14.04	14.04	-65	0.01	0.01	14.04	14.04	-64	0.01	0.01	14.04	14.04
-63	0.01	0.01	14.04	14.04	-62	0.01	0.01	14.04	14.04	-61	0.01	0.01	14.04	14.04	-60	0.01	0.01	14.04	14.04
-59	0.01	0.01	14.04	14.04	-58	0.01	0.01	9.32	9.32	-57	0.01	0.01	9.32	9.32	-56	0.01	0.01	9.32	9.32
-55	0.01	0.01	9.32	9.32	-54	0.01	0.01	14.04	14.04	-53	0.01	0.01	14.04	14.04	-52	0.01	0.01	14.04	14.04
-51	0.01	0.01	14.04	14.04	-50	0.01	0.01	14.04	14.04	-49	0.01	0.01	14.04	14.04	-48	0.01	0.01	14.04	14.04
-47	0.01	0.01	14.04	14.04	-45	0.03	0.03	30.65	30.65	-29	0.03	0.03	34.74	34.74	-26	0.03	0.03	34.74	34.74
-18	0.02	0.02	23.96	23.96	-15	0.04	0.04	38.74	38.74	-14	0.04	0.04	38.74	38.74	-13	0.04	0.04	38.74	38.74
-12	0.04	0.04	38.74	38.74	-11	0.02	0.02	25.50	25.50	-10	0.02	0.02	25.50	25.50	-9	0.04	0.04	38.74	38.74
-8	0.04	0.04	38.74	38.74	-7	0.04	0.04	38.74	38.74	-6	0.04	0.04	38.74	38.74	-3	0.02	0.02	23.96	23.96
201	0.03	0.03	32.27	32.27	202	0.02	0.02	23.27	23.27	203	0.03	0.03	30.65	30.65					

Totali forze sismiche

Fx	Fy
<daN>	<daN>
1038.93	1038.93

Domanda in duttilità di curvatura

Direzione X $\mu_{Edx}=9.35$
Direzione Y $\mu_{Edy}=9.35$

Spostamenti relativi massimi allo stato limite di danno

Simbologia

δ = Spostamento relativo
 δ/h = Rapporto (*1000) tra lo spostamento relativo e l'altezza
CC = Numero della combinazione delle condizioni di carico elementari
N1 = Nod1
N2 = Nod2
h = Altezza teorica

I valori degli spostamenti relativi per CC di tipo sismico sono amplificati come da normativa

N1	N2	h	δ	δ/h	CC
		<cm>	<cm>		
315	-45	3.29	0.15	0.45	14
2	202	3.29	0.18	0.54	16
3	203	3.29	0.15	0.45	16

Min = 0.45
Max = 0.54

Reazioni vincolari

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Fx = Reazione vincolare (forza) in dir. X
Fy = Reazione vincolare (forza) in dir. Y
Fz = Reazione vincolare (forza) in dir. Z
Mx = Reazione vincolare (momento) intorno all'asse X
My = Reazione vincolare (momento) intorno all'asse Y
Mz = Reazione vincolare (momento) intorno all'asse Z
Nodo = Numero del nodo
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SND = Stato limite di salvaguardia della vita (non dissipativo)

Nodo	CC	TCC	Fx	CC	TCC	Fy	CC	TCC	Fz	CC	TCC	Mx	CC	TCC	My	CC	TCC	Mz
			<daN>			<daN>			<daN>			<daNm>			<daNm>			<daNm>
2	Max	5	SND 401.25	13	SND	414.28	29	SLU	8791.91	9	SND	1308.25	5	SND	679.97	13	SND	0.00
2	Min	1	SND -401.25	9	SND	-414.28	25	SLE F	2223.66	13	SND	-1308.25	11	SND	-679.96	1	SND	0.00
3	Max	5	SND 225.69	13	SND	312.32	29	SLU	6620.24	9	SND	1052.31	5	SND	490.11	11	SND	0.14
3	Min	1	SND -411.99	9	SND	-312.32	25	SLE F	1700.15	13	SND	-1052.31	13	SND	-691.10	1	SND	-0.14
315	Max	5	SND 411.99	13	SND	312.32	29	SLU	6620.23	9	SND	1052.31	5	SND	691.10	15	SND	0.14
315	Min	1	SND -225.69	9	SND	-312.32	25	SLE F	1700.15	13	SND	-1052.31	9	SND	-490.11	1	SND	-0.14

Sollecitazioni aste

Simbologia

Asta = Numero dell'asta
CC = Numero della combinazione delle condizioni di carico elementari
Mx = Momento torcente intorno all'asse X
My = Momento flettente intorno all'asse Y
Mz = Momento flettente intorno all'asse Z
N = Sforzo normale
N1 = Nod1
N2 = Nod2
Ty = Taglio in dir. Y
Tz = Taglio in dir. Z
X = Coordinata progressiva rispetto al nodo iniziale

Tipo di combinazione di carico: SND

Asta	N1	N2	X	N	CC	Ty	CC	Tz	CC	My	CC	Mx	CC
			<cm>	<daN>		<daN>		<daN>		<daNm>		<daNm>	
1	315	-45	Max	0.00	-1854.89	1	225.69	1	691.10	5	312.32	9	1052.31
1	315	-45	Max	328.50	-1616.82	1	225.69	1	251.28	1	312.32	9	26.33
1	315	-45	Min.	0.00	-2061.78	5	-411.99	5	-490.11	1	-312.32	13	-1052.31
1	315	-45	Min.	328.50	-1823.72	5	-411.99	5	-662.29	5	-312.32	13	-26.33

2	2	202	Max	0.00	-2569.15	1	401.25	1	679.97	5	414.28	9	1308.25	13	0.00	11
2	2	202	Max	328.50	-2331.08	1	401.25	1	638.14	1	414.28	9	52.66	11	0.00	11
2	2	202	Min.	0.00	-2569.15	1	-401.25	5	-679.96	1	-414.28	13	-1308.25	9	0.00	13
2	2	202	Min.	328.50	-2331.08	1	-401.25	5	-638.14	5	-414.28	13	-52.66	13	0.00	13
3	3	203	Max	0.00	-1854.89	5	411.99	1	490.11	5	312.32	9	1052.31	13	0.14	13
3	3	203	Max	328.50	-1616.82	5	411.99	1	662.30	1	312.32	9	26.33	15	0.14	13
3	3	203	Min.	0.00	-2061.78	1	-225.69	5	-691.10	1	-312.32	13	-1052.31	9	-0.14	11
3	3	203	Min.	328.50	-1823.72	1	-225.69	5	-251.28	5	-312.32	13	-26.33	9	-0.14	11
201	-3	-29	Max	0.00	42.59	5	42.59	9	0.00	5	-189.50	1	0.00	13	0.00	1
201	-3	-29	Max	135.63	42.59	5	42.59	9	57.77	11	-313.01	1	-340.77	1	0.00	1
201	-3	-29	Min.	0.00	-42.59	1	-42.59	13	0.00	3	-189.50	1	0.00	9	0.00	1
201	-3	-29	Min.	135.63	-42.59	1	-42.59	13	-57.77	13	-313.01	1	-340.77	1	0.00	1
201	-29	-45	Max	0.00	105.41	5	105.41	9	57.77	11	-583.68	1	-340.77	1	0.00	1
201	-29	-45	Max	83.77	105.41	5	105.41	9	146.07	9	-659.97	1	-861.68	1	0.00	1
201	-29	-45	Min.	0.00	-105.41	1	-105.41	13	-57.77	13	-583.68	1	-340.77	1	0.00	1
201	-29	-45	Min.	83.77	-105.41	1	-105.41	13	-146.07	13	-659.97	1	-861.68	1	0.00	1
201	-45	201	Max	0.00	89.63	1	176.27	13	146.21	9	1163.75	5	-610.41	1	26.33	15
201	-45	201	Max	51.86	89.63	1	176.27	13	54.81	11	1116.53	5	-126.45	1	26.33	15
201	-45	201	Min.	0.00	-275.94	5	-176.27	9	-146.21	13	956.86	1	-1523.98	5	-26.33	9
201	-45	201	Min.	51.86	-275.94	5	-176.27	9	-54.81	13	909.63	1	-932.73	5	-26.33	9
201	201	-6	Max	0.00	29.27	1	115.91	13	54.81	11	845.85	5	-126.44	1	26.33	15
201	201	-6	Max	135.63	29.27	1	115.91	13	102.40	15	722.35	5	656.41	1	26.33	15
201	201	-6	Min.	0.00	-215.58	5	-115.91	11	-54.81	13	638.96	1	-932.72	5	-26.33	9
201	201	-6	Min.	135.63	-215.58	5	-115.91	11	-102.40	9	515.45	1	130.74	5	-26.33	9
201	-6	-7	Max	0.00	-37.55	1	49.09	13	102.41	15	451.67	5	656.43	1	26.33	15
201	-6	-7	Max	135.63	-37.55	1	49.09	13	168.99	15	328.16	5	904.65	1	26.33	15
201	-6	-7	Min.	0.00	-148.76	5	-49.09	11	-102.41	9	244.77	1	130.76	5	-26.33	9
201	-6	-7	Min.	135.63	-148.76	5	-49.09	11	-168.99	9	121.27	1	659.60	5	-26.33	9
201	-7	-8	Max	0.00	-81.94	5	17.73	9	168.98	15	57.49	5	904.64	1	26.33	15
201	-7	-8	Max	63.14					-47.34	5			677.72	5		
201	-7	-8	Max	135.63	-81.94	5	17.73	9	144.93	13	-66.01	5	653.79	5	26.33	15
201	-7	-8	Min.	0.00	-104.37	1	-17.73	15	-168.98	9	-149.40	1	659.57	5	-26.33	9
201	-7	-8	Min.	63.14					-47.34	5			677.72	5		
201	-7	-8	Min.	135.63	-104.37	1	-17.73	15	-144.93	9	-272.91	1	618.26	1	-26.33	9
201	-8	-9	Max	0.00	-15.12	5	84.55	9	144.93	15	-336.69	5	653.79	5	26.33	15
201	-8	-9	Max	135.63	-15.12	5	84.55	9	30.26	15	-460.19	5	113.39	5	26.33	15
201	-8	-9	Min.	0.00	-171.19	1	-84.55	15	-144.93	9	-543.59	1	618.25	1	-26.33	9
201	-8	-9	Min.	135.63	-171.19	1	-84.55	15	-30.26	9	-667.09	1	-202.75	1	-26.33	9
201	-9	-10	Max	0.00	51.70	5	151.37	9	30.26	15	-730.87	5	113.38	5	26.33	15
201	-9	-10	Max	135.63	51.70	5	151.37	9	175.05	9	-854.38	5	-961.64	5	26.33	15
201	-9	-10	Min.	0.00	-238.01	1	-151.37	13	-30.26	9	-937.77	1	-202.77	1	-26.33	9
201	-9	-10	Min.	135.63	-238.01	1	-151.37	13	-175.05	13	-1061.27	1	-1558.40	1	-26.33	9
201	-10	202	Max	0.00	95.84	5	195.51	9	175.05	11	-1043.88	5	-961.65	5	26.33	15
201	-10	202	Max	20.00	95.84	5	195.51	9	214.15	11	-1062.09	5	-1172.26	5	26.33	15
201	-10	202	Min.	0.00	-282.14	1	-195.51	13	-175.05	13	-1250.78	1	-1558.41	1	-26.33	9
201	-10	202	Min.	20.00	-282.14	1	-195.51	13	-214.15	13	-1268.99	1	-1810.39	1	-26.33	9
202	202	-11	Max	0.00	95.84	1	195.51	13	214.15	11	1268.99	5	-1172.25	1	26.33	9
202	202	-11	Max	20.00	95.84	1	195.51	13	175.05	11	1250.78	5	-961.65	1	26.33	9
202	202	-11	Min.	0.00	-282.14	5	-195.51	9	-214.15	13	1062.09	1	-1810.39	5	-26.33	13
202	202	-11	Min.	20.00	-282.14	5	-195.51	9	-175.05	13	1043.88	1	-1558.41	5	-26.33	13
202	-11	-12	Max	0.00	51.70	1	151.37	13	175.05	11	1061.27	5	-961.66	1	26.33	9
202	-11	-12	Max	135.63	51.70	1	151.37	13	30.25	15	937.77	5	113.37	1	26.33	9
202	-11	-12	Min.	0.00	-238.01	5	-151.37	9	-175.05	13	854.38	1	-1558.41	5	-26.33	13
202	-11	-12	Min.	135.63	-238.01	5	-151.37	9	-30.25	9	730.88	1	-202.78	5	-26.33	13
202	-12	-13	Max	0.00	-15.12	1	84.55	13	30.26	15	667.09	5	113.38	1	26.33	9
202	-12	-13	Max	135.63	-15.12	1	84.55	13	144.93	13	543.59	5	653.79	1	26.33	9
202	-12	-13	Min.	0.00	-171.19	5	-84.55	9	-30.26	9	460.20	1	-202.76	5	-26.33	13
202	-12	-13	Min.	135.63	-171.19	5	-84.55	9	-144.93	9	336.69	1	618.25	5	-26.33	13
202	-13	-14	Max	0.00	-81.94	1	17.73	13	144.93	13	272.91	5	653.79	1	26.33	9
202	-13	-14	Max	72.49					-47.34	1			677.72	1		
202	-13	-14	Max	135.63	-81.94	1	17.73	13	168.98	13	149.40	5	904.64	5	26.33	9
202	-13	-14	Min.	0.00	-104.37	5	-17.73	11	-144.93	9	66.01	1	618.25	5	-26.33	13
202	-13	-14	Min.	72.49					-47.34	1			677.72	1		
202	-13	-14	Min.	135.63	-104.37	5	-17.73	11	-168.98	11	-57.49	1	659.57	1	-26.33	13
202	-14	-15	Max	0.00	-37.55	5	49.09	9	168.98	13	-121.28	5	904.64	5	26.33	9
202	-14	-15	Max	135.63	-37.55	5	49.09	9	102.40	13	-244.78	5	656.41	5	26.33	9
202	-14	-15	Min.	0.00	-148.76	1	-49.09	13	-168.98	11	-328.17	1	659.57	1	-26.33	13
202	-14	-15	Min.	135.63	-148.76	1	-49.09	13	-102.40	11	-451.67	1	130.73	1	-26.33	13
202	-15	-77	Max	0.00	29.27	5	115.91	9	102.41	13	-515.45	5	656.43	5	26.33	9
202	-15	-77	Max	135.63	29.27	5	115.91	9	54.80	9	-638.95	5	-126.42	7	26.33	9
202	-15	-77	Min.	0.00	-215.58	1	-115.91	13	-102.41	11	-722.34	1	130.76	1	-26.33	13
202	-15	-77	Min.	135.63	-215.58	1	-115.91	13	-54.80	15	-845.85	1	-932.69	1	-26.33	13
202	-77	203	Max	0.00	89.63	5	176.27	9	54.80	9	-909.63	5	-126.43	7	26.33	9
202	-77	203	Max	51.86	89.63	5	176.27	9	146.21	9	-956.85	5	-610.38	5	26.33	9
202	-77	203	Min.	0.00	-275.94	1	-176.27	13	-54.80	15	-1116.53	1	-932.70	1	-26.33	13
202	-77	203	Min.	51.86	-275.94	1	-176.27	13	-146.21	13	-1163.75	1	-1523.95	1	-26.33	13



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202	203	-26	Max	0.00	105.41	1	105.41	13	146.07	9	659.97	1	-861.68	1	0.00	1
202	203	-26	Max	83.77	105.41	1	105.41	13	57.77	9	583.68	1	-340.77	1	0.00	1
202	203	-26	Min.	0.00	-105.41	5	-105.41	9	-146.07	13	659.97	1	-861.68	1	0.00	1
202	203	-26	Min.	83.77	-105.41	5	-105.41	9	-57.77	15	583.68	1	-340.77	1	0.00	1
202	-26	-18	Max	0.00	42.59	1	42.59	13	57.77	9	313.01	1	-340.78	1	0.00	1
202	-26	-18	Max	135.63	42.59	1	42.59	13	0.00	9	189.50	1	-0.00	1	0.00	1
202	-26	-18	Min.	0.00	-42.59	5	-42.59	9	-57.77	15	313.01	1	-340.78	1	0.00	1
202	-26	-18	Min.	135.63	-42.59	5	-42.59	9	0.00	15	189.50	1	-0.00	1	0.00	1
302	-3	-69	Max	0.00	9.32	13	9.32	5	13.97	1	94.75	1	-82.43	1	0.00	1
302	-3	-69	Max	150.00	9.32	13	9.32	5	0.00	5	15.16	1	0.00	1	0.00	1
302	-3	-69	Min.	0.00	-9.32	9	-9.32	1	-13.97	5	94.75	1	-82.43	1	0.00	1
302	-3	-69	Min.	150.00	-9.32	9	-9.32	1	0.00	1	15.16	1	0.00	1	0.00	1
302	-68	-3	Max	0.00	9.32	9	9.32	1	0.00	3	-15.16	1	0.00	9	0.00	1
302	-68	-3	Max	150.00	9.32	9	9.32	1	13.97	1	-94.75	1	-82.43	1	0.00	1
302	-68	-3	Min.	0.00	-9.32	13	-9.32	5	0.00	5	-15.16	1	0.00	13	0.00	1
302	-68	-3	Min.	150.00	-9.32	13	-9.32	5	-13.97	5	-94.75	1	-82.43	1	0.00	1
303	-29	-76	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
303	-29	-76	Max	150.00	14.04	13	14.04	5	0.00	1	30.31	1	0.00	1	0.00	1
303	-29	-76	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
303	-29	-76	Min.	150.00	-14.04	9	-14.04	1	0.00	1	30.31	1	0.00	1	0.00	1
303	-75	-29	Max	0.00	14.04	9	14.04	1	0.00	3	-30.31	1	0.00	9	0.00	1
303	-75	-29	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
303	-75	-29	Min.	0.00	-14.04	13	-14.04	5	0.00	5	-30.31	1	0.00	15	0.00	1
303	-75	-29	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
305	-6	-48	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
305	-6	-48	Max	150.00	14.04	13	14.04	5	0.00	9	30.31	1	0.00	1	0.00	1
305	-6	-48	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
305	-6	-48	Min.	150.00	-14.04	9	-14.04	1	0.00	13	30.31	1	0.00	1	0.00	1
305	-47	-6	Max	0.00	14.04	9	14.04	1	0.00	5	-30.31	1	0.00	1	0.00	1
305	-47	-6	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
305	-47	-6	Min.	0.00	-14.04	13	-14.04	5	0.00	1	-30.31	1	0.00	5	0.00	1
305	-47	-6	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
306	-7	-50	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
306	-7	-50	Max	150.00	14.04	13	14.04	5	0.00	13	30.31	1	0.00	1	0.00	1
306	-7	-50	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
306	-7	-50	Min.	150.00	-14.04	9	-14.04	1	0.00	9	30.31	1	0.00	1	0.00	1
306	-49	-7	Max	0.00	14.04	9	14.04	1	0.00	7	-30.31	1	0.00	9	0.00	1
306	-49	-7	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
306	-49	-7	Min.	0.00	-14.04	13	-14.04	5	0.00	1	-30.31	1	0.00	15	0.00	1
306	-49	-7	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
307	-8	-52	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
307	-8	-52	Max	150.00	14.04	13	14.04	5	0.00	1	30.31	1	0.00	1	0.00	1
307	-8	-52	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
307	-8	-52	Min.	150.00	-14.04	9	-14.04	1	0.00	1	30.31	1	0.00	1	0.00	1
307	-51	-8	Max	0.00	14.04	9	14.04	1	0.00	7	-30.31	1	0.00	15	0.00	1
307	-51	-8	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
307	-51	-8	Min.	0.00	-14.04	13	-14.04	5	0.00	1	-30.31	1	0.00	9	0.00	1
307	-51	-8	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
308	-9	-54	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
308	-9	-54	Max	150.00	14.04	13	14.04	5	0.00	13	30.31	1	0.00	1	0.00	1
308	-9	-54	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
308	-9	-54	Min.	150.00	-14.04	9	-14.04	1	0.00	9	30.31	1	0.00	1	0.00	1
308	-53	-9	Max	0.00	14.04	9	14.04	1	0.00	5	-30.31	1	0.00	13	0.00	1
308	-53	-9	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
308	-53	-9	Min.	0.00	-14.04	13	-14.04	5	0.00	3	-30.31	1	0.00	11	0.00	1
308	-53	-9	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
309	-10	-56	Max	0.00	9.32	13	9.32	5	13.97	1	94.75	1	-82.43	1	0.00	1
309	-10	-56	Max	150.00	9.32	13	9.32	5	0.00	5	15.16	1	0.00	1	0.00	1
309	-10	-56	Min.	0.00	-9.32	9	-9.32	1	-13.97	5	94.75	1	-82.43	1	0.00	1
309	-10	-56	Min.	150.00	-9.32	9	-9.32	1	0.00	1	15.16	1	0.00	1	0.00	1
309	-55	-10	Max	0.00	9.32	9	9.32	1	0.00	1	-15.16	1	0.00	15	0.00	9
309	-55	-10	Max	150.00	9.32	9	9.32	1	13.97	1	-94.75	1	-82.43	1	0.00	9
309	-55	-10	Min.	0.00	-9.32	13	-9.32	5	0.00	5	-15.16	1	0.00	9	0.00	13
309	-55	-10	Min.	150.00	-9.32	13	-9.32	5	-13.97	5	-94.75	1	-82.43	1	0.00	13
310	-11	-58	Max	0.00	9.32	13	9.32	5	13.97	1	94.75	1	-82.43	1	0.00	1
310	-11	-58	Max	150.00	9.32	13	9.32	5	0.00	5	15.16	1	0.00	1	0.00	1
310	-11	-58	Min.	0.00	-9.32	9	-9.32	1	-13.97	5	94.75	1	-82.43	1	0.00	1
310	-11	-58	Min.	150.00	-9.32	9	-9.32	1	0.00	1	15.16	1	0.00	1	0.00	1
310	-57	-11	Max	0.00	9.32	9	9.32	1	0.00	9	-15.16	1	0.00	13	0.00	1
310	-57	-11	Max	150.00	9.32	9	9.32	1	13.97	1	-94.75	1	-82.43	1	0.00	1
310	-57	-11	Min.	0.00	-9.32	13	-9.32	5	0.00	13	-15.16	1	0.00	9	0.00	1
310	-57	-11	Min.	150.00	-9.32	13	-9.32	5	-13.97	5	-94.75	1	-82.43	1	0.00	1
311	-12	-60	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
311	-12	-60	Max	150.00	14.04	13	14.04	5	0.00	1	30.31	1	0.00	1	0.00	1
311	-12	-60	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
311	-12	-60	Min.	150.00	-14.04	9	-14.04	1	0.00	1	30.31	1	0.00	1	0.00	1

311	-59	-12	Max	0.00	14.04	9	14.04	1	0.00	1	-30.31	1	0.00	15	0.00	1
311	-59	-12	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
311	-59	-12	Min.	0.00	-14.04	13	-14.04	5	0.00	5	-30.31	1	0.00	9	0.00	1
311	-59	-12	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
312	-13	-62	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
312	-13	-62	Max	150.00	14.04	13	14.04	5	0.00	1	30.31	1	0.00	1	0.00	1
312	-13	-62	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
312	-13	-62	Min.	150.00	-14.04	9	-14.04	1	0.00	1	30.31	1	0.00	1	0.00	1
312	-61	-13	Max	0.00	14.04	9	14.04	1	0.00	1	-30.31	1	0.00	1	0.00	1
312	-61	-13	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
312	-61	-13	Min.	0.00	-14.04	13	-14.04	5	0.00	5	-30.31	1	0.00	1	0.00	1
312	-61	-13	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
313	-14	-64	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
313	-14	-64	Max	150.00	14.04	13	14.04	5	0.00	13	30.31	1	0.00	1	0.00	1
313	-14	-64	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
313	-14	-64	Min.	150.00	-14.04	9	-14.04	1	0.00	9	30.31	1	0.00	1	0.00	1
313	-63	-14	Max	0.00	14.04	9	14.04	1	0.00	7	-30.31	1	0.00	9	0.00	1
313	-63	-14	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
313	-63	-14	Min.	0.00	-14.04	13	-14.04	5	0.00	1	-30.31	1	0.00	13	0.00	1
313	-63	-14	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
314	-15	-66	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
314	-15	-66	Max	150.00	14.04	13	14.04	5	0.00	13	30.31	1	0.00	1	0.00	1
314	-15	-66	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
314	-15	-66	Min.	150.00	-14.04	9	-14.04	1	0.00	9	30.31	1	0.00	1	0.00	1
314	-65	-15	Max	0.00	14.04	9	14.04	1	0.00	3	-30.31	1	0.00	13	0.00	1
314	-65	-15	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
314	-65	-15	Min.	0.00	-14.04	13	-14.04	5	0.00	5	-30.31	1	0.00	9	0.00	1
314	-65	-15	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
316	-26	-74	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
316	-26	-74	Max	150.00	14.04	13	14.04	5	0.00	5	30.31	1	0.00	1	0.00	1
316	-26	-74	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
316	-26	-74	Min.	150.00	-14.04	9	-14.04	1	0.00	1	30.31	1	0.00	1	0.00	1
316	-73	-26	Max	0.00	14.04	9	14.04	1	0.00	7	-30.31	1	0.00	13	0.00	1
316	-73	-26	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
316	-73	-26	Min.	0.00	-14.04	13	-14.04	5	0.00	1	-30.31	1	0.00	9	0.00	1
316	-73	-26	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
317	-18	-71	Max	0.00	9.32	13	9.32	5	13.97	1	94.75	1	-82.43	1	0.00	1
317	-18	-71	Max	150.00	9.32	13	9.32	5	0.00	5	15.16	1	0.00	1	0.00	1
317	-18	-71	Min.	0.00	-9.32	9	-9.32	1	-13.97	5	94.75	1	-82.43	1	0.00	1
317	-18	-71	Min.	150.00	-9.32	9	-9.32	1	0.00	1	15.16	1	0.00	1	0.00	1
317	-70	-18	Max	0.00	9.32	9	9.32	1	0.00	9	-15.16	1	0.00	9	0.00	1
317	-70	-18	Max	150.00	9.32	9	9.32	1	13.97	1	-94.75	1	-82.43	1	0.00	1
317	-70	-18	Min.	0.00	-9.32	13	-9.32	5	0.00	13	-15.16	1	0.00	13	0.00	1
317	-70	-18	Min.	150.00	-9.32	13	-9.32	5	-13.97	5	-94.75	1	-82.43	1	0.00	1
318	201	-81	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
318	201	-81	Max	150.00	14.04	13	14.04	5	0.00	9	30.31	1	0.00	1	0.00	1
318	201	-81	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
318	201	-81	Min.	150.00	-14.04	9	-14.04	1	0.00	13	30.31	1	0.00	1	0.00	1
318	-80	201	Max	0.00	14.04	9	14.04	1	0.00	5	-30.31	1	0.00	5	0.00	1
318	-80	201	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	1
318	-80	201	Min.	0.00	-14.04	13	-14.04	5	0.00	1	-30.31	1	0.00	1	0.00	1
318	-80	201	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1
319	-77	-79	Max	0.00	14.04	13	14.04	5	21.06	1	135.34	1	-124.24	1	0.00	1
319	-77	-79	Max	150.00	14.04	13	14.04	5	0.00	5	30.31	1	0.00	1	0.00	1
319	-77	-79	Min.	0.00	-14.04	9	-14.04	1	-21.06	5	135.34	1	-124.24	1	0.00	1
319	-77	-79	Min.	150.00	-14.04	9	-14.04	1	0.00	1	30.31	1	0.00	1	0.00	1
319	-78	-77	Max	0.00	14.04	9	14.04	1	0.00	7	-30.31	1	0.00	13	0.00	5
319	-78	-77	Max	150.00	14.04	9	14.04	1	21.06	1	-135.34	1	-124.24	1	0.00	5
319	-78	-77	Min.	0.00	-14.04	13	-14.04	5	0.00	1	-30.31	1	0.00	9	0.00	1
319	-78	-77	Min.	150.00	-14.04	13	-14.04	5	-21.06	5	-135.34	1	-124.24	1	0.00	1

Tipologia di combinazione di carico: SLD

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	315	-45	Max	0.00	-1902.06	2	80.30	2	421.80	6	169.91	12	572.48	14	0.08	10
1	315	-45	Max	328.50	-1663.99	2	80.30	2	42.99	2	169.91	12	14.33	16	0.08	10
1	315	-45	Min.	0.00	-2014.61	6	-266.61	6	-220.80	2	-169.91	14	-572.48	12	-0.08	16
1	315	-45	Min.	328.50	-1776.55	6	-266.61	6	-454.01	6	-169.91	14	-14.32	10	-0.08	16
2	2	202	Max	0.00	-2569.15	2	218.29	2	369.92	6	225.38	12	711.72	14	0.00	12
2	2	202	Max	328.50	-2331.08	2	218.29	2	347.16	2	225.38	12	28.65	12	0.00	12
2	2	202	Min.	0.00	-2569.15	2	-218.29	6	-369.91	2	-225.38	14	-711.72	10	0.00	14
2	2	202	Min.	328.50	-2331.08	2	-218.29	6	-347.16	6	-225.38	14	-28.65	14	0.00	14
3	3	203	Max	0.00	-1902.06	6	266.61	2	220.80	6	169.91	12	572.48	14	0.08	14
3	3	203	Max	328.50	-1663.99	6	266.61	2	454.01	2	169.91	12	14.33	16	0.08	14
3	3	203	Min.	0.00	-2014.61	2	-80.30	6	-421.80	2	-169.91	14	-572.48	10	-0.08	12

3	3	203	Min.	328.50	-1776.55	2	-80.30	6	-42.99	8	-169.91	14	-14.32	10	-0.08	12
201	-3	-29	Max	0.00	23.17	6	23.17	10	0.00	6	-189.50	2	0.00	2	0.00	2
201	-3	-29	Max	135.63	23.17	6	23.17	10	31.43	12	-313.01	2	-340.77	2	0.00	2
201	-3	-29	Min.	0.00	-23.17	2	-23.17	14	0.00	4	-189.50	2	0.00	2	0.00	2
201	-3	-29	Min.	135.63	-23.17	2	-23.17	14	-31.43	14	-313.01	2	-340.77	2	0.00	2
201	-29	-45	Max	0.00	57.35	6	57.35	10	31.43	12	-583.68	2	-340.77	2	0.00	2
201	-29	-45	Max	83.77	57.35	6	57.35	10	79.47	10	-659.97	2	-861.68	2	0.00	2
201	-29	-45	Min.	0.00	-57.35	2	-57.35	14	-31.43	14	-583.68	2	-340.77	2	0.00	2
201	-29	-45	Min.	83.77	-57.35	2	-57.35	14	-79.47	14	-659.97	2	-861.68	2	0.00	2
201	-45	201	Max	0.00	6.28	2	95.89	14	79.54	12	1116.58	6	-818.69	2	14.33	16
201	-45	201	Max	51.86	6.28	2	95.89	14	29.82	12	1069.36	6	-310.27	2	14.33	16
201	-45	201	Min.	0.00	-192.59	6	-95.89	12	-79.54	14	1004.02	2	-1315.69	6	-14.32	10
201	-45	201	Min.	51.86	-192.59	6	-95.89	12	-29.82	14	956.80	2	-748.91	6	-14.32	10
201	201	-6	Max	0.00	-26.55	2	63.06	14	29.82	12	798.68	6	-310.27	2	14.32	16
201	201	-6	Max	135.63	-26.55	2	63.06	14	55.71	16	675.18	6	536.56	2	14.32	16
201	201	-6	Min.	0.00	-159.76	6	-63.06	12	-29.82	14	686.12	2	-748.90	6	-14.32	10
201	201	-6	Min.	135.63	-159.76	6	-63.06	12	-55.71	10	562.62	2	250.58	6	-14.32	10
201	-6	-7	Max	0.00	-62.90	2	26.71	14	55.71	16	404.50	6	536.58	2	14.32	16
201	-6	-7	Max	135.63	-62.90	2	26.71	14	91.93	14	280.99	6	848.78	2	14.32	16
201	-6	-7	Min.	0.00	-123.40	6	-26.71	12	-55.71	10	291.94	2	250.61	6	-14.32	10
201	-6	-7	Min.	135.63	-123.40	6	-26.71	12	-91.93	10	168.44	2	715.47	6	-14.32	10
201	-7	-8	Max	0.00	-87.05	6	9.65	10	91.93	16	10.32	8	848.77	2	14.32	16
201	-7	-8	Max	11.34					-27.25	6			716.03	6		
201	-7	-8	Max	135.63	-87.05	6	9.65	10	78.85	14	-113.18	6	645.69	6	14.32	16
201	-7	-8	Min.	0.00	-99.25	2	-9.65	16	-91.93	10	-102.23	2	715.44	6	-14.32	10
201	-7	-8	Min.	11.34					-27.25	6			716.03	6		
201	-7	-8	Min.	135.63	-99.25	2	-9.65	16	-78.85	10	-225.74	2	626.36	2	-14.32	10
201	-8	-9	Max	0.00	-50.70	6	46.00	10	78.85	16	-383.86	6	645.69	6	14.32	16
201	-8	-9	Max	135.63	-50.70	6	46.00	10	16.46	16	-507.36	6	41.31	6	14.32	16
201	-8	-9	Min.	0.00	-135.60	2	-46.00	16	-78.85	10	-496.42	2	626.36	2	-14.32	10
201	-8	-9	Min.	135.63	-135.60	2	-46.00	16	-16.46	10	-619.92	2	-130.68	2	-14.32	10
201	-9	-10	Max	0.00	-14.35	6	82.35	10	16.46	16	-778.04	6	41.30	6	14.32	16
201	-9	-10	Max	135.63	-14.35	6	82.35	10	95.23	10	-901.54	6	-1097.69	6	14.32	16
201	-9	-10	Min.	0.00	-171.96	2	-82.35	16	-16.46	10	-890.60	2	-130.69	2	-14.32	10
201	-9	-10	Min.	135.63	-171.96	2	-82.35	16	-95.23	14	-1014.10	2	-1422.34	2	-14.32	10
201	-10	202	Max	0.00	9.66	6	106.36	10	95.23	10	-1091.05	6	-1097.71	6	14.32	16
201	-10	202	Max	20.00	9.66	6	106.36	10	116.50	10	-1109.26	6	-1317.74	6	14.32	16
201	-10	202	Min.	0.00	-195.97	2	-106.36	16	-95.23	14	-1203.61	2	-1422.36	2	-14.33	10
201	-10	202	Min.	20.00	-195.97	2	-106.36	16	-116.50	14	-1221.82	2	-1664.90	2	-14.33	10
202	202	-11	Max	0.00	9.66	2	106.36	14	116.50	10	1221.82	6	-1317.74	2	14.33	10
202	202	-11	Max	20.00	9.66	2	106.36	14	95.23	10	1203.61	6	-1097.71	2	14.33	10
202	202	-11	Min.	0.00	-195.97	6	-106.36	10	-116.50	14	1109.26	2	-1664.90	6	-14.32	16
202	202	-11	Min.	20.00	-195.97	6	-106.36	10	-95.23	14	1091.05	2	-1422.36	6	-14.32	16
202	-11	-12	Max	0.00	-14.35	2	82.35	14	95.23	12	1014.10	6	-1097.71	2	14.32	10
202	-11	-12	Max	135.63	-14.35	2	82.35	14	16.46	16	890.60	6	41.29	2	14.32	10
202	-11	-12	Min.	0.00	-171.96	6	-82.35	10	-95.23	14	901.55	2	-1422.36	6	-14.32	14
202	-11	-12	Min.	135.63	-171.96	6	-82.35	10	-16.46	10	778.04	2	-130.70	6	-14.32	14
202	-12	-13	Max	0.00	-50.70	2	46.00	14	16.46	16	619.92	6	41.30	2	14.32	10
202	-12	-13	Max	135.63	-50.70	2	46.00	14	78.85	14	496.42	6	645.68	2	14.32	10
202	-12	-13	Min.	0.00	-135.61	6	-46.00	10	-16.46	10	507.37	2	-130.69	6	-14.32	14
202	-12	-13	Min.	135.63	-135.61	6	-46.00	10	-78.85	10	383.86	2	626.35	6	-14.32	14
202	-13	-14	Max	0.00	-87.05	2	9.65	14	78.85	14	225.74	6	645.69	2	14.32	10
202	-13	-14	Max	124.30					-27.25	2			716.03	2		
202	-13	-14	Max	135.63	-87.05	2	9.65	14	91.93	14	102.23	6	848.77	6	14.32	10
202	-13	-14	Min.	0.00	-99.25	6	-9.65	10	-78.85	10	113.18	2	626.36	6	-14.32	16
202	-13	-14	Min.	124.30					-27.25	2			716.03	2		
202	-13	-14	Min.	135.63	-99.25	6	-9.65	10	-91.93	10	-10.32	2	715.44	2	-14.32	16
202	-14	-15	Max	0.00	-62.90	6	26.71	10	91.93	14	-168.44	6	848.77	6	14.32	10
202	-14	-15	Max	135.63	-62.90	6	26.71	10	55.71	14	-291.95	6	536.56	6	14.32	10
202	-14	-15	Min.	0.00	-123.40	2	-26.71	16	-91.93	12	-281.00	2	715.44	2	-14.32	16
202	-14	-15	Min.	135.63	-123.40	2	-26.71	16	-55.71	12	-404.50	2	250.58	2	-14.32	16
202	-15	-77	Max	0.00	-26.55	6	63.06	10	55.71	14	-562.62	6	536.58	6	14.32	10
202	-15	-77	Max	135.63	-26.55	6	63.06	10	29.81	10	-686.12	6	-310.24	6	14.32	10
202	-15	-77	Min.	0.00	-159.76	2	-63.06	14	-55.71	12	-675.17	2	250.61	2	-14.32	16
202	-15	-77	Min.	135.63	-159.76	2	-63.06	14	-29.81	16	-798.68	2	-748.87	2	-14.32	16
202	-77	203	Max	0.00	6.28	6	95.89	10	29.81	10	-956.80	6	-310.25	6	14.32	10
202	-77	203	Max	51.86	6.28	6	95.89	10	79.54	10	-1004.02	6	-818.66	6	14.32	10
202	-77	203	Min.	0.00	-192.59	2	-95.89	14	-29.81	16	-1069.36	2	-748.88	2	-14.33	16
202	-77	203	Min.	51.86	-192.59	2	-95.89	14	-79.54	16	-1116.58	2	-1315.66	2	-14.33	16
202	203	-26	Max	0.00	57.35	2	57.35	14	79.47	10	659.97	2	-861.68	2	0.00	2
202	203	-26	Max	83.77	57.35	2	57.35	14	31.43	10	583.68	2	-340.77	2	0.00	2
202	203	-26	Min.	0.00	-57.35	6	-57.35	10	-79.47	14	659.97	2	-861.68	2	0.00	2
202	203	-26	Min.	83.77	-57.35	6	-57.35	10	-31.43	16	583.68	2	-340.77	2	0.00	2
202	-26	-18	Max	0.00	23.17	2	23.17	14	31.43	10	313.01	2	-340.78	2	0.00	2
202	-26	-18	Max	135.63	23.17	2	23.17	14	0.00	10	189.50	2	-0.00	2	0.00	2
202	-26	-18	Min.	0.00	-23.17	6	-23.17	10	-31.43	16	313.01	2	-340.78	2	0.00	2

202	-26	-18	Min.	135.63	-23.17	6	-23.17	10	0.00	16	189.50	2	-0.00	2	0.00	2
302	-3	-69	Max	0.00	5.07	14	5.07	6	7.60	2	94.75	2	-82.43	2	0.00	2
302	-3	-69	Max	150.00	5.07	14	5.07	6	0.00	6	15.16	2	0.00	2	0.00	2
302	-3	-69	Min.	0.00	-5.07	10	-5.07	2	-7.60	6	94.75	2	-82.43	2	0.00	2
302	-3	-69	Min.	150.00	-5.07	10	-5.07	2	0.00	2	15.16	2	0.00	2	0.00	2
302	-68	-3	Max	0.00	5.07	10	5.07	2	0.00	4	-15.16	2	0.00	10	0.00	2
302	-68	-3	Max	150.00	5.07	10	5.07	2	7.60	2	-94.75	2	-82.43	2	0.00	2
302	-68	-3	Min.	0.00	-5.07	14	-5.07	6	0.00	6	-15.16	2	0.00	14	0.00	2
302	-68	-3	Min.	150.00	-5.07	14	-5.07	6	-7.60	6	-94.75	2	-82.43	2	0.00	2
303	-29	-76	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
303	-29	-76	Max	150.00	7.64	14	7.64	6	0.00	2	30.31	2	0.00	2	0.00	2
303	-29	-76	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
303	-29	-76	Min.	150.00	-7.64	10	-7.64	2	0.00	2	30.31	2	0.00	2	0.00	2
303	-75	-29	Max	0.00	7.64	10	7.64	2	0.00	4	-30.31	2	0.00	10	0.00	2
303	-75	-29	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
303	-75	-29	Min.	0.00	-7.64	14	-7.64	6	0.00	6	-30.31	2	0.00	16	0.00	2
303	-75	-29	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
305	-6	-48	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
305	-6	-48	Max	150.00	7.64	14	7.64	6	0.00	10	30.31	2	0.00	2	0.00	2
305	-6	-48	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
305	-6	-48	Min.	150.00	-7.64	10	-7.64	2	0.00	14	30.31	2	0.00	2	0.00	2
305	-47	-6	Max	0.00	7.64	10	7.64	2	0.00	6	-30.31	2	0.00	2	0.00	2
305	-47	-6	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
305	-47	-6	Min.	0.00	-7.64	14	-7.64	6	0.00	2	-30.31	2	0.00	6	0.00	2
305	-47	-6	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
306	-7	-50	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
306	-7	-50	Max	150.00	7.64	14	7.64	6	0.00	14	30.31	2	0.00	2	0.00	2
306	-7	-50	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
306	-7	-50	Min.	150.00	-7.64	10	-7.64	2	0.00	10	30.31	2	0.00	2	0.00	2
306	-49	-7	Max	0.00	7.64	10	7.64	2	0.00	8	-30.31	2	0.00	10	0.00	2
306	-49	-7	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
306	-49	-7	Min.	0.00	-7.64	14	-7.64	6	0.00	2	-30.31	2	0.00	16	0.00	2
306	-49	-7	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
307	-8	-52	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
307	-8	-52	Max	150.00	7.64	14	7.64	6	0.00	2	30.31	2	0.00	2	0.00	2
307	-8	-52	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
307	-8	-52	Min.	150.00	-7.64	10	-7.64	2	0.00	2	30.31	2	0.00	2	0.00	2
307	-51	-8	Max	0.00	7.64	10	7.64	2	0.00	8	-30.31	2	0.00	16	0.00	2
307	-51	-8	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
307	-51	-8	Min.	0.00	-7.64	14	-7.64	6	0.00	2	-30.31	2	0.00	10	0.00	2
307	-51	-8	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
308	-9	-54	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
308	-9	-54	Max	150.00	7.64	14	7.64	6	0.00	14	30.31	2	0.00	2	0.00	2
308	-9	-54	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
308	-9	-54	Min.	150.00	-7.64	10	-7.64	2	0.00	10	30.31	2	0.00	2	0.00	2
308	-53	-9	Max	0.00	7.64	10	7.64	2	0.00	6	-30.31	2	0.00	14	0.00	2
308	-53	-9	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
308	-53	-9	Min.	0.00	-7.64	14	-7.64	6	0.00	4	-30.31	2	0.00	12	0.00	2
308	-53	-9	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
309	-10	-56	Max	0.00	5.07	14	5.07	6	7.60	2	94.75	2	-82.43	2	0.00	2
309	-10	-56	Max	150.00	5.07	14	5.07	6	0.00	6	15.16	2	0.00	2	0.00	2
309	-10	-56	Min.	0.00	-5.07	10	-5.07	2	-7.60	6	94.75	2	-82.43	2	0.00	2
309	-10	-56	Min.	150.00	-5.07	10	-5.07	2	0.00	2	15.16	2	0.00	2	0.00	2
309	-55	-10	Max	0.00	5.07	10	5.07	2	0.00	2	-15.16	2	0.00	16	0.00	10
309	-55	-10	Max	150.00	5.07	10	5.07	2	7.60	2	-94.75	2	-82.43	2	0.00	10
309	-55	-10	Min.	0.00	-5.07	14	-5.07	6	0.00	6	-15.16	2	0.00	10	0.00	14
309	-55	-10	Min.	150.00	-5.07	14	-5.07	6	-7.60	6	-94.75	2	-82.43	2	0.00	14
310	-11	-58	Max	0.00	5.07	14	5.07	6	7.60	2	94.75	2	-82.43	2	0.00	2
310	-11	-58	Max	150.00	5.07	14	5.07	6	0.00	6	15.16	2	0.00	2	0.00	2
310	-11	-58	Min.	0.00	-5.07	10	-5.07	2	-7.60	6	94.75	2	-82.43	2	0.00	2
310	-11	-58	Min.	150.00	-5.07	10	-5.07	2	0.00	2	15.16	2	0.00	2	0.00	2
310	-57	-11	Max	0.00	5.07	10	5.07	2	0.00	10	-15.16	2	0.00	14	0.00	2
310	-57	-11	Max	150.00	5.07	10	5.07	2	7.60	2	-94.75	2	-82.43	2	0.00	2
310	-57	-11	Min.	0.00	-5.07	14	-5.07	6	0.00	14	-15.16	2	0.00	10	0.00	2
310	-57	-11	Min.	150.00	-5.07	14	-5.07	6	-7.60	6	-94.75	2	-82.43	2	0.00	2
311	-12	-60	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
311	-12	-60	Max	150.00	7.64	14	7.64	6	0.00	2	30.31	2	0.00	2	0.00	2
311	-12	-60	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
311	-12	-60	Min.	150.00	-7.64	10	-7.64	2	0.00	2	30.31	2	0.00	2	0.00	2
311	-59	-12	Max	0.00	7.64	10	7.64	2	0.00	2	-30.31	2	0.00	16	0.00	2
311	-59	-12	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
311	-59	-12	Min.	0.00	-7.64	14	-7.64	6	0.00	6	-30.31	2	0.00	10	0.00	2
311	-59	-12	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
312	-13	-62	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
312	-13	-62	Max	150.00	7.64	14	7.64	6	0.00	2	30.31	2	0.00	2	0.00	2
312	-13	-62	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2

312	-13	-62	Min.	150.00	-7.64	10	-7.64	2	0.00	2	30.31	2	0.00	2	0.00	2
312	-61	-13	Max	0.00	7.64	10	7.64	2	0.00	2	-30.31	2	0.00	2	0.00	2
312	-61	-13	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
312	-61	-13	Min.	0.00	-7.64	14	-7.64	6	0.00	6	-30.31	2	0.00	2	0.00	2
312	-61	-13	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
313	-14	-64	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
313	-14	-64	Max	150.00	7.64	14	7.64	6	0.00	14	30.31	2	0.00	2	0.00	2
313	-14	-64	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
313	-14	-64	Min.	150.00	-7.64	10	-7.64	2	0.00	10	30.31	2	0.00	2	0.00	2
313	-63	-14	Max	0.00	7.64	10	7.64	2	0.00	8	-30.31	2	0.00	10	0.00	2
313	-63	-14	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
313	-63	-14	Min.	0.00	-7.64	14	-7.64	6	0.00	2	-30.31	2	0.00	14	0.00	2
313	-63	-14	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
314	-15	-66	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
314	-15	-66	Max	150.00	7.64	14	7.64	6	0.00	14	30.31	2	0.00	2	0.00	2
314	-15	-66	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
314	-15	-66	Min.	150.00	-7.64	10	-7.64	2	0.00	10	30.31	2	0.00	2	0.00	2
314	-65	-15	Max	0.00	7.64	10	7.64	2	0.00	4	-30.31	2	0.00	14	0.00	2
314	-65	-15	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
314	-65	-15	Min.	0.00	-7.64	14	-7.64	6	0.00	6	-30.31	2	0.00	10	0.00	2
314	-65	-15	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
316	-26	-74	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
316	-26	-74	Max	150.00	7.64	14	7.64	6	0.00	6	30.31	2	0.00	2	0.00	2
316	-26	-74	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
316	-26	-74	Min.	150.00	-7.64	10	-7.64	2	0.00	2	30.31	2	0.00	2	0.00	2
316	-73	-26	Max	0.00	7.64	10	7.64	2	0.00	8	-30.31	2	0.00	14	0.00	2
316	-73	-26	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
316	-73	-26	Min.	0.00	-7.64	14	-7.64	6	0.00	2	-30.31	2	0.00	10	0.00	2
316	-73	-26	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
317	-18	-71	Max	0.00	5.07	14	5.07	6	7.60	2	94.75	2	-82.43	2	0.00	2
317	-18	-71	Max	150.00	5.07	14	5.07	6	0.00	6	15.16	2	0.00	2	0.00	2
317	-18	-71	Min.	0.00	-5.07	10	-5.07	2	-7.60	6	94.75	2	-82.43	2	0.00	2
317	-18	-71	Min.	150.00	-5.07	10	-5.07	2	0.00	2	15.16	2	0.00	2	0.00	2
317	-70	-18	Max	0.00	5.07	10	5.07	2	0.00	10	-15.16	2	0.00	10	0.00	2
317	-70	-18	Max	150.00	5.07	10	5.07	2	7.60	2	-94.75	2	-82.43	2	0.00	2
317	-70	-18	Min.	0.00	-5.07	14	-5.07	6	0.00	14	-15.16	2	0.00	14	0.00	2
317	-70	-18	Min.	150.00	-5.07	14	-5.07	6	-7.60	6	-94.75	2	-82.43	2	0.00	2
318	201	-81	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
318	201	-81	Max	150.00	7.64	14	7.64	6	0.00	10	30.31	2	0.00	2	0.00	2
318	201	-81	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
318	201	-81	Min.	150.00	-7.64	10	-7.64	2	0.00	14	30.31	2	0.00	2	0.00	2
318	-80	201	Max	0.00	7.64	10	7.64	2	0.00	6	-30.31	2	0.00	6	0.00	2
318	-80	201	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	2
318	-80	201	Min.	0.00	-7.64	14	-7.64	6	0.00	2	-30.31	2	0.00	2	0.00	2
318	-80	201	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2
319	-77	-79	Max	0.00	7.64	14	7.64	6	11.46	2	135.34	2	-124.24	2	0.00	2
319	-77	-79	Max	150.00	7.64	14	7.64	6	0.00	6	30.31	2	0.00	2	0.00	2
319	-77	-79	Min.	0.00	-7.64	10	-7.64	2	-11.46	6	135.34	2	-124.24	2	0.00	2
319	-77	-79	Min.	150.00	-7.64	10	-7.64	2	0.00	2	30.31	2	0.00	2	0.00	2
319	-78	-77	Max	0.00	7.64	10	7.64	2	0.00	8	-30.31	2	0.00	14	0.00	6
319	-78	-77	Max	150.00	7.64	10	7.64	2	11.46	2	-135.34	2	-124.24	2	0.00	6
319	-78	-77	Min.	0.00	-7.64	14	-7.64	6	0.00	2	-30.31	2	0.00	10	0.00	2
319	-78	-77	Min.	150.00	-7.64	14	-7.64	6	-11.46	6	-135.34	2	-124.24	2	0.00	2

Tipo di combinazione di carico: SLU

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	315	-45	Max	0.00	-2481.84	21	-116.77	21	428.12	29	0.00	21	0.00	29	0.00	22
1	315	-45	Max	328.50	-2172.35	21	-116.77	21	-257.61	21	0.00	21	0.00	29	0.00	22
1	315	-45	Min.	0.00	-6620.23	29	-396.83	29	125.97	21	-0.00	28	0.00	21	0.00	28
1	315	-45	Min.	328.50	-6310.75	29	-396.83	29	-875.48	29	-0.00	28	0.00	21	0.00	28
2	2	202	Max	0.00	-3254.25	21	-0.00	21	0.00	29	0.00	21	0.00	29	0.00	29
2	2	202	Max	328.50	-2944.76	21	-0.00	21	0.00	21	0.00	21	0.00	29	0.00	29
2	2	202	Min.	0.00	-8791.91	29	-0.00	29	0.00	21	-0.00	28	0.00	21	0.00	21
2	2	202	Min.	328.50	-8482.42	29	-0.00	29	-0.01	29	-0.00	28	0.00	21	0.00	21
3	3	203	Max	0.00	-2481.83	21	396.84	29	-125.97	21	0.00	21	0.00	29	0.00	29
3	3	203	Max	328.50	-2172.35	21	396.84	29	875.49	29	0.00	21	0.00	29	0.00	29
3	3	203	Min.	0.00	-6620.24	29	116.77	21	-428.12	29	-0.00	28	0.00	21	0.00	21
3	3	203	Min.	328.50	-6310.75	29	116.77	21	257.61	21	-0.00	28	0.00	21	0.00	21
201	-3	-29	Max	0.00	0.00	17	0.00	21	0.00	29	-238.72	21	0.00	21	0.00	21
201	-3	-29	Max	135.63	0.00	17	0.00	21	0.00	21	-399.28	21	-432.66	21	0.00	21
201	-3	-29	Min.	0.00	0.00	17	0.00	28	0.00	21	-732.10	29	0.00	17	0.00	29
201	-3	-29	Min.	135.63	0.00	17	0.00	28	0.00	28	-892.65	29	-1101.81	29	0.00	29
201	-29	-45	Max	0.00	0.00	17	0.00	21	0.00	21	-735.90	21	-432.66	21	0.00	21
201	-29	-45	Max	83.77	0.00	17	0.00	21	0.00	21	-835.07	21	-1090.66	21	0.00	21

201	-29	-45	Min.	0.00	0.00	17	-0.00	28	0.00	28	-2216.02	29	-1101.81	29	-0.00	29
201	-29	-45	Min.	83.77	0.00	17	-0.00	28	0.00	28	-2315.19	29	-2999.73	29	-0.00	29
201	-45	201	Max	0.00	-116.77	21	0.00	28	0.00	21	3995.56	29	-1348.27	21	0.00	29
201	-45	201	Max	51.86	-116.77	21	0.00	28	0.00	21	3934.17	29	-670.71	21	0.00	29
201	-45	201	Min.	0.00	-396.83	29	-0.00	21	0.00	28	1337.28	21	-3875.20	29	0.00	21
201	-45	201	Min.	51.86	-396.83	29	-0.00	21	0.00	28	1275.89	21	-1819.13	29	0.00	21
201	201	-6	Max	0.00	-116.77	21	0.00	28	0.00	21	2610.80	29	-670.70	21	0.00	29
201	201	-6	Max	135.63	-116.77	21	0.00	28	0.00	28	2450.25	29	1613.01	29	0.00	29
201	201	-6	Min.	0.00	-396.83	29	-0.00	21	0.00	28	939.27	21	-1819.10	29	0.00	21
201	201	-6	Min.	135.63	-396.83	29	-0.00	21	0.00	21	778.72	21	494.34	21	0.00	21
201	-6	-7	Max	0.00	-116.77	21	0.00	28	0.00	28	1126.88	29	1613.10	29	0.00	29
201	-6	-7	Max	135.63	-116.77	21	0.00	28	0.00	28	966.32	29	3032.59	29	0.00	29
201	-6	-7	Min.	0.00	-396.83	29	-0.00	21	0.00	21	442.09	21	494.37	21	0.00	21
201	-6	-7	Min.	135.63	-396.83	29	-0.00	21	0.00	21	281.54	21	985.10	21	0.00	21
201	-7	-8	Max	0.00	-116.77	21	0.00	21	0.00	28	-55.07	21	3032.50	29	0.00	28
201	-7	-8	Max	135.63	-116.77	21	0.00	21	0.00	28	-215.63	21	2439.39	29	0.00	28
201	-7	-8	Min.	0.00	-396.83	29	0.00	28	0.00	21	-357.03	29	985.07	21	0.00	22
201	-7	-8	Min.	135.63	-396.83	29	0.00	28	0.00	21	-517.59	29	801.50	21	0.00	22
201	-8	-9	Max	0.00	-116.77	21	0.00	21	0.00	28	-552.25	21	2439.38	29	0.00	21
201	-8	-9	Max	135.63	-116.77	21	0.00	21	0.00	29	-712.80	21	-56.39	21	0.00	21
201	-8	-9	Min.	0.00	-396.83	29	-0.00	28	0.00	21	-1840.96	29	801.50	21	-0.00	29
201	-8	-9	Min.	135.63	-396.83	29	-0.00	28	0.00	21	-2001.51	29	-166.36	29	-0.00	29
201	-9	-10	Max	0.00	-116.77	21	0.00	21	0.00	29	-1049.42	21	-56.40	21	0.00	21
201	-9	-10	Max	135.63	-116.77	21	0.00	21	0.00	21	-1209.98	21	-1588.59	21	0.00	21
201	-9	-10	Min.	0.00	-396.83	29	-0.00	28	0.00	21	-3324.88	29	-166.39	29	-0.00	29
201	-9	-10	Min.	135.63	-396.83	29	-0.00	28	0.00	28	-3485.43	29	-4784.75	29	-0.00	29
201	-10	202	Max	0.00	-116.77	21	0.00	21	0.00	21	-1448.71	21	-1588.61	21	0.00	21
201	-10	202	Max	20.00	-116.77	21	0.00	21	0.00	21	-1472.38	21	-1880.73	21	0.00	21
201	-10	202	Min.	0.00	-396.83	29	-0.00	28	0.00	28	-4217.53	29	-4784.81	29	-0.00	29
201	-10	202	Min.	20.00	-396.83	29	-0.00	28	0.00	28	-4241.21	29	-5630.70	29	-0.00	29
202	202	-11	Max	0.00	-116.77	21	0.00	28	0.00	21	4241.21	29	-1880.72	21	0.00	29
202	202	-11	Max	20.00	-116.77	21	0.00	28	0.00	21	4217.54	29	-1588.61	21	0.00	29
202	202	-11	Min.	0.00	-396.84	29	-0.00	21	0.00	28	1472.38	21	-5630.69	29	0.00	21
202	202	-11	Min.	20.00	-396.84	29	-0.00	21	0.00	28	1448.70	21	-4784.80	29	0.00	21
202	-11	-12	Max	0.00	-116.77	21	0.00	28	0.00	21	3485.44	29	-1588.61	21	0.00	29
202	-11	-12	Max	135.63	-116.77	21	0.00	28	0.00	29	3324.89	29	-56.41	21	0.00	29
202	-11	-12	Min.	0.00	-396.84	29	-0.00	21	0.00	28	1209.98	21	-4784.81	29	0.00	21
202	-11	-12	Min.	135.63	-396.84	29	-0.00	21	0.00	21	1049.43	21	-166.44	29	0.00	21
202	-12	-13	Max	0.00	-116.77	21	0.00	28	0.00	29	2001.52	29	-56.40	21	0.00	29
202	-12	-13	Max	135.63	-116.77	21	0.00	28	0.00	28	1840.96	29	2439.36	29	0.00	29
202	-12	-13	Min.	0.00	-396.84	29	-0.00	21	0.00	21	712.80	21	-166.39	29	0.00	21
202	-12	-13	Min.	135.63	-396.84	29	-0.00	21	0.00	21	552.25	21	801.49	21	0.00	21
202	-13	-14	Max	0.00	-116.77	21	0.00	28	0.00	28	517.59	29	2439.38	29	0.00	21
202	-13	-14	Max	135.63	-116.77	21	0.00	28	0.00	28	357.04	29	3032.51	29	0.00	21
202	-13	-14	Min.	0.00	-396.84	29	-0.00	21	0.00	21	215.63	21	801.50	21	0.00	29
202	-13	-14	Min.	135.63	-396.84	29	-0.00	21	0.00	21	55.07	21	985.07	21	0.00	29
202	-14	-15	Max	0.00	-116.77	21	0.00	21	0.00	28	-281.55	21	3032.51	29	0.00	21
202	-14	-15	Max	135.63	-116.77	21	0.00	21	0.00	28	-442.10	21	1613.02	29	0.00	21
202	-14	-15	Min.	0.00	-396.84	29	-0.00	28	0.00	21	-966.33	29	985.07	21	0.00	29
202	-14	-15	Min.	135.63	-396.84	29	-0.00	28	0.00	21	-1126.89	29	494.33	21	0.00	29
202	-15	-77	Max	0.00	-116.77	21	0.00	21	0.00	28	-778.71	21	1613.11	29	0.00	21
202	-15	-77	Max	135.63	-116.77	21	0.00	21	0.00	21	-939.27	21	-670.66	21	0.00	21
202	-15	-77	Min.	0.00	-396.84	29	-0.00	28	0.00	21	-2450.24	29	494.37	21	-0.00	29
202	-15	-77	Min.	135.63	-396.84	29	-0.00	28	0.00	28	-2610.80	29	-1818.99	29	-0.00	29
202	-77	203	Max	0.00	-116.77	21	0.00	21	0.00	21	-1275.89	21	-670.68	21	0.00	21
202	-77	203	Max	51.86	-116.77	21	0.00	21	0.00	21	-1337.28	21	-1348.23	21	0.00	21
202	-77	203	Min.	0.00	-396.84	29	-0.00	28	0.00	28	-3934.17	29	-1819.03	29	-0.00	29
202	-77	203	Min.	51.86	-396.84	29	-0.00	28	0.00	28	-3995.55	29	-3875.10	29	-0.00	29
202	203	-26	Max	0.00	0.00	17	0.00	28	0.00	21	2315.19	29	-1090.66	21	0.00	29
202	203	-26	Max	83.77	0.00	17	0.00	28	0.00	21	2216.02	29	-432.65	21	0.00	29
202	203	-26	Min.	0.00	0.00	17	-0.00	21	0.00	28	835.07	21	-2999.73	29	0.00	21
202	203	-26	Min.	83.77	0.00	17	-0.00	21	0.00	28	735.90	21	-1101.80	29	0.00	21
202	-26	-18	Max	0.00	0.00	17	0.00	28	0.00	21	892.66	29	-432.66	21	0.00	29
202	-26	-18	Max	135.63	0.00	17	0.00	28	0.00	21	732.10	29	-0.00	21	0.00	29
202	-26	-18	Min.	0.00	0.00	17	-0.00	21	0.00	28	399.28	21	-1101.83	29	0.00	21
202	-26	-18	Min.	135.63	0.00	17	-0.00	21	0.00	28	238.73	21	-0.01	29	0.00	21
302	-3	-69	Max	0.00	0.00	28	0.00	17	0.00	17	366.05	29	-103.23	21	0.00	17
302	-3	-69	Max	150.00	0.00	21	0.00	17	0.00	17	110.40	29	0.00	22	0.00	17
302	-3	-69	Min.	0.00	0.00	21	0.00	17	0.00	17	119.36	21	-357.34	29	0.00	17
302	-3	-69	Min.	150.00	0.00	28	0.00	17	0.00	17	18.28	21	0.00	28	0.00	17
302	-68	-3	Max	0.00	0.00	28	0.00	17	0.00	17	-18.28	21	0.00	21	0.00	17
302	-68	-3	Max	150.00	-0.00	21	0.00	17	0.00	17	-119.36	21	-103.23	21	0.00	17
302	-68	-3	Min.	0.00	0.00	21	0.00	17	0.00	17	-110.40	29	0.00	17	0.00	17
302	-68	-3	Min.	150.00	-0.00	29	0.00	17	0.00	17	-366.05	29	-357.34	29	0.00	17
303	-29	-76	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
303	-29	-76	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17

303	-29	-76	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
303	-29	-76	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	28	0.00	17
303	-75	-29	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	21	0.00	17
303	-75	-29	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
303	-75	-29	Min.	0.00	0.00	28	0.00	17	0.00	17	-220.80	29	0.00	28	0.00	17
303	-75	-29	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
305	-6	-48	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
305	-6	-48	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	29	0.00	17
305	-6	-48	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
305	-6	-48	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
305	-47	-6	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	17	0.00	17
305	-47	-6	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
305	-47	-6	Min.	0.00	0.00	28	0.00	17	0.00	17	-220.80	29	0.00	21	0.00	17
305	-47	-6	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
306	-7	-50	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
306	-7	-50	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	29	0.00	17
306	-7	-50	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
306	-7	-50	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
306	-49	-7	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	21	0.00	17
306	-49	-7	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
306	-49	-7	Min.	0.00	0.00	28	0.00	17	0.00	17	-220.80	29	0.00	17	0.00	17
306	-49	-7	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
307	-8	-52	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
307	-8	-52	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17
307	-8	-52	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
307	-8	-52	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
307	-51	-8	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	22	0.00	17
307	-51	-8	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
307	-51	-8	Min.	0.00	0.00	17	0.00	17	0.00	17	-220.80	29	0.00	28	0.00	17
307	-51	-8	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
308	-9	-54	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
308	-9	-54	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	29	0.00	17
308	-9	-54	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
308	-9	-54	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
308	-53	-9	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	29	0.00	17
308	-53	-9	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
308	-53	-9	Min.	0.00	0.00	28	0.00	17	0.00	17	-220.80	29	0.00	21	0.00	17
308	-53	-9	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
309	-10	-56	Max	0.00	0.00	28	0.00	17	0.00	17	366.05	29	-103.23	21	0.00	17
309	-10	-56	Max	150.00	0.00	21	0.00	17	0.00	17	110.40	29	0.00	29	0.00	17
309	-10	-56	Min.	0.00	0.00	21	0.00	17	0.00	17	119.36	21	-357.34	29	0.00	17
309	-10	-56	Min.	150.00	0.00	28	0.00	17	0.00	17	18.28	21	0.00	21	0.00	17
309	-55	-10	Max	0.00	0.00	28	0.00	17	0.00	17	-18.28	21	0.00	17	0.00	17
309	-55	-10	Max	150.00	-0.00	21	0.00	17	0.00	17	-119.36	21	-103.23	21	0.00	17
309	-55	-10	Min.	0.00	0.00	17	0.00	17	0.00	17	-110.40	29	0.00	21	0.00	17
309	-55	-10	Min.	150.00	-0.00	29	0.00	17	0.00	17	-366.05	29	-357.34	29	0.00	17
310	-11	-58	Max	0.00	0.00	28	0.00	17	0.00	17	366.05	29	-103.23	21	0.00	17
310	-11	-58	Max	150.00	0.00	21	0.00	17	0.00	17	110.40	29	0.00	17	0.00	17
310	-11	-58	Min.	0.00	0.00	21	0.00	17	0.00	17	119.36	21	-357.34	29	0.00	17
310	-11	-58	Min.	150.00	0.00	28	0.00	17	0.00	17	18.28	21	0.00	21	0.00	17
310	-57	-11	Max	0.00	0.00	21	0.00	17	0.00	17	-18.28	21	0.00	17	0.00	17
310	-57	-11	Max	150.00	-0.00	21	0.00	17	0.00	17	-119.36	21	-103.23	21	0.00	17
310	-57	-11	Min.	0.00	0.00	17	0.00	17	0.00	17	-110.40	29	0.00	28	0.00	17
310	-57	-11	Min.	150.00	-0.00	29	0.00	17	0.00	17	-366.05	29	-357.34	29	0.00	17
311	-12	-60	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
311	-12	-60	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17
311	-12	-60	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
311	-12	-60	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
311	-59	-12	Max	0.00	0.00	28	0.00	17	0.00	17	-36.56	21	0.00	22	0.00	17
311	-59	-12	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
311	-59	-12	Min.	0.00	0.00	17	0.00	17	0.00	17	-220.80	29	0.00	28	0.00	17
311	-59	-12	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
312	-13	-62	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
312	-13	-62	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17
312	-13	-62	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
312	-13	-62	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
312	-61	-13	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	22	0.00	17
312	-61	-13	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
312	-61	-13	Min.	0.00	0.00	28	0.00	17	0.00	17	-220.80	29	0.00	28	0.00	17
312	-61	-13	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
313	-14	-64	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
313	-14	-64	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17
313	-14	-64	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
313	-14	-64	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
313	-63	-14	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	17	0.00	17
313	-63	-14	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17

313	-63	-14	Min.	0.00	0.00	17	0.00	17	0.00	17	-220.80	29	0.00	21	0.00	17
313	-63	-14	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
314	-15	-66	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
314	-15	-66	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17
314	-15	-66	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
314	-15	-66	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
314	-65	-15	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	29	0.00	17
314	-65	-15	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
314	-65	-15	Min.	0.00	0.00	17	0.00	17	0.00	17	-220.80	29	0.00	21	0.00	17
314	-65	-15	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
316	-26	-74	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
316	-26	-74	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17
316	-26	-74	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
316	-26	-74	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
316	-73	-26	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	29	0.00	17
316	-73	-26	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
316	-73	-26	Min.	0.00	0.00	28	0.00	17	0.00	17	-220.80	29	0.00	21	0.00	17
316	-73	-26	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
317	-18	-71	Max	0.00	0.00	28	0.00	17	0.00	17	366.05	29	-103.23	21	0.00	17
317	-18	-71	Max	150.00	0.00	21	0.00	17	0.00	17	110.40	29	0.00	29	0.00	17
317	-18	-71	Min.	0.00	0.00	21	0.00	17	0.00	17	119.36	21	-357.34	29	0.00	17
317	-18	-71	Min.	150.00	0.00	28	0.00	17	0.00	17	18.28	21	0.00	28	0.00	17
317	-70	-18	Max	0.00	0.00	21	0.00	17	0.00	17	-18.28	21	0.00	21	0.00	17
317	-70	-18	Max	150.00	-0.00	21	0.00	17	0.00	17	-119.36	21	-103.23	21	0.00	17
317	-70	-18	Min.	0.00	0.00	28	0.00	17	0.00	17	-110.40	29	0.00	22	0.00	17
317	-70	-18	Min.	150.00	-0.00	29	0.00	17	0.00	17	-366.05	29	-357.34	29	0.00	17
318	201	-81	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
318	201	-81	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17
318	201	-81	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
318	201	-81	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	28	0.00	17
318	-80	201	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	28	0.00	17
318	-80	201	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
318	-80	201	Min.	0.00	0.00	28	0.00	17	0.00	17	-220.80	29	0.00	22	0.00	17
318	-80	201	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17
319	-77	-79	Max	0.00	0.00	28	0.00	17	0.00	17	661.68	29	-153.65	21	0.00	17
319	-77	-79	Max	150.00	0.00	21	0.00	17	0.00	17	220.80	29	0.00	17	0.00	17
319	-77	-79	Min.	0.00	-0.00	21	0.00	17	0.00	17	168.31	21	-661.86	29	0.00	17
319	-77	-79	Min.	150.00	0.00	28	0.00	17	0.00	17	36.56	21	0.00	21	0.00	17
319	-78	-77	Max	0.00	0.00	21	0.00	17	0.00	17	-36.56	21	0.00	29	0.00	17
319	-78	-77	Max	150.00	-0.00	21	0.00	17	0.00	17	-168.31	21	-153.65	21	0.00	17
319	-78	-77	Min.	0.00	0.00	17	0.00	17	0.00	17	-220.80	29	0.00	21	0.00	17
319	-78	-77	Min.	150.00	-0.00	29	0.00	17	0.00	17	-661.68	29	-661.86	29	0.00	17

Tipo di combinazione di carico: SLE R

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	315	-45	Max	0.00	-1824.89	23	-84.12	23	292.18	31	0.00	23	0.00	31	0.00	24
1	315	-45	Max	328.50	-1586.82	23	-84.12	23	-185.59	23	0.00	23	0.00	31	0.00	24
1	315	-45	Min.	0.00	-4583.82	31	-270.83	31	90.75	23	-0.00	30	0.00	23	0.00	30
1	315	-45	Min.	328.50	-4345.75	31	-270.83	31	-597.50	31	-0.00	30	0.00	23	0.00	30
2	2	202	Max	0.00	-2390.57	23	-0.00	23	0.00	31	0.00	23	0.00	31	0.00	31
2	2	202	Max	328.50	-2152.50	23	-0.00	23	0.00	23	0.00	23	0.00	31	0.00	31
2	2	202	Min.	0.00	-6082.35	31	-0.00	31	0.00	23	-0.00	30	0.00	23	0.00	23
2	2	202	Min.	328.50	-5844.28	31	-0.00	31	-0.00	31	-0.00	30	0.00	23	0.00	23
3	3	203	Max	0.00	-1824.88	23	270.83	31	-90.75	23	0.00	23	0.00	31	0.00	31
3	3	203	Max	328.50	-1586.82	23	270.83	31	597.50	31	0.00	23	0.00	31	0.00	31
3	3	203	Min.	0.00	-4583.82	31	84.12	23	-292.19	31	-0.00	30	0.00	23	0.00	23
3	3	203	Min.	328.50	-4345.75	31	84.12	23	185.59	23	-0.00	30	0.00	23	0.00	23
201	-3	-29	Max	0.00	0.00	18	0.00	23	0.00	31	-173.59	23	0.00	23	0.00	23
201	-3	-29	Max	135.63	0.00	18	0.00	23	0.00	23	-297.10	23	-319.19	23	0.00	23
201	-3	-29	Min.	0.00	0.00	18	0.00	30	0.00	23	-502.51	31	0.00	18	0.00	31
201	-3	-29	Min.	135.63	0.00	18	0.00	30	0.00	30	-626.01	31	-765.30	31	0.00	31
201	-29	-45	Max	0.00	0.00	18	0.00	23	0.00	23	-535.96	23	-319.19	23	0.00	23
201	-29	-45	Max	83.77	0.00	18	0.00	23	0.00	23	-612.24	23	-800.12	23	0.00	23
201	-29	-45	Min.	0.00	0.00	18	-0.00	30	0.00	30	-1522.70	31	-765.30	31	0.00	31
201	-29	-45	Min.	83.77	0.00	18	-0.00	30	0.00	30	-1598.98	31	-2072.83	31	0.00	31
201	-45	201	Max	0.00	-84.12	23	0.00	30	0.00	23	2746.77	31	-985.71	23	0.00	31
201	-45	201	Max	51.86	-84.12	23	0.00	30	0.00	23	2699.54	31	-492.56	23	0.00	31
201	-45	201	Min.	0.00	-270.83	31	-0.00	23	0.00	30	974.58	23	-2670.33	31	0.00	23
201	-45	201	Min.	51.86	-270.83	31	-0.00	23	0.00	30	927.36	23	-1258.17	31	0.00	23
201	201	-6	Max	0.00	-84.12	23	0.00	30	0.00	23	1802.85	31	-492.55	23	0.00	31
201	201	-6	Max	135.63	-84.12	23	0.00	30	0.00	30	1679.35	31	1103.28	31	0.00	31
201	201	-6	Min.	0.00	-270.83	31	-0.00	23	0.00	30	688.50	23	-1258.15	31	0.00	23
201	201	-6	Min.	135.63	-270.83	31	-0.00	23	0.00	23	565.00	23	357.50	23	0.00	23
201	-6	-7	Max	0.00	-84.12	23	0.00	30	0.00	30	782.66	31	1103.34	31	0.00	31

201	-6	-7	Max	135.63	-84.12	23	0.00	30	0.00	30	659.16	31	2081.09	31	0.00	31
201	-6	-7	Min.	0.00	-270.83	31	-0.00	23	0.00	23	326.14	23	357.52	23	0.00	23
201	-6	-7	Max	135.63	-270.83	31	-0.00	23	0.00	23	202.63	23	716.10	23	0.00	23
201	-7	-8	Max	0.00	-84.12	23	0.00	23	0.00	30	-36.22	23	2081.04	31	0.00	30
201	-7	-8	Max	135.63	-84.12	23	0.00	23	0.00	30	-159.72	23	1675.13	31	0.00	30
201	-7	-8	Min.	0.00	-270.83	31	0.00	30	0.00	23	-237.53	31	716.08	23	0.00	24
201	-7	-8	Min.	135.63	-270.83	31	0.00	30	0.00	23	-361.03	31	583.21	23	0.00	24
201	-8	-9	Max	0.00	-84.12	23	0.00	23	0.00	30	-398.58	23	1675.12	31	0.00	23
201	-8	-9	Max	135.63	-84.12	23	0.00	23	0.00	31	-522.08	23	-41.14	23	0.00	23
201	-8	-9	Min.	0.00	-270.83	31	0.00	30	0.00	23	-1257.72	31	583.20	23	0.00	31
201	-8	-9	Min.	135.63	-270.83	31	0.00	30	0.00	23	-1381.22	31	-114.45	31	0.00	31
201	-9	-10	Max	0.00	-84.12	23	0.00	23	0.00	31	-760.94	23	-41.14	23	0.00	23
201	-9	-10	Max	135.63	-84.12	23	0.00	23	0.00	23	-884.45	23	-1156.95	23	0.00	23
201	-9	-10	Min.	0.00	-270.83	31	-0.00	30	0.00	23	-2277.91	31	-114.47	31	-0.00	31
201	-9	-10	Min.	135.63	-270.83	31	-0.00	30	0.00	30	-2401.42	31	-3287.72	31	-0.00	31
201	-10	202	Max	0.00	-84.12	23	0.00	23	0.00	23	-1058.04	23	-1156.97	23	0.00	23
201	-10	202	Max	20.00	-84.12	23	0.00	23	0.00	23	-1076.25	23	-1370.40	23	0.00	23
201	-10	202	Min.	0.00	-270.83	31	-0.00	30	0.00	30	-2903.93	31	-3287.76	31	-0.00	31
201	-10	202	Min.	20.00	-270.83	31	-0.00	30	0.00	30	-2922.14	31	-3870.38	31	-0.00	31
202	202	-11	Max	0.00	-84.12	23	0.00	30	0.00	23	2922.14	31	-1370.39	23	0.00	31
202	202	-11	Max	20.00	-84.12	23	0.00	30	0.00	23	2903.93	31	-1156.96	23	0.00	31
202	202	-11	Min.	0.00	-270.83	31	-0.00	23	0.00	30	1076.25	23	-3870.37	31	0.00	23
202	202	-11	Min.	20.00	-270.83	31	-0.00	23	0.00	30	1058.04	23	-3287.76	31	0.00	23
202	-11	-12	Max	0.00	-84.12	23	0.00	30	0.00	23	2401.42	31	-1156.97	23	0.00	31
202	-11	-12	Max	135.63	-84.12	23	0.00	30	0.00	31	2277.92	31	-41.16	23	0.00	31
202	-11	-12	Min.	0.00	-270.83	31	-0.00	23	0.00	30	884.45	23	-3287.77	31	0.00	23
202	-11	-12	Min.	135.63	-270.83	31	-0.00	23	0.00	23	760.94	23	-114.51	31	0.00	23
202	-12	-13	Max	0.00	-84.12	23	0.00	30	0.00	31	1381.23	31	-41.14	23	0.00	31
202	-12	-13	Max	135.63	-84.12	23	0.00	30	0.00	30	1257.72	31	1675.11	31	0.00	31
202	-12	-13	Min.	0.00	-270.83	31	-0.00	23	0.00	23	522.09	23	-114.47	31	0.00	23
202	-12	-13	Min.	135.63	-270.83	31	-0.00	23	0.00	23	398.58	23	583.20	23	0.00	23
202	-13	-14	Max	0.00	-84.12	23	0.00	30	0.00	30	361.03	31	1675.13	31	0.00	23
202	-13	-14	Max	135.63	-84.12	23	0.00	30	0.00	30	237.53	31	2081.04	31	0.00	23
202	-13	-14	Min.	0.00	-270.83	31	0.00	23	0.00	23	159.72	23	583.20	23	0.00	31
202	-13	-14	Min.	135.63	-270.83	31	0.00	23	0.00	23	36.22	23	716.08	23	0.00	31
202	-14	-15	Max	0.00	-84.12	23	0.00	23	0.00	30	-202.64	23	2081.04	31	0.00	23
202	-14	-15	Max	135.63	-84.12	23	0.00	23	0.00	30	-326.14	23	1103.28	31	0.00	23
202	-14	-15	Min.	0.00	-270.83	31	-0.00	30	0.00	23	-659.16	31	716.08	23	0.00	31
202	-14	-15	Min.	135.63	-270.83	31	-0.00	30	0.00	23	-782.66	31	357.49	23	0.00	31
202	-15	-77	Max	0.00	-84.12	23	0.00	23	0.00	30	-564.99	23	1103.35	31	0.00	23
202	-15	-77	Max	135.63	-84.12	23	0.00	23	0.00	23	-688.50	23	-492.52	23	0.00	23
202	-15	-77	Min.	0.00	-270.83	31	-0.00	30	0.00	23	-1679.35	31	357.52	23	0.00	31
202	-15	-77	Min.	135.63	-270.83	31	-0.00	30	0.00	30	-1802.85	31	-1258.08	31	0.00	31
202	-77	203	Max	0.00	-84.12	23	0.00	23	0.00	23	-927.36	23	-492.54	23	0.00	23
202	-77	203	Max	51.86	-84.12	23	0.00	23	0.00	23	-974.58	23	-985.68	23	0.00	23
202	-77	203	Min.	0.00	-270.83	31	-0.00	30	0.00	30	-2699.54	31	-1258.11	31	-0.00	31
202	-77	203	Min.	51.86	-270.83	31	-0.00	30	0.00	30	-2746.76	31	-2670.26	31	-0.00	31
202	203	-26	Max	0.00	0.00	18	0.00	30	0.00	23	1598.99	31	-800.12	23	0.00	31
202	203	-26	Max	83.77	0.00	18	0.00	30	0.00	23	1522.70	31	-319.19	23	0.00	31
202	203	-26	Min.	0.00	0.00	18	-0.00	23	0.00	30	612.24	23	-2072.83	31	0.00	23
202	203	-26	Min.	83.77	0.00	18	-0.00	23	0.00	30	535.96	23	-765.29	31	0.00	23
202	-26	-18	Max	0.00	0.00	18	0.00	30	0.00	23	626.01	31	-319.20	23	0.00	31
202	-26	-18	Max	135.63	0.00	18	0.00	30	0.00	23	502.51	31	-0.00	23	0.00	31
202	-26	-18	Min.	0.00	0.00	18	-0.00	23	0.00	30	297.10	23	-765.31	31	0.00	23
202	-26	-18	Min.	135.63	0.00	18	-0.00	23	0.00	30	173.59	23	-0.01	31	0.00	23
302	-3	-69	Max	0.00	0.00	30	0.00	18	0.00	18	251.25	31	-74.24	23	0.00	18
302	-3	-69	Max	150.00	0.00	23	0.00	18	0.00	18	73.60	31	0.00	24	0.00	18
302	-3	-69	Min.	0.00	0.00	23	0.00	18	0.00	18	86.80	23	-243.64	31	0.00	18
302	-3	-69	Min.	150.00	0.00	30	0.00	18	0.00	18	12.19	23	0.00	30	0.00	18
302	-68	-3	Max	0.00	0.00	30	0.00	18	0.00	18	-12.19	23	0.00	23	0.00	18
302	-68	-3	Max	150.00	-0.00	23	0.00	18	0.00	18	-86.80	23	-74.24	23	0.00	18
302	-68	-3	Min.	0.00	0.00	23	0.00	18	0.00	18	-73.60	31	0.00	18	0.00	18
302	-68	-3	Min.	150.00	-0.00	31	0.00	18	0.00	18	-251.25	31	-243.64	31	0.00	18
303	-29	-76	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
303	-29	-76	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
303	-29	-76	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
303	-29	-76	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	30	0.00	18
303	-75	-29	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	23	0.00	18
303	-75	-29	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
303	-75	-29	Min.	0.00	0.00	30	0.00	18	0.00	18	-147.20	31	0.00	30	0.00	18
303	-75	-29	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.34	31	-446.66	31	0.00	18
305	-6	-48	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
305	-6	-48	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	31	0.00	18
305	-6	-48	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
305	-6	-48	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
305	-47	-6	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	18	0.00	18

305	-47	-6	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
305	-47	-6	Min.	0.00	0.00	30	0.00	18	0.00	18	-147.20	31	0.00	23	0.00	18
305	-47	-6	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.34	31	-446.66	31	0.00	18
306	-7	-50	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
306	-7	-50	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	31	0.00	18
306	-7	-50	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
306	-7	-50	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
306	-49	-7	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	23	0.00	18
306	-49	-7	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
306	-49	-7	Min.	0.00	0.00	30	0.00	18	0.00	18	-147.20	31	0.00	18	0.00	18
306	-49	-7	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.34	31	-446.66	31	0.00	18
307	-8	-52	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
307	-8	-52	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
307	-8	-52	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
307	-8	-52	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
307	-51	-8	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	24	0.00	18
307	-51	-8	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
307	-51	-8	Min.	0.00	0.00	18	0.00	18	0.00	18	-147.20	31	0.00	30	0.00	18
307	-51	-8	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.34	31	-446.66	31	0.00	18
308	-9	-54	Max	0.00	0.00	30	0.00	18	0.00	18	448.34	31	-107.85	23	0.00	18
308	-9	-54	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	31	0.00	18
308	-9	-54	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
308	-9	-54	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
308	-53	-9	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	31	0.00	18
308	-53	-9	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
308	-53	-9	Min.	0.00	0.00	30	0.00	18	0.00	18	-147.20	31	0.00	23	0.00	18
308	-53	-9	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.34	31	-446.66	31	0.00	18
309	-10	-56	Max	0.00	0.00	30	0.00	18	0.00	18	251.25	31	-74.24	23	0.00	18
309	-10	-56	Max	150.00	0.00	23	0.00	18	0.00	18	73.60	31	0.00	31	0.00	18
309	-10	-56	Min.	0.00	0.00	23	0.00	18	0.00	18	86.80	23	-243.64	31	0.00	18
309	-10	-56	Min.	150.00	0.00	30	0.00	18	0.00	18	12.19	23	0.00	23	0.00	18
309	-55	-10	Max	0.00	0.00	30	0.00	18	0.00	18	-12.19	23	0.00	18	0.00	18
309	-55	-10	Max	150.00	-0.00	23	0.00	18	0.00	18	-86.80	23	-74.24	23	0.00	18
309	-55	-10	Min.	0.00	0.00	18	0.00	18	0.00	18	-73.60	31	0.00	23	0.00	18
309	-55	-10	Min.	150.00	-0.00	31	0.00	18	0.00	18	-251.25	31	-243.64	31	0.00	18
310	-11	-58	Max	0.00	0.00	30	0.00	18	0.00	18	251.25	31	-74.24	23	0.00	18
310	-11	-58	Max	150.00	0.00	23	0.00	18	0.00	18	73.60	31	0.00	18	0.00	18
310	-11	-58	Min.	0.00	0.00	23	0.00	18	0.00	18	86.80	23	-243.64	31	0.00	18
310	-11	-58	Min.	150.00	0.00	30	0.00	18	0.00	18	12.19	23	0.00	23	0.00	18
310	-57	-11	Max	0.00	0.00	23	0.00	18	0.00	18	-12.19	23	0.00	18	0.00	18
310	-57	-11	Max	150.00	-0.00	23	0.00	18	0.00	18	-86.80	23	-74.24	23	0.00	18
310	-57	-11	Min.	0.00	0.00	18	0.00	18	0.00	18	-73.60	31	0.00	30	0.00	18
310	-57	-11	Min.	150.00	-0.00	31	0.00	18	0.00	18	-251.25	31	-243.64	31	0.00	18
311	-12	-60	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
311	-12	-60	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
311	-12	-60	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
311	-12	-60	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
311	-59	-12	Max	0.00	0.00	30	0.00	18	0.00	18	-24.37	23	0.00	24	0.00	18
311	-59	-12	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
311	-59	-12	Min.	0.00	0.00	18	0.00	18	0.00	18	-147.20	31	0.00	30	0.00	18
311	-59	-12	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.35	31	-446.66	31	0.00	18
312	-13	-62	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
312	-13	-62	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
312	-13	-62	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
312	-13	-62	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
312	-61	-13	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	24	0.00	18
312	-61	-13	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
312	-61	-13	Min.	0.00	0.00	30	0.00	18	0.00	18	-147.20	31	0.00	30	0.00	18
312	-61	-13	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.35	31	-446.66	31	0.00	18
313	-14	-64	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
313	-14	-64	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
313	-14	-64	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
313	-14	-64	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
313	-63	-14	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	18	0.00	18
313	-63	-14	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
313	-63	-14	Min.	0.00	0.00	18	0.00	18	0.00	18	-147.20	31	0.00	23	0.00	18
313	-63	-14	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.35	31	-446.66	31	0.00	18
314	-15	-66	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
314	-15	-66	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
314	-15	-66	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
314	-15	-66	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
314	-65	-15	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	31	0.00	18
314	-65	-15	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
314	-65	-15	Min.	0.00	0.00	18	0.00	18	0.00	18	-147.20	31	0.00	23	0.00	18
314	-65	-15	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.35	31	-446.66	31	0.00	18
316	-26	-74	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18

316	-26	-74	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
316	-26	-74	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
316	-26	-74	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
316	-73	-26	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	31	0.00	18
316	-73	-26	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
316	-73	-26	Min.	0.00	0.00	30	0.00	18	0.00	18	-147.20	31	0.00	23	0.00	18
316	-73	-26	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.35	31	-446.66	31	0.00	18
317	-18	-71	Max	0.00	0.00	30	0.00	18	0.00	18	251.25	31	-74.24	23	0.00	18
317	-18	-71	Max	150.00	0.00	23	0.00	18	0.00	18	73.60	31	0.00	18	0.00	18
317	-18	-71	Min.	0.00	0.00	23	0.00	18	0.00	18	86.80	23	-243.64	31	0.00	18
317	-18	-71	Min.	150.00	0.00	30	0.00	18	0.00	18	12.19	23	0.00	30	0.00	18
317	-70	-18	Max	0.00	0.00	23	0.00	18	0.00	18	-12.19	23	0.00	23	0.00	18
317	-70	-18	Max	150.00	-0.00	23	0.00	18	0.00	18	-86.80	23	-74.24	23	0.00	18
317	-70	-18	Min.	0.00	0.00	30	0.00	18	0.00	18	-73.60	31	0.00	24	0.00	18
317	-70	-18	Min.	150.00	-0.00	31	0.00	18	0.00	18	-251.25	31	-243.64	31	0.00	18
318	201	-81	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
318	201	-81	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
318	201	-81	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
318	201	-81	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	30	0.00	18
318	-80	201	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	30	0.00	18
318	-80	201	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
318	-80	201	Min.	0.00	0.00	30	0.00	18	0.00	18	-147.20	31	0.00	24	0.00	18
318	-80	201	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.34	31	-446.66	31	0.00	18
319	-77	-79	Max	0.00	0.00	30	0.00	18	0.00	18	448.35	31	-107.85	23	0.00	18
319	-77	-79	Max	150.00	0.00	23	0.00	18	0.00	18	147.20	31	0.00	18	0.00	18
319	-77	-79	Min.	0.00	0.00	23	0.00	18	0.00	18	119.43	23	-446.66	31	0.00	18
319	-77	-79	Min.	150.00	0.00	30	0.00	18	0.00	18	24.37	23	0.00	23	0.00	18
319	-78	-77	Max	0.00	0.00	23	0.00	18	0.00	18	-24.37	23	0.00	31	0.00	18
319	-78	-77	Max	150.00	-0.00	23	0.00	18	0.00	18	-119.43	23	-107.85	23	0.00	18
319	-78	-77	Min.	0.00	0.00	18	0.00	18	0.00	18	-147.20	31	0.00	23	0.00	18
319	-78	-77	Min.	150.00	-0.00	31	0.00	18	0.00	18	-448.35	31	-446.66	31	0.00	18

Tipo di combinazione di carico: SLE F

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	315	-45	Max	0.00	-1700.15	25	-75.68	25	134.30	19	0.00	25	0.00	19	0.00	19
1	315	-45	Max	328.50	-1462.08	25	-75.68	25	-166.96	25	0.00	25	0.00	19	0.00	19
1	315	-45	Min.	0.00	-2421.34	19	-124.49	19	81.65	25	0.00	32	0.00	25	0.00	32
1	315	-45	Min.	328.50	-2183.27	19	-124.49	19	-274.64	19	0.00	32	0.00	25	0.00	32
2	2	202	Max	0.00	-2223.66	25	-0.00	25	0.00	19	0.00	25	0.00	19	0.00	19
2	2	202	Max	328.50	-1985.59	25	-0.00	25	0.00	25	0.00	25	0.00	19	0.00	19
2	2	202	Min.	0.00	-3188.70	19	-0.00	19	0.00	25	0.00	32	0.00	25	0.00	25
2	2	202	Min.	328.50	-2950.63	19	-0.00	19	-0.00	19	0.00	32	0.00	25	0.00	25
3	3	203	Max	0.00	-1700.15	25	124.49	19	-81.65	25	0.00	25	0.00	19	0.00	19
3	3	203	Max	328.50	-1462.08	25	124.49	19	274.64	19	0.00	25	0.00	19	0.00	19
3	3	203	Min.	0.00	-2421.34	19	75.68	25	-134.30	19	-0.00	32	0.00	25	0.00	25
3	3	203	Min.	328.50	-2183.27	19	75.68	25	166.96	25	-0.00	32	0.00	25	0.00	25
201	-3	-29	Max	0.00	0.00	19	0.00	25	0.00	19	-158.72	25	0.00	25	0.00	25
201	-3	-29	Max	135.63	0.00	19	0.00	25	0.00	25	-282.23	25	-299.03	25	0.00	25
201	-3	-29	Min.	0.00	0.00	19	0.00	32	0.00	25	-244.70	19	0.00	19	0.00	19
201	-3	-29	Min.	135.63	0.00	19	0.00	32	0.00	32	-368.20	19	-415.64	19	0.00	19
201	-29	-45	Max	0.00	0.00	19	0.00	25	0.00	25	-491.34	25	-299.02	25	0.00	25
201	-29	-45	Max	83.77	0.00	19	0.00	25	0.00	25	-567.62	25	-742.58	25	0.00	25
201	-29	-45	Min.	0.00	0.00	19	0.00	32	0.00	32	-749.28	19	-415.64	19	0.00	19
201	-29	-45	Min.	83.77	0.00	19	0.00	32	0.00	32	-825.56	19	-1075.27	19	0.00	19
201	-45	201	Max	0.00	-75.68	25	0.00	32	0.00	25	1357.71	19	-909.54	25	0.00	19
201	-45	201	Max	51.86	-75.68	25	0.00	32	0.00	25	1310.49	19	-457.94	25	0.00	19
201	-45	201	Min.	0.00	-124.49	19	-0.00	25	0.00	32	894.46	25	-1349.90	19	0.00	25
201	-45	201	Min.	51.86	-124.49	19	-0.00	25	0.00	32	847.23	25	-658.08	19	0.00	25
201	201	-6	Max	0.00	-75.68	25	0.00	32	0.00	25	929.41	19	-457.94	25	0.00	19
201	201	-6	Max	135.63	-75.68	25	0.00	32	0.00	32	805.91	19	518.73	19	0.00	19
201	201	-6	Min.	0.00	-124.49	19	0.00	25	0.00	32	638.12	25	-658.07	19	0.00	25
201	201	-6	Min.	135.63	-124.49	19	0.00	25	0.00	25	514.61	25	323.78	25	0.00	25
201	-6	-7	Max	0.00	-75.68	25	0.00	32	0.00	32	424.83	19	518.76	19	0.00	19
201	-6	-7	Max	135.63	-75.68	25	0.00	32	0.00	32	301.33	19	1011.19	19	0.00	19
201	-6	-7	Min.	0.00	-124.49	19	0.00	25	0.00	25	305.50	25	323.80	25	0.00	25
201	-6	-7	Min.	135.63	-124.49	19	0.00	25	0.00	25	181.99	25	654.38	25	0.00	25
201	-7	-8	Max	0.00	-75.68	25	0.00	25	0.00	32	-27.12	25	1011.17	19	0.00	32
201	-7	-8	Max	135.63	-75.68	25	0.00	25	0.00	32	-150.62	25	819.27	19	0.00	32
201	-7	-8	Min.	0.00	-124.49	19	0.00	32	0.00	25	-79.74	19	654.37	25	0.00	19
201	-7	-8	Min.	135.63	-124.49	19	0.00	32	0.00	25	-203.24	19	533.84	25	0.00	19
201	-8	-9	Max	0.00	-75.68	25	0.00	25	0.00	32	-359.74	25	819.27	19	0.00	25
201	-8	-9	Max	135.63	-75.68	25	0.00	25	0.00	19	-483.24	25	-37.82	25	0.00	25
201	-8	-9	Min.	0.00	-124.49	19	0.00	32	0.00	25	-584.32	19	533.84	25	0.00	19
201	-8	-9	Min.	135.63	-124.49	19	0.00	32	0.00	25	-707.82	19	-56.99	19	0.00	19

201	-9	-10	Max	0.00	-75.68	25	0.00	25	0.00	19	-692.36	25	-37.83	25	0.00	25
201	-9	-10	Max	135.63	-75.68	25	0.00	25	0.00	25	-815.86	25	-1060.61	25	0.00	25
201	-9	-10	Min.	0.00	-124.49	19	0.00	32	0.00	25	-1088.90	19	-57.00	19	0.00	19
201	-9	-10	Min.	135.63	-124.49	19	0.00	32	0.00	32	-1212.40	19	-1617.60	19	0.00	19
201	-10	202	Max	0.00	-75.68	25	0.00	25	0.00	25	-974.58	25	-1060.63	25	0.00	25
201	-10	202	Max	20.00	-75.68	25	0.00	25	0.00	25	-992.80	25	-1257.37	25	0.00	25
201	-10	202	Min.	0.00	-124.49	19	0.00	32	0.00	32	-1457.10	19	-1617.62	19	0.00	19
201	-10	202	Min.	20.00	-124.49	19	0.00	32	0.00	32	-1475.31	19	-1910.87	19	0.00	19
202	202	-11	Max	0.00	-75.68	25	0.00	32	0.00	25	1475.32	19	-1257.37	25	0.00	19
202	202	-11	Max	20.00	-75.68	25	0.00	32	0.00	25	1457.10	19	-1060.62	25	0.00	19
202	202	-11	Min.	0.00	-124.49	19	-0.00	25	0.00	32	992.80	25	-1910.86	19	0.00	25
202	202	-11	Min.	20.00	-124.49	19	-0.00	25	0.00	32	974.58	25	-1617.62	19	0.00	25
202	-11	-12	Max	0.00	-75.68	25	0.00	32	0.00	25	1212.40	19	-1060.63	25	0.00	19
202	-11	-12	Max	135.63	-75.68	25	0.00	32	0.00	19	1088.90	19	-37.84	25	0.00	19
202	-11	-12	Min.	0.00	-124.49	19	-0.00	25	0.00	32	815.86	25	-1617.62	19	0.00	25
202	-11	-12	Min.	135.63	-124.49	19	-0.00	25	0.00	25	692.36	25	-57.01	19	0.00	25
202	-12	-13	Max	0.00	-75.68	25	0.00	32	0.00	19	707.82	19	-37.83	25	0.00	19
202	-12	-13	Max	135.63	-75.68	25	0.00	32	0.00	32	584.32	19	819.26	19	0.00	19
202	-12	-13	Min.	0.00	-124.49	19	0.00	25	0.00	25	483.24	25	-57.00	19	0.00	25
202	-12	-13	Min.	135.63	-124.49	19	0.00	25	0.00	25	359.74	25	533.83	25	0.00	25
202	-13	-14	Max	0.00	-75.68	25	0.00	32	0.00	32	203.24	19	819.27	19	0.00	25
202	-13	-14	Max	135.63	-75.68	25	0.00	32	0.00	32	79.74	19	1011.17	19	0.00	25
202	-13	-14	Min.	0.00	-124.49	19	0.00	25	0.00	25	150.62	25	533.84	25	0.00	19
202	-13	-14	Min.	135.63	-124.49	19	0.00	25	0.00	25	27.12	25	654.37	25	0.00	19
202	-14	-15	Max	0.00	-75.68	25	0.00	25	0.00	32	-182.00	25	1011.17	19	0.00	25
202	-14	-15	Max	135.63	-75.68	25	0.00	25	0.00	32	-305.50	25	518.72	19	0.00	25
202	-14	-15	Min.	0.00	-124.49	19	0.00	32	0.00	25	-301.33	19	654.37	25	0.00	19
202	-14	-15	Min.	135.63	-124.49	19	0.00	32	0.00	25	-424.84	19	323.77	25	0.00	19
202	-15	-77	Max	0.00	-75.68	25	0.00	25	0.00	32	-514.61	25	518.76	19	0.00	25
202	-15	-77	Max	135.63	-75.68	25	0.00	25	0.00	25	-638.11	25	-457.91	25	0.00	25
202	-15	-77	Min.	0.00	-124.49	19	0.00	32	0.00	25	-805.90	19	323.80	25	0.00	19
202	-15	-77	Min.	135.63	-124.49	19	0.00	32	0.00	32	-929.41	19	-658.03	19	0.00	19
202	-77	203	Max	0.00	-75.68	25	0.00	25	0.00	25	-847.23	25	-457.92	25	0.00	25
202	-77	203	Max	51.86	-75.68	25	0.00	25	0.00	25	-894.45	25	-909.52	25	0.00	25
202	-77	203	Min.	0.00	-124.49	19	0.00	32	0.00	32	-1310.48	19	-658.04	19	0.00	19
202	-77	203	Min.	51.86	-124.49	19	0.00	32	0.00	32	-1357.70	19	-1349.87	19	0.00	19
202	203	-26	Max	0.00	0.00	19	0.00	32	0.00	25	825.56	19	-742.58	25	0.00	19
202	203	-26	Max	83.77	0.00	19	0.00	32	0.00	25	749.28	19	-299.02	25	0.00	19
202	203	-26	Min.	0.00	0.00	19	0.00	25	0.00	32	567.62	25	-1075.27	19	0.00	25
202	203	-26	Min.	83.77	0.00	19	0.00	25	0.00	32	491.34	25	-415.63	19	0.00	25
202	-26	-18	Max	0.00	0.00	19	0.00	32	0.00	25	368.21	19	-299.03	25	0.00	19
202	-26	-18	Max	135.63	0.00	19	0.00	32	0.00	25	244.70	19	-0.00	25	0.00	19
202	-26	-18	Min.	0.00	0.00	19	0.00	25	0.00	32	282.23	25	-415.64	19	0.00	25
202	-26	-18	Min.	135.63	0.00	19	0.00	25	0.00	32	158.72	25	-0.00	19	0.00	25
302	-3	-69	Max	0.00	0.00	32	0.00	19	0.00	19	122.35	19	-66.58	25	0.00	19
302	-3	-69	Max	150.00	0.00	25	0.00	19	0.00	19	25.46	19	0.00	19	0.00	19
302	-3	-69	Min.	0.00	0.00	25	0.00	19	0.00	19	79.36	25	-110.86	19	0.00	19
302	-3	-69	Min.	150.00	0.00	32	0.00	19	0.00	19	9.41	25	0.00	32	0.00	19
302	-68	-3	Max	0.00	0.00	32	0.00	19	0.00	19	-9.41	25	0.00	25	0.00	19
302	-68	-3	Max	150.00	-0.00	25	0.00	19	0.00	19	-79.36	25	-66.58	25	0.00	19
302	-68	-3	Min.	0.00	0.00	25	0.00	19	0.00	19	-25.46	19	0.00	19	0.00	19
302	-68	-3	Min.	150.00	-0.00	19	0.00	19	0.00	19	-122.35	19	-110.86	19	0.00	19
303	-29	-76	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
303	-29	-76	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
303	-29	-76	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
303	-29	-76	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	32	0.00	19
303	-75	-29	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	25	0.00	19
303	-75	-29	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
303	-75	-29	Min.	0.00	0.00	32	0.00	19	0.00	19	-50.93	19	0.00	32	0.00	19
303	-75	-29	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
305	-6	-48	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
305	-6	-48	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
305	-6	-48	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
305	-6	-48	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
305	-47	-6	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
305	-47	-6	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
305	-47	-6	Min.	0.00	0.00	32	0.00	19	0.00	19	-50.93	19	0.00	25	0.00	19
305	-47	-6	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
306	-7	-50	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
306	-7	-50	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
306	-7	-50	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
306	-7	-50	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
306	-49	-7	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	25	0.00	19
306	-49	-7	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
306	-49	-7	Min.	0.00	0.00	32	0.00	19	0.00	19	-50.93	19	0.00	19	0.00	19
306	-49	-7	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19

307	-8	-52	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
307	-8	-52	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
307	-8	-52	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
307	-8	-52	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
307	-51	-8	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
307	-51	-8	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
307	-51	-8	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.93	19	0.00	32	0.00	19
307	-51	-8	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
308	-9	-54	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
308	-9	-54	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
308	-9	-54	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
308	-9	-54	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
308	-53	-9	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
308	-53	-9	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
308	-53	-9	Min.	0.00	0.00	32	0.00	19	0.00	19	-50.93	19	0.00	25	0.00	19
308	-53	-9	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
309	-10	-56	Max	0.00	0.00	32	0.00	19	0.00	19	122.35	19	-66.58	25	0.00	19
309	-10	-56	Max	150.00	0.00	25	0.00	19	0.00	19	25.46	19	0.00	19	0.00	19
309	-10	-56	Min.	0.00	0.00	25	0.00	19	0.00	19	79.36	25	-110.86	19	0.00	19
309	-10	-56	Min.	150.00	0.00	32	0.00	19	0.00	19	9.41	25	0.00	25	0.00	19
309	-55	-10	Max	0.00	0.00	32	0.00	19	0.00	19	-9.41	25	0.00	32	0.00	19
309	-55	-10	Max	150.00	-0.00	25	0.00	19	0.00	19	-79.36	25	-66.58	25	0.00	19
309	-55	-10	Min.	0.00	0.00	19	0.00	19	0.00	19	-25.46	19	0.00	25	0.00	19
309	-55	-10	Min.	150.00	-0.00	19	0.00	19	0.00	19	-122.35	19	-110.86	19	0.00	19
310	-11	-58	Max	0.00	0.00	32	0.00	19	0.00	19	122.35	19	-66.58	25	0.00	19
310	-11	-58	Max	150.00	0.00	25	0.00	19	0.00	19	25.46	19	0.00	19	0.00	19
310	-11	-58	Min.	0.00	0.00	25	0.00	19	0.00	19	79.36	25	-110.86	19	0.00	19
310	-11	-58	Min.	150.00	0.00	32	0.00	19	0.00	19	9.41	25	0.00	25	0.00	19
310	-57	-11	Max	0.00	0.00	25	0.00	19	0.00	19	-9.41	25	0.00	19	0.00	19
310	-57	-11	Max	150.00	-0.00	25	0.00	19	0.00	19	-79.36	25	-66.58	25	0.00	19
310	-57	-11	Min.	0.00	0.00	19	0.00	19	0.00	19	-25.46	19	0.00	32	0.00	19
310	-57	-11	Min.	150.00	-0.00	19	0.00	19	0.00	19	-122.35	19	-110.86	19	0.00	19
311	-12	-60	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
311	-12	-60	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
311	-12	-60	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
311	-12	-60	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
311	-59	-12	Max	0.00	0.00	32	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
311	-59	-12	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
311	-59	-12	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.93	19	0.00	32	0.00	19
311	-59	-12	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
312	-13	-62	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
312	-13	-62	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
312	-13	-62	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
312	-13	-62	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
312	-61	-13	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
312	-61	-13	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
312	-61	-13	Min.	0.00	0.00	32	0.00	19	0.00	19	-50.93	19	0.00	32	0.00	19
312	-61	-13	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
313	-14	-64	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
313	-14	-64	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
313	-14	-64	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
313	-14	-64	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
313	-63	-14	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
313	-63	-14	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
313	-63	-14	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.93	19	0.00	25	0.00	19
313	-63	-14	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
314	-15	-66	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
314	-15	-66	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
314	-15	-66	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
314	-15	-66	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
314	-65	-15	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
314	-65	-15	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
314	-65	-15	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.93	19	0.00	25	0.00	19
314	-65	-15	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
316	-26	-74	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
316	-26	-74	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
316	-26	-74	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
316	-26	-74	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
316	-73	-26	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
316	-73	-26	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
316	-73	-26	Min.	0.00	0.00	32	0.00	19	0.00	19	-50.93	19	0.00	25	0.00	19
316	-73	-26	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
317	-18	-71	Max	0.00	0.00	32	0.00	19	0.00	19	122.35	19	-66.58	25	0.00	19
317	-18	-71	Max	150.00	0.00	25	0.00	19	0.00	19	25.46	19	0.00	19	0.00	19
317	-18	-71	Min.	0.00	0.00	25	0.00	19	0.00	19	79.36	25	-110.86	19	0.00	19
317	-18	-71	Min.	150.00	0.00	32	0.00	19	0.00	19	9.41	25	0.00	32	0.00	19

317	-70	-18	Max	0.00	0.00	25	0.00	19	0.00	19	-9.41	25	0.00	25	0.00	19
317	-70	-18	Max	150.00	-0.00	25	0.00	19	0.00	19	-79.36	25	-66.58	25	0.00	19
317	-70	-18	Min.	0.00	0.00	32	0.00	19	0.00	19	-25.46	19	0.00	19	0.00	19
317	-70	-18	Min.	150.00	-0.00	19	0.00	19	0.00	19	-122.35	19	-110.86	19	0.00	19
318	201	-81	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
318	201	-81	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
318	201	-81	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
318	201	-81	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	32	0.00	19
318	-80	201	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	32	0.00	19
318	-80	201	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
318	-80	201	Min.	0.00	0.00	32	0.00	19	0.00	19	-50.93	19	0.00	19	0.00	19
318	-80	201	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19
319	-77	-79	Max	0.00	0.00	32	0.00	19	0.00	19	190.54	19	-92.53	25	0.00	19
319	-77	-79	Max	150.00	0.00	25	0.00	19	0.00	19	50.93	19	0.00	19	0.00	19
319	-77	-79	Min.	0.00	0.00	25	0.00	19	0.00	19	104.56	25	-181.10	19	0.00	19
319	-77	-79	Min.	150.00	0.00	32	0.00	19	0.00	19	18.82	25	0.00	25	0.00	19
319	-78	-77	Max	0.00	0.00	25	0.00	19	0.00	19	-18.82	25	0.00	19	0.00	19
319	-78	-77	Max	150.00	-0.00	25	0.00	19	0.00	19	-104.56	25	-92.53	25	0.00	19
319	-78	-77	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.93	19	0.00	25	0.00	19
319	-78	-77	Min.	150.00	-0.00	19	0.00	19	0.00	19	-190.54	19	-181.10	19	0.00	19

Tipologia di combinazione di carico: SLE Q

Asta	N1	N2		X <cm>	N <daN>	CC <daN>	Ty <daN>	CC <daNm>	Mz <daNm>	CC <daN>	Tz <daN>	CC <daNm>	My <daNm>	CC <daNm>	Mx <daNm>	CC
1	315	-45	Max	0.00	-1958.34	20	-93.15	20	100.50	20	0.00	20	0.00	20	0.00	20
1	315	-45	Max	328.50	-1720.27	20	-93.15	20	-205.51	20	0.00	20	0.00	20	0.00	20
1	315	-45	Min.	0.00	-1958.34	20	-93.15	20	100.50	20	0.00	20	0.00	20	0.00	20
1	315	-45	Min.	328.50	-1720.27	20	-93.15	20	-205.51	20	0.00	20	0.00	20	0.00	20
2	2	202	Max	0.00	-2569.15	20	-0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
2	2	202	Max	328.50	-2331.08	20	-0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
2	2	202	Min.	0.00	-2569.15	20	-0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
2	2	202	Min.	328.50	-2331.08	20	-0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	0.00	-1958.34	20	93.15	20	-100.50	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	328.50	-1720.27	20	93.15	20	205.51	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	0.00	-1958.34	20	93.15	20	-100.50	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	328.50	-1720.27	20	93.15	20	205.51	20	0.00	20	0.00	20	0.00	20
201	-3	-29	Max	0.00	0.00	20	0.00	20	0.00	20	-189.50	20	0.00	20	0.00	20
201	-3	-29	Max	135.63	0.00	20	0.00	20	0.00	20	-313.01	20	-340.77	20	0.00	20
201	-3	-29	Min.	0.00	0.00	20	0.00	20	0.00	20	-189.50	20	0.00	20	0.00	20
201	-3	-29	Min.	135.63	0.00	20	0.00	20	0.00	20	-313.01	20	-340.77	20	0.00	20
201	-29	-45	Max	0.00	0.00	20	0.00	20	0.00	20	-583.68	20	-340.77	20	0.00	20
201	-29	-45	Max	83.77	0.00	20	0.00	20	0.00	20	-659.97	20	-861.68	20	0.00	20
201	-29	-45	Min.	0.00	0.00	20	0.00	20	0.00	20	-583.68	20	-340.77	20	0.00	20
201	-29	-45	Min.	83.77	0.00	20	0.00	20	0.00	20	-659.97	20	-861.68	20	0.00	20
201	-45	201	Max	0.00	-93.15	20	0.00	20	0.00	20	1060.30	20	-1067.19	20	0.00	20
201	-45	201	Max	51.86	-93.15	20	0.00	20	0.00	20	1013.08	20	-529.59	20	0.00	20
201	-45	201	Min.	0.00	-93.15	20	0.00	20	0.00	20	1060.30	20	-1067.19	20	0.00	20
201	-45	201	Min.	51.86	-93.15	20	0.00	20	0.00	20	1013.08	20	-529.59	20	0.00	20
201	201	-6	Max	0.00	-93.15	20	0.00	20	0.00	20	742.40	20	-529.58	20	0.00	20
201	201	-6	Max	135.63	-93.15	20	0.00	20	0.00	20	618.90	20	393.57	20	0.00	20
201	201	-6	Min.	0.00	-93.15	20	0.00	20	0.00	20	742.40	20	-529.58	20	0.00	20
201	201	-6	Min.	135.63	-93.15	20	0.00	20	0.00	20	618.90	20	393.57	20	0.00	20
201	-6	-7	Max	0.00	-93.15	20	0.00	20	0.00	20	348.22	20	393.59	20	0.00	20
201	-6	-7	Max	135.63	-93.15	20	0.00	20	0.00	20	224.72	20	782.12	20	0.00	20
201	-6	-7	Min.	0.00	-93.15	20	0.00	20	0.00	20	348.22	20	393.59	20	0.00	20
201	-6	-7	Min.	135.63	-93.15	20	0.00	20	0.00	20	224.72	20	782.12	20	0.00	20
201	-7	-8	Max	0.00	-93.15	20	0.00	20	0.00	20	-45.95	20	782.11	20	0.00	20
201	-7	-8	Max	135.63	-93.15	20	0.00	20	0.00	20	-169.46	20	636.02	20	0.00	20
201	-7	-8	Min.	0.00	-93.15	20	0.00	20	0.00	20	-45.95	20	782.11	20	0.00	20
201	-7	-8	Min.	135.63	-93.15	20	0.00	20	0.00	20	-169.46	20	636.02	20	0.00	20
201	-8	-9	Max	0.00	-93.15	20	0.00	20	0.00	20	-440.14	20	636.02	20	0.00	20
201	-8	-9	Max	135.63	-93.15	20	0.00	20	0.00	20	-563.64	20	-44.68	20	0.00	20
201	-8	-9	Min.	0.00	-93.15	20	0.00	20	0.00	20	-440.14	20	636.02	20	0.00	20
201	-8	-9	Min.	135.63	-93.15	20	0.00	20	0.00	20	-563.64	20	-44.68	20	0.00	20
201	-9	-10	Max	0.00	-93.15	20	0.00	20	0.00	20	-834.32	20	-44.69	20	0.00	20
201	-9	-10	Max	135.63	-93.15	20	0.00	20	0.00	20	-957.82	20	-1260.02	20	0.00	20
201	-9	-10	Min.	0.00	-93.15	20	0.00	20	0.00	20	-834.32	20	-44.69	20	0.00	20
201	-9	-10	Min.	135.63	-93.15	20	0.00	20	0.00	20	-957.82	20	-1260.02	20	0.00	20
201	-10	202	Max	0.00	-93.15	20	0.00	20	0.00	20	-1147.33	20	-1260.03	20	0.00	20
201	-10	202	Max	20.00	-93.15	20	0.00	20	0.00	20	-1165.54	20	-1491.32	20	0.00	20
201	-10	202	Min.	0.00	-93.15	20	0.00	20	0.00	20	-1147.33	20	-1260.03	20	0.00	20
201	-10	202	Min.	20.00	-93.15	20	0.00	20	0.00	20	-1165.54	20	-1491.32	20	0.00	20
202	202	-11	Max	0.00	-93.15	20	0.00	20	0.00	20	1165.54	20	-1491.32	20	0.00	20
202	202	-11	Max	20.00	-93.15	20	0.00	20	0.00	20	1147.33	20	-1260.03	20	0.00	20
202	202	-11	Min.	0.00	-93.15	20	0.00	20	0.00	20	1165.54	20	-1491.32	20	0.00	20



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202	202	-11	Min.	20.00	-93.15	20	0.00	20	0.00	20	1147.33	20	-1260.03	20	0.00	20
202	-11	-12	Max	0.00	-93.15	20	0.00	20	0.00	20	957.83	20	-1260.03	20	0.00	20
202	-11	-12	Max	135.63	-93.15	20	0.00	20	0.00	20	834.32	20	-44.70	20	0.00	20
202	-11	-12	Min.	0.00	-93.15	20	0.00	20	0.00	20	957.83	20	-1260.03	20	0.00	20
202	-11	-12	Min.	135.63	-93.15	20	0.00	20	0.00	20	834.32	20	-44.70	20	0.00	20
202	-12	-13	Max	0.00	-93.15	20	0.00	20	0.00	20	563.64	20	-44.69	20	0.00	20
202	-12	-13	Max	135.63	-93.15	20	0.00	20	0.00	20	440.14	20	636.02	20	0.00	20
202	-12	-13	Min.	0.00	-93.15	20	0.00	20	0.00	20	563.64	20	-44.69	20	0.00	20
202	-12	-13	Min.	135.63	-93.15	20	0.00	20	0.00	20	440.14	20	636.02	20	0.00	20
202	-13	-14	Max	0.00	-93.15	20	0.00	20	0.00	20	169.46	20	636.02	20	0.00	20
202	-13	-14	Max	135.63	-93.15	20	0.00	20	0.00	20	45.96	20	782.11	20	0.00	20
202	-13	-14	Min.	0.00	-93.15	20	0.00	20	0.00	20	169.46	20	636.02	20	0.00	20
202	-13	-14	Min.	135.63	-93.15	20	0.00	20	0.00	20	45.96	20	782.11	20	0.00	20
202	-14	-15	Max	0.00	-93.15	20	0.00	20	0.00	20	-224.72	20	782.11	20	0.00	20
202	-14	-15	Max	135.63	-93.15	20	0.00	20	0.00	20	-348.23	20	393.57	20	0.00	20
202	-14	-15	Min.	0.00	-93.15	20	0.00	20	0.00	20	-224.72	20	782.11	20	0.00	20
202	-14	-15	Min.	135.63	-93.15	20	0.00	20	0.00	20	-348.23	20	393.57	20	0.00	20
202	-15	-77	Max	0.00	-93.15	20	0.00	20	0.00	20	-618.90	20	393.60	20	0.00	20
202	-15	-77	Max	135.63	-93.15	20	0.00	20	0.00	20	-742.40	20	-529.55	20	0.00	20
202	-15	-77	Min.	0.00	-93.15	20	0.00	20	0.00	20	-618.90	20	393.60	20	0.00	20
202	-15	-77	Min.	135.63	-93.15	20	0.00	20	0.00	20	-742.40	20	-529.55	20	0.00	20
202	-77	203	Max	0.00	-93.15	20	0.00	20	0.00	20	-1013.08	20	-529.57	20	0.00	20
202	-77	203	Max	51.86	-93.15	20	0.00	20	0.00	20	-1060.30	20	-1067.16	20	0.00	20
202	-77	203	Min.	0.00	-93.15	20	0.00	20	0.00	20	-1013.08	20	-529.57	20	0.00	20
202	-77	203	Min.	51.86	-93.15	20	0.00	20	0.00	20	-1060.30	20	-1067.16	20	0.00	20
202	203	-26	Max	0.00	0.00	20	0.00	20	0.00	20	659.97	20	-861.68	20	0.00	20
202	203	-26	Max	83.77	0.00	20	0.00	20	0.00	20	583.68	20	-340.77	20	0.00	20
202	203	-26	Min.	0.00	0.00	20	0.00	20	0.00	20	659.97	20	-861.68	20	0.00	20
202	203	-26	Min.	83.77	0.00	20	0.00	20	0.00	20	583.68	20	-340.77	20	0.00	20
202	-26	-18	Max	0.00	0.00	20	0.00	20	0.00	20	313.01	20	-340.78	20	0.00	20
202	-26	-18	Max	135.63	0.00	20	0.00	20	0.00	20	189.50	20	-0.00	20	0.00	20
202	-26	-18	Min.	0.00	0.00	20	0.00	20	0.00	20	313.01	20	-340.78	20	0.00	20
202	-26	-18	Min.	135.63	0.00	20	0.00	20	0.00	20	189.50	20	-0.00	20	0.00	20
302	-3	-69	Max	0.00	0.00	20	0.00	20	0.00	20	94.75	20	-82.43	20	0.00	20
302	-3	-69	Max	150.00	0.00	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
302	-3	-69	Min.	0.00	0.00	20	0.00	20	0.00	20	94.75	20	-82.43	20	0.00	20
302	-3	-69	Min.	150.00	0.00	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
302	-68	-3	Max	0.00	0.00	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
302	-68	-3	Max	150.00	-0.00	20	0.00	20	0.00	20	-94.75	20	-82.43	20	0.00	20
302	-68	-3	Min.	0.00	0.00	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
302	-68	-3	Min.	150.00	-0.00	20	0.00	20	0.00	20	-94.75	20	-82.43	20	0.00	20
303	-29	-76	Max	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
303	-29	-76	Max	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
303	-29	-76	Min.	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
303	-29	-76	Min.	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
303	-75	-29	Max	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
303	-75	-29	Max	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
303	-75	-29	Min.	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
303	-75	-29	Min.	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
305	-6	-48	Max	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
305	-6	-48	Max	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
305	-6	-48	Min.	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
305	-6	-48	Min.	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
305	-47	-6	Max	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
305	-47	-6	Max	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
305	-47	-6	Min.	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
305	-47	-6	Min.	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
306	-7	-50	Max	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
306	-7	-50	Max	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
306	-7	-50	Min.	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
306	-7	-50	Min.	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
306	-49	-7	Max	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
306	-49	-7	Max	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
306	-49	-7	Min.	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
306	-49	-7	Min.	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
307	-8	-52	Max	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
307	-8	-52	Max	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
307	-8	-52	Min.	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
307	-8	-52	Min.	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
307	-51	-8	Max	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
307	-51	-8	Max	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
307	-51	-8	Min.	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
307	-51	-8	Min.	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
308	-9	-54	Max	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
308	-9	-54	Max	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
308	-9	-54	Min.	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20



318	-80	201	Min.	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
319	-77	-79	Max	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
319	-77	-79	Max	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
319	-77	-79	Min.	0.00	0.00	20	0.00	20	0.00	20	135.34	20	-124.24	20	0.00	20
319	-77	-79	Min.	150.00	0.00	20	0.00	20	0.00	20	30.31	20	0.00	20	0.00	20
319	-78	-77	Max	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
319	-78	-77	Max	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20
319	-78	-77	Min.	0.00	0.00	20	0.00	20	0.00	20	-30.31	20	0.00	20	0.00	20
319	-78	-77	Min.	150.00	-0.00	20	0.00	20	0.00	20	-135.34	20	-124.24	20	0.00	20

Verifiche aste in acciaio

Simbologia

Φ_{LT}	=	Coefficiente Φ per stabilità laterale membrature inflesse
Φ_y	=	Coefficiente Φ per inflessione intorno all'asse y(c)
Φ_z	=	Coefficiente Φ per inflessione intorno all'asse z(e)
α_{imp}	=	Coefficiente di imperfezione
$\alpha_{my}, \alpha_{mz}, \alpha_{LT}$	=	Coefficienti correttivi per il momento flettente
β_{LT}	=	Coefficiente per calcolo Φ_{LT}
χ_{LT}	=	Coefficiente di riduzione per stabilità laterale membrature inflesse
χ_y	=	Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
χ_z	=	Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
δ	<cm>	= Spostamento relativo asta
λ^*_y	=	Snellezza adimensionale per inflessione intorno all'asse y(c)
λ^*_z	=	Snellezza adimensionale per inflessione intorno all'asse z(e)
λ_{LT}	=	Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$	=	Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
λ_y	=	Snellezza per inflessione intorno all'asse y(c)
λ_z	=	Snellezza per inflessione intorno all'asse z(e)
$\sigma_{TD,max}$	<daN/cm²>	= Tensione ideale massima
σ_M	<daN/cm²>	= Tensione normale per momento flettente
σ_N	<daN/cm²>	= Tensione normale per sforzo normale
τ	<daN/cm²>	= Tensione tangenziale per taglio e/o torsione
ψ	=	Coeff. di correzione momento critico per stabilità laterale membrature inflesse
A_{eff}	<cm²>	= Area effettiva per trazione
A_{net}	<cm²>	= Area netta per compressione
A_{area}	<cm²>	= Area
$A_{tag,y}$	<cm²>	= Area resistente a taglio in dir. Y
$A_{tag,z}$	<cm²>	= Area resistente a taglio in dir. Z
CC	=	Numero della combinazione delle condizioni di carico elementari
$Cod.$	=	Codice
$Curva$	=	Curva di instabilità adottata
D	<cm>	= Distanza
F_{yk}	<daN/cm²>	= Tensione caratteristica di snervamento dell'acciaio
F_{yt}	<daN/cm²>	= Tensione caratteristica di rottura
I_y	<cm⁴>	= Raggio giratorio d'inerzia rispetto all'asse Y
I_z	<cm⁴>	= Raggio giratorio d'inerzia rispetto all'asse Z
J_0	<cm⁶>	= Costante di ingobbamento
J_y	<cm⁴>	= Momento d'inerzia rispetto all'asse Y
J_z	<cm⁴>	= Momento d'inerzia rispetto all'asse Z
$K_{yy}, K_{yz}, K_{zy}, K_{zz}$	=	Coefficienti di interazione
L	<cm>	= Lunghezza dell'asta
L_{cr}	<cm>	= Lunghezza di libera inflessione laterale fra ritegni torsionali
M_{cr}	<daNm>	= Momento critico per instabilità flesso torsionale
$M_{Ny,c,Rd}$	<daNm>	= Resistenza di calcolo a pressoflessione intorno all'asse Y
M_x	<daNm>	= Momento torcente intorno all'asse X
M_y	<daNm>	= Momento flettente intorno all'asse Y
$M_{y,Ed}$	<daNm>	= Momento flettente di calcolo intorno all'asse Y
$M_{y,V,c,Rd}$	<daNm>	= Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y
M_z	<daNm>	= Momento flettente intorno all'asse Z
$M_{z,Ed}$	<daNm>	= Momento flettente di calcolo intorno all'asse Z
N	<daN>	= Sforzo normale
N_{Ed}	<daN>	= Forza assiale di calcolo
$N_{c,Rd}$	<daN>	= Resistenza a compressione
$N_{cr,y}$	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
$N_{cr,z}$	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
$Sez.$	=	Numero della sezione
Tip	=	Tipologia
		Rc = Rettangolare cava
		Is = I stondata
Tp	=	Tipo di acciaio
T_y	<daN>	= Taglio in dir. Y
T_z	<daN>	= Taglio in dir. Z
V_{Ed}	<daN>	= Forza di taglio di calcolo
$V_{c,Rd}$	<daN>	= Resistenza a taglio
$W_{y,plas}$	<cm³>	= Modulo di resistenza plastico intorno all'asse Y
W_{ymin}	<cm³>	= Modulo di resistenza minimo rispetto all'asse Y
$W_{z,plas}$	<cm³>	= Modulo di resistenza plastico intorno all'asse Z
W_{zmin}	<cm³>	= Modulo di resistenza minimo rispetto all'asse Z
$X1$	<cm>	= Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
f	=	Fattore di modifica per il coefficiente di riduzione
$f_{z,G}$	<cm>	= Freccia in direzione Z globale
$f_{z,L}$	<cm>	= Freccia in direzione Z locale
k_c	=	Coeff. di correzione momento flettente per stabilità laterale membrature inflesse

Caratteristiche profilati utilizzati

Sez.	Cod.	Tip	D	Area	A _{net}	A _{eff}	J _y	J _z	I _y	I _z	W _{ymin}	W _{zmin}	Tp	F _{yk}	F _{yt}
			<cm>	<cm²>	<cm²>	<cm²>	<cm⁴>	<cm⁴>	<cm⁴>	<cm⁴>	<cm³>	<cm³>		<daN/cm²>	<daN/cm²>
1	COL HEA280	Is	--	97.27	97.27	97.27	13673.70	4762.65	11.86	7.00	1012.87	340.19	S355 UNI EN 10025-2	3550.00	5100.00
2	TRV PRINC SHS300x300x10	Rc	--	116.00	116.00	116.00	16278.70	16278.70	11.85	11.85	1085.24	1085.24	S355H UNI EN 10210-1	3550.00	5100.00
3	TRV SEC RHS150x100x10	Rc	--	46.00	46.00	46.00	1347.83	695.33	5.41	3.89	179.71	139.07	S355H UNI EN 10210-1	3550.00	5100.00

Caratteristiche profilati utilizzati

Sez.	Cod.	W _{y,plas}	W _{z,plas}	A _{tag,y}	A _{tag,z}	J ₀
		<cm³>	<cm³>	<cm²>	<cm²>	

						<cm6>
1	COL HEA280	1117.45	518.72	81.59	31.75	785367.00
2	TRV PRINC SHS300x300x10	1262.00	1262.00	58.00	58.00	
3	TRV SEC RHS150x100x10	224.50	167.00	18.40	27.60	

Asta n. 1 (315 -45) - Sez. 1 (COL HEA280) - Crit. 1

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2061.78 T_z=-93.70 M_y=-315.69 T_y=-411.99 M_z=691.10
 Tensioni: σ_N=-21.20 σ_{m,d}=-234.32 τ=0.00 σ_{max}=-255.52 (sfrut=0.08)
 Tensioni: σ_N=-21.20 σ_{m,d}=68.80 τ=8.16 τ_{max}=8.16 (sfrut=0.00)
 Tensioni: σ_N=-21.20 σ_{m,d}=-234.32 τ=0.00 σ_{ID,max}=255.52 (sfrut=0.08)
 - Verifica in termini tensionali [4.2.4] - CC 29 SLU Xl=3.29 - Classe 3
 Sollecitazioni: N=-6310.75 T_y=-396.83 M_z=-875.48
 Tensioni: σ_N=-64.88 σ_{m,d}=-257.35 τ=0.00 σ_{max}=-322.23 (sfrut=0.10)
 Tensioni: σ_N=-64.88 σ_{m,d}=51.47 τ=7.84 τ_{max}=7.84 (sfrut=0.00)
 Tensioni: σ_N=-64.88 σ_{m,d}=-257.35 τ=0.00 σ_{ID,max}=322.23 (sfrut=0.10)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-6620.23 My,Ed=-0.00 Mz,Ed=-875.48 L=3.29
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 L_{cr}=3.29 Curva b: α_{imp}=0.34 k_e=0.94 ψ=1.01 M_{cr}=134989.00 λ_{LT}=0.52
 λ_{LT,0}=0.40 Φ_{LT}=0.62 β_{LT}=0.75 f=0.97 χ_{LT}=0.98
 λ_y=27.71 N_{cr,y}=2626240.00 λ_y'=0.36 Curva b: Φ_y=0.59 χ_y=0.94
 λ_z=46.95 N_{cr,z}=914738.00 λ_z'=0.61 Curva c: Φ_z=0.79 χ_z=0.78
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.02+0.07=0.09
 Verifica ZZ: 0.03+0.07=0.10
 - Verifica Spostamento relativo massimo per singola asta - CC 31
 δ=0.02 (L/13466)

Asta n. 2 (2 202) - Sez. 1 (COL HEA280) - Crit. 1

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2569.15 T_z=-124.28 M_y=-392.48 T_y=-401.25 M_z=679.97
 Tensioni: σ_N=-26.41 σ_{m,d}=-238.63 τ=0.00 σ_{max}=-265.04 (sfrut=0.08)
 Tensioni: σ_N=-26.41 σ_{m,d}=74.99 τ=7.96 τ_{max}=7.96 (sfrut=0.00)
 Tensioni: σ_N=-26.41 σ_{m,d}=-238.63 τ=0.00 σ_{ID,max}=265.04 (sfrut=0.08)
 - Verifica a compressione (4.2.4.1.2.2) - CC 29 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-8791.91
 Verifica a compressione [4.2.9]
 N,Ed=-8791.91 N_c,R_d=-328857.00 N,Ed/N_c,R_d=0.03
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3
 Sollecitazioni: N,Ed=-2569.15 My,Ed=-392.48 Mz,Ed=679.97 L=3.29
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 L_{cr}=3.29 Curva b: α_{imp}=0.34 k_e=0.94 ψ=1.79 M_{cr}=240012.00 λ_{LT}=0.39
 λ_{LT,0}=0.40 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
 λ_y=27.71 N_{cr,y}=2626240.00 λ_y'=0.36 Curva b: Φ_y=0.59 χ_y=0.94
 λ_z=46.95 N_{cr,z}=914738.00 λ_z'=0.61 Curva c: Φ_z=0.79 χ_z=0.78
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.01+0.06=0.08
 Verifica ZZ: 0.01+0.01+0.06=0.08

Asta n. 3 (3 203) - Sez. 1 (COL HEA280) - Crit. 1

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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2061.78 T_z=-93.70 M_y=-315.69 T_y=411.99 M_z=-691.10
 Tensioni: σ_N=-21.20 σ_{m,d}=-234.32 τ=0.00 σ_{max}=-255.52 (sfrut=0.08)
 Tensioni: σ_N=-21.20 σ_{m,d}=-12.46 τ=8.16 τ_{max}=8.16 (sfrut=0.00)
 Tensioni: σ_N=-21.20 σ_{m,d}=-234.32 τ=0.00 σ_{ID,max}=255.52 (sfrut=0.08)
 - Verifica in termini tensionali [4.2.4] - CC 29 SLU Xl=3.29 - Classe 3
 Sollecitazioni: N=-6310.75 T_y=396.84 M_z=875.49
 Tensioni: σ_N=-64.88 σ_{m,d}=-257.35 τ=0.00 σ_{max}=-322.23 (sfrut=0.10)
 Tensioni: σ_N=-64.88 σ_{m,d}=-51.47 τ=7.84 τ_{max}=7.84 (sfrut=0.00)
 Tensioni: σ_N=-64.88 σ_{m,d}=-257.35 τ=0.00 σ_{ID,max}=322.23 (sfrut=0.10)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-6620.24 My,Ed=-0.00 Mz,Ed=875.49 L=3.29
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95

$L_{cr}=3.29$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.03$ $M_{cr}=138333.00$ $\lambda_{LT}=0.51$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.62$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=0.98$
 $\lambda_y=27.71$ Ncr, $y=2626240.00$ $\lambda'_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ Ncr, $z=914738.00$ $\lambda'_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.02+0.07=0.09$
 Verifica ZZ: $0.03+0.07=0.10$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.02$ (L/13415)

Asta n. 201 (-3 -29) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=1.36$ - Classe 3
 Sollecitazioni: $N=-12.78$ $T_z=-313.01$ $M_y=340.77$ $T_y=42.59$ $M_z=57.77$
 Tensioni: $\sigma_N=-0.11$ $\sigma_{m,d}=-36.72$ $\tau=0.00$ $\sigma_{max}=-36.83$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.11$ $\sigma_{m,d}=4.97$ $\tau=6.07$ $\tau_{max}=6.07$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.11$ $\sigma_{m,d}=-36.72$ $\tau=0.00$ $\sigma_{ID,max}=36.83$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.36$ - Classe 2
 Sollecitazioni: $T_z=-892.65$
 $V, Ed=-892.65$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.36$ - Classe 2
 Sollecitazioni: $T_z=-892.65$ $M_y=1101.81$
 $M_y, Ed=1101.81$ $M_y, V, c, Rd=42667.60$ $M_y, Ed/M_y, V, c, Rd=0.03$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
 Sollecitazioni: $N, Ed=-12.78$ $M_y, Ed=340.77$ $M_z, Ed=-57.77$ $L=1.36$
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr, $y=18341600.00$ $\lambda'_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr, $z=18341600.00$ $\lambda'_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.01+0.00=0.01$
 Verifica ZZ: $0.00+0.01+0.00=0.01$

Asta n. 201 (-29 -45) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.84$ - Classe 3
 Sollecitazioni: $N=-31.62$ $T_z=-659.97$ $M_y=861.68$ $T_y=105.41$ $M_z=146.07$
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-92.86$ $\tau=0.00$ $\sigma_{max}=-93.13$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=12.56$ $\tau=12.79$ $\tau_{max}=12.79$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-92.86$ $\tau=0.00$ $\sigma_{ID,max}=93.13$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.84$ - Classe 2
 Sollecitazioni: $T_z=-2315.19$
 $V, Ed=-2315.19$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.02$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=0.84$ - Classe 2
 Sollecitazioni: $T_z=-2315.19$ $M_y=2999.73$
 $M_y, Ed=2999.73$ $M_y, V, c, Rd=42667.60$ $M_y, Ed/M_y, V, c, Rd=0.07$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N, Ed=-31.62$ $M_y, Ed=861.68$ $M_z, Ed=146.07$ $L=0.84$
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=7.07$ Ncr, $y=48078400.00$ $\lambda'_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.07$ Ncr, $z=48078400.00$ $\lambda'_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.03$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 201 (-45 201) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 5 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-275.94$ $T_z=1163.75$ $M_y=1523.98$ $T_y=-52.88$ $M_z=43.86$ $M_x=-7.90$
 Tensioni: $\sigma_N=-2.38$ $\sigma_{m,d}=-144.47$ $\tau=0.47$ $\sigma_{max}=-146.85$ (sfrut=0.04)
 Tensioni: $\sigma_N=-2.38$ $\sigma_{m,d}=-3.77$ $\tau=23.02$ $\tau_{max}=23.02$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.38$ $\sigma_{m,d}=-144.47$ $\tau=0.47$ $\sigma_{ID,max}=146.85$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=3995.56$
 $V, Ed=3995.56$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.04$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $N=-396.83$ $T_z=3995.56$ $M_y=3875.20$

My,Ed=3875.20 My,V,c,Rd=42667.60
 N,Ed=-396.83 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-396.83 My,Ed=3875.20 Mz,Ed=-0.00 L=0.52
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.38$ Ncr,y=125463000.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=4.38$ Ncr,z=125463000.00 $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.10=0.10
 Verifica ZZ: 0.00+0.08=0.08

Asta n. 201 (201 -6) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-215.58 Tz=845.85 My=932.72 Ty=-34.77 Mz=16.44 Mx=-7.90
 Tensioni: $\sigma_N=-1.86 \sigma_{m,d}=-87.46 \tau=0.47 \sigma_{max}=-89.32$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.86 \sigma_{m,d}=-1.41 \tau=16.86 \tau_{max}=16.86$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.86 \sigma_{m,d}=-87.46 \tau=0.47 \sigma_{ID,max}=89.32$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=2610.80
 V,Ed=2610.80 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.02
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: N=-396.83 Tz=2610.80 My=1819.10
 My,Ed=1819.10 My,V,c,Rd=42667.60
 N,Ed=-396.83 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.04

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-396.83 My,Ed=1819.10 Mz,Ed=0.00 L=1.36
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341600.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341600.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00+0.04=0.04

Asta n. 201 (-6 -7) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.36 - Classe 3
 Sollecitazioni: N=-76.47 Tz=193.68 My=-818.88 Ty=-49.09 Mz=-168.99 Mx=-26.33
 Tensioni: $\sigma_N=-0.66 \sigma_{m,d}=-91.03 \tau=1.57 \sigma_{max}=-91.69$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.66 \sigma_{m,d}=14.53 \tau=5.32 \tau_{max}=5.32$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.66 \sigma_{m,d}=-91.03 \tau=1.57 \sigma_{ID,max}=91.73$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=1126.88
 V,Ed=1126.88 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.36 - Classe 2
 Sollecitazioni: N=-396.83 Tz=966.32 My=-3032.59
 My,Ed=-3032.59 My,V,c,Rd=42667.60
 N,Ed=-396.83 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.07

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-396.83 My,Ed=-3032.59 Mz,Ed=0.00 L=1.36
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341600.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341600.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.08=0.08
 Verifica ZZ: 0.00+0.06=0.06

Asta n. 201 (-7 -8) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-96.52 Tz=-76.99 My=-818.87 Ty=17.73 Mz=-168.98 Mx=-26.33
 Tensioni: $\sigma_N=-0.83 \sigma_{m,d}=-91.03 \tau=1.57 \sigma_{max}=-91.86$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.83 \sigma_{m,d}=-14.53 \tau=3.06 \tau_{max}=3.06$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.83 \sigma_{m,d}=-91.03 \tau=1.57 \sigma_{ID,max}=91.90$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.36 - Classe 2
 Sollecitazioni: Tz=-517.59
 V,Ed=-517.59 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-396.83 T_z=-357.03 M_y=-3032.50
M_y,Ed=-3032.50 M_y,V,c,Rd=42667.60
N,Ed=-396.83 N_c,Rd=-392190.00 YY n=N,Ed/N_c,Rd=0.00 M_{Ny},c,Rd=42667.60 M_y,Ed/M_{Ny},c,Rd=0.07

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-396.83 M_y,Ed=-3032.50 M_z,Ed=0.00 L=1.36
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=11.45 N_{cr,y}=18341600.00 λ_y^{*}=0.15 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=11.45 N_{cr,z}=18341600.00 λ_z^{*}=0.15 Curva a: Φ_z=0.00 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00+0.06=0.06

Asta n. 201 (-8 -9) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-69.74 T_z=-409.10 M_y=-641.35 T_y=84.55 M_z=-144.93 M_x=-26.33
Tensioni: σ_N=-0.60 σ_{m,d}=-72.45 τ=1.57 σ_{max}=-73.05 (sfrut=0.02)
Tensioni: σ_N=-0.60 σ_{m,d}=-12.46 τ=9.49 τ_{max}=9.49 (sfrut=0.00)
Tensioni: σ_N=-0.60 σ_{m,d}=-72.45 τ=1.57 σ_{ID,max}=73.10 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.36 - Classe 2
Sollecitazioni: T_z=-2001.51
V,Ed=-2001.51 V_c,Rd=113219.00 V,Ed/V_c,Rd=0.02

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-396.83 T_z=-1840.96 M_y=-2439.38
M_y,Ed=-2439.38 M_y,V,c,Rd=42667.60
N,Ed=-396.83 N_c,Rd=-392190.00 YY n=N,Ed/N_c,Rd=0.00 M_{Ny},c,Rd=42667.60 M_y,Ed/M_{Ny},c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-396.83 M_y,Ed=-2439.38 M_z,Ed=0.00 L=1.36
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=11.45 N_{cr,y}=18341500.00 λ_y^{*}=0.15 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=11.45 N_{cr,z}=18341500.00 λ_z^{*}=0.15 Curva a: Φ_z=0.00 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00+0.05=0.05

Asta n. 201 (-9 -10) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.36 - Classe 3
Sollecitazioni: N=-238.01 T_z=-1061.27 M_y=1558.40 T_y=45.41 M_z=52.51 M_x=-7.90
Tensioni: σ_N=-2.05 σ_{m,d}=-148.44 τ=0.47 σ_{max}=-150.49 (sfrut=0.04)
Tensioni: σ_N=-2.05 σ_{m,d}=4.52 τ=21.04 τ_{max}=21.04 (sfrut=0.01)
Tensioni: σ_N=-2.05 σ_{m,d}=-148.44 τ=0.47 σ_{ID,max}=150.49 (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.36 - Classe 2
Sollecitazioni: T_z=-3485.43
V,Ed=-3485.43 V_c,Rd=113219.00 V,Ed/V_c,Rd=0.03

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.36 - Classe 2
Sollecitazioni: N=-396.83 T_z=-3485.43 M_y=4784.75
M_y,Ed=4784.75 M_y,V,c,Rd=42667.60
N,Ed=-396.83 N_c,Rd=-392190.00 YY n=N,Ed/N_c,Rd=0.00 M_{Ny},c,Rd=42667.60 M_y,Ed/M_{Ny},c,Rd=0.11

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-396.83 M_y,Ed=4784.75 M_z,Ed=0.00 L=1.36
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=11.45 N_{cr,y}=18341600.00 λ_y^{*}=0.15 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=11.45 N_{cr,z}=18341600.00 λ_z^{*}=0.15 Curva a: Φ_z=0.00 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.12=0.12
Verifica ZZ: 0.00+0.10=0.10

Asta n. 201 (-10 202) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.20 - Classe 3
Sollecitazioni: N=-282.14 T_z=-1268.99 M_y=1810.39 T_y=58.65 M_z=64.25 M_x=-7.90
Tensioni: σ_N=-2.43 σ_{m,d}=-172.74 τ=0.47 σ_{max}=-175.17 (sfrut=0.05)
Tensioni: σ_N=-2.43 σ_{m,d}=5.53 τ=25.06 τ_{max}=25.06 (sfrut=0.01)
Tensioni: σ_N=-2.43 σ_{m,d}=-172.74 τ=0.47 σ_{ID,max}=175.17 (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.20 - Classe 2
Sollecitazioni: T_z=-4241.21

V,Ed=-4241.21 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.04

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.20 - Classe 2
Sollecitazioni: N=-396.83 Tz=-4241.21 My=5630.70
My,Ed=5630.70 My,V,c,Rd=42667.60
N,Ed=-396.83 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.13

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-396.83 My,Ed=5630.70 Mz,Ed=0.00 L=0.20
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=1.69$ Ncr,y=843464000.00 $\lambda^*_y=0.02$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=1.69$ Ncr,z=843463000.00 $\lambda^*_z=0.02$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.15=0.15
Verifica ZZ: 0.00+0.12=0.12

Asta n. 202 (202 -11) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-282.14 Tz=1268.99 My=1810.39 Ty=-58.65 Mz=64.25 Mx=7.90
Tensioni: $\sigma_N=-2.43 \sigma_{m,d}=-172.74 \tau=0.47 \sigma_{max}=-175.17$ (sfrut=0.05)
Tensioni: $\sigma_N=-2.43 \sigma_{m,d}=5.53 \tau=25.06 \tau_{max}=25.06$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.43 \sigma_{m,d}=-172.74 \tau=0.47 \sigma_{ID,max}=175.17$ (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: Tz=4241.21
V,Ed=4241.21 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.04

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-396.84 Tz=4241.21 My=5630.69
My,Ed=5630.69 My,V,c,Rd=42667.60
N,Ed=-396.84 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.13

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-396.84 My,Ed=5630.69 Mz,Ed=0.00 L=0.20
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=1.69$ Ncr,y=843464000.00 $\lambda^*_y=0.02$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=1.69$ Ncr,z=843463000.00 $\lambda^*_z=0.02$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.15=0.15
Verifica ZZ: 0.00+0.12=0.12

Asta n. 202 (-11 -12) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-238.01 Tz=1061.27 My=1558.41 Ty=-45.41 Mz=52.51 Mx=7.90
Tensioni: $\sigma_N=-2.05 \sigma_{m,d}=-148.44 \tau=0.47 \sigma_{max}=-150.49$ (sfrut=0.04)
Tensioni: $\sigma_N=-2.05 \sigma_{m,d}=4.52 \tau=21.04 \tau_{max}=21.04$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.05 \sigma_{m,d}=-148.44 \tau=0.47 \sigma_{ID,max}=150.49$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: Tz=3485.44
V,Ed=3485.44 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.03

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-396.84 Tz=3485.44 My=4784.81
My,Ed=4784.81 My,V,c,Rd=42667.60
N,Ed=-396.84 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.11

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-396.84 My,Ed=4784.81 Mz,Ed=0.00 L=1.36
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341500.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00 \chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341500.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00 \chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.12=0.12
Verifica ZZ: 0.00+0.10=0.10

Asta n. 202 (-12 -13) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.36 - Classe 3
Sollecitazioni: N=-69.74 Tz=409.11 My=-641.35 Ty=-84.55 Mz=-144.93 Mx=26.33
Tensioni: $\sigma_N=-0.60 \sigma_{m,d}=-72.45 \tau=1.57 \sigma_{max}=-73.05$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.60 \sigma_{m,d}=-12.46 \tau=9.49 \tau_{max}=9.49$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.60 \sigma_{m,d}=-72.45 \tau=1.57 \sigma_{ID,max}=73.10$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $T_z=2001.52$
 $V, Ed=2001.52$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.02$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.36 - Classe 2
Sollecitazioni: $N=-396.84$ $T_z=1840.96$ $M_y=-2439.36$
 $M_y, Ed=-2439.36$ $M_y, V, c, Rd=42667.60$
 $N, Ed=-396.84$ $N_c, Rd=-392190.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MN_y, c, Rd=42667.60$ $M_y, Ed/MN_y, c, Rd=0.06$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N, Ed=-396.84$ $M_y, Ed=-2439.36$ $M_z, Ed=0.00$ $L=1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ $N_{cr,y}=18341500.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ $N_{cr,z}=18341500.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.06=0.06$
Verifica ZZ: $0.00+0.05=0.05$

Asta n. 202 (-13 -14) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=1.36 - Classe 3
Sollecitazioni: $N=-96.52$ $T_z=76.99$ $M_y=-818.87$ $T_y=-17.73$ $M_z=-168.98$ $M_x=26.33$
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=-91.03$ $\tau=1.57$ $\sigma_{max}=-91.86$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=-14.53$ $\tau=3.06$ $\tau_{max}=3.06$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=-91.03$ $\tau=1.57$ $\sigma_{ID,max}=91.90$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $T_z=517.59$
 $V, Ed=517.59$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.36 - Classe 2
Sollecitazioni: $N=-396.84$ $T_z=357.04$ $M_y=-3032.51$
 $M_y, Ed=-3032.51$ $M_y, V, c, Rd=42667.60$
 $N, Ed=-396.84$ $N_c, Rd=-392190.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MN_y, c, Rd=42667.60$ $M_y, Ed/MN_y, c, Rd=0.07$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N, Ed=-396.84$ $M_y, Ed=-3032.51$ $M_z, Ed=0.00$ $L=1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ $N_{cr,y}=18341500.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ $N_{cr,z}=18341500.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.08=0.08$
Verifica ZZ: $0.00+0.06=0.06$

Asta n. 202 (-14 -15) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=-76.47$ $T_z=-193.69$ $M_y=-818.87$ $T_y=49.09$ $M_z=-168.98$ $M_x=26.33$
Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=-91.03$ $\tau=1.57$ $\sigma_{max}=-91.68$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=14.53$ $\tau=5.32$ $\tau_{max}=5.32$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=-91.03$ $\tau=1.57$ $\sigma_{ID,max}=91.72$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.36 - Classe 2
Sollecitazioni: $T_z=-1126.89$
 $V, Ed=-1126.89$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $N=-396.84$ $T_z=-966.33$ $M_y=-3032.51$
 $M_y, Ed=-3032.51$ $M_y, V, c, Rd=42667.60$
 $N, Ed=-396.84$ $N_c, Rd=-392190.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MN_y, c, Rd=42667.60$ $M_y, Ed/MN_y, c, Rd=0.07$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N, Ed=-396.84$ $M_y, Ed=-3032.51$ $M_z, Ed=0.00$ $L=1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ $N_{cr,y}=18341500.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ $N_{cr,z}=18341500.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.08=0.08$
Verifica ZZ: $0.00+0.06=0.06$

Asta n. 202 (-15 -77) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.36 - Classe 3
Sollecitazioni: $N=-215.58$ $T_z=-845.85$ $M_y=932.69$ $T_y=34.77$ $M_z=16.44$ $M_x=7.90$
Tensioni: $\sigma_N=-1.86$ $\sigma_{m,d}=-87.46$ $\tau=0.47$ $\sigma_{max}=-89.32$ (sfrut=0.03)
Tensioni: $\sigma_N=-1.86$ $\sigma_{m,d}=-1.41$ $\tau=16.86$ $\tau_{max}=16.86$ (sfrut=0.01)

Tensioni: $\sigma_N = -1.86$ $\sigma_{m,d} = -87.46$ $\tau = 0.47$ $\sigma_{ID,max} = 89.32$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 1.36$ - Classe 2
 Sollecitazioni: $T_z = -2610.80$
 $V, Ed = -2610.80$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.02$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l = 1.36$ - Classe 2
 Sollecitazioni: $N = -396.84$ $T_z = -2610.80$ $M_y = 1818.99$
 $M_y, Ed = 1818.99$ $M_y, V, c, Rd = 42667.60$
 $N, Ed = -396.84$ $N_c, Rd = -392190.00$ YY $n = N, Ed/N_c, Rd = 0.00$ $MN_y, c, Rd = 42667.60$ $M_y, Ed/MN_y, c, Rd = 0.04$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $N, Ed = -396.84$ $M_y, Ed = 1818.99$ $M_z, Ed = 0.00$ $L = 1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 11.45$ $N_{cr,y} = 18341500.00$ $\lambda^*_y = 0.15$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 11.45$ $N_{cr,z} = 18341500.00$ $\lambda^*_z = 0.15$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.05 = 0.05$
 Verifica ZZ: $0.00 + 0.04 = 0.04$

Asta n. 202 (-77 203) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.52$ - Classe 3
 Sollecitazioni: $N = -275.94$ $T_z = -1163.75$ $M_y = 1523.95$ $T_y = 52.88$ $M_z = 43.86$ $M_x = 7.90$
 Tensioni: $\sigma_N = -2.38$ $\sigma_{m,d} = -144.47$ $\tau = 0.47$ $\sigma_{max} = -146.84$ (sfrut=0.04)
 Tensioni: $\sigma_N = -2.38$ $\sigma_{m,d} = -3.77$ $\tau = 23.02$ $\tau_{max} = 23.02$ (sfrut=0.01)
 Tensioni: $\sigma_N = -2.38$ $\sigma_{m,d} = -144.47$ $\tau = 0.47$ $\sigma_{ID,max} = 146.85$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.52$ - Classe 2
 Sollecitazioni: $T_z = -3995.55$
 $V, Ed = -3995.55$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.04$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l = 0.52$ - Classe 2
 Sollecitazioni: $N = -396.84$ $T_z = -3995.55$ $M_y = 3875.10$
 $M_y, Ed = 3875.10$ $M_y, V, c, Rd = 42667.60$
 $N, Ed = -396.84$ $N_c, Rd = -392190.00$ YY $n = N, Ed/N_c, Rd = 0.00$ $MN_y, c, Rd = 42667.60$ $M_y, Ed/MN_y, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $N, Ed = -396.84$ $M_y, Ed = 3875.10$ $M_z, Ed = -0.00$ $L = 0.52$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.38$ $N_{cr,y} = 125464000.00$ $\lambda^*_y = 0.06$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 4.38$ $N_{cr,z} = 125464000.00$ $\lambda^*_z = 0.06$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.10 = 0.10$
 Verifica ZZ: $0.00 + 0.08 = 0.08$

Asta n. 202 (203 -26) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = 31.62$ $T_z = 659.97$ $M_y = 861.68$ $T_y = -105.41$ $M_z = 146.07$
 Tensioni: $\sigma_N = 0.27$ $\sigma_{m,d} = 92.86$ $\tau = 0.00$ $\sigma_{max} = 93.13$ (sfrut=0.03)
 Tensioni: $\sigma_N = 0.27$ $\sigma_{m,d} = 12.56$ $\tau = 12.79$ $\tau_{max} = 12.79$ (sfrut=0.01)
 Tensioni: $\sigma_N = 0.27$ $\sigma_{m,d} = 92.86$ $\tau = 0.00$ $\sigma_{ID,max} = 93.13$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 2
 Sollecitazioni: $T_z = 2315.19$
 $V, Ed = 2315.19$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.02$

- Verifica a flessione e taglio YY [4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 2
 Sollecitazioni: $T_z = 2315.19$ $M_y = 2999.73$
 $M_y, Ed = 2999.73$ $M_y, V, c, Rd = 42667.60$ $M_y, Ed/M_y, V, c, Rd = 0.07$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
 Sollecitazioni: $N, Ed = -31.62$ $M_y, Ed = 861.68$ $M_z, Ed = 146.07$ $L = 0.84$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 7.07$ $N_{cr,y} = 48078100.00$ $\lambda^*_y = 0.09$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 7.07$ $N_{cr,z} = 48078100.00$ $\lambda^*_z = 0.09$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.03$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 202 (-26 -18) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = 12.78$ $T_z = 313.01$ $M_y = 340.78$ $T_y = -42.59$ $M_z = 57.77$
 Tensioni: $\sigma_N = 0.11$ $\sigma_{m,d} = 36.72$ $\tau = 0.00$ $\sigma_{max} = 36.83$ (sfrut=0.01)

Tensioni: $\sigma_N=0.11$ $\sigma_{m,d}=4.97$ $\tau=6.07$ $\tau_{max}=6.07$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.11$ $\sigma_{m,d}=36.72$ $\tau=0.00$ $\sigma_{ID,max}=36.83$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=892.66$
 $V,Ed=892.66$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=892.66$ $M_y=1101.83$
 $M_y,Ed=1101.83$ $M_y,V,c,Rd=42667.60$ $M_y,Ed/M_y,V,c,Rd=0.03$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 15 SND - Classe 3
 Sollecitazioni: $N,Ed=-12.78$ $M_y,Ed=340.78$ $M_z,Ed=-57.77$ $L=1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ $N_{cr,y}=18341500.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ $N_{cr,z}=18341500.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.01+0.00=0.01$
 Verifica ZZ: $0.00+0.01+0.00=0.01$

Asta n. 302 (-3 -69) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-2.79$ $T_z=94.75$ $M_y=82.43$ $T_y=-9.32$ $M_z=13.97$
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.92$ $\tau=0.00$ $\sigma_{max}=-55.98$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=8.04$ $\tau=3.95$ $\tau_{max}=3.95$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.92$ $\tau=0.00$ $\sigma_{ID,max}=55.98$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=366.05$
 $V,Ed=366.05$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=366.05$ $M_y=357.34$
 $M_y,Ed=357.34$ $M_y,V,c,Rd=7590.24$ $M_y,Ed/M_y,V,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-2.79$ $M_y,Ed=82.43$ $M_z,Ed=13.97$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.01+0.00=0.02$
 Verifica ZZ: $0.00+0.01+0.00=0.01$

Asta n. 302 (-68 -3) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=2.79$ $T_z=-94.75$ $M_y=82.43$ $T_y=9.32$ $M_z=13.97$
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.92$ $\tau=0.00$ $\sigma_{max}=55.98$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=8.04$ $\tau=3.95$ $\tau_{max}=3.95$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.92$ $\tau=0.00$ $\sigma_{ID,max}=55.98$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-366.05$
 $V,Ed=-366.05$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-366.05$ $M_y=357.34$
 $M_y,Ed=357.34$ $M_y,V,c,Rd=7590.24$ $M_y,Ed/M_y,V,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=-0.00$ $M_y,Ed=357.34$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.04=0.04$
 Verifica ZZ: $0.00=0.00$

Asta n. 303 (-29 -76) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-4.21$ $T_z=135.34$ $M_y=124.24$ $T_y=-14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{max}=-84.37$ (sfrut=0.02)

Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$
 $V, Ed = 661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$ $M_y = 661.86$
 $M_y, Ed = 661.86$ $M_y, V, c, Rd = 7590.24$ $M_y, Ed/M_y, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -4.21$ $M_y, Ed = 124.24$ $M_z, Ed = 21.06$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 303 (-75 -29) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 4.21$ $T_z = -135.34$ $M_y = 124.24$ $T_y = 14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{max} = 84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -661.68$
 $V, Ed = -661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -661.68$ $M_y = 661.86$
 $M_y, Ed = 661.86$ $M_y, V, c, Rd = 7590.24$ $M_y, Ed/M_y, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N, Ed = -0.00$ $M_y, Ed = 661.86$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640514.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00 + 0.08 = 0.08$
 Verifica ZZ: $0.00 = 0.00$

Asta n. 305 (-6 -48) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -4.21$ $T_z = 135.34$ $M_y = 124.24$ $T_y = -14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{max} = -84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$
 $V, Ed = 661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$ $M_y = 661.86$
 $M_y, Ed = 661.86$ $M_y, V, c, Rd = 7590.24$ $M_y, Ed/M_y, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -4.21$ $M_y, Ed = 124.24$ $M_z, Ed = 21.06$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 305 (-47 -6) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 4.21$ $T_z = -135.34$ $M_y = 124.24$ $T_y = 14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{max} = 84.37$ (sfrut=0.02)

Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Asta n. 306 (-7 -50) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-4.21$ $T_z=135.34$ $M_y=124.24$ $T_y=-14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{max}=-84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=661.68$
 $V,Ed=661.68$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-4.21$ $My,Ed=124.24$ $M_z,Ed=21.06$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 306 (-49 -7) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=4.21$ $T_z=-135.34$ $M_y=124.24$ $T_y=14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{max}=84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Asta n. 307 (-8 -52) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-4.21$ $T_z=135.34$ $M_y=124.24$ $T_y=-14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{max}=-84.37$ (sfrut=0.02)

Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$
 $V, Ed = 661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$ $M_y = 661.86$
 $My, Ed = 661.86$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -4.21$ $My, Ed = 124.24$ $Mz, Ed = 21.06$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 307 (-51 -8) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 4.21$ $T_z = -135.34$ $M_y = 124.24$ $T_y = 14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{max} = 84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -661.68$
 $V, Ed = -661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -661.68$ $M_y = 661.86$
 $My, Ed = 661.86$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N, Ed = -0.00$ $My, Ed = 661.86$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640514.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00 + 0.08 = 0.08$
 Verifica ZZ: $0.00 = 0.00$

Asta n. 308 (-9 -54) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -4.21$ $T_z = 135.34$ $M_y = 124.24$ $T_y = -14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{max} = -84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$
 $V, Ed = 661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$ $M_y = 661.86$
 $My, Ed = 661.86$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -4.21$ $My, Ed = 124.24$ $Mz, Ed = 21.06$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 308 (-53 -9) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 4.21$ $T_z = -135.34$ $M_y = 124.24$ $T_y = 14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{max} = 84.37$ (sfrut=0.02)

Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Asta n. 309 (-10 -56) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-2.79$ $T_z=94.75$ $M_y=82.43$ $T_y=-9.32$ $M_z=13.97$
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.92$ $\tau=0.00$ $\sigma_{max}=-55.98$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=8.04$ $\tau=3.95$ $\tau_{max}=3.95$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.92$ $\tau=0.00$ $\sigma_{ID,max}=55.98$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=366.05$
 $V,Ed=366.05$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=366.05$ $M_y=357.34$
 $My,Ed=357.34$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-2.79$ $My,Ed=82.43$ $M_z,Ed=13.97$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.01+0.00=0.02$
 Verifica ZZ: $0.00+0.01+0.00=0.01$

Asta n. 309 (-55 -10) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 3 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=-2.79$ $T_z=-94.75$ $M_y=82.43$ $T_y=9.32$ $M_z=13.97$
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.92$ $\tau=0.00$ $\sigma_{max}=-55.98$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=8.04$ $\tau=3.95$ $\tau_{max}=3.95$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.92$ $\tau=0.00$ $\sigma_{ID,max}=55.98$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-366.05$
 $V,Ed=-366.05$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-366.05$ $M_y=357.34$
 $My,Ed=357.34$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=357.34$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.04=0.04$
 Verifica ZZ: $0.00=0.00$

Asta n. 310 (-11 -58) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-2.79$ $T_z=94.75$ $M_y=82.43$ $T_y=-9.32$ $M_z=13.97$
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.92$ $\tau=0.00$ $\sigma_{max}=-55.98$ (sfrut=0.02)

Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = 8.04$ $\tau = 3.95$ $\tau_{max} = 3.95$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = -55.92$ $\tau = 0.00$ $\sigma_{ID,max} = 55.98$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 366.05$
 $V, Ed = 366.05$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 366.05$ $M_y = 357.34$
 $M_y, Ed = 357.34$ $M_y, V, c, Rd = 7590.24$ $M_y, Ed/M_y, V, c, Rd = 0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -2.79$ $M_y, Ed = 82.43$ $M_z, Ed = 13.97$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.01 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.01 + 0.00 = 0.01$

Asta n. 310 (-57 -11) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 2.79$ $T_z = -94.75$ $M_y = 82.43$ $T_y = 9.32$ $M_z = 13.97$
 Tensioni: $\sigma_N = 0.06$ $\sigma_{m,d} = 55.92$ $\tau = 0.00$ $\sigma_{max} = 55.98$ (sfrut=0.02)
 Tensioni: $\sigma_N = 0.06$ $\sigma_{m,d} = 8.04$ $\tau = 3.95$ $\tau_{max} = 3.95$ (sfrut=0.00)
 Tensioni: $\sigma_N = 0.06$ $\sigma_{m,d} = 55.92$ $\tau = 0.00$ $\sigma_{ID,max} = 55.98$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -366.05$
 $V, Ed = -366.05$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -366.05$ $M_y = 357.34$
 $M_y, Ed = 357.34$ $M_y, V, c, Rd = 7590.24$ $M_y, Ed/M_y, V, c, Rd = 0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N, Ed = -0.00$ $M_y, Ed = 357.34$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640514.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00 + 0.04 = 0.04$
 Verifica ZZ: $0.00 = 0.00$

Asta n. 311 (-12 -60) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -4.21$ $T_z = 135.34$ $M_y = 124.24$ $T_y = -14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{max} = -84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$
 $V, Ed = 661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$ $M_y = 661.86$
 $M_y, Ed = 661.86$ $M_y, V, c, Rd = 7590.24$ $M_y, Ed/M_y, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -4.21$ $M_y, Ed = 124.24$ $M_z, Ed = 21.06$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $N_{cr,y} = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $N_{cr,z} = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 311 (-59 -12) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 4.21$ $T_z = -135.34$ $M_y = 124.24$ $T_y = 14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{max} = 84.37$ (sfrut=0.02)

Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $Xl=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Asta n. 312 (-13 -62) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.00$ - Classe 3
 Sollecitazioni: $N=-4.21$ $T_z=135.34$ $M_y=124.24$ $T_y=-14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{max}=-84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=0.00$ - Classe 1
 Sollecitazioni: $T_z=661.68$
 $V,Ed=661.68$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $Xl=0.00$ - Classe 1
 Sollecitazioni: $T_z=661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-4.21$ $My,Ed=124.24$ $Mz,Ed=21.06$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 312 (-61 -13) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=1.50$ - Classe 3
 Sollecitazioni: $N=4.21$ $T_z=-135.34$ $M_y=124.24$ $T_y=14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{max}=84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $Xl=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Asta n. 313 (-14 -64) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.00$ - Classe 3
 Sollecitazioni: $N=-4.21$ $T_z=135.34$ $M_y=124.24$ $T_y=-14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{max}=-84.37$ (sfrut=0.02)

Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$
 $V, Ed = 661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$ $M_y = 661.86$
 $My, Ed = 661.86$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -4.21$ $My, Ed = 124.24$ $Mz, Ed = 21.06$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $Ncr, y = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $Ncr, z = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 313 (-63 -14) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 4.21$ $T_z = -135.34$ $M_y = 124.24$ $T_y = 14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{max} = 84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -661.68$
 $V, Ed = -661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -661.68$ $M_y = 661.86$
 $My, Ed = 661.86$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N, Ed = -0.00$ $My, Ed = 661.86$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $Ncr, y = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $Ncr, z = 640514.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00 + 0.08 = 0.08$
 Verifica ZZ: $0.00 = 0.00$

Asta n. 314 (-15 -66) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -4.21$ $T_z = 135.34$ $M_y = 124.24$ $T_y = -14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{max} = -84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$
 $V, Ed = 661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$ $M_y = 661.86$
 $My, Ed = 661.86$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -4.21$ $My, Ed = 124.24$ $Mz, Ed = 21.06$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $Ncr, y = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $Ncr, z = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 314 (-65 -15) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 4.21$ $T_z = -135.34$ $M_y = 124.24$ $T_y = 14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{max} = 84.37$ (sfrut=0.02)

Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Asta n. 316 (-26 -74) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-4.21$ $T_z=135.34$ $M_y=124.24$ $T_y=-14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{max}=-84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=661.68$
 $V,Ed=661.68$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-4.21$ $My,Ed=124.24$ $M_z,Ed=21.06$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 316 (-73 -26) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=4.21$ $T_z=-135.34$ $M_y=124.24$ $T_y=14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{max}=84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Asta n. 317 (-18 -71) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-2.79$ $T_z=94.75$ $M_y=82.43$ $T_y=-9.32$ $M_z=13.97$
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.92$ $\tau=0.00$ $\sigma_{max}=-55.98$ (sfrut=0.02)

Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = 8.04$ $\tau = 3.95$ $\tau_{max} = 3.95$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = -55.92$ $\tau = 0.00$ $\sigma_{ID,max} = 55.98$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 366.05$
 $V, Ed = 366.05$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 366.05$ $M_y = 357.34$
 $My, Ed = 357.34$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -2.79$ $My, Ed = 82.43$ $Mz, Ed = 13.97$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $Ncr, y = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $Ncr, z = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.01 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.01 + 0.00 = 0.01$

Asta n. 317 (-70 -18) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 3 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = -2.79$ $T_z = -94.75$ $M_y = 82.43$ $T_y = 9.32$ $M_z = 13.97$
 Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = -55.92$ $\tau = 0.00$ $\sigma_{max} = -55.98$ (sfrut=0.02)
 Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = 8.04$ $\tau = 3.95$ $\tau_{max} = 3.95$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = -55.92$ $\tau = 0.00$ $\sigma_{ID,max} = 55.98$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -366.05$
 $V, Ed = -366.05$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -366.05$ $M_y = 357.34$
 $My, Ed = 357.34$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N, Ed = -0.00$ $My, Ed = 357.34$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $Ncr, y = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $Ncr, z = 640514.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00 + 0.04 = 0.04$
 Verifica ZZ: $0.00 = 0.00$

Asta n. 318 (201 -81) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -4.21$ $T_z = 135.34$ $M_y = 124.24$ $T_y = -14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{max} = -84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = 12.12$ $\tau = 5.64$ $\tau_{max} = 5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.09$ $\sigma_{m,d} = -84.28$ $\tau = 0.00$ $\sigma_{ID,max} = 84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$
 $V, Ed = 661.68$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 661.68$ $M_y = 661.86$
 $My, Ed = 661.86$ $My, V, c, Rd = 7590.24$ $My, Ed/My, V, c, Rd = 0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed = -4.21$ $My, Ed = 124.24$ $Mz, Ed = 21.06$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.71$ $Ncr, y = 1241570.00$ $\lambda^*_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 38.58$ $Ncr, z = 640515.00$ $\lambda^*_z = 0.50$ Curva a: $\Phi_z = 0.66$ $\chi_z = 0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.00 = 0.02$
 Verifica ZZ: $0.00 + 0.02 + 0.00 = 0.02$

Asta n. 318 (-80 201) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l = 1.50$ - Classe 3
 Sollecitazioni: $N = 4.21$ $T_z = -135.34$ $M_y = 124.24$ $T_y = 14.04$ $M_z = 21.06$
 Tensioni: $\sigma_N = 0.09$ $\sigma_{m,d} = 84.28$ $\tau = 0.00$ $\sigma_{max} = 84.37$ (sfrut=0.02)

Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $Xl=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Asta n. 319 (-77 -79) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=0.00$ - Classe 3
 Sollecitazioni: $N=-4.21$ $T_z=135.34$ $M_y=124.24$ $T_y=-14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{max}=-84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=0.00$ - Classe 1
 Sollecitazioni: $T_z=661.68$
 $V,Ed=661.68$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $Xl=0.00$ - Classe 1
 Sollecitazioni: $T_z=661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-4.21$ $My,Ed=124.24$ $M_z,Ed=21.06$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 319 (-78 -77) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=1.50$ - Classe 3
 Sollecitazioni: $N=4.21$ $T_z=-135.34$ $M_y=124.24$ $T_y=14.04$ $M_z=21.06$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{max}=84.37$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.12$ $\tau=5.64$ $\tau_{max}=5.64$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=84.28$ $\tau=0.00$ $\sigma_{ID,max}=84.37$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$
 $V,Ed=-661.68$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $Xl=1.50$ - Classe 1
 Sollecitazioni: $T_z=-661.68$ $M_y=661.86$
 $My,Ed=661.86$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: $N,Ed=0.00$ $My,Ed=661.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.08=0.08$
 Verifica ZZ: $0.00=0.00$

Membratura

Asta 201 Nodi -3 -29 -45 201 -6 -7 -8 -9 -10 202 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $N,Ed=-396.83$ $My,Ed=5630.70$ $M_z,Ed=0.00$ $L=9.69$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=81.83$ Ncr, $y=359032.00$ $\lambda'_y=1.07$ Curva a: $\Phi_y=1.16$ $\chi_y=0.62$
 $\lambda_z=81.83$ Ncr, $z=359031.00$ $\lambda'_z=1.07$ Curva a: $\Phi_z=1.16$ $\chi_z=0.62$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.15=0.15
 Verifica ZZ: 0.00+0.12=0.12

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.16$ (L/5973) $f_{z,G}=0.16$ (L/6078)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.25$ (L/3819) $f_{z,G}=0.25$ (L/3855)

Membratura

Asta 202 Nodi 202 -11 -12 -13 -14 -15 -77 203 -26 -18 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-396.84 My,Ed=5630.69 Mz,Ed=0.00 L=9.69
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=81.83$ Ncr, $y=359031.00$ $\lambda'_y=1.07$ Curva a: $\Phi_y=1.16$ $\chi_y=0.62$
 $\lambda_z=81.83$ Ncr, $z=359031.00$ $\lambda'_z=1.07$ Curva a: $\Phi_z=1.16$ $\chi_z=0.62$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.15=0.15
 Verifica ZZ: 0.00+0.12=0.12

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,G}=0.16$ (L/6080)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,G}=0.25$ (L/3857) $f_{z,L}=0.25$ (L/3886)

Membratura

Asta 302 Nodi -69 -3 -68 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: N,Ed=-0.00 My,Ed=357.34 L=3.00
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.04=0.04
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/7786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.06$ (L/5284)

Membratura

Asta 303 Nodi -76 -29 -75 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.08=0.08
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3894)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 305 Nodi -48 -6 -47 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
 Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.08=0.08
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3894)

- Verifica freccia massima carichi totali - CC 31

$f_{z,L}=0.11$ (L/2850)

Membratura

Asta 306 Nodi -50 -7 -49 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3895)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 307 Nodi -52 -8 -51 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3894)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 308 Nodi -54 -9 -53 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3895)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 309 Nodi -56 -10 -55 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=357.34 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.04=0.04
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/7786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.06$ (L/5284)

Membratura

Asta 310 Nodi -58 -11 -57 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=357.34 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.04=0.04
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/7786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.06$ (L/5284)

Membratura

Asta 311 Nodi -60 -12 -59 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3895)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 312 Nodi -62 -13 -61 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3895)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 313 Nodi -64 -14 -63 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3895)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 314 Nodi -66 -15 -65 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3894)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 316 Nodi -74 -26 -73 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3894)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 317 Nodi -71 -18 -70 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=357.34 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.04=0.04
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/7786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.06$ (L/5284)

Membratura

Asta 318 Nodi -81 201 -80 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3894)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

Membratura

Asta 319 Nodi -79 -77 -78 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 1
Sollecitazioni: N,Ed=-0.00 My,Ed=661.86 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.08=0.08
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3894)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.11$ (L/2850)

5.2 Tracker 2x14 – configurazione in esercizio ($\alpha = 60^\circ$)

5.2.1 Diagrammi tassi di sfruttamento

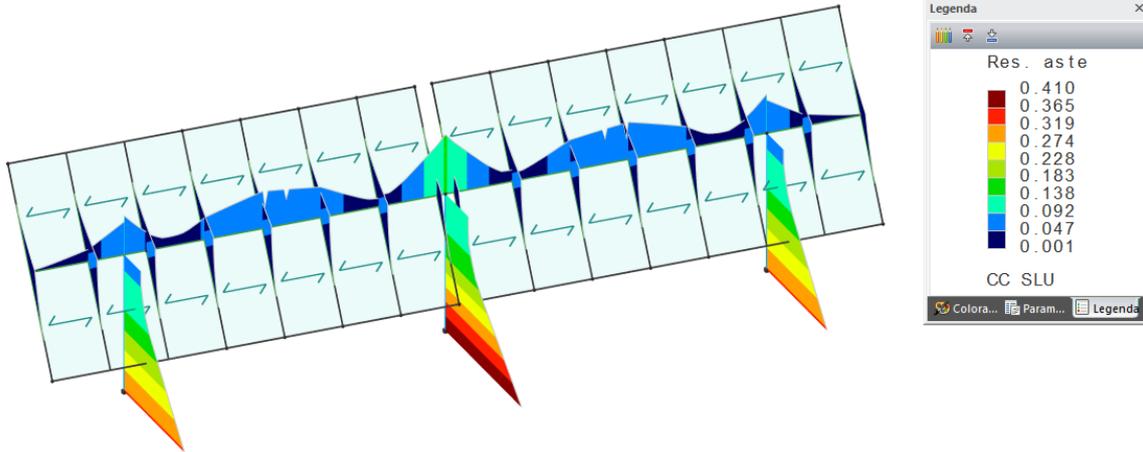


Diagramma tassi di sfruttamento resistenza aste combo SLU con valore massimo pari a 0,410

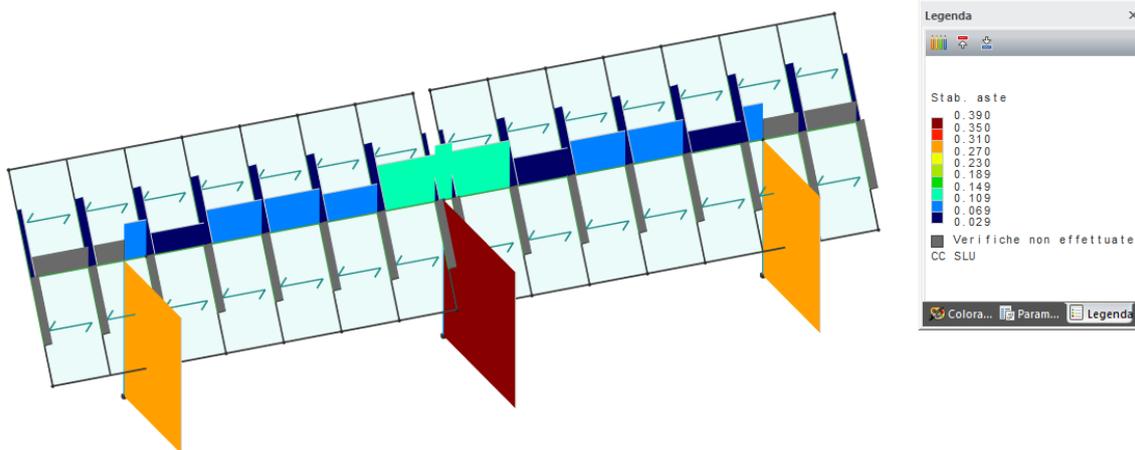


Diagramma tassi di sfruttamento stabilità aste combo SLU con valore massimo pari a 0,390

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

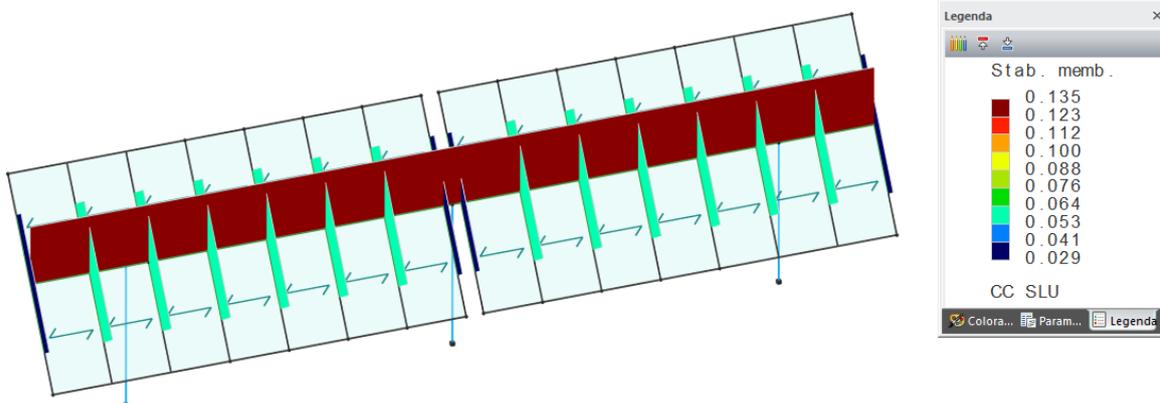


Diagramma tassi di sfruttamento stabilità membrature combo SLU con valore massimo pari a 0,135

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

Figure 12: Tassi di sfruttamento SLU (Stato limite ultimo)

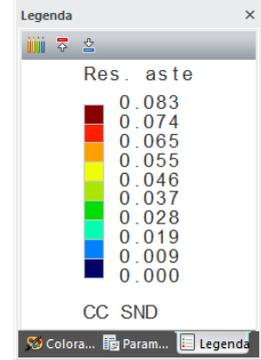
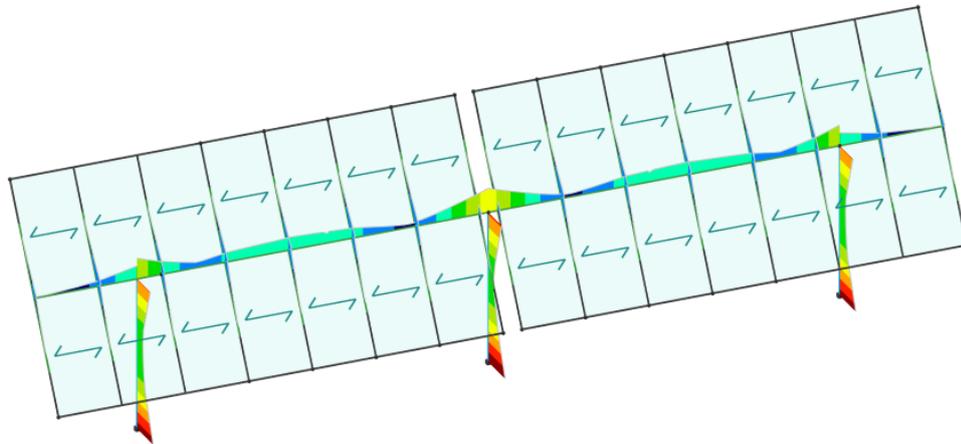


Diagramma tassi di sfruttamento resistenza aste combo SND con valore massimo pari a 0,083

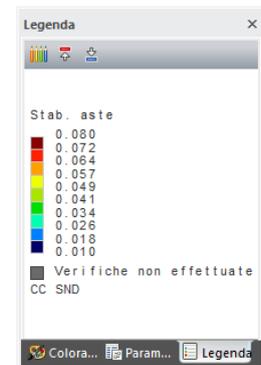
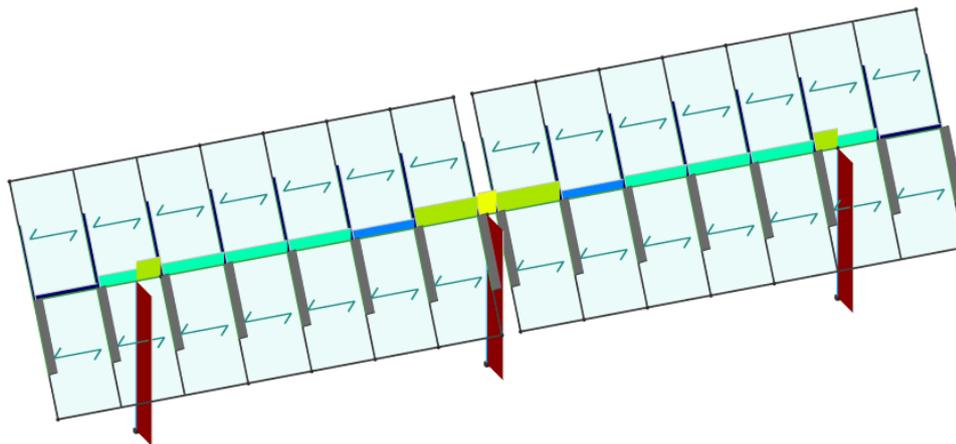


Diagramma tassi di sfruttamento stabilità aste combo SND con valore massimo pari a 0,080

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

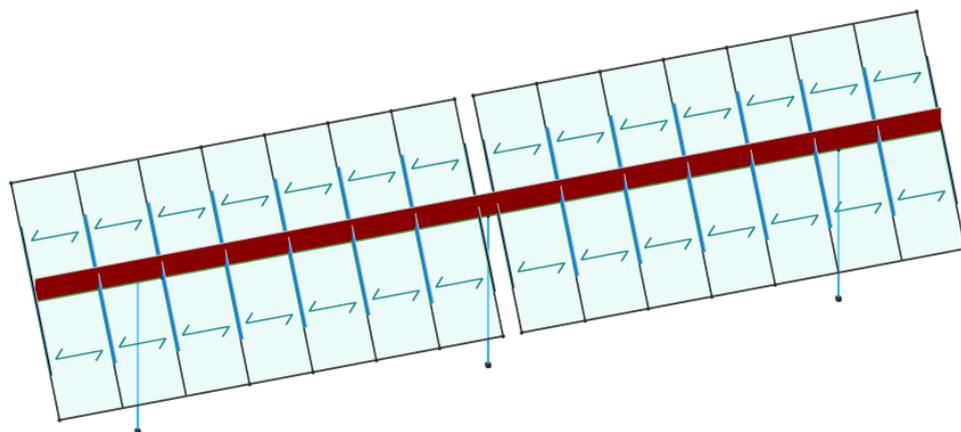


Diagramma tassi di sfruttamento stabilità membrature combo SND con valore massimo pari a 0,050

Figure 13: Tassi di sfruttamento SND (Stato limite di vita non dissipativo)

5.2.2 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:

ModeSt ver. 8.31, licenza n. 7429, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:

Xfinest ver. 9.6.2, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18

Tipo di calcolo: sismica statica

Vincoli esterni: Considera sempre vincoli assegnati in modellazione

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Tipo di analisi: Lineare
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Non sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

Opzioni generali:

- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Si
- Check sequenza di Sturm: Si
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No

Opzioni per analisi P-Delta:

- Numero massimo di iterazioni: 15
- Valore della norma euclidea degli spostamenti: 1.0000E-04

Opzioni per analisi pushover:

- Esegui analisi in regime di piccoli spostamenti: Si

Opzioni per analisi pushover murature:

- Interrompi analisi nel caso di plasticizzazione per carichi statici: Si
- Utilizza sforzo normale medio: Si

Metodo di convergenza:

- Forze e momenti residui (F)
Valore della norma euclidea delle forze: 1.0000E-03
Valore della norma euclidea dei momenti: 1.0000E-02

- Opzioni aggiuntive per analisi non lineari in presenza di elementi bidimensionali con comportamento Drucker-Prager:

OPTION PARAM AUTO_INCREMENT=YES
OPTION PARAM LINE_SEARCHES=YES
OPTION PARAM BGINCRS=1.0
OPTION PARAM AVINCRS=1.0

Dati struttura

- Sito di costruzione: PP5J+MR Ploaghe SS, Italia LON. 8.73206 LAT. 40.70920
Contenuto tra ID reticolo: 26271 26049 26272 26050

Simbologia

- Ag =Accelerazione orizzontale massima al sito
- Cc =Coefficiente funzione della categoria del suolo
- Fo =Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
- Ss =Coefficiente di amplificazione stratigrafica
- Tr =Periodo di ritorno <anni>
- TCC=Tipo di combinazione di carico
 - SLU = Stato limite ultimo
 - SLE R = Stato limite d'esercizio, combinazione rara
 - SLE F = Stato limite d'esercizio, combinazione frequente
 - SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 - SLD = Stato limite di danno
 - SND = Stato limite di salvaguardia della vita (non dissipativo)
- Tc* =Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

TCC	Tr	Ag <g>	Fo	Tc*	Ss	Cc
SLD	50	0.0217	2.63	0.19	1.80	2.89
SLV	475	0.0395	2.77	0.29	1.80	2.30

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale VN: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 5.36 <m>
- Altezza della struttura: 5.36 <m>
- Numero piani edificio: 0
- Coefficiente θ : 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di calcolo

- Categoria del suolo di fondazione: D
- Tipologia strutturale: acciaio a mensola o a pendolo inverso

Periodo T ₁	0.29936
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovraresistenza (α_u/α_1)	1.00
Valore di riferimento del fattore di comportamento (q_0)	2.00
Fattore riduttivo (K_w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di comportamento dissipativo (q)	2.00
Fattore di comportamento non dissipativo (qND)	1.33
Fattore di comportamento per SLD (qD)	1.33

- Categoria topografica: T2 - Pendii con inclinazione media $i > 15^\circ$
- Coeff. amplificazione topografica S_T: 1.20
- Accelerazione di picco del terreno AgS: 0.0853 <g>
- Fattore di comportamento per sisma verticale (qv): 1.50
- Smorzamento spettro: 5.00%

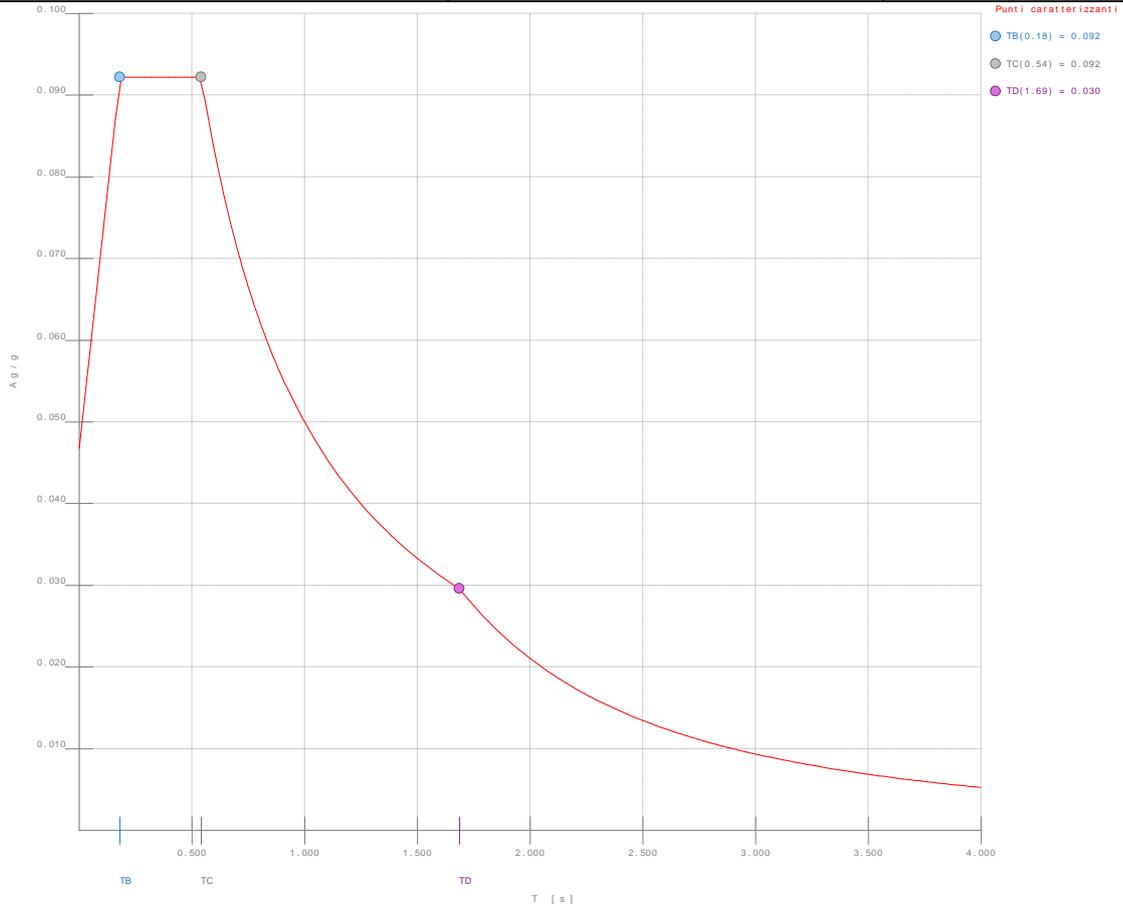


Figura numero 1: Spettro SLD

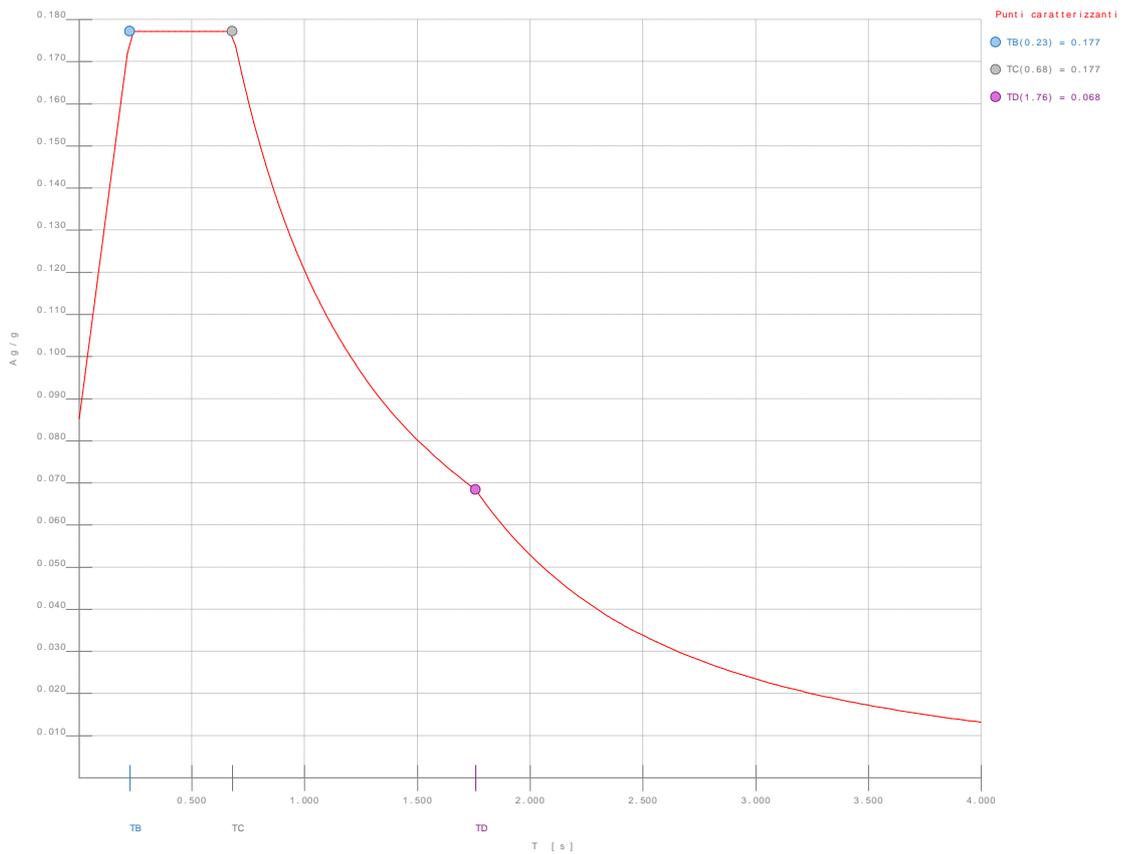


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>
- Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

- N = Numero
- Comm. = Commento
- 1 = G1 - Peso Proprio
- 2 = G2 - Permanenti non strutturali
- 3 = Q - Variabili neve
- 4 = Vento da retro - Cond. A
- 5 = Vento da retro - Cond. B
- 6 = Vento da fronte - Cond. C
- 7 = Vento da fronte - Cond. D
- F = azioni orizzontali convenzionali
- SLU = Stato limite ultimo
- SLR = Stato limite per combinazioni rare
- SLF = Stato limite per combinazioni frequenti
- SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
- S = Sì
- N = No

N	Comm.	1	2	3	4	5	6	7	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	S	S	S	N	N	N	N	S	N	N	N	N
2	Calcolo statico	S	S	S	N	N	N	N	S	S	S	S	S
3	Vento cond A	S	S	S	N	N	N	N	S	S	S	S	S
4	Vento cond B	S	S	S	N	N	N	N	S	S	S	S	S
5	Vento cond C	S	S	S	N	N	N	N	S	S	S	S	S
6	Vento cond D	S	S	S	N	N	N	N	S	S	S	S	S

Elenco combinazioni di carico simboliche

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	1	2	3	4	5	6	7	S
1	Amb. 1 (Sisma)	SLU S	1	1	Ψ_2	-----	-----	-----	-----	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	-----	-----
3	Amb. 2 (SLE R)	SLE R	1	1	1	-----	-----	-----	-----	-----
4	Amb. 2 (SLE F)	SLE F	1	1	Ψ_1	-----	-----	-----	-----	-----
5	Amb. 2 (SLE Q)	SLE Q	1	1	Ψ_2	-----	-----	-----	-----	-----
6	Amb. 3 (SLU)	SLU	γ max	γ max	$\Psi_0 * \gamma$ max	γ max	-----	-----	-----	-----
7	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	$\Psi_0 * \gamma$ max	-----	-----	-----	-----
8	Amb. 3 (SLE R)	SLE R	1	1	Ψ_0	1	-----	-----	-----	-----
9	Amb. 3 (SLE R)	SLE R	1	1	1	Ψ_0	-----	-----	-----	-----
10	Amb. 3 (SLE F)	SLE F	1	1	Ψ_2	Ψ_1	-----	-----	-----	-----
11	Amb. 3 (SLE F)	SLE F	1	1	Ψ_1	Ψ_2	-----	-----	-----	-----
12	Amb. 3 (SLE Q)	SLE Q	1	1	Ψ_2	Ψ_2	-----	-----	-----	-----
13	Amb. 4 (SLU)	SLU	γ max	γ max	$\Psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
14	Amb. 4 (SLU)	SLU	γ max	γ max	γ max	-----	$\Psi_0 * \gamma$ max	-----	-----	-----
15	Amb. 4 (SLE R)	SLE R	1	1	Ψ_0	1	-----	Ψ_0	-----	-----
16	Amb. 4 (SLE R)	SLE R	1	1	1	-----	Ψ_0	-----	-----	-----
17	Amb. 4 (SLE F)	SLE F	1	1	Ψ_2	-----	Ψ_1	-----	-----	-----
18	Amb. 4 (SLE F)	SLE F	1	1	Ψ_1	-----	Ψ_2	-----	-----	-----
19	Amb. 4 (SLE Q)	SLE Q	1	1	Ψ_2	-----	Ψ_2	-----	-----	-----
20	Amb. 5 (SLU)	SLU	γ max	γ max	$\Psi_0 * \gamma$ max	-----	-----	γ max	-----	-----
21	Amb. 5 (SLU)	SLU	γ max	γ max	γ max	-----	-----	$\Psi_0 * \gamma$ max	-----	-----
22	Amb. 5 (SLE R)	SLE R	1	1	Ψ_0	-----	-----	1	-----	-----
23	Amb. 5 (SLE R)	SLE R	1	1	1	-----	-----	Ψ_0	-----	-----
24	Amb. 5 (SLE F)	SLE F	1	1	Ψ_2	-----	-----	Ψ_1	-----	-----
25	Amb. 5 (SLE F)	SLE F	1	1	Ψ_1	-----	-----	Ψ_2	-----	-----
26	Amb. 5 (SLE Q)	SLE Q	1	1	Ψ_2	-----	-----	Ψ_2	-----	-----
27	Amb. 6 (SLU)	SLU	γ max	γ max	$\Psi_0 * \gamma$ max	-----	-----	-----	γ max	-----

28	Amb. 6 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	$\Psi_0 * \gamma$ max	-----
29	Amb. 6 (SLE R)	SLE R	1	1	Ψ_0	-----	-----	-----	1	-----
30	Amb. 6 (SLE R)	SLE R	1	1	1	-----	-----	-----	Ψ_0	-----
31	Amb. 6 (SLE F)	SLE F	1	1	Ψ_2	-----	-----	-----	Ψ_1	-----
32	Amb. 6 (SLE F)	SLE F	1	1	Ψ_1	-----	-----	-----	Ψ_2	-----
33	Amb. 6 (SLE Q)	SLE Q	1	1	Ψ_2	-----	-----	-----	Ψ_2	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: Si

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

An. = Tipo di analisi
 L = Lineare
 NL = Non lineare
 PD = P-Delta

Bk = Buckling
 S = Si
 N = No

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	S X	S Y
1	Amb. 1 (SLU S) S +X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
2	Amb. 1 (SLE S) S +X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
3	Amb. 1 (SLU S) S +X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
4	Amb. 1 (SLE S) S +X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
5	Amb. 1 (SLU S) S -X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
6	Amb. 1 (SLE S) S -X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
7	Amb. 1 (SLU S) S -X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
8	Amb. 1 (SLE S) S -X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
9	Amb. 1 (SLU S) S +0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
10	Amb. 1 (SLE S) S +0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
11	Amb. 1 (SLU S) S -0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
12	Amb. 1 (SLE S) S -0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
13	Amb. 1 (SLU S) S +0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
14	Amb. 1 (SLE S) S +0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
15	Amb. 1 (SLU S) S -0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
16	Amb. 1 (SLE S) S -0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
17	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.00	0.00	0.00
18	Amb. 2 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
19	Amb. 2 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
20	Amb. 2 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	0.75	1.50	0.00	0.00	0.00	0.00	0.00
22	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
23	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	0.50	1.00	0.00	0.00	0.00	0.00	0.00
24	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
25	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.20	0.00	0.00	0.00	0.00	0.00
26	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
27	Amb. 3 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	1.50	0.00	0.00	0.00	0.00
29	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.90	0.00	0.00	0.00	0.00
30	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	1.00	0.00	0.00	0.00	0.00
31	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.60	0.00	0.00	0.00	0.00
32	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.20	0.00	0.00	0.00	0.00
33	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
34	Amb. 4 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	1.50	0.00	0.00	0.00
36	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.90	0.00	0.00	0.00
37	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00
38	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00
39	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00
40	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
41	Amb. 5 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	0.00	1.50	0.00	0.00
43	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.90	0.00	0.00
44	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00

45	Amb. 6 (SLE R)	SLE R L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00
46	Amb. 6 (SLE F)	SLE F L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.20	0.00	0.00
47	Amb. 6 (SLE F)	SLE F L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
48	Amb. 6 (SLE Q)	SLE Q L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Elenco masse nodi

Simbologia

Mo = Massa orizzontale

Nodo = Numero del nodo

Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo
	<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>
-81	84.43	-80	84.43	-79	84.43	-78	84.43	-77	194.07	-76	84.43	-75	84.43	-74	84.43	-73	84.43	-72	84.43
-71	56.02	-70	56.02	-69	56.02	-68	56.02	-66	84.43	-65	84.43	-64	84.43	-63	84.43	-62	84.43	-61	84.43
-61	84.43	-60	84.43	-59	84.43	-58	56.02	-57	56.02	-56	56.02	-55	56.02	-54	84.43	-53	84.43	-52	84.43
-52	84.43	-51	84.43	-50	84.43	-49	84.43	-48	84.43	-47	84.43	-45	184.29	-29	208.89	-26	208.89	-25	84.43
-18	144.09	-15	232.96	-14	232.96	-13	232.96	-12	232.96	-11	153.37	-10	153.37	-9	232.96	-8	232.96	-7	232.96
-7	232.96	-6	232.96	-3	144.09	201	194.08	202	139.90	203	184.29								

Totali masse nodi

Mo
<kg>
6247.42

Elenco forze sismiche nodali allo SLD

Simbologia

Fx = Forza in dir. X

Fy = Forza in dir. Y

Nodo = Numero del nodo

cx = Coeff. c in dir. X

cy = Coeff. c in dir. Y

Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy
			<daN>	<daN>				<daN>	<daN>				<daN>	<daN>				<daN>	<daN>				<daN>	<daN>
-81	0.01	0.01	4.62	4.62	-80	0.02	0.02	10.66	10.66	-79	0.01	0.01	4.62	4.62	-78	0.02	0.02	10.66	10.66	-77	0.03	0.03	17.56	17.56
-77	0.03	0.03	17.56	17.56	-76	0.01	0.01	4.62	4.62	-75	0.02	0.02	10.66	10.66	-74	0.01	0.01	4.62	4.62	-73	0.02	0.02	10.66	10.66
-73	0.02	0.02	10.66	10.66	-71	0.01	0.01	3.06	3.06	-70	0.01	0.01	7.07	7.07	-69	0.01	0.01	3.06	3.06	-68	0.01	0.01	7.07	7.07
-68	0.01	0.01	7.07	7.07	-66	0.01	0.01	4.62	4.62	-65	0.02	0.02	10.66	10.66	-64	0.01	0.01	4.62	4.62	-63	0.02	0.02	10.66	10.66
-63	0.02	0.02	10.66	10.66	-62	0.01	0.01	4.62	4.62	-61	0.02	0.02	10.66	10.66	-60	0.01	0.01	4.62	4.62	-59	0.02	0.02	10.66	10.66
-59	0.02	0.02	10.66	10.66	-58	0.01	0.01	3.06	3.06	-57	0.01	0.01	7.07	7.07	-56	0.01	0.01	3.06	3.06	-55	0.01	0.01	7.07	7.07
-55	0.01	0.01	7.07	7.07	-54	0.01	0.01	4.62	4.62	-53	0.02	0.02	10.66	10.66	-52	0.01	0.01	4.62	4.62	-51	0.02	0.02	10.66	10.66
-51	0.02	0.02	10.66	10.66	-50	0.01	0.01	4.62	4.62	-49	0.02	0.02	10.66	10.66	-48	0.01	0.01	4.62	4.62	-47	0.02	0.02	10.66	10.66
-47	0.02	0.02	10.66	10.66	-45	0.03	0.03	16.67	16.67	-29	0.03	0.03	18.90	18.90	-26	0.03	0.03	18.90	18.90	-18	0.02	0.02	13.04	13.04
-18	0.02	0.02	13.04	13.04	-15	0.04	0.04	21.08	21.08	-14	0.04	0.04	21.08	21.08	-13	0.04	0.04	21.08	21.08	-12	0.04	0.04	21.08	21.08
-12	0.04	0.04	21.08	21.08	-11	0.02	0.02	13.88	13.88	-10	0.02	0.02	13.88	13.88	-9	0.04	0.04	21.08	21.08	-8	0.04	0.04	21.08	21.08
-8	0.04	0.04	21.08	21.08	-7	0.04	0.04	21.08	21.08	-6	0.04	0.04	21.08	21.08	-3	0.02	0.02	13.04	13.04	201	0.03	0.03	17.56	17.56
201	0.03	0.03	17.56	17.56	202	0.02	0.02	12.66	12.66	203	0.03	0.03	16.67	16.67										

Totali forze sismiche

Fx	Fy
<daN>	<daN>
565.20	565.20

Elenco forze sismiche nodali allo SND

Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy
			<daN>	<daN>				<daN>	<daN>				<daN>	<daN>				<daN>	<daN>
-81	0.01	0.01	8.87	8.87	-80	0.02	0.02	20.48	20.48	-79	0.01	0.01	8.87	8.87	-78	0.02	0.02	20.48	20.48
-77	0.03	0.03	33.73	33.73	-76	0.01	0.01	8.87	8.87	-75	0.02	0.02	20.48	20.48	-74	0.01	0.01	8.87	8.87
-73	0.02	0.02	20.48	20.48	-71	0.01	0.01	5.89	5.89	-70	0.01	0.01	13.59	13.59	-69	0.01	0.01	5.89	5.89
-68	0.01	0.01	13.59	13.59	-66	0.01	0.01	8.87	8.87	-65	0.02	0.02	20.48	20.48	-64	0.01	0.01	8.87	8.87
-63	0.02	0.02	20.48	20.48	-62	0.01	0.01	8.87	8.87	-61	0.02	0.02	20.48	20.48	-60	0.01	0.01	8.87	8.87

-59	0.02	0.02	20.48	20.48	-58	0.01	0.01	5.89	5.89	-57	0.01	0.01	13.59	13.59	-56	0.01	0.01	5.89	5.89
-55	0.01	0.01	13.59	13.59	-54	0.01	0.01	8.87	8.87	-53	0.02	0.02	20.48	20.48	-52	0.01	0.01	8.87	8.87
-51	0.02	0.02	20.48	20.48	-50	0.01	0.01	8.87	8.87	-49	0.02	0.02	20.48	20.48	-48	0.01	0.01	8.87	8.87
-47	0.02	0.02	20.48	20.48	-45	0.03	0.03	32.03	32.03	-29	0.03	0.03	36.31	36.31	-26	0.03	0.03	36.31	36.31
-18	0.02	0.02	25.05	25.05	-15	0.04	0.04	40.49	40.49	-14	0.04	0.04	40.49	40.49	-13	0.04	0.04	40.49	40.49
-12	0.04	0.04	40.49	40.49	-11	0.02	0.02	26.66	26.66	-10	0.02	0.02	26.66	26.66	-9	0.04	0.04	40.49	40.49
-8	0.04	0.04	40.49	40.49	-7	0.04	0.04	40.49	40.49	-6	0.04	0.04	40.49	40.49	-3	0.02	0.02	25.05	25.05
201	0.03	0.03	33.73	33.73	202	0.02	0.02	24.32	24.32	203	0.03	0.03	32.03	32.03					

Totali forze sismiche

Fx	Fy
<daN>	<daN>
1085.94	1085.94

Domanda in duttilità di curvatura

Direzione X $\mu_{EdX}=6.85$

Direzione Y $\mu_{EdY}=6.85$

Spostamenti relativi massimi allo stato limite di danno

Simbologia

δ =Spostamento relativo

δ/h =Rapporto (*1000) tra lo spostamento relativo e l'altezza

CC =Numero della combinazione delle condizioni di carico elementari

N1 =Nodo1

N2 =Nodo2

h =Altezza teorica

I valori degli spostamenti relativi per CC di tipo sismico sono amplificati come da normativa

N1	N2	h	δ	δ/h	CC
		<m>	<cm>		
315	-45	3.29	0.14	0.42	10
2	202	3.29	0.16	0.50	16
3	203	3.29	0.14	0.42	12

Min = 0.42

Max = 0.50

Reazioni vincolari

Simbologia

CC =Numero della combinazione delle condizioni di carico elementari

Fx =Reazione vincolare (forza) in dir. X

Fy =Reazione vincolare (forza) in dir. Y

Fz =Reazione vincolare (forza) in dir. Z

Mx =Reazione vincolare (momento) intorno all'asse X

My =Reazione vincolare (momento) intorno all'asse Y

Mz =Reazione vincolare (momento) intorno all'asse Z

Nodo =Numero del nodo

TCC =Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

Nodo		CC	TCC	Fx	CC	TCC	Fy	CC	TCC	Fz	CC	TCC	Mx	CC	TCC	My	CC	TCC	Mz
				<daN>			<daN>			<daN>			<daNm>			<daNm>			<daNm>
2	Max	5	SND	424.69	21	SLU	4423.60	28	SLU	5388.96	28	SLU	9888.92	5	SND	718.65	7	SND	0.00
2	Min	1	SND	-424.69	28	SLU	-3139.94	23	SLE R	925.53	21	SLU	-13931.70	1	SND	-718.65	1	SND	-0.00
3	Max	5	SND	237.47	21	SLU	3262.21	28	SLU	4077.14	28	SLU	7819.54	5	SND	516.16	28	SLU	1.29
3	Min	1	SND	-423.77	28	SLU	-2315.57	23	SLE R	730.03	21	SLU	-11016.30	21	SLU	-717.15	1	SND	-1.82
315	Max	5	SND	423.77	21	SLU	3262.21	28	SLU	4077.14	28	SLU	7819.54	5	SND	717.15	21	SLU	1.82
315	Min	1	SND	-237.47	28	SLU	-2315.57	23	SLE R	730.03	21	SLU	-11016.30	28	SLU	-516.16	1	SND	-1.29

Sollecitazioni aste

Simbologia

Asta = Numero dell'asta
 CC = Numero della combinazione delle condizioni di carico elementari
 Mx = Momento torcente intorno all'asse X
 My = Momento flettente intorno all'asse Y
 Mz = Momento flettente intorno all'asse Z
 N = Sforzo normale
 N1 = Nodo1
 N2 = Nodo2
 Ty = Taglio in dir. Y
 Tz = Taglio in dir. Z
 X = Coordinata progressiva rispetto al nodo iniziale

Tipo di combinazione di carico: SND

Asta	N1	N2		X <cm>	N <daN>	CC	Ty <daN>	CC	Mz <daNm>	CC	Tz <daN>	CC	My <daNm>	CC	Mx <daNm>	CC
1	315	-45	Max	0.00	-1835.92	1	237.47	1	717.15	5	329.33	9	1178.96	15	0.16	11
1	315	-45	Max	328.50	-1597.85	1	237.47	1	263.93	1	329.33	9	99.04	13	0.16	11
1	315	-45	Min.	0.00	-2080.76	5	-423.77	5	-516.16	1	-329.33	15	-1178.96	9	-0.16	13
1	315	-45	Min.	328.50	-1842.69	5	-423.77	5	-674.95	5	-329.33	15	-99.03	11	-0.16	13
2	2	202	Max	0.00	-2569.15	1	424.69	1	718.65	5	432.38	9	1445.18	13	0.00	1
2	2	202	Max	328.50	-2331.08	1	424.69	1	676.47	1	432.38	9	24.80	15	0.00	1
2	2	202	Min.	0.00	-2569.15	1	-424.69	5	-718.65	1	-432.38	13	-1445.18	9	-0.00	7
2	2	202	Min.	328.50	-2331.08	1	-424.69	5	-676.47	5	-432.38	13	-24.80	9	-0.00	7
3	3	203	Max	0.00	-1835.92	5	423.77	1	516.16	5	329.33	11	1178.96	13	0.16	15
3	3	203	Max	328.50	-1597.85	5	423.77	1	674.95	1	329.33	11	99.04	15	0.16	15
3	3	203	Min.	0.00	-2080.76	1	-237.47	5	-717.15	1	-329.33	13	-1178.96	11	-0.16	9
3	3	203	Min.	328.50	-1842.69	1	-237.47	5	-263.93	5	-329.33	13	-99.03	9	-0.16	9
201	-3	-29	Max	0.00	44.52	5	44.52	9	5.78	1	-189.50	1	10.00	1	10.00	9
201	-3	-29	Max	135.63	44.52	5	44.52	9	62.11	9	-313.01	1	-330.77	1	10.00	9
201	-3	-29	Min.	0.00	-44.52	1	-44.52	13	-5.78	5	-189.50	1	-10.00	5	-10.00	13
201	-3	-29	Min.	135.63	-44.52	1	-44.52	13	-62.11	15	-313.01	1	-350.78	5	-10.00	13
201	-29	-45	Max	0.00	110.18	5	110.18	9	64.73	9	-583.68	1	-315.69	1	25.08	9
201	-29	-45	Max	83.77	110.18	5	110.18	9	157.03	9	-659.97	1	-836.60	1	25.08	9
201	-29	-45	Min.	0.00	-110.18	1	-110.18	13	-64.73	15	-583.68	1	-365.86	5	-25.08	13
201	-29	-45	Min.	83.77	-110.18	1	-110.18	13	-157.03	15	-659.97	1	-886.76	5	-25.08	13
201	-45	201	Max	0.00	95.26	1	187.12	15	157.17	9	1182.72	5	-572.67	1	73.95	13
201	-45	201	Max	51.86	95.26	1	187.12	15	60.14	9	1135.50	5	-98.55	1	73.95	13
201	-45	201	Min.	0.00	-281.56	5	-187.12	9	-157.17	15	937.88	1	-1561.71	5	-73.95	11
201	-45	201	Min.	51.86	-281.56	5	-187.12	9	-60.14	15	890.66	1	-960.63	5	-73.95	11
201	201	-6	Max	0.00	32.17	1	124.03	15	62.75	9	864.82	5	-83.47	1	58.88	13
201	201	-6	Max	135.63	32.17	1	124.03	15	109.81	13	741.32	5	673.65	1	58.88	13
201	201	-6	Min.	0.00	-218.47	5	-124.03	9	-62.75	15	619.98	1	-975.70	5	-58.88	11
201	201	-6	Min.	135.63	-218.47	5	-124.03	9	-109.81	11	496.48	1	113.49	5	-58.88	11
201	-6	-7	Max	0.00	-37.67	1	54.18	15	112.42	13	470.64	5	688.75	1	43.80	13
201	-6	-7	Max	135.63	-37.67	1	54.18	15	178.99	13	347.13	5	911.24	1	43.80	13
201	-6	-7	Min.	0.00	-148.63	5	-54.18	9	-112.42	11	225.80	1	98.44	5	-43.80	11
201	-6	-7	Min.	135.63	-148.63	5	-54.18	9	-178.99	11	102.30	1	653.01	5	-43.80	11
201	-7	-8	Max	0.00	-78.79	5	20.76	11	181.60	13	76.46	5	926.31	1	28.72	13
201	-7	-8	Max	83.97					-54.68	5			670.01	5		
201	-7	-8	Max	135.63	-78.79	5	20.76	11	153.44	13	-47.04	5	657.86	5	28.72	13
201	-7	-8	Min.	0.00	-107.52	1	-20.76	13	-181.60	11	-168.38	1	637.90	5	-28.72	11
201	-7	-8	Min.	83.97					-54.68	5			670.01	5		
201	-7	-8	Min.	135.63	-107.52	1	-20.76	13	-153.44	11	-291.88	1	614.19	1	-28.72	11
201	-8	-9	Max	0.00	-8.94	5	90.61	11	156.05	13	-317.72	5	642.78	5	13.64	13
201	-8	-9	Max	135.63	-8.94	5	90.61	11	33.92	15	-441.22	5	128.11	5	13.64	13
201	-8	-9	Min.	0.00	-177.36	1	-90.61	13	-156.05	11	-562.56	1	629.27	1	-13.64	11
201	-8	-9	Min.	135.63	-177.36	1	-90.61	13	-33.92	9	-686.06	1	-217.48	1	-13.64	11
201	-9	-10	Max	0.00	60.90	5	160.45	11	35.78	13	-711.90	5	113.02	5	3.92	1
201	-9	-10	Max	135.63	60.90	5	160.45	11	181.84	11	-835.40	5	-936.27	5	3.92	1
201	-9	-10	Min.	0.00	-247.21	1	-160.45	13	-35.78	11	-956.74	1	-202.41	1	-3.92	7
201	-9	-10	Min.	135.63	-247.21	1	-160.45	13	-181.84	13	-1080.24	1	-1583.77	1	-3.92	7
201	-10	202	Max	0.00	107.03	5	206.58	11	181.13	9	-1024.91	5	-946.28	5	13.36	9
201	-10	202	Max	20.00	107.03	5	206.58	11	221.43	11	-1043.12	5	-1153.09	5	13.36	9
201	-10	202	Min.	0.00	-293.34	1	-206.58	13	-181.13	15	-1269.75	1	-1573.78	1	-13.36	15
201	-10	202	Min.	20.00	-293.34	1	-206.58	13	-221.43	13	-1287.96	1	-1829.56	1	-13.36	15
202	202	-11	Max	0.00	107.03	1	206.58	15	221.43	9	1287.96	5	-1153.09	1	13.36	13
202	202	-11	Max	20.00	107.03	1	206.58	15	181.13	11	1269.75	5	-946.28	1	13.36	13
202	202	-11	Min.	0.00	-293.34	5	-206.58	9	-221.43	15	1043.12	1	-1829.56	5	-13.36	11
202	202	-11	Min.	20.00	-293.34	5	-206.58	9	-181.13	13	1024.91	1	-1573.78	5	-13.36	11
202	-11	-12	Max	0.00	60.90	1	160.45	15	181.84	9	1080.25	5	-936.28	1	3.92	3
202	-11	-12	Max	135.63	60.90	1	160.45	15	35.77	15	956.74	5	113.01	1	3.92	3
202	-11	-12	Min.	0.00	-247.21	5	-160.45	9	-181.84	15	835.41	1	-1583.79	5	-3.92	5
202	-11	-12	Min.	135.63	-247.21	5	-160.45	9	-35.77	9	711.90	1	-202.42	5	-3.92	5
202	-12	-13	Max	0.00	-8.94	1	90.61	15	33.92	13	686.06	5	128.10	1	13.64	9
202	-12	-13	Max	135.63	-8.94	1	90.61	15	156.05	15	562.56	5	642.77	1	13.64	9
202	-12	-13	Min.	0.00	-177.36	5	-90.61	9	-33.92	11	441.22	1	-217.49	5	-13.64	15



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202	-12	-13	Min.	135.63	-177.36	5	-90.61	9	-156.05	9	317.72	1	629.26	5	-13.64	15
202	-13	-14	Max	0.00	-78.79	1	20.76	15	153.44	15	291.88	5	657.86	1	28.72	9
202	-13	-14	Max	51.66					-54.68	1			670.01	1		
202	-13	-14	Max	135.63	-78.79	1	20.76	15	181.60	15	168.38	5	926.31	5	28.72	9
202	-13	-14	Min.	0.00	-107.52	5	-20.76	9	-153.44	9	47.04	1	614.19	5	-28.72	15
202	-13	-14	Min.	51.66					-54.68	1			670.01	1		
202	-13	-14	Min.	135.63	-107.52	5	-20.76	9	-181.60	9	-76.46	1	637.90	1	-28.72	15
202	-14	-15	Max	0.00	-37.67	5	54.18	11	178.99	15	-102.30	5	911.23	5	43.80	9
202	-14	-15	Max	135.63	-37.67	5	54.18	11	112.42	15	-225.81	5	688.73	5	43.80	9
202	-14	-15	Min.	0.00	-148.63	1	-54.18	13	-178.99	9	-347.14	1	652.98	1	-43.80	15
202	-14	-15	Min.	135.63	-148.63	1	-54.18	13	-112.42	9	-470.64	1	98.41	1	-43.80	15
202	-15	-77	Max	0.00	32.17	5	124.03	11	109.81	15	-496.48	5	673.67	5	58.88	9
202	-15	-77	Max	135.63	32.17	5	124.03	11	62.74	11	-619.98	5	-83.45	7	58.88	9
202	-15	-77	Min.	0.00	-218.47	1	-124.03	13	-109.81	9	-741.32	1	113.52	1	-58.88	15
202	-15	-77	Min.	135.63	-218.47	1	-124.03	13	-62.74	13	-864.82	1	-975.66	1	-58.88	15
202	-77	203	Max	0.00	95.26	5	187.12	11	60.13	11	-890.66	5	-98.53	7	73.95	9
202	-77	203	Max	51.86	95.26	5	187.12	11	157.17	11	-937.88	5	-572.65	5	73.95	9
202	-77	203	Min.	0.00	-281.56	1	-187.12	13	-60.13	13	-1135.50	1	-960.60	1	-73.95	15
202	-77	203	Min.	51.86	-281.56	1	-187.12	13	-157.17	13	-1182.72	1	-1561.68	1	-73.95	15
202	203	-26	Max	0.00	110.18	1	110.18	13	157.02	11	659.97	1	-836.60	5	25.08	13
202	203	-26	Max	83.77	110.18	1	110.18	13	64.72	11	583.68	1	-315.69	5	25.08	13
202	203	-26	Min.	0.00	-110.18	5	-110.18	9	-157.02	13	659.97	1	-886.77	1	-25.08	9
202	203	-26	Min.	83.77	-110.18	5	-110.18	9	-64.72	13	583.68	1	-365.85	1	-25.08	9
202	-26	-18	Max	0.00	44.52	1	44.52	13	62.11	11	313.01	1	-330.77	5	10.00	13
202	-26	-18	Max	135.63	44.52	1	44.52	13	5.78	5	189.50	1	10.00	5	10.00	13
202	-26	-18	Min.	0.00	-44.52	5	-44.52	9	-62.11	13	313.01	1	-350.78	1	-10.00	9
202	-26	-18	Min.	135.63	-44.52	5	-44.52	9	-5.78	3	189.50	1	-10.01	1	-10.00	9
302	-3	-69	Max	0.00	85.00	13	5.89	5	8.83	1	52.47	9	-33.57	13	0.00	1
302	-3	-69	Max	150.00	16.07	13	5.89	5	0.00	1	12.68	9	0.00	13	0.00	1
302	-3	-69	Min.	0.00	79.11	9	-5.89	1	-8.83	5	42.28	13	-48.86	9	0.00	1
302	-3	-69	Min.	150.00	10.18	9	-5.89	1	0.00	5	2.48	13	0.00	9	0.00	1
302	-68	-3	Max	0.00	-6.33	9	13.59	1	0.00	7	4.19	13	0.00	9	0.00	7
302	-68	-3	Max	15.79					0.64	13			0.33	13		
302	-68	-3	Max	150.00	-75.26	9	13.59	1	20.38	1	-35.61	13	-23.56	13	0.00	7
302	-68	-3	Min.	0.00	-19.92	13	-13.59	5	0.00	1	-19.35	9	0.00	15	0.00	1
302	-68	-3	Min.	15.79					0.64	13			0.33	13		
302	-68	-3	Min.	150.00	-88.85	13	-13.59	5	-20.38	5	-59.14	9	-58.87	9	0.00	1
303	-29	-76	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
303	-29	-76	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
303	-29	-76	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
303	-29	-76	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
303	-75	-29	Max	0.00	-16.01	9	20.48	1	0.00	7	2.58	13	0.00	9	0.00	5
303	-75	-29	Max	7.37					0.45	13			0.10	13		
303	-75	-29	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	5
303	-75	-29	Min.	0.00	-36.49	13	-20.48	5	0.00	1	-32.89	9	0.00	13	0.00	3
303	-75	-29	Min.	7.37					0.45	13			0.10	13		
303	-75	-29	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	3
305	-6	-48	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
305	-6	-48	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
305	-6	-48	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
305	-6	-48	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
305	-47	-6	Max	0.00	-16.01	9	20.48	1	0.00	5	2.58	13	0.00	11	0.00	1
305	-47	-6	Max	7.37					0.45	13			0.10	13		
305	-47	-6	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	1
305	-47	-6	Min.	0.00	-36.49	13	-20.48	5	0.00	3	-32.89	9	0.00	13	0.00	5
305	-47	-6	Min.	7.37					0.45	13			0.10	13		
305	-47	-6	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	5
306	-7	-50	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
306	-7	-50	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
306	-7	-50	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
306	-7	-50	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
306	-49	-7	Max	0.00	-16.01	9	20.48	1	0.00	7	2.58	13	0.00	11	0.00	1
306	-49	-7	Max	7.37					0.45	13			0.10	13		
306	-49	-7	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	1
306	-49	-7	Min.	0.00	-36.49	13	-20.48	5	0.00	1	-32.89	9	0.00	13	0.00	7
306	-49	-7	Min.	7.37					0.45	13			0.10	13		
306	-49	-7	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	7
307	-8	-52	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
307	-8	-52	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
307	-8	-52	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
307	-8	-52	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
307	-51	-8	Max	0.00	-16.01	9	20.48	1	0.00	1	2.58	13	0.00	9	0.00	5
307	-51	-8	Max	7.37					0.45	13			0.10	13		
307	-51	-8	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	5
307	-51	-8	Min.	0.00	-36.49	13	-20.48	5	0.00	7	-32.89	9	0.00	15	0.00	3
307	-51	-8	Min.	7.37					0.45	13			0.10	13		

307	-51	-8	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	3
308	-9	-54	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
308	-9	-54	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
308	-9	-54	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
308	-9	-54	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
308	-53	-9	Max	0.00	-16.01	9	20.48	1	0.00	5	2.58	13	0.00	13	0.00	5
308	-53	-9	Max	7.37					0.45	13			0.10	13		
308	-53	-9	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	5
308	-53	-9	Min.	0.00	-36.49	13	-20.48	5	0.00	1	-32.89	9	0.00	11	0.00	3
308	-53	-9	Min.	7.37					0.45	13			0.10	13		
308	-53	-9	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	3
309	-10	-56	Max	0.00	85.00	13	5.89	5	8.83	1	52.47	9	-33.57	13	0.00	1
309	-10	-56	Max	150.00	16.07	13	5.89	5	0.00	1	12.68	9	0.00	13	0.00	1
309	-10	-56	Min.	0.00	79.11	9	-5.89	1	-8.83	5	42.28	13	-48.86	9	0.00	1
309	-10	-56	Min.	150.00	10.18	9	-5.89	1	0.00	5	2.48	13	0.00	9	0.00	1
309	-55	-10	Max	0.00	-6.33	9	13.59	1	0.00	5	4.19	13	0.00	9	0.00	3
309	-55	-10	Max	15.79					0.64	13			0.33	13		
309	-55	-10	Max	150.00	-75.26	9	13.59	1	20.38	1	-35.61	13	-23.56	13	0.00	3
309	-55	-10	Min.	0.00	-19.92	13	-13.59	5	0.00	3	-19.35	9	0.00	13	0.00	5
309	-55	-10	Min.	15.79					0.64	13			0.33	13		
309	-55	-10	Min.	150.00	-88.85	13	-13.59	5	-20.38	5	-59.14	9	-58.87	9	0.00	5
310	-11	-58	Max	0.00	85.00	13	5.89	5	8.83	1	52.47	9	-33.57	13	0.00	1
310	-11	-58	Max	150.00	16.07	13	5.89	5	0.00	1	12.68	9	0.00	13	0.00	1
310	-11	-58	Min.	0.00	79.11	9	-5.89	1	-8.83	5	42.28	13	-48.86	9	0.00	1
310	-11	-58	Min.	150.00	10.18	9	-5.89	1	0.00	5	2.48	13	0.00	9	0.00	1
310	-57	-11	Max	0.00	-6.33	9	13.59	1	0.00	1	4.19	13	0.00	5	0.00	5
310	-57	-11	Max	15.79					0.64	13			0.33	13		
310	-57	-11	Max	150.00	-75.26	9	13.59	1	20.38	1	-35.61	13	-23.56	13	0.00	5
310	-57	-11	Min.	0.00	-19.92	13	-13.59	5	0.00	5	-19.35	9	0.00	1	0.00	1
310	-57	-11	Min.	15.79					0.64	13			0.33	13		
310	-57	-11	Min.	150.00	-88.85	13	-13.59	5	-20.38	5	-59.14	9	-58.87	9	0.00	1
311	-12	-60	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
311	-12	-60	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
311	-12	-60	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
311	-12	-60	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
311	-59	-12	Max	0.00	-16.01	9	20.48	1	0.00	1	2.58	13	0.00	5	0.00	1
311	-59	-12	Max	7.37					0.45	13			0.10	13		
311	-59	-12	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	1
311	-59	-12	Min.	0.00	-36.49	13	-20.48	5	0.00	5	-32.89	9	0.00	1	0.00	5
311	-59	-12	Min.	7.37					0.45	13			0.10	13		
311	-59	-12	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	5
312	-13	-62	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
312	-13	-62	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
312	-13	-62	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
312	-13	-62	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
312	-61	-13	Max	0.00	-16.01	9	20.48	1	0.00	5	2.58	13	0.00	11	0.00	3
312	-61	-13	Max	7.37					0.45	13			0.10	13		
312	-61	-13	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	3
312	-61	-13	Min.	0.00	-36.49	13	-20.48	5	0.00	1	-32.89	9	0.00	13	0.00	5
312	-61	-13	Min.	7.37					0.45	13			0.10	13		
312	-61	-13	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	5
313	-14	-64	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
313	-14	-64	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
313	-14	-64	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
313	-14	-64	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
313	-63	-14	Max	0.00	-16.01	9	20.48	1	0.00	5	2.58	13	0.00	15	0.00	5
313	-63	-14	Max	7.37					0.45	13			0.10	13		
313	-63	-14	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	5
313	-63	-14	Min.	0.00	-36.49	13	-20.48	5	0.00	3	-32.89	9	0.00	9	0.00	3
313	-63	-14	Min.	7.37					0.45	13			0.10	13		
313	-63	-14	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	3
314	-15	-66	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
314	-15	-66	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
314	-15	-66	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
314	-15	-66	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
314	-65	-15	Max	0.00	-16.01	9	20.48	1	0.00	1	2.58	13	0.00	11	0.00	7
314	-65	-15	Max	7.37					0.45	13			0.10	13		
314	-65	-15	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	7
314	-65	-15	Min.	0.00	-36.49	13	-20.48	5	0.00	7	-32.89	9	0.00	13	0.00	1
314	-65	-15	Min.	7.37					0.45	13			0.10	13		
314	-65	-15	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	1
316	-26	-74	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
316	-26	-74	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
316	-26	-74	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
316	-26	-74	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
316	-73	-26	Max	0.00	-16.01	9	20.48	1	0.00	5	2.58	13	0.00	1	0.00	1

316	-73	-26	Max	7.37				0.45	13			0.10	13			
316	-73	-26	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	1
316	-73	-26	Min.	0.00	-36.49	13	-20.48	5	0.00	1	-32.89	9	0.00	1	0.00	5
316	-73	-26	Min.	7.37				0.45	13			0.10	13			
316	-73	-26	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	5
317	-18	-71	Max	0.00	85.00	13	5.89	5	8.83	1	52.47	9	-33.57	13	0.00	1
317	-18	-71	Max	150.00	16.07	13	5.89	5	0.00	1	12.68	9	0.00	13	0.00	1
317	-18	-71	Min.	0.00	79.11	9	-5.89	1	-8.83	5	42.28	13	-48.86	9	0.00	1
317	-18	-71	Min.	150.00	10.18	9	-5.89	1	0.00	5	2.48	13	0.00	9	0.00	1
317	-70	-18	Max	0.00	-6.33	9	13.59	1	0.00	5	4.19	13	0.00	11	0.00	7
317	-70	-18	Max	15.79				0.64	13			0.33	13			
317	-70	-18	Max	150.00	-75.26	9	13.59	1	20.38	1	-35.61	13	-23.56	13	0.00	7
317	-70	-18	Min.	0.00	-19.92	13	-13.59	5	0.00	3	-19.35	9	0.00	13	0.00	1
317	-70	-18	Min.	15.79				0.64	13			0.33	13			
317	-70	-18	Min.	150.00	-88.85	13	-13.59	5	-20.38	5	-59.14	9	-58.87	9	0.00	1
318	201	-81	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
318	201	-81	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
318	201	-81	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
318	201	-81	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
318	-80	201	Max	0.00	-16.01	9	20.48	1	0.00	5	2.58	13	0.00	13	0.00	1
318	-80	201	Max	7.37				0.45	13			0.10	13			
318	-80	201	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	1
318	-80	201	Min.	0.00	-36.49	13	-20.48	5	0.00	3	-32.89	9	0.00	9	0.00	7
318	-80	201	Min.	7.37				0.45	13			0.10	13			
318	-80	201	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	7
319	-77	-79	Max	0.00	121.64	13	8.87	5	13.31	1	75.35	9	-50.59	13	0.00	1
319	-77	-79	Max	150.00	30.69	13	8.87	5	0.00	1	22.84	9	0.00	13	0.00	1
319	-77	-79	Min.	0.00	112.77	9	-8.87	1	-13.31	5	59.99	13	-73.64	9	0.00	1
319	-77	-79	Min.	150.00	21.82	9	-8.87	1	0.00	5	7.47	13	0.00	9	0.00	1
319	-78	-77	Max	0.00	-16.01	9	20.48	1	0.00	5	2.58	13	0.00	9	0.00	5
319	-78	-77	Max	7.37				0.45	13			0.10	13			
319	-78	-77	Max	150.00	-106.97	9	20.48	1	30.72	1	-49.93	13	-35.52	13	0.00	5
319	-78	-77	Min.	0.00	-36.49	13	-20.48	5	0.00	3	-32.89	9	0.00	13	0.00	3
319	-78	-77	Min.	7.37				0.45	13			0.10	13			
319	-78	-77	Min.	150.00	-127.45	13	-20.48	5	-30.72	5	-85.41	9	-88.72	9	0.00	3

Tipo di combinazione di carico: SLD

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	315	-45	Max	0.00	-1894.62	2	78.93	2	421.45	6	171.41	10	613.61	16	0.08	12
1	315	-45	Max	328.50	-1656.55	2	78.93	2	38.82	2	171.41	10	51.55	14	0.08	12
1	315	-45	Min.	0.00	-2022.05	6	-265.23	6	-220.46	2	-171.41	16	-613.61	10	-0.08	14
1	315	-45	Min.	328.50	-1783.99	6	-265.23	6	-449.84	6	-171.41	16	-51.54	12	-0.08	14
2	2	202	Max	0.00	-2569.15	2	221.04	2	374.04	6	225.04	12	752.17	14	0.00	2
2	2	202	Max	328.50	-2331.08	2	221.04	2	352.08	2	225.04	12	12.91	16	0.00	2
2	2	202	Min.	0.00	-2569.15	2	-221.04	6	-374.04	2	-225.04	14	-752.17	10	0.00	8
2	2	202	Min.	328.50	-2331.08	2	-221.04	6	-352.08	6	-225.04	14	-12.91	10	0.00	8
3	3	203	Max	0.00	-1894.62	6	265.23	2	220.45	6	171.41	12	613.61	14	0.08	16
3	3	203	Max	328.50	-1656.55	6	265.23	2	449.84	2	171.41	12	51.55	16	0.08	16
3	3	203	Min.	0.00	-2022.05	2	-78.93	6	-421.45	2	-171.41	14	-613.61	12	-0.08	10
3	3	203	Min.	328.50	-1783.99	2	-78.93	6	-38.82	8	-171.41	14	-51.54	10	-0.08	10
201	-3	-29	Max	0.00	23.17	6	23.17	10	3.01	2	-189.50	2	5.21	2	5.21	10
201	-3	-29	Max	135.63	23.17	6	23.17	10	32.33	10	-313.01	2	-335.57	2	5.21	10
201	-3	-29	Min.	0.00	-23.17	2	-23.17	14	-3.01	6	-189.50	2	-5.21	6	-5.21	14
201	-3	-29	Min.	135.63	-23.17	2	-23.17	14	-32.33	16	-313.01	2	-345.98	6	-5.21	14
201	-29	-45	Max	0.00	57.35	6	57.35	10	33.69	10	-583.68	2	-327.72	2	13.05	10
201	-29	-45	Max	83.77	57.35	6	57.35	10	81.73	10	-659.97	2	-848.63	2	13.05	10
201	-29	-45	Min.	0.00	-57.35	2	-57.35	14	-33.69	16	-583.68	2	-353.83	6	-13.05	14
201	-29	-45	Min.	83.77	-57.35	2	-57.35	14	-81.73	16	-659.97	2	-874.74	6	-13.05	14
201	-45	201	Max	0.00	4.91	2	97.39	16	81.80	10	1124.02	6	-809.81	2	38.49	14
201	-45	201	Max	51.86	4.91	2	97.39	16	31.30	10	1076.80	6	-305.25	2	38.49	14
201	-45	201	Min.	0.00	-191.21	6	-97.39	10	-81.80	16	996.59	2	-1324.58	6	-38.49	12
201	-45	201	Min.	51.86	-191.21	6	-97.39	10	-31.30	16	949.37	2	-753.93	6	-38.49	12
201	-6	201	Max	0.00	-27.93	2	64.55	16	32.66	10	806.12	6	-297.40	2	30.64	14
201	201	-6	Max	135.63	-27.93	2	64.55	16	57.15	14	682.62	6	539.34	2	30.64	14
201	201	-6	Min.	0.00	-158.38	6	-64.55	10	-32.66	16	678.69	2	-761.77	6	-30.64	12
201	201	-6	Min.	135.63	-158.38	6	-64.55	10	-57.15	12	555.18	2	247.80	6	-30.64	12
201	-6	-7	Max	0.00	-64.28	2	28.20	16	58.51	14	411.93	6	547.21	2	22.80	14
201	-6	-7	Max	135.63	-64.28	2	28.20	16	93.16	14	288.43	6	849.33	2	22.80	14
201	-6	-7	Min.	0.00	-122.03	6	-28.20	10	-58.51	12	284.50	2	239.98	6	-22.80	12
201	-6	-7	Min.	135.63	-122.03	6	-28.20	10	-93.16	12	161.00	2	714.92	6	-22.80	12
201	-7	-8	Max	0.00	-85.68	6	10.81	12	94.52	14	17.76	6	857.16	2	14.95	14
201	-7	-8	Max	19.50				-33.14	6			708.78	6			
201	-7	-8	Max	135.63	-85.68	6	10.81	12	79.86	14	-105.74	6	647.39	6	14.95	14
201	-7	-8	Min.	0.00	-100.63	2	-10.81	14	-94.52	12	-109.67	2	707.05	6	-14.95	12

201	-7	-8	Min.	19.50					-33.14	6			708.78	6			
201	-7	-8	Min.	135.63	-100.63	2		-10.81	14	-79.86	12	-233.17	2	624.66	2	-14.95	12
201	-8	-9	Max	0.00	-49.32	6		47.16	12	81.22	14	-376.42	6	639.54	6	7.10	14
201	-8	-9	Max	135.63	-49.32	6		47.16	12	17.65	16	-499.93	6	45.25	6	7.10	14
201	-8	-9	Min.	0.00	-136.98	2		-47.16	14	-81.22	12	-503.85	2	632.50	2	-7.10	12
201	-8	-9	Min.	135.63	-136.98	2		-47.16	14	-17.65	10	-627.36	2	-134.62	2	-7.10	12
201	-9	-10	Max	0.00	-12.97	6		83.51	12	18.62	14	-770.60	6	37.39	6	2.04	2
201	-9	-10	Max	135.63	-12.97	6		83.51	12	94.64	12	-894.11	6	-1091.52	6	2.04	2
201	-9	-10	Min.	0.00	-173.33	2		-83.51	14	-18.62	12	-898.04	2	-126.78	2	-2.04	8
201	-9	-10	Min.	135.63	-173.33	2		-83.51	14	-94.64	14	-1021.54	2	-1428.52	2	-2.04	8
201	-10	202	Max	0.00	11.04	6		107.52	12	94.27	10	-1083.61	6	-1096.74	6	6.95	10
201	-10	202	Max	20.00	11.04	6		107.52	12	115.25	12	-1101.82	6	-1315.28	6	6.95	10
201	-10	202	Min.	0.00	-197.34	2		-107.52	14	-94.27	16	-1211.04	2	-1423.33	2	-6.95	16
201	-10	202	Min.	20.00	-197.34	2		-107.52	14	-115.25	14	-1229.26	2	-1667.37	2	-6.95	16
202	202	-11	Max	0.00	11.04	2		107.52	16	115.25	10	1229.26	6	-1315.28	2	6.95	14
202	202	-11	Max	20.00	11.04	2		107.52	16	94.27	12	1211.05	6	-1096.73	2	6.95	14
202	202	-11	Min.	0.00	-197.34	6		-107.52	10	-115.25	16	1101.83	2	-1667.36	6	-6.95	12
202	202	-11	Min.	20.00	-197.34	6		-107.52	10	-94.27	14	1083.61	2	-1423.33	6	-6.95	12
202	-11	-12	Max	0.00	-12.97	2		83.51	16	94.64	10	1021.54	6	-1091.53	2	2.04	4
202	-11	-12	Max	135.63	-12.97	2		83.51	16	18.62	16	898.04	6	37.38	2	2.04	4
202	-11	-12	Min.	0.00	-173.33	6		-83.51	10	-94.64	16	894.11	2	-1428.54	6	-2.04	6
202	-11	-12	Min.	135.63	-173.33	6		-83.51	10	-18.62	10	770.61	2	-126.79	6	-2.04	6
202	-12	-13	Max	0.00	-49.32	2		47.16	16	17.65	14	627.36	6	45.24	2	7.10	10
202	-12	-13	Max	135.63	-49.32	2		47.16	16	81.22	16	503.86	6	639.53	2	7.10	10
202	-12	-13	Min.	0.00	-136.98	6		-47.16	10	-17.65	12	499.93	2	-134.63	6	-7.10	16
202	-12	-13	Min.	135.63	-136.98	6		-47.16	10	-81.22	10	376.42	2	632.50	6	-7.10	16
202	-13	-14	Max	0.00	-85.68	2		10.81	16	79.86	16	233.18	6	647.39	2	14.95	10
202	-13	-14	Max	116.13					-33.15	2				708.79	2		
202	-13	-14	Max	135.63	-85.68	2		10.81	16	94.52	16	109.67	6	857.16	6	14.95	10
202	-13	-14	Min.	0.00	-100.63	6		-10.81	10	-79.86	10	105.74	2	624.66	6	-14.95	16
202	-13	-14	Min.	116.13						-33.15	2			708.79	2		
202	-13	-14	Min.	135.63	-100.63	6		-10.81	10	-94.52	10	-17.76	2	707.05	2	-14.95	16
202	-14	-15	Max	0.00	-64.28	6		28.20	12	93.16	16	-161.01	6	849.31	6	22.80	10
202	-14	-15	Max	135.63	-64.28	6		28.20	12	58.51	16	-284.51	6	547.19	6	22.80	10
202	-14	-15	Min.	0.00	-122.03	2		-28.20	14	-93.16	10	-288.44	2	714.90	2	-22.80	16
202	-14	-15	Min.	135.63	-122.03	2		-28.20	14	-58.51	10	-411.94	2	239.94	2	-22.80	16
202	-15	-77	Max	0.00	-27.93	6		64.55	12	57.15	16	-555.18	6	539.37	6	30.64	10
202	-15	-77	Max	135.63	-27.93	6		64.55	12	32.66	12	-678.68	6	-297.37	6	30.64	10
202	-15	-77	Min.	0.00	-158.38	2		-64.55	14	-57.15	10	-682.61	2	247.83	2	-30.64	16
202	-15	-77	Min.	135.63	-158.38	2		-64.55	14	-32.66	14	-806.12	2	-761.74	2	-30.64	16
202	-77	203	Max	0.00	4.91	6		97.39	12	31.30	12	-949.36	6	-305.23	6	38.49	10
202	-77	203	Max	51.86	4.91	6		97.39	12	81.80	12	-996.58	6	-809.78	6	38.49	10
202	-77	203	Min.	0.00	-191.21	2		-97.39	14	-31.30	14	-1076.79	2	-753.91	2	-38.49	16
202	-77	203	Min.	51.86	-191.21	2		-97.39	14	-81.80	14	-1124.02	2	-1324.55	2	-38.49	16
202	203	-26	Max	0.00	57.35	2		57.35	14	81.73	12	659.97	2	-848.63	6	13.05	14
202	203	-26	Max	83.77	57.35	2		57.35	14	33.69	12	583.68	2	-327.72	6	13.05	14
202	203	-26	Min.	0.00	-57.35	6		-57.35	10	-81.73	14	659.97	2	-874.74	2	-13.05	10
202	203	-26	Min.	83.77	-57.35	6		-57.35	10	-33.69	14	583.68	2	-353.83	2	-13.05	10
202	-26	-18	Max	0.00	23.17	2		23.17	14	32.33	12	313.01	2	-335.57	6	5.21	14
202	-26	-18	Max	135.63	23.17	2		23.17	14	3.01	6	189.50	2	5.20	6	5.21	14
202	-26	-18	Min.	0.00	-23.17	6		-23.17	10	-32.33	14	313.01	2	-345.99	2	-5.21	10
202	-26	-18	Min.	135.63	-23.17	6		-23.17	10	-3.01	4	189.50	2	-5.21	2	-5.21	10
302	-3	-69	Max	0.00	83.59	14		3.06	6	4.60	2	50.03	10	-37.24	14	0.00	2
302	-3	-69	Max	150.00	14.66	14		3.06	6	0.00	2	10.23	10	0.00	14	0.00	2
302	-3	-69	Min.	0.00	80.53	10		-3.06	2	-4.60	6	44.72	14	-45.20	10	0.00	2
302	-3	-69	Min.	150.00	11.59	10		-3.06	2	0.00	6	4.92	14	0.00	10	0.00	2
302	-68	-3	Max	0.00	-9.59	10		7.07	2	0.00	8	-1.45	14	0.00	10	0.00	8
302	-68	-3	Max	150.00	-78.52	10		7.07	2	10.61	2	-41.25	14	-32.03	14	0.00	8
302	-68	-3	Min.	0.00	-16.66	14		-7.07	6	0.00	2	-13.70	10	0.00	16	0.00	2
302	-68	-3	Min.	150.00	-85.59	14		-7.07	6	-10.61	6	-53.50	10	-50.40	10	0.00	2
303	-29	-76	Max	0.00	119.52	14		4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
303	-29	-76	Max	150.00	28.56	14		4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
303	-29	-76	Min.	0.00	114.90	10		-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
303	-29	-76	Min.	150.00	23.94	10		-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
303	-75	-29	Max	0.00	-20.92	10		10.66	2	0.00	8	-5.93	14	0.00	10	0.00	6
303	-75	-29	Max	150.00	-111.88	10		10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	6
303	-75	-29	Min.	0.00	-31.58	14		-10.66	6	0.00	2	-24.39	10	0.00	14	0.00	4
303	-75	-29	Min.	150.00	-122.54	14		-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	4
305	-6	-48	Max	0.00	119.52	14		4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
305	-6	-48	Max	150.00	28.56	14		4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
305	-6	-48	Min.	0.00	114.90	10		-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
305	-6	-48	Min.	150.00	23.94	10		-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
305	-47	-6	Max	0.00	-20.92	10		10.66	2	0.00	6	-5.93	14	0.00	12	0.00	2
305	-47	-6	Max	150.00	-111.88	10		10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	2
305	-47	-6	Min.	0.00	-31.58	14		-10.66	6	0.00	4	-24.39	10	0.00	14	0.00	6
305	-47	-6	Min.	150.00	-122.54	14		-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	6

306	-7	-50	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
306	-7	-50	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
306	-7	-50	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
306	-7	-50	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
306	-49	-7	Max	0.00	-20.92	10	10.66	2	0.00	8	-5.93	14	0.00	12	0.00	2
306	-49	-7	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	2
306	-49	-7	Min.	0.00	-31.58	14	-10.66	6	0.00	2	-24.39	10	0.00	14	0.00	8
306	-49	-7	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	8
307	-8	-52	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
307	-8	-52	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
307	-8	-52	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
307	-8	-52	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
307	-51	-8	Max	0.00	-20.92	10	10.66	2	0.00	2	-5.93	14	0.00	10	0.00	6
307	-51	-8	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	6
307	-51	-8	Min.	0.00	-31.58	14	-10.66	6	0.00	8	-24.39	10	0.00	16	0.00	4
307	-51	-8	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	4
308	-9	-54	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
308	-9	-54	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
308	-9	-54	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
308	-9	-54	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
308	-53	-9	Max	0.00	-20.92	10	10.66	2	0.00	6	-5.93	14	0.00	14	0.00	6
308	-53	-9	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	6
308	-53	-9	Min.	0.00	-31.58	14	-10.66	6	0.00	2	-24.39	10	0.00	12	0.00	4
308	-53	-9	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	4
309	-10	-56	Max	0.00	83.59	14	3.06	6	4.60	2	50.03	10	-37.24	14	0.00	2
309	-10	-56	Max	150.00	14.66	14	3.06	6	0.00	2	10.23	10	0.00	14	0.00	2
309	-10	-56	Min.	0.00	80.53	10	-3.06	2	-4.60	6	44.72	14	-45.20	10	0.00	2
309	-10	-56	Min.	150.00	11.59	10	-3.06	2	0.00	6	4.92	14	0.00	10	0.00	2
309	-55	-10	Max	0.00	-9.59	10	7.07	2	0.00	6	-1.45	14	0.00	10	0.00	4
309	-55	-10	Max	150.00	-78.52	10	7.07	2	10.61	2	-41.25	14	-32.03	14	0.00	4
309	-55	-10	Min.	0.00	-16.66	14	-7.07	6	0.00	4	-13.70	10	0.00	14	0.00	6
309	-55	-10	Min.	150.00	-85.59	14	-7.07	6	-10.61	6	-53.50	10	-50.40	10	0.00	6
310	-11	-58	Max	0.00	83.59	14	3.06	6	4.60	2	50.03	10	-37.24	14	0.00	2
310	-11	-58	Max	150.00	14.66	14	3.06	6	0.00	2	10.23	10	0.00	14	0.00	2
310	-11	-58	Min.	0.00	80.53	10	-3.06	2	-4.60	6	44.72	14	-45.20	10	0.00	2
310	-11	-58	Min.	150.00	11.59	10	-3.06	2	0.00	6	4.92	14	0.00	10	0.00	2
310	-57	-11	Max	0.00	-9.59	10	7.07	2	0.00	2	-1.45	14	0.00	6	0.00	6
310	-57	-11	Max	150.00	-78.52	10	7.07	2	10.61	2	-41.25	14	-32.03	14	0.00	6
310	-57	-11	Min.	0.00	-16.66	14	-7.07	6	0.00	6	-13.70	10	0.00	2	0.00	2
310	-57	-11	Min.	150.00	-85.59	14	-7.07	6	-10.61	6	-53.50	10	-50.40	10	0.00	2
311	-12	-60	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
311	-12	-60	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
311	-12	-60	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
311	-12	-60	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
311	-59	-12	Max	0.00	-20.92	10	10.66	2	0.00	2	-5.93	14	0.00	6	0.00	2
311	-59	-12	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	2
311	-59	-12	Min.	0.00	-31.58	14	-10.66	6	0.00	6	-24.39	10	0.00	2	0.00	6
311	-59	-12	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	6
312	-13	-62	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
312	-13	-62	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
312	-13	-62	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
312	-13	-62	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
312	-61	-13	Max	0.00	-20.92	10	10.66	2	0.00	6	-5.93	14	0.00	12	0.00	4
312	-61	-13	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	4
312	-61	-13	Min.	0.00	-31.58	14	-10.66	6	0.00	2	-24.39	10	0.00	14	0.00	6
312	-61	-13	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	6
313	-14	-64	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
313	-14	-64	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
313	-14	-64	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
313	-14	-64	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
313	-63	-14	Max	0.00	-20.92	10	10.66	2	0.00	6	-5.93	14	0.00	16	0.00	6
313	-63	-14	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	6
313	-63	-14	Min.	0.00	-31.58	14	-10.66	6	0.00	4	-24.39	10	0.00	10	0.00	4
313	-63	-14	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	4
314	-15	-66	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
314	-15	-66	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
314	-15	-66	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
314	-15	-66	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
314	-65	-15	Max	0.00	-20.92	10	10.66	2	0.00	2	-5.93	14	0.00	10	0.00	8
314	-65	-15	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	8
314	-65	-15	Min.	0.00	-31.58	14	-10.66	6	0.00	8	-24.39	10	0.00	14	0.00	2
314	-65	-15	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	2
316	-26	-74	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
316	-26	-74	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
316	-26	-74	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
316	-26	-74	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2

316	-73	-26	Max	0.00	-20.92	10	10.66	2	0.00	6	-5.93	14	0.00	2	0.00	2
316	-73	-26	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	2
316	-73	-26	Min.	0.00	-31.58	14	-10.66	6	0.00	2	-24.39	10	0.00	2	0.00	6
316	-73	-26	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	6
317	-18	-71	Max	0.00	83.59	14	3.06	6	4.60	2	50.03	10	-37.24	14	0.00	2
317	-18	-71	Max	150.00	14.66	14	3.06	6	0.00	2	10.23	10	0.00	14	0.00	2
317	-18	-71	Min.	0.00	80.53	10	-3.06	2	-4.60	6	44.72	14	-45.20	10	0.00	2
317	-18	-71	Min.	150.00	11.59	10	-3.06	2	0.00	6	4.92	14	0.00	10	0.00	2
317	-70	-18	Max	0.00	-9.59	10	7.07	2	0.00	6	-1.45	14	0.00	12	0.00	8
317	-70	-18	Max	150.00	-78.52	10	7.07	2	10.61	2	-41.25	14	-32.03	14	0.00	8
317	-70	-18	Min.	0.00	-16.66	14	-7.07	6	0.00	4	-13.70	10	0.00	14	0.00	2
317	-70	-18	Min.	150.00	-85.59	14	-7.07	6	-10.61	6	-53.50	10	-50.40	10	0.00	2
318	201	-81	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
318	201	-81	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
318	201	-81	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
318	201	-81	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
318	-80	201	Max	0.00	-20.92	10	10.66	2	0.00	6	-5.93	14	0.00	14	0.00	2
318	-80	201	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	2
318	-80	201	Min.	0.00	-31.58	14	-10.66	6	0.00	4	-24.39	10	0.00	10	0.00	8
318	-80	201	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	8
319	-77	-79	Max	0.00	119.52	14	4.62	6	6.93	2	71.67	10	-56.12	14	0.00	2
319	-77	-79	Max	150.00	28.56	14	4.62	6	0.00	2	19.16	10	0.00	14	0.00	2
319	-77	-79	Min.	0.00	114.90	10	-4.62	2	-6.93	6	63.67	14	-68.12	10	0.00	2
319	-77	-79	Min.	150.00	23.94	10	-4.62	2	0.00	6	11.16	14	0.00	10	0.00	2
319	-78	-77	Max	0.00	-20.92	10	10.66	2	0.00	6	-5.93	14	0.00	10	0.00	6
319	-78	-77	Max	150.00	-111.88	10	10.66	2	15.99	2	-58.44	14	-48.27	14	0.00	6
319	-78	-77	Min.	0.00	-31.58	14	-10.66	6	0.00	4	-24.39	10	0.00	14	0.00	4
319	-78	-77	Min.	150.00	-122.54	14	-10.66	6	-15.99	6	-76.90	10	-75.97	10	0.00	4

Tipo di combinazione di carico: SLU

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	315	-45	Max	0.00	-839.55	21	-5.63	21	242.45	28	2315.57	28	11016.30	21	1.29	28
1	315	-45	Max	328.50	-530.06	21	-5.63	21	-12.41	21	2315.57	28	299.93	21	1.29	28
1	315	-45	Min.	0.00	-4077.14	28	-224.73	28	6.07	21	-3262.21	21	-7819.54	28	-1.82	21
1	315	-45	Min.	328.50	-3767.65	28	-224.73	28	-495.79	28	-3262.21	21	-212.89	28	-1.82	21
2	2	202	Max	0.00	-1056.68	21	-0.00	21	0.00	28	3139.94	28	13931.70	21	0.00	28
2	2	202	Max	328.50	-747.19	21	-0.00	21	0.00	21	3139.94	28	425.80	28	0.00	28
2	2	202	Min.	0.00	-5388.96	28	-0.00	28	0.00	21	-4423.60	21	-9888.92	28	0.00	21
2	2	202	Min.	328.50	-5079.47	28	-0.00	28	-0.00	28	-4423.60	21	-599.87	21	0.00	21
3	3	203	Max	0.00	-839.55	21	224.73	28	-6.07	21	2315.57	28	11016.30	21	1.82	21
3	3	203	Max	328.50	-530.06	21	224.73	28	495.79	28	2315.57	28	299.93	21	1.82	21
3	3	203	Min.	0.00	-4077.14	28	5.62	21	-242.45	28	-3262.21	21	-7819.54	28	-1.29	28
3	3	203	Min.	328.50	-3767.66	28	5.62	21	12.41	21	-3262.21	21	-212.90	28	-1.29	28
201	-3	-29	Max	0.00	0.00	17	277.54	28	0.00	28	-42.93	21	0.00	28	0.00	21
201	-3	-29	Max	135.63	0.00	17	277.54	28	376.42	28	-203.49	21	-167.11	21	0.00	21
201	-3	-29	Min.	0.00	0.00	17	-391.00	21	0.00	21	-428.92	28	0.00	17	0.00	17
201	-3	-29	Min.	135.63	0.00	17	-391.00	21	-530.31	21	-589.47	28	-690.61	28	0.00	17
201	-29	-45	Max	0.00	0.00	17	832.62	28	376.42	28	-148.53	21	-167.11	21	0.00	21
201	-29	-45	Max	83.77	0.00	17	832.62	28	1073.91	28	-247.69	21	-333.07	21	0.00	21
201	-29	-45	Min.	0.00	0.00	17	-1173.00	21	-530.31	21	-1306.47	28	-690.61	28	0.00	29
201	-29	-45	Min.	83.77	0.00	17	-1173.00	21	-1512.94	21	-1405.64	28	-1826.59	28	0.00	29
201	-45	201	Max	0.00	-5.63	21	2089.21	21	1075.20	28	2362.02	28	-345.48	21	299.93	21
201	-45	201	Max	51.86	-5.63	21	2089.21	21	306.18	28	2300.63	28	-214.97	21	299.93	21
201	-45	201	Min.	0.00	-224.73	28	-1482.95	28	-1514.76	21	282.37	21	-2322.37	28	-212.90	28
201	-45	201	Min.	51.86	-224.73	28	-1482.95	28	-431.35	21	220.98	21	-1113.41	28	-212.90	28
201	201	-6	Max	0.00	-5.63	21	1307.20	21	306.17	28	1583.63	28	-214.97	21	299.93	21
201	201	-6	Max	135.63	-5.63	21	1307.20	21	1341.60	21	1423.07	28	925.58	28	299.93	21
201	201	-6	Min.	0.00	-224.73	28	-927.88	28	-431.34	21	275.94	21	-1113.40	28	-212.90	28
201	201	-6	Min.	135.63	-224.73	28	-927.88	28	-952.29	28	115.39	21	50.41	21	-212.90	28
201	-6	-7	Max	0.00	-5.63	21	525.20	21	1341.65	21	706.07	28	925.63	28	299.93	21
201	-6	-7	Max	135.63	-5.63	21	525.20	21	2053.98	21	545.52	28	1774.38	28	299.93	21
201	-6	-7	Min.	0.00	-224.73	28	-372.80	28	-952.33	28	170.34	21	50.41	21	-212.90	28
201	-6	-7	Min.	135.63	-224.73	28	-372.80	28	-1457.95	28	9.79	21	172.57	21	-212.90	28
201	-7	-8	Max	0.00	-5.63	21	182.28	28	2053.93	21	64.76	21	1774.33	28	299.93	21
201	-7	-8	Max	4.87					1224.85	22			572.70	22		
201	-7	-8	Max	135.63	-5.63	21	182.28	28	1705.64	21	-95.79	21	1432.89	28	299.93	21
201	-7	-8	Min.	0.00	-224.73	28	-256.80	21	-1457.91	28	-171.47	28	172.57	21	-212.90	28
201	-7	-8	Min.	54.63					1913.65	21			190.28	21		
201	-7	-8	Min.	135.63	-224.73	28	-256.80	21	-1210.69	28	-332.03	28	151.52	21	-212.90	28
201	-8	-9	Max	0.00	-5.63	21	737.36	28	1705.64	21	-40.84	21	1432.88	28	299.93	21
201	-8	-9	Max	135.63	-5.63	21	737.36	28	296.74	21	-201.39	21	-12.74	21	299.93	21
201	-8	-9	Min.	0.00	-224.73	28	-1038.80	21	-1210.69	28	-1049.03	28	151.52	21	-212.90	28
201	-8	-9	Min.	135.63	-224.73	28	-1038.80	21	-210.63	28	-1209.59	28	-98.78	28	-212.90	28
201	-9	-10	Max	0.00	-5.63	21	1292.43	28	296.72	21	-146.43	21	-12.75	21	299.93	21

201	-9	-10	Max	135.63	-5.63	21	1292.43	28	1542.29	28	-306.99	21	-320.23	21	299.93	21
201	-9	-10	Min.	0.00	-224.73	28	-1820.80	21	-210.62	28	-1926.59	28	-98.80	28	-212.90	28
201	-9	-10	Min.	135.63	-224.73	28	-1820.80	21	-2172.80	21	-2087.14	28	-2820.68	28	-212.90	28
201	-10	202	Max	0.00	-5.63	21	1569.97	28	1542.31	28	-349.92	21	-320.23	21	299.93	21
201	-10	202	Max	20.00	-5.63	21	1569.97	28	1856.31	28	-373.60	21	-392.58	21	299.93	21
201	-10	202	Min.	0.00	-224.73	28	-2211.80	21	-2172.83	21	-2516.06	28	-2820.71	28	-212.90	28
201	-10	202	Min.	20.00	-224.73	28	-2211.80	21	-2615.19	21	-2539.73	28	-3326.30	28	-212.90	28
202	202	-11	Max	0.00	-5.63	21	2211.80	21	1856.30	28	2539.74	28	-392.58	21	212.90	28
202	202	-11	Max	20.00	-5.63	21	2211.80	21	1542.31	28	2516.06	28	-320.23	21	212.90	28
202	202	-11	Min.	0.00	-224.73	28	-1569.97	28	-2615.19	21	373.60	21	-3326.30	28	-299.93	21
202	202	-11	Min.	20.00	-224.73	28	-1569.97	28	-2172.82	21	349.92	21	-2820.71	28	-299.93	21
202	-11	-12	Max	0.00	-5.63	21	1820.80	21	1542.31	28	2087.15	28	-320.23	21	212.90	28
202	-11	-12	Max	135.63	-5.63	21	1820.80	21	296.70	21	1926.59	28	-12.75	21	212.90	28
202	-11	-12	Min.	0.00	-224.73	28	-1292.43	28	-2172.83	21	306.99	21	-2820.72	28	-299.93	21
202	-11	-12	Min.	135.63	-224.73	28	-1292.43	28	-210.60	28	146.43	21	-98.83	28	-299.93	21
202	-12	-13	Max	0.00	-5.63	21	1038.80	21	296.72	21	1209.59	28	-12.75	21	212.90	28
202	-12	-13	Max	135.63	-5.63	21	1038.80	21	1705.63	21	1049.04	28	1432.87	28	212.90	28
202	-12	-13	Min.	0.00	-224.73	28	-737.36	28	-210.62	28	201.39	21	-98.80	28	-299.93	21
202	-12	-13	Min.	135.63	-224.73	28	-737.36	28	-1210.69	28	40.84	21	151.52	21	-299.93	21
202	-13	-14	Max	0.00	-5.63	21	256.80	21	1705.65	21	332.03	28	1432.89	28	212.90	28
202	-13	-14	Max	130.76					1224.86	22			572.70	22		
202	-13	-14	Max	135.63	-5.63	21	256.80	21	2053.94	21	171.48	28	1774.34	28	212.90	28
202	-13	-14	Min.	0.00	-224.73	28	-182.28	28	-1210.70	28	95.80	21	151.52	21	-299.93	21
202	-13	-14	Min.	81.00					1913.66	21			190.28	21		
202	-13	-14	Min.	135.63	-224.73	28	-182.28	28	-1457.92	28	-64.76	21	172.57	21	-299.93	21
202	-14	-15	Max	0.00	-5.63	21	372.80	28	2053.94	21	-9.80	21	1774.34	28	212.90	28
202	-14	-15	Max	135.63	-5.63	21	372.80	28	1341.62	21	-170.35	21	925.58	28	212.90	28
202	-14	-15	Min.	0.00	-224.73	28	-525.20	21	-1457.92	28	-545.52	28	172.57	21	-299.93	21
202	-14	-15	Min.	135.63	-224.73	28	-525.20	21	-952.30	28	-706.08	28	50.40	21	-299.93	21
202	-15	-77	Max	0.00	-5.63	21	927.88	28	1341.66	21	-115.38	21	925.64	28	212.90	28
202	-15	-77	Max	135.63	-5.63	21	927.88	28	306.13	28	-275.94	21	-214.96	21	212.90	28
202	-15	-77	Min.	0.00	-224.73	28	-1307.20	21	-952.34	28	-1423.07	28	50.41	21	-299.93	21
202	-15	-77	Min.	135.63	-224.73	28	-1307.20	21	-431.28	21	-1583.62	28	-1113.33	28	-299.93	21
202	-77	203	Max	0.00	-5.63	21	1482.95	28	306.14	28	-220.98	21	-214.96	21	212.90	28
202	-77	203	Max	51.86	-5.63	21	1482.95	28	1075.16	28	-282.37	21	-345.47	21	212.90	28
202	-77	203	Min.	0.00	-224.73	28	-2089.20	21	-431.30	21	-2300.63	28	-1113.36	28	-299.93	21
202	-77	203	Min.	51.86	-224.73	28	-2089.20	21	-1514.70	21	-2362.02	28	-2322.31	28	-299.93	21
202	203	-26	Max	0.00	0.00	17	1173.00	21	1073.91	28	1405.64	28	-333.07	21	0.00	28
202	203	-26	Max	83.77	0.00	17	1173.00	21	376.42	28	1306.47	28	-167.11	21	0.00	28
202	203	-26	Min.	0.00	0.00	17	-832.62	28	-1512.94	21	247.69	21	-1826.59	28	0.00	21
202	203	-26	Min.	83.77	0.00	17	-832.62	28	-530.30	21	148.53	21	-690.60	28	0.00	21
202	-26	-18	Max	0.00	0.00	17	391.00	21	376.43	28	589.47	28	-167.11	21	0.00	28
202	-26	-18	Max	135.63	0.00	17	391.00	21	0.00	28	428.92	28	0.00	21	0.00	28
202	-26	-18	Min.	0.00	0.00	17	-277.54	28	-530.32	21	203.49	21	-690.62	28	0.00	21
202	-26	-18	Min.	135.63	0.00	17	-277.54	28	-0.01	21	42.94	21	-0.01	28	0.00	21
302	-3	-69	Max	0.00	118.98	22	0.00	17	0.00	17	227.41	28	173.21	21	0.00	17
302	-3	-69	Max	150.00	21.66	22	0.00	17	0.00	17	71.77	28	0.00	21	0.00	17
302	-3	-69	Min.	0.00	116.34	28	0.00	17	0.00	17	-158.57	21	-224.38	28	0.00	17
302	-3	-69	Min.	150.00	20.67	28	0.00	17	0.00	17	-72.36	21	0.00	28	0.00	17
302	-68	-3	Max	0.00	-20.67	21	0.00	17	0.00	17	72.36	21	0.00	28	0.00	17
302	-68	-3	Max	150.00	-116.34	21	0.00	17	0.00	17	158.57	21	173.20	21	0.00	17
302	-68	-3	Min.	0.00	-21.66	17	0.00	17	0.00	17	-71.77	28	0.00	17	0.00	17
302	-68	-3	Min.	150.00	-118.98	17	0.00	17	0.00	17	-227.41	28	-224.38	28	0.00	17
303	-29	-76	Max	0.00	176.97	22	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
303	-29	-76	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
303	-29	-76	Min.	0.00	171.70	28	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
303	-29	-76	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
303	-75	-29	Max	0.00	-41.35	28	0.00	17	0.00	17	144.73	21	0.00	28	0.00	17
303	-75	-29	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
303	-75	-29	Min.	0.00	-43.32	17	0.00	17	0.00	17	-143.55	28	0.00	21	0.00	17
303	-75	-29	Min.	150.00	-176.97	17	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
305	-6	-48	Max	0.00	176.97	22	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
305	-6	-48	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
305	-6	-48	Min.	0.00	171.70	28	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
305	-6	-48	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
305	-47	-6	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	21	0.00	17
305	-47	-6	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
305	-47	-6	Min.	0.00	-43.32	17	0.00	17	0.00	17	-143.55	28	0.00	28	0.00	17
305	-47	-6	Min.	150.00	-176.97	17	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
306	-7	-50	Max	0.00	176.97	22	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
306	-7	-50	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
306	-7	-50	Min.	0.00	171.70	28	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
306	-7	-50	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
306	-49	-7	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	28	0.00	17
306	-49	-7	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
306	-49	-7	Min.	0.00	-43.32	17	0.00	17	0.00	17	-143.55	28	0.00	17	0.00	17



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306	-49	-7	Min.	150.00	-176.97	17	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
307	-8	-52	Max	0.00	176.97	22	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
307	-8	-52	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
307	-8	-52	Min.	0.00	171.70	28	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
307	-8	-52	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
307	-51	-8	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	21	0.00	17
307	-51	-8	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
307	-51	-8	Min.	0.00	-43.32	29	0.00	17	0.00	17	-143.55	28	0.00	28	0.00	17
307	-51	-8	Min.	150.00	-176.97	29	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
308	-9	-54	Max	0.00	176.97	22	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
308	-9	-54	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
308	-9	-54	Min.	0.00	171.70	28	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
308	-9	-54	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
308	-53	-9	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	21	0.00	17
308	-53	-9	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
308	-53	-9	Min.	0.00	-43.32	29	0.00	17	0.00	17	-143.55	28	0.00	17	0.00	17
308	-53	-9	Min.	150.00	-176.97	29	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
309	-10	-56	Max	0.00	118.98	17	0.00	17	0.00	17	227.41	28	173.21	21	0.00	17
309	-10	-56	Max	150.00	21.66	17	0.00	17	0.00	17	71.77	28	0.00	21	0.00	17
309	-10	-56	Min.	0.00	116.34	28	0.00	17	0.00	17	-158.57	21	-224.38	28	0.00	17
309	-10	-56	Min.	150.00	20.67	28	0.00	17	0.00	17	-72.36	21	0.00	28	0.00	17
309	-55	-10	Max	0.00	-20.67	21	0.00	17	0.00	17	72.36	21	0.00	17	0.00	17
309	-55	-10	Max	150.00	-116.34	21	0.00	17	0.00	17	158.57	21	173.20	21	0.00	17
309	-55	-10	Min.	0.00	-21.66	29	0.00	17	0.00	17	-71.77	28	0.00	21	0.00	17
309	-55	-10	Min.	150.00	-118.98	29	0.00	17	0.00	17	-227.41	28	-224.38	28	0.00	17
310	-11	-58	Max	0.00	118.98	29	0.00	17	0.00	17	227.41	28	173.21	21	0.00	17
310	-11	-58	Max	150.00	21.66	22	0.00	17	0.00	17	71.77	28	0.00	21	0.00	17
310	-11	-58	Min.	0.00	116.34	21	0.00	17	0.00	17	-158.57	21	-224.38	28	0.00	17
310	-11	-58	Min.	150.00	20.67	28	0.00	17	0.00	17	-72.36	21	0.00	28	0.00	17
310	-57	-11	Max	0.00	-20.67	21	0.00	17	0.00	17	72.36	21	0.00	21	0.00	17
310	-57	-11	Max	150.00	-116.34	21	0.00	17	0.00	17	158.57	21	173.21	21	0.00	17
310	-57	-11	Min.	0.00	-21.66	29	0.00	17	0.00	17	-71.77	28	0.00	28	0.00	17
310	-57	-11	Min.	150.00	-118.98	29	0.00	17	0.00	17	-227.41	28	-224.38	28	0.00	17
311	-12	-60	Max	0.00	176.97	29	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
311	-12	-60	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
311	-12	-60	Min.	0.00	171.70	21	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
311	-12	-60	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
311	-59	-12	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	21	0.00	17
311	-59	-12	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
311	-59	-12	Min.	0.00	-43.32	29	0.00	17	0.00	17	-143.55	28	0.00	28	0.00	17
311	-59	-12	Min.	150.00	-176.97	29	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
312	-13	-62	Max	0.00	176.97	29	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
312	-13	-62	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
312	-13	-62	Min.	0.00	171.70	21	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
312	-13	-62	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
312	-61	-13	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	21	0.00	17
312	-61	-13	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
312	-61	-13	Min.	0.00	-43.32	29	0.00	17	0.00	17	-143.55	28	0.00	28	0.00	17
312	-61	-13	Min.	150.00	-176.97	29	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
313	-14	-64	Max	0.00	176.97	29	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
313	-14	-64	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
313	-14	-64	Min.	0.00	171.70	21	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
313	-14	-64	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
313	-63	-14	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	21	0.00	17
313	-63	-14	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
313	-63	-14	Min.	0.00	-43.32	29	0.00	17	0.00	17	-143.55	28	0.00	28	0.00	17
313	-63	-14	Min.	150.00	-176.97	29	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
314	-15	-66	Max	0.00	176.97	29	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
314	-15	-66	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
314	-15	-66	Min.	0.00	171.70	21	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
314	-15	-66	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
314	-65	-15	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	21	0.00	17
314	-65	-15	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
314	-65	-15	Min.	0.00	-43.32	29	0.00	17	0.00	17	-143.55	28	0.00	28	0.00	17
314	-65	-15	Min.	150.00	-176.97	29	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
316	-26	-74	Max	0.00	176.97	29	0.00	17	0.00	17	419.61	28	372.82	21	0.00	17
316	-26	-74	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
316	-26	-74	Min.	0.00	171.70	21	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
316	-26	-74	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
316	-73	-26	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	28	0.00	17
316	-73	-26	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
316	-73	-26	Min.	0.00	-43.32	29	0.00	17	0.00	17	-143.55	28	0.00	21	0.00	17
316	-73	-26	Min.	150.00	-176.97	29	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
317	-18	-71	Max	0.00	118.98	17	0.00	17	0.00	17	227.41	28	173.21	21	0.00	17
317	-18	-71	Max	150.00	21.66	22	0.00	17	0.00	17	71.77	28	0.00	21	0.00	17
317	-18	-71	Min.	0.00	116.34	21	0.00	17	0.00	17	-158.57	21	-224.39	28	0.00	17

317	-18	-71	Min.	150.00	20.67	28	0.00	17	0.00	17	-72.36	21	0.00	28	0.00	17
317	-70	-18	Max	0.00	-20.67	21	0.00	17	0.00	17	72.36	21	0.00	28	0.00	17
317	-70	-18	Max	150.00	-116.34	21	0.00	17	0.00	17	158.57	21	173.21	21	0.00	17
317	-70	-18	Min.	0.00	-21.66	29	0.00	17	0.00	17	-71.77	28	0.00	21	0.00	17
317	-70	-18	Min.	150.00	-118.98	29	0.00	17	0.00	17	-227.41	28	-224.38	28	0.00	17
318	201	-81	Max	0.00	176.97	22	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
318	201	-81	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
318	201	-81	Min.	0.00	171.70	28	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
318	201	-81	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
318	-80	201	Max	0.00	-41.35	28	0.00	17	0.00	17	144.73	21	0.00	28	0.00	17
318	-80	201	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
318	-80	201	Min.	0.00	-43.32	17	0.00	17	0.00	17	-143.55	28	0.00	17	0.00	17
318	-80	201	Min.	150.00	-176.97	17	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17
319	-77	-79	Max	0.00	176.97	29	0.00	17	0.00	17	419.61	28	372.81	21	0.00	17
319	-77	-79	Max	150.00	43.32	22	0.00	17	0.00	17	143.55	28	0.00	21	0.00	17
319	-77	-79	Min.	0.00	171.70	21	0.00	17	0.00	17	-352.36	21	-422.37	28	0.00	17
319	-77	-79	Min.	150.00	41.35	28	0.00	17	0.00	17	-144.73	21	0.00	28	0.00	17
319	-78	-77	Max	0.00	-41.35	21	0.00	17	0.00	17	144.73	21	0.00	28	0.00	17
319	-78	-77	Max	150.00	-171.70	21	0.00	17	0.00	17	352.36	21	372.81	21	0.00	17
319	-78	-77	Min.	0.00	-43.32	29	0.00	17	0.00	17	-143.55	28	0.00	17	0.00	17
319	-78	-77	Min.	150.00	-176.97	29	0.00	17	0.00	17	-419.61	28	-422.37	28	0.00	17

Tipo di combinazione di carico: SLE R

Asta	N1	N2		X <cm>	N <daN>	CC	Ty <daN>	CC	Mz <daNm>	CC	Tz <daN>	CC	My <daNm>	CC	Mx <daNm>	CC
1	315	-45	Max	0.00	-730.03	23	-10.03	23	168.40	30	1543.71	30	7344.19	23	0.86	30
1	315	-45	Max	328.50	-491.96	23	-10.03	23	-22.12	23	1543.71	30	199.96	23	0.86	30
1	315	-45	Min.	0.00	-2888.42	30	-156.10	30	10.82	23	-2174.80	23	-5213.03	30	-1.21	23
1	315	-45	Min.	328.50	-2650.35	30	-156.10	30	-344.37	30	-2174.80	23	-141.93	30	-1.21	23
2	2	202	Max	0.00	-925.53	23	0.00	23	0.00	30	2093.30	30	9287.77	23	0.00	30
2	2	202	Max	328.50	-687.46	23	0.00	23	0.00	23	2093.30	30	283.86	30	0.00	30
2	2	202	Min.	0.00	-3813.71	30	-0.00	30	0.00	23	-2949.06	23	-6592.61	30	0.00	23
2	2	202	Min.	328.50	-3575.65	30	-0.00	30	-0.00	30	-2949.06	23	-399.91	23	0.00	23
3	3	203	Max	0.00	-730.03	23	156.10	30	-10.82	23	1543.71	30	7344.19	23	1.21	23
3	3	203	Max	328.50	-491.96	23	156.10	30	344.38	30	1543.71	30	199.96	23	1.21	23
3	3	203	Min.	0.00	-2888.42	30	10.03	23	-168.40	30	-2174.80	23	-5213.03	30	-0.86	30
3	3	203	Min.	328.50	-2650.36	30	10.03	23	-22.12	23	-2174.80	23	-141.93	30	-0.86	30
201	-3	-29	Max	0.00	0.00	18	185.03	30	0.00	30	-43.07	23	0.00	30	0.00	23
201	-3	-29	Max	135.63	0.00	18	185.03	30	250.95	30	-166.57	23	-142.16	23	0.00	23
201	-3	-29	Min.	0.00	0.00	18	-260.67	23	0.00	23	-300.39	30	0.00	18	0.00	18
201	-3	-29	Min.	135.63	0.00	18	-260.67	23	-353.54	23	-423.89	30	-491.16	30	0.00	18
201	-29	-45	Max	0.00	0.00	18	555.08	30	250.95	30	-144.37	23	-142.16	23	0.00	23
201	-29	-45	Max	83.77	0.00	18	555.08	30	715.94	30	-220.66	23	-295.06	23	0.00	23
201	-29	-45	Min.	0.00	0.00	18	-782.00	23	-353.54	23	-916.34	30	-491.16	30	0.00	31
201	-29	-45	Min.	83.77	0.00	18	-782.00	23	-1008.63	23	-992.62	30	-1290.74	30	0.00	31
201	-45	201	Max	0.00	-10.03	23	1392.80	23	1716.80	30	1657.74	30	-317.18	23	199.95	23
201	-45	201	Max	51.86	-10.03	23	1392.80	23	204.12	30	1610.52	30	-188.73	23	199.95	23
201	-45	201	Min.	0.00	-156.10	30	-988.63	30	-1009.84	23	271.30	23	-1635.11	30	-141.93	30
201	-45	201	Min.	51.86	-156.10	30	-988.63	30	-287.57	23	224.08	23	-787.69	30	-141.93	30
201	201	-6	Max	0.00	-10.03	23	871.47	23	204.11	30	1118.07	30	-188.73	23	199.95	23
201	201	-6	Max	135.63	-10.03	23	871.47	23	894.40	23	994.57	30	644.99	30	199.95	23
201	201	-6	Min.	0.00	-156.10	30	-618.58	30	-287.56	23	246.28	23	-787.68	30	-141.93	30
201	201	-6	Min.	135.63	-156.10	30	-618.58	30	-634.86	30	122.78	23	61.54	23	-141.93	30
201	-6	-7	Max	0.00	-10.03	23	350.14	23	894.43	23	502.12	30	645.02	30	199.95	23
201	-6	-7	Max	135.63	-10.03	23	350.14	23	1369.32	23	378.62	30	1242.29	30	199.95	23
201	-6	-7	Min.	0.00	-156.10	30	-248.53	30	-634.88	30	144.97	23	61.55	23	-141.93	30
201	-6	-7	Min.	135.63	-156.10	30	-248.53	30	-971.96	30	21.47	23	174.41	23	-141.93	30
201	-7	-8	Max	0.00	-10.03	23	121.52	30	1369.29	23	43.67	23	1242.26	30	199.96	23
201	-7	-8	Max	4.77					816.67	24			441.17	24		
201	-7	-8	Max	135.63	-10.03	23	121.52	30	1137.10	23	-79.83	23	1004.13	30	199.96	23
201	-7	-8	Min.	0.00	-156.10	30	-171.20	23	-971.94	30	-113.82	30	174.41	23	-141.93	30
201	-7	-8	Min.	47.96					1287.19	23			184.88	23		
201	-7	-8	Min.	135.63	-156.10	30	-171.20	23	-807.13	30	-237.32	30	149.89	23	-141.93	30
201	-8	-9	Max	0.00	-10.03	23	491.57	30	1137.09	23	-57.64	23	1004.13	30	199.96	23
201	-8	-9	Max	135.63	-10.03	23	491.57	30	197.82	23	-181.14	23	-12.04	23	199.96	23
201	-8	-9	Min.	0.00	-156.10	30	-692.53	23	-807.13	30	-729.77	30	149.88	23	-141.93	30
201	-8	-9	Min.	135.63	-156.10	30	-692.53	23	-140.42	30	-853.27	30	-69.40	30	-141.93	30
201	-9	-10	Max	0.00	-10.03	23	861.62	30	197.81	23	-158.95	23	-12.04	23	199.96	23
201	-9	-10	Max	135.63	-10.03	23	861.62	30	1028.19	30	-282.45	23	-311.37	23	199.96	23
201	-9	-10	Min.	0.00	-156.10	30	-1213.86	23	-140.41	30	-1345.72	30	-69.41	30	-141.93	30
201	-9	-10	Min.	135.63	-156.10	30	-1213.86	23	-1448.53	23	-1469.22	30	-1978.34	30	-141.93	30
201	-10	202	Max	0.00	-10.03	23	1046.65	30	1028.21	30	-325.52	23	-311.38	23	199.96	23
201	-10	202	Max	20.00	-10.03	23	1046.65	30	1237.54	30	-343.73	23	-378.30	23	199.96	23
201	-10	202	Min.	0.00	-156.10	30	-1474.53	23	-1448.55	23	-1769.61	30	-1978.36	30	-141.93	30
201	-10	202	Min.	20.00	-156.10	30	-1474.53	23	-1743.46	23	-1787.82	30	-2334.11	30	-141.93	30

202	202	-11	Max	0.00	-10.03	23	1474.53	23	1237.54	30	1787.82	30	-378.30	23	141.93	30
202	202	-11	Max	20.00	-10.03	23	1474.53	23	1028.20	30	1769.61	30	-311.38	23	141.93	30
202	202	-11	Min.	0.00	-156.10	30	-1046.65	30	-1743.46	23	343.73	23	-2334.11	30	-199.96	23
202	202	-11	Min.	20.00	-156.10	30	-1046.65	30	-1448.55	23	325.52	23	-1978.36	30	-199.96	23
202	-11	-12	Max	0.00	-10.03	23	1213.87	23	1028.21	30	1469.22	30	-311.38	23	141.93	30
202	-11	-12	Max	135.63	-10.03	23	1213.87	23	197.80	23	1345.72	30	-12.05	23	141.93	30
202	-11	-12	Min.	0.00	-156.10	30	-861.62	30	-1448.55	23	282.45	23	-1978.37	30	-199.96	23
202	-11	-12	Min.	135.63	-156.10	30	-861.62	30	-140.40	30	158.95	23	-69.43	30	-199.96	23
202	-12	-13	Max	0.00	-10.03	23	692.53	23	197.82	23	853.27	30	-12.04	23	141.93	30
202	-12	-13	Max	135.63	-10.03	23	692.53	23	1137.09	23	729.77	30	1004.12	30	141.93	30
202	-12	-13	Min.	0.00	-156.10	30	-491.57	30	-140.41	30	181.14	23	-69.41	30	-199.96	23
202	-12	-13	Min.	135.63	-156.10	30	-491.57	30	-807.12	30	57.64	23	149.88	23	-199.96	23
202	-13	-14	Max	0.00	-10.03	23	171.20	23	1137.10	23	237.33	30	1004.13	30	141.93	30
202	-13	-14	Max	130.86					816.68	24			441.17	24		
202	-13	-14	Max	135.63	-10.03	23	171.20	23	1369.29	23	113.82	30	1242.26	30	141.93	30
202	-13	-14	Min.	0.00	-156.10	30	-121.52	30	-807.13	30	79.83	23	149.88	23	-199.95	23
202	-13	-14	Min.	87.67					1287.19	23			184.88	23		
202	-13	-14	Min.	135.63	-156.10	30	-121.52	30	-971.95	30	-43.67	23	174.41	23	-199.95	23
202	-14	-15	Max	0.00	-10.03	23	248.53	30	1369.30	23	-21.47	23	1242.26	30	141.93	30
202	-14	-15	Max	135.63	-10.03	23	248.53	30	894.41	23	-144.98	23	644.99	30	141.93	30
202	-14	-15	Min.	0.00	-156.10	30	-350.13	23	-971.95	30	-378.62	30	174.41	23	-199.96	23
202	-14	-15	Min.	135.63	-156.10	30	-350.13	23	-634.87	30	-502.13	30	61.53	23	-199.96	23
202	-15	-77	Max	0.00	-10.03	23	618.58	30	894.44	23	-122.77	23	645.03	30	141.93	30
202	-15	-77	Max	135.63	-10.03	23	618.58	30	204.08	30	-246.28	23	-188.72	23	141.93	30
202	-15	-77	Min.	0.00	-156.10	30	-871.47	23	-634.89	30	-994.56	30	61.55	23	-199.95	23
202	-15	-77	Min.	135.63	-156.10	30	-871.47	23	-287.52	23	-1118.07	30	-787.64	30	-199.95	23
202	-77	203	Max	0.00	-10.03	23	988.63	30	204.09	30	-224.08	23	-188.72	23	141.93	30
202	-77	203	Max	51.86	-10.03	23	988.63	30	716.77	30	-271.30	23	-317.17	23	141.93	30
202	-77	203	Min.	0.00	-156.10	30	-1392.80	23	-287.53	23	-1610.51	30	-787.65	30	-199.95	23
202	-77	203	Min.	51.86	-156.10	30	-1392.80	23	-1009.80	23	-1657.74	30	-1635.07	30	-199.95	23
202	203	-26	Max	0.00	0.00	18	782.00	23	715.94	30	992.62	30	-295.06	23	0.00	30
202	203	-26	Max	83.77	0.00	18	782.00	23	250.94	30	916.34	30	-142.16	23	0.00	30
202	203	-26	Min.	0.00	0.00	18	-555.08	30	-1008.63	23	220.66	23	-1290.74	30	0.00	23
202	203	-26	Min.	83.77	0.00	18	-555.08	30	-353.53	23	144.37	23	-491.16	30	0.00	23
202	-26	-18	Max	0.00	0.00	18	260.67	23	250.95	30	423.89	30	-142.17	23	0.00	30
202	-26	-18	Max	135.63	0.00	18	260.67	23	0.00	30	300.39	30	0.00	23	0.00	30
202	-26	-18	Min.	0.00	0.00	18	-185.03	30	-353.54	23	166.57	23	-491.17	30	0.00	23
202	-26	-18	Min.	135.63	0.00	18	-185.03	30	-0.00	23	43.07	23	-0.00	30	0.00	23
302	-3	-69	Max	0.00	85.57	24	0.00	18	0.00	18	155.22	30	112.76	23	0.00	18
302	-3	-69	Max	150.00	14.44	24	0.00	18	0.00	18	47.85	30	0.00	23	0.00	18
302	-3	-69	Min.	0.00	83.82	30	0.00	18	0.00	18	-102.11	23	-152.30	30	0.00	18
302	-3	-69	Min.	150.00	13.78	30	0.00	18	0.00	18	-48.24	23	0.00	30	0.00	18
302	-68	-3	Max	0.00	-13.78	23	0.00	18	0.00	18	48.24	23	0.00	30	0.00	18
302	-68	-3	Max	150.00	-83.81	23	0.00	18	0.00	18	102.11	23	112.76	23	0.00	18
302	-68	-3	Min.	0.00	-14.44	18	0.00	18	0.00	18	-47.85	30	0.00	18	0.00	18
302	-68	-3	Min.	150.00	-85.57	18	0.00	18	0.00	18	-155.22	30	-152.30	30	0.00	18
303	-29	-76	Max	0.00	124.24	24	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
303	-29	-76	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
303	-29	-76	Min.	0.00	120.72	30	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
303	-29	-76	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
303	-75	-29	Max	0.00	-27.56	30	0.00	18	0.00	18	96.49	23	0.00	30	0.00	18
303	-75	-29	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
303	-75	-29	Min.	0.00	-28.88	18	0.00	18	0.00	18	-95.70	30	0.00	23	0.00	18
303	-75	-29	Min.	150.00	-124.24	18	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
305	-6	-48	Max	0.00	124.24	24	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
305	-6	-48	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
305	-6	-48	Min.	0.00	120.72	30	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
305	-6	-48	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
305	-47	-6	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	23	0.00	18
305	-47	-6	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
305	-47	-6	Min.	0.00	-28.88	18	0.00	18	0.00	18	-95.70	30	0.00	30	0.00	18
305	-47	-6	Min.	150.00	-124.24	18	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
306	-7	-50	Max	0.00	124.24	24	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
306	-7	-50	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
306	-7	-50	Min.	0.00	120.72	30	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
306	-7	-50	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
306	-49	-7	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	30	0.00	18
306	-49	-7	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
306	-49	-7	Min.	0.00	-28.88	18	0.00	18	0.00	18	-95.70	30	0.00	18	0.00	18
306	-49	-7	Min.	150.00	-124.24	18	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
307	-8	-52	Max	0.00	124.24	24	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
307	-8	-52	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
307	-8	-52	Min.	0.00	120.72	30	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
307	-8	-52	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
307	-51	-8	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	23	0.00	18
307	-51	-8	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18

307	-51	-8	Min.	0.00	-28.88	31	0.00	18	0.00	18	-95.70	30	0.00	30	0.00	18
307	-51	-8	Min.	150.00	-124.24	31	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
308	-9	-54	Max	0.00	124.24	24	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
308	-9	-54	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
308	-9	-54	Min.	0.00	120.72	30	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
308	-9	-54	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
308	-53	-9	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	23	0.00	18
308	-53	-9	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
308	-53	-9	Min.	0.00	-28.88	31	0.00	18	0.00	18	-95.70	30	0.00	18	0.00	18
308	-53	-9	Min.	150.00	-124.24	31	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
309	-10	-56	Max	0.00	85.57	18	0.00	18	0.00	18	155.22	30	112.76	23	0.00	18
309	-10	-56	Max	150.00	14.44	18	0.00	18	0.00	18	47.85	30	0.00	23	0.00	18
309	-10	-56	Min.	0.00	83.81	30	0.00	18	0.00	18	-102.11	23	-152.30	30	0.00	18
309	-10	-56	Min.	150.00	13.78	30	0.00	18	0.00	18	-48.24	23	0.00	30	0.00	18
309	-55	-10	Max	0.00	-13.78	23	0.00	18	0.00	18	48.24	23	0.00	18	0.00	18
309	-55	-10	Max	150.00	-83.81	23	0.00	18	0.00	18	102.11	23	112.76	23	0.00	18
309	-55	-10	Min.	0.00	-14.44	31	0.00	18	0.00	18	-47.85	30	0.00	23	0.00	18
309	-55	-10	Min.	150.00	-85.57	31	0.00	18	0.00	18	-155.22	30	-152.30	30	0.00	18
310	-11	-58	Max	0.00	85.57	31	0.00	18	0.00	18	155.22	30	112.76	23	0.00	18
310	-11	-58	Max	150.00	14.44	24	0.00	18	0.00	18	47.85	30	0.00	23	0.00	18
310	-11	-58	Min.	0.00	83.82	23	0.00	18	0.00	18	-102.11	23	-152.30	30	0.00	18
310	-11	-58	Min.	150.00	13.78	30	0.00	18	0.00	18	-48.24	23	0.00	30	0.00	18
310	-57	-11	Max	0.00	-13.78	23	0.00	18	0.00	18	48.24	23	0.00	23	0.00	18
310	-57	-11	Max	150.00	-83.81	23	0.00	18	0.00	18	102.11	23	112.76	23	0.00	18
310	-57	-11	Min.	0.00	-14.44	31	0.00	18	0.00	18	-47.85	30	0.00	30	0.00	18
310	-57	-11	Min.	150.00	-85.57	31	0.00	18	0.00	18	-155.22	30	-152.30	30	0.00	18
311	-12	-60	Max	0.00	124.24	31	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
311	-12	-60	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
311	-12	-60	Min.	0.00	120.72	23	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
311	-12	-60	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
311	-59	-12	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	23	0.00	18
311	-59	-12	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
311	-59	-12	Min.	0.00	-28.88	31	0.00	18	0.00	18	-95.70	30	0.00	30	0.00	18
311	-59	-12	Min.	150.00	-124.24	31	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
312	-13	-62	Max	0.00	124.24	31	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
312	-13	-62	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
312	-13	-62	Min.	0.00	120.72	23	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
312	-13	-62	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
312	-61	-13	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	23	0.00	18
312	-61	-13	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
312	-61	-13	Min.	0.00	-28.88	31	0.00	18	0.00	18	-95.70	30	0.00	30	0.00	18
312	-61	-13	Min.	150.00	-124.24	31	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
313	-14	-64	Max	0.00	124.24	31	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
313	-14	-64	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
313	-14	-64	Min.	0.00	120.72	23	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
313	-14	-64	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
313	-63	-14	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	23	0.00	18
313	-63	-14	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
313	-63	-14	Min.	0.00	-28.88	31	0.00	18	0.00	18	-95.70	30	0.00	30	0.00	18
313	-63	-14	Min.	150.00	-124.24	31	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
314	-15	-66	Max	0.00	124.24	31	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
314	-15	-66	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
314	-15	-66	Min.	0.00	120.72	23	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
314	-15	-66	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
314	-65	-15	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	23	0.00	18
314	-65	-15	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
314	-65	-15	Min.	0.00	-28.88	31	0.00	18	0.00	18	-95.70	30	0.00	30	0.00	18
314	-65	-15	Min.	150.00	-124.24	31	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
316	-26	-74	Max	0.00	124.24	31	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
316	-26	-74	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
316	-26	-74	Min.	0.00	120.72	23	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
316	-26	-74	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
316	-73	-26	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	30	0.00	18
316	-73	-26	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
316	-73	-26	Min.	0.00	-28.88	31	0.00	18	0.00	18	-95.70	30	0.00	23	0.00	18
316	-73	-26	Min.	150.00	-124.24	31	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
317	-18	-71	Max	0.00	85.57	18	0.00	18	0.00	18	155.22	30	112.76	23	0.00	18
317	-18	-71	Max	150.00	14.44	24	0.00	18	0.00	18	47.85	30	0.00	23	0.00	18
317	-18	-71	Min.	0.00	83.82	23	0.00	18	0.00	18	-102.11	23	-152.30	30	0.00	18
317	-18	-71	Min.	150.00	13.78	30	0.00	18	0.00	18	-48.24	23	0.00	30	0.00	18
317	-70	-18	Max	0.00	-13.78	23	0.00	18	0.00	18	48.24	23	0.00	30	0.00	18
317	-70	-18	Max	150.00	-83.81	23	0.00	18	0.00	18	102.11	23	112.76	23	0.00	18
317	-70	-18	Min.	0.00	-14.44	31	0.00	18	0.00	18	-47.85	30	0.00	23	0.00	18
317	-70	-18	Min.	150.00	-85.57	31	0.00	18	0.00	18	-155.22	30	-152.30	30	0.00	18
318	201	-81	Max	0.00	124.24	24	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
318	201	-81	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18

318	201	-81	Min.	0.00	120.72	30	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
318	201	-81	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
318	-80	201	Max	0.00	-27.56	30	0.00	18	0.00	18	96.49	23	0.00	30	0.00	18
318	-80	201	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
318	-80	201	Min.	0.00	-28.88	18	0.00	18	0.00	18	-95.70	30	0.00	18	0.00	18
318	-80	201	Min.	150.00	-124.24	18	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18
319	-77	-79	Max	0.00	124.24	31	0.00	18	0.00	18	283.35	30	245.84	23	0.00	18
319	-77	-79	Max	150.00	28.88	24	0.00	18	0.00	18	95.70	30	0.00	23	0.00	18
319	-77	-79	Min.	0.00	120.72	23	0.00	18	0.00	18	-231.29	23	-284.29	30	0.00	18
319	-77	-79	Min.	150.00	27.56	30	0.00	18	0.00	18	-96.49	23	0.00	30	0.00	18
319	-78	-77	Max	0.00	-27.56	23	0.00	18	0.00	18	96.49	23	0.00	30	0.00	18
319	-78	-77	Max	150.00	-120.72	23	0.00	18	0.00	18	231.29	23	245.84	23	0.00	18
319	-78	-77	Min.	0.00	-28.88	31	0.00	18	0.00	18	-95.70	30	0.00	18	0.00	18
319	-78	-77	Min.	150.00	-124.24	31	0.00	18	0.00	18	-283.35	30	-284.29	30	0.00	18

Tipo di combinazione di carico: SLE F

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	315	-45	Max	0.00	-1705.87	25	-76.07	25	113.58	32	308.74	32	1468.84	25	0.17	32
1	315	-45	Max	328.50	-1467.80	25	-76.07	25	-167.81	25	308.74	32	39.99	25	0.17	32
1	315	-45	Min.	0.00	-2137.55	32	-105.28	32	82.06	25	-434.96	25	-1042.60	32	-0.24	25
1	315	-45	Min.	328.50	-1899.48	32	-105.28	32	-232.27	32	-434.96	25	-28.39	32	-0.24	25
2	2	202	Max	0.00	-2231.31	25	-0.00	25	0.00	32	418.66	32	1857.55	25	0.00	32
2	2	202	Max	328.50	-1993.25	25	-0.00	25	0.00	25	418.66	32	56.77	32	0.00	32
2	2	202	Min.	0.00	-2808.95	32	-0.00	32	0.00	25	-589.81	25	-1318.52	32	0.00	25
2	2	202	Min.	328.50	-2570.88	32	-0.00	32	-0.00	32	-589.81	25	-79.98	25	0.00	25
3	3	203	Max	0.00	-1705.87	25	105.28	32	-82.06	25	308.74	32	1468.84	25	0.24	25
3	3	203	Max	328.50	-1467.80	25	105.28	32	232.27	32	308.74	32	39.99	25	0.24	25
3	3	203	Min.	0.00	-2137.55	32	76.07	25	-113.58	32	-434.96	25	-1042.60	32	-0.17	32
3	3	203	Min.	328.50	-1899.48	32	76.07	25	167.82	25	-434.96	25	-28.39	32	-0.17	32
201	-3	-29	Max	0.00	0.00	19	37.01	32	0.00	32	-159.41	25	0.00	32	0.00	25
201	-3	-29	Max	135.63	0.00	19	37.01	32	50.19	32	-282.91	25	-299.95	25	0.00	25
201	-3	-29	Min.	0.00	0.00	19	-52.13	25	0.00	25	-210.87	32	0.00	19	0.00	19
201	-3	-29	Min.	135.63	0.00	19	-52.13	25	-70.71	25	-334.37	32	-369.75	32	0.00	19
201	-29	-45	Max	0.00	0.00	19	111.02	32	50.19	32	-493.39	25	-299.95	25	0.00	25
201	-29	-45	Max	83.77	0.00	19	111.02	32	143.19	32	-569.67	25	-745.22	25	0.00	25
201	-29	-45	Min.	0.00	0.00	19	-156.40	25	-70.71	25	-647.78	32	-369.75	32	0.00	19
201	-29	-45	Min.	83.77	0.00	19	-156.40	25	-201.73	25	-724.06	32	-944.35	32	0.00	19
201	-45	201	Max	0.00	-76.07	25	278.56	25	143.36	32	1175.42	32	-913.03	25	39.99	25
201	-45	201	Max	51.86	-76.07	25	278.56	25	40.82	32	1128.19	32	-459.53	25	39.99	25
201	-45	201	Min.	0.00	-105.28	32	-197.73	32	-201.97	25	898.13	25	-1176.62	32	-28.39	32
201	-45	201	Min.	51.86	-105.28	32	-197.73	32	-57.51	25	850.91	25	-579.32	32	-28.39	32
201	201	-6	Max	0.00	-76.07	25	174.29	25	40.82	32	814.79	32	-459.52	25	39.99	25
201	201	-6	Max	135.63	-76.07	25	174.29	25	178.88	25	691.28	32	442.01	32	39.99	25
201	201	-6	Min.	0.00	-105.28	32	-123.72	32	-57.51	25	640.43	25	-579.32	32	-28.39	32
201	201	-6	Min.	135.63	-105.28	32	-123.72	32	-126.97	32	516.92	25	325.33	25	-28.39	32
201	-6	-7	Max	0.00	-76.07	25	70.03	25	178.89	25	377.87	32	442.04	32	39.99	25
201	-6	-7	Max	135.63	-76.07	25	70.03	25	273.86	25	254.37	32	870.79	32	39.99	25
201	-6	-7	Min.	0.00	-105.28	32	-49.71	32	-126.98	32	306.44	25	325.34	25	-28.39	32
201	-6	-7	Min.	135.63	-105.28	32	-49.71	32	-194.39	32	182.94	25	657.21	25	-28.39	32
201	-7	-8	Max	0.00	-76.07	25	24.30	32	273.86	25	-27.53	25	870.77	32	39.99	25
201	-7	-8	Max	135.63	-76.07	25	24.30	32	227.42	25	-151.04	25	706.95	32	39.99	25
201	-7	-8	Min.	0.00	-105.28	32	-34.24	25	-194.39	32	-59.03	32	657.20	25	-28.39	32
201	-7	-8	Min.	135.63	-105.28	32	-34.24	25	-161.43	32	-182.53	32	536.10	25	-28.39	32
201	-8	-9	Max	0.00	-76.07	25	98.31	32	227.42	25	-361.52	25	706.95	32	39.99	25
201	-8	-9	Max	135.63	-76.07	25	98.31	32	39.56	25	-485.02	25	-37.97	25	39.99	25
201	-8	-9	Min.	0.00	-105.28	32	-138.51	25	-161.43	32	-495.94	32	536.10	25	-28.39	32
201	-8	-9	Min.	135.63	-105.28	32	-138.51	25	-28.08	32	-619.45	32	-49.45	32	-28.39	32
201	-9	-10	Max	0.00	-76.07	25	172.32	32	39.56	25	-695.50	25	-37.98	25	39.99	25
201	-9	-10	Max	135.63	-76.07	25	172.32	32	205.64	32	-819.00	25	-1065.03	25	39.99	25
201	-9	-10	Min.	0.00	-105.28	32	-242.77	25	-28.08	32	-932.86	32	-49.45	32	-28.39	32
201	-9	-10	Min.	135.63	-105.28	32	-242.77	25	-289.71	25	-1056.36	32	-1398.42	32	-28.39	32
201	-10	202	Max	0.00	-76.07	25	209.33	32	205.64	32	-978.41	25	-1065.04	25	39.99	25
201	-10	202	Max	20.00	-76.07	25	209.33	32	247.51	32	-996.62	25	-1262.55	25	39.99	25
201	-10	202	Min.	0.00	-105.28	32	-294.91	25	-289.71	25	-1267.23	32	-1398.44	32	-28.39	32
201	-10	202	Min.	20.00	-105.28	32	-294.91	25	-348.69	25	-1285.44	32	-1653.71	32	-28.39	32
202	202	-11	Max	0.00	-76.07	25	294.91	25	247.51	32	1285.44	32	-1262.55	25	28.39	32
202	202	-11	Max	20.00	-76.07	25	294.91	25	205.64	32	1267.23	32	-1065.04	25	28.39	32
202	202	-11	Min.	0.00	-105.28	32	-209.33	32	-348.69	25	996.62	25	-1653.71	32	-39.99	25
202	202	-11	Min.	20.00	-105.28	32	-209.33	32	-289.71	25	978.41	25	-1398.44	32	-39.99	25
202	-11	-12	Max	0.00	-76.07	25	242.77	25	205.64	32	1056.36	32	-1065.05	25	28.39	32
202	-11	-12	Max	135.63	-76.07	25	242.77	25	39.56	25	932.86	32	-37.99	25	28.39	32
202	-11	-12	Min.	0.00	-105.28	32	-172.32	32	-289.71	25	819.01	25	-1398.44	32	-39.99	25
202	-11	-12	Min.	135.63	-105.28	32	-172.32	32	-28.08	32	695.50	25	-49.47	32	-39.99	25
202	-12	-13	Max	0.00	-76.07	25	138.51	25	39.56	25	619.45	32	-37.98	25	28.39	32



202	-12	-13	Max	135.63	-76.07	25	138.51	25	227.42	25	495.95	32	706.94	32	28.39	32
202	-12	-13	Min.	0.00	-105.28	32	-98.31	32	-28.08	32	485.02	25	-49.45	32	-39.99	25
202	-12	-13	Min.	135.63	-105.28	32	-98.31	32	-161.43	32	361.52	25	536.10	25	-39.99	25
202	-13	-14	Max	0.00	-76.07	25	34.24	25	227.42	25	182.54	32	706.95	32	28.39	32
202	-13	-14	Max	135.63	-76.07	25	34.24	25	273.86	25	59.03	32	870.77	32	28.39	32
202	-13	-14	Min.	0.00	-105.28	32	-24.30	32	-161.43	32	151.04	25	536.10	25	-39.99	25
202	-13	-14	Min.	135.63	-105.28	32	-24.30	32	-194.39	32	27.54	25	657.20	25	-39.99	25
202	-14	-15	Max	0.00	-76.07	25	49.71	32	273.86	25	-182.95	25	870.77	32	28.39	32
202	-14	-15	Max	135.63	-76.07	25	49.71	32	178.88	25	-306.45	25	442.01	32	28.39	32
202	-14	-15	Min.	0.00	-105.28	32	-70.03	25	-194.39	32	-254.38	32	657.20	25	-39.99	25
202	-14	-15	Min.	135.63	-105.28	32	-70.03	25	-126.97	32	-377.88	32	325.32	25	-39.99	25
202	-15	-77	Max	0.00	-76.07	25	123.72	32	178.89	25	-516.92	25	442.04	32	28.39	32
202	-15	-77	Max	135.63	-76.07	25	123.72	32	40.82	32	-640.42	25	-459.50	25	28.39	32
202	-15	-77	Min.	0.00	-105.28	32	-174.29	25	-126.98	32	-691.28	32	325.35	25	-39.99	25
202	-15	-77	Min.	135.63	-105.28	32	-174.29	25	-57.50	25	-814.78	32	-579.28	32	-39.99	25
202	-77	203	Max	0.00	-76.07	25	197.73	32	40.82	32	-850.90	25	-459.51	25	28.39	32
202	-77	203	Max	51.86	-76.07	25	197.73	32	143.35	32	-898.13	25	-913.01	25	28.39	32
202	-77	203	Min.	0.00	-105.28	32	-278.56	25	-57.51	25	-1128.19	32	-579.29	32	-39.99	25
202	-77	203	Min.	51.86	-105.28	32	-278.56	25	-201.96	25	-1175.41	32	-1176.59	32	-39.99	25
202	203	-26	Max	0.00	0.00	19	156.40	25	143.19	32	724.06	32	-745.22	25	0.00	32
202	203	-26	Max	83.77	0.00	19	156.40	25	50.19	32	647.78	32	-299.95	25	0.00	32
202	203	-26	Min.	0.00	0.00	19	-111.02	32	-201.72	25	569.67	25	-944.35	32	0.00	25
202	203	-26	Min.	83.77	0.00	19	-111.02	32	-70.71	25	493.39	25	-369.75	32	0.00	25
202	-26	-18	Max	0.00	0.00	19	52.13	25	50.19	32	334.37	32	-299.95	25	0.00	32
202	-26	-18	Max	135.63	0.00	19	52.13	25	0.00	32	210.87	32	-0.00	25	0.00	32
202	-26	-18	Min.	0.00	0.00	19	-37.01	32	-70.71	25	282.91	25	-369.76	32	0.00	25
202	-26	-18	Min.	135.63	0.00	19	-37.01	32	0.00	25	159.41	25	-0.00	32	0.00	25
302	-3	-69	Max	0.00	82.76	19	0.00	19	0.00	19	68.74	32	-10.21	25	0.00	19
302	-3	-69	Max	123.77									0.48	25		
302	-3	-69	Max	150.00	13.39	19	0.00	19	0.00	19	15.56	32	0.00	25	0.00	19
302	-3	-69	Min.	0.00	82.06	32	0.00	19	0.00	19	17.28	25	-63.22	32	0.00	19
302	-3	-69	Min.	123.77									0.48	25		
302	-3	-69	Min.	150.00	13.13	32	0.00	19	0.00	19	-3.66	25	0.00	32	0.00	19
302	-68	-3	Max	0.00	-13.13	25	0.00	19	0.00	19	3.66	25	0.00	32	0.00	19
302	-68	-3	Max	26.23									0.48	25		
302	-68	-3	Max	150.00	-82.06	25	0.00	19	0.00	19	-17.28	25	-10.21	25	0.00	19
302	-68	-3	Min.	0.00	-13.39	19	0.00	19	0.00	19	-15.56	32	0.00	19	0.00	19
302	-68	-3	Min.	26.23									0.48	25		
302	-68	-3	Min.	150.00	-82.76	19	0.00	19	0.00	19	-68.74	32	-63.22	32	0.00	19
303	-29	-76	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
303	-29	-76	Max	75.75									2.72	25		
303	-29	-76	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
303	-29	-76	Min.	0.00	117.21	32	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
303	-29	-76	Min.	75.75									2.72	25		
303	-29	-76	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
303	-75	-29	Max	0.00	-26.25	32	0.00	19	0.00	19	7.32	25	0.00	32	0.00	19
303	-75	-29	Max	74.25									2.72	25		
303	-75	-29	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
303	-75	-29	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	25	0.00	19
303	-75	-29	Min.	74.25									2.72	25		
303	-75	-29	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
305	-6	-48	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
305	-6	-48	Max	75.75									2.72	25		
305	-6	-48	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
305	-6	-48	Min.	0.00	117.21	32	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
305	-6	-48	Min.	75.75									2.72	25		
305	-6	-48	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
305	-47	-6	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	25	0.00	19
305	-47	-6	Max	74.25									2.72	25		
305	-47	-6	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
305	-47	-6	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	32	0.00	19
305	-47	-6	Min.	74.25									2.72	25		
305	-47	-6	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
306	-7	-50	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
306	-7	-50	Max	75.75									2.72	25		
306	-7	-50	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
306	-7	-50	Min.	0.00	117.21	32	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
306	-7	-50	Min.	75.75									2.72	25		
306	-7	-50	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
306	-49	-7	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	32	0.00	19
306	-49	-7	Max	74.25									2.72	25		
306	-49	-7	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
306	-49	-7	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	19	0.00	19
306	-49	-7	Min.	74.25									2.72	25		
306	-49	-7	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
307	-8	-52	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19

307	-8	-52	Max	75.75								2.72	25			
307	-8	-52	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
307	-8	-52	Min.	0.00	117.21	32	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
307	-8	-52	Min.	75.75									2.72	25		
307	-8	-52	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
307	-51	-8	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	25	0.00	19
307	-51	-8	Max	74.25									2.72	25		
307	-51	-8	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
307	-51	-8	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	32	0.00	19
307	-51	-8	Min.	74.25									2.72	25		
307	-51	-8	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
308	-9	-54	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
308	-9	-54	Max	75.75									2.72	25		
308	-9	-54	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
308	-9	-54	Min.	0.00	117.21	32	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
308	-9	-54	Min.	75.75									2.72	25		
308	-9	-54	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
308	-53	-9	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	25	0.00	19
308	-53	-9	Max	74.25									2.72	25		
308	-53	-9	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
308	-53	-9	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	19	0.00	19
308	-53	-9	Min.	74.25									2.72	25		
308	-53	-9	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
309	-10	-56	Max	0.00	82.76	19	0.00	19	0.00	19	68.74	32	-10.21	25	0.00	19
309	-10	-56	Max	123.77									0.48	25		
309	-10	-56	Max	150.00	13.39	19	0.00	19	0.00	19	15.56	32	0.00	25	0.00	19
309	-10	-56	Min.	0.00	82.06	32	0.00	19	0.00	19	17.28	25	-63.22	32	0.00	19
309	-10	-56	Min.	123.77									0.48	25		
309	-10	-56	Min.	150.00	13.13	32	0.00	19	0.00	19	-3.66	25	0.00	32	0.00	19
309	-55	-10	Max	0.00	-13.13	25	0.00	19	0.00	19	3.66	25	0.00	19	0.00	19
309	-55	-10	Max	26.23									0.48	25		
309	-55	-10	Max	150.00	-82.06	25	0.00	19	0.00	19	-17.28	25	-10.21	25	0.00	19
309	-55	-10	Min.	0.00	-13.39	19	0.00	19	0.00	19	-15.56	32	0.00	25	0.00	19
309	-55	-10	Min.	26.23									0.48	25		
309	-55	-10	Min.	150.00	-82.76	19	0.00	19	0.00	19	-68.74	32	-63.22	32	0.00	19
310	-11	-58	Max	0.00	82.76	19	0.00	19	0.00	19	68.74	32	-10.21	25	0.00	19
310	-11	-58	Max	123.77									0.48	25		
310	-11	-58	Max	150.00	13.39	19	0.00	19	0.00	19	15.56	32	0.00	25	0.00	19
310	-11	-58	Min.	0.00	82.06	25	0.00	19	0.00	19	17.28	25	-63.22	32	0.00	19
310	-11	-58	Min.	123.77									0.48	25		
310	-11	-58	Min.	150.00	13.13	32	0.00	19	0.00	19	-3.66	25	0.00	32	0.00	19
310	-57	-11	Max	0.00	-13.13	25	0.00	19	0.00	19	3.66	25	0.00	25	0.00	19
310	-57	-11	Max	26.23									0.48	25		
310	-57	-11	Max	150.00	-82.06	25	0.00	19	0.00	19	-17.28	25	-10.21	25	0.00	19
310	-57	-11	Min.	0.00	-13.39	19	0.00	19	0.00	19	-15.56	32	0.00	32	0.00	19
310	-57	-11	Min.	26.23									0.48	25		
310	-57	-11	Min.	150.00	-82.76	19	0.00	19	0.00	19	-68.74	32	-63.22	32	0.00	19
311	-12	-60	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
311	-12	-60	Max	75.75									2.72	25		
311	-12	-60	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
311	-12	-60	Min.	0.00	117.21	25	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
311	-12	-60	Min.	75.75									2.72	25		
311	-12	-60	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
311	-59	-12	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	25	0.00	19
311	-59	-12	Max	74.25									2.72	25		
311	-59	-12	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
311	-59	-12	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	32	0.00	19
311	-59	-12	Min.	74.25									2.72	25		
311	-59	-12	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
312	-13	-62	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
312	-13	-62	Max	75.75									2.72	25		
312	-13	-62	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
312	-13	-62	Min.	0.00	117.21	25	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
312	-13	-62	Min.	75.75									2.72	25		
312	-13	-62	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
312	-61	-13	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	25	0.00	19
312	-61	-13	Max	74.25									2.72	25		
312	-61	-13	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
312	-61	-13	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	32	0.00	19
312	-61	-13	Min.	74.25									2.72	25		
312	-61	-13	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
313	-14	-64	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
313	-14	-64	Max	75.75									2.72	25		
313	-14	-64	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
313	-14	-64	Min.	0.00	117.21	25	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
313	-14	-64	Min.	75.75									2.72	25		

313	-14	-64	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
313	-63	-14	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	25	0.00	19
313	-63	-14	Max	74.25									2.72	25		
313	-63	-14	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
313	-63	-14	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	32	0.00	19
313	-63	-14	Min.	74.25									2.72	25		
313	-63	-14	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
314	-15	-66	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
314	-15	-66	Max	75.75									2.72	25		
314	-15	-66	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
314	-15	-66	Min.	0.00	117.21	25	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
314	-15	-66	Min.	75.75									2.72	25		
314	-15	-66	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
314	-65	-15	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	25	0.00	19
314	-65	-15	Max	74.25									2.72	25		
314	-65	-15	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
314	-65	-15	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	32	0.00	19
314	-65	-15	Min.	74.25									2.72	25		
314	-65	-15	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
316	-26	-74	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
316	-26	-74	Max	75.75									2.72	25		
316	-26	-74	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
316	-26	-74	Min.	0.00	117.21	25	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
316	-26	-74	Min.	75.75									2.72	25		
316	-26	-74	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
316	-73	-26	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	32	0.00	19
316	-73	-26	Max	74.25									2.72	25		
316	-73	-26	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
316	-73	-26	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	32	0.00	19
316	-73	-26	Min.	74.25									2.72	25		
316	-73	-26	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
317	-18	-71	Max	0.00	82.76	19	0.00	19	0.00	19	68.74	32	-10.21	25	0.00	19
317	-18	-71	Max	123.77									0.48	25		
317	-18	-71	Max	150.00	13.39	19	0.00	19	0.00	19	15.56	32	0.00	25	0.00	19
317	-18	-71	Min.	0.00	82.06	25	0.00	19	0.00	19	17.28	25	-63.22	32	0.00	19
317	-18	-71	Min.	123.77									0.48	25		
317	-18	-71	Min.	150.00	13.13	32	0.00	19	0.00	19	-3.66	25	0.00	32	0.00	19
317	-70	-18	Max	0.00	-13.13	25	0.00	19	0.00	19	3.66	25	0.00	32	0.00	19
317	-70	-18	Max	26.23									0.48	25		
317	-70	-18	Max	150.00	-82.06	25	0.00	19	0.00	19	-17.28	25	-10.21	25	0.00	19
317	-70	-18	Min.	0.00	-13.39	19	0.00	19	0.00	19	-15.56	32	0.00	25	0.00	19
317	-70	-18	Min.	26.23									0.48	25		
317	-70	-18	Min.	150.00	-82.76	19	0.00	19	0.00	19	-68.74	32	-63.22	32	0.00	19
318	201	-81	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
318	201	-81	Max	75.75									2.72	25		
318	201	-81	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
318	201	-81	Min.	0.00	117.21	32	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
318	201	-81	Min.	75.75									2.72	25		
318	201	-81	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
318	-80	201	Max	0.00	-26.25	32	0.00	19	0.00	19	7.32	25	0.00	32	0.00	19
318	-80	201	Max	74.25									2.72	25		
318	-80	201	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
318	-80	201	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	19	0.00	19
318	-80	201	Min.	74.25									2.72	25		
318	-80	201	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19
319	-77	-79	Max	0.00	118.61	19	0.00	19	0.00	19	110.40	32	-0.11	25	0.00	19
319	-77	-79	Max	75.75									2.72	25		
319	-77	-79	Max	150.00	26.78	19	0.00	19	0.00	19	31.11	32	0.00	25	0.00	19
319	-77	-79	Min.	0.00	117.21	25	0.00	19	0.00	19	7.47	25	-106.14	32	0.00	19
319	-77	-79	Min.	75.75									2.72	25		
319	-77	-79	Min.	150.00	26.25	32	0.00	19	0.00	19	-7.32	25	0.00	32	0.00	19
319	-78	-77	Max	0.00	-26.25	25	0.00	19	0.00	19	7.32	25	0.00	32	0.00	19
319	-78	-77	Max	74.25									2.72	25		
319	-78	-77	Max	150.00	-117.21	25	0.00	19	0.00	19	-7.47	25	-0.11	25	0.00	19
319	-78	-77	Min.	0.00	-26.78	19	0.00	19	0.00	19	-31.11	32	0.00	19	0.00	19
319	-78	-77	Min.	74.25									2.72	25		
319	-78	-77	Min.	150.00	-118.61	19	0.00	19	0.00	19	-110.40	32	-106.13	32	0.00	19

Tipo di combinazione di carico: SLE Q

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC	
1	315	-45	Max	0.00	-1958.34	20	-93.15	20	100.50	20	0.00	20
1	315	-45	Max	328.50	-1720.27	20	-93.15	20	-205.51	20	0.00	20
1	315	-45	Min.	0.00	-1958.34	20	-93.15	20	100.50	20	0.00	20
1	315	-45	Min.	328.50	-1720.27	20	-93.15	20	-205.51	20	0.00	20

2	2	202	Max	0.00	-2569.15	20	-0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
2	2	202	Max	328.50	-2331.08	20	-0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
2	2	202	Min.	0.00	-2569.15	20	-0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
2	2	202	Min.	328.50	-2331.08	20	-0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	0.00	-1958.34	20	93.15	20	-100.50	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	328.50	-1720.27	20	93.15	20	205.51	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	0.00	-1958.34	20	93.15	20	-100.50	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	328.50	-1720.27	20	93.15	20	205.51	20	0.00	20	0.00	20	0.00	20
201	-3	-29	Max	0.00	0.00	20	0.00	20	0.00	20	-189.50	20	0.00	20	0.00	20
201	-3	-29	Max	135.63	0.00	20	0.00	20	0.00	20	-313.01	20	-340.77	20	0.00	20
201	-3	-29	Min.	0.00	0.00	20	0.00	20	0.00	20	-189.50	20	0.00	20	0.00	20
201	-3	-29	Min.	135.63	0.00	20	0.00	20	0.00	20	-313.01	20	-340.77	20	0.00	20
201	-29	-45	Max	0.00	0.00	20	0.00	20	0.00	20	-583.68	20	-340.77	20	0.00	20
201	-29	-45	Max	83.77	0.00	20	0.00	20	0.00	20	-659.97	20	-861.68	20	0.00	20
201	-29	-45	Min.	0.00	0.00	20	0.00	20	0.00	20	-583.68	20	-340.77	20	0.00	20
201	-29	-45	Min.	83.77	0.00	20	0.00	20	0.00	20	-659.97	20	-861.68	20	0.00	20
201	-45	201	Max	0.00	-93.15	20	0.00	20	0.00	20	1060.30	20	-1067.19	20	0.00	20
201	-45	201	Max	51.86	-93.15	20	0.00	20	0.00	20	1013.08	20	-529.59	20	0.00	20
201	-45	201	Min.	0.00	-93.15	20	0.00	20	0.00	20	1060.30	20	-1067.19	20	0.00	20
201	-45	201	Min.	51.86	-93.15	20	0.00	20	0.00	20	1013.08	20	-529.59	20	0.00	20
201	201	-6	Max	0.00	-93.15	20	0.00	20	0.00	20	742.40	20	-529.59	20	0.00	20
201	201	-6	Max	135.63	-93.15	20	0.00	20	0.00	20	618.90	20	393.57	20	0.00	20
201	201	-6	Min.	0.00	-93.15	20	0.00	20	0.00	20	742.40	20	-529.59	20	0.00	20
201	201	-6	Min.	135.63	-93.15	20	0.00	20	0.00	20	618.90	20	393.57	20	0.00	20
201	-6	-7	Max	0.00	-93.15	20	0.00	20	0.00	20	348.22	20	393.59	20	0.00	20
201	-6	-7	Max	135.63	-93.15	20	0.00	20	0.00	20	224.72	20	782.12	20	0.00	20
201	-6	-7	Min.	0.00	-93.15	20	0.00	20	0.00	20	348.22	20	393.59	20	0.00	20
201	-6	-7	Min.	135.63	-93.15	20	0.00	20	0.00	20	224.72	20	782.12	20	0.00	20
201	-7	-8	Max	0.00	-93.15	20	0.00	20	0.00	20	-45.96	20	782.11	20	0.00	20
201	-7	-8	Max	135.63	-93.15	20	0.00	20	0.00	20	-169.46	20	636.02	20	0.00	20
201	-7	-8	Min.	0.00	-93.15	20	0.00	20	0.00	20	-45.96	20	782.11	20	0.00	20
201	-7	-8	Min.	135.63	-93.15	20	0.00	20	0.00	20	-169.46	20	636.02	20	0.00	20
201	-8	-9	Max	0.00	-93.15	20	0.00	20	0.00	20	-440.14	20	636.02	20	0.00	20
201	-8	-9	Max	135.63	-93.15	20	0.00	20	0.00	20	-563.64	20	-44.68	20	0.00	20
201	-8	-9	Min.	0.00	-93.15	20	0.00	20	0.00	20	-440.14	20	636.02	20	0.00	20
201	-8	-9	Min.	135.63	-93.15	20	0.00	20	0.00	20	-563.64	20	-44.68	20	0.00	20
201	-9	-10	Max	0.00	-93.15	20	0.00	20	0.00	20	-834.32	20	-44.69	20	0.00	20
201	-9	-10	Max	135.63	-93.15	20	0.00	20	0.00	20	-957.82	20	-1260.02	20	0.00	20
201	-9	-10	Min.	0.00	-93.15	20	0.00	20	0.00	20	-834.32	20	-44.69	20	0.00	20
201	-9	-10	Min.	135.63	-93.15	20	0.00	20	0.00	20	-957.82	20	-1260.02	20	0.00	20
201	-10	202	Max	0.00	-93.15	20	0.00	20	0.00	20	-1147.33	20	-1260.03	20	0.00	20
201	-10	202	Max	20.00	-93.15	20	0.00	20	0.00	20	-1165.54	20	-1491.32	20	0.00	20
201	-10	202	Min.	0.00	-93.15	20	0.00	20	0.00	20	-1147.33	20	-1260.03	20	0.00	20
201	-10	202	Min.	20.00	-93.15	20	0.00	20	0.00	20	-1165.54	20	-1491.32	20	0.00	20
202	202	-11	Max	0.00	-93.15	20	0.00	20	0.00	20	1165.54	20	-1491.32	20	0.00	20
202	202	-11	Max	20.00	-93.15	20	0.00	20	0.00	20	1147.33	20	-1260.03	20	0.00	20
202	202	-11	Min.	0.00	-93.15	20	0.00	20	0.00	20	1165.54	20	-1491.32	20	0.00	20
202	202	-11	Min.	20.00	-93.15	20	0.00	20	0.00	20	1147.33	20	-1260.03	20	0.00	20
202	-11	-12	Max	0.00	-93.15	20	0.00	20	0.00	20	957.83	20	-1260.04	20	0.00	20
202	-11	-12	Max	135.63	-93.15	20	0.00	20	0.00	20	834.32	20	-44.70	20	0.00	20
202	-11	-12	Min.	0.00	-93.15	20	0.00	20	0.00	20	957.83	20	-1260.04	20	0.00	20
202	-11	-12	Min.	135.63	-93.15	20	0.00	20	0.00	20	834.32	20	-44.70	20	0.00	20
202	-12	-13	Max	0.00	-93.15	20	0.00	20	0.00	20	563.64	20	-44.69	20	0.00	20
202	-12	-13	Max	135.63	-93.15	20	0.00	20	0.00	20	440.14	20	636.02	20	0.00	20
202	-12	-13	Min.	0.00	-93.15	20	0.00	20	0.00	20	563.64	20	-44.69	20	0.00	20
202	-12	-13	Min.	135.63	-93.15	20	0.00	20	0.00	20	440.14	20	636.02	20	0.00	20
202	-13	-14	Max	0.00	-93.15	20	0.00	20	0.00	20	169.46	20	636.02	20	0.00	20
202	-13	-14	Max	135.63	-93.15	20	0.00	20	0.00	20	45.96	20	782.11	20	0.00	20
202	-13	-14	Min.	0.00	-93.15	20	0.00	20	0.00	20	169.46	20	636.02	20	0.00	20
202	-13	-14	Min.	135.63	-93.15	20	0.00	20	0.00	20	45.96	20	782.11	20	0.00	20
202	-14	-15	Max	0.00	-93.15	20	0.00	20	0.00	20	-224.72	20	782.11	20	0.00	20
202	-14	-15	Max	135.63	-93.15	20	0.00	20	0.00	20	-348.23	20	393.57	20	0.00	20
202	-14	-15	Min.	0.00	-93.15	20	0.00	20	0.00	20	-224.72	20	782.11	20	0.00	20
202	-14	-15	Min.	135.63	-93.15	20	0.00	20	0.00	20	-348.23	20	393.57	20	0.00	20
202	-15	-77	Max	0.00	-93.15	20	0.00	20	0.00	20	-618.90	20	393.60	20	0.00	20
202	-15	-77	Max	135.63	-93.15	20	0.00	20	0.00	20	-742.40	20	-529.56	20	0.00	20
202	-15	-77	Min.	0.00	-93.15	20	0.00	20	0.00	20	-618.90	20	393.60	20	0.00	20
202	-15	-77	Min.	135.63	-93.15	20	0.00	20	0.00	20	-742.40	20	-529.56	20	0.00	20
202	-77	203	Max	0.00	-93.15	20	0.00	20	0.00	20	-1013.08	20	-529.57	20	0.00	20
202	-77	203	Max	51.86	-93.15	20	0.00	20	0.00	20	-1060.30	20	-1067.16	20	0.00	20
202	-77	203	Min.	0.00	-93.15	20	0.00	20	0.00	20	-1013.08	20	-529.57	20	0.00	20
202	-77	203	Min.	51.86	-93.15	20	0.00	20	0.00	20	-1060.30	20	-1067.16	20	0.00	20
202	203	-26	Max	0.00	0.00	20	0.00	20	0.00	20	659.97	20	-861.68	20	0.00	20
202	203	-26	Max	83.77	0.00	20	0.00	20	0.00	20	583.68	20	-340.77	20	0.00	20
202	203	-26	Min.	0.00	0.00	20	0.00	20	0.00	20	659.97	20	-861.68	20	0.00	20
202	203	-26	Min.	83.77	0.00	20	0.00	20	0.00	20	583.68	20	-340.77	20	0.00	20



202	-26	-18	Max	0.00	0.00	20	0.00	20	0.00	20	313.01	20	-340.78	20	0.00	20
202	-26	-18	Max	135.63	0.00	20	0.00	20	0.00	20	189.50	20	-0.00	20	0.00	20
202	-26	-18	Min.	0.00	0.00	20	0.00	20	0.00	20	313.01	20	-340.78	20	0.00	20
202	-26	-18	Min.	135.63	0.00	20	0.00	20	0.00	20	189.50	20	-0.00	20	0.00	20
302	-3	-69	Max	0.00	82.06	20	0.00	20	0.00	20	47.38	20	-41.22	20	0.00	20
302	-3	-69	Max	150.00	13.13	20	0.00	20	0.00	20	7.58	20	0.00	20	0.00	20
302	-3	-69	Min.	0.00	82.06	20	0.00	20	0.00	20	47.38	20	-41.22	20	0.00	20
302	-3	-69	Min.	150.00	13.13	20	0.00	20	0.00	20	7.58	20	0.00	20	0.00	20
302	-68	-3	Max	0.00	-13.13	20	0.00	20	0.00	20	-7.58	20	0.00	20	0.00	20
302	-68	-3	Max	150.00	-82.06	20	0.00	20	0.00	20	-47.38	20	-41.22	20	0.00	20
302	-68	-3	Min.	0.00	-13.13	20	0.00	20	0.00	20	-7.58	20	0.00	20	0.00	20
302	-68	-3	Min.	150.00	-82.06	20	0.00	20	0.00	20	-47.38	20	-41.22	20	0.00	20
303	-29	-76	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
303	-29	-76	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
303	-29	-76	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
303	-29	-76	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
303	-75	-29	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
303	-75	-29	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
303	-75	-29	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
303	-75	-29	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
305	-6	-48	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
305	-6	-48	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
305	-6	-48	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
305	-6	-48	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
305	-47	-6	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
305	-47	-6	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
305	-47	-6	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
305	-47	-6	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
306	-7	-50	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
306	-7	-50	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
306	-7	-50	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
306	-7	-50	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
306	-49	-7	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
306	-49	-7	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
306	-49	-7	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
306	-49	-7	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
307	-8	-52	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
307	-8	-52	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
307	-8	-52	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
307	-8	-52	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
307	-51	-8	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
307	-51	-8	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
307	-51	-8	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
307	-51	-8	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
308	-9	-54	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
308	-9	-54	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
308	-9	-54	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
308	-9	-54	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
308	-53	-9	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
308	-53	-9	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
308	-53	-9	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
308	-53	-9	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
309	-10	-56	Max	0.00	82.06	20	0.00	20	0.00	20	47.38	20	-41.22	20	0.00	20
309	-10	-56	Max	150.00	13.13	20	0.00	20	0.00	20	7.58	20	0.00	20	0.00	20
309	-10	-56	Min.	0.00	82.06	20	0.00	20	0.00	20	47.38	20	-41.22	20	0.00	20
309	-10	-56	Min.	150.00	13.13	20	0.00	20	0.00	20	7.58	20	0.00	20	0.00	20
309	-55	-10	Max	0.00	-13.13	20	0.00	20	0.00	20	-7.58	20	0.00	20	0.00	20
309	-55	-10	Max	150.00	-82.06	20	0.00	20	0.00	20	-47.38	20	-41.22	20	0.00	20
309	-55	-10	Min.	0.00	-13.13	20	0.00	20	0.00	20	-7.58	20	0.00	20	0.00	20
309	-55	-10	Min.	150.00	-82.06	20	0.00	20	0.00	20	-47.38	20	-41.22	20	0.00	20
310	-11	-58	Max	0.00	82.06	20	0.00	20	0.00	20	47.38	20	-41.22	20	0.00	20
310	-11	-58	Max	150.00	13.13	20	0.00	20	0.00	20	7.58	20	0.00	20	0.00	20
310	-11	-58	Min.	0.00	82.06	20	0.00	20	0.00	20	47.38	20	-41.22	20	0.00	20
310	-11	-58	Min.	150.00	13.13	20	0.00	20	0.00	20	7.58	20	0.00	20	0.00	20
310	-57	-11	Max	0.00	-13.13	20	0.00	20	0.00	20	-7.58	20	0.00	20	0.00	20
310	-57	-11	Max	150.00	-82.06	20	0.00	20	0.00	20	-47.38	20	-41.22	20	0.00	20
310	-57	-11	Min.	0.00	-13.13	20	0.00	20	0.00	20	-7.58	20	0.00	20	0.00	20
310	-57	-11	Min.	150.00	-82.06	20	0.00	20	0.00	20	-47.38	20	-41.22	20	0.00	20
311	-12	-60	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
311	-12	-60	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
311	-12	-60	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
311	-12	-60	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
311	-59	-12	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
311	-59	-12	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
311	-59	-12	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
311	-59	-12	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20

312	-13	-62	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
312	-13	-62	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
312	-13	-62	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
312	-13	-62	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
312	-61	-13	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
312	-61	-13	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
312	-61	-13	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
312	-61	-13	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
313	-14	-64	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
313	-14	-64	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
313	-14	-64	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
313	-14	-64	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
313	-63	-14	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
313	-63	-14	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
313	-63	-14	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
313	-63	-14	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
314	-15	-66	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
314	-15	-66	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
314	-15	-66	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
314	-15	-66	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
314	-65	-15	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
314	-65	-15	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
314	-65	-15	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
314	-65	-15	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
316	-26	-74	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
316	-26	-74	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
316	-26	-74	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
316	-26	-74	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
316	-73	-26	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
316	-73	-26	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
316	-73	-26	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
316	-73	-26	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
317	-18	-71	Max	0.00	82.06	20	0.00	20	0.00	20	47.38	20	-41.22	20	0.00	20
317	-18	-71	Max	150.00	13.13	20	0.00	20	0.00	20	7.58	20	0.00	20	0.00	20
317	-18	-71	Min.	0.00	82.06	20	0.00	20	0.00	20	47.38	20	-41.22	20	0.00	20
317	-18	-71	Min.	150.00	13.13	20	0.00	20	0.00	20	7.58	20	0.00	20	0.00	20
317	-70	-18	Max	0.00	-13.13	20	0.00	20	0.00	20	-7.58	20	0.00	20	0.00	20
317	-70	-18	Max	150.00	-82.06	20	0.00	20	0.00	20	-47.38	20	-41.22	20	0.00	20
317	-70	-18	Min.	0.00	-13.13	20	0.00	20	0.00	20	-7.58	20	0.00	20	0.00	20
317	-70	-18	Min.	150.00	-82.06	20	0.00	20	0.00	20	-47.38	20	-41.22	20	0.00	20
318	201	-81	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
318	201	-81	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
318	201	-81	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
318	201	-81	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
318	-80	201	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
318	-80	201	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
318	-80	201	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
318	-80	201	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
319	-77	-79	Max	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
319	-77	-79	Max	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
319	-77	-79	Min.	0.00	117.21	20	0.00	20	0.00	20	67.67	20	-62.12	20	0.00	20
319	-77	-79	Min.	150.00	26.25	20	0.00	20	0.00	20	15.16	20	0.00	20	0.00	20
319	-78	-77	Max	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
319	-78	-77	Max	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20
319	-78	-77	Min.	0.00	-26.25	20	0.00	20	0.00	20	-15.16	20	0.00	20	0.00	20
319	-78	-77	Min.	150.00	-117.21	20	0.00	20	0.00	20	-67.67	20	-62.12	20	0.00	20

Verifiche aste in acciaio

Simbologia

Φ_{LT}	=	Coefficiente Φ per stabilità laterale membrature inflesse
Φ_y	=	Coefficiente Φ per inflessione intorno all'asse y(c)
Φ_z	=	Coefficiente Φ per inflessione intorno all'asse z(e)
α_{imp}	=	Coefficiente di imperfezione
$\alpha_{my}, \alpha_{mz}, \alpha_{LT}$	=	Coefficienti correttivi per il momento flettente
β_{LT}	=	Coefficiente per calcolo Φ_{LT}
χ_{LT}	=	Coefficiente di riduzione per stabilità laterale membrature inflesse
χ_y	=	Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
χ_z	=	Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
δ	=	Spostamento relativo asta
λ^*_y	=	Snellezza adimensionale per inflessione intorno all'asse y(c)
λ^*_z	=	Snellezza adimensionale per inflessione intorno all'asse z(e)
λ_{LT}	=	Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$	=	Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
λ_y	=	Snellezza per inflessione intorno all'asse y(c)
λ_z	=	Snellezza per inflessione intorno all'asse z(e)
$\sigma_{D,max}$	<daN/cmq>	= Tensione ideale massima
σ_M	<daN/cmq>	= Tensione normale per momento flettente

σ_N	<daN/cmq>	=Tensione normale per sforzo normale
τ	<daN/cmq>	=Tensione tangenziale per taglio e/o torsione
ψ		=Coeff. di correzione momento critico per stabilità laterale membrature inflesse
Aeff	<cmq>	=Area effettiva per trazione
Anet	<cmq>	=Area netta per compressione
Area	<cmq>	=Area
Atag,y	<cmq>	=Area resistente a taglio in dir. Y
Atag,z	<cmq>	=Area resistente a taglio in dir. Z
CC		=Numero della combinazione delle condizioni di carico elementari
Cod.		=Codice
Curva		=Curva di instabilità adottata
D	<cm>	=Distanza
Fyk	<daN/cmq>	=Tensione caratteristica di snervamento dell'acciaio
Fyt	<daN/cmq>	=Tensione caratteristica di rottura
Iy	<cm>	=Raggio giratorio d'inerzia rispetto all'asse Y
Iz	<cm>	=Raggio giratorio d'inerzia rispetto all'asse Z
J0	<cm6>	=Costante di ingobbamento
Jy	<cm4>	=Momento d'inerzia rispetto all'asse Y
Jz	<cm4>	=Momento d'inerzia rispetto all'asse Z
Kyy, Kyz, Kzy, Kzz		=Coefficienti di interazione
L	<cm>	=Lunghezza dell'asta
Lcr	<cm>	=Lunghezza di libera inflessione laterale fra ritegni torsionali
M,cr	<daNm>	=Momento critico per instabilità flessione torsionale
MNy,c,Rd	<daNm>	=Resistenza di calcolo a pressoflessione intorno all'asse Y
Mx	<daNm>	=Momento torcente intorno all'asse X
My	<daNm>	=Momento flettente intorno all'asse Y
My,Ed	<daNm>	=Momento flettente di calcolo intorno all'asse Y
My,V,c,Rd	<daNm>	=Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y
Mz	<daNm>	=Momento flettente intorno all'asse Z
Mz,Ed	<daNm>	=Momento flettente di calcolo intorno all'asse Z
N	<daN>	=Sforzo normale
N,Ed	<daN>	=Forza assiale di calcolo
Nc,Rd	<daN>	=Resistenza a compressione
Ncr,y	<daN>	=Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
Ncr,z	<daN>	=Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
Sez.		=Numero della sezione
Tipologia		=Tipologia
		Rc = Rettangolare cava
		Is = I stondata
Tip		=Tipo di acciaio
Ty	<daN>	=Taglio in dir. Y
Tz	<daN>	=Taglio in dir. Z
V,Ed	<daN>	=Forza di taglio di calcolo
Vc,Rd	<daN>	=Resistenza a taglio
Vc,Rd,Red	<daN>	=Resistenza a taglio ridotta
Wy,plas	<cmc>	=Modulo di resistenza plastico intorno all'asse Y
Wymin	<cmc>	=Modulo di resistenza minimo rispetto all'asse Y
Wz,plas	<cmc>	=Modulo di resistenza plastico intorno all'asse Z
Wzmin	<cmc>	=Modulo di resistenza minimo rispetto all'asse Z
Xl	<cm>	=Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
f		=Fattore di modifica per il coefficiente di riduzione
fz,g	<cm>	=Freccia in direzione Z globale
fz,l	<cm>	=Freccia in direzione Z locale
kc		=Coeff. di correzione momento flettente per stabilità laterale membrature inflesse

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D	Area	Anet	Aeff	Jy	Jz	Iy	Iz	Wymin	Wzmin	Tip	Fyk	Fyt
			<cm>	<cmq>	<cmq>	<cmq>	<cm4>	<cm4>	<cm>	<cm>	<cmc>	<cmc>		<daN/cmq>	<daN/cmq>
1	COL HEA280	Is	--	97.27	97.27	97.27	13673.70	4762.65	11.86	7.00	1012.87	340.19	S355 UNI EN 10025-2	3550.00	5100.00
2	TRV PRINC SHS300x300x10	Rc	--	116.00	116.00	116.00	16278.70	16278.70	11.85	11.85	1085.24	1085.24	S355H UNI EN 10210-1	3550.00	5100.00
3	TRV SEC RHS150x100x10	Rc	--	46.00	46.00	46.00	1347.83	695.33	5.41	3.89	179.71	139.07	S355H UNI EN 10210-1	3550.00	5100.00

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy,plas	Wz,plas	Atag,y	Atag,z	J0
		<cmc>	<cmc>	<cmq>	<cmq>	<cm6>
1	COL HEA280	1117.45	518.72	81.59	31.75	785367.00
2	TRV PRINC SHS300x300x10	1262.00	1262.00	58.00	58.00	
3	TRV SEC RHS150x100x10	224.50	167.00	18.40	27.60	

Asta n. 1 (315 -45) - Sez. 1 (COL HEA280) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2080.76 Tz=-106.53 My=-376.19 Ty=-423.77 Mz=717.15
 Tensioni: $\sigma_N=-21.39$ $\sigma_{m,d}=-247.95$ $\tau=0.00$ $\sigma_{max}=-269.34$ (sfrut=0.08)
 Tensioni: $\sigma_N=-21.39$ $\sigma_{m,d}=75.73$ $\tau=8.40$ $\tau_{max}=8.40$ (sfrut=0.00)
 Tensioni: $\sigma_N=-21.39$ $\sigma_{m,d}=-247.95$ $\tau=0.00$ $\sigma_{TD,max}=269.34$ (sfrut=0.08)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-839.55 Tz=-3262.21 My=-11016.30 Ty=-5.63 Mz=6.07 Mx=-1.82
 Tensioni: $\sigma_N=-8.63$ $\sigma_{m,d}=-1089.42$ $\tau=4.23$ $\sigma_{max}=-1098.05$ (sfrut=0.32)
 Tensioni: $\sigma_N=-8.63$ $\sigma_{m,d}=-0.05$ $\tau=176.88$ $\tau_{max}=176.88$ (sfrut=0.09)
 Tensioni: $\sigma_N=-8.63$ $\sigma_{m,d}=-1089.42$ $\tau=4.23$ $\sigma_{TD,max}=1098.07$ (sfrut=0.32)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-839.55 My,Ed=-11016.30 Mz,Ed=-12.41 L=3.29
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $L_{cr}=3.29$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.72$ $M_{cr}=230491.00$ $\lambda_{LT}=0.39$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.56$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=27.71$ $N_{cr,y}=2626240.00$ $\lambda'_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ $N_{cr,z}=914738.00$ $\lambda'_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.31+0.00=0.31
 Verifica ZZ: 0.00+0.24+0.00=0.25

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=0.97$ (L/337)

Asta n. 2 (2 202) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2569.15 T_z=-129.72 M_y=-433.55 T_y=-424.69 M_z=718.65
 Tensioni: $\sigma_N=-26.41$ $\sigma_{m,d}=-254.06$ $\tau=0.00$ $\sigma_{max}=-280.47$ (sfrut=0.08)
 Tensioni: $\sigma_N=-26.41$ $\sigma_{m,d}=80.93$ $\tau=8.43$ $\tau_{max}=8.43$ (sfrut=0.00)
 Tensioni: $\sigma_N=-26.41$ $\sigma_{m,d}=-254.06$ $\tau=0.00$ $\sigma_{ID,max}=280.47$ (sfrut=0.08)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-1056.68 T_z=-4423.60 M_y=-13931.70
 Tensioni: $\sigma_N=-10.86$ $\sigma_{m,d}=-1375.47$ $\tau=0.00$ $\sigma_{max}=-1386.33$ (sfrut=0.41)
 Tensioni: $\sigma_N=-10.86$ $\sigma_{m,d}=0.00$ $\tau=239.78$ $\tau_{max}=239.78$ (sfrut=0.12)
 Tensioni: $\sigma_N=-10.86$ $\sigma_{m,d}=-1375.47$ $\tau=0.00$ $\sigma_{ID,max}=1386.33$ (sfrut=0.41)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-1056.68 M_{y,Ed}=-13931.70 M_{z,Ed}=0.00 L=3.29
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 L_{cr}=3.29 Curva b: $\alpha_{imp}=0.34$ k_c=0.94 $\psi=1.80$ M_{cr}=240416.00 $\lambda_{LT}=0.39$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.55$ $\beta_{LT}=0.75$ f=0.98 $\chi_{LT}=1.00$
 $\lambda_y=27.71$ Ncr,y=2626240.00 $\lambda^*_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ Ncr,z=914738.00 $\lambda^*_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.39=0.39
 Verifica ZZ: 0.00+0.31=0.31

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=1.19$ (L/275)

Asta n. 3 (3 203) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2080.76 T_z=-106.53 M_y=-376.19 T_y=423.77 M_z=-717.15
 Tensioni: $\sigma_N=-21.39$ $\sigma_{m,d}=-247.95$ $\tau=0.00$ $\sigma_{max}=-269.34$ (sfrut=0.08)
 Tensioni: $\sigma_N=-21.39$ $\sigma_{m,d}=-8.60$ $\tau=8.40$ $\tau_{max}=8.40$ (sfrut=0.00)
 Tensioni: $\sigma_N=-21.39$ $\sigma_{m,d}=-247.95$ $\tau=0.00$ $\sigma_{ID,max}=269.34$ (sfrut=0.08)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-839.55 T_z=-3262.21 M_y=-11016.30 T_y=5.62 M_z=-6.07 M_x=1.82
 Tensioni: $\sigma_N=-8.63$ $\sigma_{m,d}=-1089.42$ $\tau=4.23$ $\sigma_{max}=-1098.05$ (sfrut=0.32)
 Tensioni: $\sigma_N=-8.63$ $\sigma_{m,d}=0.05$ $\tau=176.88$ $\tau_{max}=176.88$ (sfrut=0.09)
 Tensioni: $\sigma_N=-8.63$ $\sigma_{m,d}=-1089.42$ $\tau=4.23$ $\sigma_{ID,max}=1098.07$ (sfrut=0.32)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-839.55 M_{y,Ed}=-11016.30 M_{z,Ed}=12.41 L=3.29
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 L_{cr}=3.29 Curva b: $\alpha_{imp}=0.34$ k_c=0.94 $\psi=1.72$ M_{cr}=230491.00 $\lambda_{LT}=0.39$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.56$ $\beta_{LT}=0.75$ f=0.98 $\chi_{LT}=1.00$
 $\lambda_y=27.71$ Ncr,y=2626240.00 $\lambda^*_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ Ncr,z=914738.00 $\lambda^*_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.31+0.00=0.31
 Verifica ZZ: 0.00+0.24+0.00=0.25

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=0.97$ (L/337)

Asta n. 201 (-3 -29) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=1.36 - Classe 3
 Sollecitazioni: N=13.36 T_z=-313.01 M_y=343.77 T_y=-44.52 M_z=-62.11 M_x=-10.00
 Tensioni: $\sigma_N=0.12$ $\sigma_{m,d}=37.40$ $\tau=0.59$ $\sigma_{max}=37.52$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.12$ $\sigma_{m,d}=-5.34$ $\tau=6.66$ $\tau_{max}=6.66$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.12$ $\sigma_{m,d}=37.40$ $\tau=0.59$ $\sigma_{ID,max}=37.53$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.36 - Classe 2
 Sollecitazioni: T_z=-435.32
 V,Ed=-435.32 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.36 - Classe 3
 Sollecitazioni: $T_z=-589.47$ $M_y=690.61$ $T_y=277.54$ $M_z=376.42$
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-98.32$ $\tau=0.00$ $\sigma_{max}=-98.32$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=32.37$ $\tau=11.43$ $\tau_{max}=11.43$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-98.32$ $\tau=0.00$ $\sigma_{ID,max}=98.32$ (sfrut=0.03)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-13.36$ $M_y,Ed=337.77$ $M_z,Ed=62.11$ $L=1.36$
 $\alpha_y, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341600.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341600.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.01+0.00=0.01$
 Verifica ZZ: $0.00+0.01+0.00=0.01$

Asta n. 201 (-29 -45) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.84 - Classe 3
 Sollecitazioni: $N=33.05$ $T_z=-659.97$ $M_y=869.21$ $T_y=-110.18$ $M_z=-157.03$ $M_x=-25.08$
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=94.56$ $\tau=1.49$ $\sigma_{max}=94.85$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=-13.50$ $\tau=14.28$ $\tau_{max}=14.28$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=94.56$ $\tau=1.49$ $\sigma_{ID,max}=94.88$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.84 - Classe 2
 Sollecitazioni: $T_z=-943.19$
 $V,Ed=-943.19$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.84 - Classe 3
 Sollecitazioni: $T_z=-1405.64$ $M_y=1826.59$ $T_y=832.62$ $M_z=1073.91$
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-267.27$ $\tau=0.00$ $\sigma_{max}=-267.27$ (sfrut=0.08)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=92.36$ $\tau=27.25$ $\tau_{max}=27.25$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-267.27$ $\tau=0.00$ $\sigma_{ID,max}=267.27$ (sfrut=0.08)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: $N,Ed=-33.05$ $M_y,Ed=854.16$ $M_z,Ed=157.03$ $L=0.84$
 $\alpha_y, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=7.07$ Ncr,y=48078400.00 $\lambda^*_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.07$ Ncr,z=48078400.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.03$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 201 (-45 201) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-281.56$ $T_z=1182.72$ $M_y=1561.71$ $T_y=63.87$ $M_z=-60.31$ $M_x=18.70$
 Tensioni: $\sigma_N=-2.43$ $\sigma_{m,d}=-149.46$ $\tau=1.11$ $\sigma_{max}=-151.89$ (sfrut=0.04)
 Tensioni: $\sigma_N=-2.43$ $\sigma_{m,d}=-5.19$ $\tau=24.03$ $\tau_{max}=24.03$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.43$ $\sigma_{m,d}=-149.46$ $\tau=1.11$ $\sigma_{ID,max}=151.90$ (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: $T_z=1531.47$
 $V,Ed=1531.47$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: $N=-224.73$ $T_z=2362.02$ $M_y=2322.37$ $T_y=-1482.95$ $M_z=1075.20$ $M_x=-212.90$
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-313.07$ $\tau=12.66$ $\sigma_{max}=-315.01$ (sfrut=0.09)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-92.47$ $\tau=58.45$ $\tau_{max}=58.45$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-313.07$ $\tau=12.66$ $\sigma_{ID,max}=315.77$ (sfrut=0.09)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-224.73$ $M_y,Ed=2322.37$ $M_z,Ed=1075.20$ $L=0.52$
 $\alpha_y, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.38$ Ncr,y=125463000.00 $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=4.38$ Ncr,z=125463000.00 $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.06+0.03=0.09$
 Verifica ZZ: $0.00+0.05+0.03=0.08$

Asta n. 201 (201 -6) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-218.47$ $T_z=864.82$ $M_y=975.70$ $T_y=44.95$ $M_z=-35.89$ $M_x=14.17$
 Tensioni: $\sigma_N=-1.88$ $\sigma_{m,d}=-93.21$ $\tau=0.84$ $\sigma_{max}=-95.10$ (sfrut=0.03)

Tensioni: $\sigma_N=-1.88$ $\sigma_{m,d}=-3.09$ $\tau=17.60$ $\tau_{max}=17.60$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.88$ $\sigma_{m,d}=-93.21$ $\tau=0.84$ $\sigma_{ID,max}=95.11$ (sfrut=0.03)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU $X_l=0.99$ - Classe 2
 Sollecitazioni: $T_y=1307.20$ $M_x=299.93$
 $V,Ed=1307.20$ $V_c,Rd,Red=112185.00$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU $X_l=0.99$ - Classe 2
 Sollecitazioni: $T_z=159.17$ $M_x=299.93$
 $V,Ed=159.17$ $V_c,Rd,Red=112185.00$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=1.36$ - Classe 3
 Sollecitazioni: $N=-224.73$ $T_z=1423.07$ $M_y=-925.58$ $T_y=-927.88$ $M_z=-952.29$ $M_x=-212.90$
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-173.04$ $\tau=12.66$ $\sigma_{max}=-174.97$ (sfrut=0.05)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=81.90$ $\tau=40.25$ $\tau_{max}=40.25$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-173.04$ $\tau=12.66$ $\sigma_{ID,max}=176.34$ (sfrut=0.05)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-224.73$ $M_y,Ed=1113.40$ $M_z,Ed=-952.29$ $L=1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ $N_{cr,y}=18341600.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ $N_{cr,z}=18341600.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.03+0.02=0.05$
 Verifica ZZ: $0.00+0.02+0.02=0.05$

Asta n. 201 (-6 -7) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND $X_l=1.36$ - Classe 3
 Sollecitazioni: $N=-76.51$ $T_z=187.99$ $M_y=-820.86$ $T_y=49.08$ $M_z=178.99$ $M_x=43.80$
 Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=-92.13$ $\tau=2.60$ $\sigma_{max}=-92.79$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=15.39$ $\tau=6.25$ $\tau_{max}=6.25$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=-92.13$ $\tau=2.60$ $\sigma_{ID,max}=92.90$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=492.12$
 $V,Ed=492.12$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=1.36$ - Classe 3
 Sollecitazioni: $N=-224.73$ $T_z=545.52$ $M_y=-1774.38$ $T_y=-372.80$ $M_z=-1457.95$ $M_x=-212.90$
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-297.84$ $\tau=12.66$ $\sigma_{max}=-299.78$ (sfrut=0.09)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=125.39$ $\tau=23.23$ $\tau_{max}=23.23$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-297.84$ $\tau=12.66$ $\sigma_{ID,max}=300.58$ (sfrut=0.09)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-224.73$ $M_y,Ed=-1774.38$ $M_z,Ed=-1457.95$ $L=1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ $N_{cr,y}=18341600.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ $N_{cr,z}=18341600.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.05+0.04=0.08$
 Verifica ZZ: $0.00+0.04+0.04=0.08$

Asta n. 201 (-7 -8) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-97.46$ $T_z=-82.68$ $M_y=-825.37$ $T_y=-20.76$ $M_z=181.60$ $M_x=28.72$
 Tensioni: $\sigma_N=-0.84$ $\sigma_{m,d}=-92.79$ $\tau=1.71$ $\sigma_{max}=-93.63$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.84$ $\sigma_{m,d}=-15.62$ $\tau=3.31$ $\tau_{max}=3.31$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.84$ $\sigma_{m,d}=-92.79$ $\tau=1.71$ $\sigma_{ID,max}=93.67$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=1.36$ - Classe 2
 Sollecitazioni: $T_z=-237.68$
 $V,Ed=-237.68$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-224.73$ $T_z=-171.47$ $M_y=-1774.33$ $T_y=182.28$ $M_z=-1457.91$ $M_x=-212.90$
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-297.84$ $\tau=12.66$ $\sigma_{max}=-299.77$ (sfrut=0.09)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-152.60$ $\tau=16.19$ $\tau_{max}=16.19$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-297.84$ $\tau=12.66$ $\sigma_{ID,max}=300.57$ (sfrut=0.09)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-224.73$ $M_y,Ed=-1774.33$ $M_z,Ed=-1457.91$ $L=1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ $N_{cr,y}=18341600.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=11.45$ Ncr,z=18341600.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.05+0.04=0.08
 Verifica ZZ: 0.00+0.04+0.04=0.08

Asta n. 201 (-8 -9) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-118.42 Tz=-476.86 My=-634.00 Ty=-90.61 Mz=156.05 Mx=13.64
 Tensioni: $\sigma_N=-1.02$ $\sigma_{m,d}=-72.80$ $\tau=0.81$ $\sigma_{max}=-73.82$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.02$ $\sigma_{m,d}=-13.42$ $\tau=10.05$ $\tau_{max}=10.05$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.02$ $\sigma_{m,d}=-72.80$ $\tau=0.81$ $\sigma_{ID,max}=73.83$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.36 - Classe 2
 Sollecitazioni: Tz=-806.94
 V,Ed=-806.94 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-224.73 Tz=-1049.03 My=-1432.88 Ty=737.36 Mz=-1210.69 Mx=-212.90
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-243.59$ $\tau=12.66$ $\sigma_{max}=-245.53$ (sfrut=0.07)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-104.12$ $\tau=33.00$ $\tau_{max}=33.00$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-243.59$ $\tau=12.66$ $\sigma_{ID,max}=246.51$ (sfrut=0.07)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-224.73 My,Ed=-1432.88 Mz,Ed=-1210.69 L=1.36
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341500.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341500.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.03=0.07
 Verifica ZZ: 0.00+0.03+0.03=0.06

Asta n. 201 (-9 -10) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.36 - Classe 3
 Sollecitazioni: N=-247.21 Tz=-1080.24 My=1583.77 Ty=-55.87 Mz=-58.26 Mx=2.48
 Tensioni: $\sigma_N=-2.13$ $\sigma_{m,d}=-151.31$ $\tau=0.15$ $\sigma_{max}=-153.44$ (sfrut=0.05)
 Tensioni: $\sigma_N=-2.13$ $\sigma_{m,d}=5.01$ $\tau=21.08$ $\tau_{max}=21.08$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.13$ $\sigma_{m,d}=-151.31$ $\tau=0.15$ $\sigma_{ID,max}=153.44$ (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.36 - Classe 2
 Sollecitazioni: Tz=-1376.20
 V,Ed=-1376.20 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.36 - Classe 3
 Sollecitazioni: N=-224.73 Tz=-2087.14 My=2820.68 Ty=1292.43 Mz=1542.29 Mx=-212.90
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-402.03$ $\tau=12.66$ $\sigma_{max}=-403.96$ (sfrut=0.12)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=132.64$ $\tau=53.12$ $\tau_{max}=53.12$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-402.03$ $\tau=12.66$ $\sigma_{ID,max}=404.56$ (sfrut=0.12)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-224.73 My,Ed=2820.68 Mz,Ed=1542.29 L=1.36
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341600.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341600.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.07+0.04=0.11
 Verifica ZZ: 0.00+0.06+0.04=0.10

Asta n. 201 (-10 202) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.20 - Classe 3
 Sollecitazioni: N=-293.34 Tz=-1287.96 My=1829.56 Ty=52.71 Mz=66.43 Mx=6.92
 Tensioni: $\sigma_N=-2.53$ $\sigma_{m,d}=-174.71$ $\tau=0.41$ $\sigma_{max}=-177.24$ (sfrut=0.05)
 Tensioni: $\sigma_N=-2.53$ $\sigma_{m,d}=-5.71$ $\tau=25.37$ $\tau_{max}=25.37$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.53$ $\sigma_{m,d}=-174.71$ $\tau=0.41$ $\sigma_{ID,max}=177.24$ (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.20 - Classe 2
 Sollecitazioni: Tz=-1674.65
 V,Ed=-1674.65 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.20 - Classe 3
 Sollecitazioni: N=-224.73 Tz=-2539.73 My=3326.30 Ty=1569.97 Mz=1856.31 Mx=-212.90
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-477.55$ $\tau=12.66$ $\sigma_{max}=-479.49$ (sfrut=0.14)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=159.65$ $\tau=61.90$ $\tau_{max}=61.90$ (sfrut=0.03)

Tensioni: $\sigma_N = -1.94$ $\sigma_{m,d} = -477.55$ $\tau = 12.66$ $\sigma_{ID,max} = 479.99$ (sfrut=0.14)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed = -224.73$ $M_y, Ed = 3326.30$ $M_z, Ed = 1856.31$ $L = 0.20$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 1.69$ Ncr, $y = 843464000.00$ $\lambda^*_y = 0.02$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 1.69$ Ncr, $z = 843463000.00$ $\lambda^*_z = 0.02$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.09 + 0.05 = 0.13$
 Verifica ZZ: $0.00 + 0.07 + 0.05 = 0.12$

Asta n. 202 (202 -11) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -293.34$ $T_z = 1287.96$ $M_y = 1829.56$ $T_y = -52.71$ $M_z = 66.43$ $M_x = -6.92$
 Tensioni: $\sigma_N = -2.53$ $\sigma_{m,d} = -174.71$ $\tau = 0.41$ $\sigma_{max} = -177.23$ (sfrut=0.05)
 Tensioni: $\sigma_N = -2.53$ $\sigma_{m,d} = -5.71$ $\tau = 25.37$ $\tau_{max} = 25.37$ (sfrut=0.01)
 Tensioni: $\sigma_N = -2.53$ $\sigma_{m,d} = -174.71$ $\tau = 0.41$ $\sigma_{ID,max} = 177.24$ (sfrut=0.05)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l = 0.00$ - Classe 2
 Sollecitazioni: $T_z = 1674.65$
 $V, Ed = 1674.65$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -224.73$ $T_z = 2539.74$ $M_y = 3326.30$ $T_y = -1569.97$ $M_z = 1856.30$ $M_x = 212.90$
 Tensioni: $\sigma_N = -1.94$ $\sigma_{m,d} = -477.55$ $\tau = 12.66$ $\sigma_{max} = -479.49$ (sfrut=0.14)
 Tensioni: $\sigma_N = -1.94$ $\sigma_{m,d} = 159.65$ $\tau = 61.90$ $\tau_{max} = 61.90$ (sfrut=0.03)
 Tensioni: $\sigma_N = -1.94$ $\sigma_{m,d} = -477.55$ $\tau = 12.66$ $\sigma_{ID,max} = 479.99$ (sfrut=0.14)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed = -224.73$ $M_y, Ed = 3326.30$ $M_z, Ed = 1856.30$ $L = 0.20$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 1.69$ Ncr, $y = 843464000.00$ $\lambda^*_y = 0.02$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 1.69$ Ncr, $z = 843463000.00$ $\lambda^*_z = 0.02$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.09 + 0.05 = 0.13$
 Verifica ZZ: $0.00 + 0.07 + 0.05 = 0.12$

Asta n. 202 (-11 -12) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -247.21$ $T_z = 1080.25$ $M_y = 1583.79$ $T_y = 55.87$ $M_z = -58.26$ $M_x = -2.48$
 Tensioni: $\sigma_N = -2.13$ $\sigma_{m,d} = -151.31$ $\tau = 0.15$ $\sigma_{max} = -153.44$ (sfrut=0.05)
 Tensioni: $\sigma_N = -2.13$ $\sigma_{m,d} = 5.01$ $\tau = 21.08$ $\tau_{max} = 21.08$ (sfrut=0.01)
 Tensioni: $\sigma_N = -2.13$ $\sigma_{m,d} = -151.31$ $\tau = 0.15$ $\sigma_{ID,max} = 153.44$ (sfrut=0.05)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l = 0.00$ - Classe 2
 Sollecitazioni: $T_z = 1376.21$
 $V, Ed = 1376.21$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -224.73$ $T_z = 2087.15$ $M_y = 2820.72$ $T_y = -1292.43$ $M_z = 1542.31$ $M_x = 212.90$
 Tensioni: $\sigma_N = -1.94$ $\sigma_{m,d} = -402.03$ $\tau = 12.66$ $\sigma_{max} = -403.97$ (sfrut=0.12)
 Tensioni: $\sigma_N = -1.94$ $\sigma_{m,d} = 132.64$ $\tau = 53.12$ $\tau_{max} = 53.12$ (sfrut=0.03)
 Tensioni: $\sigma_N = -1.94$ $\sigma_{m,d} = -402.03$ $\tau = 12.66$ $\sigma_{ID,max} = 404.56$ (sfrut=0.12)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed = -224.73$ $M_y, Ed = 2820.72$ $M_z, Ed = 1542.31$ $L = 1.36$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 11.45$ Ncr, $y = 18341500.00$ $\lambda^*_y = 0.15$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 11.45$ Ncr, $z = 18341500.00$ $\lambda^*_z = 0.15$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.07 + 0.04 = 0.11$
 Verifica ZZ: $0.00 + 0.06 + 0.04 = 0.10$

Asta n. 202 (-12 -13) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND $X_l = 1.36$ - Classe 3
 Sollecitazioni: $N = -118.42$ $T_z = 476.87$ $M_y = -633.99$ $T_y = 90.61$ $M_z = 156.05$ $M_x = -13.64$
 Tensioni: $\sigma_N = -1.02$ $\sigma_{m,d} = -72.80$ $\tau = 0.81$ $\sigma_{max} = -73.82$ (sfrut=0.02)
 Tensioni: $\sigma_N = -1.02$ $\sigma_{m,d} = -13.42$ $\tau = 10.05$ $\tau_{max} = 10.05$ (sfrut=0.01)
 Tensioni: $\sigma_N = -1.02$ $\sigma_{m,d} = -72.80$ $\tau = 0.81$ $\sigma_{ID,max} = 73.83$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l = 0.00$ - Classe 2
 Sollecitazioni: $T_z = 806.95$

V,Ed=806.95 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.36 - Classe 3
 Sollecitazioni: N=-224.73 Tz=1049.04 My=-1432.87 Ty=-737.36 Mz=-1210.69 Mx=212.90
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-243.59$ $\tau=12.66$ $\sigma_{max}=-245.53$ (sfrut=0.07)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-104.12$ $\tau=33.00$ $\tau_{max}=33.00$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-243.59$ $\tau=12.66$ $\sigma_{ID,max}=246.50$ (sfrut=0.07)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-224.73 My,Ed=-1432.87 Mz,Ed=-1210.69 L=1.36
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341500.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341500.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.03=0.07
 Verifica ZZ: 0.00+0.03+0.03=0.06

Asta n. 202 (-13 -14) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=1.36 - Classe 3
 Sollecitazioni: N=-97.46 Tz=82.68 My=-825.37 Ty=20.76 Mz=181.60 Mx=-28.72
 Tensioni: $\sigma_N=-0.84$ $\sigma_{m,d}=-92.79$ $\tau=1.71$ $\sigma_{max}=-93.63$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.84$ $\sigma_{m,d}=-15.62$ $\tau=3.31$ $\tau_{max}=3.31$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.84$ $\sigma_{m,d}=-92.79$ $\tau=1.71$ $\sigma_{ID,max}=93.67$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=237.69
 V,Ed=237.69 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.36 - Classe 3
 Sollecitazioni: N=-224.73 Tz=171.48 My=-1774.34 Ty=-182.28 Mz=-1457.92 Mx=212.90
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-297.84$ $\tau=12.66$ $\sigma_{max}=-299.77$ (sfrut=0.09)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-152.60$ $\tau=16.19$ $\tau_{max}=16.19$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-297.84$ $\tau=12.66$ $\sigma_{ID,max}=300.57$ (sfrut=0.09)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-224.73 My,Ed=-1774.34 Mz,Ed=-1457.92 L=1.36
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341500.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341500.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.05+0.04=0.08
 Verifica ZZ: 0.00+0.04+0.04=0.08

Asta n. 202 (-14 -15) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-76.51 Tz=-188.00 My=-820.85 Ty=-49.08 Mz=178.99 Mx=-43.80
 Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=-92.13$ $\tau=2.60$ $\sigma_{max}=-92.79$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=15.39$ $\tau=6.25$ $\tau_{max}=6.25$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.66$ $\sigma_{m,d}=-92.13$ $\tau=2.60$ $\sigma_{ID,max}=92.90$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.36 - Classe 2
 Sollecitazioni: Tz=-492.13
 V,Ed=-492.13 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-224.73 Tz=-545.52 My=-1774.34 Ty=372.80 Mz=-1457.92 Mx=212.90
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-297.84$ $\tau=12.66$ $\sigma_{max}=-299.77$ (sfrut=0.09)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=125.39$ $\tau=23.23$ $\tau_{max}=23.23$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-297.84$ $\tau=12.66$ $\sigma_{ID,max}=300.57$ (sfrut=0.09)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-224.73 My,Ed=-1774.34 Mz,Ed=-1457.92 L=1.36
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr,y=18341500.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr,z=18341500.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.05+0.04=0.08
 Verifica ZZ: 0.00+0.04+0.04=0.08

Asta n. 202 (-15 -77) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.36 - Classe 3
 Sollecitazioni: N=-218.47 Tz=-864.82 My=975.66 Ty=-44.95 Mz=-35.89 Mx=-14.17

Tensioni: $\sigma_N=-1.88$ $\sigma_{m,d}=-93.21$ $\tau=0.84$ $\sigma_{max}=-95.09$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.88$ $\sigma_{m,d}=-3.09$ $\tau=17.60$ $\tau_{max}=17.60$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.88$ $\sigma_{m,d}=-93.21$ $\tau=0.84$ $\sigma_{ID,max}=95.10$ (sfrut=0.03)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU $X_l=0.37$ - Classe 2
 Sollecitazioni: $T_y=-1307.20$ $M_x=-299.93$
 $V,Ed=-1307.20$ $V_c,Rd,Red=112185.00$ $V,Ed/V_c,Rd,Red=0.01$

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU $X_l=0.37$ - Classe 2
 Sollecitazioni: $T_z=-159.17$ $M_x=-299.93$
 $V,Ed=-159.17$ $V_c,Rd,Red=112185.00$ $V,Ed/V_c,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-224.73$ $T_z=-1423.07$ $M_y=-925.64$ $T_y=927.88$ $M_z=-952.34$ $M_x=212.90$
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-173.05$ $\tau=12.66$ $\sigma_{max}=-174.98$ (sfrut=0.05)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=81.90$ $\tau=40.25$ $\tau_{max}=40.25$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-173.05$ $\tau=12.66$ $\sigma_{ID,max}=176.35$ (sfrut=0.05)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-224.73$ $M_y,Ed=1113.33$ $M_z,Ed=-952.34$ $L=1.36$
 $\alpha_y, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.45$ Ncr, $y=18341500.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr, $z=18341500.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.03+0.02=0.05$
 Verifica ZZ: $0.00+0.02+0.02=0.05$

Asta n. 202 (-77 203) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND $X_l=0.52$ - Classe 3
 Sollecitazioni: $N=-281.56$ $T_z=-1182.72$ $M_y=1561.68$ $T_y=-63.87$ $M_z=-60.31$ $M_x=-18.70$
 Tensioni: $\sigma_N=-2.43$ $\sigma_{m,d}=-149.46$ $\tau=1.11$ $\sigma_{max}=-151.89$ (sfrut=0.04)
 Tensioni: $\sigma_N=-2.43$ $\sigma_{m,d}=-5.19$ $\tau=24.03$ $\tau_{max}=24.03$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.43$ $\sigma_{m,d}=-149.46$ $\tau=1.11$ $\sigma_{ID,max}=151.90$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.52$ - Classe 2
 Sollecitazioni: $T_z=-1531.47$
 $V,Ed=-1531.47$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.52$ - Classe 3
 Sollecitazioni: $N=-224.73$ $T_z=-2362.02$ $M_y=2322.31$ $T_y=1482.95$ $M_z=1075.16$ $M_x=212.90$
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-313.06$ $\tau=12.66$ $\sigma_{max}=-315.00$ (sfrut=0.09)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-92.47$ $\tau=58.45$ $\tau_{max}=58.45$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-313.06$ $\tau=12.66$ $\sigma_{ID,max}=315.76$ (sfrut=0.09)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-224.73$ $M_y,Ed=2322.31$ $M_z,Ed=1075.16$ $L=0.52$
 $\alpha_y, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.38$ Ncr, $y=125464000.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=4.38$ Ncr, $z=125464000.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.06+0.03=0.09$
 Verifica ZZ: $0.00+0.05+0.03=0.08$

Asta n. 202 (203 -26) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=33.05$ $T_z=659.97$ $M_y=869.21$ $T_y=110.18$ $M_z=-157.02$ $M_x=25.08$
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=94.56$ $\tau=1.49$ $\sigma_{max}=94.85$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=-13.50$ $\tau=14.28$ $\tau_{max}=14.28$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=94.56$ $\tau=1.49$ $\sigma_{ID,max}=94.88$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=943.19$
 $V,Ed=943.19$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.00$ - Classe 3
 Sollecitazioni: $T_z=1405.64$ $M_y=1826.59$ $T_y=-832.62$ $M_z=1073.91$
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-267.27$ $\tau=0.00$ $\sigma_{max}=-267.27$ (sfrut=0.08)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=92.36$ $\tau=27.25$ $\tau_{max}=27.25$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-267.27$ $\tau=0.00$ $\sigma_{ID,max}=267.27$ (sfrut=0.08)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
 Sollecitazioni: $N,Ed=-33.05$ $M_y,Ed=854.16$ $M_z,Ed=157.02$ $L=0.84$
 $\alpha_y, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=7.07$ Ncr, $y=48078100.00$ $\lambda^*_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.07$ Ncr, $z=48078100.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.03
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 202 (-26 -18) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=13.36 T_z=313.01 M_y=343.78 T_y=44.52 M_z=-62.11 M_x=10.00
 Tensioni: $\sigma_N=0.12$ $\sigma_{m,d}=37.40$ $\tau=0.59$ $\sigma_{max}=37.52$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.12$ $\sigma_{m,d}=-5.34$ $\tau=6.66$ $\tau_{max}=6.66$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.12$ $\sigma_{m,d}=37.40$ $\tau=0.59$ $\sigma_{ID,max}=37.53$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: T_z=435.32
 V,Ed=435.32 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: T_z=589.47 M_y=690.62 T_y=-277.54 M_z=376.43
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-98.32$ $\tau=0.00$ $\sigma_{max}=-98.32$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=32.37$ $\tau=11.43$ $\tau_{max}=11.43$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-98.32$ $\tau=0.00$ $\sigma_{ID,max}=98.32$ (sfrut=0.03)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
 Sollecitazioni: N,Ed=-13.36 M_y,Ed=337.78 M_z,Ed=62.11 L=1.36
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=11.45$ Ncr, $y=18341500.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.45$ Ncr, $z=18341500.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.00=0.01
 Verifica ZZ: 0.00+0.01+0.00=0.01

Asta n. 302 (-3 -69) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=81.17 T_z=48.91 M_y=43.51 T_y=-5.89 M_z=8.83
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.56$ $\tau=0.00$ $\sigma_{max}=32.33$ (sfrut=0.01)
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=5.08$ $\tau=2.04$ $\tau_{max}=2.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.56$ $\tau=0.00$ $\sigma_{ID,max}=32.33$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=227.41
 V,Ed=227.41 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=116.34 T_z=227.41 M_y=224.38
 M_y,Ed=224.38 M_y,V,c,Rd=7590.24
 N,Ed=116.34 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 M_{Ny},c,Rd=7590.24 M_y,Ed/M_{Ny},c,Rd=0.03

Asta n. 302 (-68 -3) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-80.02 T_z=-50.91 M_y=46.51 T_y=13.59 M_z=20.38
 Tensioni: $\sigma_N=-1.74$ $\sigma_{m,d}=-40.54$ $\tau=0.00$ $\sigma_{max}=-42.28$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.74$ $\sigma_{m,d}=11.72$ $\tau=2.12$ $\tau_{max}=2.12$ (sfrut=0.00)
 Tensioni: $\sigma_N=-1.74$ $\sigma_{m,d}=-40.54$ $\tau=0.00$ $\sigma_{ID,max}=42.28$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-227.41
 V,Ed=-227.41 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-116.34 T_z=-227.41 M_y=224.38
 M_y,Ed=224.38 M_y,V,c,Rd=7590.24
 N,Ed=-116.34 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 M_{Ny},c,Rd=7590.24 M_y,Ed/M_{Ny},c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-116.34 M_y,Ed=224.38 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.03=0.03
 Verifica ZZ: 0.00=0.00

Asta n. 303 (-29 -76) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.88 T_z=69.97 M_y=65.58 T_y=-8.87 M_z=13.31
 Tensioni: σ_N=2.52 σ_{m,d}=46.06 τ=0.00 σ_{max}=48.58 (sfrut=0.01)
 Tensioni: σ_N=2.52 σ_{m,d}=7.66 τ=2.91 τ_{max}=2.91 (sfrut=0.00)
 Tensioni: σ_N=2.52 σ_{m,d}=46.06 τ=0.00 σ_{ID,max}=48.58 (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=419.61
 V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=171.70 T_z=419.61 M_y=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 303 (-75 -29) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-114.14 T_z=-72.99 M_y=70.10 T_y=20.48 M_z=30.72
 Tensioni: σ_N=-2.48 σ_{m,d}=-61.10 τ=0.00 σ_{max}=-63.58 (sfrut=0.02)
 Tensioni: σ_N=-2.48 σ_{m,d}=17.67 τ=3.04 τ_{max}=3.04 (sfrut=0.00)
 Tensioni: σ_N=-2.48 σ_{m,d}=-61.10 τ=0.00 σ_{ID,max}=63.58 (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-419.61
 V,Ed=-419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-171.70 T_z=-419.61 M_y=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=-171.70 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=1.50
 α_{my}, α_{LT}=0.95, 0.95, 0.95
 λ_y=27.71 Ncr,y=1241570.00 λ_y^{*}=0.36 Curva a: Φ_y=0.58 χ_y=0.96
 λ_z=38.58 Ncr,z=640514.00 λ_z^{*}=0.50 Curva a: Φ_z=0.66 χ_z=0.92
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 305 (-6 -48) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.88 T_z=69.97 M_y=65.58 T_y=-8.87 M_z=13.31
 Tensioni: σ_N=2.52 σ_{m,d}=46.06 τ=0.00 σ_{max}=48.58 (sfrut=0.01)
 Tensioni: σ_N=2.52 σ_{m,d}=7.66 τ=2.91 τ_{max}=2.91 (sfrut=0.00)
 Tensioni: σ_N=2.52 σ_{m,d}=46.06 τ=0.00 σ_{ID,max}=48.58 (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=419.61
 V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=171.70 T_z=419.61 M_y=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 305 (-47 -6) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-114.14 T_z=-72.99 M_y=70.10 T_y=20.48 M_z=30.72
 Tensioni: σ_N=-2.48 σ_{m,d}=-61.10 τ=0.00 σ_{max}=-63.58 (sfrut=0.02)
 Tensioni: σ_N=-2.48 σ_{m,d}=17.67 τ=3.04 τ_{max}=3.04 (sfrut=0.00)
 Tensioni: σ_N=-2.48 σ_{m,d}=-61.10 τ=0.00 σ_{ID,max}=63.58 (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-419.61
 V,Ed=-419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-171.70 T_z=-419.61 M_y=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24

N,Ed=-171.70 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640514.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 306 (-7 -50) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.88 Tz=69.97 My=65.58 Ty=-8.87 Mz=13.31
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{max}=48.58$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=7.66$ $\tau=2.91$ $\tau_{max}=2.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{ID,max}=48.58$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=419.61
 V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=171.70 Tz=419.61 My=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 306 (-49 -7) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-114.14 Tz=-72.99 My=70.10 Ty=20.48 Mz=30.72
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{max}=-63.58$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=17.67$ $\tau=3.04$ $\tau_{max}=3.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{ID,max}=63.58$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-419.61
 V,Ed=-419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-171.70 Tz=-419.61 My=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=-171.70 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640514.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 307 (-8 -52) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.88 Tz=69.97 My=65.58 Ty=-8.87 Mz=13.31
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{max}=48.58$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=7.66$ $\tau=2.91$ $\tau_{max}=2.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{ID,max}=48.58$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=419.61
 V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=171.70 Tz=419.61 My=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 307 (-51 -8) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-114.14 Tz=-72.99 My=70.10 Ty=20.48 Mz=30.72
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{max}=-63.58$ (sfrut=0.02)

Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=17.67$ $\tau=3.04$ $\tau_{max}=3.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{ID,max}=63.58$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-419.61$
 $V,Ed=-419.61$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $N=-171.70$ $T_z=-419.61$ $M_y=422.37$
 $M_y,Ed=422.37$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-171.70$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.06$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-171.70$ $M_y,Ed=422.37$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.57 , 0.00 , 0.95
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 308 (-9 -54) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=115.88$ $T_z=69.97$ $M_y=65.58$ $T_y=-8.87$ $M_z=13.31$
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{max}=48.58$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=7.66$ $\tau=2.91$ $\tau_{max}=2.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{ID,max}=48.58$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=419.61$
 $V,Ed=419.61$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=171.70$ $T_z=419.61$ $M_y=422.37$
 $M_y,Ed=422.37$ $M_y,V,c,Rd=7590.24$
 $N,Ed=171.70$ $N_c,Rd=155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.06$

Asta n. 308 (-53 -9) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=-114.14$ $T_z=-72.99$ $M_y=70.10$ $T_y=20.48$ $M_z=30.72$
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{max}=-63.58$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=17.67$ $\tau=3.04$ $\tau_{max}=3.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{ID,max}=63.58$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-419.61$
 $V,Ed=-419.61$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $N=-171.70$ $T_z=-419.61$ $M_y=422.37$
 $M_y,Ed=422.37$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-171.70$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.06$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-171.70$ $M_y,Ed=422.37$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.57 , 0.00 , 0.95
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 309 (-10 -56) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=81.17$ $T_z=48.91$ $M_y=43.51$ $T_y=-5.89$ $M_z=8.83$
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.56$ $\tau=0.00$ $\sigma_{max}=32.33$ (sfrut=0.01)
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=5.08$ $\tau=2.04$ $\tau_{max}=2.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.56$ $\tau=0.00$ $\sigma_{ID,max}=32.33$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=227.41$
 $V,Ed=227.41$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.00$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=116.34 T_z=227.41 M_y=224.38
My,Ed=224.38 My,V,c,Rd=7590.24
N,Ed=116.34 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

Asta n. 309 (-55 -10) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-80.02 T_z=-50.91 M_y=46.51 T_y=13.59 M_z=20.38
Tensioni: σ_N=-1.74 σ_{m,d}=-40.54 τ=0.00 σ_{max}=-42.28 (sfrut=0.01)
Tensioni: σ_N=-1.74 σ_{m,d}=11.72 τ=2.12 τ_{max}=2.12 (sfrut=0.00)
Tensioni: σ_N=-1.74 σ_{m,d}=-40.54 τ=0.00 σ_{ID,max}=42.28 (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_z=-227.41
V,Ed=-227.41 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-116.34 T_z=-227.41 M_y=224.38
My,Ed=224.38 My,V,c,Rd=7590.24
N,Ed=-116.34 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-116.34 My,Ed=224.38 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.71 Ncr,y=1241570.00 λ_y^{*}=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=38.58 Ncr,z=640514.00 λ_z^{*}=0.50 Curva a: Φ_z=0.66 χ_z=0.92
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

Asta n. 310 (-11 -58) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=81.17 T_z=48.91 M_y=43.51 T_y=-5.89 M_z=8.83
Tensioni: σ_N=1.76 σ_{m,d}=30.56 τ=0.00 σ_{max}=32.33 (sfrut=0.01)
Tensioni: σ_N=1.76 σ_{m,d}=5.08 τ=2.04 τ_{max}=2.04 (sfrut=0.00)
Tensioni: σ_N=1.76 σ_{m,d}=30.56 τ=0.00 σ_{ID,max}=32.33 (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=227.41
V,Ed=227.41 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=116.34 T_z=227.41 M_y=224.38
My,Ed=224.38 My,V,c,Rd=7590.24
N,Ed=116.34 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

Asta n. 310 (-57 -11) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-80.02 T_z=-50.91 M_y=46.51 T_y=13.59 M_z=20.38
Tensioni: σ_N=-1.74 σ_{m,d}=-40.54 τ=0.00 σ_{max}=-42.28 (sfrut=0.01)
Tensioni: σ_N=-1.74 σ_{m,d}=11.72 τ=2.12 τ_{max}=2.12 (sfrut=0.00)
Tensioni: σ_N=-1.74 σ_{m,d}=-40.54 τ=0.00 σ_{ID,max}=42.28 (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_z=-227.41
V,Ed=-227.41 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-116.34 T_z=-227.41 M_y=224.38
My,Ed=224.38 My,V,c,Rd=7590.24
N,Ed=-116.34 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-116.34 My,Ed=224.38 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.71 Ncr,y=1241570.00 λ_y^{*}=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=38.58 Ncr,z=640514.00 λ_z^{*}=0.50 Curva a: Φ_z=0.66 χ_z=0.92
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

Asta n. 311 (-12 -60) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.88 T_z=69.97 M_y=65.58 T_y=-8.87 M_z=13.31
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{max}=48.58$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=7.66$ $\tau=2.91$ $\tau_{max}=2.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{ID,max}=48.58$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=419.61
 V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=171.70 T_z=419.61 M_y=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 311 (-59 -12) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-114.14 T_z=-72.99 M_y=70.10 T_y=20.48 M_z=30.72
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{max}=-63.58$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=17.67$ $\tau=3.04$ $\tau_{max}=3.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{ID,max}=63.58$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-419.61
 V,Ed=-419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-171.70 T_z=-419.61 M_y=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=-171.70 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640514.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 312 (-13 -62) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.88 T_z=69.97 M_y=65.58 T_y=-8.87 M_z=13.31
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{max}=48.58$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=7.66$ $\tau=2.91$ $\tau_{max}=2.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{ID,max}=48.58$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=419.61
 V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=171.70 T_z=419.61 M_y=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 312 (-61 -13) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-114.14 T_z=-72.99 M_y=70.10 T_y=20.48 M_z=30.72
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{max}=-63.58$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=17.67$ $\tau=3.04$ $\tau_{max}=3.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{ID,max}=63.58$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-419.61
 V,Ed=-419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-171.70 T_z=-419.61 M_y=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=-171.70 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640514.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 313 (-14 -64) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.88 Tz=69.97 My=65.58 Ty=-8.87 Mz=13.31
 Tensioni: $\sigma_N=2.52 \sigma_{m,d}=46.06 \tau=0.00 \sigma_{max}=48.58$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.52 \sigma_{m,d}=7.66 \tau=2.91 \tau_{max}=2.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.52 \sigma_{m,d}=46.06 \tau=0.00 \sigma_{ID,max}=48.58$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=419.61
 V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=171.70 Tz=419.61 My=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 313 (-63 -14) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-114.14 Tz=-72.99 My=70.10 Ty=20.48 Mz=30.72
 Tensioni: $\sigma_N=-2.48 \sigma_{m,d}=-61.10 \tau=0.00 \sigma_{max}=-63.58$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.48 \sigma_{m,d}=17.67 \tau=3.04 \tau_{max}=3.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.48 \sigma_{m,d}=-61.10 \tau=0.00 \sigma_{ID,max}=63.58$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-419.61
 V,Ed=-419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-171.70 Tz=-419.61 My=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=-171.70 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640514.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 314 (-15 -66) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.88 Tz=69.97 My=65.58 Ty=-8.87 Mz=13.31
 Tensioni: $\sigma_N=2.52 \sigma_{m,d}=46.06 \tau=0.00 \sigma_{max}=48.58$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.52 \sigma_{m,d}=7.66 \tau=2.91 \tau_{max}=2.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.52 \sigma_{m,d}=46.06 \tau=0.00 \sigma_{ID,max}=48.58$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=419.61
 V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=171.70 Tz=419.61 My=422.37
 My,Ed=422.37 My,V,c,Rd=7590.24
 N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 314 (-65 -15) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-114.14 Tz=-72.99 My=70.10 Ty=20.48 Mz=30.72
 Tensioni: $\sigma_N=-2.48 \sigma_{m,d}=-61.10 \tau=0.00 \sigma_{max}=-63.58$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.48 \sigma_{m,d}=17.67 \tau=3.04 \tau_{max}=3.04$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.48 \sigma_{m,d}=-61.10 \tau=0.00 \sigma_{ID,max}=63.58$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: $T_z=-419.61$
 $V,Ed=-419.61$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: $N=-171.70$ $T_z=-419.61$ $M_y=422.37$
 $M_y,Ed=422.37$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-171.70$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.06$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N,Ed=-171.70$ $M_y,Ed=422.37$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
Verifica YY: $0.00+0.05=0.05$
Verifica ZZ: $0.00=0.00$

Asta n. 316 (-26 -74) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=115.88$ $T_z=69.97$ $M_y=65.58$ $T_y=-8.87$ $M_z=13.31$
Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{max}=48.58$ (sfrut=0.01)
Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=7.66$ $\tau=2.91$ $\tau_{max}=2.91$ (sfrut=0.00)
Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{ID,max}=48.58$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: $T_z=419.61$
 $V,Ed=419.61$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: $N=171.70$ $T_z=419.61$ $M_y=422.37$
 $M_y,Ed=422.37$ $M_y,V,c,Rd=7590.24$
 $N,Ed=171.70$ $N_c,Rd=155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.06$

Asta n. 316 (-73 -26) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: $N=-114.14$ $T_z=-72.99$ $M_y=70.10$ $T_y=20.48$ $M_z=30.72$
Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{max}=-63.58$ (sfrut=0.02)
Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=17.67$ $\tau=3.04$ $\tau_{max}=3.04$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{ID,max}=63.58$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: $T_z=-419.61$
 $V,Ed=-419.61$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: $N=-171.70$ $T_z=-419.61$ $M_y=422.37$
 $M_y,Ed=422.37$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-171.70$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.06$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N,Ed=-171.70$ $M_y,Ed=422.37$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
Verifica YY: $0.00+0.05=0.05$
Verifica ZZ: $0.00=0.00$

Asta n. 317 (-18 -71) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=81.17$ $T_z=48.91$ $M_y=43.51$ $T_y=-5.89$ $M_z=8.83$
Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.56$ $\tau=0.00$ $\sigma_{max}=32.33$ (sfrut=0.01)
Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=5.08$ $\tau=2.04$ $\tau_{max}=2.04$ (sfrut=0.00)
Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.56$ $\tau=0.00$ $\sigma_{ID,max}=32.33$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: $T_z=227.41$
 $V,Ed=227.41$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: $N=116.34$ $T_z=227.41$ $M_y=224.39$
 $M_y,Ed=224.39$ $M_y,V,c,Rd=7590.24$

N,Ed=116.34 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

Asta n. 317 (-70 -18) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.02 Tz=-50.91 My=46.51 Ty=13.59 Mz=20.38

Tensioni: $\sigma_N=-1.74$ $\sigma_{m,d}=-40.54$ $\tau=0.00$ $\sigma_{max}=-42.28$ (sfrut=0.01)

Tensioni: $\sigma_N=-1.74$ $\sigma_{m,d}=11.72$ $\tau=2.12$ $\tau_{max}=2.12$ (sfrut=0.00)

Tensioni: $\sigma_N=-1.74$ $\sigma_{m,d}=-40.54$ $\tau=0.00$ $\sigma_{ID,max}=42.28$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: Tz=-227.41

V,Ed=-227.41 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-116.34 Tz=-227.41 My=224.38

My,Ed=224.38 My,V,c,Rd=7590.24

N,Ed=-116.34 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-116.34 My,Ed=224.38 L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=38.58$ Ncr,z=640514.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.03=0.03

Verifica ZZ: 0.00=0.00

Asta n. 318 (201 -81) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=115.88 Tz=69.97 My=65.58 Ty=-8.87 Mz=13.31

Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{max}=48.58$ (sfrut=0.01)

Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=7.66$ $\tau=2.91$ $\tau_{max}=2.91$ (sfrut=0.00)

Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{ID,max}=48.58$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: Tz=419.61

V,Ed=419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=171.70 Tz=419.61 My=422.37

My,Ed=422.37 My,V,c,Rd=7590.24

N,Ed=171.70 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

Asta n. 318 (-80 201) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-114.14 Tz=-72.99 My=70.10 Ty=20.48 Mz=30.72

Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{max}=-63.58$ (sfrut=0.02)

Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=17.67$ $\tau=3.04$ $\tau_{max}=3.04$ (sfrut=0.00)

Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{ID,max}=63.58$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: Tz=-419.61

V,Ed=-419.61 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-171.70 Tz=-419.61 My=422.37

My,Ed=422.37 My,V,c,Rd=7590.24

N,Ed=-171.70 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=38.58$ Ncr,z=640514.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

Asta n. 319 (-77 -79) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=115.88 Tz=69.97 My=65.58 Ty=-8.87 Mz=13.31

Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{max}=48.58$ (sfrut=0.01)

Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=7.66$ $\tau=2.91$ $\tau_{max}=2.91$ (sfrut=0.00)
Tensioni: $\sigma_N=2.52$ $\sigma_{m,d}=46.06$ $\tau=0.00$ $\sigma_{ID,max}=48.58$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $Xl=0.00$ - Classe 1
Sollecitazioni: $T_z=419.61$
 $V,Ed=419.61$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $Xl=0.00$ - Classe 1
Sollecitazioni: $N=171.70$ $T_z=419.61$ $M_y=422.37$
 $M_y,Ed=422.37$ $M_y,V,c,Rd=7590.24$
 $N,Ed=171.70$ $Nc,Rd=155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.06$

Asta n. 319 (-78 -77) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=1.50$ - Classe 3
Sollecitazioni: $N=-114.14$ $T_z=-72.99$ $M_y=70.10$ $T_y=20.48$ $M_z=30.72$
Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{max}=-63.58$ (sfrut=0.02)
Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=17.67$ $\tau=3.04$ $\tau_{max}=3.04$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.48$ $\sigma_{m,d}=-61.10$ $\tau=0.00$ $\sigma_{ID,max}=63.58$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $Xl=1.50$ - Classe 1
Sollecitazioni: $T_z=-419.61$
 $V,Ed=-419.61$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $Xl=1.50$ - Classe 1
Sollecitazioni: $N=-171.70$ $T_z=-419.61$ $M_y=422.37$
 $M_y,Ed=422.37$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-171.70$ $Nc,Rd=-155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.06$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N,Ed=-171.70$ $M_y,Ed=422.37$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640514.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.57 , 0.00 , 0.95
Verifica YY: $0.00+0.05=0.05$
Verifica ZZ: $0.00=0.00$

Membratura

Asta 201 Nodi -3 -29 -45 201 -6 -7 -8 -9 -10 202 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: $N,Ed=-224.73$ $M_y,Ed=3326.30$ $M_z,Ed=1856.31$ $L=9.69$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=81.83$ $Ncr,y=359032.00$ $\lambda^*_y=1.07$ Curva a: $\Phi_y=1.16$ $\chi_y=0.62$
 $\lambda_z=81.83$ $Ncr,z=359031.00$ $\lambda^*_z=1.07$ Curva a: $\Phi_z=1.16$ $\chi_z=0.62$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
Verifica YY: $0.00+0.09+0.05=0.14$
Verifica ZZ: $0.00+0.07+0.05=0.12$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.08$ (L/12765) $f_{z,G}=0.07$ (L/12990)

- Verifica freccia massima carichi totali - CC 30
 $f_{z,L}=0.15$ (L/6506)

Membratura

Asta 202 Nodi 202 -11 -12 -13 -14 -15 -77 203 -26 -18 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: $N,Ed=-224.73$ $M_y,Ed=3326.30$ $M_z,Ed=1856.30$ $L=9.69$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=81.83$ $Ncr,y=359031.00$ $\lambda^*_y=1.07$ Curva a: $\Phi_y=1.16$ $\chi_y=0.62$
 $\lambda_z=81.83$ $Ncr,z=359031.00$ $\lambda^*_z=1.07$ Curva a: $\Phi_z=1.16$ $\chi_z=0.62$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
Verifica YY: $0.00+0.09+0.05=0.14$
Verifica ZZ: $0.00+0.07+0.05=0.12$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,G}=0.07$ (L/12998)

- Verifica freccia massima carichi totali - CC 30
 $f_{z,G}=0.15$ (L/6534) $f_{z,L}=0.15$ (L/6593)

Membratura

Asta 302 Nodi -69 -3 -68 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-116.34 My,Ed=224.38 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.68$ (L/438) $f_{z,G}=0.04$ (L/8156)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.67$ (L/444) $f_{z,G}=0.03$ (L/10828)

Membratura

Asta 303 Nodi -76 -29 -75 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.72$ (L/416) $f_{z,G}=0.07$ (L/4076)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.71$ (L/424) $f_{z,G}=0.06$ (L/5041)

Membratura

Asta 305 Nodi -48 -6 -47 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.75$ (L/400) $f_{z,G}=0.07$ (L/4075)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.74$ (L/407) $f_{z,G}=0.06$ (L/5042)

Membratura

Asta 306 Nodi -50 -7 -49 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.77$ (L/389) $f_{z,G}=0.07$ (L/4076)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.76$ (L/396) $f_{z,G}=0.06$ (L/5042)

Membratura

Asta 307 Nodi -52 -8 -51 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.79$ (L/379) $f_{z,G}=0.07$ (L/4076)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.78$ (L/385) $f_{z,G}=0.06$ (L/5041)

Membratura

Asta 308 Nodi -54 -9 -53 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.81$ (L/369) $f_{z,G}=0.07$ (L/4076)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.80$ (L/375) $f_{z,G}=0.06$ (L/5042)

Membratura

Asta 309 Nodi -56 -10 -55 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-116.34 My,Ed=224.38 L=3.00

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.03=0.03
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.80$ (L/376) $f_{z,G}=0.04$ (L/8152)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.79$ (L/381) $f_{z,G}=0.03$ (L/10828)

Membratura

Asta 310 Nodi -58 -11 -57 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-116.34 My,Ed=224.38 L=3.00

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.03=0.03
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.80$ (L/376) $f_{z,G}=0.04$ (L/8152)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.79$ (L/381) $f_{z,G}=0.03$ (L/10831)

Membratura

Asta 311 Nodi -60 -12 -59 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
f_{z,L}=0.81 (L/369) f_{z,G}=0.07 (L/4076)
- Verifica freccia massima carichi totali - CC 23
f_{z,L}=0.80 (L/375) f_{z,G}=0.06 (L/5042)

Membratura

Asta 312 Nodi -62 -13 -61 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=55.42 Ncr,y=310393.00 λ_y^{*}=0.73 Curva a: Φ_y=0.82 χ_y=0.84
λ_z=77.16 Ncr,z=160129.00 λ_z^{*}=1.01 Curva a: Φ_z=1.09 χ_z=0.66
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
f_{z,L}=0.79 (L/379) f_{z,G}=0.07 (L/4076)
- Verifica freccia massima carichi totali - CC 23
f_{z,L}=0.78 (L/385) f_{z,G}=0.06 (L/5041)

Membratura

Asta 313 Nodi -64 -14 -63 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=55.42 Ncr,y=310393.00 λ_y^{*}=0.73 Curva a: Φ_y=0.82 χ_y=0.84
λ_z=77.16 Ncr,z=160129.00 λ_z^{*}=1.01 Curva a: Φ_z=1.09 χ_z=0.66
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
f_{z,L}=0.77 (L/389) f_{z,G}=0.07 (L/4076)
- Verifica freccia massima carichi totali - CC 23
f_{z,L}=0.76 (L/396) f_{z,G}=0.06 (L/5042)

Membratura

Asta 314 Nodi -66 -15 -65 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=55.42 Ncr,y=310393.00 λ_y^{*}=0.73 Curva a: Φ_y=0.82 χ_y=0.84
λ_z=77.16 Ncr,z=160129.00 λ_z^{*}=1.01 Curva a: Φ_z=1.09 χ_z=0.66
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
f_{z,L}=0.75 (L/400) f_{z,G}=0.07 (L/4075)
- Verifica freccia massima carichi totali - CC 23
f_{z,L}=0.74 (L/407) f_{z,G}=0.06 (L/5042)

Membratura

Asta 316 Nodi -74 -26 -73 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=55.42 Ncr,y=310393.00 λ_y^{*}=0.73 Curva a: Φ_y=0.82 χ_y=0.84
λ_z=77.16 Ncr,z=160129.00 λ_z^{*}=1.01 Curva a: Φ_z=1.09 χ_z=0.66
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
f_{z,L}=0.72 (L/416) f_{z,G}=0.07 (L/4077)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,l}=0.71$ (L/424) $f_{z,g}=0.06$ (L/5041)

Membratura

Asta 317 Nodi -71 -18 -70 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-116.34 My,Ed=224.39 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,l}=0.68$ (L/438) $f_{z,g}=0.04$ (L/8156)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,l}=0.67$ (L/444) $f_{z,g}=0.03$ (L/10831)

Membratura

Asta 318 Nodi -81 201 -80 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,l}=0.73$ (L/411) $f_{z,g}=0.07$ (L/4076)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,l}=0.71$ (L/419) $f_{z,g}=0.06$ (L/5041)

Membratura

Asta 319 Nodi -79 -77 -78 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-171.70 My,Ed=422.37 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,l}=0.73$ (L/411) $f_{z,g}=0.07$ (L/4076)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,l}=0.71$ (L/419) $f_{z,g}=0.06$ (L/5041)

5.3 Tracker 2x28 – configurazione a riposo ($\alpha = 0^\circ$)

5.3.1 Diagrammi tassi di sfruttamento

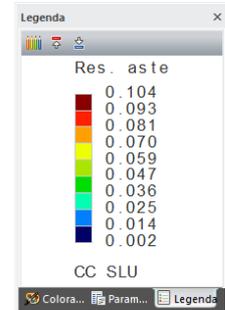
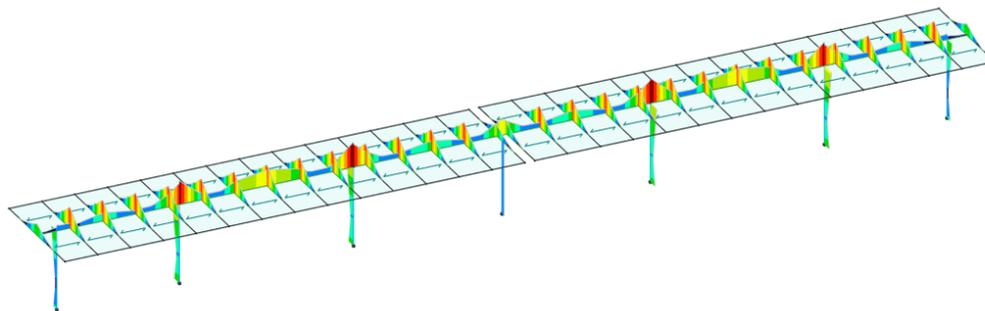


Diagramma tassi di sfruttamento resistenza aste combo SLU con valore massimo pari a 0,104

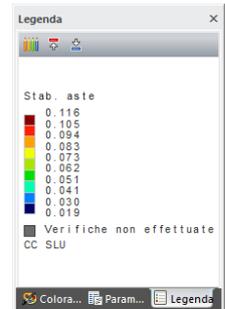
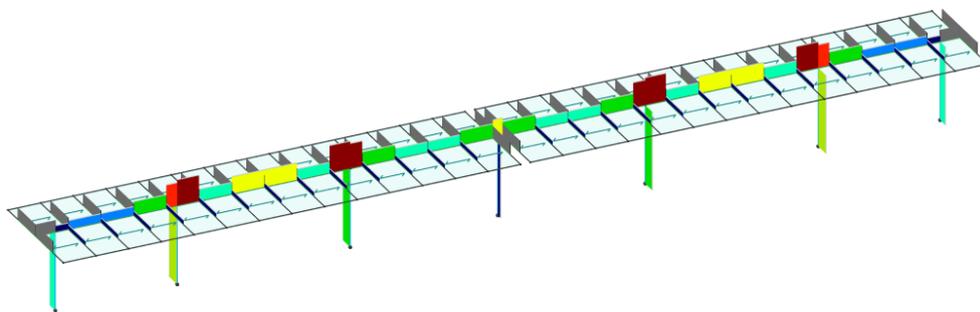


Diagramma tassi di sfruttamento stabilità aste combo SLU con valore massimo pari a 0,116

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

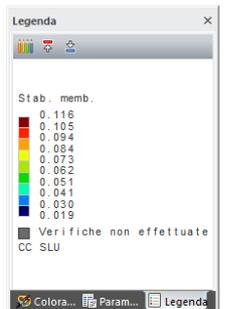
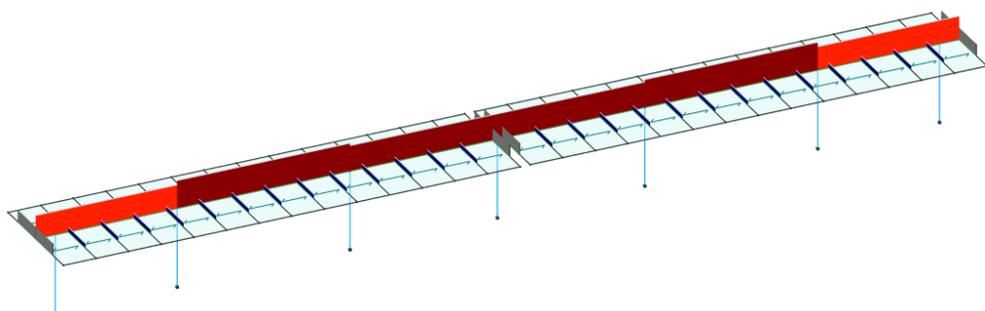


Diagramma tassi di sfruttamento stabilità membrature combo SLU con valore massimo pari a 0,116

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

Figure 14: Tassi di sfruttamento SLU (Stato limite ultimo)

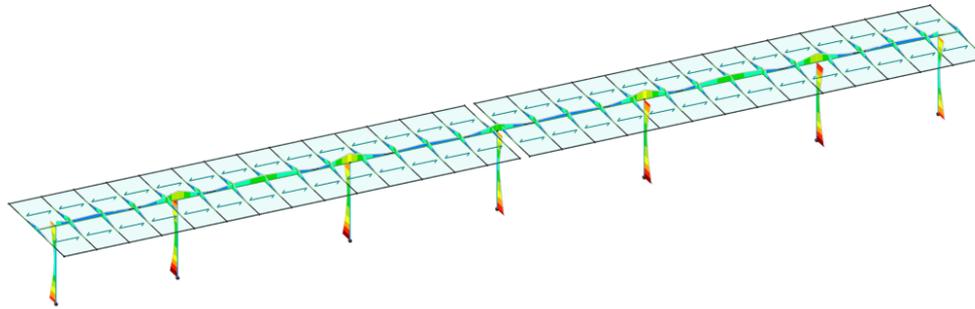


Diagramma tassi di sfruttamento resistenza aste combo SND con valore massimo pari a 0,066

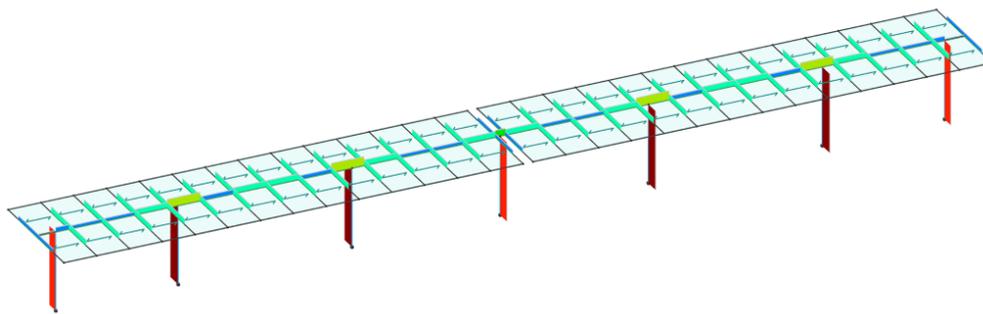


Diagramma tassi di sfruttamento stabilità aste combo SND con valore massimo pari a 0,066

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

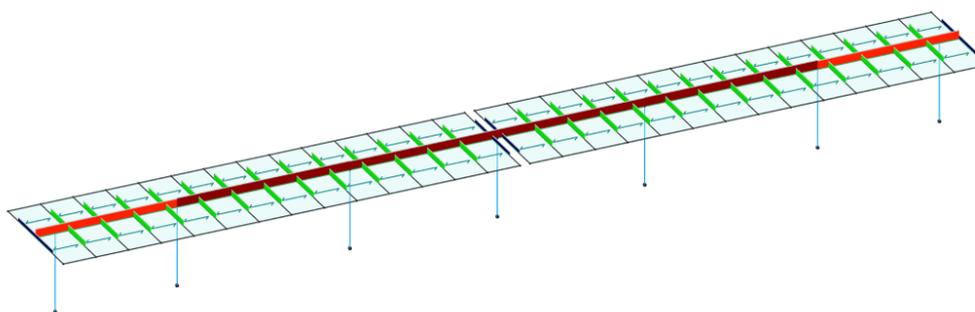


Diagramma tassi di sfruttamento stabilità membrane combo SND con valore massimo pari a 0,038

Figure 15: Tassi di sfruttamento SND (Stato limite di vita non dissipativo)

5.3.2 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:

ModeSt ver. 8.31, licenza n. 7429, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:

Xfinest ver. 9.6.2, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18

Tipo di calcolo: sismica statica

Vincoli esterni: Considera sempre vincoli assegnati in modellazione

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Tipo di analisi: Lineare
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Non sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

Opzioni generali:

- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

- Tipo di elemento bidimensionale: QF46

- Calcolo sforzo nei nodi: No

Opzioni per analisi P-Delta:

- Numero massimo di iterazioni: 15
- Valore della norma euclidea degli spostamenti: 1.0000E-04

Opzioni per analisi pushover:

- Esegui analisi in regime di piccoli spostamenti: Sì

Opzioni per analisi pushover murature:

- Interrompi analisi nel caso di plasticizzazione per carichi statici: Sì
- Utilizza sforzo normale medio: Sì

Metodo di convergenza:

- Forze e momenti residui (F)
Valore della norma euclidea delle forze: 1.0000E-03
Valore della norma euclidea dei momenti: 1.0000E-02

- Opzioni aggiuntive per analisi non lineari in presenza di elementi bidimensionali con comportamento Drucker-Prager:

OPTION PARAM CONV=E
OPTION PARAM RESENORM=1.E-8
OPTION PARAM AUTO_INCREMENT=YES
OPTION PARAM LINE_SEARCHES=YES
OPTION PARAM BGINCRS=1.0
OPTION PARAM AVINCRS=1.0

Dati struttura

- Sito di costruzione: PP5J+MV Ploaghe SS, Italia LON. 8.73219 LAT. 40.70920
Contenuto tra ID reticolo: 26271 26049 26272 26050

Simbologia

Ag =Accelerazione orizzontale massima al sito
C_c =Coefficiente funzione della categoria del suolo
Fo =Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
S_s =Coefficiente di amplificazione stratigrafica
T_R =Periodo di ritorno <anni>
TCC=Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SND = Stato limite di salvaguardia della vita (non dissipativo)
Tc* =Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

TCC	T _R	Ag <g>	Fo	Tc*	S _s	C _c
SLD	50	0.0217	2.63	0.19	1.80	2.89
SLV	475	0.0395	2.77	0.29	1.80	2.30

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale V_N: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 3.29 <m>
- Altezza della struttura: 3.29 <m>
- Numero piani edificio: 0
- Coefficiente θ: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di calcolo

- Categoria del suolo di fondazione: D
- Tipologia strutturale: acciaio a mensola o a pendolo inverso

Periodo T ₁	0.20741
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovraresistenza (α _u /α ₁)	1.00
Valore di riferimento del fattore di comportamento (q ₀)	2.00
Fattore riduttivo (K _w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di comportamento dissipativo (q)	2.00
Fattore di comportamento non dissipativo (q _{ND})	1.33
Fattore di comportamento per SLD (q _D)	1.33

- Categoria topografica: T2 - Pendii con inclinazione media i > 15°
- Coeff. amplificazione topografica S_T: 1.20
- Accelerazione di picco del terreno AgS: 0.0853 <g>
- Fattore di comportamento per sisma verticale (qv): 1.50
- Smorzamento spettro: 5.00%

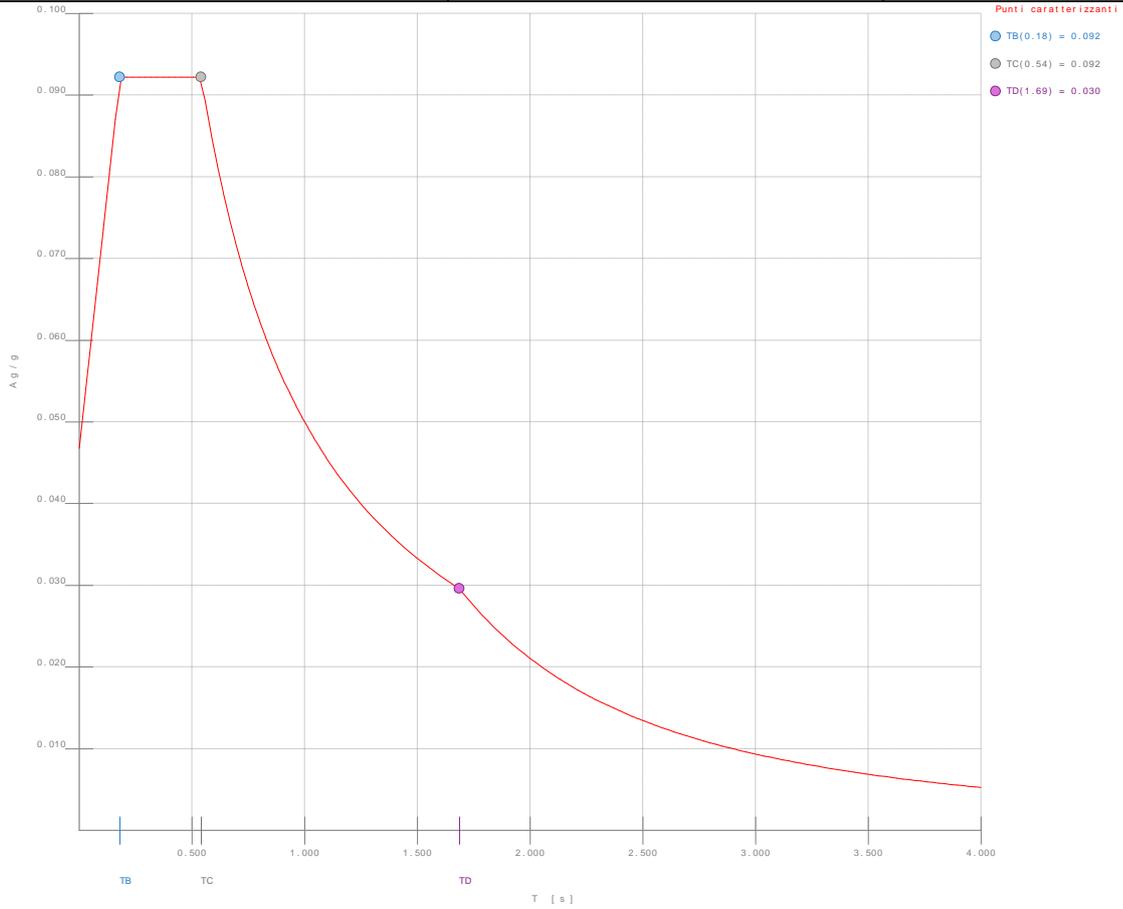


Figura numero 1: Spettro SLD

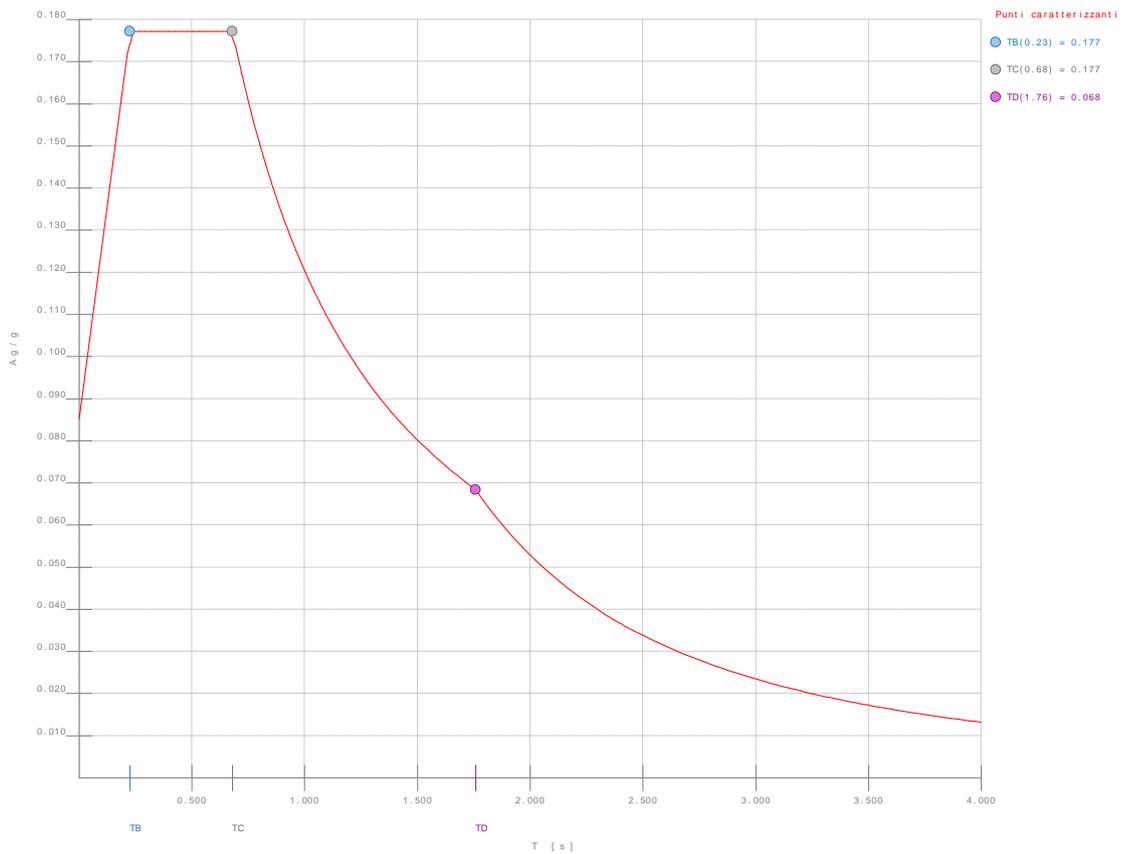


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>
- Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

- N = Numero
- Comm. = Commento
- 1 = G1 - Peso Proprio
- 2 = G2 - Permanenti non strutturali
- 3 = Q - Variabili neve
- 4 = Q - Vento retro Cond.A
- 5 = Q - Vento retro Cond.B
- 6 = Q - Vento fronte Cond.C
- 7 = Q - Vento fronte Cond.D
- F = azioni orizzontali convenzionali
- SLU = Stato limite ultimo
- SLR = Stato limite per combinazioni rare
- SLF = Stato limite per combinazioni frequenti
- SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
- S = Si
- N = No

N	Comm.	1	2	3	4	5	6	7	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	S	S	S	N	N	N	N	S	N	N	N	N
2	Calcolo statico	S	S	N	N	N	N	N	S	S	S	S	S
3	Vento cond A	S	S	S	N	N	N	N	S	S	S	S	S
4	Vento cond B	S	S	S	N	N	N	N	S	S	S	S	S
5	Vento cond C	S	S	N	N	N	N	N	S	S	S	S	S
6	Vento cond D	S	S	N	N	N	N	N	S	S	S	S	S

Elenco combinazioni di carico simboliche

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	1	2	3	4	5	6	7	S
1	Amb. 1 (Sisma)	SLU S	1	1	ψ_2	-----	-----	-----	-----	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	-----	-----
3	Amb. 2 (SLE R)	SLE R	1	1	ψ_1	-----	-----	-----	-----	-----
4	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	-----	-----	-----	-----	-----
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	-----	-----	-----	-----	-----
6	Amb. 3 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	γ max	-----	-----	-----	-----
7	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	-----
8	Amb. 3 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
9	Amb. 3 (SLE R)	SLE R	1	1	1	ψ_0	-----	-----	-----	-----
10	Amb. 3 (SLE F)	SLE F	1	1	ψ_2	ψ_1	-----	-----	-----	-----
11	Amb. 3 (SLE F)	SLE F	1	1	ψ_1	ψ_2	-----	-----	-----	-----
12	Amb. 3 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	-----	-----	-----	-----
13	Amb. 4 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
14	Amb. 4 (SLU)	SLU	γ max	γ max	γ max	-----	$\psi_0 * \gamma$ max	-----	-----	-----
15	Amb. 4 (SLE R)	SLE R	1	1	ψ_0	-----	1	-----	-----	-----
16	Amb. 4 (SLE R)	SLE R	1	1	1	-----	ψ_0	-----	-----	-----
17	Amb. 4 (SLE F)	SLE F	1	1	ψ_2	-----	ψ_1	-----	-----	-----
18	Amb. 4 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_2	-----	-----	-----
19	Amb. 4 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	-----	-----	-----
20	Amb. 5 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	γ max	-----	-----
21	Amb. 5 (SLU)	SLU	γ max	γ max	γ max	-----	-----	$\psi_0 * \gamma$ max	-----	-----
22	Amb. 5 (SLE R)	SLE R	1	1	ψ_0	-----	-----	1	-----	-----
23	Amb. 5 (SLE R)	SLE R	1	1	1	-----	-----	ψ_0	-----	-----
24	Amb. 5 (SLE F)	SLE F	1	1	ψ_2	-----	-----	ψ_1	-----	-----
25	Amb. 5 (SLE F)	SLE F	1	1	ψ_1	-----	-----	ψ_2	-----	-----
26	Amb. 5 (SLE Q)	SLE Q	1	1	ψ_2	-----	-----	ψ_2	-----	-----
27	Amb. 6 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	γ max	-----

28	Amb. 6 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	$\Psi_0 * \gamma$ max	-----
29	Amb. 6 (SLE R)	SLE R	1	1	Ψ_0	-----	-----	-----	1	-----
30	Amb. 6 (SLE F)	SLE R	1	1	1	-----	-----	-----	Ψ_0	-----
31	Amb. 6 (SLE F)	SLE F	1	1	Ψ_2	-----	-----	-----	Ψ_1	-----
32	Amb. 6 (SLE F)	SLE F	1	1	Ψ_1	-----	-----	-----	Ψ_2	-----
33	Amb. 6 (SLE Q)	SLE Q	1	1	Ψ_2	-----	-----	-----	Ψ_2	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: Si

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

An. = Tipo di analisi
 L = Lineare
 NL = Non lineare
 PD = P-Delta

Bk = Buckling
 S = Si
 N = No

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	S X	S Y
1	Amb. 1 (SLU S) S +X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
2	Amb. 1 (SLE) S +X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
3	Amb. 1 (SLU S) S +X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
4	Amb. 1 (SLE) S +X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
5	Amb. 1 (SLU S) S -X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
6	Amb. 1 (SLE) S -X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
7	Amb. 1 (SLU S) S -X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
8	Amb. 1 (SLE) S -X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
9	Amb. 1 (SLU S) S +0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
10	Amb. 1 (SLE) S +0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
11	Amb. 1 (SLU S) S -0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
12	Amb. 1 (SLE) S -0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
13	Amb. 1 (SLU S) S +0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
14	Amb. 1 (SLE) S +0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
15	Amb. 1 (SLU S) S -0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
16	Amb. 1 (SLE) S -0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
17	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.00	0.00	0.00
18	Amb. 2 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
19	Amb. 2 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
20	Amb. 2 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	0.75	1.50	0.00	0.00	0.00	0.00	0.00
22	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
23	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	0.50	1.00	0.00	0.00	0.00	0.00	0.00
24	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
25	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.20	0.00	0.00	0.00	0.00	0.00
26	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
27	Amb. 3 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	1.50	0.00	0.00	0.00	0.00
29	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.90	0.00	0.00	0.00	0.00
30	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	1.00	0.00	0.00	0.00	0.00
31	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.60	0.00	0.00	0.00	0.00
32	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.20	0.00	0.00	0.00	0.00
33	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
34	Amb. 4 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	1.50	0.00	0.00	0.00
36	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.90	0.00	0.00	0.00
37	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00
38	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00
39	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00
40	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
41	Amb. 5 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	0.00	1.50	0.00	0.00
43	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.90	0.00	0.00
44	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00

45	Amb. 6 (SLE R)	SLE R L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00
46	Amb. 6 (SLE F)	SLE F L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.20	0.00	0.00
47	Amb. 6 (SLE F)	SLE F L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
48	Amb. 6 (SLE Q)	SLE Q L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Elenco masse nodi

Simbologia

Mo = Massa orizzontale

Nodo = Numero del nodo

Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo		
<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>	<kg>		
-104	55.67	-103	55.67	-102	83.72	-101	83.72	-98	83.72	-97	83.72	-96	83.72	-95	83.72	-94	83.72	-85	83.72		
-93	83.72	-92	83.72	-91	83.72	-90	83.72	-89	83.72	-88	83.72	-87	83.72	-86	83.72	-85	83.72	-84	83.72	-83	83.72
-84	83.72	-83	83.72	-82	83.72	-81	83.72	-80	83.72	-79	83.72	-78	83.72	-77	83.72	-76	83.72	-75	83.72	-74	83.72
-75	83.72	-74	83.72	-73	83.72	-72	83.72	-71	83.72	-70	83.72	-69	83.72	-68	83.72	-67	83.72	-66	83.72	-65	55.67
-66	83.72	-65	55.67	-64	83.72	-63	55.67	-62	83.72	-61	83.72	-58	83.72	-57	83.72	-56	83.72	-55	83.72	-54	83.72
-55	83.72	-54	83.72	-53	83.72	-52	83.72	-51	55.67	-50	55.67	-49	83.72	-48	83.72	-47	55.67	-46	55.67	-45	83.72
-46	55.67	-45	83.72	-44	83.72	-43	83.72	-42	83.72	-41	83.72	-37	118.22	-36	183.50	-35	193.34	-34	230.75	-33	230.75
-34	230.75	-33	230.75	-32	189.39	-31	183.50	-30	209.94	-29	230.75	-28	230.75	-27	230.75	-26	207.90	-25	191.43	-24	230.75
-25	191.43	-24	230.75	-23	230.75	-22	230.75	-21	152.26	-20	152.26	-19	230.75	-18	230.75	-17	230.75	-16	191.43	-15	207.90
-16	191.43	-15	207.90	-14	230.75	-13	230.75	-12	230.75	-11	209.94	-10	183.50	-9	189.39	-8	230.75	-7	230.75	-6	193.34
-7	230.75	-6	193.34	-5	183.50	-4	118.22	203	183.50	204	139.90	205	183.50								

Totali masse nodi

Mo
<kg>
12256.80

Elenco forze sismiche nodali allo SLD

Simbologia

Fx = Forza in dir. X

Fy = Forza in dir. Y

Nodo = Numero del nodo

cx = Coeff. c in dir. X

cy = Coeff. c in dir. Y

Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy
<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>
-104	0.00	0.00	5.04	5.04	-103	0.00	0.00	5.04	5.04	-102	0.01	0.01	7.57	7.57	-101	0.01	0.01	7.57	7.57	-95	0.01	0.01	7.57	7.57
-98	0.01	0.01	7.57	7.57	-97	0.01	0.01	7.57	7.57	-96	0.01	0.01	7.57	7.57	-95	0.01	0.01	7.57	7.57	-91	0.01	0.01	7.57	7.57
-94	0.01	0.01	7.57	7.57	-93	0.01	0.01	7.57	7.57	-92	0.01	0.01	7.57	7.57	-91	0.01	0.01	7.57	7.57	-87	0.01	0.01	7.57	7.57
-90	0.01	0.01	7.57	7.57	-89	0.01	0.01	7.57	7.57	-88	0.01	0.01	7.57	7.57	-87	0.01	0.01	7.57	7.57	-83	0.01	0.01	7.57	7.57
-86	0.01	0.01	7.57	7.57	-85	0.01	0.01	7.57	7.57	-84	0.01	0.01	7.57	7.57	-83	0.01	0.01	7.57	7.57	-79	0.01	0.01	7.57	7.57
-82	0.01	0.01	7.57	7.57	-81	0.01	0.01	7.57	7.57	-80	0.01	0.01	7.57	7.57	-79	0.01	0.01	7.57	7.57	-75	0.01	0.01	7.57	7.57
-78	0.01	0.01	7.57	7.57	-77	0.01	0.01	7.57	7.57	-76	0.01	0.01	7.57	7.57	-75	0.01	0.01	7.57	7.57	-71	0.01	0.01	7.57	7.57
-74	0.01	0.01	7.57	7.57	-73	0.01	0.01	7.57	7.57	-72	0.01	0.01	7.57	7.57	-71	0.01	0.01	7.57	7.57	-67	0.01	0.01	7.57	7.57
-70	0.01	0.01	7.57	7.57	-69	0.01	0.01	7.57	7.57	-68	0.01	0.01	7.57	7.57	-67	0.01	0.01	7.57	7.57	-63	0.00	0.00	5.04	5.04
-66	0.01	0.01	7.57	7.57	-65	0.00	0.00	5.04	5.04	-64	0.01	0.01	7.57	7.57	-63	0.00	0.00	5.04	5.04	-57	0.01	0.01	7.57	7.57
-62	0.01	0.01	7.57	7.57	-61	0.01	0.01	7.57	7.57	-58	0.01	0.01	7.57	7.57	-57	0.01	0.01	7.57	7.57	-53	0.01	0.01	7.57	7.57
-56	0.01	0.01	7.57	7.57	-55	0.01	0.01	7.57	7.57	-54	0.01	0.01	7.57	7.57	-53	0.01	0.01	7.57	7.57	-49	0.01	0.01	7.57	7.57
-52	0.01	0.01	7.57	7.57	-51	0.00	0.00	5.04	5.04	-50	0.00	0.00	5.04	5.04	-49	0.01	0.01	7.57	7.57	-45	0.01	0.01	7.57	7.57
-48	0.01	0.01	7.57	7.57	-47	0.00	0.00	5.04	5.04	-46	0.00	0.00	5.04	5.04	-45	0.01	0.01	7.57	7.57	-41	0.01	0.01	7.57	7.57
-44	0.01	0.01	7.57	7.57	-43	0.01	0.01	7.57	7.57	-42	0.01	0.01	7.57	7.57	-41	0.01	0.01	7.57	7.57	-34	0.02	0.02	20.88	20.88
-37	0.01	0.01	10.70	10.70	-36	0.01	0.01	16.60	16.60	-35	0.02	0.02	17.49	17.49	-34	0.02	0.02	20.88	20.88	-30	0.02	0.02	18.99	18.99
-33	0.02	0.02	20.88	20.88	-32	0.02	0.02	17.13	17.13	-31	0.01	0.01	16.60	16.60	-30	0.02	0.02	18.99	18.99	-26	0.02	0.02	18.81	18.81
-29	0.02	0.02	20.88	20.88	-28	0.02	0.02	20.88	20.88	-27	0.02	0.02	20.88	20.88	-26	0.02	0.02	18.81	18.81	-22	0.02	0.02	20.88	20.88
-25	0.02	0.02	17.32	17.32	-24	0.02	0.02	20.88	20.88	-23	0.02	0.02	20.88	20.88	-22	0.02	0.02	20.88	20.88	-18	0.02	0.02	20.88	20.88
-21	0.01	0.01	13.78	13.78	-20	0.01	0.01	13.78	13.78	-19	0.02	0.02	20.88	20.88	-18	0.02	0.02	20.88	20.88	-14	0.02	0.02	20.88	20.88
-17	0.02	0.02	20.88	20.88	-16	0.02	0.02	17.32	17.32	-15	0.02	0.02	18.81	18.81	-14	0.02	0.02	20.88	20.88	-10	0.01	0.01	16.60	16.60
-13	0.02	0.02	20.88	20.88	-12	0.02	0.02	20.88	20.88	-11	0.02	0.02	18.99	18.99	-10	0.01	0.01	16.60	16.60	-6	0.02	0.02	17.49	17.49
-9	0.02	0.02	17.13	17.13	-8	0.02	0.02	20.88	20.88	-7	0.02	0.02	20.88	20.88	-6	0.02	0.02	17.49	17.49	-5	0.01	0.01	16.60	16.60
-5	0.01	0.01	16.60	16.60	-4	0.01	0.01	10.70	10.70	203	0.01	0.01	16.60	16.60	204	0.01	0.01	12.66	12.66					
205	0.01	0.01	16.60	16.60																				

Totali forze sismiche

Fx	Fy
<daN>	<daN>
1108.86	1108.86

Elenco forze sismiche nodali allo SND

Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy					
<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>	<daN>					
-104	0.00	0.00	9.26	9.26	-103	0.00	0.00	9.26	9.26	-102	0.01	0.01	13.92	13.92	-101	0.01	0.01	13.92	13.92	-95	0.01	0.01	13.92	13.92
-98	0.01	0.01	13.92	13.92	-97	0.01	0.01	13.92	13.92	-96	0.01	0.01	13.92	13.92	-95	0.01	0.01	13.92	13.92					

-94	0.01	0.01	13.92	13.92	-93	0.01	0.01	13.92	13.92	-92	0.01	0.01	13.92	13.92	-91	0.01	0.01	13.92	13.92
-90	0.01	0.01	13.92	13.92	-89	0.01	0.01	13.92	13.92	-88	0.01	0.01	13.92	13.92	-87	0.01	0.01	13.92	13.92
-86	0.01	0.01	13.92	13.92	-85	0.01	0.01	13.92	13.92	-84	0.01	0.01	13.92	13.92	-83	0.01	0.01	13.92	13.92
-82	0.01	0.01	13.92	13.92	-81	0.01	0.01	13.92	13.92	-80	0.01	0.01	13.92	13.92	-79	0.01	0.01	13.92	13.92
-78	0.01	0.01	13.92	13.92	-77	0.01	0.01	13.92	13.92	-76	0.01	0.01	13.92	13.92	-75	0.01	0.01	13.92	13.92
-74	0.01	0.01	13.92	13.92	-73	0.01	0.01	13.92	13.92	-72	0.01	0.01	13.92	13.92	-71	0.01	0.01	13.92	13.92
-70	0.01	0.01	13.92	13.92	-69	0.01	0.01	13.92	13.92	-68	0.01	0.01	13.92	13.92	-67	0.01	0.01	13.92	13.92
-66	0.01	0.01	13.92	13.92	-65	0.00	0.00	9.26	9.26	-64	0.01	0.01	13.92	13.92	-63	0.00	0.00	9.26	9.26
-62	0.01	0.01	13.92	13.92	-61	0.01	0.01	13.92	13.92	-58	0.01	0.01	13.92	13.92	-57	0.01	0.01	13.92	13.92
-56	0.01	0.01	13.92	13.92	-55	0.01	0.01	13.92	13.92	-54	0.01	0.01	13.92	13.92	-53	0.01	0.01	13.92	13.92
-52	0.01	0.01	13.92	13.92	-51	0.00	0.00	9.26	9.26	-50	0.00	0.00	9.26	9.26	-49	0.01	0.01	13.92	13.92
-48	0.01	0.01	13.92	13.92	-47	0.00	0.00	9.26	9.26	-46	0.00	0.00	9.26	9.26	-45	0.01	0.01	13.92	13.92
-44	0.01	0.01	13.92	13.92	-43	0.01	0.01	13.92	13.92	-42	0.01	0.01	13.92	13.92	-41	0.01	0.01	13.92	13.92
-37	0.01	0.01	19.66	19.66	-36	0.01	0.01	30.52	30.52	-35	0.02	0.02	32.15	32.15	-34	0.02	0.02	38.37	38.37
-33	0.02	0.02	38.37	38.37	-32	0.02	0.02	31.49	31.49	-31	0.01	0.01	30.52	30.52	-30	0.02	0.02	34.91	34.91
-29	0.02	0.02	38.37	38.37	-28	0.02	0.02	38.37	38.37	-27	0.02	0.02	38.37	38.37	-26	0.02	0.02	34.57	34.57
-25	0.02	0.02	31.83	31.83	-24	0.02	0.02	38.37	38.37	-23	0.02	0.02	38.37	38.37	-22	0.02	0.02	38.37	38.37
-21	0.01	0.01	25.32	25.32	-20	0.01	0.01	25.32	25.32	-19	0.02	0.02	38.37	38.37	-18	0.02	0.02	38.37	38.37
-17	0.02	0.02	38.37	38.37	-16	0.02	0.02	31.83	31.83	-15	0.02	0.02	34.57	34.57	-14	0.02	0.02	38.37	38.37
-13	0.02	0.02	38.37	38.37	-12	0.02	0.02	38.37	38.37	-11	0.02	0.02	34.91	34.91	-10	0.01	0.01	30.52	30.52
-9	0.02	0.02	31.49	31.49	-8	0.02	0.02	38.37	38.37	-7	0.02	0.02	38.37	38.37	-6	0.02	0.02	32.15	32.15
-5	0.01	0.01	30.52	30.52	-4	0.01	0.01	19.66	19.66	203	0.01	0.01	30.52	30.52	204	0.01	0.01	23.27	23.27
205	0.01	0.01	30.52	30.52															

Totali forze sismiche

Fx	Fy
<daN>	<daN>
2038.27	2038.27

Domanda in duttilità di curvatura

Direzione X $\mu_{Edx}=9.35$

Direzione Y $\mu_{Edy}=9.35$

Spostamenti relativi massimi allo stato limite di danno

Simbologia

δ =Spostamento relativo

δ/h =Rapporto (*1000) tra lo spostamento relativo e l'altezza

CC =Numero della combinazione delle condizioni di carico elementari

N1 =Nodo1

N2 =Nodo2

h =Altezza teorica

I valori degli spostamenti relativi per CC di tipo sismico sono amplificati come da normativa

N1	N2	h	δ	δ/h	CC	N1	N2	h	δ	δ/h	CC	N1	N2	h	δ	δ/h	CC	N1	N2	h	δ	δ/h	CC
		<m>	<cm>					<m>	<cm>					<m>	<cm>					<m>	<cm>		
1	-5	3.29	0.11	0.33	4	2	-10	3.29	0.14	0.43	14	3	203	3.29	0.15	0.47	14	4	204	3.29	0.15	0.44	14
5	205	3.29	0.15	0.47	16	6	-31	3.29	0.14	0.43	16	7	-36	3.29	0.11	0.33	8						

Min = 0.33

Max = 0.47

Reazioni vincolari

Simbologia

CC =Numero della combinazione delle condizioni di carico elementari

Fx =Reazione vincolare (forza) in dir. X

Fy =Reazione vincolare (forza) in dir. Y

Fz =Reazione vincolare (forza) in dir. Z

Mx =Reazione vincolare (momento) intorno all'asse X

My =Reazione vincolare (momento) intorno all'asse Y

Mz =Reazione vincolare (momento) intorno all'asse Z

Nodo =Numero del nodo

TCC =Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

Nodo		CC	TCC	Fx	CC	TCC	Fy	CC	TCC	Fz	CC	TCC	Mx	CC	TCC	My	CC	TCC	Mz
				<daN>			<daN>			<daN>			<daNm>			<daNm>			<daNm>
1	Max	5	SND	311.68	13	SND	173.77	29	SLU	3451.54	9	SND	636.24	5	SND	524.78	15	SND	0.17
1	Min	1	SND	-224.58	11	SND	-173.77	1	SND	971.63	13	SND	-636.24	9	SND	-432.22	1	SND	-0.17

2	Max	5	SND	362.07	13	SND	331.24	29	SLU	7452.92	9	SND	1041.40	5	SND	579.89	13	SND	0.12
2	Min	1	SND	-251.79	9	SND	-331.24	25	SLE F	1839.73	13	SND	-1041.40	9	SND	-461.85	1	SND	-0.12
3	Max	5	SND	248.81	13	SND	354.53	29	SLU	7700.60	9	SND	1139.06	5	SND	457.93	11	SND	0.04
3	Min	1	SND	-338.37	9	SND	-354.53	25	SLE F	1900.83	13	SND	-1139.06	13	SND	-555.56	1	SND	-0.04
4	Max	5	SND	300.98	13	SND	319.19	29	SLU	6367.78	9	SND	1062.32	5	SND	514.82	13	SND	0.00
4	Min	1	SND	-300.98	9	SND	-319.19	25	SLE F	1701.01	13	SND	-1062.32	11	SND	-514.82	1	SND	0.00
5	Max	5	SND	338.37	13	SND	354.53	29	SLU	7700.60	9	SND	1139.06	5	SND	555.55	13	SND	0.04
5	Min	1	SND	-248.81	9	SND	-354.53	25	SLE F	1900.83	13	SND	-1139.06	9	SND	-457.93	1	SND	-0.04
6	Max	5	SND	251.79	13	SND	331.24	29	SLU	7452.91	11	SND	1041.39	5	SND	461.85	9	SND	0.12
6	Min	1	SND	-362.07	9	SND	-331.24	25	SLE F	1839.73	13	SND	-1041.40	13	SND	-579.89	1	SND	-0.12
7	Max	5	SND	224.58	13	SND	173.77	29	SLU	3451.53	9	SND	636.24	5	SND	432.22	11	SND	0.17
7	Min	1	SND	-311.68	9	SND	-173.77	5	SND	971.62	13	SND	-636.24	13	SND	-524.78	1	SND	-0.17

Sollecitazioni aste

Simbologia

Asta = Numero dell'asta

CC = Numero della combinazione delle condizioni di carico elementari

Mx = Momento torcente intorno all'asse X

My = Momento flettente intorno all'asse Y

Mz = Momento flettente intorno all'asse Z

N = Sforzo normale

N1 = Nodo1

N2 = Nodo2

Ty = Taglio in dir. Y

Tz = Taglio in dir. Z

X = Coordinata progressiva rispetto al nodo iniziale

Tipo di combinazione di carico: SND

Asta	N1	N2		X <cm>	N <daN>	CC	Ty <daN>	CC	Mz <daNm>	CC	Tz <daN>	CC	My <daNm>	CC	Mx <daNm>	CC
1	1	-5	Max	0.00	-971.63	1	311.68	5	432.22	1	173.77	15	636.24	9	0.17	9
1	1	-5	Max	328.50	-733.56	1	311.68	5	499.07	5	173.77	15	65.41	11	0.17	9
1	1	-5	Min.	0.00	-1255.09	5	-224.58	1	-524.78	5	-173.77	9	-636.24	13	-0.17	15
1	1	-5	Min.	328.50	-1017.02	5	-224.58	1	-305.53	1	-173.77	9	-65.41	13	-0.17	15
2	2	-10	Max	0.00	-2048.81	5	362.07	5	461.85	1	331.24	13	1041.40	9	0.12	9
2	2	-10	Max	328.50	-1810.74	5	362.07	5	609.50	5	331.24	13	46.72	15	0.12	9
2	2	-10	Min.	0.00	-2223.28	1	-251.79	1	-579.89	5	-331.24	9	-1041.40	15	-0.12	13
2	2	-10	Min.	328.50	-1985.22	1	-251.79	1	-365.27	1	-331.24	9	-46.72	9	-0.12	13
3	3	203	Max	0.00	-2180.66	1	248.81	5	555.56	1	354.53	13	1139.06	9	0.04	13
3	3	203	Max	328.50	-1942.60	1	248.81	5	359.41	5	354.53	13	25.58	15	0.04	13
3	3	203	Min.	0.00	-2233.33	5	-338.37	1	-457.93	5	-354.53	9	-1139.06	13	-0.04	11
3	3	203	Min.	328.50	-1995.26	5	-338.37	1	-555.98	1	-354.53	9	-25.58	9	-0.04	11
4	4	204	Max	0.00	-1944.35	1	300.98	1	514.82	5	319.19	9	1062.32	13	0.00	11
4	4	204	Max	328.50	-1706.28	1	300.98	1	473.90	1	319.19	9	13.79	15	0.00	11
4	4	204	Min.	0.00	-1944.35	1	-300.98	5	-514.82	1	-319.19	13	-1062.32	9	0.00	13
4	4	204	Min.	328.50	-1706.28	1	-300.98	5	-473.90	5	-319.19	13	-13.79	9	0.00	13
5	5	205	Max	0.00	-2180.66	5	248.81	1	555.55	5	354.53	9	1139.06	13	0.04	9
5	5	205	Max	328.50	-1942.60	5	248.81	1	359.41	1	354.53	9	25.58	11	0.04	9
5	5	205	Min.	0.00	-2233.33	1	-338.37	5	-457.93	1	-354.53	13	-1139.06	9	-0.04	13
5	5	205	Min.	328.50	-1995.26	1	-338.37	5	-555.98	5	-354.53	13	-25.58	13	-0.04	13
6	6	-31	Max	0.00	-2048.80	1	362.07	1	461.85	5	331.24	9	1041.40	13	0.12	13
6	6	-31	Max	328.50	-1810.74	1	362.07	1	609.50	1	331.24	9	46.72	11	0.12	13
6	6	-31	Min.	0.00	-2223.28	5	-251.79	5	-579.89	1	-331.24	13	-1041.39	11	-0.12	9
6	6	-31	Min.	328.50	-1985.22	5	-251.79	5	-365.27	5	-331.24	13	-46.72	13	-0.12	9
7	7	-36	Max	0.00	-971.62	5	311.68	1	432.22	5	173.77	11	636.24	13	0.17	13
7	7	-36	Max	328.50	-733.56	5	311.68	1	499.07	1	173.77	11	65.41	15	0.17	13
7	7	-36	Min.	0.00	-1255.09	1	-224.58	5	-524.78	1	-173.77	13	-636.24	9	-0.17	11
7	7	-36	Min.	328.50	-1017.02	1	-224.58	5	-305.53	5	-173.77	13	-65.41	9	-0.17	11
201	-5	-4	Max	0.00	38.17	5	38.17	9	30.77	13	261.89	1	-181.50	1	0.00	1
201	-5	-4	Max	80.60	38.17	5	38.17	9	0.00	9	188.50	1	0.00	1	0.00	1
201	-5	-4	Min.	0.00	-38.17	1	-38.17	13	-30.77	11	261.89	1	-181.50	1	0.00	1
201	-5	-4	Min.	80.60	-38.17	1	-38.17	13	0.00	15	188.50	1	0.00	1	0.00	1
201	-6	-5	Max	0.00	155.89	1	105.08	13	25.12	9	-423.10	1	362.67	1	65.41	15
201	-6	-5	Max	53.34	155.89	1	105.08	13	30.94	13	-471.67	1	124.03	1	65.41	15
201	-6	-5	Min.	0.00	-242.99	5	-105.08	11	-25.12	15	-706.56	5	-290.72	5	-65.41	9
201	-6	-5	Min.	53.34	-242.99	5	-105.08	11	-30.94	11	-755.13	5	-680.57	5	-65.41	9
201	-7	-6	Max	0.00	95.89	1	45.08	13	85.50	9	-32.47	1	487.84	1	65.41	13
201	-7	-6	Max	133.94	95.89	1	45.08	13	25.12	9	-154.44	1	362.67	1	65.41	13
201	-7	-6	Min.	0.00	-182.99	5	-45.08	11	-85.50	13	-315.93	5	214.13	5	-65.41	9
201	-7	-6	Min.	133.94	-182.99	5	-45.08	11	-25.12	15	-437.90	5	-290.72	5	-65.41	9
201	-8	-7	Max	0.00	29.68	1	21.14	9	57.19	11	358.16	1	195.76	5	65.41	15
201	-8	-7	Max	82.03					22.36	5			226.40	5		
201	-8	-7	Max	133.94	29.68	1	21.14	9	85.50	9	236.19	1	487.84	1	65.41	15
201	-8	-7	Min.	0.00	-116.77	5	-21.14	15	-57.19	13	74.70	5	89.80	1	-65.41	9
201	-8	-7	Min.	82.03					22.36	5			226.40	5		



201	-8	-7	Min.	133.94	-116.77	5	-21.14	15	-85.50	15	-47.27	5	214.13	5	-65.41	9
201	-9	-8	Max	0.00	-36.54	1	87.35	9	59.81	13	748.79	1	-345.82	5	65.41	15
201	-9	-8	Max	133.94	-36.54	1	87.35	9	57.19	9	626.82	1	195.76	5	65.41	15
201	-9	-8	Min.	0.00	-50.55	7	-87.35	15	-59.81	9	465.33	5	-831.47	1	-65.41	9
201	-9	-8	Min.	133.94	-50.55	7	-87.35	15	-57.19	15	343.36	5	89.80	1	-65.41	9
201	-10	-9	Max	0.00	8.79	5	146.69	9	125.58	13	1058.27	1	-684.01	5	65.41	13
201	-10	-9	Max	44.83	8.79	5	146.69	9	59.81	13	1017.45	1	-345.82	5	65.41	13
201	-10	-9	Min.	0.00	-95.88	1	-146.69	15	-125.58	11	774.81	5	-1296.74	1	-65.41	9
201	-10	-9	Min.	44.83	-95.88	1	-146.69	15	-59.81	11	733.99	5	-831.47	1	-65.41	9
202	-11	-10	Max	0.00	125.39	1	154.03	13	11.56	11	-845.80	1	-141.58	1	18.69	15
202	-11	-10	Max	89.11	125.39	1	154.03	13	125.69	13	-926.95	1	-931.46	1	18.69	15
202	-11	-10	Min.	0.00	-322.76	5	-154.03	9	-11.56	13	-954.78	5	-406.51	5	-18.69	9
202	-11	-10	Min.	89.11	-322.76	5	-154.03	9	-125.69	11	-1035.93	5	-1293.51	5	-18.69	9
202	-12	-11	Max	0.00	62.63	1	91.27	13	133.81	9	-455.17	1	549.77	1	18.69	15
202	-12	-11	Max	133.94	62.63	1	91.27	13	11.56	9	-577.14	1	-141.58	1	18.69	15
202	-12	-11	Min.	0.00	-260.00	5	-91.27	11	-133.81	13	-564.16	5	430.82	5	-18.69	9
202	-12	-11	Min.	133.94	-260.00	5	-91.27	11	-11.56	15	-686.12	5	-406.51	5	-18.69	9
202	-13	-12	Max	0.00	-3.59	1	25.05	13	167.36	9	-64.54	1	744.93	5	18.69	15
202	-13	-12	Max	133.94	-3.59	1	25.05	13	133.81	9	-186.51	1	549.77	1	18.69	15
202	-13	-12	Min.	0.00	-193.78	5	-25.05	11	-167.36	13	-173.53	5	717.90	1	-18.69	9
202	-13	-12	Min.	133.94	-193.78	5	-25.05	11	-133.81	13	-295.50	5	430.82	5	-18.69	9
202	-14	-13	Max	0.00	-69.81	1	41.17	9	112.22	11	326.09	1	535.83	5	18.69	15
202	-14	-13	Max	133.94	-69.81	1	41.17	9	167.36	9	204.12	1	744.93	5	18.69	15
202	-14	-13	Min.	0.00	-127.57	7	-41.17	15	-112.22	13	217.10	5	362.82	1	-18.69	9
202	-14	-13	Min.	133.94	-127.57	7	-41.17	15	-167.36	13	95.13	5	717.90	1	-18.69	9
202	-15	-14	Max	0.00	-61.35	5	107.39	9	31.62	15	716.72	1	-196.50	5	18.69	15
202	-15	-14	Max	133.94	-61.35	5	107.39	9	112.22	9	594.75	1	535.83	5	18.69	15
202	-15	-14	Min.	0.00	-136.03	1	-107.39	15	-31.62	9	607.73	5	-515.49	1	-18.69	9
202	-15	-14	Min.	133.94	-136.03	1	-107.39	15	-112.22	13	485.76	5	362.82	1	-18.69	9
202	203	-15	Max	0.00	1.07	5	169.81	9	175.47	15	1062.52	1	-971.61	5	18.69	15
202	203	-15	Max	84.71	1.07	5	169.81	9	31.62	13	985.38	1	-196.50	5	18.69	15
202	203	-15	Min.	0.00	-198.45	1	-169.81	13	-175.47	9	953.53	5	-1382.92	1	-18.69	9
202	203	-15	Min.	84.71	-198.45	1	-169.81	13	-31.62	9	876.39	5	-515.49	1	-18.69	9
203	-16	203	Max	0.00	109.41	1	154.21	13	99.51	15	-835.25	1	-404.71	1	6.89	9
203	-16	203	Max	49.23	109.41	1	154.21	13	175.43	15	-880.08	1	-826.92	1	6.89	9
203	-16	203	Min.	0.00	-217.22	7	-154.21	9	-99.51	9	-996.90	5	-829.21	5	-6.89	15
203	-16	203	Min.	49.23	-217.22	7	-154.21	9	-175.43	9	-1041.73	5	-1331.00	5	-6.89	15
203	-17	-16	Max	0.00	49.73	1	94.53	13	27.10	11	-444.63	1	272.50	1	6.89	9
203	-17	-16	Max	133.94	49.73	1	94.53	13	99.51	13	-566.60	1	-404.73	1	6.89	9
203	-17	-16	Min.	0.00	-157.54	7	-94.53	9	-27.10	13	-606.28	5	64.52	5	-6.89	15
203	-17	-16	Min.	133.94	-157.54	7	-94.53	9	-99.51	9	-728.25	5	-829.23	5	-6.89	15
203	-18	-17	Max	0.00	-16.49	1	28.31	13	65.02	9	-54.00	1	435.04	5	6.89	9
203	-18	-17	Max	133.94	-16.49	1	28.31	13	27.10	9	-175.97	1	272.50	1	6.89	9
203	-18	-17	Min.	0.00	-91.32	7	-28.31	11	-65.02	13	-215.65	5	426.51	1	-6.89	15
203	-18	-17	Min.	133.94	-91.32	7	-28.31	11	-27.10	15	-337.62	5	64.51	5	-6.89	15
203	-19	-18	Max	0.00	-25.11	5	37.91	9	14.25	9	336.63	1	282.34	5	6.89	9
203	-19	-18	Max	133.94	-25.11	5	37.91	9	65.02	9	214.67	1	435.04	5	6.89	9
203	-19	-18	Min.	0.00	-82.71	3	-37.91	15	-14.25	15	174.99	5	57.28	1	-6.89	15
203	-19	-18	Min.	133.94	-82.71	3	-37.91	15	-65.02	15	53.02	5	426.50	1	-6.89	15
203	-20	-19	Max	0.00	41.11	5	104.13	9	125.22	13	727.26	1	-393.56	5	6.89	9
203	-20	-19	Max	133.94	41.11	5	104.13	9	14.25	9	605.29	1	282.35	5	6.89	9
203	-20	-19	Min.	0.00	-148.93	3	-104.13	13	-125.22	11	565.61	5	-835.13	1	-6.89	15
203	-20	-19	Min.	133.94	-148.93	3	-104.13	13	-14.25	15	443.64	5	57.30	1	-6.89	15
203	204	-20	Max	0.00	84.95	5	147.96	9	154.81	13	933.97	1	-546.20	5	6.89	9
203	204	-20	Max	20.00	84.95	5	147.96	9	125.22	13	915.75	1	-393.56	5	6.89	9
203	204	-20	Min.	0.00	-192.76	3	-147.96	13	-154.81	9	772.32	5	-1020.10	1	-6.89	15
203	204	-20	Min.	20.00	-192.76	3	-147.96	13	-125.22	9	754.11	5	-835.13	1	-6.89	15
204	204	-21	Max	0.00	84.95	1	147.96	13	154.81	9	933.97	5	-546.20	1	6.89	13
204	204	-21	Max	20.00	84.95	1	147.96	13	125.22	9	915.75	5	-393.56	1	6.89	13
204	204	-21	Min.	0.00	-192.76	5	-147.96	9	-154.81	13	772.32	1	-1020.10	5	-6.89	11
204	204	-21	Min.	20.00	-192.76	5	-147.96	9	-125.22	13	754.11	1	-835.13	5	-6.89	11
204	-21	-22	Max	0.00	41.11	1	104.13	13	125.22	11	727.26	5	-393.56	1	6.89	13
204	-21	-22	Max	133.94	41.11	1	104.13	13	14.25	15	605.29	5	282.35	1	6.89	13
204	-21	-22	Min.	0.00	-148.93	5	-104.13	9	-125.22	13	565.61	1	-835.13	5	-6.89	9
204	-21	-22	Min.	133.94	-148.93	5	-104.13	9	-14.25	9	443.64	1	57.30	5	-6.89	9
204	-22	-23	Max	0.00	-25.11	1	37.91	13	14.25	13	336.63	5	282.34	1	6.89	13
204	-22	-23	Max	133.94	-25.11	1	37.91	13	65.02	13	214.67	5	435.04	1	6.89	13
204	-22	-23	Min.	0.00	-82.71	7	-37.91	11	-14.25	11	174.99	1	57.28	5	-6.89	11
204	-22	-23	Min.	133.94	-82.71	7	-37.91	11	-65.02	11	53.02	1	426.50	5	-6.89	11
204	-23	-24	Max	0.00	-16.49	5	28.31	9	65.02	13	-54.00	5	435.04	1	6.89	13
204	-23	-24	Max	133.94	-16.49	5	28.31	9	27.10	13	-175.97	5	272.50	5	6.89	13
204	-23	-24	Min.	0.00	-91.32	3	-28.31	15	-65.02	9	-215.65	1	426.51	5	-6.89	11
204	-23	-24	Min.	133.94	-91.32	3	-28.31	15	-27.10	11	-337.62	1	64.51	1	-6.89	11
204	-24	-25	Max	0.00	49.73	5	94.53	9	27.10	15	-444.63	5	272.51	5	6.89	13
204	-24	-25	Max	133.94	49.73	5	94.53	9	99.51	9	-566.59	5	-404.72	5	6.89	13
204	-24	-25	Min.	0.00	-157.54	1	-94.53	13	-27.10	9	-606.27	1	64.52	1	-6.89	11

204	-24	-25	Min.	133.94	-157.54	1	-94.53	13	-99.51	13	-728.24	1	-829.23	1	-6.89	11
204	-25	205	Max	0.00	109.41	5	154.21	9	99.51	11	-835.25	5	-404.71	5	6.89	13
204	-25	205	Max	49.23	109.41	5	154.21	9	175.42	11	-880.08	5	-826.92	5	6.89	13
204	-25	205	Min.	0.00	-217.22	1	-154.21	13	-99.51	13	-996.90	1	-829.21	1	-6.89	9
204	-25	205	Min.	49.23	-217.22	1	-154.21	13	-175.42	13	-1041.73	1	-1331.00	1	-6.89	9
205	205	-26	Max	0.00	1.07	1	169.81	13	175.47	11	1062.52	5	-971.60	1	18.69	9
205	205	-26	Max	84.71	1.07	1	169.81	13	31.62	11	985.38	5	-196.50	1	18.69	9
205	205	-26	Min.	0.00	-198.44	5	-169.81	9	-175.47	13	953.53	1	-1382.91	5	-18.69	13
205	205	-26	Min.	84.71	-198.44	5	-169.81	9	-31.62	13	876.39	1	-515.48	5	-18.69	13
205	-26	-27	Max	0.00	-61.35	1	107.39	13	31.62	9	716.72	5	-196.54	1	18.69	9
205	-26	-27	Max	133.94	-61.35	1	107.39	13	112.21	13	594.75	5	535.79	1	18.69	9
205	-26	-27	Min.	0.00	-136.03	5	-107.39	9	-31.62	15	607.73	1	-515.53	5	-18.69	13
205	-26	-27	Min.	133.94	-136.03	5	-107.39	9	-112.21	11	485.76	1	362.78	5	-18.69	13
205	-27	-28	Max	0.00	-69.81	5	41.17	13	112.22	13	326.08	5	535.83	1	18.69	9
205	-27	-28	Max	133.94	-69.81	5	41.17	13	167.36	13	204.12	5	744.93	1	18.69	9
205	-27	-28	Min.	0.00	-127.56	3	-41.17	11	-112.22	9	217.10	1	362.82	5	-18.69	13
205	-27	-28	Min.	133.94	-127.56	3	-41.17	11	-167.36	9	95.13	1	717.91	5	-18.69	13
205	-28	-29	Max	0.00	-3.59	5	25.05	9	167.36	13	-64.54	5	744.93	1	18.69	9
205	-28	-29	Max	133.94	-3.59	5	25.05	9	133.81	13	-186.51	5	549.77	5	18.69	9
205	-28	-29	Min.	0.00	-193.78	1	-25.05	15	-167.36	9	-173.53	1	717.90	5	-18.69	13
205	-28	-29	Min.	133.94	-193.78	1	-25.05	15	-133.81	9	-295.50	1	430.82	1	-18.69	13
205	-29	-30	Max	0.00	62.63	5	91.27	9	133.81	13	-455.17	5	549.78	5	18.69	9
205	-29	-30	Max	133.94	62.63	5	91.27	9	11.57	15	-577.13	5	-141.57	5	18.69	9
205	-29	-30	Min.	0.00	-260.00	1	-91.27	13	-133.81	9	-564.15	1	430.83	1	-18.69	13
205	-29	-30	Min.	133.94	-260.00	1	-91.27	13	-11.57	9	-686.12	1	-406.50	1	-18.69	13
205	-30	-31	Max	0.00	125.39	5	154.03	9	11.56	13	-845.80	5	-141.61	5	18.69	9
205	-30	-31	Max	89.11	125.39	5	154.03	9	125.70	9	-926.95	5	-931.49	5	18.69	9
205	-30	-31	Min.	0.00	-322.76	1	-154.03	13	-11.56	11	-954.79	1	-406.55	1	-18.69	13
205	-30	-31	Min.	89.11	-322.76	1	-154.03	13	-125.70	15	-1035.93	1	-1293.55	1	-18.69	13
206	-31	-32	Max	0.00	8.79	1	146.69	13	125.58	9	1058.27	5	-684.01	1	65.41	9
206	-31	-32	Max	44.83	8.79	1	146.69	13	59.81	9	1017.45	5	-345.82	1	65.41	9
206	-31	-32	Min.	0.00	-95.88	5	-146.69	9	-125.58	15	774.81	1	-1296.73	5	-65.41	13
206	-31	-32	Min.	44.83	-95.88	5	-146.69	9	-59.81	15	733.99	1	-831.47	5	-65.41	13
206	-32	-33	Max	0.00	-36.54	5	87.35	13	59.81	9	748.79	5	-345.81	1	65.41	11
206	-32	-33	Max	133.94	-36.54	5	87.35	13	57.19	13	626.82	5	195.77	1	65.41	11
206	-32	-33	Min.	0.00	-50.55	1	-87.35	11	-59.81	13	465.32	1	-831.46	5	-65.41	13
206	-32	-33	Min.	133.94	-50.55	1	-87.35	11	-57.19	11	343.36	1	89.81	5	-65.41	13
206	-33	-34	Max	0.00	29.68	5	21.14	13	57.19	13	358.16	5	195.76	1	65.41	11
206	-33	-34	Max	82.03					-22.36	1			226.40	1		
206	-33	-34	Max	133.94	29.68	5	21.14	13	85.50	13	236.20	5	487.84	5	65.41	11
206	-33	-34	Min.	0.00	-116.77	1	-21.14	11	-57.19	11	74.70	1	89.79	5	-65.41	13
206	-33	-34	Min.	82.03					-22.36	1			226.40	1		
206	-33	-34	Min.	133.94	-116.77	1	-21.14	11	-85.50	11	-47.27	1	214.13	1	-65.41	13
206	-34	-35	Max	0.00	95.89	5	45.08	9	85.50	13	-32.46	5	487.83	5	65.41	9
206	-34	-35	Max	133.94	95.89	5	45.08	9	25.12	13	-154.43	5	362.67	5	65.41	9
206	-34	-35	Min.	0.00	-182.99	1	-45.08	15	-85.50	9	-315.93	1	214.14	1	-65.41	13
206	-34	-35	Min.	133.94	-182.99	1	-45.08	15	-25.12	11	-437.89	1	-290.71	1	-65.41	13
206	-35	-36	Max	0.00	155.89	5	105.08	9	25.11	13	-423.10	5	362.66	5	65.41	11
206	-35	-36	Max	53.34	155.89	5	105.08	9	30.94	9	-471.67	5	124.01	5	65.41	11
206	-35	-36	Min.	0.00	-242.98	1	-105.08	15	-25.11	11	-706.56	1	-290.74	1	-65.41	13
206	-35	-36	Min.	53.34	-242.98	1	-105.08	15	-30.94	15	-755.13	1	-680.59	1	-65.41	13
206	-36	-37	Max	0.00	38.17	1	38.17	13	30.77	9	261.89	1	-181.50	1	0.00	1
206	-36	-37	Max	80.60	38.17	1	38.17	13	0.00	13	188.50	1	0.00	1	0.00	1
206	-36	-37	Min.	0.00	-38.17	5	-38.17	9	-30.77	15	261.89	1	-181.50	1	0.00	1
206	-36	-37	Min.	80.60	-38.17	5	-38.17	9	0.00	11	188.50	1	0.00	1	0.00	1
302	-4	-47	Max	0.00	9.26	13	9.26	5	13.89	1	94.25	1	-81.91	1	0.00	1
302	-4	-47	Max	150.00	9.26	13	9.26	5	0.00	1	14.97	1	0.00	1	0.00	1
302	-4	-47	Min.	0.00	-9.26	9	-9.26	1	-13.89	5	94.25	1	-81.91	1	0.00	1
302	-4	-47	Min.	150.00	-9.26	9	-9.26	1	0.00	5	14.97	1	0.00	1	0.00	1
302	-46	-4	Max	0.00	9.26	9	9.26	1	0.00	1	-14.97	1	0.00	13	0.00	1
302	-46	-4	Max	150.00	9.26	9	9.26	1	13.89	1	-94.25	1	-81.91	1	0.00	1
302	-46	-4	Min.	0.00	-9.26	13	-9.26	5	0.00	7	-14.97	1	0.00	9	0.00	1
302	-46	-4	Min.	150.00	-9.26	13	-9.26	5	-13.89	5	-94.25	1	-81.91	1	0.00	1
303	-6	-48	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
303	-6	-48	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
303	-6	-48	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
303	-6	-48	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
303	-49	-6	Max	0.00	13.92	9	13.92	1	0.00	9	-29.94	1	0.00	9	0.00	1
303	-49	-6	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
303	-49	-6	Min.	0.00	-13.92	13	-13.92	5	0.00	13	-29.94	1	0.00	13	0.00	1
303	-49	-6	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
304	-7	-96	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
304	-7	-96	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
304	-7	-96	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
304	-7	-96	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
304	-95	-7	Max	0.00	13.92	9	13.92	1	0.00	9	-29.94	1	0.00	13	0.00	1

304	-95	-7	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
304	-95	-7	Min.	0.00	-13.92	13	-13.92	5	0.00	13	-29.94	1	0.00	9	0.00	1
304	-95	-7	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
305	-8	-66	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
305	-8	-66	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
305	-8	-66	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
305	-8	-66	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
305	-67	-8	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	11	0.00	1
305	-67	-8	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
305	-67	-8	Min.	0.00	-13.92	13	-13.92	5	0.00	5	-29.94	1	0.00	13	0.00	1
305	-67	-8	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
306	-9	-69	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
306	-9	-69	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
306	-9	-69	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
306	-9	-69	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
306	-68	-9	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	15	0.00	1
306	-68	-9	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
306	-68	-9	Min.	0.00	-13.92	13	-13.92	5	0.00	7	-29.94	1	0.00	9	0.00	1
306	-68	-9	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
307	-11	-70	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
307	-11	-70	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
307	-11	-70	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
307	-11	-70	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
307	-71	-11	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	15	0.00	1
307	-71	-11	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
307	-71	-11	Min.	0.00	-13.92	13	-13.92	5	0.00	7	-29.94	1	0.00	9	0.00	1
307	-71	-11	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
308	-12	-72	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
308	-12	-72	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
308	-12	-72	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
308	-12	-72	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
308	-73	-12	Max	0.00	13.92	9	13.92	1	0.00	5	-29.94	1	0.00	11	0.00	1
308	-73	-12	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
308	-73	-12	Min.	0.00	-13.92	13	-13.92	5	0.00	1	-29.94	1	0.00	13	0.00	1
308	-73	-12	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
309	-13	-74	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
309	-13	-74	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
309	-13	-74	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
309	-13	-74	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
309	-75	-13	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	15	0.00	1
309	-75	-13	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
309	-75	-13	Min.	0.00	-13.92	13	-13.92	5	0.00	5	-29.94	1	0.00	9	0.00	1
309	-75	-13	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
310	-14	-90	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
310	-14	-90	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
310	-14	-90	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
310	-14	-90	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
310	-91	-14	Max	0.00	13.92	9	13.92	1	0.00	5	-29.94	1	0.00	15	0.00	1
310	-91	-14	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
310	-91	-14	Min.	0.00	-13.92	13	-13.92	5	0.00	3	-29.94	1	0.00	9	0.00	1
310	-91	-14	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
311	-15	-92	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
311	-15	-92	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
311	-15	-92	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
311	-15	-92	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
311	-93	-15	Max	0.00	13.92	9	13.92	1	0.00	7	-29.94	1	0.00	9	0.00	1
311	-93	-15	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
311	-93	-15	Min.	0.00	-13.92	13	-13.92	5	0.00	1	-29.94	1	0.00	13	0.00	1
311	-93	-15	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
312	-16	-98	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
312	-16	-98	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
312	-16	-98	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
312	-16	-98	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
312	-94	-16	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	9	0.00	1
312	-94	-16	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
312	-94	-16	Min.	0.00	-13.92	13	-13.92	5	0.00	7	-29.94	1	0.00	13	0.00	1
312	-94	-16	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
313	-17	-97	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
313	-17	-97	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
313	-17	-97	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
313	-17	-97	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
313	-42	-17	Max	0.00	13.92	9	13.92	1	0.00	7	-29.94	1	0.00	9	0.00	1
313	-42	-17	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
313	-42	-17	Min.	0.00	-13.92	13	-13.92	5	0.00	1	-29.94	1	0.00	13	0.00	1
313	-42	-17	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
314	-18	-43	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1

314	-18	-43	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
314	-18	-43	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
314	-18	-43	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
314	-44	-18	Max	0.00	13.92	9	13.92	1	0.00	3	-29.94	1	0.00	9	0.00	1
314	-44	-18	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
314	-44	-18	Min.	0.00	-13.92	13	-13.92	5	0.00	5	-29.94	1	0.00	13	0.00	1
314	-44	-18	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
315	-19	-45	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
315	-19	-45	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
315	-19	-45	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
315	-19	-45	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
315	-58	-19	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	15	0.00	1
315	-58	-19	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
315	-58	-19	Min.	0.00	-13.92	13	-13.92	5	0.00	7	-29.94	1	0.00	9	0.00	1
315	-58	-19	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
316	-20	-63	Max	0.00	9.26	13	9.26	5	13.89	1	94.25	1	-81.91	1	0.00	1
316	-20	-63	Max	150.00	9.26	13	9.26	5	0.00	1	14.97	1	0.00	1	0.00	1
316	-20	-63	Min.	0.00	-9.26	9	-9.26	1	-13.89	5	94.25	1	-81.91	1	0.00	1
316	-20	-63	Min.	150.00	-9.26	9	-9.26	1	0.00	5	14.97	1	0.00	1	0.00	1
316	-65	-20	Max	0.00	9.26	9	9.26	1	0.00	7	-14.97	1	0.00	15	0.00	1
316	-65	-20	Max	150.00	9.26	9	9.26	1	13.89	1	-94.25	1	-81.91	1	0.00	1
316	-65	-20	Min.	0.00	-9.26	13	-9.26	5	0.00	1	-14.97	1	0.00	9	0.00	1
316	-65	-20	Min.	150.00	-9.26	13	-9.26	5	-13.89	5	-94.25	1	-81.91	1	0.00	1
317	-21	-51	Max	0.00	9.26	13	9.26	5	13.89	1	94.25	1	-81.91	1	0.00	1
317	-21	-51	Max	150.00	9.26	13	9.26	5	0.00	1	14.97	1	0.00	1	0.00	1
317	-21	-51	Min.	0.00	-9.26	9	-9.26	1	-13.89	5	94.25	1	-81.91	1	0.00	1
317	-21	-51	Min.	150.00	-9.26	9	-9.26	1	0.00	5	14.97	1	0.00	1	0.00	1
317	-50	-21	Max	0.00	9.26	9	9.26	1	0.00	1	-14.97	1	0.00	1	0.00	1
317	-50	-21	Max	150.00	9.26	9	9.26	1	13.89	1	-94.25	1	-81.91	1	0.00	1
317	-50	-21	Min.	0.00	-9.26	13	-9.26	5	0.00	1	-14.97	1	0.00	1	0.00	1
317	-50	-21	Min.	150.00	-9.26	13	-9.26	5	-13.89	5	-94.25	1	-81.91	1	0.00	1
318	-22	-53	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	9
318	-22	-53	Max	150.00	13.92	13	13.92	5	0.00	1	29.94	1	0.00	1	0.00	9
318	-22	-53	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	13
318	-22	-53	Min.	150.00	-13.92	9	-13.92	1	0.00	5	29.94	1	0.00	1	0.00	13
318	-52	-22	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	11	0.00	1
318	-52	-22	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
318	-52	-22	Min.	0.00	-13.92	13	-13.92	5	0.00	5	-29.94	1	0.00	13	0.00	1
318	-52	-22	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
319	-23	-55	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
319	-23	-55	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
319	-23	-55	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
319	-23	-55	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
319	-54	-23	Max	0.00	13.92	9	13.92	1	0.00	13	-29.94	1	0.00	9	0.00	1
319	-54	-23	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
319	-54	-23	Min.	0.00	-13.92	13	-13.92	5	0.00	9	-29.94	1	0.00	13	0.00	1
319	-54	-23	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
320	-24	-57	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
320	-24	-57	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
320	-24	-57	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
320	-24	-57	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
320	-56	-24	Max	0.00	13.92	9	13.92	1	0.00	5	-29.94	1	0.00	1	0.00	1
320	-56	-24	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
320	-56	-24	Min.	0.00	-13.92	13	-13.92	5	0.00	1	-29.94	1	0.00	1	0.00	1
320	-56	-24	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
322	-25	-41	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
322	-25	-41	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
322	-25	-41	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
322	-25	-41	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
322	-64	-25	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	11	0.00	1
322	-64	-25	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
322	-64	-25	Min.	0.00	-13.92	13	-13.92	5	0.00	5	-29.94	1	0.00	13	0.00	1
322	-64	-25	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
323	-26	-77	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
323	-26	-77	Max	150.00	13.92	13	13.92	5	0.00	1	29.94	1	0.00	1	0.00	1
323	-26	-77	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
323	-26	-77	Min.	150.00	-13.92	9	-13.92	1	0.00	5	29.94	1	0.00	1	0.00	1
323	-76	-26	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	9	0.00	1
323	-76	-26	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
323	-76	-26	Min.	0.00	-13.92	13	-13.92	5	0.00	7	-29.94	1	0.00	13	0.00	1
323	-76	-26	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
324	-27	-79	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
324	-27	-79	Max	150.00	13.92	13	13.92	5	0.00	1	29.94	1	0.00	1	0.00	1
324	-27	-79	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
324	-27	-79	Min.	150.00	-13.92	9	-13.92	1	0.00	5	29.94	1	0.00	1	0.00	1
324	-78	-27	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	13	0.00	1

324	-78	-27	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
324	-78	-27	Min.	0.00	-13.92	13	-13.92	5	0.00	1	-29.94	1	0.00	9	0.00	1
324	-78	-27	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
325	-28	-81	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
325	-28	-81	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
325	-28	-81	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
325	-28	-81	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
325	-80	-28	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	15	0.00	1
325	-80	-28	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
325	-80	-28	Min.	0.00	-13.92	13	-13.92	5	0.00	5	-29.94	1	0.00	9	0.00	1
325	-80	-28	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
326	-29	-83	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
326	-29	-83	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
326	-29	-83	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
326	-29	-83	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
326	-82	-29	Max	0.00	13.92	9	13.92	1	0.00	5	-29.94	1	0.00	15	0.00	1
326	-82	-29	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
326	-82	-29	Min.	0.00	-13.92	13	-13.92	5	0.00	3	-29.94	1	0.00	9	0.00	1
326	-82	-29	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
327	-30	-85	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
327	-30	-85	Max	150.00	13.92	13	13.92	5	0.00	1	29.94	1	0.00	1	0.00	1
327	-30	-85	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
327	-30	-85	Min.	150.00	-13.92	9	-13.92	1	0.00	5	29.94	1	0.00	1	0.00	1
327	-84	-30	Max	0.00	13.92	9	13.92	1	0.00	13	-29.94	1	0.00	9	0.00	1
327	-84	-30	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
327	-84	-30	Min.	0.00	-13.92	13	-13.92	5	0.00	9	-29.94	1	0.00	13	0.00	1
327	-84	-30	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
329	-32	-86	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
329	-32	-86	Max	150.00	13.92	13	13.92	5	0.00	1	29.94	1	0.00	1	0.00	1
329	-32	-86	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
329	-32	-86	Min.	150.00	-13.92	9	-13.92	1	0.00	5	29.94	1	0.00	1	0.00	1
329	-87	-32	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	13	0.00	1
329	-87	-32	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
329	-87	-32	Min.	0.00	-13.92	13	-13.92	5	0.00	5	-29.94	1	0.00	9	0.00	1
329	-87	-32	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
330	-33	-89	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
330	-33	-89	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
330	-33	-89	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
330	-33	-89	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
330	-88	-33	Max	0.00	13.92	9	13.92	1	0.00	3	-29.94	1	0.00	15	0.00	1
330	-88	-33	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
330	-88	-33	Min.	0.00	-13.92	13	-13.92	5	0.00	5	-29.94	1	0.00	9	0.00	1
330	-88	-33	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
331	-34	-61	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
331	-34	-61	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
331	-34	-61	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
331	-34	-61	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
331	-62	-34	Max	0.00	13.92	9	13.92	1	0.00	7	-29.94	1	0.00	9	0.00	1
331	-62	-34	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
331	-62	-34	Min.	0.00	-13.92	13	-13.92	5	0.00	1	-29.94	1	0.00	15	0.00	1
331	-62	-34	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
332	-35	-102	Max	0.00	13.92	13	13.92	5	20.88	1	134.33	1	-123.20	1	0.00	1
332	-35	-102	Max	150.00	13.92	13	13.92	5	0.00	5	29.94	1	0.00	1	0.00	1
332	-35	-102	Min.	0.00	-13.92	9	-13.92	1	-20.88	5	134.33	1	-123.20	1	0.00	1
332	-35	-102	Min.	150.00	-13.92	9	-13.92	1	0.00	1	29.94	1	0.00	1	0.00	1
332	-101	-35	Max	0.00	13.92	9	13.92	1	0.00	1	-29.94	1	0.00	13	0.00	1
332	-101	-35	Max	150.00	13.92	9	13.92	1	20.88	1	-134.33	1	-123.20	1	0.00	1
332	-101	-35	Min.	0.00	-13.92	13	-13.92	5	0.00	7	-29.94	1	0.00	9	0.00	1
332	-101	-35	Min.	150.00	-13.92	13	-13.92	5	-20.88	5	-134.33	1	-123.20	1	0.00	1
333	-37	-103	Max	0.00	9.26	13	9.26	5	13.89	1	94.25	1	-81.91	1	0.00	1
333	-37	-103	Max	150.00	9.26	13	9.26	5	0.00	1	14.97	1	0.00	13	0.00	1
333	-37	-103	Min.	0.00	-9.26	9	-9.26	1	-13.89	5	94.25	1	-81.91	1	0.00	1
333	-37	-103	Min.	150.00	-9.26	9	-9.26	1	0.00	5	14.97	1	0.00	9	0.00	1
333	-104	-37	Max	0.00	9.26	9	9.26	1	0.00	7	-14.97	1	0.00	15	0.00	1
333	-104	-37	Max	150.00	9.26	9	9.26	1	13.89	1	-94.25	1	-81.91	1	0.00	1
333	-104	-37	Min.	0.00	-9.26	13	-9.26	5	0.00	1	-14.97	1	0.00	9	0.00	1
333	-104	-37	Min.	150.00	-9.26	13	-9.26	5	-13.89	5	-94.25	1	-81.91	1	0.00	1

Tipo di combinazione di carico: SLD

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-1036.25	2	189.41	6	214.03	2	94.53	14	346.13	10	0.09	10
1	1	-5	Max	328.50	-798.19	2	189.41	6	315.63	6	94.53	14	35.58	12	0.09	10
1	1	-5	Min.	0.00	-1190.46	6	-102.32	2	-306.60	6	-94.53	10	-346.13	14	-0.09	16
1	1	-5	Min.	328.50	-952.40	6	-102.32	2	-122.09	2	-94.53	10	-35.58	14	-0.09	16

2	2	-10	Max	0.00	-2088.59	6	222.12	6	224.34	2	180.20	14	566.54	10	0.06	10
2	2	-10	Max	328.50	-1850.52	6	222.12	6	387.27	6	180.20	14	25.42	16	0.06	10
2	2	-10	Min.	0.00	-2183.51	2	-111.83	2	-342.38	6	-180.20	10	-566.54	14	-0.06	14
2	2	-10	Min.	328.50	-1945.44	2	-111.83	2	-143.03	2	-180.20	10	-25.42	10	-0.06	14
3	3	203	Max	0.00	-2192.67	2	114.94	6	324.49	2	192.87	16	619.67	10	0.02	14
3	3	203	Max	328.50	-1954.60	2	114.94	6	150.71	6	192.87	16	13.92	16	0.02	14
3	3	203	Min.	0.00	-2221.32	6	-204.50	2	-226.87	6	-192.87	10	-619.67	14	-0.02	12
3	3	203	Min.	328.50	-1983.25	6	-204.50	2	-347.28	2	-192.87	10	-13.92	10	-0.02	12
4	4	204	Max	0.00	-1944.35	2	163.74	2	280.07	6	173.64	10	577.92	14	0.00	12
4	4	204	Max	328.50	-1706.28	2	163.74	2	257.81	2	173.64	10	7.50	16	0.00	12
4	4	204	Min.	0.00	-1944.35	2	-163.74	6	-280.07	2	-173.64	14	-577.92	12	0.00	14
4	4	204	Min.	328.50	-1706.28	2	-163.74	6	-257.81	6	-173.64	14	-7.50	10	0.00	14
5	5	205	Max	0.00	-2192.67	6	114.94	2	324.49	6	192.87	10	619.67	14	0.02	12
5	5	205	Max	328.50	-1954.60	6	114.94	2	150.71	2	192.87	10	13.92	12	0.02	12
5	5	205	Min.	0.00	-2221.32	2	-204.50	6	-226.87	2	-192.87	14	-619.67	10	-0.02	14
5	5	205	Min.	328.50	-1983.25	2	-204.50	6	-347.28	6	-192.87	14	-13.92	14	-0.02	14
6	6	-31	Max	0.00	-2088.58	2	222.12	2	224.34	6	180.20	10	566.54	14	0.06	14
6	6	-31	Max	328.50	-1850.52	2	222.12	2	387.26	2	180.20	10	25.42	12	0.06	14
6	6	-31	Min.	0.00	-2183.50	6	-111.83	6	-342.38	2	-180.20	14	-566.54	10	-0.06	10
6	6	-31	Min.	328.50	-1945.44	6	-111.83	6	-143.03	6	-180.20	14	-25.42	14	-0.06	10
7	7	-36	Max	0.00	-1036.25	6	189.41	2	214.03	6	94.53	10	346.13	14	0.09	14
7	7	-36	Max	328.50	-798.18	6	189.41	2	315.63	2	94.53	10	35.58	16	0.09	14
7	7	-36	Min.	0.00	-1190.46	2	-102.32	6	-306.60	2	-94.53	14	-346.13	10	-0.09	12
7	7	-36	Min.	328.50	-952.39	2	-102.32	6	-122.09	6	-94.53	14	-35.58	10	-0.09	12
201	-5	-4	Max	0.00	20.77	6	20.77	10	16.74	14	261.89	2	-181.50	2	0.00	2
201	-5	-4	Max	80.60	20.77	6	20.77	10	0.00	10	188.50	2	0.00	2	0.00	2
201	-5	-4	Min.	0.00	-20.77	2	-20.77	14	-16.74	12	261.89	2	-181.50	2	0.00	2
201	-5	-4	Min.	80.60	-20.77	2	-20.77	14	0.00	16	188.50	2	0.00	2	0.00	2
201	-6	-5	Max	0.00	64.95	2	57.17	14	13.66	10	-487.72	2	213.71	2	35.58	14
201	-6	-5	Max	53.34	64.95	2	57.17	14	16.83	14	-536.30	2	-59.41	2	35.58	14
201	-6	-5	Min.	0.00	-152.04	6	-57.17	12	-13.66	16	-641.93	6	-141.75	6	-35.58	10
201	-6	-5	Min.	53.34	-152.04	6	-57.17	12	-16.83	12	-690.51	6	-497.13	6	-35.58	10
201	-7	-6	Max	0.00	32.31	2	24.53	14	46.51	10	-97.09	2	425.44	2	35.58	14
201	-7	-6	Max	133.94	32.31	2	24.53	14	13.66	10	-219.06	2	213.71	2	35.58	14
201	-7	-6	Min.	0.00	-119.41	6	-24.53	12	-46.51	14	-251.30	6	276.54	6	-35.58	10
201	-7	-6	Min.	133.94	-119.41	6	-24.53	12	-13.66	16	-373.27	6	-141.75	6	-35.58	10
201	-8	-7	Max	0.00	-3.71	2	11.50	10	31.11	10	293.54	2	171.60	6	35.58	16
201	-8	-7	Max	133.94	-3.71	2	11.50	10	46.51	10	171.57	2	425.44	2	35.58	16
201	-8	-7	Min.	0.00	-83.38	6	-11.50	16	-31.11	14	139.32	6	113.95	2	-35.58	10
201	-8	-7	Min.	133.94	-83.38	6	-11.50	16	-46.51	16	17.36	6	276.54	6	-35.58	10
201	-9	-8	Max	0.00	-39.74	2	47.52	10	32.54	14	684.16	2	-456.55	6	35.58	16
201	-9	-8	Max	133.94	-39.74	2	47.52	10	31.11	10	562.20	2	171.60	6	35.58	16
201	-9	-8	Min.	0.00	-47.36	6	-47.52	16	-32.54	10	529.95	6	-720.75	2	-35.58	10
201	-9	-8	Min.	133.94	-47.36	6	-47.52	16	-31.11	16	407.99	6	113.95	2	-35.58	10
201	-10	-9	Max	0.00	-15.07	6	79.81	10	68.32	14	993.64	2	-823.71	6	35.58	14
201	-10	-9	Max	44.83	-15.07	6	79.81	10	32.54	14	952.82	2	-456.55	6	35.58	14
201	-10	-9	Min.	0.00	-72.02	2	-79.81	16	-68.32	10	839.43	6	-1157.04	2	-35.58	10
201	-10	-9	Min.	44.83	-72.02	2	-79.81	16	-32.54	12	798.61	6	-720.75	2	-35.58	10
202	-11	-10	Max	0.00	23.21	2	83.79	14	6.29	12	-870.65	2	-201.98	2	10.17	16
202	-11	-10	Max	89.11	23.21	2	83.79	14	68.38	14	-951.79	2	-1014.01	2	10.17	16
202	-11	-10	Min.	0.00	-220.59	6	-83.79	10	-6.29	14	-929.94	6	-346.11	6	-10.16	10
202	-11	-10	Min.	89.11	-220.59	6	-83.79	10	-68.38	10	-1011.08	6	-1210.97	6	-10.16	10
202	-12	-11	Max	0.00	-10.93	2	49.65	14	72.80	10	-480.02	2	522.65	2	10.17	16
202	-12	-11	Max	133.94	-10.93	2	49.65	14	6.29	10	-601.99	2	-201.98	2	10.17	16
202	-12	-11	Min.	0.00	-186.45	6	-49.65	12	-72.80	14	-539.31	6	457.94	6	-10.17	10
202	-12	-11	Min.	133.94	-186.45	6	-49.65	12	-6.29	16	-661.28	6	-346.11	6	-10.17	10
202	-13	-12	Max	0.00	-46.95	2	13.63	14	91.05	10	-89.39	2	738.77	6	10.17	16
202	-13	-12	Max	133.94	-46.95	2	13.63	14	72.80	10	-211.36	2	522.65	2	10.17	16
202	-13	-12	Min.	0.00	-150.42	6	-13.63	12	-91.05	14	-148.68	6	724.07	2	-10.17	10
202	-13	-12	Min.	133.94	-150.42	6	-13.63	12	-72.80	14	-270.65	6	457.94	6	-10.17	10
202	-14	-13	Max	0.00	-82.98	2	22.40	10	61.05	12	301.24	2	496.38	6	10.17	16
202	-14	-13	Max	133.94	-82.98	2	22.40	10	91.05	10	179.27	2	738.77	6	10.17	16
202	-14	-13	Min.	0.00	-114.40	6	-22.40	16	-61.05	14	241.95	6	402.26	2	-10.17	10
202	-14	-13	Min.	133.94	-114.40	6	-22.40	16	-91.05	14	119.98	6	724.07	2	-10.17	10
202	-15	-14	Max	0.00	-78.37	6	58.42	10	17.20	16	691.87	2	-269.23	6	10.17	16
202	-15	-14	Max	133.94	-78.37	6	58.42	10	61.05	10	569.90	2	496.38	6	10.17	16
202	-15	-14	Min.	0.00	-119.00	2	-58.42	16	-17.20	10	632.58	6	-442.76	2	-10.17	10
202	-15	-14	Min.	133.94	-119.00	2	-58.42	16	-61.05	16	510.61	6	402.26	2	-10.17	10
202	203	-15	Max	0.00	-44.42	6	92.38	10	95.46	16	1037.67	2	-1065.38	6	10.16	16
202	203	-15	Max	84.71	-44.42	6	92.38	10	17.20	14	960.53	2	-269.23	6	10.16	16
202	203	-15	Min.	0.00	-152.96	2	-92.38	14	-95.46	10	978.38	6	-1289.15	2	-10.17	10
202	203	-15	Min.	84.71	-152.96	2	-92.38	14	-17.20	10	901.24	6	-442.76	2	-10.17	10
203	-16	203	Max	0.00	34.94	2	83.89	14	54.14	16	-872.11	2	-501.49	2	3.75	10
203	-16	203	Max	49.23	34.94	2	83.89	14	95.44	16	-916.93	2	-941.85	2	3.75	10
203	-16	203	Min.	0.00	-142.75	6	-83.89	10	-54.14	10	-960.05	6	-732.43	6	-3.75	16
203	-16	203	Min.	49.23	-142.75	6	-83.89	10	-95.44	10	-1004.87	6	-1216.08	6	-3.75	16



203	-17	-16	Max	0.00	2.47	2	51.43	14	14.74	12	-481.48	2	225.09	2	3.75	10
203	-17	-16	Max	133.94	2.47	2	51.43	14	54.14	14	-603.45	2	-501.51	2	3.75	10
203	-17	-16	Min.	0.00	-110.29	8	-51.43	12	-14.74	14	-569.42	6	111.94	6	-3.75	16
203	-17	-16	Min.	133.94	-110.29	8	-51.43	12	-54.14	10	-691.39	6	-732.45	6	-3.75	16
203	-18	-17	Max	0.00	-33.55	2	15.40	14	35.37	10	-90.86	2	433.10	6	3.75	10
203	-18	-17	Max	133.94	-33.55	2	15.40	14	14.74	10	-212.82	2	225.08	2	3.75	10
203	-18	-17	Min.	0.00	-74.26	8	-15.40	12	-35.37	14	-178.80	6	428.46	2	-3.75	16
203	-18	-17	Min.	133.94	-74.26	8	-15.40	12	-14.74	16	-300.76	6	111.93	6	-3.75	16
203	-19	-18	Max	0.00	-38.24	6	20.62	10	7.75	10	299.78	2	231.03	6	3.75	10
203	-19	-18	Max	133.94	-38.24	6	20.62	10	35.37	10	177.81	2	433.09	6	3.75	10
203	-19	-18	Min.	0.00	-69.58	4	-20.62	16	-7.75	16	211.84	6	108.59	2	-3.75	16
203	-19	-18	Min.	133.94	-69.58	4	-20.62	16	-35.37	16	89.87	6	428.44	2	-3.75	16
203	-20	-19	Max	0.00	-2.21	6	56.65	10	68.12	14	690.41	2	-494.23	6	3.75	10
203	-20	-19	Max	133.94	-2.21	6	56.65	10	7.75	10	568.44	2	231.04	6	3.75	10
203	-20	-19	Min.	0.00	-105.60	4	-56.65	16	-68.12	12	602.47	6	-734.45	2	-3.75	16
203	-20	-19	Min.	133.94	-105.60	4	-56.65	16	-7.75	16	480.50	6	108.61	2	-3.75	16
203	204	-20	Max	0.00	21.63	6	80.49	10	84.22	14	897.11	2	-654.24	6	3.75	10
203	204	-20	Max	20.00	21.63	6	80.49	10	68.12	14	878.90	2	-494.23	6	3.75	10
203	204	-20	Min.	0.00	-129.45	2	-80.49	14	-84.22	10	809.17	6	-912.06	2	-3.75	16
203	204	-20	Min.	20.00	-129.45	2	-80.49	14	-68.12	10	790.96	6	-734.46	2	-3.75	16
204	204	-21	Max	0.00	21.63	2	80.49	14	84.22	10	897.11	6	-654.25	2	3.75	14
204	204	-21	Max	20.00	21.63	2	80.49	14	68.12	10	878.90	6	-494.23	2	3.75	14
204	204	-21	Min.	0.00	-129.45	6	-80.49	10	-84.22	14	809.17	2	-912.06	6	-3.75	12
204	204	-21	Min.	20.00	-129.45	6	-80.49	10	-68.12	14	790.96	2	-734.46	6	-3.75	12
204	-21	-22	Max	0.00	-2.21	2	56.65	14	68.12	12	690.41	6	-494.23	2	3.75	14
204	-21	-22	Max	133.94	-2.21	2	56.65	14	7.75	16	568.44	6	231.04	2	3.75	14
204	-21	-22	Min.	0.00	-105.60	8	-56.65	12	-68.12	14	602.47	2	-734.45	6	-3.75	10
204	-21	-22	Min.	133.94	-105.60	8	-56.65	12	-7.75	10	480.50	2	108.61	6	-3.75	10
204	-22	-23	Max	0.00	-38.24	2	20.62	14	7.75	14	299.78	6	231.03	2	3.75	14
204	-22	-23	Max	133.94	-38.24	2	20.62	14	35.37	14	177.81	6	433.09	2	3.75	14
204	-22	-23	Min.	0.00	-69.58	8	-20.62	12	-7.75	12	211.84	2	108.59	6	-3.75	12
204	-22	-23	Min.	133.94	-69.58	8	-20.62	12	-35.37	12	89.87	2	428.44	6	-3.75	12
204	-23	-24	Max	0.00	-33.55	6	15.40	10	35.37	14	-90.86	6	433.10	2	3.75	14
204	-23	-24	Max	133.94	-33.55	6	15.40	10	14.74	14	-212.82	6	225.08	6	3.75	14
204	-23	-24	Min.	0.00	-74.26	4	-15.40	16	-35.37	10	-178.79	2	428.46	6	-3.75	10
204	-23	-24	Min.	133.94	-74.26	4	-15.40	16	-14.74	12	-300.76	2	111.93	2	-3.75	10
204	-24	-25	Max	0.00	2.47	6	51.43	10	14.74	16	-481.48	6	225.09	6	3.75	14
204	-24	-25	Max	133.94	2.47	6	51.43	10	54.14	10	-603.45	6	-501.51	6	3.75	14
204	-24	-25	Min.	0.00	-110.29	4	-51.43	16	-14.74	10	-569.42	2	111.94	2	-3.75	12
204	-24	-25	Min.	133.94	-110.29	4	-51.43	16	-54.14	14	-691.39	2	-732.45	2	-3.75	12
204	-25	205	Max	0.00	34.94	6	83.89	10	54.14	12	-872.11	6	-501.49	6	3.75	14
204	-25	205	Max	49.23	34.94	6	83.89	10	95.43	12	-916.93	6	-941.85	6	3.75	14
204	-25	205	Min.	0.00	-142.75	2	-83.89	14	-54.14	14	-960.05	2	-732.42	2	-3.75	12
204	-25	205	Min.	49.23	-142.75	2	-83.89	14	-95.43	14	-1004.87	2	-1216.07	2	-3.75	12
205	205	-26	Max	0.00	-44.42	2	92.38	14	95.46	12	1037.67	6	-1065.38	2	10.17	10
205	205	-26	Max	84.71	-44.42	2	92.38	14	17.20	12	960.53	6	-269.22	2	10.17	10
205	205	-26	Min.	0.00	-152.96	6	-92.38	10	-95.46	14	978.38	2	-1289.14	6	-10.17	14
205	205	-26	Min.	84.71	-152.96	6	-92.38	10	-17.20	14	901.24	2	-442.76	6	-10.17	14
205	-26	-27	Max	0.00	-78.37	2	58.42	14	17.20	10	691.87	6	-269.26	2	10.17	10
205	-26	-27	Max	133.94	-78.37	2	58.42	14	61.05	14	569.90	6	496.35	2	10.17	10
205	-26	-27	Min.	0.00	-119.00	6	-58.42	12	-17.20	16	632.58	2	-442.80	6	-10.17	14
205	-26	-27	Min.	133.94	-119.00	6	-58.42	12	-61.05	12	510.61	2	402.23	6	-10.17	14
205	-27	-28	Max	0.00	-82.98	6	22.40	14	61.05	14	301.24	6	496.38	2	10.17	10
205	-27	-28	Max	133.94	-82.98	6	22.40	14	91.05	14	179.27	6	738.77	2	10.17	10
205	-27	-28	Min.	0.00	-114.40	2	-22.40	12	-61.05	10	241.95	2	402.27	6	-10.17	14
205	-27	-28	Min.	133.94	-114.40	2	-22.40	12	-91.05	10	119.98	2	724.07	6	-10.17	14
205	-28	-29	Max	0.00	-46.95	6	13.63	10	91.05	14	-89.39	6	738.77	2	10.17	10
205	-28	-29	Max	133.94	-46.95	6	13.63	10	72.80	14	-211.36	6	522.65	6	10.17	10
205	-28	-29	Min.	0.00	-150.42	2	-13.63	16	-91.05	10	-148.68	2	724.06	6	-10.17	14
205	-28	-29	Min.	133.94	-150.42	2	-13.63	16	-72.80	10	-270.65	2	457.94	2	-10.17	14
205	-29	-30	Max	0.00	-10.93	6	49.65	10	72.80	16	-480.01	6	522.66	6	10.17	10
205	-29	-30	Max	133.94	-10.93	6	49.65	10	6.29	16	-601.98	6	-201.97	6	10.17	10
205	-29	-30	Min.	0.00	-186.44	2	-49.65	16	-72.80	10	-539.30	2	457.95	2	-10.17	14
205	-29	-30	Min.	133.94	-186.44	2	-49.65	16	-6.29	10	-661.27	2	-346.10	2	-10.17	14
205	-30	-31	Max	0.00	23.22	6	83.79	10	6.29	14	-870.65	6	-202.01	6	10.16	10
205	-30	-31	Max	89.11	23.22	6	83.79	10	68.38	10	-951.79	6	-1014.04	6	10.16	10
205	-30	-31	Min.	0.00	-220.59	2	-83.79	14	-6.29	12	-929.94	2	-346.14	2	-10.17	14
205	-30	-31	Min.	89.11	-220.59	2	-83.79	14	-68.38	16	-1011.09	2	-1211.00	2	-10.17	14
206	-31	-32	Max	0.00	-15.07	2	79.81	14	68.32	10	993.64	6	-823.70	2	35.58	10
206	-31	-32	Max	44.83	-15.07	2	79.81	14	32.54	10	952.82	6	-456.54	2	35.58	10
206	-31	-32	Min.	0.00	-72.02	6	-79.81	12	-68.32	16	839.43	2	-1157.04	6	-35.58	14
206	-31	-32	Min.	44.83	-72.02	6	-79.81	12	-32.54	16	798.61	2	-720.75	6	-35.58	14
206	-32	-33	Max	0.00	-39.74	6	47.52	14	32.54	10	684.16	6	-456.53	2	35.58	12
206	-32	-33	Max	133.94	-39.74	6	47.52	14	31.11	14	562.20	6	171.62	2	35.58	12
206	-32	-33	Min.	0.00	-47.36	2	-47.52	12	-32.54	14	529.95	2	-720.74	6	-35.58	14
206	-32	-33	Min.	133.94	-47.36	2	-47.52	12	-31.11	12	407.98	2	113.97	6	-35.58	14

206	-33	-34	Max	0.00	-3.71	6	11.50	14	31.11	14	293.54	6	171.60	2	35.58	12
206	-33	-34	Max	133.94	-3.71	6	11.50	14	46.51	14	171.57	6	425.44	6	35.58	12
206	-33	-34	Min.	0.00	-83.38	2	-11.50	12	-31.11	10	139.33	2	113.95	6	-35.58	14
206	-33	-34	Min.	133.94	-83.38	2	-11.50	12	-46.51	12	17.36	2	276.54	2	-35.58	14
206	-34	-35	Max	0.00	32.31	6	24.53	10	46.51	14	-97.09	6	425.44	6	35.58	10
206	-34	-35	Max	133.94	32.31	6	24.53	10	13.66	14	-219.06	6	213.71	6	35.58	10
206	-34	-35	Min.	0.00	-119.40	2	-24.53	16	-46.51	10	-251.30	2	276.54	2	-35.58	14
206	-34	-35	Min.	133.94	-119.40	2	-24.53	16	-13.66	12	-373.27	2	-141.74	2	-35.58	14
206	-35	-36	Max	0.00	64.95	6	57.17	10	13.66	14	-487.72	6	213.69	6	35.58	10
206	-35	-36	Max	53.34	64.95	6	57.17	10	16.83	10	-536.30	6	-59.43	6	35.58	10
206	-35	-36	Min.	0.00	-152.04	2	-57.17	16	-13.66	12	-641.93	2	-141.77	2	-35.58	14
206	-35	-36	Min.	53.34	-152.04	2	-57.17	16	-16.83	16	-690.51	2	-497.15	2	-35.58	14
206	-36	-37	Max	0.00	20.77	2	20.77	14	16.74	10	261.89	2	-181.50	2	0.00	2
206	-36	-37	Max	80.60	20.77	2	20.77	14	0.00	14	188.50	2	0.00	2	0.00	2
206	-36	-37	Min.	0.00	-20.77	6	-20.77	10	-16.74	16	261.89	2	-181.50	2	0.00	2
206	-36	-37	Min.	80.60	-20.77	6	-20.77	10	0.00	12	188.50	2	0.00	2	0.00	2
302	-4	-47	Max	0.00	5.04	14	5.04	6	7.55	2	94.25	2	-81.91	2	0.00	2
302	-4	-47	Max	150.00	5.04	14	5.04	6	0.00	2	14.97	2	0.00	2	0.00	2
302	-4	-47	Min.	0.00	-5.04	10	-5.04	2	-7.55	6	94.25	2	-81.91	2	0.00	2
302	-4	-47	Min.	150.00	-5.04	10	-5.04	2	0.00	6	14.97	2	0.00	2	0.00	2
302	-46	-4	Max	0.00	5.04	10	5.04	2	0.00	2	-14.97	2	0.00	14	0.00	2
302	-46	-4	Max	150.00	5.04	10	5.04	2	7.55	2	-94.25	2	-81.91	2	0.00	2
302	-46	-4	Min.	0.00	-5.04	14	-5.04	6	0.00	8	-14.97	2	0.00	10	0.00	2
302	-46	-4	Min.	150.00	-5.04	14	-5.04	6	-7.55	6	-94.25	2	-81.91	2	0.00	2
303	-6	-48	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
303	-6	-48	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
303	-6	-48	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
303	-6	-48	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
303	-49	-6	Max	0.00	7.57	10	7.57	2	0.00	10	-29.94	2	0.00	10	0.00	2
303	-49	-6	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
303	-49	-6	Min.	0.00	-7.57	14	-7.57	6	0.00	14	-29.94	2	0.00	14	0.00	2
303	-49	-6	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
304	-7	-96	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
304	-7	-96	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
304	-7	-96	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
304	-7	-96	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
304	-95	-7	Max	0.00	7.57	10	7.57	2	0.00	10	-29.94	2	0.00	14	0.00	2
304	-95	-7	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
304	-95	-7	Min.	0.00	-7.57	14	-7.57	6	0.00	14	-29.94	2	0.00	10	0.00	2
304	-95	-7	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
305	-8	-66	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
305	-8	-66	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
305	-8	-66	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
305	-8	-66	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
305	-67	-8	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	12	0.00	2
305	-67	-8	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
305	-67	-8	Min.	0.00	-7.57	14	-7.57	6	0.00	6	-29.94	2	0.00	14	0.00	2
305	-67	-8	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
306	-9	-69	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
306	-9	-69	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
306	-9	-69	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
306	-9	-69	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
306	-68	-9	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	16	0.00	2
306	-68	-9	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
306	-68	-9	Min.	0.00	-7.57	14	-7.57	6	0.00	8	-29.94	2	0.00	10	0.00	2
306	-68	-9	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
307	-11	-70	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
307	-11	-70	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
307	-11	-70	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
307	-11	-70	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
307	-71	-11	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	16	0.00	2
307	-71	-11	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
307	-71	-11	Min.	0.00	-7.57	14	-7.57	6	0.00	8	-29.94	2	0.00	10	0.00	2
307	-71	-11	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
308	-12	-72	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
308	-12	-72	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
308	-12	-72	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
308	-12	-72	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
308	-73	-12	Max	0.00	7.57	10	7.57	2	0.00	6	-29.94	2	0.00	12	0.00	2
308	-73	-12	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
308	-73	-12	Min.	0.00	-7.57	14	-7.57	6	0.00	2	-29.94	2	0.00	14	0.00	2
308	-73	-12	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
309	-13	-74	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
309	-13	-74	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
309	-13	-74	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
309	-13	-74	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2

309	-75	-13	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	16	0.00	2
309	-75	-13	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
309	-75	-13	Min.	0.00	-7.57	14	-7.57	6	0.00	6	-29.94	2	0.00	10	0.00	2
309	-75	-13	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
310	-14	-90	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
310	-14	-90	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
310	-14	-90	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
310	-14	-90	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
310	-91	-14	Max	0.00	7.57	10	7.57	2	0.00	6	-29.94	2	0.00	16	0.00	2
310	-91	-14	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
310	-91	-14	Min.	0.00	-7.57	14	-7.57	6	0.00	4	-29.94	2	0.00	10	0.00	2
310	-91	-14	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
311	-15	-92	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
311	-15	-92	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
311	-15	-92	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
311	-15	-92	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
311	-93	-15	Max	0.00	7.57	10	7.57	2	0.00	8	-29.94	2	0.00	10	0.00	2
311	-93	-15	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
311	-93	-15	Min.	0.00	-7.57	14	-7.57	6	0.00	2	-29.94	2	0.00	14	0.00	2
311	-93	-15	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
312	-16	-98	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
312	-16	-98	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
312	-16	-98	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
312	-16	-98	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
312	-94	-16	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	10	0.00	2
312	-94	-16	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
312	-94	-16	Min.	0.00	-7.57	14	-7.57	6	0.00	8	-29.94	2	0.00	14	0.00	2
312	-94	-16	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
313	-17	-97	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
313	-17	-97	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
313	-17	-97	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
313	-17	-97	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
313	-42	-17	Max	0.00	7.57	10	7.57	2	0.00	8	-29.94	2	0.00	10	0.00	2
313	-42	-17	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
313	-42	-17	Min.	0.00	-7.57	14	-7.57	6	0.00	2	-29.94	2	0.00	14	0.00	2
313	-42	-17	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
314	-18	-43	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
314	-18	-43	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
314	-18	-43	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
314	-18	-43	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
314	-44	-18	Max	0.00	7.57	10	7.57	2	0.00	4	-29.94	2	0.00	10	0.00	2
314	-44	-18	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
314	-44	-18	Min.	0.00	-7.57	14	-7.57	6	0.00	6	-29.94	2	0.00	14	0.00	2
314	-44	-18	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
315	-19	-45	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
315	-19	-45	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
315	-19	-45	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
315	-19	-45	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
315	-58	-19	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	16	0.00	2
315	-58	-19	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
315	-58	-19	Min.	0.00	-7.57	14	-7.57	6	0.00	8	-29.94	2	0.00	10	0.00	2
315	-58	-19	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
316	-20	-63	Max	0.00	5.04	14	5.04	6	7.55	2	94.25	2	-81.91	2	0.00	2
316	-20	-63	Max	150.00	5.04	14	5.04	6	0.00	2	14.97	2	0.00	2	0.00	2
316	-20	-63	Min.	0.00	-5.04	10	-5.04	2	-7.55	6	94.25	2	-81.91	2	0.00	2
316	-20	-63	Min.	150.00	-5.04	10	-5.04	2	0.00	6	14.97	2	0.00	2	0.00	2
316	-65	-20	Max	0.00	5.04	10	5.04	2	0.00	8	-14.97	2	0.00	16	0.00	2
316	-65	-20	Max	150.00	5.04	10	5.04	2	7.55	2	-94.25	2	-81.91	2	0.00	2
316	-65	-20	Min.	0.00	-5.04	14	-5.04	6	0.00	2	-14.97	2	0.00	10	0.00	2
316	-65	-20	Min.	150.00	-5.04	14	-5.04	6	-7.55	6	-94.25	2	-81.91	2	0.00	2
317	-21	-51	Max	0.00	5.04	14	5.04	6	7.55	2	94.25	2	-81.91	2	0.00	2
317	-21	-51	Max	150.00	5.04	14	5.04	6	0.00	2	14.97	2	0.00	2	0.00	2
317	-21	-51	Min.	0.00	-5.04	10	-5.04	2	-7.55	6	94.25	2	-81.91	2	0.00	2
317	-21	-51	Min.	150.00	-5.04	10	-5.04	2	0.00	6	14.97	2	0.00	2	0.00	2
317	-50	-21	Max	0.00	5.04	10	5.04	2	0.00	2	-14.97	2	0.00	2	0.00	2
317	-50	-21	Max	150.00	5.04	10	5.04	2	7.55	2	-94.25	2	-81.91	2	0.00	2
317	-50	-21	Min.	0.00	-5.04	14	-5.04	6	0.00	2	-14.97	2	0.00	2	0.00	2
317	-50	-21	Min.	150.00	-5.04	14	-5.04	6	-7.55	6	-94.25	2	-81.91	2	0.00	2
318	-22	-53	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	10
318	-22	-53	Max	150.00	7.57	14	7.57	6	0.00	2	29.94	2	0.00	2	0.00	10
318	-22	-53	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	14
318	-22	-53	Min.	150.00	-7.57	10	-7.57	2	0.00	6	29.94	2	0.00	2	0.00	14
318	-52	-22	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	12	0.00	2
318	-52	-22	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
318	-52	-22	Min.	0.00	-7.57	14	-7.57	6	0.00	6	-29.94	2	0.00	14	0.00	2
318	-52	-22	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2

319	-23	-55	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
319	-23	-55	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
319	-23	-55	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
319	-23	-55	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
319	-54	-23	Max	0.00	7.57	10	7.57	2	0.00	14	-29.94	2	0.00	10	0.00	2
319	-54	-23	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
319	-54	-23	Min.	0.00	-7.57	14	-7.57	6	0.00	10	-29.94	2	0.00	14	0.00	2
319	-54	-23	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
320	-24	-57	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
320	-24	-57	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
320	-24	-57	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
320	-24	-57	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
320	-56	-24	Max	0.00	7.57	10	7.57	2	0.00	6	-29.94	2	0.00	2	0.00	2
320	-56	-24	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
320	-56	-24	Min.	0.00	-7.57	14	-7.57	6	0.00	2	-29.94	2	0.00	2	0.00	2
320	-56	-24	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
322	-25	-41	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
322	-25	-41	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
322	-25	-41	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
322	-25	-41	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
322	-64	-25	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	12	0.00	2
322	-64	-25	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
322	-64	-25	Min.	0.00	-7.57	14	-7.57	6	0.00	6	-29.94	2	0.00	14	0.00	2
322	-64	-25	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
323	-26	-77	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
323	-26	-77	Max	150.00	7.57	14	7.57	6	0.00	2	29.94	2	0.00	2	0.00	2
323	-26	-77	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
323	-26	-77	Min.	150.00	-7.57	10	-7.57	2	0.00	6	29.94	2	0.00	2	0.00	2
323	-76	-26	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	10	0.00	2
323	-76	-26	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
323	-76	-26	Min.	0.00	-7.57	14	-7.57	6	0.00	8	-29.94	2	0.00	14	0.00	2
323	-76	-26	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
324	-27	-79	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
324	-27	-79	Max	150.00	7.57	14	7.57	6	0.00	2	29.94	2	0.00	2	0.00	2
324	-27	-79	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
324	-27	-79	Min.	150.00	-7.57	10	-7.57	2	0.00	6	29.94	2	0.00	2	0.00	2
324	-78	-27	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	14	0.00	2
324	-78	-27	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
324	-78	-27	Min.	0.00	-7.57	14	-7.57	6	0.00	2	-29.94	2	0.00	10	0.00	2
324	-78	-27	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
325	-28	-81	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
325	-28	-81	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
325	-28	-81	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
325	-28	-81	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
325	-80	-28	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	16	0.00	2
325	-80	-28	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
325	-80	-28	Min.	0.00	-7.57	14	-7.57	6	0.00	6	-29.94	2	0.00	10	0.00	2
325	-80	-28	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
326	-29	-83	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
326	-29	-83	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
326	-29	-83	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
326	-29	-83	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
326	-82	-29	Max	0.00	7.57	10	7.57	2	0.00	6	-29.94	2	0.00	16	0.00	2
326	-82	-29	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
326	-82	-29	Min.	0.00	-7.57	14	-7.57	6	0.00	4	-29.94	2	0.00	10	0.00	2
326	-82	-29	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
327	-30	-85	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
327	-30	-85	Max	150.00	7.57	14	7.57	6	0.00	2	29.94	2	0.00	2	0.00	2
327	-30	-85	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
327	-30	-85	Min.	150.00	-7.57	10	-7.57	2	0.00	6	29.94	2	0.00	2	0.00	2
327	-84	-30	Max	0.00	7.57	10	7.57	2	0.00	14	-29.94	2	0.00	10	0.00	2
327	-84	-30	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
327	-84	-30	Min.	0.00	-7.57	14	-7.57	6	0.00	10	-29.94	2	0.00	14	0.00	2
327	-84	-30	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
329	-32	-86	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
329	-32	-86	Max	150.00	7.57	14	7.57	6	0.00	2	29.94	2	0.00	2	0.00	2
329	-32	-86	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
329	-32	-86	Min.	150.00	-7.57	10	-7.57	2	0.00	6	29.94	2	0.00	2	0.00	2
329	-87	-32	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	14	0.00	2
329	-87	-32	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
329	-87	-32	Min.	0.00	-7.57	14	-7.57	6	0.00	6	-29.94	2	0.00	10	0.00	2
329	-87	-32	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
330	-33	-89	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
330	-33	-89	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
330	-33	-89	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
330	-33	-89	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2

330	-88	-33	Max	0.00	7.57	10	7.57	2	0.00	4	-29.94	2	0.00	16	0.00	2
330	-88	-33	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
330	-88	-33	Min.	0.00	-7.57	14	-7.57	6	0.00	6	-29.94	2	0.00	10	0.00	2
330	-88	-33	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
331	-34	-61	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
331	-34	-61	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
331	-34	-61	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
331	-34	-61	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
331	-62	-34	Max	0.00	7.57	10	7.57	2	0.00	8	-29.94	2	0.00	10	0.00	2
331	-62	-34	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
331	-62	-34	Min.	0.00	-7.57	14	-7.57	6	0.00	2	-29.94	2	0.00	16	0.00	2
331	-62	-34	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
332	-35	-102	Max	0.00	7.57	14	7.57	6	11.36	2	134.33	2	-123.20	2	0.00	2
332	-35	-102	Max	150.00	7.57	14	7.57	6	0.00	6	29.94	2	0.00	2	0.00	2
332	-35	-102	Min.	0.00	-7.57	10	-7.57	2	-11.36	6	134.33	2	-123.20	2	0.00	2
332	-35	-102	Min.	150.00	-7.57	10	-7.57	2	0.00	2	29.94	2	0.00	2	0.00	2
332	-101	-35	Max	0.00	7.57	10	7.57	2	0.00	2	-29.94	2	0.00	14	0.00	2
332	-101	-35	Max	150.00	7.57	10	7.57	2	11.36	2	-134.33	2	-123.20	2	0.00	2
332	-101	-35	Min.	0.00	-7.57	14	-7.57	6	0.00	8	-29.94	2	0.00	10	0.00	2
332	-101	-35	Min.	150.00	-7.57	14	-7.57	6	-11.36	6	-134.33	2	-123.20	2	0.00	2
333	-37	-103	Max	0.00	5.04	14	5.04	6	7.55	2	94.25	2	-81.91	2	0.00	2
333	-37	-103	Max	150.00	5.04	14	5.04	6	0.00	2	14.97	2	0.00	14	0.00	2
333	-37	-103	Min.	0.00	-5.04	10	-5.04	2	-7.55	6	94.25	2	-81.91	2	0.00	2
333	-37	-103	Min.	150.00	-5.04	10	-5.04	2	0.00	6	14.97	2	0.00	10	0.00	2
333	-104	-37	Max	0.00	5.04	10	5.04	2	0.00	8	-14.97	2	0.00	16	0.00	2
333	-104	-37	Max	150.00	5.04	10	5.04	2	7.55	2	-94.25	2	-81.91	2	0.00	2
333	-104	-37	Min.	0.00	-5.04	14	-5.04	6	0.00	2	-14.97	2	0.00	10	0.00	2
333	-104	-37	Min.	150.00	-5.04	14	-5.04	6	-7.55	6	-94.25	2	-81.91	2	0.00	2

Tipo di combinazione di carico: SLU

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-1415.88	21	175.04	29	-58.19	21	0.00	29	0.00	21	0.00	21
1	1	-5	Max	328.50	-1106.40	21	175.04	29	388.86	29	0.00	29	0.00	21	0.00	21
1	1	-5	Min.	0.00	-3451.54	29	54.75	21	-186.15	29	-0.00	21	-0.00	29	0.00	29
1	1	-5	Min.	328.50	-3142.05	29	54.75	21	121.67	21	-0.00	21	-0.00	29	0.00	29
2	2	-10	Max	0.00	-2703.40	21	204.25	29	-74.50	21	0.00	28	0.00	21	0.00	21
2	2	-10	Max	328.50	-2393.92	21	204.25	29	452.47	29	0.00	28	0.00	21	0.00	21
2	2	-10	Min.	0.00	-7452.92	29	69.60	21	-218.50	29	-0.00	21	-0.00	29	0.00	29
2	2	-10	Min.	328.50	-7143.43	29	69.60	21	154.14	21	-0.00	21	-0.00	29	0.00	29
3	3	203	Max	0.00	-2793.20	21	-56.48	21	183.46	29	0.00	28	0.00	21	0.00	28
3	3	203	Max	328.50	-2483.71	21	-56.48	21	-123.98	21	0.00	28	0.00	21	0.00	28
3	3	203	Min.	0.00	-7700.60	29	-168.27	29	61.57	21	-0.00	21	-0.00	29	0.00	21
3	3	203	Min.	328.50	-7391.11	29	-168.27	29	-369.29	29	-0.00	21	-0.00	29	0.00	21
4	4	204	Max	0.00	-2467.33	21	-0.00	21	0.00	21	0.00	21	0.00	29	0.00	21
4	4	204	Max	328.50	-2157.85	21	-0.00	21	0.00	21	0.00	21	0.00	29	0.00	21
4	4	204	Min.	0.00	-6367.78	29	-0.00	29	0.00	29	-0.00	29	0.00	21	0.00	29
4	4	204	Min.	328.50	-6058.29	29	-0.00	29	0.00	29	-0.00	29	0.00	21	0.00	29
5	5	205	Max	0.00	-2793.20	21	-56.48	21	183.46	29	0.00	21	0.00	29	0.00	21
5	5	205	Max	328.50	-2483.71	21	-56.48	21	-123.97	21	0.00	21	0.00	29	0.00	21
5	5	205	Min.	0.00	-7700.60	29	-168.26	29	61.57	21	-0.00	28	0.00	21	0.00	28
5	5	205	Min.	328.50	-7391.11	29	-168.26	29	-369.28	29	-0.00	28	0.00	21	0.00	28
6	6	-31	Max	0.00	-2703.40	21	204.25	29	-74.50	21	0.00	21	0.00	29	0.00	29
6	6	-31	Max	328.50	-2393.92	21	204.25	29	452.46	29	0.00	21	0.00	29	0.00	29
6	6	-31	Min.	0.00	-7452.91	29	69.60	21	-218.50	29	-0.00	28	0.00	21	0.00	21
6	6	-31	Min.	328.50	-7143.43	29	69.60	21	154.13	21	-0.00	28	0.00	21	0.00	21
7	7	-36	Max	0.00	-1415.88	21	175.04	29	-58.19	21	0.00	21	0.00	29	0.00	29
7	7	-36	Max	328.50	-1106.39	21	175.04	29	388.85	29	0.00	21	0.00	29	0.00	29
7	7	-36	Min.	0.00	-3451.53	29	54.75	21	-186.15	29	-0.00	29	0.00	21	0.00	21
7	7	-36	Min.	328.50	-3142.04	29	54.75	21	121.67	21	-0.00	29	0.00	21	0.00	21
201	-5	-4	Max	0.00	0.00	17	0.00	21	0.00	28	820.16	29	-229.88	21	0.00	21
201	-5	-4	Max	80.60	0.00	17	0.00	21	0.00	21	724.75	29	0.00	29	0.00	21
201	-5	-4	Min.	0.00	0.00	17	0.00	28	0.00	21	332.92	21	-622.60	29	0.00	29
201	-5	-4	Min.	80.60	0.00	17	0.00	28	0.00	28	237.51	21	0.00	21	0.00	29
201	-6	-5	Max	0.00	-54.75	21	0.00	29	0.00	21	-710.33	21	210.27	29	0.00	29
201	-6	-5	Max	53.34	-54.75	21	0.00	29	0.00	28	-773.47	21	-351.55	21	0.00	29
201	-6	-5	Min.	0.00	-175.04	29	-0.00	21	0.00	29	-2258.74	29	44.20	21	0.00	21
201	-6	-5	Min.	53.34	-175.04	29	-0.00	21	0.00	21	-2321.89	29	-1011.45	29	0.00	21
201	-7	-6	Max	0.00	-54.75	21	0.00	29	0.00	21	-217.58	21	1376.63	29	0.00	29
201	-7	-6	Max	133.94	-54.75	21	0.00	29	0.00	21	-376.14	21	210.27	29	0.00	29
201	-7	-6	Min.	0.00	-175.04	29	0.00	21	0.00	29	-791.51	29	441.83	21	0.00	21
201	-7	-6	Min.	133.94	-175.04	29	0.00	21	0.00	29	-950.07	29	44.20	21	0.00	21
201	-8	-7	Max	0.00	-54.75	21	0.00	29	0.00	21	675.72	29	577.74	29	0.00	29
201	-8	-7	Max	133.94	-54.75	21	0.00	29	0.00	21	517.16	29	1376.63	29	0.00	29
201	-8	-7	Min.	0.00	-175.04	29	0.00	21	0.00	29	275.16	21	179.46	21	0.00	21

201	-8	-7	Min.	133.94	-175.04	29	0.00	21	0.00	29	116.61	21	441.83	21	0.00	21
201	-9	-8	Max	0.00	-54.75	21	0.00	22	0.00	21	2142.95	29	-742.92	21	0.00	21
201	-9	-8	Max	133.94	-54.75	21	0.00	22	0.00	21	1984.39	29	577.73	29	0.00	21
201	-9	-8	Min.	0.00	-175.04	29	0.00	28	0.00	29	767.91	21	-2186.41	29	0.00	29
201	-9	-8	Min.	133.94	-175.04	29	0.00	28	0.00	29	609.35	21	179.45	21	0.00	29
201	-10	-9	Max	0.00	-54.75	21	0.00	21	0.00	21	3504.69	29	-1248.87	21	0.00	21
201	-10	-9	Max	44.83	-54.75	21	0.00	21	0.00	21	3451.62	29	-742.92	21	0.00	21
201	-10	-9	Min.	0.00	-175.04	29	0.00	28	0.00	29	1155.16	21	-3745.63	29	-0.00	29
201	-10	-9	Min.	44.83	-175.04	29	0.00	28	0.00	29	1102.10	21	-2186.41	29	-0.00	29
202	-11	-10	Max	0.00	-124.35	21	0.00	28	0.00	21	-1133.26	21	-346.11	21	0.00	29
202	-11	-10	Max	89.11	-124.35	21	0.00	28	0.00	21	-1238.75	21	-1403.01	21	0.00	29
202	-11	-10	Min.	0.00	-379.30	29	-0.00	21	0.00	29	-3533.24	29	-1002.48	29	0.00	21
202	-11	-10	Min.	89.11	-379.30	29	-0.00	21	0.00	29	-3638.74	29	-4198.10	29	0.00	21
202	-12	-11	Max	0.00	-124.35	21	0.00	28	0.00	21	-640.51	21	1870.99	29	0.00	29
202	-12	-11	Max	133.94	-124.35	21	0.00	28	0.00	21	-799.07	21	-346.11	21	0.00	29
202	-12	-11	Min.	0.00	-379.30	29	-0.00	21	0.00	29	-2066.01	29	618.00	21	0.00	21
202	-12	-11	Min.	133.94	-379.30	29	-0.00	21	0.00	29	-2224.57	29	-1002.48	29	0.00	21
202	-13	-12	Max	0.00	-124.35	21	0.00	28	0.00	21	-147.77	21	2779.21	29	0.00	29
202	-13	-12	Max	133.94	-124.35	21	0.00	28	0.00	21	-306.33	21	1870.99	29	0.00	29
202	-13	-12	Min.	0.00	-379.30	29	0.00	22	0.00	29	-598.78	29	922.12	21	0.00	21
202	-13	-12	Min.	133.94	-379.30	29	0.00	22	0.00	29	-757.34	29	618.00	21	0.00	21
202	-14	-13	Max	0.00	-124.35	21	0.00	21	0.00	21	868.45	29	1722.18	29	0.00	21
202	-14	-13	Max	133.94	-124.35	21	0.00	21	0.00	21	709.89	29	2779.21	29	0.00	21
202	-14	-13	Min.	0.00	-379.30	29	0.00	29	0.00	29	344.98	21	566.24	21	0.00	29
202	-14	-13	Min.	133.94	-379.30	29	0.00	29	0.00	29	186.42	21	922.12	21	0.00	29
202	-15	-14	Max	0.00	-124.35	21	0.00	21	0.00	21	2335.68	29	-449.64	21	0.00	21
202	-15	-14	Max	133.94	-124.35	21	0.00	21	0.00	21	2177.12	29	1722.18	29	0.00	21
202	-15	-14	Min.	0.00	-379.30	29	-0.00	28	0.00	29	837.72	21	-1300.10	29	0.00	29
202	-15	-14	Min.	133.94	-379.30	29	-0.00	28	0.00	29	679.16	21	566.24	21	0.00	29
202	203	-15	Max	0.00	-124.35	21	0.00	21	0.00	28	3744.63	29	-1484.90	21	0.00	21
202	203	-15	Max	84.71	-124.35	21	0.00	21	0.00	21	3644.35	29	-449.64	21	0.00	21
202	203	-15	Min.	0.00	-379.30	29	-0.00	28	0.00	22	1272.19	21	-4429.89	29	-0.00	29
202	203	-15	Min.	84.71	-379.30	29	-0.00	28	0.00	29	1171.91	21	-1300.12	29	-0.00	29
203	-16	203	Max	0.00	-67.87	21	0.00	28	0.00	28	-1153.24	21	-778.83	21	0.00	29
203	-16	203	Max	49.23	-67.87	21	0.00	28	0.00	28	-1211.52	21	-1360.90	21	0.00	29
203	-16	203	Min.	0.00	-211.03	29	-0.00	21	0.00	22	-3588.20	29	-2279.78	29	0.00	21
203	-16	203	Min.	49.23	-211.03	29	-0.00	21	0.00	22	-3646.48	29	-4060.54	29	0.00	21
203	-17	-16	Max	0.00	-67.87	21	0.00	28	0.00	21	-660.50	21	667.24	29	0.00	29
203	-17	-16	Max	133.94	-67.87	21	0.00	28	0.00	28	-819.06	21	-778.86	21	0.00	29
203	-17	-16	Min.	0.00	-211.03	29	-0.00	22	0.00	29	-2120.97	29	212.02	21	0.00	21
203	-17	-16	Min.	133.94	-211.03	29	-0.00	22	0.00	22	-2279.53	29	-2279.85	29	0.00	21
203	-18	-17	Max	0.00	-67.87	21	0.00	21	0.00	21	-167.76	21	1649.05	29	0.00	29
203	-18	-17	Max	133.94	-67.87	21	0.00	21	0.00	21	-326.32	21	667.22	29	0.00	29
203	-18	-17	Min.	0.00	-211.03	29	-0.00	29	0.00	28	-653.75	29	542.90	21	0.00	21
203	-18	-17	Min.	133.94	-211.03	29	-0.00	29	0.00	29	-812.31	29	212.01	21	0.00	21
203	-19	-18	Max	0.00	-67.87	21	0.00	21	0.00	29	813.49	29	665.58	29	0.00	21
203	-19	-18	Max	133.94	-67.87	21	0.00	21	0.00	21	654.93	29	1649.01	29	0.00	21
203	-19	-18	Min.	0.00	-211.03	29	-0.00	29	0.00	21	325.00	21	213.77	21	0.00	29
203	-19	-18	Min.	133.94	-211.03	29	-0.00	29	0.00	28	166.44	21	542.89	21	0.00	29
203	-20	-19	Max	0.00	-67.87	21	0.00	21	0.00	29	2280.72	29	-775.33	21	0.00	21
203	-20	-19	Max	133.94	-67.87	21	0.00	21	0.00	29	2122.16	29	665.64	29	0.00	21
203	-20	-19	Min.	0.00	-211.03	29	-0.00	29	0.00	21	817.74	21	-2283.03	29	-0.00	29
203	-20	-19	Min.	133.94	-211.03	29	-0.00	29	0.00	21	659.18	21	213.79	21	-0.00	29
203	204	-20	Max	0.00	-67.87	21	0.00	21	0.00	29	3029.15	29	-988.75	21	0.00	21
203	204	-20	Max	20.00	-67.87	21	0.00	21	0.00	29	3005.47	29	-775.33	21	0.00	21
203	204	-20	Min.	0.00	-211.03	29	-0.00	29	0.00	21	1078.92	21	-2886.49	29	-0.00	29
203	204	-20	Min.	20.00	-211.03	29	-0.00	29	0.00	21	1055.25	21	-2283.03	29	-0.00	29
204	204	-21	Max	0.00	-67.87	21	0.00	29	0.00	21	3029.15	29	-988.75	21	0.00	29
204	204	-21	Max	20.00	-67.87	21	0.00	29	0.00	21	3005.47	29	-775.33	21	0.00	29
204	204	-21	Min.	0.00	-211.03	29	-0.00	21	0.00	29	1078.92	21	-2886.49	29	0.00	21
204	204	-21	Min.	20.00	-211.03	29	-0.00	21	0.00	29	1055.25	21	-2283.03	29	0.00	21
204	-21	-22	Max	0.00	-67.87	21	0.00	29	0.00	21	2280.72	29	-775.33	21	0.00	29
204	-21	-22	Max	133.94	-67.87	21	0.00	29	0.00	21	2122.16	29	665.65	29	0.00	29
204	-21	-22	Min.	0.00	-211.03	29	-0.00	21	0.00	29	817.74	21	-2283.03	29	0.00	21
204	-21	-22	Min.	133.94	-211.03	29	-0.00	21	0.00	29	659.18	21	213.79	21	0.00	21
204	-22	-23	Max	0.00	-67.87	21	0.00	29	0.00	21	813.49	29	665.58	29	0.00	29
204	-22	-23	Max	133.94	-67.87	21	0.00	29	0.00	28	654.93	29	1649.01	29	0.00	29
204	-22	-23	Min.	0.00	-211.03	29	0.00	21	0.00	29	325.00	21	213.77	21	0.00	21
204	-22	-23	Min.	133.94	-211.03	29	0.00	21	0.00	17	166.44	21	542.89	21	0.00	21
204	-23	-24	Max	0.00	-67.87	21	0.00	22	0.00	28	-167.76	21	1649.06	29	0.00	21
204	-23	-24	Max	133.94	-67.87	21	0.00	22	0.00	29	-326.31	21	667.22	29	0.00	21
204	-23	-24	Min.	0.00	-211.03	29	0.00	28	0.00	17	-653.74	29	542.90	21	0.00	29
204	-23	-24	Min.	133.94	-211.03	29	0.00	28	0.00	21	-812.30	29	212.02	21	0.00	29
204	-24	-25	Max	0.00	-67.87	21	0.00	22	0.00	29	-660.50	21	667.25	29	0.00	21
204	-24	-25	Max	133.94	-67.87	21	0.00	22	0.00	22	-819.06	21	-778.86	21	0.00	21
204	-24	-25	Min.	0.00	-211.03	29	0.00	28	0.00	21	-2120.97	29	212.03	21	0.00	29

204	-24	-25	Min.	133.94	-211.03	29	0.00	28	0.00	28	-2279.53	29	-2279.83	29	0.00	29
204	-25	205	Max	0.00	-67.87	21	0.00	21	0.00	22	-1153.24	21	-778.83	21	0.00	21
204	-25	205	Max	49.23	-67.87	21	0.00	21	0.00	22	-1211.52	21	-1360.90	21	0.00	21
204	-25	205	Min.	0.00	-211.03	29	0.00	28	0.00	28	-3588.20	29	-2279.77	29	-0.00	29
204	-25	205	Min.	49.23	-211.03	29	0.00	28	0.00	28	-3646.48	29	-4060.52	29	-0.00	29
205	205	-26	Max	0.00	-124.35	21	0.00	28	0.00	22	3744.63	29	-1484.89	21	0.00	29
205	205	-26	Max	84.71	-124.35	21	0.00	28	0.00	29	3644.35	29	-449.63	21	0.00	29
205	205	-26	Min.	0.00	-379.29	29	-0.00	21	0.00	28	1272.19	21	-4429.86	29	0.00	21
205	205	-26	Min.	84.71	-379.29	29	-0.00	21	0.00	21	1171.91	21	-1300.08	29	0.00	21
205	-26	-27	Max	0.00	-124.35	21	0.00	28	0.00	29	2335.68	29	-449.69	21	0.00	29
205	-26	-27	Max	133.94	-124.35	21	0.00	28	0.00	29	2177.12	29	1722.04	29	0.00	29
205	-26	-27	Min.	0.00	-379.29	29	-0.00	21	0.00	21	837.73	21	-1300.25	29	0.00	21
205	-26	-27	Min.	133.94	-379.29	29	-0.00	21	0.00	21	679.17	21	566.20	21	0.00	21
205	-27	-28	Max	0.00	-124.35	21	0.00	29	0.00	29	868.45	29	1722.19	29	0.00	29
205	-27	-28	Max	133.94	-124.35	21	0.00	29	0.00	29	709.89	29	2779.23	29	0.00	29
205	-27	-28	Min.	0.00	-379.29	29	0.00	21	0.00	21	344.97	21	566.25	21	0.00	21
205	-27	-28	Min.	133.94	-379.29	29	0.00	21	0.00	21	186.41	21	922.13	21	0.00	21
205	-28	-29	Max	0.00	-124.35	21	0.00	22	0.00	29	-147.77	21	2779.20	29	0.00	21
205	-28	-29	Max	133.94	-124.35	21	0.00	22	0.00	29	-306.33	21	1870.99	29	0.00	21
205	-28	-29	Min.	0.00	-379.29	29	0.00	28	0.00	21	-598.78	29	922.12	21	0.00	29
205	-28	-29	Min.	133.94	-379.29	29	0.00	28	0.00	21	-757.34	29	618.01	21	0.00	29
205	-29	-30	Max	0.00	-124.35	21	0.00	21	0.00	29	-640.51	21	1871.01	29	0.00	21
205	-29	-30	Max	133.94	-124.35	21	0.00	21	0.00	29	-799.07	21	-346.09	21	0.00	21
205	-29	-30	Min.	0.00	-379.29	29	0.00	28	0.00	21	-2066.01	29	618.01	21	-0.00	29
205	-29	-30	Min.	133.94	-379.29	29	0.00	28	0.00	21	-2224.57	29	-1002.45	29	-0.00	29
205	-30	-31	Max	0.00	-124.35	21	0.00	21	0.00	29	-1133.27	21	-346.15	21	0.00	21
205	-30	-31	Max	89.11	-124.35	21	0.00	21	0.00	29	-1238.76	21	-1403.05	21	0.00	21
205	-30	-31	Min.	0.00	-379.29	29	0.00	28	0.00	21	-3533.25	29	-1002.61	29	-0.00	29
205	-30	-31	Min.	89.11	-379.29	29	0.00	28	0.00	21	-3638.74	29	-4198.22	29	-0.00	29
206	-31	-32	Max	0.00	-54.75	21	0.00	28	0.00	29	3504.69	29	-1248.87	21	0.00	29
206	-31	-32	Max	44.83	-54.75	21	0.00	28	0.00	29	3451.63	29	-742.91	21	0.00	29
206	-31	-32	Min.	0.00	-175.04	29	-0.00	21	0.00	21	1155.16	21	-3745.62	29	0.00	21
206	-31	-32	Min.	44.83	-175.04	29	-0.00	21	0.00	21	1102.10	21	-2186.39	29	0.00	21
206	-32	-33	Max	0.00	-54.75	21	0.00	28	0.00	29	2142.95	29	-742.90	21	0.00	29
206	-32	-33	Max	133.94	-54.75	21	0.00	28	0.00	29	1984.40	29	577.79	29	0.00	29
206	-32	-33	Min.	0.00	-175.04	29	-0.00	22	0.00	21	767.91	21	-2186.36	29	0.00	21
206	-32	-33	Min.	133.94	-175.04	29	-0.00	22	0.00	21	609.35	21	179.47	21	0.00	21
206	-33	-34	Max	0.00	-54.75	21	-0.00	21	0.00	29	675.73	29	577.73	29	0.00	21
206	-33	-34	Max	133.94	-54.75	21	-0.00	21	0.00	29	517.17	29	1376.63	29	0.00	21
206	-33	-34	Min.	0.00	-175.04	29	-0.00	29	0.00	21	275.17	21	179.45	21	0.00	29
206	-33	-34	Min.	133.94	-175.04	29	-0.00	29	0.00	21	116.61	21	441.83	21	0.00	29
206	-34	-35	Max	0.00	-54.75	21	0.00	21	0.00	29	-217.58	21	1376.62	29	0.00	21
206	-34	-35	Max	133.94	-54.75	21	0.00	21	0.00	29	-376.13	21	210.27	29	0.00	21
206	-34	-35	Min.	0.00	-175.04	29	-0.00	29	0.00	21	-791.50	29	441.82	21	0.00	29
206	-34	-35	Min.	133.94	-175.04	29	-0.00	29	0.00	21	-950.06	29	44.21	21	0.00	29
206	-35	-36	Max	0.00	-54.75	21	0.00	21	0.00	29	-710.33	21	210.20	29	0.00	21
206	-35	-36	Max	53.34	-54.75	21	0.00	21	0.00	21	-773.48	21	-351.57	21	0.00	21
206	-35	-36	Min.	0.00	-175.04	29	-0.00	29	0.00	21	-2258.74	29	44.18	21	-0.00	29
206	-35	-36	Min.	53.34	-175.04	29	-0.00	29	0.00	28	-2321.88	29	-1011.51	29	-0.00	29
206	-36	-37	Max	0.00	0.00	17	0.00	28	0.00	21	820.16	29	-229.88	21	0.00	29
206	-36	-37	Max	80.60	0.00	17	0.00	28	0.00	28	724.75	29	0.00	29	0.00	29
206	-36	-37	Min.	0.00	0.00	17	0.00	21	0.00	28	332.92	21	-622.60	29	0.00	21
206	-36	-37	Min.	80.60	0.00	17	0.00	21	0.00	21	237.51	21	0.00	21	0.00	21
302	-4	-47	Max	0.00	0.00	28	0.00	17	0.00	17	362.38	29	-102.60	21	0.00	17
302	-4	-47	Max	150.00	0.00	17	0.00	17	0.00	17	109.03	29	0.00	22	0.00	17
302	-4	-47	Min.	0.00	0.00	21	0.00	17	0.00	17	118.75	21	-353.55	29	0.00	17
302	-4	-47	Min.	150.00	0.00	21	0.00	17	0.00	17	18.05	21	0.00	28	0.00	17
302	-46	-4	Max	0.00	0.00	17	0.00	17	0.00	17	-18.05	21	0.00	21	0.00	17
302	-46	-4	Max	150.00	0.00	17	0.00	17	0.00	17	-118.75	21	-102.60	21	0.00	17
302	-46	-4	Min.	0.00	0.00	17	0.00	17	0.00	17	-109.03	29	0.00	29	0.00	17
302	-46	-4	Min.	150.00	0.00	17	0.00	17	0.00	17	-362.38	29	-353.55	29	0.00	17
303	-6	-48	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
303	-6	-48	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	28	0.00	17
303	-6	-48	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
303	-6	-48	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	17	0.00	17
303	-49	-6	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	22	0.00	17
303	-49	-6	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
303	-49	-6	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	28	0.00	17
303	-49	-6	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
304	-7	-96	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
304	-7	-96	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	28	0.00	17
304	-7	-96	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
304	-7	-96	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	21	0.00	17
304	-95	-7	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	28	0.00	17
304	-95	-7	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
304	-95	-7	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	22	0.00	17

314	-18	-43	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	21	0.00	17
314	-44	-18	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	21	0.00	17
314	-44	-18	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
314	-44	-18	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	29	0.00	17
314	-44	-18	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
315	-19	-45	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
315	-19	-45	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	28	0.00	17
315	-19	-45	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
315	-19	-45	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	21	0.00	17
315	-58	-19	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	22	0.00	17
315	-58	-19	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
315	-58	-19	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	28	0.00	17
315	-58	-19	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
316	-20	-63	Max	0.00	0.00	28	0.00	17	0.00	17	362.38	29	-102.60	21	0.00	17
316	-20	-63	Max	150.00	0.00	17	0.00	17	0.00	17	109.03	29	0.00	28	0.00	17
316	-20	-63	Min.	0.00	0.00	21	0.00	17	0.00	17	118.75	21	-353.55	29	0.00	17
316	-20	-63	Min.	150.00	0.00	21	0.00	17	0.00	17	18.05	21	0.00	22	0.00	17
316	-65	-20	Max	0.00	0.00	17	0.00	17	0.00	17	-18.05	21	0.00	21	0.00	17
316	-65	-20	Max	150.00	0.00	17	0.00	17	0.00	17	-118.75	21	-102.60	21	0.00	17
316	-65	-20	Min.	0.00	0.00	17	0.00	17	0.00	17	-109.03	29	0.00	28	0.00	17
316	-65	-20	Min.	150.00	0.00	17	0.00	17	0.00	17	-362.38	29	-353.55	29	0.00	17
317	-21	-51	Max	0.00	0.00	28	0.00	17	0.00	17	362.38	29	-102.60	21	0.00	17
317	-21	-51	Max	150.00	0.00	17	0.00	17	0.00	17	109.03	29	0.00	29	0.00	17
317	-21	-51	Min.	0.00	0.00	21	0.00	17	0.00	17	118.75	21	-353.55	29	0.00	17
317	-21	-51	Min.	150.00	0.00	21	0.00	17	0.00	17	18.05	21	0.00	21	0.00	17
317	-50	-21	Max	0.00	0.00	17	0.00	17	0.00	17	-18.05	21	0.00	22	0.00	17
317	-50	-21	Max	150.00	0.00	17	0.00	17	0.00	17	-118.75	21	-102.60	21	0.00	17
317	-50	-21	Min.	0.00	0.00	17	0.00	17	0.00	17	-109.03	29	0.00	28	0.00	17
317	-50	-21	Min.	150.00	0.00	17	0.00	17	0.00	17	-362.38	29	-353.55	29	0.00	17
318	-22	-53	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
318	-22	-53	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	22	0.00	17
318	-22	-53	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
318	-22	-53	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	28	0.00	17
318	-52	-22	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	28	0.00	17
318	-52	-22	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
318	-52	-22	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	22	0.00	17
318	-52	-22	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
319	-23	-55	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
319	-23	-55	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	22	0.00	17
319	-23	-55	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
319	-23	-55	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	28	0.00	17
319	-54	-23	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	21	0.00	17
319	-54	-23	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
319	-54	-23	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	29	0.00	17
319	-54	-23	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
320	-24	-57	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
320	-24	-57	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	29	0.00	17
320	-24	-57	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
320	-24	-57	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	21	0.00	17
320	-56	-24	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	21	0.00	17
320	-56	-24	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
320	-56	-24	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	29	0.00	17
320	-56	-24	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
322	-25	-41	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
322	-25	-41	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	29	0.00	17
322	-25	-41	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
322	-25	-41	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	21	0.00	17
322	-64	-25	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	22	0.00	17
322	-64	-25	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
322	-64	-25	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	28	0.00	17
322	-64	-25	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
323	-26	-77	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
323	-26	-77	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	22	0.00	17
323	-26	-77	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
323	-26	-77	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	28	0.00	17
323	-76	-26	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	28	0.00	17
323	-76	-26	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
323	-76	-26	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	22	0.00	17
323	-76	-26	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
324	-27	-79	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
324	-27	-79	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	21	0.00	17
324	-27	-79	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
324	-27	-79	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	17	0.00	17
324	-78	-27	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	28	0.00	17
324	-78	-27	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
324	-78	-27	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	22	0.00	17

324	-78	-27	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
325	-28	-81	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
325	-28	-81	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	22	0.00	17
325	-28	-81	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
325	-28	-81	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	28	0.00	17
325	-80	-28	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	21	0.00	17
325	-80	-28	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
325	-80	-28	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	17	0.00	17
325	-80	-28	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
326	-29	-83	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
326	-29	-83	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	29	0.00	17
326	-29	-83	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
326	-29	-83	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	21	0.00	17
326	-82	-29	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	21	0.00	17
326	-82	-29	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
326	-82	-29	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	28	0.00	17
326	-82	-29	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
327	-30	-85	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
327	-30	-85	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	22	0.00	17
327	-30	-85	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
327	-30	-85	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	28	0.00	17
327	-84	-30	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	21	0.00	17
327	-84	-30	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
327	-84	-30	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	28	0.00	17
327	-84	-30	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
329	-32	-86	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
329	-32	-86	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	21	0.00	17
329	-32	-86	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
329	-32	-86	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	21	0.00	17
329	-87	-32	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	22	0.00	17
329	-87	-32	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
329	-87	-32	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	28	0.00	17
329	-87	-32	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
330	-33	-89	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
330	-33	-89	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	21	0.00	17
330	-33	-89	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
330	-33	-89	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	21	0.00	17
330	-88	-33	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	29	0.00	17
330	-88	-33	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
330	-88	-33	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	21	0.00	17
330	-88	-33	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
331	-34	-61	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
331	-34	-61	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	21	0.00	17
331	-34	-61	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
331	-34	-61	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	17	0.00	17
331	-62	-34	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	21	0.00	17
331	-62	-34	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
331	-62	-34	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	17	0.00	17
331	-62	-34	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
332	-35	-102	Max	0.00	0.00	28	0.00	17	0.00	17	654.34	29	-152.40	21	0.00	17
332	-35	-102	Max	150.00	0.00	17	0.00	17	0.00	17	218.06	29	0.00	21	0.00	17
332	-35	-102	Min.	0.00	-0.00	21	0.00	17	0.00	17	167.09	21	-654.29	29	0.00	17
332	-35	-102	Min.	150.00	0.00	21	0.00	17	0.00	17	36.10	21	0.00	17	0.00	17
332	-101	-35	Max	0.00	0.00	17	0.00	17	0.00	17	-36.10	21	0.00	21	0.00	17
332	-101	-35	Max	150.00	0.00	17	0.00	17	0.00	17	-167.09	21	-152.40	21	0.00	17
332	-101	-35	Min.	0.00	0.00	17	0.00	17	0.00	17	-218.06	29	0.00	29	0.00	17
332	-101	-35	Min.	150.00	0.00	17	0.00	17	0.00	17	-654.34	29	-654.29	29	0.00	17
333	-37	-103	Max	0.00	0.00	28	0.00	17	0.00	17	362.38	29	-102.60	21	0.00	17
333	-37	-103	Max	150.00	0.00	17	0.00	17	0.00	17	109.03	29	0.00	21	0.00	17
333	-37	-103	Min.	0.00	0.00	21	0.00	17	0.00	17	118.75	21	-353.55	29	0.00	17
333	-37	-103	Min.	150.00	0.00	21	0.00	17	0.00	17	18.05	21	0.00	29	0.00	17
333	-104	-37	Max	0.00	0.00	17	0.00	17	0.00	17	-18.05	21	0.00	28	0.00	17
333	-104	-37	Max	150.00	0.00	17	0.00	17	0.00	17	-118.75	21	-102.61	21	0.00	17
333	-104	-37	Min.	0.00	0.00	17	0.00	17	0.00	17	-109.03	29	0.00	21	0.00	17
333	-104	-37	Min.	150.00	0.00	17	0.00	17	0.00	17	-362.38	29	-353.55	29	0.00	17

Tipo di combinazione di carico: SLE R

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-1047.71	23	119.86	31	-42.15	23	0.00	31	0.00	23	0.00	23
1	1	-5	Max	301.52					180.02	30			0.00	30		
1	1	-5	Max	328.50	-809.65	23	119.86	31	266.28	31	0.00	31	0.00	23	0.00	23
1	1	-5	Min.	0.00	-2404.82	31	39.67	23	-127.47	31	-0.00	23	-0.00	31	0.00	31
1	1	-5	Min.	301.52					180.02	30			0.00	30		
1	1	-5	Min.	328.50	-2166.75	31	39.67	23	88.15	23	-0.00	23	-0.00	31	0.00	31

2	2	-10	Max	0.00	-1982.88	23	140.57	31	-54.38	23	0.00	30	0.00	23	0.00	23
2	2	-10	Max	328.50	-1744.82	23	140.57	31	311.39	31	0.00	30	0.00	23	0.00	23
2	2	-10	Min.	0.00	-5149.23	31	50.80	23	-150.38	31	-0.00	23	-0.00	31	0.00	31
2	2	-10	Min.	328.50	-4911.16	31	50.80	23	112.50	23	-0.00	23	-0.00	31	0.00	31
3	3	203	Max	0.00	-2048.74	23	-41.17	23	126.14	31	0.00	30	0.00	23	0.00	30
3	3	203	Max	328.50	-1810.68	23	-41.17	23	-90.37	23	0.00	30	0.00	23	0.00	30
3	3	203	Min.	0.00	-5320.34	31	-115.70	31	44.88	23	-0.00	23	-0.00	31	0.00	23
3	3	203	Min.	328.50	-5082.28	31	-115.70	31	-253.92	31	-0.00	23	-0.00	31	0.00	23
4	4	204	Max	0.00	-1818.57	23	-0.00	23	0.00	23	0.00	23	0.00	31	0.00	23
4	4	204	Max	328.50	-1580.51	23	-0.00	23	0.00	23	0.00	23	0.00	31	0.00	23
4	4	204	Min.	0.00	-4418.87	31	-0.00	31	0.00	31	-0.00	31	0.00	23	0.00	31
4	4	204	Min.	328.50	-4180.80	31	-0.00	31	0.00	31	-0.00	31	0.00	23	0.00	31
5	5	205	Max	0.00	-2048.74	23	-41.17	23	126.14	31	0.00	23	0.00	31	0.00	23
5	5	205	Max	328.50	-1810.68	23	-41.17	23	-90.37	23	0.00	23	0.00	31	0.00	23
5	5	205	Min.	0.00	-5320.34	31	-115.69	31	44.88	23	0.00	30	0.00	23	0.00	30
5	5	205	Min.	328.50	-5082.28	31	-115.69	31	-253.91	31	0.00	30	0.00	23	0.00	30
6	6	-31	Max	0.00	-1982.89	23	140.57	31	-54.38	23	0.00	23	0.00	31	0.00	31
6	6	-31	Max	328.50	-1744.82	23	140.57	31	311.38	31	0.00	23	0.00	31	0.00	31
6	6	-31	Min.	0.00	-5149.23	31	50.80	23	-150.38	31	-0.00	30	0.00	23	0.00	23
6	6	-31	Min.	328.50	-4911.16	31	50.80	23	112.49	23	-0.00	30	0.00	23	0.00	23
7	7	-36	Max	0.00	-1047.71	23	119.86	31	-42.15	23	0.00	23	0.00	31	0.00	31
7	7	-36	Max	328.50	-809.64	23	119.86	31	266.27	31	0.00	23	0.00	31	0.00	31
7	7	-36	Min.	0.00	-2404.81	31	39.67	23	-127.46	31	-0.00	31	0.00	23	0.00	23
7	7	-36	Min.	328.50	-2166.75	31	39.67	23	88.15	23	-0.00	31	0.00	23	0.00	23
201	-5	-4	Max	0.00	0.00	18	0.00	23	0.00	30	571.01	31	-168.84	23	0.00	23
201	-5	-4	Max	80.60	0.00	18	0.00	23	0.00	23	497.61	31	0.00	31	0.00	23
201	-5	-4	Min.	0.00	0.00	18	0.00	30	0.00	23	246.18	23	-430.65	31	0.00	31
201	-5	-4	Min.	80.60	0.00	18	0.00	30	0.00	30	172.78	23	0.00	23	0.00	31
201	-6	-5	Max	0.00	-39.67	23	0.00	31	0.00	23	-514.89	23	141.33	31	0.00	31
201	-6	-5	Max	53.34	-39.67	23	0.00	31	0.00	30	-563.47	23	-256.99	23	0.00	31
201	-6	-5	Min.	0.00	-119.86	31	-0.00	23	0.00	31	-1547.17	31	30.62	23	0.00	23
201	-6	-5	Min.	53.34	-119.86	31	-0.00	23	0.00	23	-1595.74	31	-696.92	31	0.00	23
201	-7	-6	Max	0.00	-39.67	23	0.00	31	0.00	23	-155.69	23	944.04	31	0.00	31
201	-7	-6	Max	133.94	-39.67	23	0.00	31	0.00	23	-277.66	23	141.33	31	0.00	31
201	-7	-6	Min.	0.00	-119.86	31	0.00	23	0.00	31	-538.31	31	320.84	23	0.00	23
201	-7	-6	Min.	133.94	-119.86	31	0.00	23	0.00	31	-660.28	31	30.62	23	0.00	23
201	-8	-7	Max	0.00	-39.67	23	0.00	31	0.00	23	470.55	31	395.46	31	0.00	31
201	-8	-7	Max	133.94	-39.67	23	0.00	31	0.00	23	348.58	31	944.04	31	0.00	31
201	-8	-7	Min.	0.00	-119.86	31	0.00	23	0.00	31	203.51	23	129.94	23	0.00	23
201	-8	-7	Min.	133.94	-119.86	31	0.00	23	0.00	31	81.54	23	320.84	23	0.00	23
201	-9	-8	Max	0.00	-39.67	23	0.00	24	0.00	23	1479.41	31	-542.10	23	0.00	23
201	-9	-8	Max	133.94	-39.67	23	0.00	24	0.00	23	1357.44	31	395.46	31	0.00	23
201	-9	-8	Min.	0.00	-119.86	31	0.00	30	0.00	31	562.72	23	-1504.43	31	0.00	31
201	-9	-8	Min.	133.94	-119.86	31	0.00	30	0.00	31	440.75	23	129.94	23	0.00	31
201	-10	-9	Max	0.00	-39.67	23	0.00	23	0.00	23	2407.12	31	-909.86	23	0.00	23
201	-10	-9	Max	44.83	-39.67	23	0.00	23	0.00	23	2366.30	31	-542.10	23	0.00	23
201	-10	-9	Min.	0.00	-119.86	31	0.00	30	0.00	31	840.77	23	-2574.37	31	0.00	31
201	-10	-9	Min.	44.83	-119.86	31	0.00	30	0.00	31	799.95	23	-1504.43	31	0.00	31
202	-11	-10	Max	0.00	-90.47	23	0.00	30	0.00	23	-822.90	23	-252.88	23	0.00	31
202	-11	-10	Max	89.11	-90.47	23	0.00	30	0.00	23	-904.04	23	-1022.35	23	0.00	31
202	-11	-10	Min.	0.00	-260.43	31	-0.00	23	0.00	31	-2422.89	31	-690.46	31	0.00	23
202	-11	-10	Min.	89.11	-260.43	31	-0.00	23	0.00	31	-2504.03	31	-2885.75	31	0.00	23
202	-12	-11	Max	0.00	-90.47	23	0.00	30	0.00	23	-463.69	23	1285.21	31	0.00	31
202	-12	-11	Max	133.94	-90.47	23	0.00	30	0.00	23	-585.66	23	-252.88	23	0.00	31
202	-12	-11	Min.	0.00	-260.43	31	-0.00	23	0.00	31	-1414.03	31	449.89	23	0.00	23
202	-12	-11	Min.	133.94	-260.43	31	-0.00	23	0.00	31	-1536.00	31	-690.46	31	0.00	23
202	-13	-12	Max	0.00	-90.47	23	0.00	30	0.00	23	-104.49	23	1909.59	31	0.00	31
202	-13	-12	Max	133.94	-90.47	23	0.00	30	0.00	23	-226.46	23	1285.21	31	0.00	31
202	-13	-12	Min.	0.00	-260.43	31	0.00	24	0.00	31	-405.17	31	671.53	23	0.00	23
202	-13	-12	Min.	133.94	-260.43	31	0.00	24	0.00	31	-527.13	31	449.89	23	0.00	23
202	-14	-13	Max	0.00	-90.47	23	0.00	23	0.00	23	603.69	31	1182.67	31	0.00	23
202	-14	-13	Max	133.94	-90.47	23	0.00	23	0.00	23	481.72	31	1909.59	31	0.00	23
202	-14	-13	Min.	0.00	-260.43	31	0.00	31	0.00	31	254.71	23	412.05	23	0.00	31
202	-14	-13	Min.	133.94	-260.43	31	0.00	31	0.00	31	132.74	23	671.53	23	0.00	31
202	-15	-14	Max	0.00	-90.47	23	0.00	23	0.00	23	1612.55	31	-328.57	23	0.00	23
202	-15	-14	Max	133.94	-90.47	23	0.00	23	0.00	23	1490.58	31	1182.67	31	0.00	23
202	-15	-14	Min.	0.00	-260.43	31	0.00	30	0.00	31	613.92	23	-895.54	31	0.00	31
202	-15	-14	Min.	133.94	-260.43	31	0.00	30	0.00	31	491.95	23	412.05	23	0.00	31
202	203	-15	Max	0.00	-90.47	23	0.00	30	0.00	30	2576.59	31	-1082.30	23	0.00	23
202	203	-15	Max	84.71	-90.47	23	0.00	23	0.00	23	2499.44	31	-328.57	23	0.00	23
202	203	-15	Min.	0.00	-260.43	31	-0.00	30	0.00	24	928.29	23	-3045.62	31	-0.00	31
202	203	-15	Min.	84.71	-260.43	31	-0.00	30	0.00	31	851.15	23	-895.56	31	-0.00	31
203	-16	203	Max	0.00	-49.29	23	0.00	30	0.00	30	-837.55	23	-568.56	23	0.00	31
203	-16	203	Max	49.23	-49.29	23	0.00	30	0.00	30	-882.38	23	-991.91	23	0.00	31
203	-16	203	Min.	0.00	-144.73	31	-0.00	23	0.00	24	-2460.86	31	-1569.19	31	0.00	23
203	-16	203	Min.	49.23	-144.73	31	-0.00	23	0.00	24	-2505.69	31	-2791.67	31	0.00	23

203	-17	-16	Max	0.00	-49.29	23	0.00	30	0.00	23	-478.35	23	457.31	31	0.00	31
203	-17	-16	Max	133.94	-49.29	23	0.00	30	0.00	30	-600.32	23	-568.58	23	0.00	31
203	-17	-16	Min.	0.00	-144.73	31	-0.00	24	0.00	31	-1452.00	31	153.83	23	0.00	23
203	-17	-16	Min.	133.94	-144.73	31	-0.00	24	0.00	24	-1573.97	31	-1569.24	31	0.00	23
203	-18	-17	Max	0.00	-49.29	23	0.00	23	0.00	23	-119.15	23	1132.54	31	0.00	31
203	-18	-17	Max	133.94	-49.29	23	0.00	23	0.00	23	-241.12	23	457.29	31	0.00	31
203	-18	-17	Min.	0.00	-144.73	31	-0.00	31	0.00	30	-443.15	31	395.11	23	0.00	23
203	-18	-17	Min.	133.94	-144.73	31	-0.00	31	0.00	31	-565.12	31	153.82	23	0.00	23
203	-19	-18	Max	0.00	-49.29	23	0.00	23	0.00	31	565.72	31	456.45	31	0.00	23
203	-19	-18	Max	133.94	-49.29	23	0.00	23	0.00	23	443.75	31	1132.51	31	0.00	23
203	-19	-18	Min.	0.00	-144.73	31	-0.00	31	0.00	23	240.06	23	155.24	23	0.00	31
203	-19	-18	Min.	133.94	-144.73	31	-0.00	31	0.00	30	118.09	23	395.10	23	0.00	31
203	-20	-19	Max	0.00	-49.29	23	0.00	23	0.00	31	1574.58	31	-565.72	23	0.00	23
203	-20	-19	Max	133.94	-49.29	23	0.00	23	0.00	31	1452.61	31	456.49	31	0.00	23
203	-20	-19	Min.	0.00	-144.73	31	-0.00	31	0.00	23	599.26	23	-1570.86	31	0.00	31
203	-20	-19	Min.	133.94	-144.73	31	-0.00	31	0.00	23	477.29	23	155.26	23	0.00	31
203	204	-20	Max	0.00	-49.29	23	0.00	23	0.00	31	2090.40	31	-721.95	23	0.00	23
203	204	-20	Max	20.00	-49.29	23	0.00	23	0.00	31	2072.19	31	-565.72	23	0.00	23
203	204	-20	Min.	0.00	-144.73	31	-0.00	31	0.00	23	790.25	23	-1987.12	31	0.00	31
203	204	-20	Min.	20.00	-144.73	31	-0.00	31	0.00	23	772.04	23	-1570.86	31	0.00	31
204	204	-21	Max	0.00	-49.29	23	0.00	31	0.00	23	2090.40	31	-721.95	23	0.00	31
204	204	-21	Max	20.00	-49.29	23	0.00	31	0.00	23	2072.19	31	-565.72	23	0.00	31
204	204	-21	Min.	0.00	-144.73	31	-0.00	23	0.00	31	790.25	23	-1987.12	31	0.00	23
204	204	-21	Min.	20.00	-144.73	31	-0.00	23	0.00	31	772.04	23	-1570.86	31	0.00	23
204	-21	-22	Max	0.00	-49.29	23	0.00	31	0.00	23	1574.58	31	-565.72	23	0.00	31
204	-21	-22	Max	133.94	-49.29	23	0.00	31	0.00	23	1452.61	31	456.50	31	0.00	31
204	-21	-22	Min.	0.00	-144.73	31	-0.00	23	0.00	31	599.26	23	-1570.86	31	0.00	23
204	-21	-22	Min.	133.94	-144.73	31	-0.00	23	0.00	31	477.29	23	155.26	23	0.00	23
204	-22	-23	Max	0.00	-49.29	23	0.00	31	0.00	23	565.72	31	456.45	31	0.00	31
204	-22	-23	Max	133.94	-49.29	23	0.00	31	0.00	30	443.75	31	1132.51	31	0.00	31
204	-22	-23	Min.	0.00	-144.73	31	0.00	23	0.00	31	240.06	23	155.24	23	0.00	23
204	-22	-23	Min.	133.94	-144.73	31	0.00	23	0.00	18	118.09	23	395.10	23	0.00	23
204	-23	-24	Max	0.00	-49.29	23	0.00	24	0.00	30	-119.15	23	1132.54	31	0.00	23
204	-23	-24	Max	133.94	-49.29	23	0.00	24	0.00	31	-241.12	23	457.30	31	0.00	23
204	-23	-24	Min.	0.00	-144.73	31	0.00	30	0.00	18	-443.14	31	395.11	23	0.00	31
204	-23	-24	Min.	133.94	-144.73	31	0.00	30	0.00	23	-565.11	31	153.82	23	0.00	31
204	-24	-25	Max	0.00	-49.29	23	0.00	24	0.00	31	-478.35	23	457.31	31	0.00	23
204	-24	-25	Max	133.94	-49.29	23	0.00	24	0.00	24	-600.32	23	-568.57	23	0.00	23
204	-24	-25	Min.	0.00	-144.73	31	0.00	30	0.00	23	-1452.00	31	153.83	23	0.00	31
204	-24	-25	Min.	133.94	-144.73	31	0.00	30	0.00	30	-1573.97	31	-1569.23	31	0.00	31
204	-25	205	Max	0.00	-49.29	23	0.00	23	0.00	24	-837.55	23	-568.55	23	0.00	23
204	-25	205	Max	49.23	-49.29	23	0.00	23	0.00	24	-882.38	23	-991.90	23	0.00	23
204	-25	205	Min.	0.00	-144.73	31	0.00	30	0.00	30	-2460.86	31	-1569.18	31	-0.00	31
204	-25	205	Min.	49.23	-144.73	31	0.00	30	0.00	30	-2505.69	31	-2791.65	31	-0.00	31
205	205	-26	Max	0.00	-90.46	23	0.00	30	0.00	24	2576.59	31	-1082.29	23	0.00	31
205	205	-26	Max	84.71	-90.46	23	0.00	30	0.00	31	2499.45	31	-328.56	23	0.00	31
205	205	-26	Min.	0.00	-260.43	31	-0.00	23	0.00	30	928.29	23	-3045.60	31	0.00	23
205	205	-26	Min.	84.71	-260.43	31	-0.00	23	0.00	23	851.15	23	-895.53	31	0.00	23
205	-26	-27	Max	0.00	-90.46	23	0.00	30	0.00	31	1612.56	31	-328.61	23	0.00	31
205	-26	-27	Max	133.94	-90.46	23	0.00	30	0.00	31	1490.59	31	1182.57	31	0.00	31
205	-26	-27	Min.	0.00	-260.43	31	-0.00	23	0.00	23	613.92	23	-895.65	31	0.00	23
205	-26	-27	Min.	133.94	-260.43	31	-0.00	23	0.00	23	491.95	23	412.01	23	0.00	23
205	-27	-28	Max	0.00	-90.46	23	0.00	31	0.00	31	603.69	31	1182.68	31	0.00	31
205	-27	-28	Max	133.94	-90.46	23	0.00	31	0.00	31	481.73	31	1909.60	31	0.00	31
205	-27	-28	Min.	0.00	-260.43	31	0.00	23	0.00	23	254.71	23	412.05	23	0.00	23
205	-27	-28	Min.	133.94	-260.43	31	0.00	23	0.00	23	132.74	23	671.53	23	0.00	23
205	-28	-29	Max	0.00	-90.46	23	0.00	24	0.00	31	-104.49	23	1909.59	31	0.00	23
205	-28	-29	Max	133.94	-90.46	23	0.00	24	0.00	31	-226.46	23	1285.21	31	0.00	23
205	-28	-29	Min.	0.00	-260.43	31	0.00	30	0.00	23	-405.16	31	671.53	23	0.00	31
205	-28	-29	Min.	133.94	-260.43	31	0.00	30	0.00	23	-527.13	31	449.89	23	0.00	31
205	-29	-30	Max	0.00	-90.46	23	0.00	23	0.00	31	-463.69	23	1285.23	31	0.00	23
205	-29	-30	Max	133.94	-90.46	23	0.00	23	0.00	31	-585.66	23	-252.87	23	0.00	23
205	-29	-30	Min.	0.00	-260.43	31	0.00	30	0.00	23	-1414.02	31	449.90	23	0.00	31
205	-29	-30	Min.	133.94	-260.43	31	0.00	30	0.00	23	-1535.99	31	-690.44	31	0.00	31
205	-30	-31	Max	0.00	-90.46	23	0.00	23	0.00	31	-822.90	23	-252.91	23	0.00	23
205	-30	-31	Max	89.11	-90.46	23	0.00	23	0.00	31	-904.05	23	-1022.38	23	0.00	23
205	-30	-31	Min.	0.00	-260.43	31	0.00	30	0.00	23	-2422.89	31	-690.55	31	-0.00	31
205	-30	-31	Min.	89.11	-260.43	31	0.00	30	0.00	23	-2504.04	31	-2885.83	31	-0.00	31
206	-31	-32	Max	0.00	-39.67	23	0.00	30	0.00	31	2407.13	31	-909.86	23	0.00	31
206	-31	-32	Max	44.83	-39.67	23	0.00	30	0.00	31	2366.31	31	-542.10	23	0.00	31
206	-31	-32	Min.	0.00	-119.86	31	-0.00	23	0.00	23	840.77	23	-2574.36	31	0.00	23
206	-31	-32	Min.	44.83	-119.86	31	-0.00	23	0.00	23	799.95	23	-1504.41	31	0.00	23
206	-32	-33	Max	0.00	-39.67	23	0.00	30	0.00	31	1479.41	31	-542.09	23	0.00	31
206	-32	-33	Max	133.94	-39.67	23	0.00	30	0.00	31	1357.44	31	395.49	31	0.00	31
206	-32	-33	Min.	0.00	-119.86	31	-0.00	24	0.00	23	562.72	23	-1504.39	31	0.00	23
206	-32	-33	Min.	133.94	-119.86	31	-0.00	24	0.00	23	440.75	23	129.95	23	0.00	23

206	-33	-34	Max	0.00	-39.67	23	0.00	23	0.00	31	470.56	31	395.45	31	0.00	23
206	-33	-34	Max	133.94	-39.67	23	0.00	23	0.00	31	348.59	31	944.05	31	0.00	23
206	-33	-34	Min.	0.00	-119.86	31	-0.00	31	0.00	23	203.51	23	129.93	23	0.00	31
206	-33	-34	Min.	133.94	-119.86	31	-0.00	31	0.00	23	81.55	23	320.84	23	0.00	31
206	-34	-35	Max	0.00	-39.67	23	0.00	23	0.00	31	-155.69	23	944.04	31	0.00	23
206	-34	-35	Max	133.94	-39.67	23	0.00	23	0.00	31	-277.65	23	141.34	31	0.00	23
206	-34	-35	Min.	0.00	-119.86	31	-0.00	31	0.00	23	-538.30	31	320.84	23	0.00	31
206	-34	-35	Min.	133.94	-119.86	31	-0.00	31	0.00	23	-660.27	31	30.63	23	0.00	31
206	-35	-36	Max	0.00	-39.67	23	0.00	23	0.00	31	-514.90	23	141.29	31	0.00	23
206	-35	-36	Max	53.34	-39.67	23	0.00	23	0.00	23	-563.47	23	-257.01	23	0.00	23
206	-35	-36	Min.	0.00	-119.86	31	-0.00	31	0.00	23	-1547.17	31	30.61	23	-0.00	31
206	-35	-36	Min.	53.34	-119.86	31	-0.00	31	0.00	30	-1595.74	31	-696.97	31	-0.00	31
206	-36	-37	Max	0.00	0.00	18	0.00	30	0.00	23	571.01	31	-168.84	23	0.00	31
206	-36	-37	Max	80.60	0.00	18	0.00	30	0.00	30	497.61	31	0.00	31	0.00	31
206	-36	-37	Min.	0.00	0.00	18	0.00	23	0.00	30	246.18	23	-430.65	31	0.00	23
206	-36	-37	Min.	80.60	0.00	18	0.00	23	0.00	23	172.78	23	0.00	23	0.00	23
302	-4	-47	Max	0.00	0.00	30	0.00	18	0.00	18	248.81	31	-73.82	23	0.00	18
302	-4	-47	Max	150.00	0.00	18	0.00	18	0.00	18	72.69	31	0.00	24	0.00	18
302	-4	-47	Min.	0.00	0.00	23	0.00	18	0.00	18	86.39	23	-241.12	31	0.00	18
302	-4	-47	Min.	150.00	0.00	23	0.00	18	0.00	18	12.03	23	0.00	30	0.00	18
302	-46	-4	Max	0.00	0.00	18	0.00	18	0.00	18	-12.03	23	0.00	23	0.00	18
302	-46	-4	Max	150.00	0.00	18	0.00	18	0.00	18	-86.39	23	-73.82	23	0.00	18
302	-46	-4	Min.	0.00	0.00	18	0.00	18	0.00	18	-72.69	31	0.00	31	0.00	18
302	-46	-4	Min.	150.00	0.00	18	0.00	18	0.00	18	-248.81	31	-241.12	31	0.00	18
303	-6	-48	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
303	-6	-48	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
303	-6	-48	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
303	-6	-48	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	18	0.00	18
303	-49	-6	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	24	0.00	18
303	-49	-6	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
303	-49	-6	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	30	0.00	18
303	-49	-6	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
304	-7	-96	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
304	-7	-96	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
304	-7	-96	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
304	-7	-96	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	23	0.00	18
304	-95	-7	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	30	0.00	18
304	-95	-7	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
304	-95	-7	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	24	0.00	18
304	-95	-7	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
305	-8	-66	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
305	-8	-66	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
305	-8	-66	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
305	-8	-66	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	24	0.00	18
305	-67	-8	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	23	0.00	18
305	-67	-8	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
305	-67	-8	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	30	0.00	18
305	-67	-8	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
306	-9	-69	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
306	-9	-69	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
306	-9	-69	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
306	-9	-69	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	24	0.00	18
306	-68	-9	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	30	0.00	18
306	-68	-9	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
306	-68	-9	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	23	0.00	18
306	-68	-9	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
307	-11	-70	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
307	-11	-70	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
307	-11	-70	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
307	-11	-70	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	24	0.00	18
307	-71	-11	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	24	0.00	18
307	-71	-11	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
307	-71	-11	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	30	0.00	18
307	-71	-11	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
308	-12	-72	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
308	-12	-72	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
308	-12	-72	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
308	-12	-72	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	24	0.00	18
308	-73	-12	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	18	0.00	18
308	-73	-12	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
308	-73	-12	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	30	0.00	18
308	-73	-12	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
309	-13	-74	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
309	-13	-74	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
309	-13	-74	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
309	-13	-74	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	24	0.00	18



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309	-75	-13	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	23	0.00	18
309	-75	-13	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
309	-75	-13	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	18	0.00	18
309	-75	-13	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
310	-14	-90	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
310	-14	-90	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
310	-14	-90	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
310	-14	-90	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	24	0.00	18
310	-91	-14	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	18	0.00	18
310	-91	-14	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
310	-91	-14	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	30	0.00	18
310	-91	-14	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
311	-15	-92	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
311	-15	-92	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
311	-15	-92	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
311	-15	-92	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	24	0.00	18
311	-93	-15	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	30	0.00	18
311	-93	-15	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
311	-93	-15	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	24	0.00	18
311	-93	-15	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
312	-16	-98	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
312	-16	-98	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
312	-16	-98	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
312	-16	-98	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	23	0.00	18
312	-94	-16	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	18	0.00	18
312	-94	-16	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
312	-94	-16	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	23	0.00	18
312	-94	-16	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
313	-17	-97	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
313	-17	-97	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
313	-17	-97	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
313	-17	-97	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	23	0.00	18
313	-42	-17	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	24	0.00	18
313	-42	-17	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
313	-42	-17	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	30	0.00	18
313	-42	-17	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
314	-18	-43	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
314	-18	-43	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
314	-18	-43	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
314	-18	-43	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	23	0.00	18
314	-44	-18	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	23	0.00	18
314	-44	-18	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
314	-44	-18	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	31	0.00	18
314	-44	-18	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
315	-19	-45	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
315	-19	-45	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	30	0.00	18
315	-19	-45	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
315	-19	-45	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	23	0.00	18
315	-58	-19	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	24	0.00	18
315	-58	-19	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
315	-58	-19	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	30	0.00	18
315	-58	-19	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
316	-20	-63	Max	0.00	0.00	30	0.00	18	0.00	18	248.81	31	-73.82	23	0.00	18
316	-20	-63	Max	150.00	0.00	18	0.00	18	0.00	18	72.69	31	0.00	30	0.00	18
316	-20	-63	Min.	0.00	0.00	23	0.00	18	0.00	18	86.39	23	-241.12	31	0.00	18
316	-20	-63	Min.	150.00	0.00	23	0.00	18	0.00	18	12.03	23	0.00	24	0.00	18
316	-65	-20	Max	0.00	0.00	18	0.00	18	0.00	18	-12.03	23	0.00	23	0.00	18
316	-65	-20	Max	150.00	0.00	18	0.00	18	0.00	18	-86.39	23	-73.82	23	0.00	18
316	-65	-20	Min.	0.00	0.00	18	0.00	18	0.00	18	-72.69	31	0.00	30	0.00	18
316	-65	-20	Min.	150.00	0.00	18	0.00	18	0.00	18	-248.81	31	-241.12	31	0.00	18
317	-21	-51	Max	0.00	0.00	30	0.00	18	0.00	18	248.81	31	-73.82	23	0.00	18
317	-21	-51	Max	150.00	0.00	18	0.00	18	0.00	18	72.69	31	0.00	31	0.00	18
317	-21	-51	Min.	0.00	0.00	23	0.00	18	0.00	18	86.39	23	-241.12	31	0.00	18
317	-21	-51	Min.	150.00	0.00	23	0.00	18	0.00	18	12.03	23	0.00	23	0.00	18
317	-50	-21	Max	0.00	0.00	18	0.00	18	0.00	18	-12.03	23	0.00	24	0.00	18
317	-50	-21	Max	150.00	0.00	18	0.00	18	0.00	18	-86.39	23	-73.82	23	0.00	18
317	-50	-21	Min.	0.00	0.00	18	0.00	18	0.00	18	-72.69	31	0.00	30	0.00	18
317	-50	-21	Min.	150.00	0.00	18	0.00	18	0.00	18	-248.81	31	-241.12	31	0.00	18
318	-22	-53	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
318	-22	-53	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	24	0.00	18
318	-22	-53	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
318	-22	-53	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	30	0.00	18
318	-52	-22	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	30	0.00	18
318	-52	-22	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
318	-52	-22	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	24	0.00	18
318	-52	-22	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18

330	-88	-33	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	31	0.00	18
330	-88	-33	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
330	-88	-33	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	23	0.00	18
330	-88	-33	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
331	-34	-61	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
331	-34	-61	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	23	0.00	18
331	-34	-61	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
331	-34	-61	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	18	0.00	18
331	-62	-34	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	23	0.00	18
331	-62	-34	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
331	-62	-34	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	18	0.00	18
331	-62	-34	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
332	-35	-102	Max	0.00	0.00	30	0.00	18	0.00	18	443.45	31	-107.02	23	0.00	18
332	-35	-102	Max	150.00	0.00	18	0.00	18	0.00	18	145.37	31	0.00	23	0.00	18
332	-35	-102	Min.	0.00	0.00	23	0.00	18	0.00	18	118.62	23	-441.61	31	0.00	18
332	-35	-102	Min.	150.00	0.00	23	0.00	18	0.00	18	24.07	23	0.00	18	0.00	18
332	-101	-35	Max	0.00	0.00	18	0.00	18	0.00	18	-24.07	23	0.00	23	0.00	18
332	-101	-35	Max	150.00	0.00	18	0.00	18	0.00	18	-118.62	23	-107.02	23	0.00	18
332	-101	-35	Min.	0.00	0.00	18	0.00	18	0.00	18	-145.37	31	0.00	31	0.00	18
332	-101	-35	Min.	150.00	0.00	18	0.00	18	0.00	18	-443.45	31	-441.61	31	0.00	18
333	-37	-103	Max	0.00	0.00	30	0.00	18	0.00	18	248.81	31	-73.82	23	0.00	18
333	-37	-103	Max	150.00	0.00	18	0.00	18	0.00	18	72.69	31	0.00	23	0.00	18
333	-37	-103	Min.	0.00	0.00	23	0.00	18	0.00	18	86.39	23	-241.12	31	0.00	18
333	-37	-103	Min.	150.00	0.00	23	0.00	18	0.00	18	12.03	23	0.00	31	0.00	18
333	-104	-37	Max	0.00	0.00	18	0.00	18	0.00	18	-12.03	23	0.00	30	0.00	18
333	-104	-37	Max	150.00	0.00	18	0.00	18	0.00	18	-86.39	23	-73.82	23	0.00	18
333	-104	-37	Min.	0.00	0.00	18	0.00	18	0.00	18	-72.69	31	0.00	23	0.00	18
333	-104	-37	Min.	150.00	0.00	18	0.00	18	0.00	18	-248.81	31	-241.12	31	0.00	18

Tipo di combinazione di carico: SLE F

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-986.36	25	57.00	19	-38.30	25	0.00	19	0.00	25	0.00	25
1	1	-5	Max	328.50	-748.29	25	57.00	19	126.66	19	0.00	19	0.00	25	0.00	25
1	1	-5	Min.	0.00	-1341.11	19	36.04	25	-60.60	19	0.00	25	0.00	19	0.00	19
1	1	-5	Min.	328.50	-1103.04	19	36.04	25	80.10	25	0.00	25	0.00	19	0.00	19
2	2	-10	Max	0.00	-1839.73	25	70.21	19	-50.04	25	0.00	32	0.00	25	0.00	25
2	2	-10	Max	328.50	-1601.66	25	70.21	19	155.49	19	0.00	32	0.00	25	0.00	25
2	2	-10	Min.	0.00	-2667.42	19	46.74	25	-75.13	19	-0.00	25	0.00	19	0.00	19
2	2	-10	Min.	328.50	-2429.35	19	46.74	25	103.50	25	-0.00	25	0.00	19	0.00	19
3	3	203	Max	0.00	-1900.83	25	-37.80	25	62.45	19	0.00	32	0.00	25	0.00	32
3	3	203	Max	328.50	-1662.76	25	-37.80	25	-82.98	25	0.00	32	0.00	25	0.00	32
3	3	203	Min.	0.00	-2756.03	19	-57.28	19	41.21	25	-0.00	25	0.00	19	0.00	25
3	3	203	Min.	328.50	-2517.96	19	-57.28	19	-125.73	19	-0.00	25	0.00	19	0.00	25
4	4	204	Max	0.00	-1701.01	25	0.00	25	0.00	25	0.00	25	0.00	19	0.00	25
4	4	204	Max	328.50	-1462.94	25	0.00	25	0.00	25	0.00	25	0.00	19	0.00	25
4	4	204	Min.	0.00	-2380.73	19	-0.00	19	0.00	19	0.00	32	0.00	25	0.00	19
4	4	204	Min.	328.50	-2142.66	19	-0.00	19	0.00	19	0.00	32	0.00	25	0.00	19
5	5	205	Max	0.00	-1900.83	25	-37.80	25	62.45	19	0.00	25	0.00	19	0.00	25
5	5	205	Max	328.50	-1662.76	25	-37.80	25	-82.98	25	0.00	25	0.00	19	0.00	25
5	5	205	Min.	0.00	-2756.03	19	-57.28	19	41.21	25	0.00	32	0.00	25	0.00	32
5	5	205	Min.	328.50	-2517.96	19	-57.28	19	-125.73	19	0.00	32	0.00	25	0.00	32
6	6	-31	Max	0.00	-1839.73	25	70.20	19	-50.04	25	0.00	25	0.00	19	0.00	19
6	6	-31	Max	328.50	-1601.66	25	70.20	19	155.49	19	0.00	25	0.00	19	0.00	19
6	6	-31	Min.	0.00	-2667.41	19	46.74	25	-75.13	19	0.00	32	0.00	25	0.00	25
6	6	-31	Min.	328.50	-2429.35	19	46.74	25	103.50	25	0.00	32	0.00	25	0.00	25
7	7	-36	Max	0.00	-986.36	25	57.00	19	-38.30	25	0.00	25	0.00	19	0.00	19
7	7	-36	Max	328.50	-748.29	25	57.00	19	126.66	19	0.00	25	0.00	19	0.00	19
7	7	-36	Min.	0.00	-1341.10	19	36.04	25	-60.60	19	0.00	25	0.00	19	0.00	25
7	7	-36	Min.	328.50	-1103.04	19	36.04	25	80.10	25	0.00	19	0.00	19	0.00	25
201	-5	-4	Max	0.00	0.00	19	0.00	25	0.00	32	316.40	19	-157.00	25	0.00	25
201	-5	-4	Max	80.60	0.00	19	0.00	25	0.00	25	243.01	19	0.00	19	0.00	25
201	-5	-4	Min.	0.00	0.00	19	0.00	32	0.00	25	231.49	25	-225.44	19	0.00	19
201	-5	-4	Min.	80.60	0.00	19	0.00	32	0.00	32	158.10	25	0.00	25	0.00	19
201	-6	-5	Max	0.00	-36.04	25	0.00	19	0.00	25	-468.22	25	54.56	19	0.00	19
201	-6	-5	Max	53.34	-36.04	25	0.00	19	0.00	32	-516.80	25	-237.10	25	0.00	19
201	-6	-5	Min.	0.00	-57.00	19	0.00	25	0.00	19	-738.06	19	25.62	25	0.00	25
201	-6	-5	Min.	53.34	-57.00	19	0.00	25	0.00	25	-786.64	19	-352.10	19	0.00	25
201	-7	-6	Max	0.00	-36.04	25	0.00	19	0.00	25	-138.39	25	455.57	19	0.00	19
201	-7	-6	Max	133.94	-36.04	25	0.00	19	0.00	25	-260.36	25	54.56	19	0.00	19
201	-7	-6	Min.	0.00	-57.00	19	0.00	25	0.00	19	-238.41	19	292.67	25	0.00	25
201	-7	-6	Min.	133.94	-57.00	19	0.00	25	0.00	19	-360.38	19	25.62	25	0.00	25
201	-8	-7	Max	0.00	-36.04	25	0.00	19	0.00	25	261.24	19	187.34	19	0.00	19
201	-8	-7	Max	133.94	-36.04	25	0.00	19	0.00	25	139.28	19	455.57	19	0.00	19
201	-8	-7	Min.	0.00	-57.00	19	0.00	25	0.00	19	191.44	25	117.93	25	0.00	25

201	-8	-7	Min.	133.94	-57.00	19	0.00	25	0.00	19	69.47	25	292.67	25	0.00	25
201	-9	-8	Max	0.00	-36.04	25	0.00	19	0.00	25	760.90	19	-498.59	25	0.00	25
201	-9	-8	Max	133.94	-36.04	25	0.00	19	0.00	25	638.93	19	187.34	19	0.00	25
201	-9	-8	Min.	0.00	-57.00	19	0.00	32	0.00	19	521.27	25	-750.14	19	0.00	19
201	-9	-8	Min.	133.94	-57.00	19	0.00	32	0.00	19	399.30	25	117.93	25	0.00	19
201	-10	-9	Max	0.00	-36.04	25	0.00	25	0.00	25	1179.40	19	-834.60	25	0.00	25
201	-10	-9	Max	44.83	-36.04	25	0.00	25	0.00	25	1138.58	19	-498.59	25	0.00	25
201	-10	-9	Min.	0.00	-57.00	19	0.00	32	0.00	19	769.96	25	-1269.71	19	0.00	19
201	-10	-9	Min.	44.83	-57.00	19	0.00	32	0.00	19	729.13	25	-750.14	19	0.00	19
202	-11	-10	Max	0.00	-82.78	25	0.00	32	0.00	25	-750.56	25	-233.10	25	0.00	19
202	-11	-10	Max	89.11	-82.78	25	0.00	32	0.00	25	-831.71	25	-938.11	25	0.00	19
202	-11	-10	Min.	0.00	-127.21	19	0.00	25	0.00	19	-1168.80	19	-347.48	19	0.00	25
202	-11	-10	Min.	89.11	-127.21	19	0.00	25	0.00	19	-1249.95	19	-1425.20	19	0.00	25
202	-12	-11	Max	0.00	-82.78	25	0.00	32	0.00	25	-420.73	25	630.48	19	0.00	19
202	-12	-11	Max	133.94	-82.78	25	0.00	32	0.00	25	-542.70	25	-233.10	25	0.00	19
202	-12	-11	Min.	0.00	-127.21	19	0.00	25	0.00	19	-669.15	19	412.12	25	0.00	25
202	-12	-11	Min.	133.94	-127.21	19	0.00	25	0.00	19	-791.12	19	-347.48	19	0.00	25
202	-13	-12	Max	0.00	-82.78	25	0.00	32	0.00	25	-90.90	25	939.19	19	0.00	19
202	-13	-12	Max	133.94	-82.78	25	0.00	32	0.00	25	-212.86	25	630.48	19	0.00	19
202	-13	-12	Min.	0.00	-127.21	19	0.00	19	0.00	19	-169.49	19	615.56	25	0.00	25
202	-13	-12	Min.	133.94	-127.21	19	0.00	19	0.00	19	-291.46	19	412.12	25	0.00	25
202	-14	-13	Max	0.00	-82.78	25	0.00	25	0.00	25	330.16	19	578.65	19	0.00	25
202	-14	-13	Max	133.94	-82.78	25	0.00	25	0.00	25	208.19	19	939.19	19	0.00	25
202	-14	-13	Min.	0.00	-127.21	19	0.00	32	0.00	19	238.94	25	377.20	25	0.00	19
202	-14	-13	Min.	133.94	-127.21	19	0.00	32	0.00	19	116.97	25	615.56	25	0.00	19
202	-15	-14	Max	0.00	-82.78	25	0.00	25	0.00	25	829.81	19	-302.93	25	0.00	25
202	-15	-14	Max	133.94	-82.78	25	0.00	25	0.00	25	707.84	19	578.65	19	0.00	25
202	-15	-14	Min.	0.00	-127.21	19	0.00	32	0.00	19	568.77	25	-451.14	19	0.00	19
202	-15	-14	Min.	133.94	-127.21	19	0.00	32	0.00	19	446.80	25	377.20	25	0.00	19
202	203	-15	Max	0.00	-82.78	25	0.00	25	0.00	32	1284.64	19	-993.53	25	0.00	25
202	203	-15	Max	84.71	-82.78	25	0.00	25	0.00	25	1207.50	19	-302.94	25	0.00	25
202	203	-15	Min.	0.00	-127.21	19	0.00	32	0.00	19	853.77	25	-1506.75	19	0.00	19
202	203	-15	Min.	84.71	-127.21	19	0.00	32	0.00	19	776.63	25	-451.15	19	0.00	19
203	-16	203	Max	0.00	-44.98	25	0.00	32	0.00	32	-764.16	25	-523.32	25	0.00	19
203	-16	203	Max	49.23	-44.98	25	0.00	32	0.00	32	-808.99	25	-910.54	25	0.00	19
203	-16	203	Min.	0.00	-69.93	19	0.00	25	0.00	19	-1188.50	19	-784.88	19	0.00	25
203	-16	203	Min.	49.23	-69.93	19	0.00	25	0.00	19	-1233.33	19	-1381.00	19	0.00	25
203	-17	-16	Max	0.00	-44.98	25	0.00	32	0.00	25	-434.33	25	219.44	19	0.00	19
203	-17	-16	Max	133.94	-44.98	25	0.00	32	0.00	32	-556.30	25	-523.33	25	0.00	19
203	-17	-16	Min.	0.00	-69.93	19	0.00	19	0.00	19	-688.85	19	140.11	25	0.00	25
203	-17	-16	Min.	133.94	-69.93	19	0.00	19	0.00	19	-810.82	19	-784.91	19	0.00	25
203	-18	-17	Max	0.00	-44.98	25	0.00	25	0.00	25	-104.50	25	554.53	19	0.00	19
203	-18	-17	Max	133.94	-44.98	25	0.00	25	0.00	25	-226.47	25	219.43	19	0.00	19
203	-18	-17	Min.	0.00	-69.93	19	0.00	19	0.00	32	-189.20	19	361.76	25	0.00	25
203	-18	-17	Min.	133.94	-69.93	19	0.00	19	0.00	19	-311.17	19	140.10	25	0.00	25
203	-19	-18	Max	0.00	-44.98	25	0.00	25	0.00	19	310.46	19	220.36	19	0.00	25
203	-19	-18	Max	133.94	-44.98	25	0.00	25	0.00	25	188.49	19	554.52	19	0.00	25
203	-19	-18	Min.	0.00	-69.93	19	0.00	19	0.00	25	225.33	25	141.62	25	0.00	19
203	-19	-18	Min.	133.94	-69.93	19	0.00	19	0.00	32	103.36	25	361.76	25	0.00	19
203	-20	-19	Max	0.00	-44.98	25	0.00	25	0.00	19	810.11	19	-520.28	25	0.00	25
203	-20	-19	Max	133.94	-44.98	25	0.00	25	0.00	19	688.14	19	220.38	19	0.00	25
203	-20	-19	Min.	0.00	-69.93	19	0.00	19	0.00	25	555.16	25	-783.02	19	0.00	19
203	-20	-19	Min.	133.94	-69.93	19	0.00	19	0.00	25	433.19	25	141.64	25	0.00	19
203	204	-20	Max	0.00	-44.98	25	0.00	25	0.00	19	1071.33	19	-664.75	25	0.00	25
203	204	-20	Max	20.00	-44.98	25	0.00	25	0.00	19	1053.12	19	-520.28	25	0.00	25
203	204	-20	Min.	0.00	-69.93	19	0.00	32	0.00	25	731.47	25	-995.47	19	0.00	19
203	204	-20	Min.	20.00	-69.93	19	0.00	32	0.00	25	713.26	25	-783.02	19	0.00	19
204	204	-21	Max	0.00	-44.98	25	0.00	32	0.00	25	1071.33	19	-664.75	25	0.00	19
204	204	-21	Max	20.00	-44.98	25	0.00	32	0.00	25	1053.12	19	-520.28	25	0.00	19
204	204	-21	Min.	0.00	-69.93	19	0.00	25	0.00	19	731.47	25	-995.47	19	0.00	25
204	204	-21	Min.	20.00	-69.93	19	0.00	25	0.00	19	713.26	25	-783.02	19	0.00	25
204	-21	-22	Max	0.00	-44.98	25	0.00	19	0.00	25	810.11	19	-520.28	25	0.00	19
204	-21	-22	Max	133.94	-44.98	25	0.00	19	0.00	25	688.14	19	220.38	19	0.00	19
204	-21	-22	Min.	0.00	-69.93	19	0.00	25	0.00	19	555.16	25	-783.02	19	0.00	25
204	-21	-22	Min.	133.94	-69.93	19	0.00	25	0.00	19	433.19	25	141.64	25	0.00	25
204	-22	-23	Max	0.00	-44.98	25	0.00	19	0.00	25	310.46	19	220.36	19	0.00	19
204	-22	-23	Max	133.94	-44.98	25	0.00	19	0.00	32	188.49	19	554.52	19	0.00	19
204	-22	-23	Min.	0.00	-69.93	19	0.00	25	0.00	19	225.33	25	141.62	25	0.00	25
204	-22	-23	Min.	133.94	-69.93	19	0.00	25	0.00	19	103.36	25	361.76	25	0.00	25
204	-23	-24	Max	0.00	-44.98	25	0.00	19	0.00	32	-104.50	25	554.53	19	0.00	25
204	-23	-24	Max	133.94	-44.98	25	0.00	19	0.00	19	-226.47	25	219.43	19	0.00	25
204	-23	-24	Min.	0.00	-69.93	19	0.00	32	0.00	19	-189.20	19	361.76	25	0.00	19
204	-23	-24	Min.	133.94	-69.93	19	0.00	32	0.00	25	-311.17	19	140.10	25	0.00	19
204	-24	-25	Max	0.00	-44.98	25	0.00	25	0.00	19	-434.33	25	219.44	19	0.00	25
204	-24	-25	Max	133.94	-44.98	25	0.00	25	0.00	19	-556.30	25	-523.33	25	0.00	25
204	-24	-25	Min.	0.00	-69.93	19	0.00	32	0.00	25	-688.85	19	140.11	25	0.00	19



204	-24	-25	Min.	133.94	-69.93	19	0.00	32	0.00	32	-810.82	19	-784.90	19	0.00	19
204	-25	205	Max	0.00	-44.98	25	0.00	25	0.00	19	-764.16	25	-523.32	25	0.00	25
204	-25	205	Max	49.23	-44.98	25	0.00	25	0.00	19	-808.99	25	-910.53	25	0.00	25
204	-25	205	Min.	0.00	-69.93	19	0.00	32	0.00	32	-1188.50	19	-784.88	19	0.00	19
204	-25	205	Min.	49.23	-69.93	19	0.00	32	0.00	32	-1233.32	19	-1380.99	19	0.00	19
205	205	-26	Max	0.00	-82.78	25	0.00	32	0.00	19	1284.64	19	-993.52	25	0.00	19
205	205	-26	Max	84.71	-82.78	25	0.00	32	0.00	19	1207.50	19	-302.93	25	0.00	19
205	205	-26	Min.	0.00	-127.21	19	0.00	25	0.00	32	853.77	25	-1506.74	19	0.00	25
205	205	-26	Min.	84.71	-127.21	19	0.00	25	0.00	25	776.63	25	-451.14	19	0.00	25
205	-26	-27	Max	0.00	-82.78	25	0.00	32	0.00	19	829.82	19	-302.97	25	0.00	19
205	-26	-27	Max	133.94	-82.78	25	0.00	32	0.00	19	707.85	19	578.60	19	0.00	19
205	-26	-27	Min.	0.00	-127.21	19	0.00	25	0.00	25	568.77	25	-451.19	19	0.00	25
205	-26	-27	Min.	133.94	-127.21	19	0.00	25	0.00	25	446.80	25	377.18	25	0.00	25
205	-27	-28	Max	0.00	-82.78	25	0.00	32	0.00	19	330.16	19	578.65	19	0.00	19
205	-27	-28	Max	133.94	-82.78	25	0.00	32	0.00	19	208.19	19	939.19	19	0.00	19
205	-27	-28	Min.	0.00	-127.21	19	0.00	25	0.00	25	238.93	25	377.21	25	0.00	25
205	-27	-28	Min.	133.94	-127.21	19	0.00	25	0.00	25	116.97	25	615.56	25	0.00	25
205	-28	-29	Max	0.00	-82.78	25	0.00	19	0.00	19	-90.90	25	939.18	19	0.00	25
205	-28	-29	Max	133.94	-82.78	25	0.00	19	0.00	19	-212.86	25	630.48	19	0.00	25
205	-28	-29	Min.	0.00	-127.21	19	0.00	32	0.00	25	-169.49	19	615.55	25	0.00	19
205	-28	-29	Min.	133.94	-127.21	19	0.00	32	0.00	25	-291.46	19	412.12	25	0.00	19
205	-29	-30	Max	0.00	-82.78	25	0.00	25	0.00	19	-420.72	25	630.49	19	0.00	25
205	-29	-30	Max	133.94	-82.78	25	0.00	25	0.00	19	-542.69	25	-233.09	25	0.00	25
205	-29	-30	Min.	0.00	-127.21	19	0.00	32	0.00	25	-669.14	19	412.13	25	0.00	19
205	-29	-30	Min.	133.94	-127.21	19	0.00	32	0.00	25	-791.11	19	-347.47	19	0.00	19
205	-30	-31	Max	0.00	-82.78	25	0.00	25	0.00	19	-750.56	25	-233.12	25	0.00	25
205	-30	-31	Max	89.11	-82.78	25	0.00	25	0.00	19	-831.71	25	-938.13	25	0.00	25
205	-30	-31	Min.	0.00	-127.21	19	0.00	32	0.00	25	-1168.80	19	-347.52	19	0.00	19
205	-30	-31	Min.	89.11	-127.21	19	0.00	32	0.00	25	-1249.95	19	-1425.24	19	0.00	19
206	-31	-32	Max	0.00	-36.04	25	0.00	32	0.00	19	1179.40	19	-834.60	25	0.00	19
206	-31	-32	Max	44.83	-36.04	25	0.00	32	0.00	19	1138.58	19	-498.59	25	0.00	19
206	-31	-32	Min.	0.00	-57.00	19	0.00	25	0.00	25	769.96	25	-1269.70	19	0.00	25
206	-31	-32	Min.	44.83	-57.00	19	0.00	25	0.00	25	729.13	25	-750.14	19	0.00	25
206	-32	-33	Max	0.00	-36.04	25	0.00	32	0.00	19	760.90	19	-498.58	25	0.00	19
206	-32	-33	Max	133.94	-36.04	25	0.00	32	0.00	19	638.93	19	187.35	19	0.00	19
206	-32	-33	Min.	0.00	-57.00	19	0.00	19	0.00	25	521.27	25	-750.13	19	0.00	25
206	-32	-33	Min.	133.94	-57.00	19	0.00	19	0.00	25	399.30	25	117.94	25	0.00	25
206	-33	-34	Max	0.00	-36.04	25	0.00	25	0.00	19	261.25	19	187.34	19	0.00	25
206	-33	-34	Max	133.94	-36.04	25	0.00	25	0.00	19	139.28	19	455.57	19	0.00	25
206	-33	-34	Min.	0.00	-57.00	19	0.00	19	0.00	25	191.44	25	117.93	25	0.00	19
206	-33	-34	Min.	133.94	-57.00	19	0.00	19	0.00	25	69.47	25	292.67	25	0.00	19
206	-34	-35	Max	0.00	-36.04	25	0.00	25	0.00	19	-138.39	25	455.57	19	0.00	25
206	-34	-35	Max	133.94	-36.04	25	0.00	25	0.00	19	-260.36	25	54.56	19	0.00	25
206	-34	-35	Min.	0.00	-57.00	19	0.00	19	0.00	25	-238.40	19	292.67	25	0.00	19
206	-34	-35	Min.	133.94	-57.00	19	0.00	19	0.00	25	-360.37	19	25.62	25	0.00	19
206	-35	-36	Max	0.00	-36.04	25	0.00	25	0.00	19	-468.23	25	54.54	19	0.00	25
206	-35	-36	Max	53.34	-36.04	25	0.00	25	0.00	25	-516.80	25	-237.12	25	0.00	25
206	-35	-36	Min.	0.00	-57.00	19	0.00	19	0.00	25	-738.06	19	25.60	25	0.00	19
206	-35	-36	Min.	53.34	-57.00	19	0.00	19	0.00	32	-786.64	19	-352.12	19	0.00	19
206	-36	-37	Max	0.00	0.00	19	0.00	32	0.00	25	316.40	19	-157.00	25	0.00	19
206	-36	-37	Max	80.60	0.00	19	0.00	32	0.00	32	243.01	19	0.00	19	0.00	19
206	-36	-37	Min.	0.00	0.00	19	0.00	25	0.00	32	231.49	25	-225.44	19	0.00	25
206	-36	-37	Min.	80.60	0.00	19	0.00	25	0.00	25	158.10	25	0.00	25	0.00	25
302	-4	-47	Max	0.00	0.00	32	0.00	19	0.00	19	121.50	19	-66.26	25	0.00	19
302	-4	-47	Max	150.00	0.00	19	0.00	19	0.00	19	25.15	19	0.00	19	0.00	19
302	-4	-47	Min.	0.00	0.00	25	0.00	19	0.00	19	79.05	25	-109.99	19	0.00	19
302	-4	-47	Min.	150.00	0.00	25	0.00	19	0.00	19	9.29	25	0.00	32	0.00	19
302	-46	-4	Max	0.00	0.00	19	0.00	19	0.00	19	-9.29	25	0.00	25	0.00	19
302	-46	-4	Max	150.00	0.00	19	0.00	19	0.00	19	-79.05	25	-66.26	25	0.00	19
302	-46	-4	Min.	0.00	0.00	19	0.00	19	0.00	19	-25.15	19	0.00	19	0.00	19
302	-46	-4	Min.	150.00	0.00	19	0.00	19	0.00	19	-121.50	19	-109.99	19	0.00	19
303	-6	-48	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
303	-6	-48	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	32	0.00	19
303	-6	-48	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
303	-6	-48	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	19	0.00	19
303	-49	-6	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	19	0.00	19
303	-49	-6	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
303	-49	-6	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	32	0.00	19
303	-49	-6	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
304	-7	-96	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
304	-7	-96	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	32	0.00	19
304	-7	-96	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
304	-7	-96	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	25	0.00	19
304	-95	-7	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	32	0.00	19
304	-95	-7	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
304	-95	-7	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19



314	-18	-43	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	25	0.00	19
314	-44	-18	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
314	-44	-18	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
314	-44	-18	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19
314	-44	-18	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
315	-19	-45	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
315	-19	-45	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	32	0.00	19
315	-19	-45	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
315	-19	-45	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	25	0.00	19
315	-58	-19	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
315	-58	-19	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
315	-58	-19	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	32	0.00	19
315	-58	-19	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
316	-20	-63	Max	0.00	0.00	32	0.00	19	0.00	19	121.50	19	-66.26	25	0.00	19
316	-20	-63	Max	150.00	0.00	19	0.00	19	0.00	19	25.15	19	0.00	32	0.00	19
316	-20	-63	Min.	0.00	0.00	25	0.00	19	0.00	19	79.05	25	-109.99	19	0.00	19
316	-20	-63	Min.	150.00	0.00	25	0.00	19	0.00	19	9.29	25	0.00	19	0.00	19
316	-65	-20	Max	0.00	0.00	19	0.00	19	0.00	19	-9.29	25	0.00	25	0.00	19
316	-65	-20	Max	150.00	0.00	19	0.00	19	0.00	19	-79.05	25	-66.26	25	0.00	19
316	-65	-20	Min.	0.00	0.00	19	0.00	19	0.00	19	-25.15	19	0.00	32	0.00	19
316	-65	-20	Min.	150.00	0.00	19	0.00	19	0.00	19	-121.50	19	-109.99	19	0.00	19
317	-21	-51	Max	0.00	0.00	32	0.00	19	0.00	19	121.50	19	-66.26	25	0.00	19
317	-21	-51	Max	150.00	0.00	19	0.00	19	0.00	19	25.15	19	0.00	19	0.00	19
317	-21	-51	Min.	0.00	0.00	25	0.00	19	0.00	19	79.05	25	-109.99	19	0.00	19
317	-21	-51	Min.	150.00	0.00	25	0.00	19	0.00	19	9.29	25	0.00	25	0.00	19
317	-50	-21	Max	0.00	0.00	19	0.00	19	0.00	19	-9.29	25	0.00	19	0.00	19
317	-50	-21	Max	150.00	0.00	19	0.00	19	0.00	19	-79.05	25	-66.26	25	0.00	19
317	-50	-21	Min.	0.00	0.00	19	0.00	19	0.00	19	-25.15	19	0.00	32	0.00	19
317	-50	-21	Min.	150.00	0.00	19	0.00	19	0.00	19	-121.50	19	-109.99	19	0.00	19
318	-22	-53	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
318	-22	-53	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	19	0.00	19
318	-22	-53	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
318	-22	-53	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	32	0.00	19
318	-52	-22	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	32	0.00	19
318	-52	-22	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
318	-52	-22	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19
318	-52	-22	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
319	-23	-55	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
319	-23	-55	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	19	0.00	19
319	-23	-55	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
319	-23	-55	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	32	0.00	19
319	-54	-23	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
319	-54	-23	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
319	-54	-23	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19
319	-54	-23	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
320	-24	-57	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
320	-24	-57	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	19	0.00	19
320	-24	-57	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
320	-24	-57	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	25	0.00	19
320	-56	-24	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
320	-56	-24	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
320	-56	-24	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19
320	-56	-24	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
322	-25	-41	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
322	-25	-41	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	19	0.00	19
322	-25	-41	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
322	-25	-41	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	25	0.00	19
322	-64	-25	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	19	0.00	19
322	-64	-25	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
322	-64	-25	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	32	0.00	19
322	-64	-25	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
323	-26	-77	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
323	-26	-77	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	19	0.00	19
323	-26	-77	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
323	-26	-77	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	32	0.00	19
323	-76	-26	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	32	0.00	19
323	-76	-26	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
323	-76	-26	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19
323	-76	-26	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
324	-27	-79	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
324	-27	-79	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	25	0.00	19
324	-27	-79	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
324	-27	-79	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	19	0.00	19
324	-78	-27	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	32	0.00	19
324	-78	-27	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
324	-78	-27	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19

324	-78	-27	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
325	-28	-81	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
325	-28	-81	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	19	0.00	19
325	-28	-81	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
325	-28	-81	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	32	0.00	19
325	-80	-28	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
325	-80	-28	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
325	-80	-28	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19
325	-80	-28	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
326	-29	-83	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
326	-29	-83	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	19	0.00	19
326	-29	-83	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
326	-29	-83	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	25	0.00	19
326	-82	-29	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
326	-82	-29	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
326	-82	-29	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	32	0.00	19
326	-82	-29	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
327	-30	-85	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
327	-30	-85	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	19	0.00	19
327	-30	-85	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
327	-30	-85	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	32	0.00	19
327	-84	-30	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
327	-84	-30	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
327	-84	-30	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	32	0.00	19
327	-84	-30	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
329	-32	-86	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
329	-32	-86	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	25	0.00	19
329	-32	-86	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
329	-32	-86	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	19	0.00	19
329	-87	-32	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	19	0.00	19
329	-87	-32	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
329	-87	-32	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	32	0.00	19
329	-87	-32	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
330	-33	-89	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
330	-33	-89	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	25	0.00	19
330	-33	-89	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
330	-33	-89	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	19	0.00	19
330	-88	-33	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	19	0.00	19
330	-88	-33	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
330	-88	-33	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	25	0.00	19
330	-88	-33	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
331	-34	-61	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
331	-34	-61	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	25	0.00	19
331	-34	-61	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
331	-34	-61	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	19	0.00	19
331	-62	-34	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
331	-62	-34	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
331	-62	-34	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19
331	-62	-34	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
332	-35	-102	Max	0.00	0.00	32	0.00	19	0.00	19	188.84	19	-91.89	25	0.00	19
332	-35	-102	Max	150.00	0.00	19	0.00	19	0.00	19	50.29	19	0.00	25	0.00	19
332	-35	-102	Min.	0.00	0.00	25	0.00	19	0.00	19	103.93	25	-179.35	19	0.00	19
332	-35	-102	Min.	150.00	0.00	25	0.00	19	0.00	19	18.58	25	0.00	19	0.00	19
332	-101	-35	Max	0.00	0.00	19	0.00	19	0.00	19	-18.58	25	0.00	25	0.00	19
332	-101	-35	Max	150.00	0.00	19	0.00	19	0.00	19	-103.93	25	-91.89	25	0.00	19
332	-101	-35	Min.	0.00	0.00	19	0.00	19	0.00	19	-50.29	19	0.00	19	0.00	19
332	-101	-35	Min.	150.00	0.00	19	0.00	19	0.00	19	-188.84	19	-179.35	19	0.00	19
333	-37	-103	Max	0.00	0.00	32	0.00	19	0.00	19	121.50	19	-66.26	25	0.00	19
333	-37	-103	Max	150.00	0.00	19	0.00	19	0.00	19	25.15	19	0.00	25	0.00	19
333	-37	-103	Min.	0.00	0.00	25	0.00	19	0.00	19	79.05	25	-109.99	19	0.00	19
333	-37	-103	Min.	150.00	0.00	25	0.00	19	0.00	19	9.29	25	0.00	19	0.00	19
333	-104	-37	Max	0.00	0.00	19	0.00	19	0.00	19	-9.29	25	0.00	32	0.00	19
333	-104	-37	Max	150.00	0.00	19	0.00	19	0.00	19	-79.05	25	-66.26	25	0.00	19
333	-104	-37	Min.	0.00	0.00	19	0.00	19	0.00	19	-25.15	19	0.00	25	0.00	19
333	-104	-37	Min.	150.00	0.00	19	0.00	19	0.00	19	-121.50	19	-109.99	19	0.00	19

Tipo di combinazione di carico: SLE Q

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-1113.36	20	43.55	20	-46.28	20	0.00	20	0.00	20	0.00	20
1	1	-5	Max	328.50	-875.29	20	43.55	20	96.77	20	0.00	20	0.00	20	0.00	20
1	1	-5	Min.	0.00	-1113.36	20	43.55	20	-46.28	20	0.00	20	0.00	20	0.00	20
1	1	-5	Min.	328.50	-875.29	20	43.55	20	96.77	20	0.00	20	0.00	20	0.00	20
2	2	-10	Max	0.00	-2136.05	20	55.14	20	-59.02	20	0.00	20	0.00	20	0.00	20
2	2	-10	Max	328.50	-1897.98	20	55.14	20	122.12	20	0.00	20	0.00	20	0.00	20

2	2	-10	Min.	0.00	-2136.05	20	55.14	20	-59.02	20	0.00	20	0.00	20	0.00	20
2	2	-10	Min.	328.50	-1897.98	20	55.14	20	122.12	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	0.00	-2207.00	20	-44.78	20	48.81	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	328.50	-1968.93	20	-44.78	20	-98.29	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	0.00	-2207.00	20	-44.78	20	48.81	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	328.50	-1968.93	20	-44.78	20	-98.29	20	0.00	20	0.00	20	0.00	20
4	4	204	Max	0.00	-1944.35	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Max	328.50	-1706.28	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Min.	0.00	-1944.35	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Min.	328.50	-1706.28	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
5	5	205	Max	0.00	-2207.00	20	-44.78	20	48.81	20	0.00	20	0.00	20	0.00	20
5	5	205	Max	328.50	-1968.93	20	-44.78	20	-98.28	20	0.00	20	0.00	20	0.00	20
5	5	205	Min.	0.00	-2207.00	20	-44.78	20	48.81	20	0.00	20	0.00	20	0.00	20
5	5	205	Min.	328.50	-1968.93	20	-44.78	20	-98.28	20	0.00	20	0.00	20	0.00	20
6	6	-31	Max	0.00	-2136.04	20	55.14	20	-59.02	20	0.00	20	0.00	20	0.00	20
6	6	-31	Max	328.50	-1897.98	20	55.14	20	122.11	20	0.00	20	0.00	20	0.00	20
6	6	-31	Min.	0.00	-2136.04	20	55.14	20	-59.02	20	0.00	20	0.00	20	0.00	20
6	6	-31	Min.	328.50	-1897.98	20	55.14	20	122.11	20	0.00	20	0.00	20	0.00	20
7	7	-36	Max	0.00	-1113.36	20	43.55	20	-46.28	20	0.00	20	0.00	20	0.00	20
7	7	-36	Max	328.50	-875.29	20	43.55	20	96.77	20	0.00	20	0.00	20	0.00	20
7	7	-36	Min.	0.00	-1113.36	20	43.55	20	-46.28	20	0.00	20	0.00	20	0.00	20
7	7	-36	Min.	328.50	-875.29	20	43.55	20	96.77	20	0.00	20	0.00	20	0.00	20
201	-5	-4	Max	0.00	0.00	20	0.00	20	0.00	20	261.89	20	-181.50	20	0.00	20
201	-5	-4	Max	80.60	0.00	20	0.00	20	0.00	20	188.50	20	0.00	20	0.00	20
201	-5	-4	Min.	0.00	0.00	20	0.00	20	0.00	20	261.89	20	-181.50	20	0.00	20
201	-5	-4	Min.	80.60	0.00	20	0.00	20	0.00	20	188.50	20	0.00	20	0.00	20
201	-6	-5	Max	0.00	-43.55	20	0.00	20	0.00	20	-564.83	20	35.98	20	0.00	20
201	-6	-5	Max	53.34	-43.55	20	0.00	20	0.00	20	-613.40	20	-278.27	20	0.00	20
201	-6	-5	Min.	0.00	-43.55	20	0.00	20	0.00	20	-564.83	20	35.98	20	0.00	20
201	-6	-5	Min.	53.34	-43.55	20	0.00	20	0.00	20	-613.40	20	-278.27	20	0.00	20
201	-7	-6	Max	0.00	-43.55	20	0.00	20	0.00	20	-174.20	20	350.99	20	0.00	20
201	-7	-6	Max	133.94	-43.55	20	0.00	20	0.00	20	-296.17	20	35.98	20	0.00	20
201	-7	-6	Min.	0.00	-43.55	20	0.00	20	0.00	20	-174.20	20	350.99	20	0.00	20
201	-7	-6	Min.	133.94	-43.55	20	0.00	20	0.00	20	-296.17	20	35.98	20	0.00	20
201	-8	-7	Max	0.00	-43.55	20	0.00	20	0.00	20	216.43	20	142.78	20	0.00	20
201	-8	-7	Max	133.94	-43.55	20	0.00	20	0.00	20	94.46	20	350.99	20	0.00	20
201	-8	-7	Min.	0.00	-43.55	20	0.00	20	0.00	20	216.43	20	142.78	20	0.00	20
201	-8	-7	Min.	133.94	-43.55	20	0.00	20	0.00	20	94.46	20	350.99	20	0.00	20
201	-9	-8	Max	0.00	-43.55	20	0.00	20	0.00	20	607.06	20	-588.65	20	0.00	20
201	-9	-8	Max	133.94	-43.55	20	0.00	20	0.00	20	485.09	20	142.78	20	0.00	20
201	-9	-8	Min.	0.00	-43.55	20	0.00	20	0.00	20	607.06	20	-588.65	20	0.00	20
201	-9	-8	Min.	133.94	-43.55	20	0.00	20	0.00	20	485.09	20	142.78	20	0.00	20
201	-10	-9	Max	0.00	-43.55	20	0.00	20	0.00	20	916.54	20	-990.37	20	0.00	20
201	-10	-9	Max	44.83	-43.55	20	0.00	20	0.00	20	875.72	20	-588.65	20	0.00	20
201	-10	-9	Min.	0.00	-43.55	20	0.00	20	0.00	20	916.54	20	-990.37	20	0.00	20
201	-10	-9	Min.	44.83	-43.55	20	0.00	20	0.00	20	875.72	20	-588.65	20	0.00	20
202	-11	-10	Max	0.00	-98.69	20	0.00	20	0.00	20	-900.29	20	-274.05	20	0.00	20
202	-11	-10	Max	89.11	-98.69	20	0.00	20	0.00	20	-981.44	20	-1112.49	20	0.00	20
202	-11	-10	Min.	0.00	-98.69	20	0.00	20	0.00	20	-900.29	20	-274.05	20	0.00	20
202	-11	-10	Min.	89.11	-98.69	20	0.00	20	0.00	20	-981.44	20	-1112.49	20	0.00	20
202	-12	-11	Max	0.00	-98.69	20	0.00	20	0.00	20	-509.66	20	490.30	20	0.00	20
202	-12	-11	Max	133.94	-98.69	20	0.00	20	0.00	20	-631.63	20	-274.05	20	0.00	20
202	-12	-11	Min.	0.00	-98.69	20	0.00	20	0.00	20	-509.66	20	490.30	20	0.00	20
202	-12	-11	Min.	133.94	-98.69	20	0.00	20	0.00	20	-631.63	20	-274.05	20	0.00	20
202	-13	-12	Max	0.00	-98.69	20	0.00	20	0.00	20	-119.03	20	731.42	20	0.00	20
202	-13	-12	Max	133.94	-98.69	20	0.00	20	0.00	20	-241.00	20	490.30	20	0.00	20
202	-13	-12	Min.	0.00	-98.69	20	0.00	20	0.00	20	-119.03	20	731.42	20	0.00	20
202	-13	-12	Min.	133.94	-98.69	20	0.00	20	0.00	20	-241.00	20	490.30	20	0.00	20
202	-14	-13	Max	0.00	-98.69	20	0.00	20	0.00	20	271.59	20	449.32	20	0.00	20
202	-14	-13	Max	133.94	-98.69	20	0.00	20	0.00	20	149.62	20	731.42	20	0.00	20
202	-14	-13	Min.	0.00	-98.69	20	0.00	20	0.00	20	271.59	20	449.32	20	0.00	20
202	-14	-13	Min.	133.94	-98.69	20	0.00	20	0.00	20	149.62	20	731.42	20	0.00	20
202	-15	-14	Max	0.00	-98.69	20	0.00	20	0.00	20	662.22	20	-355.99	20	0.00	20
202	-15	-14	Max	133.94	-98.69	20	0.00	20	0.00	20	540.25	20	449.32	20	0.00	20
202	-15	-14	Min.	0.00	-98.69	20	0.00	20	0.00	20	662.22	20	-355.99	20	0.00	20
202	-15	-14	Min.	133.94	-98.69	20	0.00	20	0.00	20	540.25	20	449.32	20	0.00	20
202	203	-15	Max	0.00	-98.69	20	0.00	20	0.00	20	1008.02	20	-1177.26	20	0.00	20
202	203	-15	Max	84.71	-98.69	20	0.00	20	0.00	20	930.88	20	-356.00	20	0.00	20
202	203	-15	Min.	0.00	-98.69	20	0.00	20	0.00	20	1008.02	20	-1177.26	20	0.00	20
202	203	-15	Min.	84.71	-98.69	20	0.00	20	0.00	20	930.88	20	-356.00	20	0.00	20
203	-16	203	Max	0.00	-53.91	20	0.00	20	0.00	20	-916.08	20	-616.96	20	0.00	20
203	-16	203	Max	49.23	-53.91	20	0.00	20	0.00	20	-960.90	20	-1078.96	20	0.00	20
203	-16	203	Min.	0.00	-53.91	20	0.00	20	0.00	20	-916.08	20	-616.96	20	0.00	20
203	-16	203	Min.	49.23	-53.91	20	0.00	20	0.00	20	-960.90	20	-1078.96	20	0.00	20
203	-17	-16	Max	0.00	-53.91	20	0.00	20	0.00	20	-525.45	20	168.51	20	0.00	20
203	-17	-16	Max	133.94	-53.91	20	0.00	20	0.00	20	-647.42	20	-616.98	20	0.00	20

203	-17	-16	Min.	0.00	-53.91	20	0.00	20	0.00	20	-525.45	20	168.51	20	0.00	20
203	-17	-16	Min.	133.94	-53.91	20	0.00	20	0.00	20	-647.42	20	-616.98	20	0.00	20
203	-18	-17	Max	0.00	-53.91	20	0.00	20	0.00	20	-134.82	20	430.78	20	0.00	20
203	-18	-17	Max	133.94	-53.91	20	0.00	20	0.00	20	-256.79	20	168.50	20	0.00	20
203	-18	-17	Min.	0.00	-53.91	20	0.00	20	0.00	20	-134.82	20	430.78	20	0.00	20
203	-18	-17	Min.	133.94	-53.91	20	0.00	20	0.00	20	-256.79	20	168.50	20	0.00	20
203	-19	-18	Max	0.00	-53.91	20	0.00	20	0.00	20	255.81	20	169.81	20	0.00	20
203	-19	-18	Max	133.94	-53.91	20	0.00	20	0.00	20	133.84	20	430.77	20	0.00	20
203	-19	-18	Min.	0.00	-53.91	20	0.00	20	0.00	20	255.81	20	169.81	20	0.00	20
203	-19	-18	Min.	133.94	-53.91	20	0.00	20	0.00	20	133.84	20	430.77	20	0.00	20
203	-20	-19	Max	0.00	-53.91	20	0.00	20	0.00	20	646.43	20	-614.34	20	0.00	20
203	-20	-19	Max	133.94	-53.91	20	0.00	20	0.00	20	524.47	20	169.83	20	0.00	20
203	-20	-19	Min.	0.00	-53.91	20	0.00	20	0.00	20	646.43	20	-614.34	20	0.00	20
203	-20	-19	Min.	133.94	-53.91	20	0.00	20	0.00	20	524.47	20	169.83	20	0.00	20
203	204	-20	Max	0.00	-53.91	20	0.00	20	0.00	20	853.14	20	-783.15	20	0.00	20
203	204	-20	Max	20.00	-53.91	20	0.00	20	0.00	20	834.93	20	-614.34	20	0.00	20
203	204	-20	Min.	0.00	-53.91	20	0.00	20	0.00	20	853.14	20	-783.15	20	0.00	20
203	204	-20	Min.	20.00	-53.91	20	0.00	20	0.00	20	834.93	20	-614.34	20	0.00	20
204	204	-21	Max	0.00	-53.91	20	0.00	20	0.00	20	853.14	20	-783.15	20	0.00	20
204	204	-21	Max	20.00	-53.91	20	0.00	20	0.00	20	834.93	20	-614.34	20	0.00	20
204	204	-21	Min.	0.00	-53.91	20	0.00	20	0.00	20	853.14	20	-783.15	20	0.00	20
204	204	-21	Min.	20.00	-53.91	20	0.00	20	0.00	20	834.93	20	-614.34	20	0.00	20
204	-21	-22	Max	0.00	-53.91	20	0.00	20	0.00	20	646.43	20	-614.34	20	0.00	20
204	-21	-22	Max	133.94	-53.91	20	0.00	20	0.00	20	524.47	20	169.83	20	0.00	20
204	-21	-22	Min.	0.00	-53.91	20	0.00	20	0.00	20	646.43	20	-614.34	20	0.00	20
204	-21	-22	Min.	133.94	-53.91	20	0.00	20	0.00	20	524.47	20	169.83	20	0.00	20
204	-22	-23	Max	0.00	-53.91	20	0.00	20	0.00	20	255.81	20	169.81	20	0.00	20
204	-22	-23	Max	133.94	-53.91	20	0.00	20	0.00	20	133.84	20	430.77	20	0.00	20
204	-22	-23	Min.	0.00	-53.91	20	0.00	20	0.00	20	255.81	20	169.81	20	0.00	20
204	-22	-23	Min.	133.94	-53.91	20	0.00	20	0.00	20	133.84	20	430.77	20	0.00	20
204	-23	-24	Max	0.00	-53.91	20	0.00	20	0.00	20	-134.82	20	430.78	20	0.00	20
204	-23	-24	Max	133.94	-53.91	20	0.00	20	0.00	20	-256.79	20	168.50	20	0.00	20
204	-23	-24	Min.	0.00	-53.91	20	0.00	20	0.00	20	-134.82	20	430.78	20	0.00	20
204	-23	-24	Min.	133.94	-53.91	20	0.00	20	0.00	20	-256.79	20	168.50	20	0.00	20
204	-24	-25	Max	0.00	-53.91	20	0.00	20	0.00	20	-525.45	20	168.51	20	0.00	20
204	-24	-25	Max	133.94	-53.91	20	0.00	20	0.00	20	-647.42	20	-616.98	20	0.00	20
204	-24	-25	Min.	0.00	-53.91	20	0.00	20	0.00	20	-525.45	20	168.51	20	0.00	20
204	-24	-25	Min.	133.94	-53.91	20	0.00	20	0.00	20	-647.42	20	-616.98	20	0.00	20
204	-25	205	Max	0.00	-53.91	20	0.00	20	0.00	20	-916.08	20	-616.96	20	0.00	20
204	-25	205	Max	49.23	-53.91	20	0.00	20	0.00	20	-960.90	20	-1078.96	20	0.00	20
204	-25	205	Min.	0.00	-53.91	20	0.00	20	0.00	20	-916.08	20	-616.96	20	0.00	20
204	-25	205	Min.	49.23	-53.91	20	0.00	20	0.00	20	-960.90	20	-1078.96	20	0.00	20
205	205	-26	Max	0.00	-98.69	20	0.00	20	0.00	20	1008.02	20	-1177.26	20	0.00	20
205	205	-26	Max	84.71	-98.69	20	0.00	20	0.00	20	930.88	20	-355.99	20	0.00	20
205	205	-26	Min.	0.00	-98.69	20	0.00	20	0.00	20	1008.02	20	-1177.26	20	0.00	20
205	205	-26	Min.	84.71	-98.69	20	0.00	20	0.00	20	930.88	20	-355.99	20	0.00	20
205	-26	-27	Max	0.00	-98.69	20	0.00	20	0.00	20	662.23	20	-356.03	20	0.00	20
205	-26	-27	Max	133.94	-98.69	20	0.00	20	0.00	20	540.26	20	449.29	20	0.00	20
205	-26	-27	Min.	0.00	-98.69	20	0.00	20	0.00	20	662.23	20	-356.03	20	0.00	20
205	-26	-27	Min.	133.94	-98.69	20	0.00	20	0.00	20	540.26	20	449.29	20	0.00	20
205	-27	-28	Max	0.00	-98.69	20	0.00	20	0.00	20	271.59	20	449.33	20	0.00	20
205	-27	-28	Max	133.94	-98.69	20	0.00	20	0.00	20	149.62	20	731.42	20	0.00	20
205	-27	-28	Min.	0.00	-98.69	20	0.00	20	0.00	20	271.59	20	449.33	20	0.00	20
205	-27	-28	Min.	133.94	-98.69	20	0.00	20	0.00	20	149.62	20	731.42	20	0.00	20
205	-28	-29	Max	0.00	-98.69	20	0.00	20	0.00	20	-119.03	20	731.42	20	0.00	20
205	-28	-29	Max	133.94	-98.69	20	0.00	20	0.00	20	-241.00	20	490.30	20	0.00	20
205	-28	-29	Min.	0.00	-98.69	20	0.00	20	0.00	20	-119.03	20	731.42	20	0.00	20
205	-28	-29	Min.	133.94	-98.69	20	0.00	20	0.00	20	-241.00	20	490.30	20	0.00	20
205	-29	-30	Max	0.00	-98.69	20	0.00	20	0.00	20	-509.66	20	490.30	20	0.00	20
205	-29	-30	Max	133.94	-98.69	20	0.00	20	0.00	20	-631.63	20	-274.03	20	0.00	20
205	-29	-30	Min.	0.00	-98.69	20	0.00	20	0.00	20	-509.66	20	490.30	20	0.00	20
205	-29	-30	Min.	133.94	-98.69	20	0.00	20	0.00	20	-631.63	20	-274.03	20	0.00	20
205	-30	-31	Max	0.00	-98.69	20	0.00	20	0.00	20	-900.29	20	-274.08	20	0.00	20
205	-30	-31	Max	89.11	-98.69	20	0.00	20	0.00	20	-981.44	20	-1112.52	20	0.00	20
205	-30	-31	Min.	0.00	-98.69	20	0.00	20	0.00	20	-900.29	20	-274.08	20	0.00	20
205	-30	-31	Min.	89.11	-98.69	20	0.00	20	0.00	20	-981.44	20	-1112.52	20	0.00	20
206	-31	-32	Max	0.00	-43.55	20	0.00	20	0.00	20	916.54	20	-990.37	20	0.00	20
206	-31	-32	Max	44.83	-43.55	20	0.00	20	0.00	20	875.72	20	-588.64	20	0.00	20
206	-31	-32	Min.	0.00	-43.55	20	0.00	20	0.00	20	916.54	20	-990.37	20	0.00	20
206	-31	-32	Min.	44.83	-43.55	20	0.00	20	0.00	20	875.72	20	-588.64	20	0.00	20
206	-32	-33	Max	0.00	-43.55	20	0.00	20	0.00	20	607.06	20	-588.63	20	0.00	20
206	-32	-33	Max	133.94	-43.55	20	0.00	20	0.00	20	485.09	20	142.79	20	0.00	20
206	-32	-33	Min.	0.00	-43.55	20	0.00	20	0.00	20	607.06	20	-588.63	20	0.00	20
206	-32	-33	Min.	133.94	-43.55	20	0.00	20	0.00	20	485.09	20	142.79	20	0.00	20
206	-33	-34	Max	0.00	-43.55	20	0.00	20	0.00	20	216.43	20	142.78	20	0.00	20
206	-33	-34	Max	133.94	-43.55	20	0.00	20	0.00	20	94.46	20	350.99	20	0.00	20



206	-33	-34	Min.	0.00	-43.55	20	0.00	20	0.00	20	216.43	20	142.78	20	0.00	20
206	-33	-34	Min.	133.94	-43.55	20	0.00	20	0.00	20	94.46	20	350.99	20	0.00	20
206	-34	-35	Max	0.00	-43.55	20	0.00	20	0.00	20	-174.19	20	350.99	20	0.00	20
206	-34	-35	Max	133.94	-43.55	20	0.00	20	0.00	20	-296.16	20	35.98	20	0.00	20
206	-34	-35	Min.	0.00	-43.55	20	0.00	20	0.00	20	-174.19	20	350.99	20	0.00	20
206	-34	-35	Min.	133.94	-43.55	20	0.00	20	0.00	20	-296.16	20	35.98	20	0.00	20
206	-35	-36	Max	0.00	-43.55	20	0.00	20	0.00	20	-564.83	20	35.96	20	0.00	20
206	-35	-36	Max	53.34	-43.55	20	0.00	20	0.00	20	-613.40	20	-278.29	20	0.00	20
206	-35	-36	Min.	0.00	-43.55	20	0.00	20	0.00	20	-564.83	20	35.96	20	0.00	20
206	-35	-36	Min.	53.34	-43.55	20	0.00	20	0.00	20	-613.40	20	-278.29	20	0.00	20
206	-36	-37	Max	0.00	0.00	20	0.00	20	0.00	20	261.89	20	-181.50	20	0.00	20
206	-36	-37	Max	80.60	0.00	20	0.00	20	0.00	20	188.50	20	0.00	20	0.00	20
206	-36	-37	Min.	0.00	0.00	20	0.00	20	0.00	20	261.89	20	-181.50	20	0.00	20
206	-36	-37	Min.	80.60	0.00	20	0.00	20	0.00	20	188.50	20	0.00	20	0.00	20
302	-4	-47	Max	0.00	0.00	20	0.00	20	0.00	20	94.25	20	-81.91	20	0.00	20
302	-4	-47	Max	150.00	0.00	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
302	-4	-47	Min.	0.00	0.00	20	0.00	20	0.00	20	94.25	20	-81.91	20	0.00	20
302	-4	-47	Min.	150.00	0.00	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
302	-46	-4	Max	0.00	0.00	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
302	-46	-4	Max	150.00	0.00	20	0.00	20	0.00	20	-94.25	20	-81.91	20	0.00	20
302	-46	-4	Min.	0.00	0.00	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
302	-46	-4	Min.	150.00	0.00	20	0.00	20	0.00	20	-94.25	20	-81.91	20	0.00	20
303	-6	-48	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
303	-6	-48	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
303	-6	-48	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
303	-6	-48	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
303	-49	-6	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
303	-49	-6	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
303	-49	-6	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
303	-49	-6	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
304	-7	-96	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
304	-7	-96	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
304	-7	-96	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
304	-7	-96	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
304	-95	-7	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
304	-95	-7	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
304	-95	-7	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
304	-95	-7	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
305	-8	-66	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
305	-8	-66	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
305	-8	-66	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
305	-8	-66	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
305	-67	-8	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
305	-67	-8	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
305	-67	-8	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
305	-67	-8	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
306	-9	-69	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
306	-9	-69	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
306	-9	-69	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
306	-9	-69	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
306	-68	-9	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
306	-68	-9	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
306	-68	-9	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
306	-68	-9	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
307	-11	-70	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
307	-11	-70	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
307	-11	-70	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
307	-11	-70	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
307	-71	-11	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
307	-71	-11	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
307	-71	-11	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
307	-71	-11	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
308	-12	-72	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
308	-12	-72	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
308	-12	-72	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
308	-12	-72	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
308	-73	-12	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
308	-73	-12	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
308	-73	-12	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
308	-73	-12	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
309	-13	-74	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
309	-13	-74	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
309	-13	-74	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
309	-13	-74	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
309	-75	-13	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
309	-75	-13	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20

330	-88	-33	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
330	-88	-33	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
331	-34	-61	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
331	-34	-61	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
331	-34	-61	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
331	-34	-61	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
331	-62	-34	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
331	-62	-34	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
331	-62	-34	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
331	-62	-34	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
332	-35	-102	Max	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
332	-35	-102	Max	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
332	-35	-102	Min.	0.00	0.00	20	0.00	20	0.00	20	134.33	20	-123.20	20	0.00	20
332	-35	-102	Min.	150.00	0.00	20	0.00	20	0.00	20	29.94	20	0.00	20	0.00	20
332	-101	-35	Max	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
332	-101	-35	Max	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
332	-101	-35	Min.	0.00	0.00	20	0.00	20	0.00	20	-29.94	20	0.00	20	0.00	20
332	-101	-35	Min.	150.00	0.00	20	0.00	20	0.00	20	-134.33	20	-123.20	20	0.00	20
333	-37	-103	Max	0.00	0.00	20	0.00	20	0.00	20	94.25	20	-81.91	20	0.00	20
333	-37	-103	Max	150.00	0.00	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
333	-37	-103	Min.	0.00	0.00	20	0.00	20	0.00	20	94.25	20	-81.91	20	0.00	20
333	-37	-103	Min.	150.00	0.00	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
333	-104	-37	Max	0.00	0.00	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
333	-104	-37	Max	150.00	0.00	20	0.00	20	0.00	20	-94.25	20	-81.91	20	0.00	20
333	-104	-37	Min.	0.00	0.00	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
333	-104	-37	Min.	150.00	0.00	20	0.00	20	0.00	20	-94.25	20	-81.91	20	0.00	20

Verifiche aste in acciaio

Simbologia

Φ_{LT}		= Coefficiente Φ per stabilità laterale membrature inflesse
Φ_y		= Coefficiente Φ per inflessione intorno all'asse y(c)
Φ_z		= Coefficiente Φ per inflessione intorno all'asse z(e)
α_{imp}		= Coefficiente di imperfezione
$\alpha_{my}, \alpha_{mz}, \alpha_{LT}$		= Coefficienti correttivi per il momento flettente
β_{LT}		= Coefficiente per calcolo Φ_{LT}
χ_{LT}		= Coefficiente di riduzione per stabilità laterale membrature inflesse
χ_y		= Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
χ_z		= Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
δ	<cm>	= Spostamento relativo asta
λ'_y		= Snellezza adimensionale per inflessione intorno all'asse y(c)
λ'_z		= Snellezza adimensionale per inflessione intorno all'asse z(e)
λ_{LT}		= Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$		= Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
λ_y		= Snellezza per inflessione intorno all'asse y(c)
λ_z		= Snellezza per inflessione intorno all'asse z(e)
$\sigma_{TD,max}$	<daN/cm²>	= Tensione ideale massima
σ_n	<daN/cm²>	= Tensione normale per momento flettente
σ_N	<daN/cm²>	= Tensione normale per sforzo normale
τ	<daN/cm²>	= Tensione tangenziale per taglio e/o torsione
ψ		= Coeff. di correzione momento critico per stabilità laterale membrature inflesse
A_{eff}	<cm²>	= Area effettiva per trazione
A_{net}	<cm²>	= Area netta per compressione
Area	<cm²>	= Area
$A_{tag,y}$	<cm²>	= Area resistente a taglio in dir. Y
$A_{tag,z}$	<cm²>	= Area resistente a taglio in dir. Z
CC		= Numero della combinazione delle condizioni di carico elementari
Cod.		= Codice
Curva		= Curva di instabilità adottata
D	<cm>	= Distanza
F_{yk}	<daN/cm²>	= Tensione caratteristica di snervamento dell'acciaio
F_{yt}	<daN/cm²>	= Tensione caratteristica di rottura
I_y	<cm⁴>	= Raggio giratorio d'inerzia rispetto all'asse Y
I_z	<cm⁴>	= Raggio giratorio d'inerzia rispetto all'asse Z
J_0	<cm⁶>	= Costante di ingobbamento
J_y	<cm⁴>	= Momento d'inerzia rispetto all'asse Y
J_z	<cm⁴>	= Momento d'inerzia rispetto all'asse Z
$K_{yy}, K_{yz}, K_{zy}, K_{zz}$		= Coefficienti di interazione
L	<m>	= Lunghezza dell'asta
L_{cr}	<m>	= Lunghezza di libera inflessione laterale fra ritegni torsionali
M, cr	<daNm>	= Momento critico per instabilità flessione torsionale
M_{Ny}, c, Rd	<daNm>	= Resistenza di calcolo a pressoflessione intorno all'asse Y
M_x	<daNm>	= Momento torcente intorno all'asse X
M_y	<daNm>	= Momento flettente intorno all'asse Y
M_y, Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Y
M_y, V, c, Rd	<daNm>	= Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y
M_z	<daNm>	= Momento flettente intorno all'asse Z
M_z, Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Z
N	<daN>	= Sforzo normale
N, Ed	<daN>	= Forza assiale di calcolo
N_c, Rd	<daN>	= Resistenza a compressione
$N_{cr,y}$	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
$N_{cr,z}$	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
Sez.		= Numero della sezione
Tipo		= Tipologia
		Rc = Rettangolare cava
		Is = I stondata
Tp		= Tipo di acciaio
T_y	<daN>	= Taglio in dir. Y
T_z	<daN>	= Taglio in dir. Z

V,Ed <daN> = Forza di taglio di calcolo
 Vc,Rd <daN> = Resistenza a taglio
 Wy,plas <cmc> = Modulo di resistenza plastico intorno all'asse Y
 Wymmin <cmc> = Modulo di resistenza minimo rispetto all'asse Y
 Wz,plas <cmc> = Modulo di resistenza plastico intorno all'asse Z
 Wzmin <cmc> = Modulo di resistenza minimo rispetto all'asse Z
 Xl <m> = Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
 f = Fattore di modifica per il coefficiente di riduzione
 f_{Z,G} <cm> = Freccia in direzione Z globale
 f_{Z,L} <cm> = Freccia in direzione Z locale
 k_c = Coeff. di correzione momento flettente per stabilità laterale membrature inflesse

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D	Area	Anet	Aeff	Jy	Jz	Iy	Iz	Wymmin	Wzmin	Ip	Fyk	Fyt
			<cm>	<cmq>	<cmq>	<cmq>	<cm4>	<cm4>	<cm>	<cm>	<cmc>	<cmc>		<daN/cmq>	<daN/cmq>
1	COL HEA280	Is	--	97.27	97.27	97.27	13673.70	4762.65	11.86	7.00	1012.87	340.19	S355 UNI EN 10025-2	3550.00	5100.00
2	TRV PRINC SHS300x300x10	Rc	--	116.00	116.00	116.00	16278.70	16278.70	11.85	11.85	1085.24	1085.24	S355H UNI EN 10210-1	3550.00	5100.00
3	TRV SEC RHS150x100x10	Rc	--	46.00	46.00	46.00	1347.83	695.33	5.41	3.89	179.71	139.07	S355H UNI EN 10210-1	3550.00	5100.00

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy,plas	Wz,plas	Atag,y	Atag,z	J ₀
		<cmc>	<cmc>	<cmq>	<cmq>	<cm6>
1	COL HEA280	1117.45	518.72	81.59	31.75	785367.00
2	TRV PRINC SHS300x300x10	1262.00	1262.00	58.00	58.00	
3	TRV SEC RHS150x100x10	224.50	167.00	18.40	27.60	

Asta n. 1 (1 -5) - Sez. 1 (COL HEA280) - Crit. 1

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-1255.09 T_z=52.13 M_y=190.87 T_y=311.68 M_z=-524.78
 Tensioni: σ_N=-12.90 σ_{m,d}=-173.11 τ=0.00 σ_{max}=-186.01 (sfrut=0.06)
 Tensioni: σ_N=-12.90 σ_{m,d}=-47.88 τ=6.16 τ_{max}=6.16 (sfrut=0.00)
 Tensioni: σ_N=-12.90 σ_{m,d}=-173.11 τ=0.00 σ_{ID,max}=186.01 (sfrut=0.06)
 - Verifica in termini tensionali [4.2.4] - CC 29 SLU Xl=3.29 - Classe 3
 Sollecitazioni: N=-3142.05 T_y=175.04 M_z=388.86
 Tensioni: σ_N=-32.30 σ_{m,d}=-114.31 τ=0.00 σ_{max}=-146.61 (sfrut=0.04)
 Tensioni: σ_N=-32.30 σ_{m,d}=-22.86 τ=3.46 τ_{max}=3.46 (sfrut=0.00)
 Tensioni: σ_N=-32.30 σ_{m,d}=-114.31 τ=0.00 σ_{ID,max}=146.61 (sfrut=0.04)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3
 Sollecitazioni: N,Ed=-1255.09 M_{y,Ed}=190.87 M_{z,Ed}=-524.78 L=3.29
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 L_{cr}=3.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.65 M_{cr}=220262.00 λ_{LT}=0.40
 λ_{LT,0}=0.40 Φ_{LT}=0.56 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
 λ_y=27.71 Ncr,y=2626240.00 λ_y'=0.36 Curva b: Φ_y=0.59 χ_y=0.94
 λ_z=46.95 Ncr,z=914738.00 λ_z'=0.61 Curva c: Φ_z=0.79 χ_z=0.78
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.04=0.05
 Verifica ZZ: 0.00+0.00+0.04=0.05
 - Verifica Spostamento relativo massimo per singola asta - CC 31
 δ=0.01 (L/28990)

Asta n. 2 (2 -10) - Sez. 1 (COL HEA280) - Crit. 1

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2048.81 T_z=99.37 M_y=312.42 T_y=362.07 M_z=-579.89
 Tensioni: σ_N=-21.06 σ_{m,d}=-201.31 τ=0.00 σ_{max}=-222.37 (sfrut=0.07)
 Tensioni: σ_N=-21.06 σ_{m,d}=-61.97 τ=7.18 τ_{max}=7.18 (sfrut=0.00)
 Tensioni: σ_N=-21.06 σ_{m,d}=-201.31 τ=0.00 σ_{ID,max}=222.37 (sfrut=0.07)
 - Verifica in termini tensionali [4.2.4] - CC 29 SLU Xl=3.29 - Classe 3
 Sollecitazioni: N=-7143.43 T_y=204.25 M_z=452.47
 Tensioni: σ_N=-73.44 σ_{m,d}=-133.01 τ=0.00 σ_{max}=-206.45 (sfrut=0.06)
 Tensioni: σ_N=-73.44 σ_{m,d}=-26.60 τ=4.03 τ_{max}=4.03 (sfrut=0.00)
 Tensioni: σ_N=-73.44 σ_{m,d}=-133.01 τ=0.00 σ_{ID,max}=206.45 (sfrut=0.06)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-7452.92 M_{y,Ed}=0.00 M_{z,Ed}=452.47 L=3.29
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 L_{cr}=3.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.00 M_{cr}=133911.00 λ_{LT}=0.52
 λ_{LT,0}=0.40 Φ_{LT}=0.62 β_{LT}=0.75 f=0.97 χ_{LT}=0.98
 λ_y=27.71 Ncr,y=2626240.00 λ_y'=0.36 Curva b: Φ_y=0.59 χ_y=0.94
 λ_z=46.95 Ncr,z=914738.00 λ_z'=0.61 Curva c: Φ_z=0.79 χ_z=0.78
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96
 Verifica YY: 0.02+0.04=0.06
 Verifica ZZ: 0.03+0.04=0.07

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.01$ (L/25253)

Asta n. 3 (3 203) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 3 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-2180.66$ $T_x=106.36$ $M_y=341.72$ $T_y=-338.37$ $M_z=555.56$
 Tensioni: $\sigma_N=-22.42$ $\sigma_{m,d}=-197.05$ $\tau=0.00$ $\sigma_{max}=-219.47$ (sfrut=0.06)
 Tensioni: $\sigma_N=-22.42$ $\sigma_{m,d}=2.17$ $\tau=6.72$ $\tau_{max}=6.72$ (sfrut=0.00)
 Tensioni: $\sigma_N=-22.42$ $\sigma_{m,d}=-197.05$ $\tau=0.00$ $\sigma_{TD,max}=219.47$ (sfrut=0.06)

- Verifica in termini tensionali [4.2.4] - CC 29 SLU $X_1=3.29$ - Classe 3
 Sollecitazioni: $N=-7391.11$ $T_y=-168.27$ $M_z=-369.29$
 Tensioni: $\sigma_N=-75.99$ $\sigma_{m,d}=-108.55$ $\tau=0.00$ $\sigma_{max}=-184.54$ (sfrut=0.05)
 Tensioni: $\sigma_N=-75.99$ $\sigma_{m,d}=21.71$ $\tau=3.32$ $\tau_{max}=3.32$ (sfrut=0.00)
 Tensioni: $\sigma_N=-75.99$ $\sigma_{m,d}=-108.55$ $\tau=0.00$ $\sigma_{TD,max}=184.54$ (sfrut=0.05)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-2180.66$ $M_y,Ed=341.72$ $M_z,Ed=-555.98$ $L=3.29$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $L_{cr}=3.29$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.77$ $M_{cr}=237466.00$ $\lambda_{LT}=0.39$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.55$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=27.71$ Ncr, $y=2626240.00$ $\lambda^*_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ Ncr, $z=914738.00$ $\lambda^*_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.01+0.01+0.05=0.06$
 Verifica ZZ: $0.01+0.01+0.05=0.06$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.01$ (L/31617)

Asta n. 4 (4 204) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 3 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-1944.35$ $T_x=-95.76$ $M_y=-318.70$ $T_y=300.98$ $M_z=-514.82$
 Tensioni: $\sigma_N=-19.99$ $\sigma_{m,d}=-182.80$ $\tau=0.00$ $\sigma_{max}=-202.79$ (sfrut=0.06)
 Tensioni: $\sigma_N=-19.99$ $\sigma_{m,d}=-1.83$ $\tau=5.97$ $\tau_{max}=5.97$ (sfrut=0.00)
 Tensioni: $\sigma_N=-19.99$ $\sigma_{m,d}=-182.80$ $\tau=0.00$ $\sigma_{TD,max}=202.79$ (sfrut=0.06)

- Verifica a compressione (4.2.4.1.2.2) - CC 29 SLU $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-6367.78$
 Verifica a compressione [4.2.9]
 $N,Ed=-6367.78$ $N_c,Rd=-328857.00$ $N,Ed/N_c,Rd=0.02$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-1944.35$ $M_y,Ed=-318.70$ $M_z,Ed=-514.82$ $L=3.29$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $L_{cr}=3.29$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.74$ $M_{cr}=232471.00$ $\lambda_{LT}=0.39$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.56$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=27.71$ Ncr, $y=2626240.00$ $\lambda^*_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ Ncr, $z=914738.00$ $\lambda^*_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.01+0.01+0.04=0.06$
 Verifica ZZ: $0.01+0.01+0.04=0.06$

Asta n. 5 (5 205) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 7 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-2180.66$ $T_x=-106.36$ $M_y=-341.72$ $T_y=-338.37$ $M_z=555.55$
 Tensioni: $\sigma_N=-22.42$ $\sigma_{m,d}=-197.04$ $\tau=0.00$ $\sigma_{max}=-219.46$ (sfrut=0.06)
 Tensioni: $\sigma_N=-22.42$ $\sigma_{m,d}=63.15$ $\tau=6.72$ $\tau_{max}=6.72$ (sfrut=0.00)
 Tensioni: $\sigma_N=-22.42$ $\sigma_{m,d}=-197.04$ $\tau=0.00$ $\sigma_{TD,max}=219.46$ (sfrut=0.06)

- Verifica in termini tensionali [4.2.4] - CC 29 SLU $X_1=3.29$ - Classe 3
 Sollecitazioni: $N=-7391.11$ $T_y=-168.26$ $M_z=-369.28$
 Tensioni: $\sigma_N=-75.99$ $\sigma_{m,d}=-108.55$ $\tau=0.00$ $\sigma_{max}=-184.54$ (sfrut=0.05)
 Tensioni: $\sigma_N=-75.99$ $\sigma_{m,d}=21.71$ $\tau=3.32$ $\tau_{max}=3.32$ (sfrut=0.00)
 Tensioni: $\sigma_N=-75.99$ $\sigma_{m,d}=-108.55$ $\tau=0.00$ $\sigma_{TD,max}=184.54$ (sfrut=0.05)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3
 Sollecitazioni: $N,Ed=-2180.66$ $M_y,Ed=-341.72$ $M_z,Ed=-555.98$ $L=3.29$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $L_{cr}=3.29$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.77$ $M_{cr}=237466.00$ $\lambda_{LT}=0.39$

$\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.55$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=27.71$ $N_{cr,y}=2626240.00$ $\lambda^*_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ $N_{cr,z}=914738.00$ $\lambda^*_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.01+0.05=0.06$
 Verifica ZZ: $0.01+0.01+0.05=0.06$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.01$ (L/31971)

Asta n. 6 (6 -31) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 3 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-2048.80$ $T_z=-99.37$ $M_y=-312.42$ $T_y=362.07$ $M_z=-579.89$
 Tensioni: $\sigma_N=-21.06$ $\sigma_{m,d}=-201.31$ $\tau=0.00$ $\sigma_{max}=-222.37$ (sfrut=0.07)
 Tensioni: $\sigma_N=-21.06$ $\sigma_{m,d}=-6.22$ $\tau=7.18$ $\tau_{max}=7.18$ (sfrut=0.00)
 Tensioni: $\sigma_N=-21.06$ $\sigma_{m,d}=-201.31$ $\tau=0.00$ $\sigma_{ID,max}=222.37$ (sfrut=0.07)

- Verifica in termini tensionali [4.2.4] - CC 29 SLU $X_l=3.29$ - Classe 3
 Sollecitazioni: $N=-7143.43$ $T_y=204.25$ $M_z=452.46$
 Tensioni: $\sigma_N=-73.44$ $\sigma_{m,d}=-133.00$ $\tau=0.00$ $\sigma_{max}=-206.44$ (sfrut=0.06)
 Tensioni: $\sigma_N=-73.44$ $\sigma_{m,d}=-26.60$ $\tau=4.03$ $\tau_{max}=4.03$ (sfrut=0.00)
 Tensioni: $\sigma_N=-73.44$ $\sigma_{m,d}=-133.00$ $\tau=0.00$ $\sigma_{ID,max}=206.44$ (sfrut=0.06)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $N, Ed=-7452.91$ $M_y, Ed=-0.00$ $M_z, Ed=452.46$ $L=3.29$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $L_{cr}=3.29$ Curva b: $\alpha_{imp}=0.34$ $k_e=0.94$ $\psi=1.00$ $M_{cr}=133911.00$ $\lambda_{LT}=0.52$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.62$ $\beta_{LT}=0.75$ $f=0.97$ $\chi_{LT}=0.98$
 $\lambda_y=27.71$ $N_{cr,y}=2626240.00$ $\lambda^*_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ $N_{cr,z}=914738.00$ $\lambda^*_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.96, 0.76, 0.96$
 Verifica YY: $0.02+0.04=0.06$
 Verifica ZZ: $0.03+0.04=0.07$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.01$ (L/25295)

Asta n. 7 (7 -36) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 3 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-1255.09$ $T_z=-52.13$ $M_y=-190.87$ $T_y=311.68$ $M_z=-524.78$
 Tensioni: $\sigma_N=-12.90$ $\sigma_{m,d}=-173.11$ $\tau=0.00$ $\sigma_{max}=-186.01$ (sfrut=0.06)
 Tensioni: $\sigma_N=-12.90$ $\sigma_{m,d}=-13.82$ $\tau=6.16$ $\tau_{max}=6.16$ (sfrut=0.00)
 Tensioni: $\sigma_N=-12.90$ $\sigma_{m,d}=-173.11$ $\tau=0.00$ $\sigma_{ID,max}=186.01$ (sfrut=0.06)

- Verifica in termini tensionali [4.2.4] - CC 29 SLU $X_l=3.29$ - Classe 3
 Sollecitazioni: $N=-3142.04$ $T_y=175.04$ $M_z=388.85$
 Tensioni: $\sigma_N=-32.30$ $\sigma_{m,d}=-114.30$ $\tau=0.00$ $\sigma_{max}=-146.61$ (sfrut=0.04)
 Tensioni: $\sigma_N=-32.30$ $\sigma_{m,d}=-22.86$ $\tau=3.46$ $\tau_{max}=3.46$ (sfrut=0.00)
 Tensioni: $\sigma_N=-32.30$ $\sigma_{m,d}=-114.30$ $\tau=0.00$ $\sigma_{ID,max}=146.61$ (sfrut=0.04)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N, Ed=-1255.09$ $M_y, Ed=-190.87$ $M_z, Ed=-524.78$ $L=3.29$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $L_{cr}=3.29$ Curva b: $\alpha_{imp}=0.34$ $k_e=0.94$ $\psi=1.65$ $M_{cr}=220262.00$ $\lambda_{LT}=0.40$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.56$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=27.71$ $N_{cr,y}=2626240.00$ $\lambda^*_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ $N_{cr,z}=914738.00$ $\lambda^*_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.01+0.04=0.05$
 Verifica ZZ: $0.00+0.00+0.04=0.05$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.01$ (L/28805)

Asta n. 201 (-5 -4) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-11.45$ $T_z=261.89$ $M_y=181.50$ $T_y=38.17$ $M_z=-30.77$
 Tensioni: $\sigma_N=-0.10$ $\sigma_{m,d}=-19.56$ $\tau=0.00$ $\sigma_{max}=-19.66$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.10$ $\sigma_{m,d}=-2.65$ $\tau=5.08$ $\tau_{max}=5.08$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.10$ $\sigma_{m,d}=-19.56$ $\tau=0.00$ $\sigma_{ID,max}=19.66$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 2
Sollecitazioni: $T_z=820.16$
 $V, Ed=820.16$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.01$
- Verifica a flessione e taglio YY [4.2.32] - CC 29 SLU $X_l=0.00$ - Classe 2
Sollecitazioni: $T_z=820.16$ $M_y=622.60$
 $M_y, Ed=622.60$ $M_y, V, c, Rd=42667.60$ $M_y, Ed/M_y, V, c, Rd=0.01$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: $N, Ed=-11.45$ $M_y, Ed=181.50$ $M_z, Ed=30.77$ $L=0.81$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=6.80$ $N_{cr,y}=51935400.00$ $\lambda^*_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.80$ $N_{cr,z}=51935400.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.00+0.00=0.01$
Verifica ZZ: $0.00+0.00+0.00=0.00$
- Asta n. 201 (-6 -5) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 5 SND $X_l=0.53$ - Classe 3
Sollecitazioni: $N=-242.99$ $T_z=-755.13$ $M_y=680.57$ $T_y=-31.52$ $M_z=-9.28$ $M_x=-19.62$
Tensioni: $\sigma_N=-2.09$ $\sigma_{m,d}=-63.57$ $\tau=1.17$ $\sigma_{max}=-65.66$ (sfrut=0.02)
Tensioni: $\sigma_N=-2.09$ $\sigma_{m,d}=-0.80$ $\tau=15.80$ $\tau_{max}=15.80$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.09$ $\sigma_{m,d}=-63.57$ $\tau=1.17$ $\sigma_{ID,max}=65.69$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.53$ - Classe 2
Sollecitazioni: $T_z=-2321.89$
 $V, Ed=-2321.89$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.02$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=0.53$ - Classe 2
Sollecitazioni: $N=-175.04$ $T_z=-2321.89$ $M_y=1011.45$
 $M_y, Ed=1011.45$ $M_y, V, c, Rd=42667.60$
 $N, Ed=-175.04$ $N_c, Rd=-392190.00$ YY $n=N, Ed/N_c, Rd=0.00$ $M_{Ny}, c, Rd=42667.60$ $M_y, Ed/M_{Ny}, c, Rd=0.02$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N, Ed=-175.04$ $M_y, Ed=1011.45$ $M_z, Ed=-0.00$ $L=0.53$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.50$ $N_{cr,y}=118574000.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=4.50$ $N_{cr,z}=118574000.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.03=0.03$
Verifica ZZ: $0.00+0.02=0.02$
- Asta n. 201 (-7 -6) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 3 SND $X_l=0.00$ - Classe 3
Sollecitazioni: $N=95.89$ $T_z=-32.47$ $M_y=-487.84$ $T_y=13.52$ $M_z=-25.65$ $M_x=19.62$
Tensioni: $\sigma_N=0.83$ $\sigma_{m,d}=47.32$ $\tau=1.17$ $\sigma_{max}=48.14$ (sfrut=0.01)
Tensioni: $\sigma_N=0.83$ $\sigma_{m,d}=2.21$ $\tau=1.80$ $\tau_{max}=1.80$ (sfrut=0.00)
Tensioni: $\sigma_N=0.83$ $\sigma_{m,d}=47.32$ $\tau=1.17$ $\sigma_{ID,max}=48.19$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.34$ - Classe 2
Sollecitazioni: $T_z=-950.07$
 $V, Ed=-950.07$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=0.00$ - Classe 2
Sollecitazioni: $N=-175.04$ $T_z=-791.51$ $M_y=-1376.63$
 $M_y, Ed=-1376.63$ $M_y, V, c, Rd=42667.60$
 $N, Ed=-175.04$ $N_c, Rd=-392190.00$ YY $n=N, Ed/N_c, Rd=0.00$ $M_{Ny}, c, Rd=42667.60$ $M_y, Ed/M_{Ny}, c, Rd=0.03$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N, Ed=-175.04$ $M_y, Ed=-1376.63$ $M_z, Ed=-0.00$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ $N_{cr,y}=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ $N_{cr,z}=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.04=0.04$
Verifica ZZ: $0.00+0.03=0.03$
- Asta n. 201 (-8 -7) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.34$ - Classe 3
Sollecitazioni: $N=29.68$ $T_z=236.19$ $M_y=-487.84$ $T_y=6.34$ $M_z=25.65$ $M_x=-19.62$
Tensioni: $\sigma_N=0.26$ $\sigma_{m,d}=47.32$ $\tau=1.17$ $\sigma_{max}=47.57$ (sfrut=0.01)
Tensioni: $\sigma_N=0.26$ $\sigma_{m,d}=-2.21$ $\tau=5.74$ $\tau_{max}=5.74$ (sfrut=0.00)
Tensioni: $\sigma_N=0.26$ $\sigma_{m,d}=47.32$ $\tau=1.17$ $\sigma_{ID,max}=47.61$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $T_z=675.72$
 $V, Ed=675.72$ $Vc, Rd=113219.00$ $V, Ed/Vc, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 2
Sollecitazioni: $N=-175.04$ $T_z=517.16$ $M_y=-1376.63$
 $M_y, Ed=-1376.63$ $M_y, V, c, Rd=42667.60$
 $N, Ed=-175.04$ $Nc, Rd=-392190.00$ YY $n=N, Ed/Nc, Rd=0.00$ $MNy, c, Rd=42667.60$ $M_y, Ed/MNy, c, Rd=0.03$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N, Ed=-175.04$ $M_y, Ed=-1376.63$ $M_z, Ed=-0.00$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ $Ncr, y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ $Ncr, z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.04=0.04$
Verifica ZZ: $0.00+0.03=0.03$

Asta n. 201 (-9 -8) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=-36.54$ $T_z=748.79$ $M_y=831.47$ $T_y=26.21$ $M_z=-17.94$ $M_x=-19.62$
Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=-78.27$ $\tau=1.17$ $\sigma_{max}=-78.58$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=1.54$ $\tau=15.68$ $\tau_{max}=15.68$ (sfrut=0.01)
Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=-78.27$ $\tau=1.17$ $\sigma_{ID,max}=78.61$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $T_z=2142.95$
 $V, Ed=2142.95$ $Vc, Rd=113219.00$ $V, Ed/Vc, Rd=0.02$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $N=-175.04$ $T_z=2142.95$ $M_y=2186.41$
 $M_y, Ed=2186.41$ $M_y, V, c, Rd=42667.60$
 $N, Ed=-175.04$ $Nc, Rd=-392190.00$ YY $n=N, Ed/Nc, Rd=0.00$ $MNy, c, Rd=42667.60$ $M_y, Ed/MNy, c, Rd=0.05$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N, Ed=-175.04$ $M_y, Ed=2186.41$ $M_z, Ed=-0.00$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ $Ncr, y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ $Ncr, z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.06=0.06$
Verifica ZZ: $0.00+0.05=0.05$

Asta n. 201 (-10 -9) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=-95.88$ $T_z=1058.27$ $M_y=1296.74$ $T_y=44.01$ $M_z=-37.67$ $M_x=-19.62$
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=-122.96$ $\tau=1.17$ $\sigma_{max}=-123.79$ (sfrut=0.04)
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=3.24$ $\tau=21.68$ $\tau_{max}=21.68$ (sfrut=0.01)
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=-122.96$ $\tau=1.17$ $\sigma_{ID,max}=123.80$ (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $T_z=3504.69$
 $V, Ed=3504.69$ $Vc, Rd=113219.00$ $V, Ed/Vc, Rd=0.03$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $N=-175.04$ $T_z=3504.69$ $M_y=3745.63$
 $M_y, Ed=3745.63$ $M_y, V, c, Rd=42667.60$
 $N, Ed=-175.04$ $Nc, Rd=-392190.00$ YY $n=N, Ed/Nc, Rd=0.00$ $MNy, c, Rd=42667.60$ $M_y, Ed/MNy, c, Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N, Ed=-175.04$ $M_y, Ed=3745.63$ $M_z, Ed=-0.00$ $L=0.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.78$ $Ncr, y=167889000.00$ $\lambda^*_y=0.05$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=3.78$ $Ncr, z=167889000.00$ $\lambda^*_z=0.05$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.10=0.10$
Verifica ZZ: $0.00+0.08=0.08$

Asta n. 202 (-11 -10) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.89 - Classe 3
Sollecitazioni: $N=-322.76$ $T_z=-1035.93$ $M_y=1293.51$ $T_y=-46.21$ $M_z=-37.71$ $M_x=-5.61$
Tensioni: $\sigma_N=-2.78$ $\sigma_{m,d}=-122.67$ $\tau=0.33$ $\sigma_{max}=-125.45$ (sfrut=0.04)

Tensioni: $\sigma_N=-2.78$ $\sigma_{m,d}=-3.24$ $\tau=20.41$ $\tau_{max}=20.41$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.78$ $\sigma_{m,d}=-122.67$ $\tau=0.33$ $\sigma_{ID,max}=125.45$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.89$ - Classe 2
Sollecitazioni: $T_z=-3638.74$
 $V,Ed=-3638.74$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.03$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=0.89$ - Classe 2
Sollecitazioni: $N=-379.30$ $T_z=-3638.74$ $M_y=4198.10$
 $M_y,Ed=4198.10$ $M_y,V,c,Rd=42667.60$
 $N,Ed=-379.30$ $N_c,Rd=-392190.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=42667.60$ $M_y,Ed/MN_y,c,Rd=0.10$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N,Ed=-379.30$ $M_y,Ed=4198.10$ $M_z,Ed=-0.00$ $L=0.89$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=7.52$ Ncr, $y=42486100.00$ $\lambda^*_y=0.10$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.52$ Ncr, $z=42486100.00$ $\lambda^*_z=0.10$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
Verifica YY: $0.00+0.11=0.11$
Verifica ZZ: $0.00+0.09=0.09$

Asta n. 202 (-12 -11) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND $X_l=0.00$ - Classe 3
Sollecitazioni: $N=-50.29$ $T_z=-493.31$ $M_y=-508.14$ $T_y=91.27$ $M_z=-133.81$ $M_x=18.69$
Tensioni: $\sigma_N=-0.43$ $\sigma_{m,d}=-59.15$ $\tau=1.11$ $\sigma_{max}=-59.59$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.43$ $\sigma_{m,d}=11.51$ $\tau=10.67$ $\tau_{max}=10.67$ (sfrut=0.01)
Tensioni: $\sigma_N=-0.43$ $\sigma_{m,d}=-59.15$ $\tau=1.11$ $\sigma_{ID,max}=59.62$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.34$ - Classe 2
Sollecitazioni: $T_z=-2224.57$
 $V,Ed=-2224.57$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.02$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=0.00$ - Classe 2
Sollecitazioni: $N=-379.30$ $T_z=-2066.01$ $M_y=-1870.99$
 $M_y,Ed=-1870.99$ $M_y,V,c,Rd=42667.60$
 $N,Ed=-379.30$ $N_c,Rd=-392190.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=42667.60$ $M_y,Ed/MN_y,c,Rd=0.04$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N,Ed=-379.30$ $M_y,Ed=-1870.99$ $M_z,Ed=-0.00$ $L=1.34$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=11.31$ Ncr, $y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr, $z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
Verifica YY: $0.00+0.05=0.05$
Verifica ZZ: $0.00+0.04=0.04$

Asta n. 202 (-13 -12) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND $X_l=0.00$ - Classe 3
Sollecitazioni: $N=127.22$ $T_z=-135.38$ $M_y=-735.47$ $T_y=-25.05$ $M_z=167.36$ $M_x=-18.69$
Tensioni: $\sigma_N=-1.10$ $\sigma_{m,d}=-83.19$ $\tau=1.11$ $\sigma_{max}=-84.29$ (sfrut=0.02)
Tensioni: $\sigma_N=-1.10$ $\sigma_{m,d}=14.39$ $\tau=3.73$ $\tau_{max}=3.73$ (sfrut=0.00)
Tensioni: $\sigma_N=-1.10$ $\sigma_{m,d}=-83.19$ $\tau=1.11$ $\sigma_{ID,max}=84.31$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.34$ - Classe 2
Sollecitazioni: $T_z=-757.34$
 $V,Ed=-757.34$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=0.00$ - Classe 2
Sollecitazioni: $N=-379.30$ $T_z=-598.78$ $M_y=-2779.21$
 $M_y,Ed=-2779.21$ $M_y,V,c,Rd=42667.60$
 $N,Ed=-379.30$ $N_c,Rd=-392190.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=42667.60$ $M_y,Ed/MN_y,c,Rd=0.07$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N,Ed=-379.30$ $M_y,Ed=-2779.21$ $M_z,Ed=-0.00$ $L=1.34$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=11.31$ Ncr, $y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr, $z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
Verifica YY: $0.00+0.07=0.07$
Verifica ZZ: $0.00+0.06=0.06$

Asta n. 202 (-14 -13) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND $X_l=1.34$ - Classe 3

Sollecitazioni: $N=-107.35$ $T_z=133.28$ $M_y=-735.47$ $T_y=41.17$ $M_z=167.36$ $M_x=-18.69$
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-83.19$ $\tau=1.11$ $\sigma_{max}=-84.12$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-14.39$ $\tau=3.69$ $\tau_{max}=3.69$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-83.19$ $\tau=1.11$ $\sigma_{ID,max}=84.14$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=868.45$
 $V,Ed=868.45$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=1.34$ - Classe 2
 Sollecitazioni: $N=-379.30$ $T_z=709.89$ $M_y=-2779.21$
 $M_y,Ed=-2779.21$ $M_y,V,c,Rd=42667.60$
 $N,Ed=-379.30$ $N_c,Rd=-392190.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=42667.60$ $M_y,Ed/MN_y,c,Rd=0.07$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $N,Ed=-379.30$ $M_y,Ed=-2779.21$ $M_z,Ed=-0.00$ $L=1.34$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=11.31$ $Ncr,y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ $Ncr,z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.00+0.07=0.07$
 Verifica ZZ: $0.00+0.06=0.06$

Asta n. 202 (-15 -14) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 11 SND $X_l=1.34$ - Classe 3
 Sollecitazioni: $N=-87.49$ $T_z=523.90$ $M_y=-475.27$ $T_y=107.39$ $M_z=112.22$ $M_x=-18.69$
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=-54.13$ $\tau=1.11$ $\sigma_{max}=-54.89$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=-9.65$ $\tau=11.27$ $\tau_{max}=11.27$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=-54.13$ $\tau=1.11$ $\sigma_{ID,max}=54.92$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=2335.68$
 $V,Ed=2335.68$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.02$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=1.34$ - Classe 2
 Sollecitazioni: $N=-379.30$ $T_z=2177.12$ $M_y=-1722.18$
 $M_y,Ed=-1722.18$ $M_y,V,c,Rd=42667.60$
 $N,Ed=-379.30$ $N_c,Rd=-392190.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=42667.60$ $M_y,Ed/MN_y,c,Rd=0.04$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $N,Ed=-379.30$ $M_y,Ed=-1722.18$ $M_z,Ed=-0.00$ $L=1.34$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=11.31$ $Ncr,y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ $Ncr,z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.00+0.04=0.04$
 Verifica ZZ: $0.00+0.04=0.04$

Asta n. 202 (203 -15) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-198.45$ $T_z=1062.52$ $M_y=1382.92$ $T_y=50.94$ $M_z=-52.64$ $M_x=-5.61$
 Tensioni: $\sigma_N=-1.71$ $\sigma_{m,d}=-132.28$ $\tau=0.33$ $\sigma_{max}=-133.99$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.71$ $\sigma_{m,d}=4.53$ $\tau=20.93$ $\tau_{max}=20.93$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.71$ $\sigma_{m,d}=-132.28$ $\tau=0.33$ $\sigma_{ID,max}=133.99$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=3744.63$
 $V,Ed=3744.63$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.03$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $N=-379.30$ $T_z=3744.63$ $M_y=4429.89$
 $M_y,Ed=4429.89$ $M_y,V,c,Rd=42667.60$
 $N,Ed=-379.30$ $N_c,Rd=-392190.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=42667.60$ $M_y,Ed/MN_y,c,Rd=0.10$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $N,Ed=-379.30$ $M_y,Ed=4429.89$ $M_z,Ed=-0.00$ $L=0.85$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=7.15$ $Ncr,y=47013500.00$ $\lambda^*_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.15$ $Ncr,z=47013500.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.00+0.11=0.11$
 Verifica ZZ: $0.00+0.09=0.09$

Asta n. 203 (-16 203) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.49 - Classe 3
 Sollecitazioni: N=-217.22 T_z=-1041.73 M_y=1331.00 T_y=-46.26 M_z=-52.63 M_x=2.07
 Tensioni: σ_N =-1.87 $\sigma_{m,d}$ =-127.50 τ =0.12 σ_{max} =-129.37 (sfrut=0.04)
 Tensioni: σ_N =-1.87 $\sigma_{m,d}$ =4.53 τ =20.31 τ_{max} =20.31 (sfrut=0.01)
 Tensioni: σ_N =-1.87 $\sigma_{m,d}$ =-127.50 τ =0.12 $\sigma_{ID,max}$ =129.37 (sfrut=0.04)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.49 - Classe 2
 Sollecitazioni: T_z=-3646.48
 V,Ed=-3646.48 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.03
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.49 - Classe 2
 Sollecitazioni: N=-211.03 T_z=-3646.48 M_y=4060.54
 M_y,Ed=4060.54 M_y,V,c,Rd=42667.60
 N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MN_y,c,Rd=42667.60 M_y,Ed/MN_y,c,Rd=0.10
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-211.03 M_y,Ed=4060.54 M_z,Ed=-0.00 L=0.49
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =4.16 Ncr,y=139222000.00 λ^*_y =0.05 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =4.16 Ncr,z=139222000.00 λ^*_z =0.05 Curva a: Φ_z =0.00 χ_z =1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.11=0.11
 Verifica ZZ: 0.00+0.08=0.08

Asta n. 203 (-17 -16) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-157.54 T_z=-728.25 M_y=829.23 T_y=-28.36 M_z=-29.85 M_x=2.07
 Tensioni: σ_N =-1.36 $\sigma_{m,d}$ =-79.16 τ =0.12 σ_{max} =-80.52 (sfrut=0.02)
 Tensioni: σ_N =-1.36 $\sigma_{m,d}$ =2.57 τ =14.24 τ_{max} =14.24 (sfrut=0.01)
 Tensioni: σ_N =-1.36 $\sigma_{m,d}$ =-79.16 τ =0.12 $\sigma_{ID,max}$ =80.52 (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 2
 Sollecitazioni: T_z=-2279.53
 V,Ed=-2279.53 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.02
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 2
 Sollecitazioni: N=-211.03 T_z=-2279.53 M_y=2279.85
 M_y,Ed=2279.85 M_y,V,c,Rd=42667.60
 N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MN_y,c,Rd=42667.60 M_y,Ed/MN_y,c,Rd=0.05
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-211.03 M_y,Ed=2279.85 M_z,Ed=-0.00 L=1.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =11.31 Ncr,y=18806100.00 λ^*_y =0.15 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =11.31 Ncr,z=18806100.00 λ^*_z =0.15 Curva a: Φ_z =0.00 χ_z =1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.06=0.06
 Verifica ZZ: 0.00+0.05=0.05

Asta n. 203 (-18 -17) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-65.13 T_z=-159.07 M_y=-432.06 T_y=-28.31 M_z=65.02 M_x=6.89
 Tensioni: σ_N =-0.56 $\sigma_{m,d}$ =-45.80 τ =0.41 σ_{max} =-46.36 (sfrut=0.01)
 Tensioni: σ_N =-0.56 $\sigma_{m,d}$ =-5.59 τ =3.49 τ_{max} =3.49 (sfrut=0.00)
 Tensioni: σ_N =-0.56 $\sigma_{m,d}$ =-45.80 τ =0.41 $\sigma_{ID,max}$ =46.37 (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 2
 Sollecitazioni: T_z=-812.31
 V,Ed=-812.31 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: N=-211.03 T_z=-653.75 M_y=-1649.05
 M_y,Ed=-1649.05 M_y,V,c,Rd=42667.60
 N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MN_y,c,Rd=42667.60 M_y,Ed/MN_y,c,Rd=0.04
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-211.03 M_y,Ed=-1649.05 M_z,Ed=-0.00 L=1.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =11.31 Ncr,y=18806100.00 λ^*_y =0.15 Curva a: Φ_y =0.00 χ_y =1.00
 λ_z =11.31 Ncr,z=18806100.00 λ^*_z =0.15 Curva a: Φ_z =0.00 χ_z =1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04=0.04
 Verifica ZZ: 0.00+0.03=0.03

Asta n. 203 (-19 -18) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-45.27 T_z=109.59 M_y=-432.05 T_y=37.91 M_z=65.02 M_x=6.89
 Tensioni: $\sigma_N=-0.39$ $\sigma_{m,d}=-45.80$ $\tau=0.41$ $\sigma_{max}=-46.19$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.39$ $\sigma_{m,d}=5.59$ $\tau=2.53$ $\tau_{max}=2.53$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.39$ $\sigma_{m,d}=-45.80$ $\tau=0.41$ $\sigma_{ID,max}=46.20$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: T_z=813.49
 V,Ed=813.49 V_c,Rd=113219.00 V,Ed/V_c,Rd=0.01
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 2
 Sollecitazioni: N=-211.03 T_z=654.93 M_y=-1649.01
 M_y,Ed=-1649.01 M_y,V,c,Rd=42667.60
 N,Ed=-211.03 N_c,Rd=-392190.00 YY n=N,Ed/N_c,Rd=0.00 M_{Ny},c,Rd=42667.60 M_y,Ed/M_{Ny},c,Rd=0.04
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-211.03 M_y,Ed=-1649.01 M_z,Ed=0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy}, K_{yz}, K_{zy}, K<sub>zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04=0.04
 Verifica ZZ: 0.00+0.03=0.03</sub>

Asta n. 203 (-20 -19) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-148.93 T_z=727.26 M_y=835.13 T_y=-31.24 M_z=37.57 M_x=-2.07
 Tensioni: $\sigma_N=-1.28$ $\sigma_{m,d}=-80.41$ $\tau=0.12$ $\sigma_{max}=-81.70$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.28$ $\sigma_{m,d}=-3.23$ $\tau=14.22$ $\tau_{max}=14.22$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.28$ $\sigma_{m,d}=-80.41$ $\tau=0.12$ $\sigma_{ID,max}=81.70$ (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: T_z=2280.72
 V,Ed=2280.72 V_c,Rd=113219.00 V,Ed/V_c,Rd=0.02
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: N=-211.03 T_z=2280.72 M_y=2283.03
 M_y,Ed=2283.03 M_y,V,c,Rd=42667.60
 N,Ed=-211.03 N_c,Rd=-392190.00 YY n=N,Ed/N_c,Rd=0.00 M_{Ny},c,Rd=42667.60 M_y,Ed/M_{Ny},c,Rd=0.05
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-211.03 M_y,Ed=2283.03 M_z,Ed=0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy}, K_{yz}, K_{zy}, K<sub>zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.06=0.06
 Verifica ZZ: 0.00+0.05=0.05</sub>

Asta n. 203 (204 -20) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

-
- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-192.76 T_z=933.97 M_y=1020.10 T_y=-44.39 M_z=46.44 M_x=-2.07
 Tensioni: $\sigma_N=-1.66$ $\sigma_{m,d}=-98.28$ $\tau=0.12$ $\sigma_{max}=-99.94$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.66$ $\sigma_{m,d}=-3.99$ $\tau=18.22$ $\tau_{max}=18.22$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.66$ $\sigma_{m,d}=-98.28$ $\tau=0.12$ $\sigma_{ID,max}=99.94$ (sfrut=0.03)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: T_z=3029.15
 V,Ed=3029.15 V_c,Rd=113219.00 V,Ed/V_c,Rd=0.03
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: N=-211.03 T_z=3029.15 M_y=2886.49
 M_y,Ed=2886.49 M_y,V,c,Rd=42667.60
 N,Ed=-211.03 N_c,Rd=-392190.00 YY n=N,Ed/N_c,Rd=0.00 M_{Ny},c,Rd=42667.60 M_y,Ed/M_{Ny},c,Rd=0.07
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-211.03 M_y,Ed=2886.49 M_z,Ed=0.00 L=0.20
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=1.69$ Ncr,y=843496000.00 $\lambda^*_y=0.02$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=1.69$ Ncr,z=843496000.00 $\lambda^*_z=0.02$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95}

Verifica YY: 0.00+0.07=0.08
Verifica ZZ: 0.00+0.06=0.06

Asta n. 204 (204 -21) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

-
- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-192.76 T_z=933.97 M_y=1020.10 T_y=-44.39 M_z=46.44 M_x=-2.07
Tensioni: σ_N=-1.66 σ_{m,d}=-98.28 τ=0.12 σ_{max}=-99.94 (sfrut=0.03)
Tensioni: σ_N=-1.66 σ_{m,d}=-3.99 τ=18.22 τ_{max}=18.22 (sfrut=0.01)
Tensioni: σ_N=-1.66 σ_{m,d}=-98.28 τ=0.12 σ_{ID,max}=99.94 (sfrut=0.03)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: T_z=3029.15
V,Ed=3029.15 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.03
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-211.03 T_z=3029.15 M_y=2886.49
My,Ed=2886.49 My,V,c,Rd=42667.60
N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.07
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-211.03 My,Ed=2886.49 Mz,Ed=-0.00 L=0.20
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=1.69 Ncr,y=843496000.00 λ_y^{*}=0.02 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=1.69 Ncr,z=843496000.00 λ_z^{*}=0.02 Curva a: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.07=0.08
Verifica ZZ: 0.00+0.06=0.06

Asta n. 204 (-21 -22) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

-
- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-148.93 T_z=727.26 M_y=835.13 T_y=-31.24 M_z=37.57 M_x=-2.07
Tensioni: σ_N=-1.28 σ_{m,d}=-80.41 τ=0.12 σ_{max}=-81.70 (sfrut=0.02)
Tensioni: σ_N=-1.28 σ_{m,d}=-3.23 τ=14.22 τ_{max}=14.22 (sfrut=0.01)
Tensioni: σ_N=-1.28 σ_{m,d}=-80.41 τ=0.12 σ_{ID,max}=81.70 (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: T_z=2280.72
V,Ed=2280.72 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.02
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-211.03 T_z=2280.72 M_y=2283.03
My,Ed=2283.03 My,V,c,Rd=42667.60
N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.05
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-211.03 My,Ed=2283.03 Mz,Ed=-0.00 L=1.34
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=11.31 Ncr,y=18806100.00 λ_y^{*}=0.15 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=11.31 Ncr,z=18806100.00 λ_z^{*}=0.15 Curva a: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00+0.05=0.05

Asta n. 204 (-22 -23) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.34 - Classe 3
Sollecitazioni: N=-45.27 T_z=109.59 M_y=-432.05 T_y=37.91 M_z=65.02 M_x=6.89
Tensioni: σ_N=-0.39 σ_{m,d}=-45.80 τ=0.41 σ_{max}=-46.19 (sfrut=0.01)
Tensioni: σ_N=-0.39 σ_{m,d}=5.59 τ=2.53 τ_{max}=2.53 (sfrut=0.00)
Tensioni: σ_N=-0.39 σ_{m,d}=-45.80 τ=0.41 σ_{ID,max}=46.20 (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: T_z=813.49
V,Ed=813.49 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 2
Sollecitazioni: N=-211.03 T_z=654.93 M_y=-1649.01
My,Ed=-1649.01 My,V,c,Rd=42667.60
N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.04
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-211.03 My,Ed=-1649.01 Mz,Ed=-0.00 L=1.34
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=11.31 Ncr,y=18806100.00 λ_y^{*}=0.15 Curva a: Φ_y=0.00 χ_y=1.00

$\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04=0.04
Verifica ZZ: 0.00+0.03=0.03

Asta n. 204 (-23 -24) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-65.13 Tz=-159.07 My=-432.06 Ty=28.31 Mz=-65.02 Mx=-6.89
Tensioni: $\sigma_N=-0.56$ $\sigma_{m,d}=-45.80$ $\tau=0.41$ $\sigma_{max}=-46.36$ (sfrut=0.01)
Tensioni: $\sigma_N=-0.56$ $\sigma_{m,d}=-5.59$ $\tau=3.49$ $\tau_{max}=3.49$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.56$ $\sigma_{m,d}=-45.80$ $\tau=0.41$ $\sigma_{ID,max}=46.37$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 2
Sollecitazioni: Tz=-812.30
V,Ed=-812.30 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-211.03 Tz=-653.74 My=-1649.06
My,Ed=-1649.06 My,V,c,Rd=42667.60
N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.04
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-211.03 My,Ed=-1649.06 Mz,Ed=0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04=0.04
Verifica ZZ: 0.00+0.03=0.03

Asta n. 204 (-24 -25) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

-
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.34 - Classe 3
Sollecitazioni: N=-157.54 Tz=-728.24 My=829.23 Ty=28.36 Mz=29.85 Mx=-2.07
Tensioni: $\sigma_N=-1.36$ $\sigma_{m,d}=-79.16$ $\tau=0.12$ $\sigma_{max}=-80.52$ (sfrut=0.02)
Tensioni: $\sigma_N=-1.36$ $\sigma_{m,d}=2.57$ $\tau=14.24$ $\tau_{max}=14.24$ (sfrut=0.01)
Tensioni: $\sigma_N=-1.36$ $\sigma_{m,d}=-79.16$ $\tau=0.12$ $\sigma_{ID,max}=80.52$ (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 2
Sollecitazioni: Tz=-2279.53
V,Ed=-2279.53 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.02
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 2
Sollecitazioni: N=-211.03 Tz=-2279.53 My=2279.83
My,Ed=2279.83 My,V,c,Rd=42667.60
N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.05
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-211.03 My,Ed=2279.83 Mz,Ed=0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00+0.05=0.05

Asta n. 204 (-25 205) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

-
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.49 - Classe 3
Sollecitazioni: N=-217.22 Tz=-1041.73 My=1331.00 Ty=46.26 Mz=52.63 Mx=-2.07
Tensioni: $\sigma_N=-1.87$ $\sigma_{m,d}=-127.49$ $\tau=0.12$ $\sigma_{max}=-129.37$ (sfrut=0.04)
Tensioni: $\sigma_N=-1.87$ $\sigma_{m,d}=4.53$ $\tau=20.31$ $\tau_{max}=20.31$ (sfrut=0.01)
Tensioni: $\sigma_N=-1.87$ $\sigma_{m,d}=-127.49$ $\tau=0.12$ $\sigma_{ID,max}=129.37$ (sfrut=0.04)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.49 - Classe 2
Sollecitazioni: Tz=-3646.48
V,Ed=-3646.48 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.03
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.49 - Classe 2
Sollecitazioni: N=-211.03 Tz=-3646.48 My=4060.52
My,Ed=4060.52 My,V,c,Rd=42667.60
N,Ed=-211.03 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.10
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-211.03 My,Ed=4060.52 Mz,Ed=0.00 L=0.49

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=4.16$ Ncr,y=139222000.00 $\lambda^*_y=0.05$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=4.16$ Ncr,z=139222000.00 $\lambda^*_z=0.05$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.11=0.11
 Verifica ZZ: 0.00+0.08=0.08

Asta n. 205 (205 -26) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-198.44 Tz=1062.52 My=1382.91 Ty=-50.94 Mz=52.64 Mx=5.61
 Tensioni: $\sigma_N=-1.71$ $\sigma_{m,d}=-132.28$ $\tau=0.33$ $\sigma_{max}=-133.99$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.71$ $\sigma_{m,d}=4.53$ $\tau=20.93$ $\tau_{max}=20.93$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.71$ $\sigma_{m,d}=-132.28$ $\tau=0.33$ $\sigma_{ID,max}=133.99$ (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=3744.63
 V,Ed=3744.63 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.03
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: N=-379.29 Tz=3744.63 My=4429.86
 My,Ed=4429.86 My,V,c,Rd=42667.60
 N,Ed=-379.29 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.10
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-379.29 My,Ed=4429.86 Mz,Ed=0.00 L=0.85
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=7.15$ Ncr,y=47013300.00 $\lambda^*_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.15$ Ncr,z=47013300.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.11=0.12
 Verifica ZZ: 0.00+0.09=0.09

Asta n. 205 (-26 -27) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-87.48 Tz=523.91 My=-475.24 Ty=107.39 Mz=112.21 Mx=-18.69
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=-54.13$ $\tau=1.11$ $\sigma_{max}=-54.89$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=-9.65$ $\tau=11.27$ $\tau_{max}=11.27$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=-54.13$ $\tau=1.11$ $\sigma_{ID,max}=54.92$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=2335.68
 V,Ed=2335.68 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.02
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 2
 Sollecitazioni: N=-379.29 Tz=2177.12 My=-1722.04
 My,Ed=-1722.04 My,V,c,Rd=42667.60
 N,Ed=-379.29 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.04
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-379.29 My,Ed=-1722.04 Mz,Ed=0.00 L=1.34
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04=0.05
 Verifica ZZ: 0.00+0.04=0.04

Asta n. 205 (-27 -28) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-107.35 Tz=133.28 My=-735.47 Ty=-41.17 Mz=-167.36 Mx=18.69
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-83.19$ $\tau=1.11$ $\sigma_{max}=-84.12$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-14.39$ $\tau=3.69$ $\tau_{max}=3.69$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-83.19$ $\tau=1.11$ $\sigma_{ID,max}=84.14$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=868.45
 V,Ed=868.45 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 2
 Sollecitazioni: N=-379.29 Tz=709.89 My=-2779.23
 My,Ed=-2779.23 My,V,c,Rd=42667.60
 N,Ed=-379.29 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.07

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-379.29 My,Ed=-2779.23 Mz,Ed=0.00 L=1.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.07=0.07
Verifica ZZ: 0.00+0.06=0.06

Asta n. 205 (-28 -29) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-127.22 Tz=-135.38 My=-735.47 Ty=25.05 Mz=-167.36 Mx=18.69
Tensioni: $\sigma_N=-1.10$ $\sigma_{m,d}=-83.19$ $\tau=1.11$ $\sigma_{max}=-84.29$ (sfrut=0.02)
Tensioni: $\sigma_N=-1.10$ $\sigma_{m,d}=14.39$ $\tau=3.73$ $\tau_{max}=3.73$ (sfrut=0.00)
Tensioni: $\sigma_N=-1.10$ $\sigma_{m,d}=-83.19$ $\tau=1.11$ $\sigma_{ID,max}=84.31$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 2
Sollecitazioni: Tz=-757.34
V,Ed=-757.34 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-379.29 Tz=-598.78 My=-2779.20
My,Ed=-2779.20 My,V,c,Rd=42667.60
N,Ed=-379.29 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.07

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-379.29 My,Ed=-2779.20 Mz,Ed=0.00 L=1.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.07=0.07
Verifica ZZ: 0.00+0.06=0.06

Asta n. 205 (-29 -30) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-50.29 Tz=-493.31 My=-508.14 Ty=-91.27 Mz=133.81 Mx=-18.69
Tensioni: $\sigma_N=-0.43$ $\sigma_{m,d}=-59.15$ $\tau=1.11$ $\sigma_{max}=-59.59$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.43$ $\sigma_{m,d}=11.51$ $\tau=10.67$ $\tau_{max}=10.67$ (sfrut=0.01)
Tensioni: $\sigma_N=-0.43$ $\sigma_{m,d}=-59.15$ $\tau=1.11$ $\sigma_{ID,max}=59.62$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 2
Sollecitazioni: Tz=-2224.57
V,Ed=-2224.57 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.02
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-379.29 Tz=-2066.01 My=-1871.01
My,Ed=-1871.01 My,V,c,Rd=42667.60
N,Ed=-379.29 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.04

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-379.29 My,Ed=-1871.01 Mz,Ed=0.00 L=1.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00+0.04=0.04

Asta n. 205 (-30 -31) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.89 - Classe 3
Sollecitazioni: N=-322.76 Tz=-1035.93 My=1293.55 Ty=46.21 Mz=37.71 Mx=5.61
Tensioni: $\sigma_N=-2.78$ $\sigma_{m,d}=-122.67$ $\tau=0.33$ $\sigma_{max}=-125.45$ (sfrut=0.04)
Tensioni: $\sigma_N=-2.78$ $\sigma_{m,d}=-3.24$ $\tau=20.41$ $\tau_{max}=20.41$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.78$ $\sigma_{m,d}=-122.67$ $\tau=0.33$ $\sigma_{ID,max}=125.45$ (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.89 - Classe 2
Sollecitazioni: Tz=-3638.74
V,Ed=-3638.74 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.03
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.89 - Classe 2
Sollecitazioni: N=-379.29 Tz=-3638.74 My=4198.22
My,Ed=4198.22 My,V,c,Rd=42667.60

N,Ed=-379.29 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-379.29 My,Ed=4198.22 Mz,Ed=0.00 L=0.89
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=7.52$ Ncr,y=42486200.00 $\lambda^*_y=0.10$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.52$ Ncr,z=42486200.00 $\lambda^*_z=0.10$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.11=0.11
Verifica ZZ: 0.00+0.09=0.09

Asta n. 206 (-31 -32) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-95.88 Tz=1058.27 My=1296.73 Ty=-44.01 Mz=37.67 Mx=19.62
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=-122.96$ $\tau=1.17$ $\sigma_{max}=-123.78$ (sfrut=0.04)
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=3.24$ $\tau=21.68$ $\tau_{max}=21.68$ (sfrut=0.01)
Tensioni: $\sigma_N=-0.83$ $\sigma_{m,d}=-122.96$ $\tau=1.17$ $\sigma_{ID,max}=123.80$ (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: Tz=3504.69
V,Ed=3504.69 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.03
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-175.04 Tz=3504.69 My=3745.62
My,Ed=3745.62 My,V,c,Rd=42667.60
N,Ed=-175.04 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-175.04 My,Ed=3745.62 Mz,Ed=0.00 L=0.45
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.78$ Ncr,y=167888000.00 $\lambda^*_y=0.05$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=3.78$ Ncr,z=167888000.00 $\lambda^*_z=0.05$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.10=0.10
Verifica ZZ: 0.00+0.08=0.08

Asta n. 206 (-32 -33) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-36.54 Tz=748.79 My=831.46 Ty=-26.21 Mz=17.94 Mx=19.62
Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=-78.27$ $\tau=1.17$ $\sigma_{max}=-78.58$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=1.54$ $\tau=15.68$ $\tau_{max}=15.68$ (sfrut=0.01)
Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=-78.27$ $\tau=1.17$ $\sigma_{ID,max}=78.61$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: Tz=2142.95
V,Ed=2142.95 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.02
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: N=-175.04 Tz=2142.95 My=2186.36
My,Ed=2186.36 My,V,c,Rd=42667.60
N,Ed=-175.04 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-175.04 My,Ed=2186.36 Mz,Ed=0.00 L=1.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00+0.05=0.05

Asta n. 206 (-33 -34) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.34 - Classe 3
Sollecitazioni: N=29.68 Tz=236.20 My=-487.84 Ty=-6.34 Mz=-25.65 Mx=19.62
Tensioni: $\sigma_N=0.26$ $\sigma_{m,d}=47.32$ $\tau=1.17$ $\sigma_{max}=47.57$ (sfrut=0.01)
Tensioni: $\sigma_N=0.26$ $\sigma_{m,d}=-2.21$ $\tau=5.74$ $\tau_{max}=5.74$ (sfrut=0.00)
Tensioni: $\sigma_N=0.26$ $\sigma_{m,d}=47.32$ $\tau=1.17$ $\sigma_{ID,max}=47.61$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: Tz=675.73
V,Ed=675.73 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 2

Sollecitazioni: N=-175.04 T_z=517.17 M_y=-1376.63
 My,Ed=-1376.63 My,V,c,Rd=42667.60
 N,Ed=-175.04 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-175.04 My,Ed=-1376.63 Mz,Ed=0.00 L=1.34
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=11.31 Ncr,y=18806000.00 λ_y^{*}=0.15 Curva a: Φ_y=0.00 χ_y=1.00
 λ_z=11.31 Ncr,z=18806000.00 λ_z^{*}=0.15 Curva a: Φ_z=0.00 χ_z=1.00
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04=0.04
 Verifica ZZ: 0.00+0.03=0.03

Asta n. 206 (-34 -35) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=95.89 T_z=-32.46 M_y=-487.83 T_y=-13.52 M_z=25.65 M_x=-19.62
 Tensioni: σ_N=0.83 σ_{m,d}=47.32 τ=1.17 σ_{max}=48.14 (sfrut=0.01)
 Tensioni: σ_N=0.83 σ_{m,d}=2.21 τ=1.80 τ_{max}=1.80 (sfrut=0.00)
 Tensioni: σ_N=0.83 σ_{m,d}=47.32 τ=1.17 σ_{ID,max}=48.18 (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 2
 Sollecitazioni: T_z=-950.06
 V,Ed=-950.06 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: N=-175.04 T_z=-791.50 M_y=-1376.62
 My,Ed=-1376.62 My,V,c,Rd=42667.60
 N,Ed=-175.04 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-175.04 My,Ed=-1376.62 Mz,Ed=0.00 L=1.34
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=11.31 Ncr,y=18806100.00 λ_y^{*}=0.15 Curva a: Φ_y=0.00 χ_y=1.00
 λ_z=11.31 Ncr,z=18806100.00 λ_z^{*}=0.15 Curva a: Φ_z=0.00 χ_z=1.00
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04=0.04
 Verifica ZZ: 0.00+0.03=0.03

Asta n. 206 (-35 -36) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.53 - Classe 3
 Sollecitazioni: N=-242.98 T_z=-755.13 M_y=680.59 T_y=31.52 M_z=9.28 M_x=19.62
 Tensioni: σ_N=-2.09 σ_{m,d}=-63.57 τ=1.17 σ_{max}=-65.66 (sfrut=0.02)
 Tensioni: σ_N=-2.09 σ_{m,d}=-0.80 τ=15.80 τ_{max}=15.80 (sfrut=0.01)
 Tensioni: σ_N=-2.09 σ_{m,d}=-63.57 τ=1.17 σ_{ID,max}=65.69 (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.53 - Classe 2
 Sollecitazioni: T_z=-2321.88
 V,Ed=-2321.88 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.02
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.53 - Classe 2
 Sollecitazioni: N=-175.04 T_z=-2321.88 M_y=1011.51
 My,Ed=1011.51 My,V,c,Rd=42667.60
 N,Ed=-175.04 Nc,Rd=-392190.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=42667.60 My,Ed/MNy,c,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-175.04 My,Ed=1011.51 Mz,Ed=0.00 L=0.53
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=4.50 Ncr,y=118573000.00 λ_y^{*}=0.06 Curva a: Φ_y=0.00 χ_y=1.00
 λ_z=4.50 Ncr,z=118573000.00 λ_z^{*}=0.06 Curva a: Φ_z=0.00 χ_z=1.00
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03=0.03
 Verifica ZZ: 0.00+0.02=0.02

Asta n. 206 (-36 -37) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=11.45 T_z=261.89 M_y=181.50 T_y=-38.17 M_z=30.77
 Tensioni: σ_N=0.10 σ_{m,d}=19.56 τ=0.00 σ_{max}=19.66 (sfrut=0.01)
 Tensioni: σ_N=0.10 σ_{m,d}=2.65 τ=5.08 τ_{max}=5.08 (sfrut=0.00)
 Tensioni: σ_N=0.10 σ_{m,d}=19.56 τ=0.00 σ_{ID,max}=19.66 (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 2
 Sollecitazioni: T_z=820.16
 V,Ed=820.16 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 2
Sollecitazioni: $T_z=820.16$ $M_y=622.60$
 $M_y, Ed=622.60$ $M_y, V, c, Rd=42667.60$ $M_y, Ed/M_y, V, c, Rd=0.01$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 15 SND - Classe 3
Sollecitazioni: $N, Ed=-11.45$ $M_y, Ed=181.50$ $M_z, Ed=-30.77$ $L=0.81$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=6.80$ $N_{cr,y}=51935500.00$ $\lambda^*_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.80$ $N_{cr,z}=51935500.00$ $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.00+0.00=0.01$
Verifica ZZ: $0.00+0.00+0.00=0.00$

Asta n. 302 (-4 -47) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=-2.78$ $T_z=94.25$ $M_y=81.91$ $T_y=-9.26$ $M_z=13.89$
Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.56$ $\tau=0.00$ $\sigma_{max}=-55.62$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=7.99$ $\tau=3.93$ $\tau_{max}=3.93$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.56$ $\tau=0.00$ $\sigma_{ID,max}=55.62$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: $T_z=362.38$
 $V, Ed=362.38$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: $T_z=362.38$ $M_y=353.55$
 $M_y, Ed=353.55$ $M_y, V, c, Rd=7590.24$ $M_y, Ed/M_y, V, c, Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N, Ed=-2.78$ $M_y, Ed=81.91$ $M_z, Ed=13.89$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.01+0.00=0.02$
Verifica ZZ: $0.00+0.01+0.00=0.01$

Asta n. 302 (-46 -4) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: $N=2.78$ $T_z=-94.25$ $M_y=81.91$ $T_y=9.26$ $M_z=13.89$
Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.56$ $\tau=0.00$ $\sigma_{max}=55.62$ (sfrut=0.02)
Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=7.99$ $\tau=3.93$ $\tau_{max}=3.93$ (sfrut=0.00)
Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.56$ $\tau=0.00$ $\sigma_{ID,max}=55.62$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: $T_z=-362.38$
 $V, Ed=-362.38$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: $T_z=-362.38$ $M_y=353.55$
 $M_y, Ed=353.55$ $M_y, V, c, Rd=7590.24$ $M_y, Ed/M_y, V, c, Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: $N, Ed=-2.78$ $M_y, Ed=81.91$ $M_z, Ed=13.89$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.01+0.00=0.02$
Verifica ZZ: $0.00+0.01+0.00=0.01$

Asta n. 303 (-6 -48) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=-4.18$ $T_z=134.33$ $M_y=123.20$ $T_y=-13.92$ $M_z=20.88$
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: $T_z=654.34$
 $V, Ed=654.34$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_z=654.34$ $M_y=654.29$
 $M_y, Ed=654.29$ $M_y, V, c, Rd=7590.24$ $M_y, Ed/M_y, V, c, Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed=-4.18$ $M_y, Ed=123.20$ $M_z, Ed=20.88$ $L=1.50$
 $\alpha_m, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr, y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr, z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$
- Asta n. 303 (-49 -6) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: $N=4.18$ $T_z=-134.33$ $M_y=123.20$ $T_y=13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m, d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m, d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m, d}=83.57$ $\tau=0.00$ $\sigma_{ID, max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-654.34$
 $V, Ed=-654.34$ $Vc, Rd=53876.60$ $V, Ed/Vc, Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-654.34$ $M_y=654.29$
 $M_y, Ed=654.29$ $M_y, V, c, Rd=7590.24$ $M_y, Ed/M_y, V, c, Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N, Ed=-4.18$ $M_y, Ed=123.20$ $M_z, Ed=20.88$ $L=1.50$
 $\alpha_m, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr, y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr, z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$
- Asta n. 304 (-7 -96) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-4.18$ $T_z=134.33$ $M_y=123.20$ $T_y=-13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m, d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m, d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m, d}=-83.57$ $\tau=0.00$ $\sigma_{ID, max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_z=654.34$
 $V, Ed=654.34$ $Vc, Rd=53876.60$ $V, Ed/Vc, Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_z=654.34$ $M_y=654.29$
 $M_y, Ed=654.29$ $M_y, V, c, Rd=7590.24$ $M_y, Ed/M_y, V, c, Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed=-4.18$ $M_y, Ed=123.20$ $M_z, Ed=20.88$ $L=1.50$
 $\alpha_m, \alpha_mz, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr, y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr, z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$
- Asta n. 304 (-95 -7) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: $N=4.18$ $T_z=-134.33$ $M_y=123.20$ $T_y=13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m, d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m, d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m, d}=83.57$ $\tau=0.00$ $\sigma_{ID, max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-654.34$
 $V, Ed=-654.34$ $Vc, Rd=53876.60$ $V, Ed/Vc, Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: $T_z=-654.34$ $M_y=654.29$
 $M_y,Ed=654.29$ $M_y,V,c,Rd=7590.24$ $M_y,Ed/M_y,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-4.18$ $M_y,Ed=123.20$ $M_z,Ed=20.88$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 305 (-8 -66) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-4.18$ $T_z=134.33$ $M_y=123.20$ $T_y=-13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=654.34$
 $V,Ed=654.34$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=654.34$ $M_y=654.29$
 $M_y,Ed=654.29$ $M_y,V,c,Rd=7590.24$ $M_y,Ed/M_y,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-4.18$ $M_y,Ed=123.20$ $M_z,Ed=20.88$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 305 (-67 -8) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=4.18$ $T_z=-134.33$ $M_y=123.20$ $T_y=13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-654.34$
 $V,Ed=-654.34$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-654.34$ $M_y=654.29$
 $M_y,Ed=654.29$ $M_y,V,c,Rd=7590.24$ $M_y,Ed/M_y,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-4.18$ $M_y,Ed=123.20$ $M_z,Ed=20.88$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

Asta n. 306 (-9 -69) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-4.18$ $T_z=134.33$ $M_y=123.20$ $T_y=-13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=654.34$
 $V,Ed=654.34$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=654.34$ $M_y=654.29$

My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 306 (-68 -9) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 307 (-11 -70) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 307 (-71 -11) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 308 (-12 -72) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: Tz=654.34
V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: Tz=654.34 My=654.29
My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 308 (-73 -12) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: Tz=-654.34
V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: Tz=-654.34 My=654.29
My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 309 (-13 -74) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: Tz=654.34
V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: Tz=654.34 My=654.29
My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 309 (-75 -13) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 $T_z=-134.33$ $M_y=123.20$ $T_y=13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-654.34$
 $V,Ed=-654.34$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-654.34$ $M_y=654.29$
 $My,Ed=654.29$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 310 (-14 -90) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 $T_z=134.33$ $M_y=123.20$ $T_y=-13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_z=654.34$
 $V,Ed=654.34$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_z=654.34$ $M_y=654.29$
 $My,Ed=654.29$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 310 (-91 -14) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 $T_z=-134.33$ $M_y=123.20$ $T_y=13.92$ $M_z=20.88$
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-654.34$
 $V,Ed=-654.34$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-654.34$ $M_y=654.29$
 $My,Ed=654.29$ $My,V,c,Rd=7590.24$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 311 (-15 -92) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09 \sigma_{m,d}=-83.57 \tau=0.00 \sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09 \sigma_{m,d}=12.01 \tau=5.59 \tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09 \sigma_{m,d}=-83.57 \tau=0.00 \sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 311 (-93 -15) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09 \sigma_{m,d}=83.57 \tau=0.00 \sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09 \sigma_{m,d}=12.01 \tau=5.59 \tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09 \sigma_{m,d}=83.57 \tau=0.00 \sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 312 (-16 -98) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09 \sigma_{m,d}=-83.57 \tau=0.00 \sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09 \sigma_{m,d}=12.01 \tau=5.59 \tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09 \sigma_{m,d}=-83.57 \tau=0.00 \sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 312 (-94 -16) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 313 (-17 -97) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 313 (-42 -17) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 314 (-18 -43) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 314 (-44 -18) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 315 (-19 -45) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 315 (-58 -19) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 316 (-20 -63) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2.78 Tz=94.25 My=81.91 Ty=-9.26 Mz=13.89
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.56$ $\tau=0.00$ $\sigma_{max}=-55.62$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=7.99$ $\tau=3.93$ $\tau_{max}=3.93$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.56$ $\tau=0.00$ $\sigma_{ID,max}=55.62$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=362.38
 V,Ed=362.38 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=362.38 My=353.55
 My,Ed=353.55 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.00=0.02
 Verifica ZZ: 0.00+0.01+0.00=0.01

Asta n. 316 (-65 -20) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=2.78 Tz=-94.25 My=81.91 Ty=9.26 Mz=13.89
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.56$ $\tau=0.00$ $\sigma_{max}=55.62$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=7.99$ $\tau=3.93$ $\tau_{max}=3.93$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.56$ $\tau=0.00$ $\sigma_{ID,max}=55.62$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-362.38
 V,Ed=-362.38 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-362.38 My=353.55
 My,Ed=353.55 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.00=0.02
 Verifica ZZ: 0.00+0.01+0.00=0.01

Asta n. 317 (-21 -51) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2.78 Tz=94.25 My=81.91 Ty=-9.26 Mz=13.89
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.56$ $\tau=0.00$ $\sigma_{max}=-55.62$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=7.99$ $\tau=3.93$ $\tau_{max}=3.93$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.56$ $\tau=0.00$ $\sigma_{ID,max}=55.62$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=362.38
 V,Ed=362.38 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=362.38 My=353.55
 My,Ed=353.55 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.05
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.00=0.02
 Verifica ZZ: 0.00+0.01+0.00=0.01

Asta n. 317 (-50 -21) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=2.78 Tz=-94.25 My=81.91 Ty=9.26 Mz=13.89
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.56$ $\tau=0.00$ $\sigma_{max}=55.62$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=7.99$ $\tau=3.93$ $\tau_{max}=3.93$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.56$ $\tau=0.00$ $\sigma_{ID,max}=55.62$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-362.38
 V,Ed=-362.38 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-362.38 My=353.55
 My,Ed=353.55 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.05
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr, $y=1241570.00$ $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr, $z=640515.00$ $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.00=0.02
 Verifica ZZ: 0.00+0.01+0.00=0.01

Asta n. 318 (-22 -53) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 318 (-52 -22) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 319 (-23 -55) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 319 (-54 -23) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 320 (-24 -57) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 320 (-56 -24) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 322 (-25 -41) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 322 (-64 -25) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 323 (-26 -77) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 323 (-76 -26) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 324 (-27 -79) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 324 (-78 -27) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 325 (-28 -81) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 325 (-80 -28) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 326 (-29 -83) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 326 (-82 -29) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 327 (-30 -85) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 327 (-84 -30) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 329 (-32 -86) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 329 (-87 -32) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 330 (-33 -89) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 330 (-88 -33) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 331 (-34 -61) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 331 (-62 -34) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 Tz=-134.33 My=123.20 Ty=13.92 Mz=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda_y^*=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda_z^*=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 332 (-35 -102) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-4.18 Tz=134.33 My=123.20 Ty=-13.92 Mz=20.88
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{max}=-83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.09$ $\sigma_{m,d}=-83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34
 V,Ed=654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=654.34 My=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 332 (-101 -35) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=4.18 T_z=-134.33 M_y=123.20 T_y=13.92 M_z=20.88
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{max}=83.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=12.01$ $\tau=5.59$ $\tau_{max}=5.59$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.09$ $\sigma_{m,d}=83.57$ $\tau=0.00$ $\sigma_{ID,max}=83.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-654.34
 V,Ed=-654.34 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-654.34 M_y=654.29
 My,Ed=654.29 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

Asta n. 333 (-37 -103) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2.78 T_z=94.25 M_y=81.91 T_y=-9.26 M_z=13.89
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.56$ $\tau=0.00$ $\sigma_{max}=-55.62$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=7.99$ $\tau=3.93$ $\tau_{max}=3.93$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-55.56$ $\tau=0.00$ $\sigma_{ID,max}=55.62$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=362.38
 V,Ed=362.38 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=362.38 M_y=353.55
 My,Ed=353.55 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=1.50
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.00=0.02
 Verifica ZZ: 0.00+0.01+0.00=0.01

Asta n. 333 (-104 -37) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=2.78 T_z=-94.25 M_y=81.91 T_y=9.26 M_z=13.89
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.56$ $\tau=0.00$ $\sigma_{max}=55.62$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=7.99$ $\tau=3.93$ $\tau_{max}=3.93$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.06$ $\sigma_{m,d}=55.56$ $\tau=0.00$ $\sigma_{ID,max}=55.62$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-362.38
 V,Ed=-362.38 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-362.38 M_y=353.55
 My,Ed=353.55 My,V,c,Rd=7590.24 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=1.50

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.00=0.02
 Verifica ZZ: 0.00+0.01+0.00=0.01

Membratura

Asta 201 Nodi -4 -5 -6 -7 -8 -9 -10 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-175.04 My,Ed=0.00 L=5.81

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=49.01$ Ncr,y=1000880.00 $\lambda^*_y=0.64$ Curva a: $\Phi_y=0.75$ $\chi_y=0.87$
 $\lambda_z=49.01$ Ncr,z=1000880.00 $\lambda^*_z=0.64$ Curva a: $\Phi_z=0.75$ $\chi_z=0.87$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.10=0.10
 Verifica ZZ: 0.00+0.08=0.08

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,G}=0.03$ (L/19069)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,G}=0.05$ (L/11966)

Membratura

Asta 202 Nodi -10 -11 -12 -13 -14 -15 203 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-379.30 My,Ed=4429.89 Mz,Ed=0.00 L=7.10

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=59.90$ Ncr,y=670055.00 $\lambda^*_y=0.78$ Curva a: $\Phi_y=0.87$ $\chi_y=0.80$
 $\lambda_z=59.90$ Ncr,z=670055.00 $\lambda^*_z=0.78$ Curva a: $\Phi_z=0.87$ $\chi_z=0.80$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.11=0.12
 Verifica ZZ: 0.00+0.09=0.09

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.12$ (L/5841)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.20$ (L/3578)

Membratura

Asta 203 Nodi 203 -16 -17 -18 -19 -20 204 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-211.03 My,Ed=4060.54 Mz,Ed=0.00 L=6.05

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=51.07$ Ncr,y=921780.00 $\lambda^*_y=0.67$ Curva a: $\Phi_y=0.77$ $\chi_y=0.86$
 $\lambda_z=51.07$ Ncr,z=921780.00 $\lambda^*_z=0.67$ Curva a: $\Phi_z=0.77$ $\chi_z=0.86$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.11=0.11
 Verifica ZZ: 0.00+0.08=0.08

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/14426)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.07$ (L/8835)

Membratura

Asta 204 Nodi 204 -21 -22 -23 -24 -25 205 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-211.03 My,Ed=4060.52 Mz,Ed=0.00 L=6.05

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=51.07$ Ncr,y=921780.00 $\lambda^*_y=0.67$ Curva a: $\Phi_y=0.77$ $\chi_y=0.86$
 $\lambda_z=51.07$ Ncr,z=921780.00 $\lambda^*_z=0.67$ Curva a: $\Phi_z=0.77$ $\chi_z=0.86$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.11=0.11
 Verifica ZZ: 0.00+0.08=0.08

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/14426)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,l}=0.07$ (L/8832)

Membratura

Asta 205 Nodi 205 -26 -27 -28 -29 -30 -31 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-379.29 My,Ed=4429.86 Mz,Ed=0.00 L=7.10
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=59.90$ Ncr, $y=670055.00$ $\lambda^*_y=0.78$ Curva a: $\Phi_y=0.87$ $\chi_y=0.80$
 $\lambda_z=59.90$ Ncr, $z=670055.00$ $\lambda^*_z=0.78$ Curva a: $\Phi_z=0.87$ $\chi_z=0.80$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.11=0.12
Verifica ZZ: 0.00+0.09=0.09

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,l}=0.12$ (L/5840)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,l}=0.20$ (L/3578)

Membratura

Asta 206 Nodi -31 -32 -33 -34 -35 -36 -37 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-175.04 My,Ed=3745.62 Mz,Ed=0.00 L=5.81
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=49.01$ Ncr, $y=1000880.00$ $\lambda^*_y=0.64$ Curva a: $\Phi_y=0.75$ $\chi_y=0.87$
 $\lambda_z=49.01$ Ncr, $z=1000880.00$ $\lambda^*_z=0.64$ Curva a: $\Phi_z=0.75$ $\chi_z=0.87$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.10=0.10
Verifica ZZ: 0.00+0.08=0.08

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,g}=0.03$ (L/19069)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,g}=0.05$ (L/11966)

Membratura

Asta 302 Nodi -47 -4 -46 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.00=0.02
Verifica ZZ: 0.00+0.01+0.00=0.01

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,l}=0.04$ (L/7888)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,l}=0.06$ (L/5343)

Membratura

Asta 303 Nodi -48 -6 -49 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,l}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,l}=0.10$ (L/2883)

Membratura

Asta 304 Nodi -96 -7 -95 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 305 Nodi -66 -8 -67 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 306 Nodi -69 -9 -68 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 307 Nodi -70 -11 -71 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.00=0.02$
 Verifica ZZ: $0.00+0.02+0.00=0.02$

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 308 Nodi -72 -12 -73 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 309 Nodi -74 -13 -75 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 310 Nodi -90 -14 -91 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3944)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2884)

Membratura

Asta 311 Nodi -92 -15 -93 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3944)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2884)

Membratura

Asta 312 Nodi -98 -16 -94 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02

Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 313 Nodi -97 -17 -42 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 314 Nodi -43 -18 -44 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 315 Nodi -45 -19 -58 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 316 Nodi -63 -20 -65 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.00=0.02
Verifica ZZ: 0.00+0.01+0.00=0.01

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/7893)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.06$ (L/5345)

Membratura

Asta 317 Nodi -51 -21 -50 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.00=0.02
 Verifica ZZ: 0.00+0.01+0.00=0.01

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/7893)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.06$ (L/5345)

Membratura

Asta 318 Nodi -53 -22 -52 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 319 Nodi -55 -23 -54 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 320 Nodi -57 -24 -56 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 322 Nodi -41 -25 -64 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 323 Nodi -77 -26 -76 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3944)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2884)

Membratura

Asta 324 Nodi -79 -27 -78 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3944)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2884)

Membratura

Asta 325 Nodi -81 -28 -80 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.00=0.02
Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 326 Nodi -83 -29 -82 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

$\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 327 Nodi -85 -30 -84 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 329 Nodi -86 -32 -87 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 330 Nodi -89 -33 -88 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02
 Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 331 Nodi -61 -34 -62 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.00=0.02

Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2882)

Membratura

Asta 332 Nodi -102 -35 -101 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-4.18 My,Ed=123.20 Mz,Ed=20.88 L=3.00

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$

$\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.00=0.02

Verifica ZZ: 0.00+0.02+0.00=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.08$ (L/3943)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.10$ (L/2883)

Membratura

Asta 333 Nodi -103 -37 -104 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-2.78 My,Ed=81.91 Mz,Ed=13.89 L=3.00

$\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$

$\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.01+0.00=0.02

Verifica ZZ: 0.00+0.01+0.00=0.01

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,L}=0.04$ (L/7888)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,L}=0.06$ (L/5343)

5.4 Tracker 2x28 - configurazione in esercizio ($\alpha = 60^\circ$)

5.4.1 Diagrammi tassi di sfruttamento

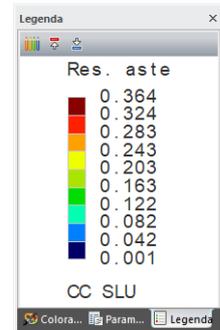
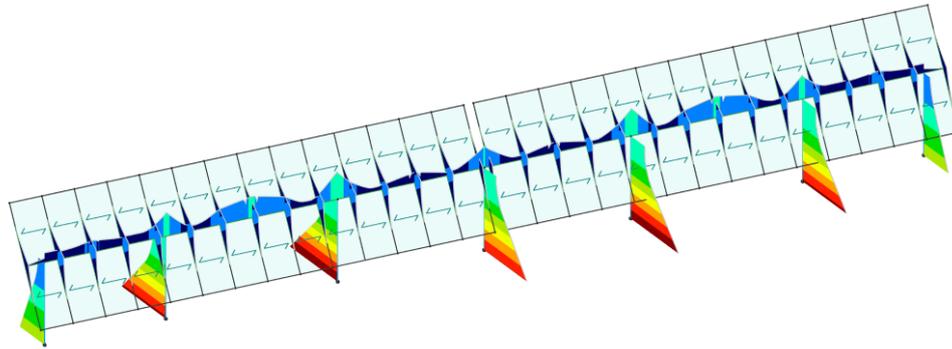


Diagramma tassi di sfruttamento resistenza aste combo SLU con valore massimo pari a 0,364

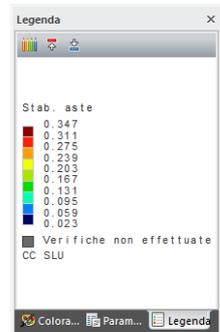
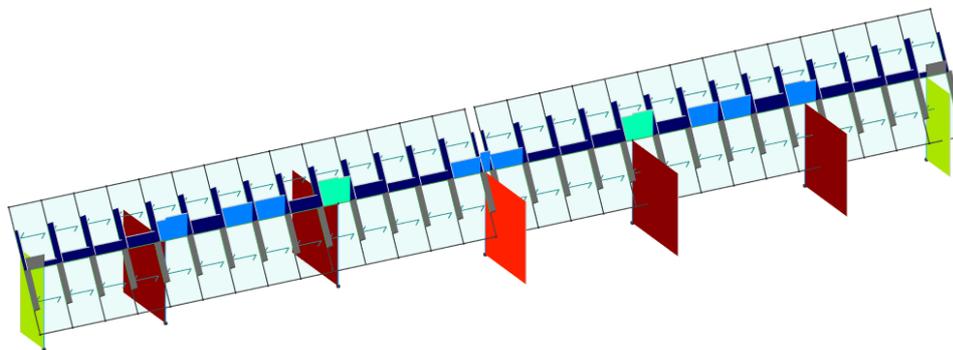


Diagramma tassi di sfruttamento stabilità aste combo SLU con valore massimo pari a 0,347

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

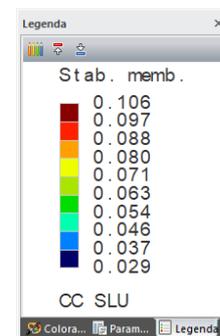
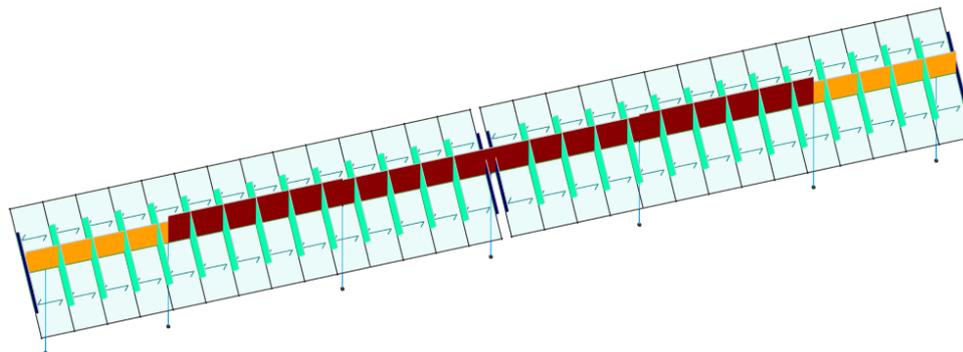


Diagramma tassi di sfruttamento stabilità membrature combo SLU con valore massimo pari a 0,106

Figure 16: Tassi di sfruttamento SLU (Stato limite ultimo)

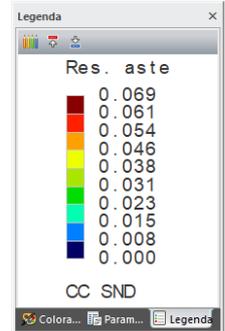
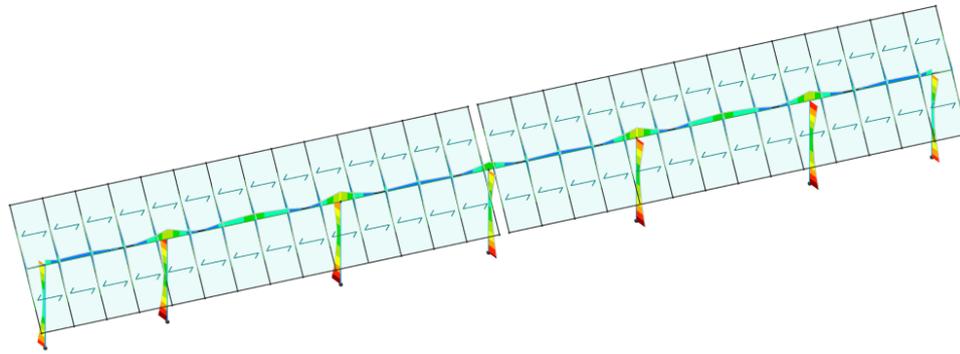


Diagramma tassi di sfruttamento resistenza aste combo SND con valore massimo pari a 0,069

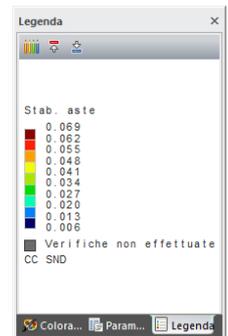
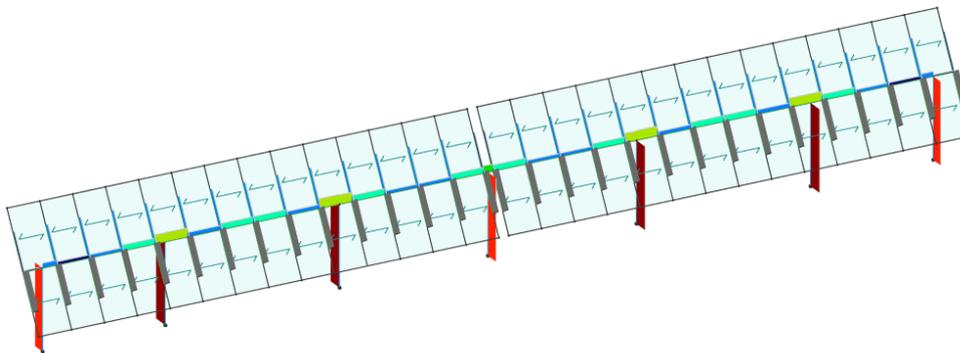


Diagramma tassi di sfruttamento stabilità aste combo SND con valore massimo pari a 0,069

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

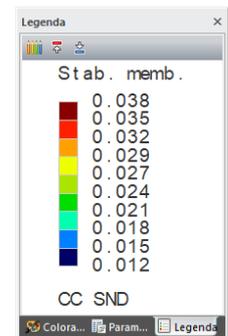
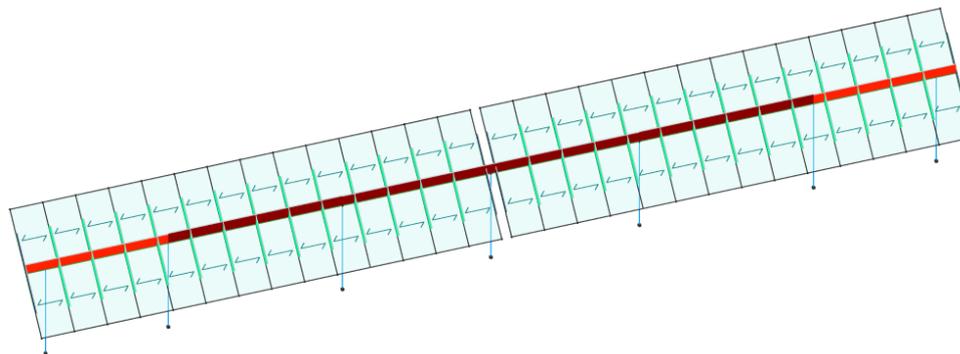


Diagramma tassi di sfruttamento stabilità membrature combo SND con valore massimo pari a 0,038

Figure 17: Tassi di sfruttamento SND (Stato limite di vita non dissipativo)

5.4.2 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:

ModeSt ver. 8.31, licenza n. 7429, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:

Xfinest ver. 9.6.2, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18

Tipo di calcolo: sismica statica

Vincoli esterni: Considera sempre vincoli assegnati in modellazione

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Tipo di analisi: Lineare
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Non sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

Opzioni generali:

- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

- Tipo di elemento bidimensionale: QF46

- Calcolo sforzo nei nodi: No

Opzioni per analisi P-Delta:

- Numero massimo di iterazioni: 15
- Valore della norma euclidea degli spostamenti: 1.0000E-04

Opzioni per analisi pushover:

- Esegui analisi in regime di piccoli spostamenti: Sì

Opzioni per analisi pushover murature:

- Interrompi analisi nel caso di plasticizzazione per carichi statici: Sì
- Utilizza sforzo normale medio: Sì

Metodo di convergenza:

- Forze e momenti residui (F)
Valore della norma euclidea delle forze: 1.0000E-03
Valore della norma euclidea dei momenti: 1.0000E-02

- Opzioni aggiuntive per analisi non lineari in presenza di elementi bidimensionali con comportamento Drucker-Prager:

OPTION PARAM CONV=E
OPTION PARAM RESENNORM=1.E-8
OPTION PARAM AUTO_INCREMENT=YES
OPTION PARAM LINE_SEARCHES=YES
OPTION PARAM BGINCRS=1.0
OPTION PARAM AVINCRS=1.0

Dati struttura

- Sito di costruzione: PP5J+JV Ploaghe SS, Italia LON. 8.73219 LAT. 40.70910
Contenuto tra ID reticolo: 26271 26049 26272 26050

Simbologia

- Ag =Accelerazione orizzontale massima al sito
 Cc =Coefficiente funzione della categoria del suolo
 Fo =Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
 S_s =Coefficiente di amplificazione stratigrafica
 T_R =Periodo di ritorno <anni>
 TCC=Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SND = Stato limite di salvaguardia della vita (non dissipativo)
 Tc* =Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

TCC	T _R	Ag <g>	Fo	Tc*	S _s	C _c
SLD	50	0.0217	2.63	0.19	1.80	2.89
SLV	475	0.0395	2.77	0.29	1.80	2.30

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale V_N: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 5.36 <m>
- Altezza della struttura: 5.36 <m>
- Numero piani edificio: 0
- Coefficiente θ: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di calcolo

- Categoria del suolo di fondazione: D
- Tipologia strutturale: acciaio a mensola o a pendolo inverso

Periodo T ₁	0.29936
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovraresistenza (α _u /α ₁)	1.00
Valore di riferimento del fattore di comportamento (q ₀)	2.00
Fattore riduttivo (K _w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di comportamento dissipativo (q)	2.00
Fattore di comportamento non dissipativo (qND)	1.33
Fattore di comportamento per SLD (qD)	1.33

- Categoria topografica: T2 - Pendii con inclinazione media i > 15°
- Coeff. amplificazione topografica S_T: 1.20
- Accelerazione di picco del terreno AgS: 0.0853 <g>
- Fattore di comportamento per sisma verticale (q_v): 1.50
- Smorzamento spettro: 5.00%

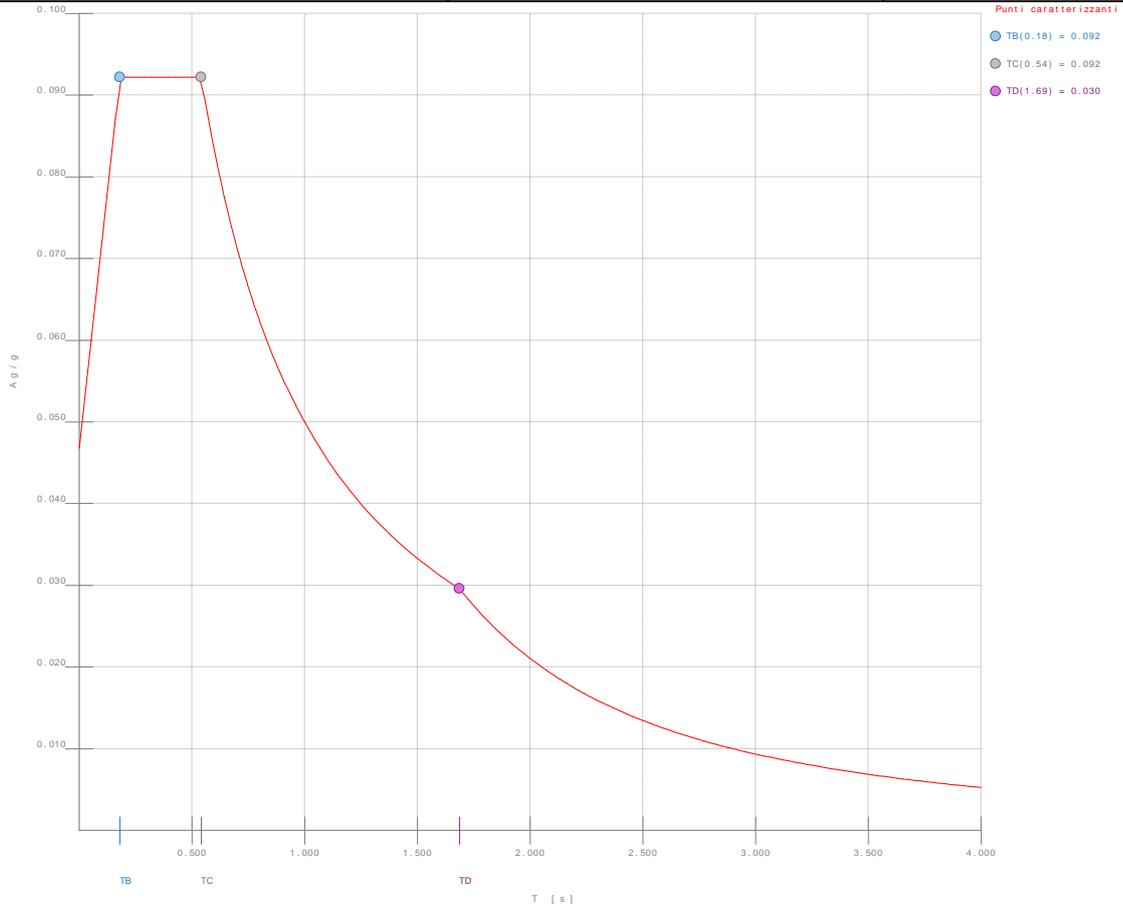


Figura numero 1: Spettro SLD

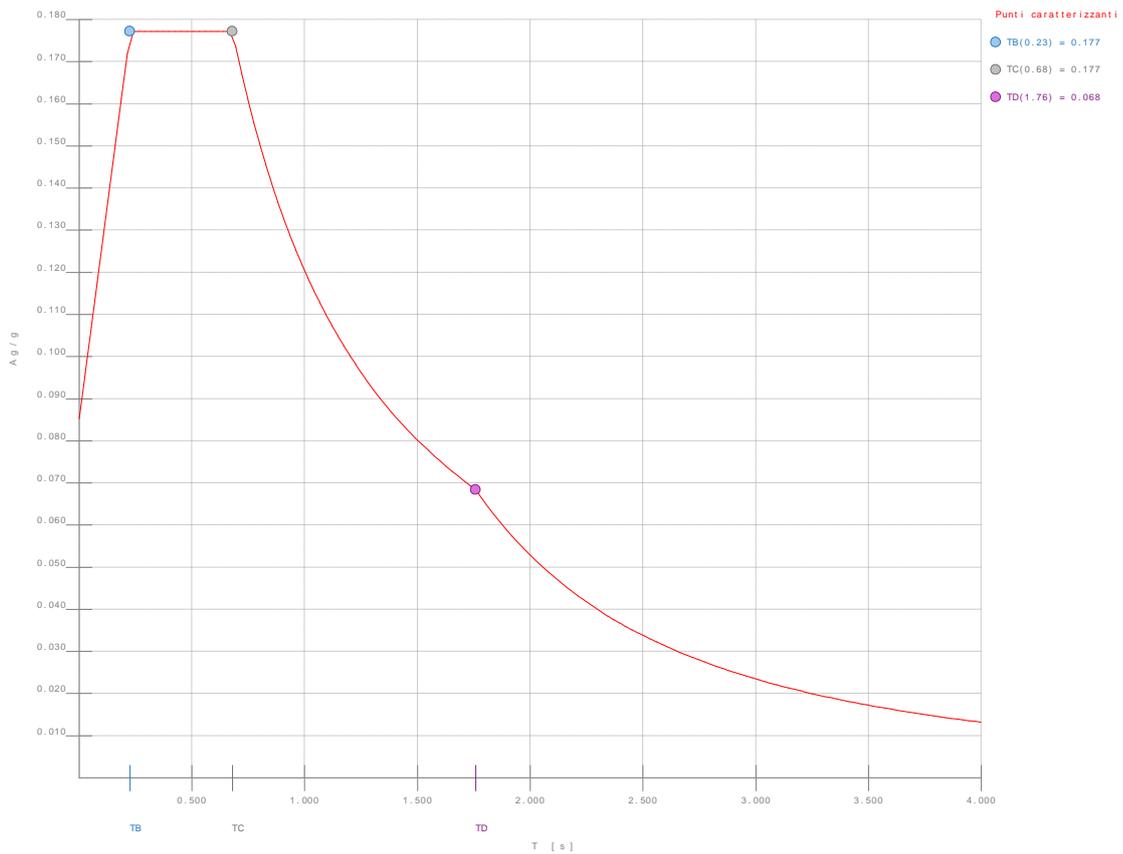


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>
- Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

- N = Numero
- Comm. = Commento
- 1 = G1 - Peso Proprio
- 2 = G2 - Permanenti non strutturali
- 3 = Q - Variabili neve
- 4 = Q - Vento retro Cond.A
- 5 = Q - Vento retro Cond.B
- 6 = Q - Vento fronte Cond.C
- 7 = Q - Vento fronte Cond.D
- F = azioni orizzontali convenzionali
- SLU = Stato limite ultimo
- SLR = Stato limite per combinazioni rare
- SLF = Stato limite per combinazioni frequenti
- SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
- S = Si
- N = No

N	Comm.	1	2	3	4	5	6	7	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	S	S	S	N	N	N	N	S	N	N	N	N
2	Calcolo statico	S	S	S	N	N	N	N	S	S	S	S	S
3	Vento cond A	S	S	S	N	N	N	N	S	S	S	S	S
4	Vento cond B	S	S	S	N	N	N	N	S	S	S	S	S
5	Vento cond C	S	S	S	N	N	N	N	S	S	S	S	S
6	Vento cond D	S	S	S	N	N	N	N	S	S	S	S	S

Elenco combinazioni di carico simboliche

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	1	2	3	4	5	6	7	S
1	Amb. 1 (Sisma)	SLU S	1	1	Ψ_2	-----	-----	-----	-----	1
2	Amb. 2 (SLU)	SLU γ max	γ max	γ max	γ max	-----	-----	-----	-----	-----
3	Amb. 2 (SLE R)	SLE R	1	1	1	-----	-----	-----	-----	-----
4	Amb. 2 (SLE F)	SLE F	1	1	Ψ_1	-----	-----	-----	-----	-----
5	Amb. 2 (SLE Q)	SLE Q	1	1	Ψ_2	-----	-----	-----	-----	-----
6	Amb. 3 (SLU)	SLU γ max	γ max	γ max	$\Psi_0 * \gamma$ max	γ max	-----	-----	-----	-----
7	Amb. 3 (SLU)	SLU γ max	γ max	γ max	$\Psi_0 * \gamma$ max	$\Psi_0 * \gamma$ max	-----	-----	-----	-----
8	Amb. 3 (SLE R)	SLE R	1	1	Ψ_0	1	-----	-----	-----	-----
9	Amb. 3 (SLE R)	SLE R	1	1	1	Ψ_0	-----	-----	-----	-----
10	Amb. 3 (SLE F)	SLE F	1	1	Ψ_2	Ψ_1	-----	-----	-----	-----
11	Amb. 3 (SLE F)	SLE F	1	1	Ψ_1	Ψ_2	-----	-----	-----	-----
12	Amb. 3 (SLE Q)	SLE Q	1	1	Ψ_2	Ψ_2	-----	-----	-----	-----
13	Amb. 4 (SLU)	SLU γ max	γ max	γ max	$\Psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
14	Amb. 4 (SLU)	SLU γ max	γ max	γ max	γ max	-----	$\Psi_0 * \gamma$ max	-----	-----	-----
15	Amb. 4 (SLE R)	SLE R	1	1	Ψ_0	-----	1	-----	-----	-----
16	Amb. 4 (SLE R)	SLE R	1	1	1	-----	Ψ_0	-----	-----	-----
17	Amb. 4 (SLE F)	SLE F	1	1	Ψ_2	-----	Ψ_1	-----	-----	-----
18	Amb. 4 (SLE F)	SLE F	1	1	Ψ_1	-----	Ψ_2	-----	-----	-----
19	Amb. 4 (SLE Q)	SLE Q	1	1	Ψ_2	-----	Ψ_2	-----	-----	-----
20	Amb. 5 (SLU)	SLU γ max	γ max	γ max	$\Psi_0 * \gamma$ max	-----	-----	γ max	-----	-----
21	Amb. 5 (SLU)	SLU γ max	γ max	γ max	γ max	-----	-----	$\Psi_0 * \gamma$ max	-----	-----
22	Amb. 5 (SLE R)	SLE R	1	1	Ψ_0	-----	-----	1	-----	-----
23	Amb. 5 (SLE R)	SLE R	1	1	1	-----	-----	Ψ_0	-----	-----
24	Amb. 5 (SLE F)	SLE F	1	1	Ψ_2	-----	-----	Ψ_1	-----	-----
25	Amb. 5 (SLE F)	SLE F	1	1	Ψ_1	-----	-----	Ψ_2	-----	-----
26	Amb. 5 (SLE Q)	SLE Q	1	1	Ψ_2	-----	-----	Ψ_2	-----	-----
27	Amb. 6 (SLU)	SLU γ max	γ max	γ max	$\Psi_0 * \gamma$ max	-----	-----	-----	γ max	-----

28	Amb. 6 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	$\Psi_0 * \gamma$ max	-----
29	Amb. 6 (SLE R)	SLE R	1	1	Ψ_0	-----	-----	-----	1	-----
30	Amb. 6 (SLE F)	SLE R	1	1	1	-----	-----	-----	Ψ_0	-----
31	Amb. 6 (SLE F)	SLE F	1	1	Ψ_2	-----	-----	-----	Ψ_1	-----
32	Amb. 6 (SLE F)	SLE F	1	1	Ψ_1	-----	-----	-----	Ψ_2	-----
33	Amb. 6 (SLE Q)	SLE Q	1	1	Ψ_2	-----	-----	-----	Ψ_2	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: Si

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

An. = Tipo di analisi
 L = Lineare
 NL = Non lineare
 PD = P-Delta

Bk = Buckling
 S = Si
 N = No

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	S X	S Y
1	Amb. 1 (SLU S) S +X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
2	Amb. 1 (SLE) S +X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
3	Amb. 1 (SLU S) S +X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
4	Amb. 1 (SLE) S +X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
5	Amb. 1 (SLU S) S -X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
6	Amb. 1 (SLE) S -X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
7	Amb. 1 (SLU S) S -X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
8	Amb. 1 (SLE) S -X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
9	Amb. 1 (SLU S) S +0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
10	Amb. 1 (SLE) S +0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
11	Amb. 1 (SLU S) S -0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
12	Amb. 1 (SLE) S -0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
13	Amb. 1 (SLU S) S +0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
14	Amb. 1 (SLE) S +0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
15	Amb. 1 (SLU S) S -0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
16	Amb. 1 (SLE) S -0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
17	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.00	0.00	0.00
18	Amb. 2 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
19	Amb. 2 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
20	Amb. 2 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	0.75	1.50	0.00	0.00	0.00	0.00	0.00
22	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
23	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	0.50	1.00	0.00	0.00	0.00	0.00	0.00
24	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
25	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.20	0.00	0.00	0.00	0.00	0.00
26	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
27	Amb. 3 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	1.50	0.00	0.00	0.00	0.00
29	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.90	0.00	0.00	0.00	0.00
30	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	1.00	0.00	0.00	0.00	0.00
31	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.60	0.00	0.00	0.00	0.00
32	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.20	0.00	0.00	0.00	0.00
33	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
34	Amb. 4 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	1.50	0.00	0.00	0.00
36	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.90	0.00	0.00	0.00
37	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00
38	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00
39	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00
40	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
41	Amb. 5 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	0.00	1.50	0.00	0.00
43	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.90	0.00	0.00
44	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00

45	Amb. 6 (SLE R)	SLE R L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00
46	Amb. 6 (SLE F)	SLE F L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.20	0.00	0.00
47	Amb. 6 (SLE F)	SLE F L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
48	Amb. 6 (SLE Q)	SLE Q L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Elenco masse nodi

Simbologia

Mo = Massa orizzontale

Nodo = Numero del nodo

Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo
	<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>
-104	55.67	-103	55.67	-102	83.72	-101	83.72	-98	83.72	-97	83.72	-96	83.72	-95	83.72	-94	83.72	-89	83.72
-93	83.72	-92	83.72	-91	83.72	-90	83.72	-89	83.72	-88	83.72	-87	83.72	-86	83.72	-85	83.72	-84	83.72
-84	83.72	-83	83.72	-82	83.72	-81	83.72	-80	83.72	-79	83.72	-78	83.72	-77	83.72	-76	83.72	-75	83.72
-75	83.72	-74	83.72	-73	83.72	-72	83.72	-71	83.72	-70	83.72	-69	83.72	-68	83.72	-67	83.72	-66	83.72
-66	83.72	-65	55.67	-64	83.72	-63	55.67	-62	83.72	-61	83.72	-58	83.72	-57	83.72	-56	83.72	-55	83.72
-55	83.72	-54	83.72	-53	83.72	-52	83.72	-51	55.67	-50	55.67	-49	83.72	-48	83.72	-47	55.67	-46	55.67
-46	55.67	-45	83.72	-44	83.72	-43	83.72	-42	83.72	-41	83.72	-37	118.22	-36	183.50	-35	193.34	-34	230.75
-34	230.75	-33	230.75	-32	189.39	-31	183.50	-30	209.94	-29	230.75	-28	230.75	-27	230.75	-26	207.90	-25	191.43
-25	191.43	-24	230.75	-23	230.75	-22	230.75	-21	152.26	-20	152.26	-19	230.75	-18	230.75	-17	230.75	-16	191.43
-16	191.43	-15	207.90	-14	230.75	-13	230.75	-12	230.75	-11	209.94	-10	183.50	-9	189.39	-8	230.75	-7	230.75
-7	230.75	-6	193.34	-5	183.50	-4	118.22	203	183.50	204	139.90	205	183.50						

Totali masse nodi

Mo
<kg>
12256.80

Elenco forze sismiche nodali allo SLD

Simbologia

Fx = Forza in dir. X

Fy = Forza in dir. Y

Nodo = Numero del nodo

cx = Coeff. c in dir. X

cy = Coeff. c in dir. Y

Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy	Nodo	cx	cy	Fx	Fy
			<daN>	<daN>				<daN>	<daN>				<daN>	<daN>				<daN>	<daN>
-104	0.01	0.01	7.03	7.03	-103	0.00	0.00	3.04	3.04	-102	0.00	0.00	4.58	4.58	-101	0.01	0.01	10.57	10.57
-98	0.00	0.00	4.58	4.58	-97	0.00	0.00	4.58	4.58	-96	0.00	0.00	4.58	4.58	-95	0.01	0.01	10.57	10.57
-94	0.01	0.01	10.57	10.57	-93	0.01	0.01	10.57	10.57	-92	0.00	0.00	4.58	4.58	-91	0.01	0.01	10.57	10.57
-90	0.00	0.00	4.58	4.58	-89	0.00	0.00	4.58	4.58	-88	0.01	0.01	10.57	10.57	-87	0.01	0.01	10.57	10.57
-86	0.00	0.00	4.58	4.58	-85	0.00	0.00	4.58	4.58	-84	0.01	0.01	10.57	10.57	-83	0.00	0.00	4.58	4.58
-82	0.01	0.01	10.57	10.57	-81	0.00	0.00	4.58	4.58	-80	0.01	0.01	10.57	10.57	-79	0.00	0.00	4.58	4.58
-78	0.01	0.01	10.57	10.57	-77	0.00	0.00	4.58	4.58	-76	0.01	0.01	10.57	10.57	-75	0.01	0.01	10.57	10.57
-74	0.00	0.00	4.58	4.58	-73	0.01	0.01	10.57	10.57	-72	0.00	0.00	4.58	4.58	-71	0.01	0.01	10.57	10.57
-70	0.00	0.00	4.58	4.58	-69	0.00	0.00	4.58	4.58	-68	0.01	0.01	10.57	10.57	-67	0.01	0.01	10.57	10.57
-66	0.00	0.00	4.58	4.58	-65	0.01	0.01	7.03	7.03	-64	0.01	0.01	10.57	10.57	-63	0.00	0.00	3.04	3.04
-62	0.01	0.01	10.57	10.57	-61	0.00	0.00	4.58	4.58	-58	0.01	0.01	10.57	10.57	-57	0.00	0.00	4.58	4.58
-56	0.01	0.01	10.57	10.57	-55	0.00	0.00	4.58	4.58	-54	0.01	0.01	10.57	10.57	-53	0.00	0.00	4.58	4.58
-52	0.01	0.01	10.57	10.57	-51	0.00	0.00	3.04	3.04	-50	0.01	0.01	7.03	7.03	-49	0.01	0.01	10.57	10.57
-48	0.00	0.00	4.58	4.58	-47	0.00	0.00	3.04	3.04	-46	0.01	0.01	7.03	7.03	-45	0.00	0.00	4.58	4.58
-44	0.01	0.01	10.57	10.57	-43	0.00	0.00	4.58	4.58	-42	0.01	0.01	10.57	10.57	-41	0.00	0.00	4.58	4.58
-37	0.01	0.01	10.70	10.70	-36	0.01	0.01	16.60	16.60	-35	0.02	0.02	17.49	17.49	-34	0.02	0.02	20.88	20.88
-33	0.02	0.02	20.88	20.88	-32	0.02	0.02	17.13	17.13	-31	0.01	0.01	16.60	16.60	-30	0.02	0.02	18.99	18.99
-29	0.02	0.02	20.88	20.88	-28	0.02	0.02	20.88	20.88	-27	0.02	0.02	20.88	20.88	-26	0.02	0.02	18.81	18.81
-25	0.02	0.02	17.32	17.32	-24	0.02	0.02	20.88	20.88	-23	0.02	0.02	20.88	20.88	-22	0.02	0.02	20.88	20.88
-21	0.01	0.01	13.78	13.78	-20	0.01	0.01	13.78	13.78	-19	0.02	0.02	20.88	20.88	-18	0.02	0.02	20.88	20.88

-17	0.02	0.02	20.88	20.88	-16	0.02	0.02	17.32	17.32	-15	0.02	0.02	18.81	18.81	-14	0.02	0.02	20.88	20.88
-13	0.02	0.02	20.88	20.88	-12	0.02	0.02	20.88	20.88	-11	0.02	0.02	18.99	18.99	-10	0.01	0.01	16.60	16.60
-9	0.02	0.02	17.13	17.13	-8	0.02	0.02	20.88	20.88	-7	0.02	0.02	20.88	20.88	-6	0.02	0.02	17.49	17.49
-5	0.01	0.01	16.60	16.60	-4	0.01	0.01	10.70	10.70	203	0.01	0.01	16.60	16.60	204	0.01	0.01	12.66	12.66
205	0.01	0.01	16.60	16.60															

Totali forze sismiche

Fx	Fy
<daN>	<daN>
1108.86	1108.86

Elenco forze sismiche nodali allo SND

Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>
-104	0.01	0.01	13.50	13.50	-103	0.00	0.00	5.85	5.85	-102	0.00	0.00	8.80	8.80	-101	0.01	0.01	20.31	20.31
-98	0.00	0.00	8.80	8.80	-97	0.00	0.00	8.80	8.80	-96	0.00	0.00	8.80	8.80	-95	0.01	0.01	20.31	20.31
-94	0.01	0.01	20.31	20.31	-93	0.01	0.01	20.31	20.31	-92	0.00	0.00	8.80	8.80	-91	0.01	0.01	20.31	20.31
-90	0.00	0.00	8.80	8.80	-89	0.00	0.00	8.80	8.80	-88	0.01	0.01	20.31	20.31	-87	0.01	0.01	20.31	20.31
-86	0.00	0.00	8.80	8.80	-85	0.00	0.00	8.80	8.80	-84	0.01	0.01	20.31	20.31	-83	0.00	0.00	8.80	8.80
-82	0.01	0.01	20.31	20.31	-81	0.00	0.00	8.80	8.80	-80	0.01	0.01	20.31	20.31	-79	0.00	0.00	8.80	8.80
-78	0.01	0.01	20.31	20.31	-77	0.00	0.00	8.80	8.80	-76	0.01	0.01	20.31	20.31	-75	0.01	0.01	20.31	20.31
-74	0.00	0.00	8.80	8.80	-73	0.01	0.01	20.31	20.31	-72	0.00	0.00	8.80	8.80	-71	0.01	0.01	20.31	20.31
-70	0.00	0.00	8.80	8.80	-69	0.00	0.00	8.80	8.80	-68	0.01	0.01	20.31	20.31	-67	0.01	0.01	20.31	20.31
-66	0.00	0.00	8.80	8.80	-65	0.01	0.01	13.50	13.50	-64	0.01	0.01	20.31	20.31	-63	0.00	0.00	5.85	5.85
-62	0.01	0.01	20.31	20.31	-61	0.00	0.00	8.80	8.80	-58	0.01	0.01	20.31	20.31	-57	0.00	0.00	8.80	8.80
-56	0.01	0.01	20.31	20.31	-55	0.00	0.00	8.80	8.80	-54	0.01	0.01	20.31	20.31	-53	0.00	0.00	8.80	8.80
-52	0.01	0.01	20.31	20.31	-51	0.00	0.00	5.85	5.85	-50	0.01	0.01	13.50	13.50	-49	0.01	0.01	20.31	20.31
-48	0.00	0.00	8.80	8.80	-47	0.00	0.00	5.85	5.85	-46	0.01	0.01	13.50	13.50	-45	0.00	0.00	8.80	8.80
-44	0.01	0.01	20.31	20.31	-43	0.00	0.00	8.80	8.80	-42	0.01	0.01	20.31	20.31	-41	0.00	0.00	8.80	8.80
-37	0.01	0.01	20.55	20.55	-36	0.01	0.01	31.90	31.90	-35	0.02	0.02	33.61	33.61	-34	0.02	0.02	40.11	40.11
-33	0.02	0.02	40.11	40.11	-32	0.02	0.02	32.92	32.92	-31	0.01	0.01	31.90	31.90	-30	0.02	0.02	36.49	36.49
-29	0.02	0.02	40.11	40.11	-28	0.02	0.02	40.11	40.11	-27	0.02	0.02	40.11	40.11	-26	0.02	0.02	36.14	36.14
-25	0.02	0.02	33.27	33.27	-24	0.02	0.02	40.11	40.11	-23	0.02	0.02	40.11	40.11	-22	0.02	0.02	40.11	40.11
-21	0.01	0.01	26.47	26.47	-20	0.01	0.01	26.47	26.47	-19	0.02	0.02	40.11	40.11	-18	0.02	0.02	40.11	40.11
-17	0.02	0.02	40.11	40.11	-16	0.02	0.02	33.27	33.27	-15	0.02	0.02	36.14	36.14	-14	0.02	0.02	40.11	40.11
-13	0.02	0.02	40.11	40.11	-12	0.02	0.02	40.11	40.11	-11	0.02	0.02	36.49	36.49	-10	0.01	0.01	31.90	31.90
-9	0.02	0.02	32.92	32.92	-8	0.02	0.02	40.11	40.11	-7	0.02	0.02	40.11	40.11	-6	0.02	0.02	33.61	33.61
-5	0.01	0.01	31.90	31.90	-4	0.01	0.01	20.55	20.55	203	0.01	0.01	31.90	31.90	204	0.01	0.01	24.32	24.32
205	0.01	0.01	31.90	31.90															

Totali forze sismiche

Fx	Fy
<daN>	<daN>
2130.50	2130.50

Domanda in duttilità di curvatura

Direzione X $\mu_{EdX}=6.85$

Direzione Y $\mu_{EdY}=6.85$

Spostamenti relativi massimi allo stato limite di danno

Simbologia

δ =Spostamento relativo

δ/h =Rapporto (*1000) tra lo spostamento relativo e l'altezza

CC =Numero della combinazione delle condizioni di carico elementari

N1 =Nodo1

N2 =Nodo2

h =Altezza teorica

I valori degli spostamenti relativi per CC di tipo sismico sono amplificati come da normativa

N1	N2	h	δ	δ/h	CC	N1	N2	h	δ	δ/h	CC	N1	N2	h	δ	δ/h	CC	N1	N2	h	δ	δ/h	CC
		<m>	<cm>					<m>	<cm>					<m>	<cm>					<m>	<cm>		
1	-5	3.29	0.09	0.28	2	2	-10	3.29	0.13	0.39	10	3	203	3.29	0.14	0.43	14	4	204	3.29	0.14	0.41	10
5	205	3.29	0.14	0.43	16	6	-31	3.29	0.13	0.39	12	7	-36	3.29	0.09	0.28	6						

Min = 0.28
Max = 0.43

Reazioni vincolari

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
 Fx = Reazione vincolare (forza) in dir. X
 Fy = Reazione vincolare (forza) in dir. Y
 Fz = Reazione vincolare (forza) in dir. Z
 Mx = Reazione vincolare (momento) intorno all'asse X
 My = Reazione vincolare (momento) intorno all'asse Y
 Mz = Reazione vincolare (momento) intorno all'asse Z
 Nodo = Numero del nodo
 TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SND = Stato limite di salvaguardia della vita (non dissipativo)

Nodo		CC	TCC	Fx	CC	TCC	Fy	CC	TCC	Fz	CC	TCC	Mx	CC	TCC	My	CC	TCC	Mz
				<daN>			<daN>			<daN>			<daNm>			<daNm>			<daNm>
1	Max	5	SND	322.47	21	SLU	1676.27	28	SLU	2200.61	28	SLU	4481.79	5	SND	545.29	21	SLU	2.12
1	Min	1	SND	-235.38	28	SLU	-1189.85	23	SLE R	509.16	21	SLU	-6314.01	28	SLU	-452.73	1	SND	-1.51
2	Max	5	SND	376.82	21	SLU	3639.14	28	SLU	4534.29	28	SLU	8054.13	5	SND	604.70	21	SLU	1.42
2	Min	1	SND	-266.54	28	SLU	-2583.12	23	SLE R	726.36	21	SLU	-11346.80	28	SLU	-486.66	1	SND	-1.01
3	Max	5	SND	262.47	21	SLU	3857.05	28	SLU	4684.95	28	SLU	8758.75	5	SND	481.56	28	SLU	0.42
3	Min	1	SND	-352.02	28	SLU	-2737.80	23	SLE R	750.44	21	SLU	-12339.40	21	SLU	-579.19	1	SND	-0.60
4	Max	5	SND	314.80	21	SLU	3278.98	28	SLU	3970.91	28	SLU	7832.16	5	SND	538.63	3	SND	0.00
4	Min	1	SND	-314.80	28	SLU	-2327.47	23	SLE R	786.67	21	SLU	-11034.10	5	SND	-538.63	1	SND	0.00
5	Max	5	SND	352.02	21	SLU	3857.06	28	SLU	4684.95	28	SLU	8758.75	5	SND	579.19	21	SLU	0.60
5	Min	1	SND	-262.47	28	SLU	-2737.80	23	SLE R	750.44	21	SLU	-12339.50	28	SLU	-481.57	1	SND	-0.42
6	Max	5	SND	266.54	21	SLU	3639.14	28	SLU	4534.29	28	SLU	8054.13	5	SND	486.66	28	SLU	1.01
6	Min	1	SND	-376.82	28	SLU	-2583.12	23	SLE R	726.35	21	SLU	-11346.80	21	SLU	-604.70	1	SND	-1.42
7	Max	5	SND	235.38	21	SLU	1676.27	28	SLU	2200.60	28	SLU	4481.79	5	SND	452.73	28	SLU	1.51
7	Min	1	SND	-322.47	28	SLU	-1189.84	23	SLE R	509.16	21	SLU	-6314.01	21	SLU	-545.29	1	SND	-2.12

Sollecitazioni aste

Simbologia

Asta = Numero dell'asta
 CC = Numero della combinazione delle condizioni di carico elementari
 Mx = Momento torcente intorno all'asse X
 My = Momento flettente intorno all'asse Y
 Mz = Momento flettente intorno all'asse Z
 N = Sforzo normale
 N1 = Nodo1
 N2 = Nodo2
 Ty = Taglio in dir. Y
 Tz = Taglio in dir. Z
 X = Coordinata progressiva rispetto al nodo iniziale

Tipo di combinazione di carico: SND

Asta	N1	N2		X	N	CC	Ty	CC	Mz	CC	Tz	CC	My	CC	Mx	CC
				<cm>	<daN>		<daN>		<daNm>		<daN>		<daNm>		<daNm>	
1	1	-5	Max	0.00	-951.89	1	322.47	5	452.73	1	184.31	15	719.02	9	0.19	11
1	1	-5	Max	328.50	-713.82	1	322.47	5	514.02	5	184.31	15	115.47	11	0.19	11
1	1	-5	Min.	0.00	-1274.83	5	-235.38	1	-545.29	5	-184.31	9	-719.02	15	-0.19	13
1	1	-5	Min.	328.50	-1036.76	5	-235.38	1	-320.48	1	-184.31	9	-115.47	13	-0.19	13
2	2	-10	Max	0.00	-2042.54	5	376.82	5	486.66	1	345.74	13	1149.89	9	0.13	11
2	2	-10	Max	328.50	-1804.47	5	376.82	5	633.15	5	345.74	13	15.22	9	0.13	11
2	2	-10	Min.	0.00	-2229.56	1	-266.54	1	-604.70	5	-345.74	11	-1149.89	15	-0.13	13
2	2	-10	Min.	328.50	-1991.49	1	-266.54	1	-388.92	1	-345.74	11	-15.22	15	-0.13	13
3	3	203	Max	0.00	-2179.16	1	262.47	5	579.19	1	370.57	13	1260.78	11	0.04	13
3	3	203	Max	328.50	-1941.09	1	262.47	5	380.64	5	370.57	13	43.80	9	0.04	13

3	3	203	Min.	0.00	-2234.84	5	-352.02	1	-481.56	5	-370.57	11	-1260.78	13	-0.04	11
3	3	203	Min.	328.50	-1996.77	5	-352.02	1	-577.21	1	-370.57	11	-43.80	15	-0.04	11
4	4	204	Max	0.00	-1944.35	1	314.80	1	538.63	5	334.19	9	1181.16	13	0.00	5
4	4	204	Max	328.50	-1706.29	1	314.80	1	495.49	1	334.19	9	83.34	15	0.00	5
4	4	204	Min.	0.00	-1944.35	1	-314.80	5	-538.63	1	-334.19	13	-1181.16	9	0.00	3
4	4	204	Min.	328.50	-1706.29	1	-314.80	5	-495.49	5	-334.19	13	-83.34	9	0.00	3
5	5	205	Max	0.00	-2179.16	5	262.47	1	579.19	5	370.57	9	1260.78	15	0.04	9
5	5	205	Max	328.50	-1941.09	5	262.47	1	380.64	1	370.57	9	43.80	13	0.04	9
5	5	205	Min.	0.00	-2234.83	1	-352.02	5	-481.57	1	-370.57	15	-1260.78	9	-0.04	15
5	5	205	Min.	328.50	-1996.77	1	-352.02	5	-577.21	5	-370.57	15	-43.80	11	-0.04	15
6	6	-31	Max	0.00	-2042.54	1	376.82	1	486.66	5	345.74	9	1149.89	13	0.13	15
6	6	-31	Max	328.50	-1804.47	1	376.82	1	633.15	1	345.74	9	15.22	13	0.13	15
6	6	-31	Min.	0.00	-2229.55	5	-266.54	5	-604.70	1	-345.74	15	-1149.89	11	-0.13	9
6	6	-31	Min.	328.50	-1991.49	5	-266.54	5	-388.92	5	-345.74	15	-15.22	11	-0.13	9
7	7	-36	Max	0.00	-951.89	5	322.47	1	452.73	5	184.31	11	719.02	13	0.19	15
7	7	-36	Max	328.50	-713.82	5	322.47	1	514.02	1	184.31	11	115.47	15	0.19	15
7	7	-36	Min.	0.00	-1274.83	1	-235.38	5	-545.29	1	-184.31	13	-719.02	11	-0.19	9
7	7	-36	Min.	328.50	-1036.76	1	-235.38	5	-320.48	5	-184.31	13	-115.47	9	-0.19	9
201	-5	-4	Max	0.00	39.90	5	39.90	9	33.88	15	261.89	1	-171.56	1	9.94	9
201	-5	-4	Max	80.60	39.90	5	39.90	9	5.74	5	188.50	1	9.94	1	9.94	9
201	-5	-4	Min.	0.00	-39.90	1	-39.90	13	-33.88	9	261.89	1	-191.45	5	-9.94	13
201	-5	-4	Min.	80.60	-39.90	1	-39.90	13	-5.74	3	188.50	1	-9.94	5	-9.94	13
201	-6	-5	Max	0.00	163.58	1	112.51	15	27.05	11	-403.36	1	377.04	1	105.52	13
201	-6	-5	Max	53.34	163.58	1	112.51	15	34.06	15	-451.93	1	148.92	1	105.52	13
201	-6	-5	Min.	0.00	-250.67	5	-112.51	9	-27.05	13	-726.30	5	-305.08	5	-105.52	11
201	-6	-5	Min.	53.34	-250.67	5	-112.51	9	-34.06	9	-774.87	5	-705.46	5	-105.52	11
201	-7	-6	Max	0.00	100.87	1	49.80	15	90.46	11	-12.73	1	490.72	1	90.57	13
201	-7	-6	Max	133.94	100.87	1	49.80	15	29.64	11	-134.70	1	391.99	1	90.57	13
201	-7	-6	Min.	0.00	-187.96	5	-49.80	9	-90.46	13	-335.67	5	211.26	5	-90.57	11
201	-7	-6	Min.	133.94	-187.96	5	-49.80	9	-29.64	13	-457.64	5	-320.03	5	-90.57	11
201	-8	-7	Max	0.00	31.65	1	23.81	11	61.48	9	377.90	1	204.38	5	75.62	13
201	-8	-7	Max	60.35					26.20	5			220.96	5		
201	-8	-7	Max	133.94	31.65	1	23.81	11	93.05	11	255.93	1	505.67	1	75.62	13
201	-8	-7	Min.	0.00	-118.74	5	-23.81	13	-61.48	15	54.96	5	81.18	1	-75.62	11
201	-8	-7	Min.	60.35					26.20	5			220.96	5		
201	-8	-7	Min.	133.94	-118.74	5	-23.81	13	-93.05	13	-67.01	5	196.31	5	-75.62	11
201	-9	-8	Max	0.00	-37.56	1	93.02	11	60.85	13	768.53	1	-325.73	5	60.67	13
201	-9	-8	Max	133.94	-37.56	1	93.02	11	63.75	11	646.56	1	189.42	5	60.67	13
201	-9	-8	Min.	0.00	-49.53	7	-93.02	13	-60.85	11	445.59	5	-851.57	1	-60.67	11
201	-9	-8	Min.	133.94	-49.53	7	-93.02	13	-63.75	13	323.62	5	96.14	1	-60.67	11
201	-10	-9	Max	0.00	12.50	5	155.05	11	129.95	15	1078.01	1	-670.02	5	45.72	13
201	-10	-9	Max	44.83	12.50	5	155.05	11	62.41	15	1037.19	1	-340.68	5	45.72	13
201	-10	-9	Min.	0.00	-99.59	1	-155.05	13	-129.95	9	755.07	5	-1310.73	1	-45.72	11
201	-10	-9	Min.	44.83	-99.59	1	-155.05	13	-62.41	9	714.25	5	-836.62	1	-45.72	11
202	-11	-10	Max	0.00	135.05	1	162.86	15	15.05	9	-832.33	1	-143.93	1	59.36	13
202	-11	-10	Max	89.11	135.05	1	162.86	15	130.08	15	-913.48	1	-921.81	1	59.36	13
202	-11	-10	Min.	0.00	-332.43	5	-162.86	9	-15.05	15	-968.25	5	-404.16	5	-59.36	11
202	-11	-10	Min.	89.11	-332.43	5	-162.86	9	-130.08	9	-1049.40	5	-1303.17	5	-59.36	11
202	-12	-11	Max	0.00	69.45	1	97.26	15	142.73	9	-441.70	1	544.33	1	44.41	13
202	-12	-11	Max	133.94	69.45	1	97.26	15	16.20	11	-563.67	1	-128.98	1	44.41	13
202	-12	-11	Min.	0.00	-266.83	5	-97.26	9	-142.73	15	-577.63	5	436.26	5	-44.41	11
202	-12	-11	Min.	133.94	-266.83	5	-97.26	9	-16.20	13	-699.59	5	-419.12	5	-44.41	11
202	-13	-12	Max	0.00	0.24	1	28.04	15	177.71	9	-51.07	1	753.46	5	29.46	13
202	-13	-12	Max	133.94	0.24	1	28.04	15	143.61	11	-173.04	1	559.28	1	29.46	13
202	-13	-12	Min.	0.00	-197.61	5	-28.04	9	-177.71	15	-187.00	5	709.38	1	-29.46	11
202	-13	-12	Min.	133.94	-197.61	5	-28.04	9	-143.61	13	-308.96	5	421.31	5	-29.46	11
202	-14	-13	Max	0.00	-68.98	1	45.24	11	119.97	9	339.56	1	547.44	5	14.50	13
202	-14	-13	Max	133.94	-68.98	1	45.24	11	178.32	11	217.59	1	738.51	5	14.50	13
202	-14	-13	Min.	0.00	-128.40	5	-45.24	13	-119.97	15	203.63	5	351.20	1	-14.50	11
202	-14	-13	Min.	133.94	-128.40	5	-45.24	13	-178.32	13	81.66	5	724.33	1	-14.50	11
202	-15	-14	Max	0.00	-59.18	5	114.45	11	32.98	13	730.18	1	-181.79	5	0.78	9
202	-15	-14	Max	133.94	-59.18	5	114.45	11	120.32	11	608.22	1	532.49	5	0.78	9
202	-15	-14	Min.	0.00	-138.19	1	-114.45	13	-32.98	11	594.26	5	-530.19	1	-0.78	15
202	-15	-14	Min.	133.94	-138.19	1	-114.45	13	-120.32	13	472.29	5	366.15	1	-0.78	15
202	203	-15	Max	0.00	6.06	5	179.69	11	182.62	13	1075.99	1	-960.44	5	15.73	9
202	203	-15	Max	84.71	6.06	5	179.69	11	33.06	15	998.85	1	-196.75	5	15.73	9
202	203	-15	Min.	0.00	-203.43	1	-179.69	13	-182.62	11	940.06	5	-1394.09	1	-15.73	15
202	203	-15	Min.	84.71	-203.43	1	-179.69	13	-33.06	9	862.92	5	-515.25	1	-15.73	15
203	-16	203	Max	0.00	116.69	1	162.84	15	104.32	13	-820.28	1	-402.02	1	28.08	15
203	-16	203	Max	49.23	116.69	1	162.84	15	182.58	13	-865.10	1	-816.86	1	28.08	15
203	-16	203	Min.	0.00	-224.51	7	-162.84	9	-104.32	11	-1011.88	5	-831.90	5	-28.08	9
203	-16	203	Min.	49.23	-224.51	7	-162.84	9	-182.58	11	-1056.71	5	-1341.06	5	-28.08	9
203	-17	-16	Max	0.00	54.31	1	100.46	15	30.33	9	-429.65	1	270.08	1	13.12	15
203	-17	-16	Max	133.94	54.31	1	100.46	15	104.23	15	-551.62	1	-387.09	1	13.12	15
203	-17	-16	Min.	0.00	-162.13	7	-100.46	9	-30.33	15	-621.25	5	66.94	5	-13.12	9
203	-17	-16	Min.	133.94	-162.13	7	-100.46	9	-104.23	9	-743.22	5	-846.87	5	-13.12	9

203	-18	-17	Max	0.00	-14.90	1	31.24	15	69.59	9	-39.03	1	442.56	5	1.83	11
203	-18	-17	Max	133.94	-14.90	1	31.24	15	30.24	11	-160.99	1	285.03	1	1.83	11
203	-18	-17	Min.	0.00	-92.92	7	-31.24	9	-69.59	15	-230.63	5	418.99	1	-1.83	13
203	-18	-17	Min.	133.94	-92.92	7	-31.24	9	-30.24	13	-352.59	5	51.97	5	-1.83	13
203	-19	-18	Max	0.00	-23.70	5	41.84	11	16.13	9	351.61	1	294.97	5	16.78	11
203	-19	-18	Max	133.94	-23.70	5	41.84	11	69.50	11	229.64	1	433.92	1	16.78	11
203	-19	-18	Min.	0.00	-84.12	3	-41.84	13	-16.13	15	160.01	5	44.65	1	-16.78	13
203	-19	-18	Min.	133.94	-84.12	3	-41.84	13	-69.50	13	38.04	5	427.61	5	-16.78	13
203	-20	-19	Max	0.00	45.51	5	111.05	11	132.69	13	742.24	1	-375.82	5	31.73	11
203	-20	-19	Max	133.94	45.51	5	111.05	11	16.05	11	620.27	1	280.03	5	31.73	11
203	-20	-19	Min.	0.00	-153.33	3	-111.05	13	-132.69	11	550.63	5	-852.87	1	-31.73	13
203	-20	-19	Min.	133.94	-153.33	3	-111.05	13	-16.05	13	428.67	5	59.62	1	-31.73	13
203	204	-20	Max	0.00	91.33	5	156.87	11	162.34	15	948.94	1	-535.41	5	41.67	11
203	204	-20	Max	20.00	91.33	5	156.87	11	131.74	15	930.73	1	-385.76	5	41.67	11
203	204	-20	Min.	0.00	-199.15	3	-156.87	13	-162.34	9	757.34	5	-1030.89	1	-41.67	13
203	204	-20	Min.	20.00	-199.15	3	-156.87	13	-131.74	9	739.13	5	-842.93	1	-41.67	13
204	204	-21	Max	0.00	91.33	1	156.87	15	162.34	11	948.94	5	-535.41	1	41.67	15
204	204	-21	Max	20.00	91.33	1	156.87	15	131.74	11	930.73	5	-385.76	1	41.67	15
204	204	-21	Min.	0.00	-199.15	7	-156.87	9	-162.34	13	757.34	1	-1030.89	5	-41.67	9
204	204	-21	Min.	20.00	-199.15	7	-156.87	9	-131.74	13	739.13	1	-842.93	5	-41.67	9
204	-21	-22	Max	0.00	45.51	1	111.05	15	132.69	9	742.24	5	-375.82	1	31.73	15
204	-21	-22	Max	133.94	45.51	1	111.05	15	16.05	15	620.27	5	280.04	1	31.73	15
204	-21	-22	Min.	0.00	-153.33	7	-111.05	9	-132.69	15	550.63	1	-852.87	5	-31.73	9
204	-21	-22	Min.	133.94	-153.33	7	-111.05	9	-16.05	9	428.67	1	59.62	5	-31.73	9
204	-22	-23	Max	0.00	-23.70	1	41.84	15	16.13	13	351.61	5	294.97	1	16.78	15
204	-22	-23	Max	133.94	-23.70	1	41.84	15	69.50	15	229.64	5	433.92	5	16.78	15
204	-22	-23	Min.	0.00	-84.12	7	-41.84	9	-16.13	11	160.01	1	44.65	5	-16.78	9
204	-22	-23	Min.	133.94	-84.12	7	-41.84	9	-69.50	9	38.04	1	427.61	1	-16.78	9
204	-23	-24	Max	0.00	-14.90	5	31.24	11	69.59	13	-39.02	5	442.56	1	1.83	15
204	-23	-24	Max	133.94	-14.90	5	31.24	11	30.24	15	-160.99	5	285.03	5	1.83	15
204	-23	-24	Min.	0.00	-92.92	3	-31.24	13	-69.59	11	-230.62	1	418.99	5	-1.83	9
204	-23	-24	Min.	133.94	-92.92	3	-31.24	13	-30.24	9	-352.59	1	51.98	1	-1.83	9
204	-24	-25	Max	0.00	54.31	5	100.46	11	100.33	13	-429.65	5	270.09	5	13.12	11
204	-24	-25	Max	133.94	54.31	5	100.46	11	30.33	11	-551.62	5	-387.08	5	13.12	11
204	-24	-25	Min.	0.00	-162.13	3	-100.46	13	-30.33	11	-621.25	1	66.94	1	-13.12	13
204	-24	-25	Min.	133.94	-162.13	3	-100.46	13	-104.23	13	-743.22	1	-846.87	1	-13.12	13
204	-25	205	Max	0.00	116.69	5	162.84	11	104.32	9	-820.28	5	-402.02	5	28.08	11
204	-25	205	Max	49.23	116.69	5	162.84	11	182.58	9	-865.10	5	-816.86	5	28.08	11
204	-25	205	Min.	0.00	-224.51	3	-162.84	13	-104.32	15	-1011.88	1	-831.89	1	-28.08	13
204	-25	205	Min.	49.23	-224.51	3	-162.84	13	-182.58	15	-1056.70	1	-1341.06	1	-28.08	13
205	205	-26	Max	0.00	6.06	1	179.69	15	182.62	9	1075.99	5	-960.44	1	15.73	13
205	205	-26	Max	84.71	6.06	1	179.69	15	33.06	11	998.84	5	-196.74	1	15.73	13
205	205	-26	Min.	0.00	-203.43	5	-179.69	9	-182.62	15	940.06	1	-1394.08	5	-15.73	11
205	205	-26	Min.	84.71	-203.43	5	-179.69	9	-33.06	13	862.92	1	-515.24	5	-15.73	11
205	-26	-27	Max	0.00	-59.18	1	114.45	15	32.99	9	730.19	5	-181.83	1	0.78	13
205	-26	-27	Max	133.94	-59.18	1	114.45	15	120.31	15	608.22	5	532.46	1	0.78	13
205	-26	-27	Min.	0.00	-138.19	5	-114.45	9	-32.99	15	594.26	1	-530.24	5	-0.78	11
205	-26	-27	Min.	133.94	-138.19	5	-114.45	9	-120.31	9	472.30	1	366.12	5	-0.78	11
205	-27	-28	Max	0.00	-68.97	5	45.24	15	119.97	13	339.56	5	547.45	1	14.50	9
205	-27	-28	Max	133.94	-68.97	5	45.24	15	178.32	15	217.59	5	738.51	1	14.50	9
205	-27	-28	Min.	0.00	-128.40	1	-45.24	9	-119.97	11	203.63	1	351.21	5	-14.50	15
205	-27	-28	Min.	133.94	-128.40	1	-45.24	9	-178.32	9	81.66	1	724.33	5	-14.50	15
205	-28	-29	Max	0.00	0.24	5	28.04	11	177.71	13	-51.07	5	753.46	1	29.46	9
205	-28	-29	Max	133.94	0.24	5	28.04	11	143.61	15	-173.04	5	559.28	5	29.46	9
205	-28	-29	Min.	0.00	-197.61	1	-28.04	13	-177.71	11	-187.00	1	709.38	5	-29.46	15
205	-28	-29	Min.	133.94	-197.61	1	-28.04	13	-143.61	9	-308.96	1	421.31	1	-29.46	15
205	-29	-30	Max	0.00	69.46	5	97.26	11	142.73	13	-441.70	5	544.34	5	44.41	9
205	-29	-30	Max	133.94	69.46	5	97.26	11	16.20	15	-563.66	5	-128.97	5	44.41	9
205	-29	-30	Min.	0.00	-266.83	1	-97.26	13	-142.73	11	-577.62	1	436.27	1	-44.41	15
205	-29	-30	Min.	133.94	-266.83	1	-97.26	13	-16.20	9	-699.59	1	-419.10	1	-44.41	15
205	-30	-31	Max	0.00	135.05	5	162.86	11	15.04	13	-832.33	5	-143.96	5	59.36	9
205	-30	-31	Max	89.11	135.05	5	162.86	11	130.09	11	-913.48	5	-921.84	5	59.36	9
205	-30	-31	Min.	0.00	-332.43	1	-162.86	13	-15.04	11	-968.26	1	-404.20	1	-59.36	15
205	-30	-31	Min.	89.11	-332.43	1	-162.86	13	-130.09	13	-1049.40	1	-1303.21	1	-59.36	15
206	-31	-32	Max	0.00	12.50	1	155.05	15	129.95	11	1078.01	5	-670.01	1	45.72	9
206	-31	-32	Max	44.83	12.50	1	155.05	15	62.41	11	1037.19	5	-340.67	1	45.72	9
206	-31	-32	Min.	0.00	-99.59	5	-155.05	9	-129.95	13	755.07	1	-1310.73	5	-45.72	15
206	-31	-32	Min.	44.83	-99.59	5	-155.05	9	-62.41	13	714.25	1	-836.62	5	-45.72	15
206	-32	-33	Max	0.00	-37.56	5	93.02	15	60.85	9	768.53	5	-325.71	1	60.67	9
206	-32	-33	Max	133.94	-37.56	5	93.02	15	63.75	15	646.56	5	189.43	1	60.67	9
206	-32	-33	Min.	0.00	-49.53	1	-93.02	9	-60.85	15	445.59	1	-851.56	5	-60.67	15
206	-32	-33	Min.	133.94	-49.53	1	-93.02	9	-63.75	9	323.62	1	96.15	5	-60.67	15
206	-33	-34	Max	0.00	31.65	5	23.81	15	61.48	13	377.90	5	204.38	1	75.62	9
206	-33	-34	Max	60.36	31.65	5	23.81	15	-26.20	1	220.96	1	220.96	1	75.62	9
206	-33	-34	Max	133.94	31.65	5	23.81	15	93.05	15	255.94	5	505.67	5	75.62	9
206	-33	-34	Min.	0.00	-118.74	1	-23.81	9	-61.48	11	54.96	1	81.18	5	-75.62	15

308	-12	-72	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
308	-12	-72	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
308	-73	-12	Max	0.00	-15.77	9	20.31	1	0.00	1	2.62	13	0.00	13	0.00	3
308	-73	-12	Max	7.53					0.46	13			0.10	13		
308	-73	-12	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	3
308	-73	-12	Min.	0.00	-36.08	13	-20.31	5	0.00	5	-32.56	9	0.00	9	0.00	5
308	-73	-12	Min.	7.53					0.46	13			0.10	13		
308	-73	-12	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	5
309	-13	-74	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
309	-13	-74	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
309	-13	-74	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
309	-13	-74	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
309	-75	-13	Max	0.00	-15.77	9	20.31	1	0.00	3	2.62	13	0.00	9	0.00	1
309	-75	-13	Max	7.53					0.46	13			0.10	13		
309	-75	-13	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	1
309	-75	-13	Min.	0.00	-36.08	13	-20.31	5	0.00	5	-32.56	9	0.00	13	0.00	5
309	-75	-13	Min.	7.53					0.46	13			0.10	13		
309	-75	-13	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	5
310	-14	-90	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
310	-14	-90	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
310	-14	-90	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
310	-14	-90	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
310	-91	-14	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	15	0.00	1
310	-91	-14	Max	7.53					0.46	13			0.10	13		
310	-91	-14	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	1
310	-91	-14	Min.	0.00	-36.08	13	-20.31	5	0.00	3	-32.56	9	0.00	9	0.00	7
310	-91	-14	Min.	7.53					0.46	13			0.10	13		
310	-91	-14	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	7
311	-15	-92	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
311	-15	-92	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
311	-15	-92	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
311	-15	-92	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
311	-93	-15	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	1	0.00	5
311	-93	-15	Max	7.53					0.46	13			0.10	13		
311	-93	-15	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
311	-93	-15	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	5	0.00	1
311	-93	-15	Min.	7.53					0.46	13			0.10	13		
311	-93	-15	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	1
312	-16	-98	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
312	-16	-98	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
312	-16	-98	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
312	-16	-98	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
312	-94	-16	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	5	0.00	5
312	-94	-16	Max	7.53					0.46	13			0.10	13		
312	-94	-16	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
312	-94	-16	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	1	0.00	1
312	-94	-16	Min.	7.53					0.46	13			0.10	13		
312	-94	-16	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	1
313	-17	-97	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
313	-17	-97	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
313	-17	-97	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
313	-17	-97	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
313	-42	-17	Max	0.00	-15.77	9	20.31	1	0.00	7	2.62	13	0.00	15	0.00	3
313	-42	-17	Max	7.53					0.46	13			0.10	13		
313	-42	-17	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	3
313	-42	-17	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	9	0.00	5
313	-42	-17	Min.	7.53					0.46	13			0.10	13		
313	-42	-17	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	5
314	-18	-43	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
314	-18	-43	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
314	-18	-43	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
314	-18	-43	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
314	-44	-18	Max	0.00	-15.77	9	20.31	1	0.00	1	2.62	13	0.00	15	0.00	5
314	-44	-18	Max	7.53					0.46	13			0.10	13		
314	-44	-18	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
314	-44	-18	Min.	0.00	-36.08	13	-20.31	5	0.00	5	-32.56	9	0.00	9	0.00	3
314	-44	-18	Min.	7.53					0.46	13			0.10	13		
314	-44	-18	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	3
315	-19	-45	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
315	-19	-45	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
315	-19	-45	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
315	-19	-45	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
315	-58	-19	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	5	0.00	5
315	-58	-19	Max	7.53					0.46	13			0.10	13		
315	-58	-19	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
315	-58	-19	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	1	0.00	1



315	-58	-19	Min.	7.53				0.46	13			0.10	13			
315	-58	-19	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	1
316	-20	-63	Max	0.00	84.55	13	5.85	5	8.77	1	52.19	9	-33.36	13	0.00	1
316	-20	-63	Max	150.00	15.89	13	5.85	5	0.00	1	12.55	9	0.00	13	0.00	1
316	-20	-63	Min.	0.00	78.70	9	-5.85	1	-8.77	5	42.06	13	-48.55	9	0.00	1
316	-20	-63	Min.	150.00	10.04	9	-5.85	1	0.00	5	2.42	13	0.00	9	0.00	1
316	-65	-20	Max	0.00	-6.21	9	13.50	1	0.00	1	4.21	13	0.00	9	0.00	7
316	-65	-20	Max	15.93					0.65	13			0.34	13		
316	-65	-20	Max	150.00	-74.87	9	13.50	1	20.25	1	-35.43	13	-23.42	13	0.00	7
316	-65	-20	Min.	0.00	-19.71	13	-13.50	5	0.00	7	-19.18	9	0.00	13	0.00	1
316	-65	-20	Min.	15.93					0.65	13			0.34	13		
316	-65	-20	Min.	150.00	-88.37	13	-13.50	5	-20.25	5	-58.82	9	-58.50	9	0.00	1
317	-21	-51	Max	0.00	84.55	13	5.85	5	8.77	1	52.19	9	-33.36	13	0.00	1
317	-21	-51	Max	150.00	15.89	13	5.85	5	0.00	1	12.55	9	0.00	13	0.00	1
317	-21	-51	Min.	0.00	78.70	9	-5.85	1	-8.77	5	42.06	13	-48.55	9	0.00	1
317	-21	-51	Min.	150.00	10.04	9	-5.85	1	0.00	5	2.42	13	0.00	9	0.00	1
317	-50	-21	Max	0.00	-6.21	9	13.50	1	0.00	5	4.21	13	0.00	15	0.00	7
317	-50	-21	Max	15.93					0.65	13			0.34	13		
317	-50	-21	Max	150.00	-74.87	9	13.50	1	20.25	1	-35.43	13	-23.42	13	0.00	7
317	-50	-21	Min.	0.00	-19.71	13	-13.50	5	0.00	3	-19.18	9	0.00	9	0.00	1
317	-50	-21	Min.	15.93					0.65	13			0.34	13		
317	-50	-21	Min.	150.00	-88.37	13	-13.50	5	-20.25	5	-58.82	9	-58.50	9	0.00	1
318	-22	-53	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
318	-22	-53	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
318	-22	-53	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
318	-22	-53	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
318	-52	-22	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	1	0.00	1
318	-52	-22	Max	7.53					0.46	13			0.10	13		
318	-52	-22	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	1
318	-52	-22	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	1	0.00	5
318	-52	-22	Min.	7.53					0.46	13			0.10	13		
318	-52	-22	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	5
319	-23	-55	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
319	-23	-55	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
319	-23	-55	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
319	-23	-55	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
319	-54	-23	Max	0.00	-15.77	9	20.31	1	0.00	3	2.62	13	0.00	11	0.00	5
319	-54	-23	Max	7.53					0.46	13			0.10	13		
319	-54	-23	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
319	-54	-23	Min.	0.00	-36.08	13	-20.31	5	0.00	5	-32.56	9	0.00	13	0.00	3
319	-54	-23	Min.	7.53					0.46	13			0.10	13		
319	-54	-23	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	3
320	-24	-57	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
320	-24	-57	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
320	-24	-57	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
320	-24	-57	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
320	-56	-24	Max	0.00	-15.77	9	20.31	1	0.00	1	2.62	13	0.00	1	0.00	1
320	-56	-24	Max	7.53					0.46	13			0.10	13		
320	-56	-24	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	1
320	-56	-24	Min.	0.00	-36.08	13	-20.31	5	0.00	5	-32.56	9	0.00	1	0.00	5
320	-56	-24	Min.	7.53					0.46	13			0.10	13		
320	-56	-24	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	5
322	-25	-41	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
322	-25	-41	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
322	-25	-41	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
322	-25	-41	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
322	-64	-25	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	1	0.00	5
322	-64	-25	Max	7.53					0.46	13			0.10	13		
322	-64	-25	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
322	-64	-25	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	1	0.00	1
322	-64	-25	Min.	7.53					0.46	13			0.10	13		
322	-64	-25	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	1
323	-26	-77	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
323	-26	-77	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
323	-26	-77	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
323	-26	-77	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
323	-76	-26	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	1	0.00	1
323	-76	-26	Max	7.53					0.46	13			0.10	13		
323	-76	-26	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	1
323	-76	-26	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	1	0.00	1
323	-76	-26	Min.	7.53					0.46	13			0.10	13		
323	-76	-26	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	1
324	-27	-79	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
324	-27	-79	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
324	-27	-79	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
324	-27	-79	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1

324	-78	-27	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	1	0.00	5
324	-78	-27	Max	7.53					0.46	13			0.10	13		
324	-78	-27	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
324	-78	-27	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	1	0.00	1
324	-78	-27	Min.	7.53					0.46	13			0.10	13		
324	-78	-27	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	1
325	-28	-81	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
325	-28	-81	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
325	-28	-81	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
325	-28	-81	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
325	-80	-28	Max	0.00	-15.77	9	20.31	1	0.00	1	2.62	13	0.00	1	0.00	1
325	-80	-28	Max	7.53					0.46	13			0.10	13		
325	-80	-28	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	1
325	-80	-28	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	1	0.00	5
325	-80	-28	Min.	7.53					0.46	13			0.10	13		
325	-80	-28	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	5
326	-29	-83	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
326	-29	-83	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
326	-29	-83	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
326	-29	-83	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
326	-82	-29	Max	0.00	-15.77	9	20.31	1	0.00	5	2.62	13	0.00	9	0.00	5
326	-82	-29	Max	7.53					0.46	13			0.10	13		
326	-82	-29	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
326	-82	-29	Min.	0.00	-36.08	13	-20.31	5	0.00	1	-32.56	9	0.00	15	0.00	3
326	-82	-29	Min.	7.53					0.46	13			0.10	13		
326	-82	-29	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	3
327	-30	-85	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
327	-30	-85	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
327	-30	-85	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
327	-30	-85	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
327	-84	-30	Max	0.00	-15.77	9	20.31	1	0.00	1	2.62	13	0.00	1	0.00	5
327	-84	-30	Max	7.53					0.46	13			0.10	13		
327	-84	-30	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	5
327	-84	-30	Min.	0.00	-36.08	13	-20.31	5	0.00	5	-32.56	9	0.00	1	0.00	1
327	-84	-30	Min.	7.53					0.46	13			0.10	13		
327	-84	-30	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	1
329	-32	-86	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
329	-32	-86	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
329	-32	-86	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
329	-32	-86	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
329	-87	-32	Max	0.00	-15.77	9	20.31	1	0.00	1	2.62	13	0.00	11	0.00	15
329	-87	-32	Max	7.53					0.46	13			0.10	13		
329	-87	-32	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	15
329	-87	-32	Min.	0.00	-36.08	13	-20.31	5	0.00	5	-32.56	9	0.00	13	0.00	9
329	-87	-32	Min.	7.53					0.46	13			0.10	13		
329	-87	-32	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	9
330	-33	-89	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
330	-33	-89	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
330	-33	-89	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
330	-33	-89	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
330	-88	-33	Max	0.00	-15.77	9	20.31	1	0.00	1	2.62	13	0.00	9	0.00	9
330	-88	-33	Max	7.53					0.46	13			0.10	13		
330	-88	-33	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	9
330	-88	-33	Min.	0.00	-36.08	13	-20.31	5	0.00	7	-32.56	9	0.00	15	0.00	13
330	-88	-33	Min.	7.53					0.46	13			0.10	13		
330	-88	-33	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	13
331	-34	-61	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
331	-34	-61	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
331	-34	-61	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
331	-34	-61	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
331	-62	-34	Max	0.00	-15.77	9	20.31	1	0.00	3	2.62	13	0.00	9	0.00	3
331	-62	-34	Max	7.53					0.46	13			0.10	13		
331	-62	-34	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	3
331	-62	-34	Min.	0.00	-36.08	13	-20.31	5	0.00	5	-32.56	9	0.00	15	0.00	5
331	-62	-34	Min.	7.53					0.46	13			0.10	13		
331	-62	-34	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	5
332	-35	-102	Max	0.00	120.73	13	8.80	5	13.20	1	74.78	9	-50.17	13	0.00	1
332	-35	-102	Max	150.00	30.32	13	8.80	5	0.00	1	22.59	9	0.00	13	0.00	1
332	-35	-102	Min.	0.00	111.93	9	-8.80	1	-13.20	5	59.55	13	-73.03	9	0.00	1
332	-35	-102	Min.	150.00	21.53	9	-8.80	1	0.00	5	7.35	13	0.00	9	0.00	1
332	-101	-35	Max	0.00	-15.77	9	20.31	1	0.00	9	2.62	13	0.00	9	0.00	13
332	-101	-35	Max	7.53					0.46	13			0.10	13		
332	-101	-35	Max	150.00	-106.18	9	20.31	1	30.46	1	-49.58	13	-35.22	13	0.00	13
332	-101	-35	Min.	0.00	-36.08	13	-20.31	5	0.00	13	-32.56	9	0.00	13	0.00	9
332	-101	-35	Min.	7.53					0.46	13			0.10	13		
332	-101	-35	Min.	150.00	-126.49	13	-20.31	5	-30.46	5	-84.75	9	-87.98	9	0.00	9

333	-37	-103	Max	0.00	84.55	13	5.85	5	8.77	1	52.19	9	-33.36	13	0.00	1
333	-37	-103	Max	150.00	15.89	13	5.85	5	0.00	1	12.55	9	0.00	13	0.00	1
333	-37	-103	Min.	0.00	78.70	9	-5.85	1	-8.77	5	42.06	13	-48.55	9	0.00	1
333	-37	-103	Min.	150.00	10.04	9	-5.85	1	0.00	5	2.42	13	0.00	9	0.00	1
333	-104	-37	Max	0.00	-6.21	9	13.50	1	0.00	5	4.21	13	0.00	15	0.00	7
333	-104	-37	Max	15.93					0.65	13			0.34	13		
333	-104	-37	Max	150.00	-74.87	9	13.50	1	20.25	1	-35.43	13	-23.42	13	0.00	7
333	-104	-37	Min.	0.00	-19.71	13	-13.50	5	0.00	3	-19.18	9	0.00	9	0.00	1
333	-104	-37	Min.	15.93					0.65	13			0.34	13		
333	-104	-37	Min.	150.00	-88.37	13	-13.50	5	-20.25	5	-58.82	9	-58.50	9	0.00	1

Tipo di combinazione di carico: SLD

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-1029.32	2	188.72	6	213.44	2	95.93	16	374.23	10	0.10	12
1	1	-5	Max	328.50	-791.25	2	188.72	6	313.94	6	95.93	16	60.10	12	0.10	12
1	1	-5	Min.	0.00	-1197.40	6	-101.62	2	-306.00	6	-95.93	10	-374.23	16	-0.10	14
1	1	-5	Min.	328.50	-959.33	6	-101.62	2	-120.40	2	-95.93	10	-60.10	14	-0.10	14
2	2	-10	Max	0.00	-2087.38	6	222.56	6	224.99	2	179.94	14	598.48	10	0.07	12
2	2	-10	Max	328.50	-1849.31	6	222.56	6	388.10	6	179.94	14	7.92	10	0.07	12
2	2	-10	Min.	0.00	-2184.72	2	-112.28	2	-343.03	6	-179.94	12	-598.48	16	-0.07	14
2	2	-10	Min.	328.50	-1946.65	2	-112.28	2	-143.86	2	-179.94	12	-7.92	16	-0.07	14
3	3	203	Max	0.00	-2192.51	2	115.13	6	324.86	2	192.87	14	656.20	12	0.02	14
3	3	203	Max	328.50	-1954.44	2	115.13	6	150.98	6	192.87	14	22.80	10	0.02	14
3	3	203	Min.	0.00	-2221.49	6	-204.69	2	-227.23	6	-192.87	12	-656.20	14	-0.02	12
3	3	203	Min.	328.50	-1983.42	6	-204.69	2	-347.55	2	-192.87	12	-22.80	16	-0.02	12
4	4	204	Max	0.00	-1944.35	2	163.84	2	280.34	6	173.94	10	614.76	14	0.00	6
4	4	204	Max	328.50	-1706.29	2	163.84	2	257.89	2	173.94	10	43.38	16	0.00	6
4	4	204	Min.	0.00	-1944.35	2	-163.84	6	-280.34	2	-173.94	14	-614.76	10	0.00	4
4	4	204	Min.	328.50	-1706.29	2	-163.84	6	-257.89	6	-173.94	14	-43.38	10	0.00	4
5	5	205	Max	0.00	-2192.51	6	115.14	2	324.86	6	192.87	10	656.20	16	0.02	10
5	5	205	Max	328.50	-1954.44	6	115.14	2	150.98	2	192.87	10	22.80	14	0.02	10
5	5	205	Min.	0.00	-2221.49	2	-204.69	6	-227.24	2	-192.87	16	-656.20	10	-0.02	16
5	5	205	Min.	328.50	-1983.42	2	-204.69	6	-347.55	6	-192.87	16	-22.80	12	-0.02	16
6	6	-31	Max	0.00	-2087.38	2	222.56	2	224.99	6	179.94	10	598.48	14	0.07	16
6	6	-31	Max	328.50	-1849.31	2	222.56	2	388.10	2	179.94	10	7.92	14	0.07	16
6	6	-31	Min.	0.00	-2184.71	6	-112.28	6	-343.03	2	-179.94	16	-598.48	12	-0.07	10
6	6	-31	Min.	328.50	-1946.65	6	-112.28	6	-143.87	6	-179.94	16	-7.92	12	-0.07	10
7	7	-36	Max	0.00	-1029.32	6	188.72	2	213.44	6	95.93	12	374.23	14	0.10	16
7	7	-36	Max	328.50	-791.25	6	188.72	2	313.93	2	95.93	12	60.10	16	0.10	16
7	7	-36	Min.	0.00	-1197.40	2	-101.63	6	-306.00	2	-95.93	14	-374.23	12	-0.10	10
7	7	-36	Min.	328.50	-959.33	2	-101.63	6	-120.40	6	-95.93	14	-60.10	10	-0.10	10
201	-5	-4	Max	0.00	20.77	6	20.77	10	17.63	16	261.89	2	-176.33	2	5.17	10
201	-5	-4	Max	80.60	20.77	6	20.77	10	2.99	6	188.50	2	5.17	2	5.17	10
201	-5	-4	Min.	0.00	-20.77	2	-20.77	14	-17.63	10	261.89	2	-186.68	6	-5.17	14
201	-5	-4	Min.	80.60	-20.77	2	-20.77	14	-2.99	4	188.50	2	-5.17	6	-5.17	14
201	-6	-5	Max	0.00	64.26	2	58.56	16	14.08	12	-480.79	2	213.49	2	54.92	14
201	-6	-5	Max	53.34	64.26	2	58.56	16	17.73	16	-529.36	2	-55.93	2	54.92	14
201	-6	-5	Min.	0.00	-151.35	6	-58.56	10	-14.08	14	-648.87	6	-141.53	6	-54.92	12
201	-6	-5	Min.	53.34	-151.35	6	-58.56	10	-17.73	10	-697.44	6	-500.61	6	-54.92	12
201	-7	-6	Max	0.00	31.62	2	25.92	16	47.08	12	-90.16	2	423.71	2	47.14	14
201	-7	-6	Max	133.94	31.62	2	25.92	16	15.43	12	-212.13	2	221.27	2	47.14	14
201	-7	-6	Min.	0.00	-118.71	6	-25.92	10	-47.08	14	-258.24	6	278.26	6	-47.14	12
201	-7	-6	Min.	133.94	-118.71	6	-25.92	10	-15.43	14	-380.21	6	-149.31	6	-47.14	12
201	-8	-7	Max	0.00	-4.41	2	12.39	12	32.00	10	300.47	2	174.84	6	39.36	14
201	-8	-7	Max	133.94	-4.41	2	12.39	12	48.43	12	178.50	2	431.50	2	39.36	14
201	-8	-7	Min.	0.00	-82.68	6	-12.39	14	-32.00	16	132.39	6	110.72	2	-39.36	12
201	-8	-7	Min.	133.94	-82.68	6	-12.39	14	-48.43	14	10.42	6	270.48	6	-39.36	12
201	-9	-8	Max	0.00	-40.43	2	48.42	12	31.67	14	691.10	2	-451.80	6	31.58	14
201	-9	-8	Max	133.94	-40.43	2	48.42	12	33.18	12	569.13	2	167.06	6	31.58	14
201	-9	-8	Min.	0.00	-46.66	6	-48.42	14	-31.67	12	523.02	6	-725.49	2	-31.58	12
201	-9	-8	Min.	133.94	-46.66	6	-48.42	14	-33.18	14	401.05	6	118.50	2	-31.58	12
201	-10	-9	Max	0.00	-14.38	6	80.70	12	67.64	16	1000.58	2	-823.64	6	23.79	14
201	-10	-9	Max	44.83	-14.38	6	80.70	12	32.48	16	959.76	2	-459.59	6	23.79	14
201	-10	-9	Min.	0.00	-72.71	2	-80.70	14	-67.64	10	832.50	6	-1157.11	2	-23.79	12
201	-10	-9	Min.	44.83	-72.71	2	-80.70	14	-32.48	10	791.68	6	-717.71	2	-23.79	12
202	-11	-10	Max	0.00	22.97	2	84.76	16	7.83	10	-864.92	2	-206.32	2	30.90	14
202	-11	-10	Max	89.11	22.97	2	84.76	16	67.70	16	-946.07	2	-1013.25	2	30.90	14
202	-11	-10	Min.	0.00	-220.34	6	-84.76	10	-7.83	16	-935.66	6	-341.77	6	-30.90	12
202	-11	-10	Min.	89.11	-220.34	6	-84.76	10	-67.70	10	-1016.81	6	-1211.73	6	-30.90	12
202	-12	-11	Max	0.00	-11.17	2	50.62	16	74.29	10	-474.29	2	518.42	2	23.11	14
202	-12	-11	Max	133.94	-11.17	2	50.62	16	8.43	12	-596.26	2	-198.54	2	23.11	14
202	-12	-11	Min.	0.00	-186.20	6	-50.62	10	-74.29	16	-545.04	6	462.17	6	-23.11	12
202	-12	-11	Min.	133.94	-186.20	6	-50.62	10	-8.43	14	-667.00	6	-349.55	6	-23.11	12
202	-13	-12	Max	0.00	-47.20	2	14.60	16	92.49	10	-83.66	2	742.89	6	15.33	14

202	-13	-12	Max	133.94	-47.20	2	14.60	16	74.75	12	-205.63	2	526.20	2	15.33	14
202	-13	-12	Min.	0.00	-150.18	6	-14.60	10	-92.49	16	-154.41	6	719.95	2	-15.33	12
202	-13	-12	Min.	133.94	-150.18	6	-14.60	10	-74.75	14	-276.38	6	454.39	6	-15.33	12
202	-14	-13	Max	0.00	-83.22	2	23.54	12	62.44	10	306.97	2	500.39	6	7.55	14
202	-14	-13	Max	133.94	-83.22	2	23.54	12	92.81	12	185.00	2	735.11	6	7.55	14
202	-14	-13	Min.	0.00	-114.15	6	-23.54	14	-62.44	16	236.22	6	398.25	2	-7.55	12
202	-14	-13	Min.	133.94	-114.15	6	-23.54	14	-92.81	14	114.25	6	727.73	2	-7.55	12
202	-15	-14	Max	0.00	-78.13	6	59.57	12	17.17	14	697.60	2	-265.33	6	0.40	10
202	-15	-14	Max	133.94	-78.13	6	59.57	12	62.62	12	575.63	2	492.61	6	0.40	10
202	-15	-14	Min.	0.00	-119.25	2	-59.57	14	-17.17	12	626.85	6	-446.66	2	-0.40	16
202	-15	-14	Min.	133.94	-119.25	2	-59.57	14	-62.62	14	504.88	6	406.04	2	-0.40	16
202	203	-15	Max	0.00	-44.17	6	93.53	12	95.05	14	1043.40	2	-1064.42	6	8.19	10
202	203	-15	Max	84.71	-44.17	6	93.53	12	17.21	16	966.25	2	-273.11	6	8.19	10
202	203	-15	Min.	0.00	-153.21	2	-93.53	14	-95.05	12	972.65	6	-1290.11	2	-8.19	16
202	203	-15	Min.	84.71	-153.21	2	-93.53	14	-17.21	10	895.51	6	-438.88	2	-8.19	16
203	-16	203	Max	0.00	34.88	2	84.75	16	54.29	14	-866.22	2	-505.09	2	14.61	16
203	-16	203	Max	49.23	34.88	2	84.75	16	95.03	14	-911.04	2	-942.55	2	14.61	16
203	-16	203	Min.	0.00	-142.70	6	-84.75	10	-54.29	12	-965.94	6	-728.83	6	-14.61	10
203	-16	203	Min.	49.23	-142.70	6	-84.75	10	-95.03	12	-1010.77	6	-1215.38	6	-14.61	10
203	-17	-16	Max	0.00	2.42	2	52.29	16	15.79	10	-475.59	2	221.38	2	6.83	16
203	-17	-16	Max	133.94	2.42	2	52.29	16	54.25	16	-597.56	2	-497.33	2	6.83	16
203	-17	-16	Min.	0.00	-110.23	8	-52.29	10	-15.79	16	-575.31	6	115.64	6	-6.83	10
203	-17	-16	Min.	133.94	-110.23	8	-52.29	10	-54.25	10	-697.28	6	-736.63	6	-6.83	10
203	-18	-17	Max	0.00	-33.61	2	16.26	16	36.22	10	-84.96	2	436.91	6	0.95	12
203	-18	-17	Max	133.94	-33.61	2	16.26	16	15.74	12	-206.93	2	229.15	2	0.95	12
203	-18	-17	Min.	0.00	-74.21	8	-16.26	10	-36.22	16	-184.69	6	424.64	2	-0.95	14
203	-18	-17	Min.	133.94	-74.21	8	-16.26	10	-15.74	14	-306.65	6	107.85	6	-0.95	14
203	-19	-18	Max	0.00	-38.19	6	21.77	12	8.40	10	305.67	2	234.96	6	8.73	12
203	-19	-18	Max	133.94	-38.19	6	21.77	12	36.17	12	183.70	2	432.41	2	8.73	12
203	-19	-18	Min.	0.00	-69.63	4	-21.77	14	-8.40	16	205.95	6	104.67	2	-8.73	14
203	-19	-18	Min.	133.94	-69.63	4	-21.77	14	-36.17	14	83.98	6	429.12	6	-8.73	14
203	-20	-19	Max	0.00	-2.16	6	57.80	12	69.06	14	696.30	2	-490.20	6	16.52	12
203	-20	-19	Max	133.94	-2.16	6	57.80	12	8.36	12	574.33	2	227.19	6	16.52	12
203	-20	-19	Min.	0.00	-105.66	4	-57.80	14	-69.06	12	596.57	6	-738.49	2	-16.52	14
203	-20	-19	Min.	133.94	-105.66	4	-57.80	14	-8.36	14	474.61	6	112.47	2	-16.52	14
203	204	-20	Max	0.00	21.68	6	81.65	12	84.50	16	903.00	2	-654.21	6	21.69	12
203	204	-20	Max	20.00	21.68	6	81.65	12	68.57	16	884.79	2	-495.37	6	21.69	12
203	204	-20	Min.	0.00	-129.50	2	-81.65	14	-84.50	10	803.28	6	-912.09	2	-21.69	14
203	204	-20	Min.	20.00	-129.50	2	-81.65	14	-68.57	10	785.07	6	-733.32	2	-21.69	14
204	204	-21	Max	0.00	21.68	2	81.65	16	84.50	12	903.00	6	-654.21	2	21.69	16
204	204	-21	Max	20.00	21.68	2	81.65	16	68.57	12	884.79	6	-495.37	2	21.69	16
204	204	-21	Min.	0.00	-129.50	6	-81.65	10	-84.50	14	803.28	2	-912.09	6	-21.69	10
204	204	-21	Min.	20.00	-129.50	6	-81.65	10	-68.57	14	785.07	2	-733.32	6	-21.69	10
204	-21	-22	Max	0.00	-2.16	2	57.80	16	69.06	10	696.30	6	-490.20	2	16.52	16
204	-21	-22	Max	133.94	-2.16	2	57.80	16	8.36	16	574.33	6	227.19	2	16.52	16
204	-21	-22	Min.	0.00	-105.66	8	-57.80	10	-69.06	16	596.57	2	-738.49	6	-16.52	10
204	-21	-22	Min.	133.94	-105.66	8	-57.80	10	-8.36	10	474.61	2	112.47	6	-16.52	10
204	-22	-23	Max	0.00	-38.19	2	21.77	16	8.40	14	305.67	6	234.96	2	8.73	16
204	-22	-23	Max	133.94	-38.19	2	21.77	16	36.17	16	183.70	6	432.41	6	8.73	16
204	-22	-23	Min.	0.00	-69.63	8	-21.77	10	-8.40	12	205.95	2	104.67	6	-8.73	10
204	-22	-23	Min.	133.94	-69.63	8	-21.77	10	-36.17	10	83.98	2	429.12	2	-8.73	10
204	-23	-24	Max	0.00	-33.61	6	16.26	12	36.22	14	-84.96	6	436.91	2	0.95	16
204	-23	-24	Max	133.94	-33.61	6	16.26	12	15.74	16	-206.93	6	229.16	6	0.95	16
204	-23	-24	Min.	0.00	-74.21	4	-16.26	14	-36.22	12	-184.69	2	424.64	6	-0.95	10
204	-23	-24	Min.	133.94	-74.21	4	-16.26	14	-15.74	10	-306.65	2	107.85	2	-0.95	10
204	-24	-25	Max	0.00	2.42	6	52.29	12	15.79	14	-475.59	6	221.38	6	6.83	12
204	-24	-25	Max	133.94	2.42	6	52.29	12	54.25	12	-597.56	6	-497.32	6	6.83	12
204	-24	-25	Min.	0.00	-110.23	4	-52.29	14	-15.79	12	-575.31	2	115.65	2	-6.83	14
204	-24	-25	Min.	133.94	-110.23	4	-52.29	14	-54.25	14	-697.28	2	-736.63	2	-6.83	14
204	-25	205	Max	0.00	34.88	6	84.75	12	54.29	10	-866.22	6	-505.09	6	14.61	12
204	-25	205	Max	49.23	34.88	6	84.75	12	95.03	10	-911.04	6	-942.54	6	14.61	12
204	-25	205	Min.	0.00	-142.70	2	-84.75	14	-54.29	16	-965.94	2	-728.83	2	-14.61	14
204	-25	205	Min.	49.23	-142.70	2	-84.75	14	-95.03	16	-1010.77	2	-1215.37	2	-14.61	14
205	205	-26	Max	0.00	-44.17	2	93.53	16	95.05	10	1043.40	6	-1064.41	2	8.19	14
205	205	-26	Max	84.71	-44.17	2	93.53	16	17.21	12	966.25	6	-273.11	2	8.19	14
205	205	-26	Min.	0.00	-153.20	6	-93.53	10	-95.05	16	972.65	2	-1290.11	6	-8.19	12
205	205	-26	Min.	84.71	-153.20	6	-93.53	10	-17.21	14	895.51	2	-438.87	6	-8.19	12
205	-26	-27	Max	0.00	-78.13	2	59.57	16	17.17	10	697.60	6	-265.37	2	0.40	14
205	-26	-27	Max	133.94	-78.13	2	59.57	16	62.62	16	575.63	6	492.58	2	0.40	14
205	-26	-27	Min.	0.00	-119.25	6	-59.57	10	-17.17	16	626.85	2	-446.70	6	-0.40	12
205	-26	-27	Min.	133.94	-119.25	6	-59.57	10	-62.62	10	504.89	2	406.00	6	-0.40	12
205	-27	-28	Max	0.00	-83.22	6	23.54	16	62.44	14	306.96	6	500.39	2	7.55	10
205	-27	-28	Max	133.94	-83.22	6	23.54	16	92.81	16	185.00	6	735.11	2	7.55	10
205	-27	-28	Min.	0.00	-114.15	2	-23.54	10	-62.44	12	236.22	6	398.26	6	-7.55	16
205	-27	-28	Min.	133.94	-114.15	2	-23.54	10	-92.81	10	114.25	2	727.73	6	-7.55	16
205	-28	-29	Max	0.00	-47.20	6	14.60	12	74.75	14	-83.66	6	742.89	2	15.33	10

205	-28	-29	Max	133.94	-47.20	6	14.60	12	74.75	16	-205.63	6	526.20	6	15.33	10
205	-28	-29	Min.	0.00	-150.18	2	-14.60	14	-92.49	12	-154.41	2	719.95	6	-15.33	16
205	-28	-29	Min.	133.94	-150.18	2	-14.60	14	-74.75	10	-276.37	2	454.39	2	-15.33	16
205	-29	-30	Max	0.00	-11.17	6	50.62	12	74.29	14	-474.29	6	518.43	6	23.11	10
205	-29	-30	Max	133.94	-11.17	6	50.62	12	8.43	16	-596.25	6	-198.53	6	23.11	10
205	-29	-30	Min.	0.00	-186.20	2	-50.62	14	-74.29	12	-545.03	2	462.18	2	-23.11	16
205	-29	-30	Min.	133.94	-186.20	2	-50.62	14	-8.43	10	-667.00	2	-349.54	2	-23.11	16
205	-30	-31	Max	0.00	22.97	6	84.76	12	7.83	14	-864.92	6	-206.35	6	30.90	10
205	-30	-31	Max	89.11	22.97	6	84.76	12	67.71	12	-946.07	6	-1013.28	6	30.90	10
205	-30	-31	Min.	0.00	-220.34	2	-84.76	14	-7.83	12	-935.67	2	-341.80	2	-30.90	16
205	-30	-31	Min.	89.11	-220.34	2	-84.76	14	-67.71	14	-1016.81	2	-1211.77	2	-30.90	16
206	-31	-32	Max	0.00	-14.38	2	80.70	16	67.63	12	1000.58	6	-823.63	2	23.79	10
206	-31	-32	Max	44.83	-14.38	2	80.70	16	32.48	12	959.76	6	-459.58	2	23.79	10
206	-31	-32	Min.	0.00	-72.71	6	-80.70	10	-67.63	14	832.50	2	-1157.11	6	-23.79	16
206	-31	-32	Min.	44.83	-72.71	6	-80.70	10	-32.48	14	791.68	2	-717.71	6	-23.79	16
206	-32	-33	Max	0.00	-40.43	6	48.42	16	31.67	10	691.10	6	-451.79	2	31.58	10
206	-32	-33	Max	133.94	-40.43	6	48.42	16	33.18	16	569.13	6	167.07	2	31.58	10
206	-32	-33	Min.	0.00	-46.66	2	-48.42	10	-31.67	16	523.02	2	-725.48	6	-31.58	16
206	-32	-33	Min.	133.94	-46.66	2	-48.42	10	-33.18	10	401.05	2	118.52	6	-31.58	16
206	-33	-34	Max	0.00	-4.41	6	12.39	16	32.00	14	300.47	6	174.84	2	39.36	10
206	-33	-34	Max	133.94	-4.41	6	12.39	16	48.43	16	178.50	6	431.50	6	39.36	10
206	-33	-34	Min.	0.00	-82.68	2	-12.39	10	-32.00	12	132.39	2	110.72	6	-39.36	16
206	-33	-34	Min.	133.94	-82.68	2	-12.39	10	-48.43	10	10.42	2	270.48	2	-39.36	16
206	-34	-35	Max	0.00	31.62	6	25.92	12	47.08	16	-90.15	6	423.71	6	47.14	10
206	-34	-35	Max	133.94	31.62	6	25.92	12	15.43	16	-212.12	6	221.27	6	47.14	10
206	-34	-35	Min.	0.00	-118.71	2	-25.92	14	-47.08	10	-258.24	2	278.26	2	-47.14	16
206	-34	-35	Min.	133.94	-118.71	2	-25.92	14	-15.43	10	-380.20	2	-149.31	2	-47.14	16
206	-35	-36	Max	0.00	64.26	6	58.56	12	14.08	16	-480.79	6	213.47	6	54.92	10
206	-35	-36	Max	53.34	64.26	6	58.56	12	17.73	12	-529.36	6	-55.95	6	54.92	10
206	-35	-36	Min.	0.00	-151.35	2	-58.56	14	-14.08	10	-648.87	2	-141.55	2	-54.92	16
206	-35	-36	Min.	53.34	-151.35	2	-58.56	14	-17.73	14	-697.44	2	-500.63	2	-54.92	16
206	-36	-37	Max	0.00	20.77	2	20.77	14	17.63	12	261.89	2	-176.33	6	5.17	14
206	-36	-37	Max	80.60	20.77	2	20.77	14	2.99	8	188.50	2	5.17	6	5.17	14
206	-36	-37	Min.	0.00	-20.77	6	-20.77	10	-17.63	14	261.89	2	-186.68	2	-5.17	10
206	-36	-37	Min.	80.60	-20.77	6	-20.77	10	-2.99	2	188.50	2	-5.17	2	-5.17	10
302	-4	-47	Max	0.00	83.14	14	3.04	6	4.57	2	49.76	10	-37.00	14	0.00	2
302	-4	-47	Max	150.00	14.49	14	3.04	6	0.00	2	10.12	10	0.00	14	0.00	2
302	-4	-47	Min.	0.00	80.10	10	-3.04	2	-4.57	6	44.49	14	-44.91	10	0.00	2
302	-4	-47	Min.	150.00	11.44	10	-3.04	2	0.00	6	4.85	14	0.00	10	0.00	2
302	-46	-4	Max	0.00	-9.45	10	7.03	2	0.00	2	-1.40	14	0.00	2	0.00	6
302	-46	-4	Max	150.00	-78.11	10	7.03	2	10.54	2	-41.04	14	-31.83	14	0.00	6
302	-46	-4	Min.	0.00	-16.48	14	-7.03	6	0.00	6	-13.57	10	0.00	6	0.00	2
302	-46	-4	Min.	150.00	-85.13	14	-7.03	6	-10.54	6	-53.21	10	-50.08	10	0.00	2
303	-6	-48	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
303	-6	-48	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
303	-6	-48	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
303	-6	-48	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
303	-49	-6	Max	0.00	-20.64	10	10.57	2	0.00	4	-5.81	14	0.00	14	0.00	8
303	-49	-6	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	8
303	-49	-6	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	10	0.00	2
303	-49	-6	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
304	-7	-96	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
304	-7	-96	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
304	-7	-96	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
304	-7	-96	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
304	-95	-7	Max	0.00	-20.64	10	10.57	2	0.00	8	-5.81	14	0.00	14	0.00	6
304	-95	-7	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
304	-95	-7	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	10	0.00	2
304	-95	-7	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
305	-8	-66	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
305	-8	-66	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
305	-8	-66	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
305	-8	-66	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
305	-67	-8	Max	0.00	-20.64	10	10.57	2	0.00	4	-5.81	14	0.00	16	0.00	6
305	-67	-8	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
305	-67	-8	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	10	0.00	2
305	-67	-8	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
306	-9	-69	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
306	-9	-69	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
306	-9	-69	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
306	-9	-69	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
306	-68	-9	Max	0.00	-20.64	10	10.57	2	0.00	4	-5.81	14	0.00	10	0.00	4
306	-68	-9	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	4
306	-68	-9	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	14	0.00	6
306	-68	-9	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	6
307	-11	-70	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2

307	-11	-70	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
307	-11	-70	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
307	-11	-70	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
307	-71	-11	Max	0.00	-20.64	10	10.57	2	0.00	2	-5.81	14	0.00	10	0.00	8
307	-71	-11	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	8
307	-71	-11	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	14	0.00	2
307	-71	-11	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
308	-12	-72	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
308	-12	-72	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
308	-12	-72	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
308	-12	-72	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
308	-73	-12	Max	0.00	-20.64	10	10.57	2	0.00	2	-5.81	14	0.00	14	0.00	4
308	-73	-12	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	4
308	-73	-12	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	10	0.00	6
308	-73	-12	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	6
309	-13	-74	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
309	-13	-74	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
309	-13	-74	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
309	-13	-74	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
309	-75	-13	Max	0.00	-20.64	10	10.57	2	0.00	4	-5.81	14	0.00	10	0.00	2
309	-75	-13	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	2
309	-75	-13	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	14	0.00	6
309	-75	-13	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	6
310	-14	-90	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
310	-14	-90	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
310	-14	-90	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
310	-14	-90	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
310	-91	-14	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	16	0.00	2
310	-91	-14	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	2
310	-91	-14	Min.	0.00	-31.21	14	-10.57	6	0.00	4	-24.12	10	0.00	10	0.00	8
310	-91	-14	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	8
311	-15	-92	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
311	-15	-92	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
311	-15	-92	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
311	-15	-92	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
311	-93	-15	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	2	0.00	6
311	-93	-15	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
311	-93	-15	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	6	0.00	2
311	-93	-15	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
312	-16	-98	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
312	-16	-98	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
312	-16	-98	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
312	-16	-98	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
312	-94	-16	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	6	0.00	6
312	-94	-16	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
312	-94	-16	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	2	0.00	2
312	-94	-16	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
313	-17	-97	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
313	-17	-97	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
313	-17	-97	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
313	-17	-97	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
313	-42	-17	Max	0.00	-20.64	10	10.57	2	0.00	8	-5.81	14	0.00	16	0.00	4
313	-42	-17	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	4
313	-42	-17	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	10	0.00	6
313	-42	-17	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	6
314	-18	-43	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
314	-18	-43	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
314	-18	-43	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
314	-18	-43	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
314	-44	-18	Max	0.00	-20.64	10	10.57	2	0.00	2	-5.81	14	0.00	16	0.00	6
314	-44	-18	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
314	-44	-18	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	10	0.00	4
314	-44	-18	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	4
315	-19	-45	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
315	-19	-45	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
315	-19	-45	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
315	-19	-45	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
315	-58	-19	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	6	0.00	6
315	-58	-19	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
315	-58	-19	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	2	0.00	2
315	-58	-19	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
316	-20	-63	Max	0.00	83.14	14	3.04	6	4.57	2	49.76	10	-37.00	14	0.00	2
316	-20	-63	Max	150.00	14.49	14	3.04	6	0.00	2	10.12	10	0.00	14	0.00	2
316	-20	-63	Min.	0.00	80.10	10	-3.04	2	-4.57	6	44.49	14	-44.91	10	0.00	2
316	-20	-63	Min.	150.00	11.44	10	-3.04	2	0.00	6	4.85	14	0.00	10	0.00	2
316	-65	-20	Max	0.00	-9.45	10	7.03	2	0.00	2	-1.40	14	0.00	10	0.00	8

316	-65	-20	Max	150.00	-78.11	10	7.03	2	10.54	2	-41.04	14	-31.83	14	0.00	8
316	-65	-20	Min.	0.00	-16.48	14	-7.03	6	0.00	8	-13.57	10	0.00	14	0.00	2
316	-65	-20	Min.	150.00	-85.13	14	-7.03	6	-10.54	6	-53.21	10	-50.08	10	0.00	2
317	-21	-51	Max	0.00	83.14	14	3.04	6	4.57	2	49.76	10	-37.00	14	0.00	2
317	-21	-51	Max	150.00	14.49	14	3.04	6	0.00	2	10.12	10	0.00	14	0.00	2
317	-21	-51	Min.	0.00	80.10	10	-3.04	2	-4.57	6	44.49	14	-44.91	10	0.00	2
317	-21	-51	Min.	150.00	11.44	10	-3.04	2	0.00	6	4.85	14	0.00	10	0.00	2
317	-50	-21	Max	0.00	-9.45	10	7.03	2	0.00	6	-1.40	14	0.00	16	0.00	8
317	-50	-21	Max	150.00	-78.11	10	7.03	2	10.54	2	-41.04	14	-31.83	14	0.00	8
317	-50	-21	Min.	0.00	-16.48	14	-7.03	6	0.00	4	-13.57	10	0.00	10	0.00	2
317	-50	-21	Min.	150.00	-85.13	14	-7.03	6	-10.54	6	-53.21	10	-50.08	10	0.00	2
318	-22	-53	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
318	-22	-53	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
318	-22	-53	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
318	-22	-53	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
318	-52	-22	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	2	0.00	2
318	-52	-22	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	2
318	-52	-22	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	2	0.00	6
318	-52	-22	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	6
319	-23	-55	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
319	-23	-55	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
319	-23	-55	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
319	-23	-55	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
319	-54	-23	Max	0.00	-20.64	10	10.57	2	0.00	4	-5.81	14	0.00	12	0.00	6
319	-54	-23	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
319	-54	-23	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	14	0.00	4
319	-54	-23	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	4
320	-24	-57	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
320	-24	-57	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
320	-24	-57	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
320	-24	-57	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
320	-56	-24	Max	0.00	-20.64	10	10.57	2	0.00	2	-5.81	14	0.00	2	0.00	2
320	-56	-24	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	2
320	-56	-24	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	2	0.00	6
320	-56	-24	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	6
322	-25	-41	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
322	-25	-41	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
322	-25	-41	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
322	-25	-41	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
322	-64	-25	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	2	0.00	6
322	-64	-25	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
322	-64	-25	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	2	0.00	2
322	-64	-25	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
323	-26	-77	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
323	-26	-77	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
323	-26	-77	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
323	-26	-77	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
323	-76	-26	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	2	0.00	2
323	-76	-26	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	2
323	-76	-26	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	2	0.00	2
323	-76	-26	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
324	-27	-79	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
324	-27	-79	Max	150.00	28.21	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
324	-27	-79	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
324	-27	-79	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
324	-78	-27	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	2	0.00	6
324	-78	-27	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
324	-78	-27	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	2	0.00	2
324	-78	-27	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
325	-28	-81	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
325	-28	-81	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
325	-28	-81	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
325	-28	-81	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
325	-80	-28	Max	0.00	-20.64	10	10.57	2	0.00	2	-5.81	14	0.00	2	0.00	2
325	-80	-28	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	2
325	-80	-28	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	2	0.00	6
325	-80	-28	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	6
326	-29	-83	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
326	-29	-83	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
326	-29	-83	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
326	-29	-83	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
326	-82	-29	Max	0.00	-20.64	10	10.57	2	0.00	6	-5.81	14	0.00	10	0.00	6
326	-82	-29	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
326	-82	-29	Min.	0.00	-31.21	14	-10.57	6	0.00	2	-24.12	10	0.00	16	0.00	4
326	-82	-29	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	4
327	-30	-85	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2

327	-30	-85	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
327	-30	-85	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
327	-30	-85	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
327	-84	-30	Max	0.00	-20.64	10	10.57	2	0.00	2	-5.81	14	0.00	2	0.00	6
327	-84	-30	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	6
327	-84	-30	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	2	0.00	2
327	-84	-30	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	2
329	-32	-86	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
329	-32	-86	Max	150.00	28.21	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
329	-32	-86	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
329	-32	-86	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
329	-87	-32	Max	0.00	-20.64	10	10.57	2	0.00	2	-5.81	14	0.00	12	0.00	16
329	-87	-32	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	16
329	-87	-32	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	14	0.00	10
329	-87	-32	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	10
330	-33	-89	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
330	-33	-89	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
330	-33	-89	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
330	-33	-89	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
330	-88	-33	Max	0.00	-20.64	10	10.57	2	0.00	2	-5.81	14	0.00	10	0.00	10
330	-88	-33	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	10
330	-88	-33	Min.	0.00	-31.21	14	-10.57	6	0.00	8	-24.12	10	0.00	16	0.00	14
330	-88	-33	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	14
331	-34	-61	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
331	-34	-61	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
331	-34	-61	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
331	-34	-61	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
331	-62	-34	Max	0.00	-20.64	10	10.57	2	0.00	4	-5.81	14	0.00	10	0.00	4
331	-62	-34	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	4
331	-62	-34	Min.	0.00	-31.21	14	-10.57	6	0.00	6	-24.12	10	0.00	16	0.00	6
331	-62	-34	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	6
332	-35	-102	Max	0.00	118.62	14	4.58	6	6.87	2	71.13	10	-55.65	14	0.00	2
332	-35	-102	Max	150.00	28.22	14	4.58	6	0.00	2	18.93	10	0.00	14	0.00	2
332	-35	-102	Min.	0.00	114.04	10	-4.58	2	-6.87	6	63.20	14	-67.55	10	0.00	2
332	-35	-102	Min.	150.00	23.64	10	-4.58	2	0.00	6	11.00	14	0.00	10	0.00	2
332	-101	-35	Max	0.00	-20.64	10	10.57	2	0.00	10	-5.81	14	0.00	10	0.00	14
332	-101	-35	Max	150.00	-111.05	10	10.57	2	15.85	2	-58.01	14	-47.87	14	0.00	14
332	-101	-35	Min.	0.00	-31.21	14	-10.57	6	0.00	14	-24.12	10	0.00	14	0.00	10
332	-101	-35	Min.	150.00	-121.62	14	-10.57	6	-15.85	6	-76.32	10	-75.33	10	0.00	10
333	-37	-103	Max	0.00	83.14	14	3.04	6	4.57	2	49.76	10	-37.00	14	0.00	2
333	-37	-103	Max	150.00	14.49	14	3.04	6	0.00	2	10.12	10	0.00	14	0.00	2
333	-37	-103	Min.	0.00	80.10	10	-3.04	2	-4.57	6	44.49	14	-44.91	10	0.00	2
333	-37	-103	Min.	150.00	11.44	10	-3.04	2	0.00	6	4.85	14	0.00	10	0.00	2
333	-104	-37	Max	0.00	-9.45	10	7.03	2	0.00	6	-1.40	14	0.00	16	0.00	8
333	-104	-37	Max	150.00	-78.11	10	7.03	2	10.54	2	-41.04	14	-31.83	14	0.00	8
333	-104	-37	Min.	0.00	-16.48	14	-7.03	6	0.00	4	-13.57	10	0.00	10	0.00	2
333	-104	-37	Min.	150.00	-85.13	14	-7.03	6	-10.54	6	-53.21	10	-50.08	10	0.00	2

Tipo di combinazione di carico: SLU

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-608.05	21	101.12	28	-7.40	21	1676.27	21	4481.79	28	1.51	28
1	1	-5	Max	328.50	-298.56	21	101.12	28	224.66	28	1676.27	21	573.15	28	1.51	28
1	1	-5	Min.	0.00	-2200.61	28	7.01	21	-107.52	28	-1189.85	28	-6314.01	21	-2.12	21
1	1	-5	Min.	328.50	-1891.12	28	7.01	21	15.64	21	-1189.85	28	-807.46	21	-2.12	21
2	2	-10	Max	0.00	-818.61	21	121.51	28	-17.35	21	3639.14	21	8054.13	28	1.01	28
2	2	-10	Max	328.50	-509.12	21	121.51	28	269.14	28	3639.14	21	607.80	21	1.01	28
2	2	-10	Min.	0.00	-4534.29	28	16.16	21	-130.01	28	-2583.12	28	-11346.80	21	-1.42	21
2	2	-10	Min.	328.50	-4224.80	28	16.16	21	35.75	21	-2583.12	28	-431.43	28	-1.42	21
3	3	203	Max	0.00	-845.75	21	-12.12	21	108.56	28	3857.05	21	8758.75	28	0.60	21
3	3	203	Max	328.50	-536.26	21	-12.12	21	-26.63	21	3857.05	21	330.97	21	0.60	21
3	3	203	Min.	0.00	-4684.95	28	-99.57	28	13.20	21	-2737.80	28	-12339.40	21	-0.42	28
3	3	203	Min.	328.50	-4375.46	28	-99.57	28	-218.54	28	-2737.80	28	-234.93	28	-0.42	28
4	4	204	Max	0.00	-919.48	21	0.00	28	0.00	21	2327.47	28	11034.10	21	0.00	28
4	4	204	Max	328.50	-609.99	21	0.00	28	0.00	21	2327.47	28	262.62	21	0.00	28
4	4	204	Min.	0.00	-3970.91	28	-0.00	21	0.00	28	-3278.98	21	-7832.16	28	0.00	21
4	4	204	Min.	328.50	-3661.43	28	-0.00	21	0.00	28	-3278.98	21	-186.41	28	0.00	21
5	5	205	Max	0.00	-845.74	21	-12.12	21	108.56	28	2737.80	28	12339.50	21	0.42	28
5	5	205	Max	328.50	-536.25	21	-12.12	21	-26.63	21	2737.80	28	234.93	28	0.42	28
5	5	205	Min.	0.00	-4684.95	28	-99.57	28	13.20	21	-3857.06	21	-8758.75	28	-0.60	21
5	5	205	Min.	328.50	-4375.46	28	-99.57	28	-218.53	28	-3857.06	21	-330.98	21	-0.60	21
6	6	-31	Max	0.00	-818.60	21	121.51	28	-17.36	21	2583.12	28	11346.80	21	1.42	21
6	6	-31	Max	328.50	-509.12	21	121.51	28	269.14	28	2583.12	28	431.42	28	1.42	21
6	6	-31	Min.	0.00	-4534.29	28	16.16	21	-130.01	28	-3639.14	21	-8054.13	28	-1.01	28
6	6	-31	Min.	328.50	-4224.80	28	16.16	21	35.75	21	-3639.14	21	-607.80	21	-1.01	28



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7	7	-36	Max	0.00	-608.05	21	101.12	28	-7.40	21	1189.84	28	6314.01	21	2.12	21
7	7	-36	Max	328.50	-298.56	21	101.12	28	224.66	28	1189.84	28	807.46	21	2.12	21
7	7	-36	Min.	0.00	-2200.60	28	7.01	21	-107.52	28	-1676.27	21	-4481.79	28	-1.51	28
7	7	-36	Min.	328.50	-1891.11	28	7.01	21	15.64	21	-1676.27	21	-573.15	28	-1.51	28
201	-5	-4	Max	0.00	0.00	17	274.09	28	311.23	21	520.75	28	-74.04	21	0.00	21
201	-5	-4	Max	80.60	0.00	17	274.09	28	0.00	28	425.33	28	0.00	28	0.00	21
201	-5	-4	Min.	0.00	0.00	17	-386.14	21	-220.92	28	139.56	21	-381.27	28	0.00	17
201	-5	-4	Min.	80.60	0.00	17	-386.14	21	-0.00	21	44.15	21	0.00	21	0.00	17
201	-6	-5	Max	0.00	-7.01	21	1290.13	21	266.07	28	-95.86	21	108.22	28	807.46	21
201	-6	-5	Max	53.34	-7.01	21	1290.13	21	313.35	21	-159.00	21	-89.67	21	807.46	21
201	-6	-5	Min.	0.00	-101.12	28	-915.76	28	-374.84	21	-1307.22	28	-21.70	21	-573.15	28
201	-6	-5	Min.	53.34	-101.12	28	-915.76	28	-222.42	28	-1370.37	28	-605.93	28	-573.15	28
201	-7	-6	Max	0.00	-7.01	21	517.85	21	758.41	28	10.18	21	802.18	28	807.46	21
201	-7	-6	Max	8.60					-1023.95	21			71.30	21		
201	-7	-6	Min.	133.94	-7.01	21	517.85	21	266.07	28	-148.38	21	108.22	28	807.46	21
201	-7	-6	Min.	0.00	-101.12	28	-367.58	28	-1068.46	21	-438.82	28	70.86	21	-573.15	28
201	-7	-6	Min.	8.60					-1023.95	21			71.30	21		
201	-7	-6	Min.	133.94	-101.12	28	-367.58	28	-374.84	21	-597.38	28	-21.70	21	-573.15	28
201	-8	-7	Max	0.00	-7.01	21	180.60	28	516.51	28	429.57	28	332.99	28	807.46	21
201	-8	-7	Max	98.17					-977.43	21			78.44	21		
201	-8	-7	Max	133.94	-7.01	21	180.60	28	758.41	28	271.02	28	802.18	28	807.46	21
201	-8	-7	Min.	0.00	-101.12	28	-254.44	21	-727.66	21	116.21	21	21.40	21	-573.15	28
201	-8	-7	Min.	98.17					-977.43	21			78.44	21		
201	-8	-7	Min.	133.94	-101.12	28	-254.44	21	-1068.46	21	-42.35	21	70.86	21	-573.15	28
201	-9	-8	Max	0.00	-7.01	21	728.78	28	647.55	21	1297.97	28	-170.08	21	807.46	21
201	-9	-8	Max	133.94	-7.01	21	728.78	28	516.51	28	1139.41	28	332.99	28	807.46	21
201	-9	-8	Min.	0.00	-101.12	28	-1026.72	21	-459.64	28	222.24	21	-1299.37	28	-573.15	28
201	-9	-8	Min.	133.94	-101.12	28	-1026.72	21	-727.66	21	63.68	21	21.40	21	-573.15	28
201	-10	-9	Max	0.00	-7.01	21	1276.96	28	1454.03	21	2060.88	28	-258.06	21	807.46	21
201	-10	-9	Max	44.83	-7.01	21	1276.96	28	647.56	21	2007.81	28	-170.08	21	807.46	21
201	-10	-9	Min.	0.00	-101.12	28	-1799.00	21	-1032.09	28	222.78	21	-2211.34	28	-573.15	28
201	-10	-9	Min.	44.83	-101.12	28	-1799.00	21	-459.65	28	169.71	21	-1299.37	28	-573.15	28
202	-11	-10	Max	0.00	-23.18	21	1840.14	21	130.87	28	-180.85	21	-85.63	21	199.66	21
202	-11	-10	Max	89.11	-23.18	21	1840.14	21	1455.45	21	-286.34	21	-293.80	21	199.66	21
202	-11	-10	Min.	0.00	-222.63	28	-1306.16	28	-184.37	21	-2058.43	28	-599.13	28	-141.73	28
202	-11	-10	Min.	89.11	-222.63	28	-1306.16	28	-1033.10	28	-2163.92	28	-2480.49	28	-141.73	28
202	-12	-11	Max	0.00	-23.18	21	1067.86	21	1146.14	28	-74.82	21	1101.02	28	199.66	21
202	-12	-11	Max	133.94	-23.18	21	1067.86	21	130.87	28	-233.38	21	-85.63	21	199.66	21
202	-12	-11	Min.	0.00	-222.63	28	-757.98	28	-1614.69	21	-1190.03	28	120.77	21	-141.73	28
202	-12	-11	Min.	133.94	-222.63	28	-757.98	28	-184.38	21	-1348.59	28	-599.13	28	-141.73	28
202	-13	-12	Max	0.00	-23.18	21	295.57	21	1427.16	28	31.21	21	1638.01	28	199.66	21
202	-13	-12	Max	26.41					-1932.52	21			189.27	21		
202	-13	-12	Max	133.94	-23.18	21	295.57	21	1146.14	28	-127.35	21	1101.02	28	199.66	21
202	-13	-12	Min.	0.00	-222.63	28	-209.80	28	-2010.60	21	-321.63	28	185.16	21	-141.73	28
202	-13	-12	Min.	26.41					-1932.52	21			189.27	21		
202	-13	-12	Min.	133.94	-222.63	28	-209.80	28	-1614.69	21	-480.19	28	120.77	21	-141.73	28
202	-14	-13	Max	0.00	-23.18	21	338.38	28	973.93	28	546.77	28	1011.84	28	199.66	21
202	-14	-13	Max	115.94					-1924.75	21			187.07	21		
202	-14	-13	Max	133.94	-23.18	21	338.38	28	1427.16	28	388.21	28	1638.01	28	199.66	21
202	-14	-13	Min.	0.00	-222.63	28	-476.71	21	-1372.08	21	137.24	21	107.52	21	-141.73	28
202	-14	-13	Min.	115.94					-1924.75	21			187.07	21		
202	-14	-13	Min.	133.94	-222.63	28	-476.71	21	-2010.60	21	-21.32	21	185.16	21	-141.73	28
202	-15	-14	Max	0.00	-23.18	21	886.55	28	300.85	21	1415.17	28	-112.14	21	199.66	21
202	-15	-14	Max	133.94	-23.18	21	886.55	28	973.93	28	1256.61	28	1011.84	28	199.66	21
202	-15	-14	Min.	0.00	-222.63	28	-1248.99	21	-213.55	28	243.27	21	-777.48	28	-141.73	28
202	-15	-14	Min.	133.94	-222.63	28	-1248.99	21	-1372.08	21	84.71	21	107.52	21	-141.73	28
202	203	-15	Max	0.00	-23.18	21	1434.73	28	2013.17	21	2225.29	28	-316.21	21	199.66	21
202	203	-15	Max	84.71	-23.18	21	1434.73	28	300.86	21	2125.01	28	-112.14	21	199.66	21
202	203	-15	Min.	0.00	-222.63	28	-2021.27	21	-1428.98	28	291.03	21	-2620.16	28	-141.73	28
202	203	-15	Min.	84.71	-222.63	28	-2021.27	21	-213.55	28	190.75	21	-777.49	28	-141.73	28
203	-16	203	Max	0.00	-11.06	21	1835.78	21	1108.82	21	-186.95	21	-183.20	21	93.20	28
203	-16	203	Max	49.23	-11.06	21	1835.78	21	2012.54	21	-245.23	21	-289.58	21	93.20	28
203	-16	203	Min.	0.00	-123.05	28	-1303.07	28	-787.06	28	-2091.89	28	-1357.43	28	-131.31	21
203	-16	203	Min.	49.23	-123.05	28	-1303.07	28	-1428.54	28	-2150.17	28	-2401.58	28	-131.31	21
203	-17	-16	Max	0.00	-11.06	21	1063.50	21	224.04	28	-80.92	21	387.50	28	93.20	28
203	-17	-16	Max	133.94	-11.06	21	1063.50	21	1108.85	21	-239.48	21	-183.21	21	93.20	28
203	-17	-16	Min.	0.00	-123.05	28	-754.89	28	-315.64	21	-1223.50	28	31.38	21	-131.31	21
203	-17	-16	Min.	133.94	-123.05	28	-754.89	28	-787.08	28	-1382.06	28	-1357.47	28	-131.31	21
203	-18	-17	Max	0.00	-11.06	21	291.22	21	500.91	28	25.10	21	969.31	28	93.20	28
203	-18	-17	Max	21.21					-643.94	21			106.60	21		
203	-18	-17	Max	133.94	-11.06	21	291.22	21	224.04	28	-133.46	21	387.49	28	93.20	28
203	-18	-17	Min.	0.00	-123.05	28	-206.71	28	-705.69	21	-355.10	28	103.94	21	-131.31	21
203	-18	-17	Min.	21.21					-643.94	21			106.60	21		
203	-18	-17	Min.	133.94	-123.05	28	-206.71	28	-315.63	21	-513.66	28	31.37	21	-131.31	21
203	-19	-18	Max	0.00	-11.06	21	341.47	28	43.52	28	513.31	28	387.94	28	93.20	28
203	-19	-18	Max	110.78					-594.25	21			107.11	21		

203	-19	-18	Max	133.94	-11.06	21	341.47	28	500.89	28	354.75	28	969.28	28	93.20	28
203	-19	-18	Min.	0.00	-123.05	28	-481.06	21	-61.31	21	131.14	21	34.47	21	-131.31	21
203	-19	-18	Min.	110.78					-594.25	21			107.11	21		
203	-19	-18	Min.	133.94	-123.05	28	-481.06	21	-705.66	21	-27.42	21	103.94	21	-131.31	21
203	-20	-19	Max	0.00	-11.06	21	889.65	28	1617.42	21	1381.70	28	-177.01	21	93.20	28
203	-20	-19	Max	133.94	-11.06	21	889.65	28	43.54	28	1223.14	28	387.97	28	93.20	28
203	-20	-19	Min.	0.00	-123.05	28	-1253.35	21	-1148.07	28	237.17	21	-1356.53	28	-131.31	21
203	-20	-19	Min.	133.94	-123.05	28	-1253.35	21	-61.34	21	78.61	21	34.47	21	-131.31	21
203	204	-20	Max	0.00	-11.06	21	1163.74	28	1945.32	21	1830.71	28	-235.64	21	93.20	28
203	204	-20	Max	20.00	-11.06	21	1163.74	28	1617.43	21	1807.04	28	-177.01	21	93.20	28
203	204	-20	Min.	0.00	-123.05	28	-1639.49	21	-1380.82	28	305.00	21	-1720.30	28	-131.31	21
203	204	-20	Min.	20.00	-123.05	28	-1639.49	21	-1148.08	28	281.32	21	-1356.53	28	-131.31	21
204	204	-21	Max	0.00	-11.05	21	1639.49	21	1380.82	28	1830.71	28	-235.64	21	131.31	21
204	204	-21	Max	20.00	-11.05	21	1639.49	21	1148.08	28	1807.04	28	-177.01	21	131.31	21
204	204	-21	Min.	0.00	-123.05	28	-1163.74	28	-1945.32	21	305.00	21	-1720.31	28	-93.20	28
204	204	-21	Min.	20.00	-123.05	28	-1163.74	28	-1617.43	21	281.32	21	-1356.53	28	-93.20	28
204	-21	-22	Max	0.00	-11.05	21	1253.35	21	1148.07	28	1381.70	28	-177.01	21	131.31	21
204	-21	-22	Max	133.94	-11.05	21	1253.35	21	61.35	21	1223.14	28	387.97	28	131.31	21
204	-21	-22	Min.	0.00	-123.05	28	-889.65	28	-1617.42	21	237.17	21	-1356.53	28	-93.20	28
204	-21	-22	Min.	133.94	-123.05	28	-889.65	28	-43.55	28	78.61	21	34.47	21	-93.20	28
204	-22	-23	Max	0.00	-11.05	21	481.07	21	61.31	21	513.31	28	387.94	28	131.31	21
204	-22	-23	Max	110.78					594.25	21			107.11	21		
204	-22	-23	Max	133.94	-11.05	21	481.07	21	705.66	21	354.75	28	969.29	28	131.31	21
204	-22	-23	Min.	0.00	-123.05	28	-341.47	28	-43.52	28	131.14	21	34.47	21	-93.20	28
204	-22	-23	Min.	110.78					594.25	21			107.11	21		
204	-22	-23	Min.	133.94	-123.05	28	-341.47	28	-500.89	28	-27.42	21	103.94	21	-93.20	28
204	-23	-24	Max	0.00	-11.05	21	206.71	28	705.70	21	25.10	21	969.31	28	131.31	21
204	-23	-24	Max	21.21					643.94	21			106.60	21		
204	-23	-24	Max	133.94	-11.05	21	206.71	28	315.64	21	-133.46	21	387.49	28	131.31	21
204	-23	-24	Min.	0.00	-123.05	28	-291.22	21	-500.92	28	-355.10	28	103.94	21	-93.20	28
204	-23	-24	Min.	21.21					643.94	21			106.60	21		
204	-23	-24	Min.	133.94	-123.05	28	-291.22	21	-224.04	28	-513.66	28	31.37	21	-93.20	28
204	-24	-25	Max	0.00	-11.05	21	754.89	28	315.65	21	-80.92	21	387.51	28	131.31	21
204	-24	-25	Max	133.94	-11.05	21	754.89	28	787.07	28	-239.48	21	-183.21	21	131.31	21
204	-24	-25	Min.	0.00	-123.05	28	-1063.50	21	-224.05	28	-1223.49	28	31.38	21	-93.20	28
204	-24	-25	Min.	133.94	-123.05	28	-1063.50	21	-1108.84	21	-1382.05	28	-1357.47	28	-93.20	28
204	-25	205	Max	0.00	-11.05	21	1303.07	28	787.05	28	-186.95	21	-183.20	21	131.31	21
204	-25	205	Max	49.23	-11.05	21	1303.07	28	1428.53	28	-245.23	21	-289.57	21	131.31	21
204	-25	205	Min.	0.00	-123.05	28	-1835.78	21	-1108.80	21	-2091.89	28	-1357.42	28	-93.20	28
204	-25	205	Min.	49.23	-123.05	28	-1835.78	21	-2012.53	21	-2150.17	28	-2401.57	28	-93.20	28
205	205	-26	Max	0.00	-23.18	21	2021.27	21	1428.97	28	2225.29	28	-316.21	21	141.73	28
205	205	-26	Max	84.71	-23.18	21	2021.27	21	213.54	28	2125.01	28	-112.14	21	141.73	28
205	205	-26	Min.	0.00	-222.62	28	-1434.73	28	-2013.16	21	291.03	21	-2620.14	28	-199.67	21
205	205	-26	Min.	84.71	-222.62	28	-1434.73	28	-300.84	21	190.74	21	-777.47	28	-199.67	21
205	-26	-27	Max	0.00	-23.18	21	1248.99	21	213.61	28	1415.17	28	-112.15	21	141.73	28
205	-26	-27	Max	133.94	-23.18	21	1248.99	21	1372.00	21	1256.61	28	1011.76	28	141.73	28
205	-26	-27	Min.	0.00	-222.62	28	-886.55	28	-300.94	21	243.28	21	-777.57	28	-199.67	21
205	-26	-27	Min.	133.94	-222.62	28	-886.55	28	-973.87	28	84.72	21	107.51	21	-199.67	21
205	-27	-28	Max	0.00	-23.18	21	476.71	21	1372.09	21	546.77	28	1011.85	28	141.73	28
205	-27	-28	Max	115.93					1924.75	21			187.07	21		
205	-27	-28	Max	133.94	-23.18	21	476.71	21	2010.61	21	388.21	28	1638.02	28	141.73	28
205	-27	-28	Min.	0.00	-222.62	28	-338.38	28	-973.93	28	137.24	21	107.52	21	-199.67	21
205	-27	-28	Min.	115.93					1924.75	21			187.07	21		
205	-27	-28	Min.	133.94	-222.62	28	-338.38	28	-1427.16	28	-21.32	21	185.15	21	-199.67	21
205	-28	-29	Max	0.00	-23.18	21	209.80	28	2010.59	21	31.21	21	1638.01	28	141.73	28
205	-28	-29	Max	26.41					1932.52	21			189.27	21		
205	-28	-29	Max	133.94	-23.18	21	209.80	28	1614.70	21	-127.35	21	1101.02	28	141.73	28
205	-28	-29	Min.	0.00	-222.62	28	-295.57	21	-1427.15	28	-321.63	28	185.15	21	-199.67	21
205	-28	-29	Min.	26.41					1932.52	21			189.27	21		
205	-28	-29	Min.	133.94	-222.62	28	-295.57	21	-1146.14	28	-480.19	28	120.77	21	-199.67	21
205	-29	-30	Max	0.00	-23.18	21	757.98	28	1614.70	21	-74.82	21	1101.03	28	141.73	28
205	-29	-30	Max	133.94	-23.18	21	757.98	28	184.39	21	-233.37	21	-85.62	21	141.73	28
205	-29	-30	Min.	0.00	-222.62	28	-1067.86	21	-1146.14	28	-1190.02	28	120.77	21	-199.67	21
205	-29	-30	Min.	133.94	-222.62	28	-1067.86	21	-130.88	28	-1348.58	28	-599.11	28	-199.67	21
205	-30	-31	Max	0.00	-23.18	21	1306.16	28	184.31	21	-180.85	21	-85.64	21	141.73	28
205	-30	-31	Max	89.11	-23.18	21	1306.16	28	1033.14	28	-286.35	21	-293.81	21	141.73	28
205	-30	-31	Min.	0.00	-222.62	28	-1840.14	21	-130.83	28	-2058.43	28	-599.21	28	-199.67	21
205	-30	-31	Min.	89.11	-222.62	28	-1840.14	21	-1455.50	21	-2163.92	28	-2480.56	28	-199.67	21
206	-31	-32	Max	0.00	-7.01	21	1799.00	21	1032.08	28	2060.88	28	-258.05	21	573.15	28
206	-31	-32	Max	44.83	-7.01	21	1799.00	21	459.63	28	2007.81	28	-170.08	21	573.15	28
206	-31	-32	Min.	0.00	-101.12	28	-1276.96	28	-1454.02	21	222.78	21	-2211.34	28	-807.46	21
206	-31	-32	Min.	44.83	-101.12	28	-1276.96	28	-647.54	21	169.71	21	-1299.36	28	-807.46	21
206	-32	-33	Max	0.00	-7.01	21	1026.72	21	459.62	28	1297.97	28	-170.08	21	573.15	28
206	-32	-33	Max	133.94	-7.01	21	1026.72	21	727.69	21	1139.42	28	333.02	28	573.15	28
206	-32	-33	Min.	0.00	-101.12	28	-728.78	28	-647.52	21	222.24	21	-1299.34	28	-807.46	21
206	-32	-33	Min.	133.94	-101.12	28	-728.78	28	-516.53	28	63.68	21	21.40	21	-807.46	21

206	-33	-34	Max	0.00	-7.01	21	254.44	21	727.66	21	429.58	28	332.98	28	573.15	28
206	-33	-34	Max	98.17					977.44	21			78.44	21		
206	-33	-34	Max	133.94	-7.01	21	254.44	21	1068.47	21	271.02	28	802.18	28	573.15	28
206	-33	-34	Min.	0.00	-101.12	28	-180.60	28	-516.51	28	116.21	21	21.40	21	-807.46	21
206	-33	-34	Min.	98.17					977.44	21			78.44	21		
206	-33	-34	Min.	133.94	-101.12	28	-180.60	28	-758.41	28	-42.35	21	70.86	21	-807.46	21
206	-34	-35	Max	0.00	-7.01	21	367.58	28	1068.46	21	10.18	21	802.18	28	573.15	28
206	-34	-35	Max	8.60					1023.92	21			71.30	21		
206	-34	-35	Max	133.94	-7.01	21	367.58	28	374.84	21	-148.38	21	108.22	28	573.15	28
206	-34	-35	Min.	0.00	-101.12	28	-517.85	21	-758.41	28	-438.82	28	70.86	21	-807.46	21
206	-34	-35	Min.	8.60					1023.92	21			71.30	21		
206	-34	-35	Min.	133.94	-101.12	28	-517.85	21	-266.07	28	-597.38	28	-21.69	21	-807.46	21
206	-35	-36	Max	0.00	-7.01	21	915.75	28	374.80	21	-95.86	21	108.18	28	573.15	28
206	-35	-36	Max	53.34	-7.01	21	915.75	28	222.45	28	-159.00	21	-89.68	21	573.15	28
206	-35	-36	Min.	0.00	-101.12	28	-1290.13	21	-266.04	28	-1307.22	28	-21.70	21	-807.46	21
206	-35	-36	Min.	53.34	-101.12	28	-1290.13	21	-313.39	21	-1370.37	28	-605.97	28	-807.46	21
206	-36	-37	Max	0.00	0.00	17	386.14	21	220.92	28	520.75	28	-74.04	21	0.00	21
206	-36	-37	Max	80.60	0.00	17	386.14	21	0.00	21	425.33	28	0.00	28	0.00	21
206	-36	-37	Min.	0.00	0.00	17	-274.09	28	-311.23	21	139.56	21	-381.27	28	0.00	17
206	-36	-37	Min.	80.60	0.00	17	-274.09	28	-0.00	28	44.15	21	0.00	21	0.00	17
302	-4	-47	Max	0.00	118.26	29	0.00	17	0.00	17	225.02	28	170.72	21	0.00	17
302	-4	-47	Max	150.00	21.39	29	0.00	17	0.00	17	70.88	28	0.00	21	0.00	17
302	-4	-47	Min.	0.00	115.65	21	0.00	17	0.00	17	-156.17	21	-221.93	28	0.00	17
302	-4	-47	Min.	150.00	20.42	21	0.00	17	0.00	17	-71.47	21	0.00	28	0.00	17
302	-46	-4	Max	0.00	-20.42	21	0.00	17	0.00	17	71.47	21	0.00	17	0.00	17
302	-46	-4	Max	150.00	-115.65	21	0.00	17	0.00	17	156.17	21	170.72	21	0.00	17
302	-46	-4	Min.	0.00	-21.39	29	0.00	17	0.00	17	-70.88	28	0.00	28	0.00	17
302	-46	-4	Min.	150.00	-118.26	29	0.00	17	0.00	17	-225.02	28	-221.93	28	0.00	17
303	-6	-48	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
303	-6	-48	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
303	-6	-48	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
303	-6	-48	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
303	-49	-6	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	21	0.00	17
303	-49	-6	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
303	-49	-6	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	17	0.00	17
303	-49	-6	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
304	-7	-96	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
304	-7	-96	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
304	-7	-96	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
304	-7	-96	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
304	-95	-7	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	17	0.00	17
304	-95	-7	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
304	-95	-7	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	21	0.00	17
304	-95	-7	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
305	-8	-66	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
305	-8	-66	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
305	-8	-66	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
305	-8	-66	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
305	-67	-8	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	17	0.00	17
305	-67	-8	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
305	-67	-8	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	21	0.00	17
305	-67	-8	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
306	-9	-69	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
306	-9	-69	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
306	-9	-69	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
306	-9	-69	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
306	-68	-9	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	28	0.00	17
306	-68	-9	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
306	-68	-9	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	21	0.00	17
306	-68	-9	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
307	-11	-70	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
307	-11	-70	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
307	-11	-70	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
307	-11	-70	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
307	-71	-11	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	28	0.00	17
307	-71	-11	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
307	-71	-11	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	21	0.00	17
307	-71	-11	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
308	-12	-72	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
308	-12	-72	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
308	-12	-72	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
308	-12	-72	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
308	-73	-12	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	17	0.00	17
308	-73	-12	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
308	-73	-12	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	28	0.00	17
308	-73	-12	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17

309	-13	-74	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
309	-13	-74	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
309	-13	-74	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
309	-13	-74	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
309	-75	-13	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	28	0.00	17
309	-75	-13	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
309	-75	-13	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	17	0.00	17
309	-75	-13	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
310	-14	-90	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
310	-14	-90	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
310	-14	-90	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
310	-14	-90	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
310	-91	-14	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	28	0.00	17
310	-91	-14	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
310	-91	-14	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	17	0.00	17
310	-91	-14	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
311	-15	-92	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
311	-15	-92	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
311	-15	-92	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
311	-15	-92	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
311	-93	-15	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	21	0.00	17
311	-93	-15	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
311	-93	-15	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	17	0.00	17
311	-93	-15	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
312	-16	-98	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
312	-16	-98	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
312	-16	-98	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
312	-16	-98	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
312	-94	-16	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	21	0.00	17
312	-94	-16	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
312	-94	-16	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	28	0.00	17
312	-94	-16	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
313	-17	-97	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
313	-17	-97	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
313	-17	-97	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
313	-17	-97	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
313	-42	-17	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	17	0.00	17
313	-42	-17	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
313	-42	-17	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	21	0.00	17
313	-42	-17	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
314	-18	-43	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
314	-18	-43	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
314	-18	-43	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
314	-18	-43	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
314	-44	-18	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	17	0.00	17
314	-44	-18	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
314	-44	-18	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	21	0.00	17
314	-44	-18	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
315	-19	-45	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
315	-19	-45	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
315	-19	-45	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
315	-19	-45	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17
315	-58	-19	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	28	0.00	17
315	-58	-19	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
315	-58	-19	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	17	0.00	17
315	-58	-19	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
316	-20	-63	Max	0.00	118.26	29	0.00	17	0.00	17	225.02	28	170.72	21	0.00	17
316	-20	-63	Max	150.00	21.39	29	0.00	17	0.00	17	70.88	28	0.00	21	0.00	17
316	-20	-63	Min.	0.00	115.65	21	0.00	17	0.00	17	-156.17	21	-221.93	28	0.00	17
316	-20	-63	Min.	150.00	20.42	21	0.00	17	0.00	17	-71.47	21	0.00	28	0.00	17
316	-65	-20	Max	0.00	-20.42	21	0.00	17	0.00	17	71.47	21	0.00	28	0.00	17
316	-65	-20	Max	150.00	-115.65	21	0.00	17	0.00	17	156.17	21	170.72	21	0.00	17
316	-65	-20	Min.	0.00	-21.39	29	0.00	17	0.00	17	-70.88	28	0.00	17	0.00	17
316	-65	-20	Min.	150.00	-118.26	29	0.00	17	0.00	17	-225.02	28	-221.93	28	0.00	17
317	-21	-51	Max	0.00	118.26	29	0.00	17	0.00	17	225.02	28	170.72	21	0.00	17
317	-21	-51	Max	150.00	21.39	29	0.00	17	0.00	17	70.88	28	0.00	21	0.00	17
317	-21	-51	Min.	0.00	115.65	21	0.00	17	0.00	17	-156.17	21	-221.93	28	0.00	17
317	-21	-51	Min.	150.00	20.42	21	0.00	17	0.00	17	-71.47	21	0.00	28	0.00	17
317	-50	-21	Max	0.00	-20.42	21	0.00	17	0.00	17	71.47	21	0.00	21	0.00	17
317	-50	-21	Max	150.00	-115.65	21	0.00	17	0.00	17	156.17	21	170.72	21	0.00	17
317	-50	-21	Min.	0.00	-21.39	29	0.00	17	0.00	17	-70.88	28	0.00	28	0.00	17
317	-50	-21	Min.	150.00	-118.26	29	0.00	17	0.00	17	-225.02	28	-221.93	28	0.00	17
318	-22	-53	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
318	-22	-53	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	21	0.00	17
318	-22	-53	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
318	-22	-53	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	28	0.00	17

330	-33	-89	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
330	-33	-89	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	17	0.00	17
330	-33	-89	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
330	-33	-89	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	21	0.00	17
330	-88	-33	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	21	0.00	17
330	-88	-33	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
330	-88	-33	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	17	0.00	17
330	-88	-33	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
331	-34	-61	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
331	-34	-61	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	17	0.00	17
331	-34	-61	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
331	-34	-61	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	21	0.00	17
331	-62	-34	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	17	0.00	17
331	-62	-34	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
331	-62	-34	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	28	0.00	17
331	-62	-34	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
332	-35	-102	Max	0.00	175.53	29	0.00	17	0.00	17	414.83	28	367.85	21	0.00	17
332	-35	-102	Max	150.00	42.78	29	0.00	17	0.00	17	141.76	28	0.00	17	0.00	17
332	-35	-102	Min.	0.00	170.32	21	0.00	17	0.00	17	-347.54	21	-417.44	28	0.00	17
332	-35	-102	Min.	150.00	40.83	21	0.00	17	0.00	17	-142.93	21	0.00	21	0.00	17
332	-101	-35	Max	0.00	-40.83	21	0.00	17	0.00	17	142.93	21	0.00	17	0.00	17
332	-101	-35	Max	150.00	-170.32	21	0.00	17	0.00	17	347.54	21	367.85	21	0.00	17
332	-101	-35	Min.	0.00	-42.78	29	0.00	17	0.00	17	-141.76	28	0.00	21	0.00	17
332	-101	-35	Min.	150.00	-175.53	29	0.00	17	0.00	17	-414.83	28	-417.44	28	0.00	17
333	-37	-103	Max	0.00	118.26	29	0.00	17	0.00	17	225.02	28	170.72	21	0.00	17
333	-37	-103	Max	150.00	21.39	29	0.00	17	0.00	17	70.88	28	0.00	21	0.00	17
333	-37	-103	Min.	0.00	115.65	21	0.00	17	0.00	17	-156.17	21	-221.93	28	0.00	17
333	-37	-103	Min.	150.00	20.42	21	0.00	17	0.00	17	-71.47	21	0.00	28	0.00	17
333	-104	-37	Max	0.00	-20.42	21	0.00	17	0.00	17	71.47	21	0.00	28	0.00	17
333	-104	-37	Max	150.00	-115.65	21	0.00	17	0.00	17	156.17	21	170.72	21	0.00	17
333	-104	-37	Min.	0.00	-21.39	29	0.00	17	0.00	17	-70.88	28	0.00	21	0.00	17
333	-104	-37	Min.	150.00	-118.26	29	0.00	17	0.00	17	-225.02	28	-221.93	28	0.00	17

Tipo di combinazione di carico: SLE R

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-509.16	23	70.58	30	-8.30	23	1117.51	23	2987.86	30	1.00	30
1	1	-5	Max	328.50	-271.09	23	70.58	30	156.82	30	1117.51	23	382.10	30	1.00	30
1	1	-5	Min.	0.00	-1570.86	30	7.84	23	-75.04	30	-793.23	30	-4209.34	23	-1.42	23
1	1	-5	Min.	328.50	-1332.79	30	7.84	23	17.47	23	-793.23	30	-538.31	23	-1.42	23
2	2	-10	Max	0.00	-726.36	23	85.40	30	-16.28	23	2426.09	23	5369.42	30	0.67	30
2	2	-10	Max	328.50	-488.29	23	85.40	30	189.17	30	2426.09	23	405.20	23	0.67	30
2	2	-10	Min.	0.00	-3203.48	30	15.17	23	-91.39	30	-1722.08	30	-7564.52	23	-0.95	23
2	2	-10	Min.	328.50	-2965.41	30	15.17	23	33.57	23	-1722.08	30	-287.62	30	-0.95	23
3	3	203	Max	0.00	-750.44	23	-11.60	23	76.21	30	2571.37	23	5839.17	30	0.40	23
3	3	203	Max	328.50	-512.38	23	-11.60	23	-25.47	23	2571.37	23	220.65	23	0.40	23
3	3	203	Min.	0.00	-3309.91	30	-69.90	30	12.63	23	-1825.20	30	-8226.30	23	-0.28	30
3	3	203	Min.	328.50	-3071.84	30	-69.90	30	-153.42	30	-1825.20	30	-156.62	30	-0.28	30
4	4	204	Max	0.00	-786.67	23	0.00	30	0.00	23	1551.65	30	7356.04	23	0.00	30
4	4	204	Max	328.50	-548.60	23	0.00	30	0.00	23	1551.65	30	175.08	23	0.00	30
4	4	204	Min.	0.00	-2820.96	30	0.00	23	0.00	30	-2185.99	23	-5221.44	30	0.00	23
4	4	204	Min.	328.50	-2582.89	30	0.00	23	0.00	30	-2185.99	23	-124.27	30	0.00	23
5	5	205	Max	0.00	-750.44	23	-11.60	23	76.20	30	1825.20	30	8226.30	23	0.28	30
5	5	205	Max	328.50	-512.37	23	-11.60	23	-25.47	23	1825.20	30	156.62	30	0.28	30
5	5	205	Min.	0.00	-3309.91	30	-69.90	30	12.63	23	-2571.37	23	-5839.16	30	-0.40	23
5	5	205	Min.	328.50	-3071.84	30	-69.90	30	-153.41	30	-2571.37	23	-220.65	23	-0.40	23
6	6	-31	Max	0.00	-726.35	23	85.40	30	-16.28	23	1722.08	30	7564.52	23	0.95	23
6	6	-31	Max	328.50	-488.28	23	85.40	30	189.16	30	1722.08	30	287.62	30	0.95	23
6	6	-31	Min.	0.00	-3203.47	30	15.17	23	-91.38	30	-2426.09	23	-5369.42	30	-0.67	30
6	6	-31	Min.	328.50	-2965.41	30	15.17	23	33.57	23	-2426.09	23	-405.20	23	-0.67	30
7	7	-36	Max	0.00	-509.16	23	70.58	30	-8.30	23	793.23	30	4209.34	23	1.42	23
7	7	-36	Max	328.50	-271.09	23	70.58	30	156.81	30	793.23	30	538.31	23	1.42	23
7	7	-36	Min.	0.00	-1570.86	30	7.84	23	-75.04	30	-1117.51	23	-2987.86	30	-1.00	30
7	7	-36	Min.	328.50	-1332.79	30	7.84	23	17.47	23	-1117.51	23	-382.10	30	-1.00	30
201	-5	-4	Max	0.00	0.00	18	182.73	30	207.49	23	371.39	30	-64.94	23	0.00	23
201	-5	-4	Max	80.60	0.00	18	182.73	30	0.00	30	298.00	30	0.00	30	0.00	23
201	-5	-4	Min.	0.00	0.00	18	-257.43	23	-147.28	30	117.27	23	-269.77	30	0.00	18
201	-5	-4	Min.	80.60	0.00	18	-257.43	23	-0.00	23	43.88	23	0.00	23	0.00	18
201	-6	-5	Max	0.00	-7.84	23	860.09	23	177.38	30	-105.25	23	73.30	30	538.31	23
201	-6	-5	Max	53.34	-7.84	23	860.09	23	208.90	23	-153.82	23	-82.41	23	538.31	23
201	-6	-5	Min.	0.00	-70.58	30	-610.50	30	-249.89	23	-912.83	30	-13.31	23	-382.10	30
201	-6	-5	Min.	53.34	-70.58	30	-610.50	30	-148.28	30	-961.40	30	-426.58	30	-382.10	30
201	-7	-6	Max	0.00	-7.84	23	345.23	23	505.61	30	-3.85	23	561.08	30	538.31	23
201	-7	-6	Max	133.94	-7.84	23	345.23	23	177.38	30	-125.82	23	73.30	30	538.31	23
201	-7	-6	Min.	0.00	-70.58	30	-245.05	30	-712.31	23	-303.19	30	73.53	23	-382.10	30

201	-7	-6	Min.	133.94	-70.58	30	-245.05	30	-249.89	23	-425.15	30	-13.31	23	-382.10	30
201	-8	-7	Max	0.00	-7.84	23	120.40	30	344.34	30	306.45	30	232.29	30	538.31	23
201	-8	-7	Max	107.15					-666.87	23			76.81	23		
201	-8	-7	Max	133.94	-7.84	23	120.40	30	505.61	30	184.49	30	561.08	30	538.31	23
201	-8	-7	Min.	0.00	-70.58	30	-169.62	23	-485.11	23	97.54	23	24.57	23	-382.10	30
201	-8	-7	Min.	107.15					-666.87	23			76.81	23		
201	-8	-7	Min.	133.94	-70.58	30	-169.62	23	-712.31	23	-24.43	23	73.53	23	-382.10	30
201	-9	-8	Max	0.00	-7.84	23	485.85	30	431.70	23	916.09	30	-160.21	23	538.31	23
201	-9	-8	Max	133.94	-7.84	23	485.85	30	344.34	30	794.12	30	232.29	30	538.31	23
201	-9	-8	Min.	0.00	-70.58	30	-684.48	23	-306.43	30	198.94	23	-913.07	30	-382.10	30
201	-9	-8	Min.	133.94	-70.58	30	-684.48	23	-485.11	23	76.97	23	24.57	23	-382.10	30
201	-10	-9	Max	0.00	-7.84	23	851.31	30	969.35	23	1444.58	30	-249.32	23	538.31	23
201	-10	-9	Max	44.83	-7.84	23	851.31	30	431.70	23	1403.76	30	-160.21	23	538.31	23
201	-10	-9	Min.	0.00	-70.58	30	-1199.33	23	-688.06	30	219.18	23	-1551.51	30	-382.10	30
201	-10	-9	Min.	44.83	-70.58	30	-1199.33	23	-306.43	30	178.36	23	-913.07	30	-382.10	30
202	-11	-10	Max	0.00	-23.02	23	1226.76	23	87.25	30	-187.96	23	-79.23	23	133.11	23
202	-11	-10	Max	89.11	-23.02	23	1226.76	23	970.30	23	-269.11	23	-282.88	23	133.11	23
202	-11	-10	Min.	0.00	-155.99	30	-870.77	30	-122.92	23	-1439.68	30	-421.56	30	-94.48	30
202	-11	-10	Min.	89.11	-155.99	30	-870.77	30	-688.73	30	-1520.82	30	-1740.67	30	-94.48	30
202	-12	-11	Max	0.00	-23.02	23	711.90	30	764.09	30	-86.56	23	771.90	30	133.11	23
202	-12	-11	Max	133.94	-23.02	23	711.90	23	87.25	30	-208.53	23	-79.23	23	133.11	23
202	-12	-11	Min.	0.00	-155.99	30	-505.32	30	-1076.46	23	-830.04	30	118.40	23	-94.48	30
202	-12	-11	Min.	133.94	-155.99	30	-505.32	30	-122.92	23	-952.00	30	-421.56	30	-94.48	30
202	-13	-12	Max	0.00	-23.02	23	197.05	23	951.44	30	14.83	23	1148.79	30	133.11	23
202	-13	-12	Max	16.29					-1308.30	23			181.43	23		
202	-13	-12	Max	133.94	-23.02	23	197.05	23	764.09	30	-107.14	23	771.90	30	133.11	23
202	-13	-12	Min.	0.00	-155.99	30	-139.87	30	-1340.40	23	-220.40	30	180.22	23	-94.48	30
202	-13	-12	Min.	16.29					-1308.30	23			181.43	23		
202	-13	-12	Min.	133.94	-155.99	30	-139.87	30	-1076.46	23	-342.37	30	118.40	23	-94.48	30
202	-14	-13	Max	0.00	-23.02	23	225.58	30	649.29	30	389.24	30	709.12	30	133.11	23
202	-14	-13	Max	127.63					-1320.35	23			180.40	23		
202	-14	-13	Max	133.94	-23.02	23	225.58	30	951.44	30	267.27	30	1148.79	30	133.11	23
202	-14	-13	Min.	0.00	-155.99	30	-317.81	23	-914.72	23	116.22	23	106.23	23	-94.48	30
202	-14	-13	Min.	127.63					-1320.35	23			180.40	23		
202	-14	-13	Min.	133.94	-155.99	30	-317.81	23	-1340.40	23	-5.74	23	180.22	23	-94.48	30
202	-15	-14	Max	0.00	-23.02	23	591.04	30	200.57	23	998.88	30	-103.57	23	133.11	23
202	-15	-14	Max	133.94	-23.02	23	591.04	30	649.29	30	876.91	30	709.11	30	133.11	23
202	-15	-14	Min.	0.00	-155.99	30	-832.66	23	-142.37	30	217.62	30	-547.13	30	-94.48	30
202	-15	-14	Min.	133.94	-155.99	30	-832.66	23	-914.72	23	95.65	23	106.23	23	-94.48	30
202	203	-15	Max	0.00	-23.02	23	956.49	30	1342.11	23	1563.69	30	-303.17	23	133.11	23
202	203	-15	Max	84.71	-23.02	23	956.49	30	200.57	23	1486.55	30	-103.57	23	133.11	23
202	203	-15	Min.	0.00	-155.99	30	-1347.51	23	-952.65	30	274.19	23	-1839.14	30	-94.48	30
202	203	-15	Min.	84.71	-155.99	30	-1347.51	23	-142.37	30	197.04	23	-547.14	30	-94.48	30
203	-16	203	Max	0.00	-11.42	23	1223.85	23	739.21	23	-193.36	23	-171.47	23	62.14	30
203	-16	203	Max	49.23	-11.42	23	1223.85	23	1341.69	23	-238.19	23	-277.69	23	62.14	30
203	-16	203	Min.	0.00	-86.08	30	-868.71	30	-524.70	30	-1463.32	30	-954.29	30	-87.54	23
203	-16	203	Min.	49.23	-86.08	30	-868.71	30	-952.36	30	-1508.15	30	-1685.69	30	-87.54	23
203	-17	-16	Max	0.00	-11.42	23	709.00	23	149.36	30	-91.97	23	270.82	30	62.14	30
203	-17	-16	Max	133.94	-11.42	23	709.00	23	739.23	23	-213.94	23	-171.47	23	62.14	30
203	-17	-16	Min.	0.00	-86.08	30	-503.26	30	-210.42	23	-853.69	30	33.40	23	-87.54	23
203	-17	-16	Min.	133.94	-86.08	30	-503.26	30	-524.72	30	-975.65	30	-954.32	30	-87.54	23
203	-18	-17	Max	0.00	-11.42	23	194.15	23	333.94	30	9.42	23	679.38	30	62.14	30
203	-18	-17	Max	10.35					-450.38	23			102.95	23		
203	-18	-17	Max	133.94	-11.42	23	194.15	23	149.36	30	-112.55	23	270.81	30	62.14	30
203	-18	-17	Min.	0.00	-86.08	30	-137.81	30	-470.46	23	-244.05	30	102.46	23	-87.54	23
203	-18	-17	Min.	10.35					-450.38	23			102.95	23		
203	-18	-17	Min.	133.94	-86.08	30	-137.81	30	-210.42	23	-366.02	30	33.40	23	-87.54	23
203	-19	-18	Max	0.00	-11.42	23	227.65	30	29.01	30	365.60	30	271.35	30	62.14	30
203	-19	-18	Max	121.70					-431.18	23			103.14	23		
203	-19	-18	Max	133.94	-11.42	23	227.65	30	333.93	30	243.63	30	679.36	30	62.14	30
203	-19	-18	Min.	0.00	-86.08	30	-320.71	23	-40.87	23	110.82	23	35.71	23	-87.54	23
203	-19	-18	Min.	121.70					-431.18	23			103.14	23		
203	-19	-18	Min.	133.94	-86.08	30	-320.71	23	-470.44	23	-11.15	23	102.46	23	-87.54	23
203	-20	-19	Max	0.00	-11.42	23	593.10	30	1078.28	23	975.23	30	-166.84	23	62.14	30
203	-20	-19	Max	133.94	-11.42	23	593.10	30	29.03	30	853.26	30	271.38	30	62.14	30
203	-20	-19	Min.	0.00	-86.08	30	-835.57	23	-765.38	30	212.21	23	-953.19	30	-87.54	23
203	-20	-19	Min.	133.94	-86.08	30	-835.57	23	-40.90	23	90.24	23	35.71	23	-87.54	23
203	204	-20	Max	0.00	-11.42	23	775.82	30	1296.88	23	1291.44	30	-219.88	23	62.14	30
203	204	-20	Max	20.00	-11.42	23	775.82	30	1078.28	23	1273.23	30	-166.84	23	62.14	30
203	204	-20	Min.	0.00	-86.08	30	-1092.99	23	-920.55	30	274.30	23	-1209.66	30	-87.54	23
203	204	-20	Min.	20.00	-86.08	30	-1092.99	23	-765.38	30	256.09	23	-953.19	30	-87.54	23
204	204	-21	Max	0.00	-11.42	23	1092.99	23	920.55	30	1291.45	30	-219.88	23	87.54	23
204	204	-21	Max	20.00	-11.42	23	1092.99	23	765.38	30	1273.23	30	-166.84	23	87.54	23
204	204	-21	Min.	0.00	-86.08	30	-775.83	30	-1296.88	23	274.30	23	-1209.66	30	-62.14	30
204	204	-21	Min.	20.00	-86.08	30	-775.83	30	-1078.28	23	256.09	23	-953.19	30	-62.14	30
204	-21	-22	Max	0.00	-11.42	23	835.57	23	765.38	30	975.23	30	-166.84	23	87.54	23



204	-21	-22	Max	133.94	-11.42	23	835.57	23	40.90	23	853.26	30	271.38	30	87.54	23
204	-21	-22	Min.	0.00	-86.08	30	-593.10	30	-1078.28	23	212.21	23	-953.19	30	-62.14	30
204	-21	-22	Min.	133.94	-86.08	30	-593.10	30	-29.03	30	90.24	23	35.71	23	-62.14	30
204	-22	-23	Max	0.00	-11.42	23	320.71	23	40.87	23	365.60	30	271.36	30	87.54	23
204	-22	-23	Max	121.70					431.18	23			103.14	23		
204	-22	-23	Max	133.94	-11.42	23	320.71	23	470.44	23	243.63	30	679.36	30	87.54	23
204	-22	-23	Min.	0.00	-86.08	30	-227.65	30	-29.01	30	110.82	23	35.71	23	-62.14	30
204	-22	-23	Min.	121.70					431.18	23			103.14	23		
204	-22	-23	Min.	133.94	-86.08	30	-227.65	30	-333.93	30	-11.15	23	102.46	23	-62.14	30
204	-23	-24	Max	0.00	-11.42	23	137.81	30	470.47	23	9.42	23	679.38	30	87.54	23
204	-23	-24	Max	10.35					450.38	23			102.95	23		
204	-23	-24	Max	133.94	-11.42	23	137.81	30	210.43	23	-112.55	23	270.81	30	87.54	23
204	-23	-24	Min.	0.00	-86.08	30	-194.14	23	-333.94	30	-244.05	30	102.46	23	-62.14	30
204	-23	-24	Min.	10.35					450.38	23			102.95	23		
204	-23	-24	Min.	133.94	-86.08	30	-194.14	23	-149.36	30	-366.02	30	33.40	23	-62.14	30
204	-24	-25	Max	0.00	-11.42	23	503.26	30	210.43	23	-91.97	23	270.82	30	87.54	23
204	-24	-25	Max	133.94	-11.42	23	503.26	30	524.71	30	-213.94	23	-171.47	23	87.54	23
204	-24	-25	Min.	0.00	-86.08	30	-709.00	23	-149.37	30	-853.68	30	33.40	23	-62.14	30
204	-24	-25	Min.	133.94	-86.08	30	-709.00	23	-739.22	23	-975.65	30	-954.31	30	-62.14	30
204	-25	205	Max	0.00	-11.42	23	868.71	30	524.70	30	-193.36	23	-171.47	23	87.54	23
204	-25	205	Max	49.23	-11.42	23	868.71	30	952.35	30	-238.19	23	-277.69	23	87.54	23
204	-25	205	Min.	0.00	-86.08	30	-1223.85	23	-739.20	23	-1463.32	30	-954.28	30	-62.14	30
204	-25	205	Min.	49.23	-86.08	30	-1223.85	23	-1341.69	23	-1508.15	30	-1685.69	30	-62.14	30
205	205	-26	Max	0.00	-23.02	23	1347.52	23	952.65	30	1563.69	30	-303.17	23	94.48	30
205	205	-26	Max	84.71	-23.02	23	1347.52	23	142.36	30	1486.55	30	-103.57	23	94.48	30
205	205	-26	Min.	0.00	-155.98	30	-956.49	30	-1342.10	23	274.18	23	-1839.13	30	-133.11	23
205	205	-26	Min.	84.71	-155.98	30	-956.49	30	-200.56	23	197.04	23	-547.12	30	-133.11	23
205	-26	-27	Max	0.00	-23.02	23	832.66	23	142.41	30	998.88	30	-103.58	23	94.48	30
205	-26	-27	Max	133.94	-23.02	23	832.66	23	914.67	23	876.92	30	709.06	30	94.48	30
205	-26	-27	Min.	0.00	-155.98	30	-591.04	30	-200.62	23	217.62	23	-547.19	30	-133.11	23
205	-26	-27	Min.	133.94	-155.98	30	-591.04	30	-649.25	30	95.65	23	106.23	23	-133.11	23
205	-27	-28	Max	0.00	-23.02	23	317.81	23	914.73	23	389.24	30	709.12	30	94.48	30
205	-27	-28	Max	127.63					1320.35	23			180.40	23		
205	-27	-28	Max	133.94	-23.02	23	317.81	23	1340.40	23	267.27	30	1148.79	30	94.48	30
205	-27	-28	Min.	0.00	-155.98	30	-225.58	30	-649.29	30	116.22	23	106.23	23	-133.11	23
205	-27	-28	Min.	127.63					1320.35	23			180.40	23		
205	-27	-28	Min.	133.94	-155.98	30	-225.58	30	-951.44	30	-5.75	23	180.22	23	-133.11	23
205	-28	-29	Max	0.00	-23.02	23	139.87	30	1340.40	23	14.83	23	1148.79	30	94.48	30
205	-28	-29	Max	16.29					1308.30	23			181.43	23		
205	-28	-29	Max	133.94	-23.02	23	139.87	30	1076.46	23	-107.14	23	771.90	30	94.48	30
205	-28	-29	Min.	0.00	-155.98	30	-197.05	23	-951.43	30	-220.40	30	180.22	23	-133.11	23
205	-28	-29	Min.	16.29					1308.30	23			181.43	23		
205	-28	-29	Min.	133.94	-155.98	30	-197.05	23	-764.09	30	-342.37	30	118.40	23	-133.11	23
205	-29	-30	Max	0.00	-23.02	23	505.32	30	1076.47	23	-86.56	23	771.91	30	94.48	30
205	-29	-30	Max	133.94	-23.02	23	505.32	30	122.92	23	-208.53	23	-79.22	23	94.48	30
205	-29	-30	Min.	0.00	-155.98	30	-711.90	23	-764.10	30	-830.03	30	118.40	23	-133.11	23
205	-29	-30	Min.	133.94	-155.98	30	-711.90	23	-87.25	30	-952.00	30	-421.55	30	-133.11	23
205	-30	-31	Max	0.00	-23.02	23	870.77	30	122.87	23	-187.96	23	-79.24	23	94.48	30
205	-30	-31	Max	89.11	-23.02	23	870.77	30	688.76	30	-269.11	23	-282.89	23	94.48	30
205	-30	-31	Min.	0.00	-155.98	30	-1226.76	23	-87.22	30	-1439.68	30	-421.61	30	-133.11	23
205	-30	-31	Min.	89.11	-155.98	30	-1226.76	23	-970.34	23	-1520.82	30	-1740.72	30	-133.11	23
206	-31	-32	Max	0.00	-7.84	23	1199.33	23	688.06	30	1444.58	30	-249.31	23	382.10	30
206	-31	-32	Max	44.83	-7.84	23	1199.33	23	306.42	30	1403.76	30	-160.21	23	382.10	30
206	-31	-32	Min.	0.00	-70.58	30	-851.31	30	-969.34	23	219.18	23	-1551.50	30	-538.31	23
206	-31	-32	Min.	44.83	-70.58	30	-851.31	30	-431.69	23	178.36	23	-913.06	30	-538.31	23
206	-32	-33	Max	0.00	-7.84	23	684.48	23	306.42	30	916.09	30	-160.21	23	382.10	30
206	-32	-33	Max	133.94	-7.84	23	684.48	23	485.13	23	794.12	30	232.31	30	382.10	30
206	-32	-33	Min.	0.00	-70.58	30	-485.86	30	-431.68	23	198.93	23	-913.04	30	-538.31	23
206	-32	-33	Min.	133.94	-70.58	30	-485.86	30	-344.35	30	76.96	23	24.57	23	-538.31	23
206	-33	-34	Max	0.00	-7.84	23	169.62	23	485.11	23	306.46	30	232.29	30	382.10	30
206	-33	-34	Max	107.16					666.87	23			76.81	23		
206	-33	-34	Max	133.94	-7.84	23	169.62	23	712.31	23	184.49	30	561.08	30	382.10	30
206	-33	-34	Min.	0.00	-70.58	30	-120.40	30	-344.34	30	97.54	23	24.56	23	-538.31	23
206	-33	-34	Min.	107.16					666.87	23			76.81	23		
206	-33	-34	Min.	133.94	-70.58	30	-120.40	30	-505.61	30	-24.43	23	73.53	23	-538.31	23
206	-34	-35	Max	0.00	-7.84	23	245.05	30	712.30	23	-3.85	23	561.08	30	382.10	30
206	-34	-35	Max	133.94	-7.84	23	245.05	30	249.89	23	-125.82	23	73.30	30	382.10	30
206	-34	-35	Min.	0.00	-70.58	30	-345.23	23	-505.61	30	-303.18	30	73.53	23	-538.31	23
206	-34	-35	Min.	133.94	-70.58	30	-345.23	23	-177.38	30	-425.15	30	-13.31	23	-538.31	23
206	-35	-36	Max	0.00	-7.84	23	610.50	30	249.87	23	-105.25	23	73.27	30	382.10	30
206	-35	-36	Max	53.34	-7.84	23	610.50	30	148.30	30	-153.82	23	-82.41	23	382.10	30
206	-35	-36	Min.	0.00	-70.58	30	-860.09	23	-177.36	30	-912.83	30	-13.31	23	-538.31	23
206	-35	-36	Min.	53.34	-70.58	30	-860.09	23	-208.93	23	-961.40	30	-426.61	30	-538.31	23
206	-36	-37	Max	0.00	0.00	18	257.43	23	147.28	30	371.39	30	-64.94	23	0.00	23
206	-36	-37	Max	80.60	0.00	18	257.43	23	0.00	23	298.00	30	0.00	30	0.00	23
206	-36	-37	Min.	0.00	0.00	18	-182.73	30	-207.49	23	117.27	23	-269.77	30	0.00	18

206	-36	-37	Min.	80.60	0.00	18	-182.73	30	0.00	30	43.88	23	0.00	23	0.00	18
302	-4	-47	Max	0.00	85.09	31	0.00	18	0.00	18	153.62	30	111.11	23	0.00	18
302	-4	-47	Max	150.00	14.26	31	0.00	18	0.00	18	47.25	30	0.00	23	0.00	18
302	-4	-47	Min.	0.00	83.36	23	0.00	18	0.00	18	-100.50	23	-150.66	30	0.00	18
302	-4	-47	Min.	150.00	13.61	23	0.00	18	0.00	18	-47.64	23	0.00	30	0.00	18
302	-46	-4	Max	0.00	-13.61	23	0.00	18	0.00	18	47.64	23	0.00	18	0.00	18
302	-46	-4	Max	150.00	-83.36	23	0.00	18	0.00	18	100.50	23	111.11	23	0.00	18
302	-46	-4	Min.	0.00	-14.26	31	0.00	18	0.00	18	-47.25	30	0.00	30	0.00	18
302	-46	-4	Min.	150.00	-85.09	31	0.00	18	0.00	18	-153.62	30	-150.66	30	0.00	18
303	-6	-48	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
303	-6	-48	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
303	-6	-48	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
303	-6	-48	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
303	-49	-6	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	23	0.00	18
303	-49	-6	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
303	-49	-6	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	18	0.00	18
303	-49	-6	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
304	-7	-96	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
304	-7	-96	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
304	-7	-96	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
304	-7	-96	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
304	-95	-7	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	18	0.00	18
304	-95	-7	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
304	-95	-7	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	23	0.00	18
304	-95	-7	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
305	-8	-66	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
305	-8	-66	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
305	-8	-66	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
305	-8	-66	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
305	-67	-8	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	18	0.00	18
305	-67	-8	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
305	-67	-8	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	23	0.00	18
305	-67	-8	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
306	-9	-69	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
306	-9	-69	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
306	-9	-69	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
306	-9	-69	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
306	-68	-9	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	30	0.00	18
306	-68	-9	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
306	-68	-9	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	23	0.00	18
306	-68	-9	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
307	-11	-70	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
307	-11	-70	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
307	-11	-70	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
307	-11	-70	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
307	-71	-11	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	30	0.00	18
307	-71	-11	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
307	-71	-11	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	23	0.00	18
307	-71	-11	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
308	-12	-72	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
308	-12	-72	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
308	-12	-72	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
308	-12	-72	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
308	-73	-12	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	18	0.00	18
308	-73	-12	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
308	-73	-12	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	30	0.00	18
308	-73	-12	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
309	-13	-74	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
309	-13	-74	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
309	-13	-74	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
309	-13	-74	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
309	-75	-13	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	30	0.00	18
309	-75	-13	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
309	-75	-13	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	18	0.00	18
309	-75	-13	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
310	-14	-90	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
310	-14	-90	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
310	-14	-90	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
310	-14	-90	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
310	-91	-14	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	30	0.00	18
310	-91	-14	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
310	-91	-14	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	18	0.00	18
310	-91	-14	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
311	-15	-92	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
311	-15	-92	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
311	-15	-92	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18

311	-15	-92	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
311	-93	-15	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	23	0.00	18
311	-93	-15	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
311	-93	-15	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	18	0.00	18
311	-93	-15	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
312	-16	-98	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
312	-16	-98	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
312	-16	-98	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
312	-16	-98	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
312	-94	-16	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	23	0.00	18
312	-94	-16	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
312	-94	-16	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	30	0.00	18
312	-94	-16	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
313	-17	-97	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
313	-17	-97	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
313	-17	-97	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
313	-17	-97	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
313	-42	-17	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	18	0.00	18
313	-42	-17	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
313	-42	-17	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	23	0.00	18
313	-42	-17	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
314	-18	-43	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
314	-18	-43	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
314	-18	-43	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
314	-18	-43	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
314	-44	-18	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	18	0.00	18
314	-44	-18	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
314	-44	-18	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	23	0.00	18
314	-44	-18	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
315	-19	-45	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
315	-19	-45	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
315	-19	-45	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
315	-19	-45	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
315	-58	-19	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	30	0.00	18
315	-58	-19	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
315	-58	-19	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	18	0.00	18
315	-58	-19	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
316	-20	-63	Max	0.00	85.09	31	0.00	18	0.00	18	153.62	30	111.11	23	0.00	18
316	-20	-63	Max	150.00	14.26	31	0.00	18	0.00	18	47.25	30	0.00	23	0.00	18
316	-20	-63	Min.	0.00	83.36	23	0.00	18	0.00	18	-100.50	23	-150.66	30	0.00	18
316	-20	-63	Min.	150.00	13.61	23	0.00	18	0.00	18	-47.64	23	0.00	30	0.00	18
316	-65	-20	Max	0.00	-13.61	23	0.00	18	0.00	18	47.64	23	0.00	30	0.00	18
316	-65	-20	Max	150.00	-83.36	23	0.00	18	0.00	18	100.50	23	111.11	23	0.00	18
316	-65	-20	Min.	0.00	-14.26	31	0.00	18	0.00	18	-47.25	30	0.00	18	0.00	18
316	-65	-20	Min.	150.00	-85.09	31	0.00	18	0.00	18	-153.62	30	-150.66	30	0.00	18
317	-21	-51	Max	0.00	85.09	31	0.00	18	0.00	18	153.62	30	111.11	23	0.00	18
317	-21	-51	Max	150.00	14.26	31	0.00	18	0.00	18	47.25	30	0.00	23	0.00	18
317	-21	-51	Min.	0.00	83.36	23	0.00	18	0.00	18	-100.50	23	-150.66	30	0.00	18
317	-21	-51	Min.	150.00	13.61	23	0.00	18	0.00	18	-47.64	23	0.00	30	0.00	18
317	-50	-21	Max	0.00	-13.61	23	0.00	18	0.00	18	47.64	23	0.00	23	0.00	18
317	-50	-21	Max	150.00	-83.36	23	0.00	18	0.00	18	100.50	23	111.11	23	0.00	18
317	-50	-21	Min.	0.00	-14.26	31	0.00	18	0.00	18	-47.25	30	0.00	30	0.00	18
317	-50	-21	Min.	150.00	-85.09	31	0.00	18	0.00	18	-153.62	30	-150.66	30	0.00	18
318	-22	-53	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
318	-22	-53	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
318	-22	-53	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
318	-22	-53	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
318	-52	-22	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	30	0.00	18
318	-52	-22	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
318	-52	-22	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	18	0.00	18
318	-52	-22	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
319	-23	-55	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
319	-23	-55	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
319	-23	-55	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
319	-23	-55	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
319	-54	-23	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	23	0.00	18
319	-54	-23	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
319	-54	-23	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	18	0.00	18
319	-54	-23	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
320	-24	-57	Max	0.00	123.28	31	0.00	18	0.00	18	280.16	30	242.53	23	0.00	18
320	-24	-57	Max	150.00	28.52	31	0.00	18	0.00	18	94.51	30	0.00	23	0.00	18
320	-24	-57	Min.	0.00	119.80	23	0.00	18	0.00	18	-228.08	23	-281.00	30	0.00	18
320	-24	-57	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	30	0.00	18
320	-56	-24	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	18	0.00	18
320	-56	-24	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
320	-56	-24	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	23	0.00	18

332	-35	-102	Min.	150.00	27.22	23	0.00	18	0.00	18	-95.29	23	0.00	23	0.00	18
332	-101	-35	Max	0.00	-27.22	23	0.00	18	0.00	18	95.29	23	0.00	18	0.00	18
332	-101	-35	Max	150.00	-119.80	23	0.00	18	0.00	18	228.08	23	242.53	23	0.00	18
332	-101	-35	Min.	0.00	-28.52	31	0.00	18	0.00	18	-94.51	30	0.00	23	0.00	18
332	-101	-35	Min.	150.00	-123.28	31	0.00	18	0.00	18	-280.16	30	-281.00	30	0.00	18
333	-37	-103	Max	0.00	85.09	31	0.00	18	0.00	18	153.62	30	111.11	23	0.00	18
333	-37	-103	Max	150.00	14.26	31	0.00	18	0.00	18	47.25	30	0.00	23	0.00	18
333	-37	-103	Min.	0.00	83.36	23	0.00	18	0.00	18	-100.50	23	-150.66	30	0.00	18
333	-37	-103	Min.	150.00	13.61	23	0.00	18	0.00	18	-47.64	23	0.00	30	0.00	18
333	-104	-37	Max	0.00	-13.61	23	0.00	18	0.00	18	47.64	23	0.00	30	0.00	18
333	-104	-37	Max	150.00	-83.36	23	0.00	18	0.00	18	100.50	23	111.11	23	0.00	18
333	-104	-37	Min.	0.00	-14.26	31	0.00	18	0.00	18	-47.25	30	0.00	23	0.00	18
333	-104	-37	Min.	150.00	-85.09	31	0.00	18	0.00	18	-153.62	30	-150.66	30	0.00	18

Tipo di combinazione di carico: SLE F

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-989.17	25	48.76	32	-38.47	25	223.50	25	597.57	32	0.20	32
1	1	-5	Max	328.50	-751.10	25	48.76	32	108.34	32	223.50	25	76.42	32	0.20	32
1	1	-5	Min.	0.00	-1201.51	32	36.21	25	-51.82	32	-158.65	32	-841.87	25	-0.28	25
1	1	-5	Min.	328.50	-963.44	32	36.21	25	80.47	25	-158.65	32	-107.66	25	-0.28	25
2	2	-10	Max	0.00	-1846.29	25	60.97	32	-50.24	25	485.22	25	1073.88	32	0.13	32
2	2	-10	Max	328.50	-1608.23	25	60.97	32	135.03	32	485.22	25	81.04	25	0.13	32
2	2	-10	Min.	0.00	-2341.72	32	46.93	25	-65.26	32	-344.42	32	-1512.90	25	-0.19	25
2	2	-10	Min.	328.50	-2103.65	32	46.93	25	103.92	25	-344.42	32	-57.52	32	-0.19	25
3	3	203	Max	0.00	-1907.61	25	-37.96	25	54.09	32	514.27	25	1167.83	32	0.08	25
3	3	203	Max	328.50	-1669.55	25	-37.96	25	-83.32	25	514.27	25	44.13	25	0.08	25
3	3	203	Min.	0.00	-2419.51	32	-49.62	32	41.38	25	-365.04	32	-1645.26	25	-0.06	32
3	3	203	Min.	328.50	-2181.44	32	-49.62	32	-108.91	32	-365.04	32	-31.32	32	-0.06	32
4	4	204	Max	0.00	-1706.40	25	0.00	32	0.00	25	310.33	32	1471.21	25	0.00	32
4	4	204	Max	328.50	-1468.33	25	0.00	32	0.00	25	310.33	32	35.02	25	0.00	32
4	4	204	Min.	0.00	-2113.26	32	0.00	25	0.00	32	-437.20	25	-1044.29	32	0.00	25
4	4	204	Min.	328.50	-1875.19	32	0.00	25	0.00	32	-437.20	25	-24.85	32	0.00	25
5	5	205	Max	0.00	-1907.61	25	-37.96	25	54.09	32	365.04	32	1645.26	25	0.06	32
5	5	205	Max	328.50	-1669.54	25	-37.96	25	-83.32	25	365.04	32	31.32	32	0.06	32
5	5	205	Min.	0.00	-2419.51	32	-49.62	32	41.38	25	-514.27	25	-1167.83	32	-0.08	25
5	5	205	Min.	328.50	-2181.44	32	-49.62	32	-108.91	32	-514.27	25	-44.13	25	-0.08	25
6	6	-31	Max	0.00	-1846.29	25	60.97	32	-50.24	25	344.42	32	1512.90	25	0.19	25
6	6	-31	Max	328.50	-1608.22	25	60.97	32	135.03	32	344.42	32	57.52	32	0.19	25
6	6	-31	Min.	0.00	-2341.72	32	46.93	25	-65.26	32	-485.22	25	-1073.88	32	-0.13	32
6	6	-31	Min.	328.50	-2103.65	32	46.93	25	103.91	25	-485.22	25	-81.04	25	-0.13	32
7	7	-36	Max	0.00	-989.17	25	48.75	32	-38.47	25	158.65	32	841.87	25	0.28	25
7	7	-36	Max	328.50	-751.10	25	48.75	32	108.34	32	158.65	32	107.66	25	0.28	25
7	7	-36	Min.	0.00	-1201.51	32	36.21	25	-51.82	32	-223.50	25	-597.57	32	-0.20	32
7	7	-36	Min.	328.50	-963.44	32	36.21	25	80.47	25	-223.50	25	-76.42	32	-0.20	32
201	-5	-4	Max	0.00	0.00	19	36.55	32	41.50	25	282.99	32	-157.55	25	0.00	25
201	-5	-4	Max	80.60	0.00	19	36.55	32	0.00	32	209.59	32	0.00	32	0.00	25
201	-5	-4	Min.	0.00	0.00	19	-51.49	25	-29.46	32	232.16	25	-198.51	32	0.00	19
201	-5	-4	Min.	80.60	0.00	19	-51.49	25	0.00	25	158.77	25	0.00	25	0.00	19
201	-6	-5	Max	0.00	-36.21	25	172.02	25	35.48	32	-470.36	25	43.17	32	107.66	25
201	-6	-5	Max	53.34	-36.21	25	172.02	25	41.78	25	-518.94	25	-238.01	25	107.66	25
201	-6	-5	Min.	0.00	-48.76	32	-122.10	32	-49.98	25	-631.88	32	25.85	25	-76.42	32
201	-6	-5	Min.	53.34	-48.76	32	-122.10	32	-29.66	32	-680.45	32	-306.85	32	-76.42	32
201	-7	-6	Max	0.00	-36.21	25	69.05	25	101.12	32	-139.19	25	391.47	32	107.66	25
201	-7	-6	Max	133.94	-36.21	25	69.05	25	35.48	32	-261.15	25	43.17	32	107.66	25
201	-7	-6	Min.	0.00	-48.76	32	-49.01	32	-142.46	25	-199.05	32	293.96	25	-76.42	32
201	-7	-6	Min.	133.94	-48.76	32	-49.01	32	-49.98	25	-321.02	32	25.85	25	-76.42	32
201	-8	-7	Max	0.00	-36.21	25	24.08	32	68.87	32	233.78	32	160.03	32	107.66	25
201	-8	-7	Max	133.94	-36.21	25	24.08	32	101.12	32	111.81	32	391.47	32	107.66	25
201	-8	-7	Min.	0.00	-48.76	32	-33.92	25	-97.02	25	191.99	25	118.48	25	-76.42	32
201	-8	-7	Min.	133.94	-48.76	32	-33.92	25	-142.46	25	70.02	25	293.96	25	-76.42	32
201	-9	-8	Max	0.00	-36.21	25	97.17	32	86.34	25	666.60	32	-500.58	25	107.66	25
201	-9	-8	Max	133.94	-36.21	25	97.17	32	68.87	32	544.63	32	160.03	32	107.66	25
201	-9	-8	Min.	0.00	-48.76	32	-136.90	25	-61.29	32	523.17	25	-651.16	32	-76.42	32
201	-9	-8	Min.	133.94	-48.76	32	-136.90	25	-97.02	25	401.20	25	118.48	25	-76.42	32
201	-10	-9	Max	0.00	-36.21	25	170.26	32	193.87	25	1018.28	32	-838.05	25	107.66	25
201	-10	-9	Max	44.83	-36.21	25	170.26	32	86.34	25	977.46	32	-500.59	25	107.66	25
201	-10	-9	Min.	0.00	-48.76	32	-239.87	25	-137.61	32	773.20	25	-1098.49	32	-76.42	32
201	-10	-9	Min.	44.83	-48.76	32	-239.87	25	-61.29	32	732.38	25	-651.16	32	-76.42	32
202	-11	-10	Max	0.00	-83.13	25	245.35	25	17.45	32	-753.88	25	-234.00	25	26.62	25
202	-11	-10	Max	89.11	-83.13	25	245.35	25	194.06	25	-835.02	25	-941.97	25	26.62	25
202	-11	-10	Min.	0.00	-109.73	32	-174.16	32	-24.58	25	-1004.22	32	-302.47	32	-18.90	32
202	-11	-10	Min.	89.11	-109.73	32	-174.16	32	-137.75	32	-1085.37	32	-1233.53	32	-18.90	32
202	-12	-11	Max	0.00	-83.13	25	142.38	25	152.82	32	-422.70	25	544.55	32	26.62	25
202	-12	-11	Max	133.94	-83.13	25	142.38	25	17.45	32	-544.67	25	-234.00	25	26.62	25

202	-12	-11	Min.	0.00	-109.73	32	-101.06	32	-215.29	25	-571.39	32	413.86	25	-18.90	32
202	-12	-11	Min.	133.94	-109.73	32	-101.06	32	-24.58	25	-693.36	32	-302.47	32	-18.90	32
202	-13	-12	Max	0.00	-83.13	25	39.41	25	190.29	32	-91.52	25	811.84	32	26.62	25
202	-13	-12	Max	133.94	-83.13	25	39.41	25	152.82	32	-213.49	25	544.55	32	26.62	25
202	-13	-12	Min.	0.00	-109.73	32	-27.97	32	-268.08	25	-138.56	32	618.12	25	-18.90	32
202	-13	-12	Min.	133.94	-109.73	32	-27.97	32	-215.29	25	-260.53	32	413.86	25	-18.90	32
202	-14	-13	Max	0.00	-83.13	25	45.12	32	129.86	32	294.26	32	499.38	32	26.62	25
202	-14	-13	Max	133.94	-83.13	25	45.12	32	190.29	32	172.29	32	811.84	32	26.62	25
202	-14	-13	Min.	0.00	-109.73	32	-63.56	25	-182.94	25	239.66	25	378.80	25	-18.90	32
202	-14	-13	Min.	133.94	-109.73	32	-63.56	25	-268.08	25	117.69	25	618.12	25	-18.90	32
202	-15	-14	Max	0.00	-83.13	25	118.21	32	40.11	25	727.09	32	-304.11	25	26.62	25
202	-15	-14	Max	133.94	-83.13	25	118.21	32	129.86	32	605.12	32	499.38	32	26.62	25
202	-15	-14	Min.	0.00	-109.73	32	-166.53	25	-28.47	32	570.84	25	-392.82	32	-18.90	32
202	-15	-14	Min.	133.94	-109.73	32	-166.53	25	-182.94	25	448.87	25	378.80	25	-18.90	32
202	203	-15	Max	0.00	-83.13	25	191.30	32	268.42	25	1115.09	32	-997.60	25	26.62	25
202	203	-15	Max	84.71	-83.13	25	191.30	32	40.11	25	1037.95	32	-304.11	25	26.62	25
202	203	-15	Min.	0.00	-109.73	32	-269.50	25	-190.53	32	857.19	25	-1304.79	32	-18.90	32
202	203	-15	Min.	84.71	-109.73	32	-269.50	25	-28.47	32	780.05	25	-392.83	32	-18.90	32
203	-16	203	Max	0.00	-45.17	25	244.77	25	147.84	25	-767.53	25	-525.39	25	12.43	32
203	-16	203	Max	49.23	-45.17	25	244.77	25	268.34	25	-812.36	25	-914.27	25	12.43	32
203	-16	203	Min.	0.00	-60.11	32	-173.74	32	-104.94	32	-1021.52	32	-681.96	32	-17.51	25
203	-16	203	Min.	49.23	-60.11	32	-173.74	32	-190.47	32	-1066.35	32	-1195.87	32	-17.51	25
203	-17	-16	Max	0.00	-45.17	25	141.80	25	29.87	32	-436.35	25	188.22	32	12.43	32
203	-17	-16	Max	133.94	-45.17	25	141.80	25	147.85	25	-558.32	25	-525.41	25	12.43	32
203	-17	-16	Min.	0.00	-60.11	32	-100.65	32	-42.08	25	-588.70	32	140.74	25	-17.51	25
203	-17	-16	Min.	133.94	-60.11	32	-100.65	32	-104.94	32	-710.66	32	-681.98	32	-17.51	25
203	-18	-17	Max	0.00	-45.17	25	38.83	25	66.79	32	-105.18	25	478.68	32	12.43	32
203	-18	-17	Max	133.94	-45.17	25	38.83	25	29.87	32	-227.15	25	188.22	32	12.43	32
203	-18	-17	Min.	0.00	-60.11	32	-27.56	32	-94.09	25	-155.87	32	363.29	25	-17.51	25
203	-18	-17	Min.	133.94	-60.11	32	-27.56	32	-42.08	25	-277.84	32	140.73	25	-17.51	25
203	-19	-18	Max	0.00	-45.17	25	45.53	32	5.80	32	276.96	32	189.38	32	12.43	32
203	-19	-18	Max	133.94	-45.17	25	45.53	32	66.79	32	155.00	32	478.67	32	12.43	32
203	-19	-18	Min.	0.00	-60.11	32	-64.14	25	-8.17	25	226.01	25	142.25	25	-17.51	25
203	-19	-18	Min.	133.94	-60.11	32	-64.14	25	-94.09	25	104.04	25	363.29	25	-17.51	25
203	-20	-19	Max	0.00	-45.17	25	118.62	32	215.66	25	709.79	32	-522.36	25	12.43	32
203	-20	-19	Max	133.94	-45.17	25	118.62	32	5.81	32	587.82	32	189.39	32	12.43	32
203	-20	-19	Min.	0.00	-60.11	32	-167.11	25	-153.08	32	557.18	25	-679.63	32	-17.51	25
203	-20	-19	Min.	133.94	-60.11	32	-167.11	25	-8.18	25	435.21	25	142.26	25	-17.51	25
203	204	-20	Max	0.00	-45.17	25	155.16	32	259.38	25	937.59	32	-667.38	25	12.43	32
203	204	-20	Max	20.00	-45.17	25	155.16	32	215.66	25	919.38	32	-522.36	25	12.43	32
203	204	-20	Min.	0.00	-60.11	32	-218.60	25	-184.11	32	734.17	25	-865.33	32	-17.51	25
203	204	-20	Min.	20.00	-60.11	32	-218.60	25	-153.08	32	715.95	25	-679.63	32	-17.51	25
204	204	-21	Max	0.00	-45.17	25	218.60	25	184.11	32	937.60	32	-667.38	25	17.51	25
204	204	-21	Max	20.00	-45.17	25	218.60	25	153.08	32	919.38	32	-522.36	25	17.51	25
204	204	-21	Min.	0.00	-60.11	32	-155.16	32	-259.38	25	734.17	25	-865.33	32	-12.43	32
204	204	-21	Min.	20.00	-60.11	32	-155.16	32	-215.66	25	715.95	25	-679.63	32	-12.43	32
204	-21	-22	Max	0.00	-45.17	25	167.11	25	153.08	32	709.79	32	-522.36	25	17.51	25
204	-21	-22	Max	133.94	-45.17	25	167.11	25	8.18	25	587.82	32	189.40	32	17.51	25
204	-21	-22	Min.	0.00	-60.11	32	-118.62	32	-215.66	25	557.18	25	-679.63	32	-12.43	32
204	-21	-22	Min.	133.94	-60.11	32	-118.62	32	-5.81	32	435.21	25	142.26	25	-12.43	32
204	-22	-23	Max	0.00	-45.17	25	64.14	25	8.17	25	276.96	32	189.38	32	17.51	25
204	-22	-23	Max	133.94	-45.17	25	64.14	25	94.09	25	155.00	32	478.67	32	17.51	25
204	-22	-23	Min.	0.00	-60.11	32	-45.53	32	-5.80	32	226.01	25	142.25	25	-12.43	32
204	-22	-23	Min.	133.94	-60.11	32	-45.53	32	-66.79	32	104.04	25	363.29	25	-12.43	32
204	-23	-24	Max	0.00	-45.17	25	27.56	32	94.09	25	-105.18	25	478.68	32	17.51	25
204	-23	-24	Max	133.94	-45.17	25	27.56	32	42.08	25	-227.15	25	188.22	32	17.51	25
204	-23	-24	Min.	0.00	-60.11	32	-38.83	25	-66.79	32	-155.87	32	363.29	25	-12.43	32
204	-23	-24	Min.	133.94	-60.11	32	-38.83	25	-29.87	32	-277.84	32	140.73	25	-12.43	32
204	-24	-25	Max	0.00	-45.17	25	100.65	32	42.09	25	-436.35	25	188.22	32	17.51	25
204	-24	-25	Max	133.94	-45.17	25	100.65	32	104.94	32	-558.32	25	-525.41	25	17.51	25
204	-24	-25	Min.	0.00	-60.11	32	-141.80	25	-29.87	32	-588.69	32	140.74	25	-12.43	32
204	-24	-25	Min.	133.94	-60.11	32	-141.80	25	-147.84	25	-710.66	32	-681.97	32	-12.43	32
204	-25	205	Max	0.00	-45.17	25	173.74	32	104.94	32	-767.53	25	-525.39	25	17.51	25
204	-25	205	Max	49.23	-45.17	25	173.74	32	190.47	32	-812.36	25	-914.26	25	17.51	25
204	-25	205	Min.	0.00	-60.11	32	-244.77	25	-147.84	25	-1021.52	32	-681.95	32	-12.43	32
204	-25	205	Min.	49.23	-60.11	32	-244.77	25	-268.34	25	-1066.35	32	-1195.86	32	-12.43	32
205	205	-26	Max	0.00	-83.13	25	269.50	25	190.53	32	1115.09	32	-997.60	25	18.90	32
205	205	-26	Max	84.71	-83.13	25	269.50	25	28.47	32	1037.95	32	-304.11	25	18.90	32
205	205	-26	Min.	0.00	-109.73	32	-191.30	32	-268.42	25	857.19	25	-1304.79	32	-26.62	25
205	205	-26	Min.	84.71	-109.73	32	-191.30	32	-40.11	25	780.05	25	-392.82	32	-26.62	25
205	-26	-27	Max	0.00	-83.13	25	166.53	25	28.48	32	727.09	32	-304.14	25	18.90	32
205	-26	-27	Max	133.94	-83.13	25	166.53	25	182.93	25	605.12	32	499.34	32	18.90	32
205	-26	-27	Min.	0.00	-109.73	32	-118.21	32	-40.12	25	570.84	25	-392.87	32	-26.62	25
205	-26	-27	Min.	133.94	-109.73	32	-118.21	32	-129.85	32	448.87	25	378.77	25	-26.62	25
205	-27	-28	Max	0.00	-83.13	25	63.56	25	182.94	25	294.26	32	499.38	32	18.90	32
205	-27	-28	Max	133.94	-83.13	25	63.56	25	268.08	25	172.29	32	811.84	32	18.90	32

205	-27	-28	Min.	0.00	-109.73	32	-45.12	32	-129.86	32	239.66	25	378.81	25	-26.62	25
205	-27	-28	Min.	133.94	-109.73	32	-45.12	32	-190.29	32	117.69	25	618.12	25	-26.62	25
205	-28	-29	Max	0.00	-83.13	25	27.97	32	268.08	25	-91.52	25	811.84	32	18.90	32
205	-28	-29	Max	133.94	-83.13	25	27.97	32	215.29	25	-213.49	25	544.55	32	18.90	32
205	-28	-29	Min.	0.00	-109.73	32	-39.41	25	-190.29	32	-138.56	32	618.12	25	-26.62	25
205	-28	-29	Min.	133.94	-109.73	32	-39.41	25	-152.82	32	-260.53	32	413.86	25	-26.62	25
205	-29	-30	Max	0.00	-83.13	25	101.06	32	215.29	25	-422.69	25	544.56	32	18.90	32
205	-29	-30	Max	133.94	-83.13	25	101.06	32	24.58	25	-544.66	25	-233.99	25	18.90	32
205	-29	-30	Min.	0.00	-109.73	32	-142.38	25	-152.82	32	-571.39	32	413.86	25	-26.62	25
205	-29	-30	Min.	133.94	-109.73	32	-142.38	25	-17.45	32	-693.36	32	-302.46	32	-26.62	25
205	-30	-31	Max	0.00	-83.13	25	174.16	32	24.57	25	-753.88	25	-234.03	25	18.90	32
205	-30	-31	Max	89.11	-83.13	25	174.16	32	137.75	32	-835.03	25	-942.00	25	18.90	32
205	-30	-31	Min.	0.00	-109.73	32	-245.35	25	-17.44	32	-1004.22	32	-302.51	32	-26.62	25
205	-30	-31	Min.	89.11	-109.73	32	-245.35	25	-194.07	25	-1085.37	32	-1233.56	32	-26.62	25
206	-31	-32	Max	0.00	-36.21	25	239.87	25	137.61	32	1018.28	32	-838.05	25	76.42	32
206	-31	-32	Max	44.83	-36.21	25	239.87	25	61.28	32	977.46	32	-500.58	25	76.42	32
206	-31	-32	Min.	0.00	-48.75	32	-170.26	32	-193.87	25	773.20	25	-1098.49	32	-107.66	25
206	-31	-32	Min.	44.83	-48.75	32	-170.26	32	-86.34	25	732.38	25	-651.15	32	-107.66	25
206	-32	-33	Max	0.00	-36.21	25	136.90	25	61.28	32	666.60	32	-500.57	25	76.42	32
206	-32	-33	Max	133.94	-36.21	25	136.90	25	97.03	25	544.63	32	160.04	32	76.42	32
206	-32	-33	Min.	0.00	-48.75	32	-97.17	32	-86.34	25	523.17	25	-651.14	32	-107.66	25
206	-32	-33	Min.	133.94	-48.75	32	-97.17	32	-68.87	32	401.20	25	118.49	25	-107.66	25
206	-33	-34	Max	0.00	-36.21	25	33.92	25	97.02	25	233.78	32	160.03	32	76.42	32
206	-33	-34	Max	133.94	-36.21	25	33.92	25	142.46	25	111.81	32	391.47	32	76.42	32
206	-33	-34	Min.	0.00	-48.75	32	-24.08	32	-68.87	32	192.00	25	118.48	25	-107.66	25
206	-33	-34	Min.	133.94	-48.75	32	-24.08	32	-101.12	32	70.03	25	293.96	25	-107.66	25
206	-34	-35	Max	0.00	-36.21	25	49.01	32	142.46	25	-139.18	25	391.47	32	76.42	32
206	-34	-35	Max	133.94	-36.21	25	49.01	32	49.98	25	-261.15	25	43.17	32	76.42	32
206	-34	-35	Min.	0.00	-48.75	32	-69.05	25	-101.12	32	-199.05	32	293.96	25	-107.66	25
206	-34	-35	Min.	133.94	-48.75	32	-69.05	25	-35.48	32	-321.01	32	25.85	25	-107.66	25
206	-35	-36	Max	0.00	-36.21	25	122.10	32	49.97	25	-470.37	25	43.15	32	76.42	32
206	-35	-36	Max	53.34	-36.21	25	122.10	32	29.66	32	-518.94	25	-238.03	25	76.42	32
206	-35	-36	Min.	0.00	-48.75	32	-172.02	25	-35.47	32	-631.88	32	25.83	25	-107.66	25
206	-35	-36	Min.	53.34	-48.75	32	-172.02	25	-41.79	25	-680.45	32	-306.87	32	-107.66	25
206	-36	-37	Max	0.00	0.00	19	51.49	25	29.46	32	282.99	32	-157.55	25	0.00	25
206	-36	-37	Max	80.60	0.00	19	51.49	25	0.00	25	209.59	32	0.00	32	0.00	25
206	-36	-37	Min.	0.00	0.00	19	-36.55	32	-41.50	25	232.16	25	-198.51	32	0.00	19
206	-36	-37	Min.	80.60	0.00	19	-36.55	32	0.00	32	158.77	25	0.00	25	0.00	19
302	-4	-47	Max	0.00	82.32	19	0.00	19	0.00	19	68.22	32	-10.34	25	0.00	19
302	-4	-47	Max	124.19								0.47	25			
302	-4	-47	Max	150.00	13.22	19	0.00	19	0.00	19	15.36	32	0.00	25	0.00	19
302	-4	-47	Min.	0.00	81.62	25	0.00	19	0.00	19	17.40	25	-62.69	32	0.00	19
302	-4	-47	Min.	124.19								0.47	25			
302	-4	-47	Min.	150.00	12.96	25	0.00	19	0.00	19	-3.62	25	0.00	32	0.00	19
302	-46	-4	Max	0.00	-12.96	25	0.00	19	0.00	19	3.62	25	0.00	19	0.00	19
302	-46	-4	Max	25.81								0.47	25			
302	-46	-4	Max	150.00	-81.62	25	0.00	19	0.00	19	-17.40	25	-10.34	25	0.00	19
302	-46	-4	Min.	0.00	-13.22	19	0.00	19	0.00	19	-15.36	32	0.00	32	0.00	19
302	-46	-4	Min.	25.81								0.47	25			
302	-46	-4	Min.	150.00	-82.32	19	0.00	19	0.00	19	-68.22	32	-62.69	32	0.00	19
303	-6	-48	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
303	-6	-48	Max	77.42								2.62	25			
303	-6	-48	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
303	-6	-48	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
303	-6	-48	Min.	77.42								2.62	25			
303	-6	-48	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
303	-49	-6	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
303	-49	-6	Max	72.58								2.62	25			
303	-49	-6	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
303	-49	-6	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
303	-49	-6	Min.	72.58								2.62	25			
303	-49	-6	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
304	-7	-96	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
304	-7	-96	Max	77.42								2.62	25			
304	-7	-96	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
304	-7	-96	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
304	-7	-96	Min.	77.42								2.62	25			
304	-7	-96	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
304	-95	-7	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
304	-95	-7	Max	72.58								2.62	25			
304	-95	-7	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
304	-95	-7	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
304	-95	-7	Min.	72.58								2.62	25			
304	-95	-7	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
305	-8	-66	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
305	-8	-66	Max	77.42								2.62	25			

305	-8	-66	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
305	-8	-66	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
305	-8	-66	Min.	77.42									2.62	25		
305	-8	-66	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
305	-67	-8	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
305	-67	-8	Max	72.58									2.62	25		
305	-67	-8	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
305	-67	-8	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
305	-67	-8	Min.	72.58									2.62	25		
305	-67	-8	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
306	-9	-69	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
306	-9	-69	Max	77.42									2.62	25		
306	-9	-69	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
306	-9	-69	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
306	-9	-69	Min.	77.42									2.62	25		
306	-9	-69	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
306	-68	-9	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	32	0.00	19
306	-68	-9	Max	72.58									2.62	25		
306	-68	-9	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
306	-68	-9	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
306	-68	-9	Min.	72.58									2.62	25		
306	-68	-9	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
307	-11	-70	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
307	-11	-70	Max	77.42									2.62	25		
307	-11	-70	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
307	-11	-70	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
307	-11	-70	Min.	77.42									2.62	25		
307	-11	-70	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
307	-71	-11	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	32	0.00	19
307	-71	-11	Max	72.58									2.62	25		
307	-71	-11	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
307	-71	-11	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
307	-71	-11	Min.	72.58									2.62	25		
307	-71	-11	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
308	-12	-72	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
308	-12	-72	Max	77.42									2.62	25		
308	-12	-72	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
308	-12	-72	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
308	-12	-72	Min.	77.42									2.62	25		
308	-12	-72	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
308	-73	-12	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
308	-73	-12	Max	72.58									2.62	25		
308	-73	-12	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
308	-73	-12	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	32	0.00	19
308	-73	-12	Min.	72.58									2.62	25		
308	-73	-12	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
309	-13	-74	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
309	-13	-74	Max	77.42									2.62	25		
309	-13	-74	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
309	-13	-74	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
309	-13	-74	Min.	77.42									2.62	25		
309	-13	-74	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
309	-75	-13	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	32	0.00	19
309	-75	-13	Max	72.58									2.62	25		
309	-75	-13	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
309	-75	-13	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
309	-75	-13	Min.	72.58									2.62	25		
309	-75	-13	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
310	-14	-90	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
310	-14	-90	Max	77.42									2.62	25		
310	-14	-90	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
310	-14	-90	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
310	-14	-90	Min.	77.42									2.62	25		
310	-14	-90	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
310	-91	-14	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	32	0.00	19
310	-91	-14	Max	72.58									2.62	25		
310	-91	-14	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
310	-91	-14	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
310	-91	-14	Min.	72.58									2.62	25		
310	-91	-14	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
311	-15	-92	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
311	-15	-92	Max	77.42									2.62	25		
311	-15	-92	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
311	-15	-92	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
311	-15	-92	Min.	77.42									2.62	25		
311	-15	-92	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19

311	-93	-15	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
311	-93	-15	Max	72.58									2.62	25		
311	-93	-15	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
311	-93	-15	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
311	-93	-15	Min.	72.58									2.62	25		
311	-93	-15	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
312	-16	-98	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
312	-16	-98	Max	77.42									2.62	25		
312	-16	-98	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
312	-16	-98	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
312	-16	-98	Min.	77.42									2.62	25		
312	-16	-98	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
312	-94	-16	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
312	-94	-16	Max	72.58									2.62	25		
312	-94	-16	Min.	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
312	-94	-16	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	32	0.00	19
312	-94	-16	Min.	72.58									2.62	25		
312	-94	-16	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
313	-17	-97	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
313	-17	-97	Max	77.42									2.62	25		
313	-17	-97	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
313	-17	-97	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
313	-17	-97	Min.	77.42									2.62	25		
313	-17	-97	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
313	-42	-17	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
313	-42	-17	Max	72.58									2.62	25		
313	-42	-17	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
313	-42	-17	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
313	-42	-17	Min.	72.58									2.62	25		
313	-42	-17	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
314	-18	-43	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
314	-18	-43	Max	77.42									2.62	25		
314	-18	-43	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
314	-18	-43	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
314	-18	-43	Min.	77.42									2.62	25		
314	-18	-43	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
314	-44	-18	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
314	-44	-18	Max	72.58									2.62	25		
314	-44	-18	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
314	-44	-18	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
314	-44	-18	Min.	72.58									2.62	25		
314	-44	-18	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
315	-19	-45	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
315	-19	-45	Max	77.42									2.62	25		
315	-19	-45	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
315	-19	-45	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
315	-19	-45	Min.	77.42									2.62	25		
315	-19	-45	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
315	-58	-19	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	32	0.00	19
315	-58	-19	Max	72.58									2.62	25		
315	-58	-19	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
315	-58	-19	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
315	-58	-19	Min.	72.58									2.62	25		
315	-58	-19	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
316	-20	-63	Max	0.00	82.31	19	0.00	19	0.00	19	68.22	32	-10.34	25	0.00	19
316	-20	-63	Max	124.19									0.47	25		
316	-20	-63	Max	150.00	13.22	19	0.00	19	0.00	19	15.36	32	0.00	25	0.00	19
316	-20	-63	Min.	0.00	81.62	25	0.00	19	0.00	19	17.40	25	-62.69	32	0.00	19
316	-20	-63	Min.	124.19									0.47	25		
316	-20	-63	Min.	150.00	12.96	25	0.00	19	0.00	19	-3.62	25	0.00	32	0.00	19
316	-65	-20	Max	0.00	-12.96	25	0.00	19	0.00	19	3.62	25	0.00	32	0.00	19
316	-65	-20	Max	25.81									0.47	25		
316	-65	-20	Max	150.00	-81.62	25	0.00	19	0.00	19	-17.40	25	-10.34	25	0.00	19
316	-65	-20	Min.	0.00	-13.22	19	0.00	19	0.00	19	-15.36	32	0.00	19	0.00	19
316	-65	-20	Min.	25.81									0.47	25		
316	-65	-20	Min.	150.00	-82.31	19	0.00	19	0.00	19	-68.22	32	-62.69	32	0.00	19
317	-21	-51	Max	0.00	82.31	19	0.00	19	0.00	19	68.22	32	-10.34	25	0.00	19
317	-21	-51	Max	124.19									0.47	25		
317	-21	-51	Max	150.00	13.22	19	0.00	19	0.00	19	15.36	32	0.00	25	0.00	19
317	-21	-51	Min.	0.00	81.62	25	0.00	19	0.00	19	17.40	25	-62.69	32	0.00	19
317	-21	-51	Min.	124.19									0.47	25		
317	-21	-51	Min.	150.00	12.96	25	0.00	19	0.00	19	-3.62	25	0.00	32	0.00	19
317	-50	-21	Max	0.00	-12.96	25	0.00	19	0.00	19	3.62	25	0.00	25	0.00	19
317	-50	-21	Max	25.81									0.47	25		
317	-50	-21	Max	150.00	-81.62	25	0.00	19	0.00	19	-17.40	25	-10.34	25	0.00	19
317	-50	-21	Min.	0.00	-13.22	19	0.00	19	0.00	19	-15.36	32	0.00	32	0.00	19

317	-50	-21	Min.	25.81						0.47	25					
317	-50	-21	Min.	150.00	-82.31	19	0.00	19	0.00	19	-68.22	32	-62.69	32	0.00	19
318	-22	-53	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
318	-22	-53	Max	77.42									2.62	25		
318	-22	-53	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
318	-22	-53	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
318	-22	-53	Min.	77.42									2.62	25		
318	-22	-53	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
318	-52	-22	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	32	0.00	19
318	-52	-22	Max	72.58									2.62	25		
318	-52	-22	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
318	-52	-22	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
318	-52	-22	Min.	72.58									2.62	25		
318	-52	-22	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
319	-23	-55	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
319	-23	-55	Max	77.42									2.62	25		
319	-23	-55	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
319	-23	-55	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
319	-23	-55	Min.	77.42									2.62	25		
319	-23	-55	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
319	-54	-23	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
319	-54	-23	Max	72.58									2.62	25		
319	-54	-23	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
319	-54	-23	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
319	-54	-23	Min.	72.58									2.62	25		
319	-54	-23	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
320	-24	-57	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
320	-24	-57	Max	77.42									2.62	25		
320	-24	-57	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
320	-24	-57	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
320	-24	-57	Min.	77.42									2.62	25		
320	-24	-57	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
320	-56	-24	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
320	-56	-24	Max	72.58									2.62	25		
320	-56	-24	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
320	-56	-24	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
320	-56	-24	Min.	72.58									2.62	25		
320	-56	-24	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
322	-25	-41	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
322	-25	-41	Max	77.42									2.62	25		
322	-25	-41	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
322	-25	-41	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
322	-25	-41	Min.	77.42									2.62	25		
322	-25	-41	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
322	-64	-25	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
322	-64	-25	Max	72.58									2.62	25		
322	-64	-25	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
322	-64	-25	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
322	-64	-25	Min.	72.58									2.62	25		
322	-64	-25	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
323	-26	-77	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
323	-26	-77	Max	77.42									2.62	25		
323	-26	-77	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
323	-26	-77	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
323	-26	-77	Min.	77.42									2.62	25		
323	-26	-77	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
323	-76	-26	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
323	-76	-26	Max	72.58									2.62	25		
323	-76	-26	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
323	-76	-26	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
323	-76	-26	Min.	72.58									2.62	25		
323	-76	-26	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
324	-27	-79	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
324	-27	-79	Max	77.42									2.62	25		
324	-27	-79	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
324	-27	-79	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
324	-27	-79	Min.	77.42									2.62	25		
324	-27	-79	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	19	0.00	19
324	-78	-27	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	32	0.00	19
324	-78	-27	Max	72.58									2.62	25		
324	-78	-27	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
324	-78	-27	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
324	-78	-27	Min.	72.58									2.62	25		
324	-78	-27	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
325	-28	-81	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
325	-28	-81	Max	77.42									2.62	25		

325	-28	-81	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
325	-28	-81	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
325	-28	-81	Min.	77.42									2.62	25		
325	-28	-81	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
325	-80	-28	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
325	-80	-28	Max	72.58									2.62	25		
325	-80	-28	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
325	-80	-28	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
325	-80	-28	Min.	72.58									2.62	25		
325	-80	-28	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
326	-29	-83	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
326	-29	-83	Max	77.42									2.62	25		
326	-29	-83	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
326	-29	-83	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
326	-29	-83	Min.	77.42									2.62	25		
326	-29	-83	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
326	-82	-29	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
326	-82	-29	Max	72.58									2.62	25		
326	-82	-29	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
326	-82	-29	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	32	0.00	19
326	-82	-29	Min.	72.58									2.62	25		
326	-82	-29	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
327	-30	-85	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
327	-30	-85	Max	77.42									2.62	25		
327	-30	-85	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
327	-30	-85	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
327	-30	-85	Min.	77.42									2.62	25		
327	-30	-85	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	32	0.00	19
327	-84	-30	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
327	-84	-30	Max	72.58									2.62	25		
327	-84	-30	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
327	-84	-30	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
327	-84	-30	Min.	72.58									2.62	25		
327	-84	-30	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
329	-32	-86	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
329	-32	-86	Max	77.42									2.62	25		
329	-32	-86	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	25	0.00	19
329	-32	-86	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
329	-32	-86	Min.	77.42									2.62	25		
329	-32	-86	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	19	0.00	19
329	-87	-32	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	32	0.00	19
329	-87	-32	Max	72.58									2.62	25		
329	-87	-32	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
329	-87	-32	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
329	-87	-32	Min.	72.58									2.62	25		
329	-87	-32	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
330	-33	-89	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
330	-33	-89	Max	77.42									2.62	25		
330	-33	-89	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	19	0.00	19
330	-33	-89	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
330	-33	-89	Min.	77.42									2.62	25		
330	-33	-89	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	25	0.00	19
330	-88	-33	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	25	0.00	19
330	-88	-33	Max	72.58									2.62	25		
330	-88	-33	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
330	-88	-33	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	19	0.00	19
330	-88	-33	Min.	72.58									2.62	25		
330	-88	-33	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
331	-34	-61	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
331	-34	-61	Max	77.42									2.62	25		
331	-34	-61	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	19	0.00	19
331	-34	-61	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
331	-34	-61	Min.	77.42									2.62	25		
331	-34	-61	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	25	0.00	19
331	-62	-34	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
331	-62	-34	Max	72.58									2.62	25		
331	-62	-34	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
331	-62	-34	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	32	0.00	19
331	-62	-34	Min.	72.58									2.62	25		
331	-62	-34	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
332	-35	-102	Max	0.00	117.72	19	0.00	19	0.00	19	109.36	32	-0.36	25	0.00	19
332	-35	-102	Max	77.42									2.62	25		
332	-35	-102	Max	150.00	26.44	19	0.00	19	0.00	19	30.73	32	0.00	19	0.00	19
332	-35	-102	Min.	0.00	116.33	25	0.00	19	0.00	19	7.71	25	-105.07	32	0.00	19
332	-35	-102	Min.	77.42									2.62	25		
332	-35	-102	Min.	150.00	25.93	25	0.00	19	0.00	19	-7.23	25	0.00	25	0.00	19

332	-101	-35	Max	0.00	-25.93	25	0.00	19	0.00	19	7.23	25	0.00	19	0.00	19
332	-101	-35	Max	72.58									2.62	25		
332	-101	-35	Max	150.00	-116.33	25	0.00	19	0.00	19	-7.71	25	-0.36	25	0.00	19
332	-101	-35	Min.	0.00	-26.44	19	0.00	19	0.00	19	-30.73	32	0.00	25	0.00	19
332	-101	-35	Min.	72.58									2.62	25		
332	-101	-35	Min.	150.00	-117.72	19	0.00	19	0.00	19	-109.36	32	-105.07	32	0.00	19
333	-37	-103	Max	0.00	82.32	19	0.00	19	0.00	19	68.22	32	-10.34	25	0.00	19
333	-37	-103	Max	124.19									0.47	25		
333	-37	-103	Max	150.00	13.22	19	0.00	19	0.00	19	15.36	32	0.00	25	0.00	19
333	-37	-103	Min.	0.00	81.62	25	0.00	19	0.00	19	17.40	25	-62.69	32	0.00	19
333	-37	-103	Min.	124.19									0.47	25		
333	-37	-103	Min.	150.00	12.96	25	0.00	19	0.00	19	-3.62	25	0.00	32	0.00	19
333	-104	-37	Max	0.00	-12.96	25	0.00	19	0.00	19	3.62	25	0.00	32	0.00	19
333	-104	-37	Max	25.81									0.47	25		
333	-104	-37	Max	150.00	-81.62	25	0.00	19	0.00	19	-17.40	25	-10.34	25	0.00	19
333	-104	-37	Min.	0.00	-13.22	19	0.00	19	0.00	19	-15.36	32	0.00	25	0.00	19
333	-104	-37	Min.	25.81									0.47	25		
333	-104	-37	Min.	150.00	-82.32	19	0.00	19	0.00	19	-68.22	32	-62.69	32	0.00	19

Tipo di combinazione di carico: SLE Q

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-1113.36	20	43.55	20	-46.28	20	0.00	20	0.00	20	0.00	20
1	1	-5	Max	328.50	-875.29	20	43.55	20	96.77	20	0.00	20	0.00	20	0.00	20
1	1	-5	Min.	0.00	-1113.36	20	43.55	20	-46.28	20	0.00	20	0.00	20	0.00	20
1	1	-5	Min.	328.50	-875.29	20	43.55	20	96.77	20	0.00	20	0.00	20	0.00	20
2	2	-10	Max	0.00	-2136.05	20	55.14	20	-59.02	20	0.00	20	0.00	20	0.00	20
2	2	-10	Max	328.50	-1897.98	20	55.14	20	122.12	20	0.00	20	0.00	20	0.00	20
2	2	-10	Min.	0.00	-2136.05	20	55.14	20	-59.02	20	0.00	20	0.00	20	0.00	20
2	2	-10	Min.	328.50	-1897.98	20	55.14	20	122.12	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	0.00	-2207.00	20	-44.78	20	48.81	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	328.50	-1968.93	20	-44.78	20	-98.29	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	0.00	-2207.00	20	-44.78	20	48.81	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	328.50	-1968.93	20	-44.78	20	-98.29	20	0.00	20	0.00	20	0.00	20
4	4	204	Max	0.00	-1944.35	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Max	328.50	-1706.29	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Min.	0.00	-1944.35	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Min.	328.50	-1706.29	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
5	5	205	Max	0.00	-2207.00	20	-44.78	20	48.81	20	0.00	20	0.00	20	0.00	20
5	5	205	Max	328.50	-1968.93	20	-44.78	20	-98.28	20	0.00	20	0.00	20	0.00	20
5	5	205	Min.	0.00	-2207.00	20	-44.78	20	48.81	20	0.00	20	0.00	20	0.00	20
5	5	205	Min.	328.50	-1968.93	20	-44.78	20	-98.28	20	0.00	20	0.00	20	0.00	20
6	6	-31	Max	0.00	-2136.04	20	55.14	20	-59.02	20	0.00	20	0.00	20	0.00	20
6	6	-31	Max	328.50	-1897.98	20	55.14	20	122.11	20	0.00	20	0.00	20	0.00	20
6	6	-31	Min.	0.00	-2136.04	20	55.14	20	-59.02	20	0.00	20	0.00	20	0.00	20
6	6	-31	Min.	328.50	-1897.98	20	55.14	20	122.11	20	0.00	20	0.00	20	0.00	20
7	7	-36	Max	0.00	-1113.36	20	43.55	20	-46.28	20	0.00	20	0.00	20	0.00	20
7	7	-36	Max	328.50	-875.29	20	43.55	20	96.77	20	0.00	20	0.00	20	0.00	20
7	7	-36	Min.	0.00	-1113.36	20	43.55	20	-46.28	20	0.00	20	0.00	20	0.00	20
7	7	-36	Min.	328.50	-875.29	20	43.55	20	96.77	20	0.00	20	0.00	20	0.00	20
201	-5	-4	Max	0.00	0.00	20	0.00	20	261.89	20	-181.50	20	0.00	20	0.00	20
201	-5	-4	Max	80.60	0.00	20	0.00	20	188.50	20	0.00	20	0.00	20	0.00	20
201	-5	-4	Min.	0.00	0.00	20	0.00	20	261.89	20	-181.50	20	0.00	20	0.00	20
201	-5	-4	Min.	80.60	0.00	20	0.00	20	188.50	20	0.00	20	0.00	20	0.00	20
201	-6	-5	Max	0.00	-43.55	20	0.00	20	-564.83	20	35.98	20	0.00	20	0.00	20
201	-6	-5	Max	53.34	-43.55	20	0.00	20	-613.40	20	-278.27	20	0.00	20	0.00	20
201	-6	-5	Min.	0.00	-43.55	20	0.00	20	-564.83	20	35.98	20	0.00	20	0.00	20
201	-6	-5	Min.	53.34	-43.55	20	0.00	20	-613.40	20	-278.27	20	0.00	20	0.00	20
201	-7	-6	Max	0.00	-43.55	20	0.00	20	-174.20	20	350.99	20	0.00	20	0.00	20
201	-7	-6	Max	133.94	-43.55	20	0.00	20	-296.17	20	35.98	20	0.00	20	0.00	20
201	-7	-6	Min.	0.00	-43.55	20	0.00	20	-174.20	20	350.99	20	0.00	20	0.00	20
201	-7	-6	Min.	133.94	-43.55	20	0.00	20	-296.17	20	35.98	20	0.00	20	0.00	20
201	-8	-7	Max	0.00	-43.55	20	0.00	20	216.43	20	142.78	20	0.00	20	0.00	20
201	-8	-7	Max	133.94	-43.55	20	0.00	20	94.46	20	350.99	20	0.00	20	0.00	20
201	-8	-7	Min.	0.00	-43.55	20	0.00	20	216.43	20	142.78	20	0.00	20	0.00	20
201	-8	-7	Min.	133.94	-43.55	20	0.00	20	94.46	20	350.99	20	0.00	20	0.00	20
201	-9	-8	Max	0.00	-43.55	20	0.00	20	607.06	20	-588.65	20	0.00	20	0.00	20
201	-9	-8	Max	133.94	-43.55	20	0.00	20	485.09	20	142.78	20	0.00	20	0.00	20
201	-9	-8	Min.	0.00	-43.55	20	0.00	20	607.06	20	-588.65	20	0.00	20	0.00	20
201	-9	-8	Min.	133.94	-43.55	20	0.00	20	485.09	20	142.78	20	0.00	20	0.00	20
201	-10	-9	Max	0.00	-43.55	20	0.00	20	916.54	20	-990.37	20	0.00	20	0.00	20
201	-10	-9	Max	44.83	-43.55	20	0.00	20	875.72	20	-588.65	20	0.00	20	0.00	20
201	-10	-9	Min.	0.00	-43.55	20	0.00	20	916.54	20	-990.37	20	0.00	20	0.00	20
201	-10	-9	Min.	44.83	-43.55	20	0.00	20	875.72	20	-588.65	20	0.00	20	0.00	20
202	-11	-10	Max	0.00	-98.69	20	0.00	20	-900.29	20	-274.05	20	0.00	20	0.00	20

202	-11	-10	Max	89.11	-98.69	20	0.00	20	0.00	20	-981.44	20	-1112.49	20	0.00	20
202	-11	-10	Min.	0.00	-98.69	20	0.00	20	0.00	20	-900.29	20	-274.05	20	0.00	20
202	-11	-10	Min.	89.11	-98.69	20	0.00	20	0.00	20	-981.44	20	-1112.49	20	0.00	20
202	-12	-11	Max	0.00	-98.69	20	0.00	20	0.00	20	-509.66	20	490.30	20	0.00	20
202	-12	-11	Max	133.94	-98.69	20	0.00	20	0.00	20	-631.63	20	-274.05	20	0.00	20
202	-12	-11	Min.	0.00	-98.69	20	0.00	20	0.00	20	-509.66	20	490.30	20	0.00	20
202	-12	-11	Min.	133.94	-98.69	20	0.00	20	0.00	20	-631.63	20	-274.05	20	0.00	20
202	-13	-12	Max	0.00	-98.69	20	0.00	20	0.00	20	-119.03	20	731.42	20	0.00	20
202	-13	-12	Max	133.94	-98.69	20	0.00	20	0.00	20	-241.00	20	490.30	20	0.00	20
202	-13	-12	Min.	0.00	-98.69	20	0.00	20	0.00	20	-119.03	20	731.42	20	0.00	20
202	-13	-12	Min.	133.94	-98.69	20	0.00	20	0.00	20	-241.00	20	490.30	20	0.00	20
202	-14	-13	Max	0.00	-98.69	20	0.00	20	0.00	20	271.59	20	449.32	20	0.00	20
202	-14	-13	Max	133.94	-98.69	20	0.00	20	0.00	20	149.62	20	731.42	20	0.00	20
202	-14	-13	Min.	0.00	-98.69	20	0.00	20	0.00	20	271.59	20	449.32	20	0.00	20
202	-14	-13	Min.	133.94	-98.69	20	0.00	20	0.00	20	149.62	20	731.42	20	0.00	20
202	-15	-14	Max	0.00	-98.69	20	0.00	20	0.00	20	662.22	20	-355.99	20	0.00	20
202	-15	-14	Max	133.94	-98.69	20	0.00	20	0.00	20	540.25	20	449.32	20	0.00	20
202	-15	-14	Min.	0.00	-98.69	20	0.00	20	0.00	20	662.22	20	-355.99	20	0.00	20
202	-15	-14	Min.	133.94	-98.69	20	0.00	20	0.00	20	540.25	20	449.32	20	0.00	20
202	203	-15	Max	0.00	-98.69	20	0.00	20	0.00	20	1008.02	20	-1177.26	20	0.00	20
202	203	-15	Max	84.71	-98.69	20	0.00	20	0.00	20	930.88	20	-356.00	20	0.00	20
202	203	-15	Min.	0.00	-98.69	20	0.00	20	0.00	20	1008.02	20	-1177.26	20	0.00	20
202	203	-15	Min.	84.71	-98.69	20	0.00	20	0.00	20	930.88	20	-356.00	20	0.00	20
203	-16	203	Max	0.00	-53.91	20	0.00	20	0.00	20	-916.08	20	-616.96	20	0.00	20
203	-16	203	Max	49.23	-53.91	20	0.00	20	0.00	20	-960.90	20	-1078.96	20	0.00	20
203	-16	203	Min.	0.00	-53.91	20	0.00	20	0.00	20	-916.08	20	-616.96	20	0.00	20
203	-16	203	Min.	49.23	-53.91	20	0.00	20	0.00	20	-960.90	20	-1078.96	20	0.00	20
203	-17	-16	Max	0.00	-53.91	20	0.00	20	0.00	20	-525.45	20	168.51	20	0.00	20
203	-17	-16	Max	133.94	-53.91	20	0.00	20	0.00	20	-647.42	20	-616.98	20	0.00	20
203	-17	-16	Min.	0.00	-53.91	20	0.00	20	0.00	20	-525.45	20	168.51	20	0.00	20
203	-17	-16	Min.	133.94	-53.91	20	0.00	20	0.00	20	-647.42	20	-616.98	20	0.00	20
203	-18	-17	Max	0.00	-53.91	20	0.00	20	0.00	20	-134.83	20	430.78	20	0.00	20
203	-18	-17	Max	133.94	-53.91	20	0.00	20	0.00	20	-256.79	20	168.50	20	0.00	20
203	-18	-17	Min.	0.00	-53.91	20	0.00	20	0.00	20	-134.83	20	430.78	20	0.00	20
203	-18	-17	Min.	133.94	-53.91	20	0.00	20	0.00	20	-256.79	20	168.50	20	0.00	20
203	-19	-18	Max	0.00	-53.91	20	0.00	20	0.00	20	255.81	20	169.81	20	0.00	20
203	-19	-18	Max	133.94	-53.91	20	0.00	20	0.00	20	133.84	20	430.77	20	0.00	20
203	-19	-18	Min.	0.00	-53.91	20	0.00	20	0.00	20	255.81	20	169.81	20	0.00	20
203	-19	-18	Min.	133.94	-53.91	20	0.00	20	0.00	20	133.84	20	430.77	20	0.00	20
203	-20	-19	Max	0.00	-53.91	20	0.00	20	0.00	20	646.43	20	-614.34	20	0.00	20
203	-20	-19	Max	133.94	-53.91	20	0.00	20	0.00	20	524.47	20	169.83	20	0.00	20
203	-20	-19	Min.	0.00	-53.91	20	0.00	20	0.00	20	646.43	20	-614.34	20	0.00	20
203	-20	-19	Min.	133.94	-53.91	20	0.00	20	0.00	20	524.47	20	169.83	20	0.00	20
203	204	-20	Max	0.00	-53.91	20	0.00	20	0.00	20	853.14	20	-783.15	20	0.00	20
203	204	-20	Max	20.00	-53.91	20	0.00	20	0.00	20	834.93	20	-614.34	20	0.00	20
203	204	-20	Min.	0.00	-53.91	20	0.00	20	0.00	20	853.14	20	-783.15	20	0.00	20
203	204	-20	Min.	20.00	-53.91	20	0.00	20	0.00	20	834.93	20	-614.34	20	0.00	20
204	204	-21	Max	0.00	-53.91	20	0.00	20	0.00	20	853.14	20	-783.15	20	0.00	20
204	204	-21	Max	20.00	-53.91	20	0.00	20	0.00	20	834.93	20	-614.34	20	0.00	20
204	204	-21	Min.	0.00	-53.91	20	0.00	20	0.00	20	853.14	20	-783.15	20	0.00	20
204	204	-21	Min.	20.00	-53.91	20	0.00	20	0.00	20	834.93	20	-614.34	20	0.00	20
204	-21	-22	Max	0.00	-53.91	20	0.00	20	0.00	20	646.44	20	-614.34	20	0.00	20
204	-21	-22	Max	133.94	-53.91	20	0.00	20	0.00	20	524.47	20	169.83	20	0.00	20
204	-21	-22	Min.	0.00	-53.91	20	0.00	20	0.00	20	646.44	20	-614.34	20	0.00	20
204	-21	-22	Min.	133.94	-53.91	20	0.00	20	0.00	20	524.47	20	169.83	20	0.00	20
204	-22	-23	Max	0.00	-53.91	20	0.00	20	0.00	20	255.81	20	169.81	20	0.00	20
204	-22	-23	Max	133.94	-53.91	20	0.00	20	0.00	20	133.84	20	430.77	20	0.00	20
204	-22	-23	Min.	0.00	-53.91	20	0.00	20	0.00	20	255.81	20	169.81	20	0.00	20
204	-22	-23	Min.	133.94	-53.91	20	0.00	20	0.00	20	133.84	20	430.77	20	0.00	20
204	-23	-24	Max	0.00	-53.91	20	0.00	20	0.00	20	-134.82	20	430.78	20	0.00	20
204	-23	-24	Max	133.94	-53.91	20	0.00	20	0.00	20	-256.79	20	168.50	20	0.00	20
204	-23	-24	Min.	0.00	-53.91	20	0.00	20	0.00	20	-134.82	20	430.78	20	0.00	20
204	-23	-24	Min.	133.94	-53.91	20	0.00	20	0.00	20	-256.79	20	168.50	20	0.00	20
204	-24	-25	Max	0.00	-53.91	20	0.00	20	0.00	20	-525.45	20	168.51	20	0.00	20
204	-24	-25	Max	133.94	-53.91	20	0.00	20	0.00	20	-647.42	20	-616.98	20	0.00	20
204	-24	-25	Min.	0.00	-53.91	20	0.00	20	0.00	20	-525.45	20	168.51	20	0.00	20
204	-24	-25	Min.	133.94	-53.91	20	0.00	20	0.00	20	-647.42	20	-616.98	20	0.00	20
204	-25	205	Max	0.00	-53.91	20	0.00	20	0.00	20	-916.08	20	-616.96	20	0.00	20
204	-25	205	Max	49.23	-53.91	20	0.00	20	0.00	20	-960.90	20	-1078.96	20	0.00	20
204	-25	205	Min.	0.00	-53.91	20	0.00	20	0.00	20	-916.08	20	-616.96	20	0.00	20
204	-25	205	Min.	49.23	-53.91	20	0.00	20	0.00	20	-960.90	20	-1078.96	20	0.00	20
205	205	-26	Max	0.00	-98.69	20	0.00	20	0.00	20	1008.02	20	-1177.26	20	0.00	20
205	205	-26	Max	84.71	-98.69	20	0.00	20	0.00	20	930.88	20	-355.99	20	0.00	20
205	205	-26	Min.	0.00	-98.69	20	0.00	20	0.00	20	1008.02	20	-1177.26	20	0.00	20
205	205	-26	Min.	84.71	-98.69	20	0.00	20	0.00	20	930.88	20	-355.99	20	0.00	20
205	-26	-27	Max	0.00	-98.69	20	0.00	20	0.00	20	662.23	20	-356.03	20	0.00	20

205	-26	-27	Max	133.94	-98.69	20	0.00	20	0.00	20	540.26	20	449.29	20	0.00	20
205	-26	-27	Min.	0.00	-98.69	20	0.00	20	0.00	20	662.23	20	-356.03	20	0.00	20
205	-26	-27	Min.	133.94	-98.69	20	0.00	20	0.00	20	540.26	20	449.29	20	0.00	20
205	-27	-28	Max	0.00	-98.69	20	0.00	20	0.00	20	271.59	20	449.33	20	0.00	20
205	-27	-28	Max	133.94	-98.69	20	0.00	20	0.00	20	149.62	20	731.42	20	0.00	20
205	-27	-28	Min.	0.00	-98.69	20	0.00	20	0.00	20	271.59	20	449.33	20	0.00	20
205	-27	-28	Min.	133.94	-98.69	20	0.00	20	0.00	20	149.62	20	731.42	20	0.00	20
205	-28	-29	Max	0.00	-98.69	20	0.00	20	0.00	20	-119.03	20	731.42	20	0.00	20
205	-28	-29	Max	133.94	-98.69	20	0.00	20	0.00	20	-241.00	20	490.30	20	0.00	20
205	-28	-29	Min.	0.00	-98.69	20	0.00	20	0.00	20	-119.03	20	731.42	20	0.00	20
205	-28	-29	Min.	133.94	-98.69	20	0.00	20	0.00	20	-241.00	20	490.30	20	0.00	20
205	-29	-30	Max	0.00	-98.69	20	0.00	20	0.00	20	-509.66	20	490.30	20	0.00	20
205	-29	-30	Max	133.94	-98.69	20	0.00	20	0.00	20	-631.63	20	-274.03	20	0.00	20
205	-29	-30	Min.	0.00	-98.69	20	0.00	20	0.00	20	-509.66	20	490.30	20	0.00	20
205	-29	-30	Min.	133.94	-98.69	20	0.00	20	0.00	20	-631.63	20	-274.03	20	0.00	20
205	-30	-31	Max	0.00	-98.69	20	0.00	20	0.00	20	-900.29	20	-274.08	20	0.00	20
205	-30	-31	Max	89.11	-98.69	20	0.00	20	0.00	20	-981.44	20	-1112.52	20	0.00	20
205	-30	-31	Min.	0.00	-98.69	20	0.00	20	0.00	20	-900.29	20	-274.08	20	0.00	20
205	-30	-31	Min.	89.11	-98.69	20	0.00	20	0.00	20	-981.44	20	-1112.52	20	0.00	20
206	-31	-32	Max	0.00	-43.55	20	0.00	20	0.00	20	916.54	20	-990.37	20	0.00	20
206	-31	-32	Max	44.83	-43.55	20	0.00	20	0.00	20	875.72	20	-588.64	20	0.00	20
206	-31	-32	Min.	0.00	-43.55	20	0.00	20	0.00	20	916.54	20	-990.37	20	0.00	20
206	-31	-32	Min.	44.83	-43.55	20	0.00	20	0.00	20	875.72	20	-588.64	20	0.00	20
206	-32	-33	Max	0.00	-43.55	20	0.00	20	0.00	20	607.06	20	-588.63	20	0.00	20
206	-32	-33	Max	133.94	-43.55	20	0.00	20	0.00	20	485.09	20	142.79	20	0.00	20
206	-32	-33	Min.	0.00	-43.55	20	0.00	20	0.00	20	607.06	20	-588.63	20	0.00	20
206	-32	-33	Min.	133.94	-43.55	20	0.00	20	0.00	20	485.09	20	142.79	20	0.00	20
206	-33	-34	Max	0.00	-43.55	20	0.00	20	0.00	20	216.43	20	142.78	20	0.00	20
206	-33	-34	Max	133.94	-43.55	20	0.00	20	0.00	20	94.46	20	350.99	20	0.00	20
206	-33	-34	Min.	0.00	-43.55	20	0.00	20	0.00	20	216.43	20	142.78	20	0.00	20
206	-33	-34	Min.	133.94	-43.55	20	0.00	20	0.00	20	94.46	20	350.99	20	0.00	20
206	-34	-35	Max	0.00	-43.55	20	0.00	20	0.00	20	-174.19	20	350.99	20	0.00	20
206	-34	-35	Max	133.94	-43.55	20	0.00	20	0.00	20	-296.16	20	35.98	20	0.00	20
206	-34	-35	Min.	0.00	-43.55	20	0.00	20	0.00	20	-174.19	20	350.99	20	0.00	20
206	-34	-35	Min.	133.94	-43.55	20	0.00	20	0.00	20	-296.16	20	35.98	20	0.00	20
206	-35	-36	Max	0.00	-43.55	20	0.00	20	0.00	20	-564.83	20	35.96	20	0.00	20
206	-35	-36	Max	53.34	-43.55	20	0.00	20	0.00	20	-613.40	20	-278.29	20	0.00	20
206	-35	-36	Min.	0.00	-43.55	20	0.00	20	0.00	20	-564.83	20	35.96	20	0.00	20
206	-35	-36	Min.	53.34	-43.55	20	0.00	20	0.00	20	-613.40	20	-278.29	20	0.00	20
206	-36	-37	Max	0.00	0.00	20	0.00	20	0.00	20	261.89	20	-181.50	20	0.00	20
206	-36	-37	Max	80.60	0.00	20	0.00	20	0.00	20	188.50	20	0.00	20	0.00	20
206	-36	-37	Min.	0.00	0.00	20	0.00	20	0.00	20	261.89	20	-181.50	20	0.00	20
206	-36	-37	Min.	80.60	0.00	20	0.00	20	0.00	20	188.50	20	0.00	20	0.00	20
302	-4	-47	Max	0.00	81.62	20	0.00	20	0.00	20	47.12	20	-40.96	20	0.00	20
302	-4	-47	Max	150.00	12.96	20	0.00	20	0.00	20	7.48	20	0.00	20	0.00	20
302	-4	-47	Min.	0.00	81.62	20	0.00	20	0.00	20	47.12	20	-40.96	20	0.00	20
302	-4	-47	Min.	150.00	12.96	20	0.00	20	0.00	20	7.48	20	0.00	20	0.00	20
302	-46	-4	Max	0.00	-12.96	20	0.00	20	0.00	20	-7.48	20	0.00	20	0.00	20
302	-46	-4	Max	150.00	-81.62	20	0.00	20	0.00	20	-47.12	20	-40.96	20	0.00	20
302	-46	-4	Min.	0.00	-12.96	20	0.00	20	0.00	20	-7.48	20	0.00	20	0.00	20
302	-46	-4	Min.	150.00	-81.62	20	0.00	20	0.00	20	-47.12	20	-40.96	20	0.00	20
303	-6	-48	Max	0.00	116.33	20	0.00	20	0.00	20	67.17	20	-61.60	20	0.00	20
303	-6	-48	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
303	-6	-48	Min.	0.00	116.33	20	0.00	20	0.00	20	67.17	20	-61.60	20	0.00	20
303	-6	-48	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
303	-49	-6	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
303	-49	-6	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.17	20	-61.60	20	0.00	20
303	-49	-6	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
303	-49	-6	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.17	20	-61.60	20	0.00	20
304	-7	-96	Max	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
304	-7	-96	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
304	-7	-96	Min.	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
304	-7	-96	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
304	-95	-7	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
304	-95	-7	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
304	-95	-7	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
304	-95	-7	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
305	-8	-66	Max	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
305	-8	-66	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
305	-8	-66	Min.	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
305	-8	-66	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
305	-67	-8	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
305	-67	-8	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
305	-67	-8	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
305	-67	-8	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
306	-9	-69	Max	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20

326	-29	-83	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
326	-29	-83	Min.	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
326	-29	-83	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
326	-82	-29	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
326	-82	-29	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
326	-82	-29	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
326	-82	-29	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
327	-30	-85	Max	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
327	-30	-85	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
327	-30	-85	Min.	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
327	-30	-85	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
327	-84	-30	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
327	-84	-30	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
327	-84	-30	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
327	-84	-30	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
329	-32	-86	Max	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
329	-32	-86	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
329	-32	-86	Min.	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
329	-32	-86	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
329	-87	-32	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
329	-87	-32	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
329	-87	-32	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
329	-87	-32	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.16	20	-61.60	20	0.00	20
330	-33	-89	Max	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
330	-33	-89	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
330	-33	-89	Min.	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
330	-33	-89	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
330	-88	-33	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
330	-88	-33	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.17	20	-61.60	20	0.00	20
330	-88	-33	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
330	-88	-33	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.17	20	-61.60	20	0.00	20
331	-34	-61	Max	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
331	-34	-61	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
331	-34	-61	Min.	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
331	-34	-61	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
331	-62	-34	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
331	-62	-34	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.17	20	-61.60	20	0.00	20
331	-62	-34	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
331	-62	-34	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.17	20	-61.60	20	0.00	20
332	-35	-102	Max	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
332	-35	-102	Max	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
332	-35	-102	Min.	0.00	116.33	20	0.00	20	0.00	20	67.16	20	-61.60	20	0.00	20
332	-35	-102	Min.	150.00	25.93	20	0.00	20	0.00	20	14.97	20	0.00	20	0.00	20
332	-101	-35	Max	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
332	-101	-35	Max	150.00	-116.33	20	0.00	20	0.00	20	-67.17	20	-61.60	20	0.00	20
332	-101	-35	Min.	0.00	-25.93	20	0.00	20	0.00	20	-14.97	20	0.00	20	0.00	20
332	-101	-35	Min.	150.00	-116.33	20	0.00	20	0.00	20	-67.17	20	-61.60	20	0.00	20
333	-37	-103	Max	0.00	81.62	20	0.00	20	0.00	20	47.12	20	-40.96	20	0.00	20
333	-37	-103	Max	150.00	12.96	20	0.00	20	0.00	20	7.48	20	0.00	20	0.00	20
333	-37	-103	Min.	0.00	81.62	20	0.00	20	0.00	20	47.12	20	-40.96	20	0.00	20
333	-37	-103	Min.	150.00	12.96	20	0.00	20	0.00	20	7.48	20	0.00	20	0.00	20
333	-104	-37	Max	0.00	-12.96	20	0.00	20	0.00	20	-7.48	20	0.00	20	0.00	20
333	-104	-37	Max	150.00	-81.62	20	0.00	20	0.00	20	-47.12	20	-40.96	20	0.00	20
333	-104	-37	Min.	0.00	-12.96	20	0.00	20	0.00	20	-7.48	20	0.00	20	0.00	20
333	-104	-37	Min.	150.00	-81.62	20	0.00	20	0.00	20	-47.12	20	-40.96	20	0.00	20

Verifiche aste in acciaio

Simbologia

Φ_{LT}	=	Coefficiente Φ per stabilità laterale membrature inflesse
Φ_y	=	Coefficiente Φ per inflessione intorno all'asse y(c)
Φ_z	=	Coefficiente Φ per inflessione intorno all'asse z(e)
α_{imp}	=	Coefficiente di imperfezione
$\alpha_{my}, \alpha_{mz}, \alpha_{LT}$	=	Coefficienti correttivi per il momento flettente
β_{LT}	=	Coefficiente per calcolo Φ_{LT}
χ_{LT}	=	Coefficiente di riduzione per stabilità laterale membrature inflesse
χ_y	=	Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
χ_z	=	Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
δ	<cm>	=Spostamento relativo asta
λ^*_y	=	Snellezza adimensionale per inflessione intorno all'asse y(c)
λ^*_z	=	Snellezza adimensionale per inflessione intorno all'asse z(e)
λ_{LT}	=	Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$	=	Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
λ_y	=	Snellezza per inflessione intorno all'asse y(c)
λ_z	=	Snellezza per inflessione intorno all'asse z(e)
$\sigma_{TD,max}$	<daN/cm²>	=Tensione ideale massima
σ_M	<daN/cm²>	=Tensione normale per momento flettente
σ_N	<daN/cm²>	=Tensione normale per sforzo normale
τ	<daN/cm²>	=Tensione tangenziale per taglio e/o torsione

ψ		= Coeff. di correzione momento critico per stabilità laterale membrature inflesse
Aeff	<cmq>	= Area effettiva per trazione
Anet	<cmq>	= Area netta per compressione
Area	<cmq>	= Area
Atag,y	<cmq>	= Area resistente a taglio in dir. Y
Atag,z	<cmq>	= Area resistente a taglio in dir. Z
CC		= Numero della combinazione delle condizioni di carico elementari
Cod.		= Codice
Curva		= Curva di instabilità adottata
D	<cm>	= Distanza
Fyk	<daN/cmq>	= Tensione caratteristica di snervamento dell'acciaio
Fyt	<daN/cmq>	= Tensione caratteristica di rottura
Iy	<cm>	= Raggio giratorio d'inerzia rispetto all'asse Y
Iz	<cm>	= Raggio giratorio d'inerzia rispetto all'asse Z
J0	<cm6>	= Costante di ingobbamento
Jy	<cm4>	= Momento d'inerzia rispetto all'asse Y
Jz	<cm4>	= Momento d'inerzia rispetto all'asse Z
Kyy, Kyz, Kzy, Kzz		= Coefficienti di interazione
L	<cm>	= Lunghezza dell'asta
Lcr	<cm>	= Lunghezza di libera inflessione laterale fra ritegni torsionali
M,cr	<daNm>	= Momento critico per instabilità flesso torsionale
MNy,c,Rd	<daNm>	= Resistenza di calcolo a pressoflessione intorno all'asse Y
Mx	<daNm>	= Momento torcente intorno all'asse X
My	<daNm>	= Momento flettente intorno all'asse Y
My,Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Y
My,V,c,Rd	<daNm>	= Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y
Mz	<daNm>	= Momento flettente intorno all'asse Z
Mz,Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Z
N	<daN>	= Sforzo normale
N,Ed	<daN>	= Forza assiale di calcolo
Nc,Rd	<daN>	= Resistenza a compressione
Ncr,y	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
Ncr,z	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
Sez.		= Numero della sezione
Tip		= Tipologia
		Rc = Rettangolare cava
		Is = I stondata
Tip		= Tipo di acciaio
Ty	<daN>	= Taglio in dir. Y
Tz	<daN>	= Taglio in dir. Z
V,Ed	<daN>	= Forza di taglio di calcolo
Vc,Rd	<daN>	= Resistenza a taglio
Vc,Rd,Red	<daN>	= Resistenza a taglio ridotta
Wy,plas	<cmc>	= Modulo di resistenza plastico intorno all'asse Y
Wymin	<cmc>	= Modulo di resistenza minimo rispetto all'asse Y
Wz,plas	<cmc>	= Modulo di resistenza plastico intorno all'asse Z
Wzmin	<cmc>	= Modulo di resistenza minimo rispetto all'asse Z
Xl	<m>	= Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
f		= Fattore di modifica per il coefficiente di riduzione
fz,g	<cm>	= Freccia in direzione Z globale
fz,l	<cm>	= Freccia in direzione Z locale
kc		= Coeff. di correzione momento flettente per stabilità laterale membrature inflesse

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D	Area	Anet	Aeff	Jy	Jz	Iy	Iz	Wymin	Wzmin	Tip	Fyk	Fyt
			<cm>	<cmq>	<cmq>	<cmq>	<cm4>	<cm4>	<cm>	<cm>	<cmc>	<cmc>		<daN/cmq>	<daN/cmq>
1	COL HEA280	Is	--	97.27	97.27	97.27	13673.70	4762.65	11.86	7.00	1012.87	340.19	S355 UNI EN 10025-2	3550.00	5100.00
2	TRV PRINC SHS300x300x10	Rc	--	116.00	116.00	116.00	16278.70	16278.70	11.85	11.85	1085.24	1085.24	S355H UNI EN 10210-1	3550.00	5100.00
3	TRV SEC RHS150x100x10	Rc	--	46.00	46.00	46.00	1347.83	695.33	5.41	3.89	179.71	139.07	S355H UNI EN 10210-1	3550.00	5100.00

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy,plas	Wz,plas	Atag,y	Atag,z	J0
		<cmc>	<cmc>	<cmq>	<cmq>	<cm6>
1	COL HEA280	1117.45	518.72	81.59	31.75	785367.00
2	TRV PRINC SHS300x300x10	1262.00	1262.00	58.00	58.00	
3	TRV SEC RHS150x100x10	224.50	167.00	18.40	27.60	

Asta n. 1 (1 -5) - Sez. 1 (COL HEA280) - Crit. 1

-
- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-1274.83 Tz=61.96 My=234.71 Ty=322.47 Mz=-545.29
 Tensioni: $\sigma_N=-13.11$ $\sigma_{m,d}=-183.46$ $\tau=0.00$ $\sigma_{max}=-196.57$ (sfrut=0.06)
 Tensioni: $\sigma_N=-13.11$ $\sigma_{m,d}=-53.00$ $\tau=6.38$ $\tau_{max}=6.38$ (sfrut=0.00)
 Tensioni: $\sigma_N=-13.11$ $\sigma_{m,d}=-183.46$ $\tau=0.00$ $\sigma_{ID,max}=196.57$ (sfrut=0.06)
 - Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-608.05 Tz=1676.27 My=6314.01 Ty=7.01 Mz=-7.40 Mx=-2.12
 Tensioni: $\sigma_N=-6.25$ $\sigma_{m,d}=-625.56$ $\tau=4.94$ $\sigma_{max}=-631.81$ (sfrut=0.19)
 Tensioni: $\sigma_N=-6.25$ $\sigma_{m,d}=-0.06$ $\tau=91.00$ $\tau_{max}=91.00$ (sfrut=0.05)
 Tensioni: $\sigma_N=-6.25$ $\sigma_{m,d}=-625.56$ $\tau=4.94$ $\sigma_{ID,max}=631.87$ (sfrut=0.19)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-608.05 My,Ed=6314.01 Mz,Ed=15.64 L=3.29
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $L_{cr}=3.29$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.62$ $M,cr=216969.00$ $\lambda_{LT}=0.41$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.56$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=27.71$ $N_{cr,y}=2626240.00$ $\lambda_y^*=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ $N_{cr,z}=914738.00$ $\lambda_z^*=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: 0.00+0.18+0.00=0.18
 Verifica ZZ: 0.00+0.14+0.00=0.14

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=0.58$ (L/564)

Asta n. 2 (2 -10) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2042.54 T_z=103.13 M_y=345.73 T_y=376.82 M_z=-604.70
 Tensioni: $\sigma_N=-21.00$ $\sigma_{m,d}=-211.89$ $\tau=0.00$ $\sigma_{max}=-232.89$ (sfrut=0.07)
 Tensioni: $\sigma_N=-21.00$ $\sigma_{m,d}=-66.40$ $\tau=7.47$ $\tau_{max}=7.47$ (sfrut=0.00)
 Tensioni: $\sigma_N=-21.00$ $\sigma_{m,d}=-211.89$ $\tau=0.00$ $\sigma_{ID,max}=232.89$ (sfrut=0.07)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-818.61 T_z=3639.14 M_y=11346.80 T_y=16.16 M_z=-17.35 M_x=-1.42
 Tensioni: $\sigma_N=-8.42$ $\sigma_{m,d}=-1125.36$ $\tau=3.31$ $\sigma_{max}=-1133.78$ (sfrut=0.34)
 Tensioni: $\sigma_N=-8.42$ $\sigma_{m,d}=-0.15$ $\tau=197.28$ $\tau_{max}=197.28$ (sfrut=0.10)
 Tensioni: $\sigma_N=-8.42$ $\sigma_{m,d}=-1125.36$ $\tau=3.31$ $\sigma_{ID,max}=1133.79$ (sfrut=0.34)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-818.61 M_y,Ed=11346.80 M_z,Ed=35.75 L=3.29
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 L_{cr}=3.29 Curva b: $\alpha_{imp}=0.34$ k_e=0.94 $\psi=1.81$ M_{cr}=241934.00 $\lambda_{LT}=0.39$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.55$ $\beta_{LT}=0.75$ f=0.98 $\chi_{LT}=1.00$
 $\lambda_y=27.71$ Ncr,y=2626240.00 $\lambda'_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ Ncr,z=914738.00 $\lambda'_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.31+0.00=0.32
 Verifica ZZ: 0.00+0.25+0.00=0.26

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=0.97$ (L/339)

Asta n. 3 (3 203) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2179.16 T_z=111.48 M_y=378.75 T_y=-352.02 M_z=579.19
 Tensioni: $\sigma_N=-22.40$ $\sigma_{m,d}=-207.65$ $\tau=0.00$ $\sigma_{max}=-230.05$ (sfrut=0.07)
 Tensioni: $\sigma_N=-22.40$ $\sigma_{m,d}=0.26$ $\tau=6.99$ $\tau_{max}=6.99$ (sfrut=0.00)
 Tensioni: $\sigma_N=-22.40$ $\sigma_{m,d}=-207.65$ $\tau=0.00$ $\sigma_{ID,max}=230.05$ (sfrut=0.07)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-845.75 T_z=3857.05 M_y=12339.40 T_y=-12.12 M_z=13.20
 Tensioni: $\sigma_N=-8.70$ $\sigma_{m,d}=-1222.15$ $\tau=0.00$ $\sigma_{max}=-1230.84$ (sfrut=0.36)
 Tensioni: $\sigma_N=-8.70$ $\sigma_{m,d}=0.11$ $\tau=209.07$ $\tau_{max}=209.07$ (sfrut=0.11)
 Tensioni: $\sigma_N=-8.70$ $\sigma_{m,d}=-1222.15$ $\tau=0.00$ $\sigma_{ID,max}=1230.84$ (sfrut=0.36)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-845.75 M_y,Ed=12339.40 M_z,Ed=-26.63 L=3.29
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 L_{cr}=3.29 Curva b: $\alpha_{imp}=0.34$ k_e=0.94 $\psi=1.78$ M_{cr}=238088.00 $\lambda_{LT}=0.39$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.55$ $\beta_{LT}=0.75$ f=0.98 $\chi_{LT}=1.00$
 $\lambda_y=27.71$ Ncr,y=2626240.00 $\lambda'_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ Ncr,z=914738.00 $\lambda'_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.34+0.00=0.35
 Verifica ZZ: 0.00+0.27+0.00=0.28

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=1.07$ (L/308)

Asta n. 4 (4 204) - Sez. 1 (COL HEA280) - Crit. 1

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-1944.35 T_z=100.26 M_y=354.35 T_y=314.80 M_z=-538.63
 Tensioni: $\sigma_N=-19.99$ $\sigma_{m,d}=-193.32$ $\tau=0.00$ $\sigma_{max}=-213.31$ (sfrut=0.06)
 Tensioni: $\sigma_N=-19.99$ $\sigma_{m,d}=-63.28$ $\tau=6.25$ $\tau_{max}=6.25$ (sfrut=0.00)
 Tensioni: $\sigma_N=-19.99$ $\sigma_{m,d}=-193.32$ $\tau=0.00$ $\sigma_{ID,max}=213.31$ (sfrut=0.06)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-919.48 T_z=-3278.98 M_y=-11034.10
 Tensioni: $\sigma_N=-9.45$ $\sigma_{m,d}=-1089.39$ $\tau=0.00$ $\sigma_{max}=-1098.84$ (sfrut=0.33)
 Tensioni: $\sigma_N=-9.45$ $\sigma_{m,d}=0.00$ $\tau=177.74$ $\tau_{max}=177.74$ (sfrut=0.09)

Tensioni: $\sigma_N = -9.45$ $\sigma_{m,d} = -1089.39$ $\tau = 0.00$ $\sigma_{TD,max} = 1098.84$ (sfrut=0.33)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-919.48 My,Ed=-11034.10 Mz,Ed=0.00 L=3.29

$\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $L_{cr} = 3.29$ Curva b: $\alpha_{imp} = 0.34$ $k_c = 0.94$ $\psi = 1.73$ M,cr=230966.00 $\lambda_{LT} = 0.39$
 $\lambda_{LT,0} = 0.40$ $\Phi_{LT} = 0.56$ $\beta_{LT} = 0.75$ f=0.98 $\chi_{LT} = 1.00$
 $\lambda_y = 27.71$ Ncr,y=2626240.00 $\lambda^*_y = 0.36$ Curva b: $\Phi_y = 0.59$ $\chi_y = 0.94$
 $\lambda_z = 46.95$ Ncr,z=914738.00 $\lambda^*_z = 0.61$ Curva c: $\Phi_z = 0.79$ $\chi_z = 0.78$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.31=0.31
 Verifica ZZ: 0.00+0.25=0.25

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta = 0.97$ (L/337)

Asta n. 5 (5 205) - Sez. 1 (COL HEA280) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2179.16 Tz=-111.48 My=-378.75 Ty=-352.02 Mz=579.19

Tensioni: $\sigma_N = -22.40$ $\sigma_{m,d} = -207.65$ $\tau = 0.00$ $\sigma_{max} = -230.05$ (sfrut=0.07)
 Tensioni: $\sigma_N = -22.40$ $\sigma_{m,d} = 67.84$ $\tau = 6.99$ $\tau_{max} = 6.99$ (sfrut=0.00)
 Tensioni: $\sigma_N = -22.40$ $\sigma_{m,d} = -207.65$ $\tau = 0.00$ $\sigma_{TD,max} = 230.05$ (sfrut=0.07)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-845.74 Tz=-3857.06 My=-12339.50 Ty=-12.12 Mz=13.20

Tensioni: $\sigma_N = -8.70$ $\sigma_{m,d} = -1222.15$ $\tau = 0.00$ $\sigma_{max} = -1230.84$ (sfrut=0.36)
 Tensioni: $\sigma_N = -8.70$ $\sigma_{m,d} = 0.11$ $\tau = 209.07$ $\tau_{max} = 209.07$ (sfrut=0.11)
 Tensioni: $\sigma_N = -8.70$ $\sigma_{m,d} = -1222.15$ $\tau = 0.00$ $\sigma_{TD,max} = 1230.84$ (sfrut=0.36)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-845.74 My,Ed=-12339.50 Mz,Ed=-26.63 L=3.29

$\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $L_{cr} = 3.29$ Curva b: $\alpha_{imp} = 0.34$ $k_c = 0.94$ $\psi = 1.78$ M,cr=238088.00 $\lambda_{LT} = 0.39$
 $\lambda_{LT,0} = 0.40$ $\Phi_{LT} = 0.55$ $\beta_{LT} = 0.75$ f=0.98 $\chi_{LT} = 1.00$
 $\lambda_y = 27.71$ Ncr,y=2626240.00 $\lambda^*_y = 0.36$ Curva b: $\Phi_y = 0.59$ $\chi_y = 0.94$
 $\lambda_z = 46.95$ Ncr,z=914738.00 $\lambda^*_z = 0.61$ Curva c: $\Phi_z = 0.79$ $\chi_z = 0.78$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.34+0.00=0.35
 Verifica ZZ: 0.00+0.27+0.00=0.28

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta = 1.07$ (L/308)

Asta n. 6 (6 -31) - Sez. 1 (COL HEA280) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-2042.54 Tz=-103.13 My=-345.73 Ty=376.82 Mz=-604.70

Tensioni: $\sigma_N = -21.00$ $\sigma_{m,d} = -211.89$ $\tau = 0.00$ $\sigma_{max} = -232.89$ (sfrut=0.07)
 Tensioni: $\sigma_N = -21.00$ $\sigma_{m,d} = -4.70$ $\tau = 7.47$ $\tau_{max} = 7.47$ (sfrut=0.00)
 Tensioni: $\sigma_N = -21.00$ $\sigma_{m,d} = -211.89$ $\tau = 0.00$ $\sigma_{TD,max} = 232.89$ (sfrut=0.07)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-818.60 Tz=-3639.14 My=-11346.80 Ty=16.16 Mz=-17.36 Mx=1.42

Tensioni: $\sigma_N = -8.42$ $\sigma_{m,d} = -1125.36$ $\tau = 3.31$ $\sigma_{max} = -1133.78$ (sfrut=0.34)
 Tensioni: $\sigma_N = -8.42$ $\sigma_{m,d} = 0.15$ $\tau = 197.28$ $\tau_{max} = 197.28$ (sfrut=0.10)
 Tensioni: $\sigma_N = -8.42$ $\sigma_{m,d} = -1125.36$ $\tau = 3.31$ $\sigma_{TD,max} = 1133.79$ (sfrut=0.34)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-818.60 My,Ed=-11346.80 Mz,Ed=35.75 L=3.29

$\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $L_{cr} = 3.29$ Curva b: $\alpha_{imp} = 0.34$ $k_c = 0.94$ $\psi = 1.81$ M,cr=241934.00 $\lambda_{LT} = 0.39$
 $\lambda_{LT,0} = 0.40$ $\Phi_{LT} = 0.55$ $\beta_{LT} = 0.75$ f=0.98 $\chi_{LT} = 1.00$
 $\lambda_y = 27.71$ Ncr,y=2626240.00 $\lambda^*_y = 0.36$ Curva b: $\Phi_y = 0.59$ $\chi_y = 0.94$
 $\lambda_z = 46.95$ Ncr,z=914738.00 $\lambda^*_z = 0.61$ Curva c: $\Phi_z = 0.79$ $\chi_z = 0.78$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.31+0.00=0.32
 Verifica ZZ: 0.00+0.25+0.00=0.26

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta = 0.97$ (L/339)

Asta n. 7 (7 -36) - Sez. 1 (COL HEA280) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-1274.83 T_z=-61.96 M_y=-234.71 T_y=322.47 M_z=-545.29
 Tensioni: $\sigma_N=-13.11$ $\sigma_{m,d}=-183.46$ $\tau=0.00$ $\sigma_{max}=-196.57$ (sfrut=0.06)
 Tensioni: $\sigma_N=-13.11$ $\sigma_{m,d}=-11.12$ $\tau=6.38$ $\tau_{max}=6.38$ (sfrut=0.00)
 Tensioni: $\sigma_N=-13.11$ $\sigma_{m,d}=-183.46$ $\tau=0.00$ $\sigma_{ID,max}=196.57$ (sfrut=0.06)

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-608.05 T_z=-1676.27 M_y=-6314.01 T_y=7.01 M_z=-7.40 M_x=2.12
 Tensioni: $\sigma_N=-6.25$ $\sigma_{m,d}=-625.56$ $\tau=4.94$ $\sigma_{max}=-631.81$ (sfrut=0.19)
 Tensioni: $\sigma_N=-6.25$ $\sigma_{m,d}=0.06$ $\tau=91.00$ $\tau_{max}=91.00$ (sfrut=0.05)
 Tensioni: $\sigma_N=-6.25$ $\sigma_{m,d}=-625.56$ $\tau=4.94$ $\sigma_{ID,max}=631.87$ (sfrut=0.19)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-608.05 M_{y,Ed}=-6314.01 M_{z,Ed}=15.64 L=3.29
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 L_{cr}=3.29 Curva b: $\alpha_{imp}=0.34$ k_c=0.94 $\psi=1.62$ M_{cr}=216969.00 $\lambda_{LT}=0.41$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.56$ $\beta_{LT}=0.75$ f=0.98 $\chi_{LT}=1.00$
 $\lambda_y=27.71$ N_{cr,y}=2626240.00 $\lambda^*_y=0.36$ Curva b: $\Phi_y=0.59$ $\chi_y=0.94$
 $\lambda_z=46.95$ N_{cr,z}=914738.00 $\lambda^*_z=0.61$ Curva c: $\Phi_z=0.79$ $\chi_z=0.78$
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.18+0.00=0.18
 Verifica ZZ: 0.00+0.14+0.00=0.14

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=0.58$ (L/564)

- Asta n. 201 (-5 -4) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=11.97 T_z=261.89 M_y=184.49 T_y=-39.90 M_z=33.88 M_x=-9.94
 Tensioni: $\sigma_N=0.10$ $\sigma_{m,d}=20.12$ $\tau=0.59$ $\sigma_{max}=20.22$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.10$ $\sigma_{m,d}=-2.91$ $\tau=5.67$ $\tau_{max}=5.67$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.10$ $\sigma_{m,d}=20.12$ $\tau=0.59$ $\sigma_{ID,max}=20.25$ (sfrut=0.01)

- Verifica a taglio Dir. Y [4.2.16] - CC 28 SLU Xl=0.81
 Sollecitazioni: T_y=274.09
 V,Ed=274.09 V_c,Rd=113219.00 V,Ed/V_c,Rd=0.00

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.81
 Sollecitazioni: T_z=425.33
 V,Ed=425.33 V_c,Rd=113219.00 V,Ed/V_c,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: T_z=520.75 M_y=381.27 T_y=274.09 M_z=-220.92
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-55.49$ $\tau=0.00$ $\sigma_{max}=-55.49$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-19.00$ $\tau=10.10$ $\tau_{max}=10.10$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-55.49$ $\tau=0.00$ $\sigma_{ID,max}=55.49$ (sfrut=0.02)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: N,Ed=-11.97 M_{y,Ed}=178.52 M_{z,Ed}=-33.88 L=0.81
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=6.80$ N_{cr,y}=51935400.00 $\lambda^*_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.80$ N_{cr,z}=51935400.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.00+0.00=0.01
 Verifica ZZ: 0.00+0.00+0.00=0.00

- Asta n. 201 (-6 -5) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.53 - Classe 3
 Sollecitazioni: N=-250.67 T_z=-774.87 M_y=705.46 T_y=40.42 M_z=15.43 M_x=28.19
 Tensioni: $\sigma_N=-2.16$ $\sigma_{m,d}=-66.43$ $\tau=1.68$ $\sigma_{max}=-68.59$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.16$ $\sigma_{m,d}=-1.33$ $\tau=16.69$ $\tau_{max}=16.69$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.16$ $\sigma_{m,d}=-66.43$ $\tau=1.68$ $\sigma_{ID,max}=68.65$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.53 - Classe 2
 Sollecitazioni: T_z=-886.59
 V,Ed=-886.59 V_c,Rd=113219.00 V,Ed/V_c,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.53 - Classe 3
 Sollecitazioni: N=-7.01 T_z=-159.00 M_y=89.67 T_y=1290.13 M_z=313.35 M_x=807.46
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-37.14$ $\tau=48.01$ $\sigma_{max}=-37.20$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-7.71$ $\tau=73.01$ $\tau_{max}=73.01$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.06$ $\sigma_{m,d}=-8.26$ $\tau=73.01$ $\sigma_{ID,max}=126.73$ (sfrut=0.04)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-101.12 My,Ed=605.93 Mz,Ed=266.07 L=0.53
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=4.50$ Ncr, $y=118574000.00$ $\lambda^*_y=0.06$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=4.50$ Ncr, $z=118574000.00$ $\lambda^*_z=0.06$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 201 (-7 -6) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=100.87 T_z=-12.73 M_y=-490.72 T_y=6.96 M_z=-27.72 M_x=30.06
 Tensioni: $\sigma_N=0.87$ $\sigma_{m,d}=47.77$ $\tau=1.79$ $\sigma_{max}=48.64$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.87$ $\sigma_{m,d}=2.38$ $\tau=2.03$ $\tau_{max}=2.03$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.87$ $\sigma_{m,d}=47.77$ $\tau=1.79$ $\sigma_{ID,max}=48.74$ (sfrut=0.01)
 - Verifica a taglio e torsione Dir. Y [4.2.25] - CC 7 SND Xl=1.22 - Classe 2
 Sollecitazioni: T_y=21.60 M_x=23.71
 V,Ed=21.60 Vc,Rd,Red=113137.00 V,Ed/Vc,Rd,Red=0.00
 - Verifica a taglio e torsione Dir. Z [4.2.25] - CC 7 SND Xl=1.22 - Classe 2
 Sollecitazioni: T_z=-446.55 M_x=23.71
 V,Ed=-446.55 Vc,Rd,Red=113137.00 V,Ed/Vc,Rd,Red=0.00
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-101.12 T_z=-438.82 M_y=-802.18 T_y=-367.58 M_z=758.41 M_x=-573.15
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-143.80$ $\tau=34.08$ $\sigma_{max}=-144.67$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=65.22$ $\tau=42.58$ $\tau_{max}=42.58$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-143.80$ $\tau=34.08$ $\sigma_{ID,max}=156.25$ (sfrut=0.05)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-101.12 My,Ed=-802.18 Mz,Ed=758.41 L=1.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=11.31$ Ncr, $y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr, $z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.02=0.04
 Verifica ZZ: 0.00+0.02+0.02=0.04

Asta n. 201 (-8 -7) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=31.65 T_z=255.93 M_y=-505.67 T_y=-13.81 M_z=-36.36 M_x=25.58
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=49.95$ $\tau=1.52$ $\sigma_{max}=50.22$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=-3.13$ $\tau=6.48$ $\tau_{max}=6.48$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=49.95$ $\tau=1.52$ $\sigma_{ID,max}=50.29$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: T_z=304.43
 V,Ed=304.43 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3
 Sollecitazioni: N=-101.12 T_z=271.02 M_y=-802.18 T_y=180.60 M_z=758.41 M_x=-573.15
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-143.80$ $\tau=34.08$ $\sigma_{max}=-144.67$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-65.22$ $\tau=39.33$ $\tau_{max}=39.33$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-143.80$ $\tau=34.08$ $\sigma_{ID,max}=156.25$ (sfrut=0.05)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-101.12 My,Ed=-802.18 Mz,Ed=758.41 L=1.34
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=11.31$ Ncr, $y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr, $z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.02=0.04
 Verifica ZZ: 0.00+0.02+0.02=0.04

Asta n. 201 (-9 -8) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-37.56 T_z=768.53 M_y=851.57 T_y=-34.57 M_z=19.81 M_x=21.09
 Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=-80.29$ $\tau=1.25$ $\sigma_{max}=-80.62$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=1.70$ $\tau=16.15$ $\tau_{max}=16.15$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=-80.29$ $\tau=1.25$ $\sigma_{ID,max}=80.65$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: $T_z=868.36$
 $V,Ed=868.36$ $Vc,Rd=113219.00$ $V,Ed/Vc,Rd=0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: $N=-101.12$ $T_z=1297.97$ $M_y=1299.37$ $T_y=728.78$ $M_z=-459.64$ $M_x=-573.15$
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-162.08$ $\tau=34.08$ $\sigma_{max}=-162.96$ (sfrut=0.05)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=39.53$ $\tau=59.24$ $\tau_{max}=59.24$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=154.10$ $\tau=51.42$ $\sigma_{ID,max}=177.23$ (sfrut=0.05)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-101.12$ $M_y,Ed=1299.37$ $M_z,Ed=516.51$ $L=1.34$
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ $Ncr,y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ $Ncr,z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.03+0.01=0.05$
 Verifica ZZ: $0.00+0.03+0.01=0.04$

Asta n. 201 (-10 -9) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-99.59$ $T_z=1078.01$ $M_y=1310.73$ $T_y=38.53$ $M_z=-42.30$ $M_x=-10.25$
 Tensioni: $\sigma_N=-0.86$ $\sigma_{m,d}=-124.67$ $\tau=0.61$ $\sigma_{max}=-125.53$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.86$ $\sigma_{m,d}=3.64$ $\tau=21.50$ $\tau_{max}=21.50$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.86$ $\sigma_{m,d}=-124.67$ $\tau=0.61$ $\sigma_{ID,max}=125.54$ (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: $T_z=1326.80$
 $V,Ed=1326.80$ $Vc,Rd=113219.00$ $V,Ed/Vc,Rd=0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: $N=-101.12$ $T_z=2060.88$ $M_y=2211.34$ $T_y=1276.96$ $M_z=-1032.09$ $M_x=-573.15$
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-298.87$ $\tau=34.08$ $\sigma_{max}=-299.74$ (sfrut=0.09)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=88.76$ $\tau=74.03$ $\tau_{max}=74.03$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-298.87$ $\tau=34.08$ $\sigma_{ID,max}=305.49$ (sfrut=0.09)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-101.12$ $M_y,Ed=2211.34$ $M_z,Ed=-1032.09$ $L=0.45$
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.78$ $Ncr,y=167889000.00$ $\lambda^*_y=0.05$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=3.78$ $Ncr,z=167889000.00$ $\lambda^*_z=0.05$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.06+0.03=0.08$
 Verifica ZZ: $0.00+0.05+0.03=0.07$

Asta n. 202 (-11 -10) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.89 - Classe 3
 Sollecitazioni: $N=-332.43$ $T_z=-1049.40$ $M_y=1303.17$ $T_y=55.03$ $M_z=42.33$ $M_x=17.21$
 Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-123.98$ $\tau=1.02$ $\sigma_{max}=-126.85$ (sfrut=0.04)
 Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-3.64$ $\tau=21.36$ $\tau_{max}=21.36$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-123.98$ $\tau=1.02$ $\sigma_{ID,max}=126.86$ (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.89 - Classe 2
 Sollecitazioni: $T_z=-1414.07$
 $V,Ed=-1414.07$ $Vc,Rd=113219.00$ $V,Ed/Vc,Rd=0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.89 - Classe 3
 Sollecitazioni: $N=-222.63$ $T_z=-2163.92$ $M_y=2480.49$ $T_y=-1306.16$ $M_z=-1033.10$ $M_x=-141.73$
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-323.76$ $\tau=8.43$ $\sigma_{max}=-325.68$ (sfrut=0.10)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-88.85$ $\tau=50.38$ $\tau_{max}=50.38$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-323.76$ $\tau=8.43$ $\sigma_{ID,max}=326.01$ (sfrut=0.10)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-222.63$ $M_y,Ed=2480.49$ $M_z,Ed=-1033.10$ $L=0.89$
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=7.52$ $Ncr,y=42486100.00$ $\lambda^*_y=0.10$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.52$ $Ncr,z=42486100.00$ $\lambda^*_z=0.10$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.06+0.03=0.09$
 Verifica ZZ: $0.00+0.05+0.03=0.08$

Asta n. 202 (-12 -11) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-48.24 Tz=-489.27 My=-506.51 Ty=-97.26 Mz=142.73 Mx=-44.08
 Tensioni: $\sigma_N=-0.42$ $\sigma_{m,d}=-59.82$ $\tau=2.62$ $\sigma_{max}=-60.24$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.42$ $\sigma_{m,d}=12.28$ $\tau=12.10$ $\tau_{max}=12.10$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.42$ $\sigma_{m,d}=-59.82$ $\tau=2.62$ $\sigma_{ID,max}=60.41$ (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 2
 Sollecitazioni: Tz=-903.21
 V,Ed=-903.21 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-222.63 Tz=-1190.03 My=-1101.02 Ty=-757.98 Mz=1146.14 Mx=-141.73
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-207.06$ $\tau=8.43$ $\sigma_{max}=-208.98$ (sfrut=0.06)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=98.57$ $\tau=31.50$ $\tau_{max}=31.50$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-207.06$ $\tau=8.43$ $\sigma_{ID,max}=209.49$ (sfrut=0.06)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.63 My,Ed=-1101.02 Mz,Ed=1146.14 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03+0.03=0.06
 Verifica ZZ: 0.00+0.02+0.03=0.05

Asta n. 202 (-13 -12) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-128.37 Tz=-139.42 My=-738.03 Ty=28.04 Mz=-177.71 Mx=29.13
 Tensioni: $\sigma_N=-1.11$ $\sigma_{m,d}=-84.38$ $\tau=1.73$ $\sigma_{max}=-85.49$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.11$ $\sigma_{m,d}=15.28$ $\tau=4.43$ $\tau_{max}=4.43$ (sfrut=0.00)
 Tensioni: $\sigma_N=-1.11$ $\sigma_{m,d}=-84.38$ $\tau=1.73$ $\sigma_{ID,max}=85.54$ (sfrut=0.03)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 2
 Sollecitazioni: Tz=-339.27
 V,Ed=-339.27 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-222.63 Tz=-321.63 My=-1638.01 Ty=-209.80 Mz=1427.16 Mx=-141.73
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-282.44$ $\tau=8.43$ $\sigma_{max}=-284.36$ (sfrut=0.08)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=122.74$ $\tau=14.66$ $\tau_{max}=14.66$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-282.44$ $\tau=8.43$ $\sigma_{ID,max}=284.73$ (sfrut=0.08)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.63 My,Ed=-1638.01 Mz,Ed=1427.16 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.04=0.08
 Verifica ZZ: 0.00+0.03+0.04=0.07

Asta n. 202 (-14 -13) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-107.60 Tz=129.24 My=-733.55 Ty=45.24 Mz=178.32 Mx=-14.50
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-84.02$ $\tau=0.86$ $\sigma_{max}=-84.95$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-15.34$ $\tau=3.37$ $\tau_{max}=3.37$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-84.02$ $\tau=0.86$ $\sigma_{ID,max}=84.96$ (sfrut=0.03)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=383.21
 V,Ed=383.21 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3
 Sollecitazioni: N=-222.63 Tz=388.21 My=-1638.01 Ty=338.38 Mz=1427.16 Mx=-141.73
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-282.44$ $\tau=8.43$ $\sigma_{max}=-284.36$ (sfrut=0.08)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-122.74$ $\tau=15.95$ $\tau_{max}=15.95$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-282.44$ $\tau=8.43$ $\sigma_{ID,max}=284.73$ (sfrut=0.08)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.63 My,Ed=-1638.01 Mz,Ed=1427.16 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.04=0.08
 Verifica ZZ: 0.00+0.03+0.04=0.07

Asta n. 202 (-15 -14) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-86.84 Tz=519.87 My=-474.27 Ty=114.45 Mz=120.32
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=-54.79$ $\tau=0.00$ $\sigma_{max}=-55.54$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=10.35$ $\tau=10.08$ $\tau_{max}=10.08$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.75$ $\sigma_{m,d}=-54.79$ $\tau=0.00$ $\sigma_{ID,max}=55.54$ (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=947.15
 V,Ed=947.15 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3
 Sollecitazioni: N=-222.63 Tz=1256.61 My=-1011.84 Ty=886.55 Mz=973.93 Mx=-141.73
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-182.98$ $\tau=8.43$ $\sigma_{max}=-184.90$ (sfrut=0.05)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-83.76$ $\tau=32.79$ $\tau_{max}=32.79$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-182.98$ $\tau=8.43$ $\sigma_{ID,max}=185.47$ (sfrut=0.05)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.63 My,Ed=-1011.84 Mz,Ed=973.93 L=1.34
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03+0.03=0.05
 Verifica ZZ: 0.00+0.02+0.03=0.05

Asta n. 202 (203 -15) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-203.43 Tz=1075.99 My=1394.09 Ty=-60.08 Mz=55.97 Mx=-4.12
 Tensioni: $\sigma_N=-1.75$ $\sigma_{m,d}=-133.62$ $\tau=0.25$ $\sigma_{max}=-135.37$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.75$ $\sigma_{m,d}=-4.81$ $\tau=21.10$ $\tau_{max}=21.10$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.75$ $\sigma_{m,d}=-133.62$ $\tau=0.25$ $\sigma_{ID,max}=135.37$ (sfrut=0.04)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=1452.81
 V,Ed=1452.81 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-222.63 Tz=2225.29 My=2620.16 Ty=1434.73 Mz=-1428.98 Mx=-141.73
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-373.11$ $\tau=8.43$ $\sigma_{max}=-375.03$ (sfrut=0.11)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=122.89$ $\tau=51.57$ $\tau_{max}=51.57$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-373.11$ $\tau=8.43$ $\sigma_{ID,max}=375.31$ (sfrut=0.11)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.63 My,Ed=2620.16 Mz,Ed=-1428.98 L=0.85
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=7.15$ Ncr,y=47013500.00 $\lambda^*_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.15$ Ncr,z=47013500.00 $\lambda^*_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.07+0.04=0.11
 Verifica ZZ: 0.00+0.05+0.04=0.09

Asta n. 203 (-16 203) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.49 - Classe 3
 Sollecitazioni: N=-224.51 Tz=-1056.71 My=1341.06 Ty=-41.83 Mz=-55.96 Mx=-8.42
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-128.73$ $\tau=0.50$ $\sigma_{max}=-130.66$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-4.81$ $\tau=20.98$ $\tau_{max}=20.98$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-128.73$ $\tau=0.50$ $\sigma_{ID,max}=130.67$ (sfrut=0.04)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.49 - Classe 2
 Sollecitazioni: Tz=-1389.39
 V,Ed=-1389.39 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.49 - Classe 3
 Sollecitazioni: N=-123.05 Tz=-2150.17 My=2401.58 Ty=-1303.07 Mz=-1428.54 Mx=93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-352.93$ $\tau=5.54$ $\sigma_{max}=-353.99$ (sfrut=0.10)

Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=122.86$ $\tau=47.23$ $\tau_{max}=47.23$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-352.93$ $\tau=5.54$ $\sigma_{ID,max}=354.12$ (sfrut=0.10)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=2401.58 Mz,Ed=-1428.54 L=0.49
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=4.16$ Ncr,y=139222000.00 $\lambda^*_y=0.05$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=4.16$ Ncr,z=139222000.00 $\lambda^*_z=0.05$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.06+0.04=0.10
 Verifica ZZ: 0.00+0.05+0.04=0.09

Asta n. 203 (-17 -16) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-162.13 Tz=-743.22 My=846.87 Ty=36.00 Mz=35.05 Mx=3.94
 Tensioni: $\sigma_N=-1.40$ $\sigma_{m,d}=-81.27$ $\tau=0.23$ $\sigma_{max}=-82.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.40$ $\sigma_{m,d}=-3.01$ $\tau=14.64$ $\tau_{max}=14.64$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.40$ $\sigma_{m,d}=-81.27$ $\tau=0.23$ $\sigma_{ID,max}=82.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 2
 Sollecitazioni: Tz=-925.75
 V,Ed=-925.75 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3
 Sollecitazioni: N=-123.05 Tz=-1382.06 My=1357.47 Ty=-754.89 Mz=-787.08 Mx=93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-197.61$ $\tau=5.54$ $\sigma_{max}=-198.67$ (sfrut=0.06)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=67.69$ $\tau=32.33$ $\tau_{max}=32.33$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-197.61$ $\tau=5.54$ $\sigma_{ID,max}=198.90$ (sfrut=0.06)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=1357.47 Mz,Ed=-787.08 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.02=0.06
 Verifica ZZ: 0.00+0.03+0.02=0.05

Asta n. 203 (-18 -17) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-65.61 Tz=-163.57 My=-434.31 Ty=31.24 Mz=-69.59 Mx=-1.83
 Tensioni: $\sigma_N=-0.57$ $\sigma_{m,d}=-46.43$ $\tau=0.11$ $\sigma_{max}=-47.00$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.57$ $\sigma_{m,d}=-5.98$ $\tau=3.28$ $\tau_{max}=3.28$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.57$ $\sigma_{m,d}=-46.43$ $\tau=0.11$ $\sigma_{ID,max}=47.00$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 2
 Sollecitazioni: Tz=-361.82
 V,Ed=-361.82 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-123.05 Tz=-355.10 My=-969.31 Ty=-206.71 Mz=500.91 Mx=93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-135.47$ $\tau=5.54$ $\sigma_{max}=-136.53$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-43.08$ $\tau=12.43$ $\tau_{max}=12.43$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-135.47$ $\tau=5.54$ $\sigma_{ID,max}=136.87$ (sfrut=0.04)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=-969.31 Mz,Ed=500.91 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03+0.01=0.04
 Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 203 (-19 -18) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-62.97 Tz=162.58 My=-431.71 Ty=-41.84 Mz=-69.50 Mx=-16.78
 Tensioni: $\sigma_N=-0.54$ $\sigma_{m,d}=-46.18$ $\tau=1.00$ $\sigma_{max}=-46.73$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.54$ $\sigma_{m,d}=5.98$ $\tau=4.15$ $\tau_{max}=4.15$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.54$ $\sigma_{m,d}=-46.18$ $\tau=1.00$ $\sigma_{ID,max}=46.76$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=360.68$
 $V, Ed=360.68$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=1.34$ - Classe 3
 Sollecitazioni: $N=-123.05$ $T_z=354.75$ $M_y=-969.28$ $T_y=341.47$ $M_z=500.89$ $M_x=93.20$
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-135.47$ $\tau=5.54$ $\sigma_{max}=-136.53$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=43.08$ $\tau=12.42$ $\tau_{max}=12.42$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-135.47$ $\tau=5.54$ $\sigma_{ID,max}=136.87$ (sfrut=0.04)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed=-123.05$ $M_y, Ed=-969.28$ $M_z, Ed=500.89$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr, $y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr, $z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.03+0.01=0.04$
 Verifica ZZ: $0.00+0.02+0.01=0.03$

Asta n. 203 (-20 -19) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-153.33$ $T_z=742.24$ $M_y=852.87$ $T_y=-39.18$ $M_z=43.86$ $M_x=-9.52$
 Tensioni: $\sigma_N=-1.32$ $\sigma_{m,d}=-82.63$ $\tau=0.57$ $\sigma_{max}=-83.95$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.32$ $\sigma_{m,d}=-3.77$ $\tau=14.95$ $\tau_{max}=14.95$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.32$ $\sigma_{m,d}=-82.63$ $\tau=0.57$ $\sigma_{ID,max}=83.96$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=924.61$
 $V, Ed=924.61$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-123.05$ $T_z=1381.70$ $M_y=1356.53$ $T_y=889.65$ $M_z=-1148.07$ $M_x=93.20$
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-230.79$ $\tau=5.54$ $\sigma_{max}=-231.85$ (sfrut=0.07)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-98.74$ $\tau=32.33$ $\tau_{max}=32.33$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-230.79$ $\tau=5.54$ $\sigma_{ID,max}=232.05$ (sfrut=0.07)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed=-123.05$ $M_y, Ed=1356.53$ $M_z, Ed=-1148.07$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr, $y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr, $z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.04+0.03=0.07$
 Verifica ZZ: $0.00+0.03+0.03=0.06$

Asta n. 203 (204 -20) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-199.15$ $T_z=948.94$ $M_y=1030.89$ $T_y=40.04$ $M_z=-48.70$ $M_x=12.50$
 Tensioni: $\sigma_N=-1.72$ $\sigma_{m,d}=-99.48$ $\tau=0.74$ $\sigma_{max}=-101.20$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.72$ $\sigma_{m,d}=-4.19$ $\tau=19.13$ $\tau_{max}=19.13$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.72$ $\sigma_{m,d}=-99.48$ $\tau=0.74$ $\sigma_{ID,max}=101.20$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=1221.39$
 $V, Ed=1221.39$ $V_c, Rd=113219.00$ $V, Ed/V_c, Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-123.05$ $T_z=1830.71$ $M_y=1720.30$ $T_y=1163.74$ $M_z=-1380.82$ $M_x=93.20$
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-285.75$ $\tau=5.54$ $\sigma_{max}=-286.81$ (sfrut=0.08)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-118.75$ $\tau=41.04$ $\tau_{max}=41.04$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-285.75$ $\tau=5.54$ $\sigma_{ID,max}=286.98$ (sfrut=0.08)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed=-123.05$ $M_y, Ed=1720.30$ $M_z, Ed=-1380.82$ $L=0.20$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=1.69$ Ncr, $y=843496000.00$ $\lambda^*_y=0.02$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=1.69$ Ncr, $z=843496000.00$ $\lambda^*_z=0.02$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.04+0.04=0.08$
 Verifica ZZ: $0.00+0.04+0.04=0.07$

Asta n. 204 (204 -21) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-199.15 Tz=948.94 My=1030.89 Ty=-40.04 Mz=48.70 Mx=-12.50
 Tensioni: $\sigma_N=-1.72$ $\sigma_{m,d}=-99.48$ $\tau=0.74$ $\sigma_{max}=-101.20$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.72$ $\sigma_{m,d}=-4.19$ $\tau=19.13$ $\tau_{max}=19.13$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.72$ $\sigma_{m,d}=-99.48$ $\tau=0.74$ $\sigma_{ID,max}=101.20$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=1221.39
 V,Ed=1221.39 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-123.05 Tz=1830.71 My=1720.31 Ty=-1163.74 Mz=1380.82 Mx=-93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-285.75$ $\tau=5.54$ $\sigma_{max}=-286.81$ (sfrut=0.08)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-118.75$ $\tau=41.04$ $\tau_{max}=41.04$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-285.75$ $\tau=5.54$ $\sigma_{ID,max}=286.98$ (sfrut=0.08)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=1720.31 Mz,Ed=1380.82 L=0.20
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=1.69$ Ncr,y=843496000.00 $\lambda^*_y=0.02$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=1.69$ Ncr,z=843496000.00 $\lambda^*_z=0.02$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.04=0.08
 Verifica ZZ: 0.00+0.04+0.04=0.07

- Asta n. 204 (-21 -22) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-153.33 Tz=742.24 My=852.87 Ty=39.18 Mz=-43.86 Mx=9.52
 Tensioni: $\sigma_N=-1.32$ $\sigma_{m,d}=-82.63$ $\tau=0.57$ $\sigma_{max}=-83.95$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.32$ $\sigma_{m,d}=-3.77$ $\tau=14.95$ $\tau_{max}=14.95$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.32$ $\sigma_{m,d}=-82.63$ $\tau=0.57$ $\sigma_{ID,max}=83.96$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=924.61
 V,Ed=924.61 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-123.05 Tz=1381.70 My=1356.53 Ty=-889.65 Mz=1148.07 Mx=-93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-230.79$ $\tau=5.54$ $\sigma_{max}=-231.85$ (sfrut=0.07)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-98.74$ $\tau=32.33$ $\tau_{max}=32.33$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-230.79$ $\tau=5.54$ $\sigma_{ID,max}=232.05$ (sfrut=0.07)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=1356.53 Mz,Ed=1148.07 L=1.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.03=0.07
 Verifica ZZ: 0.00+0.03+0.03=0.06

- Asta n. 204 (-22 -23) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-62.97 Tz=162.58 My=-431.71 Ty=41.84 Mz=69.50 Mx=16.78
 Tensioni: $\sigma_N=-0.54$ $\sigma_{m,d}=-46.18$ $\tau=1.00$ $\sigma_{max}=-46.73$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.54$ $\sigma_{m,d}=5.98$ $\tau=4.15$ $\tau_{max}=4.15$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.54$ $\sigma_{m,d}=-46.18$ $\tau=1.00$ $\sigma_{ID,max}=46.76$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: Tz=360.68
 V,Ed=360.68 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3
 Sollecitazioni: N=-123.05 Tz=354.75 My=-969.29 Ty=-341.47 Mz=-500.89 Mx=-93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-135.47$ $\tau=5.54$ $\sigma_{max}=-136.53$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=43.08$ $\tau=12.42$ $\tau_{max}=12.42$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-135.47$ $\tau=5.54$ $\sigma_{ID,max}=136.87$ (sfrut=0.04)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=-969.29 Mz,Ed=-500.89 L=1.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03+0.01=0.04
 Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 204 (-23 -24) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-65.61 Tz=-163.56 My=-434.31 Ty=-31.24 Mz=69.59 Mx=1.83
 Tensioni: $\sigma_N=-0.57$ $\sigma_{m,d}=-46.43$ $\tau=0.11$ $\sigma_{max}=-47.00$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.57$ $\sigma_{m,d}=-5.98$ $\tau=3.28$ $\tau_{max}=3.28$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.57$ $\sigma_{m,d}=-46.43$ $\tau=0.11$ $\sigma_{ID,max}=47.00$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 2
 Sollecitazioni: Tz=-361.82
 V,Ed=-361.82 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-123.05 Tz=-355.10 My=-969.31 Ty=206.71 Mz=-500.92 Mx=-93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-135.47$ $\tau=5.54$ $\sigma_{max}=-136.53$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-43.08$ $\tau=12.42$ $\tau_{max}=12.42$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-135.47$ $\tau=5.54$ $\sigma_{ID,max}=136.87$ (sfrut=0.04)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=-969.31 Mz,Ed=-500.92 L=1.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03+0.01=0.04
 Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 204 (-24 -25) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-162.13 Tz=-743.22 My=846.87 Ty=-36.00 Mz=-35.05 Mx=-3.94
 Tensioni: $\sigma_N=-1.40$ $\sigma_{m,d}=-81.26$ $\tau=0.23$ $\sigma_{max}=-82.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.40$ $\sigma_{m,d}=-3.01$ $\tau=14.64$ $\tau_{max}=14.64$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.40$ $\sigma_{m,d}=-81.26$ $\tau=0.23$ $\sigma_{ID,max}=82.66$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 2
 Sollecitazioni: Tz=-925.75
 V,Ed=-925.75 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3
 Sollecitazioni: N=-123.05 Tz=-1382.05 My=1357.47 Ty=754.89 Mz=787.07 Mx=-93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-197.61$ $\tau=5.54$ $\sigma_{max}=-198.67$ (sfrut=0.06)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=67.69$ $\tau=32.33$ $\tau_{max}=32.33$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-197.61$ $\tau=5.54$ $\sigma_{ID,max}=198.90$ (sfrut=0.06)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=1357.47 Mz,Ed=787.07 L=1.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.02=0.06
 Verifica ZZ: 0.00+0.03+0.02=0.05

Asta n. 204 (-25 205) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.49 - Classe 3
 Sollecitazioni: N=-224.51 Tz=-1056.70 My=1341.06 Ty=41.83 Mz=55.96 Mx=8.42
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-128.73$ $\tau=0.50$ $\sigma_{max}=-130.66$ (sfrut=0.04)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-4.81$ $\tau=20.98$ $\tau_{max}=20.98$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.94$ $\sigma_{m,d}=-128.73$ $\tau=0.50$ $\sigma_{ID,max}=130.67$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.49 - Classe 2
 Sollecitazioni: Tz=-1389.39
 V,Ed=-1389.39 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.49 - Classe 3
 Sollecitazioni: N=-123.05 Tz=-2150.17 My=2401.57 Ty=1303.07 Mz=1428.53 Mx=-93.20
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=-352.93$ $\tau=5.54$ $\sigma_{max}=-353.99$ (sfrut=0.10)
 Tensioni: $\sigma_N=-1.06$ $\sigma_{m,d}=122.86$ $\tau=47.23$ $\tau_{max}=47.23$ (sfrut=0.02)

Tensioni: $\sigma_N = -1.06$ $\sigma_{m,d} = -352.93$ $\tau = 5.54$ $\sigma_{ID,max} = 354.12$ (sfrut=0.10)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed = -123.05$ $M_y, Ed = 2401.57$ $M_z, Ed = 1428.53$ $L = 0.49$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.16$ Ncr, $y = 139222000.00$ $\lambda^*_y = 0.05$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 4.16$ Ncr, $z = 139222000.00$ $\lambda^*_z = 0.05$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.06 + 0.04 = 0.10$
 Verifica ZZ: $0.00 + 0.05 + 0.04 = 0.09$

Asta n. 205 (205 -26) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -203.43$ $T_z = 1075.99$ $M_y = 1394.08$ $T_y = 60.08$ $M_z = -55.97$ $M_x = 4.12$
 Tensioni: $\sigma_N = -1.75$ $\sigma_{m,d} = -133.62$ $\tau = 0.25$ $\sigma_{max} = -135.37$ (sfrut=0.04)
 Tensioni: $\sigma_N = -1.75$ $\sigma_{m,d} = -4.81$ $\tau = 21.10$ $\tau_{max} = 21.10$ (sfrut=0.01)
 Tensioni: $\sigma_N = -1.75$ $\sigma_{m,d} = -133.62$ $\tau = 0.25$ $\sigma_{ID,max} = 135.37$ (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l = 0.00$ - Classe 2
 Sollecitazioni: $T_z = 1452.80$
 $V, Ed = 1452.80$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l = 0.00$ - Classe 3
 Sollecitazioni: $N = -222.62$ $T_z = 2225.29$ $M_y = 2620.14$ $T_y = -1434.73$ $M_z = 1428.97$ $M_x = 141.73$
 Tensioni: $\sigma_N = -1.92$ $\sigma_{m,d} = -373.11$ $\tau = 8.43$ $\sigma_{max} = -375.02$ (sfrut=0.11)
 Tensioni: $\sigma_N = -1.92$ $\sigma_{m,d} = 122.89$ $\tau = 51.57$ $\tau_{max} = 51.57$ (sfrut=0.03)
 Tensioni: $\sigma_N = -1.92$ $\sigma_{m,d} = -373.11$ $\tau = 8.43$ $\sigma_{ID,max} = 375.31$ (sfrut=0.11)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed = -222.62$ $M_y, Ed = 2620.14$ $M_z, Ed = 1428.97$ $L = 0.85$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 7.15$ Ncr, $y = 47013300.00$ $\lambda^*_y = 0.09$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 7.15$ Ncr, $z = 47013300.00$ $\lambda^*_z = 0.09$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.07 + 0.04 = 0.11$
 Verifica ZZ: $0.00 + 0.05 + 0.04 = 0.09$

Asta n. 205 (-26 -27) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l = 1.34$ - Classe 3
 Sollecitazioni: $N = -86.84$ $T_z = 519.87$ $M_y = -474.24$ $T_y = -114.45$ $M_z = -120.31$
 Tensioni: $\sigma_N = -0.75$ $\sigma_{m,d} = -54.78$ $\tau = 0.00$ $\sigma_{max} = -55.53$ (sfrut=0.02)
 Tensioni: $\sigma_N = -0.75$ $\sigma_{m,d} = -10.35$ $\tau = 10.08$ $\tau_{max} = 10.08$ (sfrut=0.01)
 Tensioni: $\sigma_N = -0.75$ $\sigma_{m,d} = -54.78$ $\tau = 0.00$ $\sigma_{ID,max} = 55.53$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l = 0.00$ - Classe 2
 Sollecitazioni: $T_z = 947.15$
 $V, Ed = 947.15$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.01$
- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l = 1.34$ - Classe 3
 Sollecitazioni: $N = -222.62$ $T_z = 1256.61$ $M_y = -1011.76$ $T_y = -886.55$ $M_z = -973.87$ $M_x = 141.73$
 Tensioni: $\sigma_N = -1.92$ $\sigma_{m,d} = -182.97$ $\tau = 8.43$ $\sigma_{max} = -184.88$ (sfrut=0.05)
 Tensioni: $\sigma_N = -1.92$ $\sigma_{m,d} = -83.75$ $\tau = 32.79$ $\tau_{max} = 32.79$ (sfrut=0.02)
 Tensioni: $\sigma_N = -1.92$ $\sigma_{m,d} = -182.97$ $\tau = 8.43$ $\sigma_{ID,max} = 185.46$ (sfrut=0.05)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed = -222.62$ $M_y, Ed = -1011.76$ $M_z, Ed = -973.87$ $L = 1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 11.31$ Ncr, $y = 18806100.00$ $\lambda^*_y = 0.15$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 11.31$ Ncr, $z = 18806100.00$ $\lambda^*_z = 0.15$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.03 + 0.03 = 0.05$
 Verifica ZZ: $0.00 + 0.02 + 0.03 = 0.05$

Asta n. 205 (-27 -28) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X_l = 1.34$ - Classe 3
 Sollecitazioni: $N = -107.60$ $T_z = 129.24$ $M_y = -733.55$ $T_y = -45.24$ $M_z = -178.32$ $M_x = 14.50$
 Tensioni: $\sigma_N = -0.93$ $\sigma_{m,d} = -84.02$ $\tau = 0.86$ $\sigma_{max} = -84.95$ (sfrut=0.03)
 Tensioni: $\sigma_N = -0.93$ $\sigma_{m,d} = -15.34$ $\tau = 3.37$ $\tau_{max} = 3.37$ (sfrut=0.00)
 Tensioni: $\sigma_N = -0.93$ $\sigma_{m,d} = -84.02$ $\tau = 0.86$ $\sigma_{ID,max} = 84.96$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l = 0.00$ - Classe 2
 Sollecitazioni: $T_z = 383.21$

V,Ed=383.21 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3
 Sollecitazioni: N=-222.62 Tz=388.21 My=-1638.02 Ty=-338.38 Mz=-1427.16 Mx=141.73
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-282.44$ $\tau=8.43$ $\sigma_{max}=-284.36$ (sfrut=0.08)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-122.74$ $\tau=15.95$ $\tau_{max}=15.95$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-282.44$ $\tau=8.43$ $\sigma_{ID,max}=284.74$ (sfrut=0.08)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.62 My,Ed=-1638.02 Mz,Ed=-1427.16 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.04=0.08
 Verifica ZZ: 0.00+0.03+0.04=0.07

Asta n. 205 (-28 -29) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-128.36 Tz=-139.42 My=-738.03 Ty=-28.04 Mz=177.71 Mx=-29.13
 Tensioni: $\sigma_N=-1.11$ $\sigma_{m,d}=-84.38$ $\tau=1.73$ $\sigma_{max}=-85.49$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.11$ $\sigma_{m,d}=15.28$ $\tau=4.43$ $\tau_{max}=4.43$ (sfrut=0.00)
 Tensioni: $\sigma_N=-1.11$ $\sigma_{m,d}=-84.38$ $\tau=1.73$ $\sigma_{ID,max}=85.54$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 2
 Sollecitazioni: Tz=-339.27
 V,Ed=-339.27 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.00
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-222.62 Tz=-321.63 My=-1638.01 Ty=209.80 Mz=-1427.15 Mx=141.73
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-282.44$ $\tau=8.43$ $\sigma_{max}=-284.36$ (sfrut=0.08)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=122.74$ $\tau=14.66$ $\tau_{max}=14.66$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-282.44$ $\tau=8.43$ $\sigma_{ID,max}=284.73$ (sfrut=0.08)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.62 My,Ed=-1638.01 Mz,Ed=-1427.15 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.04=0.08
 Verifica ZZ: 0.00+0.03+0.04=0.07

Asta n. 205 (-29 -30) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-48.24 Tz=-489.27 My=-506.51 Ty=97.26 Mz=-142.73 Mx=44.08
 Tensioni: $\sigma_N=-0.42$ $\sigma_{m,d}=-59.82$ $\tau=2.62$ $\sigma_{max}=-60.24$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.42$ $\sigma_{m,d}=12.28$ $\tau=12.10$ $\tau_{max}=12.10$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.42$ $\sigma_{m,d}=-59.82$ $\tau=2.62$ $\sigma_{ID,max}=60.41$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 2
 Sollecitazioni: Tz=-903.20
 V,Ed=-903.20 Vc,Rd=113219.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-222.62 Tz=-1190.02 My=-1101.03 Ty=757.98 Mz=-1146.14 Mx=141.73
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-207.07$ $\tau=8.43$ $\sigma_{max}=-208.99$ (sfrut=0.06)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=98.57$ $\tau=31.50$ $\tau_{max}=31.50$ (sfrut=0.02)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-207.07$ $\tau=8.43$ $\sigma_{ID,max}=209.49$ (sfrut=0.06)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.62 My,Ed=-1101.03 Mz,Ed=-1146.14 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.31$ Ncr,y=18806100.00 $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr,z=18806100.00 $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.03+0.03=0.06
 Verifica ZZ: 0.00+0.02+0.03=0.05

Asta n. 205 (-30 -31) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.89 - Classe 3
 Sollecitazioni: N=-332.43 Tz=-1049.40 My=1303.21 Ty=-55.03 Mz=-42.33 Mx=-17.21

Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-123.98$ $\tau=1.02$ $\sigma_{max}=-126.85$ (sfrut=0.04)
 Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-3.64$ $\tau=21.36$ $\tau_{max}=21.36$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-123.98$ $\tau=1.02$ $\sigma_{ID,max}=126.86$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.89$ - Classe 2
 Sollecitazioni: $T_z=-1414.08$
 $V,Ed=-1414.08$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.89$ - Classe 3
 Sollecitazioni: $N=-222.62$ $T_z=-2163.92$ $M_y=2480.56$ $T_y=1306.16$ $M_z=1033.14$ $M_x=141.73$
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-323.77$ $\tau=8.43$ $\sigma_{max}=-325.69$ (sfrut=0.10)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-88.85$ $\tau=50.38$ $\tau_{max}=50.38$ (sfrut=0.03)
 Tensioni: $\sigma_N=-1.92$ $\sigma_{m,d}=-323.77$ $\tau=8.43$ $\sigma_{ID,max}=326.02$ (sfrut=0.10)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-222.62$ $M_y,Ed=2480.56$ $M_z,Ed=1033.14$ $L=0.89$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=7.52$ Ncr, $y=42486200.00$ $\lambda^*_y=0.10$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=7.52$ Ncr, $z=42486200.00$ $\lambda^*_z=0.10$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.06+0.03=0.09$
 Verifica ZZ: $0.00+0.05+0.03=0.08$

Asta n. 206 (-31 -32) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-99.59$ $T_z=1078.01$ $M_y=1310.73$ $T_y=-38.53$ $M_z=42.30$ $M_x=10.25$
 Tensioni: $\sigma_N=-0.86$ $\sigma_{m,d}=-124.67$ $\tau=0.61$ $\sigma_{max}=-125.53$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.86$ $\sigma_{m,d}=3.64$ $\tau=21.50$ $\tau_{max}=21.50$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.86$ $\sigma_{m,d}=-124.67$ $\tau=0.61$ $\sigma_{ID,max}=125.54$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=1326.80$
 $V,Ed=1326.80$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-101.12$ $T_z=2060.88$ $M_y=2211.34$ $T_y=-1276.96$ $M_z=1032.08$ $M_x=573.15$
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-298.87$ $\tau=34.08$ $\sigma_{max}=-299.74$ (sfrut=0.09)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=88.76$ $\tau=74.03$ $\tau_{max}=74.03$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-298.87$ $\tau=34.08$ $\sigma_{ID,max}=305.49$ (sfrut=0.09)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-101.12$ $M_y,Ed=2211.34$ $M_z,Ed=1032.08$ $L=0.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=3.78$ Ncr, $y=167888000.00$ $\lambda^*_y=0.05$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=3.78$ Ncr, $z=167888000.00$ $\lambda^*_z=0.05$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.06+0.03=0.08$
 Verifica ZZ: $0.00+0.05+0.03=0.07$

Asta n. 206 (-32 -33) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-37.56$ $T_z=768.53$ $M_y=851.56$ $T_y=34.57$ $M_z=-19.81$ $M_x=-21.09$
 Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=-80.29$ $\tau=1.25$ $\sigma_{max}=-80.62$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=1.70$ $\tau=16.15$ $\tau_{max}=16.15$ (sfrut=0.01)
 Tensioni: $\sigma_N=-0.32$ $\sigma_{m,d}=-80.29$ $\tau=1.25$ $\sigma_{ID,max}=80.65$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU $X_l=0.00$ - Classe 2
 Sollecitazioni: $T_z=868.36$
 $V,Ed=868.36$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=-101.12$ $T_z=1297.97$ $M_y=1299.34$ $T_y=-728.78$ $M_z=459.62$ $M_x=573.15$
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-162.08$ $\tau=34.08$ $\sigma_{max}=-162.95$ (sfrut=0.05)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=39.53$ $\tau=59.24$ $\tau_{max}=59.24$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=154.10$ $\tau=51.42$ $\sigma_{ID,max}=177.23$ (sfrut=0.05)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-101.12$ $M_y,Ed=1299.34$ $M_z,Ed=-516.53$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ Ncr, $y=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ Ncr, $z=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$

Verifica YY: $0.00+0.03+0.01=0.05$
 Verifica ZZ: $0.00+0.03+0.01=0.04$

Asta n. 206 (-33 -34) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=1.34 - Classe 3
 Sollecitazioni: $N=31.65$ $T_z=255.94$ $M_y=-505.67$ $T_y=13.81$ $M_z=36.36$ $M_x=-25.58$
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=49.95$ $\tau=1.52$ $\sigma_{max}=50.22$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=-3.13$ $\tau=6.48$ $\tau_{max}=6.48$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=49.95$ $\tau=1.52$ $\sigma_{ID,max}=50.29$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: $T_z=304.43$
 $V,Ed=304.43$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.00$
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3
 Sollecitazioni: $N=-101.12$ $T_z=271.02$ $M_y=-802.18$ $T_y=-180.60$ $M_z=-758.41$ $M_x=573.15$
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-143.80$ $\tau=34.08$ $\sigma_{max}=-144.67$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-65.23$ $\tau=39.33$ $\tau_{max}=39.33$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-143.80$ $\tau=34.08$ $\sigma_{ID,max}=156.25$ (sfrut=0.05)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-101.12$ $M_y,Ed=-802.18$ $M_z,Ed=-758.41$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ $N_{cr,y}=18806000.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ $N_{cr,z}=18806000.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.02=0.04$
 Verifica ZZ: $0.00+0.02+0.02=0.04$

Asta n. 206 (-34 -35) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=100.87$ $T_z=-12.72$ $M_y=-490.71$ $T_y=-6.96$ $M_z=27.72$ $M_x=-30.06$
 Tensioni: $\sigma_N=0.87$ $\sigma_{m,d}=47.77$ $\tau=1.79$ $\sigma_{max}=48.64$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.87$ $\sigma_{m,d}=2.38$ $\tau=2.03$ $\tau_{max}=2.03$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.87$ $\sigma_{m,d}=47.77$ $\tau=1.79$ $\sigma_{ID,max}=48.74$ (sfrut=0.01)
 - Verifica a taglio e torsione Dir. Y [4.2.25] - CC 3 SND Xl=1.22 - Classe 2
 Sollecitazioni: $T_y=-21.60$ $M_x=-23.71$
 $V,Ed=-21.60$ $V_c,Rd,Red=113137.00$ $V,Ed/V_c,Rd,Red=0.00$
 - Verifica a taglio e torsione Dir. Z [4.2.25] - CC 3 SND Xl=1.22 - Classe 2
 Sollecitazioni: $T_z=-446.55$ $M_x=-23.71$
 $V,Ed=-446.55$ $V_c,Rd,Red=113137.00$ $V,Ed/V_c,Rd,Red=0.00$
 - Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: $N=-101.12$ $T_z=-438.82$ $M_y=-802.18$ $T_y=367.58$ $M_z=-758.41$ $M_x=573.15$
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-143.80$ $\tau=34.08$ $\sigma_{max}=-144.67$ (sfrut=0.04)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=65.22$ $\tau=42.58$ $\tau_{max}=42.58$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.87$ $\sigma_{m,d}=-143.80$ $\tau=34.08$ $\sigma_{ID,max}=156.25$ (sfrut=0.05)
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-101.12$ $M_y,Ed=-802.18$ $M_z,Ed=-758.41$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.31$ $N_{cr,y}=18806100.00$ $\lambda^*_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.31$ $N_{cr,z}=18806100.00$ $\lambda^*_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.02=0.04$
 Verifica ZZ: $0.00+0.02+0.02=0.04$

Asta n. 206 (-35 -36) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.53 - Classe 3
 Sollecitazioni: $N=-250.67$ $T_z=-774.87$ $M_y=705.49$ $T_y=-40.42$ $M_z=-15.43$ $M_x=-28.19$
 Tensioni: $\sigma_N=-2.16$ $\sigma_{m,d}=-66.43$ $\tau=1.68$ $\sigma_{max}=-68.59$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.16$ $\sigma_{m,d}=-1.33$ $\tau=16.69$ $\tau_{max}=16.69$ (sfrut=0.01)
 Tensioni: $\sigma_N=-2.16$ $\sigma_{m,d}=-66.43$ $\tau=1.68$ $\sigma_{ID,max}=68.65$ (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.53 - Classe 2
 Sollecitazioni: $T_z=-886.59$
 $V,Ed=-886.59$ $V_c,Rd=113219.00$ $V,Ed/V_c,Rd=0.01$
 - Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.53 - Classe 3
 Sollecitazioni: $N=-7.01$ $T_z=-159.00$ $M_y=89.68$ $T_y=-1290.13$ $M_z=-313.39$ $M_x=-807.46$

Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = -37.14$ $\tau = 48.01$ $\sigma_{max} = -37.20$ (sfrut=0.01)
 Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = -7.71$ $\tau = 73.01$ $\tau_{max} = 73.01$ (sfrut=0.04)
 Tensioni: $\sigma_N = -0.06$ $\sigma_{m,d} = -8.26$ $\tau = 73.01$ $\sigma_{ID,max} = 126.73$ (sfrut=0.04)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N, Ed = -101.12$ $M_y, Ed = 605.97$ $M_z, Ed = -266.04$ $L = 0.53$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 4.50$ Ncr, $y = 118573000.00$ $\lambda^*_y = 0.06$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 4.50$ Ncr, $z = 118573000.00$ $\lambda^*_z = 0.06$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.01 = 0.02$
 Verifica ZZ: $0.00 + 0.01 + 0.01 = 0.02$

Asta n. 206 (-36 -37) - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND $X_1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 11.97$ $T_z = 261.89$ $M_y = 184.49$ $T_y = 39.90$ $M_z = -33.88$ $M_x = 9.94$
 Tensioni: $\sigma_N = 0.10$ $\sigma_{m,d} = 20.12$ $\tau = 0.59$ $\sigma_{max} = 20.22$ (sfrut=0.01)
 Tensioni: $\sigma_N = 0.10$ $\sigma_{m,d} = -2.91$ $\tau = 5.67$ $\tau_{max} = 5.67$ (sfrut=0.00)
 Tensioni: $\sigma_N = 0.10$ $\sigma_{m,d} = 20.12$ $\tau = 0.59$ $\sigma_{ID,max} = 20.25$ (sfrut=0.01)

- Verifica a taglio Dir. Y [4.2.16] - CC 28 SLU $X_1 = 0.81$
 Sollecitazioni: $T_y = -274.09$
 $V, Ed = -274.09$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.00$

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_1 = 0.81$
 Sollecitazioni: $T_z = 425.33$
 $V, Ed = 425.33$ $V_c, Rd = 113219.00$ $V, Ed/V_c, Rd = 0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU $X_1 = 0.00$ - Classe 3
 Sollecitazioni: $T_z = 520.75$ $M_y = 381.27$ $T_y = -274.09$ $M_z = 220.92$
 Tensioni: $\sigma_N = 0.00$ $\sigma_{m,d} = -55.49$ $\tau = 0.00$ $\sigma_{max} = -55.49$ (sfrut=0.02)
 Tensioni: $\sigma_N = 0.00$ $\sigma_{m,d} = 19.00$ $\tau = 10.10$ $\tau_{max} = 10.10$ (sfrut=0.01)
 Tensioni: $\sigma_N = 0.00$ $\sigma_{m,d} = -55.49$ $\tau = 0.00$ $\sigma_{ID,max} = 55.49$ (sfrut=0.02)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
 Sollecitazioni: $N, Ed = -11.97$ $M_y, Ed = 178.52$ $M_z, Ed = 33.88$ $L = 0.81$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 6.80$ Ncr, $y = 51935500.00$ $\lambda^*_y = 0.09$ Curva a: $\Phi_y = 0.00$ $\chi_y = 1.00$
 $\lambda_z = 6.80$ Ncr, $z = 51935500.00$ $\lambda^*_z = 0.09$ Curva a: $\Phi_z = 0.00$ $\chi_z = 1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.00 + 0.00 = 0.01$
 Verifica ZZ: $0.00 + 0.00 + 0.00 = 0.00$

Asta n. 302 (-4 -47) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1 = 0.00$ - Classe 3
 Sollecitazioni: $N = 80.74$ $T_z = 48.64$ $M_y = 43.24$ $T_y = -5.85$ $M_z = 8.77$
 Tensioni: $\sigma_N = 1.76$ $\sigma_{m,d} = 30.37$ $\tau = 0.00$ $\sigma_{max} = 32.12$ (sfrut=0.01)
 Tensioni: $\sigma_N = 1.76$ $\sigma_{m,d} = 5.05$ $\tau = 2.03$ $\tau_{max} = 2.03$ (sfrut=0.00)
 Tensioni: $\sigma_N = 1.76$ $\sigma_{m,d} = 30.37$ $\tau = 0.00$ $\sigma_{ID,max} = 32.12$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_1 = 0.00$ - Classe 1
 Sollecitazioni: $T_z = 225.02$
 $V, Ed = 225.02$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.00$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_1 = 0.00$ - Classe 1
 Sollecitazioni: $N = 115.65$ $T_z = 225.02$ $M_y = 221.93$
 $M_y, Ed = 221.93$ $M_y, V, c, Rd = 7590.24$
 $N, Ed = 115.65$ $N_c, Rd = 155524.00$ YY $n = N, Ed/N_c, Rd = 0.00$ $MN_y, c, Rd = 7590.24$ $M_y, Ed/MN_y, c, Rd = 0.03$

Asta n. 302 (-46 -4) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1 = 1.50$ - Classe 3
 Sollecitazioni: $N = -79.60$ $T_z = -50.63$ $M_y = 46.22$ $T_y = 13.50$ $M_z = 20.25$
 Tensioni: $\sigma_N = -1.73$ $\sigma_{m,d} = -40.28$ $\tau = 0.00$ $\sigma_{max} = -42.01$ (sfrut=0.01)
 Tensioni: $\sigma_N = -1.73$ $\sigma_{m,d} = 11.65$ $\tau = 2.11$ $\tau_{max} = 2.11$ (sfrut=0.00)
 Tensioni: $\sigma_N = -1.73$ $\sigma_{m,d} = -40.28$ $\tau = 0.00$ $\sigma_{ID,max} = 42.01$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_1 = 1.50$ - Classe 1
 Sollecitazioni: $T_z = -225.02$
 $V, Ed = -225.02$ $V_c, Rd = 53876.60$ $V, Ed/V_c, Rd = 0.00$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_1 = 1.50$ - Classe 1
 Sollecitazioni: $N = -115.65$ $T_z = -225.02$ $M_y = 221.93$

My,Ed=221.93 My,V,c,Rd=7590.24
 N,Ed=-115.65 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MMy,c,Rd=7590.24 My,Ed/MMy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-115.65 My,Ed=221.93 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.03=0.03$
 Verifica ZZ: $0.00=0.00$

Asta n. 303 (-6 -48) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20
 Tensioni: $\sigma_N=2.50 \sigma_{m,d}=45.67 \tau=0.00 \sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50 \sigma_{m,d}=7.59 \tau=2.89 \tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50 \sigma_{m,d}=45.67 \tau=0.00 \sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=414.83
 V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 Tz=414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MMy,c,Rd=7590.24 My,Ed/MMy,c,Rd=0.05

Asta n. 303 (-49 -6) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46
 Tensioni: $\sigma_N=-2.46 \sigma_{m,d}=-60.59 \tau=0.00 \sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46 \sigma_{m,d}=17.52 \tau=3.02 \tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46 \sigma_{m,d}=-60.59 \tau=0.00 \sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-414.83
 V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-170.32 Tz=-414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MMy,c,Rd=7590.24 My,Ed/MMy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 304 (-7 -96) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20
 Tensioni: $\sigma_N=2.50 \sigma_{m,d}=45.67 \tau=0.00 \sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50 \sigma_{m,d}=7.59 \tau=2.89 \tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50 \sigma_{m,d}=45.67 \tau=0.00 \sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=414.83
 V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 Tz=414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MMy,c,Rd=7590.24 My,Ed/MMy,c,Rd=0.05

Asta n. 304 (-95 -7) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46

Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=7590.24$ $M_y,Ed/MN_y,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 305 (-8 -66) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=170.32$ $N_c,Rd=155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=7590.24$ $M_y,Ed/MN_y,c,Rd=0.05$

Asta n. 305 (-67 -8) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=7590.24$ $M_y,Ed/MN_y,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 306 (-9 -69) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=170.32 T_z=414.83 M_y=417.44
M_y,Ed=417.44 M_y,V,c,Rd=7590.24
N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MN_y,c,Rd=7590.24 M_y,Ed/MN_y,c,Rd=0.05

Asta n. 306 (-68 -9) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-113.29 T_z=-72.44 M_y=69.51 T_y=20.31 M_z=30.46
Tensioni: σ_N=-2.46 σ_{m,d}=-60.59 τ=0.00 σ_{max}=-63.05 (sfrut=0.02)
Tensioni: σ_N=-2.46 σ_{m,d}=17.52 τ=3.02 τ_{max}=3.02 (sfrut=0.00)
Tensioni: σ_N=-2.46 σ_{m,d}=-60.59 τ=0.00 σ_{ID,max}=63.05 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_z=-414.83
V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-170.32 T_z=-414.83 M_y=417.44
M_y,Ed=417.44 M_y,V,c,Rd=7590.24
N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MN_y,c,Rd=7590.24 M_y,Ed/MN_y,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 M_y,Ed=417.44 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.71 Ncr,y=1241570.00 λ_{*y}=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=38.58 Ncr,z=640515.00 λ_{*z}=0.50 Curva a: Φ_z=0.66 χ_z=0.92
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

Asta n. 307 (-11 -70) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=115.01 T_z=69.45 M_y=65.03 T_y=-8.80 M_z=13.20
Tensioni: σ_N=2.50 σ_{m,d}=45.67 τ=0.00 σ_{max}=48.18 (sfrut=0.01)
Tensioni: σ_N=2.50 σ_{m,d}=7.59 τ=2.89 τ_{max}=2.89 (sfrut=0.00)
Tensioni: σ_N=2.50 σ_{m,d}=45.67 τ=0.00 σ_{ID,max}=48.18 (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=414.83
V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=170.32 T_z=414.83 M_y=417.44
M_y,Ed=417.44 M_y,V,c,Rd=7590.24
N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MN_y,c,Rd=7590.24 M_y,Ed/MN_y,c,Rd=0.05

Asta n. 307 (-71 -11) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-113.29 T_z=-72.44 M_y=69.51 T_y=20.31 M_z=30.46
Tensioni: σ_N=-2.46 σ_{m,d}=-60.59 τ=0.00 σ_{max}=-63.05 (sfrut=0.02)
Tensioni: σ_N=-2.46 σ_{m,d}=17.52 τ=3.02 τ_{max}=3.02 (sfrut=0.00)
Tensioni: σ_N=-2.46 σ_{m,d}=-60.59 τ=0.00 σ_{ID,max}=63.05 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_z=-414.83
V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-170.32 T_z=-414.83 M_y=417.44
M_y,Ed=417.44 M_y,V,c,Rd=7590.24
N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MN_y,c,Rd=7590.24 M_y,Ed/MN_y,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 M_y,Ed=417.44 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.71 Ncr,y=1241570.00 λ_{*y}=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=38.58 Ncr,z=640515.00 λ_{*z}=0.50 Curva a: Φ_z=0.66 χ_z=0.92
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

Asta n. 308 (-12 -72) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.01 T_z=69.45 M_y=65.03 T_y=-8.80 M_z=13.20
 Tensioni: σ_N=2.50 σ_{m,d}=45.67 τ=0.00 σ_{max}=48.18 (sfrut=0.01)
 Tensioni: σ_N=2.50 σ_{m,d}=7.59 τ=2.89 τ_{max}=2.89 (sfrut=0.00)
 Tensioni: σ_N=2.50 σ_{m,d}=45.67 τ=0.00 σ_{ID,max}=48.18 (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=414.83
 V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 T_z=414.83 M_y=417.44
 M_y,Ed=417.44 M_y,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 M_{Ny,c},Rd=7590.24 M_y,Ed/M_{Ny,c},Rd=0.05
- Asta n. 308 (-73 -12) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3
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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 T_z=-72.44 M_y=69.51 T_y=20.31 M_z=30.46
 Tensioni: σ_N=-2.46 σ_{m,d}=-60.59 τ=0.00 σ_{max}=-63.05 (sfrut=0.02)
 Tensioni: σ_N=-2.46 σ_{m,d}=17.52 τ=3.02 τ_{max}=3.02 (sfrut=0.00)
 Tensioni: σ_N=-2.46 σ_{m,d}=-60.59 τ=0.00 σ_{ID,max}=63.05 (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-414.83
 V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-170.32 T_z=-414.83 M_y=417.44
 M_y,Ed=417.44 M_y,V,c,Rd=7590.24
 N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 M_{Ny,c},Rd=7590.24 M_y,Ed/M_{Ny,c},Rd=0.05
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 M_y,Ed=417.44 L=1.50
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=27.71 Ncr,y=1241570.00 λ_y^{*}=0.36 Curva a: Φ_y=0.58 χ_y=0.96
 λ_z=38.58 Ncr,z=640515.00 λ_z^{*}=0.50 Curva a: Φ_z=0.66 χ_z=0.92
 K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00
- Asta n. 309 (-13 -74) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3
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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.01 T_z=69.45 M_y=65.03 T_y=-8.80 M_z=13.20
 Tensioni: σ_N=2.50 σ_{m,d}=45.67 τ=0.00 σ_{max}=48.18 (sfrut=0.01)
 Tensioni: σ_N=2.50 σ_{m,d}=7.59 τ=2.89 τ_{max}=2.89 (sfrut=0.00)
 Tensioni: σ_N=2.50 σ_{m,d}=45.67 τ=0.00 σ_{ID,max}=48.18 (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=414.83
 V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 T_z=414.83 M_y=417.44
 M_y,Ed=417.44 M_y,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 M_{Ny,c},Rd=7590.24 M_y,Ed/M_{Ny,c},Rd=0.05
- Asta n. 309 (-75 -13) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3
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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 T_z=-72.44 M_y=69.51 T_y=20.31 M_z=30.46
 Tensioni: σ_N=-2.46 σ_{m,d}=-60.59 τ=0.00 σ_{max}=-63.05 (sfrut=0.02)
 Tensioni: σ_N=-2.46 σ_{m,d}=17.52 τ=3.02 τ_{max}=3.02 (sfrut=0.00)
 Tensioni: σ_N=-2.46 σ_{m,d}=-60.59 τ=0.00 σ_{ID,max}=63.05 (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-414.83
 V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-170.32 T_z=-414.83 M_y=417.44
 M_y,Ed=417.44 M_y,V,c,Rd=7590.24
 N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 M_{Ny,c},Rd=7590.24 M_y,Ed/M_{Ny,c},Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 310 (-14 -90) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=414.83
 V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 Tz=414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 310 (-91 -14) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-414.83
 V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-170.32 Tz=-414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 311 (-15 -92) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=414.83
 V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 Tz=414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 311 (-93 -15) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: $T_z=-414.83$
 $V, Ed=-414.83$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y, Ed=417.44$ $M_y, V, c, Rd=7590.24$
 $N, Ed=-170.32$ $N_c, Rd=-155524.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=7590.24$ $M_y, Ed/MNy, c, Rd=0.05$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N, Ed=-170.32$ $M_y, Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
Verifica YY: $0.00+0.05=0.05$
Verifica ZZ: $0.00=0.00$

Asta n. 312 (-16 -98) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: $T_z=414.83$
 $V, Ed=414.83$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y, Ed=417.44$ $M_y, V, c, Rd=7590.24$
 $N, Ed=170.32$ $N_c, Rd=155524.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=7590.24$ $M_y, Ed/MNy, c, Rd=0.05$

Asta n. 312 (-94 -16) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: $T_z=-414.83$
 $V, Ed=-414.83$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y, Ed=417.44$ $M_y, V, c, Rd=7590.24$
 $N, Ed=-170.32$ $N_c, Rd=-155524.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=7590.24$ $M_y, Ed/MNy, c, Rd=0.05$
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N, Ed=-170.32$ $M_y, Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
Verifica YY: $0.00+0.05=0.05$
Verifica ZZ: $0.00=0.00$

Asta n. 313 (-17 -97) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: $T_z=414.83$
 $V, Ed=414.83$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$

My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 313 (-42 -17) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46

Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)

Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)

Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: Tz=-414.83

V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-170.32 Tz=-414.83 My=417.44

My,Ed=417.44 My,V,c,Rd=7590.24

N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

Asta n. 314 (-18 -43) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20

Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)

Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)

Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: Tz=414.83

V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=170.32 Tz=414.83 My=417.44

My,Ed=417.44 My,V,c,Rd=7590.24

N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 314 (-44 -18) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46

Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)

Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)

Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: Tz=-414.83

V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-170.32 Tz=-414.83 My=417.44

My,Ed=417.44 My,V,c,Rd=7590.24

N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95

$\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

Asta n. 315 (-19 -45) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20

Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=170.32$ $N_c,Rd=155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

Asta n. 315 (-58 -19) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 316 (-20 -63) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=80.74$ $T_z=48.64$ $M_y=43.24$ $T_y=-5.85$ $M_z=8.77$
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.37$ $\tau=0.00$ $\sigma_{max}=32.12$ (sfrut=0.01)
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=5.05$ $\tau=2.03$ $\tau_{max}=2.03$ (sfrut=0.00)
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.37$ $\tau=0.00$ $\sigma_{ID,max}=32.12$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=225.02$
 $V,Ed=225.02$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.00$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=115.65$ $T_z=225.02$ $M_y=221.93$
 $M_y,Ed=221.93$ $M_y,V,c,Rd=7590.24$
 $N,Ed=115.65$ $N_c,Rd=155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.03$

Asta n. 316 (-65 -20) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=-79.60$ $T_z=-50.63$ $M_y=46.22$ $T_y=13.50$ $M_z=20.25$
 Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=-40.28$ $\tau=0.00$ $\sigma_{max}=-42.01$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=11.65$ $\tau=2.11$ $\tau_{max}=2.11$ (sfrut=0.00)
 Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=-40.28$ $\tau=0.00$ $\sigma_{ID,max}=42.01$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-225.02$
 $V,Ed=-225.02$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.00$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $N=-115.65$ $T_z=-225.02$ $M_y=221.93$
 $M_y,Ed=221.93$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-115.65$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.03$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-115.65$ $M_y,Ed=221.93$ $L=1.50$
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.03=0.03
 Verifica ZZ: 0.00=0.00

Asta n. 317 (-21 -51) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=80.74 Tz=48.64 My=43.24 Ty=-5.85 Mz=8.77
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.37$ $\tau=0.00$ $\sigma_{max}=32.12$ (sfrut=0.01)
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=5.05$ $\tau=2.03$ $\tau_{max}=2.03$ (sfrut=0.00)
 Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.37$ $\tau=0.00$ $\sigma_{ID,max}=32.12$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=225.02
 V,Ed=225.02 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=115.65 Tz=225.02 My=221.93
 My,Ed=221.93 My,V,c,Rd=7590.24
 N,Ed=115.65 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

Asta n. 317 (-50 -21) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-79.60 Tz=-50.63 My=46.22 Ty=13.50 Mz=20.25
 Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=-40.28$ $\tau=0.00$ $\sigma_{max}=-42.01$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=11.65$ $\tau=2.11$ $\tau_{max}=2.11$ (sfrut=0.00)
 Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=-40.28$ $\tau=0.00$ $\sigma_{ID,max}=42.01$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-225.02
 V,Ed=-225.02 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-115.65 Tz=-225.02 My=221.93
 My,Ed=221.93 My,V,c,Rd=7590.24
 N,Ed=-115.65 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-115.65 My,Ed=221.93 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.03=0.03
 Verifica ZZ: 0.00=0.00

Asta n. 318 (-22 -53) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=414.83
 V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 Tz=414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 318 (-52 -22) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-414.83

V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-170.32 Tz=-414.83 My=417.44
My,Ed=417.44 My,V,c,Rd=7590.24
N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

Asta n. 319 (-23 -55) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20
Tensioni: $\sigma_N=2.50 \sigma_{m,d}=45.67 \tau=0.00 \sigma_{max}=48.18$ (sfrut=0.01)
Tensioni: $\sigma_N=2.50 \sigma_{m,d}=7.59 \tau=2.89 \tau_{max}=2.89$ (sfrut=0.00)
Tensioni: $\sigma_N=2.50 \sigma_{m,d}=45.67 \tau=0.00 \sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: Tz=414.83
V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=170.32 Tz=414.83 My=417.44
My,Ed=417.44 My,V,c,Rd=7590.24
N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 319 (-54 -23) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46
Tensioni: $\sigma_N=-2.46 \sigma_{m,d}=-60.59 \tau=0.00 \sigma_{max}=-63.05$ (sfrut=0.02)
Tensioni: $\sigma_N=-2.46 \sigma_{m,d}=17.52 \tau=3.02 \tau_{max}=3.02$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.46 \sigma_{m,d}=-60.59 \tau=0.00 \sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: Tz=-414.83
V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-170.32 Tz=-414.83 My=417.44
My,Ed=417.44 My,V,c,Rd=7590.24
N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58 \chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66 \chi_z=0.92$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

Asta n. 320 (-24 -57) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20
Tensioni: $\sigma_N=2.50 \sigma_{m,d}=45.67 \tau=0.00 \sigma_{max}=48.18$ (sfrut=0.01)
Tensioni: $\sigma_N=2.50 \sigma_{m,d}=7.59 \tau=2.89 \tau_{max}=2.89$ (sfrut=0.00)
Tensioni: $\sigma_N=2.50 \sigma_{m,d}=45.67 \tau=0.00 \sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: Tz=414.83
V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=170.32 Tz=414.83 My=417.44
My,Ed=417.44 My,V,c,Rd=7590.24
N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 320 (-56 -24) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 322 (-25 -41) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=170.32$ $N_c,Rd=155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

Asta n. 322 (-64 -25) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 323 (-26 -77) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: $T_z=414.83$
 $V, Ed=414.83$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y, Ed=417.44$ $M_y, V, c, Rd=7590.24$
 $N, Ed=170.32$ $N_c, Rd=155524.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=7590.24$ $M_y, Ed/MNy, c, Rd=0.05$

Asta n. 323 (-76 -26) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
Sollecitazioni: $T_z=-414.83$
 $V, Ed=-414.83$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y, Ed=417.44$ $M_y, V, c, Rd=7590.24$
 $N, Ed=-170.32$ $N_c, Rd=-155524.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=7590.24$ $M_y, Ed/MNy, c, Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N, Ed=-170.32$ $M_y, Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr, y=1241570.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr, z=640515.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
Verifica YY: $0.00+0.05=0.05$
Verifica ZZ: $0.00=0.00$

Asta n. 324 (-27 -79) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: $T_z=414.83$
 $V, Ed=414.83$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1
Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y, Ed=417.44$ $M_y, V, c, Rd=7590.24$
 $N, Ed=170.32$ $N_c, Rd=155524.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=7590.24$ $M_y, Ed/MNy, c, Rd=0.05$

Asta n. 324 (-78 -27) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
Sollecitazioni: $T_z=-414.83$
 $V, Ed=-414.83$ $V_c, Rd=53876.60$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y, Ed=417.44$ $M_y, V, c, Rd=7590.24$
 $N, Ed=-170.32$ $N_c, Rd=-155524.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=7590.24$ $M_y, Ed/MNy, c, Rd=0.05$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N, Ed=-170.32$ $M_y, Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr, y=1241570.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr, z=640515.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$

Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 325 (-28 -81) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=170.32$ $Nc,Rd=155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

Asta n. 325 (-80 -28) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $Nc,Rd=-155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 $\alpha_y, \alpha_z, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 326 (-29 -83) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=170.32$ $Nc,Rd=155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

Asta n. 326 (-82 -29) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $Nc,Rd=-155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 327 (-30 -85) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3

Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1

Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1

Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=170.32$ $Nc,Rd=155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

Asta n. 327 (-84 -30) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3

Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1

Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1

Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $Nc,Rd=-155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ $Ncr,y=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $Ncr,z=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 329 (-32 -86) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3

Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1

Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $Vc,Rd=53876.60$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1

Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=170.32$ $Nc,Rd=155524.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=7590.24$ $M_y,Ed/MNy,c,Rd=0.05$

Asta n. 329 (-87 -32) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3

Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=7590.24$ $M_y,Ed/MN_y,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.57 , 0.00 , 0.95
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 330 (-33 -89) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=414.83$
 $V,Ed=414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $N=170.32$ $T_z=414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=170.32$ $N_c,Rd=155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=7590.24$ $M_y,Ed/MN_y,c,Rd=0.05$

Asta n. 330 (-88 -33) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=1.50$ - Classe 3
 Sollecitazioni: $N=-113.29$ $T_z=-72.44$ $M_y=69.51$ $T_y=20.31$ $M_z=30.46$
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $T_z=-414.83$
 $V,Ed=-414.83$ $V_c,Rd=53876.60$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X_l=1.50$ - Classe 1
 Sollecitazioni: $N=-170.32$ $T_z=-414.83$ $M_y=417.44$
 $M_y,Ed=417.44$ $M_y,V,c,Rd=7590.24$
 $N,Ed=-170.32$ $N_c,Rd=-155524.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MN_y,c,Rd=7590.24$ $M_y,Ed/MN_y,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N,Ed=-170.32$ $M_y,Ed=417.44$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.71$ $N_{cr,y}=1241570.00$ $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ $N_{cr,z}=640515.00$ $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.57 , 0.00 , 0.95
 Verifica YY: $0.00+0.05=0.05$
 Verifica ZZ: $0.00=0.00$

Asta n. 331 (-34 -61) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_l=0.00$ - Classe 3
 Sollecitazioni: $N=115.01$ $T_z=69.45$ $M_y=65.03$ $T_y=-8.80$ $M_z=13.20$
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X_l=0.00$ - Classe 1
 Sollecitazioni: $T_z=414.83$

V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 Tz=414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 331 (-62 -34) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-414.83
 V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-170.32 Tz=-414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 332 (-35 -102) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=115.01 Tz=69.45 My=65.03 Ty=-8.80 Mz=13.20
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{max}=48.18$ (sfrut=0.01)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=7.59$ $\tau=2.89$ $\tau_{max}=2.89$ (sfrut=0.00)
 Tensioni: $\sigma_N=2.50$ $\sigma_{m,d}=45.67$ $\tau=0.00$ $\sigma_{ID,max}=48.18$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: Tz=414.83
 V,Ed=414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=170.32 Tz=414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=170.32 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05

Asta n. 332 (-101 -35) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=-113.29 Tz=-72.44 My=69.51 Ty=20.31 Mz=30.46
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{max}=-63.05$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=17.52$ $\tau=3.02$ $\tau_{max}=3.02$ (sfrut=0.00)
 Tensioni: $\sigma_N=-2.46$ $\sigma_{m,d}=-60.59$ $\tau=0.00$ $\sigma_{ID,max}=63.05$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: Tz=-414.83
 V,Ed=-414.83 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
 Sollecitazioni: N=-170.32 Tz=-414.83 My=417.44
 My,Ed=417.44 My,V,c,Rd=7590.24
 N,Ed=-170.32 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.05
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

Asta n. 333 (-37 -103) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=80.74 Tz=48.64 My=43.24 Ty=-5.85 Mz=8.77
Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.37$ $\tau=0.00$ $\sigma_{max}=32.12$ (sfrut=0.01)
Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=5.05$ $\tau=2.03$ $\tau_{max}=2.03$ (sfrut=0.00)
Tensioni: $\sigma_N=1.76$ $\sigma_{m,d}=30.37$ $\tau=0.00$ $\sigma_{ID,max}=32.12$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: Tz=225.02
V,Ed=225.02 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=115.65 Tz=225.02 My=221.93
My,Ed=221.93 My,V,C,Rd=7590.24
N,Ed=115.65 Nc,Rd=155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03

Asta n. 333 (-104 -37) - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-79.60 Tz=-50.63 My=46.22 Ty=13.50 Mz=20.25
Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=-40.28$ $\tau=0.00$ $\sigma_{max}=-42.01$ (sfrut=0.01)
Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=11.65$ $\tau=2.11$ $\tau_{max}=2.11$ (sfrut=0.00)
Tensioni: $\sigma_N=-1.73$ $\sigma_{m,d}=-40.28$ $\tau=0.00$ $\sigma_{ID,max}=42.01$ (sfrut=0.01)
 - Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: Tz=-225.02
V,Ed=-225.02 Vc,Rd=53876.60 V,Ed/Vc,Rd=0.00
 - Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-115.65 Tz=-225.02 My=221.93
My,Ed=221.93 My,V,C,Rd=7590.24
N,Ed=-115.65 Nc,Rd=-155524.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=7590.24 My,Ed/MNy,c,Rd=0.03
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-115.65 My,Ed=221.93 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.71$ Ncr,y=1241570.00 $\lambda^*_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=38.58$ Ncr,z=640515.00 $\lambda^*_z=0.50$ Curva a: $\Phi_z=0.66$ $\chi_z=0.92$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

Membratura

Asta 201 Nodi -4 -5 -6 -7 -8 -9 -10 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: N,Ed=-101.12 My,Ed=2211.34 Mz,Ed=1032.09 L=5.81
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=49.01$ Ncr,y=1000880.00 $\lambda^*_y=0.64$ Curva a: $\Phi_y=0.75$ $\chi_y=0.87$
 $\lambda_z=49.01$ Ncr,z=1000880.00 $\lambda^*_z=0.64$ Curva a: $\Phi_z=0.75$ $\chi_z=0.87$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.06+0.03=0.08
Verifica ZZ: 0.00+0.05+0.03=0.07
 - Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.01$ (L/40790)
 - Verifica freccia massima carichi totali - CC 30
 $f_{z,G}=0.03$ (L/20125)

Membratura

Asta 202 Nodi -10 -11 -12 -13 -14 -15 203 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: N,Ed=-222.63 My,Ed=2620.16 Mz,Ed=1428.98 L=7.10
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=59.90$ Ncr,y=670055.00 $\lambda^*_y=0.78$ Curva a: $\Phi_y=0.87$ $\chi_y=0.80$
 $\lambda_z=59.90$ Ncr,z=670055.00 $\lambda^*_z=0.78$ Curva a: $\Phi_z=0.87$ $\chi_z=0.80$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.07+0.04=0.11
Verifica ZZ: 0.00+0.05+0.04=0.09
 - Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.06$ (L/12484)

- Verifica freccia massima carichi totali - CC 30
 $f_{z,l}=0.12$ (L/5920)

Membratura

Asta 203 Nodi 203 -16 -17 -18 -19 -20 204 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=2401.58 Mz,Ed=1428.54 L=6.05
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=51.07$ Ncr,y=921780.00 $\lambda^*_y=0.67$ Curva a: $\Phi_y=0.77$ $\chi_y=0.86$
 $\lambda_z=51.07$ Ncr,z=921780.00 $\lambda^*_z=0.67$ Curva a: $\Phi_z=0.77$ $\chi_z=0.86$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.06+0.04=0.10
 Verifica ZZ: 0.00+0.05+0.04=0.09

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,l}=0.02$ (L/30832)

- Verifica freccia massima carichi totali - CC 30
 $f_{z,l}=0.04$ (L/14608)

Membratura

Asta 204 Nodi 204 -21 -22 -23 -24 -25 205 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-123.05 My,Ed=2401.57 Mz,Ed=1428.53 L=6.05
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=51.07$ Ncr,y=921780.00 $\lambda^*_y=0.67$ Curva a: $\Phi_y=0.77$ $\chi_y=0.86$
 $\lambda_z=51.07$ Ncr,z=921780.00 $\lambda^*_z=0.67$ Curva a: $\Phi_z=0.77$ $\chi_z=0.86$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.06+0.04=0.10
 Verifica ZZ: 0.00+0.05+0.04=0.09

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,l}=0.02$ (L/30832)

- Verifica freccia massima carichi totali - CC 30
 $f_{z,l}=0.04$ (L/14608)

Membratura

Asta 205 Nodi 205 -26 -27 -28 -29 -30 -31 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-222.62 My,Ed=2620.14 Mz,Ed=1428.97 L=7.10
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=59.90$ Ncr,y=670055.00 $\lambda^*_y=0.78$ Curva a: $\Phi_y=0.87$ $\chi_y=0.80$
 $\lambda_z=59.90$ Ncr,z=670055.00 $\lambda^*_z=0.78$ Curva a: $\Phi_z=0.87$ $\chi_z=0.80$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.07+0.04=0.11
 Verifica ZZ: 0.00+0.05+0.04=0.09

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,l}=0.06$ (L/12479)

- Verifica freccia massima carichi totali - CC 30
 $f_{z,l}=0.12$ (L/5919)

Membratura

Asta 206 Nodi -31 -32 -33 -34 -35 -36 -37 - Sez. 2 (TRV PRINC SHS300x300x10) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-101.12 My,Ed=2211.34 Mz,Ed=1032.08 L=5.81
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=49.01$ Ncr,y=1000880.00 $\lambda^*_y=0.64$ Curva a: $\Phi_y=0.75$ $\chi_y=0.87$
 $\lambda_z=49.01$ Ncr,z=1000880.00 $\lambda^*_z=0.64$ Curva a: $\Phi_z=0.75$ $\chi_z=0.87$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.06+0.03=0.08
 Verifica ZZ: 0.00+0.05+0.03=0.07

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,g}=0.01$ (L/40790)

- Verifica freccia massima carichi totali - CC 30
 $f_{z,g}=0.03$ (L/20125)

Membratura

Asta 302 Nodi -47 -4 -46 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-115.65 My,Ed=221.93 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.44$ (L/676) $f_{z,G}=0.04$ (L/8252)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.43$ (L/690) $f_{z,G}=0.03$ (L/10987)

Membratura

Asta 303 Nodi -48 -6 -49 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.50$ (L/597) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.49$ (L/614) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 304 Nodi -96 -7 -95 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.56$ (L/538) $f_{z,G}=0.07$ (L/4128)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.54$ (L/551) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 305 Nodi -66 -8 -67 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.61$ (L/489) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.60$ (L/500) $f_{z,G}=0.06$ (L/5111)

Membratura

Asta 306 Nodi -69 -9 -68 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

$\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.67$ (L/448) $f_{z,G}=0.07$ (L/4128)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.65$ (L/458) $f_{z,G}=0.06$ (L/5108)

Membratura

Asta 307 Nodi -70 -11 -71 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.70$ (L/430) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.68$ (L/439) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 308 Nodi -72 -12 -73 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.71$ (L/422) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.70$ (L/431) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 309 Nodi -74 -13 -75 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.72$ (L/414) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.71$ (L/422) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 310 Nodi -90 -14 -91 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.74$ (L/406) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.72$ (L/414) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 311 Nodi -92 -15 -93 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=55.42$ Ncr,y=310393.00 $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$

$\lambda_z=77.16$ Ncr,z=160129.00 $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.75$ (L/399) $f_{z,G}=0.07$ (L/4128)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.74$ (L/407) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 312 Nodi -98 -16 -94 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=55.42$ Ncr,y=310393.00 $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$

$\lambda_z=77.16$ Ncr,z=160129.00 $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.76$ (L/396) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.74$ (L/404) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 313 Nodi -97 -17 -42 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=55.42$ Ncr,y=310393.00 $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$

$\lambda_z=77.16$ Ncr,z=160129.00 $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.75$ (L/401) $f_{z,G}=0.07$ (L/4128)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.73$ (L/409) $f_{z,G}=0.06$ (L/5111)

Membratura

Asta 314 Nodi -43 -18 -44 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=55.42$ Ncr,y=310393.00 $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$

$\lambda_z=77.16$ Ncr,z=160129.00 $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.74$ (L/406) $f_{z,G}=0.07$ (L/4128)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.72$ (L/414) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 315 Nodi -45 -19 -58 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.73$ (L/411) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.72$ (L/419) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 316 Nodi -63 -20 -65 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-115.65 My,Ed=221.93 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.68$ (L/438) $f_{z,G}=0.04$ (L/8252)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.67$ (L/444) $f_{z,G}=0.03$ (L/10984)

Membratura

Asta 317 Nodi -51 -21 -50 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-115.65 My,Ed=221.93 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.68$ (L/438) $f_{z,G}=0.04$ (L/8252)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.67$ (L/444) $f_{z,G}=0.03$ (L/10984)

Membratura

Asta 318 Nodi -53 -22 -52 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.05=0.05
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.73$ (L/411) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.72$ (L/419) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 319 Nodi -55 -23 -54 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.74$ (L/406) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.72$ (L/414) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 320 Nodi -57 -24 -56 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.75$ (L/401) $f_{z,G}=0.07$ (L/4128)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.73$ (L/409) $f_{z,G}=0.06$ (L/5111)

Membratura

Asta 322 Nodi -41 -25 -64 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.76$ (L/396) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.74$ (L/404) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 323 Nodi -77 -26 -76 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.75$ (L/399) $f_{z,G}=0.07$ (L/4128)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.74$ (L/407) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 324 Nodi -79 -27 -78 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.74$ (L/406) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.72$ (L/414) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 325 Nodi -81 -28 -80 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.72$ (L/414) $f_{z,G}=0.07$ (L/4128)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.71$ (L/422) $f_{z,G}=0.06$ (L/5108)

Membratura

Asta 326 Nodi -83 -29 -82 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.71$ (L/422) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.70$ (L/431) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 327 Nodi -85 -30 -84 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.70$ (L/430) $f_{z,G}=0.07$ (L/4127)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.68$ (L/439) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 329 Nodi -86 -32 -87 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=55.42$ Ncr, $y=310393.00$ $\lambda^*_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr, $z=160129.00$ $\lambda^*_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.05=0.05

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.67$ (L/448) $f_{z,G}=0.07$ (L/4128)
- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.65$ (L/458) $f_{z,G}=0.06$ (L/5108)

Membratura

Asta 330 Nodi -89 -33 -88 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.61$ (L/489) $f_{z,G}=0.07$ (L/4127)
- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.60$ (L/500) $f_{z,G}=0.06$ (L/5111)

Membratura

Asta 331 Nodi -61 -34 -62 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.56$ (L/538) $f_{z,G}=0.07$ (L/4127)
- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.54$ (L/551) $f_{z,G}=0.06$ (L/5110)

Membratura

Asta 332 Nodi -102 -35 -101 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-170.32 My,Ed=417.44 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.05=0.05
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.50$ (L/597) $f_{z,G}=0.07$ (L/4127)
- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.49$ (L/614) $f_{z,G}=0.06$ (L/5109)

Membratura

Asta 333 Nodi -103 -37 -104 - Sez. 3 (TRV SEC RHS150x100x10) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-115.65 My,Ed=221.93 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=55.42$ Ncr,y=310393.00 $\lambda'_y=0.73$ Curva a: $\Phi_y=0.82$ $\chi_y=0.84$
 $\lambda_z=77.16$ Ncr,z=160129.00 $\lambda'_z=1.01$ Curva a: $\Phi_z=1.09$ $\chi_z=0.66$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: 0.00+0.03=0.03
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,L}=0.44$ (L/676) $f_{z,G}=0.04$ (L/8253)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,L}=0.43$ (L/690) $f_{z,G}=0.03$ (L/10989)

6.0 VALUTAZIONE DEI RISULTATI E GIUDIZIONE MOTIVATO SULLA LORO ACCETTABILITA'

Il programma di calcolo utilizzato Modest è idoneo a riprodurre nel modello matematico il comportamento della struttura e gli elementi finiti disponibili e utilizzati sono rappresentativi della realtà costruttiva. Le funzioni di controllo disponibili, innanzitutto quelle grafiche, consentono di verificare la riproduzione della realtà costruttiva ed accertare la corrispondenza del modello con la geometria strutturale e con le condizioni di carico ipotizzate. In ogni caso sono stati effettuati alcuni controlli dimensionali con gli strumenti software a disposizione dell'utente. Tutte le proprietà di rilevanza strutturale (materiali, sezioni, carichi, sconnessioni, etc.) sono state controllate attraverso le funzioni di indagine specificatamente previste.

Sono state sfruttate le funzioni di autodiagnostica presenti nel software che hanno accertato che non sussistono difetti formali di impostazione.

È stato accertato che le risultanti delle azioni verticali sono in equilibrio con i carichi applicati.

Sono state controllate le azioni taglianti di piano ed accertata la loro congruenza con quella ricavabile da semplici ed agevoli elaborazioni. Le sollecitazioni prodotte da alcune combinazioni di carico di prova hanno prodotto valori prossimi a quelli ricavabili adottando consolidate formulazioni ricavate della Scienza delle Costruzioni. Anche le deformazioni risultano prossime ai valori attesi. Il dimensionamento e le verifiche di sicurezza hanno determinato risultati che sono in linea con casi di comprovata validità, confortati anche dalla propria esperienza.

7.0 INFORMAZIONI INTEGRATIVE SULL'USO DEI CODICI DI CALCOLO

Codice di calcolo adottato, solutore e affidabilità dei risultati

Titolo del codice di calcolo: Modest;

Autore, produttore e distributore: Tecnisoft s.a.s., via F. Ferrucci 203/C, 59100 Prato (PO);

Versione: Modest Versione 8.31

Estremi della licenza d'uso o di altra forma di autorizzazione all'uso: numero di licenza 7279

AFFIDABILITA' DEL CODICE DI CALCOLO

In base a quanto richiesto al par. 10.2 del D.M. 17.01.2018 (Norme Tecniche per le Costruzioni) il produttore e distributore Tecnisoft s.a.s. espone la seguente relazione riguardante il solutore numerico e, più in generale, la procedura di analisi e dimensionamento Modest.

Si fa presente che sul proprio sito è disponibile sia il manuale teorico del solutore sia il documento comprendente i numerosi esempi di validazione.

Si riporta nel seguito la dichiarazione di affidabilità fornita dalla software house.



Strumenti solidi come i vostri progetti

Tecnisoft s.a.s. di Papi Paolo Luca & C.
Via F. Ferrucci, 203/C - 59100 Prato
Tel. 0574 583421 - Fax 0574 592705
C.F. e P.IVA 01555190972
R.E.A. C.C.I.A.A. Prato n. 421503

DICHIARAZIONE DI AFFIDABILITÀ DEL PROGRAMMA MODEST

Facendo seguito a quanto richiesto dalle Norme Tecniche per le Costruzioni, la società Tecnisoft s.a.s. produttrice e distributrice del programma ModeSt, dichiara quanto segue.

Il programma ModeSt è un pre-post processore per solutori ad elementi finiti prodotti da altre società ed alle quali si rimanda per i relativi test di affidabilità. Si segnala comunque che i solutori supportati sono di riconosciuta fama nazionale e internazionale e di comprovata affidabilità (Xfinest, SAP2000) e che vengono distribuiti con i relativi test di validazione.

ModeSt contiene comunque al suo interno procedure che l'utente può attivare per il controllo di congruenza sui dati introdotti, procedure che riconoscono in automatico la presenza dei più tipici errori di modellazione.

Al termine del calcolo sono interrogabili sia numericamente che graficamente tutti i risultati, per consentire la valutazione della bontà della modellazione effettuata.

Le procedure di progettazione delle armature degli elementi in c.a. o di verifica degli elementi in acciaio, legno o muratura segnalano sempre le situazioni in cui non sono soddisfatte le condizioni di verifica previste dalla normativa ed implementate nel software. Anche in questo caso si possono effettuare controlli grafici e numerici su stati tensionali, domini di rottura, ecc.

Le procedure di progetto e verifica sono state testate con numerosi esempi reperiti in letteratura o risolti manualmente. Tali esempi sono riportati all'interno di un manuale fornito insieme al programma.

Prato, 30 maggio 2011

Tecnisoft s.a.s.
Socio Accomandatario



Il Progettista
Luca Spaccino