

STRADA STATALE 4 "VIA SALARIA"
**Adeguamento della piattaforma stradale e messa in
sicurezza dal km 56+000 al km 64+000**
Stralcio 1 da pk 0+000 a pk 1+900

PROGETTO ESECUTIVO

COD. **RM 368**

PROGETTAZIONE: R.T.I.: PROGER S.p.A. (capogruppo mandataria)
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PROTOCOLLO _____ DATA _____ 202_

OPERE D'ARTE MINORI - TOMBINI

Tombino 2x2 pk 0+596 – Relazione di calcolo opere provvisionali

| | | | |
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Sommario

| | | |
|----------|---|-----------|
| 1 | <i>PREMESSA</i> | 1 |
| 1.1 | Descrizione dell’opera | 1 |
| 2 | <i>NORMATIVA DI RIFERIMENTO</i> | 4 |
| 2.1 | Elaborati di riferimento..... | 5 |
| 3 | <i>CARATTERISTICHE DEI MATERIALI</i> | 6 |
| 3.1 | Classe di esposizione e copriferro | 6 |
| 3.2 | Calcestruzzo micropali | 7 |
| 3.3 | Caratteristiche tiranti..... | 7 |
| 4 | <i>INQUADRAMENTO GEOTECNICO</i> | 8 |
| 4.1 | Stratigrafia di progetto e parametri geotecnici | 8 |
| 4.2 | Tiranti di ancoraggio..... | 10 |
| 5 | <i>MODELLAZIONE NUMERICA</i> | 12 |
| 5.1 | Programmi per l’analisi automatica | 12 |
| 5.2 | Modelli di calcolo | 12 |
| 5.3 | Paratia provvisoria..... | 12 |
| 6 | <i>ANALISI DEI CARICHI</i> | 14 |
| 6.1 | Condizioni di carico e spinta delle terre..... | 14 |
| 6.2 | Carico stradale | 15 |
| 7 | <i>RISULTATI</i> | 16 |
| 7.1 | Verifiche SLU | 16 |
| 7.1.1 | Modello con interasse tiranti di 2,4m | 16 |
| 7.1.2 | Modello con interasse tiranti di 4m | 18 |
| 7.2 | Verifiche SLE GEO | 20 |
| 7.2.1 | Modello con interasse tiranti di 2,4m | 20 |
| 7.2.2 | Modello con interasse tiranti di 4m | 21 |

| | | |
|-----------|--|------------|
| 7.3 | Risultati tiranti | 21 |
| 7.3.1 | Modello con interasse tiranti di 2,4m | 21 |
| 7.3.2 | Modello con interasse tiranti di 4m | 21 |
| 7.4 | Risultati trave di ripartizione | 22 |
| 7.4.1 | Modello con interasse tiranti di 2,4m | 22 |
| 7.4.2 | Modello con interasse tiranti di 4m | 22 |
| 8 | <i>VERIFICHE DEL CORDOLO</i> | 23 |
| 9 | <i>ALLEGATO 1: tabulato di calcolo paratia (interasse tiranti 2.4 m).....</i> | 24 |
| 10 | <i>ALLEGATO 2: tabulato di calcolo paratia (interasse tiranti 4m)</i> | 110 |

1 PREMESSA

Nell’ambito della progettazione definitiva dell’intervento di adeguamento della piattaforma stradale e messa in sicurezza della STRADA STATALE 4 “VIA SALARIA” dal km 56+000 al km 64+000, è prevista la realizzazione di una paratia provvisoria per la realizzazione del tombino **TM06**.

Le azioni considerate nel calcolo sono quelle tipiche di una struttura interrata determinate dall’interazione terreno – struttura, derivanti dall’applicazione della Normativa D.M. 2018 – Norme tecniche per le costruzioni.

L’opera oggetto della presente relazione è di tipo provvisorio, essa ha la finalità di sorreggere gli scavi e permettere la realizzazione del tombino in c.a.; le fasi del lavoro infatti prevedono la realizzazione dei micropali e del cordolo, uno sbancamento iniziale con conseguente realizzazione del tirante ed infine lo scavo completo. La realizzazione della paratia permette quindi di garantire il flusso veicolare in destra e, a seguito dello scavo, la realizzazione della parte di tombino in sinistra. Una volta completata la parte del tombino di sinistra si demolisce il tirante e si effettua dall’altro lato lo sbancamento (con realizzazione del tirante) e uno scavo completo per poter realizzare la parte di tombino in destra, garantendo il traffico veicolare in sinistra.

1.1 Descrizione dell’opera

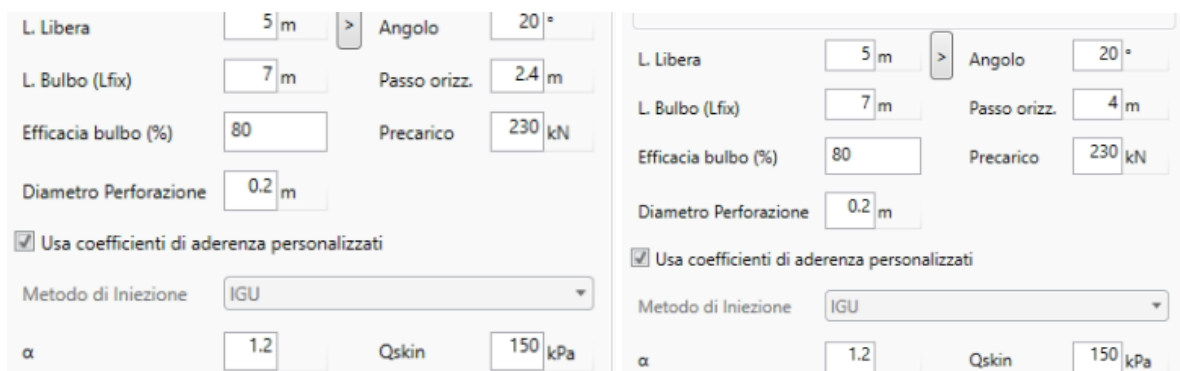
Sono stati previsti micropali tirantati di diametro Φ 240 mm, interasse 0.4 m e altezza pari a 10m.

I modelli di calcolo analizzati sono riferiti a:

- Fase iniziale: interasse tiranti pari a 2.4 m
- fase di realizzazione del tombino: interasse tiranti pari a 4 m.


| h Scavo | h tot |
|----------------|--------------|
| (m) | (m) |
| 5.3 | 10 |

I tiranti hanno le seguenti caratteristiche:



| Modello 1 (2.4m) | | Modello 2 (4m) | |
|---|---------|---|---------|
| L. Libera | 5 m | L. Libera | 5 m |
| L. Bulbo (Lfix) | 7 m | L. Bulbo (Lfix) | 7 m |
| Efficacia bulbo (%) | 80 | Efficacia bulbo (%) | 80 |
| Diametro Perforazione | 0.2 m | Diametro Perforazione | 0.2 m |
| Angolo | 20 ° | Angolo | 20 ° |
| Passo orizz. | 2.4 m | Passo orizz. | 4 m |
| Precarico | 230 kN | Precarico | 230 kN |
| <input checked="" type="checkbox"/> Usa coefficienti di aderenza personalizzati | | <input checked="" type="checkbox"/> Usa coefficienti di aderenza personalizzati | |
| Metodo di Iniezione | IGU | Metodo di Iniezione | IGU |
| α | 1.2 | α | 1.2 |
| Qskin | 150 kPa | Qskin | 150 kPa |

Il profilato metallico utilizzato è il seguente:

| | | | | |
|---|--|-----------|----------|-------------|
| Acciaio | | Materiale | | S355 |
|  | | Profilo | | CHS168.3*12 |
| Passo | | Ss | 0.4 m | |
| Diametro | | Sod | 0.1683 m | |
| Spessore | | Sot | 0.012 m | |

La trave di ripartizione usata è del tipo **2* HEB160**.

Nel seguito si riportano alcune immagini rappresentative delle sezioni oggetto di analisi:

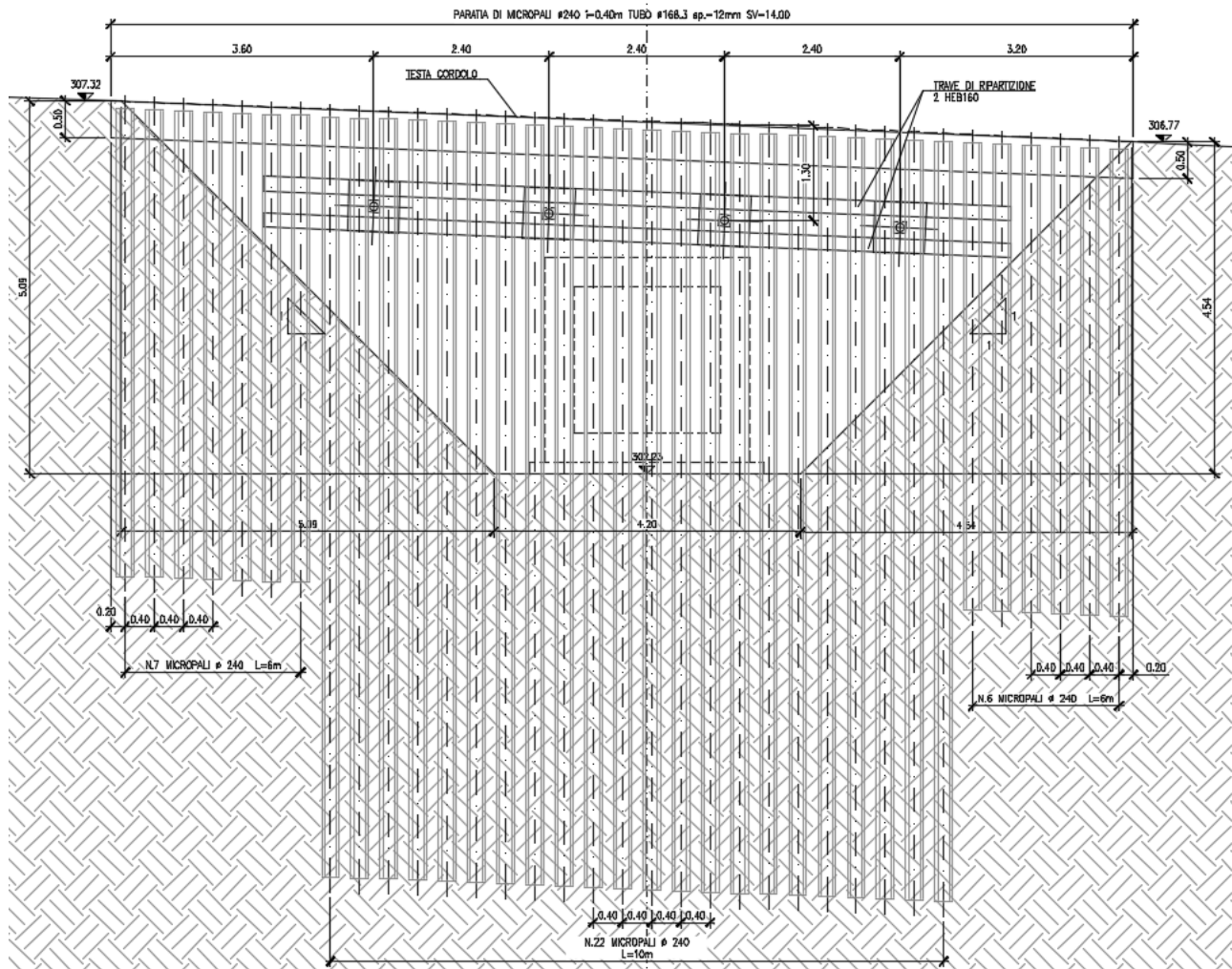


Fig. 1- prospetto fase iniziale

2 NORMATIVA DI RIFERIMENTO

Si riporta nel seguito l'elenco delle leggi e dei decreti di carattere generale, assunti come riferimento.

- D.M. 17 gennaio 2018 - *Norme Tecniche per le Costruzioni (NTC)*;
- Circolare n.7 del 21 gennaio 2019 - *Istruzioni per l'applicazione delle “Nuove norme tecniche per le costruzioni” di cui al D.M. 17 gennaio 2018*;
- UNI EN 1992-1-1 - *Progettazione delle strutture di calcestruzzo*;
- UNI EN 206-1-2014 - *Calcestruzzo: specificazione, prestazione, produzione e conformità*.
- UNI 11104_2016: *Calcestruzzo: Specificazione, prestazione, produzione e conformità - Istruzioni complementari per l'applicazione della EN 206-1*
- Decreto Protezione Civile 21 ottobre 2003: Disposizioni attuative dell'art. 2, commi 2, 3 e 4, dell'ordinanza del Presidente del Consiglio dei Ministri n. 3274 del 20 marzo 2003.
- OPCM 20 marzo 2003 n. 3274, Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica.
- OPCM 3 maggio 2005 n. 3431: Ulteriori modifiche ed integrazioni dell'ordinanza del Presidente del consiglio dei Ministri n. 3274 del 20/3/2003 recante “Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica”.
- OPCM 8 luglio 2004 n. 3362: Modalità di attivazione del Fondo per investimenti straordinari della Presidenza del Consiglio dei Ministri istituito ai sensi dell'art. 32-bis del decreto legge 30 settembre 2003 n. 269 convertito, con modificazioni, dalla legge 24 novembre 2003 n. 326.
- OPCM 28 aprile 2006: Criteri generali per l'individuazione delle zone sismiche e per la formazione e l'aggiornamento degli elenchi delle medesime zone.
- Linee Guida per la valutazione e riduzione del rischio sismico del patrimonio culturale e successive modificazioni del Ministero per i Beni e le Attività Culturali, come licenziate dal Consiglio Superiore dei Lavori Pubblici e ss. mm. ii..
- Raccomandazioni AGI (1977);
- Modalità Tecniche ANISG (1977).
- Quaderni tecnici ANAS

2.1 Elaborati di riferimento

Costituiscono parte integrante di quanto esposto nel presente documento, l’insieme degli elaborati di progetto specifici relativi all’opera in esame e riportati in elenco elaborati:

T01TM06STRCA01

3 CARATTERISTICHE DEI MATERIALI

Di seguito si riportano le caratteristiche dei materiali previsti per la realizzazione delle strutture oggetto di calcolo nell'ambito del presente documento:

3.1 Classe di esposizione e copriferro

Con riferimento alle specifiche di cui alla norma UNI EN 206-1-2006, si definiscono di seguito le classi di esposizione del calcestruzzo delle diverse parti della struttura oggetto dei dimensionamenti di cui al presente documento:

- XC2

| Classe esposizione norma UNI 9558 | Classe esposizione norma UNI 11104 UNI EN 206-1 | Descrizione dell'ambiente | Esempio | Massimo rapporto a/c | Minima Classe di resistenza | Contenuto minimo in aria (%) |
|--|---|--|--|----------------------|-----------------------------|------------------------------|
| 1 Assenza di rischio di corrosione o attacco | | | | | | |
| 1 | X0 | Per calcestruzzo privo di armatura o inserti metallici: tutte le esposizioni eccetto dove c'è gelo/disgelo, o attacco chimico. Calcestruzzi con armatura o inserti metallici in ambiente molto asciutto. | Interno di edifici con umidità relativa molto bassa. Calcestruzzo non armato all'interno di edifici. Calcestruzzo non armato immerso in suolo non aggressivo o in acqua non aggressiva. Calcestruzzo non armato soggetto a cicli di bagnato asciutto ma non soggetto ad abrasione, gelo o attacco chimico. | - | C 12/15 | |
| 2 Corrosione indotta da carbonatazione | | | | | | |
| Nota: Le condizioni di umidità si riferiscono a quelle presenti nel copriferro o nel ricoprimento di inserti metallici, ma in molti casi si può considerare che tali condizioni riflettano quelle dell'ambiente circostante. In questi casi la classificazione dell'ambiente circostante può essere adeguata. Questo può non essere il caso se c'è una barriera fra il calcestruzzo e il suo ambiente. | | | | | | |
| 2 a | XC1 | Asciutto o permanentemente bagnato. | Interni di edifici con umidità relativa bassa. Calcestruzzo armato ordinario o precompresso con le superfici all'interno di strutture con eccezione delle parti esposte a condensazione, o immerse in acqua. | 0,60 | C 25/30 | |
| 2 a | XC2 | Bagnato, raramente asciutto. | Parti di strutture di contenimento liquidi, fondazioni. Calcestruzzo armato ordinario o precompresso prevalentemente immerso in acqua o terreno non aggressivo. | 0,60 | C 25/30 | |
| 5 a | XC3 | Umidità moderata. | Calcestruzzo armato ordinario o precompresso in esterni con superfici esterne riparate dalla pioggia, o in interni con umidità da moderata ad alta. | 0,55 | C 28/35 | |
| 4 a 5 b | XC4 | Ciclicamente asciutto e bagnato. | Calcestruzzo armato ordinario o precompresso in esterni con superfici soggette a alternanze di asciutto ed umido. Calcestruzzi a vista in ambienti urbani. Superfici a contatto con l'acqua non comprese nella classe XC2. | 0,50 | C 32/40 | |
| 3 Corrosione indotta da cloruri esclusi quelli provenienti dall'acqua di mare | | | | | | |
| 5 a | XD1 | Umidità moderata. | Calcestruzzo armato ordinario o precompresso in superfici o parti di ponti e viadotti esposti a spruzzi d'acqua contenenti cloruri. | 0,55 | C 28/35 | |
| 4 a 5 b | XD2 | Bagnato, raramente asciutto. | Calcestruzzo armato ordinario o precompresso, di elementi strutturali totalmente immersi in acqua anche industriale contenente cloruri (Piscine). | 0,50 | C 32/40 | |
| 5 c | XD3 | Ciclicamente bagnato e asciutto. | Calcestruzzo armato ordinario o precompresso, elementi con una superficie immersa in acqua contenente cloruri e l'altra esposta all'aria. Parti di ponti, pavimentazioni e parcheggi per auto. | 0,45 | C 35/45 | |

| Classe esposizione norma UNI 9558 | Classe esposizione norma UNI 11104 UNI EN 206-1 | Descrizione dell'ambiente | Esempio | Massimo rapporto a/c | Minima Classe di resistenza | Contenuto minimo in aria (%) |
|---|---|--|--|----------------------|-----------------------------|------------------------------|
| 4 Corrosione indotta da cloruri presenti nell'acqua di mare | | | | | | |
| 4 a 5 b | XS1 | Esposto alla salinità marina ma non direttamente in contatto con l'acqua di mare. | Calcestruzzo armato ordinario o precompresso con elementi strutturali sulle coste o in prossimità. | 0,50 | C 32/40 | |
| | XS2 | Permanentemente sommerso. | Calcestruzzo armato ordinario o precompresso di strutture marine completamente immerse in acqua. | 0,45 | C 35/45 | |
| | XS3 | Zone esposte agli spruzzi o alle maree. | Calcestruzzo armato ordinario o precompresso di elementi strutturali esposti alla battigia o alle zone soggette agli spruzzi ed onde del mare. | 0,45 | C 35/45 | |
| 5 Attacco dei cicli di gelo/disgelo con o senza disgelanti * | | | | | | |
| 2 b | XF1 | Moderata saturazione d'acqua, in assenza di agente disgelante. | Superfici verticali di calcestruzzo come facciate e colonne esposte alla pioggia ed al gelo. Superfici non verticali e non soggette alla completa saturazione ma esposte al gelo, alla pioggia e all'acqua. | 0,50 | C 32/40 | |
| 3 | XF2 | Moderata saturazione d'acqua, in presenza di agente disgelante. | Elementi come parti di ponti che in altro modo sarebbero classificati come XF1 ma che sono esposti direttamente o indirettamente agli agenti disgelanti. | 0,50 | C 25/30 | 3,0 |
| 2 b | XF3 | Elevata saturazione d'acqua, in assenza di agente disgelante. | Superfici orizzontali in edifici dove l'acqua può accumularsi e che possono essere soggetti ai fenomeni di gelo, elementi soggetti a frequenti bagnature ed esposti al gelo. | 0,50 | C 25/30 | 3,0 |
| 3 | XF4 | Elevata saturazione d'acqua, con presenza di agente antigelo oppure acqua di mare. | Superfici orizzontali quali strade o pavimentazioni esposte al gelo, ed ai sali disgelanti in modo diretto o indiretto, elementi esposti al gelo e soggetti a frequenti bagnature in presenza di agenti disgelanti o di acqua di mare. | 0,45 | C 28/35 | 3,0 |
| 6 Attacco chimico** | | | | | | |
| 5 a | XA1 | Ambiente chimicamente debolmente aggressivo secondo il prospetto 2 della UNI EN 206-1 | Contentori di fanghi e vasche di decantazione. Contentori e vasche per acque reflue. | 0,55 | C 28/35 | |
| 4 a 5 b | XA2 | Ambiente chimicamente moderatamente aggressivo secondo il prospetto 2 della UNI EN 206-1 | Elementi strutturali o pareti a contatto di terreni aggressivi. | 0,50 | C 32/40 | |
| 5 c | XA3 | Ambiente chimicamente fortemente aggressivo secondo il prospetto 2 della UNI EN 206-1 | Elementi strutturali o pareti a contatto di acque industriali fortemente aggressive. Contentori di fanghi, mangimi e liquame provenienti dall'allevamento animale. Torri di raffreddamento di fumi di gas di scarico industriali. | 0,45 | C 35/45 | |

*) Il grado di saturazione della seconda colonna riflette la relativa frequenza con cui si verifica il gelo in condizioni di saturazione:
- moderato: occasionalmente gelato in condizione di saturazione;
- elevato: alta frequenza di gelo in condizioni di saturazione.

***) Da parte di acque del terreno e acque fluviali.

Classi di esposizione secondo norma UNI – EN 206-2006

La determinazione delle classi di resistenza dei conglomerati dei conglomerati, di cui ai successivi paragrafi, sono state inoltre determinate tenendo conto delle classi minime stabilite dalla stessa norma UNI-EN 11104, di cui alla successiva tabella:

prospetto 4 Valori limiti per la composizione e le proprietà del calcestruzzo

| | Classi di esposizione | | | | | | | | | | | | | | | | | |
|--|--|--|--------|--------|------------------------------------|--|--------|--------|--------|-------|-------|---|-------------------|-------|-------|--|------|-----|
| | Nessun rischio di corrosione dell'armatura | Corrosione delle armature indotta dalla carbonatazione | | | | Corrosione delle armature indotta da cloruri | | | | | | Attacco da cicli di gelo/disgelo | | | | Ambiente aggressivo per attacco chimico | | |
| | | Acqua di mare | | | Cloruri provenienti da altre fonti | | | | | | | | | | | | | |
| | X0 | XC1 | XC2 | XC3 | XC4 | XS1 | XS2 | XS3 | XD1 | XD2 | XD3 | XF1 | XF2 | XF3 | XF4 | XA1 | XA2 | XA3 |
| Massimo rapporto a/c | - | 0,60 | 0,55 | 0,50 | 0,50 | 0,45 | 0,55 | 0,50 | 0,45 | 0,50 | 0,45 | 0,50 | 0,50 | 0,45 | 0,55 | 0,50 | 0,45 | |
| Minima classe di resistenza ¹⁾ | C12/15 | C25/30 | C28/35 | C32/40 | C32/40 | C35/45 | C28/35 | C32/40 | C35/45 | 32/40 | 25/30 | 28/35 | 28,35 | 32/40 | 35/45 | | | |
| Minimo contenuto in cemento (kg/m ³) | - | 300 | 320 | 340 | 340 | 360 | 320 | 340 | 360 | 320 | 340 | 360 | 320 | 340 | 360 | | | |
| Contenuto minimo in aria (%) | | | | | | | | | | | | | 3,0 ²⁾ | | | | | |
| Altri requisiti | | | | | | | | | | | | Aggregati conformi alla UNI EN 12620 di adeguata resistenza al gelo/disgelo | | | | È richiesto l'impiego di cementi resistenti ai solfati ³⁾ | | |

¹⁾ Nel prospetto 7 della UNI EN 206-1 viene riportata la classe C8/10 che corrisponde a specifici calcestruzzi destinati a sottofondazioni e ricoprimenti. Per tale classe dovrebbero essere definite le prescrizioni di durabilità nei riguardi di acque o terreni aggressivi.
^{a)} Quando il calcestruzzo non contiene aria aggiunta, le sue prestazioni devono essere verificate rispetto ad un calcestruzzo aerato per il quale è provata la resistenza al gelo/disgelo, da determinarsi secondo UNI 7087, per la relativa classe di esposizione.
^{b)} Qualora la presenza di solfati comporti le classi di esposizione XA2 e XA3 è essenziale utilizzare un cemento resistente ai solfati secondo UNI 9156.

Classi di resistenza minima del calcestruzzo secondo UNI – 11104

3.2 Calcestruzzo micropali

CARATTERISTICHE CALCESTRUZZO PER PALI

- Classe di resistenza C25/30
- Contenuto minimo di cemento 300 Kg/mc
- Tipo di cemento CEM II
- Rapporto massimo acqua/cemento 0.60
- Slump : S5
- Diametro massimo dell'inerte 18 mm
- Classe di esposizione XC2

3.3 Caratteristiche tiranti

TIRANTI

- CARATTERISTICHE DEI TREFOLI:
 diametro nominale mm 15.20 (6/10").
 sezione nominale mmq 139.
 limite elastico convenzionale allo 0.1% tp(1)k = 1670 Mpa
 carico di rottura ftpk = 1860 Mpa

- CONDOTTI DI INIEZIONE:
 devono presentare il diametro minimo di 16 mm e pressione di scoppio non inferiore a 1Mpa(10 kg/cmq) per iniezione a bassa pressione. Non inferiore a 7.0 Mpa (70 kg/cmq) per iniezione ad alta pressione.

- MISCELA DI INIEZIONE DEI TIRANTI:
 Densità >= 1.85 t/mc
 Cemento tipo II
 Rapporto a/c <= 0.45
 Resistenza a compressione >= 25 Mpa dopo 3gg
 >= 35 Mpa a 7gg
 >= 50 Mpa a 28gg.

Unità Ra (riporto antropico)

| | |
|------------------------------|--------------------------------|
| $\gamma = 19 \text{ kN/m}^3$ | peso di volume naturale |
| $c' = 0 \text{ kPa}$ | coesione drenata |
| $\phi' = 35^\circ$ | angolo di resistenza al taglio |

Unità SR (calcarei marnosi)

| | |
|--------------------------------|--------------------------------|
| $\gamma = 24.5 \text{ kN/m}^3$ | peso di volume naturale |
| $c' = 40 \text{ kPa}$ | coesione drenata |
| $\phi' = 40^\circ$ | angolo di resistenza al taglio |

L'opera è interessata dalla presenza della falda alla quota 3.5m dal p.c..

4.2 Tiranti di ancoraggio

Nella scelta dei valori di α e s si rimanda ai diagrammi di Bustamante e Doix.

In particolare, data la natura del terreno attraversato dal tirante di tipo calcareo – marnoso, agendo a favore di sicurezza, si ha:

$$\alpha = 1.2$$

$$s = Q_{skin} = 150 \text{ kPa}$$

Il valore di α adottato rappresenta il limite inferiore per terreni ghiaiosi, ma assume lo stesso valore per le argille, oltre ad essere il limite superiore dei terreni limosi. Tale valore è stato assunto per la verifica dei tiranti in quanto compatibile con entrambe le tipologie di terreno (ghiaia e argille) riscontrati nel profilo geotecnico.

Indicazioni per la scelta del valore di s

| TERRENO | Tipo di iniezione | |
|---|-------------------|-----------|
| | IRS | IGU |
| Da ghiaia a sabbia limosa | SG1 | SG2 |
| Limo e argilla | AL1 | AL2 |
| Marna, calcare marnoso, calcare tenero fratturato | MC1 | MC2 |
| Roccia alterata e/o fratturata | $\geq R1$ | $\geq R2$ |

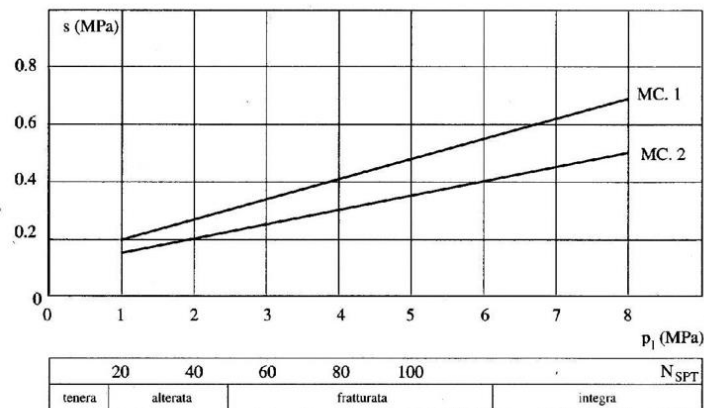


Fig. 13.18. Abaco per il calcolo di s per gessi, marne, marne calcaree

Valori del coefficiente α ($V_s = L_s \cdot \pi \cdot d_s^2 / 4$)

| TERRENO | Valori di α | | Quantità minima di miscela consigliata | |
|--------------------------------|--------------------|------------------|---|-----------------|
| | IRS | IGU | IRS | IGU |
| Ghiaia | 1.8 | 1.3 - 1.4 | 1.5 V_s | 1.5 V_s |
| Ghiaia sabbiosa | 1.6 - 1.8 | 1.2 - 1.4 | 1.5 V_s | 1.5 V_s |
| sabbia ghiaiosa | 1.5 - 1.6 | 1.2 - 1.3 | 1.5 V_s | 1.5 V_s |
| Sabbia grossa | 1.4 - 1.5 | 1.1 - 1.2 | 1.5 V_s | 1.5 V_s |
| Sabbia media | 1.4 - 1.5 | 1.1 - 1.2 | 1.5 V_s | 1.5 V_s |
| Sabbia fine | 1.4 - 1.5 | 1.1 - 1.2 | 1.5 V_s | 1.5 V_s |
| Sabbia limosa | 1.4 - 1.5 | 1.1 - 1.2 | (1.5 - 2) V_s | 1.5 V_s |
| Limo | 1.4 - 1.6 | 1.1 - 1.2 | 2 V_s | 1.5 V_s |
| Argilla | 1.8 - 2.0 | 1.2 | (2.5 - 3) V_s | (1.5 - 2) V_s |
| Marne | 1.8 | 1.1 - 1.2 | (1.5 - 2) V_s per strati compatti | |
| Calcari marnosi | 1.8 | 1.1 - 1.2 | (2 - 6) V_s o più per strati fratturati | |
| Calcari alterati o fratturati | 1.8 | 1.1 - 1.2 | | |
| Roccia alterata e/o fratturata | 1.2 | 1.1 | (1.1 - 1.5) V_s per strati poco fratturati; 2 V_s o più per strati fratturati | |

5 MODELLAZIONE NUMERICA

5.1 Programmi per l'analisi automatica

Lo stato tenso-deformativo della paratia e le verifiche strutturali sono state svolte con il codice di calcolo *PARATIEPLUS*.

5.2 Modelli di calcolo

Lo stato tenso-deformativo dei pali è stato investigato mediante il software di calcolo *PARATIE PLUS*, programma non lineare agli elementi finiti per l'analisi di strutture di sostegno flessibili.

Si è considerato un comportamento piano nelle deformazioni, analizzando una striscia di parete di larghezza unitaria. La realizzazione dello scavo sostenuto da paratie è seguita in tutte le varie fasi attraverso un'analisi statica incrementale: ogni passo di carico coincide con una ben precisa configurazione caratterizzata da una quota di scavo, da un insieme di puntoni e tiranti applicati e da una ben precisa disposizione di carichi applicati.

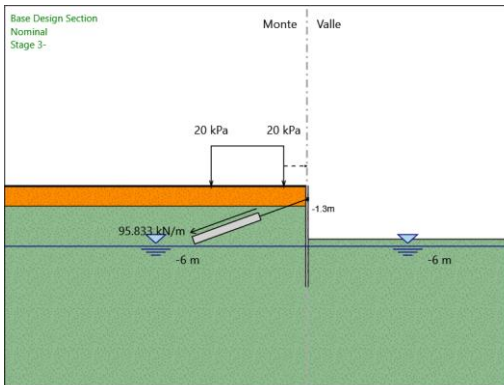
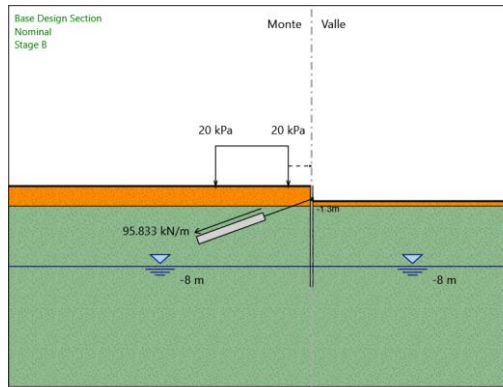
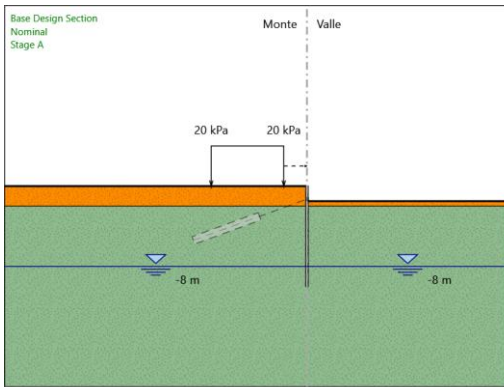
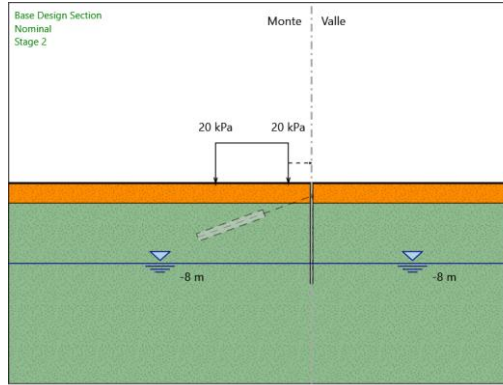
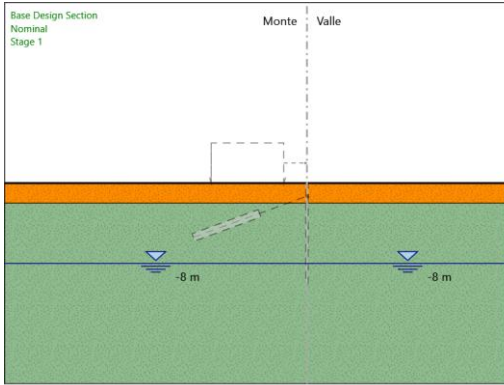
5.3 Paratia provvisoria

La paratia è costituita micropali D240 interasse 2.4 m, L=10 m.

L'altezza di scavo finale è 5.3 m.

Nella modellazione è implementata la seguente successione di step:

- 1) Inizializzazione
- 2) Realizzazione della paratia e applicazione carico stradale
- 3) Scavo per realizzazione tirante
- 4) realizzazione tirante
- 5) scavo finale



6 ANALISI DEI CARICHI

6.1 Condizioni di carico e spinta delle terre

Il peso proprio della struttura è calcolato in base alla geometria degli elementi strutturali e al peso specifico assunto per i materiali:

$$\gamma_{cls}=25.0 \quad \text{kN/m}^3$$

Nel modello di calcolo impiegato dal software di calcolo PARATIE, la spinta del terreno viene determinata investigando l'interazione statica tra terreno e la struttura deformabile a partire da uno stato di spinta a riposo del terreno sulla paratia.

I parametri che identificano il tipo di legge costitutiva possono essere distinti in due sottoclassi: parametri di spinta e parametri di deformabilità del terreno.

I parametri di spinta sono il coefficiente di spinta a riposo K_0 , il coefficiente di spinta attiva K_a e il coefficiente di spinta passiva K_p .

Il coefficiente di spinta a riposo fornisce lo stato tensionale presente in sito prima delle operazioni di scavo. Esso lega la tensione orizzontale efficace σ'_h a quella verticale σ'_v attraverso la relazione:

$$\sigma'_h = K_0 \cdot \sigma'_v$$

K_0 dipende dalla resistenza del terreno, attraverso il suo angolo di attrito efficace ϕ' e dalla sua storia geologica. Si può assumere che:

$$K_0 = K_0^{NC} \cdot (\text{OCR})^m$$

dove

$$K_0^{NC} = 1 - \text{sen } \phi'$$

è il coefficiente di spinta a riposo per un terreno normalconsolidato ($\text{OCR}=1$). OCR è il grado di sovraconsolidazione e m è un parametro empirico, di solito compreso tra 0.4 e 0.7.

I coefficienti di spinta attiva e passiva sono forniti dalla teoria di Rankine per una parete liscia dalle seguenti espressioni:

$$K_a = \tan^2(45 - \phi'/2)$$

$$K_p = \tan^2(45 + \phi'/2)$$

Per tener conto dell'angolo di attrito δ tra paratia e terreno il software PARATIE impiega per K_a e K_p la formulazione rispettivamente di Coulomb e Lancellotta.

Formulazione di Coulomb per k_a

$$k_a = \frac{\cos^2(\varphi' - \beta)}{\cos^2 \beta \cdot \cos(\beta + \delta) \cdot \left[1 + \sqrt{\frac{\sin(\delta + \varphi') \cdot \sin(\varphi' - i)}{\cos(\beta + \delta) \cdot \cos(\beta - i)}} \right]^2}$$

dove:

φ' è l'angolo di attrito del terreno

β è l'angolo d'inclinazione del diaframma rispetto alla verticale

δ è l'angolo di attrito paratia-terreno

i è l'angolo d'inclinazione del terreno a monte della paratia rispetto all'orizzontale

Il valore limite della tensione orizzontale sarà pari a

$$\sigma'_h = K_a \cdot \sigma'_v - 2 \cdot c' \cdot \sqrt{K_a}$$

$$\sigma'_h = K_p \cdot \sigma'_v + 2 \cdot c' \cdot \sqrt{K_p}$$

a seconda che il collasso avvenga in spinta attiva o passiva rispettivamente. c' è la coesione drenata del terreno.

Formulazione di Lancellotta per k_p

$$K_p = \left[\frac{\cos \delta}{1 - \sin \Phi'} (\cos \delta + \sqrt{\sin^2 \Phi' - \sin^2 \delta}) \right] e^{2\theta \tan \Phi'}$$

dove:

$$2\theta = \sin^{-1} \left(\frac{\sin \delta}{\sin \Phi'} \right) + \delta$$

6.2 Carico stradale

Si considera un carico di 20 kN/m² per la presenza del traffico veicolare a monte.

7 RISULTATI

Nei paragrafi seguenti si riportano i risultati delle analisi condotte per il modello con interasse pari a 2.4m e per quello con interasse pari a 4m.

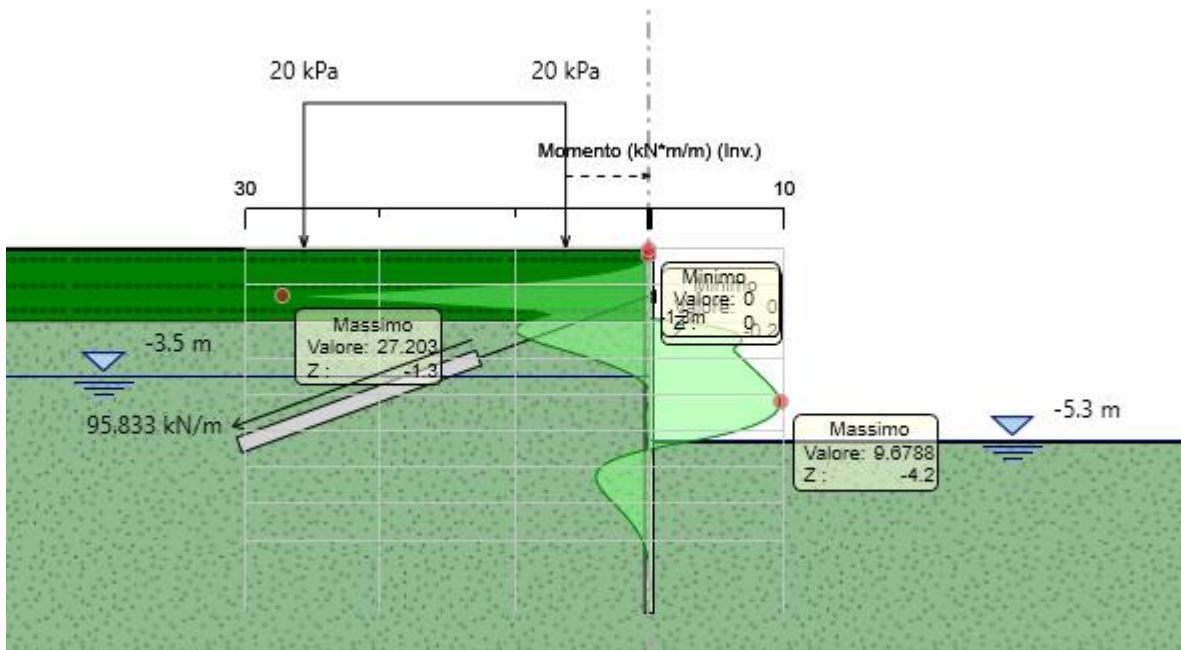
Si riporta l'indicazione dei valori massimi delle sollecitazioni flettenti e taglianti relativi all'analisi al metro.

Per i tabulati di calcolo e i risultati numerici estesi dei modelli, si rimanda agli allegati.

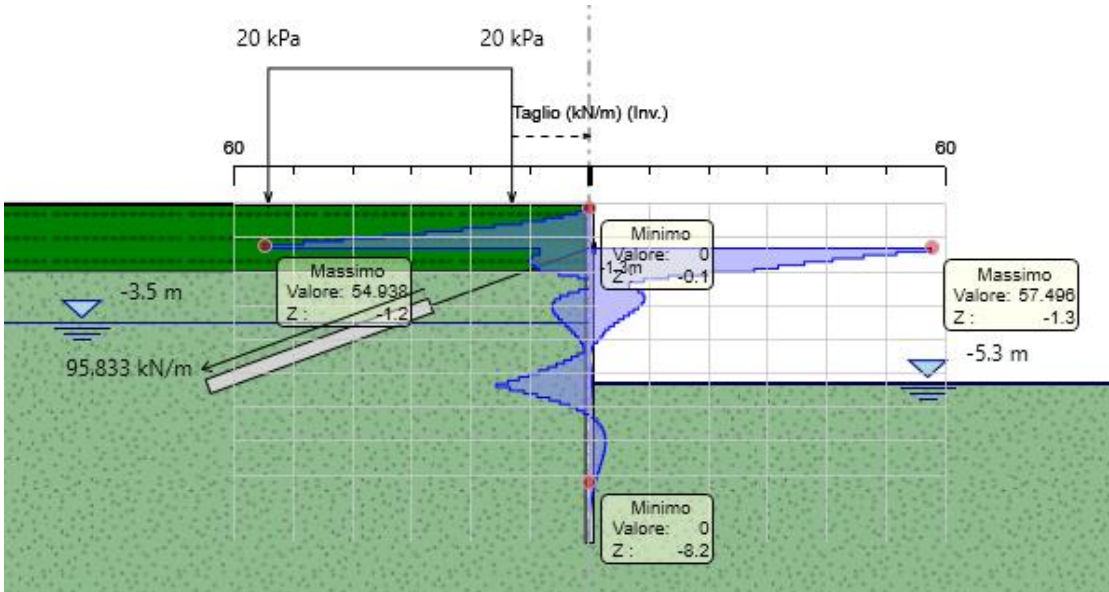
7.1 Verifiche SLU

7.1.1 Modello con interasse tiranti di 2,4m

Dall'involuppo del momento flettente si osserva che il massimo valore risulta pari a 28 kNm/m.

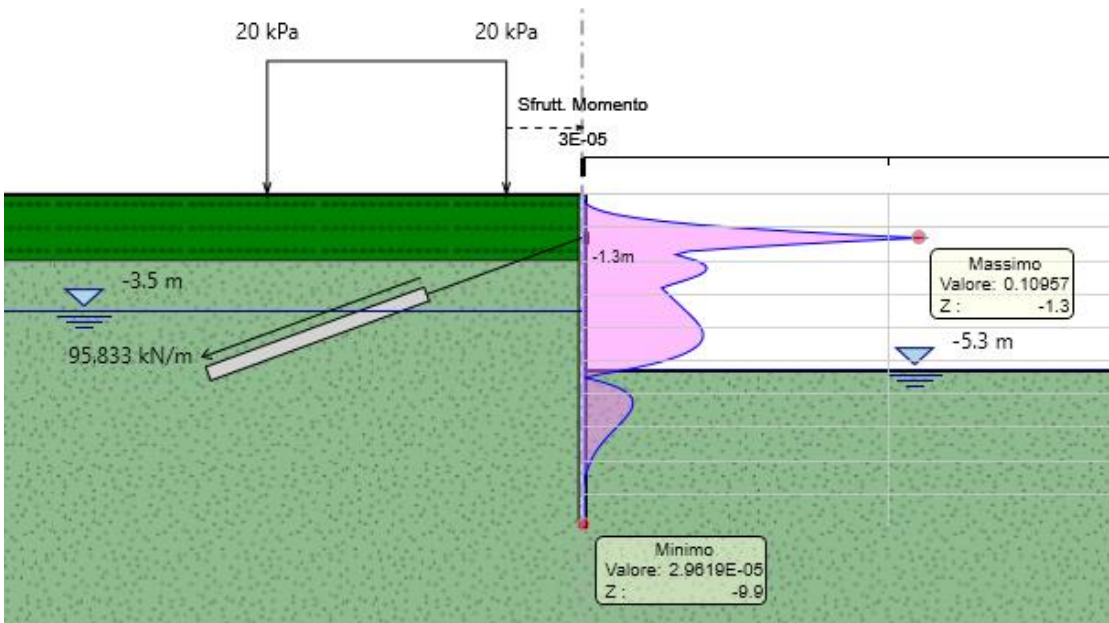


Dall'involuppo del taglio si osserva che il massimo valore risulta pari a 57 kN/m.

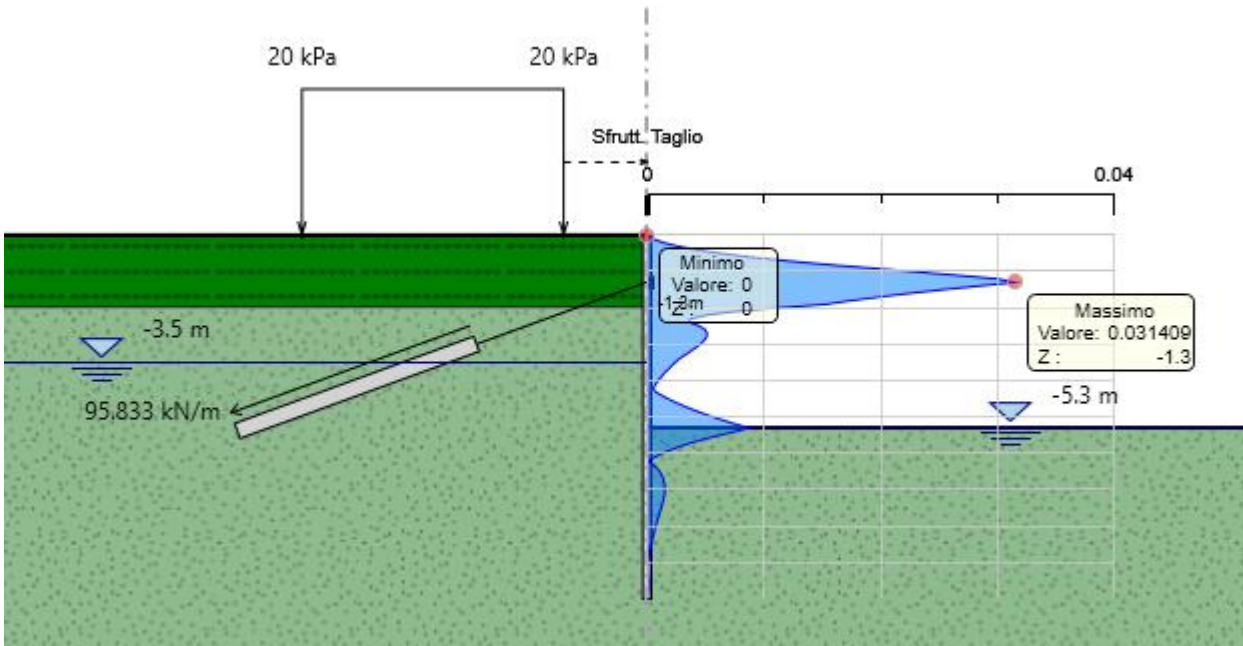


Nel seguito si riportano i risultati delle verifiche strutturali dei pali a flessione e a taglio condotte mediante l'ausilio di Paratie plus. In particolare si riportano i diagrammi dei tassi di sfruttamento, ottenuti come rapporto tra sollecitazione presente e resistenza disponibile in ogni sezione.

Tasso di sfruttamento a momento $T.S.F.max = 0.11 < 1$

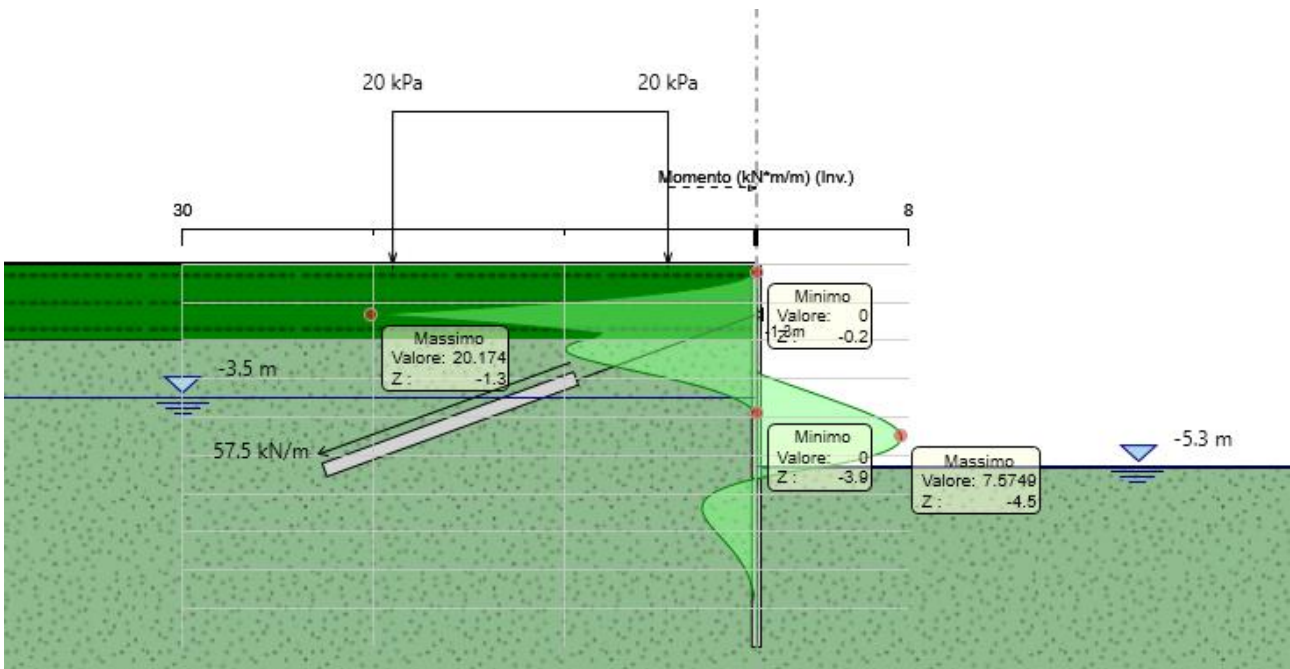


Tasso di sfruttamento a taglio T.S.F.max = 0.03 < 1

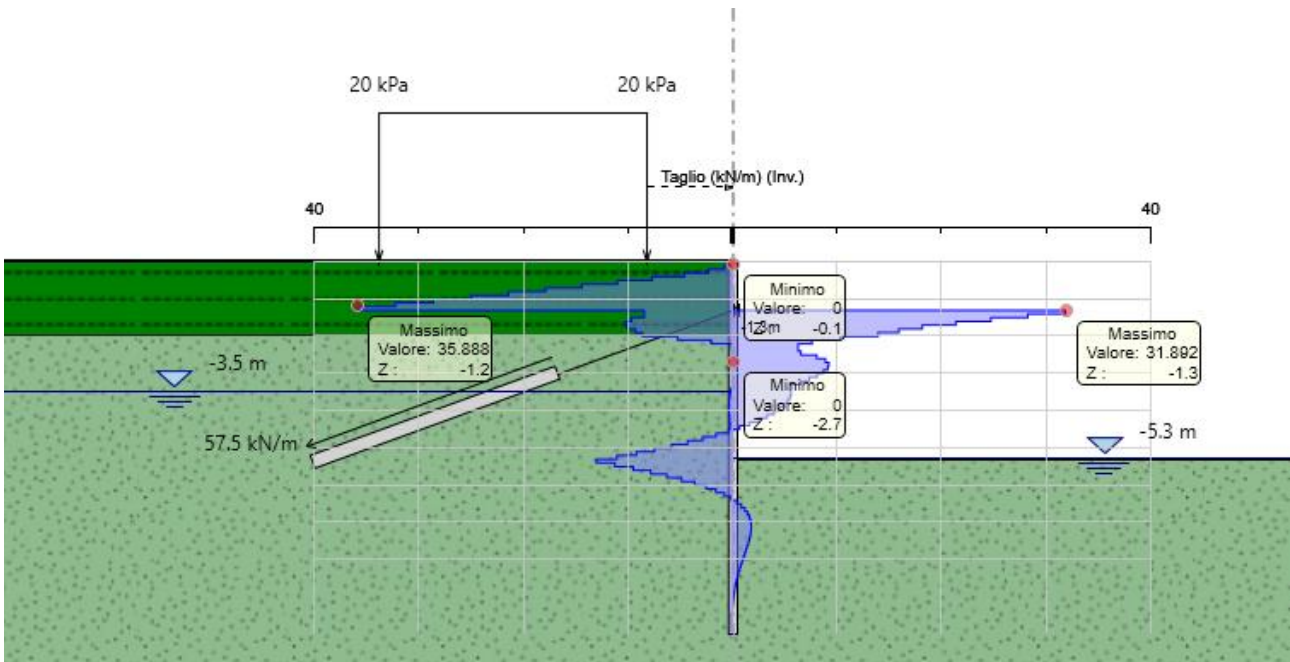


7.1.2 Modello con interasse tiranti di 4m

Dall'involuppo del momento flettente si osserva che il massimo valore risulta pari a 20 kNm/m.

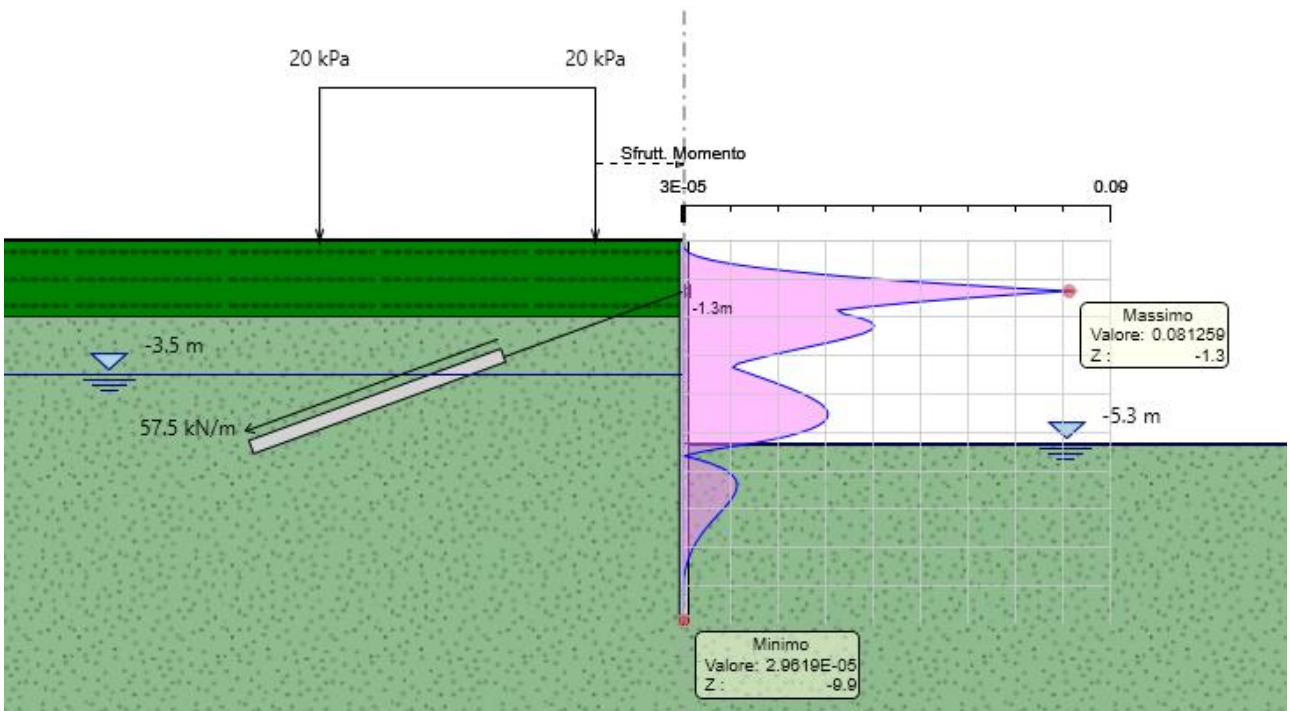


Dall'involuppo del taglio si osserva che il massimo valore risulta pari a 36 kN/m.

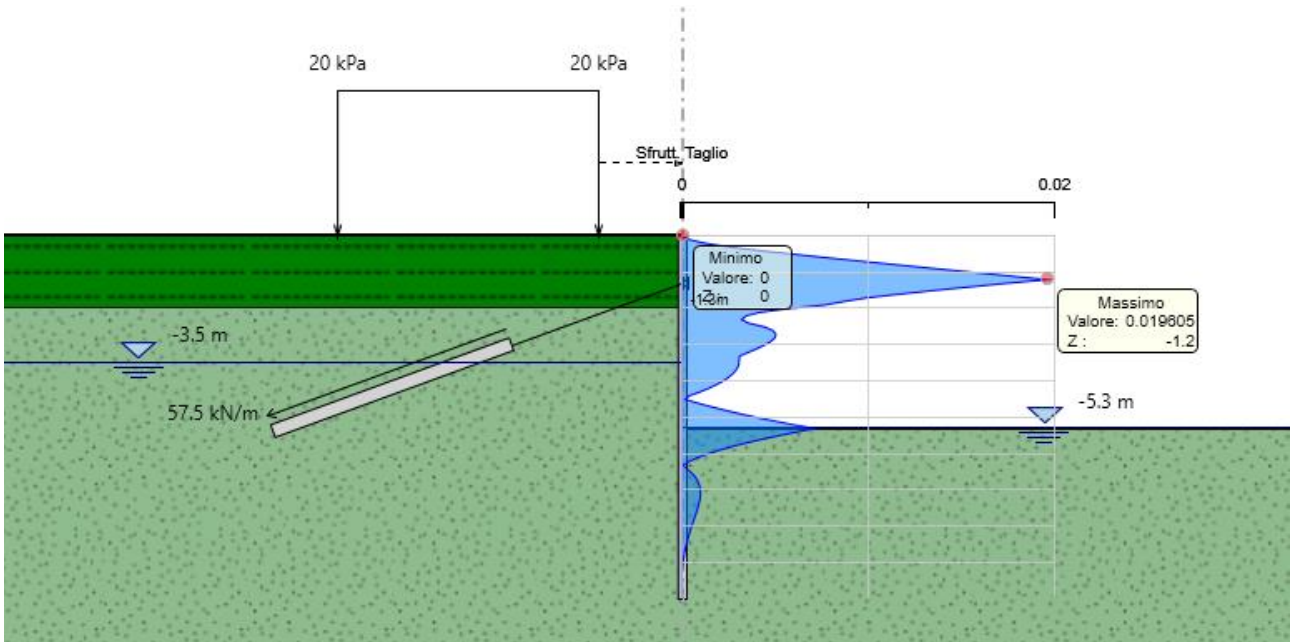


Nel seguito si riportano i risultati delle verifiche strutturali dei pali a flessione e a taglio condotte mediante l'ausilio di Paratie plus. In particolare si riportano i diagrammi dei tassi di sfruttamento, ottenuti come rapporto tra sollecitazione presente e resistenza disponibile in ogni sezione.

Tasso di sfruttamento a momento $T.S.F.max = 0.08 < 1$



Tasso di sfruttamento a taglio $T.S.F.max = 0.02 < 1$

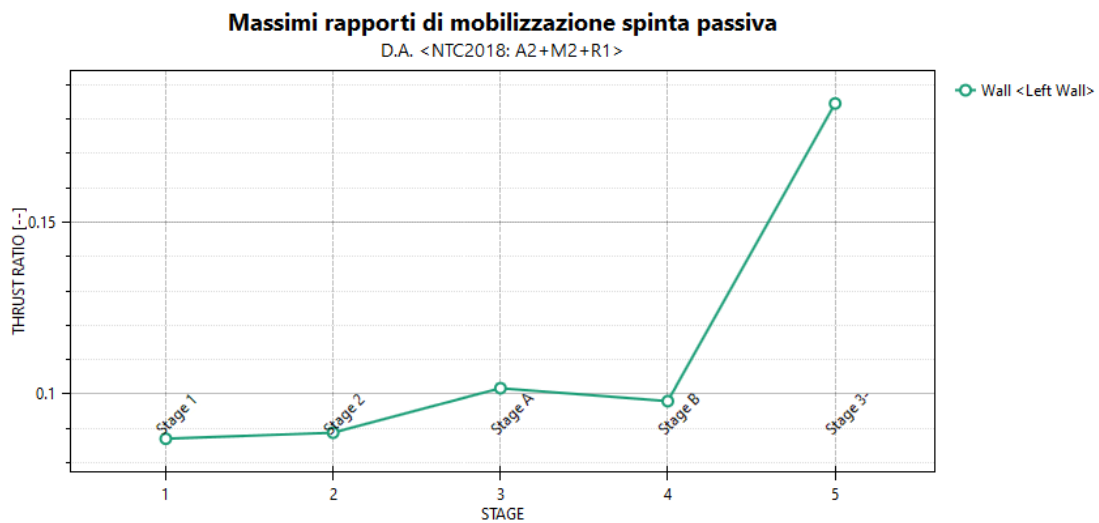


7.2 Verifiche SLE GEO

7.2.1 Modello con interasse tiranti di 2,4m

Le verifiche geotecniche sono svolte valutando il coefficiente di sicurezza in termini di rapporto di mobilitazione della spinta passiva, cioè come rapporto tra spinta passiva mobilitata al piede della paratia e la spinta passiva mobilitabile. La verifica è soddisfatta se tale rapporto è inferiore all'unità.

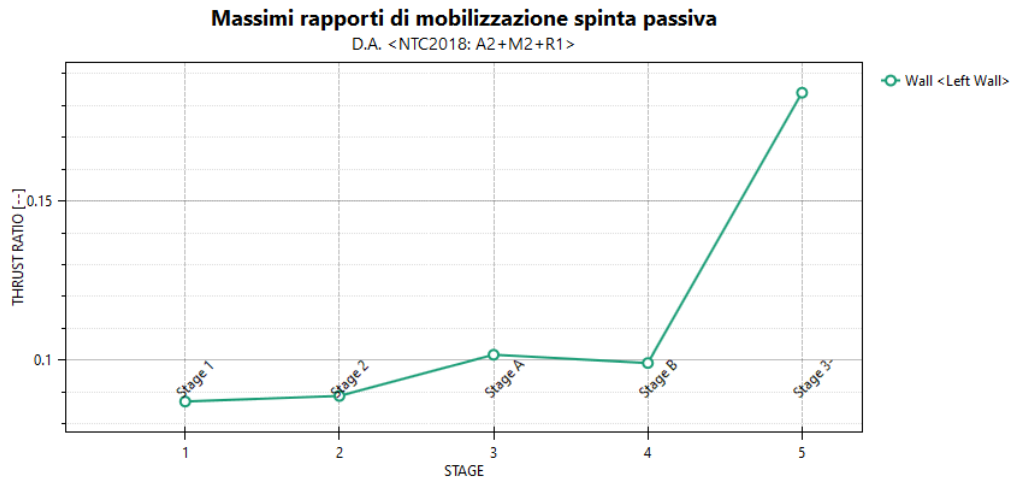
Il massimo rapporto di mobilitazione della spinta passiva è circa il 20%.



7.2.2 Modello con interasse tiranti di 4m

Le verifiche geotecniche sono svolte valutando il coefficiente di sicurezza in termini di rapporto di mobilitazione della spinta passiva, cioè come rapporto tra spinta passiva mobilitata al piede della paratia e la spinta passiva mobilitabile. La verifica è soddisfatta se tale rapporto è inferiore all'unità.

Il massimo rapporto di mobilitazione della spinta passiva è circa il 20%.



7.3 Risultati tiranti

7.3.1 Modello con interasse tiranti di 2,4m

Design Assumption:

Tiranti

| Tirante | Stage | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Sfruttamento GEO | Sfruttamento STR | Resistenza | Gerarchia delle Resistenze |
|-------------------|----------|---------------------|---------------------|---------------------|------------------|------------------|------------|----------------------------|
| Tieback_New_New_N | Stage B | 298.99 | 399.84 | 605.56 | 0.748 | 0.494 | ✓ | ✓ |
| Tieback_New_New_N | Stage 3- | 297.96 | 399.84 | 605.56 | 0.745 | 0.492 | ✓ | ✓ |

7.3.2 Modello con interasse tiranti di 4m

Design Assumption:

Tiranti

| Tirante | Stage | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Sfruttamento GEO | Sfruttamento STR | Resistenza | Gerarchia delle Resistenze |
|-------------------|----------|---------------------|---------------------|---------------------|------------------|------------------|------------|----------------------------|
| Tieback_New_New_N | Stage B | 230 | 399.84 | 605.56 | 0.575 | 0.38 | ✓ | ✓ |
| Tieback_New_New_N | Stage 3- | 230.07 | 399.84 | 605.56 | 0.575 | 0.38 | ✓ | ✓ |

7.4 Risultati trave di ripartizione

7.4.1 Modello con interasse tiranti di 2,4m

Design Assumption:

Tiranti Puntoni Travi di Ripartizione in Acciaio Travi di Ripartizione in Calcestruzzo

| Trave di Ripartizione | Connessione | Sezione | Materiale | Passo orizz. (m) | D.A. | Stage | Carico distribuito (kN/m) | Azione Assiale (kN) | Sfruttamento M-N | Sfruttamento Taglio | Instabilità |
|-----------------------|---------------|---------|-----------|------------------|---------------|----------|---------------------------|---------------------|------------------|---------------------|-------------|
| Default Waler | Tieback_New_N | HE 160B | S355 | 2.4 | NTC2018: A1+I | Stage B | 124.58 | 0 | 0.42 | 0.28 | 0 |
| Default Waler | Tieback_New_N | HE 160B | S355 | 2.4 | NTC2018: A1+I | Stage 3- | 124.15 | 0 | 0.418 | 0.279 | 0 |

7.4.2 Modello con interasse tiranti di 4m

Design Assumption:

Tiranti Puntoni Travi di Ripartizione in Acciaio Travi di Ripartizione in Calcestruzzo

| Trave di Ripartizione | Connessione | Sezione | Materiale | Passo orizz. (m) | D.A. | Stage | Carico distribuito (kN/m) | Azione Assiale (kN) | Sfruttamento M-N | Sfruttamento Taglio | Instabilità |
|-----------------------|---------------|---------|-----------|------------------|---------------|----------|---------------------------|---------------------|------------------|---------------------|-------------|
| Default Waler | Tieback_New_N | HE 160B | S355 | 4 | NTC2018: A2+I | Stage B | 57.5 | 0 | 0.538 | 0.215 | 0 |
| Default Waler | Tieback_New_N | HE 160B | S355 | 4 | NTC2018: A2+I | Stage 3- | 57.518 | 0 | 0.538 | 0.215 | 0 |

8 VERIFICHE DEL CORDOLO

Le caratteristiche della sollecitazione sono determinate modellando gli elementi strutturali oggetto di verifica alla stregua di travi continue su più appoggi; la luce delle campate è data dall'interasse dei pali ed il carico, uniformemente distribuito, è determinato ripartendo il taglio sollecitante a metro lineare alla quota inferiore del cordolo, ottenute del modello di calcolo dell'opera di sostegno. Per essere più cautelativi lo schema considerato non è quello di una trave su più appoggi, ma quello ad una sola campata con luce pari a due volte l'interasse dei pali, in modo da considerare il cordolo sollecitato anche nel caso in cui un palo non è stato opportunamente ancorato. Secondo tale modello le massime azioni di calcolo sull'elemento strutturale saranno le seguenti:

$$M_{ed} = \frac{q_{ed} \cdot l^2}{8} \quad V_{ed} = \frac{q_{ed} \cdot l}{2}$$

| Elemento | Inviluppo SLU | | | SLE frequente | | | SLU | SLE | Luce |
|----------------|---------------|----------|----------|---------------|----------|----------|--------------|--------------|-------------|
| | $M_{Y, Ed}$ | N_{ed} | V_{Ed} | $M_{, Ed}$ | V_{Ed} | N_{ed} | Ved | Ved | L |
| | [kNm] | [kN] | [kN] | [kNm] | [kN] | [kN] | [kN/m] | [kN/m] | [m] |
| Cordolo | 4.32 | 0.00 | 21.60 | 3.36 | 16.80 | 0.00 | 54.00 | 42.00 | 0.80 |

| GEOMETRIA | | | | VERIFICA A PRESSOFLESSIONE | | | | | FS | |
|----------------|---------|------|----------|----------------------------|--------------------|--------|------|----------|-----|--------------|
| Elemento | b | h | M_{ed} | Armature | As | c | d | M_{Rd} | | |
| | [mm] | [mm] | [kNm] | | [mm ²] | [mm] | [mm] | [kNm] | [-] | |
| Cordolo | Lato DX | 500 | 500 | 4.3 | 3 ϕ 16 | 603.19 | 60 | 440 | 103 | 23.84 |
| | Lato SX | | | | 3 ϕ 16 | 603.19 | 60 | | | |

| Elemento | Armature trasversali | | | Taglio Trazione | | FS | |
|----------------|----------------------|-------------|-----------|--------------------------------|-------------------|--------|-------------|
| | n_b | \emptyset | p (mm) | A_{sw} (mm ²) | V_{Rsd} (KN) | | V_{rd} |
| Cordolo | 2 | 8 | 200 | 100.53 | 194.72 | 194.72 | 9.02 |

| Verifica delle tensioni | M_{ed} | σ_c | $0,6 f_{ck}$ | FS | σ_f | $0,8 f_{yk}$ | FS |
|-------------------------|----------|------------|--------------|--------------|------------|--------------|--------------|
| | [kNm] | [Mpa] | [Mpa] | [-] | [Mpa] | [Mpa] | [-] |
| Comb. Rara | 3.4 | 0.30 | 19.9 | 66.40 | 17.00 | 360.0 | 21.18 |

| Verifica delle tensioni | M_{ed} | σ_c | $0,45 f_{ck}$ | FS |
|-------------------------|----------|------------|---------------|--------------|
| | [kNm] | [Mpa] | [Mpa] | [-] |
| Comb. Q.Perm. | 3.4 | 0.30 | 14.9 | 49.80 |

| Verifica delle tensioni | M_{ed} | σ_f | Kt | x_c | $h_{c,eff}$ | peff | ϵ_{sm} | ϕ_{eq} | K1 | K2 | $\Delta_{s,max}$ | w_f | w_1 | FS |
|-------------------------|----------|------------|-----|-------|-------------|------|-----------------|-------------|-----|-----|------------------|-------|-------|-------------|
| | [kNm] | [Mpa] | | mm | mm | | | | | | mm | mm | mm | mm |
| Comb. Q. Perm. | 3.4 | 17.00 | 0.4 | 103 | 132 | 0.01 | 0.00 | 16 | 0.8 | 0.5 | 475 | 0.039 | 0.20 | 5.10 |
| Comb. Freq. | 3.4 | 17.00 | | 103 | 132 | 0.01 | 0.00 | 16 | | | 475 | 0.039 | 0.30 | 7.65 |

9 ALLEGATO 1: tabulato di calcolo paratia (interasse tiranti 2.4 m)

Descrizione della Stratigrafia e degli Strati di Terreno

Tipo : POLYLINE

Punti

(-30;0)
(10;0)
(20;0)
(20;-40)
(-30;-40)

OCR : 1

Tipo : POLYLINE

Punti

(-30;-2)
(20;-2)
(20;-20)
(-30;-20)

OCR : 1

| Strato di Terreno | Terreno | γ dry | γ sat | ϕ' | ϕ | c | S_u | Modulo | Elastico | E_u | E_{vc} | E_{ur} | A_h | A_{vexp} | P_a | R_{ur}/R_{vc} | R_{vc} | K_u | K_{vc} | K_{ur} | |
|-------------------|----------|--------------|--------------|----------|----------|-------|-------|----------|----------|-------|----------|----------|-------|------------|-------|-----------------|----------|----------|----------|----------|--|
| | | kN/m^3 | kN/m^3 | $^\circ$ | $^\circ$ | kPa | kPa | | | | kPa | kPa | | | kPa | | kPa | kN/m^3 | kN/m^3 | kN/m^3 | |
| 1 | RILEVATO | 19 | 19 | 35 | | 0 | | Constant | | | 50000 | 80000 | | | | | | | | | |
| 2 | unità SR | 24.5 | 24.5 | 40 | | 40 | | Constant | | | 150000 | 240000 | | | | | | | | | |

Descrizione Pareti

X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Muro di sinistra

Sezione : mc 240 inter 40 cm

Area equivalente : 0.0294745535317205 m

Inerzia equivalente : 0.0001 m⁴/m

Materiale calcestruzzo : C25/30

Tipo sezione : Tangent

Spaziatura : 0.4 m

Diametro : 0.24 m

Efficacia : 1

Materiale acciaio : S355

Sezione : CHS168.3*12

Tipo sezione : O

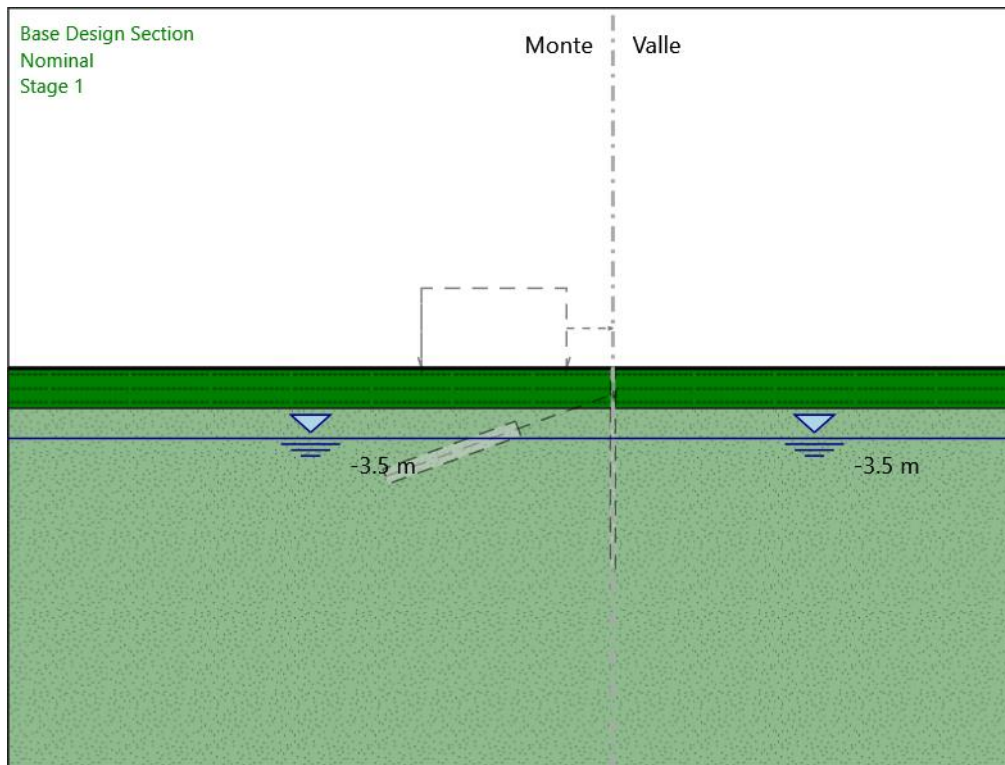
Spaziatura : 0.4 m

Spessore : 0.012 m

Diametro : 0.1683 m

Fasi di Calcolo

Stage 1



Stage 1

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : 0 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

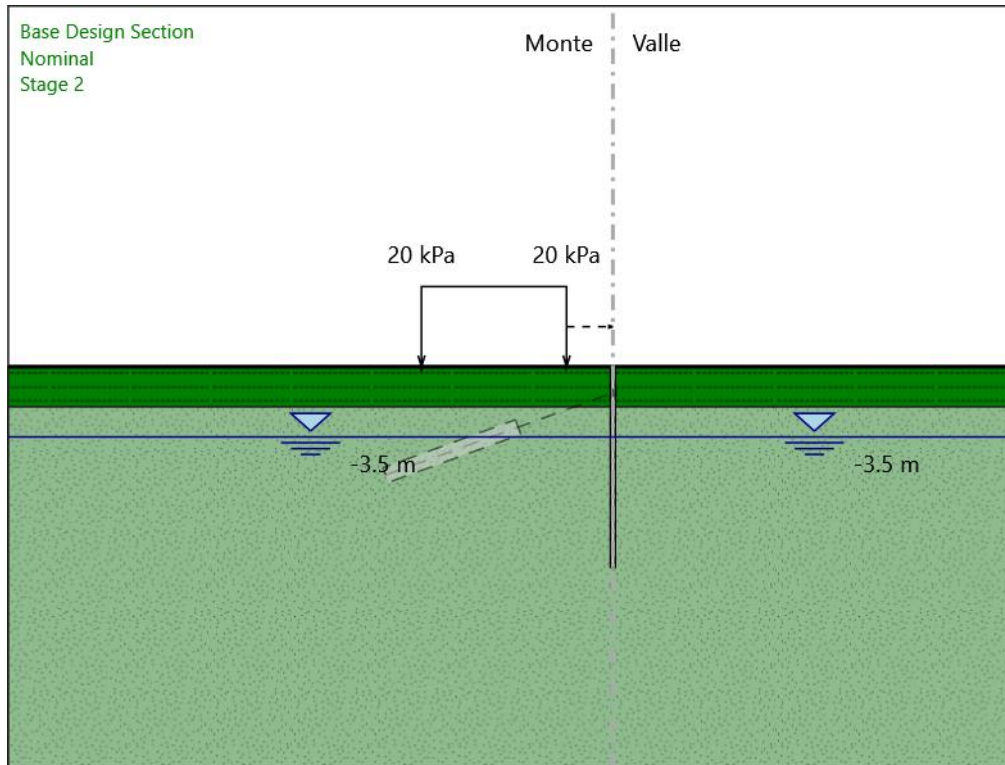
0 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -3.5 m

Stage 2



Stage 2

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : 0 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

0 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -3.5 m

Carichi

Carico lineare in superficie : SurfaceSurcharge

X iniziale : -9.5 m

X finale : -2.3 m

Pressione iniziale : 20 kPa

Pressione finale : 20 kPa

Elementi strutturali

Paratia : paratia sx

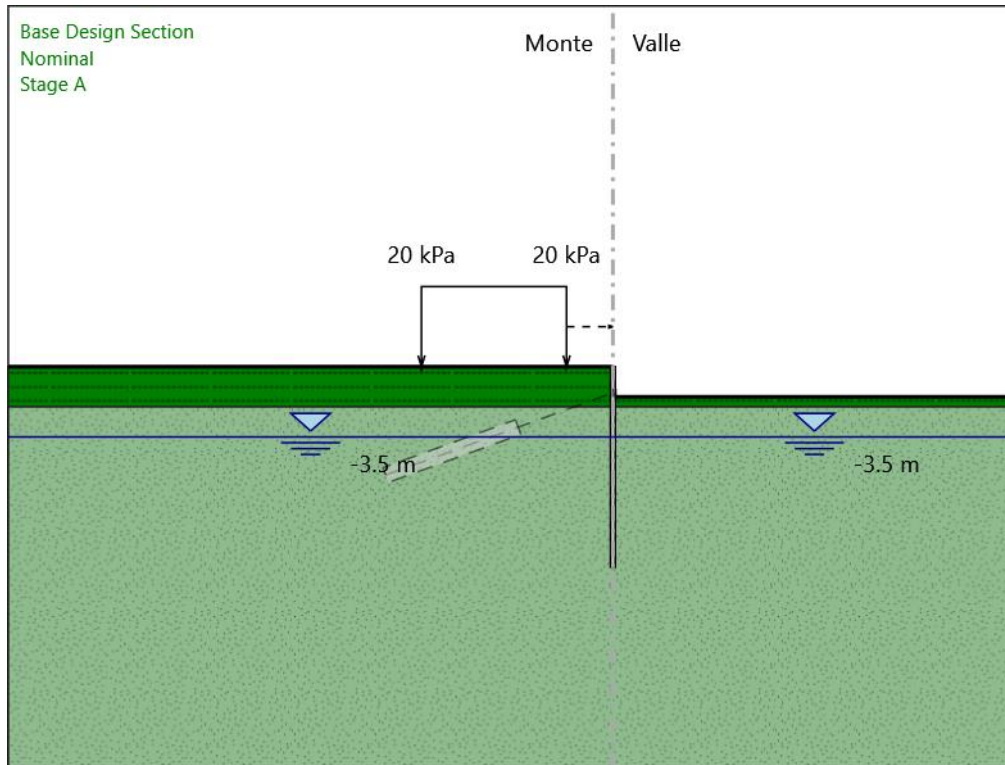
X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Sezione : mc 240 inter 40 cm

Stage A



Stage A

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : -1.5 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

-1.5 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -3.5 m

Carichi

Carico lineare in superficie : SurfaceSurcharge

X iniziale : -9.5 m

X finale : -2.3 m

Pressione iniziale : 20 kPa

Pressione finale : 20 kPa

Elementi strutturali

Paratia : paratia sx

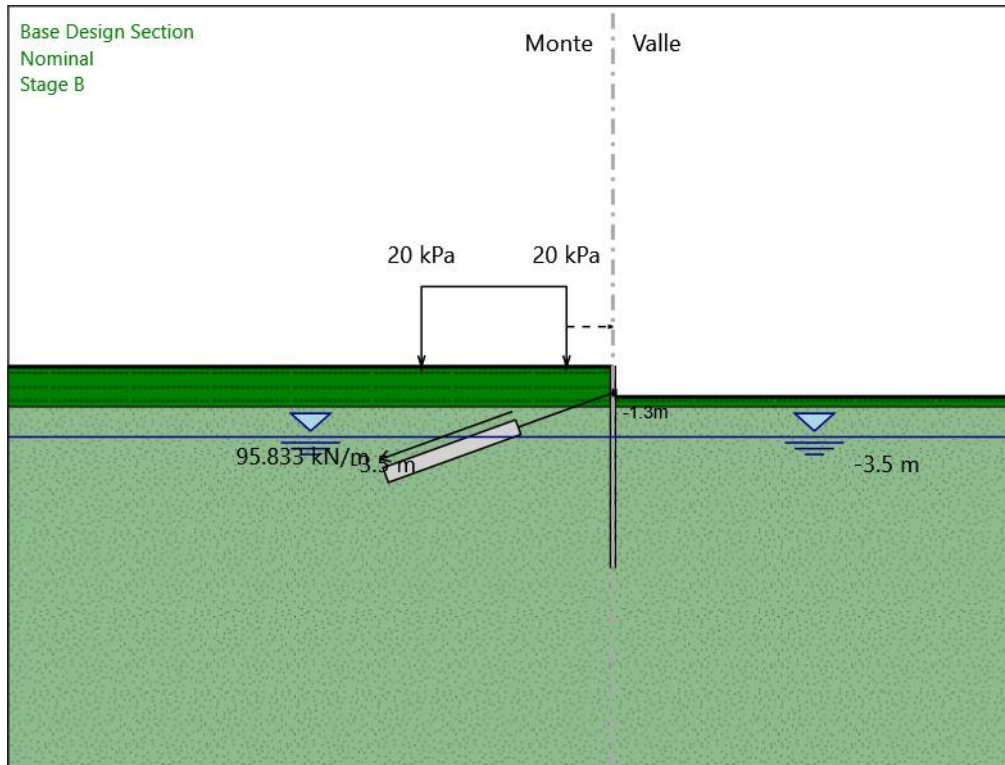
X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Sezione : mc 240 inter 40 cm

Stage B



Stage B

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : -1.5 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

-1.5 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -3.5 m

Carichi

Carico lineare in superficie : SurfaceSurcharge

X iniziale : -9.5 m

X finale : -2.3 m

Pressione iniziale : 20 kPa

Pressione finale : 20 kPa

Elementi strutturali

Paratia : paratia sx

X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Sezione : mc 240 inter 40 cm

Tirante : Tieback_New_New_New_New

X : 0 m

Z : -1.3 m

Lunghezza bulbo : 7 m

Diametro bulbo : 0.2 m

Lunghezza libera : 5 m

Spaziatura orizzontale : 2.4 m

Precarico : 230 kN

Angolo : 20 °

Sezione : 3 strands

Tipo di barre : Barre trefoli

Numero di barre : 3

Diametro : 0.01331 m

Area : 0.000417 m²

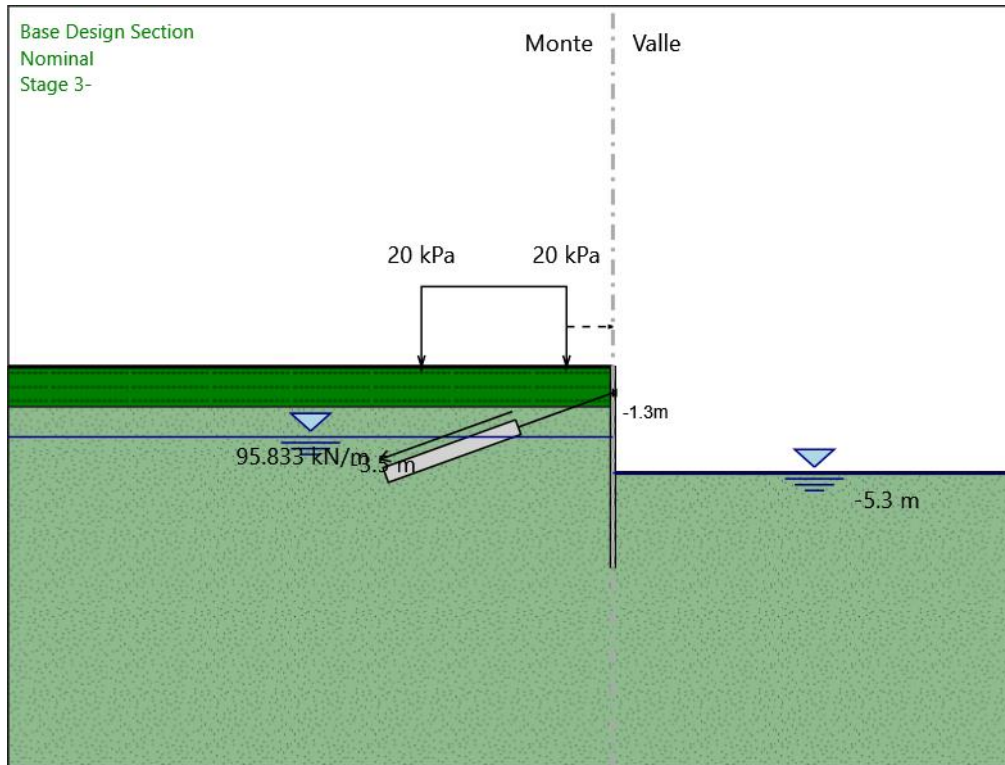
Trave di Ripartizione : Default Waler

Sezione : Waler Section 2 steel

HE 160B

Materiale : S355

Stage 3-



Stage 3-

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : -5.3 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

-5.3 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -5.3 m

Carichi

Carico lineare in superficie : SurfaceSurcharge

X iniziale : -9.5 m

X finale : -2.3 m

Pressione iniziale : 20 kPa

Pressione finale : 20 kPa

Elementi strutturali

Paratia : paratia sx

X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Sezione : mc 240 inter 40 cm

Tirante : Tieback_New_New_New_New

X : 0 m

Z : -1.3 m

Lunghezza bulbo : 7 m

Diametro bulbo : 0.2 m

Lunghezza libera : 5 m

Spaziatura orizzontale : 2.4 m

Precarico : 230 kN

Angolo : 20 °

Sezione : 3 strands

Tipo di barre : Barre trefoli

Numero di barre : 3

Diametro : 0.01331 m

Area : 0.000417 m²

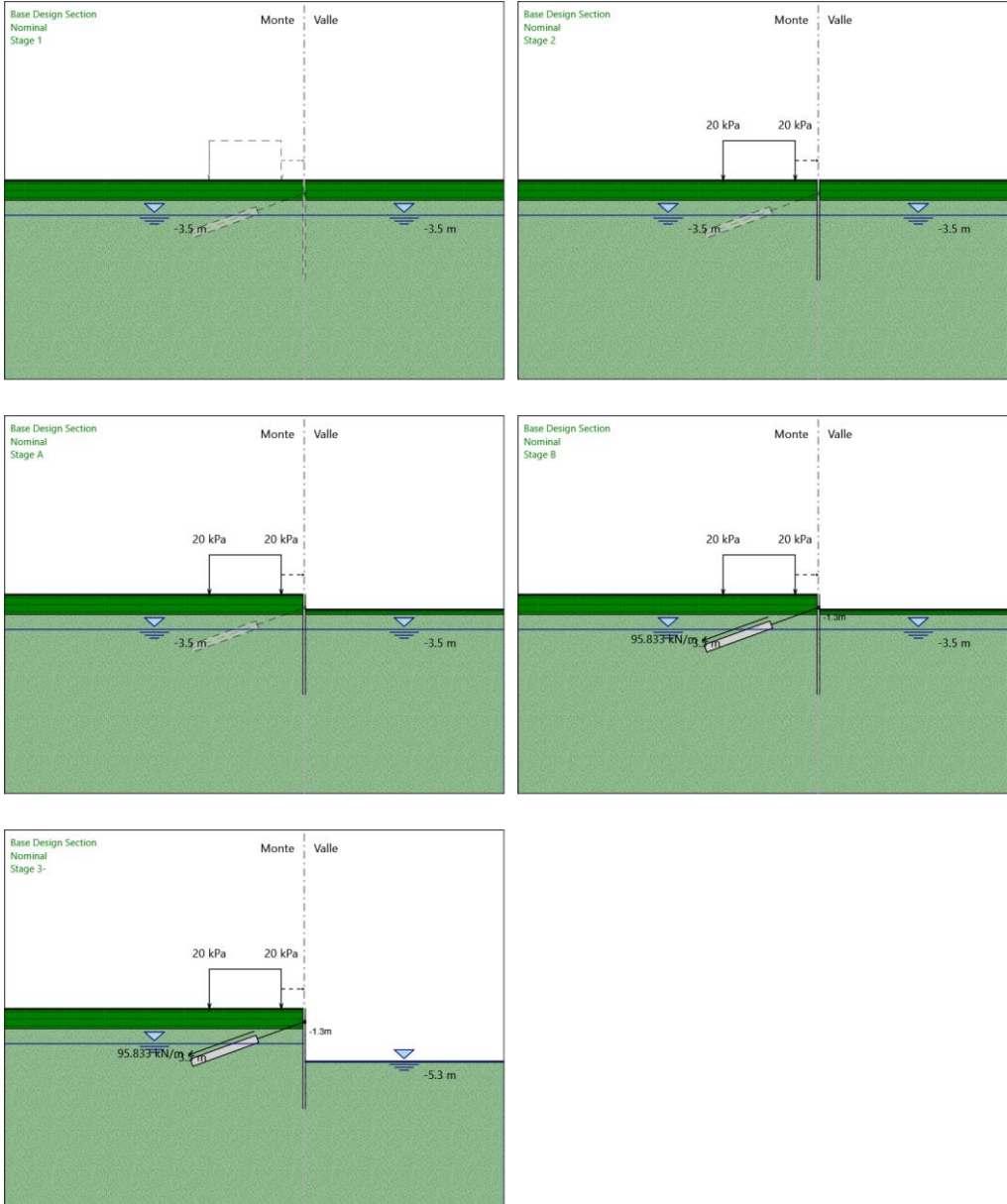
Trave di Ripartizione : Default Waler

Sezione : Waler Section 2 steel

HE 160B

Materiale : S355

Tabella Configurazione Stage (Nominal)



Grafici dei Risultati

Design Assumption : Nominal

Tabella Spostamento Nominal - LEFT Stage: Stage 1

| Design Assumption: Nominal | Tipo Risultato: Spostamento | Muro: LEFT |
|----------------------------|-----------------------------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 1 | 0 | 0 |
| Stage 1 | -0.1 | 0 |
| Stage 1 | -0.2 | 0 |
| Stage 1 | -0.3 | 0 |
| Stage 1 | -0.4 | 0 |
| Stage 1 | -0.5 | 0 |
| Stage 1 | -0.6 | 0 |
| Stage 1 | -0.7 | 0 |
| Stage 1 | -0.8 | 0 |
| Stage 1 | -0.9 | 0 |
| Stage 1 | -1 | 0 |
| Stage 1 | -1.1 | 0 |
| Stage 1 | -1.2 | 0 |
| Stage 1 | -1.3 | 0 |
| Stage 1 | -1.4 | 0 |
| Stage 1 | -1.5 | 0 |
| Stage 1 | -1.6 | 0 |
| Stage 1 | -1.7 | 0 |
| Stage 1 | -1.8 | 0 |
| Stage 1 | -1.9 | 0 |
| Stage 1 | -2 | 0 |
| Stage 1 | -2.1 | 0 |
| Stage 1 | -2.2 | 0 |
| Stage 1 | -2.3 | 0 |
| Stage 1 | -2.4 | 0 |
| Stage 1 | -2.5 | 0 |
| Stage 1 | -2.6 | 0 |
| Stage 1 | -2.7 | 0 |
| Stage 1 | -2.8 | 0 |
| Stage 1 | -2.9 | 0 |
| Stage 1 | -3 | 0 |
| Stage 1 | -3.1 | 0 |
| Stage 1 | -3.2 | 0 |
| Stage 1 | -3.3 | 0 |
| Stage 1 | -3.4 | 0 |
| Stage 1 | -3.5 | 0 |
| Stage 1 | -3.6 | 0 |
| Stage 1 | -3.7 | 0 |
| Stage 1 | -3.8 | 0 |
| Stage 1 | -3.9 | 0 |
| Stage 1 | -4 | 0 |
| Stage 1 | -4.1 | 0 |
| Stage 1 | -4.2 | 0 |
| Stage 1 | -4.3 | 0 |
| Stage 1 | -4.4 | 0 |
| Stage 1 | -4.5 | 0 |
| Stage 1 | -4.6 | 0 |
| Stage 1 | -4.7 | 0 |
| Stage 1 | -4.8 | 0 |
| Stage 1 | -4.9 | 0 |
| Stage 1 | -5 | 0 |
| Stage 1 | -5.1 | 0 |
| Stage 1 | -5.2 | 0 |
| Stage 1 | -5.3 | 0 |

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 1 | -5.4 | 0 |
| Stage 1 | -5.5 | 0 |
| Stage 1 | -5.6 | 0 |
| Stage 1 | -5.7 | 0 |
| Stage 1 | -5.8 | 0 |
| Stage 1 | -5.9 | 0 |
| Stage 1 | -6 | 0 |
| Stage 1 | -6.1 | 0 |
| Stage 1 | -6.2 | 0 |
| Stage 1 | -6.3 | 0 |
| Stage 1 | -6.4 | 0 |
| Stage 1 | -6.5 | 0 |
| Stage 1 | -6.6 | 0 |
| Stage 1 | -6.7 | 0 |
| Stage 1 | -6.8 | 0 |
| Stage 1 | -6.9 | 0 |
| Stage 1 | -7 | 0 |
| Stage 1 | -7.1 | 0 |
| Stage 1 | -7.2 | 0 |
| Stage 1 | -7.3 | 0 |
| Stage 1 | -7.4 | 0 |
| Stage 1 | -7.5 | 0 |
| Stage 1 | -7.6 | 0 |
| Stage 1 | -7.7 | 0 |
| Stage 1 | -7.8 | 0 |
| Stage 1 | -7.9 | 0 |
| Stage 1 | -8 | 0 |
| Stage 1 | -8.1 | 0 |
| Stage 1 | -8.2 | 0 |
| Stage 1 | -8.3 | 0 |
| Stage 1 | -8.4 | 0 |
| Stage 1 | -8.5 | 0 |
| Stage 1 | -8.6 | 0 |
| Stage 1 | -8.7 | 0 |
| Stage 1 | -8.8 | 0 |
| Stage 1 | -8.9 | 0 |
| Stage 1 | -9 | 0 |
| Stage 1 | -9.1 | 0 |
| Stage 1 | -9.2 | 0 |
| Stage 1 | -9.3 | 0 |
| Stage 1 | -9.4 | 0 |
| Stage 1 | -9.5 | 0 |
| Stage 1 | -9.6 | 0 |
| Stage 1 | -9.7 | 0 |
| Stage 1 | -9.8 | 0 |
| Stage 1 | -9.9 | 0 |
| Stage 1 | -10 | 0 |

Tabella Spostamento Nominal - LEFT Stage: Stage 2

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 2 | 0 | 0 |
| Stage 2 | -0.1 | 0 |
| Stage 2 | -0.2 | 0 |
| Stage 2 | -0.3 | 0 |
| Stage 2 | -0.4 | 0 |
| Stage 2 | -0.5 | 0 |
| Stage 2 | -0.6 | 0 |
| Stage 2 | -0.7 | 0 |
| Stage 2 | -0.8 | 0 |
| Stage 2 | -0.9 | 0 |
| Stage 2 | -1 | 0 |
| Stage 2 | -1.1 | 0 |
| Stage 2 | -1.2 | 0 |
| Stage 2 | -1.3 | 0 |
| Stage 2 | -1.4 | 0 |
| Stage 2 | -1.5 | 0 |
| Stage 2 | -1.6 | 0 |
| Stage 2 | -1.7 | 0 |
| Stage 2 | -1.8 | 0 |
| Stage 2 | -1.9 | 0 |
| Stage 2 | -2 | 0 |
| Stage 2 | -2.1 | 0 |
| Stage 2 | -2.2 | 0 |
| Stage 2 | -2.3 | 0 |
| Stage 2 | -2.4 | 0 |
| Stage 2 | -2.5 | 0 |
| Stage 2 | -2.6 | 0 |
| Stage 2 | -2.7 | 0 |
| Stage 2 | -2.8 | 0 |
| Stage 2 | -2.9 | 0 |
| Stage 2 | -3 | 0 |
| Stage 2 | -3.1 | 0 |
| Stage 2 | -3.2 | 0 |
| Stage 2 | -3.3 | 0 |
| Stage 2 | -3.4 | 0 |
| Stage 2 | -3.5 | 0 |
| Stage 2 | -3.6 | 0 |
| Stage 2 | -3.7 | 0 |
| Stage 2 | -3.8 | 0 |
| Stage 2 | -3.9 | 0 |
| Stage 2 | -4 | 0 |
| Stage 2 | -4.1 | 0.01 |
| Stage 2 | -4.2 | 0.01 |
| Stage 2 | -4.3 | 0.01 |
| Stage 2 | -4.4 | 0.01 |
| Stage 2 | -4.5 | 0.01 |
| Stage 2 | -4.6 | 0.01 |
| Stage 2 | -4.7 | 0.01 |
| Stage 2 | -4.8 | 0.01 |
| Stage 2 | -4.9 | 0.01 |
| Stage 2 | -5 | 0.01 |
| Stage 2 | -5.1 | 0.01 |
| Stage 2 | -5.2 | 0.01 |
| Stage 2 | -5.3 | 0.01 |
| Stage 2 | -5.4 | 0.01 |
| Stage 2 | -5.5 | 0.01 |
| Stage 2 | -5.6 | 0.01 |
| Stage 2 | -5.7 | 0.01 |
| Stage 2 | -5.8 | 0.01 |
| Stage 2 | -5.9 | 0.01 |
| Stage 2 | -6 | 0.01 |

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 2 | -6.1 | 0.01 |
| Stage 2 | -6.2 | 0.01 |
| Stage 2 | -6.3 | 0.01 |
| Stage 2 | -6.4 | 0.01 |
| Stage 2 | -6.5 | 0.01 |
| Stage 2 | -6.6 | 0.01 |
| Stage 2 | -6.7 | 0.01 |
| Stage 2 | -6.8 | 0.01 |
| Stage 2 | -6.9 | 0.01 |
| Stage 2 | -7 | 0.01 |
| Stage 2 | -7.1 | 0.01 |
| Stage 2 | -7.2 | 0.01 |
| Stage 2 | -7.3 | 0.01 |
| Stage 2 | -7.4 | 0.01 |
| Stage 2 | -7.5 | 0.01 |
| Stage 2 | -7.6 | 0.01 |
| Stage 2 | -7.7 | 0.01 |
| Stage 2 | -7.8 | 0.01 |
| Stage 2 | -7.9 | 0.01 |
| Stage 2 | -8 | 0.01 |
| Stage 2 | -8.1 | 0.01 |
| Stage 2 | -8.2 | 0.01 |
| Stage 2 | -8.3 | 0.01 |
| Stage 2 | -8.4 | 0.01 |
| Stage 2 | -8.5 | 0.01 |
| Stage 2 | -8.6 | 0.01 |
| Stage 2 | -8.7 | 0.01 |
| Stage 2 | -8.8 | 0.01 |
| Stage 2 | -8.9 | 0.01 |
| Stage 2 | -9 | 0.01 |
| Stage 2 | -9.1 | 0.01 |
| Stage 2 | -9.2 | 0.01 |
| Stage 2 | -9.3 | 0.01 |
| Stage 2 | -9.4 | 0.01 |
| Stage 2 | -9.5 | 0.01 |
| Stage 2 | -9.6 | 0.01 |
| Stage 2 | -9.7 | 0.01 |
| Stage 2 | -9.8 | 0.01 |
| Stage 2 | -9.9 | 0.01 |
| Stage 2 | -10 | 0.01 |

Tabella Spostamento Nominal - LEFT Stage: Stage A

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage A | 0 | 1.15 |
| Stage A | -0.1 | 1.09 |
| Stage A | -0.2 | 1.04 |
| Stage A | -0.3 | 0.99 |
| Stage A | -0.4 | 0.94 |
| Stage A | -0.5 | 0.88 |
| Stage A | -0.6 | 0.83 |
| Stage A | -0.7 | 0.78 |
| Stage A | -0.8 | 0.73 |
| Stage A | -0.9 | 0.68 |
| Stage A | -1 | 0.63 |
| Stage A | -1.1 | 0.57 |
| Stage A | -1.2 | 0.52 |
| Stage A | -1.3 | 0.48 |
| Stage A | -1.4 | 0.43 |
| Stage A | -1.5 | 0.38 |
| Stage A | -1.6 | 0.34 |
| Stage A | -1.7 | 0.29 |
| Stage A | -1.8 | 0.25 |
| Stage A | -1.9 | 0.21 |
| Stage A | -2 | 0.18 |
| Stage A | -2.1 | 0.15 |
| Stage A | -2.2 | 0.12 |
| Stage A | -2.3 | 0.09 |
| Stage A | -2.4 | 0.07 |
| Stage A | -2.5 | 0.06 |
| Stage A | -2.6 | 0.04 |
| Stage A | -2.7 | 0.03 |
| Stage A | -2.8 | 0.02 |
| Stage A | -2.9 | 0.02 |
| Stage A | -3 | 0.01 |
| Stage A | -3.1 | 0.01 |
| Stage A | -3.2 | 0.01 |
| Stage A | -3.3 | 0.01 |
| Stage A | -3.4 | 0.01 |
| Stage A | -3.5 | 0.01 |
| Stage A | -3.6 | 0.01 |
| Stage A | -3.7 | 0.01 |
| Stage A | -3.8 | 0.01 |
| Stage A | -3.9 | 0.02 |
| Stage A | -4 | 0.02 |
| Stage A | -4.1 | 0.02 |
| Stage A | -4.2 | 0.02 |
| Stage A | -4.3 | 0.02 |
| Stage A | -4.4 | 0.02 |
| Stage A | -4.5 | 0.02 |
| Stage A | -4.6 | 0.03 |
| Stage A | -4.7 | 0.03 |
| Stage A | -4.8 | 0.03 |
| Stage A | -4.9 | 0.03 |
| Stage A | -5 | 0.03 |
| Stage A | -5.1 | 0.03 |
| Stage A | -5.2 | 0.03 |
| Stage A | -5.3 | 0.03 |
| Stage A | -5.4 | 0.03 |
| Stage A | -5.5 | 0.03 |
| Stage A | -5.6 | 0.03 |
| Stage A | -5.7 | 0.03 |
| Stage A | -5.8 | 0.03 |
| Stage A | -5.9 | 0.03 |
| Stage A | -6 | 0.03 |

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage A | -6.1 | 0.03 |
| Stage A | -6.2 | 0.03 |
| Stage A | -6.3 | 0.03 |
| Stage A | -6.4 | 0.03 |
| Stage A | -6.5 | 0.03 |
| Stage A | -6.6 | 0.03 |
| Stage A | -6.7 | 0.03 |
| Stage A | -6.8 | 0.03 |
| Stage A | -6.9 | 0.03 |
| Stage A | -7 | 0.03 |
| Stage A | -7.1 | 0.03 |
| Stage A | -7.2 | 0.03 |
| Stage A | -7.3 | 0.03 |
| Stage A | -7.4 | 0.03 |
| Stage A | -7.5 | 0.03 |
| Stage A | -7.6 | 0.03 |
| Stage A | -7.7 | 0.03 |
| Stage A | -7.8 | 0.03 |
| Stage A | -7.9 | 0.03 |
| Stage A | -8 | 0.03 |
| Stage A | -8.1 | 0.03 |
| Stage A | -8.2 | 0.03 |
| Stage A | -8.3 | 0.03 |
| Stage A | -8.4 | 0.03 |
| Stage A | -8.5 | 0.03 |
| Stage A | -8.6 | 0.03 |
| Stage A | -8.7 | 0.03 |
| Stage A | -8.8 | 0.03 |
| Stage A | -8.9 | 0.03 |
| Stage A | -9 | 0.03 |
| Stage A | -9.1 | 0.03 |
| Stage A | -9.2 | 0.03 |
| Stage A | -9.3 | 0.03 |
| Stage A | -9.4 | 0.03 |
| Stage A | -9.5 | 0.03 |
| Stage A | -9.6 | 0.03 |
| Stage A | -9.7 | 0.03 |
| Stage A | -9.8 | 0.03 |
| Stage A | -9.9 | 0.03 |
| Stage A | -10 | 0.03 |

Tabella Spostamento Nominal - LEFT Stage: Stage B

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage B | 0 | 0.03 |
| Stage B | -0.1 | 0 |
| Stage B | -0.2 | -0.03 |
| Stage B | -0.3 | -0.06 |
| Stage B | -0.4 | -0.09 |
| Stage B | -0.5 | -0.12 |
| Stage B | -0.6 | -0.16 |
| Stage B | -0.7 | -0.19 |
| Stage B | -0.8 | -0.21 |
| Stage B | -0.9 | -0.24 |
| Stage B | -1 | -0.26 |
| Stage B | -1.1 | -0.28 |
| Stage B | -1.2 | -0.29 |
| Stage B | -1.3 | -0.29 |
| Stage B | -1.4 | -0.29 |
| Stage B | -1.5 | -0.27 |
| Stage B | -1.6 | -0.25 |
| Stage B | -1.7 | -0.23 |
| Stage B | -1.8 | -0.2 |
| Stage B | -1.9 | -0.18 |
| Stage B | -2 | -0.15 |
| Stage B | -2.1 | -0.12 |
| Stage B | -2.2 | -0.1 |
| Stage B | -2.3 | -0.07 |
| Stage B | -2.4 | -0.05 |
| Stage B | -2.5 | -0.03 |
| Stage B | -2.6 | -0.02 |
| Stage B | -2.7 | 0 |
| Stage B | -2.8 | 0.01 |
| Stage B | -2.9 | 0.02 |
| Stage B | -3 | 0.02 |
| Stage B | -3.1 | 0.03 |
| Stage B | -3.2 | 0.03 |
| Stage B | -3.3 | 0.04 |
| Stage B | -3.4 | 0.04 |
| Stage B | -3.5 | 0.04 |
| Stage B | -3.6 | 0.04 |
| Stage B | -3.7 | 0.04 |
| Stage B | -3.8 | 0.04 |
| Stage B | -3.9 | 0.04 |
| Stage B | -4 | 0.04 |
| Stage B | -4.1 | 0.03 |
| Stage B | -4.2 | 0.03 |
| Stage B | -4.3 | 0.03 |
| Stage B | -4.4 | 0.03 |
| Stage B | -4.5 | 0.03 |
| Stage B | -4.6 | 0.03 |
| Stage B | -4.7 | 0.03 |
| Stage B | -4.8 | 0.03 |
| Stage B | -4.9 | 0.03 |
| Stage B | -5 | 0.03 |
| Stage B | -5.1 | 0.03 |
| Stage B | -5.2 | 0.03 |
| Stage B | -5.3 | 0.03 |
| Stage B | -5.4 | 0.03 |
| Stage B | -5.5 | 0.03 |
| Stage B | -5.6 | 0.03 |
| Stage B | -5.7 | 0.03 |
| Stage B | -5.8 | 0.03 |
| Stage B | -5.9 | 0.03 |
| Stage B | -6 | 0.03 |

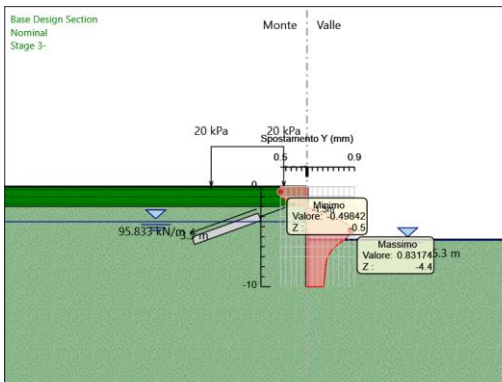
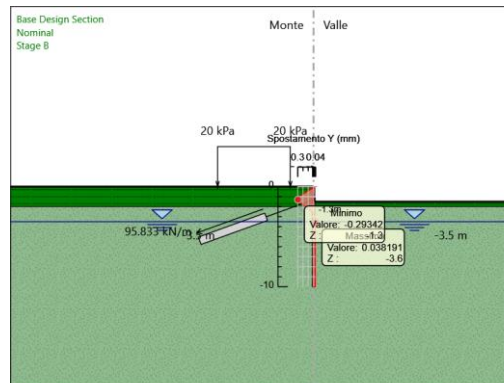
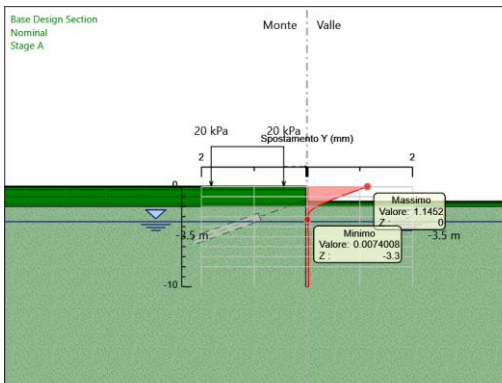
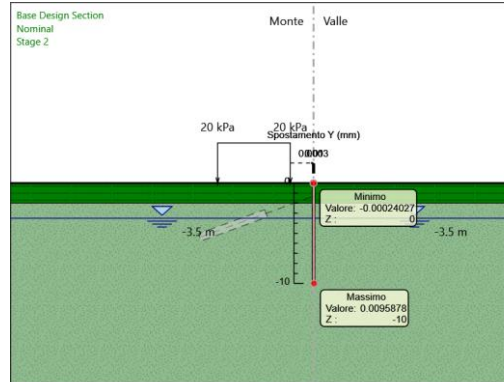
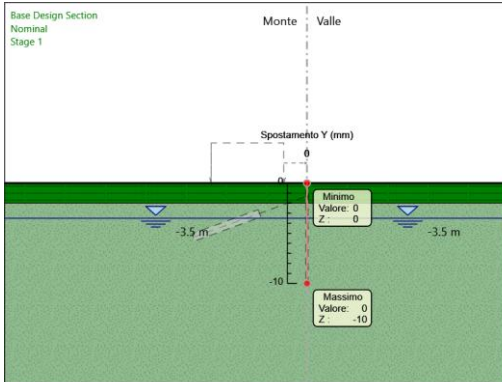
| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage B | -6.1 | 0.03 |
| Stage B | -6.2 | 0.03 |
| Stage B | -6.3 | 0.03 |
| Stage B | -6.4 | 0.03 |
| Stage B | -6.5 | 0.03 |
| Stage B | -6.6 | 0.03 |
| Stage B | -6.7 | 0.03 |
| Stage B | -6.8 | 0.03 |
| Stage B | -6.9 | 0.03 |
| Stage B | -7 | 0.03 |
| Stage B | -7.1 | 0.03 |
| Stage B | -7.2 | 0.03 |
| Stage B | -7.3 | 0.03 |
| Stage B | -7.4 | 0.03 |
| Stage B | -7.5 | 0.03 |
| Stage B | -7.6 | 0.03 |
| Stage B | -7.7 | 0.03 |
| Stage B | -7.8 | 0.03 |
| Stage B | -7.9 | 0.03 |
| Stage B | -8 | 0.03 |
| Stage B | -8.1 | 0.03 |
| Stage B | -8.2 | 0.03 |
| Stage B | -8.3 | 0.03 |
| Stage B | -8.4 | 0.03 |
| Stage B | -8.5 | 0.03 |
| Stage B | -8.6 | 0.03 |
| Stage B | -8.7 | 0.03 |
| Stage B | -8.8 | 0.03 |
| Stage B | -8.9 | 0.03 |
| Stage B | -9 | 0.03 |
| Stage B | -9.1 | 0.03 |
| Stage B | -9.2 | 0.03 |
| Stage B | -9.3 | 0.03 |
| Stage B | -9.4 | 0.03 |
| Stage B | -9.5 | 0.03 |
| Stage B | -9.6 | 0.03 |
| Stage B | -9.7 | 0.03 |
| Stage B | -9.8 | 0.03 |
| Stage B | -9.9 | 0.03 |
| Stage B | -10 | 0.03 |

Tabella Spostamento Nominal - LEFT Stage: Stage 3-

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 3- | 0 | -0.5 |
| Stage 3- | -0.1 | -0.5 |
| Stage 3- | -0.2 | -0.5 |
| Stage 3- | -0.3 | -0.5 |
| Stage 3- | -0.4 | -0.5 |
| Stage 3- | -0.5 | -0.5 |
| Stage 3- | -0.6 | -0.5 |
| Stage 3- | -0.7 | -0.5 |
| Stage 3- | -0.8 | -0.49 |
| Stage 3- | -0.9 | -0.49 |
| Stage 3- | -1 | -0.48 |
| Stage 3- | -1.1 | -0.46 |
| Stage 3- | -1.2 | -0.44 |
| Stage 3- | -1.3 | -0.42 |
| Stage 3- | -1.4 | -0.38 |
| Stage 3- | -1.5 | -0.33 |
| Stage 3- | -1.6 | -0.28 |
| Stage 3- | -1.7 | -0.23 |
| Stage 3- | -1.8 | -0.17 |
| Stage 3- | -1.9 | -0.11 |
| Stage 3- | -2 | -0.04 |
| Stage 3- | -2.1 | 0.02 |
| Stage 3- | -2.2 | 0.08 |
| Stage 3- | -2.3 | 0.14 |
| Stage 3- | -2.4 | 0.2 |
| Stage 3- | -2.5 | 0.25 |
| Stage 3- | -2.6 | 0.31 |
| Stage 3- | -2.7 | 0.36 |
| Stage 3- | -2.8 | 0.41 |
| Stage 3- | -2.9 | 0.46 |
| Stage 3- | -3 | 0.51 |
| Stage 3- | -3.1 | 0.55 |
| Stage 3- | -3.2 | 0.59 |
| Stage 3- | -3.3 | 0.63 |
| Stage 3- | -3.4 | 0.66 |
| Stage 3- | -3.5 | 0.69 |
| Stage 3- | -3.6 | 0.72 |
| Stage 3- | -3.7 | 0.75 |
| Stage 3- | -3.8 | 0.77 |
| Stage 3- | -3.9 | 0.79 |
| Stage 3- | -4 | 0.8 |
| Stage 3- | -4.1 | 0.82 |
| Stage 3- | -4.2 | 0.83 |
| Stage 3- | -4.3 | 0.83 |
| Stage 3- | -4.4 | 0.83 |
| Stage 3- | -4.5 | 0.83 |
| Stage 3- | -4.6 | 0.82 |
| Stage 3- | -4.7 | 0.82 |
| Stage 3- | -4.8 | 0.8 |
| Stage 3- | -4.9 | 0.79 |
| Stage 3- | -5 | 0.77 |
| Stage 3- | -5.1 | 0.75 |
| Stage 3- | -5.2 | 0.73 |
| Stage 3- | -5.3 | 0.7 |
| Stage 3- | -5.4 | 0.68 |
| Stage 3- | -5.5 | 0.65 |
| Stage 3- | -5.6 | 0.63 |
| Stage 3- | -5.7 | 0.61 |
| Stage 3- | -5.8 | 0.58 |
| Stage 3- | -5.9 | 0.56 |
| Stage 3- | -6 | 0.54 |

| Design Assumption: Nominal Tipo Risultato: Spostamento | Muro: LEFT | |
|--|------------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 3- | -6.1 | 0.52 |
| Stage 3- | -6.2 | 0.5 |
| Stage 3- | -6.3 | 0.48 |
| Stage 3- | -6.4 | 0.46 |
| Stage 3- | -6.5 | 0.45 |
| Stage 3- | -6.6 | 0.44 |
| Stage 3- | -6.7 | 0.42 |
| Stage 3- | -6.8 | 0.41 |
| Stage 3- | -6.9 | 0.4 |
| Stage 3- | -7 | 0.4 |
| Stage 3- | -7.1 | 0.39 |
| Stage 3- | -7.2 | 0.38 |
| Stage 3- | -7.3 | 0.38 |
| Stage 3- | -7.4 | 0.37 |
| Stage 3- | -7.5 | 0.37 |
| Stage 3- | -7.6 | 0.36 |
| Stage 3- | -7.7 | 0.36 |
| Stage 3- | -7.8 | 0.36 |
| Stage 3- | -7.9 | 0.35 |
| Stage 3- | -8 | 0.35 |
| Stage 3- | -8.1 | 0.35 |
| Stage 3- | -8.2 | 0.35 |
| Stage 3- | -8.3 | 0.34 |
| Stage 3- | -8.4 | 0.34 |
| Stage 3- | -8.5 | 0.34 |
| Stage 3- | -8.6 | 0.34 |
| Stage 3- | -8.7 | 0.34 |
| Stage 3- | -8.8 | 0.33 |
| Stage 3- | -8.9 | 0.33 |
| Stage 3- | -9 | 0.33 |
| Stage 3- | -9.1 | 0.33 |
| Stage 3- | -9.2 | 0.33 |
| Stage 3- | -9.3 | 0.33 |
| Stage 3- | -9.4 | 0.32 |
| Stage 3- | -9.5 | 0.32 |
| Stage 3- | -9.6 | 0.32 |
| Stage 3- | -9.7 | 0.32 |
| Stage 3- | -9.8 | 0.32 |
| Stage 3- | -9.9 | 0.31 |
| Stage 3- | -10 | 0.31 |

Grafici Spostamento in tabella



Involuppi Spostamento Nominal

Risultati Paratia

Tabella Risultati Paratia Nominal - Stage: Stage 1

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 1 | 0 | 0 | 0 |
| Stage 1 | -0.1 | 0 | 0 |
| Stage 1 | -0.2 | 0 | 0 |
| Stage 1 | -0.3 | 0 | 0 |
| Stage 1 | -0.4 | 0 | 0 |
| Stage 1 | -0.5 | 0 | 0 |
| Stage 1 | -0.6 | 0 | 0 |
| Stage 1 | -0.7 | 0 | 0 |
| Stage 1 | -0.8 | 0 | 0 |
| Stage 1 | -0.9 | 0 | 0 |
| Stage 1 | -1 | 0 | 0 |
| Stage 1 | -1.1 | 0 | 0 |
| Stage 1 | -1.2 | 0 | 0 |
| Stage 1 | -1.3 | 0 | 0 |
| Stage 1 | -1.4 | 0 | 0 |
| Stage 1 | -1.5 | 0 | 0 |
| Stage 1 | -1.6 | 0 | 0 |
| Stage 1 | -1.7 | 0 | 0 |
| Stage 1 | -1.8 | 0 | 0 |
| Stage 1 | -1.9 | 0 | 0 |
| Stage 1 | -2 | 0 | 0 |
| Stage 1 | -2.1 | 0 | 0 |
| Stage 1 | -2.2 | 0 | 0 |
| Stage 1 | -2.3 | 0 | 0 |
| Stage 1 | -2.4 | 0 | 0 |
| Stage 1 | -2.5 | 0 | 0 |
| Stage 1 | -2.6 | 0 | 0 |
| Stage 1 | -2.7 | 0 | 0 |
| Stage 1 | -2.8 | 0 | 0 |
| Stage 1 | -2.9 | 0 | 0 |
| Stage 1 | -3 | 0 | 0 |
| Stage 1 | -3.1 | 0 | 0 |
| Stage 1 | -3.2 | 0 | 0 |
| Stage 1 | -3.3 | 0 | 0 |
| Stage 1 | -3.4 | 0 | 0 |
| Stage 1 | -3.5 | 0 | 0 |
| Stage 1 | -3.6 | 0 | 0 |
| Stage 1 | -3.7 | 0 | 0 |
| Stage 1 | -3.8 | 0 | 0 |
| Stage 1 | -3.9 | 0 | 0 |
| Stage 1 | -4 | 0 | 0 |
| Stage 1 | -4.1 | 0 | 0 |
| Stage 1 | -4.2 | 0 | 0 |
| Stage 1 | -4.3 | 0 | 0 |
| Stage 1 | -4.4 | 0 | 0 |
| Stage 1 | -4.5 | 0 | 0 |
| Stage 1 | -4.6 | 0 | 0 |
| Stage 1 | -4.7 | 0 | 0 |
| Stage 1 | -4.8 | 0 | 0 |
| Stage 1 | -4.9 | 0 | 0 |
| Stage 1 | -5 | 0 | 0 |
| Stage 1 | -5.1 | 0 | 0 |
| Stage 1 | -5.2 | 0 | 0 |
| Stage 1 | -5.3 | 0 | 0 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 1 | -5.4 | 0 | 0 |
| Stage 1 | -5.5 | 0 | 0 |
| Stage 1 | -5.6 | 0 | 0 |
| Stage 1 | -5.7 | 0 | 0 |
| Stage 1 | -5.8 | 0 | 0 |
| Stage 1 | -5.9 | 0 | 0 |
| Stage 1 | -6 | 0 | 0 |
| Stage 1 | -6.1 | 0 | 0 |
| Stage 1 | -6.2 | 0 | 0 |
| Stage 1 | -6.3 | 0 | 0 |
| Stage 1 | -6.4 | 0 | 0 |
| Stage 1 | -6.5 | 0 | 0 |
| Stage 1 | -6.6 | 0 | 0 |
| Stage 1 | -6.7 | 0 | 0 |
| Stage 1 | -6.8 | 0 | 0 |
| Stage 1 | -6.9 | 0 | 0 |
| Stage 1 | -7 | 0 | 0 |
| Stage 1 | -7.1 | 0 | 0 |
| Stage 1 | -7.2 | 0 | 0 |
| Stage 1 | -7.3 | 0 | 0 |
| Stage 1 | -7.4 | 0 | 0 |
| Stage 1 | -7.5 | 0 | 0 |
| Stage 1 | -7.6 | 0 | 0 |
| Stage 1 | -7.7 | 0 | 0 |
| Stage 1 | -7.8 | 0 | 0 |
| Stage 1 | -7.9 | 0 | 0 |
| Stage 1 | -8 | 0 | 0 |
| Stage 1 | -8.1 | 0 | 0 |
| Stage 1 | -8.2 | 0 | 0 |
| Stage 1 | -8.3 | 0 | 0 |
| Stage 1 | -8.4 | 0 | 0 |
| Stage 1 | -8.5 | 0 | 0 |
| Stage 1 | -8.6 | 0 | 0 |
| Stage 1 | -8.7 | 0 | 0 |
| Stage 1 | -8.8 | 0 | 0 |
| Stage 1 | -8.9 | 0 | 0 |
| Stage 1 | -9 | 0 | 0 |
| Stage 1 | -9.1 | 0 | 0 |
| Stage 1 | -9.2 | 0 | 0 |
| Stage 1 | -9.3 | 0 | 0 |
| Stage 1 | -9.4 | 0 | 0 |
| Stage 1 | -9.5 | 0 | 0 |
| Stage 1 | -9.6 | 0 | 0 |
| Stage 1 | -9.7 | 0 | 0 |
| Stage 1 | -9.8 | 0 | 0 |
| Stage 1 | -9.9 | 0 | 0 |
| Stage 1 | -10 | 0 | 0 |

Tabella Risultati Paratia Nominal - Stage: Stage 2

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 2 | 0 | 0 | 0 |
| Stage 2 | -0.1 | 0 | 0 |
| Stage 2 | -0.1 | 0 | 0 |
| Stage 2 | -0.2 | 0 | 0 |
| Stage 2 | -0.3 | 0 | 0 |
| Stage 2 | -0.4 | 0 | 0 |
| Stage 2 | -0.5 | 0 | 0 |
| Stage 2 | -0.6 | 0 | 0.01 |
| Stage 2 | -0.7 | 0 | 0.01 |
| Stage 2 | -0.8 | 0 | 0.02 |
| Stage 2 | -0.9 | 0.01 | 0.02 |
| Stage 2 | -1 | 0.01 | 0.03 |
| Stage 2 | -1.1 | 0.01 | 0.03 |
| Stage 2 | -1.2 | 0.01 | 0.03 |
| Stage 2 | -1.3 | 0.02 | 0.03 |
| Stage 2 | -1.4 | 0.02 | 0.02 |
| Stage 2 | -1.5 | 0.02 | 0.01 |
| Stage 2 | -1.6 | 0.02 | 0 |
| Stage 2 | -1.7 | 0.02 | -0.02 |
| Stage 2 | -1.8 | 0.01 | -0.04 |
| Stage 2 | -1.9 | 0.01 | -0.07 |
| Stage 2 | -2 | 0 | -0.1 |
| Stage 2 | -2.1 | -0.01 | -0.08 |
| Stage 2 | -2.2 | -0.02 | -0.06 |
| Stage 2 | -2.3 | -0.02 | -0.04 |
| Stage 2 | -2.4 | -0.03 | -0.03 |
| Stage 2 | -2.5 | -0.03 | -0.02 |
| Stage 2 | -2.6 | -0.03 | -0.01 |
| Stage 2 | -2.7 | -0.03 | 0 |
| Stage 2 | -2.8 | -0.03 | 0.01 |
| Stage 2 | -2.9 | -0.03 | 0.01 |
| Stage 2 | -3 | -0.02 | 0.02 |
| Stage 2 | -3.1 | -0.02 | 0.03 |
| Stage 2 | -3.2 | -0.02 | 0.04 |
| Stage 2 | -3.3 | -0.01 | 0.04 |
| Stage 2 | -3.4 | -0.01 | 0.05 |
| Stage 2 | -3.5 | 0 | 0.04 |
| Stage 2 | -3.6 | 0 | 0.04 |
| Stage 2 | -3.7 | 0 | 0.03 |
| Stage 2 | -3.8 | 0.01 | 0.03 |
| Stage 2 | -3.9 | 0.01 | 0.02 |
| Stage 2 | -4 | 0.01 | 0.02 |
| Stage 2 | -4.1 | 0.01 | 0.01 |
| Stage 2 | -4.2 | 0.01 | 0.01 |
| Stage 2 | -4.3 | 0.01 | 0.01 |
| Stage 2 | -4.4 | 0.01 | 0.01 |
| Stage 2 | -4.5 | 0.01 | 0 |
| Stage 2 | -4.6 | 0.01 | 0 |
| Stage 2 | -4.7 | 0.01 | 0 |
| Stage 2 | -4.8 | 0.01 | 0 |
| Stage 2 | -4.9 | 0.01 | 0 |
| Stage 2 | -5 | 0.01 | -0.01 |
| Stage 2 | -5.1 | 0.01 | -0.01 |
| Stage 2 | -5.2 | 0.01 | 0 |
| Stage 2 | -5.3 | 0.01 | -0.01 |
| Stage 2 | -5.4 | 0.01 | 0 |
| Stage 2 | -5.5 | 0.01 | -0.01 |
| Stage 2 | -5.6 | 0.01 | -0.01 |
| Stage 2 | -5.7 | 0.01 | -0.01 |
| Stage 2 | -5.8 | 0.01 | -0.01 |
| Stage 2 | -5.9 | 0.01 | -0.01 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 2 | -6 | 0.01 | 0 |
| Stage 2 | -6.1 | 0.01 | 0 |
| Stage 2 | -6.2 | 0 | 0 |
| Stage 2 | -6.3 | 0 | 0 |
| Stage 2 | -6.4 | 0 | 0 |
| Stage 2 | -6.5 | 0 | 0 |
| Stage 2 | -6.6 | 0 | 0 |
| Stage 2 | -6.7 | 0 | 0 |
| Stage 2 | -6.8 | 0 | 0 |
| Stage 2 | -6.9 | 0 | 0 |
| Stage 2 | -7 | 0 | 0 |
| Stage 2 | -7.1 | 0 | 0 |
| Stage 2 | -7.2 | 0 | 0 |
| Stage 2 | -7.3 | 0 | 0 |
| Stage 2 | -7.4 | 0 | 0 |
| Stage 2 | -7.5 | 0 | 0 |
| Stage 2 | -7.6 | 0 | 0 |
| Stage 2 | -7.7 | 0 | 0 |
| Stage 2 | -7.8 | 0 | 0 |
| Stage 2 | -7.9 | 0 | 0 |
| Stage 2 | -8 | 0 | 0 |
| Stage 2 | -8.1 | 0 | 0 |
| Stage 2 | -8.2 | 0 | 0 |
| Stage 2 | -8.3 | 0 | 0.01 |
| Stage 2 | -8.4 | 0 | 0.01 |
| Stage 2 | -8.5 | 0.01 | 0.01 |
| Stage 2 | -8.6 | 0.01 | 0.01 |
| Stage 2 | -8.7 | 0.01 | 0.01 |
| Stage 2 | -8.8 | 0.01 | 0.01 |
| Stage 2 | -8.9 | 0.01 | 0.01 |
| Stage 2 | -9 | 0.01 | 0.01 |
| Stage 2 | -9.1 | 0.01 | 0 |
| Stage 2 | -9.2 | 0.01 | 0 |
| Stage 2 | -9.3 | 0.01 | 0 |
| Stage 2 | -9.4 | 0.01 | -0.01 |
| Stage 2 | -9.5 | 0.01 | -0.01 |
| Stage 2 | -9.6 | 0.01 | -0.02 |
| Stage 2 | -9.7 | 0 | -0.02 |
| Stage 2 | -9.8 | 0 | -0.02 |
| Stage 2 | -9.9 | 0 | -0.01 |
| Stage 2 | -10 | 0 | -0.01 |

Tabella Risultati Paratia Nominal - Stage: Stage A

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage A | 0 | 0 | 0 |
| Stage A | -0.1 | 0 | 0 |
| Stage A | -0.1 | 0 | 0 |
| Stage A | -0.2 | -0.01 | -0.06 |
| Stage A | -0.3 | -0.02 | -0.18 |
| Stage A | -0.4 | -0.06 | -0.37 |
| Stage A | -0.5 | -0.12 | -0.61 |
| Stage A | -0.6 | -0.21 | -0.91 |
| Stage A | -0.7 | -0.34 | -1.28 |
| Stage A | -0.8 | -0.51 | -1.71 |
| Stage A | -0.9 | -0.73 | -2.2 |
| Stage A | -1 | -1.01 | -2.76 |
| Stage A | -1.1 | -1.35 | -3.37 |
| Stage A | -1.2 | -1.75 | -4.05 |
| Stage A | -1.3 | -2.23 | -4.8 |
| Stage A | -1.4 | -2.79 | -5.6 |
| Stage A | -1.5 | -3.44 | -6.48 |
| Stage A | -1.6 | -4.18 | -7.41 |
| Stage A | -1.7 | -4.96 | -7.82 |
| Stage A | -1.8 | -5.73 | -7.71 |
| Stage A | -1.9 | -6.44 | -7.11 |
| Stage A | -2 | -7.1 | -6.58 |
| Stage A | -2.1 | -7.5 | -4.02 |
| Stage A | -2.2 | -7.66 | -1.54 |
| Stage A | -2.3 | -7.57 | 0.88 |
| Stage A | -2.4 | -7.24 | 3.27 |
| Stage A | -2.5 | -6.74 | 5.06 |
| Stage A | -2.6 | -6.11 | 6.22 |
| Stage A | -2.7 | -5.43 | 6.86 |
| Stage A | -2.8 | -4.72 | 7.1 |
| Stage A | -2.9 | -4.02 | 7.02 |
| Stage A | -3 | -3.35 | 6.71 |
| Stage A | -3.1 | -2.72 | 6.24 |
| Stage A | -3.2 | -2.16 | 5.66 |
| Stage A | -3.3 | -1.66 | 5.02 |
| Stage A | -3.4 | -1.22 | 4.37 |
| Stage A | -3.5 | -0.85 | 3.71 |
| Stage A | -3.6 | -0.54 | 3.09 |
| Stage A | -3.7 | -0.29 | 2.51 |
| Stage A | -3.8 | -0.09 | 1.98 |
| Stage A | -3.9 | 0.06 | 1.52 |
| Stage A | -4 | 0.17 | 1.12 |
| Stage A | -4.1 | 0.25 | 0.77 |
| Stage A | -4.2 | 0.3 | 0.49 |
| Stage A | -4.3 | 0.33 | 0.26 |
| Stage A | -4.4 | 0.34 | 0.08 |
| Stage A | -4.5 | 0.33 | -0.06 |
| Stage A | -4.6 | 0.31 | -0.16 |
| Stage A | -4.7 | 0.29 | -0.23 |
| Stage A | -4.8 | 0.26 | -0.28 |
| Stage A | -4.9 | 0.23 | -0.3 |
| Stage A | -5 | 0.2 | -0.31 |
| Stage A | -5.1 | 0.17 | -0.3 |
| Stage A | -5.2 | 0.14 | -0.28 |
| Stage A | -5.3 | 0.12 | -0.26 |
| Stage A | -5.4 | 0.09 | -0.24 |
| Stage A | -5.5 | 0.07 | -0.21 |
| Stage A | -5.6 | 0.05 | -0.18 |
| Stage A | -5.7 | 0.04 | -0.15 |
| Stage A | -5.8 | 0.02 | -0.13 |
| Stage A | -5.9 | 0.01 | -0.1 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage A | -6 | 0.01 | -0.08 |
| Stage A | -6.1 | 0 | -0.06 |
| Stage A | -6.2 | 0 | -0.04 |
| Stage A | -6.3 | -0.01 | -0.03 |
| Stage A | -6.4 | -0.01 | -0.02 |
| Stage A | -6.5 | -0.01 | -0.01 |
| Stage A | -6.6 | -0.01 | 0 |
| Stage A | -6.7 | -0.01 | 0 |
| Stage A | -6.8 | -0.01 | 0.01 |
| Stage A | -6.9 | -0.01 | 0.01 |
| Stage A | -7 | -0.01 | 0.01 |
| Stage A | -7.1 | -0.01 | 0.01 |
| Stage A | -7.2 | -0.01 | 0.01 |
| Stage A | -7.3 | 0 | 0.01 |
| Stage A | -7.4 | 0 | 0.01 |
| Stage A | -7.5 | 0 | 0.01 |
| Stage A | -7.6 | 0 | 0.01 |
| Stage A | -7.7 | 0 | 0.01 |
| Stage A | -7.8 | 0 | 0.01 |
| Stage A | -7.9 | 0 | 0.01 |
| Stage A | -8 | 0 | 0.01 |
| Stage A | -8.1 | 0 | 0.01 |
| Stage A | -8.2 | 0 | 0.01 |
| Stage A | -8.3 | 0 | 0.01 |
| Stage A | -8.4 | 0 | 0.01 |
| Stage A | -8.5 | 0.01 | 0.01 |
| Stage A | -8.6 | 0.01 | 0.01 |
| Stage A | -8.7 | 0.01 | 0.01 |
| Stage A | -8.8 | 0.01 | 0.01 |
| Stage A | -8.9 | 0.01 | 0.01 |
| Stage A | -9 | 0.01 | 0.01 |
| Stage A | -9.1 | 0.01 | 0 |
| Stage A | -9.2 | 0.01 | 0 |
| Stage A | -9.3 | 0.01 | 0 |
| Stage A | -9.4 | 0.01 | -0.01 |
| Stage A | -9.5 | 0.01 | -0.01 |
| Stage A | -9.6 | 0.01 | -0.02 |
| Stage A | -9.7 | 0 | -0.02 |
| Stage A | -9.8 | 0 | -0.02 |
| Stage A | -9.9 | 0 | -0.01 |
| Stage A | -10 | 0 | -0.01 |

Tabella Risultati Paratia Nominal - Stage: Stage B

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage B | 0 | 0 | 0 |
| Stage B | -0.1 | 0 | 0 |
| Stage B | -0.1 | 0 | 0 |
| Stage B | -0.2 | -0.06 | -0.59 |
| Stage B | -0.3 | -0.24 | -1.77 |
| Stage B | -0.4 | -0.59 | -3.54 |
| Stage B | -0.5 | -1.18 | -5.9 |
| Stage B | -0.6 | -2.07 | -8.86 |
| Stage B | -0.7 | -3.31 | -12.41 |
| Stage B | -0.8 | -4.96 | -16.57 |
| Stage B | -0.9 | -7.1 | -21.33 |
| Stage B | -1 | -9.74 | -26.4 |
| Stage B | -1.1 | -12.88 | -31.4 |
| Stage B | -1.2 | -16.51 | -36.33 |
| Stage B | -1.3 | -20.62 | -41.14 |
| Stage B | -1.4 | -16.2 | 44.24 |
| Stage B | -1.5 | -12.22 | 39.75 |
| Stage B | -1.6 | -8.68 | 35.47 |
| Stage B | -1.7 | -5.53 | 31.48 |
| Stage B | -1.8 | -2.75 | 27.8 |
| Stage B | -1.9 | -0.31 | 24.42 |
| Stage B | -2 | 1.83 | 21.35 |
| Stage B | -2.1 | 3.36 | 15.33 |
| Stage B | -2.2 | 4.38 | 10.22 |
| Stage B | -2.3 | 4.97 | 5.92 |
| Stage B | -2.4 | 5.26 | 2.83 |
| Stage B | -2.5 | 5.3 | 0.46 |
| Stage B | -2.6 | 5.16 | -1.41 |
| Stage B | -2.7 | 4.88 | -2.84 |
| Stage B | -2.8 | 4.49 | -3.88 |
| Stage B | -2.9 | 4.04 | -4.55 |
| Stage B | -3 | 3.55 | -4.87 |
| Stage B | -3.1 | 3.06 | -4.94 |
| Stage B | -3.2 | 2.57 | -4.81 |
| Stage B | -3.3 | 2.12 | -4.53 |
| Stage B | -3.4 | 1.71 | -4.15 |
| Stage B | -3.5 | 1.33 | -3.73 |
| Stage B | -3.6 | 1.01 | -3.27 |
| Stage B | -3.7 | 0.73 | -2.81 |
| Stage B | -3.8 | 0.49 | -2.37 |
| Stage B | -3.9 | 0.29 | -1.94 |
| Stage B | -4 | 0.14 | -1.56 |
| Stage B | -4.1 | 0.02 | -1.22 |
| Stage B | -4.2 | -0.07 | -0.91 |
| Stage B | -4.3 | -0.14 | -0.65 |
| Stage B | -4.4 | -0.18 | -0.43 |
| Stage B | -4.5 | -0.21 | -0.26 |
| Stage B | -4.6 | -0.22 | -0.12 |
| Stage B | -4.7 | -0.22 | 0 |
| Stage B | -4.8 | -0.21 | 0.08 |
| Stage B | -4.9 | -0.2 | 0.14 |
| Stage B | -5 | -0.18 | 0.18 |
| Stage B | -5.1 | -0.16 | 0.2 |
| Stage B | -5.2 | -0.14 | 0.21 |
| Stage B | -5.3 | -0.12 | 0.21 |
| Stage B | -5.4 | -0.1 | 0.2 |
| Stage B | -5.5 | -0.08 | 0.19 |
| Stage B | -5.6 | -0.06 | 0.17 |
| Stage B | -5.7 | -0.05 | 0.15 |
| Stage B | -5.8 | -0.03 | 0.13 |
| Stage B | -5.9 | -0.02 | 0.11 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage B | -6 | -0.01 | 0.1 |
| Stage B | -6.1 | -0.01 | 0.08 |
| Stage B | -6.2 | 0 | 0.06 |
| Stage B | -6.3 | 0 | 0.05 |
| Stage B | -6.4 | 0.01 | 0.03 |
| Stage B | -6.5 | 0.01 | 0.03 |
| Stage B | -6.6 | 0.01 | 0.02 |
| Stage B | -6.7 | 0.01 | 0.01 |
| Stage B | -6.8 | 0.01 | 0 |
| Stage B | -6.9 | 0.01 | 0 |
| Stage B | -7 | 0.01 | 0 |
| Stage B | -7.1 | 0.01 | -0.01 |
| Stage B | -7.2 | 0.01 | -0.01 |
| Stage B | -7.3 | 0.01 | -0.01 |
| Stage B | -7.4 | 0.01 | -0.01 |
| Stage B | -7.5 | 0.01 | -0.01 |
| Stage B | -7.6 | 0.01 | -0.01 |
| Stage B | -7.7 | 0.01 | -0.01 |
| Stage B | -7.8 | 0 | -0.01 |
| Stage B | -7.9 | 0 | 0 |
| Stage B | -8 | 0 | 0 |
| Stage B | -8.1 | 0 | 0 |
| Stage B | -8.2 | 0 | 0 |
| Stage B | -8.3 | 0 | 0 |
| Stage B | -8.4 | 0 | 0 |
| Stage B | -8.5 | 0 | 0.01 |
| Stage B | -8.6 | 0.01 | 0.01 |
| Stage B | -8.7 | 0.01 | 0.01 |
| Stage B | -8.8 | 0.01 | 0.01 |
| Stage B | -8.9 | 0.01 | 0.01 |
| Stage B | -9 | 0.01 | 0.01 |
| Stage B | -9.1 | 0.01 | 0 |
| Stage B | -9.2 | 0.01 | 0 |
| Stage B | -9.3 | 0.01 | 0 |
| Stage B | -9.4 | 0.01 | -0.01 |
| Stage B | -9.5 | 0.01 | -0.01 |
| Stage B | -9.6 | 0.01 | -0.02 |
| Stage B | -9.7 | 0 | -0.02 |
| Stage B | -9.8 | 0 | -0.02 |
| Stage B | -9.9 | 0 | -0.01 |
| Stage B | -10 | 0 | -0.01 |

Tabella Risultati Paratia Nominal - Stage: Stage 3-

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 3- | 0 | 0 | 0 |
| Stage 3- | -0.1 | 0 | 0 |
| Stage 3- | -0.1 | 0 | 0 |
| Stage 3- | -0.2 | -0.06 | -0.59 |
| Stage 3- | -0.3 | -0.24 | -1.77 |
| Stage 3- | -0.4 | -0.59 | -3.54 |
| Stage 3- | -0.5 | -1.18 | -5.9 |
| Stage 3- | -0.6 | -2.07 | -8.86 |
| Stage 3- | -0.7 | -3.31 | -12.41 |
| Stage 3- | -0.8 | -4.96 | -16.57 |
| Stage 3- | -0.9 | -7.1 | -21.33 |
| Stage 3- | -1 | -9.77 | -26.69 |
| Stage 3- | -1.1 | -12.97 | -32.01 |
| Stage 3- | -1.2 | -16.69 | -37.21 |
| Stage 3- | -1.3 | -20.91 | -42.24 |
| Stage 3- | -1.4 | -16.65 | 42.65 |
| Stage 3- | -1.5 | -12.85 | 38.02 |
| Stage 3- | -1.6 | -9.48 | 33.66 |
| Stage 3- | -1.7 | -6.52 | 29.57 |
| Stage 3- | -1.8 | -3.94 | 25.78 |
| Stage 3- | -1.9 | -1.71 | 22.31 |
| Stage 3- | -2 | 0.2 | 19.15 |
| Stage 3- | -2.1 | 1.6 | 13.95 |
| Stage 3- | -2.2 | 2.59 | 9.92 |
| Stage 3- | -2.3 | 3.29 | 6.98 |
| Stage 3- | -2.4 | 3.79 | 5.03 |
| Stage 3- | -2.5 | 4.16 | 3.66 |
| Stage 3- | -2.6 | 4.43 | 2.75 |
| Stage 3- | -2.7 | 4.66 | 2.26 |
| Stage 3- | -2.8 | 4.88 | 2.18 |
| Stage 3- | -2.9 | 5.09 | 2.18 |
| Stage 3- | -3 | 5.31 | 2.18 |
| Stage 3- | -3.1 | 5.53 | 2.18 |
| Stage 3- | -3.2 | 5.75 | 2.18 |
| Stage 3- | -3.3 | 5.96 | 2.18 |
| Stage 3- | -3.4 | 6.18 | 2.18 |
| Stage 3- | -3.5 | 6.4 | 2.18 |
| Stage 3- | -3.6 | 6.62 | 2.18 |
| Stage 3- | -3.7 | 6.83 | 2.1 |
| Stage 3- | -3.8 | 7.02 | 1.93 |
| Stage 3- | -3.9 | 7.19 | 1.68 |
| Stage 3- | -4 | 7.32 | 1.34 |
| Stage 3- | -4.1 | 7.41 | 0.92 |
| Stage 3- | -4.2 | 7.46 | 0.42 |
| Stage 3- | -4.3 | 7.44 | -0.17 |
| Stage 3- | -4.4 | 7.35 | -0.84 |
| Stage 3- | -4.5 | 7.19 | -1.6 |
| Stage 3- | -4.6 | 6.95 | -2.44 |
| Stage 3- | -4.7 | 6.62 | -3.36 |
| Stage 3- | -4.8 | 6.18 | -4.37 |
| Stage 3- | -4.9 | 5.63 | -5.46 |
| Stage 3- | -5 | 4.97 | -6.63 |
| Stage 3- | -5.1 | 4.18 | -7.89 |
| Stage 3- | -5.2 | 3.26 | -9.23 |
| Stage 3- | -5.3 | 2.19 | -10.66 |
| Stage 3- | -5.4 | 0.97 | -12.17 |
| Stage 3- | -5.5 | -0.07 | -10.44 |
| Stage 3- | -5.6 | -0.93 | -8.58 |
| Stage 3- | -5.7 | -1.62 | -6.86 |
| Stage 3- | -5.8 | -2.15 | -5.31 |
| Stage 3- | -5.9 | -2.54 | -3.93 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 3- | -6 | -2.81 | -2.72 |
| Stage 3- | -6.1 | -2.98 | -1.68 |
| Stage 3- | -6.2 | -3.06 | -0.8 |
| Stage 3- | -6.3 | -3.07 | -0.06 |
| Stage 3- | -6.4 | -3.01 | 0.54 |
| Stage 3- | -6.5 | -2.91 | 1.02 |
| Stage 3- | -6.6 | -2.77 | 1.38 |
| Stage 3- | -6.7 | -2.61 | 1.66 |
| Stage 3- | -6.8 | -2.42 | 1.84 |
| Stage 3- | -6.9 | -2.23 | 1.96 |
| Stage 3- | -7 | -2.03 | 2.01 |
| Stage 3- | -7.1 | -1.82 | 2.02 |
| Stage 3- | -7.2 | -1.63 | 1.98 |
| Stage 3- | -7.3 | -1.43 | 1.91 |
| Stage 3- | -7.4 | -1.25 | 1.81 |
| Stage 3- | -7.5 | -1.08 | 1.7 |
| Stage 3- | -7.6 | -0.93 | 1.58 |
| Stage 3- | -7.7 | -0.78 | 1.44 |
| Stage 3- | -7.8 | -0.65 | 1.31 |
| Stage 3- | -7.9 | -0.53 | 1.17 |
| Stage 3- | -8 | -0.43 | 1.04 |
| Stage 3- | -8.1 | -0.34 | 0.91 |
| Stage 3- | -8.2 | -0.26 | 0.78 |
| Stage 3- | -8.3 | -0.19 | 0.67 |
| Stage 3- | -8.4 | -0.14 | 0.56 |
| Stage 3- | -8.5 | -0.09 | 0.46 |
| Stage 3- | -8.6 | -0.05 | 0.37 |
| Stage 3- | -8.7 | -0.03 | 0.29 |
| Stage 3- | -8.8 | 0 | 0.22 |
| Stage 3- | -8.9 | 0.01 | 0.16 |
| Stage 3- | -9 | 0.02 | 0.11 |
| Stage 3- | -9.1 | 0.03 | 0.06 |
| Stage 3- | -9.2 | 0.03 | 0.02 |
| Stage 3- | -9.3 | 0.03 | -0.01 |
| Stage 3- | -9.4 | 0.03 | -0.03 |
| Stage 3- | -9.5 | 0.02 | -0.05 |
| Stage 3- | -9.6 | 0.02 | -0.06 |
| Stage 3- | -9.7 | 0.01 | -0.06 |
| Stage 3- | -9.8 | 0.01 | -0.06 |
| Stage 3- | -9.9 | 0 | -0.04 |
| Stage 3- | -10 | 0 | -0.02 |

Grafico Momento Nominal

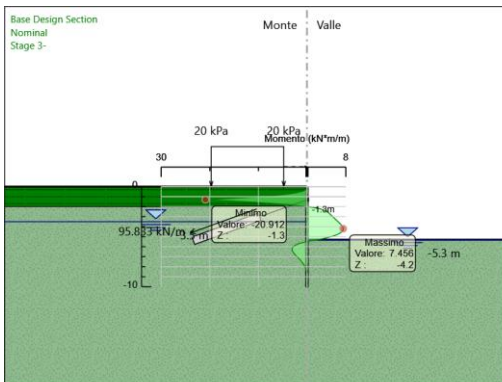
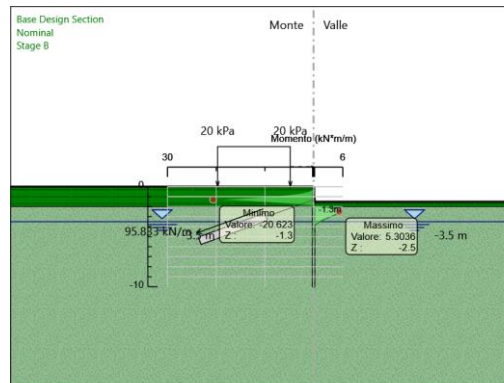
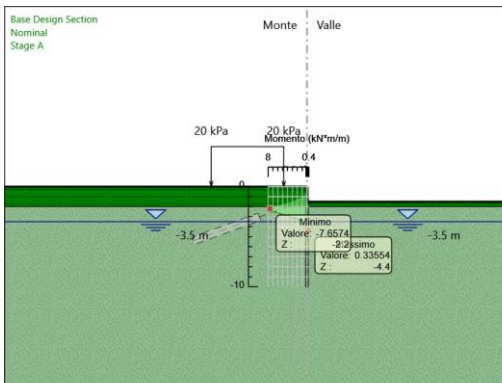
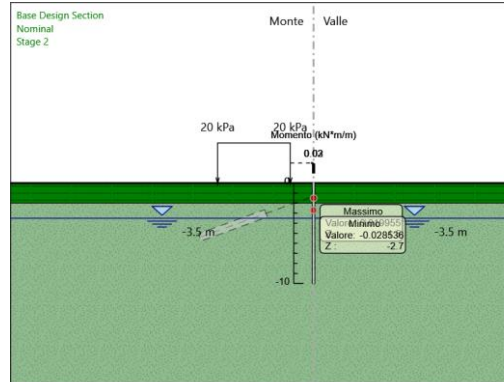
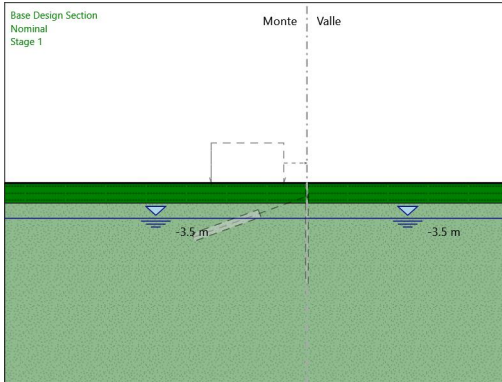
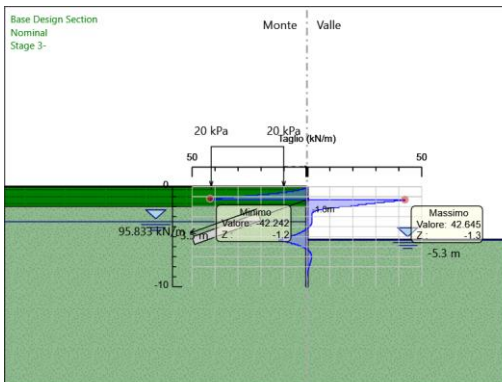
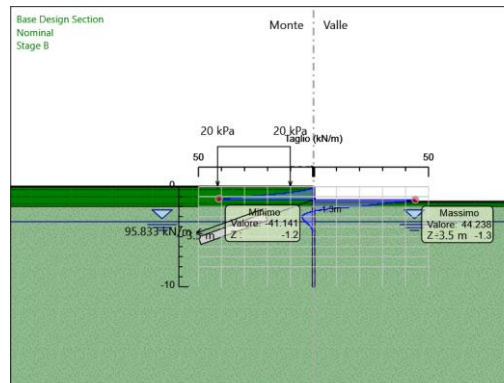
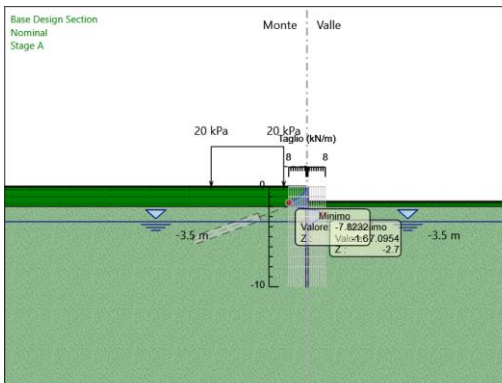
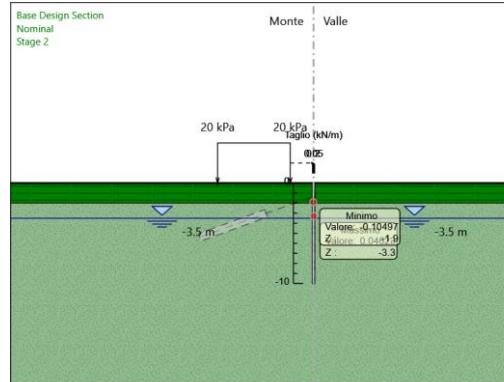
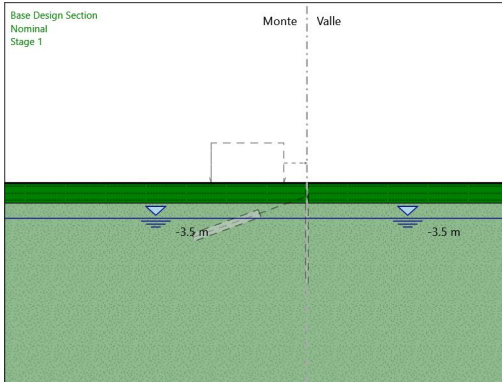


Grafico Taglio Nominal



Inviluppi Risultati Paratia Nominal

Risultati Elementi strutturali

| Design Assumption: Nominal Sollecitazione Tieback_New_New_New_New | |
|--|---------------------|
| Stage | Forza (kN/m) |
| Stage B | 95.83 |
| Stage 3- | 95.49567 |

Risultati Terreno

Tabella Risultati Terreno Left Wall - Nominal - Stage 1

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|---------------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | LEFT Ka | Lato Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 1 | 0 | 0 | 0 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage 1 | -0.1 | 1.9 | 0.95 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.95 |
| Stage 1 | -0.2 | 3.8 | 1.9 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.9 |
| Stage 1 | -0.3 | 5.7 | 2.85 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.85 |
| Stage 1 | -0.4 | 7.6 | 3.8 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.8 |
| Stage 1 | -0.5 | 9.5 | 4.75 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.75 |
| Stage 1 | -0.6 | 11.4 | 5.7 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.7 |
| Stage 1 | -0.7 | 13.3 | 6.65 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.65 |
| Stage 1 | -0.8 | 15.2 | 7.6 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.6 |
| Stage 1 | -0.9 | 17.1 | 8.55 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.55 |
| Stage 1 | -1 | 19 | 9.5 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.5 |
| Stage 1 | -1.1 | 20.9 | 10.45 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.45 |
| Stage 1 | -1.2 | 22.8 | 11.4 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.4 |
| Stage 1 | -1.3 | 24.7 | 12.35 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 12.35 |
| Stage 1 | -1.4 | 26.6 | 13.3 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 13.3 |
| Stage 1 | -1.5 | 28.5 | 14.25 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 14.25 |
| Stage 1 | -1.6 | 30.4 | 15.2 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 15.2 |
| Stage 1 | -1.7 | 32.3 | 16.15 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 16.15 |
| Stage 1 | -1.8 | 34.2 | 17.1 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.1 |
| Stage 1 | -1.9 | 36.1 | 18.05 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 18.05 |
| Stage 1 | -2 | 38 | 19 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 19 |
| Stage 1 | -2.1 | 40.45 | 20.225 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 20.225 |
| Stage 1 | -2.2 | 42.9 | 21.45 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 21.45 |
| Stage 1 | -2.3 | 45.35 | 22.675 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 22.675 |
| Stage 1 | -2.4 | 47.8 | 23.9 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 23.9 |
| Stage 1 | -2.5 | 50.25 | 25.125 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 25.125 |
| Stage 1 | -2.6 | 52.7 | 26.35 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 26.35 |
| Stage 1 | -2.7 | 55.15 | 27.575 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 27.575 |
| Stage 1 | -2.8 | 57.6 | 28.8 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 28.8 |
| Stage 1 | -2.9 | 60.05 | 30.025 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 30.025 |
| Stage 1 | -3 | 62.5 | 31.25 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 31.25 |
| Stage 1 | -3.1 | 64.95 | 32.475 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 32.475 |
| Stage 1 | -3.2 | 67.4 | 33.7 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 33.7 |
| Stage 1 | -3.3 | 69.85 | 34.925 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 34.925 |
| Stage 1 | -3.4 | 72.3 | 36.15 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 36.15 |
| Stage 1 | -3.5 | 74.75 | 37.375 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 37.375 |
| Stage 1 | -3.6 | 76.2 | 38.1 | V-C | 0.2174.599 | | 40 | 1 | 0 | 0 | 39.1 |
| Stage 1 | -3.7 | 77.65 | 38.825 | V-C | 0.2174.599 | | 40 | 2 | 0 | 0 | 40.825 |
| Stage 1 | -3.8 | 79.1 | 39.55 | V-C | 0.2174.599 | | 40 | 3 | 0 | 0 | 42.55 |
| Stage 1 | -3.9 | 80.55 | 40.275 | V-C | 0.2174.599 | | 40 | 4 | 0 | 0 | 44.275 |
| Stage 1 | -4 | 82 | 41 | V-C | 0.2174.599 | | 40 | 5 | 0 | 0 | 46 |
| Stage 1 | -4.1 | 83.45 | 41.725 | V-C | 0.2174.599 | | 40 | 6 | 0 | 0 | 47.725 |
| Stage 1 | -4.2 | 84.9 | 42.45 | V-C | 0.2174.599 | | 40 | 7 | 0 | 0 | 49.45 |
| Stage 1 | -4.3 | 86.35 | 43.175 | V-C | 0.2174.599 | | 40 | 8 | 0 | 0 | 51.175 |
| Stage 1 | -4.4 | 87.8 | 43.9 | V-C | 0.2174.599 | | 40 | 9 | 0 | 0 | 52.9 |
| Stage 1 | -4.5 | 89.25 | 44.625 | V-C | 0.2174.599 | | 40 | 10 | 0 | 0 | 54.625 |
| Stage 1 | -4.6 | 90.7 | 45.35 | V-C | 0.2174.599 | | 40 | 11 | 0 | 0 | 56.35 |
| Stage 1 | -4.7 | 92.15 | 46.075 | V-C | 0.2174.599 | | 40 | 12 | 0 | 0 | 58.075 |
| Stage 1 | -4.8 | 93.6 | 46.8 | V-C | 0.2174.599 | | 40 | 13 | 0 | 0 | 59.8 |
| Stage 1 | -4.9 | 95.05 | 47.525 | V-C | 0.2174.599 | | 40 | 14 | 0 | 0 | 61.525 |
| Stage 1 | -5 | 96.5 | 48.25 | V-C | 0.2174.599 | | 40 | 15 | 0 | 0 | 63.25 |
| Stage 1 | -5.1 | 97.95 | 48.975 | V-C | 0.2174.599 | | 40 | 16 | 0 | 0 | 64.975 |
| Stage 1 | -5.2 | 99.4 | 49.7 | V-C | 0.2174.599 | | 40 | 17 | 0 | 0 | 66.7 |
| Stage 1 | -5.3 | 100.85 | 50.425 | V-C | 0.2174.599 | | 40 | 18 | 0 | 0 | 68.425 |
| Stage 1 | -5.4 | 102.3 | 51.15 | V-C | 0.2174.599 | | 40 | 19 | 0 | 0 | 70.15 |
| Stage 1 | -5.5 | 103.75 | 51.875 | V-C | 0.2174.599 | | 40 | 20 | 0 | 0 | 71.875 |
| Stage 1 | -5.6 | 105.2 | 52.6 | V-C | 0.2174.599 | | 40 | 21 | 0 | 0 | 73.6 |
| Stage 1 | -5.7 | 106.65 | 53.325 | V-C | 0.2174.599 | | 40 | 22 | 0 | 0 | 75.325 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|---------------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | LEFT Ka | Lato Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage 1 | -5.8 | 108.1 | 54.05 | V-C | 0.2174.599 | 40 | 23 | 0 | 0 | 77.05 |
| Stage 1 | -5.9 | 109.55 | 54.775 | V-C | 0.2174.599 | 40 | 24 | 0 | 0 | 78.775 |
| Stage 1 | -6 | 111 | 55.5 | V-C | 0.2174.599 | 40 | 25 | 0 | 0 | 80.5 |
| Stage 1 | -6.1 | 112.45 | 56.225 | V-C | 0.2174.599 | 40 | 26 | 0 | 0 | 82.225 |
| Stage 1 | -6.2 | 113.9 | 56.95 | V-C | 0.2174.599 | 40 | 27 | 0 | 0 | 83.95 |
| Stage 1 | -6.3 | 115.35 | 57.675 | V-C | 0.2174.599 | 40 | 28 | 0 | 0 | 85.675 |
| Stage 1 | -6.4 | 116.8 | 58.4 | V-C | 0.2174.599 | 40 | 29 | 0 | 0 | 87.4 |
| Stage 1 | -6.5 | 118.25 | 59.125 | V-C | 0.2174.599 | 40 | 30 | 0 | 0 | 89.125 |
| Stage 1 | -6.6 | 119.7 | 59.85 | V-C | 0.2174.599 | 40 | 31 | 0 | 0 | 90.85 |
| Stage 1 | -6.7 | 121.15 | 60.575 | V-C | 0.2174.599 | 40 | 32 | 0 | 0 | 92.575 |
| Stage 1 | -6.8 | 122.6 | 61.3 | V-C | 0.2174.599 | 40 | 33 | 0 | 0 | 94.3 |
| Stage 1 | -6.9 | 124.05 | 62.025 | V-C | 0.2174.599 | 40 | 34 | 0 | 0 | 96.025 |
| Stage 1 | -7 | 125.5 | 62.75 | V-C | 0.2174.599 | 40 | 35 | 0 | 0 | 97.75 |
| Stage 1 | -7.1 | 126.95 | 63.475 | V-C | 0.2174.599 | 40 | 36 | 0 | 0 | 99.475 |
| Stage 1 | -7.2 | 128.4 | 64.2 | V-C | 0.2174.599 | 40 | 37 | 0 | 0 | 101.2 |
| Stage 1 | -7.3 | 129.85 | 64.925 | V-C | 0.2174.599 | 40 | 38 | 0 | 0 | 102.925 |
| Stage 1 | -7.4 | 131.3 | 65.65 | V-C | 0.2174.599 | 40 | 39 | 0 | 0 | 104.65 |
| Stage 1 | -7.5 | 132.75 | 66.375 | V-C | 0.2174.599 | 40 | 40 | 0 | 0 | 106.375 |
| Stage 1 | -7.6 | 134.2 | 67.1 | V-C | 0.2174.599 | 40 | 41 | 0 | 0 | 108.1 |
| Stage 1 | -7.7 | 135.65 | 67.825 | V-C | 0.2174.599 | 40 | 42 | 0 | 0 | 109.825 |
| Stage 1 | -7.8 | 137.1 | 68.55 | V-C | 0.2174.599 | 40 | 43 | 0 | 0 | 111.55 |
| Stage 1 | -7.9 | 138.55 | 69.275 | V-C | 0.2174.599 | 40 | 44 | 0 | 0 | 113.275 |
| Stage 1 | -8 | 140 | 70 | V-C | 0.2174.599 | 40 | 45 | 0 | 0 | 115 |
| Stage 1 | -8.1 | 141.45 | 70.725 | V-C | 0.2174.599 | 40 | 46 | 0 | 0 | 116.725 |
| Stage 1 | -8.2 | 142.9 | 71.45 | V-C | 0.2174.599 | 40 | 47 | 0 | 0 | 118.45 |
| Stage 1 | -8.3 | 144.35 | 72.175 | V-C | 0.2174.599 | 40 | 48 | 0 | 0 | 120.175 |
| Stage 1 | -8.4 | 145.8 | 72.9 | V-C | 0.2174.599 | 40 | 49 | 0 | 0 | 121.9 |
| Stage 1 | -8.5 | 147.25 | 73.625 | V-C | 0.2174.599 | 40 | 50 | 0 | 0 | 123.625 |
| Stage 1 | -8.6 | 148.7 | 74.35 | V-C | 0.2174.599 | 40 | 51 | 0 | 0 | 125.35 |
| Stage 1 | -8.7 | 150.15 | 75.075 | V-C | 0.2174.599 | 40 | 52 | 0 | 0 | 127.075 |
| Stage 1 | -8.8 | 151.6 | 75.8 | V-C | 0.2174.599 | 40 | 53 | 0 | 0 | 128.8 |
| Stage 1 | -8.9 | 153.05 | 76.525 | V-C | 0.2174.599 | 40 | 54 | 0 | 0 | 130.525 |
| Stage 1 | -9 | 154.5 | 77.25 | V-C | 0.2174.599 | 40 | 55 | 0 | 0 | 132.25 |
| Stage 1 | -9.1 | 155.95 | 77.975 | V-C | 0.2174.599 | 40 | 56 | 0 | 0 | 133.975 |
| Stage 1 | -9.2 | 157.4 | 78.7 | V-C | 0.2174.599 | 40 | 57 | 0 | 0 | 135.7 |
| Stage 1 | -9.3 | 158.85 | 79.425 | V-C | 0.2174.599 | 40 | 58 | 0 | 0 | 137.425 |
| Stage 1 | -9.4 | 160.3 | 80.15 | V-C | 0.2174.599 | 40 | 59 | 0 | 0 | 139.15 |
| Stage 1 | -9.5 | 161.75 | 80.875 | V-C | 0.2174.599 | 40 | 60 | 0 | 0 | 140.875 |
| Stage 1 | -9.6 | 163.2 | 81.6 | V-C | 0.2174.599 | 40 | 61 | 0 | 0 | 142.6 |
| Stage 1 | -9.7 | 164.65 | 82.325 | V-C | 0.2174.599 | 40 | 62 | 0 | 0 | 144.325 |
| Stage 1 | -9.8 | 166.1 | 83.05 | V-C | 0.2174.599 | 40 | 63 | 0 | 0 | 146.05 |
| Stage 1 | -9.9 | 167.55 | 83.775 | V-C | 0.2174.599 | 40 | 64 | 0 | 0 | 147.775 |
| Stage 1 | -10 | 169 | 84.5 | V-C | 0.2174.599 | 40 | 65 | 0 | 0 | 149.5 |

| Design Assumption: Nominal Risultati Terreno | | | Muro: | LEFT | Lato | RIGHT | | | | | |
|--|-------|---------------|---------------|-------|------------|-------|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 1 | 0 | 0 | 0 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage 1 | -0.1 | 1.9 | 0.95 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.95 |
| Stage 1 | -0.2 | 3.8 | 1.9 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.9 |
| Stage 1 | -0.3 | 5.7 | 2.85 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.85 |
| Stage 1 | -0.4 | 7.6 | 3.8 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.8 |
| Stage 1 | -0.5 | 9.5 | 4.75 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.75 |
| Stage 1 | -0.6 | 11.4 | 5.7 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.7 |
| Stage 1 | -0.7 | 13.3 | 6.65 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.65 |
| Stage 1 | -0.8 | 15.2 | 7.6 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.6 |
| Stage 1 | -0.9 | 17.1 | 8.55 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.55 |
| Stage 1 | -1 | 19 | 9.5 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.5 |
| Stage 1 | -1.1 | 20.9 | 10.45 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.45 |
| Stage 1 | -1.2 | 22.8 | 11.4 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.4 |
| Stage 1 | -1.3 | 24.7 | 12.35 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 12.35 |
| Stage 1 | -1.4 | 26.6 | 13.3 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 13.3 |
| Stage 1 | -1.5 | 28.5 | 14.25 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 14.25 |
| Stage 1 | -1.6 | 30.4 | 15.2 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 15.2 |
| Stage 1 | -1.7 | 32.3 | 16.15 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 16.15 |
| Stage 1 | -1.8 | 34.2 | 17.1 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.1 |
| Stage 1 | -1.9 | 36.1 | 18.05 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 18.05 |
| Stage 1 | -2 | 38 | 19 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 19 |
| Stage 1 | -2.1 | 40.45 | 20.225 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 20.225 |
| Stage 1 | -2.2 | 42.9 | 21.45 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 21.45 |
| Stage 1 | -2.3 | 45.35 | 22.675 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 22.675 |
| Stage 1 | -2.4 | 47.8 | 23.9 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 23.9 |
| Stage 1 | -2.5 | 50.25 | 25.125 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 25.125 |
| Stage 1 | -2.6 | 52.7 | 26.35 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 26.35 |
| Stage 1 | -2.7 | 55.15 | 27.575 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 27.575 |
| Stage 1 | -2.8 | 57.6 | 28.8 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 28.8 |
| Stage 1 | -2.9 | 60.05 | 30.025 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 30.025 |
| Stage 1 | -3 | 62.5 | 31.25 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 31.25 |
| Stage 1 | -3.1 | 64.95 | 32.475 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 32.475 |
| Stage 1 | -3.2 | 67.4 | 33.7 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 33.7 |
| Stage 1 | -3.3 | 69.85 | 34.925 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 34.925 |
| Stage 1 | -3.4 | 72.3 | 36.15 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 36.15 |
| Stage 1 | -3.5 | 74.75 | 37.375 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 37.375 |
| Stage 1 | -3.6 | 76.2 | 38.1 | V-C | 0.2174.599 | | 40 | 1 | 0 | 0 | 39.1 |
| Stage 1 | -3.7 | 77.65 | 38.825 | V-C | 0.2174.599 | | 40 | 2 | 0 | 0 | 40.825 |
| Stage 1 | -3.8 | 79.1 | 39.55 | V-C | 0.2174.599 | | 40 | 3 | 0 | 0 | 42.55 |
| Stage 1 | -3.9 | 80.55 | 40.275 | V-C | 0.2174.599 | | 40 | 4 | 0 | 0 | 44.275 |
| Stage 1 | -4 | 82 | 41 | V-C | 0.2174.599 | | 40 | 5 | 0 | 0 | 46 |
| Stage 1 | -4.1 | 83.45 | 41.725 | V-C | 0.2174.599 | | 40 | 6 | 0 | 0 | 47.725 |
| Stage 1 | -4.2 | 84.9 | 42.45 | V-C | 0.2174.599 | | 40 | 7 | 0 | 0 | 49.45 |
| Stage 1 | -4.3 | 86.35 | 43.175 | V-C | 0.2174.599 | | 40 | 8 | 0 | 0 | 51.175 |
| Stage 1 | -4.4 | 87.8 | 43.9 | V-C | 0.2174.599 | | 40 | 9 | 0 | 0 | 52.9 |
| Stage 1 | -4.5 | 89.25 | 44.625 | V-C | 0.2174.599 | | 40 | 10 | 0 | 0 | 54.625 |
| Stage 1 | -4.6 | 90.7 | 45.35 | V-C | 0.2174.599 | | 40 | 11 | 0 | 0 | 56.35 |
| Stage 1 | -4.7 | 92.15 | 46.075 | V-C | 0.2174.599 | | 40 | 12 | 0 | 0 | 58.075 |
| Stage 1 | -4.8 | 93.6 | 46.8 | V-C | 0.2174.599 | | 40 | 13 | 0 | 0 | 59.8 |
| Stage 1 | -4.9 | 95.05 | 47.525 | V-C | 0.2174.599 | | 40 | 14 | 0 | 0 | 61.525 |
| Stage 1 | -5 | 96.5 | 48.25 | V-C | 0.2174.599 | | 40 | 15 | 0 | 0 | 63.25 |
| Stage 1 | -5.1 | 97.95 | 48.975 | V-C | 0.2174.599 | | 40 | 16 | 0 | 0 | 64.975 |
| Stage 1 | -5.2 | 99.4 | 49.7 | V-C | 0.2174.599 | | 40 | 17 | 0 | 0 | 66.7 |
| Stage 1 | -5.3 | 100.85 | 50.425 | V-C | 0.2174.599 | | 40 | 18 | 0 | 0 | 68.425 |
| Stage 1 | -5.4 | 102.3 | 51.15 | V-C | 0.2174.599 | | 40 | 19 | 0 | 0 | 70.15 |
| Stage 1 | -5.5 | 103.75 | 51.875 | V-C | 0.2174.599 | | 40 | 20 | 0 | 0 | 71.875 |
| Stage 1 | -5.6 | 105.2 | 52.6 | V-C | 0.2174.599 | | 40 | 21 | 0 | 0 | 73.6 |
| Stage 1 | -5.7 | 106.65 | 53.325 | V-C | 0.2174.599 | | 40 | 22 | 0 | 0 | 75.325 |
| Stage 1 | -5.8 | 108.1 | 54.05 | V-C | 0.2174.599 | | 40 | 23 | 0 | 0 | 77.05 |
| Stage 1 | -5.9 | 109.55 | 54.775 | V-C | 0.2174.599 | | 40 | 24 | 0 | 0 | 78.775 |
| Stage 1 | -6 | 111 | 55.5 | V-C | 0.2174.599 | | 40 | 25 | 0 | 0 | 80.5 |
| Stage 1 | -6.1 | 112.45 | 56.225 | V-C | 0.2174.599 | | 40 | 26 | 0 | 0 | 82.225 |
| Stage 1 | -6.2 | 113.9 | 56.95 | V-C | 0.2174.599 | | 40 | 27 | 0 | 0 | 83.95 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|----------|----------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | RIGHT Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage 1 | -6.3 | 115.35 | 57.675 | V-C | 0.2174.599 | 40 | 28 | 0 | 0 | 85.675 |
| Stage 1 | -6.4 | 116.8 | 58.4 | V-C | 0.2174.599 | 40 | 29 | 0 | 0 | 87.4 |
| Stage 1 | -6.5 | 118.25 | 59.125 | V-C | 0.2174.599 | 40 | 30 | 0 | 0 | 89.125 |
| Stage 1 | -6.6 | 119.7 | 59.85 | V-C | 0.2174.599 | 40 | 31 | 0 | 0 | 90.85 |
| Stage 1 | -6.7 | 121.15 | 60.575 | V-C | 0.2174.599 | 40 | 32 | 0 | 0 | 92.575 |
| Stage 1 | -6.8 | 122.6 | 61.3 | V-C | 0.2174.599 | 40 | 33 | 0 | 0 | 94.3 |
| Stage 1 | -6.9 | 124.05 | 62.025 | V-C | 0.2174.599 | 40 | 34 | 0 | 0 | 96.025 |
| Stage 1 | -7 | 125.5 | 62.75 | V-C | 0.2174.599 | 40 | 35 | 0 | 0 | 97.75 |
| Stage 1 | -7.1 | 126.95 | 63.475 | V-C | 0.2174.599 | 40 | 36 | 0 | 0 | 99.475 |
| Stage 1 | -7.2 | 128.4 | 64.2 | V-C | 0.2174.599 | 40 | 37 | 0 | 0 | 101.2 |
| Stage 1 | -7.3 | 129.85 | 64.925 | V-C | 0.2174.599 | 40 | 38 | 0 | 0 | 102.925 |
| Stage 1 | -7.4 | 131.3 | 65.65 | V-C | 0.2174.599 | 40 | 39 | 0 | 0 | 104.65 |
| Stage 1 | -7.5 | 132.75 | 66.375 | V-C | 0.2174.599 | 40 | 40 | 0 | 0 | 106.375 |
| Stage 1 | -7.6 | 134.2 | 67.1 | V-C | 0.2174.599 | 40 | 41 | 0 | 0 | 108.1 |
| Stage 1 | -7.7 | 135.65 | 67.825 | V-C | 0.2174.599 | 40 | 42 | 0 | 0 | 109.825 |
| Stage 1 | -7.8 | 137.1 | 68.55 | V-C | 0.2174.599 | 40 | 43 | 0 | 0 | 111.55 |
| Stage 1 | -7.9 | 138.55 | 69.275 | V-C | 0.2174.599 | 40 | 44 | 0 | 0 | 113.275 |
| Stage 1 | -8 | 140 | 70 | V-C | 0.2174.599 | 40 | 45 | 0 | 0 | 115 |
| Stage 1 | -8.1 | 141.45 | 70.725 | V-C | 0.2174.599 | 40 | 46 | 0 | 0 | 116.725 |
| Stage 1 | -8.2 | 142.9 | 71.45 | V-C | 0.2174.599 | 40 | 47 | 0 | 0 | 118.45 |
| Stage 1 | -8.3 | 144.35 | 72.175 | V-C | 0.2174.599 | 40 | 48 | 0 | 0 | 120.175 |
| Stage 1 | -8.4 | 145.8 | 72.9 | V-C | 0.2174.599 | 40 | 49 | 0 | 0 | 121.9 |
| Stage 1 | -8.5 | 147.25 | 73.625 | V-C | 0.2174.599 | 40 | 50 | 0 | 0 | 123.625 |
| Stage 1 | -8.6 | 148.7 | 74.35 | V-C | 0.2174.599 | 40 | 51 | 0 | 0 | 125.35 |
| Stage 1 | -8.7 | 150.15 | 75.075 | V-C | 0.2174.599 | 40 | 52 | 0 | 0 | 127.075 |
| Stage 1 | -8.8 | 151.6 | 75.8 | V-C | 0.2174.599 | 40 | 53 | 0 | 0 | 128.8 |
| Stage 1 | -8.9 | 153.05 | 76.525 | V-C | 0.2174.599 | 40 | 54 | 0 | 0 | 130.525 |
| Stage 1 | -9 | 154.5 | 77.25 | V-C | 0.2174.599 | 40 | 55 | 0 | 0 | 132.25 |
| Stage 1 | -9.1 | 155.95 | 77.975 | V-C | 0.2174.599 | 40 | 56 | 0 | 0 | 133.975 |
| Stage 1 | -9.2 | 157.4 | 78.7 | V-C | 0.2174.599 | 40 | 57 | 0 | 0 | 135.7 |
| Stage 1 | -9.3 | 158.85 | 79.425 | V-C | 0.2174.599 | 40 | 58 | 0 | 0 | 137.425 |
| Stage 1 | -9.4 | 160.3 | 80.15 | V-C | 0.2174.599 | 40 | 59 | 0 | 0 | 139.15 |
| Stage 1 | -9.5 | 161.75 | 80.875 | V-C | 0.2174.599 | 40 | 60 | 0 | 0 | 140.875 |
| Stage 1 | -9.6 | 163.2 | 81.6 | V-C | 0.2174.599 | 40 | 61 | 0 | 0 | 142.6 |
| Stage 1 | -9.7 | 164.65 | 82.325 | V-C | 0.2174.599 | 40 | 62 | 0 | 0 | 144.325 |
| Stage 1 | -9.8 | 166.1 | 83.05 | V-C | 0.2174.599 | 40 | 63 | 0 | 0 | 146.05 |
| Stage 1 | -9.9 | 167.55 | 83.775 | V-C | 0.2174.599 | 40 | 64 | 0 | 0 | 147.775 |
| Stage 1 | -10 | 169 | 84.5 | V-C | 0.2174.599 | 40 | 65 | 0 | 0 | 149.5 |

Tabella Risultati Terreno Left Wall - Nominal - Stage 2

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|--------|------------|------|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT | | Lato | | LEFT | | | |
| | | | | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 2 | 0 | 0 | 0 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage 2 | -0.1 | 1.9 | 0.958 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.958 |
| Stage 2 | -0.2 | 3.803 | 1.899 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.899 |
| Stage 2 | -0.3 | 5.709 | 2.838 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.838 |
| Stage 2 | -0.4 | 7.621 | 3.779 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.779 |
| Stage 2 | -0.5 | 9.541 | 4.724 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.724 |
| Stage 2 | -0.6 | 11.469 | 5.673 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.673 |
| Stage 2 | -0.7 | 13.406 | 6.626 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.626 |
| Stage 2 | -0.8 | 15.353 | 7.585 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.585 |
| Stage 2 | -0.9 | 17.311 | 8.55 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.55 |
| Stage 2 | -1 | 19.278 | 9.519 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.519 |
| Stage 2 | -1.1 | 21.256 | 10.494 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.494 |
| Stage 2 | -1.2 | 23.242 | 11.475 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.475 |
| Stage 2 | -1.3 | 25.237 | 12.46 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 12.46 |
| Stage 2 | -1.4 | 27.24 | 13.45 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 13.45 |
| Stage 2 | -1.5 | 29.25 | 14.445 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 14.445 |
| Stage 2 | -1.6 | 31.265 | 15.443 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 15.443 |
| Stage 2 | -1.7 | 33.286 | 16.445 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 16.445 |
| Stage 2 | -1.8 | 35.31 | 17.45 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.45 |
| Stage 2 | -1.9 | 37.337 | 18.457 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 18.457 |
| Stage 2 | -2 | 39.367 | 18.955 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 18.955 |
| Stage 2 | -2.1 | 41.948 | 20.224 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 20.224 |
| Stage 2 | -2.2 | 44.529 | 21.491 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 21.491 |
| Stage 2 | -2.3 | 47.111 | 22.755 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 22.755 |
| Stage 2 | -2.4 | 49.692 | 24.014 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 24.014 |
| Stage 2 | -2.5 | 52.272 | 25.269 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 25.269 |
| Stage 2 | -2.6 | 54.85 | 26.517 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 26.517 |
| Stage 2 | -2.7 | 57.427 | 27.759 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 27.759 |
| Stage 2 | -2.8 | 60.001 | 28.995 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 28.995 |
| Stage 2 | -2.9 | 62.573 | 30.225 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 30.225 |
| Stage 2 | -3 | 65.143 | 31.448 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 31.448 |
| Stage 2 | -3.1 | 67.9 | 32.761 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 32.761 |
| Stage 2 | -3.2 | 70.524 | 34.003 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 34.003 |
| Stage 2 | -3.3 | 73.141 | 35.239 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 35.239 |
| Stage 2 | -3.4 | 75.96 | 36.574 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 36.574 |
| Stage 2 | -3.5 | 78.558 | 37.796 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 37.796 |
| Stage 2 | -3.6 | 80.348 | 38.613 | UL-RL | 0.2174.599 | | 40 | 1 | 0 | 0 | 39.613 |
| Stage 2 | -3.7 | 81.929 | 39.327 | UL-RL | 0.2174.599 | | 40 | 2 | 0 | 0 | 41.327 |
| Stage 2 | -3.8 | 83.505 | 40.038 | UL-RL | 0.2174.599 | | 40 | 3 | 0 | 0 | 43.038 |
| Stage 2 | -3.9 | 85.26 | 40.84 | UL-RL | 0.2174.599 | | 40 | 4 | 0 | 0 | 44.84 |
| Stage 2 | -4 | 86.823 | 41.547 | UL-RL | 0.2174.599 | | 40 | 5 | 0 | 0 | 46.547 |
| Stage 2 | -4.1 | 88.382 | 42.254 | UL-RL | 0.2174.599 | | 40 | 6 | 0 | 0 | 48.254 |
| Stage 2 | -4.2 | 90.108 | 43.046 | UL-RL | 0.2174.599 | | 40 | 7 | 0 | 0 | 50.046 |
| Stage 2 | -4.3 | 91.656 | 43.752 | UL-RL | 0.2174.599 | | 40 | 8 | 0 | 0 | 51.752 |
| Stage 2 | -4.4 | 93.363 | 44.539 | UL-RL | 0.2174.599 | | 40 | 9 | 0 | 0 | 53.539 |
| Stage 2 | -4.5 | 94.901 | 45.245 | UL-RL | 0.2174.599 | | 40 | 10 | 0 | 0 | 55.245 |
| Stage 2 | -4.6 | 96.436 | 45.951 | UL-RL | 0.2174.599 | | 40 | 11 | 0 | 0 | 56.951 |
| Stage 2 | -4.7 | 98.121 | 46.735 | UL-RL | 0.2174.599 | | 40 | 12 | 0 | 0 | 58.735 |
| Stage 2 | -4.8 | 99.648 | 47.442 | UL-RL | 0.2174.599 | | 40 | 13 | 0 | 0 | 60.442 |
| Stage 2 | -4.9 | 101.319 | 48.223 | UL-RL | 0.2174.599 | | 40 | 14 | 0 | 0 | 62.223 |
| Stage 2 | -5 | 102.839 | 48.931 | UL-RL | 0.2174.599 | | 40 | 15 | 0 | 0 | 63.931 |
| Stage 2 | -5.1 | 104.357 | 49.64 | UL-RL | 0.2174.599 | | 40 | 16 | 0 | 0 | 65.64 |
| Stage 2 | -5.2 | 106.011 | 50.419 | UL-RL | 0.2174.599 | | 40 | 17 | 0 | 0 | 67.419 |
| Stage 2 | -5.3 | 107.522 | 51.128 | UL-RL | 0.2174.599 | | 40 | 18 | 0 | 0 | 69.128 |
| Stage 2 | -5.4 | 109.165 | 51.905 | UL-RL | 0.2174.599 | | 40 | 19 | 0 | 0 | 70.905 |
| Stage 2 | -5.5 | 110.671 | 52.616 | UL-RL | 0.2174.599 | | 40 | 20 | 0 | 0 | 72.616 |
| Stage 2 | -5.6 | 112.176 | 53.327 | UL-RL | 0.2174.599 | | 40 | 21 | 0 | 0 | 74.327 |
| Stage 2 | -5.7 | 113.804 | 54.101 | UL-RL | 0.2174.599 | | 40 | 22 | 0 | 0 | 76.101 |
| Stage 2 | -5.8 | 115.304 | 54.813 | UL-RL | 0.2174.599 | | 40 | 23 | 0 | 0 | 77.813 |
| Stage 2 | -5.9 | 116.802 | 55.525 | UL-RL | 0.2174.599 | | 40 | 24 | 0 | 0 | 79.525 |
| Stage 2 | -6 | 118.419 | 56.297 | UL-RL | 0.2174.599 | | 40 | 25 | 0 | 0 | 81.297 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 2 | -6.1 | 119.914 | 57.009 | UL-RL | 0.2174.599 | 40 | 26 | 0 | 0 | 83.009 |
| Stage 2 | -6.2 | 121.522 | 57.779 | UL-RL | 0.2174.599 | 40 | 27 | 0 | 0 | 84.779 |
| Stage 2 | -6.3 | 123.013 | 58.491 | UL-RL | 0.2174.599 | 40 | 28 | 0 | 0 | 86.491 |
| Stage 2 | -6.4 | 124.502 | 59.203 | UL-RL | 0.2174.599 | 40 | 29 | 0 | 0 | 88.203 |
| Stage 2 | -6.5 | 126.101 | 59.971 | UL-RL | 0.2174.599 | 40 | 30 | 0 | 0 | 89.971 |
| Stage 2 | -6.6 | 127.587 | 60.683 | UL-RL | 0.2174.599 | 40 | 31 | 0 | 0 | 91.683 |
| Stage 2 | -6.7 | 129.179 | 61.449 | UL-RL | 0.2174.599 | 40 | 32 | 0 | 0 | 93.449 |
| Stage 2 | -6.8 | 130.662 | 62.161 | UL-RL | 0.2174.599 | 40 | 33 | 0 | 0 | 95.161 |
| Stage 2 | -6.9 | 132.145 | 62.874 | UL-RL | 0.2174.599 | 40 | 34 | 0 | 0 | 96.874 |
| Stage 2 | -7 | 133.729 | 63.638 | UL-RL | 0.2174.599 | 40 | 35 | 0 | 0 | 98.638 |
| Stage 2 | -7.1 | 135.208 | 64.35 | UL-RL | 0.2174.599 | 40 | 36 | 0 | 0 | 100.35 |
| Stage 2 | -7.2 | 136.787 | 65.113 | UL-RL | 0.2174.599 | 40 | 37 | 0 | 0 | 102.112 |
| Stage 2 | -7.3 | 138.264 | 65.825 | UL-RL | 0.2174.599 | 40 | 38 | 0 | 0 | 103.825 |
| Stage 2 | -7.4 | 139.741 | 66.538 | UL-RL | 0.2174.599 | 40 | 39 | 0 | 0 | 105.538 |
| Stage 2 | -7.5 | 141.312 | 67.299 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 107.298 |
| Stage 2 | -7.6 | 142.787 | 68.011 | UL-RL | 0.2174.599 | 40 | 41 | 0 | 0 | 109.011 |
| Stage 2 | -7.7 | 144.26 | 68.724 | UL-RL | 0.2174.599 | 40 | 42 | 0 | 0 | 110.724 |
| Stage 2 | -7.8 | 145.826 | 69.483 | UL-RL | 0.2174.599 | 40 | 43 | 0 | 0 | 112.483 |
| Stage 2 | -7.9 | 147.298 | 70.196 | UL-RL | 0.2174.599 | 40 | 44 | 0 | 0 | 114.196 |
| Stage 2 | -8 | 148.859 | 70.954 | UL-RL | 0.2174.599 | 40 | 45 | 0 | 0 | 115.954 |
| Stage 2 | -8.1 | 150.329 | 71.667 | UL-RL | 0.2174.599 | 40 | 46 | 0 | 0 | 117.667 |
| Stage 2 | -8.2 | 151.798 | 72.38 | UL-RL | 0.2174.599 | 40 | 47 | 0 | 0 | 119.38 |
| Stage 2 | -8.3 | 153.354 | 73.138 | UL-RL | 0.2174.599 | 40 | 48 | 0 | 0 | 121.138 |
| Stage 2 | -8.4 | 154.822 | 73.852 | UL-RL | 0.2174.599 | 40 | 49 | 0 | 0 | 122.852 |
| Stage 2 | -8.5 | 156.374 | 74.609 | UL-RL | 0.2174.599 | 40 | 50 | 0 | 0 | 124.609 |
| Stage 2 | -8.6 | 157.84 | 75.324 | UL-RL | 0.2174.599 | 40 | 51 | 0 | 0 | 126.324 |
| Stage 2 | -8.7 | 159.307 | 76.04 | UL-RL | 0.2174.599 | 40 | 52 | 0 | 0 | 128.04 |
| Stage 2 | -8.8 | 160.854 | 76.798 | UL-RL | 0.2174.599 | 40 | 53 | 0 | 0 | 129.798 |
| Stage 2 | -8.9 | 162.319 | 77.517 | UL-RL | 0.2174.599 | 40 | 54 | 0 | 0 | 131.517 |
| Stage 2 | -9 | 163.863 | 78.276 | UL-RL | 0.2174.599 | 40 | 55 | 0 | 0 | 133.276 |
| Stage 2 | -9.1 | 165.326 | 78.997 | UL-RL | 0.2174.599 | 40 | 56 | 0 | 0 | 134.997 |
| Stage 2 | -9.2 | 166.79 | 79.719 | UL-RL | 0.2174.599 | 40 | 57 | 0 | 0 | 136.719 |
| Stage 2 | -9.3 | 168.33 | 80.482 | UL-RL | 0.2174.599 | 40 | 58 | 0 | 0 | 138.482 |
| Stage 2 | -9.4 | 169.792 | 81.207 | UL-RL | 0.2174.599 | 40 | 59 | 0 | 0 | 140.207 |
| Stage 2 | -9.5 | 171.254 | 81.934 | UL-RL | 0.2174.599 | 40 | 60 | 0 | 0 | 141.934 |
| Stage 2 | -9.6 | 172.64 | 82.624 | UL-RL | 0.2174.599 | 40 | 61 | 0 | 0 | 143.624 |
| Stage 2 | -9.7 | 174.028 | 83.316 | UL-RL | 0.2174.599 | 40 | 62 | 0 | 0 | 145.316 |
| Stage 2 | -9.8 | 175.416 | 84.009 | UL-RL | 0.2174.599 | 40 | 63 | 0 | 0 | 147.008 |
| Stage 2 | -9.9 | 176.805 | 84.702 | UL-RL | 0.2174.599 | 40 | 64 | 0 | 0 | 148.702 |
| Stage 2 | -10 | 178.195 | 85.396 | UL-RL | 0.2174.599 | 40 | 65 | 0 | 0 | 150.396 |

| Design Assumption: Nominal Risultati Terreno | | | Muro: | LEFT | Lato | RIGHT | | | | | |
|--|-------|---------------|---------------|---------|------------|-------|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 2 | 0 | 0 | 0 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage 2 | -0.1 | 1.9 | 0.943 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.943 |
| Stage 2 | -0.2 | 3.8 | 1.901 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.901 |
| Stage 2 | -0.3 | 5.7 | 2.856 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.856 |
| Stage 2 | -0.4 | 7.6 | 3.811 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.811 |
| Stage 2 | -0.5 | 9.5 | 4.766 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.766 |
| Stage 2 | -0.6 | 11.4 | 5.721 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.721 |
| Stage 2 | -0.7 | 13.3 | 6.676 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.676 |
| Stage 2 | -0.8 | 15.2 | 7.631 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.631 |
| Stage 2 | -0.9 | 17.1 | 8.586 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.586 |
| Stage 2 | -1 | 19 | 9.541 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.541 |
| Stage 2 | -1.1 | 20.9 | 10.495 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.495 |
| Stage 2 | -1.2 | 22.8 | 11.45 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.45 |
| Stage 2 | -1.3 | 24.7 | 12.404 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 12.404 |
| Stage 2 | -1.4 | 26.6 | 13.358 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 13.358 |
| Stage 2 | -1.5 | 28.5 | 14.311 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 14.311 |
| Stage 2 | -1.6 | 30.4 | 15.264 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 15.264 |
| Stage 2 | -1.7 | 32.3 | 16.217 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 16.217 |
| Stage 2 | -1.8 | 34.2 | 17.169 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.169 |
| Stage 2 | -1.9 | 36.1 | 18.122 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 18.122 |
| Stage 2 | -2 | 38 | 19.198 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 19.198 |
| Stage 2 | -2.1 | 40.45 | 20.429 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 20.429 |
| Stage 2 | -2.2 | 42.9 | 21.66 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 21.66 |
| Stage 2 | -2.3 | 45.35 | 22.893 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 22.893 |
| Stage 2 | -2.4 | 47.8 | 24.126 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 24.126 |
| Stage 2 | -2.5 | 50.25 | 25.361 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 25.361 |
| Stage 2 | -2.6 | 52.7 | 26.597 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 26.597 |
| Stage 2 | -2.7 | 55.15 | 27.834 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 27.834 |
| Stage 2 | -2.8 | 57.6 | 29.073 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 29.073 |
| Stage 2 | -2.9 | 60.05 | 30.314 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 30.314 |
| Stage 2 | -3 | 62.5 | 31.555 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 31.555 |
| Stage 2 | -3.1 | 64.95 | 32.798 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 32.798 |
| Stage 2 | -3.2 | 67.4 | 34.042 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 34.042 |
| Stage 2 | -3.3 | 69.85 | 35.287 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 35.287 |
| Stage 2 | -3.4 | 72.3 | 36.532 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 36.532 |
| Stage 2 | -3.5 | 74.75 | 37.778 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 37.778 |
| Stage 2 | -3.6 | 76.2 | 38.524 | V-C | 0.2174.599 | | 40 | 1 | 0 | 0 | 39.524 |
| Stage 2 | -3.7 | 77.65 | 39.27 | V-C | 0.2174.599 | | 40 | 2 | 0 | 0 | 41.27 |
| Stage 2 | -3.8 | 79.1 | 40.016 | V-C | 0.2174.599 | | 40 | 3 | 0 | 0 | 43.016 |
| Stage 2 | -3.9 | 80.55 | 40.762 | V-C | 0.2174.599 | | 40 | 4 | 0 | 0 | 44.762 |
| Stage 2 | -4 | 82 | 41.507 | V-C | 0.2174.599 | | 40 | 5 | 0 | 0 | 46.507 |
| Stage 2 | -4.1 | 83.45 | 42.252 | V-C | 0.2174.599 | | 40 | 6 | 0 | 0 | 48.252 |
| Stage 2 | -4.2 | 84.9 | 42.996 | V-C | 0.2174.599 | | 40 | 7 | 0 | 0 | 49.996 |
| Stage 2 | -4.3 | 86.35 | 43.739 | V-C | 0.2174.599 | | 40 | 8 | 0 | 0 | 51.739 |
| Stage 2 | -4.4 | 87.8 | 44.482 | V-C | 0.2174.599 | | 40 | 9 | 0 | 0 | 53.482 |
| Stage 2 | -4.5 | 89.25 | 45.225 | V-C | 0.2174.599 | | 40 | 10 | 0 | 0 | 55.225 |
| Stage 2 | -4.6 | 90.7 | 45.966 | V-C | 0.2174.599 | | 40 | 11 | 0 | 0 | 56.966 |
| Stage 2 | -4.7 | 92.15 | 46.707 | V-C | 0.2174.599 | | 40 | 12 | 0 | 0 | 58.707 |
| Stage 2 | -4.8 | 93.6 | 47.448 | V-C | 0.2174.599 | | 40 | 13 | 0 | 0 | 60.448 |
| Stage 2 | -4.9 | 95.05 | 48.187 | V-C | 0.2174.599 | | 40 | 14 | 0 | 0 | 62.187 |
| Stage 2 | -5 | 96.5 | 48.926 | V-C | 0.2174.599 | | 40 | 15 | 0 | 0 | 63.926 |
| Stage 2 | -5.1 | 97.95 | 49.665 | V-C | 0.2174.599 | | 40 | 16 | 0 | 0 | 65.665 |
| Stage 2 | -5.2 | 99.4 | 50.403 | V-C | 0.2174.599 | | 40 | 17 | 0 | 0 | 67.403 |
| Stage 2 | -5.3 | 100.85 | 51.141 | V-C | 0.2174.599 | | 40 | 18 | 0 | 0 | 69.141 |
| Stage 2 | -5.4 | 102.3 | 51.878 | V-C | 0.2174.599 | | 40 | 19 | 0 | 0 | 70.878 |
| Stage 2 | -5.5 | 103.75 | 52.614 | V-C | 0.2174.599 | | 40 | 20 | 0 | 0 | 72.614 |
| Stage 2 | -5.6 | 105.2 | 53.35 | V-C | 0.2174.599 | | 40 | 21 | 0 | 0 | 74.35 |
| Stage 2 | -5.7 | 106.65 | 54.086 | V-C | 0.2174.599 | | 40 | 22 | 0 | 0 | 76.086 |
| Stage 2 | -5.8 | 108.1 | 54.822 | V-C | 0.2174.599 | | 40 | 23 | 0 | 0 | 77.822 |
| Stage 2 | -5.9 | 109.55 | 55.557 | V-C | 0.2174.599 | | 40 | 24 | 0 | 0 | 79.557 |
| Stage 2 | -6 | 111 | 56.292 | V-C | 0.2174.599 | | 40 | 25 | 0 | 0 | 81.292 |
| Stage 2 | -6.1 | 112.45 | 57.026 | V-C | 0.2174.599 | | 40 | 26 | 0 | 0 | 83.026 |
| Stage 2 | -6.2 | 113.9 | 57.76 | V-C | 0.2174.599 | | 40 | 27 | 0 | 0 | 84.76 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------|-------|------------|----|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Muro: | | LEFT | Lato | | RIGHT | | | | |
| | | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 2 | -6.3 | 115.35 | 58.495 | V-C | 0.2174.599 | | 40 | 28 | 0 | 0 | 86.495 |
| Stage 2 | -6.4 | 116.8 | 59.228 | V-C | 0.2174.599 | | 40 | 29 | 0 | 0 | 88.228 |
| Stage 2 | -6.5 | 118.25 | 59.962 | V-C | 0.2174.599 | | 40 | 30 | 0 | 0 | 89.962 |
| Stage 2 | -6.6 | 119.7 | 60.695 | V-C | 0.2174.599 | | 40 | 31 | 0 | 0 | 91.695 |
| Stage 2 | -6.7 | 121.15 | 61.429 | V-C | 0.2174.599 | | 40 | 32 | 0 | 0 | 93.429 |
| Stage 2 | -6.8 | 122.6 | 62.162 | V-C | 0.2174.599 | | 40 | 33 | 0 | 0 | 95.162 |
| Stage 2 | -6.9 | 124.05 | 62.894 | V-C | 0.2174.599 | | 40 | 34 | 0 | 0 | 96.894 |
| Stage 2 | -7 | 125.5 | 63.627 | V-C | 0.2174.599 | | 40 | 35 | 0 | 0 | 98.627 |
| Stage 2 | -7.1 | 126.95 | 64.359 | V-C | 0.2174.599 | | 40 | 36 | 0 | 0 | 100.359 |
| Stage 2 | -7.2 | 128.4 | 65.092 | V-C | 0.2174.599 | | 40 | 37 | 0 | 0 | 102.092 |
| Stage 2 | -7.3 | 129.85 | 65.824 | V-C | 0.2174.599 | | 40 | 38 | 0 | 0 | 103.824 |
| Stage 2 | -7.4 | 131.3 | 66.556 | V-C | 0.2174.599 | | 40 | 39 | 0 | 0 | 105.556 |
| Stage 2 | -7.5 | 132.75 | 67.288 | V-C | 0.2174.599 | | 40 | 40 | 0 | 0 | 107.288 |
| Stage 2 | -7.6 | 134.2 | 68.019 | V-C | 0.2174.599 | | 40 | 41 | 0 | 0 | 109.019 |
| Stage 2 | -7.7 | 135.65 | 68.751 | V-C | 0.2174.599 | | 40 | 42 | 0 | 0 | 110.751 |
| Stage 2 | -7.8 | 137.1 | 69.482 | V-C | 0.2174.599 | | 40 | 43 | 0 | 0 | 112.482 |
| Stage 2 | -7.9 | 138.55 | 70.213 | V-C | 0.2174.599 | | 40 | 44 | 0 | 0 | 114.213 |
| Stage 2 | -8 | 140 | 70.945 | V-C | 0.2174.599 | | 40 | 45 | 0 | 0 | 115.944 |
| Stage 2 | -8.1 | 141.45 | 71.676 | V-C | 0.2174.599 | | 40 | 46 | 0 | 0 | 117.676 |
| Stage 2 | -8.2 | 142.9 | 72.406 | V-C | 0.2174.599 | | 40 | 47 | 0 | 0 | 119.406 |
| Stage 2 | -8.3 | 144.35 | 73.137 | V-C | 0.2174.599 | | 40 | 48 | 0 | 0 | 121.137 |
| Stage 2 | -8.4 | 145.8 | 73.867 | V-C | 0.2174.599 | | 40 | 49 | 0 | 0 | 122.867 |
| Stage 2 | -8.5 | 147.25 | 74.598 | V-C | 0.2174.599 | | 40 | 50 | 0 | 0 | 124.598 |
| Stage 2 | -8.6 | 148.7 | 75.327 | V-C | 0.2174.599 | | 40 | 51 | 0 | 0 | 126.327 |
| Stage 2 | -8.7 | 150.15 | 76.057 | V-C | 0.2174.599 | | 40 | 52 | 0 | 0 | 128.057 |
| Stage 2 | -8.8 | 151.6 | 76.786 | V-C | 0.2174.599 | | 40 | 53 | 0 | 0 | 129.786 |
| Stage 2 | -8.9 | 153.05 | 77.515 | V-C | 0.2174.599 | | 40 | 54 | 0 | 0 | 131.515 |
| Stage 2 | -9 | 154.5 | 78.244 | V-C | 0.2174.599 | | 40 | 55 | 0 | 0 | 133.244 |
| Stage 2 | -9.1 | 155.95 | 78.972 | V-C | 0.2174.599 | | 40 | 56 | 0 | 0 | 134.972 |
| Stage 2 | -9.2 | 157.4 | 79.699 | V-C | 0.2174.599 | | 40 | 57 | 0 | 0 | 136.699 |
| Stage 2 | -9.3 | 158.85 | 80.426 | V-C | 0.2174.599 | | 40 | 58 | 0 | 0 | 138.426 |
| Stage 2 | -9.4 | 160.3 | 81.153 | V-C | 0.2174.599 | | 40 | 59 | 0 | 0 | 140.153 |
| Stage 2 | -9.5 | 161.75 | 81.879 | V-C | 0.2174.599 | | 40 | 60 | 0 | 0 | 141.879 |
| Stage 2 | -9.6 | 163.2 | 82.605 | V-C | 0.2174.599 | | 40 | 61 | 0 | 0 | 143.605 |
| Stage 2 | -9.7 | 164.65 | 83.33 | V-C | 0.2174.599 | | 40 | 62 | 0 | 0 | 145.33 |
| Stage 2 | -9.8 | 166.1 | 84.056 | V-C | 0.2174.599 | | 40 | 63 | 0 | 0 | 147.056 |
| Stage 2 | -9.9 | 167.55 | 84.781 | V-C | 0.2174.599 | | 40 | 64 | 0 | 0 | 148.781 |
| Stage 2 | -10 | 169 | 85.506 | V-C | 0.2174.599 | | 40 | 65 | 0 | 0 | 150.506 |

Tabella Risultati Terreno Left Wall - Nominal - Stage A

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|---------|---------|---------------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | LEFT Ka | Lato Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage A | 0 | 0 | 0 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.1 | 1.9 | 0.608 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.608 |
| Stage A | -0.2 | 3.803 | 1.217 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.217 |
| Stage A | -0.3 | 5.709 | 1.827 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.827 |
| Stage A | -0.4 | 7.621 | 2.439 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.439 |
| Stage A | -0.5 | 9.541 | 3.053 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.053 |
| Stage A | -0.6 | 11.469 | 3.67 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.67 |
| Stage A | -0.7 | 13.406 | 4.29 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.29 |
| Stage A | -0.8 | 15.353 | 4.913 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.913 |
| Stage A | -0.9 | 17.311 | 5.539 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.539 |
| Stage A | -1 | 19.278 | 6.169 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.169 |
| Stage A | -1.1 | 21.256 | 6.802 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.802 |
| Stage A | -1.2 | 23.242 | 7.438 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.438 |
| Stage A | -1.3 | 25.237 | 8.076 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.076 |
| Stage A | -1.4 | 27.24 | 8.717 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.717 |
| Stage A | -1.5 | 29.25 | 9.36 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.36 |
| Stage A | -1.6 | 31.265 | 10.005 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.005 |
| Stage A | -1.7 | 33.286 | 10.651 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.651 |
| Stage A | -1.8 | 35.31 | 11.299 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.299 |
| Stage A | -1.9 | 37.337 | 11.948 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.948 |
| Stage A | -2 | 39.367 | 0 | ACTIVE | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 0 |
| Stage A | -2.1 | 41.948 | 0 | ACTIVE | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 0 |
| Stage A | -2.2 | 44.529 | 0 | ACTIVE | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 0 |
| Stage A | -2.3 | 47.111 | 0 | ACTIVE | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 0 |
| Stage A | -2.4 | 49.692 | 5.533 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 5.533 |
| Stage A | -2.5 | 52.272 | 11.266 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 11.266 |
| Stage A | -2.6 | 54.85 | 16.168 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 16.168 |
| Stage A | -2.7 | 57.427 | 20.316 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 20.316 |
| Stage A | -2.8 | 60.001 | 23.794 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 23.794 |
| Stage A | -2.9 | 62.573 | 26.687 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 26.687 |
| Stage A | -3 | 65.143 | 29.081 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 29.081 |
| Stage A | -3.1 | 67.9 | 31.155 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 31.155 |
| Stage A | -3.2 | 70.524 | 32.824 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 32.824 |
| Stage A | -3.3 | 73.141 | 34.222 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 34.222 |
| Stage A | -3.4 | 75.96 | 35.515 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 35.515 |
| Stage A | -3.5 | 78.558 | 36.545 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 36.545 |
| Stage A | -3.6 | 80.348 | 37.065 | UL-RL | 0.217 | 4.599 | 40 | 1 | 0 | 0 | 38.065 |
| Stage A | -3.7 | 81.929 | 37.414 | UL-RL | 0.217 | 4.599 | 40 | 2 | 0 | 0 | 39.414 |
| Stage A | -3.8 | 83.505 | 37.723 | UL-RL | 0.217 | 4.599 | 40 | 3 | 0 | 0 | 40.723 |
| Stage A | -3.9 | 85.26 | 38.111 | UL-RL | 0.217 | 4.599 | 40 | 4 | 0 | 0 | 42.111 |
| Stage A | -4 | 86.823 | 38.409 | UL-RL | 0.217 | 4.599 | 40 | 5 | 0 | 0 | 43.409 |
| Stage A | -4.1 | 88.382 | 38.728 | UL-RL | 0.217 | 4.599 | 40 | 6 | 0 | 0 | 44.727 |
| Stage A | -4.2 | 90.108 | 39.16 | UL-RL | 0.217 | 4.599 | 40 | 7 | 0 | 0 | 46.16 |
| Stage A | -4.3 | 91.656 | 39.541 | UL-RL | 0.217 | 4.599 | 40 | 8 | 0 | 0 | 47.541 |
| Stage A | -4.4 | 93.363 | 40.043 | UL-RL | 0.217 | 4.599 | 40 | 9 | 0 | 0 | 49.042 |
| Stage A | -4.5 | 94.901 | 40.501 | UL-RL | 0.217 | 4.599 | 40 | 10 | 0 | 0 | 50.501 |
| Stage A | -4.6 | 96.436 | 41 | UL-RL | 0.217 | 4.599 | 40 | 11 | 0 | 0 | 52 |
| Stage A | -4.7 | 98.121 | 41.612 | UL-RL | 0.217 | 4.599 | 40 | 12 | 0 | 0 | 53.612 |
| Stage A | -4.8 | 99.648 | 42.182 | UL-RL | 0.217 | 4.599 | 40 | 13 | 0 | 0 | 55.182 |
| Stage A | -4.9 | 101.319 | 42.857 | UL-RL | 0.217 | 4.599 | 40 | 14 | 0 | 0 | 56.857 |
| Stage A | -5 | 102.839 | 43.486 | UL-RL | 0.217 | 4.599 | 40 | 15 | 0 | 0 | 58.486 |
| Stage A | -5.1 | 104.357 | 44.139 | UL-RL | 0.217 | 4.599 | 40 | 16 | 0 | 0 | 60.139 |
| Stage A | -5.2 | 106.011 | 44.881 | UL-RL | 0.217 | 4.599 | 40 | 17 | 0 | 0 | 61.881 |
| Stage A | -5.3 | 107.522 | 45.571 | UL-RL | 0.217 | 4.599 | 40 | 18 | 0 | 0 | 63.571 |
| Stage A | -5.4 | 109.165 | 46.341 | UL-RL | 0.217 | 4.599 | 40 | 19 | 0 | 0 | 65.341 |
| Stage A | -5.5 | 110.671 | 47.055 | UL-RL | 0.217 | 4.599 | 40 | 20 | 0 | 0 | 67.055 |
| Stage A | -5.6 | 112.176 | 47.777 | UL-RL | 0.217 | 4.599 | 40 | 21 | 0 | 0 | 68.777 |
| Stage A | -5.7 | 113.804 | 48.569 | UL-RL | 0.217 | 4.599 | 40 | 22 | 0 | 0 | 70.569 |
| Stage A | -5.8 | 115.304 | 49.301 | UL-RL | 0.217 | 4.599 | 40 | 23 | 0 | 0 | 72.301 |
| Stage A | -5.9 | 116.802 | 50.036 | UL-RL | 0.217 | 4.599 | 40 | 24 | 0 | 0 | 74.036 |
| Stage A | -6 | 118.419 | 50.832 | UL-RL | 0.217 | 4.599 | 40 | 25 | 0 | 0 | 75.832 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage A | -6.1 | 119.914 | 51.568 | UL-RL | 0.2174.599 | 40 | 26 | 0 | 0 | 77.568 |
| Stage A | -6.2 | 121.522 | 52.361 | UL-RL | 0.2174.599 | 40 | 27 | 0 | 0 | 79.361 |
| Stage A | -6.3 | 123.013 | 53.095 | UL-RL | 0.2174.599 | 40 | 28 | 0 | 0 | 81.095 |
| Stage A | -6.4 | 124.502 | 53.828 | UL-RL | 0.2174.599 | 40 | 29 | 0 | 0 | 82.828 |
| Stage A | -6.5 | 126.101 | 54.614 | UL-RL | 0.2174.599 | 40 | 30 | 0 | 0 | 84.614 |
| Stage A | -6.6 | 127.587 | 55.343 | UL-RL | 0.2174.599 | 40 | 31 | 0 | 0 | 86.343 |
| Stage A | -6.7 | 129.179 | 56.124 | UL-RL | 0.2174.599 | 40 | 32 | 0 | 0 | 88.124 |
| Stage A | -6.8 | 130.662 | 56.85 | UL-RL | 0.2174.599 | 40 | 33 | 0 | 0 | 89.85 |
| Stage A | -6.9 | 132.145 | 57.574 | UL-RL | 0.2174.599 | 40 | 34 | 0 | 0 | 91.574 |
| Stage A | -7 | 133.729 | 58.348 | UL-RL | 0.2174.599 | 40 | 35 | 0 | 0 | 93.348 |
| Stage A | -7.1 | 135.208 | 59.069 | UL-RL | 0.2174.599 | 40 | 36 | 0 | 0 | 95.069 |
| Stage A | -7.2 | 136.787 | 59.839 | UL-RL | 0.2174.599 | 40 | 37 | 0 | 0 | 96.839 |
| Stage A | -7.3 | 138.264 | 60.558 | UL-RL | 0.2174.599 | 40 | 38 | 0 | 0 | 98.558 |
| Stage A | -7.4 | 139.741 | 61.276 | UL-RL | 0.2174.599 | 40 | 39 | 0 | 0 | 100.276 |
| Stage A | -7.5 | 141.312 | 62.041 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 102.041 |
| Stage A | -7.6 | 142.787 | 62.758 | UL-RL | 0.2174.599 | 40 | 41 | 0 | 0 | 103.758 |
| Stage A | -7.7 | 144.26 | 63.475 | UL-RL | 0.2174.599 | 40 | 42 | 0 | 0 | 105.475 |
| Stage A | -7.8 | 145.826 | 64.237 | UL-RL | 0.2174.599 | 40 | 43 | 0 | 0 | 107.237 |
| Stage A | -7.9 | 147.298 | 64.953 | UL-RL | 0.2174.599 | 40 | 44 | 0 | 0 | 108.953 |
| Stage A | -8 | 148.859 | 65.713 | UL-RL | 0.2174.599 | 40 | 45 | 0 | 0 | 110.713 |
| Stage A | -8.1 | 150.329 | 66.429 | UL-RL | 0.2174.599 | 40 | 46 | 0 | 0 | 112.429 |
| Stage A | -8.2 | 151.798 | 67.145 | UL-RL | 0.2174.599 | 40 | 47 | 0 | 0 | 114.144 |
| Stage A | -8.3 | 153.354 | 67.904 | UL-RL | 0.2174.599 | 40 | 48 | 0 | 0 | 115.904 |
| Stage A | -8.4 | 154.822 | 68.62 | UL-RL | 0.2174.599 | 40 | 49 | 0 | 0 | 117.62 |
| Stage A | -8.5 | 156.374 | 69.38 | UL-RL | 0.2174.599 | 40 | 50 | 0 | 0 | 119.38 |
| Stage A | -8.6 | 157.84 | 70.097 | UL-RL | 0.2174.599 | 40 | 51 | 0 | 0 | 121.097 |
| Stage A | -8.7 | 159.307 | 70.816 | UL-RL | 0.2174.599 | 40 | 52 | 0 | 0 | 122.816 |
| Stage A | -8.8 | 160.854 | 71.576 | UL-RL | 0.2174.599 | 40 | 53 | 0 | 0 | 124.576 |
| Stage A | -8.9 | 162.319 | 72.296 | UL-RL | 0.2174.599 | 40 | 54 | 0 | 0 | 126.296 |
| Stage A | -9 | 163.863 | 73.058 | UL-RL | 0.2174.599 | 40 | 55 | 0 | 0 | 128.058 |
| Stage A | -9.1 | 165.326 | 73.781 | UL-RL | 0.2174.599 | 40 | 56 | 0 | 0 | 129.781 |
| Stage A | -9.2 | 166.79 | 74.506 | UL-RL | 0.2174.599 | 40 | 57 | 0 | 0 | 131.506 |
| Stage A | -9.3 | 168.33 | 75.271 | UL-RL | 0.2174.599 | 40 | 58 | 0 | 0 | 133.271 |
| Stage A | -9.4 | 169.792 | 75.998 | UL-RL | 0.2174.599 | 40 | 59 | 0 | 0 | 134.998 |
| Stage A | -9.5 | 171.254 | 76.727 | UL-RL | 0.2174.599 | 40 | 60 | 0 | 0 | 136.727 |
| Stage A | -9.6 | 172.64 | 77.42 | UL-RL | 0.2174.599 | 40 | 61 | 0 | 0 | 138.42 |
| Stage A | -9.7 | 174.028 | 78.114 | UL-RL | 0.2174.599 | 40 | 62 | 0 | 0 | 140.114 |
| Stage A | -9.8 | 175.416 | 78.809 | UL-RL | 0.2174.599 | 40 | 63 | 0 | 0 | 141.809 |
| Stage A | -9.9 | 176.805 | 79.505 | UL-RL | 0.2174.599 | 40 | 64 | 0 | 0 | 143.505 |
| Stage A | -10 | 178.195 | 80.202 | UL-RL | 0.2174.599 | 40 | 65 | 0 | 0 | 145.202 |

| Design Assumption: Nominal Risultati Terreno | | | Muro: | LEFT | Lato | RIGHT | | | | | |
|--|-------|---------------|---------------|---------|------------|-------|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage A | 0 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.5 | 0 | 0 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.6 | 1.9 | 5.89 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.89 |
| Stage A | -1.7 | 3.8 | 11.78 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.78 |
| Stage A | -1.8 | 5.7 | 17.35 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.35 |
| Stage A | -1.9 | 7.6 | 17.174 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.174 |
| Stage A | -2 | 9.5 | 25.627 | V-C | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 25.627 |
| Stage A | -2.1 | 11.95 | 24.812 | V-C | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 24.812 |
| Stage A | -2.2 | 14.4 | 24.211 | V-C | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 24.211 |
| Stage A | -2.3 | 16.85 | 23.84 | V-C | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 23.84 |
| Stage A | -2.4 | 19.3 | 23.45 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 23.45 |
| Stage A | -2.5 | 21.75 | 22.855 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 22.855 |
| Stage A | -2.6 | 24.2 | 22.603 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 22.603 |
| Stage A | -2.7 | 26.65 | 22.665 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 22.665 |
| Stage A | -2.8 | 29.1 | 23.006 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 23.006 |
| Stage A | -2.9 | 31.55 | 23.591 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 23.591 |
| Stage A | -3 | 34 | 24.384 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 24.384 |
| Stage A | -3.1 | 36.45 | 25.35 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 25.35 |
| Stage A | -3.2 | 38.9 | 26.457 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 26.457 |
| Stage A | -3.3 | 41.35 | 27.676 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 27.676 |
| Stage A | -3.4 | 43.8 | 28.98 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 28.98 |
| Stage A | -3.5 | 46.25 | 30.346 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 30.346 |
| Stage A | -3.6 | 47.7 | 31.242 | UL-RL | 0.2174.599 | 40 | 1 | 0 | 0 | 0 | 32.242 |
| Stage A | -3.7 | 49.15 | 32.166 | UL-RL | 0.2174.599 | 40 | 2 | 0 | 0 | 0 | 34.166 |
| Stage A | -3.8 | 50.6 | 33.105 | UL-RL | 0.2174.599 | 40 | 3 | 0 | 0 | 0 | 36.105 |
| Stage A | -3.9 | 52.05 | 34.049 | UL-RL | 0.2174.599 | 40 | 4 | 0 | 0 | 0 | 38.049 |
| Stage A | -4 | 53.5 | 34.988 | UL-RL | 0.2174.599 | 40 | 5 | 0 | 0 | 0 | 39.988 |
| Stage A | -4.1 | 54.95 | 35.919 | UL-RL | 0.2174.599 | 40 | 6 | 0 | 0 | 0 | 41.918 |
| Stage A | -4.2 | 56.4 | 36.835 | UL-RL | 0.2174.599 | 40 | 7 | 0 | 0 | 0 | 43.835 |
| Stage A | -4.3 | 57.85 | 37.734 | UL-RL | 0.2174.599 | 40 | 8 | 0 | 0 | 0 | 45.734 |
| Stage A | -4.4 | 59.3 | 38.616 | UL-RL | 0.2174.599 | 40 | 9 | 0 | 0 | 0 | 47.616 |
| Stage A | -4.5 | 60.75 | 39.479 | UL-RL | 0.2174.599 | 40 | 10 | 0 | 0 | 0 | 49.479 |
| Stage A | -4.6 | 62.2 | 40.324 | UL-RL | 0.2174.599 | 40 | 11 | 0 | 0 | 0 | 51.324 |
| Stage A | -4.7 | 63.65 | 41.153 | UL-RL | 0.2174.599 | 40 | 12 | 0 | 0 | 0 | 53.153 |
| Stage A | -4.8 | 65.1 | 41.965 | UL-RL | 0.2174.599 | 40 | 13 | 0 | 0 | 0 | 54.965 |
| Stage A | -4.9 | 66.55 | 42.763 | UL-RL | 0.2174.599 | 40 | 14 | 0 | 0 | 0 | 56.763 |
| Stage A | -5 | 68 | 43.548 | UL-RL | 0.2174.599 | 40 | 15 | 0 | 0 | 0 | 58.548 |
| Stage A | -5.1 | 69.45 | 44.321 | UL-RL | 0.2174.599 | 40 | 16 | 0 | 0 | 0 | 60.321 |
| Stage A | -5.2 | 70.9 | 45.086 | UL-RL | 0.2174.599 | 40 | 17 | 0 | 0 | 0 | 62.086 |
| Stage A | -5.3 | 72.35 | 45.842 | UL-RL | 0.2174.599 | 40 | 18 | 0 | 0 | 0 | 63.842 |
| Stage A | -5.4 | 73.8 | 46.592 | UL-RL | 0.2174.599 | 40 | 19 | 0 | 0 | 0 | 65.592 |
| Stage A | -5.5 | 75.25 | 47.337 | UL-RL | 0.2174.599 | 40 | 20 | 0 | 0 | 0 | 67.337 |
| Stage A | -5.6 | 76.7 | 48.077 | UL-RL | 0.2174.599 | 40 | 21 | 0 | 0 | 0 | 69.077 |
| Stage A | -5.7 | 78.15 | 48.814 | UL-RL | 0.2174.599 | 40 | 22 | 0 | 0 | 0 | 70.814 |
| Stage A | -5.8 | 79.6 | 49.55 | UL-RL | 0.2174.599 | 40 | 23 | 0 | 0 | 0 | 72.55 |
| Stage A | -5.9 | 81.05 | 50.283 | UL-RL | 0.2174.599 | 40 | 24 | 0 | 0 | 0 | 74.283 |
| Stage A | -6 | 82.5 | 51.016 | UL-RL | 0.2174.599 | 40 | 25 | 0 | 0 | 0 | 76.016 |
| Stage A | -6.1 | 83.95 | 51.748 | UL-RL | 0.2174.599 | 40 | 26 | 0 | 0 | 0 | 77.748 |
| Stage A | -6.2 | 85.4 | 52.48 | UL-RL | 0.2174.599 | 40 | 27 | 0 | 0 | 0 | 79.48 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|----------|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | RIGHT Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage A | -6.3 | 86.85 | 53.212 | UL-RL | 0.2174.599 | | 40 | 28 | 0 | 0 | 81.212 |
| Stage A | -6.4 | 88.3 | 53.944 | UL-RL | 0.2174.599 | | 40 | 29 | 0 | 0 | 82.944 |
| Stage A | -6.5 | 89.75 | 54.676 | UL-RL | 0.2174.599 | | 40 | 30 | 0 | 0 | 84.676 |
| Stage A | -6.6 | 91.2 | 55.409 | UL-RL | 0.2174.599 | | 40 | 31 | 0 | 0 | 86.409 |
| Stage A | -6.7 | 92.65 | 56.142 | UL-RL | 0.2174.599 | | 40 | 32 | 0 | 0 | 88.142 |
| Stage A | -6.8 | 94.1 | 56.876 | UL-RL | 0.2174.599 | | 40 | 33 | 0 | 0 | 89.876 |
| Stage A | -6.9 | 95.55 | 57.61 | UL-RL | 0.2174.599 | | 40 | 34 | 0 | 0 | 91.61 |
| Stage A | -7 | 97 | 58.344 | UL-RL | 0.2174.599 | | 40 | 35 | 0 | 0 | 93.344 |
| Stage A | -7.1 | 98.45 | 59.079 | UL-RL | 0.2174.599 | | 40 | 36 | 0 | 0 | 95.079 |
| Stage A | -7.2 | 99.9 | 59.814 | UL-RL | 0.2174.599 | | 40 | 37 | 0 | 0 | 96.814 |
| Stage A | -7.3 | 101.35 | 60.549 | UL-RL | 0.2174.599 | | 40 | 38 | 0 | 0 | 98.549 |
| Stage A | -7.4 | 102.8 | 61.284 | UL-RL | 0.2174.599 | | 40 | 39 | 0 | 0 | 100.284 |
| Stage A | -7.5 | 104.25 | 62.019 | UL-RL | 0.2174.599 | | 40 | 40 | 0 | 0 | 102.019 |
| Stage A | -7.6 | 105.7 | 62.754 | UL-RL | 0.2174.599 | | 40 | 41 | 0 | 0 | 103.754 |
| Stage A | -7.7 | 107.15 | 63.489 | UL-RL | 0.2174.599 | | 40 | 42 | 0 | 0 | 105.489 |
| Stage A | -7.8 | 108.6 | 64.224 | UL-RL | 0.2174.599 | | 40 | 43 | 0 | 0 | 107.224 |
| Stage A | -7.9 | 110.05 | 64.959 | UL-RL | 0.2174.599 | | 40 | 44 | 0 | 0 | 108.959 |
| Stage A | -8 | 111.5 | 65.694 | UL-RL | 0.2174.599 | | 40 | 45 | 0 | 0 | 110.694 |
| Stage A | -8.1 | 112.95 | 66.428 | UL-RL | 0.2174.599 | | 40 | 46 | 0 | 0 | 112.428 |
| Stage A | -8.2 | 114.4 | 67.163 | UL-RL | 0.2174.599 | | 40 | 47 | 0 | 0 | 114.162 |
| Stage A | -8.3 | 115.85 | 67.897 | UL-RL | 0.2174.599 | | 40 | 48 | 0 | 0 | 115.897 |
| Stage A | -8.4 | 117.3 | 68.63 | UL-RL | 0.2174.599 | | 40 | 49 | 0 | 0 | 117.63 |
| Stage A | -8.5 | 118.75 | 69.364 | UL-RL | 0.2174.599 | | 40 | 50 | 0 | 0 | 119.364 |
| Stage A | -8.6 | 120.2 | 70.097 | UL-RL | 0.2174.599 | | 40 | 51 | 0 | 0 | 121.097 |
| Stage A | -8.7 | 121.65 | 70.83 | UL-RL | 0.2174.599 | | 40 | 52 | 0 | 0 | 122.83 |
| Stage A | -8.8 | 123.1 | 71.562 | UL-RL | 0.2174.599 | | 40 | 53 | 0 | 0 | 124.562 |
| Stage A | -8.9 | 124.55 | 72.294 | UL-RL | 0.2174.599 | | 40 | 54 | 0 | 0 | 126.294 |
| Stage A | -9 | 126 | 73.025 | UL-RL | 0.2174.599 | | 40 | 55 | 0 | 0 | 128.025 |
| Stage A | -9.1 | 127.45 | 73.756 | UL-RL | 0.2174.599 | | 40 | 56 | 0 | 0 | 129.756 |
| Stage A | -9.2 | 128.9 | 74.486 | UL-RL | 0.2174.599 | | 40 | 57 | 0 | 0 | 131.486 |
| Stage A | -9.3 | 130.35 | 75.215 | UL-RL | 0.2174.599 | | 40 | 58 | 0 | 0 | 133.215 |
| Stage A | -9.4 | 131.8 | 75.944 | UL-RL | 0.2174.599 | | 40 | 59 | 0 | 0 | 134.944 |
| Stage A | -9.5 | 133.25 | 76.673 | UL-RL | 0.2174.599 | | 40 | 60 | 0 | 0 | 136.673 |
| Stage A | -9.6 | 134.7 | 77.401 | UL-RL | 0.2174.599 | | 40 | 61 | 0 | 0 | 138.401 |
| Stage A | -9.7 | 136.15 | 78.129 | UL-RL | 0.2174.599 | | 40 | 62 | 0 | 0 | 140.129 |
| Stage A | -9.8 | 137.6 | 78.857 | UL-RL | 0.2174.599 | | 40 | 63 | 0 | 0 | 141.857 |
| Stage A | -9.9 | 139.05 | 79.584 | UL-RL | 0.2174.599 | | 40 | 64 | 0 | 0 | 143.584 |
| Stage A | -10 | 140.5 | 80.311 | UL-RL | 0.2174.599 | | 40 | 65 | 0 | 0 | 145.311 |

Tabella Risultati Terreno Left Wall - Nominal - Stage B

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|---------------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage B | 0 | 0 | 0 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 |
| Stage B | -0.1 | 1.9 | 5.891 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 5.891 |
| Stage B | -0.2 | 3.803 | 11.788 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 11.788 |
| Stage B | -0.3 | 5.709 | 17.698 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 17.698 |
| Stage B | -0.4 | 7.621 | 23.626 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 23.626 |
| Stage B | -0.5 | 9.541 | 29.576 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 29.576 |
| Stage B | -0.6 | 11.469 | 35.552 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 35.552 |
| Stage B | -0.7 | 13.406 | 41.558 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 41.558 |
| Stage B | -0.8 | 15.353 | 47.595 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 47.595 |
| Stage B | -0.9 | 17.311 | 50.688 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 50.688 |
| Stage B | -1 | 19.278 | 50.06 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 50.06 |
| Stage B | -1.1 | 21.256 | 49.234 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 49.234 |
| Stage B | -1.2 | 23.242 | 48.144 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 48.144 |
| Stage B | -1.3 | 25.237 | 46.717 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 46.717 |
| Stage B | -1.4 | 27.24 | 44.903 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 44.903 |
| Stage B | -1.5 | 29.25 | 42.782 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 42.782 |
| Stage B | -1.6 | 31.265 | 40.46 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 40.46 |
| Stage B | -1.7 | 33.286 | 38.035 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 38.035 |
| Stage B | -1.8 | 35.31 | 35.597 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 35.597 |
| Stage B | -1.9 | 37.337 | 33.228 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 33.228 |
| Stage B | -2 | 39.367 | 60.11 | V-C | 0.2174.599 | | 40 | 0 | 0 | 60.11 |
| Stage B | -2.1 | 41.948 | 51.172 | V-C | 0.2174.599 | | 40 | 0 | 0 | 51.172 |
| Stage B | -2.2 | 44.529 | 43.06 | V-C | 0.2174.599 | | 40 | 0 | 0 | 43.06 |
| Stage B | -2.3 | 47.111 | 35.866 | V-C | 0.2174.599 | | 40 | 0 | 0 | 35.866 |
| Stage B | -2.4 | 49.692 | 33.089 | V-C | 0.2174.599 | | 40 | 0 | 0 | 33.089 |
| Stage B | -2.5 | 52.272 | 31.393 | V-C | 0.2174.599 | | 40 | 0 | 0 | 31.393 |
| Stage B | -2.6 | 54.85 | 30.1 | V-C | 0.2174.599 | | 40 | 0 | 0 | 30.1 |
| Stage B | -2.7 | 57.427 | 29.132 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 29.132 |
| Stage B | -2.8 | 60.001 | 27.88 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 27.88 |
| Stage B | -2.9 | 62.573 | 26.814 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 26.814 |
| Stage B | -3 | 65.143 | 26.242 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 26.242 |
| Stage B | -3.1 | 67.9 | 26.198 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 26.198 |
| Stage B | -3.2 | 70.524 | 26.464 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 26.464 |
| Stage B | -3.3 | 73.141 | 27.042 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 27.042 |
| Stage B | -3.4 | 75.96 | 27.983 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 27.983 |
| Stage B | -3.5 | 78.558 | 29.024 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 29.024 |
| Stage B | -3.6 | 80.348 | 29.826 | UL-RL | 0.2174.599 | | 40 | 1 | 0 | 30.826 |
| Stage B | -3.7 | 81.929 | 30.648 | UL-RL | 0.2174.599 | | 40 | 2 | 0 | 32.648 |
| Stage B | -3.8 | 83.505 | 31.558 | UL-RL | 0.2174.599 | | 40 | 3 | 0 | 34.558 |
| Stage B | -3.9 | 85.26 | 32.619 | UL-RL | 0.2174.599 | | 40 | 4 | 0 | 36.619 |
| Stage B | -4 | 86.823 | 33.621 | UL-RL | 0.2174.599 | | 40 | 5 | 0 | 38.621 |
| Stage B | -4.1 | 88.382 | 34.64 | UL-RL | 0.2174.599 | | 40 | 6 | 0 | 40.64 |
| Stage B | -4.2 | 90.108 | 35.746 | UL-RL | 0.2174.599 | | 40 | 7 | 0 | 42.746 |
| Stage B | -4.3 | 91.656 | 36.755 | UL-RL | 0.2174.599 | | 40 | 8 | 0 | 44.755 |
| Stage B | -4.4 | 93.363 | 37.827 | UL-RL | 0.2174.599 | | 40 | 9 | 0 | 46.827 |
| Stage B | -4.5 | 94.901 | 38.794 | UL-RL | 0.2174.599 | | 40 | 10 | 0 | 48.794 |
| Stage B | -4.6 | 96.436 | 39.734 | UL-RL | 0.2174.599 | | 40 | 11 | 0 | 50.734 |
| Stage B | -4.7 | 98.121 | 40.724 | UL-RL | 0.2174.599 | | 40 | 12 | 0 | 52.724 |
| Stage B | -4.8 | 99.648 | 41.608 | UL-RL | 0.2174.599 | | 40 | 13 | 0 | 54.608 |
| Stage B | -4.9 | 101.319 | 42.539 | UL-RL | 0.2174.599 | | 40 | 14 | 0 | 56.539 |
| Stage B | -5 | 102.839 | 43.371 | UL-RL | 0.2174.599 | | 40 | 15 | 0 | 58.371 |
| Stage B | -5.1 | 104.357 | 44.18 | UL-RL | 0.2174.599 | | 40 | 16 | 0 | 60.18 |
| Stage B | -5.2 | 106.011 | 45.038 | UL-RL | 0.2174.599 | | 40 | 17 | 0 | 62.038 |
| Stage B | -5.3 | 107.522 | 45.808 | UL-RL | 0.2174.599 | | 40 | 18 | 0 | 63.808 |
| Stage B | -5.4 | 109.165 | 46.63 | UL-RL | 0.2174.599 | | 40 | 19 | 0 | 65.63 |
| Stage B | -5.5 | 110.671 | 47.372 | UL-RL | 0.2174.599 | | 40 | 20 | 0 | 67.372 |
| Stage B | -5.6 | 112.176 | 48.104 | UL-RL | 0.2174.599 | | 40 | 21 | 0 | 69.104 |
| Stage B | -5.7 | 113.804 | 48.891 | UL-RL | 0.2174.599 | | 40 | 22 | 0 | 70.891 |
| Stage B | -5.8 | 115.304 | 49.608 | UL-RL | 0.2174.599 | | 40 | 23 | 0 | 72.608 |
| Stage B | -5.9 | 116.802 | 50.32 | UL-RL | 0.2174.599 | | 40 | 24 | 0 | 74.32 |
| Stage B | -6 | 118.419 | 51.089 | UL-RL | 0.2174.599 | | 40 | 25 | 0 | 76.089 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|----------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage B | -6.1 | 119.914 | 51.795 | UL-RL | 0.2174.599 | | 40 | 26 | 0 | 77.795 |
| Stage B | -6.2 | 121.522 | 52.558 | UL-RL | 0.2174.599 | | 40 | 27 | 0 | 79.558 |
| Stage B | -6.3 | 123.013 | 53.262 | UL-RL | 0.2174.599 | | 40 | 28 | 0 | 81.262 |
| Stage B | -6.4 | 124.502 | 53.966 | UL-RL | 0.2174.599 | | 40 | 29 | 0 | 82.966 |
| Stage B | -6.5 | 126.101 | 54.726 | UL-RL | 0.2174.599 | | 40 | 30 | 0 | 84.726 |
| Stage B | -6.6 | 127.587 | 55.432 | UL-RL | 0.2174.599 | | 40 | 31 | 0 | 86.432 |
| Stage B | -6.7 | 129.179 | 56.192 | UL-RL | 0.2174.599 | | 40 | 32 | 0 | 88.192 |
| Stage B | -6.8 | 130.662 | 56.899 | UL-RL | 0.2174.599 | | 40 | 33 | 0 | 89.899 |
| Stage B | -6.9 | 132.145 | 57.608 | UL-RL | 0.2174.599 | | 40 | 34 | 0 | 91.608 |
| Stage B | -7 | 133.729 | 58.369 | UL-RL | 0.2174.599 | | 40 | 35 | 0 | 93.369 |
| Stage B | -7.1 | 135.208 | 59.08 | UL-RL | 0.2174.599 | | 40 | 36 | 0 | 95.08 |
| Stage B | -7.2 | 136.787 | 59.842 | UL-RL | 0.2174.599 | | 40 | 37 | 0 | 96.841 |
| Stage B | -7.3 | 138.264 | 60.554 | UL-RL | 0.2174.599 | | 40 | 38 | 0 | 98.554 |
| Stage B | -7.4 | 139.741 | 61.268 | UL-RL | 0.2174.599 | | 40 | 39 | 0 | 100.268 |
| Stage B | -7.5 | 141.312 | 62.03 | UL-RL | 0.2174.599 | | 40 | 40 | 0 | 102.03 |
| Stage B | -7.6 | 142.787 | 62.745 | UL-RL | 0.2174.599 | | 40 | 41 | 0 | 103.745 |
| Stage B | -7.7 | 144.26 | 63.461 | UL-RL | 0.2174.599 | | 40 | 42 | 0 | 105.461 |
| Stage B | -7.8 | 145.826 | 64.223 | UL-RL | 0.2174.599 | | 40 | 43 | 0 | 107.223 |
| Stage B | -7.9 | 147.298 | 64.939 | UL-RL | 0.2174.599 | | 40 | 44 | 0 | 108.939 |
| Stage B | -8 | 148.859 | 65.7 | UL-RL | 0.2174.599 | | 40 | 45 | 0 | 110.7 |
| Stage B | -8.1 | 150.329 | 66.417 | UL-RL | 0.2174.599 | | 40 | 46 | 0 | 112.417 |
| Stage B | -8.2 | 151.798 | 67.134 | UL-RL | 0.2174.599 | | 40 | 47 | 0 | 114.134 |
| Stage B | -8.3 | 153.354 | 67.895 | UL-RL | 0.2174.599 | | 40 | 48 | 0 | 115.894 |
| Stage B | -8.4 | 154.822 | 68.612 | UL-RL | 0.2174.599 | | 40 | 49 | 0 | 117.612 |
| Stage B | -8.5 | 156.374 | 69.373 | UL-RL | 0.2174.599 | | 40 | 50 | 0 | 119.373 |
| Stage B | -8.6 | 157.84 | 70.091 | UL-RL | 0.2174.599 | | 40 | 51 | 0 | 121.091 |
| Stage B | -8.7 | 159.307 | 70.811 | UL-RL | 0.2174.599 | | 40 | 52 | 0 | 122.811 |
| Stage B | -8.8 | 160.854 | 71.572 | UL-RL | 0.2174.599 | | 40 | 53 | 0 | 124.572 |
| Stage B | -8.9 | 162.319 | 72.294 | UL-RL | 0.2174.599 | | 40 | 54 | 0 | 126.294 |
| Stage B | -9 | 163.863 | 73.056 | UL-RL | 0.2174.599 | | 40 | 55 | 0 | 128.056 |
| Stage B | -9.1 | 165.326 | 73.78 | UL-RL | 0.2174.599 | | 40 | 56 | 0 | 129.78 |
| Stage B | -9.2 | 166.79 | 74.505 | UL-RL | 0.2174.599 | | 40 | 57 | 0 | 131.505 |
| Stage B | -9.3 | 168.33 | 75.271 | UL-RL | 0.2174.599 | | 40 | 58 | 0 | 133.271 |
| Stage B | -9.4 | 169.792 | 75.999 | UL-RL | 0.2174.599 | | 40 | 59 | 0 | 134.998 |
| Stage B | -9.5 | 171.254 | 76.728 | UL-RL | 0.2174.599 | | 40 | 60 | 0 | 136.728 |
| Stage B | -9.6 | 172.64 | 77.421 | UL-RL | 0.2174.599 | | 40 | 61 | 0 | 138.421 |
| Stage B | -9.7 | 174.028 | 78.115 | UL-RL | 0.2174.599 | | 40 | 62 | 0 | 140.115 |
| Stage B | -9.8 | 175.416 | 78.811 | UL-RL | 0.2174.599 | | 40 | 63 | 0 | 141.811 |
| Stage B | -9.9 | 176.805 | 79.507 | UL-RL | 0.2174.599 | | 40 | 64 | 0 | 143.507 |
| Stage B | -10 | 178.195 | 80.204 | UL-RL | 0.2174.599 | | 40 | 65 | 0 | 145.204 |

| Design Assumption: Nominal Risultati Terreno | | | Muro: | LEFT | Lato | RIGHT | | | | | |
|--|-------|---------------|---------------|---------|------------|-------|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage B | 0 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.5 | 0 | 0 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.6 | 1.9 | 0.608 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.608 |
| Stage B | -1.7 | 3.8 | 1.216 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.216 |
| Stage B | -1.8 | 5.7 | 1.824 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.824 |
| Stage B | -1.9 | 7.6 | 2.432 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.432 |
| Stage B | -2 | 9.5 | 0 | ACTIVE | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 0 |
| Stage B | -2.1 | 11.95 | 0 | ACTIVE | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 0 |
| Stage B | -2.2 | 14.4 | 0.059 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 0.059 |
| Stage B | -2.3 | 16.85 | 5.03 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 5.03 |
| Stage B | -2.4 | 19.3 | 9.316 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 9.316 |
| Stage B | -2.5 | 21.75 | 12.731 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 12.731 |
| Stage B | -2.6 | 24.2 | 15.846 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 15.846 |
| Stage B | -2.7 | 26.65 | 18.673 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 18.673 |
| Stage B | -2.8 | 29.1 | 21.229 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 21.229 |
| Stage B | -2.9 | 31.55 | 23.535 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 23.535 |
| Stage B | -3 | 34 | 25.618 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 25.618 |
| Stage B | -3.1 | 36.45 | 27.505 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 27.505 |
| Stage B | -3.2 | 38.9 | 29.223 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 29.223 |
| Stage B | -3.3 | 41.35 | 30.798 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 30.798 |
| Stage B | -3.4 | 43.8 | 32.255 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 32.255 |
| Stage B | -3.5 | 46.25 | 33.617 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 0 | 33.617 |
| Stage B | -3.6 | 47.7 | 34.39 | UL-RL | 0.2174.599 | 40 | 40 | 1 | 0 | 0 | 35.39 |
| Stage B | -3.7 | 49.15 | 35.108 | UL-RL | 0.2174.599 | 40 | 40 | 2 | 0 | 0 | 37.108 |
| Stage B | -3.8 | 50.6 | 35.786 | UL-RL | 0.2174.599 | 40 | 40 | 3 | 0 | 0 | 38.786 |
| Stage B | -3.9 | 52.05 | 36.437 | UL-RL | 0.2174.599 | 40 | 40 | 4 | 0 | 0 | 40.437 |
| Stage B | -4 | 53.5 | 37.071 | UL-RL | 0.2174.599 | 40 | 40 | 5 | 0 | 0 | 42.071 |
| Stage B | -4.1 | 54.95 | 37.696 | UL-RL | 0.2174.599 | 40 | 40 | 6 | 0 | 0 | 43.696 |
| Stage B | -4.2 | 56.4 | 38.32 | UL-RL | 0.2174.599 | 40 | 40 | 7 | 0 | 0 | 45.319 |
| Stage B | -4.3 | 57.85 | 38.946 | UL-RL | 0.2174.599 | 40 | 40 | 8 | 0 | 0 | 46.946 |
| Stage B | -4.4 | 59.3 | 39.579 | UL-RL | 0.2174.599 | 40 | 40 | 9 | 0 | 0 | 48.579 |
| Stage B | -4.5 | 60.75 | 40.222 | UL-RL | 0.2174.599 | 40 | 40 | 10 | 0 | 0 | 50.222 |
| Stage B | -4.6 | 62.2 | 40.875 | UL-RL | 0.2174.599 | 40 | 40 | 11 | 0 | 0 | 51.875 |
| Stage B | -4.7 | 63.65 | 41.539 | UL-RL | 0.2174.599 | 40 | 40 | 12 | 0 | 0 | 53.539 |
| Stage B | -4.8 | 65.1 | 42.214 | UL-RL | 0.2174.599 | 40 | 40 | 13 | 0 | 0 | 55.214 |
| Stage B | -4.9 | 66.55 | 42.901 | UL-RL | 0.2174.599 | 40 | 40 | 14 | 0 | 0 | 56.901 |
| Stage B | -5 | 68 | 43.598 | UL-RL | 0.2174.599 | 40 | 40 | 15 | 0 | 0 | 58.597 |
| Stage B | -5.1 | 69.45 | 44.303 | UL-RL | 0.2174.599 | 40 | 40 | 16 | 0 | 0 | 60.303 |
| Stage B | -5.2 | 70.9 | 45.018 | UL-RL | 0.2174.599 | 40 | 40 | 17 | 0 | 0 | 62.018 |
| Stage B | -5.3 | 72.35 | 45.739 | UL-RL | 0.2174.599 | 40 | 40 | 18 | 0 | 0 | 63.739 |
| Stage B | -5.4 | 73.8 | 46.466 | UL-RL | 0.2174.599 | 40 | 40 | 19 | 0 | 0 | 65.466 |
| Stage B | -5.5 | 75.25 | 47.199 | UL-RL | 0.2174.599 | 40 | 40 | 20 | 0 | 0 | 67.199 |
| Stage B | -5.6 | 76.7 | 47.935 | UL-RL | 0.2174.599 | 40 | 40 | 21 | 0 | 0 | 68.935 |
| Stage B | -5.7 | 78.15 | 48.674 | UL-RL | 0.2174.599 | 40 | 40 | 22 | 0 | 0 | 70.674 |
| Stage B | -5.8 | 79.6 | 49.416 | UL-RL | 0.2174.599 | 40 | 40 | 23 | 0 | 0 | 72.416 |
| Stage B | -5.9 | 81.05 | 50.16 | UL-RL | 0.2174.599 | 40 | 40 | 24 | 0 | 0 | 74.16 |
| Stage B | -6 | 82.5 | 50.904 | UL-RL | 0.2174.599 | 40 | 40 | 25 | 0 | 0 | 75.904 |
| Stage B | -6.1 | 83.95 | 51.649 | UL-RL | 0.2174.599 | 40 | 40 | 26 | 0 | 0 | 77.649 |
| Stage B | -6.2 | 85.4 | 52.394 | UL-RL | 0.2174.599 | 40 | 40 | 27 | 0 | 0 | 79.394 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------|-------|------------|----|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Muro: | | LEFT | Lato | | RIGHT | | | | |
| | | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage B | -6.3 | 86.85 | 53.139 | UL-RL | 0.2174.599 | | 40 | 28 | 0 | 0 | 81.139 |
| Stage B | -6.4 | 88.3 | 53.884 | UL-RL | 0.2174.599 | | 40 | 29 | 0 | 0 | 82.883 |
| Stage B | -6.5 | 89.75 | 54.627 | UL-RL | 0.2174.599 | | 40 | 30 | 0 | 0 | 84.627 |
| Stage B | -6.6 | 91.2 | 55.371 | UL-RL | 0.2174.599 | | 40 | 31 | 0 | 0 | 86.371 |
| Stage B | -6.7 | 92.65 | 56.113 | UL-RL | 0.2174.599 | | 40 | 32 | 0 | 0 | 88.113 |
| Stage B | -6.8 | 94.1 | 56.855 | UL-RL | 0.2174.599 | | 40 | 33 | 0 | 0 | 89.854 |
| Stage B | -6.9 | 95.55 | 57.595 | UL-RL | 0.2174.599 | | 40 | 34 | 0 | 0 | 91.595 |
| Stage B | -7 | 97 | 58.335 | UL-RL | 0.2174.599 | | 40 | 35 | 0 | 0 | 93.335 |
| Stage B | -7.1 | 98.45 | 59.074 | UL-RL | 0.2174.599 | | 40 | 36 | 0 | 0 | 95.074 |
| Stage B | -7.2 | 99.9 | 59.813 | UL-RL | 0.2174.599 | | 40 | 37 | 0 | 0 | 96.812 |
| Stage B | -7.3 | 101.35 | 60.55 | UL-RL | 0.2174.599 | | 40 | 38 | 0 | 0 | 98.55 |
| Stage B | -7.4 | 102.8 | 61.287 | UL-RL | 0.2174.599 | | 40 | 39 | 0 | 0 | 100.287 |
| Stage B | -7.5 | 104.25 | 62.024 | UL-RL | 0.2174.599 | | 40 | 40 | 0 | 0 | 102.024 |
| Stage B | -7.6 | 105.7 | 62.76 | UL-RL | 0.2174.599 | | 40 | 41 | 0 | 0 | 103.76 |
| Stage B | -7.7 | 107.15 | 63.495 | UL-RL | 0.2174.599 | | 40 | 42 | 0 | 0 | 105.495 |
| Stage B | -7.8 | 108.6 | 64.23 | UL-RL | 0.2174.599 | | 40 | 43 | 0 | 0 | 107.23 |
| Stage B | -7.9 | 110.05 | 64.965 | UL-RL | 0.2174.599 | | 40 | 44 | 0 | 0 | 108.965 |
| Stage B | -8 | 111.5 | 65.699 | UL-RL | 0.2174.599 | | 40 | 45 | 0 | 0 | 110.699 |
| Stage B | -8.1 | 112.95 | 66.433 | UL-RL | 0.2174.599 | | 40 | 46 | 0 | 0 | 112.433 |
| Stage B | -8.2 | 114.4 | 67.167 | UL-RL | 0.2174.599 | | 40 | 47 | 0 | 0 | 114.167 |
| Stage B | -8.3 | 115.85 | 67.901 | UL-RL | 0.2174.599 | | 40 | 48 | 0 | 0 | 115.901 |
| Stage B | -8.4 | 117.3 | 68.634 | UL-RL | 0.2174.599 | | 40 | 49 | 0 | 0 | 117.634 |
| Stage B | -8.5 | 118.75 | 69.367 | UL-RL | 0.2174.599 | | 40 | 50 | 0 | 0 | 119.367 |
| Stage B | -8.6 | 120.2 | 70.099 | UL-RL | 0.2174.599 | | 40 | 51 | 0 | 0 | 121.099 |
| Stage B | -8.7 | 121.65 | 70.832 | UL-RL | 0.2174.599 | | 40 | 52 | 0 | 0 | 122.832 |
| Stage B | -8.8 | 123.1 | 71.563 | UL-RL | 0.2174.599 | | 40 | 53 | 0 | 0 | 124.563 |
| Stage B | -8.9 | 124.55 | 72.295 | UL-RL | 0.2174.599 | | 40 | 54 | 0 | 0 | 126.295 |
| Stage B | -9 | 126 | 73.026 | UL-RL | 0.2174.599 | | 40 | 55 | 0 | 0 | 128.026 |
| Stage B | -9.1 | 127.45 | 73.756 | UL-RL | 0.2174.599 | | 40 | 56 | 0 | 0 | 129.756 |
| Stage B | -9.2 | 128.9 | 74.486 | UL-RL | 0.2174.599 | | 40 | 57 | 0 | 0 | 131.486 |
| Stage B | -9.3 | 130.35 | 75.215 | UL-RL | 0.2174.599 | | 40 | 58 | 0 | 0 | 133.215 |
| Stage B | -9.4 | 131.8 | 75.944 | UL-RL | 0.2174.599 | | 40 | 59 | 0 | 0 | 134.944 |
| Stage B | -9.5 | 133.25 | 76.673 | UL-RL | 0.2174.599 | | 40 | 60 | 0 | 0 | 136.673 |
| Stage B | -9.6 | 134.7 | 77.401 | UL-RL | 0.2174.599 | | 40 | 61 | 0 | 0 | 138.401 |
| Stage B | -9.7 | 136.15 | 78.128 | UL-RL | 0.2174.599 | | 40 | 62 | 0 | 0 | 140.128 |
| Stage B | -9.8 | 137.6 | 78.856 | UL-RL | 0.2174.599 | | 40 | 63 | 0 | 0 | 141.856 |
| Stage B | -9.9 | 139.05 | 79.583 | UL-RL | 0.2174.599 | | 40 | 64 | 0 | 0 | 143.583 |
| Stage B | -10 | 140.5 | 80.31 | UL-RL | 0.2174.599 | | 40 | 65 | 0 | 0 | 145.31 |

Tabella Risultati Terreno Left Wall - Nominal - Stage 3-

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------|---------|------------|------|----------------|------------|--------------------|-----------|
| Stage | Z (m) | Muro: | | LEFT | | Lato | | LEFT | | |
| | | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage 3- | 0 | 0 | 0 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.1 | 1.9 | 5.891 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 5.891 |
| Stage 3- | -0.2 | 3.803 | 11.788 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 11.788 |
| Stage 3- | -0.3 | 5.709 | 17.698 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 17.698 |
| Stage 3- | -0.4 | 7.621 | 23.626 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 23.626 |
| Stage 3- | -0.5 | 9.541 | 29.576 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 29.576 |
| Stage 3- | -0.6 | 11.469 | 35.552 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 35.552 |
| Stage 3- | -0.7 | 13.406 | 41.558 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 41.558 |
| Stage 3- | -0.8 | 15.353 | 47.595 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 47.595 |
| Stage 3- | -0.9 | 17.311 | 53.663 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 53.663 |
| Stage 3- | -1 | 19.278 | 53.191 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 53.191 |
| Stage 3- | -1.1 | 21.256 | 51.913 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 51.913 |
| Stage 3- | -1.2 | 23.242 | 50.371 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 50.371 |
| Stage 3- | -1.3 | 25.237 | 48.491 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 48.491 |
| Stage 3- | -1.4 | 27.24 | 46.222 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 46.222 |
| Stage 3- | -1.5 | 29.25 | 43.643 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 43.643 |
| Stage 3- | -1.6 | 31.265 | 40.858 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 40.858 |
| Stage 3- | -1.7 | 33.286 | 37.924 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 37.924 |
| Stage 3- | -1.8 | 35.31 | 34.726 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 34.726 |
| Stage 3- | -1.9 | 37.337 | 31.584 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 31.584 |
| Stage 3- | -2 | 39.367 | 51.963 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 51.963 |
| Stage 3- | -2.1 | 41.948 | 40.324 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 40.324 |
| Stage 3- | -2.2 | 44.529 | 29.447 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 29.447 |
| Stage 3- | -2.3 | 47.111 | 19.423 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 19.423 |
| Stage 3- | -2.4 | 49.692 | 13.753 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 13.753 |
| Stage 3- | -2.5 | 52.272 | 9.111 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 9.111 |
| Stage 3- | -2.6 | 54.85 | 4.832 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 4.832 |
| Stage 3- | -2.7 | 57.427 | 0.849 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0.849 |
| Stage 3- | -2.8 | 60.001 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -2.9 | 62.573 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3 | 65.143 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.1 | 67.9 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.2 | 70.524 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.3 | 73.141 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.4 | 75.96 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.5 | 78.558 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.6 | 80.508 | 0 | ACTIVE | 0.2174.599 | | 40 | 0.839 | 0.161 | 0.839 |
| Stage 3- | -3.7 | 82.25 | 0 | ACTIVE | 0.2174.599 | | 40 | 1.679 | 0.161 | 1.679 |
| Stage 3- | -3.8 | 83.988 | 0 | ACTIVE | 0.2174.599 | | 40 | 2.518 | 0.161 | 2.518 |
| Stage 3- | -3.9 | 85.903 | 0 | ACTIVE | 0.2174.599 | | 40 | 3.357 | 0.161 | 3.357 |
| Stage 3- | -4 | 87.627 | 0 | ACTIVE | 0.2174.599 | | 40 | 4.196 | 0.161 | 4.196 |
| Stage 3- | -4.1 | 89.346 | 0 | ACTIVE | 0.2174.599 | | 40 | 5.036 | 0.161 | 5.036 |
| Stage 3- | -4.2 | 91.233 | 0 | ACTIVE | 0.2174.599 | | 40 | 5.875 | 0.161 | 5.875 |
| Stage 3- | -4.3 | 92.941 | 0 | ACTIVE | 0.2174.599 | | 40 | 6.714 | 0.161 | 6.714 |
| Stage 3- | -4.4 | 94.809 | 0 | ACTIVE | 0.2174.599 | | 40 | 7.554 | 0.161 | 7.554 |
| Stage 3- | -4.5 | 96.508 | 0 | ACTIVE | 0.2174.599 | | 40 | 8.393 | 0.161 | 8.393 |
| Stage 3- | -4.6 | 98.204 | 0 | ACTIVE | 0.2174.599 | | 40 | 9.232 | 0.161 | 9.232 |
| Stage 3- | -4.7 | 100.05 | 0 | ACTIVE | 0.2174.599 | | 40 | 10.071 | 0.161 | 10.071 |
| Stage 3- | -4.8 | 101.738 | 0 | ACTIVE | 0.2174.599 | | 40 | 10.911 | 0.161 | 10.911 |
| Stage 3- | -4.9 | 103.569 | 0 | ACTIVE | 0.2174.599 | | 40 | 11.75 | 0.161 | 11.75 |
| Stage 3- | -5 | 105.25 | 0 | ACTIVE | 0.2174.599 | | 40 | 12.589 | 0.161 | 12.589 |
| Stage 3- | -5.1 | 106.928 | 0 | ACTIVE | 0.2174.599 | | 40 | 13.429 | 0.161 | 13.429 |
| Stage 3- | -5.2 | 108.743 | 0 | ACTIVE | 0.2174.599 | | 40 | 14.268 | 0.161 | 14.268 |
| Stage 3- | -5.3 | 110.415 | 0 | ACTIVE | 0.2174.599 | | 40 | 15.107 | 0.161 | 15.107 |
| Stage 3- | -5.4 | 112.218 | 0 | ACTIVE | 0.2174.599 | | 40 | 15.946 | 0.161 | 15.946 |
| Stage 3- | -5.5 | 113.885 | 0.532 | UL-RL | 0.2174.599 | | 40 | 16.786 | 0.161 | 17.318 |
| Stage 3- | -5.6 | 115.55 | 3.283 | UL-RL | 0.2174.599 | | 40 | 17.625 | 0.161 | 20.908 |
| Stage 3- | -5.7 | 117.34 | 6.059 | UL-RL | 0.2174.599 | | 40 | 18.464 | 0.161 | 24.523 |
| Stage 3- | -5.8 | 119 | 8.707 | UL-RL | 0.2174.599 | | 40 | 19.304 | 0.161 | 28.01 |
| Stage 3- | -5.9 | 120.66 | 11.273 | UL-RL | 0.2174.599 | | 40 | 20.143 | 0.161 | 31.416 |
| Stage 3- | -6 | 122.437 | 13.804 | UL-RL | 0.2174.599 | | 40 | 20.982 | 0.161 | 34.786 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 3- | -6.1 | 124.092 | 16.169 | UL-RL | 0.2174.599 | | 40 | 21.821 | 0.161 | 0 | 37.991 |
| Stage 3- | -6.2 | 125.862 | 18.482 | UL-RL | 0.2174.599 | | 40 | 22.661 | 0.161 | 0 | 41.143 |
| Stage 3- | -6.3 | 127.513 | 20.624 | UL-RL | 0.2174.599 | | 40 | 23.5 | 0.161 | 0 | 44.124 |
| Stage 3- | -6.4 | 129.163 | 22.652 | UL-RL | 0.2174.599 | | 40 | 24.339 | 0.161 | 0 | 46.992 |
| Stage 3- | -6.5 | 130.923 | 24.626 | UL-RL | 0.2174.599 | | 40 | 25.179 | 0.161 | 0 | 49.804 |
| Stage 3- | -6.6 | 132.569 | 26.436 | UL-RL | 0.2174.599 | | 40 | 26.018 | 0.161 | 0 | 52.454 |
| Stage 3- | -6.7 | 134.322 | 28.199 | UL-RL | 0.2174.599 | | 40 | 26.857 | 0.161 | 0 | 55.056 |
| Stage 3- | -6.8 | 135.966 | 29.813 | UL-RL | 0.2174.599 | | 40 | 27.696 | 0.161 | 0 | 57.509 |
| Stage 3- | -6.9 | 137.609 | 31.338 | UL-RL | 0.2174.599 | | 40 | 28.536 | 0.161 | 0 | 59.873 |
| Stage 3- | -7 | 139.354 | 32.832 | UL-RL | 0.2174.599 | | 40 | 29.375 | 0.161 | 0 | 62.207 |
| Stage 3- | -7.1 | 140.994 | 34.201 | UL-RL | 0.2174.599 | | 40 | 30.214 | 0.161 | 0 | 64.416 |
| Stage 3- | -7.2 | 142.733 | 35.554 | UL-RL | 0.2174.599 | | 40 | 31.054 | 0.161 | 0 | 66.607 |
| Stage 3- | -7.3 | 144.371 | 36.796 | UL-RL | 0.2174.599 | | 40 | 31.893 | 0.161 | 0 | 68.689 |
| Stage 3- | -7.4 | 146.008 | 37.987 | UL-RL | 0.2174.599 | | 40 | 32.732 | 0.161 | 0 | 70.719 |
| Stage 3- | -7.5 | 147.741 | 39.179 | UL-RL | 0.2174.599 | | 40 | 33.571 | 0.161 | 0 | 72.75 |
| Stage 3- | -7.6 | 149.376 | 40.283 | UL-RL | 0.2174.599 | | 40 | 34.411 | 0.161 | 0 | 74.694 |
| Stage 3- | -7.7 | 151.01 | 41.354 | UL-RL | 0.2174.599 | | 40 | 35.25 | 0.161 | 0 | 76.604 |
| Stage 3- | -7.8 | 152.736 | 42.442 | UL-RL | 0.2174.599 | | 40 | 36.089 | 0.161 | 0 | 78.531 |
| Stage 3- | -7.9 | 154.369 | 43.46 | UL-RL | 0.2174.599 | | 40 | 36.929 | 0.161 | 0 | 80.388 |
| Stage 3- | -8 | 156.091 | 44.503 | UL-RL | 0.2174.599 | | 40 | 37.768 | 0.161 | 0 | 82.27 |
| Stage 3- | -8.1 | 157.722 | 45.485 | UL-RL | 0.2174.599 | | 40 | 38.607 | 0.161 | 0 | 84.092 |
| Stage 3- | -8.2 | 159.352 | 46.455 | UL-RL | 0.2174.599 | | 40 | 39.446 | 0.161 | 0 | 85.901 |
| Stage 3- | -8.3 | 161.068 | 47.459 | UL-RL | 0.2174.599 | | 40 | 40.286 | 0.161 | 0 | 87.744 |
| Stage 3- | -8.4 | 162.697 | 48.412 | UL-RL | 0.2174.599 | | 40 | 41.125 | 0.161 | 0 | 89.537 |
| Stage 3- | -8.5 | 164.41 | 49.403 | UL-RL | 0.2174.599 | | 40 | 41.964 | 0.161 | 0 | 91.367 |
| Stage 3- | -8.6 | 166.037 | 50.348 | UL-RL | 0.2174.599 | | 40 | 42.804 | 0.161 | 0 | 93.152 |
| Stage 3- | -8.7 | 167.664 | 51.293 | UL-RL | 0.2174.599 | | 40 | 43.643 | 0.161 | 0 | 94.935 |
| Stage 3- | -8.8 | 169.372 | 52.277 | UL-RL | 0.2174.599 | | 40 | 44.482 | 0.161 | 0 | 96.759 |
| Stage 3- | -8.9 | 170.997 | 53.222 | UL-RL | 0.2174.599 | | 40 | 45.321 | 0.161 | 0 | 98.543 |
| Stage 3- | -9 | 172.702 | 54.207 | UL-RL | 0.2174.599 | | 40 | 46.161 | 0.161 | 0 | 100.368 |
| Stage 3- | -9.1 | 174.326 | 55.154 | UL-RL | 0.2174.599 | | 40 | 47 | 0.161 | 0 | 102.154 |
| Stage 3- | -9.2 | 175.95 | 56.104 | UL-RL | 0.2174.599 | | 40 | 47.839 | 0.161 | 0 | 103.943 |
| Stage 3- | -9.3 | 177.651 | 57.095 | UL-RL | 0.2174.599 | | 40 | 48.679 | 0.161 | 0 | 105.773 |
| Stage 3- | -9.4 | 179.274 | 58.049 | UL-RL | 0.2174.599 | | 40 | 49.518 | 0.161 | 0 | 107.567 |
| Stage 3- | -9.5 | 180.897 | 59.005 | UL-RL | 0.2174.599 | | 40 | 50.357 | 0.161 | 0 | 109.362 |
| Stage 3- | -9.6 | 182.444 | 59.926 | UL-RL | 0.2174.599 | | 40 | 51.196 | 0.161 | 0 | 111.122 |
| Stage 3- | -9.7 | 183.992 | 60.848 | UL-RL | 0.2174.599 | | 40 | 52.036 | 0.161 | 0 | 112.884 |
| Stage 3- | -9.8 | 185.541 | 61.772 | UL-RL | 0.2174.599 | | 40 | 52.875 | 0.161 | 0 | 114.647 |
| Stage 3- | -9.9 | 187.091 | 62.697 | UL-RL | 0.2174.599 | | 40 | 53.714 | 0.161 | 0 | 116.411 |
| Stage 3- | -10 | 188.641 | 63.622 | UL-RL | 0.2174.599 | | 40 | 54.554 | 0.161 | 0 | 118.176 |

| Design Assumption: Nominal Risultati Terreno | | Muro: | | LEFT | Lato | | RIGHT | | | | |
|--|-------|---------------|---------------|---------|------------|----|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 3- | 0 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5.4 | 1.289 | 32.074 | UL-RL | 0.2174.599 | | 40 | 1.161 | 0.161 | 0 | 33.235 |
| Stage 3- | -5.5 | 2.579 | 33.611 | UL-RL | 0.2174.599 | | 40 | 2.321 | 0.161 | 0 | 35.933 |
| Stage 3- | -5.6 | 3.868 | 34.624 | UL-RL | 0.2174.599 | | 40 | 3.482 | 0.161 | 0 | 38.106 |
| Stage 3- | -5.7 | 5.157 | 35.387 | UL-RL | 0.2174.599 | | 40 | 4.643 | 0.161 | 0 | 40.03 |
| Stage 3- | -5.8 | 6.446 | 36.012 | UL-RL | 0.2174.599 | | 40 | 5.804 | 0.161 | 0 | 41.816 |
| Stage 3- | -5.9 | 7.736 | 36.558 | UL-RL | 0.2174.599 | | 40 | 6.964 | 0.161 | 0 | 43.522 |
| Stage 3- | -6 | 9.025 | 37.061 | UL-RL | 0.2174.599 | | 40 | 8.125 | 0.161 | 0 | 45.186 |
| Stage 3- | -6.1 | 10.314 | 37.545 | UL-RL | 0.2174.599 | | 40 | 9.286 | 0.161 | 0 | 46.831 |
| Stage 3- | -6.2 | 11.604 | 38.027 | UL-RL | 0.2174.599 | | 40 | 10.446 | 0.161 | 0 | 48.473 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------|-------|------------|----|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Muro: | | LEFT | Lato | | RIGHT | | | | |
| | | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 3- | -6.3 | 12.893 | 38.516 | UL-RL | 0.2174.599 | | 40 | 11.607 | 0.161 | 0 | 50.124 |
| Stage 3- | -6.4 | 14.182 | 39.021 | UL-RL | 0.2174.599 | | 40 | 12.768 | 0.161 | 0 | 51.789 |
| Stage 3- | -6.5 | 15.471 | 39.545 | UL-RL | 0.2174.599 | | 40 | 13.929 | 0.161 | 0 | 53.474 |
| Stage 3- | -6.6 | 16.761 | 40.092 | UL-RL | 0.2174.599 | | 40 | 15.089 | 0.161 | 0 | 55.181 |
| Stage 3- | -6.7 | 18.05 | 40.662 | UL-RL | 0.2174.599 | | 40 | 16.25 | 0.161 | 0 | 56.911 |
| Stage 3- | -6.8 | 19.339 | 41.255 | UL-RL | 0.2174.599 | | 40 | 17.411 | 0.161 | 0 | 58.665 |
| Stage 3- | -6.9 | 20.629 | 41.87 | UL-RL | 0.2174.599 | | 40 | 18.571 | 0.161 | 0 | 60.442 |
| Stage 3- | -7 | 21.918 | 42.507 | UL-RL | 0.2174.599 | | 40 | 19.732 | 0.161 | 0 | 62.239 |
| Stage 3- | -7.1 | 23.207 | 43.164 | UL-RL | 0.2174.599 | | 40 | 20.893 | 0.161 | 0 | 64.057 |
| Stage 3- | -7.2 | 24.496 | 43.838 | UL-RL | 0.2174.599 | | 40 | 22.054 | 0.161 | 0 | 65.891 |
| Stage 3- | -7.3 | 25.786 | 44.527 | UL-RL | 0.2174.599 | | 40 | 23.214 | 0.161 | 0 | 67.742 |
| Stage 3- | -7.4 | 27.075 | 45.23 | UL-RL | 0.2174.599 | | 40 | 24.375 | 0.161 | 0 | 69.605 |
| Stage 3- | -7.5 | 28.364 | 45.944 | UL-RL | 0.2174.599 | | 40 | 25.536 | 0.161 | 0 | 71.48 |
| Stage 3- | -7.6 | 29.654 | 46.667 | UL-RL | 0.2174.599 | | 40 | 26.696 | 0.161 | 0 | 73.363 |
| Stage 3- | -7.7 | 30.943 | 47.397 | UL-RL | 0.2174.599 | | 40 | 27.857 | 0.161 | 0 | 75.254 |
| Stage 3- | -7.8 | 32.232 | 48.133 | UL-RL | 0.2174.599 | | 40 | 29.018 | 0.161 | 0 | 77.151 |
| Stage 3- | -7.9 | 33.521 | 48.873 | UL-RL | 0.2174.599 | | 40 | 30.178 | 0.161 | 0 | 79.051 |
| Stage 3- | -8 | 34.811 | 49.614 | UL-RL | 0.2174.599 | | 40 | 31.339 | 0.161 | 0 | 80.954 |
| Stage 3- | -8.1 | 36.1 | 50.357 | UL-RL | 0.2174.599 | | 40 | 32.5 | 0.161 | 0 | 82.857 |
| Stage 3- | -8.2 | 37.389 | 51.1 | UL-RL | 0.2174.599 | | 40 | 33.661 | 0.161 | 0 | 84.761 |
| Stage 3- | -8.3 | 38.679 | 51.842 | UL-RL | 0.2174.599 | | 40 | 34.821 | 0.161 | 0 | 86.663 |
| Stage 3- | -8.4 | 39.968 | 52.582 | UL-RL | 0.2174.599 | | 40 | 35.982 | 0.161 | 0 | 88.564 |
| Stage 3- | -8.5 | 41.257 | 53.319 | UL-RL | 0.2174.599 | | 40 | 37.143 | 0.161 | 0 | 90.462 |
| Stage 3- | -8.6 | 42.546 | 54.053 | UL-RL | 0.2174.599 | | 40 | 38.304 | 0.161 | 0 | 92.357 |
| Stage 3- | -8.7 | 43.836 | 54.784 | UL-RL | 0.2174.599 | | 40 | 39.464 | 0.161 | 0 | 94.248 |
| Stage 3- | -8.8 | 45.125 | 55.511 | UL-RL | 0.2174.599 | | 40 | 40.625 | 0.161 | 0 | 96.136 |
| Stage 3- | -8.9 | 46.414 | 56.234 | UL-RL | 0.2174.599 | | 40 | 41.786 | 0.161 | 0 | 98.02 |
| Stage 3- | -9 | 47.704 | 56.954 | UL-RL | 0.2174.599 | | 40 | 42.946 | 0.161 | 0 | 99.9 |
| Stage 3- | -9.1 | 48.993 | 57.669 | UL-RL | 0.2174.599 | | 40 | 44.107 | 0.161 | 0 | 101.776 |
| Stage 3- | -9.2 | 50.282 | 58.38 | UL-RL | 0.2174.599 | | 40 | 45.268 | 0.161 | 0 | 103.648 |
| Stage 3- | -9.3 | 51.571 | 59.088 | UL-RL | 0.2174.599 | | 40 | 46.429 | 0.161 | 0 | 105.516 |
| Stage 3- | -9.4 | 52.861 | 59.791 | UL-RL | 0.2174.599 | | 40 | 47.589 | 0.161 | 0 | 107.381 |
| Stage 3- | -9.5 | 54.15 | 60.492 | UL-RL | 0.2174.599 | | 40 | 48.75 | 0.161 | 0 | 109.242 |
| Stage 3- | -9.6 | 55.439 | 61.189 | UL-RL | 0.2174.599 | | 40 | 49.911 | 0.161 | 0 | 111.1 |
| Stage 3- | -9.7 | 56.729 | 61.883 | UL-RL | 0.2174.599 | | 40 | 51.071 | 0.161 | 0 | 112.954 |
| Stage 3- | -9.8 | 58.018 | 62.575 | UL-RL | 0.2174.599 | | 40 | 52.232 | 0.161 | 0 | 114.807 |
| Stage 3- | -9.9 | 59.307 | 63.264 | UL-RL | 0.2174.599 | | 40 | 53.393 | 0.161 | 0 | 116.656 |
| Stage 3- | -10 | 60.596 | 63.951 | UL-RL | 0.2174.599 | | 40 | 54.554 | 0.161 | 0 | 118.504 |

Grafico Risultati Terreno Sigma V

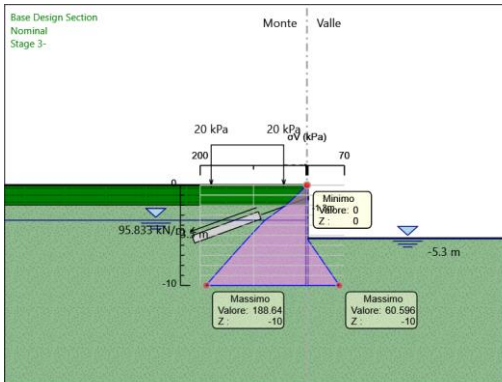
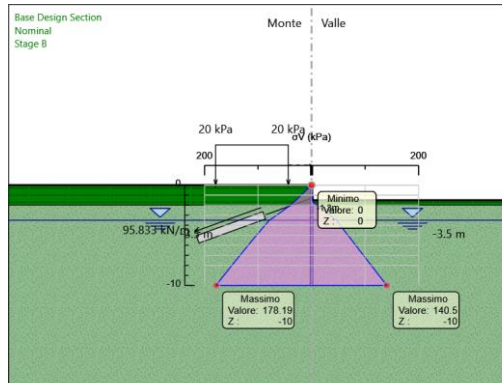
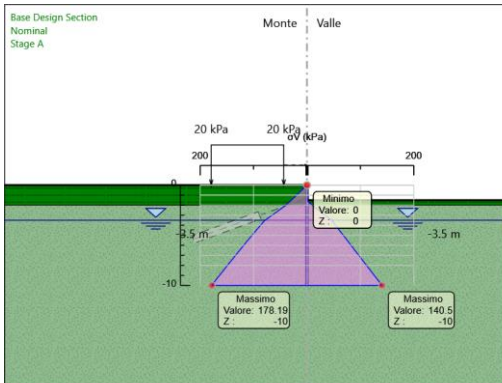
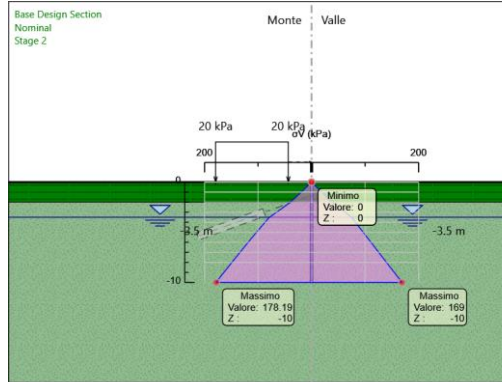
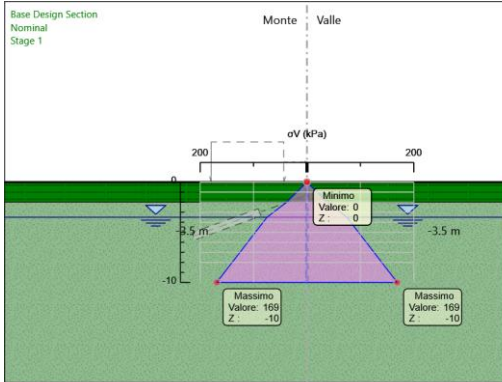


Grafico Risultati Terreno Sigma H

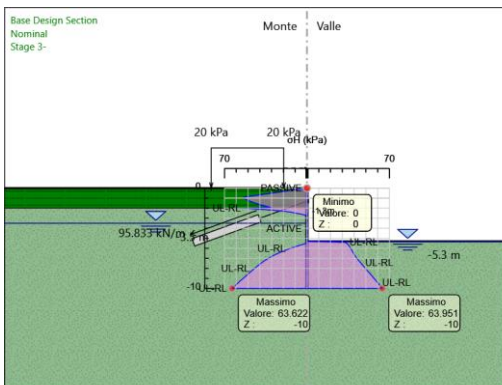
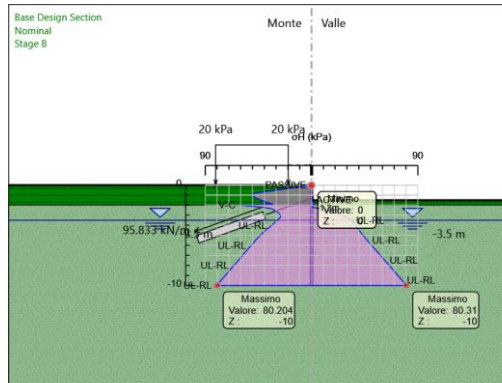
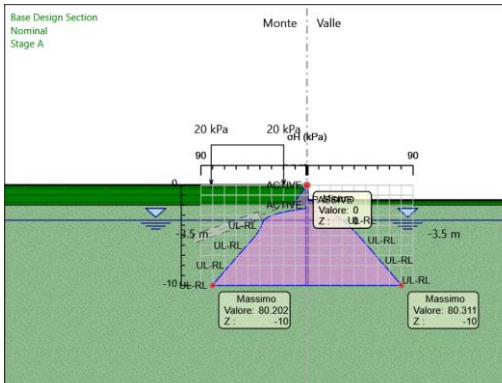
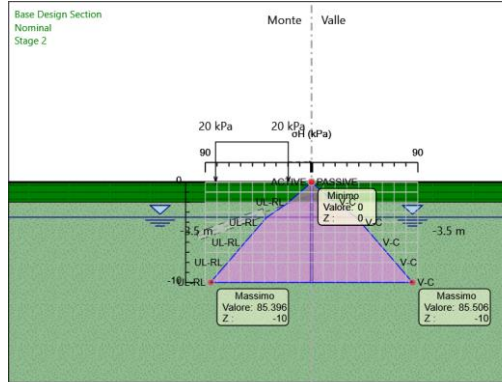
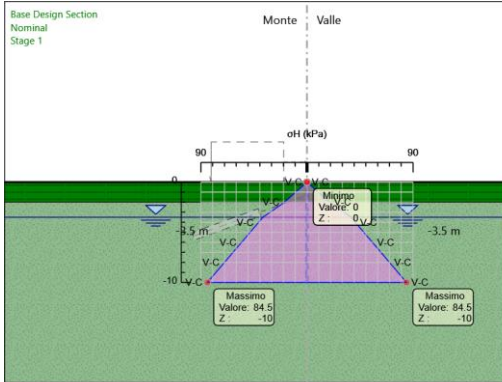
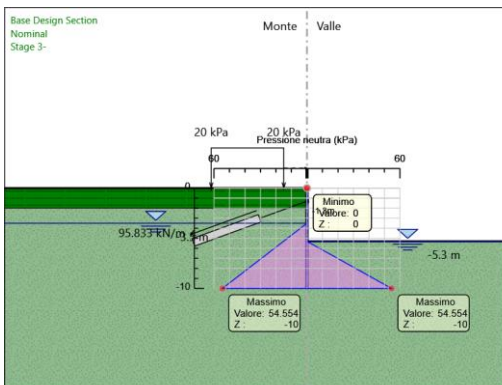
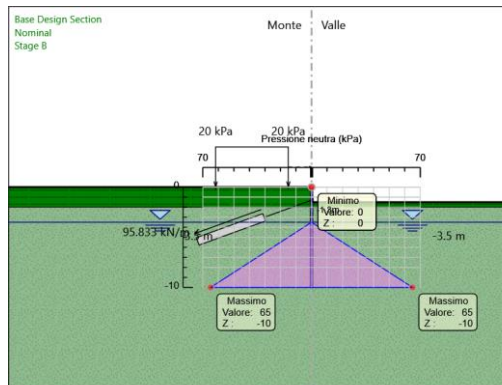
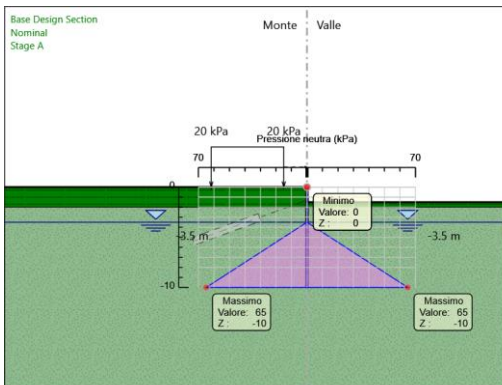
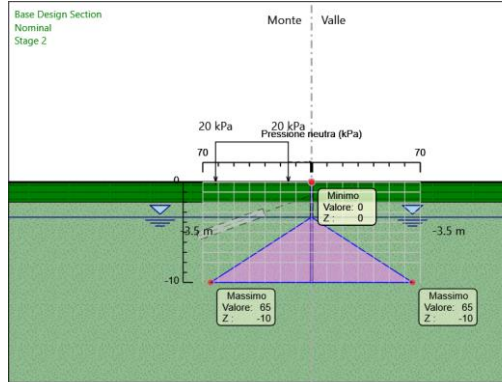
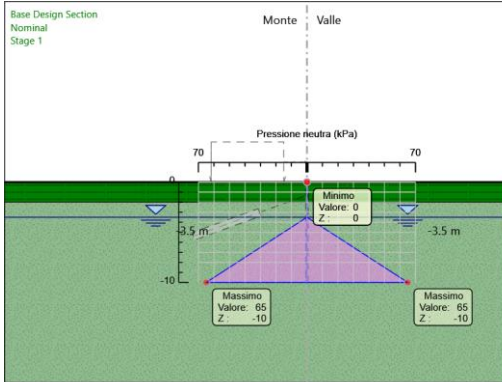


Grafico Risultati Terreno Pore



Riepilogo spinte

| Design Assumption: | Tipo Risultato: | Muro: | LEFT | Lato | LEFT | | |
|--------------------|------------------|------------------|-------------|-----------------|-----------------|-----------------------------------|---------------|
| Nominal | Riepilogo spinte | | | | | | |
| Stage | Vera effettiva | Pressione neutra | Vera Totale | Min ammissibile | Max ammissibile | Percentuale di resistenza massima | Vera / Attiva |
| | (kN/m) | (kN/m) | (kN/m) | (kN/m) | (kN/m) | | |
| Stage 1 | 457.4 | 211.2 | 668.6 | 11.6 | 5533.9 | 8.27% | 39.43 |
| Stage 2 | 463.2 | 211.2 | 674.4 | 12.1 | 5781.2 | 8.01% | 38.28 |
| Stage A | 409.5 | 211.2 | 620.7 | 12.1 | 5781.2 | 7.08% | 33.84 |
| Stage B | 485.4 | 211.2 | 696.6 | 12.1 | 5781.2 | 8.4% | 40.12 |
| Stage 3- | 262.7 | 177.3 | 440 | 13.8 | 5937.3 | 4.42% | 19.04 |

| Design Assumption: | Tipo Risultato: | Muro: | LEFT | Lato | RIGHT | | |
|--------------------|------------------|------------------|-------------|-----------------|-----------------|-----------------------------------|---------------|
| Nominal | Riepilogo spinte | | | | | | |
| Stage | Vera effettiva | Pressione neutra | Vera Totale | Min ammissibile | Max ammissibile | Percentuale di resistenza massima | Vera / Attiva |
| | (kN/m) | (kN/m) | (kN/m) | (kN/m) | (kN/m) | | |
| Stage 1 | 457.4 | 211.2 | 668.6 | 11.6 | 5533.9 | 8.27% | 39.43 |
| Stage 2 | 463.2 | 211.2 | 674.4 | 11.6 | 5533.9 | 8.37% | 39.93 |
| Stage A | 409.5 | 211.2 | 620.7 | 0.6 | 4372.8 | 9.36% | 682.5 |
| Stage B | 395.3 | 211.2 | 606.6 | 0.6 | 4372.8 | 9.04% | 658.83 |
| Stage 3- | 222.1 | 128.2 | 350.3 | 0 | 1452.7 | 15.29% | ∞ |

Descrizione Coefficienti Design Assumption

| Nome | Carichi Permanenti Sfavorevoli (F_dead_load _unfavour) | Carichi Permanenti Favorevoli (F_dead_loa d_favour) | Carichi Variabili Sfavorevoli (F_live_load _unfavour) | Carichi Variabili Favorevoli (F_live_loa d_favour) | Carico Sismico (F_seis m_load) | Pressio ni Acqua Lato Monte (F_Wat erDR) | Pressio ni Acqua Lato Valle (F_Wat erRes) | Carichi Permane nti Destabili zzanti (F_UPL_ GDStab) | Carichi Perman enti Stabilizz anti (F_UPL_ GStab) | Carichi Variabili Destabili zzanti (F_UPL_ QDStab) | Carichi Permane nti Destabili zzanti (F_HYD_ GDStab) | Carichi Perman enti Stabilizz anti (F_HYD_ GStab) | Carichi Variabili Destabili zzanti (F_HYD_ QDStab) |
|---|--|---|---|--|---|--|---|--|---|---|--|---|---|
| Simbolo | γ_G | γ_G | γ_Q | γ_Q | γ_{QE} | γ_G | γ_G | γ_{Gdst} | γ_{Gstb} | γ_{Qdst} | γ_{Gdst} | γ_{Gstb} | γ_{Qdst} |
| Nominal | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| NTC2018: SLE (Rara/Frequ ente/Quasi Permanente) | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| NTC2018: A1+M1+R1 (R3 per tiranti) | 1.3 | 1 | 1.5 | 1 | 0 | 1.3 | 1 | 1 | 1 | 1 | 1.3 | 0.9 | 1 |
| NTC2018: A2+M2+R1 | 1 | 1 | 1.3 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 1.3 | 0.9 | 1 |

| Nome | Parziale su $\tan(\phi')$ (F_Fr) | Parziale su c' (F_eff_cohe) | Parziale su Su (F_Su) | Parziale su qu (F_qu) | Parziale su peso specifico (F_gamma) |
|--|-------------------------------------|----------------------------------|--------------------------|--------------------------|---|
| Simbolo | γ_ϕ | γ_c | γ_{cu} | γ_{qu} | γ_γ |
| Nominal | 1 | 1 | 1 | 1 | 1 |
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | 1 | 1 | 1 | 1 | 1 |
| NTC2018: A1+M1+R1 (R3 per tiranti) | 1 | 1 | 1 | 1 | 1 |
| NTC2018: A2+M2+R1 | 1.25 | 1.25 | 1.4 | 1 | 1 |

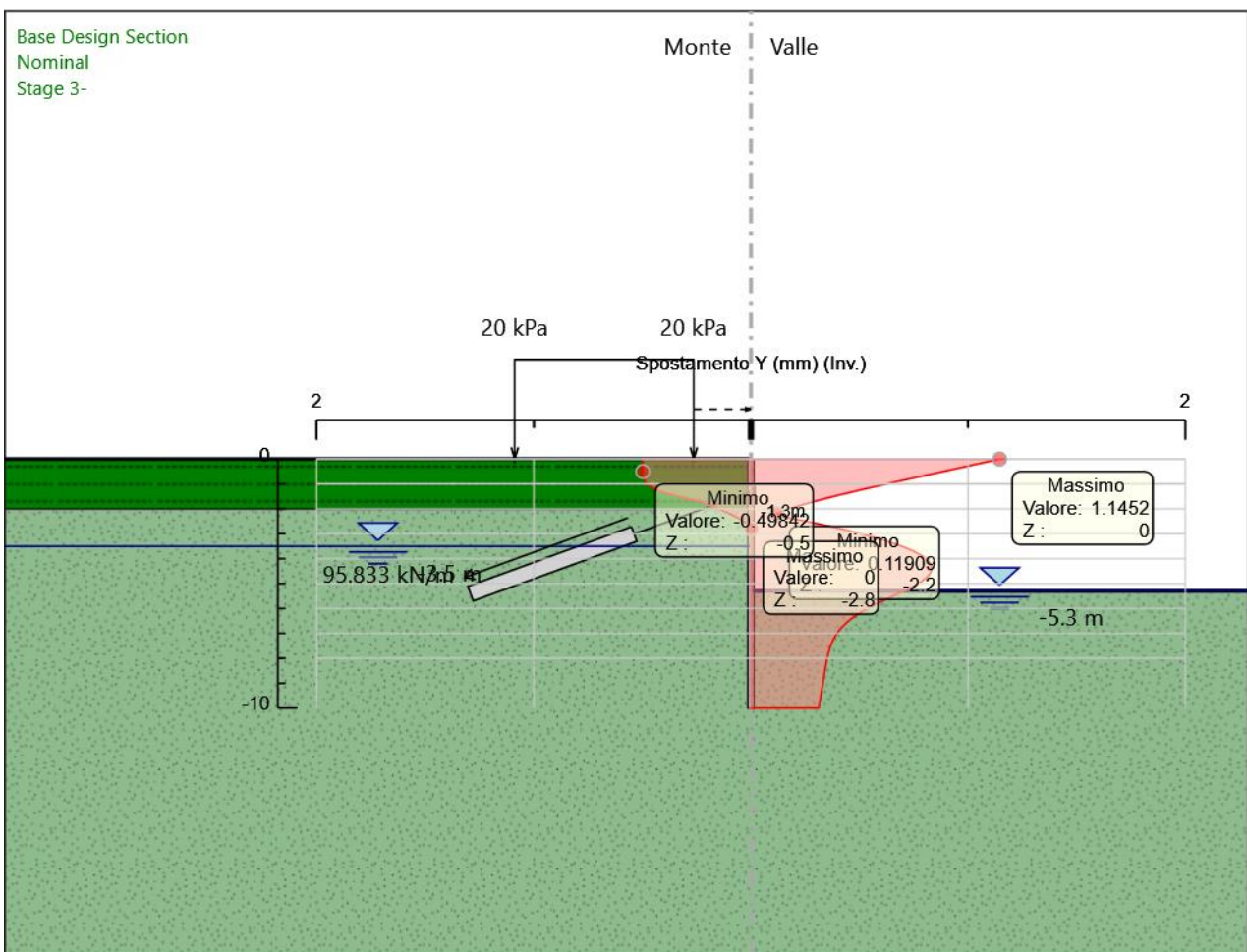
| Nome | Parziale resistenza terreno (es. Kp) (F_Soil_Res_walls) | Parziale resistenza Tiranti permanenti (F_Anch_P) | Parziale resistenza Tiranti temporanei (F_Anch_T) | Parziale elementi strutturali (F_wall) |
|--|--|--|--|---|
| Simbolo | γ_{Re} | γ_p | γ_{at} | |
| Nominal | 1 | 1 | 1 | 1 |
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | 1 | 1 | 1 | 1 |
| NTC2018: A1+M1+R1 (R3 per tiranti) | 1 | 1.2 | 1.1 | 1 |
| NTC2018: A2+M2+R1 | 1 | 1.2 | 1.1 | 1 |

Riepilogo Stage / Design Assumption per Inviluppo

| Design Assumption | Stage 1 | Stage 2 | Stage A | Stage B | Stage 3- |
|--|---------|---------|---------|---------|----------|
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | V | V | V | V | V |
| NTC2018: A1+M1+R1 (R3 per tiranti) | V | V | V | V | V |
| NTC2018: A2+M2+R1 | V | V | V | V | V |

Descrizione sintetica dei risultati delle Design Assumption (Inviluppi)

Grafico Inviluppi Spostamento



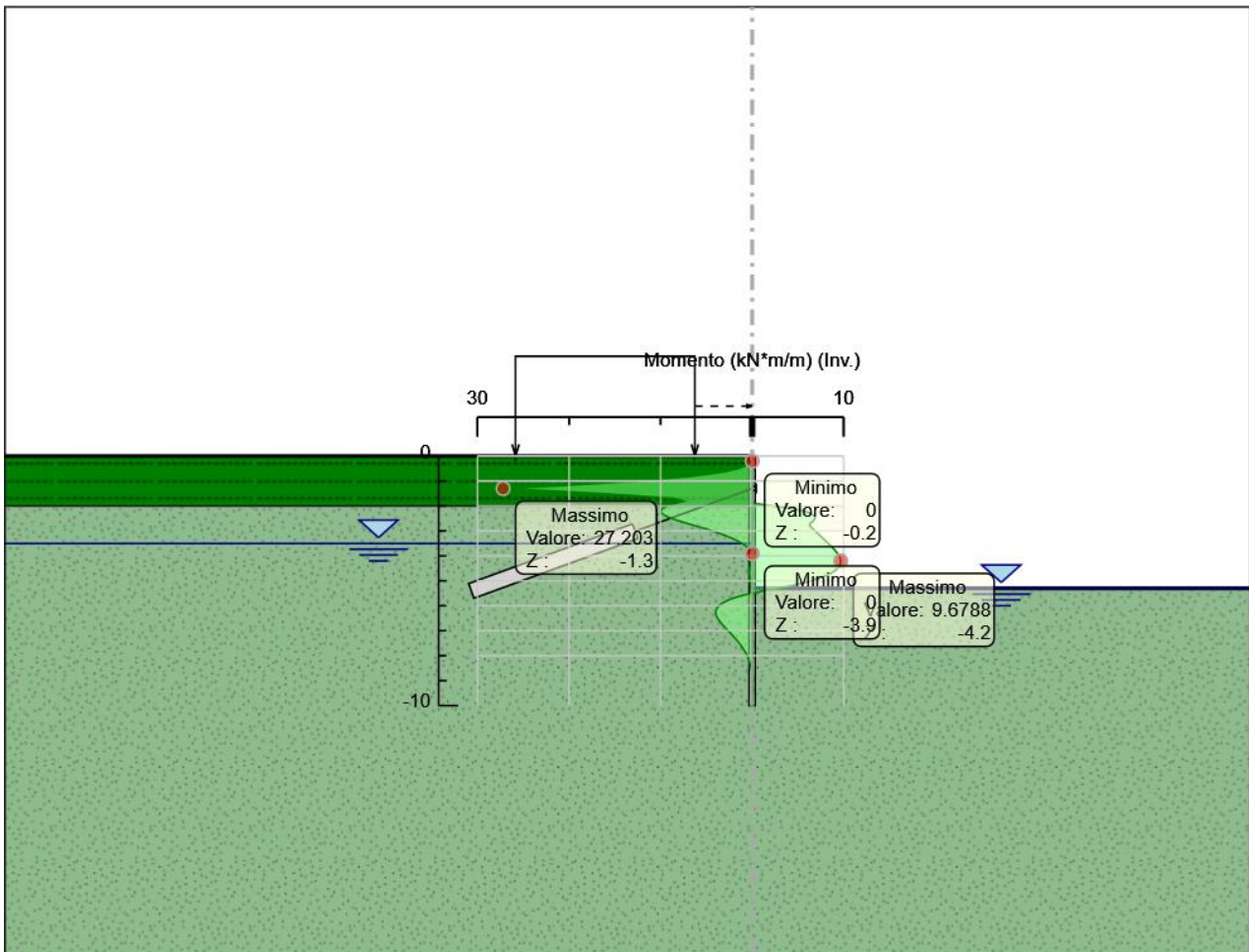
Spostamento

Tabella Inviluppi Momento paratia sx

| Selected Design Assumptions Z (m) | Inviluppi: Momento | | Muro: paratia sx |
|--------------------------------------|------------------------|----------------------|------------------|
| | Lato sinistro (kN*m/m) | Lato destro (kN*m/m) | |
| 0 | 0 | | 0 |
| -0.1 | 0 | | 0 |
| -0.2 | 0.077 | | 0 |
| -0.3 | 0.306 | | 0 |
| -0.4 | 0.766 | | 0 |
| -0.5 | 1.534 | | 0 |
| -0.6 | 2.686 | | 0.001 |
| -0.7 | 4.3 | | 0.003 |
| -0.8 | 6.456 | | 0.006 |
| -0.9 | 9.231 | | 0.009 |
| -1 | 12.705 | | 0.013 |
| -1.1 | 16.87 | | 0.017 |
| -1.2 | 21.709 | | 0.022 |
| -1.3 | 27.203 | | 0.025 |
| -1.4 | 21.661 | | 0.028 |
| -1.5 | 16.72 | | 0.03 |
| -1.6 | 12.345 | | 0.03 |
| -1.7 | 8.503 | | 0.026 |
| -1.8 | 7.468 | | 0.02 |
| -1.9 | 8.395 | | 0.137 |
| -2 | 9.255 | | 2.354 |
| -2.1 | 9.781 | | 4.339 |
| -2.2 | 9.983 | | 5.664 |
| -2.3 | 9.87 | | 6.431 |
| -2.4 | 9.447 | | 6.799 |
| -2.5 | 8.789 | | 6.858 |
| -2.6 | 7.979 | | 6.676 |
| -2.7 | 7.086 | | 6.308 |
| -2.8 | 6.161 | | 6.309 |
| -2.9 | 5.246 | | 6.594 |
| -3 | 4.371 | | 6.878 |
| -3.1 | 3.557 | | 7.162 |
| -3.2 | 2.819 | | 7.447 |
| -3.3 | 2.163 | | 7.731 |
| -3.4 | 1.593 | | 8.015 |
| -3.5 | 1.108 | | 8.3 |
| -3.6 | 0.704 | | 8.584 |
| -3.7 | 0.376 | | 8.857 |
| -3.8 | 0.116 | | 9.109 |
| -3.9 | 0 | | 9.328 |
| -4 | 0 | | 9.503 |
| -4.1 | 0 | | 9.624 |
| -4.2 | 0.094 | | 9.679 |
| -4.3 | 0.178 | | 9.658 |
| -4.4 | 0.234 | | 9.549 |
| -4.5 | 0.268 | | 9.342 |
| -4.6 | 0.283 | | 9.027 |
| -4.7 | 0.283 | | 8.591 |
| -4.8 | 0.272 | | 8.024 |
| -4.9 | 0.254 | | 7.316 |
| -5 | 0.231 | | 6.454 |
| -5.1 | 0.206 | | 5.429 |
| -5.2 | 0.178 | | 4.23 |
| -5.3 | 0.151 | | 2.845 |
| -5.4 | 0.125 | | 1.263 |
| -5.5 | 0.141 | | 0.094 |
| -5.6 | 1.206 | | 0.07 |
| -5.7 | 2.096 | | 0.05 |
| -5.8 | 2.786 | | 0.033 |
| -5.9 | 3.296 | | 0.019 |

| Selected Design Assumptions | Involupi: Momento | Muro: paratia sx |
|-----------------------------|------------------------|----------------------|
| Z (m) | Lato sinistro (kN*m/m) | Lato destro (kN*m/m) |
| -6 | 3.649 | 0.009 |
| -6.1 | 3.867 | 0.008 |
| -6.2 | 3.971 | 0.007 |
| -6.3 | 3.979 | 0.007 |
| -6.4 | 3.909 | 0.011 |
| -6.5 | 3.777 | 0.014 |
| -6.6 | 3.598 | 0.016 |
| -6.7 | 3.383 | 0.017 |
| -6.8 | 3.144 | 0.017 |
| -6.9 | 2.89 | 0.017 |
| -7 | 2.628 | 0.016 |
| -7.1 | 2.367 | 0.015 |
| -7.2 | 2.109 | 0.014 |
| -7.3 | 1.862 | 0.013 |
| -7.4 | 1.626 | 0.011 |
| -7.5 | 1.405 | 0.01 |
| -7.6 | 1.2 | 0.009 |
| -7.7 | 1.013 | 0.008 |
| -7.8 | 0.843 | 0.007 |
| -7.9 | 0.691 | 0.006 |
| -8 | 0.557 | 0.006 |
| -8.1 | 0.439 | 0.006 |
| -8.2 | 0.338 | 0.006 |
| -8.3 | 0.251 | 0.006 |
| -8.4 | 0.178 | 0.007 |
| -8.5 | 0.118 | 0.008 |
| -8.6 | 0.07 | 0.009 |
| -8.7 | 0.033 | 0.01 |
| -8.8 | 0.008 | 0.012 |
| -8.9 | 0 | 0.019 |
| -9 | 0 | 0.033 |
| -9.1 | 0 | 0.041 |
| -9.2 | 0 | 0.044 |
| -9.3 | 0 | 0.044 |
| -9.4 | 0 | 0.039 |
| -9.5 | 0 | 0.033 |
| -9.6 | 0 | 0.024 |
| -9.7 | 0 | 0.016 |
| -9.8 | 0 | 0.008 |
| -9.9 | 0 | 0.002 |
| -10 | 0 | 0 |

Grafico Involuppi Momento



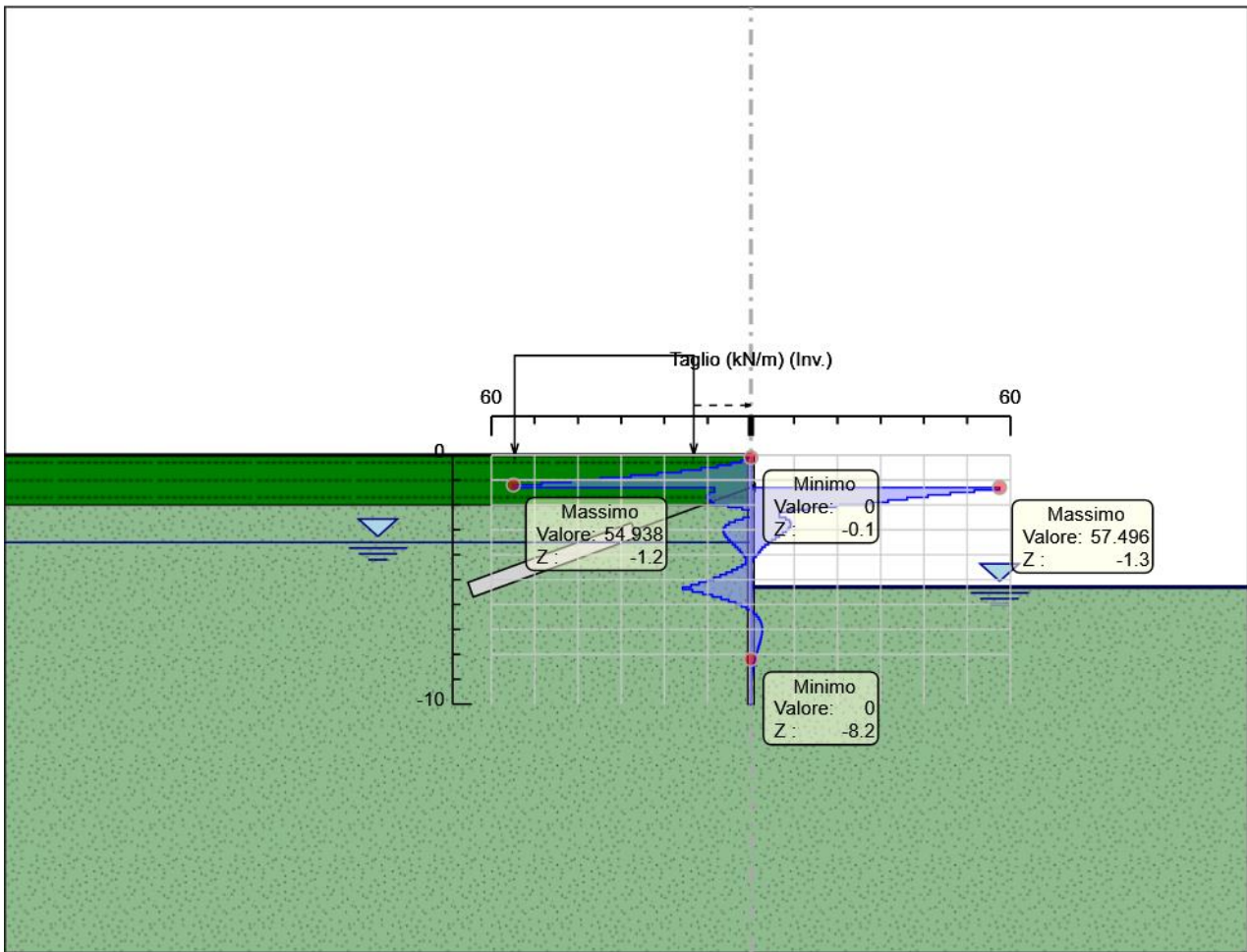
Momento

Tabella Inviluppi Taglio paratia sx

| Selected Design Assumptions Z (m) | Inviluppi: Taglio Muro: paratia sx | |
|--------------------------------------|------------------------------------|--------------------|
| | Lato sinistro (kN/m) | Lato destro (kN/m) |
| 0 | 0 | 0 |
| -0.1 | 0.766 | 0 |
| -0.2 | 2.299 | 0 |
| -0.3 | 4.6 | 0.001 |
| -0.4 | 7.673 | 0.005 |
| -0.5 | 11.52 | 0.012 |
| -0.6 | 16.146 | 0.019 |
| -0.7 | 21.555 | 0.026 |
| -0.8 | 27.752 | 0.033 |
| -0.9 | 34.741 | 0.039 |
| -1 | 41.65 | 0.042 |
| -1.1 | 48.394 | 0.042 |
| -1.2 | 54.938 | 0.042 |
| -1.3 | 54.938 | 57.496 |
| -1.4 | 8.437 | 57.496 |
| -1.5 | 9.658 | 51.658 |
| -1.6 | 10.199 | 46.094 |
| -1.7 | 10.199 | 40.91 |
| -1.8 | 10.058 | 36.119 |
| -1.9 | 9.275 | 31.723 |
| -2 | 8.598 | 27.713 |
| -2.1 | 5.258 | 19.901 |
| -2.2 | 2.024 | 13.25 |
| -2.3 | 0.065 | 9.068 |
| -2.4 | 0.044 | 6.579 |
| -2.5 | 1.824 | 8.095 |
| -2.6 | 3.673 | 8.938 |
| -2.7 | 5.031 | 9.248 |
| -2.8 | 5.887 | 9.248 |
| -2.9 | 6.308 | 9.149 |
| -3 | 6.384 | 8.748 |
| -3.1 | 6.384 | 8.139 |
| -3.2 | 6.213 | 7.384 |
| -3.3 | 5.854 | 6.555 |
| -3.4 | 5.366 | 5.703 |
| -3.5 | 4.814 | 4.85 |
| -3.6 | 4.219 | 4.041 |
| -3.7 | 3.63 | 3.28 |
| -3.8 | 3.054 | 2.595 |
| -3.9 | 2.507 | 2.188 |
| -4 | 2.015 | 1.752 |
| -4.1 | 1.569 | 1.206 |
| -4.2 | 1.174 | 0.647 |
| -4.3 | 1.228 | 0.343 |
| -4.4 | 2.067 | 0.107 |
| -4.5 | 3.158 | 0 |
| -4.6 | 4.358 | 0 |
| -4.7 | 5.667 | 0.103 |
| -4.8 | 7.086 | 0.182 |
| -4.9 | 8.613 | 0.228 |
| -5 | 10.25 | 0.257 |
| -5.1 | 11.995 | 0.273 |
| -5.2 | 13.85 | 0.273 |
| -5.3 | 15.814 | 0.27 |
| -5.4 | 15.814 | 0.261 |
| -5.5 | 13.554 | 0.239 |
| -5.6 | 11.138 | 0.217 |
| -5.7 | 8.906 | 0.195 |
| -5.8 | 6.894 | 0.167 |
| -5.9 | 5.102 | 0.142 |

| Selected Design Assumptions | Involuppi: Taglio | Muro: paratia sx |
|-----------------------------|----------------------|--------------------|
| Z (m) | Lato sinistro (kN/m) | Lato destro (kN/m) |
| -6 | 3.531 | 0.122 |
| -6.1 | 2.181 | 0.099 |
| -6.2 | 1.033 | 0.081 |
| -6.3 | 0.082 | 0.696 |
| -6.4 | 0.027 | 1.319 |
| -6.5 | 0.011 | 1.795 |
| -6.6 | 0.005 | 2.15 |
| -6.7 | 0.004 | 2.39 |
| -6.8 | 0.005 | 2.54 |
| -6.9 | 0.006 | 2.614 |
| -7 | 0.01 | 2.618 |
| -7.1 | 0.011 | 2.618 |
| -7.2 | 0.015 | 2.572 |
| -7.3 | 0.016 | 2.478 |
| -7.4 | 0.016 | 2.355 |
| -7.5 | 0.014 | 2.211 |
| -7.6 | 0.014 | 2.046 |
| -7.7 | 0.012 | 1.873 |
| -7.8 | 0.007 | 1.699 |
| -7.9 | 0.006 | 1.52 |
| -8 | 0.003 | 1.346 |
| -8.1 | 0.003 | 1.175 |
| -8.2 | 0.001 | 1.015 |
| -8.3 | 0 | 0.868 |
| -8.4 | 0 | 0.727 |
| -8.5 | 0 | 0.601 |
| -8.6 | 0 | 0.484 |
| -8.7 | 0 | 0.38 |
| -8.8 | 0 | 0.292 |
| -8.9 | 0 | 0.21 |
| -9 | 0 | 0.143 |
| -9.1 | 0 | 0.081 |
| -9.2 | 0.007 | 0.034 |
| -9.3 | 0.042 | 0.001 |
| -9.4 | 0.067 | 0 |
| -9.5 | 0.084 | 0 |
| -9.6 | 0.087 | 0 |
| -9.7 | 0.087 | 0 |
| -9.8 | 0.078 | 0 |
| -9.9 | 0.056 | 0 |
| -10 | 0.022 | 0 |

Grafico Inviluppi Taglio



Taglio

Inviluppo Spinta Reale Efficace / Spinta Passiva

| Design Assumption | Stage | Muro | Lato | Inviluppo Spinta Reale Efficace / Spinta Passiva |
|--------------------------------------|--------------|-------------|-------------|---|
| | | | | % |
| NTC2018: A2+M2+R1 Stage B Left Wall | | LEFT | | 8.8 |
| NTC2018: A2+M2+R1 Stage 3- Left Wall | | RIGHT | | 18.46 |

Inviluppo Spinta Reale Efficace / Spinta Attiva

| Design Assumption | Stage | Muro | Lato | Inviluppo Spinta Reale Efficace / Spinta Attiva |
|--------------------------------------|--------------|-------------|-------------|--|
| | | | | % |
| NTC2018: A2+M2+R1 Stage 3- Left Wall | | LEFT | | 893.13 |
| NTC2018: A2+M2+R1 Stage 1 Left Wall | | RIGHT | | 2403.2 |

Normative adottate per le verifiche degli Elementi Strutturali

Normative Verifiche

| | |
|--------------|-----|
| Calcestruzzo | NTC |
| Acciaio | NTC |
| Tirante | NTC |

Coefficienti per Verifica Tiranti

| | |
|------------|------|
| GEO FS | 1 |
| ξ_{a3} | 1.8 |
| γ_s | 1.15 |

Riepilogo Stage / Design Assumption per Inviluppo

| Design Assumption | Stage 1 | Stage 2 | Stage A | Stage B | Stage 3- |
|--|---------|---------|---------|---------|----------|
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | V | V | V | V | V |
| NTC2018: A1+M1+R1 (R3 per tiranti) | V | V | V | V | V |
| NTC2018: A2+M2+R1 | V | V | V | V | V |

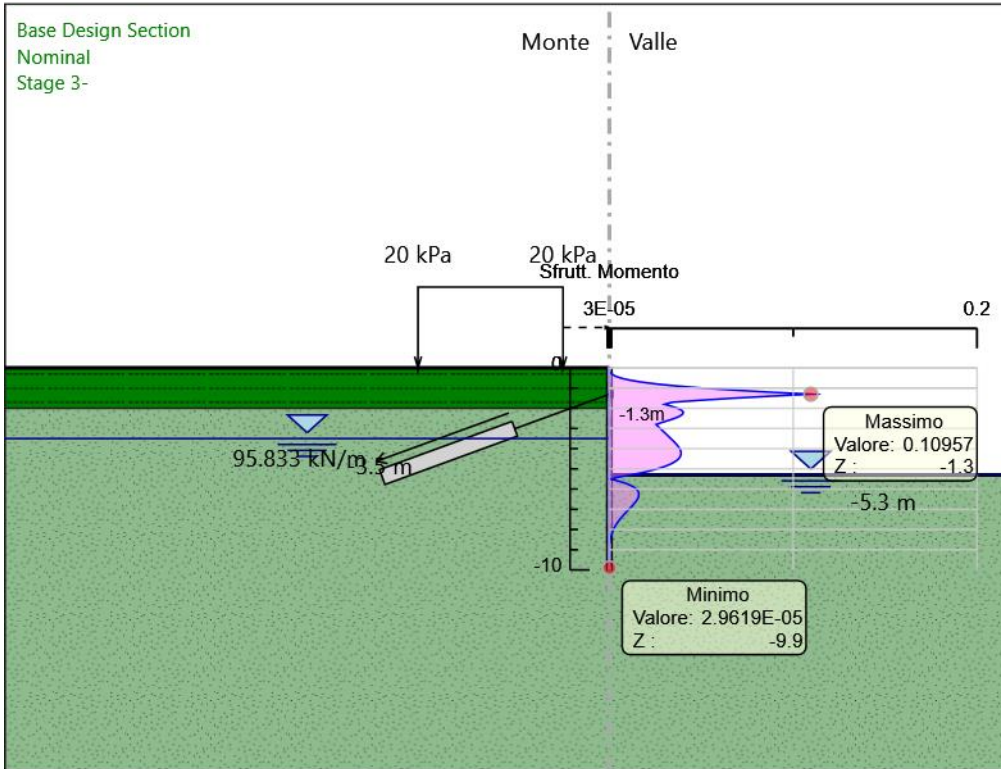
Risultati SteelWorld

Tabella Inviluppi Tasso di Sfruttamento M-N - SteelWorld : LEFT

| Inviluppi Tasso di Sfruttamento M-N - SteelWorld | | LEFT |
|--|--|------|
| Z (m) | Tasso di Sfruttamento M-N - SteelWorld | |
| 0 | 0 | |
| -0.1 | 0 | |
| -0.2 | 0 | |
| -0.3 | 0.001 | |
| -0.4 | 0.003 | |
| -0.5 | 0.006 | |
| -0.6 | 0.011 | |
| -0.7 | 0.017 | |
| -0.8 | 0.026 | |
| -0.9 | 0.037 | |
| -1 | 0.051 | |
| -1.1 | 0.068 | |
| -1.2 | 0.087 | |
| -1.3 | 0.11 | |
| -1.4 | 0.087 | |
| -1.5 | 0.067 | |
| -1.6 | 0.05 | |
| -1.7 | 0.034 | |
| -1.8 | 0.03 | |
| -1.9 | 0.034 | |
| -2 | 0.037 | |
| -2.1 | 0.039 | |
| -2.2 | 0.04 | |
| -2.3 | 0.04 | |
| -2.4 | 0.038 | |
| -2.5 | 0.035 | |
| -2.6 | 0.032 | |
| -2.7 | 0.029 | |
| -2.8 | 0.025 | |
| -2.9 | 0.027 | |
| -3 | 0.028 | |
| -3.1 | 0.029 | |
| -3.2 | 0.03 | |
| -3.3 | 0.031 | |
| -3.4 | 0.032 | |
| -3.5 | 0.033 | |
| -3.6 | 0.035 | |
| -3.7 | 0.036 | |
| -3.8 | 0.037 | |
| -3.9 | 0.038 | |
| -4 | 0.038 | |
| -4.1 | 0.039 | |
| -4.2 | 0.039 | |
| -4.3 | 0.039 | |
| -4.4 | 0.038 | |
| -4.5 | 0.038 | |
| -4.6 | 0.036 | |
| -4.7 | 0.035 | |
| -4.8 | 0.032 | |
| -4.9 | 0.029 | |
| -5 | 0.026 | |
| -5.1 | 0.022 | |
| -5.2 | 0.017 | |
| -5.3 | 0.011 | |
| -5.4 | 0.005 | |
| -5.5 | 0.001 | |
| -5.6 | 0.005 | |
| -5.7 | 0.008 | |

| Inviluppi | Tasso di Sfruttamento M-N - SteelWorld | LEFT |
|-----------|--|-------|
| Z (m) | Tasso di Sfruttamento M-N - SteelWorld | |
| -5.8 | | 0.011 |
| -5.9 | | 0.013 |
| -6 | | 0.015 |
| -6.1 | | 0.016 |
| -6.2 | | 0.016 |
| -6.3 | | 0.016 |
| -6.4 | | 0.016 |
| -6.5 | | 0.015 |
| -6.6 | | 0.014 |
| -6.7 | | 0.014 |
| -6.8 | | 0.013 |
| -6.9 | | 0.012 |
| -7 | | 0.011 |
| -7.1 | | 0.01 |
| -7.2 | | 0.008 |
| -7.3 | | 0.007 |
| -7.4 | | 0.007 |
| -7.5 | | 0.006 |
| -7.6 | | 0.005 |
| -7.7 | | 0.004 |
| -7.8 | | 0.003 |
| -7.9 | | 0.003 |
| -8 | | 0.002 |
| -8.1 | | 0.002 |
| -8.2 | | 0.001 |
| -8.3 | | 0.001 |
| -8.4 | | 0.001 |
| -8.5 | | 0 |
| -8.6 | | 0 |
| -8.7 | | 0 |
| -8.8 | | 0 |
| -8.9 | | 0 |
| -9 | | 0 |
| -9.1 | | 0 |
| -9.2 | | 0 |
| -9.3 | | 0 |
| -9.4 | | 0 |
| -9.5 | | 0 |
| -9.6 | | 0 |
| -9.7 | | 0 |
| -9.8 | | 0 |
| -9.9 | | 0 |
| -10 | | 0 |

Grafico Involuppi Tasso di Sfruttamento M-N - SteelWorld



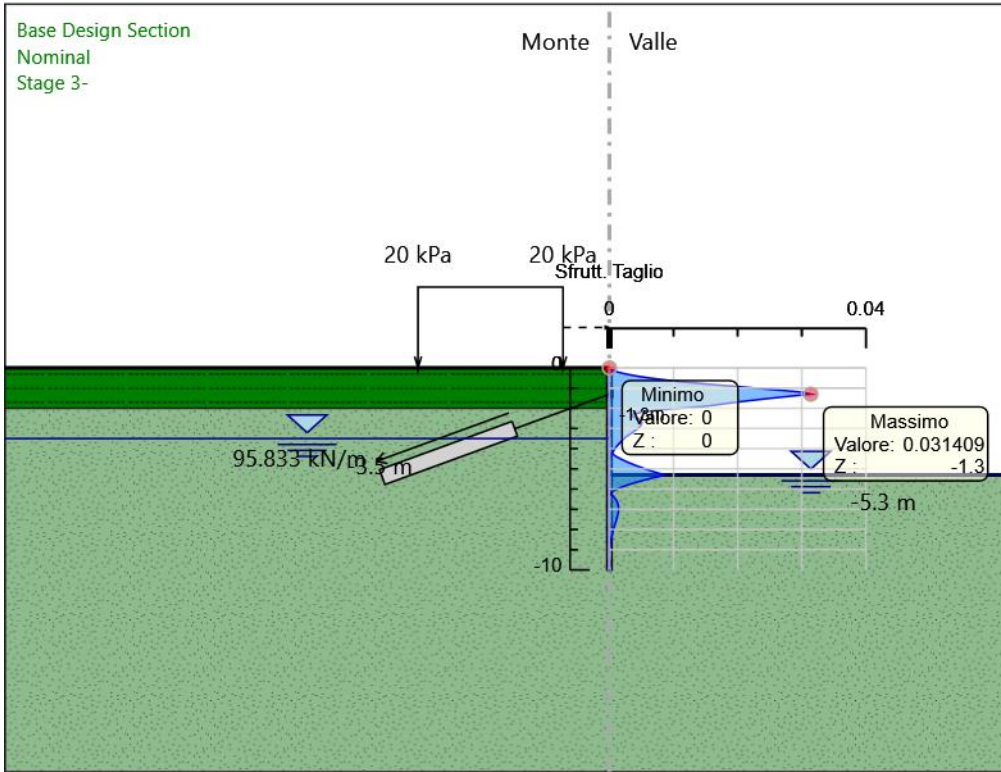
Involuppi
Tasso di Sfruttamento M-N - SteelWorld

Tabella Involuppi Tasso di Sfruttamento a Taglio - SteelWorld : LEFT

| Z (m) | Tasso di Sfruttamento a Taglio - SteelWorld |
|-------|---|
| 0 | 0 |
| -0.1 | 0 |
| -0.2 | 0.001 |
| -0.3 | 0.003 |
| -0.4 | 0.004 |
| -0.5 | 0.006 |
| -0.6 | 0.009 |
| -0.7 | 0.012 |
| -0.8 | 0.015 |
| -0.9 | 0.019 |
| -1 | 0.023 |
| -1.1 | 0.026 |
| -1.2 | 0.03 |
| -1.3 | 0.031 |
| -1.4 | 0.028 |
| -1.5 | 0.025 |
| -1.6 | 0.022 |
| -1.7 | 0.02 |
| -1.8 | 0.017 |
| -1.9 | 0.015 |
| -2 | 0.011 |
| -2.1 | 0.007 |
| -2.2 | 0.005 |
| -2.3 | 0.004 |
| -2.4 | 0.004 |
| -2.5 | 0.004 |
| -2.6 | 0.005 |
| -2.7 | 0.005 |
| -2.8 | 0.005 |
| -2.9 | 0.005 |
| -3 | 0.004 |
| -3.1 | 0.004 |
| -3.2 | 0.004 |
| -3.3 | 0.003 |
| -3.4 | 0.003 |
| -3.5 | 0.002 |
| -3.6 | 0.002 |
| -3.7 | 0.002 |
| -3.8 | 0.001 |
| -3.9 | 0.001 |
| -4 | 0.001 |
| -4.1 | 0.001 |
| -4.2 | 0 |
| -4.3 | 0.001 |
| -4.4 | 0.001 |
| -4.5 | 0.002 |
| -4.6 | 0.002 |
| -4.7 | 0.003 |
| -4.8 | 0.004 |
| -4.9 | 0.005 |
| -5 | 0.006 |
| -5.1 | 0.007 |
| -5.2 | 0.008 |
| -5.3 | 0.009 |
| -5.4 | 0.007 |
| -5.5 | 0.006 |
| -5.6 | 0.005 |
| -5.7 | 0.004 |
| -5.8 | 0.003 |
| -5.9 | 0.002 |
| -6 | 0.001 |

| Z (m) | Tasso di Sfruttamento a Taglio - SteelWorld | LEFT | Tasso di Sfruttamento a Taglio - SteelWorld |
|-------|---|-------|---|
| -6.1 | | 0.001 | |
| -6.2 | | 0 | |
| -6.3 | | 0 | |
| -6.4 | | 0.001 | |
| -6.5 | | 0.001 | |
| -6.6 | | 0.001 | |
| -6.7 | | 0.001 | |
| -6.8 | | 0.001 | |
| -6.9 | | 0.001 | |
| -7 | | 0.001 | |
| -7.1 | | 0.001 | |
| -7.2 | | 0.001 | |
| -7.3 | | 0.001 | |
| -7.4 | | 0.001 | |
| -7.5 | | 0.001 | |
| -7.6 | | 0.001 | |
| -7.7 | | 0.001 | |
| -7.8 | | 0.001 | |
| -7.9 | | 0.001 | |
| -8 | | 0.001 | |
| -8.1 | | 0.001 | |
| -8.2 | | 0 | |
| -8.3 | | 0 | |
| -8.4 | | 0 | |
| -8.5 | | 0 | |
| -8.6 | | 0 | |
| -8.7 | | 0 | |
| -8.8 | | 0 | |
| -8.9 | | 0 | |
| -9 | | 0 | |
| -9.1 | | 0 | |
| -9.2 | | 0 | |
| -9.3 | | 0 | |
| -9.4 | | 0 | |
| -9.5 | | 0 | |
| -9.6 | | 0 | |
| -9.7 | | 0 | |
| -9.8 | | 0 | |
| -9.9 | | 0 | |
| -10 | | 0 | |

Grafico Inviluppi Tasso di Sfruttamento a Taglio - SteelWorld



Inviluppi
Tasso di Sfruttamento a Taglio - SteelWorld

Verifiche Tiranti NTC2018: SLE (Rara/Frequente/Quasi Permanente)

| Design Assumption: NTC2018: SLE (Rara/Frequente/Quasi Permanente) | Tipo Risultato: Verifiche Tiranti | NTC2018 (ITA) | | | | | | Gerarchia delle Resistenze | |
|--|---|------------------|---------|------------------------|------------------------|------------------------|-----------|----------------------------------|--------------|
| | | Tirante | Stage | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Ratio GEO | | Ratio STR |
| Tieback_New_New_New_New | Stage B | | 229.992 | 791.681 | 605.557 | 0.291 | 0.38 | | NO |
| Tieback_New_New_New_New | Stage 3- | | 229.19 | 791.681 | 605.557 | 0.289 | 0.378 | | NO |

Verifiche Tiranti NTC2018: A1+M1+R1 (R3 per tiranti)

| Design Assumption: NTC2018: A1+M1+R1 (R3 per tiranti) Tirante | Tipo Risultato: Verifiche Tiranti Stage | NTC2018 | | | NTC2018 (ITA) | | Resistenza | Gerarchia delle Resistenze |
|---|---|------------------------|------------------------|------------------------|------------------|--------------|------------|-------------------------------|
| | | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Ratio GEO | Ratio STR | | |
| Tieback_New_New_New_New | Stage B | 298.99 | 399.839 | 605.557 | 0.748 | 0.494 | | |
| Tieback_New_New_New_New | Stage 3- | 297.957 | 399.839 | 605.557 | 0.745 | 0.492 | | |

Verifiche Tiranti NTC2018: A2+M2+R1

| Design Assumption: NTC2018: A2+M2+R1 Tirante | Tipo Risultato: Verifiche Tiranti Stage | NTC2018 (ITA) | | | | | | |
|--|---|------------------------|------------------------|------------------------|-----------|--------------|------------|-------------------------------|
| | | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Ratio GEO | Ratio STR | Resistenza | Gerarchia delle Resistenze |
| Tieback_New_New_New_New | Stage B | 229.992 | 399.839 | 605.557 | 0.575 | 0.38 | | |
| Tieback_New_New_New_New | Stage 3- | 229.144 | 399.839 | 605.557 | 0.573 | 0.378 | | |

Inviluppo Verifiche Tiranti (su tutte le D.A. attive)

| Tipo Risultato: | | | | | | | | | |
|-------------------------|---------|---------------------|---------------------|---------------------|-----------|-----------|------------|----------------------------|---------------------------------------|
| Verifiche Tiranti | | | | | | | | | |
| Tirante | Stage | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Ratio GEO | Ratio STR | Resistenza | Gerarchia delle Resistenze | Design Assumption |
| Tieback_New_New_New_New | Stage B | 298.99 | 399.839 | 605.557 | 0.748 | 0.494 | | | NTC2018: A1+M1+R1 (R3 per tiranti) |

Verifiche Travi di Ripartizione Nominal

| Design Assumption: Nominal Trave di Ripartizione | Tipo Risultato: Verifiche Travi di Ripartizione Elemento strutturale | Sezione | Materiale | Stage | Carico distribuito (kN/m) | Assiale (kN) | Ratio M-N | Ratio taglio | Instabilità |
|--|--|------------|-----------|-------------|------------------------------|-----------------|--------------|-----------------|-------------|
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage B | 95.83 | 0 | 0 | 0 | 0 |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage 3- | 95.496 | 0 | 0 | 0 | 0 |

Verifiche Travi di Ripartizione NTC2018: SLE (Rara/Frequente/Quasi Permanente)

| Design Assumption: NTC2018: SLE | | | | | | | | | |
|------------------------------------|-------------------------|---------|-----------|----------|---------------------------|--------------|-----------|--------------|-------------|
| Tipo Risultato: Verifiche Travi di | NTC2018 | | | | | | | | |
| (Rara/Frequente/Quasi Permanente) | Ripartizione | (ITA) | | | | | | | |
| Trave di Ripartizione | Elemento strutturale | Sezione | Materiale | Stage | Carico distribuito (kN/m) | Assiale (kN) | Ratio M-N | Ratio taglio | Instabilità |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage B | 95.83 | 0 | 0.323 | 0.215 | 0 |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage 3- | 95.496 | 0 | 0.322 | 0.214 | 0 |

Verifiche Travi di Ripartizione NTC2018: A1+M1+R1 (R3 per tiranti)

| Design Assumption: NTC2018: A1+M1+R1 (R3 per tiranti) | | Tipo Risultato: Verifiche Travi di Ripartizione | | NTC2018 (ITA) | | | | | | |
|---|-------------------------|--|-----------|------------------|---------------------------------|-----------------|--------------|-----------------|-------------|--|
| Trave di Ripartizione | Elemento strutturale | Sezione | Materiale | Stage | Carico distribuito (kN/m) | Assiale (kN) | Ratio M-N | Ratio taglio | Instabilità | |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage B | 124.579 | 0 | 0.42 | 0.28 | 0 | |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage 3- | 124.149 | 0 | 0.418 | 0.279 | 0 | |

Verifiche Travi di Ripartizione NTC2018: A2+M2+R1

| Design Assumption: NTC2018: A2+M2+R1 Trave di Ripartizione | Tipo Risultato: Verifiche Travi di Ripartizione Elemento strutturale | NTC2018 (ITA) Sezione | Materiale | Stage | Carico distribuito (kN/m) | Assiale (kN) | Ratio M-N | Ratio taglio | Instabilità |
|--|--|-----------------------------|-----------|-------------|---------------------------------|-----------------|--------------|-----------------|-------------|
| | | | | | | | | | |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage B | 95.83 | 0 | 0.323 | 0.215 | 0 |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage 3- | 95.477 | 0 | 0.322 | 0.214 | 0 |

10 ALLEGATO 2: tabulato di calcolo paratia (interasse tiranti 4m)

Descrizione della Stratigrafia e degli Strati di Terreno

Tipo : POLYLINE

Punti

(-30;0)
(10;0)
(20;0)
(20;-40)
(-30;-40)

OCR : 1

Tipo : POLYLINE

Punti

(-30;-2)
(20;-2)
(20;-20)
(-30;-20)

OCR : 1

| Strato di Terreno | Terreno | γ dry | γ sat | ϕ' | ϕ | c_v | ϕ_p | c' | Su | Modulo | Elastico | Eu | Evc | Eur | Ah | Av | exp | Pa | Rur/Rvc | Rvc | Ku | Kvc | Kur |
|-------------------|----------|-------------------|-------------------|---------|--------|-------|----------|------|-----|----------|----------|--------|--------|-----|----|----|-----|-----|---------|-----|-------------------|-------------------|-------------------|
| | | kN/m ³ | kN/m ³ | ° | ° | ° | ° | kPa | kPa | | | | kPa | kPa | | | | kPa | | kPa | kN/m ³ | kN/m ³ | kN/m ³ |
| 1 | RILEVATO | 19 | 19 | 35 | | | | 0 | | Constant | | 50000 | 80000 | | | | | | | | | | |
| 2 | unità SR | 24.5 | 24.5 | 40 | | | | 40 | | Constant | | 150000 | 240000 | | | | | | | | | | |

Descrizione Pareti

X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Muro di sinistra

Sezione : mc 240 inter 40 cm

Area equivalente : 0.0294745535317205 m

Inerzia equivalente : 0.0001 m⁴/m

Materiale calcestruzzo : C25/30

Tipo sezione : Tangent

Spaziatura : 0.4 m

Diametro : 0.24 m

Efficacia : 1

Materiale acciaio : S355

Sezione : CHS168.3*12

Tipo sezione : O

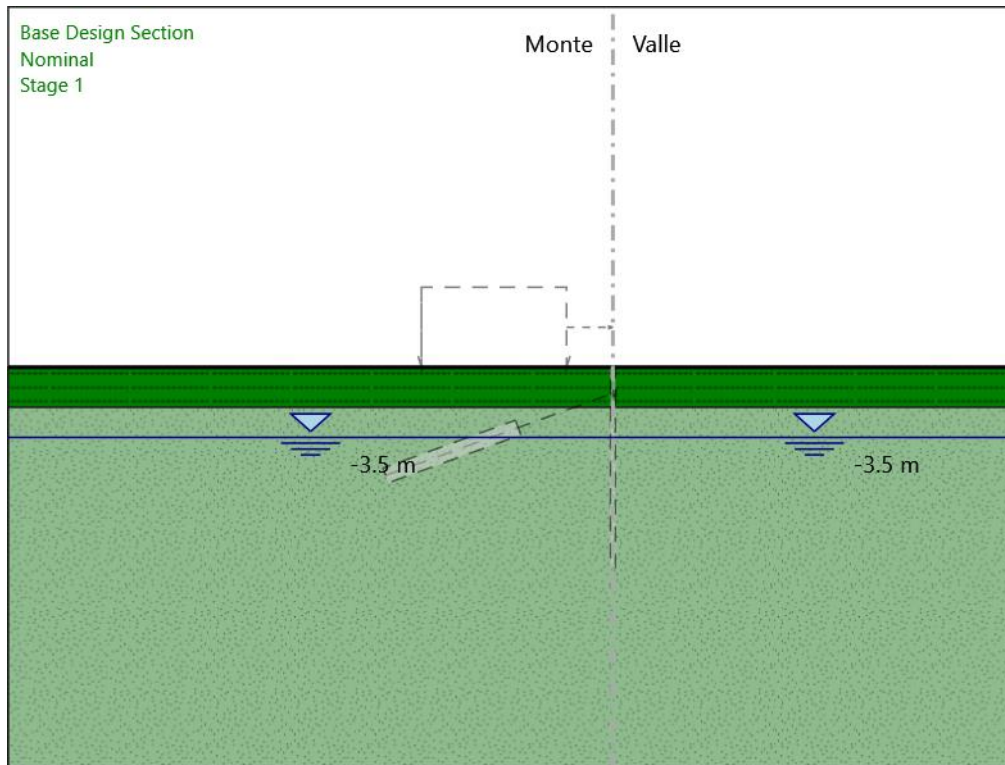
Spaziatura : 0.4 m

Spessore : 0.012 m

Diametro : 0.1683 m

Fasi di Calcolo

Stage 1



Stage 1

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : 0 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

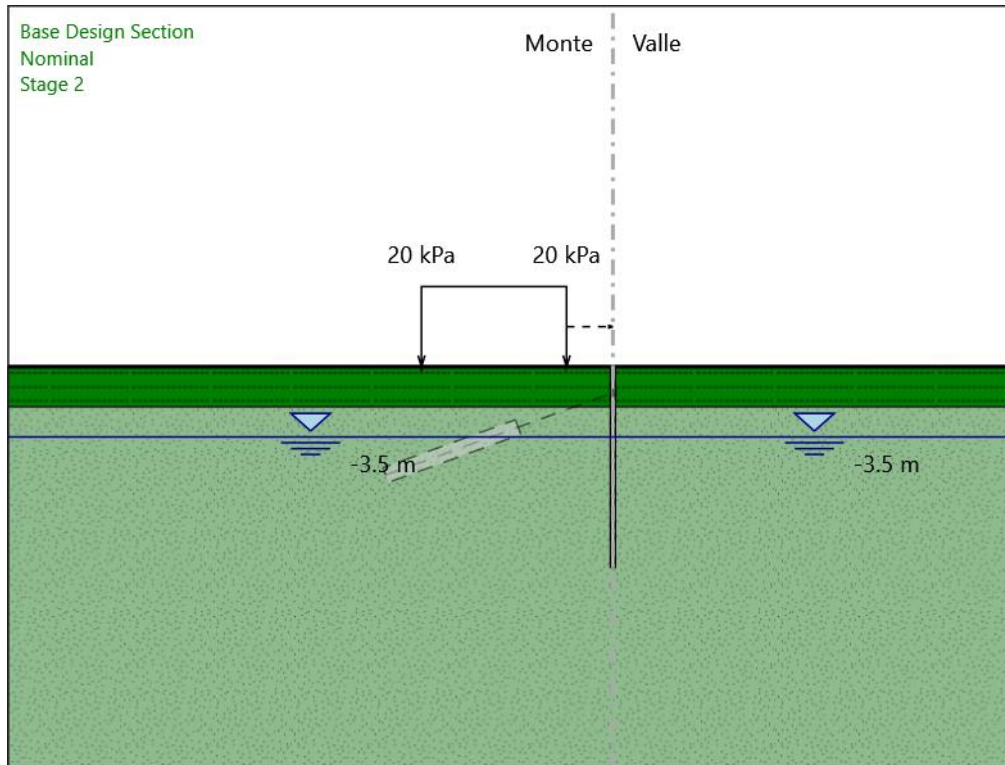
0 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -3.5 m

Stage 2



Stage 2

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : 0 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

0 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -3.5 m

Carichi

Carico lineare in superficie : SurfaceSurcharge

X iniziale : -9.5 m

X finale : -2.3 m

Pressione iniziale : 20 kPa

Pressione finale : 20 kPa

Elementi strutturali

Paratia : paratia sx

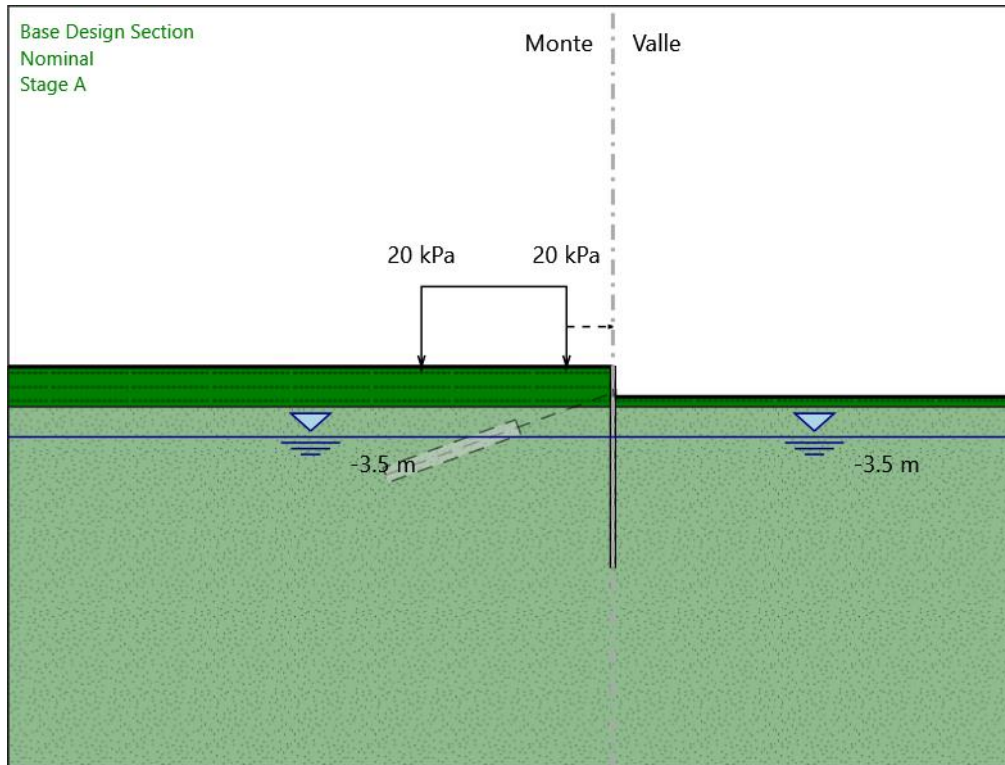
X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Sezione : mc 240 inter 40 cm

Stage A



Stage A

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : -1.5 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

-1.5 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -3.5 m

Carichi

Carico lineare in superficie : SurfaceSurcharge

X iniziale : -9.5 m

X finale : -2.3 m

Pressione iniziale : 20 kPa

Pressione finale : 20 kPa

Elementi strutturali

Paratia : paratia sx

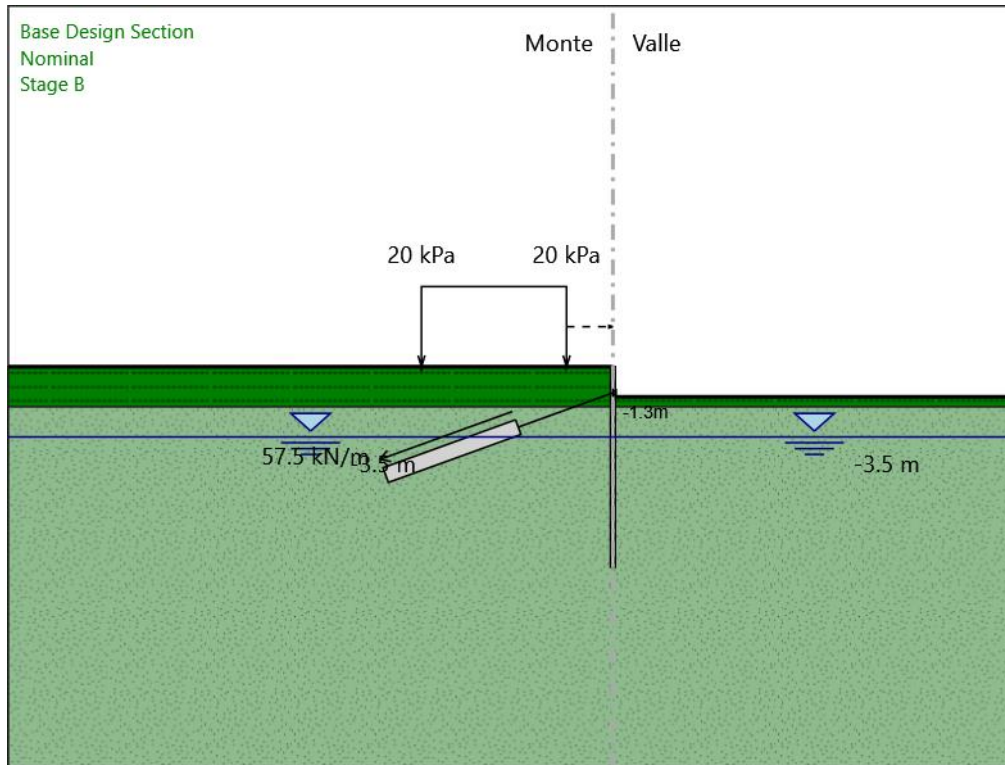
X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Sezione : mc 240 inter 40 cm

Stage B



Stage B

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : -1.5 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

-1.5 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -3.5 m

Carichi

Carico lineare in superficie : SurfaceSurcharge

X iniziale : -9.5 m

X finale : -2.3 m

Pressione iniziale : 20 kPa

Pressione finale : 20 kPa

Elementi strutturali

Paratia : paratia sx

X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Sezione : mc 240 inter 40 cm

Tirante : Tieback_New_New_New_New

X : 0 m

Z : -1.3 m

Lunghezza bulbo : 7 m

Diametro bulbo : 0.2 m

Lunghezza libera : 5 m

Spaziatura orizzontale : 4 m

Precarico : 230 kN

Angolo : 20 °

Sezione : 3 strands

Tipo di barre : Barre trefoli

Numero di barre : 3

Diametro : 0.01331 m

Area : 0.000417 m²

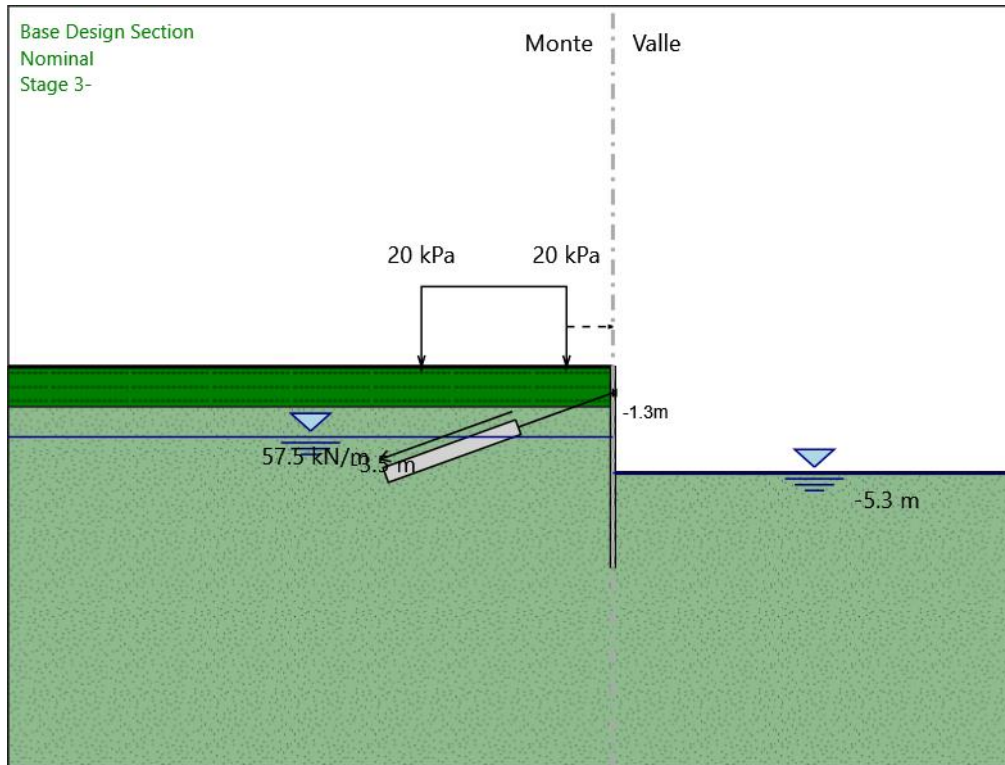
Trave di Ripartizione : Default Waler

Sezione : Waler Section 2 steel

HE 160B

Materiale : S355

Stage 3-



Stage 3-

Scavo

Muro di sinistra

Lato monte : 0 m

Lato valle : -5.3 m

Linea di scavo di sinistra (Orizzontale)

0 m

Linea di scavo di destra (Orizzontale)

-5.3 m

Falda acquifera

Falda di sinistra : -3.5 m

Falda di destra : -5.3 m

Carichi

Carico lineare in superficie : SurfaceSurcharge

X iniziale : -9.5 m

X finale : -2.3 m

Pressione iniziale : 20 kPa

Pressione finale : 20 kPa

Elementi strutturali

Paratia : paratia sx

X : 0 m

Quota in alto : 0 m

Quota di fondo : -10 m

Sezione : mc 240 inter 40 cm

Tirante : Tieback_New_New_New_New

X : 0 m

Z : -1.3 m

Lunghezza bulbo : 7 m

Diametro bulbo : 0.2 m

Lunghezza libera : 5 m

Spaziatura orizzontale : 4 m

Precarico : 230 kN

Angolo : 20 °

Sezione : 3 strands

Tipo di barre : Barre trefoli

Numero di barre : 3

Diametro : 0.01331 m

Area : 0.000417 m²

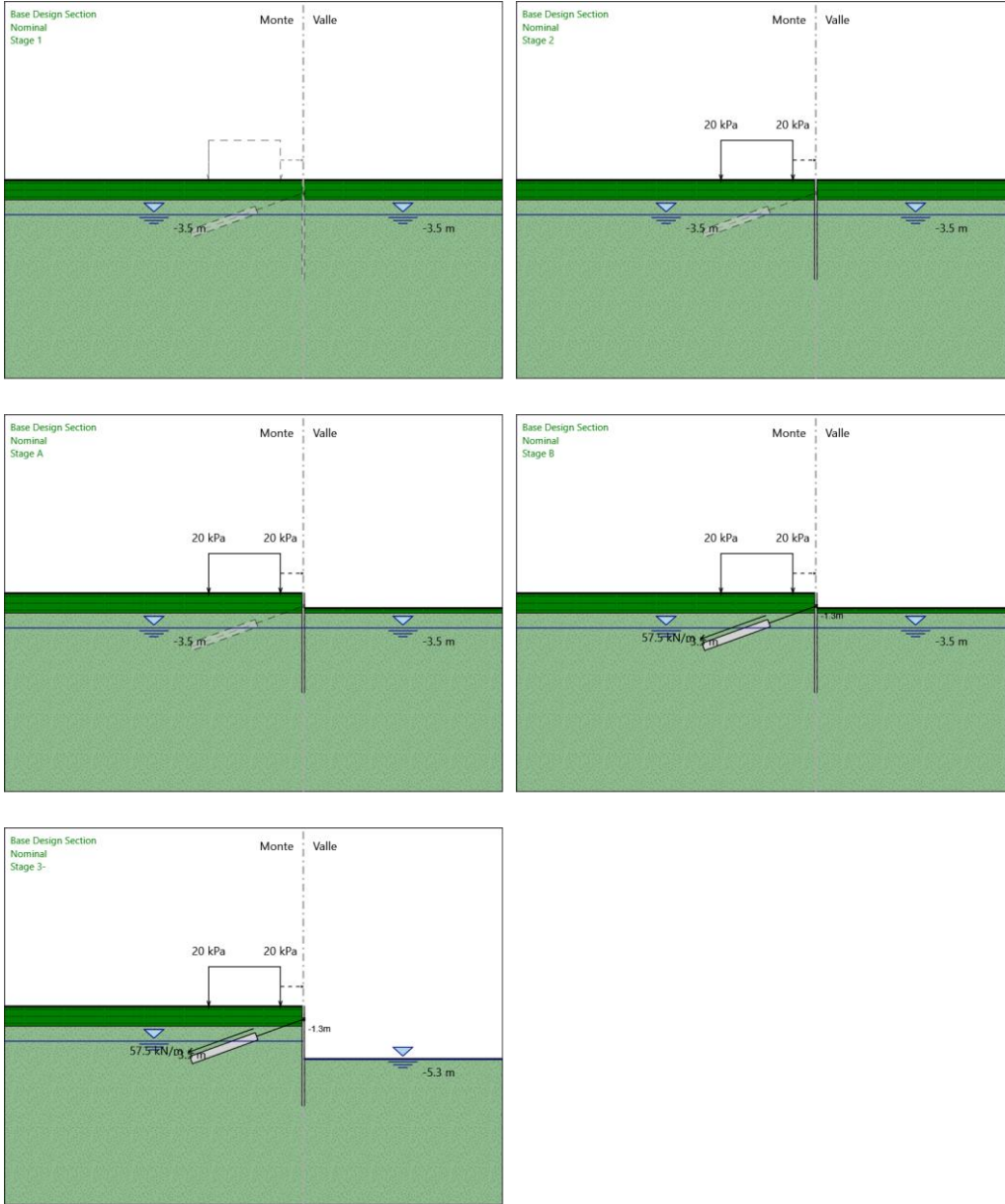
Trave di Ripartizione : Default Waler

Sezione : Waler Section 2 steel

HE 160B

Materiale : S355

Tabella Configurazione Stage (Nominal)



Grafici dei Risultati

Design Assumption : Nominal

Tabella Spostamento Nominal - LEFT Stage: Stage 1

| Design Assumption: Nominal | Tipo Risultato: Spostamento | Muro: LEFT |
|----------------------------|-----------------------------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 1 | 0 | 0 |
| Stage 1 | -0.1 | 0 |
| Stage 1 | -0.2 | 0 |
| Stage 1 | -0.3 | 0 |
| Stage 1 | -0.4 | 0 |
| Stage 1 | -0.5 | 0 |
| Stage 1 | -0.6 | 0 |
| Stage 1 | -0.7 | 0 |
| Stage 1 | -0.8 | 0 |
| Stage 1 | -0.9 | 0 |
| Stage 1 | -1 | 0 |
| Stage 1 | -1.1 | 0 |
| Stage 1 | -1.2 | 0 |
| Stage 1 | -1.3 | 0 |
| Stage 1 | -1.4 | 0 |
| Stage 1 | -1.5 | 0 |
| Stage 1 | -1.6 | 0 |
| Stage 1 | -1.7 | 0 |
| Stage 1 | -1.8 | 0 |
| Stage 1 | -1.9 | 0 |
| Stage 1 | -2 | 0 |
| Stage 1 | -2.1 | 0 |
| Stage 1 | -2.2 | 0 |
| Stage 1 | -2.3 | 0 |
| Stage 1 | -2.4 | 0 |
| Stage 1 | -2.5 | 0 |
| Stage 1 | -2.6 | 0 |
| Stage 1 | -2.7 | 0 |
| Stage 1 | -2.8 | 0 |
| Stage 1 | -2.9 | 0 |
| Stage 1 | -3 | 0 |
| Stage 1 | -3.1 | 0 |
| Stage 1 | -3.2 | 0 |
| Stage 1 | -3.3 | 0 |
| Stage 1 | -3.4 | 0 |
| Stage 1 | -3.5 | 0 |
| Stage 1 | -3.6 | 0 |
| Stage 1 | -3.7 | 0 |
| Stage 1 | -3.8 | 0 |
| Stage 1 | -3.9 | 0 |
| Stage 1 | -4 | 0 |
| Stage 1 | -4.1 | 0 |
| Stage 1 | -4.2 | 0 |
| Stage 1 | -4.3 | 0 |
| Stage 1 | -4.4 | 0 |
| Stage 1 | -4.5 | 0 |
| Stage 1 | -4.6 | 0 |
| Stage 1 | -4.7 | 0 |
| Stage 1 | -4.8 | 0 |
| Stage 1 | -4.9 | 0 |
| Stage 1 | -5 | 0 |
| Stage 1 | -5.1 | 0 |
| Stage 1 | -5.2 | 0 |
| Stage 1 | -5.3 | 0 |

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 1 | -5.4 | 0 |
| Stage 1 | -5.5 | 0 |
| Stage 1 | -5.6 | 0 |
| Stage 1 | -5.7 | 0 |
| Stage 1 | -5.8 | 0 |
| Stage 1 | -5.9 | 0 |
| Stage 1 | -6 | 0 |
| Stage 1 | -6.1 | 0 |
| Stage 1 | -6.2 | 0 |
| Stage 1 | -6.3 | 0 |
| Stage 1 | -6.4 | 0 |
| Stage 1 | -6.5 | 0 |
| Stage 1 | -6.6 | 0 |
| Stage 1 | -6.7 | 0 |
| Stage 1 | -6.8 | 0 |
| Stage 1 | -6.9 | 0 |
| Stage 1 | -7 | 0 |
| Stage 1 | -7.1 | 0 |
| Stage 1 | -7.2 | 0 |
| Stage 1 | -7.3 | 0 |
| Stage 1 | -7.4 | 0 |
| Stage 1 | -7.5 | 0 |
| Stage 1 | -7.6 | 0 |
| Stage 1 | -7.7 | 0 |
| Stage 1 | -7.8 | 0 |
| Stage 1 | -7.9 | 0 |
| Stage 1 | -8 | 0 |
| Stage 1 | -8.1 | 0 |
| Stage 1 | -8.2 | 0 |
| Stage 1 | -8.3 | 0 |
| Stage 1 | -8.4 | 0 |
| Stage 1 | -8.5 | 0 |
| Stage 1 | -8.6 | 0 |
| Stage 1 | -8.7 | 0 |
| Stage 1 | -8.8 | 0 |
| Stage 1 | -8.9 | 0 |
| Stage 1 | -9 | 0 |
| Stage 1 | -9.1 | 0 |
| Stage 1 | -9.2 | 0 |
| Stage 1 | -9.3 | 0 |
| Stage 1 | -9.4 | 0 |
| Stage 1 | -9.5 | 0 |
| Stage 1 | -9.6 | 0 |
| Stage 1 | -9.7 | 0 |
| Stage 1 | -9.8 | 0 |
| Stage 1 | -9.9 | 0 |
| Stage 1 | -10 | 0 |

Tabella Spostamento Nominal - LEFT Stage: Stage 2

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 2 | 0 | 0 |
| Stage 2 | -0.1 | 0 |
| Stage 2 | -0.2 | 0 |
| Stage 2 | -0.3 | 0 |
| Stage 2 | -0.4 | 0 |
| Stage 2 | -0.5 | 0 |
| Stage 2 | -0.6 | 0 |
| Stage 2 | -0.7 | 0 |
| Stage 2 | -0.8 | 0 |
| Stage 2 | -0.9 | 0 |
| Stage 2 | -1 | 0 |
| Stage 2 | -1.1 | 0 |
| Stage 2 | -1.2 | 0 |
| Stage 2 | -1.3 | 0 |
| Stage 2 | -1.4 | 0 |
| Stage 2 | -1.5 | 0 |
| Stage 2 | -1.6 | 0 |
| Stage 2 | -1.7 | 0 |
| Stage 2 | -1.8 | 0 |
| Stage 2 | -1.9 | 0 |
| Stage 2 | -2 | 0 |
| Stage 2 | -2.1 | 0 |
| Stage 2 | -2.2 | 0 |
| Stage 2 | -2.3 | 0 |
| Stage 2 | -2.4 | 0 |
| Stage 2 | -2.5 | 0 |
| Stage 2 | -2.6 | 0 |
| Stage 2 | -2.7 | 0 |
| Stage 2 | -2.8 | 0 |
| Stage 2 | -2.9 | 0 |
| Stage 2 | -3 | 0 |
| Stage 2 | -3.1 | 0 |
| Stage 2 | -3.2 | 0 |
| Stage 2 | -3.3 | 0 |
| Stage 2 | -3.4 | 0 |
| Stage 2 | -3.5 | 0 |
| Stage 2 | -3.6 | 0 |
| Stage 2 | -3.7 | 0 |
| Stage 2 | -3.8 | 0 |
| Stage 2 | -3.9 | 0 |
| Stage 2 | -4 | 0 |
| Stage 2 | -4.1 | 0.01 |
| Stage 2 | -4.2 | 0.01 |
| Stage 2 | -4.3 | 0.01 |
| Stage 2 | -4.4 | 0.01 |
| Stage 2 | -4.5 | 0.01 |
| Stage 2 | -4.6 | 0.01 |
| Stage 2 | -4.7 | 0.01 |
| Stage 2 | -4.8 | 0.01 |
| Stage 2 | -4.9 | 0.01 |
| Stage 2 | -5 | 0.01 |
| Stage 2 | -5.1 | 0.01 |
| Stage 2 | -5.2 | 0.01 |
| Stage 2 | -5.3 | 0.01 |
| Stage 2 | -5.4 | 0.01 |
| Stage 2 | -5.5 | 0.01 |
| Stage 2 | -5.6 | 0.01 |
| Stage 2 | -5.7 | 0.01 |
| Stage 2 | -5.8 | 0.01 |
| Stage 2 | -5.9 | 0.01 |
| Stage 2 | -6 | 0.01 |

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 2 | -6.1 | 0.01 |
| Stage 2 | -6.2 | 0.01 |
| Stage 2 | -6.3 | 0.01 |
| Stage 2 | -6.4 | 0.01 |
| Stage 2 | -6.5 | 0.01 |
| Stage 2 | -6.6 | 0.01 |
| Stage 2 | -6.7 | 0.01 |
| Stage 2 | -6.8 | 0.01 |
| Stage 2 | -6.9 | 0.01 |
| Stage 2 | -7 | 0.01 |
| Stage 2 | -7.1 | 0.01 |
| Stage 2 | -7.2 | 0.01 |
| Stage 2 | -7.3 | 0.01 |
| Stage 2 | -7.4 | 0.01 |
| Stage 2 | -7.5 | 0.01 |
| Stage 2 | -7.6 | 0.01 |
| Stage 2 | -7.7 | 0.01 |
| Stage 2 | -7.8 | 0.01 |
| Stage 2 | -7.9 | 0.01 |
| Stage 2 | -8 | 0.01 |
| Stage 2 | -8.1 | 0.01 |
| Stage 2 | -8.2 | 0.01 |
| Stage 2 | -8.3 | 0.01 |
| Stage 2 | -8.4 | 0.01 |
| Stage 2 | -8.5 | 0.01 |
| Stage 2 | -8.6 | 0.01 |
| Stage 2 | -8.7 | 0.01 |
| Stage 2 | -8.8 | 0.01 |
| Stage 2 | -8.9 | 0.01 |
| Stage 2 | -9 | 0.01 |
| Stage 2 | -9.1 | 0.01 |
| Stage 2 | -9.2 | 0.01 |
| Stage 2 | -9.3 | 0.01 |
| Stage 2 | -9.4 | 0.01 |
| Stage 2 | -9.5 | 0.01 |
| Stage 2 | -9.6 | 0.01 |
| Stage 2 | -9.7 | 0.01 |
| Stage 2 | -9.8 | 0.01 |
| Stage 2 | -9.9 | 0.01 |
| Stage 2 | -10 | 0.01 |

Tabella Spostamento Nominal - LEFT Stage: Stage A

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage A | 0 | 1.15 |
| Stage A | -0.1 | 1.09 |
| Stage A | -0.2 | 1.04 |
| Stage A | -0.3 | 0.99 |
| Stage A | -0.4 | 0.94 |
| Stage A | -0.5 | 0.88 |
| Stage A | -0.6 | 0.83 |
| Stage A | -0.7 | 0.78 |
| Stage A | -0.8 | 0.73 |
| Stage A | -0.9 | 0.68 |
| Stage A | -1 | 0.63 |
| Stage A | -1.1 | 0.57 |
| Stage A | -1.2 | 0.52 |
| Stage A | -1.3 | 0.48 |
| Stage A | -1.4 | 0.43 |
| Stage A | -1.5 | 0.38 |
| Stage A | -1.6 | 0.34 |
| Stage A | -1.7 | 0.29 |
| Stage A | -1.8 | 0.25 |
| Stage A | -1.9 | 0.21 |
| Stage A | -2 | 0.18 |
| Stage A | -2.1 | 0.15 |
| Stage A | -2.2 | 0.12 |
| Stage A | -2.3 | 0.09 |
| Stage A | -2.4 | 0.07 |
| Stage A | -2.5 | 0.06 |
| Stage A | -2.6 | 0.04 |
| Stage A | -2.7 | 0.03 |
| Stage A | -2.8 | 0.02 |
| Stage A | -2.9 | 0.02 |
| Stage A | -3 | 0.01 |
| Stage A | -3.1 | 0.01 |
| Stage A | -3.2 | 0.01 |
| Stage A | -3.3 | 0.01 |
| Stage A | -3.4 | 0.01 |
| Stage A | -3.5 | 0.01 |
| Stage A | -3.6 | 0.01 |
| Stage A | -3.7 | 0.01 |
| Stage A | -3.8 | 0.01 |
| Stage A | -3.9 | 0.02 |
| Stage A | -4 | 0.02 |
| Stage A | -4.1 | 0.02 |
| Stage A | -4.2 | 0.02 |
| Stage A | -4.3 | 0.02 |
| Stage A | -4.4 | 0.02 |
| Stage A | -4.5 | 0.02 |
| Stage A | -4.6 | 0.03 |
| Stage A | -4.7 | 0.03 |
| Stage A | -4.8 | 0.03 |
| Stage A | -4.9 | 0.03 |
| Stage A | -5 | 0.03 |
| Stage A | -5.1 | 0.03 |
| Stage A | -5.2 | 0.03 |
| Stage A | -5.3 | 0.03 |
| Stage A | -5.4 | 0.03 |
| Stage A | -5.5 | 0.03 |
| Stage A | -5.6 | 0.03 |
| Stage A | -5.7 | 0.03 |
| Stage A | -5.8 | 0.03 |
| Stage A | -5.9 | 0.03 |
| Stage A | -6 | 0.03 |

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage A | -6.1 | 0.03 |
| Stage A | -6.2 | 0.03 |
| Stage A | -6.3 | 0.03 |
| Stage A | -6.4 | 0.03 |
| Stage A | -6.5 | 0.03 |
| Stage A | -6.6 | 0.03 |
| Stage A | -6.7 | 0.03 |
| Stage A | -6.8 | 0.03 |
| Stage A | -6.9 | 0.03 |
| Stage A | -7 | 0.03 |
| Stage A | -7.1 | 0.03 |
| Stage A | -7.2 | 0.03 |
| Stage A | -7.3 | 0.03 |
| Stage A | -7.4 | 0.03 |
| Stage A | -7.5 | 0.03 |
| Stage A | -7.6 | 0.03 |
| Stage A | -7.7 | 0.03 |
| Stage A | -7.8 | 0.03 |
| Stage A | -7.9 | 0.03 |
| Stage A | -8 | 0.03 |
| Stage A | -8.1 | 0.03 |
| Stage A | -8.2 | 0.03 |
| Stage A | -8.3 | 0.03 |
| Stage A | -8.4 | 0.03 |
| Stage A | -8.5 | 0.03 |
| Stage A | -8.6 | 0.03 |
| Stage A | -8.7 | 0.03 |
| Stage A | -8.8 | 0.03 |
| Stage A | -8.9 | 0.03 |
| Stage A | -9 | 0.03 |
| Stage A | -9.1 | 0.03 |
| Stage A | -9.2 | 0.03 |
| Stage A | -9.3 | 0.03 |
| Stage A | -9.4 | 0.03 |
| Stage A | -9.5 | 0.03 |
| Stage A | -9.6 | 0.03 |
| Stage A | -9.7 | 0.03 |
| Stage A | -9.8 | 0.03 |
| Stage A | -9.9 | 0.03 |
| Stage A | -10 | 0.03 |

Tabella Spostamento Nominal - LEFT Stage: Stage B

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage B | 0 | 0.75 |
| Stage B | -0.1 | 0.69 |
| Stage B | -0.2 | 0.64 |
| Stage B | -0.3 | 0.58 |
| Stage B | -0.4 | 0.53 |
| Stage B | -0.5 | 0.47 |
| Stage B | -0.6 | 0.42 |
| Stage B | -0.7 | 0.36 |
| Stage B | -0.8 | 0.31 |
| Stage B | -0.9 | 0.26 |
| Stage B | -1 | 0.21 |
| Stage B | -1.1 | 0.17 |
| Stage B | -1.2 | 0.13 |
| Stage B | -1.3 | 0.1 |
| Stage B | -1.4 | 0.07 |
| Stage B | -1.5 | 0.05 |
| Stage B | -1.6 | 0.04 |
| Stage B | -1.7 | 0.03 |
| Stage B | -1.8 | 0.02 |
| Stage B | -1.9 | 0.01 |
| Stage B | -2 | 0.01 |
| Stage B | -2.1 | 0.01 |
| Stage B | -2.2 | 0.01 |
| Stage B | -2.3 | 0.01 |
| Stage B | -2.4 | 0.01 |
| Stage B | -2.5 | 0.01 |
| Stage B | -2.6 | 0.01 |
| Stage B | -2.7 | 0.01 |
| Stage B | -2.8 | 0.01 |
| Stage B | -2.9 | 0.02 |
| Stage B | -3 | 0.02 |
| Stage B | -3.1 | 0.02 |
| Stage B | -3.2 | 0.02 |
| Stage B | -3.3 | 0.02 |
| Stage B | -3.4 | 0.02 |
| Stage B | -3.5 | 0.02 |
| Stage B | -3.6 | 0.02 |
| Stage B | -3.7 | 0.03 |
| Stage B | -3.8 | 0.03 |
| Stage B | -3.9 | 0.03 |
| Stage B | -4 | 0.03 |
| Stage B | -4.1 | 0.03 |
| Stage B | -4.2 | 0.03 |
| Stage B | -4.3 | 0.03 |
| Stage B | -4.4 | 0.03 |
| Stage B | -4.5 | 0.03 |
| Stage B | -4.6 | 0.03 |
| Stage B | -4.7 | 0.03 |
| Stage B | -4.8 | 0.03 |
| Stage B | -4.9 | 0.03 |
| Stage B | -5 | 0.03 |
| Stage B | -5.1 | 0.03 |
| Stage B | -5.2 | 0.03 |
| Stage B | -5.3 | 0.03 |
| Stage B | -5.4 | 0.03 |
| Stage B | -5.5 | 0.03 |
| Stage B | -5.6 | 0.03 |
| Stage B | -5.7 | 0.03 |
| Stage B | -5.8 | 0.03 |
| Stage B | -5.9 | 0.03 |
| Stage B | -6 | 0.03 |

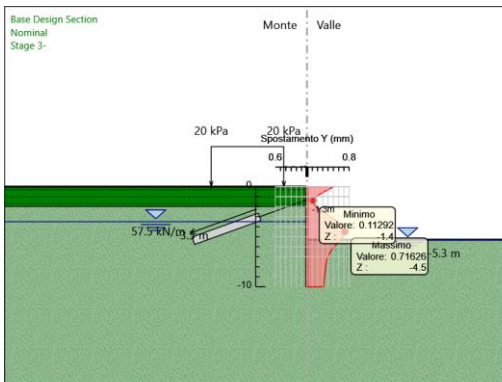
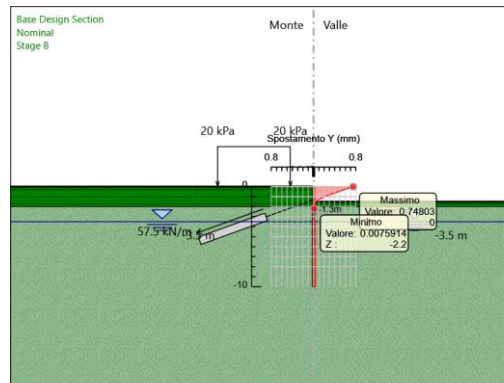
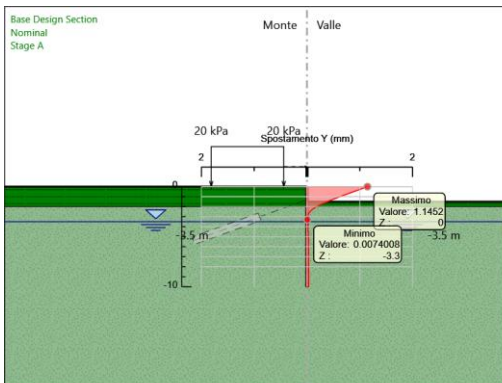
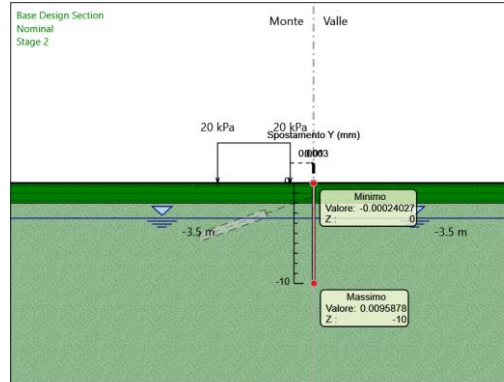
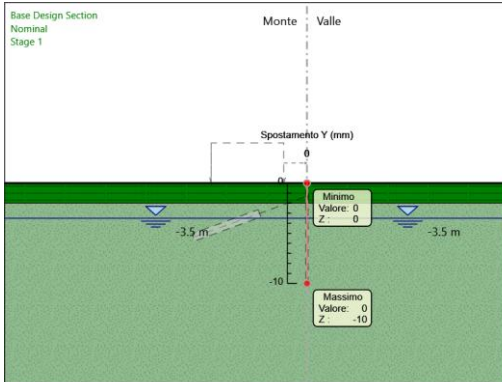
| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage B | -6.1 | 0.03 |
| Stage B | -6.2 | 0.03 |
| Stage B | -6.3 | 0.03 |
| Stage B | -6.4 | 0.03 |
| Stage B | -6.5 | 0.03 |
| Stage B | -6.6 | 0.03 |
| Stage B | -6.7 | 0.03 |
| Stage B | -6.8 | 0.03 |
| Stage B | -6.9 | 0.03 |
| Stage B | -7 | 0.03 |
| Stage B | -7.1 | 0.03 |
| Stage B | -7.2 | 0.03 |
| Stage B | -7.3 | 0.03 |
| Stage B | -7.4 | 0.03 |
| Stage B | -7.5 | 0.03 |
| Stage B | -7.6 | 0.03 |
| Stage B | -7.7 | 0.03 |
| Stage B | -7.8 | 0.03 |
| Stage B | -7.9 | 0.03 |
| Stage B | -8 | 0.03 |
| Stage B | -8.1 | 0.03 |
| Stage B | -8.2 | 0.03 |
| Stage B | -8.3 | 0.03 |
| Stage B | -8.4 | 0.03 |
| Stage B | -8.5 | 0.03 |
| Stage B | -8.6 | 0.03 |
| Stage B | -8.7 | 0.03 |
| Stage B | -8.8 | 0.03 |
| Stage B | -8.9 | 0.03 |
| Stage B | -9 | 0.03 |
| Stage B | -9.1 | 0.03 |
| Stage B | -9.2 | 0.03 |
| Stage B | -9.3 | 0.03 |
| Stage B | -9.4 | 0.03 |
| Stage B | -9.5 | 0.03 |
| Stage B | -9.6 | 0.03 |
| Stage B | -9.7 | 0.03 |
| Stage B | -9.8 | 0.03 |
| Stage B | -9.9 | 0.03 |
| Stage B | -10 | 0.03 |

Tabella Spostamento Nominal - LEFT Stage: Stage 3-

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 3- | 0 | 0.51 |
| Stage 3- | -0.1 | 0.47 |
| Stage 3- | -0.2 | 0.44 |
| Stage 3- | -0.3 | 0.4 |
| Stage 3- | -0.4 | 0.37 |
| Stage 3- | -0.5 | 0.33 |
| Stage 3- | -0.6 | 0.3 |
| Stage 3- | -0.7 | 0.26 |
| Stage 3- | -0.8 | 0.23 |
| Stage 3- | -0.9 | 0.2 |
| Stage 3- | -1 | 0.17 |
| Stage 3- | -1.1 | 0.15 |
| Stage 3- | -1.2 | 0.13 |
| Stage 3- | -1.3 | 0.12 |
| Stage 3- | -1.4 | 0.11 |
| Stage 3- | -1.5 | 0.11 |
| Stage 3- | -1.6 | 0.12 |
| Stage 3- | -1.7 | 0.13 |
| Stage 3- | -1.8 | 0.15 |
| Stage 3- | -1.9 | 0.16 |
| Stage 3- | -2 | 0.18 |
| Stage 3- | -2.1 | 0.2 |
| Stage 3- | -2.2 | 0.23 |
| Stage 3- | -2.3 | 0.25 |
| Stage 3- | -2.4 | 0.28 |
| Stage 3- | -2.5 | 0.31 |
| Stage 3- | -2.6 | 0.33 |
| Stage 3- | -2.7 | 0.36 |
| Stage 3- | -2.8 | 0.39 |
| Stage 3- | -2.9 | 0.42 |
| Stage 3- | -3 | 0.45 |
| Stage 3- | -3.1 | 0.47 |
| Stage 3- | -3.2 | 0.5 |
| Stage 3- | -3.3 | 0.53 |
| Stage 3- | -3.4 | 0.55 |
| Stage 3- | -3.5 | 0.58 |
| Stage 3- | -3.6 | 0.6 |
| Stage 3- | -3.7 | 0.62 |
| Stage 3- | -3.8 | 0.64 |
| Stage 3- | -3.9 | 0.66 |
| Stage 3- | -4 | 0.68 |
| Stage 3- | -4.1 | 0.69 |
| Stage 3- | -4.2 | 0.7 |
| Stage 3- | -4.3 | 0.71 |
| Stage 3- | -4.4 | 0.71 |
| Stage 3- | -4.5 | 0.72 |
| Stage 3- | -4.6 | 0.72 |
| Stage 3- | -4.7 | 0.71 |
| Stage 3- | -4.8 | 0.71 |
| Stage 3- | -4.9 | 0.7 |
| Stage 3- | -5 | 0.69 |
| Stage 3- | -5.1 | 0.68 |
| Stage 3- | -5.2 | 0.66 |
| Stage 3- | -5.3 | 0.64 |
| Stage 3- | -5.4 | 0.63 |
| Stage 3- | -5.5 | 0.61 |
| Stage 3- | -5.6 | 0.59 |
| Stage 3- | -5.7 | 0.57 |
| Stage 3- | -5.8 | 0.55 |
| Stage 3- | -5.9 | 0.54 |
| Stage 3- | -6 | 0.52 |

| Design Assumption: Nominal Tipo Risultato: Spostamento | | Muro: LEFT |
|--|-------|------------------------------|
| Stage | Z (m) | Spostamento orizzontale (mm) |
| Stage 3- | -6.1 | 0.5 |
| Stage 3- | -6.2 | 0.49 |
| Stage 3- | -6.3 | 0.47 |
| Stage 3- | -6.4 | 0.46 |
| Stage 3- | -6.5 | 0.45 |
| Stage 3- | -6.6 | 0.44 |
| Stage 3- | -6.7 | 0.42 |
| Stage 3- | -6.8 | 0.42 |
| Stage 3- | -6.9 | 0.41 |
| Stage 3- | -7 | 0.4 |
| Stage 3- | -7.1 | 0.39 |
| Stage 3- | -7.2 | 0.39 |
| Stage 3- | -7.3 | 0.38 |
| Stage 3- | -7.4 | 0.38 |
| Stage 3- | -7.5 | 0.37 |
| Stage 3- | -7.6 | 0.37 |
| Stage 3- | -7.7 | 0.36 |
| Stage 3- | -7.8 | 0.36 |
| Stage 3- | -7.9 | 0.36 |
| Stage 3- | -8 | 0.35 |
| Stage 3- | -8.1 | 0.35 |
| Stage 3- | -8.2 | 0.35 |
| Stage 3- | -8.3 | 0.35 |
| Stage 3- | -8.4 | 0.34 |
| Stage 3- | -8.5 | 0.34 |
| Stage 3- | -8.6 | 0.34 |
| Stage 3- | -8.7 | 0.34 |
| Stage 3- | -8.8 | 0.34 |
| Stage 3- | -8.9 | 0.33 |
| Stage 3- | -9 | 0.33 |
| Stage 3- | -9.1 | 0.33 |
| Stage 3- | -9.2 | 0.33 |
| Stage 3- | -9.3 | 0.33 |
| Stage 3- | -9.4 | 0.32 |
| Stage 3- | -9.5 | 0.32 |
| Stage 3- | -9.6 | 0.32 |
| Stage 3- | -9.7 | 0.32 |
| Stage 3- | -9.8 | 0.32 |
| Stage 3- | -9.9 | 0.31 |
| Stage 3- | -10 | 0.31 |

Grafici Spostamento in tabella



Involuppi Spostamento Nominal

Risultati Paratia

Tabella Risultati Paratia Nominal - Stage: Stage 1

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 1 | 0 | 0 | 0 |
| Stage 1 | -0.1 | 0 | 0 |
| Stage 1 | -0.2 | 0 | 0 |
| Stage 1 | -0.3 | 0 | 0 |
| Stage 1 | -0.4 | 0 | 0 |
| Stage 1 | -0.5 | 0 | 0 |
| Stage 1 | -0.6 | 0 | 0 |
| Stage 1 | -0.7 | 0 | 0 |
| Stage 1 | -0.8 | 0 | 0 |
| Stage 1 | -0.9 | 0 | 0 |
| Stage 1 | -1 | 0 | 0 |
| Stage 1 | -1.1 | 0 | 0 |
| Stage 1 | -1.2 | 0 | 0 |
| Stage 1 | -1.3 | 0 | 0 |
| Stage 1 | -1.4 | 0 | 0 |
| Stage 1 | -1.5 | 0 | 0 |
| Stage 1 | -1.6 | 0 | 0 |
| Stage 1 | -1.7 | 0 | 0 |
| Stage 1 | -1.8 | 0 | 0 |
| Stage 1 | -1.9 | 0 | 0 |
| Stage 1 | -2 | 0 | 0 |
| Stage 1 | -2.1 | 0 | 0 |
| Stage 1 | -2.2 | 0 | 0 |
| Stage 1 | -2.3 | 0 | 0 |
| Stage 1 | -2.4 | 0 | 0 |
| Stage 1 | -2.5 | 0 | 0 |
| Stage 1 | -2.6 | 0 | 0 |
| Stage 1 | -2.7 | 0 | 0 |
| Stage 1 | -2.8 | 0 | 0 |
| Stage 1 | -2.9 | 0 | 0 |
| Stage 1 | -3 | 0 | 0 |
| Stage 1 | -3.1 | 0 | 0 |
| Stage 1 | -3.2 | 0 | 0 |
| Stage 1 | -3.3 | 0 | 0 |
| Stage 1 | -3.4 | 0 | 0 |
| Stage 1 | -3.5 | 0 | 0 |
| Stage 1 | -3.6 | 0 | 0 |
| Stage 1 | -3.7 | 0 | 0 |
| Stage 1 | -3.8 | 0 | 0 |
| Stage 1 | -3.9 | 0 | 0 |
| Stage 1 | -4 | 0 | 0 |
| Stage 1 | -4.1 | 0 | 0 |
| Stage 1 | -4.2 | 0 | 0 |
| Stage 1 | -4.3 | 0 | 0 |
| Stage 1 | -4.4 | 0 | 0 |
| Stage 1 | -4.5 | 0 | 0 |
| Stage 1 | -4.6 | 0 | 0 |
| Stage 1 | -4.7 | 0 | 0 |
| Stage 1 | -4.8 | 0 | 0 |
| Stage 1 | -4.9 | 0 | 0 |
| Stage 1 | -5 | 0 | 0 |
| Stage 1 | -5.1 | 0 | 0 |
| Stage 1 | -5.2 | 0 | 0 |
| Stage 1 | -5.3 | 0 | 0 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 1 | -5.4 | 0 | 0 |
| Stage 1 | -5.5 | 0 | 0 |
| Stage 1 | -5.6 | 0 | 0 |
| Stage 1 | -5.7 | 0 | 0 |
| Stage 1 | -5.8 | 0 | 0 |
| Stage 1 | -5.9 | 0 | 0 |
| Stage 1 | -6 | 0 | 0 |
| Stage 1 | -6.1 | 0 | 0 |
| Stage 1 | -6.2 | 0 | 0 |
| Stage 1 | -6.3 | 0 | 0 |
| Stage 1 | -6.4 | 0 | 0 |
| Stage 1 | -6.5 | 0 | 0 |
| Stage 1 | -6.6 | 0 | 0 |
| Stage 1 | -6.7 | 0 | 0 |
| Stage 1 | -6.8 | 0 | 0 |
| Stage 1 | -6.9 | 0 | 0 |
| Stage 1 | -7 | 0 | 0 |
| Stage 1 | -7.1 | 0 | 0 |
| Stage 1 | -7.2 | 0 | 0 |
| Stage 1 | -7.3 | 0 | 0 |
| Stage 1 | -7.4 | 0 | 0 |
| Stage 1 | -7.5 | 0 | 0 |
| Stage 1 | -7.6 | 0 | 0 |
| Stage 1 | -7.7 | 0 | 0 |
| Stage 1 | -7.8 | 0 | 0 |
| Stage 1 | -7.9 | 0 | 0 |
| Stage 1 | -8 | 0 | 0 |
| Stage 1 | -8.1 | 0 | 0 |
| Stage 1 | -8.2 | 0 | 0 |
| Stage 1 | -8.3 | 0 | 0 |
| Stage 1 | -8.4 | 0 | 0 |
| Stage 1 | -8.5 | 0 | 0 |
| Stage 1 | -8.6 | 0 | 0 |
| Stage 1 | -8.7 | 0 | 0 |
| Stage 1 | -8.8 | 0 | 0 |
| Stage 1 | -8.9 | 0 | 0 |
| Stage 1 | -9 | 0 | 0 |
| Stage 1 | -9.1 | 0 | 0 |
| Stage 1 | -9.2 | 0 | 0 |
| Stage 1 | -9.3 | 0 | 0 |
| Stage 1 | -9.4 | 0 | 0 |
| Stage 1 | -9.5 | 0 | 0 |
| Stage 1 | -9.6 | 0 | 0 |
| Stage 1 | -9.7 | 0 | 0 |
| Stage 1 | -9.8 | 0 | 0 |
| Stage 1 | -9.9 | 0 | 0 |
| Stage 1 | -10 | 0 | 0 |

Tabella Risultati Paratia Nominal - Stage: Stage 2

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 2 | 0 | 0 | 0 |
| Stage 2 | -0.1 | 0 | 0 |
| Stage 2 | -0.1 | 0 | 0 |
| Stage 2 | -0.2 | 0 | 0 |
| Stage 2 | -0.3 | 0 | 0 |
| Stage 2 | -0.4 | 0 | 0 |
| Stage 2 | -0.5 | 0 | 0 |
| Stage 2 | -0.6 | 0 | 0.01 |
| Stage 2 | -0.7 | 0 | 0.01 |
| Stage 2 | -0.8 | 0 | 0.02 |
| Stage 2 | -0.9 | 0.01 | 0.02 |
| Stage 2 | -1 | 0.01 | 0.03 |
| Stage 2 | -1.1 | 0.01 | 0.03 |
| Stage 2 | -1.2 | 0.01 | 0.03 |
| Stage 2 | -1.3 | 0.02 | 0.03 |
| Stage 2 | -1.4 | 0.02 | 0.02 |
| Stage 2 | -1.5 | 0.02 | 0.01 |
| Stage 2 | -1.6 | 0.02 | 0 |
| Stage 2 | -1.7 | 0.02 | -0.02 |
| Stage 2 | -1.8 | 0.01 | -0.04 |
| Stage 2 | -1.9 | 0.01 | -0.07 |
| Stage 2 | -2 | 0 | -0.1 |
| Stage 2 | -2.1 | -0.01 | -0.08 |
| Stage 2 | -2.2 | -0.02 | -0.06 |
| Stage 2 | -2.3 | -0.02 | -0.04 |
| Stage 2 | -2.4 | -0.03 | -0.03 |
| Stage 2 | -2.5 | -0.03 | -0.02 |
| Stage 2 | -2.6 | -0.03 | -0.01 |
| Stage 2 | -2.7 | -0.03 | 0 |
| Stage 2 | -2.8 | -0.03 | 0.01 |
| Stage 2 | -2.9 | -0.03 | 0.01 |
| Stage 2 | -3 | -0.02 | 0.02 |
| Stage 2 | -3.1 | -0.02 | 0.03 |
| Stage 2 | -3.2 | -0.02 | 0.04 |
| Stage 2 | -3.3 | -0.01 | 0.04 |
| Stage 2 | -3.4 | -0.01 | 0.05 |
| Stage 2 | -3.5 | 0 | 0.04 |
| Stage 2 | -3.6 | 0 | 0.04 |
| Stage 2 | -3.7 | 0 | 0.03 |
| Stage 2 | -3.8 | 0.01 | 0.03 |
| Stage 2 | -3.9 | 0.01 | 0.02 |
| Stage 2 | -4 | 0.01 | 0.02 |
| Stage 2 | -4.1 | 0.01 | 0.01 |
| Stage 2 | -4.2 | 0.01 | 0.01 |
| Stage 2 | -4.3 | 0.01 | 0.01 |
| Stage 2 | -4.4 | 0.01 | 0.01 |
| Stage 2 | -4.5 | 0.01 | 0 |
| Stage 2 | -4.6 | 0.01 | 0 |
| Stage 2 | -4.7 | 0.01 | 0 |
| Stage 2 | -4.8 | 0.01 | 0 |
| Stage 2 | -4.9 | 0.01 | 0 |
| Stage 2 | -5 | 0.01 | -0.01 |
| Stage 2 | -5.1 | 0.01 | -0.01 |
| Stage 2 | -5.2 | 0.01 | 0 |
| Stage 2 | -5.3 | 0.01 | -0.01 |
| Stage 2 | -5.4 | 0.01 | 0 |
| Stage 2 | -5.5 | 0.01 | -0.01 |
| Stage 2 | -5.6 | 0.01 | -0.01 |
| Stage 2 | -5.7 | 0.01 | -0.01 |
| Stage 2 | -5.8 | 0.01 | -0.01 |
| Stage 2 | -5.9 | 0.01 | -0.01 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 2 | -6 | 0.01 | 0 |
| Stage 2 | -6.1 | 0.01 | 0 |
| Stage 2 | -6.2 | 0 | 0 |
| Stage 2 | -6.3 | 0 | 0 |
| Stage 2 | -6.4 | 0 | 0 |
| Stage 2 | -6.5 | 0 | 0 |
| Stage 2 | -6.6 | 0 | 0 |
| Stage 2 | -6.7 | 0 | 0 |
| Stage 2 | -6.8 | 0 | 0 |
| Stage 2 | -6.9 | 0 | 0 |
| Stage 2 | -7 | 0 | 0 |
| Stage 2 | -7.1 | 0 | 0 |
| Stage 2 | -7.2 | 0 | 0 |
| Stage 2 | -7.3 | 0 | 0 |
| Stage 2 | -7.4 | 0 | 0 |
| Stage 2 | -7.5 | 0 | 0 |
| Stage 2 | -7.6 | 0 | 0 |
| Stage 2 | -7.7 | 0 | 0 |
| Stage 2 | -7.8 | 0 | 0 |
| Stage 2 | -7.9 | 0 | 0 |
| Stage 2 | -8 | 0 | 0 |
| Stage 2 | -8.1 | 0 | 0 |
| Stage 2 | -8.2 | 0 | 0 |
| Stage 2 | -8.3 | 0 | 0.01 |
| Stage 2 | -8.4 | 0 | 0.01 |
| Stage 2 | -8.5 | 0.01 | 0.01 |
| Stage 2 | -8.6 | 0.01 | 0.01 |
| Stage 2 | -8.7 | 0.01 | 0.01 |
| Stage 2 | -8.8 | 0.01 | 0.01 |
| Stage 2 | -8.9 | 0.01 | 0.01 |
| Stage 2 | -9 | 0.01 | 0.01 |
| Stage 2 | -9.1 | 0.01 | 0 |
| Stage 2 | -9.2 | 0.01 | 0 |
| Stage 2 | -9.3 | 0.01 | 0 |
| Stage 2 | -9.4 | 0.01 | -0.01 |
| Stage 2 | -9.5 | 0.01 | -0.01 |
| Stage 2 | -9.6 | 0.01 | -0.02 |
| Stage 2 | -9.7 | 0 | -0.02 |
| Stage 2 | -9.8 | 0 | -0.02 |
| Stage 2 | -9.9 | 0 | -0.01 |
| Stage 2 | -10 | 0 | -0.01 |

Tabella Risultati Paratia Nominal - Stage: Stage A

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage A | 0 | 0 | 0 |
| Stage A | -0.1 | 0 | 0 |
| Stage A | -0.1 | 0 | 0 |
| Stage A | -0.2 | -0.01 | -0.06 |
| Stage A | -0.3 | -0.02 | -0.18 |
| Stage A | -0.4 | -0.06 | -0.37 |
| Stage A | -0.5 | -0.12 | -0.61 |
| Stage A | -0.6 | -0.21 | -0.91 |
| Stage A | -0.7 | -0.34 | -1.28 |
| Stage A | -0.8 | -0.51 | -1.71 |
| Stage A | -0.9 | -0.73 | -2.2 |
| Stage A | -1 | -1.01 | -2.76 |
| Stage A | -1.1 | -1.35 | -3.37 |
| Stage A | -1.2 | -1.75 | -4.05 |
| Stage A | -1.3 | -2.23 | -4.8 |
| Stage A | -1.4 | -2.79 | -5.6 |
| Stage A | -1.5 | -3.44 | -6.48 |
| Stage A | -1.6 | -4.18 | -7.41 |
| Stage A | -1.7 | -4.96 | -7.82 |
| Stage A | -1.8 | -5.73 | -7.71 |
| Stage A | -1.9 | -6.44 | -7.11 |
| Stage A | -2 | -7.1 | -6.58 |
| Stage A | -2.1 | -7.5 | -4.02 |
| Stage A | -2.2 | -7.66 | -1.54 |
| Stage A | -2.3 | -7.57 | 0.88 |
| Stage A | -2.4 | -7.24 | 3.27 |
| Stage A | -2.5 | -6.74 | 5.06 |
| Stage A | -2.6 | -6.11 | 6.22 |
| Stage A | -2.7 | -5.43 | 6.86 |
| Stage A | -2.8 | -4.72 | 7.1 |
| Stage A | -2.9 | -4.02 | 7.02 |
| Stage A | -3 | -3.35 | 6.71 |
| Stage A | -3.1 | -2.72 | 6.24 |
| Stage A | -3.2 | -2.16 | 5.66 |
| Stage A | -3.3 | -1.66 | 5.02 |
| Stage A | -3.4 | -1.22 | 4.37 |
| Stage A | -3.5 | -0.85 | 3.71 |
| Stage A | -3.6 | -0.54 | 3.09 |
| Stage A | -3.7 | -0.29 | 2.51 |
| Stage A | -3.8 | -0.09 | 1.98 |
| Stage A | -3.9 | 0.06 | 1.52 |
| Stage A | -4 | 0.17 | 1.12 |
| Stage A | -4.1 | 0.25 | 0.77 |
| Stage A | -4.2 | 0.3 | 0.49 |
| Stage A | -4.3 | 0.33 | 0.26 |
| Stage A | -4.4 | 0.34 | 0.08 |
| Stage A | -4.5 | 0.33 | -0.06 |
| Stage A | -4.6 | 0.31 | -0.16 |
| Stage A | -4.7 | 0.29 | -0.23 |
| Stage A | -4.8 | 0.26 | -0.28 |
| Stage A | -4.9 | 0.23 | -0.3 |
| Stage A | -5 | 0.2 | -0.31 |
| Stage A | -5.1 | 0.17 | -0.3 |
| Stage A | -5.2 | 0.14 | -0.28 |
| Stage A | -5.3 | 0.12 | -0.26 |
| Stage A | -5.4 | 0.09 | -0.24 |
| Stage A | -5.5 | 0.07 | -0.21 |
| Stage A | -5.6 | 0.05 | -0.18 |
| Stage A | -5.7 | 0.04 | -0.15 |
| Stage A | -5.8 | 0.02 | -0.13 |
| Stage A | -5.9 | 0.01 | -0.1 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage A | -6 | 0.01 | -0.08 |
| Stage A | -6.1 | 0 | -0.06 |
| Stage A | -6.2 | 0 | -0.04 |
| Stage A | -6.3 | -0.01 | -0.03 |
| Stage A | -6.4 | -0.01 | -0.02 |
| Stage A | -6.5 | -0.01 | -0.01 |
| Stage A | -6.6 | -0.01 | 0 |
| Stage A | -6.7 | -0.01 | 0 |
| Stage A | -6.8 | -0.01 | 0.01 |
| Stage A | -6.9 | -0.01 | 0.01 |
| Stage A | -7 | -0.01 | 0.01 |
| Stage A | -7.1 | -0.01 | 0.01 |
| Stage A | -7.2 | -0.01 | 0.01 |
| Stage A | -7.3 | 0 | 0.01 |
| Stage A | -7.4 | 0 | 0.01 |
| Stage A | -7.5 | 0 | 0.01 |
| Stage A | -7.6 | 0 | 0.01 |
| Stage A | -7.7 | 0 | 0.01 |
| Stage A | -7.8 | 0 | 0.01 |
| Stage A | -7.9 | 0 | 0.01 |
| Stage A | -8 | 0 | 0.01 |
| Stage A | -8.1 | 0 | 0.01 |
| Stage A | -8.2 | 0 | 0.01 |
| Stage A | -8.3 | 0 | 0.01 |
| Stage A | -8.4 | 0 | 0.01 |
| Stage A | -8.5 | 0.01 | 0.01 |
| Stage A | -8.6 | 0.01 | 0.01 |
| Stage A | -8.7 | 0.01 | 0.01 |
| Stage A | -8.8 | 0.01 | 0.01 |
| Stage A | -8.9 | 0.01 | 0.01 |
| Stage A | -9 | 0.01 | 0.01 |
| Stage A | -9.1 | 0.01 | 0 |
| Stage A | -9.2 | 0.01 | 0 |
| Stage A | -9.3 | 0.01 | 0 |
| Stage A | -9.4 | 0.01 | -0.01 |
| Stage A | -9.5 | 0.01 | -0.01 |
| Stage A | -9.6 | 0.01 | -0.02 |
| Stage A | -9.7 | 0 | -0.02 |
| Stage A | -9.8 | 0 | -0.02 |
| Stage A | -9.9 | 0 | -0.01 |
| Stage A | -10 | 0 | -0.01 |

Tabella Risultati Paratia Nominal - Stage: Stage B

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage B | 0 | 0 | 0 |
| Stage B | -0.1 | 0 | 0 |
| Stage B | -0.1 | 0 | 0 |
| Stage B | -0.2 | -0.06 | -0.59 |
| Stage B | -0.3 | -0.24 | -1.77 |
| Stage B | -0.4 | -0.59 | -3.54 |
| Stage B | -0.5 | -1.17 | -5.81 |
| Stage B | -0.6 | -1.99 | -8.16 |
| Stage B | -0.7 | -3.05 | -10.61 |
| Stage B | -0.8 | -4.36 | -13.13 |
| Stage B | -0.9 | -5.93 | -15.74 |
| Stage B | -1 | -7.77 | -18.41 |
| Stage B | -1.1 | -9.89 | -21.14 |
| Stage B | -1.2 | -12.28 | -23.91 |
| Stage B | -1.3 | -14.95 | -26.7 |
| Stage B | -1.4 | -12.5 | 24.54 |
| Stage B | -1.5 | -10.32 | 21.78 |
| Stage B | -1.6 | -8.41 | 19.07 |
| Stage B | -1.7 | -6.76 | 16.48 |
| Stage B | -1.8 | -5.36 | 14.04 |
| Stage B | -1.9 | -4.13 | 12.31 |
| Stage B | -2 | -3.05 | 10.78 |
| Stage B | -2.1 | -2.25 | 8 |
| Stage B | -2.2 | -1.66 | 5.91 |
| Stage B | -2.3 | -1.21 | 4.46 |
| Stage B | -2.4 | -0.85 | 3.63 |
| Stage B | -2.5 | -0.55 | 3 |
| Stage B | -2.6 | -0.31 | 2.43 |
| Stage B | -2.7 | -0.11 | 1.91 |
| Stage B | -2.8 | 0.03 | 1.46 |
| Stage B | -2.9 | 0.14 | 1.07 |
| Stage B | -3 | 0.21 | 0.75 |
| Stage B | -3.1 | 0.26 | 0.48 |
| Stage B | -3.2 | 0.29 | 0.27 |
| Stage B | -3.3 | 0.3 | 0.1 |
| Stage B | -3.4 | 0.3 | -0.03 |
| Stage B | -3.5 | 0.28 | -0.13 |
| Stage B | -3.6 | 0.26 | -0.19 |
| Stage B | -3.7 | 0.24 | -0.24 |
| Stage B | -3.8 | 0.21 | -0.26 |
| Stage B | -3.9 | 0.19 | -0.27 |
| Stage B | -4 | 0.16 | -0.27 |
| Stage B | -4.1 | 0.13 | -0.26 |
| Stage B | -4.2 | 0.11 | -0.24 |
| Stage B | -4.3 | 0.09 | -0.21 |
| Stage B | -4.4 | 0.07 | -0.19 |
| Stage B | -4.5 | 0.05 | -0.17 |
| Stage B | -4.6 | 0.04 | -0.14 |
| Stage B | -4.7 | 0.03 | -0.12 |
| Stage B | -4.8 | 0.02 | -0.1 |
| Stage B | -4.9 | 0.01 | -0.07 |
| Stage B | -5 | 0 | -0.06 |
| Stage B | -5.1 | 0 | -0.04 |
| Stage B | -5.2 | 0 | -0.03 |
| Stage B | -5.3 | -0.01 | -0.02 |
| Stage B | -5.4 | -0.01 | -0.01 |
| Stage B | -5.5 | -0.01 | -0.01 |
| Stage B | -5.6 | -0.01 | 0 |
| Stage B | -5.7 | -0.01 | 0 |
| Stage B | -5.8 | -0.01 | 0 |
| Stage B | -5.9 | -0.01 | 0.01 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage B | -6 | 0 | 0.01 |
| Stage B | -6.1 | 0 | 0.01 |
| Stage B | -6.2 | 0 | 0.01 |
| Stage B | -6.3 | 0 | 0.01 |
| Stage B | -6.4 | 0 | 0.01 |
| Stage B | -6.5 | 0 | 0.01 |
| Stage B | -6.6 | 0 | 0.01 |
| Stage B | -6.7 | 0 | 0.01 |
| Stage B | -6.8 | 0 | 0 |
| Stage B | -6.9 | 0 | 0 |
| Stage B | -7 | 0 | 0 |
| Stage B | -7.1 | 0 | 0 |
| Stage B | -7.2 | 0 | 0 |
| Stage B | -7.3 | 0 | 0 |
| Stage B | -7.4 | 0 | 0 |
| Stage B | -7.5 | 0 | 0 |
| Stage B | -7.6 | 0 | 0 |
| Stage B | -7.7 | 0 | 0 |
| Stage B | -7.8 | 0 | 0 |
| Stage B | -7.9 | 0 | 0 |
| Stage B | -8 | 0 | 0 |
| Stage B | -8.1 | 0 | 0 |
| Stage B | -8.2 | 0 | 0 |
| Stage B | -8.3 | 0 | 0.01 |
| Stage B | -8.4 | 0 | 0.01 |
| Stage B | -8.5 | 0.01 | 0.01 |
| Stage B | -8.6 | 0.01 | 0.01 |
| Stage B | -8.7 | 0.01 | 0.01 |
| Stage B | -8.8 | 0.01 | 0.01 |
| Stage B | -8.9 | 0.01 | 0.01 |
| Stage B | -9 | 0.01 | 0.01 |
| Stage B | -9.1 | 0.01 | 0 |
| Stage B | -9.2 | 0.01 | 0 |
| Stage B | -9.3 | 0.01 | 0 |
| Stage B | -9.4 | 0.01 | -0.01 |
| Stage B | -9.5 | 0.01 | -0.01 |
| Stage B | -9.6 | 0.01 | -0.02 |
| Stage B | -9.7 | 0 | -0.02 |
| Stage B | -9.8 | 0 | -0.02 |
| Stage B | -9.9 | 0 | -0.01 |
| Stage B | -10 | 0 | -0.01 |

Tabella Risultati Paratia Nominal - Stage: Stage 3-

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 3- | 0 | 0 | 0 |
| Stage 3- | -0.1 | 0 | 0 |
| Stage 3- | -0.1 | 0 | 0 |
| Stage 3- | -0.2 | -0.06 | -0.59 |
| Stage 3- | -0.3 | -0.24 | -1.77 |
| Stage 3- | -0.4 | -0.59 | -3.54 |
| Stage 3- | -0.5 | -1.18 | -5.9 |
| Stage 3- | -0.6 | -2.03 | -8.46 |
| Stage 3- | -0.7 | -3.13 | -11.07 |
| Stage 3- | -0.8 | -4.51 | -13.75 |
| Stage 3- | -0.9 | -6.15 | -16.46 |
| Stage 3- | -1 | -8.08 | -19.22 |
| Stage 3- | -1.1 | -10.28 | -22.01 |
| Stage 3- | -1.2 | -12.76 | -24.81 |
| Stage 3- | -1.3 | -15.52 | -27.6 |
| Stage 3- | -1.4 | -13.15 | 23.7 |
| Stage 3- | -1.5 | -11.04 | 21.04 |
| Stage 3- | -1.6 | -9.2 | 18.47 |
| Stage 3- | -1.7 | -7.6 | 16.01 |
| Stage 3- | -1.8 | -6.23 | 13.69 |
| Stage 3- | -1.9 | -5.08 | 11.49 |
| Stage 3- | -2 | -4.14 | 9.43 |
| Stage 3- | -2.1 | -3.41 | 7.31 |
| Stage 3- | -2.2 | -2.83 | 5.8 |
| Stage 3- | -2.3 | -2.34 | 4.88 |
| Stage 3- | -2.4 | -1.88 | 4.53 |
| Stage 3- | -2.5 | -1.45 | 4.38 |
| Stage 3- | -2.6 | -1.01 | 4.33 |
| Stage 3- | -2.7 | -0.58 | 4.33 |
| Stage 3- | -2.8 | -0.15 | 4.33 |
| Stage 3- | -2.9 | 0.29 | 4.33 |
| Stage 3- | -3 | 0.72 | 4.33 |
| Stage 3- | -3.1 | 1.15 | 4.33 |
| Stage 3- | -3.2 | 1.59 | 4.33 |
| Stage 3- | -3.3 | 2.02 | 4.33 |
| Stage 3- | -3.4 | 2.45 | 4.33 |
| Stage 3- | -3.5 | 2.88 | 4.33 |
| Stage 3- | -3.6 | 3.32 | 4.33 |
| Stage 3- | -3.7 | 3.74 | 4.25 |
| Stage 3- | -3.8 | 4.15 | 4.08 |
| Stage 3- | -3.9 | 4.53 | 3.83 |
| Stage 3- | -4 | 4.88 | 3.49 |
| Stage 3- | -4.1 | 5.19 | 3.07 |
| Stage 3- | -4.2 | 5.45 | 2.57 |
| Stage 3- | -4.3 | 5.64 | 1.98 |
| Stage 3- | -4.4 | 5.78 | 1.31 |
| Stage 3- | -4.5 | 5.83 | 0.55 |
| Stage 3- | -4.6 | 5.8 | -0.28 |
| Stage 3- | -4.7 | 5.68 | -1.21 |
| Stage 3- | -4.8 | 5.46 | -2.21 |
| Stage 3- | -4.9 | 5.13 | -3.31 |
| Stage 3- | -5 | 4.68 | -4.48 |
| Stage 3- | -5.1 | 4.11 | -5.74 |
| Stage 3- | -5.2 | 3.4 | -7.08 |
| Stage 3- | -5.3 | 2.55 | -8.51 |
| Stage 3- | -5.4 | 1.55 | -10.02 |
| Stage 3- | -5.5 | 0.68 | -8.65 |
| Stage 3- | -5.6 | -0.05 | -7.29 |
| Stage 3- | -5.7 | -0.65 | -6.01 |
| Stage 3- | -5.8 | -1.13 | -4.82 |
| Stage 3- | -5.9 | -1.51 | -3.75 |

| Design Assumption: Nominal Risultati Paratia | | Muro: LEFT | |
|--|-------|------------------|---------------|
| Stage | Z (m) | Momento (kN*m/m) | Taglio (kN/m) |
| Stage 3- | -6 | -1.78 | -2.78 |
| Stage 3- | -6.1 | -1.98 | -1.94 |
| Stage 3- | -6.2 | -2.1 | -1.21 |
| Stage 3- | -6.3 | -2.16 | -0.6 |
| Stage 3- | -6.4 | -2.17 | -0.08 |
| Stage 3- | -6.5 | -2.13 | 0.35 |
| Stage 3- | -6.6 | -2.06 | 0.68 |
| Stage 3- | -6.7 | -1.97 | 0.95 |
| Stage 3- | -6.8 | -1.86 | 1.14 |
| Stage 3- | -6.9 | -1.73 | 1.27 |
| Stage 3- | -7 | -1.59 | 1.36 |
| Stage 3- | -7.1 | -1.45 | 1.4 |
| Stage 3- | -7.2 | -1.31 | 1.41 |
| Stage 3- | -7.3 | -1.17 | 1.38 |
| Stage 3- | -7.4 | -1.04 | 1.34 |
| Stage 3- | -7.5 | -0.91 | 1.28 |
| Stage 3- | -7.6 | -0.79 | 1.2 |
| Stage 3- | -7.7 | -0.68 | 1.11 |
| Stage 3- | -7.8 | -0.58 | 1.02 |
| Stage 3- | -7.9 | -0.49 | 0.93 |
| Stage 3- | -8 | -0.4 | 0.83 |
| Stage 3- | -8.1 | -0.33 | 0.74 |
| Stage 3- | -8.2 | -0.26 | 0.65 |
| Stage 3- | -8.3 | -0.21 | 0.56 |
| Stage 3- | -8.4 | -0.16 | 0.48 |
| Stage 3- | -8.5 | -0.12 | 0.41 |
| Stage 3- | -8.6 | -0.08 | 0.34 |
| Stage 3- | -8.7 | -0.06 | 0.28 |
| Stage 3- | -8.8 | -0.03 | 0.22 |
| Stage 3- | -8.9 | -0.02 | 0.17 |
| Stage 3- | -9 | 0 | 0.13 |
| Stage 3- | -9.1 | 0.01 | 0.09 |
| Stage 3- | -9.2 | 0.01 | 0.06 |
| Stage 3- | -9.3 | 0.01 | 0.03 |
| Stage 3- | -9.4 | 0.01 | 0.01 |
| Stage 3- | -9.5 | 0.01 | -0.01 |
| Stage 3- | -9.6 | 0.01 | -0.03 |
| Stage 3- | -9.7 | 0.01 | -0.03 |
| Stage 3- | -9.8 | 0 | -0.03 |
| Stage 3- | -9.9 | 0 | -0.03 |
| Stage 3- | -10 | 0 | -0.01 |

Grafico Momento Nominal

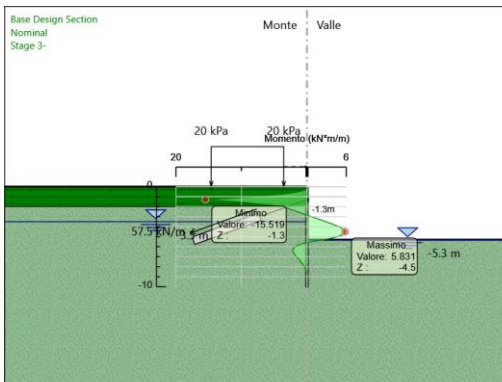
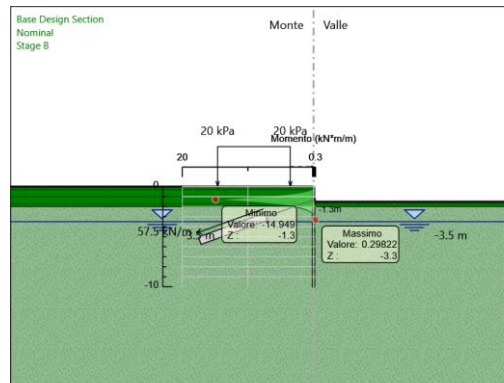
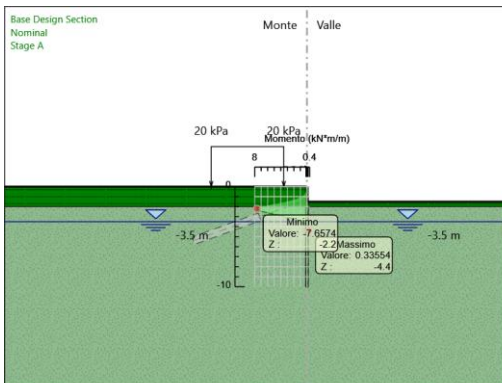
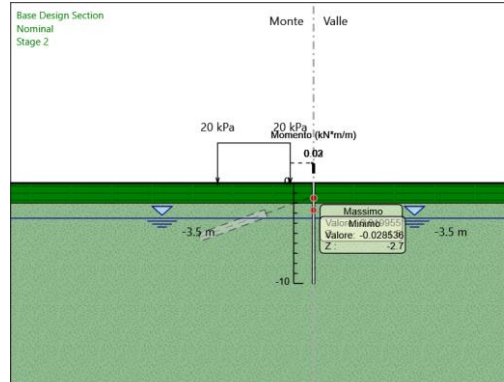
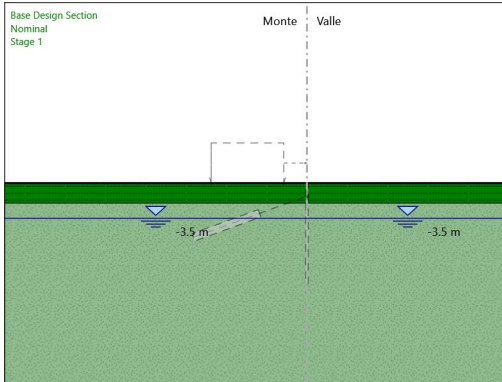
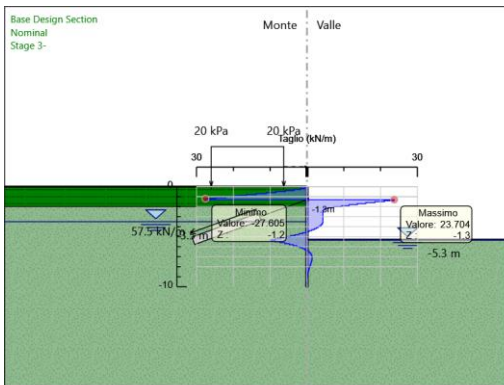
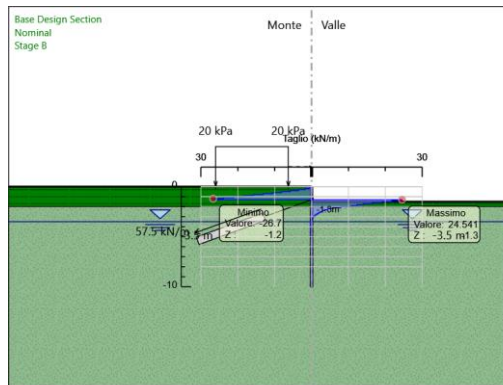
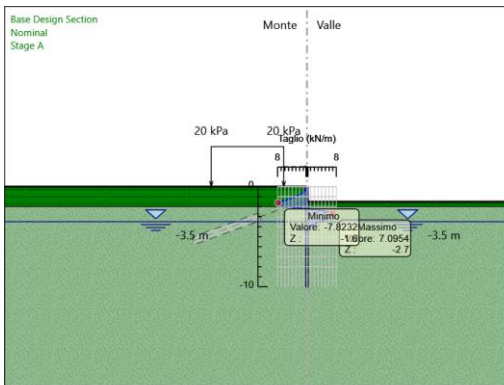
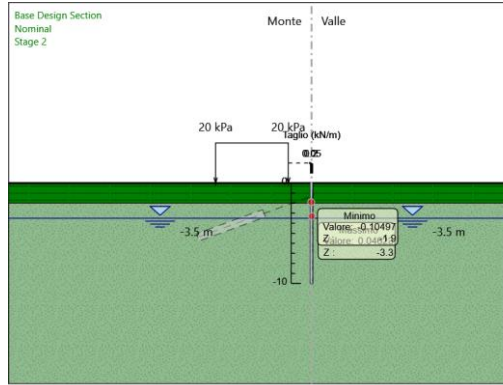
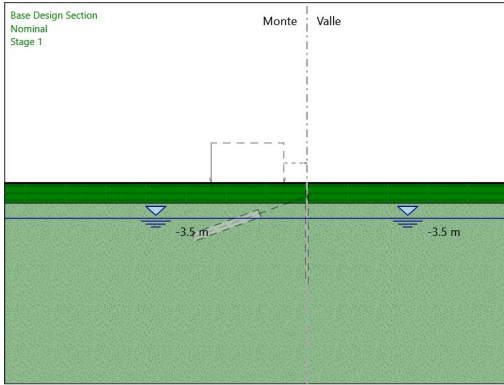


Grafico Taglio Nominal



Inviluppi Risultati Paratia Nominal

Risultati Elementi strutturali

| Design Assumption: Nominal Sollecitazione Tieback_New_New_New_New | |
|--|---------------------|
| Stage | Forza (kN/m) |
| Stage B | 57.5 |
| Stage 3- | 57.52275 |

Risultati Terreno

Tabella Risultati Terreno Left Wall - Nominal - Stage 1

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|---------------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | LEFT Ka | Lato Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 1 | 0 | 0 | 0 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage 1 | -0.1 | 1.9 | 0.95 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.95 |
| Stage 1 | -0.2 | 3.8 | 1.9 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.9 |
| Stage 1 | -0.3 | 5.7 | 2.85 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.85 |
| Stage 1 | -0.4 | 7.6 | 3.8 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.8 |
| Stage 1 | -0.5 | 9.5 | 4.75 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.75 |
| Stage 1 | -0.6 | 11.4 | 5.7 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.7 |
| Stage 1 | -0.7 | 13.3 | 6.65 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.65 |
| Stage 1 | -0.8 | 15.2 | 7.6 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.6 |
| Stage 1 | -0.9 | 17.1 | 8.55 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.55 |
| Stage 1 | -1 | 19 | 9.5 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.5 |
| Stage 1 | -1.1 | 20.9 | 10.45 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.45 |
| Stage 1 | -1.2 | 22.8 | 11.4 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.4 |
| Stage 1 | -1.3 | 24.7 | 12.35 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 12.35 |
| Stage 1 | -1.4 | 26.6 | 13.3 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 13.3 |
| Stage 1 | -1.5 | 28.5 | 14.25 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 14.25 |
| Stage 1 | -1.6 | 30.4 | 15.2 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 15.2 |
| Stage 1 | -1.7 | 32.3 | 16.15 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 16.15 |
| Stage 1 | -1.8 | 34.2 | 17.1 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.1 |
| Stage 1 | -1.9 | 36.1 | 18.05 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 18.05 |
| Stage 1 | -2 | 38 | 19 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 19 |
| Stage 1 | -2.1 | 40.45 | 20.225 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 20.225 |
| Stage 1 | -2.2 | 42.9 | 21.45 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 21.45 |
| Stage 1 | -2.3 | 45.35 | 22.675 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 22.675 |
| Stage 1 | -2.4 | 47.8 | 23.9 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 23.9 |
| Stage 1 | -2.5 | 50.25 | 25.125 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 25.125 |
| Stage 1 | -2.6 | 52.7 | 26.35 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 26.35 |
| Stage 1 | -2.7 | 55.15 | 27.575 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 27.575 |
| Stage 1 | -2.8 | 57.6 | 28.8 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 28.8 |
| Stage 1 | -2.9 | 60.05 | 30.025 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 30.025 |
| Stage 1 | -3 | 62.5 | 31.25 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 31.25 |
| Stage 1 | -3.1 | 64.95 | 32.475 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 32.475 |
| Stage 1 | -3.2 | 67.4 | 33.7 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 33.7 |
| Stage 1 | -3.3 | 69.85 | 34.925 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 34.925 |
| Stage 1 | -3.4 | 72.3 | 36.15 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 36.15 |
| Stage 1 | -3.5 | 74.75 | 37.375 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 37.375 |
| Stage 1 | -3.6 | 76.2 | 38.1 | V-C | 0.2174.599 | | 40 | 1 | 0 | 0 | 39.1 |
| Stage 1 | -3.7 | 77.65 | 38.825 | V-C | 0.2174.599 | | 40 | 2 | 0 | 0 | 40.825 |
| Stage 1 | -3.8 | 79.1 | 39.55 | V-C | 0.2174.599 | | 40 | 3 | 0 | 0 | 42.55 |
| Stage 1 | -3.9 | 80.55 | 40.275 | V-C | 0.2174.599 | | 40 | 4 | 0 | 0 | 44.275 |
| Stage 1 | -4 | 82 | 41 | V-C | 0.2174.599 | | 40 | 5 | 0 | 0 | 46 |
| Stage 1 | -4.1 | 83.45 | 41.725 | V-C | 0.2174.599 | | 40 | 6 | 0 | 0 | 47.725 |
| Stage 1 | -4.2 | 84.9 | 42.45 | V-C | 0.2174.599 | | 40 | 7 | 0 | 0 | 49.45 |
| Stage 1 | -4.3 | 86.35 | 43.175 | V-C | 0.2174.599 | | 40 | 8 | 0 | 0 | 51.175 |
| Stage 1 | -4.4 | 87.8 | 43.9 | V-C | 0.2174.599 | | 40 | 9 | 0 | 0 | 52.9 |
| Stage 1 | -4.5 | 89.25 | 44.625 | V-C | 0.2174.599 | | 40 | 10 | 0 | 0 | 54.625 |
| Stage 1 | -4.6 | 90.7 | 45.35 | V-C | 0.2174.599 | | 40 | 11 | 0 | 0 | 56.35 |
| Stage 1 | -4.7 | 92.15 | 46.075 | V-C | 0.2174.599 | | 40 | 12 | 0 | 0 | 58.075 |
| Stage 1 | -4.8 | 93.6 | 46.8 | V-C | 0.2174.599 | | 40 | 13 | 0 | 0 | 59.8 |
| Stage 1 | -4.9 | 95.05 | 47.525 | V-C | 0.2174.599 | | 40 | 14 | 0 | 0 | 61.525 |
| Stage 1 | -5 | 96.5 | 48.25 | V-C | 0.2174.599 | | 40 | 15 | 0 | 0 | 63.25 |
| Stage 1 | -5.1 | 97.95 | 48.975 | V-C | 0.2174.599 | | 40 | 16 | 0 | 0 | 64.975 |
| Stage 1 | -5.2 | 99.4 | 49.7 | V-C | 0.2174.599 | | 40 | 17 | 0 | 0 | 66.7 |
| Stage 1 | -5.3 | 100.85 | 50.425 | V-C | 0.2174.599 | | 40 | 18 | 0 | 0 | 68.425 |
| Stage 1 | -5.4 | 102.3 | 51.15 | V-C | 0.2174.599 | | 40 | 19 | 0 | 0 | 70.15 |
| Stage 1 | -5.5 | 103.75 | 51.875 | V-C | 0.2174.599 | | 40 | 20 | 0 | 0 | 71.875 |
| Stage 1 | -5.6 | 105.2 | 52.6 | V-C | 0.2174.599 | | 40 | 21 | 0 | 0 | 73.6 |
| Stage 1 | -5.7 | 106.65 | 53.325 | V-C | 0.2174.599 | | 40 | 22 | 0 | 0 | 75.325 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|---------------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | LEFT Ka | Lato Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage 1 | -5.8 | 108.1 | 54.05 | V-C | 0.2174.599 | 40 | 23 | 0 | 0 | 77.05 |
| Stage 1 | -5.9 | 109.55 | 54.775 | V-C | 0.2174.599 | 40 | 24 | 0 | 0 | 78.775 |
| Stage 1 | -6 | 111 | 55.5 | V-C | 0.2174.599 | 40 | 25 | 0 | 0 | 80.5 |
| Stage 1 | -6.1 | 112.45 | 56.225 | V-C | 0.2174.599 | 40 | 26 | 0 | 0 | 82.225 |
| Stage 1 | -6.2 | 113.9 | 56.95 | V-C | 0.2174.599 | 40 | 27 | 0 | 0 | 83.95 |
| Stage 1 | -6.3 | 115.35 | 57.675 | V-C | 0.2174.599 | 40 | 28 | 0 | 0 | 85.675 |
| Stage 1 | -6.4 | 116.8 | 58.4 | V-C | 0.2174.599 | 40 | 29 | 0 | 0 | 87.4 |
| Stage 1 | -6.5 | 118.25 | 59.125 | V-C | 0.2174.599 | 40 | 30 | 0 | 0 | 89.125 |
| Stage 1 | -6.6 | 119.7 | 59.85 | V-C | 0.2174.599 | 40 | 31 | 0 | 0 | 90.85 |
| Stage 1 | -6.7 | 121.15 | 60.575 | V-C | 0.2174.599 | 40 | 32 | 0 | 0 | 92.575 |
| Stage 1 | -6.8 | 122.6 | 61.3 | V-C | 0.2174.599 | 40 | 33 | 0 | 0 | 94.3 |
| Stage 1 | -6.9 | 124.05 | 62.025 | V-C | 0.2174.599 | 40 | 34 | 0 | 0 | 96.025 |
| Stage 1 | -7 | 125.5 | 62.75 | V-C | 0.2174.599 | 40 | 35 | 0 | 0 | 97.75 |
| Stage 1 | -7.1 | 126.95 | 63.475 | V-C | 0.2174.599 | 40 | 36 | 0 | 0 | 99.475 |
| Stage 1 | -7.2 | 128.4 | 64.2 | V-C | 0.2174.599 | 40 | 37 | 0 | 0 | 101.2 |
| Stage 1 | -7.3 | 129.85 | 64.925 | V-C | 0.2174.599 | 40 | 38 | 0 | 0 | 102.925 |
| Stage 1 | -7.4 | 131.3 | 65.65 | V-C | 0.2174.599 | 40 | 39 | 0 | 0 | 104.65 |
| Stage 1 | -7.5 | 132.75 | 66.375 | V-C | 0.2174.599 | 40 | 40 | 0 | 0 | 106.375 |
| Stage 1 | -7.6 | 134.2 | 67.1 | V-C | 0.2174.599 | 40 | 41 | 0 | 0 | 108.1 |
| Stage 1 | -7.7 | 135.65 | 67.825 | V-C | 0.2174.599 | 40 | 42 | 0 | 0 | 109.825 |
| Stage 1 | -7.8 | 137.1 | 68.55 | V-C | 0.2174.599 | 40 | 43 | 0 | 0 | 111.55 |
| Stage 1 | -7.9 | 138.55 | 69.275 | V-C | 0.2174.599 | 40 | 44 | 0 | 0 | 113.275 |
| Stage 1 | -8 | 140 | 70 | V-C | 0.2174.599 | 40 | 45 | 0 | 0 | 115 |
| Stage 1 | -8.1 | 141.45 | 70.725 | V-C | 0.2174.599 | 40 | 46 | 0 | 0 | 116.725 |
| Stage 1 | -8.2 | 142.9 | 71.45 | V-C | 0.2174.599 | 40 | 47 | 0 | 0 | 118.45 |
| Stage 1 | -8.3 | 144.35 | 72.175 | V-C | 0.2174.599 | 40 | 48 | 0 | 0 | 120.175 |
| Stage 1 | -8.4 | 145.8 | 72.9 | V-C | 0.2174.599 | 40 | 49 | 0 | 0 | 121.9 |
| Stage 1 | -8.5 | 147.25 | 73.625 | V-C | 0.2174.599 | 40 | 50 | 0 | 0 | 123.625 |
| Stage 1 | -8.6 | 148.7 | 74.35 | V-C | 0.2174.599 | 40 | 51 | 0 | 0 | 125.35 |
| Stage 1 | -8.7 | 150.15 | 75.075 | V-C | 0.2174.599 | 40 | 52 | 0 | 0 | 127.075 |
| Stage 1 | -8.8 | 151.6 | 75.8 | V-C | 0.2174.599 | 40 | 53 | 0 | 0 | 128.8 |
| Stage 1 | -8.9 | 153.05 | 76.525 | V-C | 0.2174.599 | 40 | 54 | 0 | 0 | 130.525 |
| Stage 1 | -9 | 154.5 | 77.25 | V-C | 0.2174.599 | 40 | 55 | 0 | 0 | 132.25 |
| Stage 1 | -9.1 | 155.95 | 77.975 | V-C | 0.2174.599 | 40 | 56 | 0 | 0 | 133.975 |
| Stage 1 | -9.2 | 157.4 | 78.7 | V-C | 0.2174.599 | 40 | 57 | 0 | 0 | 135.7 |
| Stage 1 | -9.3 | 158.85 | 79.425 | V-C | 0.2174.599 | 40 | 58 | 0 | 0 | 137.425 |
| Stage 1 | -9.4 | 160.3 | 80.15 | V-C | 0.2174.599 | 40 | 59 | 0 | 0 | 139.15 |
| Stage 1 | -9.5 | 161.75 | 80.875 | V-C | 0.2174.599 | 40 | 60 | 0 | 0 | 140.875 |
| Stage 1 | -9.6 | 163.2 | 81.6 | V-C | 0.2174.599 | 40 | 61 | 0 | 0 | 142.6 |
| Stage 1 | -9.7 | 164.65 | 82.325 | V-C | 0.2174.599 | 40 | 62 | 0 | 0 | 144.325 |
| Stage 1 | -9.8 | 166.1 | 83.05 | V-C | 0.2174.599 | 40 | 63 | 0 | 0 | 146.05 |
| Stage 1 | -9.9 | 167.55 | 83.775 | V-C | 0.2174.599 | 40 | 64 | 0 | 0 | 147.775 |
| Stage 1 | -10 | 169 | 84.5 | V-C | 0.2174.599 | 40 | 65 | 0 | 0 | 149.5 |

| Design Assumption: Nominal Risultati Terreno | | Muro: | | LEFT | Lato | RIGHT | | | | |
|--|-------|---------------|---------------|-------|------------|-------|----------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage 1 | 0 | 0 | 0 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 |
| Stage 1 | -0.1 | 1.9 | 0.95 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0.95 |
| Stage 1 | -0.2 | 3.8 | 1.9 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 1.9 |
| Stage 1 | -0.3 | 5.7 | 2.85 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 2.85 |
| Stage 1 | -0.4 | 7.6 | 3.8 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 3.8 |
| Stage 1 | -0.5 | 9.5 | 4.75 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 4.75 |
| Stage 1 | -0.6 | 11.4 | 5.7 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 5.7 |
| Stage 1 | -0.7 | 13.3 | 6.65 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 6.65 |
| Stage 1 | -0.8 | 15.2 | 7.6 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 7.6 |
| Stage 1 | -0.9 | 17.1 | 8.55 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 8.55 |
| Stage 1 | -1 | 19 | 9.5 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 9.5 |
| Stage 1 | -1.1 | 20.9 | 10.45 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 10.45 |
| Stage 1 | -1.2 | 22.8 | 11.4 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 11.4 |
| Stage 1 | -1.3 | 24.7 | 12.35 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 12.35 |
| Stage 1 | -1.4 | 26.6 | 13.3 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 13.3 |
| Stage 1 | -1.5 | 28.5 | 14.25 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 14.25 |
| Stage 1 | -1.6 | 30.4 | 15.2 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 15.2 |
| Stage 1 | -1.7 | 32.3 | 16.15 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 16.15 |
| Stage 1 | -1.8 | 34.2 | 17.1 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 17.1 |
| Stage 1 | -1.9 | 36.1 | 18.05 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 18.05 |
| Stage 1 | -2 | 38 | 19 | V-C | 0.2174.599 | | 40 | 0 | 0 | 19 |
| Stage 1 | -2.1 | 40.45 | 20.225 | V-C | 0.2174.599 | | 40 | 0 | 0 | 20.225 |
| Stage 1 | -2.2 | 42.9 | 21.45 | V-C | 0.2174.599 | | 40 | 0 | 0 | 21.45 |
| Stage 1 | -2.3 | 45.35 | 22.675 | V-C | 0.2174.599 | | 40 | 0 | 0 | 22.675 |
| Stage 1 | -2.4 | 47.8 | 23.9 | V-C | 0.2174.599 | | 40 | 0 | 0 | 23.9 |
| Stage 1 | -2.5 | 50.25 | 25.125 | V-C | 0.2174.599 | | 40 | 0 | 0 | 25.125 |
| Stage 1 | -2.6 | 52.7 | 26.35 | V-C | 0.2174.599 | | 40 | 0 | 0 | 26.35 |
| Stage 1 | -2.7 | 55.15 | 27.575 | V-C | 0.2174.599 | | 40 | 0 | 0 | 27.575 |
| Stage 1 | -2.8 | 57.6 | 28.8 | V-C | 0.2174.599 | | 40 | 0 | 0 | 28.8 |
| Stage 1 | -2.9 | 60.05 | 30.025 | V-C | 0.2174.599 | | 40 | 0 | 0 | 30.025 |
| Stage 1 | -3 | 62.5 | 31.25 | V-C | 0.2174.599 | | 40 | 0 | 0 | 31.25 |
| Stage 1 | -3.1 | 64.95 | 32.475 | V-C | 0.2174.599 | | 40 | 0 | 0 | 32.475 |
| Stage 1 | -3.2 | 67.4 | 33.7 | V-C | 0.2174.599 | | 40 | 0 | 0 | 33.7 |
| Stage 1 | -3.3 | 69.85 | 34.925 | V-C | 0.2174.599 | | 40 | 0 | 0 | 34.925 |
| Stage 1 | -3.4 | 72.3 | 36.15 | V-C | 0.2174.599 | | 40 | 0 | 0 | 36.15 |
| Stage 1 | -3.5 | 74.75 | 37.375 | V-C | 0.2174.599 | | 40 | 0 | 0 | 37.375 |
| Stage 1 | -3.6 | 76.2 | 38.1 | V-C | 0.2174.599 | | 40 | 1 | 0 | 39.1 |
| Stage 1 | -3.7 | 77.65 | 38.825 | V-C | 0.2174.599 | | 40 | 2 | 0 | 40.825 |
| Stage 1 | -3.8 | 79.1 | 39.55 | V-C | 0.2174.599 | | 40 | 3 | 0 | 42.55 |
| Stage 1 | -3.9 | 80.55 | 40.275 | V-C | 0.2174.599 | | 40 | 4 | 0 | 44.275 |
| Stage 1 | -4 | 82 | 41 | V-C | 0.2174.599 | | 40 | 5 | 0 | 46 |
| Stage 1 | -4.1 | 83.45 | 41.725 | V-C | 0.2174.599 | | 40 | 6 | 0 | 47.725 |
| Stage 1 | -4.2 | 84.9 | 42.45 | V-C | 0.2174.599 | | 40 | 7 | 0 | 49.45 |
| Stage 1 | -4.3 | 86.35 | 43.175 | V-C | 0.2174.599 | | 40 | 8 | 0 | 51.175 |
| Stage 1 | -4.4 | 87.8 | 43.9 | V-C | 0.2174.599 | | 40 | 9 | 0 | 52.9 |
| Stage 1 | -4.5 | 89.25 | 44.625 | V-C | 0.2174.599 | | 40 | 10 | 0 | 54.625 |
| Stage 1 | -4.6 | 90.7 | 45.35 | V-C | 0.2174.599 | | 40 | 11 | 0 | 56.35 |
| Stage 1 | -4.7 | 92.15 | 46.075 | V-C | 0.2174.599 | | 40 | 12 | 0 | 58.075 |
| Stage 1 | -4.8 | 93.6 | 46.8 | V-C | 0.2174.599 | | 40 | 13 | 0 | 59.8 |
| Stage 1 | -4.9 | 95.05 | 47.525 | V-C | 0.2174.599 | | 40 | 14 | 0 | 61.525 |
| Stage 1 | -5 | 96.5 | 48.25 | V-C | 0.2174.599 | | 40 | 15 | 0 | 63.25 |
| Stage 1 | -5.1 | 97.95 | 48.975 | V-C | 0.2174.599 | | 40 | 16 | 0 | 64.975 |
| Stage 1 | -5.2 | 99.4 | 49.7 | V-C | 0.2174.599 | | 40 | 17 | 0 | 66.7 |
| Stage 1 | -5.3 | 100.85 | 50.425 | V-C | 0.2174.599 | | 40 | 18 | 0 | 68.425 |
| Stage 1 | -5.4 | 102.3 | 51.15 | V-C | 0.2174.599 | | 40 | 19 | 0 | 70.15 |
| Stage 1 | -5.5 | 103.75 | 51.875 | V-C | 0.2174.599 | | 40 | 20 | 0 | 71.875 |
| Stage 1 | -5.6 | 105.2 | 52.6 | V-C | 0.2174.599 | | 40 | 21 | 0 | 73.6 |
| Stage 1 | -5.7 | 106.65 | 53.325 | V-C | 0.2174.599 | | 40 | 22 | 0 | 75.325 |
| Stage 1 | -5.8 | 108.1 | 54.05 | V-C | 0.2174.599 | | 40 | 23 | 0 | 77.05 |
| Stage 1 | -5.9 | 109.55 | 54.775 | V-C | 0.2174.599 | | 40 | 24 | 0 | 78.775 |
| Stage 1 | -6 | 111 | 55.5 | V-C | 0.2174.599 | | 40 | 25 | 0 | 80.5 |
| Stage 1 | -6.1 | 112.45 | 56.225 | V-C | 0.2174.599 | | 40 | 26 | 0 | 82.225 |
| Stage 1 | -6.2 | 113.9 | 56.95 | V-C | 0.2174.599 | | 40 | 27 | 0 | 83.95 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|----------|----------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | RIGHT Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage 1 | -6.3 | 115.35 | 57.675 | V-C | 0.2174.599 | 40 | 28 | 0 | 0 | 85.675 |
| Stage 1 | -6.4 | 116.8 | 58.4 | V-C | 0.2174.599 | 40 | 29 | 0 | 0 | 87.4 |
| Stage 1 | -6.5 | 118.25 | 59.125 | V-C | 0.2174.599 | 40 | 30 | 0 | 0 | 89.125 |
| Stage 1 | -6.6 | 119.7 | 59.85 | V-C | 0.2174.599 | 40 | 31 | 0 | 0 | 90.85 |
| Stage 1 | -6.7 | 121.15 | 60.575 | V-C | 0.2174.599 | 40 | 32 | 0 | 0 | 92.575 |
| Stage 1 | -6.8 | 122.6 | 61.3 | V-C | 0.2174.599 | 40 | 33 | 0 | 0 | 94.3 |
| Stage 1 | -6.9 | 124.05 | 62.025 | V-C | 0.2174.599 | 40 | 34 | 0 | 0 | 96.025 |
| Stage 1 | -7 | 125.5 | 62.75 | V-C | 0.2174.599 | 40 | 35 | 0 | 0 | 97.75 |
| Stage 1 | -7.1 | 126.95 | 63.475 | V-C | 0.2174.599 | 40 | 36 | 0 | 0 | 99.475 |
| Stage 1 | -7.2 | 128.4 | 64.2 | V-C | 0.2174.599 | 40 | 37 | 0 | 0 | 101.2 |
| Stage 1 | -7.3 | 129.85 | 64.925 | V-C | 0.2174.599 | 40 | 38 | 0 | 0 | 102.925 |
| Stage 1 | -7.4 | 131.3 | 65.65 | V-C | 0.2174.599 | 40 | 39 | 0 | 0 | 104.65 |
| Stage 1 | -7.5 | 132.75 | 66.375 | V-C | 0.2174.599 | 40 | 40 | 0 | 0 | 106.375 |
| Stage 1 | -7.6 | 134.2 | 67.1 | V-C | 0.2174.599 | 40 | 41 | 0 | 0 | 108.1 |
| Stage 1 | -7.7 | 135.65 | 67.825 | V-C | 0.2174.599 | 40 | 42 | 0 | 0 | 109.825 |
| Stage 1 | -7.8 | 137.1 | 68.55 | V-C | 0.2174.599 | 40 | 43 | 0 | 0 | 111.55 |
| Stage 1 | -7.9 | 138.55 | 69.275 | V-C | 0.2174.599 | 40 | 44 | 0 | 0 | 113.275 |
| Stage 1 | -8 | 140 | 70 | V-C | 0.2174.599 | 40 | 45 | 0 | 0 | 115 |
| Stage 1 | -8.1 | 141.45 | 70.725 | V-C | 0.2174.599 | 40 | 46 | 0 | 0 | 116.725 |
| Stage 1 | -8.2 | 142.9 | 71.45 | V-C | 0.2174.599 | 40 | 47 | 0 | 0 | 118.45 |
| Stage 1 | -8.3 | 144.35 | 72.175 | V-C | 0.2174.599 | 40 | 48 | 0 | 0 | 120.175 |
| Stage 1 | -8.4 | 145.8 | 72.9 | V-C | 0.2174.599 | 40 | 49 | 0 | 0 | 121.9 |
| Stage 1 | -8.5 | 147.25 | 73.625 | V-C | 0.2174.599 | 40 | 50 | 0 | 0 | 123.625 |
| Stage 1 | -8.6 | 148.7 | 74.35 | V-C | 0.2174.599 | 40 | 51 | 0 | 0 | 125.35 |
| Stage 1 | -8.7 | 150.15 | 75.075 | V-C | 0.2174.599 | 40 | 52 | 0 | 0 | 127.075 |
| Stage 1 | -8.8 | 151.6 | 75.8 | V-C | 0.2174.599 | 40 | 53 | 0 | 0 | 128.8 |
| Stage 1 | -8.9 | 153.05 | 76.525 | V-C | 0.2174.599 | 40 | 54 | 0 | 0 | 130.525 |
| Stage 1 | -9 | 154.5 | 77.25 | V-C | 0.2174.599 | 40 | 55 | 0 | 0 | 132.25 |
| Stage 1 | -9.1 | 155.95 | 77.975 | V-C | 0.2174.599 | 40 | 56 | 0 | 0 | 133.975 |
| Stage 1 | -9.2 | 157.4 | 78.7 | V-C | 0.2174.599 | 40 | 57 | 0 | 0 | 135.7 |
| Stage 1 | -9.3 | 158.85 | 79.425 | V-C | 0.2174.599 | 40 | 58 | 0 | 0 | 137.425 |
| Stage 1 | -9.4 | 160.3 | 80.15 | V-C | 0.2174.599 | 40 | 59 | 0 | 0 | 139.15 |
| Stage 1 | -9.5 | 161.75 | 80.875 | V-C | 0.2174.599 | 40 | 60 | 0 | 0 | 140.875 |
| Stage 1 | -9.6 | 163.2 | 81.6 | V-C | 0.2174.599 | 40 | 61 | 0 | 0 | 142.6 |
| Stage 1 | -9.7 | 164.65 | 82.325 | V-C | 0.2174.599 | 40 | 62 | 0 | 0 | 144.325 |
| Stage 1 | -9.8 | 166.1 | 83.05 | V-C | 0.2174.599 | 40 | 63 | 0 | 0 | 146.05 |
| Stage 1 | -9.9 | 167.55 | 83.775 | V-C | 0.2174.599 | 40 | 64 | 0 | 0 | 147.775 |
| Stage 1 | -10 | 169 | 84.5 | V-C | 0.2174.599 | 40 | 65 | 0 | 0 | 149.5 |

Tabella Risultati Terreno Left Wall - Nominal - Stage 2

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|---------------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | LEFT Ka | Lato Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 2 | 0 | 0 | 0 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage 2 | -0.1 | 1.9 | 0.958 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.958 |
| Stage 2 | -0.2 | 3.803 | 1.899 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.899 |
| Stage 2 | -0.3 | 5.709 | 2.838 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.838 |
| Stage 2 | -0.4 | 7.621 | 3.779 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.779 |
| Stage 2 | -0.5 | 9.541 | 4.724 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.724 |
| Stage 2 | -0.6 | 11.469 | 5.673 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.673 |
| Stage 2 | -0.7 | 13.406 | 6.626 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.626 |
| Stage 2 | -0.8 | 15.353 | 7.585 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.585 |
| Stage 2 | -0.9 | 17.311 | 8.55 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.55 |
| Stage 2 | -1 | 19.278 | 9.519 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.519 |
| Stage 2 | -1.1 | 21.256 | 10.494 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.494 |
| Stage 2 | -1.2 | 23.242 | 11.475 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.475 |
| Stage 2 | -1.3 | 25.237 | 12.46 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 12.46 |
| Stage 2 | -1.4 | 27.24 | 13.45 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 13.45 |
| Stage 2 | -1.5 | 29.25 | 14.445 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 14.445 |
| Stage 2 | -1.6 | 31.265 | 15.443 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 15.443 |
| Stage 2 | -1.7 | 33.286 | 16.445 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 16.445 |
| Stage 2 | -1.8 | 35.31 | 17.45 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.45 |
| Stage 2 | -1.9 | 37.337 | 18.457 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 18.457 |
| Stage 2 | -2 | 39.367 | 18.955 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 18.955 |
| Stage 2 | -2.1 | 41.948 | 20.224 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 20.224 |
| Stage 2 | -2.2 | 44.529 | 21.491 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 21.491 |
| Stage 2 | -2.3 | 47.111 | 22.755 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 22.755 |
| Stage 2 | -2.4 | 49.692 | 24.014 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 24.014 |
| Stage 2 | -2.5 | 52.272 | 25.269 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 25.269 |
| Stage 2 | -2.6 | 54.85 | 26.517 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 26.517 |
| Stage 2 | -2.7 | 57.427 | 27.759 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 27.759 |
| Stage 2 | -2.8 | 60.001 | 28.995 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 28.995 |
| Stage 2 | -2.9 | 62.573 | 30.225 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 30.225 |
| Stage 2 | -3 | 65.143 | 31.448 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 31.448 |
| Stage 2 | -3.1 | 67.9 | 32.761 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 32.761 |
| Stage 2 | -3.2 | 70.524 | 34.003 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 34.003 |
| Stage 2 | -3.3 | 73.141 | 35.239 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 35.239 |
| Stage 2 | -3.4 | 75.96 | 36.574 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 36.574 |
| Stage 2 | -3.5 | 78.558 | 37.796 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 37.796 |
| Stage 2 | -3.6 | 80.348 | 38.613 | UL-RL | 0.2174.599 | | 40 | 1 | 0 | 0 | 39.613 |
| Stage 2 | -3.7 | 81.929 | 39.327 | UL-RL | 0.2174.599 | | 40 | 2 | 0 | 0 | 41.327 |
| Stage 2 | -3.8 | 83.505 | 40.038 | UL-RL | 0.2174.599 | | 40 | 3 | 0 | 0 | 43.038 |
| Stage 2 | -3.9 | 85.26 | 40.84 | UL-RL | 0.2174.599 | | 40 | 4 | 0 | 0 | 44.84 |
| Stage 2 | -4 | 86.823 | 41.547 | UL-RL | 0.2174.599 | | 40 | 5 | 0 | 0 | 46.547 |
| Stage 2 | -4.1 | 88.382 | 42.254 | UL-RL | 0.2174.599 | | 40 | 6 | 0 | 0 | 48.254 |
| Stage 2 | -4.2 | 90.108 | 43.046 | UL-RL | 0.2174.599 | | 40 | 7 | 0 | 0 | 50.046 |
| Stage 2 | -4.3 | 91.656 | 43.752 | UL-RL | 0.2174.599 | | 40 | 8 | 0 | 0 | 51.752 |
| Stage 2 | -4.4 | 93.363 | 44.539 | UL-RL | 0.2174.599 | | 40 | 9 | 0 | 0 | 53.539 |
| Stage 2 | -4.5 | 94.901 | 45.245 | UL-RL | 0.2174.599 | | 40 | 10 | 0 | 0 | 55.245 |
| Stage 2 | -4.6 | 96.436 | 45.951 | UL-RL | 0.2174.599 | | 40 | 11 | 0 | 0 | 56.951 |
| Stage 2 | -4.7 | 98.121 | 46.735 | UL-RL | 0.2174.599 | | 40 | 12 | 0 | 0 | 58.735 |
| Stage 2 | -4.8 | 99.648 | 47.442 | UL-RL | 0.2174.599 | | 40 | 13 | 0 | 0 | 60.442 |
| Stage 2 | -4.9 | 101.319 | 48.223 | UL-RL | 0.2174.599 | | 40 | 14 | 0 | 0 | 62.223 |
| Stage 2 | -5 | 102.839 | 48.931 | UL-RL | 0.2174.599 | | 40 | 15 | 0 | 0 | 63.931 |
| Stage 2 | -5.1 | 104.357 | 49.64 | UL-RL | 0.2174.599 | | 40 | 16 | 0 | 0 | 65.64 |
| Stage 2 | -5.2 | 106.011 | 50.419 | UL-RL | 0.2174.599 | | 40 | 17 | 0 | 0 | 67.419 |
| Stage 2 | -5.3 | 107.522 | 51.128 | UL-RL | 0.2174.599 | | 40 | 18 | 0 | 0 | 69.128 |
| Stage 2 | -5.4 | 109.165 | 51.905 | UL-RL | 0.2174.599 | | 40 | 19 | 0 | 0 | 70.905 |
| Stage 2 | -5.5 | 110.671 | 52.616 | UL-RL | 0.2174.599 | | 40 | 20 | 0 | 0 | 72.616 |
| Stage 2 | -5.6 | 112.176 | 53.327 | UL-RL | 0.2174.599 | | 40 | 21 | 0 | 0 | 74.327 |
| Stage 2 | -5.7 | 113.804 | 54.101 | UL-RL | 0.2174.599 | | 40 | 22 | 0 | 0 | 76.101 |
| Stage 2 | -5.8 | 115.304 | 54.813 | UL-RL | 0.2174.599 | | 40 | 23 | 0 | 0 | 77.813 |
| Stage 2 | -5.9 | 116.802 | 55.525 | UL-RL | 0.2174.599 | | 40 | 24 | 0 | 0 | 79.525 |
| Stage 2 | -6 | 118.419 | 56.297 | UL-RL | 0.2174.599 | | 40 | 25 | 0 | 0 | 81.297 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 2 | -6.1 | 119.914 | 57.009 | UL-RL | 0.2174.599 | 40 | 26 | 0 | 0 | 83.009 |
| Stage 2 | -6.2 | 121.522 | 57.779 | UL-RL | 0.2174.599 | 40 | 27 | 0 | 0 | 84.779 |
| Stage 2 | -6.3 | 123.013 | 58.491 | UL-RL | 0.2174.599 | 40 | 28 | 0 | 0 | 86.491 |
| Stage 2 | -6.4 | 124.502 | 59.203 | UL-RL | 0.2174.599 | 40 | 29 | 0 | 0 | 88.203 |
| Stage 2 | -6.5 | 126.101 | 59.971 | UL-RL | 0.2174.599 | 40 | 30 | 0 | 0 | 89.971 |
| Stage 2 | -6.6 | 127.587 | 60.683 | UL-RL | 0.2174.599 | 40 | 31 | 0 | 0 | 91.683 |
| Stage 2 | -6.7 | 129.179 | 61.449 | UL-RL | 0.2174.599 | 40 | 32 | 0 | 0 | 93.449 |
| Stage 2 | -6.8 | 130.662 | 62.161 | UL-RL | 0.2174.599 | 40 | 33 | 0 | 0 | 95.161 |
| Stage 2 | -6.9 | 132.145 | 62.874 | UL-RL | 0.2174.599 | 40 | 34 | 0 | 0 | 96.874 |
| Stage 2 | -7 | 133.729 | 63.638 | UL-RL | 0.2174.599 | 40 | 35 | 0 | 0 | 98.638 |
| Stage 2 | -7.1 | 135.208 | 64.35 | UL-RL | 0.2174.599 | 40 | 36 | 0 | 0 | 100.35 |
| Stage 2 | -7.2 | 136.787 | 65.113 | UL-RL | 0.2174.599 | 40 | 37 | 0 | 0 | 102.112 |
| Stage 2 | -7.3 | 138.264 | 65.825 | UL-RL | 0.2174.599 | 40 | 38 | 0 | 0 | 103.825 |
| Stage 2 | -7.4 | 139.741 | 66.538 | UL-RL | 0.2174.599 | 40 | 39 | 0 | 0 | 105.538 |
| Stage 2 | -7.5 | 141.312 | 67.299 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 107.298 |
| Stage 2 | -7.6 | 142.787 | 68.011 | UL-RL | 0.2174.599 | 40 | 41 | 0 | 0 | 109.011 |
| Stage 2 | -7.7 | 144.26 | 68.724 | UL-RL | 0.2174.599 | 40 | 42 | 0 | 0 | 110.724 |
| Stage 2 | -7.8 | 145.826 | 69.483 | UL-RL | 0.2174.599 | 40 | 43 | 0 | 0 | 112.483 |
| Stage 2 | -7.9 | 147.298 | 70.196 | UL-RL | 0.2174.599 | 40 | 44 | 0 | 0 | 114.196 |
| Stage 2 | -8 | 148.859 | 70.954 | UL-RL | 0.2174.599 | 40 | 45 | 0 | 0 | 115.954 |
| Stage 2 | -8.1 | 150.329 | 71.667 | UL-RL | 0.2174.599 | 40 | 46 | 0 | 0 | 117.667 |
| Stage 2 | -8.2 | 151.798 | 72.38 | UL-RL | 0.2174.599 | 40 | 47 | 0 | 0 | 119.38 |
| Stage 2 | -8.3 | 153.354 | 73.138 | UL-RL | 0.2174.599 | 40 | 48 | 0 | 0 | 121.138 |
| Stage 2 | -8.4 | 154.822 | 73.852 | UL-RL | 0.2174.599 | 40 | 49 | 0 | 0 | 122.852 |
| Stage 2 | -8.5 | 156.374 | 74.609 | UL-RL | 0.2174.599 | 40 | 50 | 0 | 0 | 124.609 |
| Stage 2 | -8.6 | 157.84 | 75.324 | UL-RL | 0.2174.599 | 40 | 51 | 0 | 0 | 126.324 |
| Stage 2 | -8.7 | 159.307 | 76.04 | UL-RL | 0.2174.599 | 40 | 52 | 0 | 0 | 128.04 |
| Stage 2 | -8.8 | 160.854 | 76.798 | UL-RL | 0.2174.599 | 40 | 53 | 0 | 0 | 129.798 |
| Stage 2 | -8.9 | 162.319 | 77.517 | UL-RL | 0.2174.599 | 40 | 54 | 0 | 0 | 131.517 |
| Stage 2 | -9 | 163.863 | 78.276 | UL-RL | 0.2174.599 | 40 | 55 | 0 | 0 | 133.276 |
| Stage 2 | -9.1 | 165.326 | 78.997 | UL-RL | 0.2174.599 | 40 | 56 | 0 | 0 | 134.997 |
| Stage 2 | -9.2 | 166.79 | 79.719 | UL-RL | 0.2174.599 | 40 | 57 | 0 | 0 | 136.719 |
| Stage 2 | -9.3 | 168.33 | 80.482 | UL-RL | 0.2174.599 | 40 | 58 | 0 | 0 | 138.482 |
| Stage 2 | -9.4 | 169.792 | 81.207 | UL-RL | 0.2174.599 | 40 | 59 | 0 | 0 | 140.207 |
| Stage 2 | -9.5 | 171.254 | 81.934 | UL-RL | 0.2174.599 | 40 | 60 | 0 | 0 | 141.934 |
| Stage 2 | -9.6 | 172.64 | 82.624 | UL-RL | 0.2174.599 | 40 | 61 | 0 | 0 | 143.624 |
| Stage 2 | -9.7 | 174.028 | 83.316 | UL-RL | 0.2174.599 | 40 | 62 | 0 | 0 | 145.316 |
| Stage 2 | -9.8 | 175.416 | 84.009 | UL-RL | 0.2174.599 | 40 | 63 | 0 | 0 | 147.008 |
| Stage 2 | -9.9 | 176.805 | 84.702 | UL-RL | 0.2174.599 | 40 | 64 | 0 | 0 | 148.702 |
| Stage 2 | -10 | 178.195 | 85.396 | UL-RL | 0.2174.599 | 40 | 65 | 0 | 0 | 150.396 |

| Design Assumption: Nominal Risultati Terreno | | | Muro: | LEFT | Lato | RIGHT | | | | | |
|--|-------|---------------|---------------|---------|------------|-------|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 2 | 0 | 0 | 0 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage 2 | -0.1 | 1.9 | 0.943 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.943 |
| Stage 2 | -0.2 | 3.8 | 1.901 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.901 |
| Stage 2 | -0.3 | 5.7 | 2.856 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.856 |
| Stage 2 | -0.4 | 7.6 | 3.811 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.811 |
| Stage 2 | -0.5 | 9.5 | 4.766 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.766 |
| Stage 2 | -0.6 | 11.4 | 5.721 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.721 |
| Stage 2 | -0.7 | 13.3 | 6.676 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.676 |
| Stage 2 | -0.8 | 15.2 | 7.631 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.631 |
| Stage 2 | -0.9 | 17.1 | 8.586 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.586 |
| Stage 2 | -1 | 19 | 9.541 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.541 |
| Stage 2 | -1.1 | 20.9 | 10.495 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.495 |
| Stage 2 | -1.2 | 22.8 | 11.45 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.45 |
| Stage 2 | -1.3 | 24.7 | 12.404 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 12.404 |
| Stage 2 | -1.4 | 26.6 | 13.358 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 13.358 |
| Stage 2 | -1.5 | 28.5 | 14.311 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 14.311 |
| Stage 2 | -1.6 | 30.4 | 15.264 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 15.264 |
| Stage 2 | -1.7 | 32.3 | 16.217 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 16.217 |
| Stage 2 | -1.8 | 34.2 | 17.169 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.169 |
| Stage 2 | -1.9 | 36.1 | 18.122 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 18.122 |
| Stage 2 | -2 | 38 | 19.198 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 19.198 |
| Stage 2 | -2.1 | 40.45 | 20.429 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 20.429 |
| Stage 2 | -2.2 | 42.9 | 21.66 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 21.66 |
| Stage 2 | -2.3 | 45.35 | 22.893 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 22.893 |
| Stage 2 | -2.4 | 47.8 | 24.126 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 24.126 |
| Stage 2 | -2.5 | 50.25 | 25.361 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 25.361 |
| Stage 2 | -2.6 | 52.7 | 26.597 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 26.597 |
| Stage 2 | -2.7 | 55.15 | 27.834 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 27.834 |
| Stage 2 | -2.8 | 57.6 | 29.073 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 29.073 |
| Stage 2 | -2.9 | 60.05 | 30.314 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 30.314 |
| Stage 2 | -3 | 62.5 | 31.555 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 31.555 |
| Stage 2 | -3.1 | 64.95 | 32.798 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 32.798 |
| Stage 2 | -3.2 | 67.4 | 34.042 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 34.042 |
| Stage 2 | -3.3 | 69.85 | 35.287 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 35.287 |
| Stage 2 | -3.4 | 72.3 | 36.532 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 36.532 |
| Stage 2 | -3.5 | 74.75 | 37.778 | V-C | 0.2174.599 | | 40 | 0 | 0 | 0 | 37.778 |
| Stage 2 | -3.6 | 76.2 | 38.524 | V-C | 0.2174.599 | | 40 | 1 | 0 | 0 | 39.524 |
| Stage 2 | -3.7 | 77.65 | 39.27 | V-C | 0.2174.599 | | 40 | 2 | 0 | 0 | 41.27 |
| Stage 2 | -3.8 | 79.1 | 40.016 | V-C | 0.2174.599 | | 40 | 3 | 0 | 0 | 43.016 |
| Stage 2 | -3.9 | 80.55 | 40.762 | V-C | 0.2174.599 | | 40 | 4 | 0 | 0 | 44.762 |
| Stage 2 | -4 | 82 | 41.507 | V-C | 0.2174.599 | | 40 | 5 | 0 | 0 | 46.507 |
| Stage 2 | -4.1 | 83.45 | 42.252 | V-C | 0.2174.599 | | 40 | 6 | 0 | 0 | 48.252 |
| Stage 2 | -4.2 | 84.9 | 42.996 | V-C | 0.2174.599 | | 40 | 7 | 0 | 0 | 49.996 |
| Stage 2 | -4.3 | 86.35 | 43.739 | V-C | 0.2174.599 | | 40 | 8 | 0 | 0 | 51.739 |
| Stage 2 | -4.4 | 87.8 | 44.482 | V-C | 0.2174.599 | | 40 | 9 | 0 | 0 | 53.482 |
| Stage 2 | -4.5 | 89.25 | 45.225 | V-C | 0.2174.599 | | 40 | 10 | 0 | 0 | 55.225 |
| Stage 2 | -4.6 | 90.7 | 45.966 | V-C | 0.2174.599 | | 40 | 11 | 0 | 0 | 56.966 |
| Stage 2 | -4.7 | 92.15 | 46.707 | V-C | 0.2174.599 | | 40 | 12 | 0 | 0 | 58.707 |
| Stage 2 | -4.8 | 93.6 | 47.448 | V-C | 0.2174.599 | | 40 | 13 | 0 | 0 | 60.448 |
| Stage 2 | -4.9 | 95.05 | 48.187 | V-C | 0.2174.599 | | 40 | 14 | 0 | 0 | 62.187 |
| Stage 2 | -5 | 96.5 | 48.926 | V-C | 0.2174.599 | | 40 | 15 | 0 | 0 | 63.926 |
| Stage 2 | -5.1 | 97.95 | 49.665 | V-C | 0.2174.599 | | 40 | 16 | 0 | 0 | 65.665 |
| Stage 2 | -5.2 | 99.4 | 50.403 | V-C | 0.2174.599 | | 40 | 17 | 0 | 0 | 67.403 |
| Stage 2 | -5.3 | 100.85 | 51.141 | V-C | 0.2174.599 | | 40 | 18 | 0 | 0 | 69.141 |
| Stage 2 | -5.4 | 102.3 | 51.878 | V-C | 0.2174.599 | | 40 | 19 | 0 | 0 | 70.878 |
| Stage 2 | -5.5 | 103.75 | 52.614 | V-C | 0.2174.599 | | 40 | 20 | 0 | 0 | 72.614 |
| Stage 2 | -5.6 | 105.2 | 53.35 | V-C | 0.2174.599 | | 40 | 21 | 0 | 0 | 74.35 |
| Stage 2 | -5.7 | 106.65 | 54.086 | V-C | 0.2174.599 | | 40 | 22 | 0 | 0 | 76.086 |
| Stage 2 | -5.8 | 108.1 | 54.822 | V-C | 0.2174.599 | | 40 | 23 | 0 | 0 | 77.822 |
| Stage 2 | -5.9 | 109.55 | 55.557 | V-C | 0.2174.599 | | 40 | 24 | 0 | 0 | 79.557 |
| Stage 2 | -6 | 111 | 56.292 | V-C | 0.2174.599 | | 40 | 25 | 0 | 0 | 81.292 |
| Stage 2 | -6.1 | 112.45 | 57.026 | V-C | 0.2174.599 | | 40 | 26 | 0 | 0 | 83.026 |
| Stage 2 | -6.2 | 113.9 | 57.76 | V-C | 0.2174.599 | | 40 | 27 | 0 | 0 | 84.76 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------|-------|------------|----|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Muro: | | LEFT | Lato | | RIGHT | | | | |
| | | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 2 | -6.3 | 115.35 | 58.495 | V-C | 0.2174.599 | | 40 | 28 | 0 | 0 | 86.495 |
| Stage 2 | -6.4 | 116.8 | 59.228 | V-C | 0.2174.599 | | 40 | 29 | 0 | 0 | 88.228 |
| Stage 2 | -6.5 | 118.25 | 59.962 | V-C | 0.2174.599 | | 40 | 30 | 0 | 0 | 89.962 |
| Stage 2 | -6.6 | 119.7 | 60.695 | V-C | 0.2174.599 | | 40 | 31 | 0 | 0 | 91.695 |
| Stage 2 | -6.7 | 121.15 | 61.429 | V-C | 0.2174.599 | | 40 | 32 | 0 | 0 | 93.429 |
| Stage 2 | -6.8 | 122.6 | 62.162 | V-C | 0.2174.599 | | 40 | 33 | 0 | 0 | 95.162 |
| Stage 2 | -6.9 | 124.05 | 62.894 | V-C | 0.2174.599 | | 40 | 34 | 0 | 0 | 96.894 |
| Stage 2 | -7 | 125.5 | 63.627 | V-C | 0.2174.599 | | 40 | 35 | 0 | 0 | 98.627 |
| Stage 2 | -7.1 | 126.95 | 64.359 | V-C | 0.2174.599 | | 40 | 36 | 0 | 0 | 100.359 |
| Stage 2 | -7.2 | 128.4 | 65.092 | V-C | 0.2174.599 | | 40 | 37 | 0 | 0 | 102.092 |
| Stage 2 | -7.3 | 129.85 | 65.824 | V-C | 0.2174.599 | | 40 | 38 | 0 | 0 | 103.824 |
| Stage 2 | -7.4 | 131.3 | 66.556 | V-C | 0.2174.599 | | 40 | 39 | 0 | 0 | 105.556 |
| Stage 2 | -7.5 | 132.75 | 67.288 | V-C | 0.2174.599 | | 40 | 40 | 0 | 0 | 107.288 |
| Stage 2 | -7.6 | 134.2 | 68.019 | V-C | 0.2174.599 | | 40 | 41 | 0 | 0 | 109.019 |
| Stage 2 | -7.7 | 135.65 | 68.751 | V-C | 0.2174.599 | | 40 | 42 | 0 | 0 | 110.751 |
| Stage 2 | -7.8 | 137.1 | 69.482 | V-C | 0.2174.599 | | 40 | 43 | 0 | 0 | 112.482 |
| Stage 2 | -7.9 | 138.55 | 70.213 | V-C | 0.2174.599 | | 40 | 44 | 0 | 0 | 114.213 |
| Stage 2 | -8 | 140 | 70.945 | V-C | 0.2174.599 | | 40 | 45 | 0 | 0 | 115.944 |
| Stage 2 | -8.1 | 141.45 | 71.676 | V-C | 0.2174.599 | | 40 | 46 | 0 | 0 | 117.676 |
| Stage 2 | -8.2 | 142.9 | 72.406 | V-C | 0.2174.599 | | 40 | 47 | 0 | 0 | 119.406 |
| Stage 2 | -8.3 | 144.35 | 73.137 | V-C | 0.2174.599 | | 40 | 48 | 0 | 0 | 121.137 |
| Stage 2 | -8.4 | 145.8 | 73.867 | V-C | 0.2174.599 | | 40 | 49 | 0 | 0 | 122.867 |
| Stage 2 | -8.5 | 147.25 | 74.598 | V-C | 0.2174.599 | | 40 | 50 | 0 | 0 | 124.598 |
| Stage 2 | -8.6 | 148.7 | 75.327 | V-C | 0.2174.599 | | 40 | 51 | 0 | 0 | 126.327 |
| Stage 2 | -8.7 | 150.15 | 76.057 | V-C | 0.2174.599 | | 40 | 52 | 0 | 0 | 128.057 |
| Stage 2 | -8.8 | 151.6 | 76.786 | V-C | 0.2174.599 | | 40 | 53 | 0 | 0 | 129.786 |
| Stage 2 | -8.9 | 153.05 | 77.515 | V-C | 0.2174.599 | | 40 | 54 | 0 | 0 | 131.515 |
| Stage 2 | -9 | 154.5 | 78.244 | V-C | 0.2174.599 | | 40 | 55 | 0 | 0 | 133.244 |
| Stage 2 | -9.1 | 155.95 | 78.972 | V-C | 0.2174.599 | | 40 | 56 | 0 | 0 | 134.972 |
| Stage 2 | -9.2 | 157.4 | 79.699 | V-C | 0.2174.599 | | 40 | 57 | 0 | 0 | 136.699 |
| Stage 2 | -9.3 | 158.85 | 80.426 | V-C | 0.2174.599 | | 40 | 58 | 0 | 0 | 138.426 |
| Stage 2 | -9.4 | 160.3 | 81.153 | V-C | 0.2174.599 | | 40 | 59 | 0 | 0 | 140.153 |
| Stage 2 | -9.5 | 161.75 | 81.879 | V-C | 0.2174.599 | | 40 | 60 | 0 | 0 | 141.879 |
| Stage 2 | -9.6 | 163.2 | 82.605 | V-C | 0.2174.599 | | 40 | 61 | 0 | 0 | 143.605 |
| Stage 2 | -9.7 | 164.65 | 83.33 | V-C | 0.2174.599 | | 40 | 62 | 0 | 0 | 145.33 |
| Stage 2 | -9.8 | 166.1 | 84.056 | V-C | 0.2174.599 | | 40 | 63 | 0 | 0 | 147.056 |
| Stage 2 | -9.9 | 167.55 | 84.781 | V-C | 0.2174.599 | | 40 | 64 | 0 | 0 | 148.781 |
| Stage 2 | -10 | 169 | 85.506 | V-C | 0.2174.599 | | 40 | 65 | 0 | 0 | 150.506 |

Tabella Risultati Terreno Left Wall - Nominal - Stage A

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|---------|---------|---------------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | LEFT Ka | Lato Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage A | 0 | 0 | 0 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.1 | 1.9 | 0.608 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.608 |
| Stage A | -0.2 | 3.803 | 1.217 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.217 |
| Stage A | -0.3 | 5.709 | 1.827 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.827 |
| Stage A | -0.4 | 7.621 | 2.439 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 2.439 |
| Stage A | -0.5 | 9.541 | 3.053 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.053 |
| Stage A | -0.6 | 11.469 | 3.67 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 3.67 |
| Stage A | -0.7 | 13.406 | 4.29 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.29 |
| Stage A | -0.8 | 15.353 | 4.913 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 4.913 |
| Stage A | -0.9 | 17.311 | 5.539 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.539 |
| Stage A | -1 | 19.278 | 6.169 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.169 |
| Stage A | -1.1 | 21.256 | 6.802 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 6.802 |
| Stage A | -1.2 | 23.242 | 7.438 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.438 |
| Stage A | -1.3 | 25.237 | 8.076 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.076 |
| Stage A | -1.4 | 27.24 | 8.717 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.717 |
| Stage A | -1.5 | 29.25 | 9.36 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 9.36 |
| Stage A | -1.6 | 31.265 | 10.005 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.005 |
| Stage A | -1.7 | 33.286 | 10.651 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 10.651 |
| Stage A | -1.8 | 35.31 | 11.299 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.299 |
| Stage A | -1.9 | 37.337 | 11.948 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.948 |
| Stage A | -2 | 39.367 | 0 | ACTIVE | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 0 |
| Stage A | -2.1 | 41.948 | 0 | ACTIVE | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 0 |
| Stage A | -2.2 | 44.529 | 0 | ACTIVE | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 0 |
| Stage A | -2.3 | 47.111 | 0 | ACTIVE | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 0 |
| Stage A | -2.4 | 49.692 | 5.533 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 5.533 |
| Stage A | -2.5 | 52.272 | 11.266 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 11.266 |
| Stage A | -2.6 | 54.85 | 16.168 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 16.168 |
| Stage A | -2.7 | 57.427 | 20.316 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 20.316 |
| Stage A | -2.8 | 60.001 | 23.794 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 23.794 |
| Stage A | -2.9 | 62.573 | 26.687 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 26.687 |
| Stage A | -3 | 65.143 | 29.081 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 29.081 |
| Stage A | -3.1 | 67.9 | 31.155 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 31.155 |
| Stage A | -3.2 | 70.524 | 32.824 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 32.824 |
| Stage A | -3.3 | 73.141 | 34.222 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 34.222 |
| Stage A | -3.4 | 75.96 | 35.515 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 35.515 |
| Stage A | -3.5 | 78.558 | 36.545 | UL-RL | 0.217 | 4.599 | 40 | 0 | 0 | 0 | 36.545 |
| Stage A | -3.6 | 80.348 | 37.065 | UL-RL | 0.217 | 4.599 | 40 | 1 | 0 | 0 | 38.065 |
| Stage A | -3.7 | 81.929 | 37.414 | UL-RL | 0.217 | 4.599 | 40 | 2 | 0 | 0 | 39.414 |
| Stage A | -3.8 | 83.505 | 37.723 | UL-RL | 0.217 | 4.599 | 40 | 3 | 0 | 0 | 40.723 |
| Stage A | -3.9 | 85.26 | 38.111 | UL-RL | 0.217 | 4.599 | 40 | 4 | 0 | 0 | 42.111 |
| Stage A | -4 | 86.823 | 38.409 | UL-RL | 0.217 | 4.599 | 40 | 5 | 0 | 0 | 43.409 |
| Stage A | -4.1 | 88.382 | 38.728 | UL-RL | 0.217 | 4.599 | 40 | 6 | 0 | 0 | 44.727 |
| Stage A | -4.2 | 90.108 | 39.16 | UL-RL | 0.217 | 4.599 | 40 | 7 | 0 | 0 | 46.16 |
| Stage A | -4.3 | 91.656 | 39.541 | UL-RL | 0.217 | 4.599 | 40 | 8 | 0 | 0 | 47.541 |
| Stage A | -4.4 | 93.363 | 40.043 | UL-RL | 0.217 | 4.599 | 40 | 9 | 0 | 0 | 49.042 |
| Stage A | -4.5 | 94.901 | 40.501 | UL-RL | 0.217 | 4.599 | 40 | 10 | 0 | 0 | 50.501 |
| Stage A | -4.6 | 96.436 | 41 | UL-RL | 0.217 | 4.599 | 40 | 11 | 0 | 0 | 52 |
| Stage A | -4.7 | 98.121 | 41.612 | UL-RL | 0.217 | 4.599 | 40 | 12 | 0 | 0 | 53.612 |
| Stage A | -4.8 | 99.648 | 42.182 | UL-RL | 0.217 | 4.599 | 40 | 13 | 0 | 0 | 55.182 |
| Stage A | -4.9 | 101.319 | 42.857 | UL-RL | 0.217 | 4.599 | 40 | 14 | 0 | 0 | 56.857 |
| Stage A | -5 | 102.839 | 43.486 | UL-RL | 0.217 | 4.599 | 40 | 15 | 0 | 0 | 58.486 |
| Stage A | -5.1 | 104.357 | 44.139 | UL-RL | 0.217 | 4.599 | 40 | 16 | 0 | 0 | 60.139 |
| Stage A | -5.2 | 106.011 | 44.881 | UL-RL | 0.217 | 4.599 | 40 | 17 | 0 | 0 | 61.881 |
| Stage A | -5.3 | 107.522 | 45.571 | UL-RL | 0.217 | 4.599 | 40 | 18 | 0 | 0 | 63.571 |
| Stage A | -5.4 | 109.165 | 46.341 | UL-RL | 0.217 | 4.599 | 40 | 19 | 0 | 0 | 65.341 |
| Stage A | -5.5 | 110.671 | 47.055 | UL-RL | 0.217 | 4.599 | 40 | 20 | 0 | 0 | 67.055 |
| Stage A | -5.6 | 112.176 | 47.777 | UL-RL | 0.217 | 4.599 | 40 | 21 | 0 | 0 | 68.777 |
| Stage A | -5.7 | 113.804 | 48.569 | UL-RL | 0.217 | 4.599 | 40 | 22 | 0 | 0 | 70.569 |
| Stage A | -5.8 | 115.304 | 49.301 | UL-RL | 0.217 | 4.599 | 40 | 23 | 0 | 0 | 72.301 |
| Stage A | -5.9 | 116.802 | 50.036 | UL-RL | 0.217 | 4.599 | 40 | 24 | 0 | 0 | 74.036 |
| Stage A | -6 | 118.419 | 50.832 | UL-RL | 0.217 | 4.599 | 40 | 25 | 0 | 0 | 75.832 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage A | -6.1 | 119.914 | 51.568 | UL-RL | 0.2174.599 | 40 | 26 | 0 | 0 | 77.568 |
| Stage A | -6.2 | 121.522 | 52.361 | UL-RL | 0.2174.599 | 40 | 27 | 0 | 0 | 79.361 |
| Stage A | -6.3 | 123.013 | 53.095 | UL-RL | 0.2174.599 | 40 | 28 | 0 | 0 | 81.095 |
| Stage A | -6.4 | 124.502 | 53.828 | UL-RL | 0.2174.599 | 40 | 29 | 0 | 0 | 82.828 |
| Stage A | -6.5 | 126.101 | 54.614 | UL-RL | 0.2174.599 | 40 | 30 | 0 | 0 | 84.614 |
| Stage A | -6.6 | 127.587 | 55.343 | UL-RL | 0.2174.599 | 40 | 31 | 0 | 0 | 86.343 |
| Stage A | -6.7 | 129.179 | 56.124 | UL-RL | 0.2174.599 | 40 | 32 | 0 | 0 | 88.124 |
| Stage A | -6.8 | 130.662 | 56.85 | UL-RL | 0.2174.599 | 40 | 33 | 0 | 0 | 89.85 |
| Stage A | -6.9 | 132.145 | 57.574 | UL-RL | 0.2174.599 | 40 | 34 | 0 | 0 | 91.574 |
| Stage A | -7 | 133.729 | 58.348 | UL-RL | 0.2174.599 | 40 | 35 | 0 | 0 | 93.348 |
| Stage A | -7.1 | 135.208 | 59.069 | UL-RL | 0.2174.599 | 40 | 36 | 0 | 0 | 95.069 |
| Stage A | -7.2 | 136.787 | 59.839 | UL-RL | 0.2174.599 | 40 | 37 | 0 | 0 | 96.839 |
| Stage A | -7.3 | 138.264 | 60.558 | UL-RL | 0.2174.599 | 40 | 38 | 0 | 0 | 98.558 |
| Stage A | -7.4 | 139.741 | 61.276 | UL-RL | 0.2174.599 | 40 | 39 | 0 | 0 | 100.276 |
| Stage A | -7.5 | 141.312 | 62.041 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 102.041 |
| Stage A | -7.6 | 142.787 | 62.758 | UL-RL | 0.2174.599 | 40 | 41 | 0 | 0 | 103.758 |
| Stage A | -7.7 | 144.26 | 63.475 | UL-RL | 0.2174.599 | 40 | 42 | 0 | 0 | 105.475 |
| Stage A | -7.8 | 145.826 | 64.237 | UL-RL | 0.2174.599 | 40 | 43 | 0 | 0 | 107.237 |
| Stage A | -7.9 | 147.298 | 64.953 | UL-RL | 0.2174.599 | 40 | 44 | 0 | 0 | 108.953 |
| Stage A | -8 | 148.859 | 65.713 | UL-RL | 0.2174.599 | 40 | 45 | 0 | 0 | 110.713 |
| Stage A | -8.1 | 150.329 | 66.429 | UL-RL | 0.2174.599 | 40 | 46 | 0 | 0 | 112.429 |
| Stage A | -8.2 | 151.798 | 67.145 | UL-RL | 0.2174.599 | 40 | 47 | 0 | 0 | 114.144 |
| Stage A | -8.3 | 153.354 | 67.904 | UL-RL | 0.2174.599 | 40 | 48 | 0 | 0 | 115.904 |
| Stage A | -8.4 | 154.822 | 68.62 | UL-RL | 0.2174.599 | 40 | 49 | 0 | 0 | 117.62 |
| Stage A | -8.5 | 156.374 | 69.38 | UL-RL | 0.2174.599 | 40 | 50 | 0 | 0 | 119.38 |
| Stage A | -8.6 | 157.84 | 70.097 | UL-RL | 0.2174.599 | 40 | 51 | 0 | 0 | 121.097 |
| Stage A | -8.7 | 159.307 | 70.816 | UL-RL | 0.2174.599 | 40 | 52 | 0 | 0 | 122.816 |
| Stage A | -8.8 | 160.854 | 71.576 | UL-RL | 0.2174.599 | 40 | 53 | 0 | 0 | 124.576 |
| Stage A | -8.9 | 162.319 | 72.296 | UL-RL | 0.2174.599 | 40 | 54 | 0 | 0 | 126.296 |
| Stage A | -9 | 163.863 | 73.058 | UL-RL | 0.2174.599 | 40 | 55 | 0 | 0 | 128.058 |
| Stage A | -9.1 | 165.326 | 73.781 | UL-RL | 0.2174.599 | 40 | 56 | 0 | 0 | 129.781 |
| Stage A | -9.2 | 166.79 | 74.506 | UL-RL | 0.2174.599 | 40 | 57 | 0 | 0 | 131.506 |
| Stage A | -9.3 | 168.33 | 75.271 | UL-RL | 0.2174.599 | 40 | 58 | 0 | 0 | 133.271 |
| Stage A | -9.4 | 169.792 | 75.998 | UL-RL | 0.2174.599 | 40 | 59 | 0 | 0 | 134.998 |
| Stage A | -9.5 | 171.254 | 76.727 | UL-RL | 0.2174.599 | 40 | 60 | 0 | 0 | 136.727 |
| Stage A | -9.6 | 172.64 | 77.42 | UL-RL | 0.2174.599 | 40 | 61 | 0 | 0 | 138.42 |
| Stage A | -9.7 | 174.028 | 78.114 | UL-RL | 0.2174.599 | 40 | 62 | 0 | 0 | 140.114 |
| Stage A | -9.8 | 175.416 | 78.809 | UL-RL | 0.2174.599 | 40 | 63 | 0 | 0 | 141.809 |
| Stage A | -9.9 | 176.805 | 79.505 | UL-RL | 0.2174.599 | 40 | 64 | 0 | 0 | 143.505 |
| Stage A | -10 | 178.195 | 80.202 | UL-RL | 0.2174.599 | 40 | 65 | 0 | 0 | 145.202 |

| Design Assumption: Nominal Risultati Terreno | | | Muro: | LEFT | Lato | RIGHT | | | | | |
|--|-------|---------------|---------------|---------|------------|-------|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage A | 0 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -0.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.5 | 0 | 0 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage A | -1.6 | 1.9 | 5.89 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 5.89 |
| Stage A | -1.7 | 3.8 | 11.78 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 11.78 |
| Stage A | -1.8 | 5.7 | 17.35 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.35 |
| Stage A | -1.9 | 7.6 | 17.174 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 17.174 |
| Stage A | -2 | 9.5 | 25.627 | V-C | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 25.627 |
| Stage A | -2.1 | 11.95 | 24.812 | V-C | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 24.812 |
| Stage A | -2.2 | 14.4 | 24.211 | V-C | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 24.211 |
| Stage A | -2.3 | 16.85 | 23.84 | V-C | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 23.84 |
| Stage A | -2.4 | 19.3 | 23.45 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 23.45 |
| Stage A | -2.5 | 21.75 | 22.855 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 22.855 |
| Stage A | -2.6 | 24.2 | 22.603 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 22.603 |
| Stage A | -2.7 | 26.65 | 22.665 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 22.665 |
| Stage A | -2.8 | 29.1 | 23.006 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 23.006 |
| Stage A | -2.9 | 31.55 | 23.591 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 23.591 |
| Stage A | -3 | 34 | 24.384 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 24.384 |
| Stage A | -3.1 | 36.45 | 25.35 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 25.35 |
| Stage A | -3.2 | 38.9 | 26.457 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 26.457 |
| Stage A | -3.3 | 41.35 | 27.676 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 27.676 |
| Stage A | -3.4 | 43.8 | 28.98 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 28.98 |
| Stage A | -3.5 | 46.25 | 30.346 | UL-RL | 0.2174.599 | 40 | 0 | 0 | 0 | 0 | 30.346 |
| Stage A | -3.6 | 47.7 | 31.242 | UL-RL | 0.2174.599 | 40 | 1 | 0 | 0 | 0 | 32.242 |
| Stage A | -3.7 | 49.15 | 32.166 | UL-RL | 0.2174.599 | 40 | 2 | 0 | 0 | 0 | 34.166 |
| Stage A | -3.8 | 50.6 | 33.105 | UL-RL | 0.2174.599 | 40 | 3 | 0 | 0 | 0 | 36.105 |
| Stage A | -3.9 | 52.05 | 34.049 | UL-RL | 0.2174.599 | 40 | 4 | 0 | 0 | 0 | 38.049 |
| Stage A | -4 | 53.5 | 34.988 | UL-RL | 0.2174.599 | 40 | 5 | 0 | 0 | 0 | 39.988 |
| Stage A | -4.1 | 54.95 | 35.919 | UL-RL | 0.2174.599 | 40 | 6 | 0 | 0 | 0 | 41.918 |
| Stage A | -4.2 | 56.4 | 36.835 | UL-RL | 0.2174.599 | 40 | 7 | 0 | 0 | 0 | 43.835 |
| Stage A | -4.3 | 57.85 | 37.734 | UL-RL | 0.2174.599 | 40 | 8 | 0 | 0 | 0 | 45.734 |
| Stage A | -4.4 | 59.3 | 38.616 | UL-RL | 0.2174.599 | 40 | 9 | 0 | 0 | 0 | 47.616 |
| Stage A | -4.5 | 60.75 | 39.479 | UL-RL | 0.2174.599 | 40 | 10 | 0 | 0 | 0 | 49.479 |
| Stage A | -4.6 | 62.2 | 40.324 | UL-RL | 0.2174.599 | 40 | 11 | 0 | 0 | 0 | 51.324 |
| Stage A | -4.7 | 63.65 | 41.153 | UL-RL | 0.2174.599 | 40 | 12 | 0 | 0 | 0 | 53.153 |
| Stage A | -4.8 | 65.1 | 41.965 | UL-RL | 0.2174.599 | 40 | 13 | 0 | 0 | 0 | 54.965 |
| Stage A | -4.9 | 66.55 | 42.763 | UL-RL | 0.2174.599 | 40 | 14 | 0 | 0 | 0 | 56.763 |
| Stage A | -5 | 68 | 43.548 | UL-RL | 0.2174.599 | 40 | 15 | 0 | 0 | 0 | 58.548 |
| Stage A | -5.1 | 69.45 | 44.321 | UL-RL | 0.2174.599 | 40 | 16 | 0 | 0 | 0 | 60.321 |
| Stage A | -5.2 | 70.9 | 45.086 | UL-RL | 0.2174.599 | 40 | 17 | 0 | 0 | 0 | 62.086 |
| Stage A | -5.3 | 72.35 | 45.842 | UL-RL | 0.2174.599 | 40 | 18 | 0 | 0 | 0 | 63.842 |
| Stage A | -5.4 | 73.8 | 46.592 | UL-RL | 0.2174.599 | 40 | 19 | 0 | 0 | 0 | 65.592 |
| Stage A | -5.5 | 75.25 | 47.337 | UL-RL | 0.2174.599 | 40 | 20 | 0 | 0 | 0 | 67.337 |
| Stage A | -5.6 | 76.7 | 48.077 | UL-RL | 0.2174.599 | 40 | 21 | 0 | 0 | 0 | 69.077 |
| Stage A | -5.7 | 78.15 | 48.814 | UL-RL | 0.2174.599 | 40 | 22 | 0 | 0 | 0 | 70.814 |
| Stage A | -5.8 | 79.6 | 49.55 | UL-RL | 0.2174.599 | 40 | 23 | 0 | 0 | 0 | 72.55 |
| Stage A | -5.9 | 81.05 | 50.283 | UL-RL | 0.2174.599 | 40 | 24 | 0 | 0 | 0 | 74.283 |
| Stage A | -6 | 82.5 | 51.016 | UL-RL | 0.2174.599 | 40 | 25 | 0 | 0 | 0 | 76.016 |
| Stage A | -6.1 | 83.95 | 51.748 | UL-RL | 0.2174.599 | 40 | 26 | 0 | 0 | 0 | 77.748 |
| Stage A | -6.2 | 85.4 | 52.48 | UL-RL | 0.2174.599 | 40 | 27 | 0 | 0 | 0 | 79.48 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|-------|------------|------|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT | | Lato | | RIGHT | | | |
| | | | | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage A | -6.3 | 86.85 | 53.212 | UL-RL | 0.2174.599 | | 40 | 28 | 0 | 0 | 81.212 |
| Stage A | -6.4 | 88.3 | 53.944 | UL-RL | 0.2174.599 | | 40 | 29 | 0 | 0 | 82.944 |
| Stage A | -6.5 | 89.75 | 54.676 | UL-RL | 0.2174.599 | | 40 | 30 | 0 | 0 | 84.676 |
| Stage A | -6.6 | 91.2 | 55.409 | UL-RL | 0.2174.599 | | 40 | 31 | 0 | 0 | 86.409 |
| Stage A | -6.7 | 92.65 | 56.142 | UL-RL | 0.2174.599 | | 40 | 32 | 0 | 0 | 88.142 |
| Stage A | -6.8 | 94.1 | 56.876 | UL-RL | 0.2174.599 | | 40 | 33 | 0 | 0 | 89.876 |
| Stage A | -6.9 | 95.55 | 57.61 | UL-RL | 0.2174.599 | | 40 | 34 | 0 | 0 | 91.61 |
| Stage A | -7 | 97 | 58.344 | UL-RL | 0.2174.599 | | 40 | 35 | 0 | 0 | 93.344 |
| Stage A | -7.1 | 98.45 | 59.079 | UL-RL | 0.2174.599 | | 40 | 36 | 0 | 0 | 95.079 |
| Stage A | -7.2 | 99.9 | 59.814 | UL-RL | 0.2174.599 | | 40 | 37 | 0 | 0 | 96.814 |
| Stage A | -7.3 | 101.35 | 60.549 | UL-RL | 0.2174.599 | | 40 | 38 | 0 | 0 | 98.549 |
| Stage A | -7.4 | 102.8 | 61.284 | UL-RL | 0.2174.599 | | 40 | 39 | 0 | 0 | 100.284 |
| Stage A | -7.5 | 104.25 | 62.019 | UL-RL | 0.2174.599 | | 40 | 40 | 0 | 0 | 102.019 |
| Stage A | -7.6 | 105.7 | 62.754 | UL-RL | 0.2174.599 | | 40 | 41 | 0 | 0 | 103.754 |
| Stage A | -7.7 | 107.15 | 63.489 | UL-RL | 0.2174.599 | | 40 | 42 | 0 | 0 | 105.489 |
| Stage A | -7.8 | 108.6 | 64.224 | UL-RL | 0.2174.599 | | 40 | 43 | 0 | 0 | 107.224 |
| Stage A | -7.9 | 110.05 | 64.959 | UL-RL | 0.2174.599 | | 40 | 44 | 0 | 0 | 108.959 |
| Stage A | -8 | 111.5 | 65.694 | UL-RL | 0.2174.599 | | 40 | 45 | 0 | 0 | 110.694 |
| Stage A | -8.1 | 112.95 | 66.428 | UL-RL | 0.2174.599 | | 40 | 46 | 0 | 0 | 112.428 |
| Stage A | -8.2 | 114.4 | 67.163 | UL-RL | 0.2174.599 | | 40 | 47 | 0 | 0 | 114.162 |
| Stage A | -8.3 | 115.85 | 67.897 | UL-RL | 0.2174.599 | | 40 | 48 | 0 | 0 | 115.897 |
| Stage A | -8.4 | 117.3 | 68.63 | UL-RL | 0.2174.599 | | 40 | 49 | 0 | 0 | 117.63 |
| Stage A | -8.5 | 118.75 | 69.364 | UL-RL | 0.2174.599 | | 40 | 50 | 0 | 0 | 119.364 |
| Stage A | -8.6 | 120.2 | 70.097 | UL-RL | 0.2174.599 | | 40 | 51 | 0 | 0 | 121.097 |
| Stage A | -8.7 | 121.65 | 70.83 | UL-RL | 0.2174.599 | | 40 | 52 | 0 | 0 | 122.83 |
| Stage A | -8.8 | 123.1 | 71.562 | UL-RL | 0.2174.599 | | 40 | 53 | 0 | 0 | 124.562 |
| Stage A | -8.9 | 124.55 | 72.294 | UL-RL | 0.2174.599 | | 40 | 54 | 0 | 0 | 126.294 |
| Stage A | -9 | 126 | 73.025 | UL-RL | 0.2174.599 | | 40 | 55 | 0 | 0 | 128.025 |
| Stage A | -9.1 | 127.45 | 73.756 | UL-RL | 0.2174.599 | | 40 | 56 | 0 | 0 | 129.756 |
| Stage A | -9.2 | 128.9 | 74.486 | UL-RL | 0.2174.599 | | 40 | 57 | 0 | 0 | 131.486 |
| Stage A | -9.3 | 130.35 | 75.215 | UL-RL | 0.2174.599 | | 40 | 58 | 0 | 0 | 133.215 |
| Stage A | -9.4 | 131.8 | 75.944 | UL-RL | 0.2174.599 | | 40 | 59 | 0 | 0 | 134.944 |
| Stage A | -9.5 | 133.25 | 76.673 | UL-RL | 0.2174.599 | | 40 | 60 | 0 | 0 | 136.673 |
| Stage A | -9.6 | 134.7 | 77.401 | UL-RL | 0.2174.599 | | 40 | 61 | 0 | 0 | 138.401 |
| Stage A | -9.7 | 136.15 | 78.129 | UL-RL | 0.2174.599 | | 40 | 62 | 0 | 0 | 140.129 |
| Stage A | -9.8 | 137.6 | 78.857 | UL-RL | 0.2174.599 | | 40 | 63 | 0 | 0 | 141.857 |
| Stage A | -9.9 | 139.05 | 79.584 | UL-RL | 0.2174.599 | | 40 | 64 | 0 | 0 | 143.584 |
| Stage A | -10 | 140.5 | 80.311 | UL-RL | 0.2174.599 | | 40 | 65 | 0 | 0 | 145.311 |

Tabella Risultati Terreno Left Wall - Nominal - Stage B

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|---------------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Kp | LEFT Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage B | 0 | 0 | 0 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 |
| Stage B | -0.1 | 1.9 | 5.891 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 5.891 |
| Stage B | -0.2 | 3.803 | 11.788 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 11.788 |
| Stage B | -0.3 | 5.709 | 17.698 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 17.698 |
| Stage B | -0.4 | 7.621 | 22.679 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 22.679 |
| Stage B | -0.5 | 9.541 | 23.568 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 23.568 |
| Stage B | -0.6 | 11.469 | 24.435 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 24.435 |
| Stage B | -0.7 | 13.406 | 25.264 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 25.264 |
| Stage B | -0.8 | 15.353 | 26.035 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 26.035 |
| Stage B | -0.9 | 17.311 | 26.72 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 26.72 |
| Stage B | -1 | 19.278 | 27.288 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.288 |
| Stage B | -1.1 | 21.256 | 27.704 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.704 |
| Stage B | -1.2 | 23.242 | 27.927 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.927 |
| Stage B | -1.3 | 25.237 | 27.91 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.91 |
| Stage B | -1.4 | 27.24 | 27.623 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.623 |
| Stage B | -1.5 | 29.25 | 27.116 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.116 |
| Stage B | -1.6 | 31.265 | 26.451 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 26.451 |
| Stage B | -1.7 | 33.286 | 25.691 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 25.691 |
| Stage B | -1.8 | 35.31 | 24.89 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 24.89 |
| Stage B | -1.9 | 37.337 | 24.098 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 24.098 |
| Stage B | -2 | 39.367 | 34.523 | V-C | 0.2174.599 | | 40 | 0 | 0 | 34.523 |
| Stage B | -2.1 | 41.948 | 30.204 | V-C | 0.2174.599 | | 40 | 0 | 0 | 30.204 |
| Stage B | -2.2 | 44.529 | 26.283 | V-C | 0.2174.599 | | 40 | 0 | 0 | 26.283 |
| Stage B | -2.3 | 47.111 | 22.377 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 22.377 |
| Stage B | -2.4 | 49.692 | 22.37 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 22.37 |
| Stage B | -2.5 | 52.272 | 23.344 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 23.344 |
| Stage B | -2.6 | 54.85 | 24.247 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 24.247 |
| Stage B | -2.7 | 57.427 | 25.108 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 25.108 |
| Stage B | -2.8 | 60.001 | 25.951 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 25.951 |
| Stage B | -2.9 | 62.573 | 26.795 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 26.795 |
| Stage B | -3 | 65.143 | 27.652 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 27.652 |
| Stage B | -3.1 | 67.9 | 28.628 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 28.628 |
| Stage B | -3.2 | 70.524 | 29.567 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 29.567 |
| Stage B | -3.3 | 73.141 | 30.537 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 30.537 |
| Stage B | -3.4 | 75.96 | 31.644 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 31.644 |
| Stage B | -3.5 | 78.558 | 32.675 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 32.675 |
| Stage B | -3.6 | 80.348 | 33.337 | UL-RL | 0.2174.599 | | 40 | 1 | 0 | 34.337 |
| Stage B | -3.7 | 81.929 | 33.927 | UL-RL | 0.2174.599 | | 40 | 2 | 0 | 35.927 |
| Stage B | -3.8 | 83.505 | 34.545 | UL-RL | 0.2174.599 | | 40 | 3 | 0 | 37.545 |
| Stage B | -3.9 | 85.26 | 35.278 | UL-RL | 0.2174.599 | | 40 | 4 | 0 | 39.278 |
| Stage B | -4 | 86.823 | 35.938 | UL-RL | 0.2174.599 | | 40 | 5 | 0 | 40.938 |
| Stage B | -4.1 | 88.382 | 36.617 | UL-RL | 0.2174.599 | | 40 | 6 | 0 | 42.617 |
| Stage B | -4.2 | 90.108 | 37.396 | UL-RL | 0.2174.599 | | 40 | 7 | 0 | 44.396 |
| Stage B | -4.3 | 91.656 | 38.101 | UL-RL | 0.2174.599 | | 40 | 8 | 0 | 46.1 |
| Stage B | -4.4 | 93.363 | 38.896 | UL-RL | 0.2174.599 | | 40 | 9 | 0 | 47.896 |
| Stage B | -4.5 | 94.901 | 39.617 | UL-RL | 0.2174.599 | | 40 | 10 | 0 | 49.617 |
| Stage B | -4.6 | 96.436 | 40.344 | UL-RL | 0.2174.599 | | 40 | 11 | 0 | 51.344 |
| Stage B | -4.7 | 98.121 | 41.151 | UL-RL | 0.2174.599 | | 40 | 12 | 0 | 53.151 |
| Stage B | -4.8 | 99.648 | 41.883 | UL-RL | 0.2174.599 | | 40 | 13 | 0 | 54.883 |
| Stage B | -4.9 | 101.319 | 42.691 | UL-RL | 0.2174.599 | | 40 | 14 | 0 | 56.691 |
| Stage B | -5 | 102.839 | 43.424 | UL-RL | 0.2174.599 | | 40 | 15 | 0 | 58.424 |
| Stage B | -5.1 | 104.357 | 44.158 | UL-RL | 0.2174.599 | | 40 | 16 | 0 | 60.158 |
| Stage B | -5.2 | 106.011 | 44.961 | UL-RL | 0.2174.599 | | 40 | 17 | 0 | 61.961 |
| Stage B | -5.3 | 107.522 | 45.692 | UL-RL | 0.2174.599 | | 40 | 18 | 0 | 63.692 |
| Stage B | -5.4 | 109.165 | 46.489 | UL-RL | 0.2174.599 | | 40 | 19 | 0 | 65.489 |
| Stage B | -5.5 | 110.671 | 47.218 | UL-RL | 0.2174.599 | | 40 | 20 | 0 | 67.218 |
| Stage B | -5.6 | 112.176 | 47.946 | UL-RL | 0.2174.599 | | 40 | 21 | 0 | 68.946 |
| Stage B | -5.7 | 113.804 | 48.735 | UL-RL | 0.2174.599 | | 40 | 22 | 0 | 70.735 |
| Stage B | -5.8 | 115.304 | 49.459 | UL-RL | 0.2174.599 | | 40 | 23 | 0 | 72.459 |
| Stage B | -5.9 | 116.802 | 50.182 | UL-RL | 0.2174.599 | | 40 | 24 | 0 | 74.182 |
| Stage B | -6 | 118.419 | 50.964 | UL-RL | 0.2174.599 | | 40 | 25 | 0 | 75.964 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|------------|------------|---------|----------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT Stato | Lato Ka | LEFT Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage B | -6.1 | 119.914 | 51.685 | UL-RL | 0.2174.599 | | 40 | 26 | 0 | 77.685 |
| Stage B | -6.2 | 121.522 | 52.463 | UL-RL | 0.2174.599 | | 40 | 27 | 0 | 79.463 |
| Stage B | -6.3 | 123.013 | 53.181 | UL-RL | 0.2174.599 | | 40 | 28 | 0 | 81.181 |
| Stage B | -6.4 | 124.502 | 53.899 | UL-RL | 0.2174.599 | | 40 | 29 | 0 | 82.899 |
| Stage B | -6.5 | 126.101 | 54.672 | UL-RL | 0.2174.599 | | 40 | 30 | 0 | 84.672 |
| Stage B | -6.6 | 127.587 | 55.389 | UL-RL | 0.2174.599 | | 40 | 31 | 0 | 86.389 |
| Stage B | -6.7 | 129.179 | 56.159 | UL-RL | 0.2174.599 | | 40 | 32 | 0 | 88.159 |
| Stage B | -6.8 | 130.662 | 56.875 | UL-RL | 0.2174.599 | | 40 | 33 | 0 | 89.875 |
| Stage B | -6.9 | 132.145 | 57.591 | UL-RL | 0.2174.599 | | 40 | 34 | 0 | 91.591 |
| Stage B | -7 | 133.729 | 58.359 | UL-RL | 0.2174.599 | | 40 | 35 | 0 | 93.359 |
| Stage B | -7.1 | 135.208 | 59.075 | UL-RL | 0.2174.599 | | 40 | 36 | 0 | 95.075 |
| Stage B | -7.2 | 136.787 | 59.84 | UL-RL | 0.2174.599 | | 40 | 37 | 0 | 96.84 |
| Stage B | -7.3 | 138.264 | 60.556 | UL-RL | 0.2174.599 | | 40 | 38 | 0 | 98.556 |
| Stage B | -7.4 | 139.741 | 61.272 | UL-RL | 0.2174.599 | | 40 | 39 | 0 | 100.272 |
| Stage B | -7.5 | 141.312 | 62.036 | UL-RL | 0.2174.599 | | 40 | 40 | 0 | 102.036 |
| Stage B | -7.6 | 142.787 | 62.752 | UL-RL | 0.2174.599 | | 40 | 41 | 0 | 103.751 |
| Stage B | -7.7 | 144.26 | 63.467 | UL-RL | 0.2174.599 | | 40 | 42 | 0 | 105.467 |
| Stage B | -7.8 | 145.826 | 64.23 | UL-RL | 0.2174.599 | | 40 | 43 | 0 | 107.23 |
| Stage B | -7.9 | 147.298 | 64.945 | UL-RL | 0.2174.599 | | 40 | 44 | 0 | 108.945 |
| Stage B | -8 | 148.859 | 65.706 | UL-RL | 0.2174.599 | | 40 | 45 | 0 | 110.706 |
| Stage B | -8.1 | 150.329 | 66.423 | UL-RL | 0.2174.599 | | 40 | 46 | 0 | 112.422 |
| Stage B | -8.2 | 151.798 | 67.139 | UL-RL | 0.2174.599 | | 40 | 47 | 0 | 114.139 |
| Stage B | -8.3 | 153.354 | 67.899 | UL-RL | 0.2174.599 | | 40 | 48 | 0 | 115.899 |
| Stage B | -8.4 | 154.822 | 68.616 | UL-RL | 0.2174.599 | | 40 | 49 | 0 | 117.616 |
| Stage B | -8.5 | 156.374 | 69.376 | UL-RL | 0.2174.599 | | 40 | 50 | 0 | 119.376 |
| Stage B | -8.6 | 157.84 | 70.094 | UL-RL | 0.2174.599 | | 40 | 51 | 0 | 121.094 |
| Stage B | -8.7 | 159.307 | 70.813 | UL-RL | 0.2174.599 | | 40 | 52 | 0 | 122.813 |
| Stage B | -8.8 | 160.854 | 71.574 | UL-RL | 0.2174.599 | | 40 | 53 | 0 | 124.574 |
| Stage B | -8.9 | 162.319 | 72.295 | UL-RL | 0.2174.599 | | 40 | 54 | 0 | 126.295 |
| Stage B | -9 | 163.863 | 73.057 | UL-RL | 0.2174.599 | | 40 | 55 | 0 | 128.057 |
| Stage B | -9.1 | 165.326 | 73.781 | UL-RL | 0.2174.599 | | 40 | 56 | 0 | 129.781 |
| Stage B | -9.2 | 166.79 | 74.506 | UL-RL | 0.2174.599 | | 40 | 57 | 0 | 131.506 |
| Stage B | -9.3 | 168.33 | 75.271 | UL-RL | 0.2174.599 | | 40 | 58 | 0 | 133.271 |
| Stage B | -9.4 | 169.792 | 75.998 | UL-RL | 0.2174.599 | | 40 | 59 | 0 | 134.998 |
| Stage B | -9.5 | 171.254 | 76.728 | UL-RL | 0.2174.599 | | 40 | 60 | 0 | 136.728 |
| Stage B | -9.6 | 172.64 | 77.42 | UL-RL | 0.2174.599 | | 40 | 61 | 0 | 138.42 |
| Stage B | -9.7 | 174.028 | 78.115 | UL-RL | 0.2174.599 | | 40 | 62 | 0 | 140.115 |
| Stage B | -9.8 | 175.416 | 78.81 | UL-RL | 0.2174.599 | | 40 | 63 | 0 | 141.81 |
| Stage B | -9.9 | 176.805 | 79.506 | UL-RL | 0.2174.599 | | 40 | 64 | 0 | 143.506 |
| Stage B | -10 | 178.195 | 80.203 | UL-RL | 0.2174.599 | | 40 | 65 | 0 | 145.203 |

| Design Assumption: Nominal Risultati Terreno | | | Muro: | LEFT | Lato | RIGHT | | | | | |
|--|-------|---------------|---------------|---------|------------|-------|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage B | 0 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -0.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.5 | 0 | 0 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0 |
| Stage B | -1.6 | 1.9 | 0.608 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 0.608 |
| Stage B | -1.7 | 3.8 | 1.216 | ACTIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 1.216 |
| Stage B | -1.8 | 5.7 | 7.631 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 7.631 |
| Stage B | -1.9 | 7.6 | 8.824 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 0 | 8.824 |
| Stage B | -2 | 9.5 | 6.741 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 6.741 |
| Stage B | -2.1 | 11.95 | 9.269 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 9.269 |
| Stage B | -2.2 | 14.4 | 11.732 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 11.732 |
| Stage B | -2.3 | 16.85 | 14.109 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 14.109 |
| Stage B | -2.4 | 19.3 | 16.128 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 16.128 |
| Stage B | -2.5 | 21.75 | 17.603 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 17.603 |
| Stage B | -2.6 | 24.2 | 19.09 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 19.09 |
| Stage B | -2.7 | 26.65 | 20.581 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 20.581 |
| Stage B | -2.8 | 29.1 | 22.067 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 22.067 |
| Stage B | -2.9 | 31.55 | 23.543 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 23.543 |
| Stage B | -3 | 34 | 25.005 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 25.005 |
| Stage B | -3.1 | 36.45 | 26.449 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 26.449 |
| Stage B | -3.2 | 38.9 | 27.874 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 27.874 |
| Stage B | -3.3 | 41.35 | 29.278 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 29.278 |
| Stage B | -3.4 | 43.8 | 30.663 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 30.663 |
| Stage B | -3.5 | 46.25 | 32.029 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0 | 32.029 |
| Stage B | -3.6 | 47.7 | 32.863 | UL-RL | 0.2174.599 | | 40 | 1 | 0 | 0 | 33.863 |
| Stage B | -3.7 | 49.15 | 33.682 | UL-RL | 0.2174.599 | | 40 | 2 | 0 | 0 | 35.682 |
| Stage B | -3.8 | 50.6 | 34.488 | UL-RL | 0.2174.599 | | 40 | 3 | 0 | 0 | 37.488 |
| Stage B | -3.9 | 52.05 | 35.281 | UL-RL | 0.2174.599 | | 40 | 4 | 0 | 0 | 39.281 |
| Stage B | -4 | 53.5 | 36.063 | UL-RL | 0.2174.599 | | 40 | 5 | 0 | 0 | 41.063 |
| Stage B | -4.1 | 54.95 | 36.836 | UL-RL | 0.2174.599 | | 40 | 6 | 0 | 0 | 42.836 |
| Stage B | -4.2 | 56.4 | 37.602 | UL-RL | 0.2174.599 | | 40 | 7 | 0 | 0 | 44.602 |
| Stage B | -4.3 | 57.85 | 38.361 | UL-RL | 0.2174.599 | | 40 | 8 | 0 | 0 | 46.361 |
| Stage B | -4.4 | 59.3 | 39.114 | UL-RL | 0.2174.599 | | 40 | 9 | 0 | 0 | 48.114 |
| Stage B | -4.5 | 60.75 | 39.864 | UL-RL | 0.2174.599 | | 40 | 10 | 0 | 0 | 49.864 |
| Stage B | -4.6 | 62.2 | 40.61 | UL-RL | 0.2174.599 | | 40 | 11 | 0 | 0 | 51.61 |
| Stage B | -4.7 | 63.65 | 41.353 | UL-RL | 0.2174.599 | | 40 | 12 | 0 | 0 | 53.353 |
| Stage B | -4.8 | 65.1 | 42.095 | UL-RL | 0.2174.599 | | 40 | 13 | 0 | 0 | 55.095 |
| Stage B | -4.9 | 66.55 | 42.835 | UL-RL | 0.2174.599 | | 40 | 14 | 0 | 0 | 56.835 |
| Stage B | -5 | 68 | 43.574 | UL-RL | 0.2174.599 | | 40 | 15 | 0 | 0 | 58.574 |
| Stage B | -5.1 | 69.45 | 44.313 | UL-RL | 0.2174.599 | | 40 | 16 | 0 | 0 | 60.313 |
| Stage B | -5.2 | 70.9 | 45.051 | UL-RL | 0.2174.599 | | 40 | 17 | 0 | 0 | 62.051 |
| Stage B | -5.3 | 72.35 | 45.789 | UL-RL | 0.2174.599 | | 40 | 18 | 0 | 0 | 63.789 |
| Stage B | -5.4 | 73.8 | 46.528 | UL-RL | 0.2174.599 | | 40 | 19 | 0 | 0 | 65.528 |
| Stage B | -5.5 | 75.25 | 47.266 | UL-RL | 0.2174.599 | | 40 | 20 | 0 | 0 | 67.266 |
| Stage B | -5.6 | 76.7 | 48.004 | UL-RL | 0.2174.599 | | 40 | 21 | 0 | 0 | 69.004 |
| Stage B | -5.7 | 78.15 | 48.742 | UL-RL | 0.2174.599 | | 40 | 22 | 0 | 0 | 70.742 |
| Stage B | -5.8 | 79.6 | 49.481 | UL-RL | 0.2174.599 | | 40 | 23 | 0 | 0 | 72.481 |
| Stage B | -5.9 | 81.05 | 50.219 | UL-RL | 0.2174.599 | | 40 | 24 | 0 | 0 | 74.219 |
| Stage B | -6 | 82.5 | 50.958 | UL-RL | 0.2174.599 | | 40 | 25 | 0 | 0 | 75.958 |
| Stage B | -6.1 | 83.95 | 51.697 | UL-RL | 0.2174.599 | | 40 | 26 | 0 | 0 | 77.697 |
| Stage B | -6.2 | 85.4 | 52.436 | UL-RL | 0.2174.599 | | 40 | 27 | 0 | 0 | 79.435 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------------|-------|------------|------|----------------|------------|--------------------|-----------|--|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT | | Lato | | RIGHT | | | |
| | | | | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage B | -6.3 | 86.85 | 53.174 | UL-RL | 0.2174.599 | 40 | 28 | 0 | 0 | 81.174 | |
| Stage B | -6.4 | 88.3 | 53.913 | UL-RL | 0.2174.599 | 40 | 29 | 0 | 0 | 82.913 | |
| Stage B | -6.5 | 89.75 | 54.651 | UL-RL | 0.2174.599 | 40 | 30 | 0 | 0 | 84.651 | |
| Stage B | -6.6 | 91.2 | 55.389 | UL-RL | 0.2174.599 | 40 | 31 | 0 | 0 | 86.389 | |
| Stage B | -6.7 | 92.65 | 56.127 | UL-RL | 0.2174.599 | 40 | 32 | 0 | 0 | 88.127 | |
| Stage B | -6.8 | 94.1 | 56.865 | UL-RL | 0.2174.599 | 40 | 33 | 0 | 0 | 89.865 | |
| Stage B | -6.9 | 95.55 | 57.602 | UL-RL | 0.2174.599 | 40 | 34 | 0 | 0 | 91.602 | |
| Stage B | -7 | 97 | 58.339 | UL-RL | 0.2174.599 | 40 | 35 | 0 | 0 | 93.339 | |
| Stage B | -7.1 | 98.45 | 59.076 | UL-RL | 0.2174.599 | 40 | 36 | 0 | 0 | 95.076 | |
| Stage B | -7.2 | 99.9 | 59.813 | UL-RL | 0.2174.599 | 40 | 37 | 0 | 0 | 96.813 | |
| Stage B | -7.3 | 101.35 | 60.549 | UL-RL | 0.2174.599 | 40 | 38 | 0 | 0 | 98.549 | |
| Stage B | -7.4 | 102.8 | 61.285 | UL-RL | 0.2174.599 | 40 | 39 | 0 | 0 | 100.285 | |
| Stage B | -7.5 | 104.25 | 62.021 | UL-RL | 0.2174.599 | 40 | 40 | 0 | 0 | 102.021 | |
| Stage B | -7.6 | 105.7 | 62.757 | UL-RL | 0.2174.599 | 40 | 41 | 0 | 0 | 103.757 | |
| Stage B | -7.7 | 107.15 | 63.492 | UL-RL | 0.2174.599 | 40 | 42 | 0 | 0 | 105.492 | |
| Stage B | -7.8 | 108.6 | 64.227 | UL-RL | 0.2174.599 | 40 | 43 | 0 | 0 | 107.227 | |
| Stage B | -7.9 | 110.05 | 64.962 | UL-RL | 0.2174.599 | 40 | 44 | 0 | 0 | 108.962 | |
| Stage B | -8 | 111.5 | 65.697 | UL-RL | 0.2174.599 | 40 | 45 | 0 | 0 | 110.697 | |
| Stage B | -8.1 | 112.95 | 66.431 | UL-RL | 0.2174.599 | 40 | 46 | 0 | 0 | 112.431 | |
| Stage B | -8.2 | 114.4 | 67.165 | UL-RL | 0.2174.599 | 40 | 47 | 0 | 0 | 114.165 | |
| Stage B | -8.3 | 115.85 | 67.899 | UL-RL | 0.2174.599 | 40 | 48 | 0 | 0 | 115.899 | |
| Stage B | -8.4 | 117.3 | 68.632 | UL-RL | 0.2174.599 | 40 | 49 | 0 | 0 | 117.632 | |
| Stage B | -8.5 | 118.75 | 69.365 | UL-RL | 0.2174.599 | 40 | 50 | 0 | 0 | 119.365 | |
| Stage B | -8.6 | 120.2 | 70.098 | UL-RL | 0.2174.599 | 40 | 51 | 0 | 0 | 121.098 | |
| Stage B | -8.7 | 121.65 | 70.831 | UL-RL | 0.2174.599 | 40 | 52 | 0 | 0 | 122.831 | |
| Stage B | -8.8 | 123.1 | 71.563 | UL-RL | 0.2174.599 | 40 | 53 | 0 | 0 | 124.563 | |
| Stage B | -8.9 | 124.55 | 72.294 | UL-RL | 0.2174.599 | 40 | 54 | 0 | 0 | 126.294 | |
| Stage B | -9 | 126 | 73.025 | UL-RL | 0.2174.599 | 40 | 55 | 0 | 0 | 128.025 | |
| Stage B | -9.1 | 127.45 | 73.756 | UL-RL | 0.2174.599 | 40 | 56 | 0 | 0 | 129.756 | |
| Stage B | -9.2 | 128.9 | 74.486 | UL-RL | 0.2174.599 | 40 | 57 | 0 | 0 | 131.486 | |
| Stage B | -9.3 | 130.35 | 75.215 | UL-RL | 0.2174.599 | 40 | 58 | 0 | 0 | 133.215 | |
| Stage B | -9.4 | 131.8 | 75.944 | UL-RL | 0.2174.599 | 40 | 59 | 0 | 0 | 134.944 | |
| Stage B | -9.5 | 133.25 | 76.673 | UL-RL | 0.2174.599 | 40 | 60 | 0 | 0 | 136.673 | |
| Stage B | -9.6 | 134.7 | 77.401 | UL-RL | 0.2174.599 | 40 | 61 | 0 | 0 | 138.401 | |
| Stage B | -9.7 | 136.15 | 78.129 | UL-RL | 0.2174.599 | 40 | 62 | 0 | 0 | 140.129 | |
| Stage B | -9.8 | 137.6 | 78.856 | UL-RL | 0.2174.599 | 40 | 63 | 0 | 0 | 141.856 | |
| Stage B | -9.9 | 139.05 | 79.584 | UL-RL | 0.2174.599 | 40 | 64 | 0 | 0 | 143.584 | |
| Stage B | -10 | 140.5 | 80.311 | UL-RL | 0.2174.599 | 40 | 65 | 0 | 0 | 145.311 | |

Tabella Risultati Terreno Left Wall - Nominal - Stage 3-

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | |
|--|-------|---------------|---------------------|---------|------------|------|----------------|------------|--------------------|-----------|
| Stage | Z (m) | Sigma V (kPa) | Muro: Sigma H (kPa) | LEFT | | Lato | | LEFT | | |
| | | | | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) |
| Stage 3- | 0 | 0 | 0 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.1 | 1.9 | 5.891 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 5.891 |
| Stage 3- | -0.2 | 3.803 | 11.788 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 11.788 |
| Stage 3- | -0.3 | 5.709 | 17.698 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 17.698 |
| Stage 3- | -0.4 | 7.621 | 23.626 | PASSIVE | 0.32 | 3.1 | 0 | 0 | 0 | 23.626 |
| Stage 3- | -0.5 | 9.541 | 25.578 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 25.578 |
| Stage 3- | -0.6 | 11.469 | 26.162 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 26.162 |
| Stage 3- | -0.7 | 13.406 | 26.707 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 26.707 |
| Stage 3- | -0.8 | 15.353 | 27.193 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.193 |
| Stage 3- | -0.9 | 17.311 | 27.593 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.593 |
| Stage 3- | -1 | 19.278 | 27.875 | V-C | 0.32 | 3.1 | 0 | 0 | 0 | 27.875 |
| Stage 3- | -1.1 | 21.256 | 28.001 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 28.001 |
| Stage 3- | -1.2 | 23.242 | 27.93 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 27.93 |
| Stage 3- | -1.3 | 25.237 | 27.448 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 27.448 |
| Stage 3- | -1.4 | 27.24 | 26.684 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 26.684 |
| Stage 3- | -1.5 | 29.25 | 25.691 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 25.691 |
| Stage 3- | -1.6 | 31.265 | 24.534 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 24.534 |
| Stage 3- | -1.7 | 33.286 | 23.272 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 23.272 |
| Stage 3- | -1.8 | 35.31 | 21.96 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 21.96 |
| Stage 3- | -1.9 | 37.337 | 20.647 | UL-RL | 0.32 | 3.1 | 0 | 0 | 0 | 20.647 |
| Stage 3- | -2 | 39.367 | 21.185 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 21.185 |
| Stage 3- | -2.1 | 41.948 | 15.047 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 15.047 |
| Stage 3- | -2.2 | 44.529 | 9.264 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 9.264 |
| Stage 3- | -2.3 | 47.111 | 3.454 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 3.454 |
| Stage 3- | -2.4 | 49.692 | 1.501 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 1.501 |
| Stage 3- | -2.5 | 52.272 | 0.491 | UL-RL | 0.2174.599 | | 40 | 0 | 0 | 0.491 |
| Stage 3- | -2.6 | 54.85 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -2.7 | 57.427 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -2.8 | 60.001 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -2.9 | 62.573 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3 | 65.143 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.1 | 67.9 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.2 | 70.524 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.3 | 73.141 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.4 | 75.96 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.5 | 78.558 | 0 | ACTIVE | 0.2174.599 | | 40 | 0 | 0 | 0 |
| Stage 3- | -3.6 | 80.508 | 0 | ACTIVE | 0.2174.599 | | 40 | 0.839 | 0.161 | 0.839 |
| Stage 3- | -3.7 | 82.25 | 0 | ACTIVE | 0.2174.599 | | 40 | 1.679 | 0.161 | 1.679 |
| Stage 3- | -3.8 | 83.988 | 0 | ACTIVE | 0.2174.599 | | 40 | 2.518 | 0.161 | 2.518 |
| Stage 3- | -3.9 | 85.903 | 0 | ACTIVE | 0.2174.599 | | 40 | 3.357 | 0.161 | 3.357 |
| Stage 3- | -4 | 87.627 | 0 | ACTIVE | 0.2174.599 | | 40 | 4.196 | 0.161 | 4.196 |
| Stage 3- | -4.1 | 89.346 | 0 | ACTIVE | 0.2174.599 | | 40 | 5.036 | 0.161 | 5.036 |
| Stage 3- | -4.2 | 91.233 | 0 | ACTIVE | 0.2174.599 | | 40 | 5.875 | 0.161 | 5.875 |
| Stage 3- | -4.3 | 92.941 | 0 | ACTIVE | 0.2174.599 | | 40 | 6.714 | 0.161 | 6.714 |
| Stage 3- | -4.4 | 94.809 | 0 | ACTIVE | 0.2174.599 | | 40 | 7.554 | 0.161 | 7.554 |
| Stage 3- | -4.5 | 96.508 | 0 | ACTIVE | 0.2174.599 | | 40 | 8.393 | 0.161 | 8.393 |
| Stage 3- | -4.6 | 98.204 | 0 | ACTIVE | 0.2174.599 | | 40 | 9.232 | 0.161 | 9.232 |
| Stage 3- | -4.7 | 100.05 | 0 | ACTIVE | 0.2174.599 | | 40 | 10.071 | 0.161 | 10.071 |
| Stage 3- | -4.8 | 101.738 | 0 | ACTIVE | 0.2174.599 | | 40 | 10.911 | 0.161 | 10.911 |
| Stage 3- | -4.9 | 103.569 | 0 | ACTIVE | 0.2174.599 | | 40 | 11.75 | 0.161 | 11.75 |
| Stage 3- | -5 | 105.25 | 0 | ACTIVE | 0.2174.599 | | 40 | 12.589 | 0.161 | 12.589 |
| Stage 3- | -5.1 | 106.928 | 0 | ACTIVE | 0.2174.599 | | 40 | 13.429 | 0.161 | 13.429 |
| Stage 3- | -5.2 | 108.743 | 0 | ACTIVE | 0.2174.599 | | 40 | 14.268 | 0.161 | 14.268 |
| Stage 3- | -5.3 | 110.415 | 0 | ACTIVE | 0.2174.599 | | 40 | 15.107 | 0.161 | 15.107 |
| Stage 3- | -5.4 | 112.218 | 1.751 | UL-RL | 0.2174.599 | | 40 | 15.946 | 0.161 | 17.697 |
| Stage 3- | -5.5 | 113.885 | 3.982 | UL-RL | 0.2174.599 | | 40 | 16.786 | 0.161 | 20.768 |
| Stage 3- | -5.6 | 115.55 | 6.238 | UL-RL | 0.2174.599 | | 40 | 17.625 | 0.161 | 23.863 |
| Stage 3- | -5.7 | 117.34 | 8.555 | UL-RL | 0.2174.599 | | 40 | 18.464 | 0.161 | 27.019 |
| Stage 3- | -5.8 | 119 | 10.784 | UL-RL | 0.2174.599 | | 40 | 19.304 | 0.161 | 30.087 |
| Stage 3- | -5.9 | 120.66 | 12.971 | UL-RL | 0.2174.599 | | 40 | 20.143 | 0.161 | 33.114 |
| Stage 3- | -6 | 122.437 | 15.162 | UL-RL | 0.2174.599 | | 40 | 20.982 | 0.161 | 36.144 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------|---------------|------------|----|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Muro: | | LEFT Stato | Lato | | LEFT | | | | |
| | | Sigma V (kPa) | Sigma H (kPa) | | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 3- | -6.1 | 124.092 | 17.226 | UL-RL | 0.2174.599 | | 40 | 21.821 | 0.161 | 0 | 39.048 |
| Stage 3- | -6.2 | 125.862 | 19.275 | UL-RL | 0.2174.599 | | 40 | 22.661 | 0.161 | 0 | 41.936 |
| Stage 3- | -6.3 | 127.513 | 21.188 | UL-RL | 0.2174.599 | | 40 | 23.5 | 0.161 | 0 | 44.688 |
| Stage 3- | -6.4 | 129.163 | 23.021 | UL-RL | 0.2174.599 | | 40 | 24.339 | 0.161 | 0 | 47.36 |
| Stage 3- | -6.5 | 130.923 | 24.829 | UL-RL | 0.2174.599 | | 40 | 25.179 | 0.161 | 0 | 50.007 |
| Stage 3- | -6.6 | 132.569 | 26.502 | UL-RL | 0.2174.599 | | 40 | 26.018 | 0.161 | 0 | 52.52 |
| Stage 3- | -6.7 | 134.322 | 28.153 | UL-RL | 0.2174.599 | | 40 | 26.857 | 0.161 | 0 | 55.01 |
| Stage 3- | -6.8 | 135.966 | 29.676 | UL-RL | 0.2174.599 | | 40 | 27.696 | 0.161 | 0 | 57.373 |
| Stage 3- | -6.9 | 137.609 | 31.131 | UL-RL | 0.2174.599 | | 40 | 28.536 | 0.161 | 0 | 59.667 |
| Stage 3- | -7 | 139.354 | 32.574 | UL-RL | 0.2174.599 | | 40 | 29.375 | 0.161 | 0 | 61.949 |
| Stage 3- | -7.1 | 140.994 | 33.906 | UL-RL | 0.2174.599 | | 40 | 30.214 | 0.161 | 0 | 64.12 |
| Stage 3- | -7.2 | 142.733 | 35.234 | UL-RL | 0.2174.599 | | 40 | 31.054 | 0.161 | 0 | 66.288 |
| Stage 3- | -7.3 | 144.371 | 36.464 | UL-RL | 0.2174.599 | | 40 | 31.893 | 0.161 | 0 | 68.356 |
| Stage 3- | -7.4 | 146.008 | 37.65 | UL-RL | 0.2174.599 | | 40 | 32.732 | 0.161 | 0 | 70.382 |
| Stage 3- | -7.5 | 147.741 | 38.846 | UL-RL | 0.2174.599 | | 40 | 33.571 | 0.161 | 0 | 72.417 |
| Stage 3- | -7.6 | 149.376 | 39.959 | UL-RL | 0.2174.599 | | 40 | 34.411 | 0.161 | 0 | 74.37 |
| Stage 3- | -7.7 | 151.01 | 41.044 | UL-RL | 0.2174.599 | | 40 | 35.25 | 0.161 | 0 | 76.294 |
| Stage 3- | -7.8 | 152.736 | 42.149 | UL-RL | 0.2174.599 | | 40 | 36.089 | 0.161 | 0 | 78.238 |
| Stage 3- | -7.9 | 154.369 | 43.187 | UL-RL | 0.2174.599 | | 40 | 36.929 | 0.161 | 0 | 80.115 |
| Stage 3- | -8 | 156.091 | 44.251 | UL-RL | 0.2174.599 | | 40 | 37.768 | 0.161 | 0 | 82.019 |
| Stage 3- | -8.1 | 157.722 | 45.256 | UL-RL | 0.2174.599 | | 40 | 38.607 | 0.161 | 0 | 83.863 |
| Stage 3- | -8.2 | 159.352 | 46.249 | UL-RL | 0.2174.599 | | 40 | 39.446 | 0.161 | 0 | 85.695 |
| Stage 3- | -8.3 | 161.068 | 47.275 | UL-RL | 0.2174.599 | | 40 | 40.286 | 0.161 | 0 | 87.561 |
| Stage 3- | -8.4 | 162.697 | 48.251 | UL-RL | 0.2174.599 | | 40 | 41.125 | 0.161 | 0 | 89.376 |
| Stage 3- | -8.5 | 164.41 | 49.263 | UL-RL | 0.2174.599 | | 40 | 41.964 | 0.161 | 0 | 91.227 |
| Stage 3- | -8.6 | 166.037 | 50.229 | UL-RL | 0.2174.599 | | 40 | 42.804 | 0.161 | 0 | 93.032 |
| Stage 3- | -8.7 | 167.664 | 51.192 | UL-RL | 0.2174.599 | | 40 | 43.643 | 0.161 | 0 | 94.835 |
| Stage 3- | -8.8 | 169.372 | 52.195 | UL-RL | 0.2174.599 | | 40 | 44.482 | 0.161 | 0 | 96.677 |
| Stage 3- | -8.9 | 170.997 | 53.157 | UL-RL | 0.2174.599 | | 40 | 45.321 | 0.161 | 0 | 98.478 |
| Stage 3- | -9 | 172.702 | 54.158 | UL-RL | 0.2174.599 | | 40 | 46.161 | 0.161 | 0 | 100.319 |
| Stage 3- | -9.1 | 174.326 | 55.121 | UL-RL | 0.2174.599 | | 40 | 47 | 0.161 | 0 | 102.121 |
| Stage 3- | -9.2 | 175.95 | 56.085 | UL-RL | 0.2174.599 | | 40 | 47.839 | 0.161 | 0 | 103.924 |
| Stage 3- | -9.3 | 177.651 | 57.089 | UL-RL | 0.2174.599 | | 40 | 48.679 | 0.161 | 0 | 105.767 |
| Stage 3- | -9.4 | 179.274 | 58.055 | UL-RL | 0.2174.599 | | 40 | 49.518 | 0.161 | 0 | 107.573 |
| Stage 3- | -9.5 | 180.897 | 59.024 | UL-RL | 0.2174.599 | | 40 | 50.357 | 0.161 | 0 | 109.381 |
| Stage 3- | -9.6 | 182.444 | 59.956 | UL-RL | 0.2174.599 | | 40 | 51.196 | 0.161 | 0 | 111.153 |
| Stage 3- | -9.7 | 183.992 | 60.89 | UL-RL | 0.2174.599 | | 40 | 52.036 | 0.161 | 0 | 112.926 |
| Stage 3- | -9.8 | 185.541 | 61.826 | UL-RL | 0.2174.599 | | 40 | 52.875 | 0.161 | 0 | 114.701 |
| Stage 3- | -9.9 | 187.091 | 62.762 | UL-RL | 0.2174.599 | | 40 | 53.714 | 0.161 | 0 | 116.476 |
| Stage 3- | -10 | 188.641 | 63.698 | UL-RL | 0.2174.599 | | 40 | 54.554 | 0.161 | 0 | 118.252 |

| Design Assumption: Nominal Risultati Terreno | | Muro: | | LEFT | Lato | | RIGHT | | | | |
|--|-------|---------------|---------------|---------|------------|----|----------------|------------|--------------------|-----------|--------|
| Stage | Z (m) | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 3- | 0 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -0.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -1.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -2.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -3.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.4 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.6 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.7 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.8 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -4.9 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5.1 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5.2 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5.3 | 0 | 0 | REMOVED | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Stage 3- | -5.4 | 1.289 | 30.229 | UL-RL | 0.2174.599 | | 40 | 1.161 | 0.161 | 0 | 31.39 |
| Stage 3- | -5.5 | 2.579 | 32.011 | UL-RL | 0.2174.599 | | 40 | 2.321 | 0.161 | 0 | 34.333 |
| Stage 3- | -5.6 | 3.868 | 33.253 | UL-RL | 0.2174.599 | | 40 | 3.482 | 0.161 | 0 | 36.735 |
| Stage 3- | -5.7 | 5.157 | 34.228 | UL-RL | 0.2174.599 | | 40 | 4.643 | 0.161 | 0 | 38.871 |
| Stage 3- | -5.8 | 6.446 | 35.047 | UL-RL | 0.2174.599 | | 40 | 5.804 | 0.161 | 0 | 40.85 |
| Stage 3- | -5.9 | 7.736 | 35.769 | UL-RL | 0.2174.599 | | 40 | 6.964 | 0.161 | 0 | 42.733 |
| Stage 3- | -6 | 9.025 | 36.429 | UL-RL | 0.2174.599 | | 40 | 8.125 | 0.161 | 0 | 44.554 |
| Stage 3- | -6.1 | 10.314 | 37.053 | UL-RL | 0.2174.599 | | 40 | 9.286 | 0.161 | 0 | 46.339 |
| Stage 3- | -6.2 | 11.604 | 37.657 | UL-RL | 0.2174.599 | | 40 | 10.446 | 0.161 | 0 | 48.104 |

| Design Assumption: Nominal Risultati Terreno | | | | | | | | | | | |
|--|-------|---------------|---------------|-------|------------|----|----------------|------------|--------------------|-----------|---------|
| Stage | Z (m) | Muro: | | LEFT | Lato | | RIGHT | | | | |
| | | Sigma V (kPa) | Sigma H (kPa) | Stato | Ka | Kp | Coesione (kPa) | Pore (kPa) | Gradiente U* (kPa) | Peq (kPa) | |
| Stage 3- | -6.3 | 12.893 | 38.253 | UL-RL | 0.2174.599 | | 40 | 11.607 | 0.161 | 0 | 49.86 |
| Stage 3- | -6.4 | 14.182 | 38.849 | UL-RL | 0.2174.599 | | 40 | 12.768 | 0.161 | 0 | 51.616 |
| Stage 3- | -6.5 | 15.471 | 39.45 | UL-RL | 0.2174.599 | | 40 | 13.929 | 0.161 | 0 | 53.378 |
| Stage 3- | -6.6 | 16.761 | 40.06 | UL-RL | 0.2174.599 | | 40 | 15.089 | 0.161 | 0 | 55.149 |
| Stage 3- | -6.7 | 18.05 | 40.682 | UL-RL | 0.2174.599 | | 40 | 16.25 | 0.161 | 0 | 56.932 |
| Stage 3- | -6.8 | 19.339 | 41.317 | UL-RL | 0.2174.599 | | 40 | 17.411 | 0.161 | 0 | 58.728 |
| Stage 3- | -6.9 | 20.629 | 41.965 | UL-RL | 0.2174.599 | | 40 | 18.571 | 0.161 | 0 | 60.537 |
| Stage 3- | -7 | 21.918 | 42.627 | UL-RL | 0.2174.599 | | 40 | 19.732 | 0.161 | 0 | 62.359 |
| Stage 3- | -7.1 | 23.207 | 43.3 | UL-RL | 0.2174.599 | | 40 | 20.893 | 0.161 | 0 | 64.193 |
| Stage 3- | -7.2 | 24.496 | 43.986 | UL-RL | 0.2174.599 | | 40 | 22.054 | 0.161 | 0 | 66.039 |
| Stage 3- | -7.3 | 25.786 | 44.681 | UL-RL | 0.2174.599 | | 40 | 23.214 | 0.161 | 0 | 67.896 |
| Stage 3- | -7.4 | 27.075 | 45.386 | UL-RL | 0.2174.599 | | 40 | 24.375 | 0.161 | 0 | 69.761 |
| Stage 3- | -7.5 | 28.364 | 46.098 | UL-RL | 0.2174.599 | | 40 | 25.536 | 0.161 | 0 | 71.634 |
| Stage 3- | -7.6 | 29.654 | 46.817 | UL-RL | 0.2174.599 | | 40 | 26.696 | 0.161 | 0 | 73.514 |
| Stage 3- | -7.7 | 30.943 | 47.541 | UL-RL | 0.2174.599 | | 40 | 27.857 | 0.161 | 0 | 75.398 |
| Stage 3- | -7.8 | 32.232 | 48.269 | UL-RL | 0.2174.599 | | 40 | 29.018 | 0.161 | 0 | 77.286 |
| Stage 3- | -7.9 | 33.521 | 48.999 | UL-RL | 0.2174.599 | | 40 | 30.178 | 0.161 | 0 | 79.178 |
| Stage 3- | -8 | 34.811 | 49.731 | UL-RL | 0.2174.599 | | 40 | 31.339 | 0.161 | 0 | 81.07 |
| Stage 3- | -8.1 | 36.1 | 50.463 | UL-RL | 0.2174.599 | | 40 | 32.5 | 0.161 | 0 | 82.963 |
| Stage 3- | -8.2 | 37.389 | 51.196 | UL-RL | 0.2174.599 | | 40 | 33.661 | 0.161 | 0 | 84.856 |
| Stage 3- | -8.3 | 38.679 | 51.927 | UL-RL | 0.2174.599 | | 40 | 34.821 | 0.161 | 0 | 86.748 |
| Stage 3- | -8.4 | 39.968 | 52.656 | UL-RL | 0.2174.599 | | 40 | 35.982 | 0.161 | 0 | 88.638 |
| Stage 3- | -8.5 | 41.257 | 53.384 | UL-RL | 0.2174.599 | | 40 | 37.143 | 0.161 | 0 | 90.527 |
| Stage 3- | -8.6 | 42.546 | 54.109 | UL-RL | 0.2174.599 | | 40 | 38.304 | 0.161 | 0 | 92.412 |
| Stage 3- | -8.7 | 43.836 | 54.83 | UL-RL | 0.2174.599 | | 40 | 39.464 | 0.161 | 0 | 94.295 |
| Stage 3- | -8.8 | 45.125 | 55.549 | UL-RL | 0.2174.599 | | 40 | 40.625 | 0.161 | 0 | 96.174 |
| Stage 3- | -8.9 | 46.414 | 56.264 | UL-RL | 0.2174.599 | | 40 | 41.786 | 0.161 | 0 | 98.05 |
| Stage 3- | -9 | 47.704 | 56.976 | UL-RL | 0.2174.599 | | 40 | 42.946 | 0.161 | 0 | 99.923 |
| Stage 3- | -9.1 | 48.993 | 57.685 | UL-RL | 0.2174.599 | | 40 | 44.107 | 0.161 | 0 | 101.792 |
| Stage 3- | -9.2 | 50.282 | 58.389 | UL-RL | 0.2174.599 | | 40 | 45.268 | 0.161 | 0 | 103.657 |
| Stage 3- | -9.3 | 51.571 | 59.091 | UL-RL | 0.2174.599 | | 40 | 46.429 | 0.161 | 0 | 105.519 |
| Stage 3- | -9.4 | 52.861 | 59.788 | UL-RL | 0.2174.599 | | 40 | 47.589 | 0.161 | 0 | 107.378 |
| Stage 3- | -9.5 | 54.15 | 60.483 | UL-RL | 0.2174.599 | | 40 | 48.75 | 0.161 | 0 | 109.233 |
| Stage 3- | -9.6 | 55.439 | 61.175 | UL-RL | 0.2174.599 | | 40 | 49.911 | 0.161 | 0 | 111.085 |
| Stage 3- | -9.7 | 56.729 | 61.863 | UL-RL | 0.2174.599 | | 40 | 51.071 | 0.161 | 0 | 112.935 |
| Stage 3- | -9.8 | 58.018 | 62.55 | UL-RL | 0.2174.599 | | 40 | 52.232 | 0.161 | 0 | 114.782 |
| Stage 3- | -9.9 | 59.307 | 63.233 | UL-RL | 0.2174.599 | | 40 | 53.393 | 0.161 | 0 | 116.626 |
| Stage 3- | -10 | 60.596 | 63.915 | UL-RL | 0.2174.599 | | 40 | 54.554 | 0.161 | 0 | 118.469 |

Grafico Risultati Terreno Sigma V

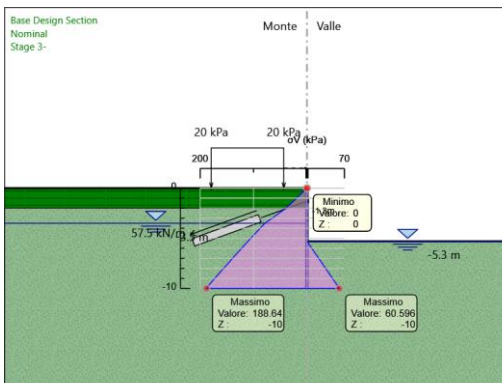
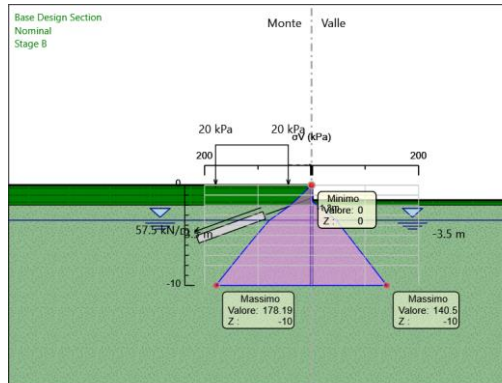
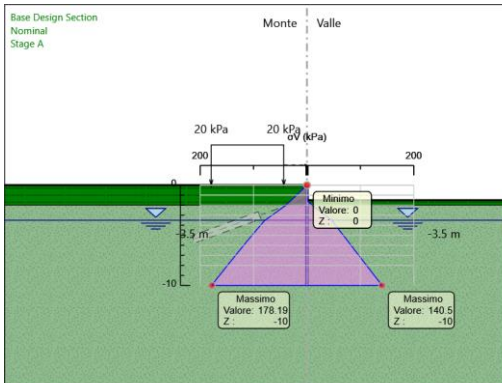
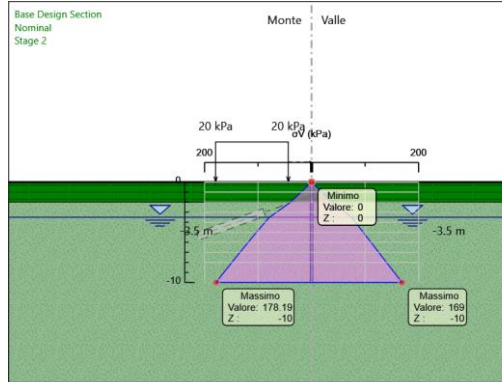
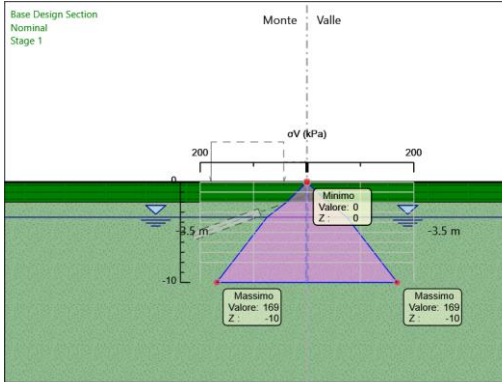


Grafico Risultati Terreno Sigma H

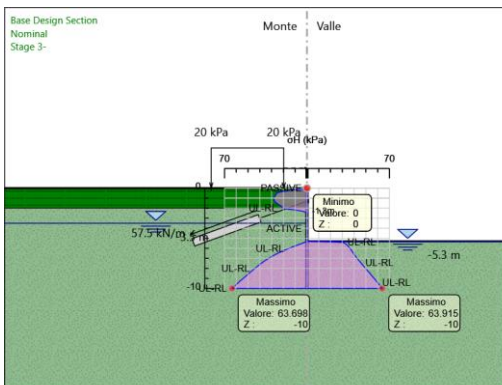
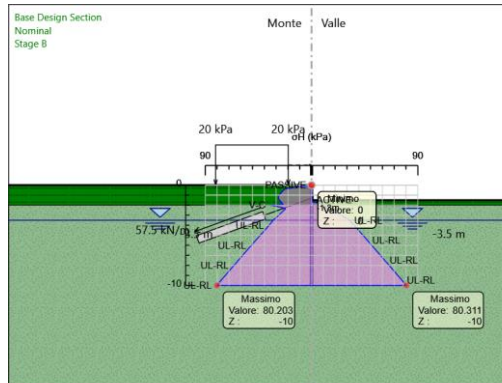
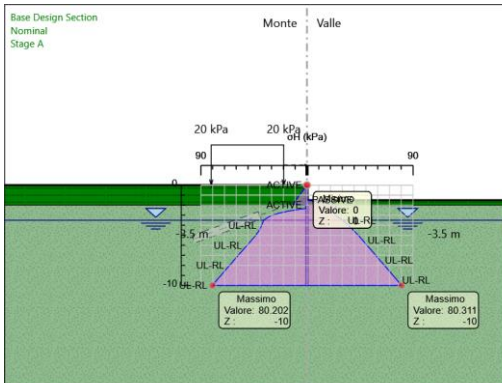
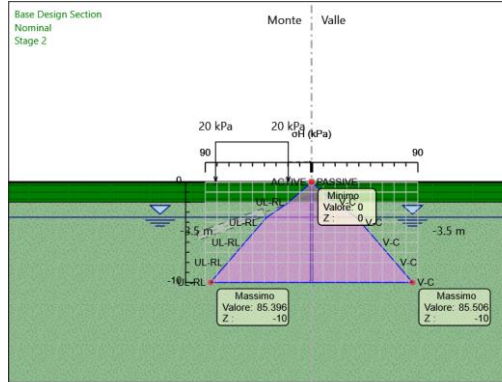
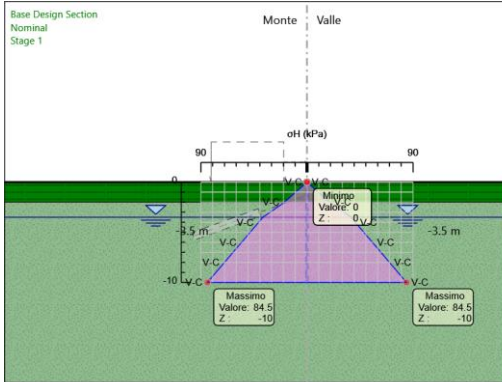


Grafico Risultati Terreno Gradiente

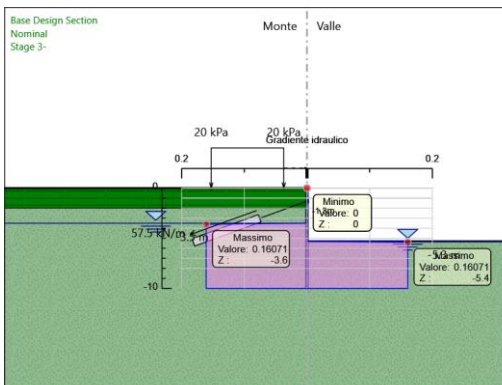
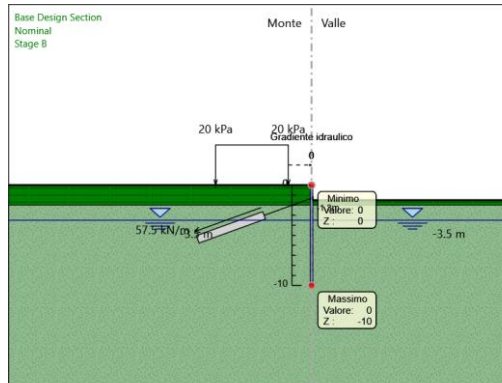
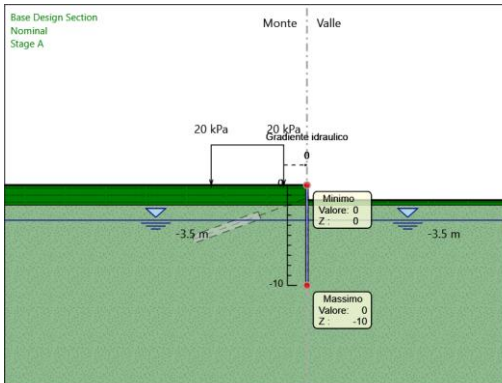
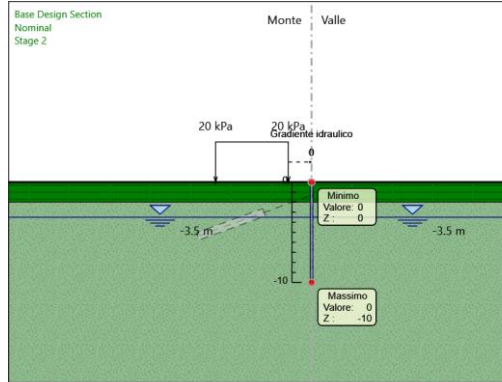
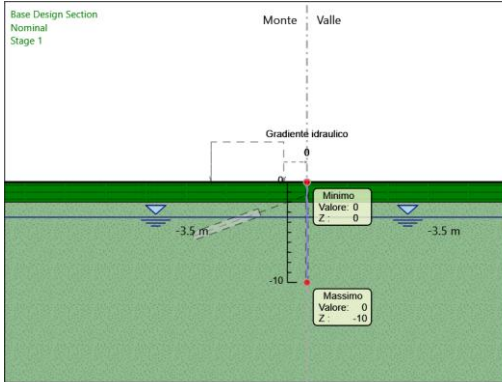
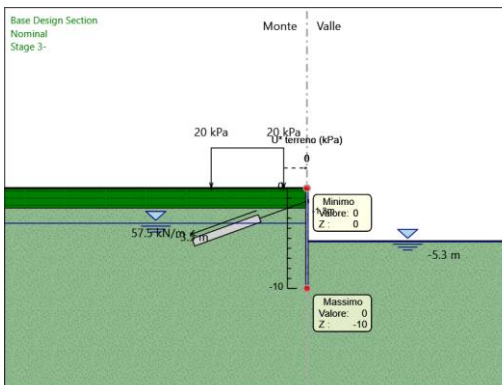
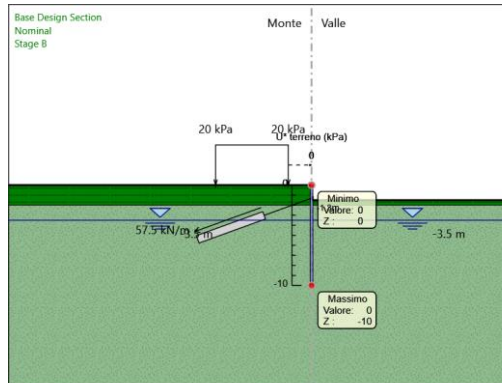
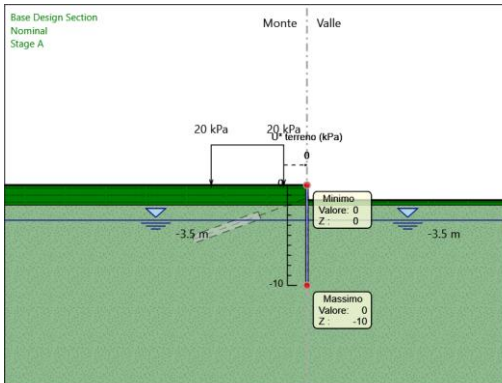
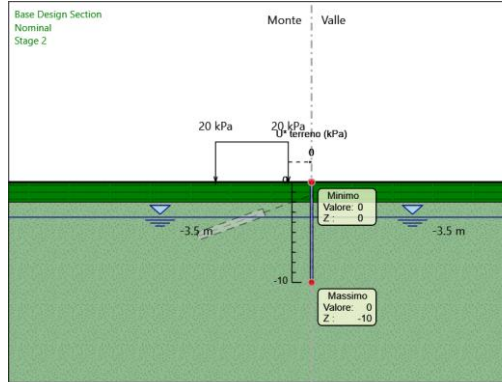
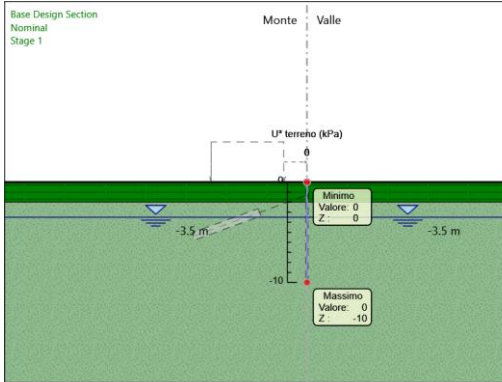


Grafico Risultati Terreno U*



Riepilogo spinte

| Design Assumption: | Tipo Risultato: | Muro: | LEFT | Lato | LEFT | | |
|--------------------|------------------|------------------|-------------|-----------------|-----------------|-----------------------------------|---------------|
| Nominal | Riepilogo spinte | | | | | | |
| Stage | Vera effettiva | Pressione neutra | Vera Totale | Min ammissibile | Max ammissibile | Percentuale di resistenza massima | Vera / Attiva |
| | (kN/m) | (kN/m) | (kN/m) | (kN/m) | (kN/m) | | |
| Stage 1 | 457.4 | 211.2 | 668.6 | 11.6 | 5533.9 | 8.27% | 39.43 |
| Stage 2 | 463.2 | 211.2 | 674.4 | 12.1 | 5781.2 | 8.01% | 38.28 |
| Stage A | 409.5 | 211.2 | 620.7 | 12.1 | 5781.2 | 7.08% | 33.84 |
| Stage B | 454.3 | 211.2 | 665.6 | 12.1 | 5781.2 | 7.86% | 37.55 |
| Stage 3- | 226.3 | 177.3 | 403.6 | 13.8 | 5937.3 | 3.81% | 16.4 |

| Design Assumption: | Tipo Risultato: | Muro: | LEFT | Lato | RIGHT | | |
|--------------------|------------------|------------------|-------------|-----------------|-----------------|-----------------------------------|---------------|
| Nominal | Riepilogo spinte | | | | | | |
| Stage | Vera effettiva | Pressione neutra | Vera Totale | Min ammissibile | Max ammissibile | Percentuale di resistenza massima | Vera / Attiva |
| | (kN/m) | (kN/m) | (kN/m) | (kN/m) | (kN/m) | | |
| Stage 1 | 457.4 | 211.2 | 668.6 | 11.6 | 5533.9 | 8.27% | 39.43 |
| Stage 2 | 463.2 | 211.2 | 674.4 | 11.6 | 5533.9 | 8.37% | 39.93 |
| Stage A | 409.5 | 211.2 | 620.7 | 0.6 | 4372.8 | 9.36% | 682.5 |
| Stage B | 400.3 | 211.2 | 611.5 | 0.6 | 4372.8 | 9.15% | 667.17 |
| Stage 3- | 221.3 | 128.2 | 349.5 | 0 | 1452.7 | 15.23% | ∞ |

Descrizione Coefficienti Design Assumption

| Nome | Carichi Permanenti Sfavorevoli (F_dead_load_unfavour) | Carichi Permanenti Favorevoli (F_dead_load_favour) | Carichi Variabili Sfavorevoli (F_live_load_unfavour) | Carichi Variabili Favorevoli (F_live_load_favour) | Carico Sismico (F_seis) | Pressioni Acqua Lato Monte (F_WaterDR) | Pressioni Acqua Lato Valle (F_WaterRes) | Carichi Permanenti Destabilizzanti (F_UPL_GDStab) | Carichi Permanenti Stabilizzanti (F_UPL_GStab) | Carichi Variabili Destabilizzanti (F_UPL_QDStab) | Carichi Permanenti Destabilizzanti (F_HYD_GDStab) | Carichi Permanenti Stabilizzanti (F_HYD_GStab) | Carichi Variabili Destabilizzanti (F_HYD_QDStab) |
|--|---|--|--|---|-------------------------|--|---|---|--|--|---|--|--|
| Simbolo | γ_G | γ_G | γ_Q | γ_Q | γ_{QE} | γ_G | γ_G | γ_{Gdst} | γ_{Gstb} | γ_{Qdst} | γ_{Gdst} | γ_{Gstb} | γ_{Qdst} |
| Nominal | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| NTC2018: A1+M1+R1 (R3 per tiranti) | 1.3 | 1 | 1.5 | 1 | 0 | 1.3 | 1 | 1 | 1 | 1 | 1.3 | 0.9 | 1 |
| NTC2018: A2+M2+R1 | 1 | 1 | 1.3 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 1.3 | 0.9 | 1 |

| Nome | Parziale su $\tan(\phi')$ (F_Fr) | Parziale su c' (F_eff_cohe) | Parziale su Su (F_Su) | Parziale su qu (F_qu) | Parziale su peso specifico (F_gamma) |
|--|----------------------------------|-------------------------------|-----------------------|-----------------------|--------------------------------------|
| Simbolo | γ_ϕ | γ_c | γ_{cu} | γ_{qu} | γ_γ |
| Nominal | 1 | 1 | 1 | 1 | 1 |
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | 1 | 1 | 1 | 1 | 1 |
| NTC2018: A1+M1+R1 (R3 per tiranti) | 1 | 1 | 1 | 1 | 1 |
| NTC2018: A2+M2+R1 | 1.25 | 1.25 | 1.4 | 1 | 1 |

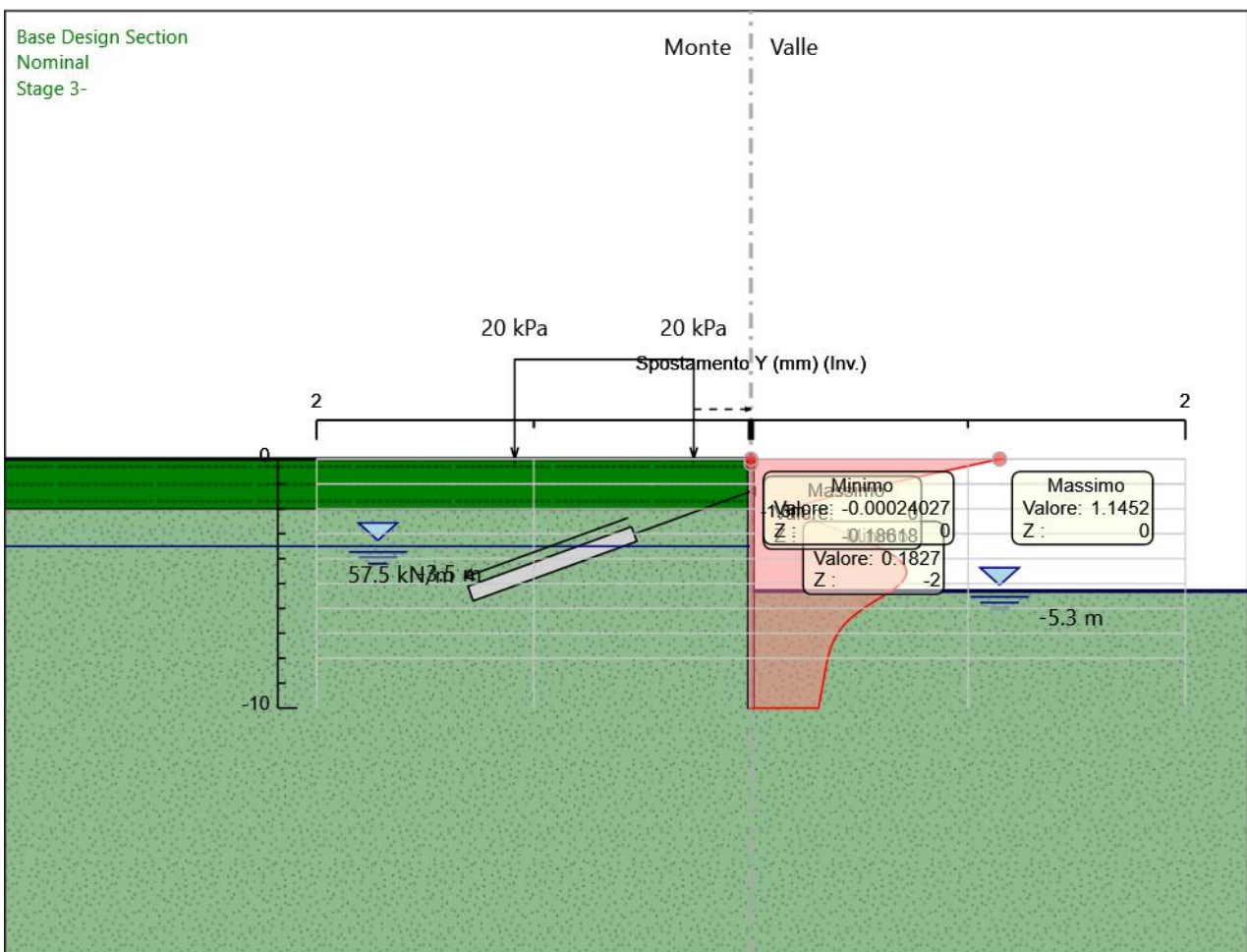
| Nome | Parziale resistenza terreno (es. Kp) (F_Soil_Res_walls) | Parziale resistenza Tiranti permanenti (F_Anch_P) | Parziale resistenza Tiranti temporanei (F_Anch_T) | Parziale elementi strutturali (F_wall) |
|--|---|---|---|--|
| Simbolo | γ_{Re} | γ_{ap} | γ_{at} | |
| Nominal | 1 | 1 | 1 | 1 |
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | 1 | 1 | 1 | 1 |
| NTC2018: A1+M1+R1 (R3 per tiranti) | 1 | 1.2 | 1.1 | 1 |
| NTC2018: A2+M2+R1 | 1 | 1.2 | 1.1 | 1 |

Riepilogo Stage / Design Assumption per Inviluppo

| Design Assumption | Stage 1 | Stage 2 | Stage A | Stage B | Stage 3- |
|--|---------|---------|---------|---------|----------|
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | V | V | V | V | V |
| NTC2018: A1+M1+R1 (R3 per tiranti) | V | V | V | V | V |
| NTC2018: A2+M2+R1 | V | V | V | V | V |

Descrizione sintetica dei risultati delle Design Assumption (Inviluppi)

Grafico Inviluppi Spostamento



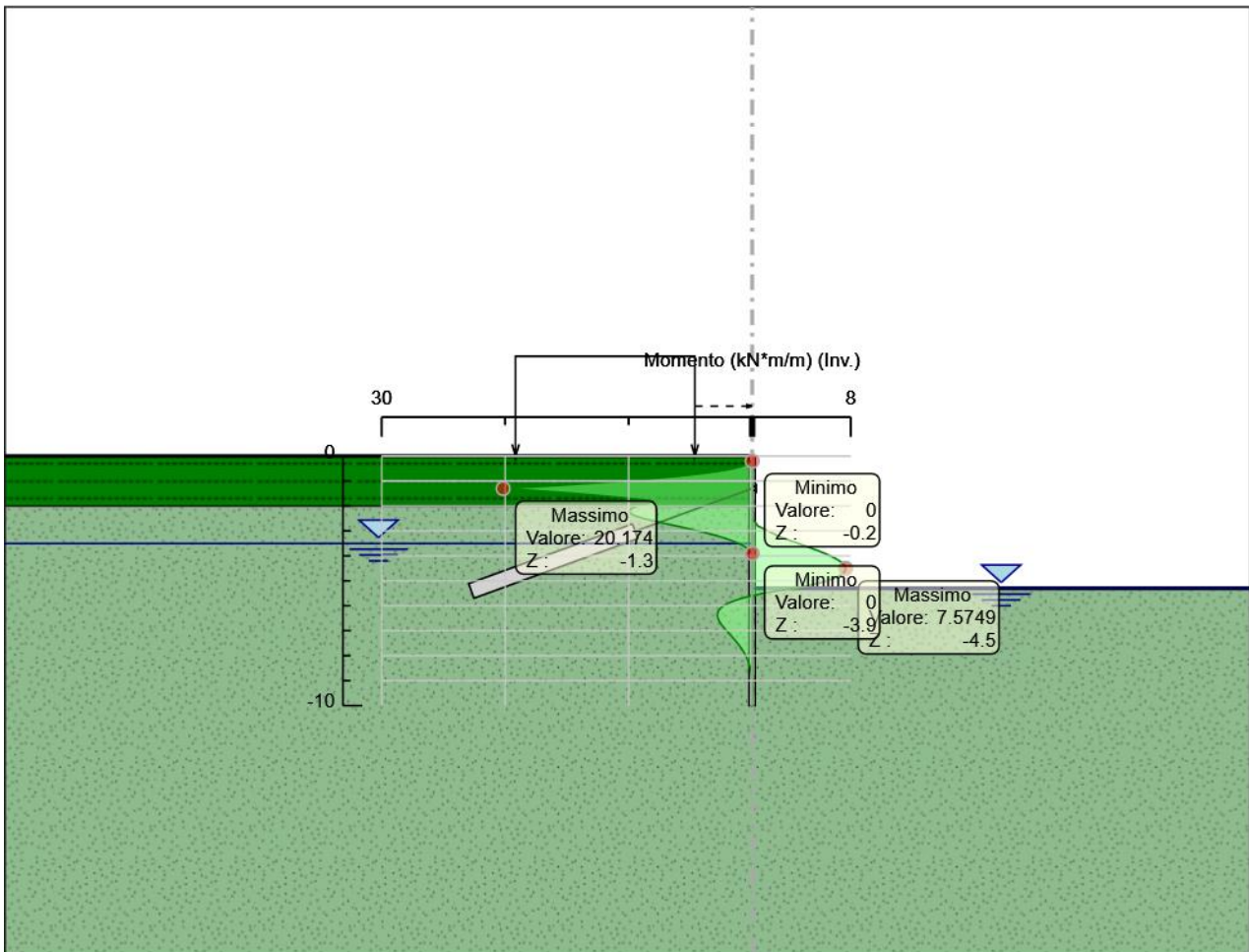
Spostamento

Tabella Inviluppi Momento paratia sx

| Selected Design Assumptions Z (m) | Inviluppi: Momento | | Muro: paratia sx |
|--------------------------------------|------------------------|----------------------|------------------|
| | Lato sinistro (kN*m/m) | Lato destro (kN*m/m) | |
| 0 | 0 | | 0 |
| -0.1 | 0 | | 0 |
| -0.2 | 0.077 | | 0 |
| -0.3 | 0.306 | | 0 |
| -0.4 | 0.766 | | 0 |
| -0.5 | 1.534 | | 0 |
| -0.6 | 2.633 | | 0.001 |
| -0.7 | 4.073 | | 0.003 |
| -0.8 | 5.86 | | 0.006 |
| -0.9 | 8 | | 0.009 |
| -1 | 10.499 | | 0.013 |
| -1.1 | 13.36 | | 0.017 |
| -1.2 | 16.586 | | 0.022 |
| -1.3 | 20.174 | | 0.025 |
| -1.4 | 17.093 | | 0.028 |
| -1.5 | 14.359 | | 0.03 |
| -1.6 | 11.959 | | 0.03 |
| -1.7 | 9.879 | | 0.026 |
| -1.8 | 8.101 | | 0.02 |
| -1.9 | 8.395 | | 0.009 |
| -2 | 9.255 | | 0 |
| -2.1 | 9.781 | | 0 |
| -2.2 | 9.983 | | 0 |
| -2.3 | 9.87 | | 0 |
| -2.4 | 9.447 | | 0 |
| -2.5 | 8.789 | | 0 |
| -2.6 | 7.979 | | 0.169 |
| -2.7 | 7.086 | | 0.323 |
| -2.8 | 6.161 | | 0.457 |
| -2.9 | 5.246 | | 0.873 |
| -3 | 4.371 | | 1.289 |
| -3.1 | 3.557 | | 1.705 |
| -3.2 | 2.819 | | 2.12 |
| -3.3 | 2.163 | | 2.61 |
| -3.4 | 1.593 | | 3.174 |
| -3.5 | 1.108 | | 3.737 |
| -3.6 | 0.704 | | 4.301 |
| -3.7 | 0.376 | | 4.854 |
| -3.8 | 0.116 | | 5.385 |
| -3.9 | 0 | | 5.883 |
| -4 | 0 | | 6.338 |
| -4.1 | 0 | | 6.738 |
| -4.2 | 0 | | 7.073 |
| -4.3 | 0 | | 7.331 |
| -4.4 | 0 | | 7.502 |
| -4.5 | 0 | | 7.575 |
| -4.6 | 0 | | 7.539 |
| -4.7 | 0 | | 7.382 |
| -4.8 | 0 | | 7.095 |
| -4.9 | 0.003 | | 6.666 |
| -5 | 0.008 | | 6.084 |
| -5.1 | 0.011 | | 5.339 |
| -5.2 | 0.012 | | 4.419 |
| -5.3 | 0.013 | | 3.313 |
| -5.4 | 0.012 | | 2.011 |
| -5.5 | 0.011 | | 0.887 |
| -5.6 | 0.086 | | 0.07 |
| -5.7 | 0.842 | | 0.05 |
| -5.8 | 1.468 | | 0.033 |
| -5.9 | 1.955 | | 0.019 |

| Selected Design Assumptions | Involupi: Momento | Muro: paratia sx |
|-----------------------------|------------------------|----------------------|
| Z (m) | Lato sinistro (kN*m/m) | Lato destro (kN*m/m) |
| -6 | 2.317 | 0.009 |
| -6.1 | 2.569 | 0.008 |
| -6.2 | 2.727 | 0.007 |
| -6.3 | 2.805 | 0.007 |
| -6.4 | 2.815 | 0.006 |
| -6.5 | 2.77 | 0.006 |
| -6.6 | 2.682 | 0.006 |
| -6.7 | 2.559 | 0.006 |
| -6.8 | 2.411 | 0.006 |
| -6.9 | 2.246 | 0.005 |
| -7 | 2.069 | 0.005 |
| -7.1 | 1.887 | 0.005 |
| -7.2 | 1.704 | 0.005 |
| -7.3 | 1.524 | 0.005 |
| -7.4 | 1.35 | 0.004 |
| -7.5 | 1.184 | 0.004 |
| -7.6 | 1.029 | 0.004 |
| -7.7 | 0.884 | 0.004 |
| -7.8 | 0.752 | 0.004 |
| -7.9 | 0.631 | 0.004 |
| -8 | 0.523 | 0.005 |
| -8.1 | 0.427 | 0.005 |
| -8.2 | 0.342 | 0.006 |
| -8.3 | 0.269 | 0.006 |
| -8.4 | 0.206 | 0.007 |
| -8.5 | 0.153 | 0.008 |
| -8.6 | 0.108 | 0.009 |
| -8.7 | 0.072 | 0.01 |
| -8.8 | 0.043 | 0.012 |
| -8.9 | 0.02 | 0.013 |
| -9 | 0.004 | 0.014 |
| -9.1 | 0 | 0.014 |
| -9.2 | 0 | 0.016 |
| -9.3 | 0 | 0.02 |
| -9.4 | 0 | 0.021 |
| -9.5 | 0 | 0.019 |
| -9.6 | 0 | 0.015 |
| -9.7 | 0 | 0.01 |
| -9.8 | 0 | 0.005 |
| -9.9 | 0 | 0.002 |
| -10 | 0 | 0 |

Grafico Involuppi Momento



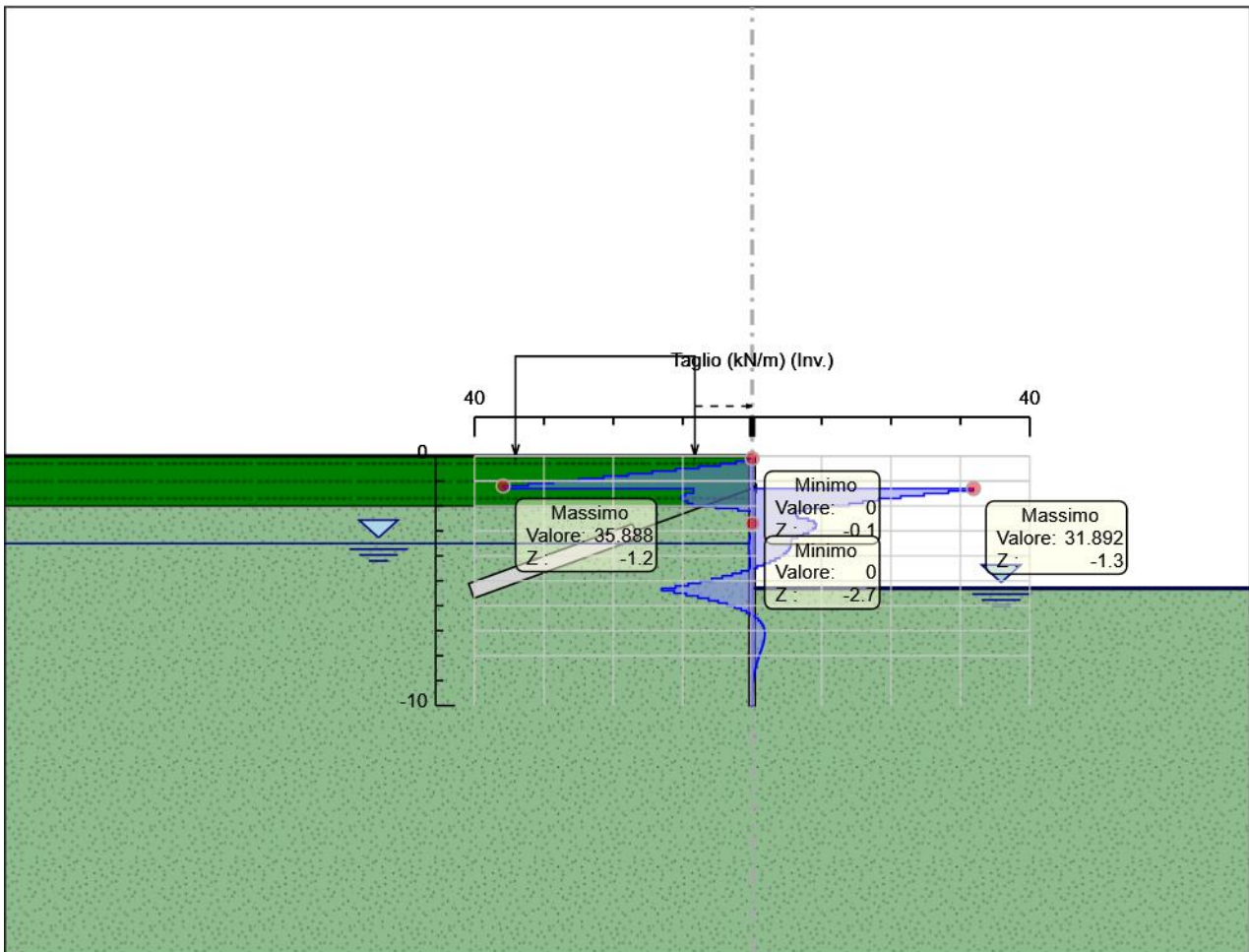
Momento

Tabella Inviluppi Taglio paratia sx

| Selected Design Assumptions Z (m) | Inviluppi: Taglio | | Muro: paratia sx |
|--------------------------------------|----------------------|--------------------|------------------|
| | Lato sinistro (kN/m) | Lato destro (kN/m) | |
| 0 | 0 | 0 | |
| -0.1 | 0.766 | 0 | |
| -0.2 | 2.299 | 0 | |
| -0.3 | 4.6 | 0.001 | |
| -0.4 | 7.673 | 0.005 | |
| -0.5 | 10.996 | 0.012 | |
| -0.6 | 14.396 | 0.019 | |
| -0.7 | 17.867 | 0.026 | |
| -0.8 | 21.402 | 0.033 | |
| -0.9 | 24.989 | 0.039 | |
| -1 | 28.613 | 0.042 | |
| -1.1 | 32.255 | 0.042 | |
| -1.2 | 35.888 | 0.042 | |
| -1.3 | 35.888 | 31.892 | |
| -1.4 | 8.437 | 31.892 | |
| -1.5 | 9.658 | 28.297 | |
| -1.6 | 10.199 | 24.766 | |
| -1.7 | 10.199 | 21.401 | |
| -1.8 | 10.058 | 18.212 | |
| -1.9 | 9.275 | 15.964 | |
| -2 | 8.598 | 13.975 | |
| -2.1 | 5.258 | 10.37 | |
| -2.2 | 2.024 | 7.653 | |
| -2.3 | 0.065 | 6.315 | |
| -2.4 | 0.044 | 6.579 | |
| -2.5 | 0.027 | 8.095 | |
| -2.6 | 0.014 | 8.938 | |
| -2.7 | 0.002 | 9.248 | |
| -2.8 | 0 | 9.248 | |
| -2.9 | 0 | 9.149 | |
| -3 | 0 | 8.748 | |
| -3.1 | 0.16 | 8.139 | |
| -3.2 | 0.294 | 7.384 | |
| -3.3 | 0.379 | 6.555 | |
| -3.4 | 0.436 | 5.703 | |
| -3.5 | 0.459 | 5.638 | |
| -3.6 | 0.467 | 5.638 | |
| -3.7 | 0.467 | 5.529 | |
| -3.8 | 0.453 | 5.311 | |
| -3.9 | 0.423 | 4.983 | |
| -4 | 0.393 | 4.547 | |
| -4.1 | 0.352 | 4.001 | |
| -4.2 | 0.305 | 3.347 | |
| -4.3 | 0.275 | 2.583 | |
| -4.4 | 0.242 | 1.71 | |
| -4.5 | 0.459 | 0.728 | |
| -4.6 | 1.563 | 0 | |
| -4.7 | 2.872 | 0 | |
| -4.8 | 4.291 | 0 | |
| -4.9 | 5.818 | 0 | |
| -5 | 7.455 | 0 | |
| -5.1 | 9.201 | 0 | |
| -5.2 | 11.055 | 0 | |
| -5.3 | 13.019 | 0.005 | |
| -5.4 | 13.019 | 0.006 | |
| -5.5 | 11.241 | 0.01 | |
| -5.6 | 9.479 | 0.015 | |
| -5.7 | 7.806 | 0.015 | |
| -5.8 | 6.267 | 0.014 | |
| -5.9 | 4.868 | 0.018 | |

| Selected Design Assumptions | Involuppi: Taglio | Muro: paratia sx |
|-----------------------------|----------------------|--------------------|
| Z (m) | Lato sinistro (kN/m) | Lato destro (kN/m) |
| -6 | 3.618 | 0.018 |
| -6.1 | 2.525 | 0.016 |
| -6.2 | 1.578 | 0.016 |
| -6.3 | 0.777 | 0.012 |
| -6.4 | 0.105 | 0.449 |
| -6.5 | 0.011 | 0.887 |
| -6.6 | 0.005 | 1.229 |
| -6.7 | 0.004 | 1.478 |
| -6.8 | 0.004 | 1.654 |
| -6.9 | 0.003 | 1.768 |
| -7 | 0.002 | 1.821 |
| -7.1 | 0.002 | 1.83 |
| -7.2 | 0.004 | 1.83 |
| -7.3 | 0.004 | 1.798 |
| -7.4 | 0.004 | 1.738 |
| -7.5 | 0.003 | 1.658 |
| -7.6 | 0.003 | 1.556 |
| -7.7 | 0.002 | 1.445 |
| -7.8 | 0 | 1.329 |
| -7.9 | 0 | 1.205 |
| -8 | 0 | 1.083 |
| -8.1 | 0 | 0.96 |
| -8.2 | 0 | 0.843 |
| -8.3 | 0 | 0.735 |
| -8.4 | 0 | 0.629 |
| -8.5 | 0 | 0.534 |
| -8.6 | 0 | 0.442 |
| -8.7 | 0 | 0.362 |
| -8.8 | 0 | 0.292 |
| -8.9 | 0 | 0.226 |
| -9 | 0 | 0.171 |
| -9.1 | 0 | 0.119 |
| -9.2 | 0.002 | 0.075 |
| -9.3 | 0.01 | 0.04 |
| -9.4 | 0.02 | 0.007 |
| -9.5 | 0.04 | 0 |
| -9.6 | 0.049 | 0 |
| -9.7 | 0.049 | 0 |
| -9.8 | 0.048 | 0 |
| -9.9 | 0.036 | 0 |
| -10 | 0.015 | 0 |

Grafico Inviluppi Taglio



Taglio

Inviluppo Spinta Reale Efficace / Spinta Passiva

| Design Assumption | Stage | Muro | Lato | Inviluppo Spinta Reale Efficace / Spinta Passiva |
|--------------------------------------|--------------|-------------|-------------|---|
| | | | | % |
| NTC2018: A2+M2+R1 Stage 1 Left Wall | LEFT | | | 8.7 |
| NTC2018: A2+M2+R1 Stage 3- Left Wall | RIGHT | | | 18.41 |

Inviluppo Spinta Reale Efficace / Spinta Attiva

| Design Assumption | Stage | Muro | Lato | Inviluppo Spinta Reale Efficace / Spinta Attiva |
|--------------------------------------|--------------|-------------|-------------|--|
| | | | | % |
| NTC2018: A2+M2+R1 Stage 3- Left Wall | | LEFT | | 776.87 |
| NTC2018: A2+M2+R1 Stage 1 Left Wall | | RIGHT | | 2403.2 |

Normative adottate per le verifiche degli Elementi Strutturali

Normative Verifiche

| | |
|--------------|-----|
| Calcestruzzo | NTC |
| Acciaio | NTC |
| Tirante | NTC |

Coefficienti per Verifica Tiranti

| | |
|------------|------|
| GEO FS | 1 |
| ξ_{a3} | 1.8 |
| γ_s | 1.15 |

Riepilogo Stage / Design Assumption per Involuppo

| Design Assumption | Stage 1 | Stage 2 | Stage A | Stage B | Stage 3- |
|--|---------|---------|---------|---------|----------|
| NTC2018: SLE (Rara/Frequente/Quasi Permanente) | V | V | V | V | V |
| NTC2018: A1+M1+R1 (R3 per tiranti) | V | V | V | V | V |
| NTC2018: A2+M2+R1 | V | V | V | V | V |

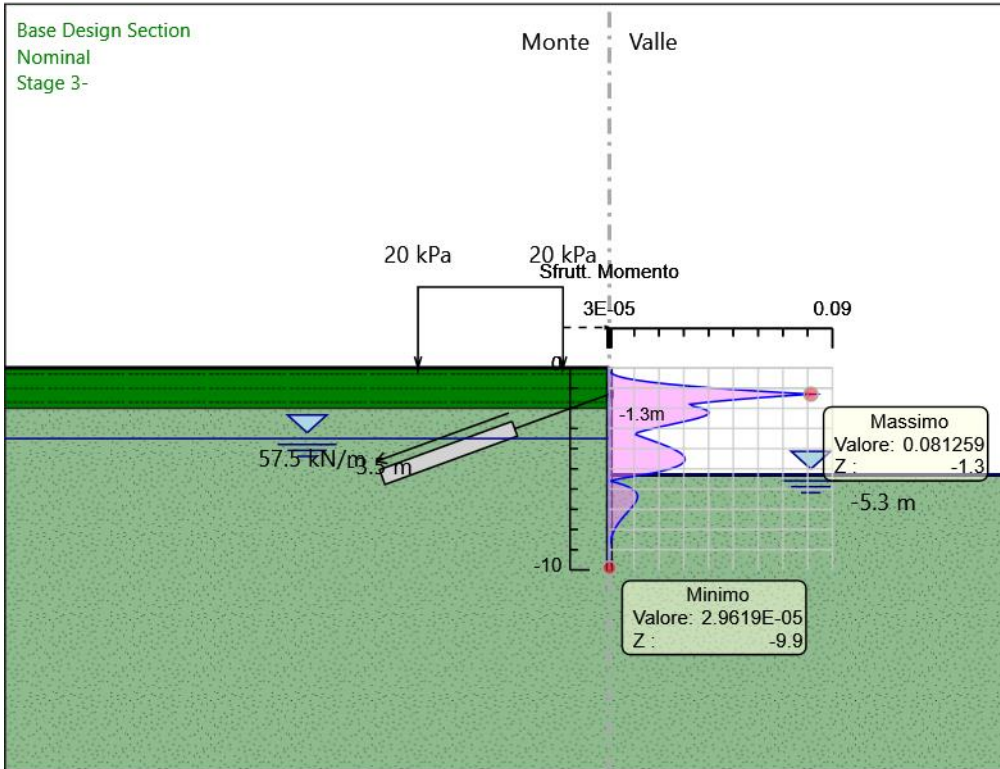
Risultati SteelWorld

Tabella Inviluppi Tasso di Sfruttamento M-N - SteelWorld : LEFT

| Z (m) | Tasso di Sfruttamento M-N - SteelWorld |
|-------|--|
| 0 | 0 |
| -0.1 | 0 |
| -0.2 | 0 |
| -0.3 | 0.001 |
| -0.4 | 0.003 |
| -0.5 | 0.006 |
| -0.6 | 0.011 |
| -0.7 | 0.016 |
| -0.8 | 0.024 |
| -0.9 | 0.032 |
| -1 | 0.042 |
| -1.1 | 0.054 |
| -1.2 | 0.067 |
| -1.3 | 0.081 |
| -1.4 | 0.069 |
| -1.5 | 0.058 |
| -1.6 | 0.048 |
| -1.7 | 0.04 |
| -1.8 | 0.033 |
| -1.9 | 0.034 |
| -2 | 0.037 |
| -2.1 | 0.039 |
| -2.2 | 0.04 |
| -2.3 | 0.04 |
| -2.4 | 0.038 |
| -2.5 | 0.035 |
| -2.6 | 0.032 |
| -2.7 | 0.029 |
| -2.8 | 0.025 |
| -2.9 | 0.021 |
| -3 | 0.018 |
| -3.1 | 0.014 |
| -3.2 | 0.011 |
| -3.3 | 0.011 |
| -3.4 | 0.013 |
| -3.5 | 0.015 |
| -3.6 | 0.017 |
| -3.7 | 0.02 |
| -3.8 | 0.022 |
| -3.9 | 0.024 |
| -4 | 0.026 |
| -4.1 | 0.027 |
| -4.2 | 0.028 |
| -4.3 | 0.03 |
| -4.4 | 0.03 |
| -4.5 | 0.031 |
| -4.6 | 0.03 |
| -4.7 | 0.03 |
| -4.8 | 0.029 |
| -4.9 | 0.027 |
| -5 | 0.025 |
| -5.1 | 0.022 |
| -5.2 | 0.018 |
| -5.3 | 0.013 |
| -5.4 | 0.008 |
| -5.5 | 0.004 |
| -5.6 | 0 |
| -5.7 | 0.003 |

| Z (m) | Tasso di Sfruttamento M-N - SteelWorld | LEFT | Tasso di Sfruttamento M-N - SteelWorld |
|-------|--|------|--|
| -5.8 | | | 0.006 |
| -5.9 | | | 0.008 |
| -6 | | | 0.009 |
| -6.1 | | | 0.01 |
| -6.2 | | | 0.011 |
| -6.3 | | | 0.011 |
| -6.4 | | | 0.011 |
| -6.5 | | | 0.011 |
| -6.6 | | | 0.011 |
| -6.7 | | | 0.01 |
| -6.8 | | | 0.01 |
| -6.9 | | | 0.009 |
| -7 | | | 0.008 |
| -7.1 | | | 0.008 |
| -7.2 | | | 0.007 |
| -7.3 | | | 0.006 |
| -7.4 | | | 0.005 |
| -7.5 | | | 0.005 |
| -7.6 | | | 0.004 |
| -7.7 | | | 0.004 |
| -7.8 | | | 0.003 |
| -7.9 | | | 0.003 |
| -8 | | | 0.002 |
| -8.1 | | | 0.002 |
| -8.2 | | | 0.001 |
| -8.3 | | | 0.001 |
| -8.4 | | | 0.001 |
| -8.5 | | | 0.001 |
| -8.6 | | | 0 |
| -8.7 | | | 0 |
| -8.8 | | | 0 |
| -8.9 | | | 0 |
| -9 | | | 0 |
| -9.1 | | | 0 |
| -9.2 | | | 0 |
| -9.3 | | | 0 |
| -9.4 | | | 0 |
| -9.5 | | | 0 |
| -9.6 | | | 0 |
| -9.7 | | | 0 |
| -9.8 | | | 0 |
| -9.9 | | | 0 |
| -10 | | | 0 |

Grafico Involuppi Tasso di Sfruttamento M-N - SteelWorld



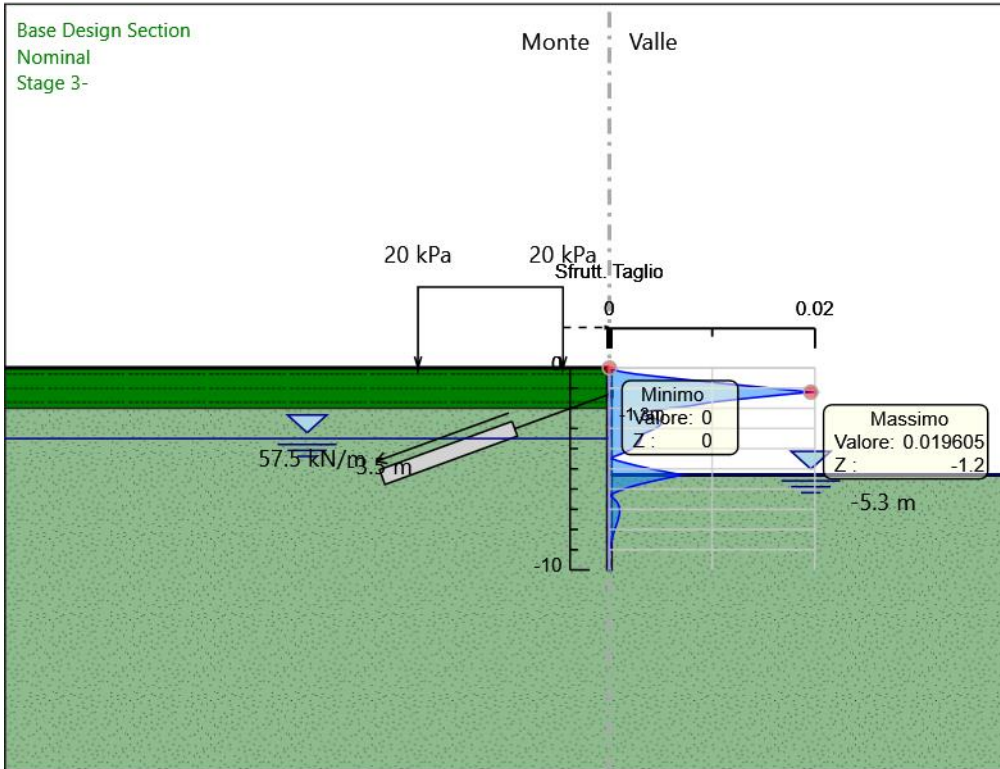
Involuppi
Tasso di Sfruttamento M-N - SteelWorld

Tabella Involuppi Tasso di Sfruttamento a Taglio - SteelWorld : LEFT

| Z (m) | Tasso di Sfruttamento a Taglio - SteelWorld |
|-------|---|
| 0 | 0 |
| -0.1 | 0 |
| -0.2 | 0.001 |
| -0.3 | 0.003 |
| -0.4 | 0.004 |
| -0.5 | 0.006 |
| -0.6 | 0.008 |
| -0.7 | 0.01 |
| -0.8 | 0.012 |
| -0.9 | 0.014 |
| -1 | 0.016 |
| -1.1 | 0.018 |
| -1.2 | 0.02 |
| -1.3 | 0.017 |
| -1.4 | 0.015 |
| -1.5 | 0.014 |
| -1.6 | 0.012 |
| -1.7 | 0.01 |
| -1.8 | 0.009 |
| -1.9 | 0.008 |
| -2 | 0.006 |
| -2.1 | 0.004 |
| -2.2 | 0.003 |
| -2.3 | 0.003 |
| -2.4 | 0.004 |
| -2.5 | 0.004 |
| -2.6 | 0.005 |
| -2.7 | 0.005 |
| -2.8 | 0.005 |
| -2.9 | 0.005 |
| -3 | 0.004 |
| -3.1 | 0.004 |
| -3.2 | 0.004 |
| -3.3 | 0.003 |
| -3.4 | 0.003 |
| -3.5 | 0.003 |
| -3.6 | 0.003 |
| -3.7 | 0.003 |
| -3.8 | 0.003 |
| -3.9 | 0.002 |
| -4 | 0.002 |
| -4.1 | 0.002 |
| -4.2 | 0.001 |
| -4.3 | 0.001 |
| -4.4 | 0 |
| -4.5 | 0 |
| -4.6 | 0.001 |
| -4.7 | 0.002 |
| -4.8 | 0.002 |
| -4.9 | 0.003 |
| -5 | 0.004 |
| -5.1 | 0.005 |
| -5.2 | 0.006 |
| -5.3 | 0.007 |
| -5.4 | 0.006 |
| -5.5 | 0.005 |
| -5.6 | 0.004 |
| -5.7 | 0.003 |
| -5.8 | 0.003 |
| -5.9 | 0.002 |
| -6 | 0.001 |

| Z (m) | Tasso di Sfruttamento a Taglio - SteelWorld | LEFT | Tasso di Sfruttamento a Taglio - SteelWorld |
|-------|---|-------|---|
| -6.1 | | 0.001 | |
| -6.2 | | 0 | |
| -6.3 | | 0 | |
| -6.4 | | 0 | |
| -6.5 | | 0 | |
| -6.6 | | 0.001 | |
| -6.7 | | 0.001 | |
| -6.8 | | 0.001 | |
| -6.9 | | 0.001 | |
| -7 | | 0.001 | |
| -7.1 | | 0.001 | |
| -7.2 | | 0.001 | |
| -7.3 | | 0.001 | |
| -7.4 | | 0.001 | |
| -7.5 | | 0.001 | |
| -7.6 | | 0.001 | |
| -7.7 | | 0.001 | |
| -7.8 | | 0.001 | |
| -7.9 | | 0.001 | |
| -8 | | 0.001 | |
| -8.1 | | 0 | |
| -8.2 | | 0 | |
| -8.3 | | 0 | |
| -8.4 | | 0 | |
| -8.5 | | 0 | |
| -8.6 | | 0 | |
| -8.7 | | 0 | |
| -8.8 | | 0 | |
| -8.9 | | 0 | |
| -9 | | 0 | |
| -9.1 | | 0 | |
| -9.2 | | 0 | |
| -9.3 | | 0 | |
| -9.4 | | 0 | |
| -9.5 | | 0 | |
| -9.6 | | 0 | |
| -9.7 | | 0 | |
| -9.8 | | 0 | |
| -9.9 | | 0 | |
| -10 | | 0 | |

Grafico Involuppi Tasso di Sfruttamento a Taglio - SteelWorld



Involuppi
Tasso di Sfruttamento a Taglio - SteelWorld

Verifiche Tiranti NTC2018: SLE (Rara/Frequente/Quasi Permanente)

| Design Assumption: NTC2018: SLE (Rara/Frequente/Quasi Permanente) | Tipo Risultato: Verifiche Tiranti | NTC2018 (ITA) | | | | | | Gerarchia delle Resistenze |
|--|---|------------------|---------|------------------------|------------------------|------------------------|-----------|----------------------------------|
| | | Tirante | Stage | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Ratio GEO | |
| Tieback_New_New_New_New | Stage B | | 230 | 791.681 | 605.557 | 0.291 | 0.38 | NO |
| Tieback_New_New_New_New | Stage 3- | | 230.091 | 791.681 | 605.557 | 0.291 | 0.38 | NO |

Verifiche Tiranti NTC2018: A1+M1+R1 (R3 per tiranti)

| Design Assumption: NTC2018: A1+M1+R1 (R3 per tiranti) Tirante | Tipo Risultato: Verifiche Tiranti Stage | NTC2018 | | | NTC2018 (ITA) | | Resistenza Gerarchia delle Resistenze |
|---|---|------------------------|------------------------|------------------------|------------------|--------------|--|
| | | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Ratio GEO | Ratio STR | |
| Tieback_New_New_New_New | Stage B | 299 | 399.839 | 605.557 | 0.748 | 0.494 | |
| Tieback_New_New_New_New | Stage 3- | 299.122 | 399.839 | 605.557 | 0.748 | 0.494 | |

Verifiche Tiranti NTC2018: A2+M2+R1

| Design Assumption: NTC2018: A2+M2+R1 Tirante | Tipo Risultato: Verifiche Tiranti Stage | NTC2018 (ITA) | | | | | | |
|--|---|------------------------|------------------------|------------------------|-----------|--------------|------------|-------------------------------|
| | | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Ratio GEO | Ratio STR | Resistenza | Gerarchia delle Resistenze |
| Tieback_New_New_New_New | Stage B | 230 | 399.839 | 605.557 | 0.575 | 0.38 | | |
| Tieback_New_New_New_New | Stage 3- | 230.071 | 399.839 | 605.557 | 0.575 | 0.38 | | |

Inviluppo Verifiche Tiranti (su tutte le D.A. attive)

| Tipo Risultato: | | | | | | | | | |
|-------------------------|---------|---------------------|---------------------|---------------------|-----------|-----------|------------|----------------------------|---------------------------------------|
| Verifiche Tiranti | | | | | | | | | |
| Tirante | Stage | Sollecitazione (kN) | Resistenza GEO (kN) | Resistenza STR (kN) | Ratio GEO | Ratio STR | Resistenza | Gerarchia delle Resistenze | Design Assumption |
| Tieback_New_New_New_New | Stage B | 299 | 399.839 | 605.557 | 0.748 | 0.494 | | | NTC2018: A1+M1+R1 (R3 per tiranti) |

Verifiche Travi di Ripartizione Nominal

| Design Assumption: Nominal | Tipo Risultato: Verifiche Travi di Ripartizione | | | | | | | | |
|-------------------------------|---|------------|-----------|-------------|------------------------------|-----------------|--------------|-----------------|-------------|
| Trave di Ripartizione | Elemento strutturale | Sezione | Materiale | Stage | Carico distribuito (kN/m) | Assiale (kN) | Ratio M-N | Ratio taglio | Instabilità |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage B | 57.5 | 0 | 0 | 0 | 0 |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage 3- | 57.523 | 0 | 0 | 0 | 0 |

Verifiche Travi di Ripartizione NTC2018: SLE (Rara/Frequente/Quasi Permanente)

| Design Assumption: NTC2018: SLE | | | | | | | | | |
|------------------------------------|-------------------------|---------|-----------|----------|---------------------------|--------------|-----------|--------------|-------------|
| Tipo Risultato: Verifiche Travi di | NTC2018 | | | | | | | | |
| (Rara/Frequente/Quasi Permanente) | Ripartizione | (ITA) | | | | | | | |
| Trave di Ripartizione | Elemento strutturale | Sezione | Materiale | Stage | Carico distribuito (kN/m) | Assiale (kN) | Ratio M-N | Ratio taglio | Instabilità |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage B | 57.5 | 0 | 0.538 | 0.215 | 0 |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage 3- | 57.523 | 0 | 0.538 | 0.215 | 0 |

Verifiche Travi di Ripartizione NTC2018: A1+M1+R1 (R3 per tiranti)

| Design Assumption: NTC2018: A1+M1+R1 (R3 per tiranti) | | Tipo Risultato: Verifiche Travi di Ripartizione | | NTC2018 (ITA) | | | | | | |
|---|-------------------------|--|-----------|------------------|---------------------------------|-----------------|--------------|-----------------|-------------|--|
| Trave di Ripartizione | Elemento strutturale | Sezione | Materiale | Stage | Carico distribuito (kN/m) | Assiale (kN) | Ratio M-N | Ratio taglio | Instabilità | |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage B | 74.75 | 0 | 0.7 | 0.28 | 0 | |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage 3- | 74.78 | 0 | 0.7 | 0.28 | 0 | |

Verifiche Travi di Ripartizione NTC2018: A2+M2+R1

| Design Assumption: NTC2018: A2+M2+R1 Trave di Ripartizione | Tipo Risultato: Verifiche Travi di Ripartizione Elemento strutturale | NTC2018 (ITA) Sezione | Materiale | Stage | Carico distribuito (kN/m) | Assiale (kN) | Ratio M-N | Ratio taglio | Instabilità |
|--|--|-----------------------------|-----------|-------------|---------------------------------|-----------------|--------------|-----------------|-------------|
| | | | | | | | | | |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage B | 57.5 | 0 | 0.538 | 0.215 | 0 |
| Default Waler | Tieback_New_New_New_New | HE 160B | S355 | Stage 3- | 57.518 | 0 | 0.538 | 0.215 | 0 |