

ALLEGATO 6
VERIFICHE DI STABILITÀ INTERFERENZA 14
SEZIONE A-A' - RELAZIONI DI CALCOLO

VERIFICA DI STABILITÀ PRE-OPERAM IN ASSENZA DI FALDA ACQUIFERA

Analisi di stabilità dei pendii con BISHOP

| | |
|--------------------------------------|------|
| Numero di strati | 2.0 |
| Numero dei conci | 50.0 |
| Coefficiente di sicurezza [R2] | 1.1 |
| Superficie di forma circolare | |

Maglia dei Centri

| | |
|--|----------|
| Ascissa vertice sinistro inferiore xi | 43.87 m |
| Ordinata vertice sinistro inferiore yi | 268.82 m |
| Ascissa vertice destro superiore xs | 126.84 m |
| Ordinata vertice destro superiore ys | 332.33 m |
| Passo di ricerca | 10.0 |
| Numero di celle lungo x | 10.0 |
| Numero di celle lungo y | 10.0 |

Coefficienti sismici [N.T.C.] 2018

Dati generali

| | |
|----------------------|---------------------|
| Descrizione: | |
| Latitudine: | 41.87 |
| Longitudine: | 14.87 |
| Tipo di costruzione: | 2 - Opere ordinarie |
| Classe d'uso: | Classe IV |
| Vita nominale: | 50.0 [anni] |
| Vita di riferimento: | 100.0 [anni] |

Parametri sismici su sito di riferimento

| | |
|------------------------|----|
| Categoria sottosuolo: | B |
| Categoria topografica: | T1 |

| S.L. Stato limite | TR Tempo ritorno [anni] | ag [m/s ²] | F0 [-] | TC* [sec] |
|----------------------|-------------------------------|---------------------------|-----------|--------------|
| S.L.O. | 60.0 | 0.68 | 2.46 | 0.32 |
| S.L.D. | 101.0 | 0.86 | 2.52 | 0.33 |
| S.L.V. | 949.0 | 2.13 | 2.51 | 0.36 |
| S.L.C. | 1950.0 | 2.77 | 2.47 | 0.37 |

Coefficienti sismici orizzontali e verticali

Opera: Stabilità dei pendii

| S.L. Stato limite | amax [m/s ²] | beta [-] | kh [-] | kv [sec] |
|----------------------|-----------------------------|-------------|-----------|-------------|
| S.L.O. | 0.816 | 0.2 | 0.0166 | 0.0083 |
| S.L.D. | 1.032 | 0.2 | 0.021 | 0.0105 |
| S.L.V. | 2.5175 | 0.28 | 0.0719 | 0.0359 |
| S.L.C. | 3.1049 | 0.28 | 0.0887 | 0.0443 |

Coefficiente azione sismica orizzontale 0.0719
 Coefficiente azione sismica verticale 0.0359

Vertici profilo

| N | X m | y m |
|----|--------|--------|
| 1 | 0.0 | 133.5 |
| 2 | 4.79 | 133.0 |
| 3 | 15.03 | 133.0 |
| 4 | 18.76 | 133.5 |
| 5 | 21.21 | 134.0 |
| 6 | 23.43 | 134.5 |
| 7 | 25.64 | 135.0 |
| 8 | 27.99 | 135.5 |
| 9 | 30.4 | 136.0 |
| 10 | 33.04 | 136.5 |
| 11 | 35.9 | 137.0 |
| 12 | 38.73 | 137.5 |
| 13 | 42.09 | 138.0 |
| 14 | 45.58 | 138.5 |
| 15 | 49.06 | 139.0 |
| 16 | 52.42 | 139.5 |
| 17 | 55.83 | 140.0 |
| 18 | 59.16 | 140.5 |
| 19 | 62.51 | 141.0 |
| 20 | 65.75 | 141.5 |
| 21 | 69.02 | 142.0 |
| 22 | 72.29 | 142.5 |
| 23 | 75.46 | 143.0 |
| 24 | 78.49 | 143.5 |
| 25 | 81.36 | 144.0 |
| 26 | 84.23 | 144.5 |
| 27 | 87.13 | 145.0 |
| 28 | 90.06 | 145.5 |
| 29 | 93.03 | 146.0 |
| 30 | 96.05 | 146.5 |
| 31 | 99.15 | 147.0 |
| 32 | 102.39 | 147.5 |
| 33 | 105.63 | 148.0 |
| 34 | 108.76 | 148.5 |
| 35 | 111.81 | 149.0 |
| 36 | 114.79 | 149.5 |
| 37 | 117.7 | 150.0 |
| 38 | 120.53 | 150.5 |
| 39 | 123.31 | 151.0 |
| 40 | 125.92 | 151.5 |
| 41 | 128.42 | 152.0 |
| 42 | 130.86 | 152.5 |
| 43 | 133.19 | 153.0 |
| 44 | 135.62 | 153.5 |
| 45 | 138.19 | 154.0 |
| 46 | 141.0 | 154.5 |
| 47 | 144.56 | 155.0 |
| 48 | 150.36 | 155.5 |
| 49 | 168.32 | 155.5 |
| 50 | 177.09 | 155.0 |

Vertici strato1

| N | X m | y m |
|----|--------|--------|
| 1 | 0.0 | 128.5 |
| 2 | 5.84 | 127.79 |
| 3 | 10.32 | 128.02 |
| 4 | 16.38 | 128.69 |
| 5 | 23.61 | 130.01 |
| 6 | 33.08 | 131.97 |
| 7 | 42.54 | 134.29 |
| 8 | 53.87 | 135.46 |
| 9 | 59.14 | 135.46 |
| 10 | 63.6 | 135.87 |
| 11 | 68.47 | 136.68 |
| 12 | 75.36 | 138.3 |
| 13 | 81.52 | 139.98 |
| 14 | 87.08 | 141.12 |
| 15 | 91.17 | 141.62 |
| 16 | 94.15 | 141.79 |
| 17 | 97.87 | 142.11 |
| 18 | 102.28 | 142.27 |
| 19 | 107.81 | 142.56 |
| 20 | 112.68 | 142.76 |
| 21 | 118.36 | 143.78 |
| 22 | 122.41 | 144.79 |
| 23 | 125.86 | 146.01 |
| 24 | 130.04 | 148.22 |
| 25 | 135.94 | 150.54 |
| 26 | 143.08 | 152.33 |
| 27 | 148.72 | 152.63 |
| 28 | 155.15 | 152.45 |
| 29 | 161.87 | 152.03 |
| 30 | 169.14 | 151.59 |
| 31 | 177.09 | 151.0 |

Stratigrafia

c: coesione; Fi: Angolo di attrito; G: Peso Specifico; Gs: Peso Specifico Saturo

| Strato | c (kg/cm ²) | Fi (°) | G (Kg/m ³) | Gs (Kg/m ³) | Litologia |
|--------|----------------------------|-----------|---------------------------|----------------------------|-----------|
| 1 | 0.04 | 17.8 | 1835 | 1947 | |
| 2 | 0.39 | 22.5 | 2090 | 2110 | |

Risultati analisi pendio [A2+M2+R2]

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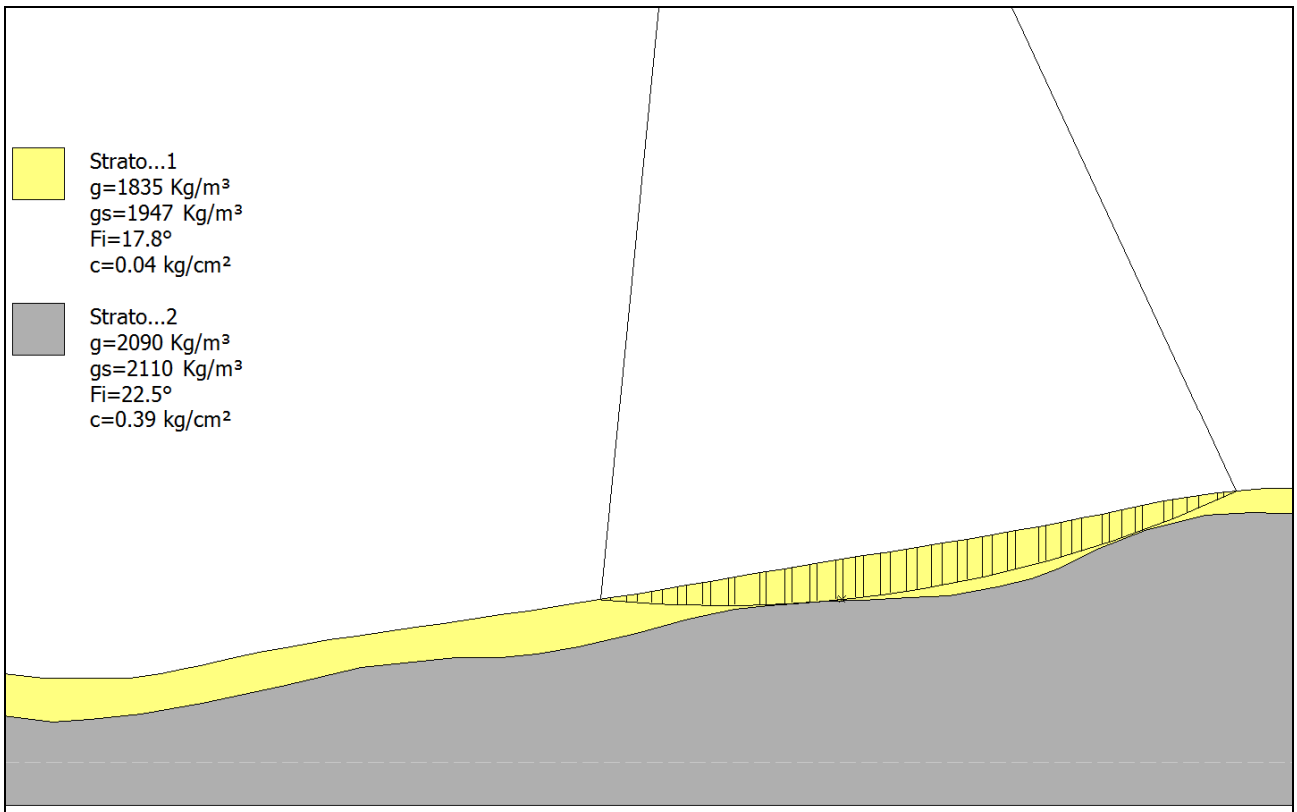
| | |
|----------------------------|----------|
| Fs minimo individuato | 1.25 |
| Ascissa centro superficie | 85.35 m |
| Ordinata centro superficie | 287.87 m |
| Raggio superficie | 146.23 m |

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B: Larghezza del concio; Alfa: Angolo di inclinazione della base del concio; Li: Lunghezza della base del concio; Wi: Peso del concio ; Ui: Forze derivanti dalle pressioni neutre; Ni: forze agenti normalmente alla direzione di scivolamento; Ti: forze agenti parallelamente alla superficie di scivolamento; Fi: Angolo di attrito; c: coesione.

Analisi dei conchi. Superficie...xc = 85.354 yc = 287.869 Rc = 146.235 Fs=1.2506

| Nr. | B m | Alfa (°) | Li m | Wi (Kg) | Kh•Wi (Kg) | Kv•Wi (Kg) | c (kg/cm ²) | Fi (°) | Ui (Kg) | N'i (Kg) | Ti (Kg) |
|-----|--------|-------------|---------|------------|---------------|---------------|----------------------------|-----------|------------|-------------|------------|
| 1 | 1.14 | -5.3 | 1.14 | 295.39 | 21.24 | 10.6 | 0.03 | 14.4 | 0.0 | 330.4 | 360.4 |
| 2 | 1.89 | -4.8 | 1.9 | 1773.52 | 127.52 | 63.67 | 0.03 | 14.4 | 0.0 | 1851.6 | 865.6 |
| 3 | 1.28 | -4.1 | 1.28 | 2077.24 | 149.35 | 74.57 | 0.03 | 14.4 | 0.0 | 2138.1 | 767.4 |
| 4 | 1.75 | -3.5 | 1.75 | 3949.88 | 284.0 | 141.8 | 0.03 | 14.4 | 0.0 | 4036.3 | 1277.2 |
| 5 | 1.28 | -2.9 | 1.28 | 3684.75 | 264.93 | 132.28 | 0.03 | 14.4 | 0.0 | 3746.0 | 1097.7 |
| 6 | 1.75 | -2.3 | 1.75 | 6072.87 | 436.64 | 218.02 | 0.03 | 14.4 | 0.0 | 6148.1 | 1710.0 |
| 7 | 1.12 | -1.8 | 1.12 | 4527.42 | 325.52 | 162.53 | 0.03 | 14.4 | 0.0 | 4567.8 | 1225.7 |
| 8 | 1.9 | -1.2 | 1.91 | 8737.74 | 628.24 | 313.68 | 0.03 | 14.4 | 0.0 | 8787.3 | 2292.2 |
| 9 | 0.97 | -0.6 | 0.97 | 4909.32 | 352.98 | 176.24 | 0.03 | 14.4 | 0.0 | 4923.4 | 1258.1 |
| 10 | 2.06 | 0.0 | 2.06 | 11521.65 | 828.41 | 413.63 | 0.03 | 14.4 | 0.0 | 11523.5 | 2894.6 |
| 11 | 0.84 | 0.5 | 0.84 | 5046.5 | 362.84 | 181.17 | 0.03 | 14.4 | 0.0 | 5035.1 | 1248.2 |
| 12 | 2.93 | 1.3 | 2.93 | 19244.62 | 1383.69 | 690.88 | 0.03 | 14.4 | 0.0 | 19145.5 | 4681.9 |
| 13 | 0.78 | 2.0 | 0.78 | 5468.73 | 393.2 | 196.33 | 0.03 | 14.4 | 0.0 | 5426.3 | 1313.0 |
| 14 | 2.19 | 2.6 | 2.2 | 16236.85 | 1167.43 | 582.9 | 0.03 | 14.4 | 0.0 | 16079.3 | 3864.3 |
| 15 | 0.83 | 3.2 | 0.84 | 6443.38 | 463.28 | 231.32 | 0.03 | 14.4 | 0.0 | 6368.9 | 1521.8 |
| 16 | 2.19 | 3.8 | 2.19 | 17523.87 | 1259.97 | 629.11 | 0.03 | 14.4 | 0.0 | 17291.2 | 4111.7 |
| 17 | 0.84 | 4.4 | 0.84 | 6970.81 | 501.2 | 250.25 | 0.03 | 14.4 | 0.0 | 6867.0 | 1626.5 |
| 18 | 2.26 | 5.0 | 2.27 | 19196.07 | 1380.2 | 689.14 | 0.03 | 14.4 | 0.0 | 18880.9 | 4457.6 |
| 19 | 0.77 | 5.6 | 0.77 | 6696.17 | 481.45 | 240.39 | 0.03 | 14.4 | 0.0 | 6577.0 | 1548.9 |
| 20 | 1.51 | 6.0 | 1.52 | 13325.19 | 958.08 | 478.37 | 0.03 | 14.4 | 0.0 | 13075.0 | 3074.9 |
| 21 | 0.96 | 6.5 | 0.96 | 8503.35 | 611.39 | 305.27 | 0.03 | 14.4 | 0.0 | 8335.3 | 1957.9 |
| 22 | 2.07 | 7.1 | 2.09 | 18655.47 | 1341.33 | 669.73 | 0.03 | 14.4 | 0.0 | 18265.8 | 4285.9 |
| 23 | 1.17 | 7.7 | 1.18 | 10585.22 | 761.08 | 380.01 | 0.03 | 14.4 | 0.0 | 10352.6 | 2427.5 |
| 24 | 1.86 | 8.3 | 1.88 | 16968.55 | 1220.04 | 609.17 | 0.03 | 14.4 | 0.0 | 16580.2 | 3886.5 |
| 25 | 1.27 | 9.0 | 1.28 | 11593.54 | 833.58 | 416.21 | 0.03 | 14.4 | 0.0 | 11318.5 | 2653.2 |
| 26 | 1.76 | 9.6 | 1.78 | 16075.77 | 1155.85 | 577.12 | 0.03 | 14.4 | 0.0 | 15682.8 | 3677.5 |
| 27 | 1.29 | 10.2 | 1.31 | 11753.01 | 845.04 | 421.93 | 0.03 | 14.4 | 0.0 | 11458.3 | 2688.7 |
| 28 | 1.74 | 10.8 | 1.77 | 15739.27 | 1131.65 | 565.04 | 0.03 | 14.4 | 0.0 | 15336.3 | 3602.4 |
| 29 | 1.24 | 11.4 | 1.27 | 11154.52 | 802.01 | 400.45 | 0.03 | 14.4 | 0.0 | 10864.0 | 2555.4 |
| 30 | 1.79 | 12.0 | 1.83 | 15860.44 | 1140.37 | 569.39 | 0.03 | 14.4 | 0.0 | 15441.6 | 3638.5 |
| 31 | 1.12 | 12.6 | 1.15 | 9842.19 | 707.65 | 353.33 | 0.03 | 14.4 | 0.0 | 9579.6 | 2262.0 |
| 32 | 1.9 | 13.2 | 1.96 | 16396.99 | 1178.94 | 588.65 | 0.03 | 14.4 | 0.0 | 15956.0 | 3777.4 |
| 33 | 0.93 | 13.7 | 0.95 | 7818.25 | 562.13 | 280.68 | 0.03 | 14.4 | 0.0 | 7607.0 | 1806.1 |
| 34 | 2.78 | 14.5 | 2.87 | 22801.33 | 1639.42 | 818.57 | 0.03 | 14.4 | 0.0 | 22183.1 | 5290.6 |
| 35 | 0.84 | 15.2 | 0.87 | 6635.24 | 477.07 | 238.21 | 0.03 | 14.4 | 0.0 | 6455.3 | 1547.7 |
| 36 | 1.77 | 15.7 | 1.84 | 13694.59 | 984.64 | 491.64 | 0.03 | 14.4 | 0.0 | 13324.1 | 3207.8 |
| 37 | 1.26 | 16.4 | 1.31 | 9371.64 | 673.82 | 336.44 | 0.03 | 14.4 | 0.0 | 9119.1 | 2207.6 |
| 38 | 1.24 | 16.9 | 1.3 | 9012.65 | 648.01 | 323.55 | 0.03 | 14.4 | 0.0 | 8770.8 | 2134.1 |
| 39 | 2.44 | 17.6 | 2.56 | 16781.66 | 1206.6 | 602.46 | 0.03 | 14.4 | 0.0 | 16334.4 | 4009.8 |
| 40 | 0.86 | 18.3 | 0.9 | 5595.43 | 402.31 | 200.88 | 0.03 | 14.4 | 0.0 | 5447.1 | 1349.9 |
| 41 | 1.47 | 18.8 | 1.56 | 9225.15 | 663.29 | 331.18 | 0.03 | 14.4 | 0.0 | 8981.5 | 2242.5 |
| 42 | 1.56 | 19.4 | 1.65 | 9159.64 | 658.58 | 328.83 | 0.03 | 14.4 | 0.0 | 8917.7 | 2253.6 |
| 43 | 0.87 | 19.9 | 0.93 | 4849.85 | 348.7 | 174.11 | 0.03 | 14.4 | 0.0 | 4720.9 | 1207.5 |
| 44 | 2.57 | 20.6 | 2.75 | 12862.04 | 924.78 | 461.75 | 0.03 | 14.4 | 0.0 | 12511.7 | 3272.3 |
| 45 | 1.1 | 21.4 | 1.18 | 4776.76 | 343.45 | 171.49 | 0.03 | 14.4 | 0.0 | 4638.9 | 1254.6 |
| 46 | 1.71 | 22.0 | 1.85 | 6472.12 | 465.35 | 232.35 | 0.03 | 14.4 | 0.0 | 6269.4 | 1760.0 |
| 47 | 1.32 | 22.6 | 1.43 | 4067.77 | 292.47 | 146.03 | 0.03 | 14.4 | 0.0 | 3919.5 | 1170.0 |
| 48 | 2.24 | 23.4 | 2.44 | 4845.77 | 348.41 | 173.96 | 0.03 | 14.4 | 0.0 | 4600.5 | 1570.3 |
| 49 | 0.78 | 24.1 | 0.86 | 1012.6 | 72.81 | 36.35 | 0.03 | 14.4 | 0.0 | 925.9 | 410.1 |
| 50 | 1.51 | 24.5 | 1.66 | 786.57 | 56.55 | 28.24 | 0.03 | 14.4 | 0.0 | 612.7 | 551.8 |



VERIFICA DI STABILITÀ PRE-OPERAM IN PRESENZA DI FALDA ACQUIFERA

Analisi di stabilità dei pendii con BISHOP

| | |
|--------------------------------|------|
| Numero di strati | 2.0 |
| Numero dei conci | 50.0 |
| Coefficiente di sicurezza [R2] | 1.1 |

Superficie di forma circolare

Maglia dei Centri

| | |
|--|----------|
| Ascissa vertice sinistro inferiore xi | 43.87 m |
| Ordinata vertice sinistro inferiore yi | 268.82 m |
| Ascissa vertice destro superiore xs | 126.84 m |
| Ordinata vertice destro superiore ys | 332.33 m |
| Passo di ricerca | 10.0 |
| Numero di celle lungo x | 10.0 |
| Numero di celle lungo y | 10.0 |

Coefficienti sismici [N.T.C.] 2018

Dati generali

| | |
|----------------------|---------------------|
| Descrizione: | |
| Latitudine: | 41.87 |
| Longitudine: | 14.87 |
| Tipo di costruzione: | 2 - Opere ordinarie |
| Classe d'uso: | Classe IV |
| Vita nominale: | 50.0 [anni] |
| Vita di riferimento: | 100.0 [anni] |

Parametri sismici su sito di riferimento

| | |
|------------------------|----|
| Categoria sottosuolo: | B |
| Categoria topografica: | T1 |

| S.L. Stato limite | TR Tempo ritorno [anni] | ag [m/s ²] | F0 [-] | TC* [sec] |
|----------------------|-------------------------------|---------------------------|-----------|--------------|
| S.L.O. | 60.0 | 0.68 | 2.46 | 0.32 |
| S.L.D. | 101.0 | 0.86 | 2.52 | 0.33 |
| S.L.V. | 949.0 | 2.13 | 2.51 | 0.36 |
| S.L.C. | 1950.0 | 2.77 | 2.47 | 0.37 |

Coefficienti sismici orizzontali e verticali

Opera: Stabilità dei pendii

| S.L. Stato limite | amax [m/s ²] | beta [-] | kh [-] | kv [sec] |
|----------------------|-----------------------------|-------------|-----------|-------------|
| S.L.O. | 0.816 | 0.2 | 0.0166 | 0.0083 |
| S.L.D. | 1.032 | 0.2 | 0.021 | 0.0105 |
| S.L.V. | 2.5175 | 0.28 | 0.0719 | 0.0359 |
| S.L.C. | 3.1049 | 0.28 | 0.0887 | 0.0443 |

| | |
|---|--------|
| Coefficiente azione sismica orizzontale | 0.0719 |
| Coefficiente azione sismica verticale | 0.0359 |

Vertici profilo

| N | X m | y m |
|----|--------|--------|
| 1 | 0.0 | 133.5 |
| 2 | 4.79 | 133.0 |
| 3 | 15.03 | 133.0 |
| 4 | 18.76 | 133.5 |
| 5 | 21.21 | 134.0 |
| 6 | 23.43 | 134.5 |
| 7 | 25.64 | 135.0 |
| 8 | 27.99 | 135.5 |
| 9 | 30.4 | 136.0 |
| 10 | 33.04 | 136.5 |
| 11 | 35.9 | 137.0 |
| 12 | 38.73 | 137.5 |
| 13 | 42.09 | 138.0 |
| 14 | 45.58 | 138.5 |
| 15 | 49.06 | 139.0 |
| 16 | 52.42 | 139.5 |
| 17 | 55.83 | 140.0 |
| 18 | 59.16 | 140.5 |
| 19 | 62.51 | 141.0 |
| 20 | 65.75 | 141.5 |
| 21 | 69.02 | 142.0 |
| 22 | 72.29 | 142.5 |
| 23 | 75.46 | 143.0 |
| 24 | 78.49 | 143.5 |
| 25 | 81.36 | 144.0 |
| 26 | 84.23 | 144.5 |
| 27 | 87.13 | 145.0 |
| 28 | 90.06 | 145.5 |
| 29 | 93.03 | 146.0 |
| 30 | 96.05 | 146.5 |
| 31 | 99.15 | 147.0 |
| 32 | 102.39 | 147.5 |
| 33 | 105.63 | 148.0 |
| 34 | 108.76 | 148.5 |
| 35 | 111.81 | 149.0 |
| 36 | 114.79 | 149.5 |
| 37 | 117.7 | 150.0 |
| 38 | 120.53 | 150.5 |
| 39 | 123.31 | 151.0 |
| 40 | 125.92 | 151.5 |
| 41 | 128.42 | 152.0 |
| 42 | 130.86 | 152.5 |
| 43 | 133.19 | 153.0 |
| 44 | 135.62 | 153.5 |
| 45 | 138.19 | 154.0 |
| 46 | 141.0 | 154.5 |
| 47 | 144.56 | 155.0 |
| 48 | 150.36 | 155.5 |
| 49 | 168.32 | 155.5 |
| 50 | 177.09 | 155.0 |

Falda

| Nr. | X m | y m |
|-----|--------|--------|
| 1 | 0.0 | 133.5 |
| 2 | 4.79 | 133.0 |

| | | |
|----|--------|-------|
| 3 | 15.03 | 133.0 |
| 4 | 18.76 | 133.5 |
| 5 | 21.21 | 134.0 |
| 6 | 23.43 | 134.5 |
| 7 | 25.64 | 135.0 |
| 8 | 27.99 | 135.5 |
| 9 | 30.4 | 136.0 |
| 10 | 33.04 | 136.5 |
| 11 | 35.9 | 137.0 |
| 12 | 38.73 | 137.5 |
| 13 | 42.09 | 138.0 |
| 14 | 45.58 | 138.5 |
| 15 | 49.06 | 139.0 |
| 16 | 52.42 | 139.5 |
| 17 | 55.83 | 140.0 |
| 18 | 59.16 | 140.5 |
| 19 | 62.51 | 141.0 |
| 20 | 65.75 | 141.5 |
| 21 | 69.02 | 142.0 |
| 22 | 72.29 | 142.5 |
| 23 | 75.46 | 143.0 |
| 24 | 78.49 | 143.5 |
| 25 | 81.36 | 144.0 |
| 26 | 84.23 | 144.5 |
| 27 | 87.13 | 145.0 |
| 28 | 90.06 | 145.5 |
| 29 | 93.03 | 146.0 |
| 30 | 96.05 | 146.5 |
| 31 | 99.15 | 147.0 |
| 32 | 102.39 | 147.5 |
| 33 | 105.63 | 148.0 |
| 34 | 108.76 | 148.5 |
| 35 | 111.81 | 149.0 |
| 36 | 114.79 | 149.5 |
| 37 | 117.7 | 150.0 |
| 38 | 120.53 | 150.5 |
| 39 | 123.31 | 151.0 |
| 40 | 125.92 | 151.5 |
| 41 | 128.42 | 152.0 |
| 42 | 130.86 | 152.5 |
| 43 | 133.19 | 153.0 |
| 44 | 135.62 | 153.5 |
| 45 | 138.19 | 154.0 |
| 46 | 141.0 | 154.5 |
| 47 | 144.56 | 155.0 |
| 48 | 150.36 | 155.5 |
| 49 | 168.32 | 155.5 |
| 50 | 177.09 | 155.0 |

Vertici strato1

| N | X m | y m |
|---|--------|--------|
| 1 | 0.0 | 128.5 |
| 2 | 5.84 | 127.79 |
| 3 | 10.32 | 128.02 |
| 4 | 16.38 | 128.69 |
| 5 | 23.61 | 130.01 |
| 6 | 33.08 | 131.97 |
| 7 | 42.54 | 134.29 |

| | | |
|----|--------|--------|
| 8 | 53.87 | 135.46 |
| 9 | 59.14 | 135.46 |
| 10 | 63.6 | 135.87 |
| 11 | 68.47 | 136.68 |
| 12 | 75.36 | 138.3 |
| 13 | 81.52 | 139.98 |
| 14 | 87.08 | 141.12 |
| 15 | 91.17 | 141.62 |
| 16 | 94.15 | 141.79 |
| 17 | 97.87 | 142.11 |
| 18 | 102.28 | 142.27 |
| 19 | 107.81 | 142.56 |
| 20 | 112.68 | 142.76 |
| 21 | 118.36 | 143.78 |
| 22 | 122.41 | 144.79 |
| 23 | 125.86 | 146.01 |
| 24 | 130.04 | 148.22 |
| 25 | 135.94 | 150.54 |
| 26 | 143.08 | 152.33 |
| 27 | 148.72 | 152.63 |
| 28 | 155.15 | 152.45 |
| 29 | 161.87 | 152.03 |
| 30 | 169.14 | 151.59 |
| 31 | 177.09 | 151.0 |

Stratigrafia

c: coesione; Fi: Angolo di attrito; G: Peso Specifico; Gs: Peso Specifico Saturo

| Strato | c (kg/cm ²) | Fi (°) | G (Kg/m ³) | Gs (Kg/m ³) | Litologia |
|--------|----------------------------|-----------|---------------------------|----------------------------|-----------|
| 1 | 0.04 | 17.8 | 1835 | 1947 | |
| 2 | 0.39 | 22.5 | 2090 | 2110 | |

Risultati analisi pendio [A2+M2+R2]

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Fs minimo individuato 0.7
 Ascissa centro superficie 85.35 m
 Ordinata centro superficie 287.87 m
 Raggio superficie 146.23 m

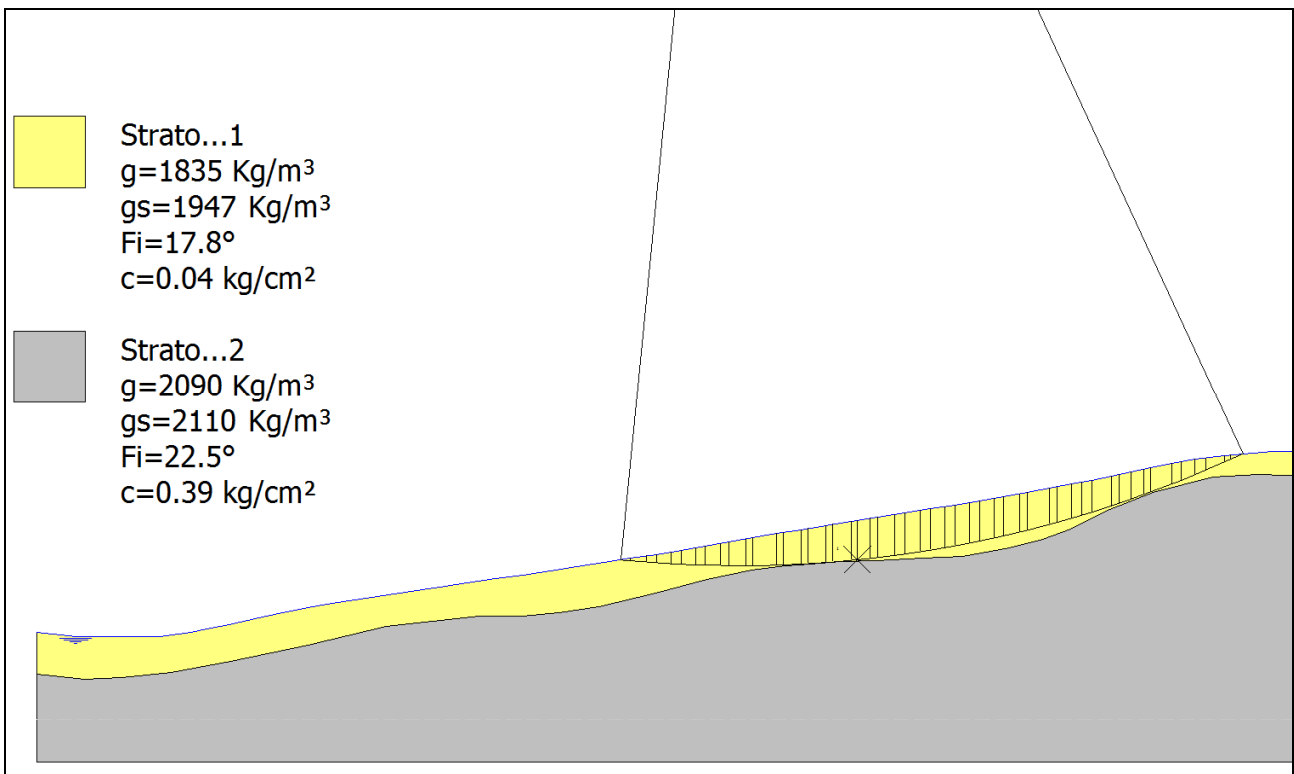
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B: Larghezza del concio; Alfa: Angolo di inclinazione della base del concio; Li: Lunghezza della base del concio; Wi: Peso del concio ; Ui: Forze derivanti dalle pressioni neutre; Ni: forze agenti normalmente alla direzione di scivolamento; Ti: forze agenti parallelamente alla superficie di scivolamento; Fi: Angolo di attrito; c: coesione.

Analisi dei concii. Superficie...xc = 85.354 yc = 287.869 Rc = 146.235 Fs=0.7016

| Nr. | B m | Alfa (°) | Li m | Wi (Kg) | Kh•Wi (Kg) | Kv•Wi (Kg) | c (kg/cm ²) | Fi (°) | Ui (Kg) | N'i (Kg) | Ti (Kg) |
|-----|--------|-------------|---------|------------|---------------|---------------|----------------------------|-----------|------------|-------------|------------|
| 1 | 1.14 | -5.3 | 1.14 | 313.42 | 22.53 | 11.25 | 0.03 | 14.4 | 141.4 | 209.1 | 597.9 |
| 2 | 1.89 | -4.8 | 1.9 | 1881.76 | 135.3 | 67.56 | 0.03 | 14.4 | 511.3 | 1021.5 | 1239.0 |
| 3 | 1.28 | -4.1 | 1.28 | 2204.03 | 158.47 | 79.12 | 0.03 | 14.4 | 884.5 | 1147.4 | 1005.3 |
| 4 | 1.75 | -3.5 | 1.75 | 4190.97 | 301.33 | 150.46 | 0.03 | 14.4 | 1231.1 | 2140.1 | 1582.4 |
| 5 | 1.28 | -2.9 | 1.28 | 3909.65 | 281.1 | 140.36 | 0.03 | 14.4 | 1566.8 | 1971.3 | 1306.9 |
| 6 | 1.75 | -2.3 | 1.75 | 3134.07 | 225.34 | 112.51 | 0.03 | 14.4 | 1894.7 | 3217.7 | 1975.3 |
| 7 | 1.12 | -1.8 | 1.12 | 4803.76 | 345.39 | 172.45 | 0.03 | 14.4 | 2196.5 | 2380.8 | 1384.1 |
| 8 | 1.9 | -1.2 | 1.91 | 9271.05 | 666.59 | 332.83 | 0.03 | 14.4 | 2499.6 | 4563.1 | 2539.6 |
| 9 | 0.97 | -0.6 | 0.97 | 5208.96 | 374.52 | 187.0 | 0.03 | 14.4 | 2772.4 | 2548.8 | 1373.2 |

| | | | | | | | | | | | |
|----|------|------|------|----------|---------|--------|------|------|--------|---------|--------|
| 10 | 2.06 | 0.0 | 2.06 | 12224.88 | 878.97 | 438.87 | 0.03 | 14.4 | 3043.1 | 5948.0 | 3118.5 |
| 11 | 0.84 | 0.5 | 0.84 | 5354.51 | 384.99 | 192.23 | 0.03 | 14.4 | 3286.9 | 2592.1 | 1330.6 |
| 12 | 2.93 | 1.3 | 2.93 | 20419.22 | 1468.14 | 733.05 | 0.03 | 14.4 | 3579.4 | 9824.7 | 4933.4 |
| 13 | 0.78 | 2.0 | 0.78 | 5802.52 | 417.2 | 208.31 | 0.03 | 14.4 | 3841.8 | 2776.2 | 1370.4 |
| 14 | 2.19 | 2.6 | 2.2 | 17227.87 | 1238.68 | 618.48 | 0.03 | 14.4 | 4032.5 | 8207.5 | 4006.5 |
| 15 | 0.83 | 3.2 | 0.84 | 3325.28 | 239.09 | 119.38 | 0.03 | 14.4 | 4210.2 | 3243.5 | 1568.4 |
| 16 | 2.19 | 3.8 | 2.19 | 18593.45 | 1336.87 | 667.5 | 0.03 | 14.4 | 4368.7 | 8785.8 | 4215.5 |
| 17 | 0.84 | 4.4 | 0.84 | 7396.27 | 531.79 | 265.53 | 0.03 | 14.4 | 4510.0 | 3481.3 | 1659.8 |
| 18 | 2.26 | 5.0 | 2.27 | 20367.71 | 1464.44 | 731.2 | 0.03 | 14.4 | 4633.5 | 9550.2 | 4529.8 |
| 19 | 0.77 | 5.6 | 0.77 | 7104.88 | 510.84 | 255.07 | 0.03 | 14.4 | 4735.5 | 3319.3 | 1568.3 |
| 20 | 1.51 | 6.0 | 1.52 | 14138.5 | 1016.56 | 507.57 | 0.03 | 14.4 | 4795.9 | 6587.6 | 3106.0 |
| 21 | 0.96 | 6.5 | 0.96 | 9022.35 | 648.71 | 323.9 | 0.03 | 14.4 | 4851.0 | 4191.9 | 1973.1 |
| 22 | 2.07 | 7.1 | 2.09 | 19794.11 | 1423.2 | 710.61 | 0.03 | 14.4 | 4904.1 | 9165.5 | 4308.2 |
| 23 | 1.17 | 7.7 | 1.18 | 11231.3 | 807.53 | 403.2 | 0.03 | 14.4 | 4943.2 | 5182.2 | 2434.3 |
| 24 | 1.86 | 8.3 | 1.88 | 18004.24 | 1294.51 | 646.35 | 0.03 | 14.4 | 4968.0 | 8280.5 | 3889.4 |
| 25 | 1.27 | 9.0 | 1.28 | 12301.16 | 884.45 | 441.61 | 0.03 | 14.4 | 4980.0 | 5639.3 | 2650.2 |
| 26 | 1.76 | 9.6 | 1.78 | 17056.96 | 1226.4 | 612.34 | 0.03 | 14.4 | 4978.7 | 7795.5 | 3667.7 |
| 27 | 1.29 | 10.2 | 1.31 | 12470.36 | 896.62 | 447.69 | 0.03 | 14.4 | 4963.6 | 5682.0 | 2678.0 |
| 28 | 1.74 | 10.8 | 1.77 | 16699.92 | 1200.72 | 599.53 | 0.03 | 14.4 | 4935.4 | 7586.5 | 3584.2 |
| 29 | 1.24 | 11.4 | 1.27 | 11835.34 | 850.96 | 424.89 | 0.03 | 14.4 | 4894.0 | 5361.1 | 2540.5 |
| 30 | 1.79 | 12.0 | 1.83 | 16828.49 | 1209.97 | 604.14 | 0.03 | 14.4 | 4838.9 | 7600.7 | 3615.3 |
| 31 | 1.12 | 12.6 | 1.15 | 10442.92 | 750.85 | 374.9 | 0.03 | 14.4 | 4772.7 | 4703.4 | 2247.0 |
| 32 | 1.9 | 13.2 | 1.96 | 17397.79 | 1250.9 | 624.58 | 0.03 | 14.4 | 4691.9 | 7812.9 | 3752.3 |
| 33 | 0.93 | 13.7 | 0.95 | 8295.44 | 596.44 | 297.81 | 0.03 | 14.4 | 4603.6 | 3715.0 | 1794.6 |
| 34 | 2.78 | 14.5 | 2.87 | 24193.02 | 1739.48 | 868.53 | 0.03 | 14.4 | 4469.7 | 10794.5 | 5261.3 |
| 35 | 0.84 | 15.2 | 0.87 | 7040.23 | 506.19 | 252.74 | 0.03 | 14.4 | 4320.5 | 3129.5 | 1541.3 |
| 36 | 1.77 | 15.7 | 1.84 | 14530.44 | 1044.74 | 521.64 | 0.03 | 14.4 | 4209.1 | 6441.3 | 3198.3 |
| 37 | 1.26 | 16.4 | 1.31 | 9943.64 | 714.95 | 356.98 | 0.03 | 14.4 | 4068.7 | 4393.2 | 2205.0 |
| 38 | 1.24 | 16.9 | 1.3 | 9562.74 | 687.56 | 343.3 | 0.03 | 14.4 | 3945.7 | 4212.7 | 2135.5 |
| 39 | 2.44 | 17.6 | 2.56 | 17805.93 | 1280.25 | 639.23 | 0.03 | 14.4 | 3748.1 | 7808.0 | 4026.1 |
| 40 | 0.86 | 18.3 | 0.9 | 5936.95 | 426.87 | 213.14 | 0.03 | 14.4 | 3555.4 | 2591.4 | 1360.7 |
| 41 | 1.47 | 18.8 | 1.56 | 9788.21 | 703.77 | 351.4 | 0.03 | 14.4 | 3414.5 | 4257.3 | 2267.9 |
| 42 | 1.56 | 19.4 | 1.65 | 9718.7 | 698.77 | 348.9 | 0.03 | 14.4 | 3208.1 | 4204.4 | 2291.6 |
| 43 | 0.87 | 19.9 | 0.93 | 5145.86 | 369.99 | 184.74 | 0.03 | 14.4 | 3023.8 | 2214.7 | 1234.8 |
| 44 | 2.57 | 20.6 | 2.75 | 13647.08 | 981.23 | 489.93 | 0.03 | 14.4 | 2727.3 | 5818.8 | 3382.8 |
| 45 | 1.1 | 21.4 | 1.18 | 5068.31 | 364.41 | 181.95 | 0.03 | 14.4 | 2370.0 | 2131.0 | 1318.2 |
| 46 | 1.71 | 22.0 | 1.85 | 6867.14 | 493.75 | 246.53 | 0.03 | 14.4 | 2060.6 | 2841.8 | 1882.4 |
| 47 | 1.32 | 22.6 | 1.43 | 2099.28 | 150.94 | 75.36 | 0.03 | 14.4 | 1683.6 | 1737.8 | 1286.9 |
| 48 | 2.24 | 23.4 | 2.44 | 2500.79 | 179.81 | 89.78 | 0.03 | 14.4 | 1177.2 | 1935.7 | 1823.5 |
| 49 | 0.78 | 24.1 | 0.86 | 1074.41 | 77.25 | 38.57 | 0.03 | 14.4 | 703.0 | 341.5 | 517.1 |
| 50 | 1.51 | 24.5 | 1.66 | 834.58 | 60.01 | 29.96 | 0.03 | 14.4 | 283.1 | 85.3 | 790.4 |



VERIFICA DI STABILITÀ POST-OPERAM IN PRESENZA DI FALDA ACQUIFERA

Analisi di stabilità dei pendii con BISHOP

| | |
|--------------------------------|------|
| Numero di strati | 2.0 |
| Numero dei conci | 50.0 |
| Coefficiente di sicurezza [R2] | 1.1 |

Superficie di forma circolare

Maglia dei Centri

| | |
|--|----------|
| Ascissa vertice sinistro inferiore xi | 47.25 m |
| Ordinata vertice sinistro inferiore yi | 243.85 m |
| Ascissa vertice destro superiore xs | 130.23 m |
| Ordinata vertice destro superiore ys | 307.35 m |
| Passo di ricerca | 10.0 |
| Numero di celle lungo x | 10.0 |
| Numero di celle lungo y | 10.0 |

Coefficienti sismici [N.T.C.] 2018

Dati generali

| | |
|----------------------|---------------------|
| Descrizione: | |
| Latitudine: | 41.87 |
| Longitudine: | 14.87 |
| Tipo opera: | 2 - Opere ordinarie |
| Classe d'uso: | Classe IV |
| Vita nominale: | 50.0 [anni] |
| Vita di riferimento: | 100.0 [anni] |

Parametri sismici su sito di riferimento

| | |
|------------------------|----|
| Categoria sottosuolo: | B |
| Categoria topografica: | T1 |

| S.L. Stato limite | TR Tempo ritorno [anni] | ag [m/s ²] | F0 [-] | TC* [sec] |
|----------------------|-------------------------------|---------------------------|-----------|--------------|
| S.L.O. | 60.0 | 0.68 | 2.46 | 0.32 |
| S.L.D. | 101.0 | 0.86 | 2.52 | 0.33 |
| S.L.V. | 949.0 | 2.13 | 2.51 | 0.36 |
| S.L.C. | 1950.0 | 2.77 | 2.47 | 0.37 |

Coefficienti sismici orizzontali e verticali

Opera: Stabilità dei pendii

| S.L. Stato limite | amax [m/s ²] | beta [-] | kh [-] | kv [sec] |
|----------------------|-----------------------------|-------------|-----------|-------------|
| S.L.O. | 0.816 | 0.2 | 0.0166 | 0.0083 |
| S.L.D. | 1.032 | 0.2 | 0.021 | 0.0105 |
| S.L.V. | 2.5175 | 0.28 | 0.0719 | 0.0359 |
| S.L.C. | 3.1049 | 0.28 | 0.0887 | 0.0443 |

| | |
|---|--------|
| Coefficiente azione sismica orizzontale | 0.0719 |
| Coefficiente azione sismica verticale | 0.0359 |

Vertici profilo

| N | X m | y m |
|----|--------|--------|
| 1 | 0.0 | 133.5 |
| 2 | 4.79 | 133.0 |
| 3 | 15.03 | 133.0 |
| 4 | 18.76 | 133.5 |
| 5 | 21.21 | 134.0 |
| 6 | 23.43 | 134.5 |
| 7 | 25.64 | 135.0 |
| 8 | 27.99 | 135.5 |
| 9 | 30.4 | 136.0 |
| 10 | 33.04 | 136.5 |
| 11 | 35.9 | 137.0 |
| 12 | 38.73 | 137.5 |
| 13 | 42.09 | 138.0 |
| 14 | 45.58 | 138.5 |
| 15 | 49.06 | 139.0 |
| 16 | 52.42 | 139.5 |
| 17 | 55.83 | 140.0 |
| 18 | 59.16 | 140.5 |
| 19 | 62.51 | 141.0 |
| 20 | 65.75 | 141.5 |
| 21 | 69.02 | 142.0 |
| 22 | 72.29 | 142.5 |
| 23 | 75.46 | 143.0 |
| 24 | 78.49 | 143.5 |
| 25 | 81.36 | 144.0 |
| 26 | 84.23 | 144.5 |
| 27 | 87.13 | 145.0 |
| 28 | 90.06 | 145.5 |
| 29 | 93.03 | 146.0 |
| 30 | 96.05 | 146.5 |
| 31 | 99.15 | 147.0 |
| 32 | 102.39 | 147.5 |
| 33 | 105.63 | 148.0 |
| 34 | 108.76 | 148.5 |
| 35 | 111.81 | 149.0 |
| 36 | 114.79 | 149.5 |
| 37 | 117.7 | 150.0 |
| 38 | 120.53 | 150.5 |
| 39 | 123.31 | 151.0 |
| 40 | 125.92 | 151.5 |
| 41 | 128.42 | 152.0 |
| 42 | 130.86 | 152.5 |
| 43 | 133.19 | 153.0 |
| 44 | 135.62 | 153.5 |
| 45 | 138.19 | 154.0 |
| 46 | 141.0 | 154.5 |
| 47 | 144.56 | 155.0 |
| 48 | 150.36 | 155.5 |
| 49 | 168.32 | 155.5 |
| 50 | 177.09 | 155.0 |

Falda

| Nr. | X m | y m |
|-----|--------|--------|
| 1 | 0.0 | 133.5 |
| 2 | 4.79 | 133.0 |

| | | |
|----|--------|-------|
| 3 | 15.03 | 133.0 |
| 4 | 18.76 | 133.5 |
| 5 | 21.21 | 134.0 |
| 6 | 23.43 | 134.5 |
| 7 | 25.64 | 135.0 |
| 8 | 27.99 | 135.5 |
| 9 | 30.4 | 136.0 |
| 10 | 33.04 | 136.5 |
| 11 | 35.9 | 137.0 |
| 12 | 38.73 | 137.5 |
| 13 | 42.09 | 138.0 |
| 14 | 45.58 | 138.5 |
| 15 | 49.06 | 139.0 |
| 16 | 52.42 | 139.5 |
| 17 | 55.83 | 140.0 |
| 18 | 59.16 | 140.5 |
| 19 | 62.51 | 141.0 |
| 20 | 65.75 | 141.5 |
| 21 | 69.02 | 142.0 |
| 22 | 72.29 | 142.5 |
| 23 | 75.46 | 143.0 |
| 24 | 78.49 | 143.5 |
| 25 | 81.36 | 144.0 |
| 26 | 84.23 | 144.5 |
| 27 | 87.13 | 145.0 |
| 28 | 90.06 | 145.5 |
| 29 | 93.03 | 146.0 |
| 30 | 96.05 | 146.5 |
| 31 | 99.15 | 147.0 |
| 32 | 102.39 | 147.5 |
| 33 | 105.63 | 148.0 |
| 34 | 108.76 | 148.5 |
| 35 | 111.81 | 149.0 |
| 36 | 114.79 | 149.5 |
| 37 | 117.7 | 150.0 |
| 38 | 120.53 | 150.5 |
| 39 | 123.31 | 151.0 |
| 40 | 125.92 | 151.5 |
| 41 | 128.42 | 152.0 |
| 42 | 130.86 | 152.5 |
| 43 | 133.19 | 153.0 |
| 44 | 135.62 | 153.5 |
| 45 | 138.19 | 154.0 |
| 46 | 141.0 | 154.5 |
| 47 | 144.56 | 155.0 |
| 48 | 150.36 | 155.5 |
| 49 | 168.32 | 155.5 |
| 50 | 177.09 | 155.0 |

Vertici strato1

| N | X m | y m |
|---|--------|--------|
| 1 | 0.0 | 128.5 |
| 2 | 5.84 | 127.79 |
| 3 | 10.32 | 128.02 |
| 4 | 16.38 | 128.69 |
| 5 | 23.61 | 130.01 |
| 6 | 33.08 | 131.97 |
| 7 | 42.54 | 134.29 |

| | | |
|----|--------|--------|
| 8 | 53.87 | 135.46 |
| 9 | 59.14 | 135.46 |
| 10 | 63.6 | 135.87 |
| 11 | 68.47 | 136.68 |
| 12 | 75.36 | 138.3 |
| 13 | 81.52 | 139.98 |
| 14 | 87.08 | 141.12 |
| 15 | 91.17 | 141.62 |
| 16 | 94.15 | 141.79 |
| 17 | 97.87 | 142.11 |
| 18 | 102.28 | 142.27 |
| 19 | 107.81 | 142.56 |
| 20 | 112.68 | 142.76 |
| 21 | 118.36 | 143.78 |
| 22 | 122.41 | 144.79 |
| 23 | 125.86 | 146.01 |
| 24 | 130.04 | 148.22 |
| 25 | 135.94 | 150.54 |
| 26 | 143.08 | 152.33 |
| 27 | 148.72 | 152.63 |
| 28 | 155.15 | 152.45 |
| 29 | 161.87 | 152.03 |
| 30 | 169.14 | 151.59 |
| 31 | 177.09 | 151.0 |

Stratigrafia

c: coesione; Fi: Angolo di attrito; G: Peso Specifico; Gs: Peso Specifico Saturo

| Strato | c (kg/cm ²) | Fi (°) | G (Kg/m ³) | Gs (Kg/m ³) | Litologia |
|--------|----------------------------|-----------|---------------------------|----------------------------|-----------|
| 1 | 0.04 | 17.8 | 1835 | 1947 | |
| 2 | 0.39 | 22.5 | 2090 | 2110 | |

Pali...

| N° | x m | y m | Diametro m | Lunghezza m | Inclinazione (°) | Interasse m |
|----|----------|----------|---------------|----------------|---------------------|----------------|
| 1 | 142.0157 | 154.6427 | 0.8 | 12 | 90 | 1 |

Risultati analisi pendio [A2+M2+R2]

```

=====
Fs minimo individuato                0.7
Ascissa centro superficie              84.59 m
Ordinata centro superficie             272.42 m
Raggio superficie                       130.96 m
=====

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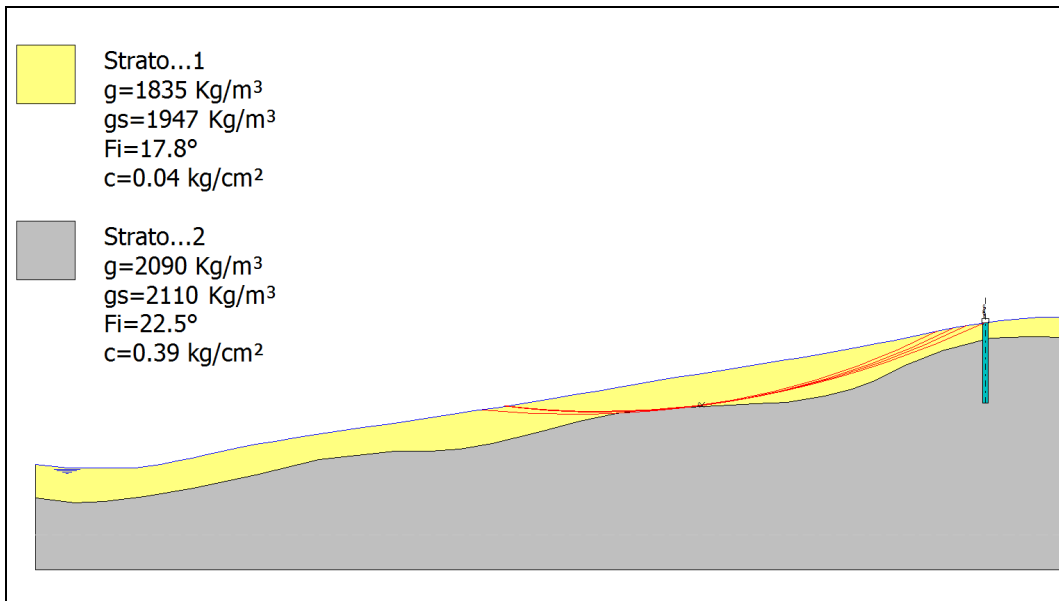
Numero di superfici esaminate....(183)

| N° | Xo | Yo | Ro | Fs |
|----|------|-------|-------|------|
| 1 | 47.3 | 243.8 | 114.3 | 2.18 |
| 2 | 51.4 | 247.0 | 115.4 | 2.19 |
| 3 | 55.6 | 243.8 | 110.8 | 2.26 |
| 4 | 59.7 | 247.0 | 112.1 | 2.23 |
| 5 | 63.8 | 243.8 | 107.7 | 1.99 |
| 6 | 68.0 | 247.0 | 109.4 | 1.79 |
| 7 | 72.1 | 243.8 | 105.2 | 1.83 |
| 8 | 76.3 | 247.0 | 107.3 | 1.63 |
| 9 | 80.4 | 243.8 | 103.3 | 1.59 |
| 10 | 84.6 | 247.0 | 105.8 | 1.17 |

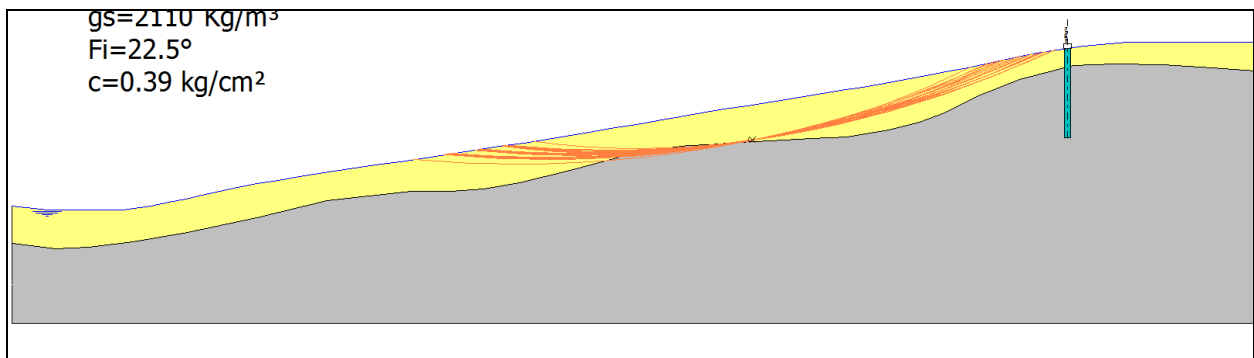
| | | | | |
|----|-------|-------|-------|------|
| 11 | 88.7 | 243.8 | 102.1 | 0.75 |
| 12 | 92.9 | 247.0 | 104.9 | 1.62 |
| 13 | 97.0 | 243.8 | 101.5 | 2.25 |
| 14 | 101.2 | 247.0 | 104.7 | 3.65 |
| 15 | 105.3 | 243.8 | 101.6 | 3.75 |
| 16 | 109.5 | 247.0 | 105.1 | 3.43 |
| 17 | 113.6 | 243.8 | 102.4 | 3.04 |
| 18 | 117.8 | 247.0 | 106.2 | 2.56 |
| 19 | 121.9 | 243.8 | 103.8 | 2.46 |
| 20 | 47.3 | 250.2 | 120.0 | 2.17 |
| 21 | 51.4 | 253.4 | 121.1 | 2.21 |
| 22 | 55.6 | 250.2 | 116.6 | 2.33 |
| 23 | 59.7 | 253.4 | 118.1 | 2.22 |
| 24 | 63.8 | 250.2 | 113.7 | 1.90 |
| 25 | 68.0 | 253.4 | 115.5 | 1.83 |
| 26 | 72.1 | 250.2 | 111.4 | 1.70 |
| 27 | 76.3 | 253.4 | 113.5 | 1.62 |
| 28 | 80.4 | 250.2 | 109.6 | 1.48 |
| 29 | 84.6 | 253.4 | 112.1 | 1.09 |
| 30 | 88.7 | 250.2 | 108.4 | 0.74 |
| 31 | 92.9 | 253.4 | 111.2 | 1.59 |
| 32 | 97.0 | 250.2 | 107.9 | 2.53 |
| 33 | 101.2 | 253.4 | 111.0 | 3.16 |
| 34 | 105.3 | 250.2 | 108.0 | 3.53 |
| 35 | 109.5 | 253.4 | 111.4 | 3.13 |
| 36 | 113.6 | 250.2 | 108.7 | 2.83 |
| 37 | 117.8 | 253.4 | 112.4 | 2.53 |
| 38 | 47.3 | 256.5 | 125.7 | 2.20 |
| 39 | 51.4 | 259.7 | 127.0 | 2.32 |
| 40 | 55.6 | 256.5 | 122.5 | 2.24 |
| 41 | 59.7 | 259.7 | 124.1 | 2.02 |
| 42 | 63.8 | 256.5 | 119.7 | 1.90 |
| 43 | 68.0 | 259.7 | 121.6 | 1.79 |
| 44 | 72.1 | 256.5 | 117.5 | 1.73 |
| 45 | 76.3 | 259.7 | 119.7 | 1.59 |
| 46 | 80.4 | 256.5 | 115.8 | 1.39 |
| 47 | 84.6 | 259.7 | 118.4 | 1.06 |
| 48 | 88.7 | 256.5 | 114.7 | 0.72 |
| 49 | 92.9 | 259.7 | 117.6 | 2.16 |
| 50 | 97.0 | 256.5 | 114.2 | 2.58 |
| 51 | 101.2 | 259.7 | 117.4 | 3.51 |
| 52 | 105.3 | 256.5 | 114.3 | 3.66 |
| 53 | 109.5 | 259.7 | 117.8 | 3.15 |
| 54 | 113.6 | 256.5 | 115.0 | 2.83 |
| 55 | 117.8 | 259.7 | 118.7 | 2.45 |
| 56 | 47.3 | 262.9 | 131.5 | 2.14 |
| 57 | 51.4 | 266.1 | 132.9 | 2.25 |
| 58 | 55.6 | 262.9 | 128.4 | 2.25 |
| 59 | 59.7 | 266.1 | 130.1 | 1.94 |
| 60 | 63.8 | 262.9 | 125.8 | 1.89 |
| 61 | 68.0 | 266.1 | 127.8 | 1.75 |
| 62 | 72.1 | 262.9 | 123.7 | 1.63 |
| 63 | 76.3 | 266.1 | 125.9 | 1.57 |
| 64 | 80.4 | 262.9 | 122.1 | 1.49 |
| 65 | 84.6 | 266.1 | 124.7 | 0.97 |
| 66 | 88.7 | 262.9 | 121.1 | 1.76 |
| 67 | 92.9 | 266.1 | 123.9 | 2.25 |
| 68 | 97.0 | 262.9 | 120.6 | 2.88 |
| 69 | 101.2 | 266.1 | 123.7 | 3.38 |

| | | | | |
|-----|-------|-------|-------|------|
| 70 | 105.3 | 262.9 | 120.7 | 3.91 |
| 71 | 109.5 | 266.1 | 124.1 | 3.11 |
| 72 | 113.6 | 262.9 | 121.3 | 2.77 |
| 73 | 117.8 | 266.1 | 125.0 | 2.58 |
| 74 | 47.3 | 269.2 | 137.4 | 2.21 |
| 75 | 51.4 | 272.4 | 138.8 | 2.27 |
| 76 | 55.6 | 269.2 | 134.4 | 2.24 |
| 77 | 59.7 | 272.4 | 136.1 | 1.85 |
| 78 | 63.8 | 269.2 | 131.9 | 1.77 |
| 79 | 68.0 | 272.4 | 133.9 | 1.69 |
| 80 | 72.1 | 269.2 | 129.9 | 1.59 |
| 81 | 76.3 | 272.4 | 132.2 | 1.52 |
| 82 | 80.4 | 269.2 | 128.4 | 1.34 |
| 83 | 84.6 | 272.4 | 131.0 | 0.70 |
| 84 | 88.7 | 269.2 | 127.4 | 1.91 |
| 85 | 92.9 | 272.4 | 130.3 | 2.55 |
| 86 | 97.0 | 269.2 | 126.9 | 3.21 |
| 87 | 101.2 | 272.4 | 130.1 | 3.38 |
| 88 | 105.3 | 269.2 | 127.0 | 3.65 |
| 89 | 109.5 | 272.4 | 130.4 | 2.98 |
| 90 | 113.6 | 269.2 | 127.6 | 2.69 |
| 91 | 117.8 | 272.4 | 131.3 | 2.50 |
| 92 | 47.3 | 275.6 | 143.3 | 2.21 |
| 93 | 51.4 | 278.8 | 144.8 | 2.28 |
| 94 | 55.6 | 275.6 | 140.4 | 2.30 |
| 95 | 59.7 | 278.8 | 142.2 | 1.79 |
| 96 | 63.8 | 275.6 | 138.0 | 1.76 |
| 97 | 68.0 | 278.8 | 140.1 | 1.62 |
| 98 | 72.1 | 275.6 | 136.1 | 1.52 |
| 99 | 76.3 | 278.8 | 138.4 | 1.42 |
| 100 | 80.4 | 275.6 | 134.7 | 1.26 |
| 101 | 84.6 | 278.8 | 137.3 | 1.75 |
| 102 | 88.7 | 275.6 | 133.7 | 2.11 |
| 103 | 92.9 | 278.8 | 136.6 | 2.80 |
| 104 | 97.0 | 275.6 | 133.3 | 2.80 |
| 105 | 101.2 | 278.8 | 136.4 | 3.67 |
| 106 | 105.3 | 275.6 | 133.4 | 3.51 |
| 107 | 109.5 | 278.8 | 136.8 | 2.92 |
| 108 | 113.6 | 275.6 | 133.9 | 2.70 |
| 109 | 47.3 | 282.0 | 149.2 | 2.22 |
| 110 | 51.4 | 285.1 | 150.8 | 2.31 |
| 111 | 55.6 | 282.0 | 146.5 | 1.93 |
| 112 | 59.7 | 285.1 | 148.3 | 1.74 |
| 113 | 63.8 | 282.0 | 144.2 | 1.65 |
| 114 | 68.0 | 285.1 | 146.3 | 1.65 |
| 115 | 72.1 | 282.0 | 142.3 | 1.50 |
| 116 | 76.3 | 285.1 | 144.7 | 1.37 |
| 117 | 80.4 | 282.0 | 140.9 | 1.19 |
| 118 | 84.6 | 285.1 | 143.6 | 1.72 |
| 119 | 88.7 | 282.0 | 140.0 | 2.32 |
| 120 | 92.9 | 285.1 | 142.9 | 2.57 |
| 121 | 97.0 | 282.0 | 139.6 | 3.07 |
| 122 | 101.2 | 285.1 | 142.8 | 3.81 |
| 123 | 105.3 | 282.0 | 139.7 | 3.49 |
| 124 | 109.5 | 285.1 | 143.1 | 2.96 |
| 125 | 113.6 | 282.0 | 140.3 | 2.78 |
| 126 | 47.3 | 288.3 | 155.1 | 2.22 |
| 127 | 51.4 | 291.5 | 156.8 | 2.27 |
| 128 | 55.6 | 288.3 | 152.5 | 1.81 |

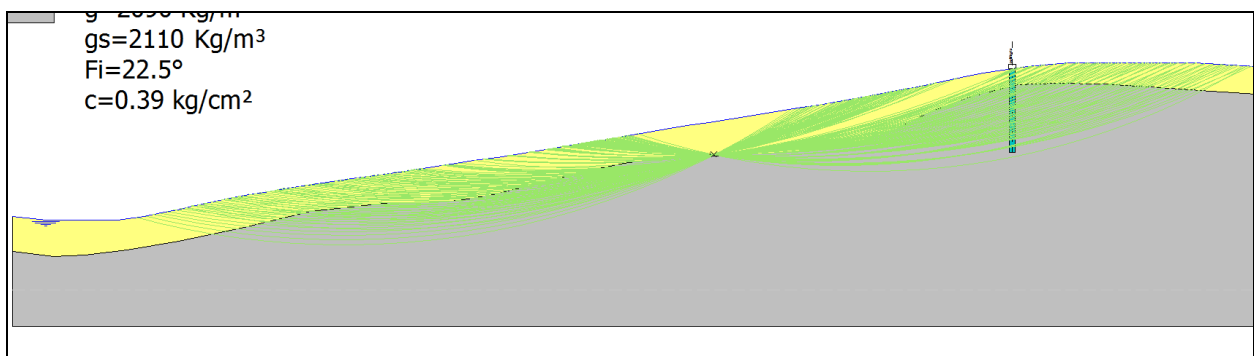
| | | | | |
|-----|-------|-------|-------|------|
| 129 | 59.7 | 291.5 | 154.4 | 1.71 |
| 130 | 63.8 | 288.3 | 150.3 | 1.71 |
| 131 | 68.0 | 291.5 | 152.5 | 1.56 |
| 132 | 72.1 | 288.3 | 148.6 | 1.47 |
| 133 | 76.3 | 291.5 | 151.0 | 1.29 |
| 134 | 80.4 | 288.3 | 147.2 | 1.08 |
| 135 | 84.6 | 291.5 | 149.9 | 1.84 |
| 136 | 88.7 | 288.3 | 146.4 | 2.35 |
| 137 | 92.9 | 291.5 | 149.3 | 2.76 |
| 138 | 97.0 | 288.3 | 146.0 | 2.80 |
| 139 | 101.2 | 291.5 | 149.1 | 3.34 |
| 140 | 105.3 | 288.3 | 146.0 | 3.14 |
| 141 | 109.5 | 291.5 | 149.4 | 2.93 |
| 142 | 113.6 | 288.3 | 146.6 | 2.68 |
| 143 | 47.3 | 294.7 | 161.1 | 2.22 |
| 144 | 51.4 | 297.8 | 162.9 | 2.22 |
| 145 | 55.6 | 294.7 | 158.6 | 1.78 |
| 146 | 59.7 | 297.8 | 160.6 | 1.76 |
| 147 | 63.8 | 294.7 | 156.5 | 1.71 |
| 148 | 68.0 | 297.8 | 158.7 | 1.48 |
| 149 | 72.1 | 294.7 | 154.8 | 1.45 |
| 150 | 76.3 | 297.8 | 157.2 | 1.21 |
| 151 | 80.4 | 294.7 | 153.5 | 2.53 |
| 152 | 84.6 | 297.8 | 156.2 | 2.02 |
| 153 | 88.7 | 294.7 | 152.7 | 2.43 |
| 154 | 92.9 | 297.8 | 155.6 | 2.67 |
| 155 | 97.0 | 294.7 | 152.3 | 2.93 |
| 156 | 101.2 | 297.8 | 155.5 | 3.47 |
| 157 | 105.3 | 294.7 | 152.4 | 3.20 |
| 158 | 109.5 | 297.8 | 155.8 | 2.93 |
| 159 | 113.6 | 294.7 | 152.9 | 2.80 |
| 160 | 47.3 | 301.0 | 167.2 | 2.20 |
| 161 | 51.4 | 304.2 | 168.9 | 2.14 |
| 162 | 55.6 | 301.0 | 164.7 | 1.72 |
| 163 | 59.7 | 304.2 | 166.7 | 1.65 |
| 164 | 63.8 | 301.0 | 162.7 | 1.59 |
| 165 | 68.0 | 304.2 | 164.9 | 1.54 |
| 166 | 72.1 | 301.0 | 161.1 | 1.50 |
| 167 | 76.3 | 304.2 | 163.5 | 3.16 |
| 168 | 80.4 | 301.0 | 159.8 | 2.36 |
| 169 | 84.6 | 304.2 | 162.5 | 2.09 |
| 170 | 88.7 | 301.0 | 159.0 | 2.27 |
| 171 | 92.9 | 304.2 | 162.0 | 2.68 |
| 172 | 97.0 | 301.0 | 158.7 | 3.03 |
| 173 | 101.2 | 304.2 | 161.8 | 3.37 |
| 174 | 105.3 | 301.0 | 158.7 | 3.15 |
| 175 | 109.5 | 304.2 | 162.1 | 2.99 |
| 176 | 47.3 | 307.4 | 173.2 | 2.28 |
| 177 | 55.6 | 307.4 | 170.9 | 1.74 |
| 178 | 63.8 | 307.4 | 168.9 | 1.61 |
| 179 | 72.1 | 307.4 | 167.3 | 1.27 |
| 180 | 80.4 | 307.4 | 166.1 | 2.02 |
| 181 | 88.7 | 307.4 | 165.4 | 2.59 |
| 182 | 97.0 | 307.4 | 165.0 | 3.03 |
| 183 | 105.3 | 307.4 | 165.1 | 3.02 |



Superfici di scorrimento con $F_s < 1.1$



Superfici di scorrimento con $1.1 < F_s < 1.5$



Superfici di scorrimento con $F_s > 1.5$