

COMMITTENTE:



PROGETTAZIONE:



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PROGETTO DEFINITIVO

RADDOPPIO LINEA CODOGNO – CREMONA – MANTOVA
TRATTA PIADENA - MANTOVA

RI – OPERE DI SOSTEGNO SEDE FERROVIARIA E STRADALE
Relazione di calcolo muro di sostegno sede stradale-NV24

SCALA:

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COMMESSA LOTTO FASE ENTE TIPO DOC. OPERA/DISCIPLINA PROGR. REV.

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1. PREMESSA

La presente relazione ha per oggetto il dimensionamento del muro di sostegno della sede stradale della nuova viabilità NV24, prevista nell'ambito della progettazione definitiva del Raddoppio Ferroviario Codogno-Cremona-Mantova, tratta Piadena Mantova.

L'opera è suddivisa in conci di altezze sezioni caratteristiche diverse:

- **Concio 1:** l'opera è costituita da un muro a mensola in c.a. gettato in opera, di altezza massima 6,50m da estradosso fondazione. Il paramento ha spessore massimo in testa di 0,40m e prosegue con andamento verticale per i primi 60cm, in modo da consentire l'alloggiamento della canaletta; l'altezza restante prosegue con una pendenza 1:10 interna. La suola di fondazione ha spessore 1,10m e larghezza totale di 6,55m, con mensola di valle lunga 0,60m.
- **Concio 2:** l'opera è costituita da un muro a mensola in c.a. gettato in opera, di altezza massima 5,00m da estradosso fondazione. Il paramento ha spessore massimo in testa di 0,40m e prosegue con andamento verticale per i primi 60cm, in modo da consentire l'alloggiamento della canaletta; l'altezza restante prosegue con una pendenza 1:10 interna. La suola di fondazione ha spessore 0,90m e larghezza totale di 5,10m, con mensola di valle lunga 0,60m.
- **Concio 3:** l'opera è costituita da un muro a mensola in c.a. gettato in opera, di altezza massima 4,15m da estradosso fondazione. Il paramento ha spessore massimo in testa di 0,40m e prosegue con andamento verticale per i primi 60cm, in modo da consentire l'alloggiamento della canaletta; l'altezza restante prosegue con una pendenza 1:10 interna. La suola di fondazione ha spessore 0,80m e larghezza totale di 4,40m, con mensola di valle lunga 0,40m.

L'opera ricade in zona sismica e sono state pertanto considerate le azioni derivanti dall'analisi sismica, secondo quanto previsto dal D.M. 17/01/18.

Di seguito si riporta una sezione tipologica dell'intervento:

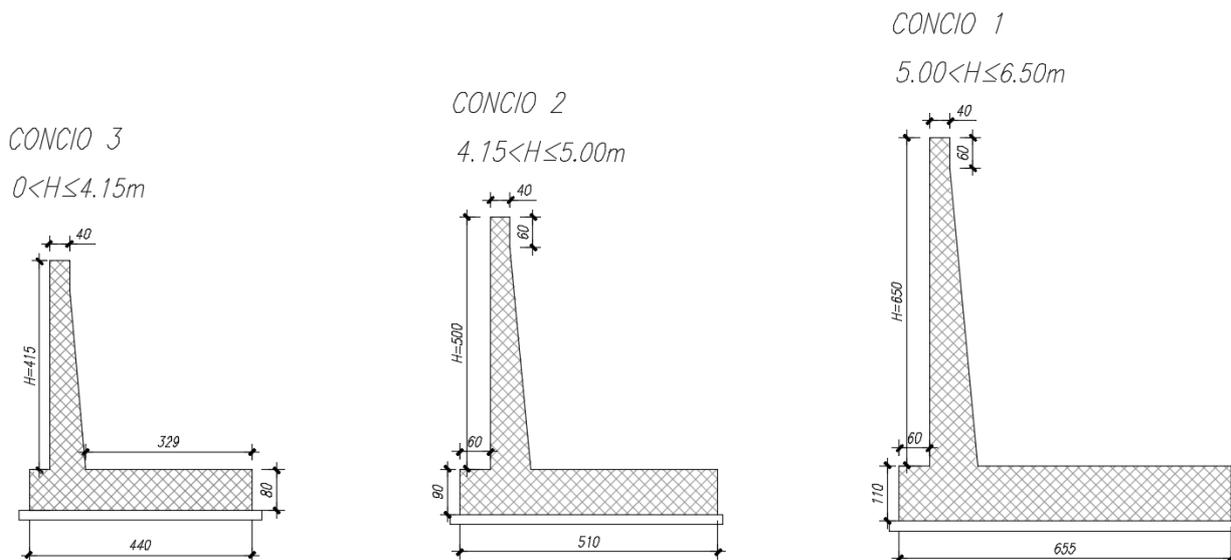


Figura 1 Sezione tipologica del muro

2. *NORMATIVE DI RIFERIMENTO*

2.1 *Normativa*

Di seguito si riportano i riferimenti delle normative prese in considerazione per lo sviluppo delle analisi e delle verifiche in oggetto:

- LEGGE n. 1086 05.11.1971: “Norme per la disciplina delle opere in conglomerato cementizio armato, normale e precompresso ed a struttura metallica”.
- Decreto Ministeriale del 17 gennaio 2018: “Aggiornamento delle «Norme Tecniche per le Costruzioni»”, G.U. Serie Generale n.42 del 20.02.2008, Supplemento Ordinario n.8.
- Circolare 21 gennaio 2019 n.7 ” Istruzioni per l’applicazione dell’«Aggiornamento delle “Norme tecniche per le costruzioni”» di cui al decreto ministeriale 17 gennaio 2018”;
- RFI DTC SI MA IFS 001 C del 21.12.2018 - “Manuale di progettazione delle opere civili”.
- RFI DTC SI PS MA IFS 001 C del 21.12.2018 - “Manuale di progettazione delle opere civili – Sezione 3 – Corpo stradale”.
- RFI DTC SI CS MA IFS 001 C del 21.12.2018 - “Capitolato generale tecnico di appalto delle opere civili”.
- Regolamento (UE) N. 1299/2014 della Commissione del 18 novembre 2014 relativo alle specifiche tecniche di interoperabilità per il sottosistema «infrastruttura» del sistema ferroviario dell’Unione europea, modificato dal Regolamento di esecuzione (UE) N° 2019/776 della Commissione del 16 maggio 2019. UNI EN 1997-1: Eurocodice 7 – Progettazione geotecnica – Parte 1: Regole generali;
- UNI EN 1998-5: Eurocodice 8 – Progettazione delle strutture per la resistenza sismica – Parte 5: Fondazioni, strutture di contenimento ed aspetti geotecnici.

2.2 *Elaborati progettuali di riferimento*

Di seguito si riportano gli elaborati di progetto di riferimento:

| | | | | | | | | | | | | | | | | | | | | | |
|--|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Opere di sostegno sede stradale – NV24 - pianta, prospetto e sezioni | N | M | 2 | 5 | 0 | 3 | D | 2 | 6 | B | Z | N | V | 2 | 4 | 0 | 5 | 0 | 0 | 1 | A |
| Relazione geotecnica generale | N | M | 2 | 5 | 0 | 3 | D | 2 | 6 | G | E | G | E | 0 | 0 | 0 | 6 | 0 | 0 | 1 | A |

3. CARATTERISTICHE DEI MATERIALI

3.1 Calcestruzzo

3.1.1 Calcestruzzo per strutture in elevazione

Si prevede l'utilizzo di calcestruzzo avente classe di resistenza 32/40 ($R_{ck} \geq 40 \text{ N/mm}^2$) che presenta le seguenti caratteristiche:

Resistenza caratteristica a compressione (cilindrica)

$$f_{ck} = 0.83 \times R_{ck} = 33.20 \text{ N/mm}^2$$

Resistenza media a compressione

$$f_{cm} = f_{ck} + 8 = 41.20 \text{ N/mm}^2$$

Modulo elastico

$$E_{cm} = 22000 \times (f_{cm}/10)^{0.3} = 33643 \text{ N/mm}^2$$

Resistenza di calcolo a compressione

$$f_{cd} = a_{cc} \times f_{ck} / \gamma_c = 0.85 \times f_{ck} / 1.5 = 18.81 \text{ N/mm}^2$$

Resistenza a trazione media

$$f_{ctm} = 0.30 \times f_{ck}^{2/3} = 3.10 \text{ N/mm}^2$$

Resistenza a trazione

$$f_{ctk} = 0.7 \times f_{ctm} = 2.17 \text{ N/mm}^2$$

Resistenza a trazione di calcolo

$$f_{ctd} = f_{ctk} / \gamma_c = 1.45 \text{ N/mm}^2$$

3.1.2 Calcestruzzo per strutture in fondazione

Si prevede l'utilizzo di calcestruzzo avente classe di resistenza 30/37 ($R_{ck} \geq 37 \text{ N/mm}^2$) che presenta le seguenti caratteristiche:

Resistenza caratteristica a compressione (cilindrica)

$$f_{ck} = 0.83 \times R_{ck} = 30.71 \text{ N/mm}^2$$

Resistenza media a compressione

$$f_{cm} = f_{ck} + 8 = 38.71 \text{ N/mm}^2$$

Modulo elastico

$$E_{cm} = 22000 \times (f_{cm}/10)^{0.3} = 33019 \text{ N/mm}^2$$

Resistenza di calcolo a compressione

$$f_{cd} = a_{cc} \times f_{ck}/\gamma_c = 0.85 * f_{ck}/1.5 = 17.40 \text{ N/mm}^2$$

Resistenza a trazione media

$$f_{ctm} = 0.30 \times f_{ck}^{2/3} = 2.94 \text{ N/mm}^2$$

Resistenza a trazione

$$f_{ctk} = 0.7 \times f_{ctm} = 2.06 \text{ N/mm}^2$$

Resistenza a trazione di calcolo

$$f_{ctd} = f_{ctk} / \gamma_c = 1.37 \text{ N/mm}^2$$

Calcestruzzo per magrone

Classe di resistenza = C12/15

3.2 Acciaio per cemento armato

| | | |
|----------------------------|------------------------------------|---|
| Tipo | B450 (controllato in stabilimento) | |
| $f_{yk} =$ | 450 MPa | Tensione caratteristica di snervamento |
| $f_{yd} = f_{yk} / 1.15 =$ | 391.30 MPa | Resistenza di calcolo |
| $\sigma_s = 0.75 f_{yk} =$ | 337.50 MPa | Tensione limite in condizione di esercizio (comb. Rara) |
| $E_s =$ | 210000 MPa | Modulo elastico |

3.3 Durabilità e prescrizioni sui materiali

Per garantire la durabilità delle strutture in calcestruzzo armato ordinario, esposte all'azione dell'ambiente, si devono adottare i provvedimenti atti a limitare gli effetti di degrado indotti dall'attacco chimico, fisico e derivante dalla corrosione delle armature e dai cicli di gelo e disgelo.

Per le opere della presente relazione, in base a quanto prescritto dal Capitolato di Costruzione RFI 2018, si adotta quanto segue:

| | | |
|------------|-----------------------|-----|
| Fondazione | Classe di esposizione | XC3 |
| Elevazione | Classe di esposizione | XC4 |

3.4 Copriferro minimo e copriferro nominale

Al fine di preservare le armature dai fenomeni di aggressione ambientale, dovrà essere previsto un idoneo copriferro; definito come la distanza tra la superficie esterna dell'armatura, inclusi collegamenti e staffe, e la superficie di calcestruzzo più vicina.

In riferimento alla Tabella 2.5.2.2.3.2.-1 del Manuale di Progettazione delle Opere Civili Parte II - Sezione 2, per l'elemento strutturale in esame risulta un copriferro minimo $c_{min}=40mm$.

4. PARAMETRI SISMICI

La vita nominale (V_N) dell'opera è stata assunta pari a 50 anni. La classe d'uso assunta è la III.

| | |
|------------------------|----------------------------------|
| Vita nominale: | $V_N = 50$ anni |
| Classe d'uso | IV |
| Coefficiente d'uso | $C_u = 1.5$ |
| Periodo di riferimento | $V_R = V_N \times C_u = 75$ anni |
| Categoria del suolo | D |
| Categoria topografica | T1 |
| Stato Limite | SLV |
| Tempo di ritorno | 712 |

Si assumono i parametri sismici corrispondenti al tratto A1, individuato dalla "Relazione geotecnica generale" dal km 55+286 al km 72+204 con il punto P2:

| | |
|-------------|--------------------------|
| latitudine | = 45.127559; |
| longitudine | = 10.369862; |
| a_g | = 0.091 g; |
| F_0 | = 2.641; |
| T^*c | = 0.319 s. |
| S | = 1.80 |
| a_{max} | = 1,603 m/s ² |

Facendo riferimento alle Norme Tecniche delle Costruzioni 2018, il coefficiente di riduzione dell'accelerazione massima attesa al sito (β_m) è pari a:

$\beta_m = 0.38$ nelle verifiche allo stato limite ultimo (SLU)

$\beta_m = 0.47$ nelle verifiche allo stato limite di esercizio (SLD).

per muri non liberi di subire spostamenti relativi rispetto al terreno, il coefficiente β_m assume valore unitario.

In accordo con il Manuale di Progettazione (SEZIONE III § 3.10.3.1), i coefficienti sismici orizzontale e verticale nel caso in esame risultano:

$$k_h = 2 \beta_m a_{max}/g = 0.76$$

$$k_v = \pm 0.5 k_h = 0.94$$

5. CARATTERIZZAZIONE GEOTECNICA

Le caratteristiche geotecniche del terreno in situ, in accordo con Relazione Geotecnica sono di seguito riportati:

| UNITA' | | Wa1 | Ws1 | WRa2 | Rs1 | Ra1 | Rs2 | |
|----------------------------|-------------|----------------------|----------|-----------|----------|----------|----------|----------|
| Stratigrafia | DA | [m P.C.] | 0.0 | 3.0 | 5.0 | 17.0 | 25.5 | |
| | A | [m P.C.] | 3.0 | 5.0 | 17.0 | 21.0 | 35.0 | |
| Parametri di resistenza | γ_n | [kN/m ³] | 19.0 | 19.0 | 19.0 | 19.0 | 19.0 | |
| | φ' | [°] | 25.0 | 33.0 | 27.0 | 33.0 | 34.0 | |
| | c' | [kPa] | 0 | 0 | 0 | 0 | 0 | |
| | c_u | [kPa] | 30 | - | 50-60 | - | 70 | - |
| Parametri di deformabilità | G_0 | [MPa] | 30.0 | 55-65 | 50-80 | 100.0 | 80.0 | 150.0 |
| | E_{op2} | [MPa] | 15.0 | 27.5-32.5 | 25-40 | 50.0 | 40.0 | 75.0 |
| | OCR | [-] | 3.0 | - | 2.000 | - | 1.0 | - |
| | CR | [-] | 0.180 | - | 0.160 | - | 0.180 | - |
| | RR | [-] | 0.036 | - | 0.032 | - | 0.036 | - |
| | C_{ac} | [%] | 0.120 | - | 0.150 | - | 0.120 | - |
| | $k_v^{(*)}$ | [m/s] | 5.00E-08 | 2.00E-07 | 1.00E-08 | 5.00E-07 | 1.00E-08 | 1.00E-06 |

Tabella 1: Caratterizzazione geotecnica

I parametri geotecnici impiegati per il rilevato stradale sono:

| | |
|---------------------------------|--------------------------------|
| $\gamma = 19.00 \text{ kN/m}^3$ | peso di volume naturale |
| $\varphi' = 35^\circ$ | angolo di resistenza al taglio |
| $c' = 0.00 \text{ kPa}$ | coesione drenata |

Si individua la presenza di falda a quota 2.0m da p.c.

6. CRITERI DI CALCOLO

Sono state effettuate le verifiche con riferimento ai seguenti stati limite:

- scorrimento sul piano di posa;
- collasso per carico limite del complesso fondazione-terreno;
- ribaltamento;
- stabilità globale del complesso opera di sostegno-terreno;
- raggiungimento della resistenza negli elementi strutturali.

6.1 VERIFICHE GEOTECNICHE

6.1.1 Verifica a ribaltamento

La verifica a ribaltamento consiste nel determinare il momento risultante di tutte le forze che tendono a fare ribaltare il muro (momento ribaltante M_r) ed il momento risultante di tutte le forze che tendono a stabilizzare il muro (momento stabilizzante M_s) rispetto allo spigolo a valle della fondazione e verificare che il rapporto M_s/M_r sia maggiore di un determinato coefficiente di sicurezza η_r .

Deve quindi essere verificata la seguente disequaglianza

$$\frac{M_s}{M_r} \geq \eta_r$$

Il momento ribaltante M_r è dato dalla componente orizzontale della spinta S , dalle forze di inerzia del muro e del terreno gravante sulla fondazione di monte (caso di presenza di sisma) per i rispettivi bracci. Nel momento stabilizzante interviene il peso del muro (applicato nel baricentro) ed il peso del terreno gravante sulla fondazione di monte. Se sono presenti dei tiranti essi contribuiscono al momento stabilizzante. Questa verifica ha significato solo per fondazione superficiale e non per fondazione su pali.

6.1.2 Verifica a scorrimento

Per la verifica a scorrimento del muro lungo il piano di fondazione deve risultare che la somma di tutte le forze parallele al piano di posa che tendono a fare scorrere il muro deve essere minore di tutte le forze, parallele al piano di scorrimento, che si oppongono allo scivolamento, secondo un certo coefficiente di sicurezza. La verifica a scorrimento risulta soddisfatta se il rapporto fra la risultante delle forze resistenti allo scivolamento F_r e la risultante delle forze che tendono a fare scorrere il muro F_s risulta maggiore di un determinato coefficiente di sicurezza η_s

$$\frac{F_r}{F_s} \geq \eta_s$$

Le forze che intervengono nella F_s sono: la componente della spinta parallela al piano di fondazione e la componente delle forze d'inerzia parallela al piano di fondazione.

La forza resistente è data dalla resistenza d'attrito e dalla resistenza per adesione lungo la base della fondazione. Detta N la componente normale al piano di fondazione del carico totale gravante in fondazione e indicando con δ_f l'angolo d'attrito terreno-fondazione, con c_a l'adesione terreno-fondazione e con B_f la larghezza della fondazione reagente, la forza resistente può esprimersi come

$$F_r = N \operatorname{tg} \delta_f + c_a B_f$$

Per quanto riguarda l'angolo d'attrito terra-fondazione, δ_f , si assume un valore di δ_f pari all'angolo d'attrito del terreno di fondazione, trascurando il contributo della spinta passiva del terreno a valle.

6.1.3 Verifica al carico limite

Il rapporto fra il carico limite in fondazione e la componente normale della risultante dei carichi trasmessi dal muro sul terreno di fondazione deve essere superiore a η_q . Cioè, detto Q_u , il carico limite ed R la risultante verticale dei carichi in fondazione, deve essere:

$$\frac{Q_u}{R} \geq \eta_q$$

dove R rappresenta la capacità portante ultima valutata con la teoria di Brinch-Hansen.

6.1.4 Verifica alla stabilità globale

La verifica alla stabilità globale del complesso muro+terreno deve fornire un coefficiente di sicurezza non inferiore a η_g . Viene usata la tecnica della suddivisione a strisce della superficie di scorrimento da analizzare. La superficie di scorrimento viene supposta circolare e determinata in modo tale da non avere intersezione con il profilo del muro o con i pali di fondazione. Si determina il minimo coefficiente di sicurezza su una maglia di centri di dimensioni 10x10 posta in prossimità della sommità del muro. Il numero di strisce è pari a 50. Si adotta per la verifica di stabilità globale il metodo di Bishop.

6.2 VERIFICHE STRUTTURALI

Le verifiche strutturali condotte sono le seguenti:

- Verifiche di stato limite di esercizio
 - Verifiche a fessurazione
 - Verifica delle tensioni
- Verifiche di stato limite di ultimo
 - Verifica a flessione
 - Verifica a taglio

6.2.1 Verifiche allo stato limite ultimo

6.2.1.1 Sollecitazioni flettenti

La verifica agli SLU è stata realizzata attraverso il calcolo dei domini di interazione N-M, ovvero il luogo dei punti rappresentativi di sollecitazioni che portano in crisi la sezione di verifica secondo i criteri di resistenza da normativa.

| | | | | | | |
|--|---|-------------------------|-------------------------|-----------------------|----------------------------------|------------------|
|  ITALFERR GRUPPO FERROVIE DELLO STATO ITALIANE | RADDOPPIO LINEA CODOGNO – CREMONA – MANTOVA TRATTA PIADENA - MANTOVA | | | | | |
| | Relazione di calcolo muro di sostegno sede stradale-NV24 | COMMESSA NM25 | LOTTO 03 D 26 | CODIFICA CL | DOCUMENTO NV 24 05 001 | REV. A |

Nel calcolo dei domini sono state mantenute le consuete ipotesi, tra cui:

- conservazione delle sezioni piane;
- legame costitutivo del calcestruzzo parabola-rettangolo non reagente a trazione, con plateau ad una deformazione pari a 0.002 e a rottura pari a 0.0035 ($\sigma_{max} = 0.85 \times 0.83 \times R_{ck} / 1.5$);
- legame costitutivo dell'armatura d'acciaio elastico-perfettamente plastico con deformazione limite di rottura a 0.01 ($\sigma_{max} = f_{yk} / 1.15$)

6.2.1.2 Sollecitazioni taglianti

La resistenza a taglio V_{Rd} di elementi sprovvisti di specifica armatura è stata calcolata sulla base della resistenza a trazione del calcestruzzo.

Con riferimento all'elemento fessurato da momento flettente, la resistenza al taglio si valuta con la seguente espressione:

$$V_{Rd} = \left\{ 0,18 \cdot k \cdot (100 \cdot \rho_1 \cdot f_{ck})^{1/3} / \gamma_c + 0,15 \cdot \sigma_{cp} \right\} \cdot b_w \cdot d \geq (v_{min} + 0,15 \cdot \sigma_{cp}) \cdot b_w \cdot d$$

$$k = 1 + (200/d)^{1/2} \leq 2$$

$$v_{min} = 0,035 k^{3/2} f_{ck}^{1/2}$$

dove:

d è l'altezza utile della sezione (in mm);

$\rho_1 = A_{sl} / (b_w \times d)$ è il rapporto geometrico di armatura longitudinale ($\leq 0,02$);

$\sigma_{cp} = N_{Ed} / A_c$ è la tensione media di compressione nella sezione ($\leq 0,2 f_{cd}$);

b_w è la larghezza minima della sezione (in mm).

La resistenza a taglio V_{Rd} di elementi strutturali dotati di specifica armatura a taglio deve essere valutata sulla base di una adeguata schematizzazione a traliccio. Gli elementi resistenti dell'ideale traliccio sono: le armature trasversali, le armature longitudinali, il corrente compresso di calcestruzzo e i puntoni d'anima inclinati. L'inclinazione θ dei puntoni di calcestruzzo rispetto all'asse della trave deve rispettare i limiti seguenti:

$$1 \leq \text{ctg} \theta \leq 2.5$$

La verifica di resistenza (SLU) è soddisfatta se è verificata la seguente relazione:

$$V_{Rd} \geq V_{Ed}$$

dove V_{Ed} è il valore di calcolo dello sforzo di taglio agente.

La resistenza di calcolo a "taglio trazione" dell'armatura trasversale è stata calcolata con la seguente relazione:

$$V_{Rsd} = 0,9 \cdot d \cdot \frac{A_{sw}}{s} \cdot f_{yd} \cdot (\text{ctg} \alpha + \text{ctg} \theta) \cdot \sin \alpha$$

La resistenza di calcolo a “taglio compressione” del calcestruzzo d’anima è stata calcolata con la seguente relazione:

$$V_{Rcd} = 0,9 \cdot d \cdot b_w \cdot \alpha_c \cdot f'_{cd} \cdot (\text{ctg}\alpha + \text{ctg}\theta) / (1 + \text{ctg}^2\theta)$$

La resistenza al taglio della trave è la minore delle due relazioni sopra definite:

$$V_{Rd} = \min (V_{Rsd}, V_{Rcd})$$

In cui:

- d è l’altezza utile della sezione;
- b_w è la larghezza minima della sezione;
- σ_{cp} è la tensione media di compressione della sezione;
- A_{sw} è l’area dell’armatura trasversale;
- S è interasse tra due armature trasversali consecutive;
- α è l’angolo di inclinazione dell’armatura trasversale rispetto all’asse della trave;
- f'_{cd} è la resistenza a compressione ridotta del calcestruzzo d’anima ($f'_{cd}=0.5f_{cd}$);
- α è un coefficiente maggiorativo pari ad 1 per membrature non compresse.

6.2.2 Verifiche allo stato limite di esercizio

Le condizioni ambientali, ai fini della protezione contro la corrosione delle armature, sono suddivise in ordinarie, aggressive e molto aggressive in relazione a quanto indicato dalla Tab. 4.1.III delle NTC2018:

| Condizioni ambientali | Classe di esposizione |
|-----------------------|-----------------------------------|
| Ordinarie | X0, XC1, XC2, XC3, XF1 |
| Aggressive | XC4, XD1, XS1, XA1, XA2, XF2, XF3 |
| Molto aggressive | XD2, XD3, XS2, XS3, XA3, XF4 |

Tabella 2 Descrizione delle condizioni ambientali (Tab. 4.1.III delle NTC18)

Nel caso in esame, le condizioni ambientali sono “*ordinarie*” per la fondazione e “*aggressive*” per il paramento.

6.2.2.1 Verifica a fessurazione

In relazione all’aggressività ambientale e alla sensibilità dell’acciaio, l’apertura limite delle fessure è pari a $w_l=0.2\text{mm}$ per la combinazione rara.

6.2.2.2 Verifica delle tensioni

I limiti tensionali considerati per i materiali sono relativi alla combinazione di carico quasi permanente e caratteristica.

Calcestruzzo:

| Combinazione di azioni | Limite tensionale |
|------------------------|-----------------------------|
| Caratteristica (rara) | $\sigma_c \leq 0.55 f_{ck}$ |
| Quasi permanente | $\sigma_c \leq 0.40 f_{ck}$ |

Acciaio:

| Combinazione di azioni | Limite tensionale |
|------------------------|-----------------------------|
| Caratteristica (rara) | $\sigma_a \leq 0.75 f_{yk}$ |

6.2.3 Verifiche in condizioni sismiche

È stato verificato che gli spostamenti permanenti allo SLD siano inferiori a 2cm, come prescritto nel Mdp Parte II – SEZIONE 3. Gli spostamenti sono stati determinati con la seguente relazione:

$$d = (S_s S_t B) e^{A(a_c/a_{max})}$$

dove:

S_s e S_t sono i coefficienti di amplificazione stratigrafica e topografica (§ 3.2.3.2 NTC2018);

a_{max} è l'accelerazione orizzontale massima attesa al sito (§ 7.11.6.2.1 NTC2018);

a_c è l'accelerazione critica e rappresenta il valore limite dell'accelerazione al di sotto del quale l'opera non subisce spostamenti;

A, B sono coefficienti raccolti nella seguente tabella in funzione di a_{max} e della categoria di sottosuolo (Rampello et al., 2008).

| Sottosuolo | Cat. A | | Cat. B | | Cat. C, D, E | |
|-------------|--------|------|--------|------|--------------|------|
| | A | B | A | B | A | B |
| a_{max}/g | | | | | | |
| 0.3 – 0.4 | -7.5 | 1.21 | -7.9 | 1.06 | -7.4 | 0.56 |
| 0.2 – 0.3 | -7.42 | 1.28 | -7.79 | 1.11 | -7.54 | 0.58 |
| 0.1 – 0.2 | -7.48 | 0.65 | -7.86 | 0.73 | -8.05 | 0.86 |
| ≤ 0.1 | -7.87 | 0.28 | -7.86 | 0.3 | -8.07 | 0.44 |

Tabella 3: Coefficienti A e B da utilizzare per valutare gli spostamenti dei muri di sostegno nelle verifiche SLE

L'accelerazione critica a_c è stata determinata imponendo che, nella verifica allo scorrimento, effettuata prendendo a riferimento i valori caratteristici di azioni e resistenze (coefficienti γ_F e γ_M pari ad 1), il rapporto Rd/Ed sia pari a 1.

7. ANALISI DEI CARICHI

Nel seguente paragrafo si descrivono le condizioni di carico elementari assunte per l'analisi delle sollecitazioni e per le verifiche della struttura in esame. Tali condizioni di carico elementari saranno opportunamente combinate secondo quanto previsto dalla normativa vigente.

7.1 CONDIZIONI DI CARICO ELEMENTARI

7.1.1 *Peso proprio del muro*

Il peso proprio del muro è stato considerato considerando un peso per unità di volume pari a $\gamma_{cls} = 25 \text{ kN/m}^3$.

7.1.2 *Peso del terrapieno*

Il peso proprio del terrapieno è stato considerato considerando un peso per unità di volume pari a $\gamma_t = 19 \text{ kN/m}^3$.

7.1.3 *Carichi permanenti non strutturali*

Si considera il peso proprio del pacchetto stradale posto a tergo dell'opera, attribuendo un peso per unità di volume pari a $\gamma_t = 18 \text{ kN/m}^3$ e uno spessore di 0.11m.

7.1.4 *Spinta da sovraccarico accidentale*

Il sovraccarico accidentale di superficie è assunto pari a 20 kPa, riprodotto il traffico stradale attivo sull'eventuale carreggiata presente a tergo delle opere.

7.1.5 *Spinta del terreno in condizioni statiche*

La spinta del terreno agente sulla struttura è stata calcolata attraverso la teoria di Culmann che adotta le stesse ipotesi di base del metodo di Coulomb. La differenza sostanziale è che mentre Coulomb considera un terrapieno con superficie a pendenza costante e carico uniformemente distribuito (il che permette di ottenere una espressione in forma chiusa per il coefficiente di spinta) il metodo di Culmann consente di analizzare situazioni con profilo di forma generica e carichi sia concentrati che distribuiti comunque disposti. Inoltre, rispetto al metodo di Coulomb, risulta più immediato e lineare tener conto della coesione del masso spingente. Il metodo di Culmann, nato come metodo essenzialmente grafico, si è evoluto per essere trattato mediante analisi numerica (noto in questa forma come metodo del cuneo di tentativo). Come il metodo di Coulomb anche questo metodo considera una superficie di rottura rettilinea. I passi del procedimento risolutivo sono i seguenti:

- si impone una superficie di rottura e si considera il cuneo di spinta delimitato dalla superficie di rottura stessa, dalla parete su cui si calcola la spinta e dal profilo del terreno;

- si valutano tutte le forze agenti sul cuneo di spinta e cioè peso proprio (W), carichi sul terrapieno, resistenza per attrito e per coesione lungo la superficie di rottura (R e C) e resistenza per coesione lungo la parete (A);

- dalle equazioni di equilibrio si ricava il valore della spinta S sulla parete.

Questo processo viene iterato fino a trovare l'angolo di rottura per cui la spinta risulta massima.

La convergenza non si raggiunge se il terrapieno risulta inclinato di un angolo maggiore dell'angolo d'attrito del terreno.

Nei casi in cui è applicabile il metodo di Coulomb (profilo a monte rettilineo e carico uniformemente distribuito) i risultati ottenuti col metodo di Culmann coincidono con quelli del metodo di Coulomb, il cui coefficiente di spinta attiva è di seguito riportata:

$$K_a = \frac{\cos^2(\phi' - \alpha)}{\cos^2 \alpha \cdot \cos(\alpha + \delta) \cdot \left[1 + \sqrt{\frac{\sin(\phi' + \delta) \cdot \sin(\phi' - \beta)}{\cos(\alpha + \delta) \cdot \cos(\alpha - \beta)}} \right]^2}$$

dove:

- α è l'inclinazione del paramento interno del muro rispetto alla verticale;
- β è l'inclinazione del piano campagna rispetto all'orizzontale;
- ϕ è l'angolo d'attrito del terreno;
- δ è l'angolo d'attrito terreno-struttura (considerato $=0^\circ$)

Per le tipologie di muro con fondazione su pali si adotta un regime di spinte a riposo, dove il coefficiente di spinta k_0 vale.

$$k_0 = 1 - \tan \phi$$

7.1.6 Spinta della falda

Il pelo libero della falda è assunto al di sotto della quota di intradosso della fondazione.

7.1.7 Azioni sismiche

7.1.7.1 Forze inerziali

In condizioni sismiche le forze inerziali orizzontali e verticali sul paramento, soletta di fondazione ed il terreno di riempimento sono valutate attraverso le seguenti espressioni:

$$F_h = k_h W$$

$$F_v = k_v W$$

7.1.7.2 Spinta del terreno in condizioni sismiche

Se la struttura è libera di spostarsi, la sovra spinta sismica attiva agente sulle strutture è calcolata secondo l'approccio di Mononobe-Okabe. La spinta totale esercitata dal terrapieno sul muro è data da:

$$E_d = \frac{1}{2} \gamma (1 \pm k_v) K H^2$$

dove:

H altezza muro

k_v coefficiente sismico verticale

γ peso per unità di volume del terreno

K coefficienti di spinta attiva totale (statico + dinamico)

Il coefficiente di spinta attiva (k_a) è calcolato secondo la seguente relazione:

$$K_a = \frac{\sin^2(\psi + \varphi - \theta)}{\cos \theta \sin^2 \psi \sin(\psi - \theta - \delta) \left[1 + \sqrt{\frac{\sin(\varphi + \delta) \sin(\varphi - \varepsilon - \theta)}{\sin(\psi - \theta - \delta) \sin(\psi + \varepsilon)}} \right]^2}$$

dove:

ψ = angolo di inclinazione del paramento interno del muro rispetto all'orizzontale

δ = angolo di attrito terreno-muro, assunto pari a 0° in condizioni sismiche

φ = angolo di resistenza al taglio

ε = angolo di inclinazione, rispetto all'orizzontale, del terreno a monte del muro ($0-\varphi$)

$$\theta = \arctan \frac{k_h}{1 \pm k_v} \quad \text{per terreno sopra falda}$$

$$\theta = \arctan \frac{\gamma}{\gamma - \gamma_w} \frac{k_h}{1 \pm k_v} \quad \text{per terreno sotto falda}$$

dove:

k_h = coefficiente sismico orizzontale

k_v = coefficiente sismico verticale

Detta S la spinta calcolata in condizioni statiche l'incremento di spinta da applicare è espresso da

$$\Delta S = AS' - S$$

7.2 COMBINAZIONI DI CARICO

La verifica di stabilità globale del complesso opera di sostegno-terreno è stata effettuata secondo l'Approccio 1, con la Combinazione 2 (A2+M2+R2), tenendo conto dei coefficienti parziali riportati nelle Tabelle 6.2.I e 6.2.II per le azioni e i parametri geotecnici e nella Tab. 6.8.I delle NTC 2018 per le verifiche di sicurezza di opere di materiali sciolti e fronti di scavo. Le rimanenti verifiche sono state effettuate secondo l'Approccio 2, con la combinazione (A1+M1+R3), tenendo conto dei valori dei coefficienti parziali riportati nelle Tabelle 6.2.I, 6.2.II e 6.5.I.

Nelle verifiche in condizioni sismiche si è controllato che la resistenza del sistema sia maggiore delle azioni, ponendo pari all'unità i coefficienti parziali sulle azioni e sui parametri geotecnici e impiegando le resistenze di progetto con i coefficienti parziali γ_R indicati nella tabella 7.11.III delle NTC 2018.

Ai fini delle verifiche degli stati limite di esercizio si definiscono le seguenti combinazioni:

Rara) $\Rightarrow G1+G2 + Q_{k1} + \sum_i \psi_{0i} \cdot Q_{ki}$

Frequente) $\Rightarrow G1+G2 + \psi_{11} \cdot Q_{k1} + \sum_i \psi_{2i} \cdot Q_{ki}$

Quasi permanente) $\Rightarrow G1+G2 + \psi_{21} \cdot Q_{k1} + \sum_i \psi_{2i} \cdot Q_{ki}$

| | Effetto | Coefficiente Parziale γ_F (o γ_E) | EQU | (A1) | (A2) |
|--------------------------------|-------------|---|-----|------|------|
| Carichi permanenti G_1 | Favorevole | γ_{G1} | 0,9 | 1,0 | 1,0 |
| | Sfavorevole | | 1,1 | 1,3 | 1,0 |
| Carichi permanenti $G_2^{(1)}$ | Favorevole | γ_{G2} | 0,8 | 0,8 | 0,8 |
| | Sfavorevole | | 1,5 | 1,5 | 1,3 |
| Azioni variabili Q | Favorevole | γ_Q | 0,0 | 0,0 | 0,0 |
| | Sfavorevole | | 1,5 | 1,5 | 1,3 |

Tabella 4: Coefficienti parziali per le azioni o per l'effetto delle azioni (Tabella 6.2.I – NTC 2018)

| Parametro | Grandezza alla quale applicare il coefficiente parziale | Coefficiente parziale γ_M | (M1) | (M2) |
|--|--|-------------------------------------|------|------|
| Tangente dell'angolo di resistenza al taglio | $\tan \varphi'_k$ | $\gamma_{\varphi'}$ | 1,0 | 1,25 |
| Coesione efficace | c'_k | γ_c | 1,0 | 1,25 |
| Resistenza non drenata | c_{uk} | γ_{cu} | 1,0 | 1,4 |
| Peso dell'unità di volume | γ_Y | γ_Y | 1,0 | 1,0 |

Tabella 5: Coefficienti parziali per i parametri geotecnici del terreno (Tabella 6.2.II – NTC 2018)

| Verifica | Coefficiente parziale (R3) |
|------------------------------------|----------------------------|
| Capacità portante della fondazione | $\gamma_R = 1,4$ |
| Scorrimento | $\gamma_R = 1,1$ |
| Ribaltamento | $\gamma_R = 1,15$ |
| Resistenza del terreno a valle | $\gamma_R = 1,4$ |

Tabella 6: Coefficienti parziali γ_R per le verifiche agli stati limite ultimi di muri di sostegno (Tabella 6.5.I – NTC 2018)

| COEFFICIENTE | R2 |
|--------------|-----|
| γ_R | 1,1 |

Tabella 7: Coefficienti parziali per le verifiche di sicurezza di opere di materiali sciolti e di fronti di scavo (Tabella 6.8.I – NTC 2018)

| Verifica | Coefficiente parziale γ_R |
|--------------------------------|----------------------------------|
| Carico limite | 1.2 |
| Scorrimento | 1.0 |
| Ribaltamento | 1.0 |
| Resistenza del terreno a valle | 1.2 |

Tabella 8: Coefficienti parziali $\square R$ per le verifiche degli stati limite (SLV) dei muri di sostegno. (Tabella 7.11.III – NTC 2018)

8. MODELLO DI CALCOLO CONCIO 1

Il modello di calcolo è stato implementato tramite il software di calcolo specifico AZTEC MAX.

8.1 DATI

Materiali

Simbologia adottata

n° Indice materiale

Descr Descrizione del materiale

Calcestruzzo armato

C Classe di resistenza del cls

A Classe di resistenza dell'acciaio

γ Peso specifico, espresso in [kN/mc]

R_{ck} Resistenza caratteristica a compressione, espressa in [kPa]

E Modulo elastico, espresso in [kPa]

ν Coeff. di Poisson

n Coeff. di omogenizzazione acciaio/cls

ntc Coeff. di omogenizzazione cls tesoro/compresso

Calcestruzzo armato

| n° | Descr | C | A | γ | R _{ck} | E | ν | n | ntc |
|----|--------|--------|-------|----------|-----------------|----------|-------|-------|------|
| | | | | [kN/mc] | [kPa] | [kPa] | | | |
| 1 | C32/40 | C32/40 | B450C | 24.5170 | 40000 | 33642648 | 0.30 | 15.00 | 0.50 |
| 5 | C30/37 | C30/37 | B450C | 24.5170 | 35000 | 32587986 | 0.30 | 15.00 | 0.50 |

Acciai

| Descr | f _{yk} | f _{uk} |
|-------|-----------------|-----------------|
| | [kPa] | [kPa] |
| B450C | 450000 | 540000 |

Geometria profilo terreno a monte del muro

Simbologia adottata

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
|----------|---------|----------|--------------|------|-----------|
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(Sistema di riferimento con origine in testa al muro, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

n° numero ordine del punto
 X ascissa del punto espressa in [m]
 Y ordinata del punto espressa in [m]
 A inclinazione del tratto espressa in [°]

| n° | X | Y | A |
|----|-------|------|-------|
| | [m] | [m] | [°] |
| 1 | 0.00 | 0.00 | 0.000 |
| 2 | 32.00 | 0.00 | 0.000 |

Inclinazione terreno a valle del muro rispetto all'orizzontale 0.000 [°]

Falda

Simbologia adottata

(Sistema di riferimento con origine in testa al muro, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

n° numero ordine del punto
 X ascissa del punto espressa in [m]
 Y ordinata del punto espressa in [m]
 A inclinazione del tratto espressa in [°]

| n° | X | Y | A |
|----|-------|-------|-------|
| | [m] | [m] | [°] |
| 1 | -5.00 | -8.00 | 0.000 |
| 2 | -0.40 | -8.00 | 0.000 |
| 3 | 10.00 | -8.00 | 0.000 |
| 4 | 15.00 | -8.00 | 0.000 |

Geometria muro

Geometria paramento e fondazione

Lunghezza muro

1.00 [m]

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
|----------|---------|----------|--------------|------|-----------|
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Paramento

| | | |
|--|--------|-----|
| Materiale | C32/40 | |
| Altezza paramento | 6.50 | [m] |
| Altezza paramento libero | 6.50 | [m] |
| Spessore in sommità | 0.40 | [m] |
| Spessore all'attacco con la fondazione | 0.91 | [m] |
| Inclinazione paramento esterno | 0.00 | [°] |
| Inclinazione paramento interno | 4.45 | [°] |

Fondazione

| | | |
|----------------------------|--------|-----|
| Materiale | C30/37 | |
| Lunghezza mensola di valle | 0.60 | [m] |
| Lunghezza mensola di monte | 5.14 | [m] |
| Lunghezza totale | 6.65 | [m] |
| Inclinazione piano di posa | 0.00 | [°] |
| Spessore | 1.10 | [m] |
| Spessore magrone | 0.20 | [m] |

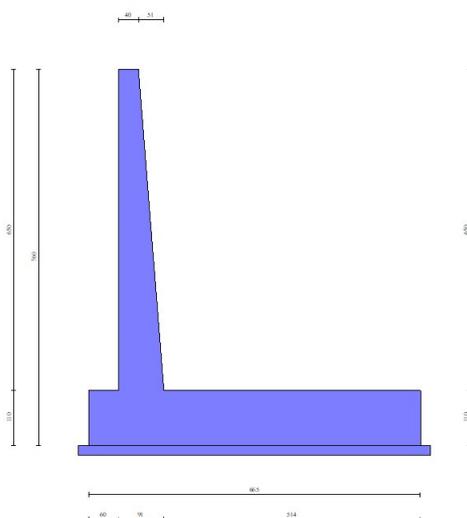


Fig. 1 - Sezione quotata del muro

Descrizione terreni

Parametri di resistenza

Simbologia adottata

| | |
|------------|---|
| n° | Indice del terreno |
| Descr | Descrizione terreno |
| γ | Peso di volume del terreno espresso in [kN/mc] |
| γ_s | Peso di volume saturo del terreno espresso in [kN/mc] |
| ϕ | Angolo d'attrito interno espresso in [°] |
| δ | Angolo d'attrito terra-muro espresso in [°] |
| c | Coesione espressa in [kPa] |
| ca | Adesione terra-muro espressa in [kPa] |

Per calcolo portanza con il metodo di Bustamante-Doix

| | |
|----------|---|
| Cesp | Coeff. di espansione laterale (solo per il metodo di Bustamante-Doix) |
| τ_l | Tensione tangenziale limite, espressa in [kPa] |

| n° | Descr | γ [kN/mc] | γ_{sat} [kN/mc] | ϕ [°] | δ [°] | c [kPa] | ca [kPa] | Cesp | τ_l [kPa] |
|----|----------|---------------------|---------------------------|---------------|-----------------|------------|-------------|------|-------------------|
| 1 | RILEVATO | 19.0000 | 19.0000 | 35.000 | 0.000 | 0 | 0 | --- | --- |
| 2 | Wa1 | 19.0000 | 19.0000 | 25.000 | 25.000 | 0 | 0 | --- | --- |
| 3 | WS1 | 19.0000 | 19.0000 | 33.000 | 33.000 | 0 | 0 | --- | --- |
| 4 | WRa2 | 19.0000 | 19.0000 | 27.000 | 27.000 | 0 | 0 | --- | --- |

Stratigrafia

Simbologia adottata

| | |
|----------|---------------------------------------|
| n° | Indice dello strato |
| H | Spessore dello strato espresso in [m] |
| α | Inclinazione espressa in [°] |
| Terreno | Terreno dello strato |

Per calcolo pali (solo se presenti)

| | |
|------|--|
| Kw | Costante di Winkler orizzontale espressa in Kg/cm ² /cm |
| Ks | Coefficiente di spinta |
| Cesp | Coefficiente di espansione laterale (per tutti i metodi tranne il metodo di Bustamante-Doix) |

Per calcolo della spinta con coeff. di spinta definiti (usati solo se attiva l'opzione 'Usa coeff. di spinta da strato')

| n° | H [m] | α [°] | Terreno | Kw [Kg/cm ³] | Ks | Cesp | K_{ststa} | K_{stsis} |
|----|----------|-----------------|----------|-----------------------------|-----|------|-------------|-------------|
| 1 | 7.60 | 0.000 | RILEVATO | --- | --- | --- | --- | --- |
| 2 | 1.40 | 0.000 | Wa1 | --- | --- | --- | --- | --- |
| 3 | 2.00 | 0.000 | WS1 | --- | --- | --- | --- | --- |
| 4 | 12.00 | 0.000 | WRa2 | --- | --- | --- | --- | --- |

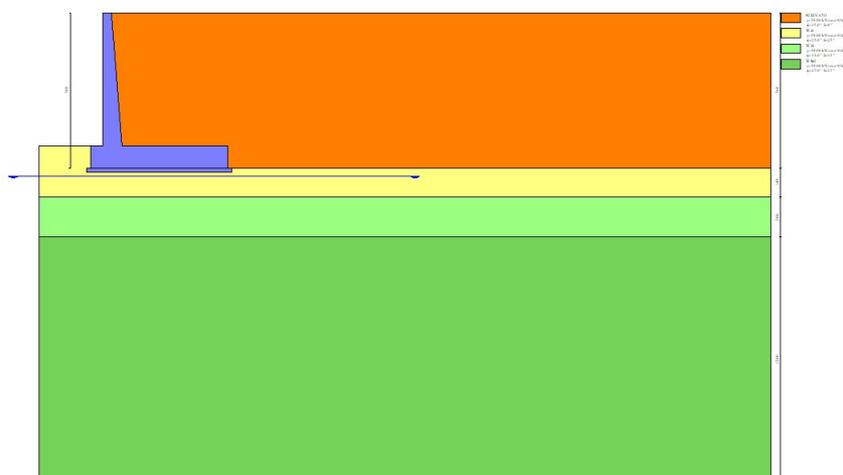


Fig. 2 - Stratigrafia

Condizioni di carico

Simbologia adottata

Carichi verticali positivi verso il basso.

Carichi orizzontali positivi verso sinistra.

Momento positivo senso antiorario.

X Ascissa del punto di applicazione del carico concentrato espressa in [m]

F_x Componente orizzontale del carico concentrato espressa in [kN]

F_y Componente verticale del carico concentrato espressa in [kN]

M Momento espresso in [kNm]

X_i Ascissa del punto iniziale del carico ripartito espressa in [m]

X_f Ascissa del punto finale del carico ripartito espressa in [m]

Q Intensità del carico per $x=X_i$ espressa in [kN]

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|-----------|
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Q_x Intensità del carico per $x=X_x$ espressa in [kN]

Condizione n° 1 (STRADA) - VARIABILE TF

Coeff. di combinazione $\Psi_0=1.00 - \Psi_1=1.00 - \Psi_2=1.00$

Carichi sul terreno

| n° | Tipo | X | Fx | Fy | M | Xi | Xf | Qi | Qf |
|----|-------------|-----|------|------|-------|------|------|---------|---------|
| | | [m] | [kN] | [kN] | [kNm] | [m] | [m] | [kN] | [kN] |
| 1 | Distribuito | | | | | 3.70 | 9.70 | 20.0000 | 20.0000 |

Condizione n° 2 (PAVIMENTAZIONE STRADALE) - PERMANENTE NS

Carichi sul terreno

| n° | Tipo | X | Fx | Fy | M | Xi | Xf | Qi | Qf |
|----|-------------|-----|------|------|-------|------|-------|--------|--------|
| | | [m] | [kN] | [kN] | [kNm] | [m] | [m] | [kN] | [kN] |
| 1 | Distribuito | | | | | 0.50 | 13.90 | 2.0000 | 2.0000 |

Normativa

Normativa usata: **Norme Tecniche sulle Costruzioni 2018 (D.M. 17.01.2018) + Circolare C.S.LL.PP. 21/01/2019 n.7**

Coeff. parziali per le azioni o per l'effetto delle azioni

| Carichi | Effetto | | Combinazioni statiche | | | | | Combinazioni sismiche | | |
|----------------------------|-------------|---------------------|-----------------------|------|------|------|------|-----------------------|------|------|
| | | | HYD | UPL | EQU | A1 | A2 | EQU | A1 | A2 |
| Permanenti strutturali | Favorevoli | $\gamma_{G1, fav}$ | 1.00 | 0.90 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Permanenti strutturali | Sfavorevoli | $\gamma_{G1, sfav}$ | 1.00 | 1.10 | 1.30 | 1.30 | 1.00 | 1.00 | 1.00 | 1.00 |
| Permanenti non strutturali | Favorevoli | $\gamma_{G2, fav}$ | 0.00 | 0.80 | 0.80 | 0.80 | 0.80 | 0.00 | 0.00 | 0.00 |
| Permanenti non strutturali | Sfavorevoli | $\gamma_{G2, sfav}$ | 1.00 | 1.50 | 1.50 | 1.50 | 1.30 | 1.00 | 1.00 | 1.00 |
| Variabili | Favorevoli | $\gamma_{Q, fav}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Variabili | Sfavorevoli | $\gamma_{Q, sfav}$ | 1.00 | 1.50 | 1.50 | 1.50 | 1.30 | 1.00 | 1.00 | 1.00 |
| Variabili da traffico | Favorevoli | $\gamma_{QT, fav}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Variabili da traffico | Sfavorevoli | $\gamma_{QT, sfav}$ | 1.00 | 1.50 | 1.35 | 1.35 | 1.15 | 1.00 | 1.00 | 1.00 |

Coeff. parziali per i parametri geotecnici del terreno

| Parametro | | Combinazioni statiche | | Combinazioni sismiche | |
|---------------------------------|---------------------------|-----------------------|------|-----------------------|------|
| | | M1 | M2 | M1 | M2 |
| Tangente dell'angolo di attrito | $\gamma_{\tan(\varphi')}$ | 1.00 | 1.25 | 1.00 | 1.00 |
| Coesione efficace | γ_c | 1.00 | 1.25 | 1.00 | 1.00 |
| Resistenza non drenata | γ_{cu} | 1.00 | 1.40 | 1.00 | 1.00 |
| Peso nell'unità di volume | γ_γ | 1.00 | 1.00 | 1.00 | 1.00 |

Coeff. parziali γ_R per le verifiche agli stati limite ultimi STR e GEO

| Verifica | Combinazioni statiche | | | Combinazioni sismiche | | |
|----------------------------|-----------------------|------|------|-----------------------|------|------|
| | R1 | R2 | R3 | R1 | R2 | R3 |
| Capacità portante | -- | -- | 1.40 | -- | -- | 1.20 |
| Scorrimento | -- | -- | 1.10 | -- | -- | 1.00 |
| Resistenza terreno a valle | -- | -- | 1.40 | -- | -- | 1.20 |
| Ribaltamento | -- | -- | 1.15 | -- | -- | 1.00 |
| Stabilità fronte di scavo | -- | 1.10 | -- | -- | 1.20 | -- |

Descrizione combinazioni di carico

Con riferimento alle azioni elementari prima determinate, si sono considerate le seguenti combinazioni di carico:

- Combinazione fondamentale, impiegata per gli stati limite ultimi (SLU):

$$\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \gamma_{Q2} Q_{k2} + \gamma_{Q3} Q_{k3} + \dots$$

- Combinazione caratteristica, cosiddetta rara, impiegata per gli stati limite di esercizio (SLE) irreversibili:

$$G_1 + G_2 + Q_{k1} + \Psi_{0,2} Q_{k2} + \Psi_{0,3} Q_{k3} + \dots$$

- Combinazione frequente, impiegata per gli stati limite di esercizio (SLE) reversibili:

$$G_1 + G_2 + \Psi_{1,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

- Combinazione quasi permanente, impiegata per gli effetti di lungo periodo:

$$G_1 + G_2 + \Psi_{2,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

- Combinazione sismica, impiegata per gli stati limite ultimi connessi all'azione sismica E:

$$E + G_1 + G_2 + \Psi_{2,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

I valori dei coeff. $\Psi_{0,j}$, $\Psi_{1,j}$, $\Psi_{2,j}$ sono definiti nelle singole condizioni variabili. I valori dei coeff. γ_G e γ_Q , sono definiti nella tabella normativa.

In particolare si sono considerate le seguenti combinazioni:

Simbologia adottata

- γ Coefficiente di partecipazione della condizione
 Ψ Coefficiente di combinazione della condizione

Combinazione n° 1 - STR (A1-M1-R3)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.30 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.50 | -- | Sfavorevole |
| STRADA | 1.35 | 1.00 | Sfavorevole |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 4 - GEO (A2-M2-R2)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.30 | -- | Sfavorevole |
| STRADA | 1.15 | 1.00 | Sfavorevole |

Combinazione n° 5 - GEO (A2-M2-R2) H + V

| Condizione | γ | Ψ | Effetto |
|------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
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| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 6 - GEO (A2-M2-R2) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 7 - EQU (A1-M1-R3)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.30 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.50 | -- | Sfavorevole |
| STRADA | 1.35 | 1.00 | Sfavorevole |

Combinazione n° 8 - EQU (A1-M1-R3) H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 9 - EQU (A1-M1-R3) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 10 - SLER

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Combinazione n° 11 - SLEF

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Combinazione n° 12 - SLEQ

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Combinazione n° 13 - SLEQ H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Dati sismici

| | |
|--------------------------------|-------------------------------|
| Comune | Mantova |
| Provincia | Mantova |
| Regione | Lombardia |
| Latitudine | 45.122392 |
| Longitudine | 10.572725 |
| Indice punti di interpolazione | 14056 - 13834 - 13833 - 14055 |
| Vita nominale | 50 anni |
| Classe d'uso | III |
| Tipo costruzione | Normali affollamenti |
| Vita di riferimento | 75 anni |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
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| | Simbolo | U.M. | SLU | SLE |
|---|---------|---------------------|-------|-------|
| Accelerazione al suolo | a_g | [m/s ²] | 0.931 | 0.438 |
| Accelerazione al suolo | a_g/g | [%] | 0.095 | 0.045 |
| Massimo fattore amplificazione spettro orizzontale | F0 | | 2.600 | 2.561 |
| Periodo inizio tratto spettro a velocità costante | Tc* | | 0.315 | 0.270 |
| Tipo di sottosuolo - Coefficiente stratigrafico | Ss | | D | 1.800 |
| Categoria topografica - Coefficiente amplificazione topografica | St | | T1 | 1.000 |

| Stato limite ... | Coeff. di riduzione β_m | kh | kv |
|-----------------------|-------------------------------|--------|-------|
| Ultimo | 0.760 | 12.977 | 6.488 |
| Ultimo - Ribaltamento | 1.000 | 17.074 | 8.537 |
| Esercizio | 0.940 | 7.560 | 3.780 |

Forma diagramma incremento sismico **Stessa forma del diagramma statico**

8.2 Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

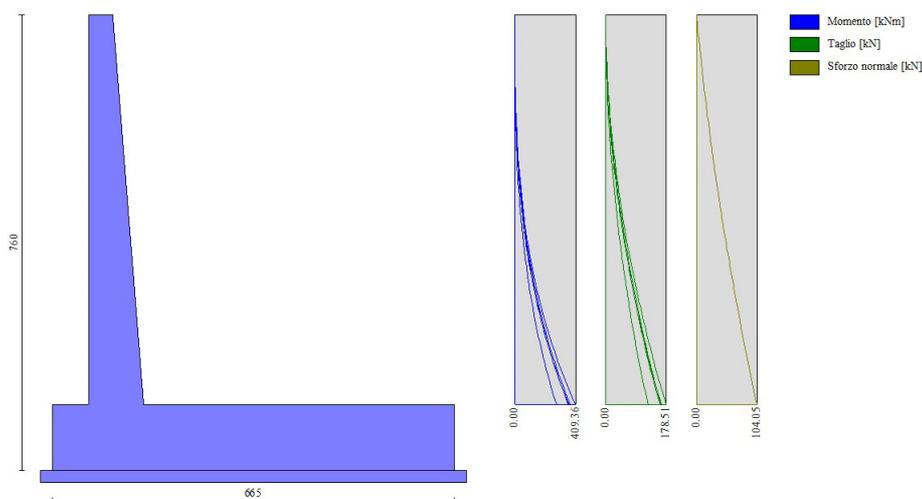
| | |
|--------------------|--|
| Cmb | Indice/Tipo combinazione |
| S | Sisma (H: componente orizzontale, V: componente verticale) |
| FS _{SCO} | Coeff. di sicurezza allo scorrimento |
| FS _{RIB} | Coeff. di sicurezza al ribaltamento |
| FS _{QLIM} | Coeff. di sicurezza a carico limite |
| FS _{STAB} | Coeff. di sicurezza a stabilità globale |
| FS _{HYD} | Coeff. di sicurezza a sifonamento |
| FS _{UPL} | Coeff. di sicurezza a sollevamento |

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{UPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|-------------------|
| 1 - STR (A1-M1-R3) | | 1.860 | | 1.790 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.413 | | 1.236 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.319 | | 1.277 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.380 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.383 | | |
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.332 | | |
| 7 - EQU (A1-M1-R3) | | | 4.968 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 3.055 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.374 | | | | |

8.3 Verifiche strutturali

8.3.1 Paramento

Nella figura seguente si riportano le sollecitazioni agenti sul paramento:



la sezione del paramento viene verificata a pressoflessione (SLU) tenendo conto di tali azioni:

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | $M_{resistente}/M_{agente}$ |
|------------|-------------|--------------|------------------|-------------|-------------------|-----------------------------|
| 409.36 | 100 x 91 | 10 ϕ 26 | 8.7 | 5 ϕ 26 | 8.7 | >1 |

Verifica al taglio

| T (kN) | BxH (cm) | As | $T_{resistente}/T_{agente}$ |
|-----------|-------------|----------------------|-----------------------------|
| 178.51 | 100 x 91 | ϕ 12 / 20x40 cm | >1 |

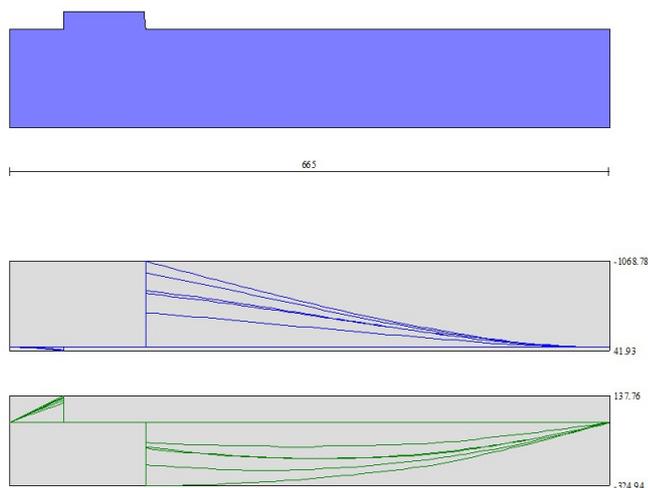
Verifica a SLE:

Verifica a fessurazione (SLE) rara, a favore di sicurezza si verifica le tensioni e le fessurazioni con la sola combinazione rara.

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | σ_s [MPa] | $\sigma_s \text{ lim}$ [MPa] | σ_c [MPa] | $\sigma_c \text{ lim}$ [MPa] | wk [mm] | wlim [mm] |
|------------|-------------|--------------|------------------|-------------|-------------------|---------------------|---------------------------------|---------------------|---------------------------------|------------|--------------|
| 282.4 | 100 x 91 | 10 ϕ 26 | 8.7 | 5 ϕ 26 | 8.7 | 27.84 | 360 | 2.35 | 18.26 | 0.00 | 0.3 |

8.3.2 Fondazione

Nella seguente figura si riportano le sollecitazioni agenti sulla fondazione:



la sezione della fondazione viene verificata a pressoflessione (SLU) tenendo conto di tali azioni:

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | $M_{resistente}/M_{agente}$ |
|------------|-------------|--------------|------------------|-------------|-------------------|-----------------------------|
| -1068.78 | 100 x 110 | 10 ϕ 24 | 8.6 | 5 ϕ 24 | 8.6 | >1 |

Verifica al taglio

| T (kN) | BxH (cm) | As | $T_{resistente}/T_{agente}$ |
|-----------|-------------|----------------------|-----------------------------|
| 481.2 | 100 x 110 | ϕ 12 / 20x40 cm | >1 |

Verifica a SLE:

Verifica a fessurazione (SLE) rara, a favore di sicurezza si verifica le tensioni e le fessurazioni con la sola combinazione rara.

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | σ_s [MPa] | σ_s lim [MPa] | σ_c [MPa] | σ_c lim [MPa] | wk [mm] | wlim [mm] |
|------------|-------------|--------------|------------------|-------------|-------------------|---------------------|-------------------------|---------------------|-------------------------|------------|--------------|
| -428 | 100 x 110 | 10 ϕ 24 | 8.6 | 5 ϕ 24 | 8.6 | 100.26 | 360 | 2.63 | 18.26 | 0.00 | 0.3 |

9. MODELLO DI CALCOLO CONCIO 2

9.1 DATI

Materiali

Simbologia adottata

n° Indice materiale

Descr Descrizione del materiale

Calcestruzzo armato

C Classe di resistenza del cls

A Classe di resistenza dell'acciaio

γ Peso specifico, espresso in [kN/mc]

R_{ck} Resistenza caratteristica a compressione, espressa in [kPa]

E Modulo elastico, espresso in [kPa]

ν Coeff. di Poisson

n Coeff. di omogenizzazione acciaio/cls

ntc Coeff. di omogenizzazione cls teso/compresso

Calcestruzzo armato

| n° | Descr | C | A | γ | R _{ck} | E | ν | n | ntc |
|----|--------|--------|-------|----------|-----------------|----------|-------|-------|------|
| | | | | [kN/mc] | [kPa] | [kPa] | | | |
| 1 | C32/40 | C32/40 | B450C | 24.5170 | 40000 | 33642648 | 0.30 | 15.00 | 0.50 |
| 5 | C30/37 | C30/37 | B450C | 24.5170 | 35000 | 32587986 | 0.30 | 15.00 | 0.50 |

Acciai

| Descr | f _{yk} | f _{uk} |
|-------|-----------------|-----------------|
| | [kPa] | [kPa] |
| B450C | 450000 | 540000 |

Geometria profilo terreno a monte del muro

Simbologia adottata

(Sistema di riferimento con origine in testa al muro, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

Relazione di calcolo muro di sostegno sede stradale-NV24

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n° numero ordine del punto
X ascissa del punto espressa in [m]
Y ordinata del punto espressa in [m]
A inclinazione del tratto espressa in [°]

| n° | X [m] | Y [m] | A [°] |
|----|----------|----------|----------|
| 1 | 0.00 | 0.00 | 0.000 |
| 2 | 32.00 | 0.00 | 0.000 |

Inclinazione terreno a valle del muro rispetto all'orizzontale 0.000 [°]

Falda

Simbologia adottata

(Sistema di riferimento con origine in testa al muro, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

n° numero ordine del punto
X ascissa del punto espressa in [m]
Y ordinata del punto espressa in [m]
A inclinazione del tratto espressa in [°]

| n° | X [m] | Y [m] | A [°] |
|----|----------|----------|----------|
| 1 | -5.00 | -6.50 | 0.000 |
| 2 | -0.40 | -6.50 | 0.000 |
| 3 | 10.00 | -6.50 | 0.000 |
| 4 | 15.00 | -6.50 | 0.000 |

Geometria muro

Geometria paramento e fondazione

Lunghezza muro 1.00 [m]

Paramento

Relazione di calcolo muro di sostegno sede stradale-NV24

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|----------|---------|----------|--------------|------|-----------|
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Materiale

C32/40

| | | |
|--|------|-----|
| Altezza paramento | 5.00 | [m] |
| Altezza paramento libero | 5.00 | [m] |
| Spessore in sommità | 0.40 | [m] |
| Spessore all'attacco con la fondazione | 0.80 | [m] |
| Inclinazione paramento esterno | 0.00 | [°] |
| Inclinazione paramento interno | 4.55 | [°] |

Fondazione

Materiale

C30/37

| | | |
|----------------------------|------|-----|
| Lunghezza mensola di valle | 0.60 | [m] |
| Lunghezza mensola di monte | 3.70 | [m] |
| Lunghezza totale | 5.10 | [m] |
| Inclinazione piano di posa | 0.00 | [°] |
| Spessore | 0.90 | [m] |
| Spessore magrone | 0.20 | [m] |

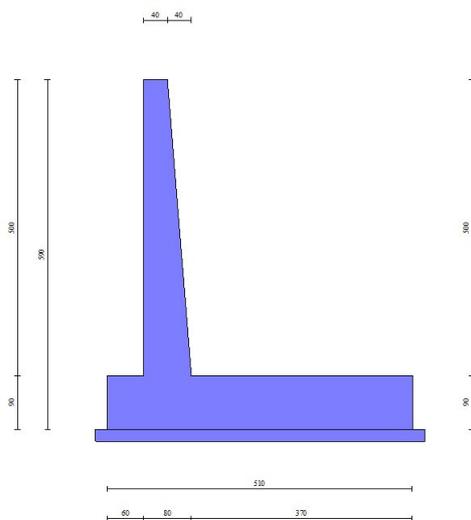


Fig. 1 - Sezione quotata del muro

Descrizione terreni

Parametri di resistenza

Simbologia adottata

| | |
|------------|---|
| n° | Indice del terreno |
| Descr | Descrizione terreno |
| γ | Peso di volume del terreno espresso in [kN/mc] |
| γ_s | Peso di volume saturo del terreno espresso in [kN/mc] |
| ϕ | Angolo d'attrito interno espresso in [°] |
| δ | Angolo d'attrito terra-muro espresso in [°] |
| c | Coesione espressa in [kPa] |
| ca | Adesione terra-muro espressa in [kPa] |

Per calcolo portanza con il metodo di Bustamante-Doix

| | |
|----------|---|
| Cesp | Coeff. di espansione laterale (solo per il metodo di Bustamante-Doix) |
| τ_l | Tensione tangenziale limite, espressa in [kPa] |

| n° | Descr | γ [kN/mc] | γ_{sat} [kN/mc] | ϕ [°] | δ [°] | c [kPa] | ca [kPa] | Cesp | τ_l [kPa] |
|----|----------|---------------------|---------------------------|---------------|-----------------|------------|-------------|------|-------------------|
| 1 | RILEVATO | 19.0000 | 19.0000 | 35.000 | 0.000 | 0 | 0 | --- | --- |
| 2 | Wa1 | 19.0000 | 19.0000 | 25.000 | 25.000 | 0 | 0 | --- | --- |
| 3 | WS1 | 19.0000 | 19.0000 | 33.000 | 33.000 | 0 | 0 | --- | --- |
| 4 | WRa2 | 19.0000 | 19.0000 | 27.000 | 27.000 | 0 | 0 | --- | --- |

Stratigrafia

Simbologia adottata

| | |
|----------|---------------------------------------|
| n° | Indice dello strato |
| H | Spessore dello strato espresso in [m] |
| α | Inclinazione espressa in [°] |
| Terreno | Terreno dello strato |

Per calcolo pali (solo se presenti)

| | |
|------|--|
| Kw | Costante di Winkler orizzontale espressa in Kg/cm ² /cm |
| Ks | Coefficiente di spinta |
| Cesp | Coefficiente di espansione laterale (per tutti i metodi tranne il metodo di Bustamante-Doix) |

Per calcolo della spinta con coeff. di spinta definiti (usati solo se attiva l'opzione 'Usa coeff. di spinta da strato')

| | |
|---|------------------------------------|
| Kst _{sta} , Kst _{sis} | Coeff. di spinta statico e sismico |
|---|------------------------------------|

| n° | H [m] | α [°] | Terreno | Kw [Kg/cm ²] | Ks | Cesp | Kststa | Kstsis |
|----|----------|-----------------|----------|-----------------------------|-----|------|--------|--------|
| 1 | 5.90 | 0.000 | RILEVATO | --- | --- | --- | --- | --- |
| 2 | 1.40 | 0.000 | Wa1 | --- | --- | --- | --- | --- |
| 3 | 2.00 | 0.000 | WS1 | --- | --- | --- | --- | --- |
| 4 | 12.00 | 0.000 | WRa2 | --- | --- | --- | --- | --- |



Fig. 2 - Stratigrafia

Condizioni di carico

Simbologia adottata

Carichi verticali positivi verso il basso.

Carichi orizzontali positivi verso sinistra.

Momento positivo senso antiorario.

| | |
|----------------|--|
| X | Ascissa del punto di applicazione del carico concentrato espressa in [m] |
| F _x | Componente orizzontale del carico concentrato espressa in [kN] |
| F _y | Componente verticale del carico concentrato espressa in [kN] |
| M | Momento espresso in [kNm] |
| X _i | Ascissa del punto iniziale del carico ripartito espressa in [m] |
| X _r | Ascissa del punto finale del carico ripartito espressa in [m] |
| Q _i | Intensità del carico per x=X _i espressa in [kN] |
| Q _r | Intensità del carico per x=X _r espressa in [kN] |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|-----------|
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Condizione n° 1 (STRADA) - VARIABILE TF

Coeff. di combinazione $\Psi_0=1.00 - \Psi_1=1.00 - \Psi_2=1.00$

Carichi sul terreno

| n° | Tipo | X [m] | Fx [kN] | Fy [kN] | M [kNm] | Xi [m] | Xf [m] | Qi [kN] | Qf [kN] |
|----|-------------|----------|------------|------------|------------|-----------|-----------|------------|------------|
| 1 | Distribuito | | | | | 3.70 | 9.70 | 20.0000 | 20.0000 |

Condizione n° 2 (PAVIMENTAZIONE STRADALE) - PERMANENTE NS

Carichi sul terreno

| n° | Tipo | X [m] | Fx [kN] | Fy [kN] | M [kNm] | Xi [m] | Xf [m] | Qi [kN] | Qf [kN] |
|----|-------------|----------|------------|------------|------------|-----------|-----------|------------|------------|
| 1 | Distribuito | | | | | 0.50 | 13.90 | 2.0000 | 2.0000 |

Normativa

Normativa usata: **Norme Tecniche sulle Costruzioni 2018 (D.M. 17.01.2018) + Circolare C.S.LL.PP. 21/01/2019 n.7**

Coeff. parziali per le azioni o per l'effetto delle azioni

| Carichi | Effetto | | Combinazioni statiche | | | | | Combinazioni sismiche | | |
|----------------------------|-------------|---------------------|-----------------------|------|------|------|------|-----------------------|------|------|
| | | | HYD | UPL | EQU | A1 | A2 | EQU | A1 | A2 |
| Permanenti strutturali | Favorevoli | $\gamma_{G1, fav}$ | 1.00 | 0.90 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Permanenti strutturali | Sfavorevoli | $\gamma_{G1, sfav}$ | 1.00 | 1.10 | 1.30 | 1.30 | 1.00 | 1.00 | 1.00 | 1.00 |
| Permanenti non strutturali | Favorevoli | $\gamma_{G2, fav}$ | 0.00 | 0.80 | 0.80 | 0.80 | 0.80 | 0.00 | 0.00 | 0.00 |
| Permanenti non strutturali | Sfavorevoli | $\gamma_{G2, sfav}$ | 1.00 | 1.50 | 1.50 | 1.50 | 1.30 | 1.00 | 1.00 | 1.00 |
| Variabili | Favorevoli | $\gamma_{Q, fav}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Variabili | Sfavorevoli | $\gamma_{Q, sfav}$ | 1.00 | 1.50 | 1.50 | 1.50 | 1.30 | 1.00 | 1.00 | 1.00 |
| Variabili da traffico | Favorevoli | $\gamma_{QT, fav}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Variabili da traffico | Sfavorevoli | $\gamma_{QT, sfav}$ | 1.00 | 1.50 | 1.35 | 1.35 | 1.15 | 1.00 | 1.00 | 1.00 |

Coeff. parziali per i parametri geotecnici del terreno

| Parametro | | Combinazioni statiche | | Combinazioni sismiche | |
|---------------------------------|-----------------------|-----------------------|------|-----------------------|------|
| | | M1 | M2 | M1 | M2 |
| Tangente dell'angolo di attrito | $\gamma_{\tan(\phi)}$ | 1.00 | 1.25 | 1.00 | 1.00 |
| Coesione efficace | γ_c | 1.00 | 1.25 | 1.00 | 1.00 |
| Resistenza non drenata | γ_{cu} | 1.00 | 1.40 | 1.00 | 1.00 |
| Peso nell'unità di volume | γ_r | 1.00 | 1.00 | 1.00 | 1.00 |

Coeff. parziali γ_R per le verifiche agli stati limite ultimi STR e GEO

| Verifica | Combinazioni statiche | | | Combinazioni sismiche | | |
|----------------------------|-----------------------|------|------|-----------------------|------|------|
| | R1 | R2 | R3 | R1 | R2 | R3 |
| Capacità portante | -- | -- | 1.40 | -- | -- | 1.20 |
| Scorrimento | -- | -- | 1.10 | -- | -- | 1.00 |
| Resistenza terreno a valle | -- | -- | 1.40 | -- | -- | 1.20 |
| Ribaltamento | -- | -- | 1.15 | -- | -- | 1.00 |
| Stabilità fronte di scavo | -- | 1.10 | -- | -- | 1.20 | -- |

Descrizione combinazioni di carico

Con riferimento alle azioni elementari prima determinate, si sono considerate le seguenti combinazioni di carico:

- Combinazione fondamentale, impiegata per gli stati limite ultimi (SLU):

$$\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \gamma_{Q2} Q_{k2} + \gamma_{Q3} Q_{k3} + \dots$$

- Combinazione caratteristica, cosiddetta rara, impiegata per gli stati limite di esercizio (SLE) irreversibili:

$$G_1 + G_2 + Q_{k1} + \Psi_{0,2} Q_{k2} + \Psi_{0,3} Q_{k3} + \dots$$

- Combinazione frequente, impiegata per gli stati limite di esercizio (SLE) reversibili:

$$G_1 + G_2 + \Psi_{1,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

- Combinazione quasi permanente, impiegata per gli effetti di lungo periodo:

$$G_1 + G_2 + \Psi_{2,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

- Combinazione sismica, impiegata per gli stati limite ultimi connessi all'azione sismica E:

$$E + G_1 + G_2 + \Psi_{2,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

I valori dei coeff. $\Psi_{0,j}$, $\Psi_{1,j}$, $\Psi_{2,j}$ sono definiti nelle singole condizioni variabili. I valori dei coeff. γ_G e γ_Q , sono definiti nella tabella normativa.

In particolare si sono considerate le seguenti combinazioni:

Simbologia adottata

| | |
|----------|---|
| γ | Coefficiente di partecipazione della condizione |
| Ψ | Coefficiente di combinazione della condizione |

Combinazione n° 1 - STR (A1-M1-R3)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.30 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.50 | -- | Sfavorevole |
| STRADA | 1.35 | 1.00 | Sfavorevole |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 4 - GEO (A2-M2-R2)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.30 | -- | Sfavorevole |
| STRADA | 1.15 | 1.00 | Sfavorevole |

Combinazione n° 5 - GEO (A2-M2-R2) H + V

| Condizione | γ | Ψ | Effetto |
|-----------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
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| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 6 - GEO (A2-M2-R2) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 7 - EQU (A1-M1-R3)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.30 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.50 | -- | Sfavorevole |
| STRADA | 1.35 | 1.00 | Sfavorevole |

Combinazione n° 8 - EQU (A1-M1-R3) H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 9 - EQU (A1-M1-R3) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 10 - SLER

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Relazione di calcolo muro di sostegno sede stradale-NV24

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|----------|---------|----------|--------------|------|-----------|
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Combinazione n° 11 - SLEF

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Combinazione n° 12 - SLEQ

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Combinazione n° 13 - SLEQ_H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Dati sismici

| | |
|--------------------------------|-------------------------------|
| Comune | Mantova |
| Provincia | Mantova |
| Regione | Lombardia |
| Latitudine | 45.122392 |
| Longitudine | 10.572725 |
| Indice punti di interpolazione | 14056 - 13834 - 13833 - 14055 |
| Vita nominale | 50 anni |
| Classe d'uso | III |
| Tipo costruzione | Normali affollamenti |
| Vita di riferimento | 75 anni |

| | Simbolo | U.M. | SLU | SLE |
|------------------------|---------|---------------------|-------|-------|
| Accelerazione al suolo | a_g | [m/s ²] | 0.931 | 0.438 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|-----------|
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| | Simbolo | U.M. | | SLU | SLE |
|---|-------------------|------|----|-------|-------|
| Accelerazione al suolo | a _g /g | [%] | | 0.095 | 0.045 |
| Massimo fattore amplificazione spettro orizzontale | F0 | | | 2.600 | 2.561 |
| Periodo inizio tratto spettro a velocità costante | Tc* | | | 0.315 | 0.270 |
| Tipo di sottosuolo - Coefficiente stratigrafico | Ss | | D | 1.800 | 1.800 |
| Categoria topografica - Coefficiente amplificazione topografica | St | | T1 | 1.000 | |

| Stato limite ... | Coeff. di riduzione β_m | kh | kv |
|-----------------------|-------------------------------|--------|-------|
| Ultimo | 0.760 | 12.977 | 6.488 |
| Ultimo - Ribaltamento | 1.000 | 17.074 | 8.537 |
| Esercizio | 0.940 | 7.560 | 3.780 |

Forma diagramma incremento sismico **Stessa forma del diagramma statico**

9.2 Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

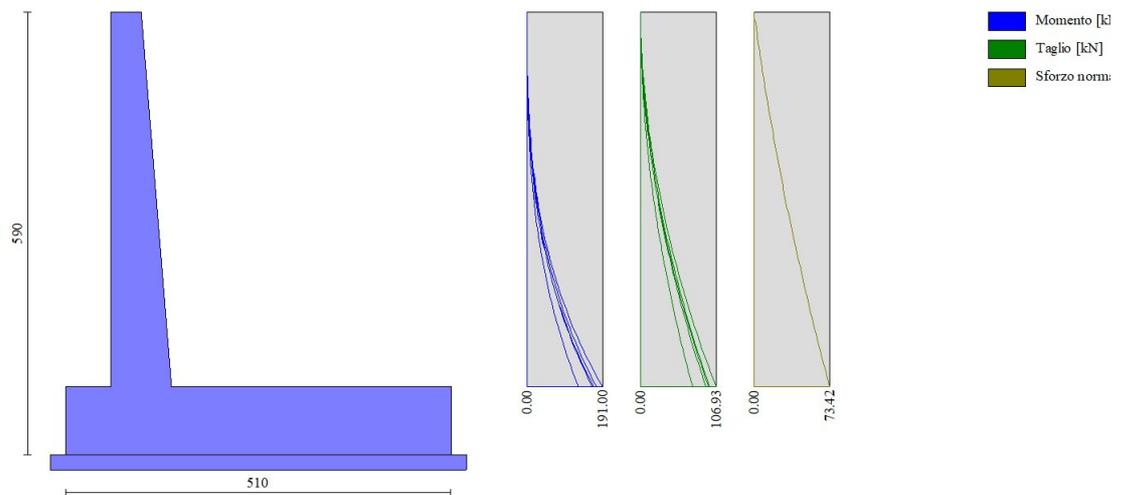
| | |
|--------------------|--|
| Cmb | Indice/Tipo combinazione |
| S | Sisma (H: componente orizzontale, V: componente verticale) |
| FS _{SCO} | Coeff. di sicurezza allo scorrimento |
| FS _{RIB} | Coeff. di sicurezza al ribaltamento |
| FS _{QLIM} | Coeff. di sicurezza a carico limite |
| FS _{STAB} | Coeff. di sicurezza a stabilità globale |
| FS _{HYD} | Coeff. di sicurezza a sifonamento |
| FS _{UPL} | Coeff. di sicurezza a sollevamento |

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{UPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|-------------------|
| 1 - STR (A1-M1-R3) | | 1.638 | | 1.872 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.359 | | 1.387 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.270 | | 1.427 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.263 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.321 | | |
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.273 | | |
| 7 - EQU (A1-M1-R3) | | | 4.287 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 2.971 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.323 | | | | |

9.3 Verifiche strutturali

9.3.1 Paramento

Nella figura seguente si riportano le sollecitazioni agenti sul paramento:



la sezione del paramento viene verificata a pressoflessione (SLU) tenendo conto di tali azioni:

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | $M_{resistente}/$ M_{agente} |
|------------|-------------|--------------|------------------|-------------|-------------------|-----------------------------------|
| 191 | 100 x 80 | 10 ϕ 26 | 8.7 | 5 ϕ 26 | 8.7 | >1 |

Verifica al taglio

| T (kN) | BxH (cm) | As | $T_{resistente}/$ T_{agente} |
|-----------|-------------|----------------------|-----------------------------------|
| 106.93 | 100 x 80 | ϕ 12 / 20x40 cm | >1 |

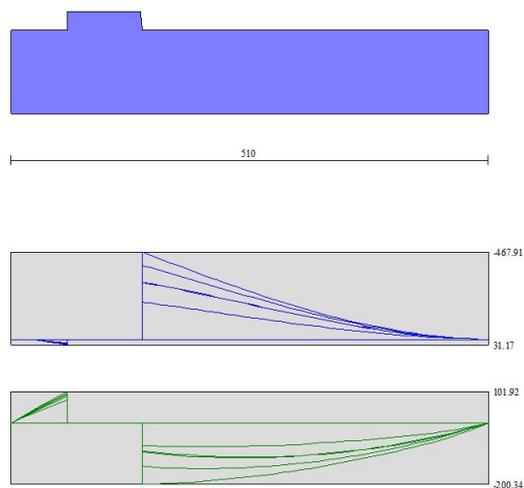
Verifica a SLE:

Verifica a fessurazione (SLE) rara, a favore di sicurezza si verifica le tensioni e le fessurazioni con la sola combinazione rara.

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | σ_s [MPa] | σ_s lim [MPa] | σ_c [MPa] | σ_c lim [MPa] | wk [mm] | wlim [mm] |
|------------|-------------|--------------|------------------|-------------|-------------------|---------------------|-------------------------|---------------------|-------------------------|------------|--------------|
| 130.48 | 100 x 91 | 10 ϕ 26 | 8.7 | 5 ϕ 26 | 8.7 | 31.59 | 360 | 1.37 | 18.26 | 0.00 | 0.3 |

9.3.2 Fondazione

Nella seguente figura si riportano le sollecitazioni agenti sulla fondazione:



la sezione della fondazione viene verificata a pressoflessione (SLU) tenendo conto di tali azioni:

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | $M_{resistente}/M_{agente}$ |
|------------|-------------|--------------|------------------|-------------|-------------------|-----------------------------|
| -448.89 | 100 x 90 | 10 ϕ 24 | 8.6 | 5 ϕ 24 | 8.6 | >1 |

Verifica al taglio

| T (kN) | BxH (cm) | As | $T_{resistente}/T_{agente}$ |
|-----------|-------------|----------------------|-----------------------------|
| 200.34 | 100 x 90 | ϕ 12 / 20x40 cm | >1 |

Verifica a SLE:

Verifica a fessurazione (SLE) rara, a favore di sicurezza si verifica le tensioni e le fessurazioni con la sola combinazione rara.

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | σ_s [MPa] | σ_s lim [MPa] | σ_c [MPa] | σ_c lim [MPa] | wk [mm] | wlim [mm] |
|------------|-------------|--------------|------------------|-------------|-------------------|---------------------|-------------------------|---------------------|-------------------------|------------|--------------|
| -199.32 | 100 x 90 | 10 ϕ 24 | 8.6 | 5 ϕ 24 | 8.6 | 58.42 | 360 | 1.72 | 18.26 | 0.00 | 0.3 |

10. MODELLO DI CALCOLO CONCIO 3

10.1 DATI

Materiali

Simbologia adottata

n° Indice materiale

Descr Descrizione del materiale

Calcestruzzo armato

C Classe di resistenza del cls

A Classe di resistenza dell'acciaio

γ Peso specifico, espresso in [kN/mc]

R_{ck} Resistenza caratteristica a compressione, espressa in [kPa]

E Modulo elastico, espresso in [kPa]

ν Coeff. di Poisson

n Coeff. di omogenizzazione acciaio/cls

ntc Coeff. di omogenizzazione cls tesoro/compresso

Calcestruzzo armato

| n° | Descr | C | A | γ | R _{ck} | E | ν | n | ntc |
|----|--------|--------|-------|----------|-----------------|----------|-------|-------|------|
| | | | | [kN/mc] | [kPa] | [kPa] | | | |
| 1 | C32/40 | C32/40 | B450C | 24.5170 | 40000 | 33642648 | 0.30 | 15.00 | 0.50 |
| 5 | C30/37 | C30/37 | B450C | 24.5170 | 35000 | 32587986 | 0.30 | 15.00 | 0.50 |

Acciai

| Descr | f _{yk} | f _{uk} |
|-------|-----------------|-----------------|
| | [kPa] | [kPa] |
| B450C | 450000 | 540000 |

Geometria profilo terreno a monte del muro

Simbologia adottata

(Sistema di riferimento con origine in testa al muro, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

Relazione di calcolo muro di sostegno sede stradale-NV24

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n° numero ordine del punto
X ascissa del punto espressa in [m]
Y ordinata del punto espressa in [m]
A inclinazione del tratto espressa in [°]

| n° | X [m] | Y [m] | A [°] |
|----|----------|----------|----------|
| 1 | 0.00 | 0.00 | 0.000 |
| 2 | 32.00 | 0.00 | 0.000 |

Inclinazione terreno a valle del muro rispetto all'orizzontale 0.000 [°]

Falda

Simbologia adottata

(Sistema di riferimento con origine in testa al muro, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

n° numero ordine del punto
X ascissa del punto espressa in [m]
Y ordinata del punto espressa in [m]
A inclinazione del tratto espressa in [°]

| n° | X [m] | Y [m] | A [°] |
|----|----------|----------|----------|
| 1 | -5.00 | -5.75 | 0.000 |
| 2 | -0.82 | -5.75 | 0.000 |
| 3 | 10.00 | -5.75 | 0.000 |
| 4 | 15.00 | -5.75 | 0.000 |

Geometria muro

Geometria paramento e fondazione

Lunghezza muro 1.00 [m]

Paramento

Relazione di calcolo muro di sostegno sede stradale-NV24

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Materiale

C32/40

| | | |
|--|------|-----|
| Altezza paramento | 4.15 | [m] |
| Altezza paramento libero | 4.15 | [m] |
| Spessore in sommità | 0.40 | [m] |
| Spessore all'attacco con la fondazione | 0.71 | [m] |
| Inclinazione paramento esterno | 0.00 | [°] |
| Inclinazione paramento interno | 4.25 | [°] |

Fondazione

Materiale

C30/37

| | | |
|----------------------------|------|-----|
| Lunghezza mensola di valle | 0.40 | [m] |
| Lunghezza mensola di monte | 3.29 | [m] |
| Lunghezza totale | 4.40 | [m] |
| Inclinazione piano di posa | 0.00 | [°] |
| Spessore | 0.80 | [m] |
| Spessore magrone | 0.20 | [m] |

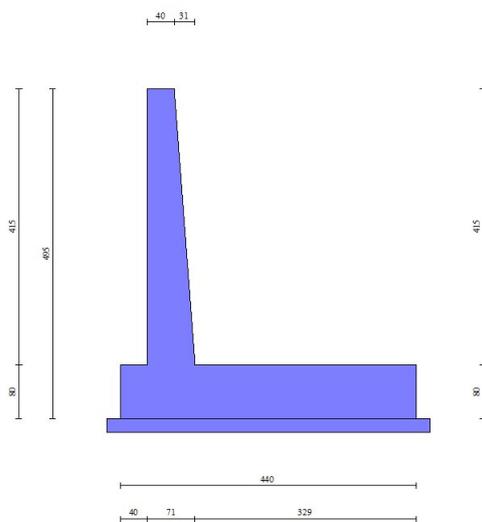


Fig. 1 - Sezione quotata del muro

Descrizione terreni

Parametri di resistenza

Simbologia adottata

| | |
|------------|---|
| n° | Indice del terreno |
| Descr | Descrizione terreno |
| γ | Peso di volume del terreno espresso in [kN/mc] |
| γ_s | Peso di volume saturo del terreno espresso in [kN/mc] |
| ϕ | Angolo d'attrito interno espresso in [°] |
| δ | Angolo d'attrito terra-muro espresso in [°] |
| c | Coesione espressa in [kPa] |
| ca | Adesione terra-muro espressa in [kPa] |

Per calcolo portanza con il metodo di Bustamante-Doix

| | |
|----------|---|
| Cesp | Coeff. di espansione laterale (solo per il metodo di Bustamante-Doix) |
| τ_l | Tensione tangenziale limite, espressa in [kPa] |

| n° | Descr | γ [kN/mc] | γ_{sat} [kN/mc] | ϕ [°] | δ [°] | c [kPa] | ca [kPa] | Cesp | τ_l [kPa] |
|----|----------|---------------------|---------------------------|---------------|-----------------|------------|-------------|------|-------------------|
| 1 | RILEVATO | 19.0000 | 19.0000 | 35.000 | 0.000 | 0 | 0 | --- | --- |
| 2 | Wa1 | 19.0000 | 19.0000 | 25.000 | 25.000 | 0 | 0 | --- | --- |
| 3 | WS1 | 19.0000 | 19.0000 | 33.000 | 33.000 | 0 | 0 | --- | --- |
| 4 | WRa2 | 19.0000 | 19.0000 | 27.000 | 27.000 | 0 | 0 | --- | --- |

Stratigrafia

Simbologia adottata

| | |
|----------|---------------------------------------|
| n° | Indice dello strato |
| H | Spessore dello strato espresso in [m] |
| α | Inclinazione espressa in [°] |
| Terreno | Terreno dello strato |

Per calcolo pali (solo se presenti)

| | |
|------|--|
| Kw | Costante di Winkler orizzontale espressa in Kg/cm ² /cm |
| Ks | Coefficiente di spinta |
| Cesp | Coefficiente di espansione laterale (per tutti i metodi tranne il metodo di Bustamante-Doix) |

Per calcolo della spinta con coeff. di spinta definiti (usati solo se attiva l'opzione 'Usa coeff. di spinta da strato')

| | |
|---|------------------------------------|
| Kst _{sta} , Kst _{sis} | Coeff. di spinta statico e sismico |
|---|------------------------------------|

| n° | H [m] | α [°] | Terreno | Kw [Kg/cm ²] | Ks | Cesp | Kststa | Kstsis |
|----|----------|-----------------|----------|-----------------------------|-----|------|--------|--------|
| 1 | 4.95 | 0.000 | RILEVATO | --- | --- | --- | --- | --- |
| 2 | 1.40 | 0.000 | Wa1 | --- | --- | --- | --- | --- |
| 3 | 2.00 | 0.000 | WS1 | --- | --- | --- | --- | --- |
| 4 | 12.00 | 0.000 | WRa2 | --- | --- | --- | --- | --- |

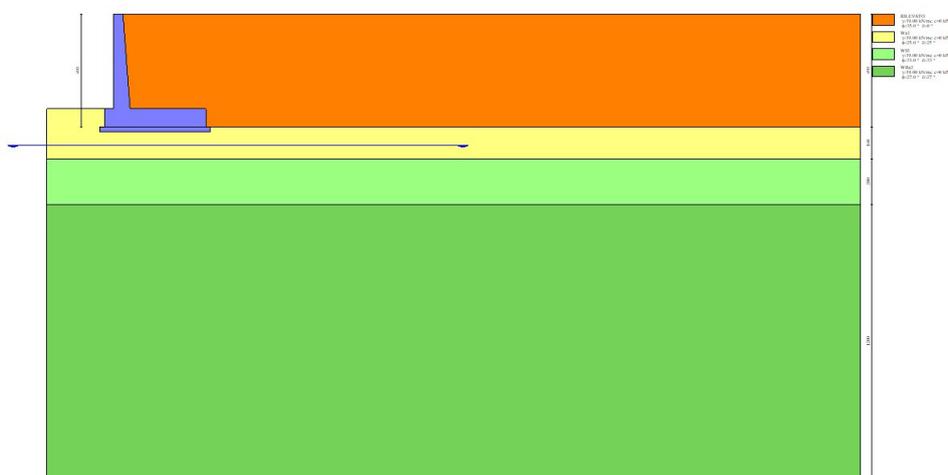


Fig. 2 - Stratigrafia

Condizioni di carico

Simbologia adottata

Carichi verticali positivi verso il basso.

Carichi orizzontali positivi verso sinistra.

Momento positivo senso antiorario.

| | |
|----------------|--|
| X | Ascissa del punto di applicazione del carico concentrato espressa in [m] |
| F _x | Componente orizzontale del carico concentrato espressa in [kN] |
| F _y | Componente verticale del carico concentrato espressa in [kN] |
| M | Momento espresso in [kNm] |
| X _i | Ascissa del punto iniziale del carico ripartito espressa in [m] |
| X _r | Ascissa del punto finale del carico ripartito espressa in [m] |
| Q _i | Intensità del carico per x=X _i espressa in [kN] |
| Q _r | Intensità del carico per x=X _r espressa in [kN] |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
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Condizione n° 1 (STRADA) - VARIABILE TF

Coeff. di combinazione $\Psi_0=1.00 - \Psi_1=1.00 - \Psi_2=1.00$

Carichi sul terreno

| n° | Tipo | X [m] | Fx [kN] | Fy [kN] | M [kNm] | Xi [m] | Xf [m] | Qi [kN] | Qf [kN] |
|----|-------------|----------|------------|------------|------------|-----------|-----------|------------|------------|
| 1 | Distribuito | | | | | 3.70 | 9.70 | 20.0000 | 20.0000 |

Condizione n° 2 (PAVIMENTAZIONE STRADALE) - PERMANENTE NS

Carichi sul terreno

| n° | Tipo | X [m] | Fx [kN] | Fy [kN] | M [kNm] | Xi [m] | Xf [m] | Qi [kN] | Qf [kN] |
|----|-------------|----------|------------|------------|------------|-----------|-----------|------------|------------|
| 1 | Distribuito | | | | | 0.50 | 13.90 | 2.0000 | 2.0000 |

Normativa

Normativa usata: **Norme Tecniche sulle Costruzioni 2018 (D.M. 17.01.2018) + Circolare C.S.LL.PP. 21/01/2019 n.7**

Coeff. parziali per le azioni o per l'effetto delle azioni

| Carichi | Effetto | | Combinazioni statiche | | | | | Combinazioni sismiche | | |
|----------------------------|-------------|---------------------|-----------------------|------|------|------|------|-----------------------|------|------|
| | | | HYD | UPL | EQU | A1 | A2 | EQU | A1 | A2 |
| Permanenti strutturali | Favorevoli | $\gamma_{G1, fav}$ | 1.00 | 0.90 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Permanenti strutturali | Sfavorevoli | $\gamma_{G1, sfav}$ | 1.00 | 1.10 | 1.30 | 1.30 | 1.00 | 1.00 | 1.00 | 1.00 |
| Permanenti non strutturali | Favorevoli | $\gamma_{G2, fav}$ | 0.00 | 0.80 | 0.80 | 0.80 | 0.80 | 0.00 | 0.00 | 0.00 |
| Permanenti non strutturali | Sfavorevoli | $\gamma_{G2, sfav}$ | 1.00 | 1.50 | 1.50 | 1.50 | 1.30 | 1.00 | 1.00 | 1.00 |
| Variabili | Favorevoli | $\gamma_{Q, fav}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Variabili | Sfavorevoli | $\gamma_{Q, sfav}$ | 1.00 | 1.50 | 1.50 | 1.50 | 1.30 | 1.00 | 1.00 | 1.00 |
| Variabili da traffico | Favorevoli | $\gamma_{QT, fav}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Variabili da traffico | Sfavorevoli | $\gamma_{QT, sfav}$ | 1.00 | 1.50 | 1.35 | 1.35 | 1.15 | 1.00 | 1.00 | 1.00 |

Coeff. parziali per i parametri geotecnici del terreno

| Parametro | | Combinazioni statiche | | Combinazioni sismiche | |
|---------------------------------|-----------------------|-----------------------|------|-----------------------|------|
| | | M1 | M2 | M1 | M2 |
| Tangente dell'angolo di attrito | $\gamma_{\tan(\phi)}$ | 1.00 | 1.25 | 1.00 | 1.00 |
| Coesione efficace | γ_c | 1.00 | 1.25 | 1.00 | 1.00 |
| Resistenza non drenata | γ_{cu} | 1.00 | 1.40 | 1.00 | 1.00 |
| Peso nell'unità di volume | γ_r | 1.00 | 1.00 | 1.00 | 1.00 |

Coeff. parziali γ_R per le verifiche agli stati limite ultimi STR e GEO

| Verifica | Combinazioni statiche | | | Combinazioni sismiche | | |
|----------------------------|-----------------------|------|------|-----------------------|------|------|
| | R1 | R2 | R3 | R1 | R2 | R3 |
| Capacità portante | -- | -- | 1.40 | -- | -- | 1.20 |
| Scorrimento | -- | -- | 1.10 | -- | -- | 1.00 |
| Resistenza terreno a valle | -- | -- | 1.40 | -- | -- | 1.20 |
| Ribaltamento | -- | -- | 1.15 | -- | -- | 1.00 |
| Stabilità fronte di scavo | -- | 1.10 | -- | -- | 1.20 | -- |

Descrizione combinazioni di carico

Con riferimento alle azioni elementari prima determinate, si sono considerate le seguenti combinazioni di carico:

- Combinazione fondamentale, impiegata per gli stati limite ultimi (SLU):

$$\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \gamma_{Q2} Q_{k2} + \gamma_{Q3} Q_{k3} + \dots$$

- Combinazione caratteristica, cosiddetta rara, impiegata per gli stati limite di esercizio (SLE) irreversibili:

$$G_1 + G_2 + Q_{k1} + \Psi_{0,2} Q_{k2} + \Psi_{0,3} Q_{k3} + \dots$$

- Combinazione frequente, impiegata per gli stati limite di esercizio (SLE) reversibili:

$$G_1 + G_2 + \Psi_{1,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

- Combinazione quasi permanente, impiegata per gli effetti di lungo periodo:

$$G_1 + G_2 + \Psi_{2,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

- Combinazione sismica, impiegata per gli stati limite ultimi connessi all'azione sismica E:

$$E + G_1 + G_2 + \Psi_{2,1} Q_{k1} + \Psi_{2,2} Q_{k2} + \Psi_{2,3} Q_{k3} + \dots$$

I valori dei coeff. $\Psi_{0,j}$, $\Psi_{1,j}$, $\Psi_{2,j}$ sono definiti nelle singole condizioni variabili. I valori dei coeff. γ_G e γ_Q , sono definiti nella tabella normativa.

In particolare si sono considerate le seguenti combinazioni:

Simbologia adottata

| | |
|----------|---|
| γ | Coefficiente di partecipazione della condizione |
| Ψ | Coefficiente di combinazione della condizione |

Combinazione n° 1 - STR (A1-M1-R3)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.30 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.50 | -- | Sfavorevole |
| STRADA | 1.35 | 1.00 | Sfavorevole |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 4 - GEO (A2-M2-R2)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.30 | -- | Sfavorevole |
| STRADA | 1.15 | 1.00 | Sfavorevole |

Combinazione n° 5 - GEO (A2-M2-R2) H + V

| Condizione | γ | Ψ | Effetto |
|-----------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
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| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 6 - GEO (A2-M2-R2) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 7 - EQU (A1-M1-R3)

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.30 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.50 | -- | Sfavorevole |
| STRADA | 1.35 | 1.00 | Sfavorevole |

Combinazione n° 8 - EQU (A1-M1-R3) H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 9 - EQU (A1-M1-R3) H - V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Favorevole |
| Peso terrapieno | 1.00 | -- | Favorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 0.20 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Combinazione n° 10 - SLER

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Relazione di calcolo muro di sostegno sede stradale-NV24

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Combinazione n° 11 - SLEF

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Combinazione n° 12 - SLEQ

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |

Combinazione n° 13 - SLEQ_H + V

| Condizione | γ | Ψ | Effetto |
|-------------------------|----------|--------|-------------|
| Peso muro | 1.00 | -- | Sfavorevole |
| Peso terrapieno | 1.00 | -- | Sfavorevole |
| Spinta terreno | 1.00 | -- | Sfavorevole |
| STRADA | 1.00 | 1.00 | Sfavorevole |
| PAVIMENTAZIONE STRADALE | 1.00 | -- | Sfavorevole |

Dati sismici

| | |
|--------------------------------|-------------------------------|
| Comune | Mantova |
| Provincia | Mantova |
| Regione | Lombardia |
| Latitudine | 45.122392 |
| Longitudine | 10.572725 |
| Indice punti di interpolazione | 14056 - 13834 - 13833 - 14055 |
| Vita nominale | 50 anni |
| Classe d'uso | III |
| Tipo costruzione | Normali affollamenti |
| Vita di riferimento | 75 anni |

| | Simbolo | U.M. | SLU | SLE |
|------------------------|---------|---------------------|-------|-------|
| Accelerazione al suolo | a_g | [m/s ²] | 0.931 | 0.438 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|-----------|
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| | Simbolo | U.M. | | SLU | SLE |
|---|-------------------|------|----|-------|-------|
| Accelerazione al suolo | a _g /g | [%] | | 0.095 | 0.045 |
| Massimo fattore amplificazione spettro orizzontale | F0 | | | 2.600 | 2.561 |
| Periodo inizio tratto spettro a velocità costante | Tc* | | | 0.315 | 0.270 |
| Tipo di sottosuolo - Coefficiente stratigrafico | Ss | | D | 1.800 | 1.800 |
| Categoria topografica - Coefficiente amplificazione topografica | St | | T1 | 1.000 | |

| Stato limite ... | Coeff. di riduzione β _m | kh | kv |
|-----------------------|------------------------------------|--------|-------|
| Ultimo | 0.760 | 12.977 | 6.488 |
| Ultimo - Ribaltamento | 1.000 | 17.074 | 8.537 |
| Esercizio | 0.940 | 7.560 | 3.780 |

Forma diagramma incremento sismico **Stessa forma del diagramma statico**

10.2 Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

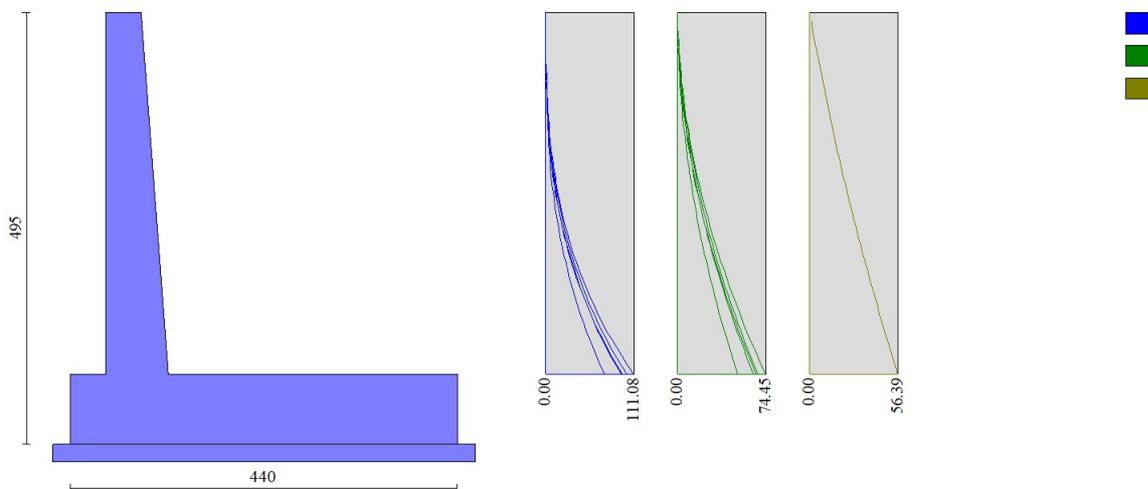
| | |
|--------------------|--|
| Cmb | Indice/Tipo combinazione |
| S | Sisma (H: componente orizzontale, V: componente verticale) |
| FS _{SCO} | Coeff. di sicurezza allo scorrimento |
| FS _{RIB} | Coeff. di sicurezza al ribaltamento |
| FS _{QLIM} | Coeff. di sicurezza a carico limite |
| FS _{STAB} | Coeff. di sicurezza a stabilità globale |
| FS _{HYD} | Coeff. di sicurezza a sifonamento |
| FS _{UPL} | Coeff. di sicurezza a sollevamento |

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{UPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|-------------------|
| 1 - STR (A1-M1-R3) | | 1.635 | | 2.015 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.394 | | 1.525 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.301 | | 1.567 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.298 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.366 | | |
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.314 | | |
| 7 - EQU (A1-M1-R3) | | | 4.296 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 3.042 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.365 | | | | |

10.3 Verifiche strutturali

10.3.1 Paramento

Nella figura seguente si riportano le sollecitazioni agenti sul paramento:



la sezione del paramento viene verificata a pressoflessione (SLU) tenendo conto di tali azioni:

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | $M_{resistente}/M_{agente}$ |
|------------|-------------|-------------|------------------|-------------|-------------------|-----------------------------|
| 111.08 | 100 x 71 | 8 ϕ 20 | 8.4 | 5 ϕ 20 | 8.4 | >1 |

Verifica al taglio

| T (kN) | BxH (cm) | As | $T_{resistente}/T_{agente}$ |
|-----------|-------------|----------------------|-----------------------------|
| 74.45 | 100 x 71 | ϕ 12 / 20x40 cm | >1 |

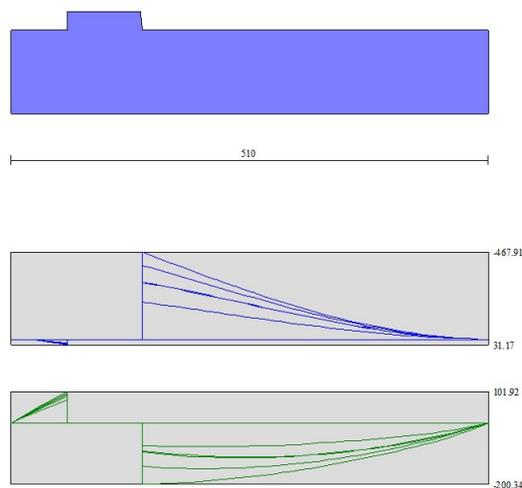
Verifica a SLE:

Verifica a fessurazione (SLE) rara, a favore di sicurezza si verifica le tensioni e le fessurazioni con la sola combinazione rara.

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | σ_s [MPa] | σ_s lim [MPa] | σ_c [MPa] | σ_c lim [MPa] | wk [mm] | wlim [mm] |
|------------|-------------|-------------|------------------|-------------|-------------------|---------------------|-------------------------|---------------------|-------------------------|------------|--------------|
| 56.39 | 100 x 71 | 8 ϕ 20 | 8.4 | 5 ϕ 20 | 8.4 | 40.38 | 360 | 1.30 | 18.26 | 0.00 | 0.3 |

10.3.2 Fondazione

Nella seguente figura si riportano le sollecitazioni agenti sulla fondazione:



la sezione della fondazione viene verificata a pressoflessione (SLU) tenendo conto di tali azioni:

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | $M_{resistente}/M_{agente}$ |
|------------|-------------|-------------|------------------|-------------|-------------------|-----------------------------|
| -305.9 | 100 x 80 | 6 ϕ 20 | 8.4 | 6 ϕ 20 | 8.4 | >1 |

Verifica al taglio

| T (kN) | BxH (cm) | As | $T_{resistente}/T_{agente}$ |
|-----------|-------------|----------------------|-----------------------------|
| 140.36 | 100 x 80 | ϕ 12 / 20x40 cm | >1 |

Verifica a SLE:

Verifica a fessurazione (SLE) rara, a favore di sicurezza si verifica le tensioni e le fessurazioni con la sola combinazione rara.

| M (kNm) | BxH (cm) | As | δ [cm] | A's | δ' [cm] | σ_s [MPa] | σ_s lim [MPa] | σ_c [MPa] | σ_c lim [MPa] | wk [mm] | wlim [mm] |
|------------|-------------|-------------|------------------|-------------|-------------------|---------------------|-------------------------|---------------------|-------------------------|------------|--------------|
| -130.87 | 100 x 80 | 6 ϕ 20 | 8.4 | 6 ϕ 20 | 8.4 | 101.78 | 360 | 1.93 | 18.26 | 0.00 | 0.3 |

11. INCIDENZE

| Elemento | Incidenza di progetto [kg/m ³] |
|------------|---|
| ELEVAZIONE | 130 |
| FONDAZIONE | 95 |



**RADDOPPIO LINEA CODOGNO – CREMONA – MANTOVA
TRATTA PIADENA - MANTOVA**

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
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12. TABULATI DI CALCOLO CONCIO 1

Il modello di calcolo è stato implementato tramite il software di calcolo specifico AZTEC MAX.

12.1 RISULTATI PER COMBINAZIONE

Spinta e forze

Simbologia adottata

| | |
|--------|--|
| Ic | Indice della combinazione |
| A | Tipo azione |
| I | Inclinazione della spinta, espressa in [°] |
| V | Valore dell'azione, espressa in [kN] |
| Cx, Cy | Componente in direzione X ed Y dell'azione, espressa in [kN] |
| Px, Py | Coordinata X ed Y del punto di applicazione dell'azione, espressa in [m] |

| Ic | A | V [kN] | I [°] | Cx [kN] | Cy [kN] | Px [m] | Py [m] |
|----|---|-----------|----------|------------|---------------|-----------|-----------|
| 1 | Spinta statica | 255.10 | 0.00 | 255.10 | 0.00 | 5.65 | -4.76 |
| | Peso/Inerzia muro | | | 0.00 | 283.28/0.00 | 1.45 | -5.81 |
| | Peso/Inerzia terrapieno | | | 0.00 | 734.00/0.00 | 2.96 | -3.20 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 2 | Spinta statica | 161.06 | 0.00 | 161.06 | 0.00 | 5.65 | -4.97 |
| | Incremento di spinta sismica | | 53.41 | 53.41 | 0.00 | 5.65 | -5.07 |
| | Peso/Inerzia muro | | | 36.76 | 283.28/18.38 | 1.45 | -5.81 |
| | Peso/Inerzia terrapieno | | | 88.77 | 684.10/44.39 | 2.95 | -3.20 |
| 3 | Spinta statica | 161.06 | 0.00 | 161.06 | 0.00 | 5.65 | -4.97 |
| | Incremento di spinta sismica | | 33.11 | 33.11 | 0.00 | 5.65 | -5.07 |
| | Peso/Inerzia muro | | | 36.76 | 283.28/-18.38 | 1.45 | -5.81 |
| | Peso/Inerzia terrapieno | | | 88.77 | 684.10/-44.39 | 2.95 | -3.20 |
| 10 | Spinta statica | 194.01 | 0.00 | 194.01 | 0.00 | 5.65 | -4.77 |
| | Peso/Inerzia muro | | | 0.00 | 283.28/0.00 | 1.45 | -5.81 |
| | Peso/Inerzia terrapieno | | | 0.00 | 715.24/0.00 | 2.96 | -3.20 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 11 | Spinta statica | 194.01 | 0.00 | 194.01 | 0.00 | 5.65 | -4.77 |
| | Peso/Inerzia muro | | | 0.00 | 283.28/0.00 | 1.45 | -5.81 |
| | Peso/Inerzia terrapieno | | | 0.00 | 715.24/0.00 | 2.96 | -3.20 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 12 | Spinta statica | 194.01 | 0.00 | 194.01 | 0.00 | 5.65 | -4.77 |
| | Peso/Inerzia muro | | | 0.00 | 283.28/0.00 | 1.45 | -5.81 |
| | Peso/Inerzia terrapieno | | | 0.00 | 715.24/0.00 | 2.96 | -3.20 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 13 | Spinta statica | 194.01 | 0.00 | 194.01 | 0.00 | 5.65 | -4.77 |
| | Incremento di spinta sismica | | 36.09 | 36.09 | 0.00 | 5.65 | -5.07 |
| | Peso/Inerzia muro | | | 21.42 | 283.28/10.71 | 1.45 | -5.81 |
| | Peso/Inerzia terrapieno | | | 54.07 | 715.24/27.04 | 2.96 | -3.20 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
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| Ic | A | V | I | Cx | Cy | Px | Py |
|----|---|------|-----|------|------|------|------|
| | | [kN] | [°] | [kN] | [kN] | [m] | [m] |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |

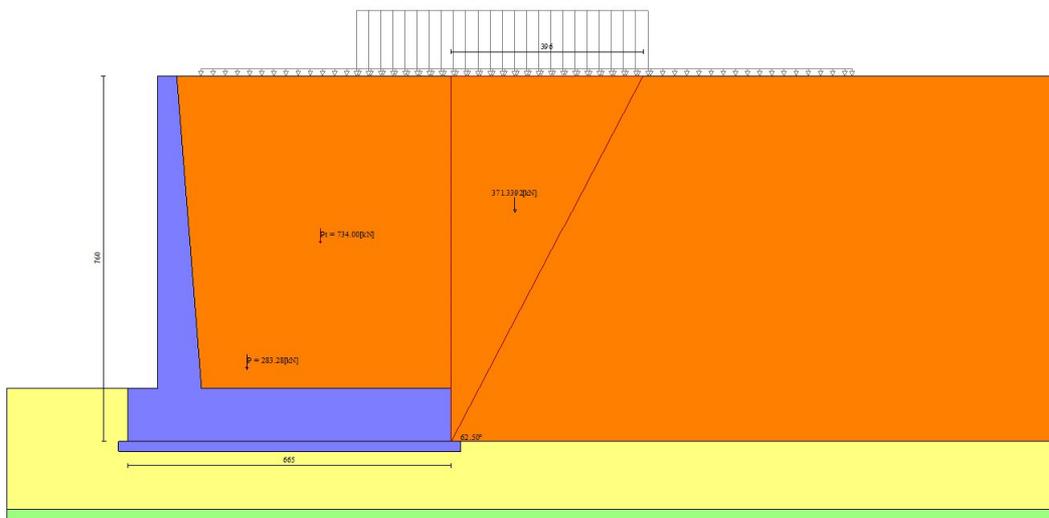


Fig. 3 - Cuneo di spinta (combinazione statica) (Combinazione n° 1)

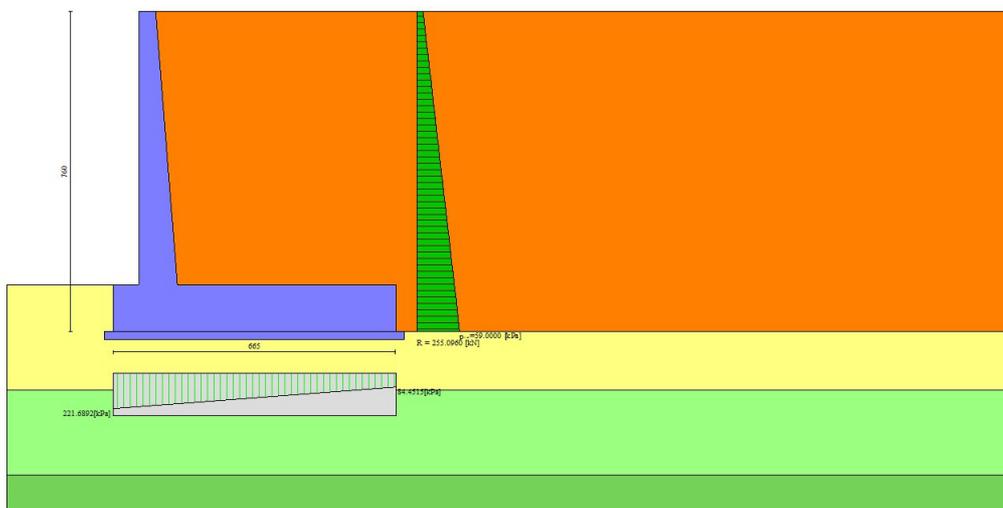


Fig. 4 - Diagramma delle pressioni (combinazione statica) (Combinazione n° 1)

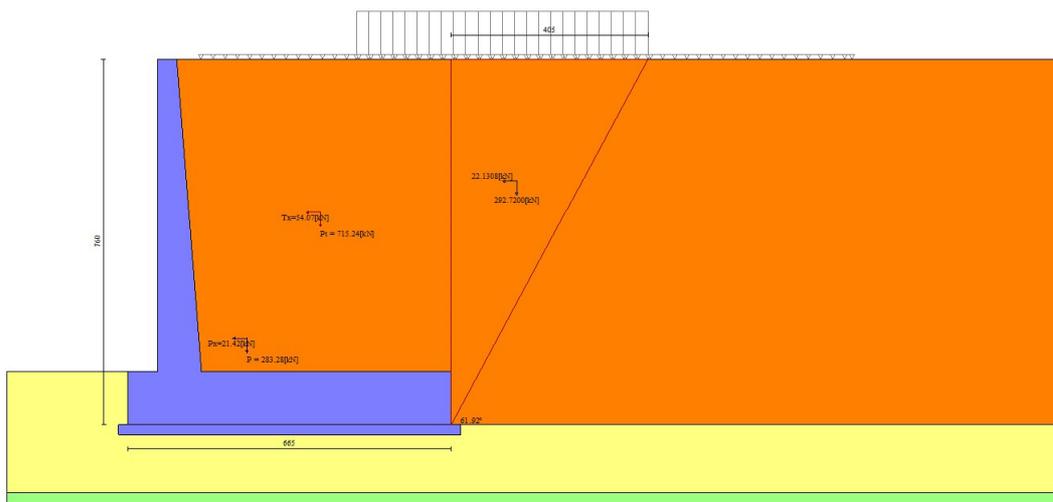


Fig. 5 - Cuneo di spinta (combinazione sismica) (Combinazione n° 13)

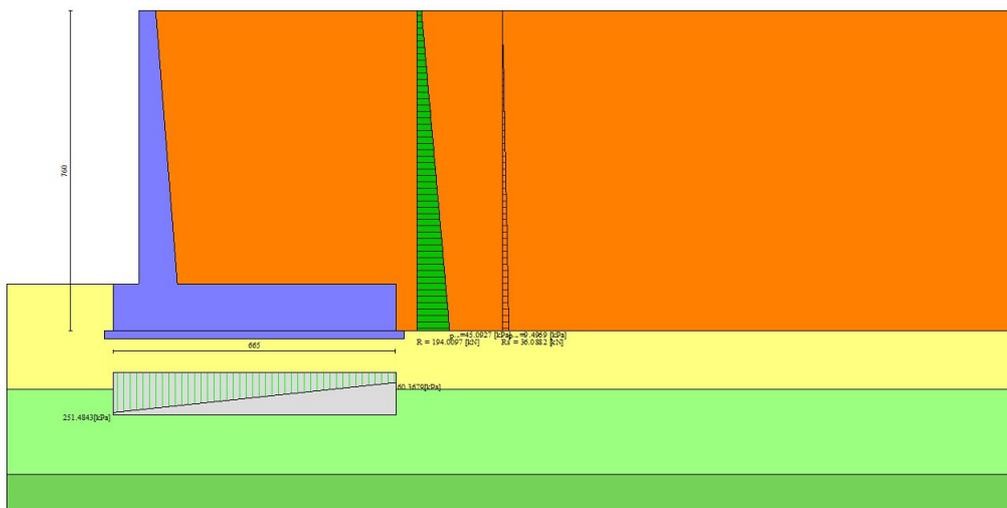


Fig. 6 - Diagramma delle pressioni (combinazione sismica) (Combinazione n° 13)

Simbologia adottata

| | |
|----------------|---|
| Cmb | Indice/Tipo combinazione |
| N | Componente normale al piano di posa, espressa in [kN] |
| T | Componente parallela al piano di posa, espressa in [kN] |
| M _r | Momento ribaltante, espresso in [kNm] |
| M _s | Momento stabilizzante, espresso in [kNm] |
| ecc | Eccentricità risultante, espressa in [m] |

| Ic | N | T | M _r | M _s | ecc |
|--------------------|---------|--------|----------------|----------------|-------|
| | [kN] | [kN] | [kNm] | [kNm] | [m] |
| 1 - STR (A1-M1-R3) | 1017.28 | 255.10 | 724.52 | 3599.76 | 0.497 |
| 2 - STR (A1-M1-R3) | 1030.15 | 340.00 | 1015.40 | 3616.76 | 0.798 |
| 3 - STR (A1-M1-R3) | 904.62 | 319.70 | 1184.33 | 3396.39 | 0.878 |
| 4 - GEO (A2-M2-R2) | 1007.44 | 254.18 | 731.09 | 3559.65 | 0.515 |
| 5 - GEO (A2-M2-R2) | 1030.15 | 340.00 | 1015.40 | 3616.76 | 0.798 |
| 6 - GEO (A2-M2-R2) | 904.62 | 319.70 | 1184.33 | 3396.39 | 0.878 |
| 7 - EQU (A1-M1-R3) | 1017.28 | 255.10 | 724.52 | 3599.76 | 0.497 |
| 8 - EQU (A1-M1-R3) | 1049.97 | 398.20 | 1206.53 | 3686.35 | 0.961 |
| 9 - EQU (A1-M1-R3) | 884.80 | 372.22 | 1430.68 | 3396.39 | 1.101 |
| 10 - SLER | 998.52 | 194.01 | 548.90 | 3523.28 | 0.344 |
| 11 - SLEF | 998.52 | 194.01 | 548.90 | 3523.28 | 0.344 |
| 12 - SLEQ | 998.52 | 194.01 | 548.90 | 3523.28 | 0.344 |
| 13 - SLEQ | 1036.26 | 305.59 | 916.47 | 3656.47 | 0.679 |

Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

| | |
|--------------------|--|
| Cmb | Indice/Tipo combinazione |
| S | Sisma (H: componente orizzontale, V: componente verticale) |
| FS _{SCO} | Coeff. di sicurezza allo scorrimento |
| FS _{RIB} | Coeff. di sicurezza al ribaltamento |
| FS _{QLIM} | Coeff. di sicurezza a carico limite |
| FS _{STAB} | Coeff. di sicurezza a stabilità globale |
| FS _{HYD} | Coeff. di sicurezza a sifonamento |
| FS _{UPL} | Coeff. di sicurezza a sollevamento |

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{UPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|-------------------|
| 1 - STR (A1-M1-R3) | | 1.860 | | 1.790 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.413 | | 1.236 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.319 | | 1.277 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.380 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.383 | | |

| Cmb | Sismica | FSsco | FSRIB | FSQLIM | FSSTAB | FSHYD | FSUPL |
|--------------------|---------|-------|-------|--------|--------|-------|-------|
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.332 | | |
| 7 - EQU (A1-M1-R3) | | | 4.968 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 3.055 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.374 | | | | |

Verifica a scorrimento fondazione

Simbologia adottata

| | |
|-----|---|
| n° | Indice combinazione |
| Rsa | Resistenza allo scorrimento per attrito, espresso in [kN] |
| Rpt | Resistenza passiva terreno antistante, espresso in [kN] |
| Rps | Resistenza passiva sperone, espresso in [kN] |
| Rp | Resistenza a carichi orizzontali pali (solo per fondazione mista), espresso in [kN] |
| Rt | Resistenza a carichi orizzontali tiranti (solo se presenti), espresso in [kN] |
| R | Resistenza allo scorrimento (somma di Rsa+Rpt+Rps+Rp), espresso in [kN] |
| T | Carico parallelo al piano di posa, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto R/T) |

| n° | Rsa | Rpt | Rps | Rp | Rt | R | T | FS |
|--------------------------|--------|------|------|------|------|--------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | |
| 1 - STR (A1-M1-R3) | 474.37 | 0.00 | 0.00 | -- | -- | 474.37 | 255.10 | 1.860 |
| 2 - STR (A1-M1-R3) H + V | 480.37 | 0.00 | 0.00 | -- | -- | 480.37 | 340.00 | 1.413 |
| 3 - STR (A1-M1-R3) H - V | 421.83 | 0.00 | 0.00 | -- | -- | 421.83 | 319.70 | 1.319 |

Verifica a carico limite

Simbologia adottata

| | |
|----|--|
| n° | Indice combinazione |
| N | Carico normale totale al piano di posa, espresso in [kN] |
| Qu | carico limite del terreno, espresso in [kN] |
| Qd | Portanza di progetto, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto tra il carico limie e carico agente al piano di posa) |

| n° | N | Qu | Qd | FS |
|--------------------------|---------|---------|---------|-------|
| | [kN] | [kN] | [kN] | |
| 1 - STR (A1-M1-R3) | 1017.28 | 1820.97 | 1300.70 | 1.790 |
| 2 - STR (A1-M1-R3) H + V | 1030.15 | 1273.69 | 1061.41 | 1.236 |
| 3 - STR (A1-M1-R3) H - V | 904.62 | 1155.14 | 962.62 | 1.277 |

Dettagli calcolo portanza

Simbologia adottata

| | |
|-----------------------|--|
| n° | Indice combinazione |
| N_c, N_q, N_γ | Fattori di capacità portante |
| i_c, i_q, i_γ | Fattori di inclinazione del carico |
| d_c, d_q, d_γ | Fattori di profondità del piano di posa |
| g_c, g_q, g_γ | Fattori di inclinazione del profilo topografico |
| b_c, b_q, b_γ | Fattori di inclinazione del piano di posa |
| s_c, s_q, s_γ | Fattori di forma della fondazione |
| p_c, p_q, p_γ | Fattori di riduzione per punzonamento secondo Vesic |
| R_e | Fattore di riduzione capacità portante per eccentricità secondo Meyerhof |
| I_r, I_{rc} | Indici di rigidezza per punzonamento secondo Vesic |
| r_γ fattore | Fattori per tener conto dell'effetto piastra. Per fondazioni che hanno larghezza maggiore di 2 m, il terzo termine della formula trinomia $0.5B_\gamma N_\gamma$, viene moltiplicato per questo fattore |
| D | Affondamento del piano di posa, espresso in [m] |
| B' | Larghezza fondazione ridotta, espresso in [m] |
| H | Altezza del cuneo di rottura, espresso in [m] |
| γ | Peso di volume del terreno medio, espresso in [kN/mc] |
| ϕ | Angolo di attrito del terreno medio, espresso in [°] |
| c | Coesione del terreno medio, espresso in [kPa] |

Per i coeff. che in tabella sono indicati con il simbolo '-' sono coeff. non presenti nel metodo scelto (Meyerhof).

| n° | N_c N_q N_γ | i_c i_q i_γ | d_c d_q d_γ | g_c g_q g_γ | b_c b_q b_γ | s_c s_q s_γ | p_c p_q p_γ | I_r | I_{rc} | R_e | r_γ |
|-----------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|-------|----------|-------|------------|
| 1 | 27.101 | 0.712 | 1.056 | -- | -- | -- | -- | -- | -- | -- | 0.870 |
| | 15.802 | 0.712 | 1.028 | -- | -- | -- | -- | -- | -- | | |
| | 12.464 | 0.259 | 1.028 | -- | -- | -- | -- | -- | -- | | |
| 2 | 27.101 | 0.635 | 1.056 | -- | -- | -- | -- | -- | -- | -- | 0.870 |
| | 15.802 | 0.635 | 1.028 | -- | -- | -- | -- | -- | -- | | |
| | 12.464 | 0.131 | 1.028 | -- | -- | -- | -- | -- | -- | | |
| 3 | 27.101 | 0.614 | 1.056 | -- | -- | -- | -- | -- | -- | -- | 0.870 |
| | 15.802 | 0.614 | 1.028 | -- | -- | -- | -- | -- | -- | | |
| | 12.464 | 0.103 | 1.028 | -- | -- | -- | -- | -- | -- | | |

| n° | D [m] | B' [m] | H [m] | γ [°] | ϕ [kN/mc] | c [kPa] |
|-----------|------------|-------------|------------|-----------------|-------------------|--------------|
| 1 | 1.10 | 5.65 | 5.60 | 9.89 | 28.64 | 0 |
| 2 | 1.10 | 5.05 | 5.60 | 9.89 | 28.64 | 0 |
| 3 | 1.10 | 4.89 | 5.60 | 9.89 | 28.64 | 0 |

Verifica a ribaltamento

Simbologia adottata

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
|----------|---------|----------|--------------|------|-----------|
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n° Indice combinazione

Ms Momento stabilizzante, espresso in [kNm]

Mr Momento ribaltante, espresso in [kNm]

FS Fattore di sicurezza (rapporto tra momento stabilizzante e momento ribaltante)

La verifica viene eseguita rispetto allo spigolo inferiore esterno della fondazione

| n° | Ms | Mr | FS |
|--------------------------|---------|---------|-------|
| | [kNm] | [kNm] | |
| 7 - EQU (A1-M1-R3) | 3599.76 | 724.52 | 4.968 |
| 8 - EQU (A1-M1-R3) H + V | 3686.35 | 1206.53 | 3.055 |
| 9 - EQU (A1-M1-R3) H - V | 3396.39 | 1430.68 | 2.374 |

Verifica stabilità globale muro + terreno

Simbologia adottata

Ic Indice/Tipo combinazione

C Centro superficie di scorrimento, espresso in [m]

R Raggio, espresso in [m]

FS Fattore di sicurezza

| Ic | C | R | FS |
|--------------------------|------------|-------|-------|
| | [m] | [m] | |
| 4 - GEO (A2-M2-R2) | 0.00; 3.50 | 12.46 | 1.380 |
| 5 - GEO (A2-M2-R2) H + V | 0.00; 4.00 | 12.91 | 1.383 |
| 6 - GEO (A2-M2-R2) H - V | 0.00; 4.00 | 12.91 | 1.332 |

Dettagli strisce verifiche stabilità

Simbologia adottata

Le ascisse X sono considerate positive verso monte

Le ordinate Y sono considerate positive verso l'alto

Origine in testa al muro (spigolo contro terra)

W peso della striscia espresso in [kN]

Qy carico sulla striscia espresso in [kN]

α angolo fra la base della striscia e l'orizzontale espresso in [°] (positivo antiorario)

ϕ angolo d'attrito del terreno lungo la base della striscia

c coesione del terreno lungo la base della striscia espressa in [kPa]

b larghezza della striscia espressa in [m]

u pressione neutra lungo la base della striscia espressa in [kPa]

Tx; Ty Resistenza al taglio fornita dai tiranti in direzione X ed Y espressa in [kPa]

Combinazione n° 4 - GEO (A2-M2-R2)

| n° | W [kN] | Qy [kN] | b [m] | α [°] | φ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|----------|----------|------------|------------|----------------|
| 1 | 14.60 | 2.02 | 11.97 - 0.78 | 68.548 | 29.256 | 0 | 0.0 | |
| 2 | 39.26 | 2.02 | 0.78 | 60.320 | 29.256 | 0 | 0.0 | |
| 3 | 57.13 | 3.37 | 0.78 | 53.693 | 29.256 | 0 | 0.0 | |
| 4 | 71.31 | 19.89 | 0.78 | 48.004 | 29.256 | 0 | 0.0 | |
| 5 | 83.01 | 19.89 | 0.78 | 42.895 | 29.256 | 0 | 0.0 | |
| 6 | 92.85 | 19.89 | 0.78 | 38.184 | 29.256 | 0 | 0.0 | |
| 7 | 101.19 | 19.89 | 0.78 | 33.762 | 29.256 | 0 | 0.0 | |
| 8 | 108.28 | 19.89 | 0.78 | 29.559 | 29.256 | 0 | 0.0 | |
| 9 | 118.32 | 19.89 | 0.78 | 25.526 | 20.458 | 0 | 0.0 | |
| 10 | 124.00 | 19.89 | 0.78 | 21.625 | 20.458 | 0 | 0.8 | |
| 11 | 128.12 | 13.57 | 0.78 | 17.827 | 20.458 | 0 | 3.5 | |
| 12 | 131.40 | 2.02 | 0.78 | 14.108 | 20.458 | 0 | 5.7 | |
| 13 | 133.90 | 2.02 | 0.78 | 10.450 | 20.458 | 0 | 7.4 | |
| 14 | 135.65 | 2.02 | 0.78 | 6.834 | 20.458 | 0 | 8.5 | |
| 15 | 137.93 | 1.54 | 0.78 | 3.246 | 20.458 | 0 | 9.2 | |
| 16 | 151.67 | 0.00 | 0.78 | -0.329 | 20.458 | 0 | 9.4 | |
| 17 | 39.13 | 0.00 | 0.78 | -3.906 | 20.458 | 0 | 9.1 | |
| 18 | 34.70 | 0.00 | 0.78 | -7.499 | 20.458 | 0 | 8.3 | |
| 19 | 32.82 | 0.00 | 0.78 | -11.121 | 20.458 | 0 | 7.1 | |
| 20 | 30.18 | 0.00 | 0.78 | -14.789 | 20.458 | 0 | 5.3 | |
| 21 | 26.74 | 0.00 | 0.78 | -18.520 | 20.458 | 0 | 3.1 | |
| 22 | 22.47 | 0.00 | 0.78 | -22.336 | 20.458 | 0 | 0.2 | |
| 23 | 17.28 | 0.00 | 0.78 | -26.259 | 20.458 | 0 | 0.0 | |
| 24 | 11.10 | 0.00 | 0.78 | -30.320 | 20.458 | 0 | 0.0 | |
| 25 | 3.79 | 0.00 | -7.45 - 0.78 | -34.011 | 20.458 | 0 | 0.0 | |

Combinazione n° 5 - GEO (A2-M2-R2) H + V

| n° | W [kN] | Qy [kN] | b [m] | α [°] | φ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|----------|----------|------------|------------|----------------|
| 1 | 14.16 | 1.58 | 12.29 - 0.79 | 67.155 | 35.000 | 0 | 0.0 | |
| 2 | 38.43 | 1.58 | 0.79 | 59.441 | 35.000 | 0 | 0.0 | |
| 3 | 56.47 | 1.58 | 0.79 | 53.054 | 35.000 | 0 | 0.0 | |
| 4 | 70.92 | 3.92 | 0.79 | 47.522 | 35.000 | 0 | 0.0 | |
| 5 | 82.91 | 4.75 | 0.79 | 42.531 | 35.000 | 0 | 0.0 | |
| 6 | 93.03 | 4.75 | 0.79 | 37.914 | 35.000 | 0 | 0.0 | |
| 7 | 101.63 | 4.75 | 0.79 | 33.574 | 35.000 | 0 | 0.0 | |
| 8 | 108.96 | 4.75 | 0.79 | 29.443 | 35.000 | 0 | 0.0 | |
| 9 | 118.16 | 4.75 | 0.79 | 25.475 | 25.000 | 0 | 0.0 | |
| 10 | 125.19 | 4.75 | 0.79 | 21.635 | 25.000 | 0 | 0.0 | |
| 11 | 129.48 | 4.23 | 0.79 | 17.895 | 25.000 | 0 | 2.7 | |
| 12 | 132.92 | 1.58 | 0.79 | 14.232 | 25.000 | 0 | 5.0 | |
| 13 | 135.56 | 1.58 | 0.79 | 10.628 | 25.000 | 0 | 6.7 | |
| 14 | 137.42 | 1.58 | 0.79 | 7.067 | 25.000 | 0 | 7.9 | |
| 15 | 138.93 | 1.38 | 0.79 | 3.533 | 25.000 | 0 | 8.6 | |
| 16 | 161.67 | 0.00 | 0.79 | 0.012 | 25.000 | 0 | 8.9 | |
| 17 | 40.55 | 0.00 | 0.79 | -3.509 | 25.000 | 0 | 8.6 | |
| 18 | 34.74 | 0.00 | 0.79 | -7.043 | 25.000 | 0 | 7.9 | |
| 19 | 32.89 | 0.00 | 0.79 | -10.604 | 25.000 | 0 | 6.7 | |
| 20 | 30.26 | 0.00 | 0.79 | -14.208 | 25.000 | 0 | 5.0 | |
| 21 | 26.83 | 0.00 | 0.79 | -17.870 | 25.000 | 0 | 2.8 | |
| 22 | 22.54 | 0.00 | 0.79 | -21.610 | 25.000 | 0 | 0.0 | |
| 23 | 17.34 | 0.00 | 0.79 | -25.449 | 25.000 | 0 | 0.0 | |
| 24 | 11.13 | 0.00 | 0.79 | -29.416 | 25.000 | 0 | 0.0 | |
| 25 | 3.81 | 0.00 | -7.53 - 0.79 | -33.072 | 25.000 | 0 | 0.0 | |

| n° | W [kN] | Qy [kN] | b [m] | α [°] | ϕ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|-----------------|---------------|------------|------------|----------------|
| 1 | 14.16 | 1.58 | 12.29 - 0.79 | 67.155 | 35.000 | 0 | 0.0 | |
| 2 | 38.43 | 1.58 | 0.79 | 59.441 | 35.000 | 0 | 0.0 | |
| 3 | 56.47 | 1.58 | 0.79 | 53.054 | 35.000 | 0 | 0.0 | |
| 4 | 70.92 | 3.92 | 0.79 | 47.522 | 35.000 | 0 | 0.0 | |
| 5 | 82.91 | 4.75 | 0.79 | 42.531 | 35.000 | 0 | 0.0 | |
| 6 | 93.03 | 4.75 | 0.79 | 37.914 | 35.000 | 0 | 0.0 | |
| 7 | 101.63 | 4.75 | 0.79 | 33.574 | 35.000 | 0 | 0.0 | |
| 8 | 108.96 | 4.75 | 0.79 | 29.443 | 35.000 | 0 | 0.0 | |
| 9 | 118.16 | 4.75 | 0.79 | 25.475 | 25.000 | 0 | 0.0 | |
| 10 | 125.19 | 4.75 | 0.79 | 21.635 | 25.000 | 0 | 0.0 | |
| 11 | 129.48 | 4.23 | 0.79 | 17.895 | 25.000 | 0 | 2.7 | |
| 12 | 132.92 | 1.58 | 0.79 | 14.232 | 25.000 | 0 | 5.0 | |
| 13 | 135.56 | 1.58 | 0.79 | 10.628 | 25.000 | 0 | 6.7 | |
| 14 | 137.42 | 1.58 | 0.79 | 7.067 | 25.000 | 0 | 7.9 | |
| 15 | 138.93 | 1.38 | 0.79 | 3.533 | 25.000 | 0 | 8.6 | |
| 16 | 161.67 | 0.00 | 0.79 | 0.012 | 25.000 | 0 | 8.9 | |
| 17 | 40.55 | 0.00 | 0.79 | -3.509 | 25.000 | 0 | 8.6 | |
| 18 | 34.74 | 0.00 | 0.79 | -7.043 | 25.000 | 0 | 7.9 | |
| 19 | 32.89 | 0.00 | 0.79 | -10.604 | 25.000 | 0 | 6.7 | |
| 20 | 30.26 | 0.00 | 0.79 | -14.208 | 25.000 | 0 | 5.0 | |
| 21 | 26.83 | 0.00 | 0.79 | -17.870 | 25.000 | 0 | 2.8 | |
| 22 | 22.54 | 0.00 | 0.79 | -21.610 | 25.000 | 0 | 0.0 | |
| 23 | 17.34 | 0.00 | 0.79 | -25.449 | 25.000 | 0 | 0.0 | |
| 24 | 11.13 | 0.00 | 0.79 | -29.416 | 25.000 | 0 | 0.0 | |
| 25 | 3.81 | 0.00 | -7.53 - 0.79 | -33.072 | 25.000 | 0 | 0.0 | |

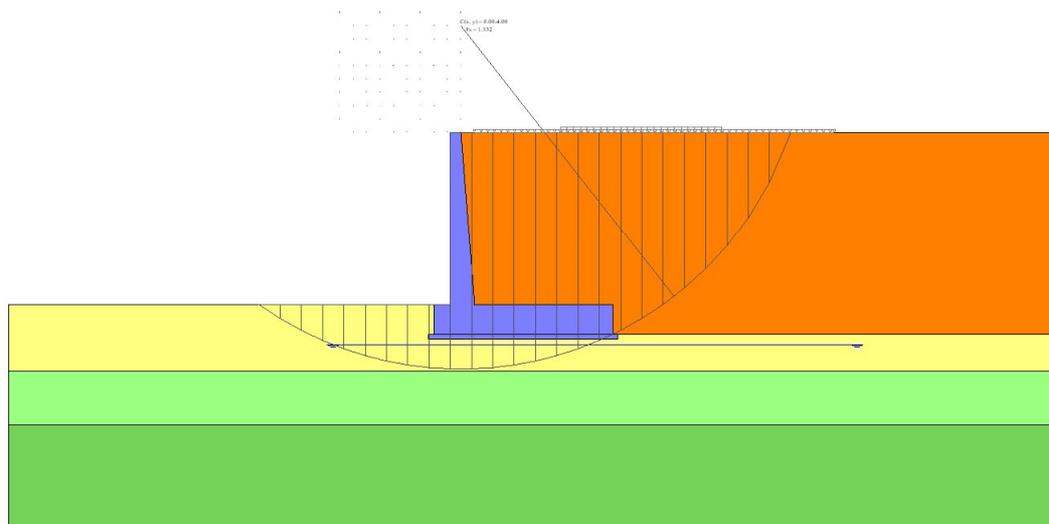


Fig. 7 - Stabilità fronte di scavo - Cerchio critico (Combinazione n° 6)

Simbologia adottata

| | |
|--------------|---|
| Cmb | Tipo combinazione |
| $a_{g,crit}$ | accelerazione critica, espressa in $[m/s^2]$ |
| Dmax | Spostamento orizzontale massimo, espressa in $[cm]$ |

| Cmb | $a_{g,crit}$ $[m/s^2]$ | Dmax $[cm]$ |
|-----------------|---------------------------|----------------|
| 13 - SLEQ H + V | 2.1328 | 0.0007 |

Sollecitazioni

Elementi calcolati a trave

Simbologia adottata

| | |
|---|--|
| N | Sforzo normale, espresso in $[kN]$. Positivo se di compressione. |
| T | Taglio, espresso in $[kN]$. Positivo se diretto da monte verso valle |
| M | Momento, espresso in $[kNm]$. Positivo se tende le fibre contro terra (a monte) |

Paramento

Combinazione n° 1 - STR (A1-M1-R3)

| n° | X $[m]$ | N $[kN]$ | T $[kN]$ | M $[kNm]$ |
|----|------------|-------------|-------------|--------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.04 | 0.00 |
| 3 | -0.20 | 2.00 | 0.15 | 0.02 |
| 4 | -0.30 | 3.03 | 0.34 | 0.05 |
| 5 | -0.40 | 4.08 | 0.60 | 0.11 |
| 6 | -0.50 | 5.14 | 0.93 | 0.20 |
| 7 | -0.60 | 6.23 | 1.34 | 0.34 |
| 8 | -0.70 | 7.33 | 1.83 | 0.52 |
| 9 | -0.80 | 8.46 | 2.41 | 0.76 |
| 10 | -0.90 | 9.60 | 3.08 | 1.07 |
| 11 | -1.00 | 10.76 | 3.85 | 1.46 |
| 12 | -1.10 | 11.94 | 4.71 | 1.93 |
| 13 | -1.20 | 13.14 | 5.64 | 2.50 |
| 14 | -1.30 | 14.36 | 6.65 | 3.16 |
| 15 | -1.40 | 15.60 | 7.73 | 3.94 |
| 16 | -1.50 | 16.86 | 8.89 | 4.84 |
| 17 | -1.60 | 18.13 | 10.13 | 5.85 |
| 18 | -1.70 | 19.43 | 11.44 | 7.00 |
| 19 | -1.80 | 20.74 | 12.82 | 8.29 |
| 20 | -1.90 | 22.08 | 14.28 | 9.73 |
| 21 | -2.00 | 23.43 | 15.81 | 11.32 |
| 22 | -2.10 | 24.80 | 17.42 | 13.08 |
| 23 | -2.20 | 26.19 | 19.10 | 15.00 |
| 24 | -2.30 | 27.60 | 20.85 | 17.11 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 25 | -2.40 | 29.03 | 22.68 | 19.39 |
| 26 | -2.50 | 30.48 | 24.58 | 21.87 |
| 27 | -2.60 | 31.95 | 26.56 | 24.55 |
| 28 | -2.70 | 33.43 | 28.61 | 27.43 |
| 29 | -2.80 | 34.94 | 30.74 | 30.53 |
| 30 | -2.90 | 36.46 | 32.94 | 33.85 |
| 31 | -3.00 | 38.01 | 35.21 | 37.41 |
| 32 | -3.10 | 39.57 | 37.56 | 41.20 |
| 33 | -3.20 | 41.15 | 39.98 | 45.23 |
| 34 | -3.30 | 42.75 | 42.48 | 49.51 |
| 35 | -3.40 | 44.37 | 45.05 | 54.06 |
| 36 | -3.50 | 46.01 | 47.69 | 58.87 |
| 37 | -3.60 | 47.67 | 50.41 | 63.96 |
| 38 | -3.70 | 49.35 | 53.20 | 69.33 |
| 39 | -3.80 | 51.04 | 56.07 | 74.98 |
| 40 | -3.90 | 52.76 | 59.01 | 80.94 |
| 41 | -4.00 | 54.49 | 62.02 | 87.20 |
| 42 | -4.10 | 56.24 | 65.11 | 93.77 |
| 43 | -4.20 | 58.02 | 68.27 | 100.66 |
| 44 | -4.30 | 59.81 | 71.51 | 107.88 |
| 45 | -4.40 | 61.62 | 74.82 | 115.43 |
| 46 | -4.50 | 63.45 | 78.20 | 123.32 |
| 47 | -4.60 | 65.30 | 81.66 | 131.57 |
| 48 | -4.70 | 67.17 | 85.19 | 140.17 |
| 49 | -4.80 | 69.05 | 88.80 | 149.13 |
| 50 | -4.90 | 70.96 | 92.48 | 158.47 |
| 51 | -5.00 | 72.88 | 96.24 | 168.18 |
| 52 | -5.10 | 74.83 | 100.06 | 178.28 |
| 53 | -5.20 | 76.79 | 103.97 | 188.78 |
| 54 | -5.30 | 78.77 | 107.94 | 199.68 |
| 55 | -5.40 | 80.78 | 112.00 | 210.98 |
| 56 | -5.50 | 82.80 | 116.12 | 222.71 |
| 57 | -5.60 | 84.84 | 120.32 | 234.85 |
| 58 | -5.70 | 86.89 | 124.59 | 247.43 |
| 59 | -5.80 | 88.97 | 129.00 | 260.45 |
| 60 | -5.90 | 91.07 | 133.64 | 273.93 |
| 61 | -6.00 | 93.18 | 138.50 | 287.90 |
| 62 | -6.10 | 95.32 | 143.61 | 302.37 |
| 63 | -6.20 | 97.47 | 148.90 | 317.37 |
| 64 | -6.30 | 99.65 | 154.27 | 332.91 |
| 65 | -6.40 | 101.84 | 159.73 | 349.00 |
| 66 | -6.50 | 104.05 | 165.28 | 365.65 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.17 | 0.01 |
| 3 | -0.20 | 2.00 | 0.41 | 0.04 |
| 4 | -0.30 | 3.03 | 0.74 | 0.11 |
| 5 | -0.40 | 4.08 | 1.14 | 0.22 |
| 6 | -0.50 | 5.14 | 1.63 | 0.37 |
| 7 | -0.60 | 6.23 | 2.19 | 0.59 |
| 8 | -0.70 | 7.33 | 2.84 | 0.86 |
| 9 | -0.80 | 8.46 | 3.57 | 1.21 |
| 10 | -0.90 | 9.60 | 4.40 | 1.65 |
| 11 | -1.00 | 10.76 | 5.32 | 2.17 |
| 12 | -1.10 | 11.94 | 6.33 | 2.80 |
| 13 | -1.20 | 13.14 | 7.42 | 3.53 |
| 14 | -1.30 | 14.36 | 8.59 | 4.39 |
| 15 | -1.40 | 15.60 | 9.84 | 5.36 |
| 16 | -1.50 | 16.86 | 11.17 | 6.48 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 17 | -1.60 | 18.13 | 12.58 | 7.73 |
| 18 | -1.70 | 19.43 | 14.07 | 9.14 |
| 19 | -1.80 | 20.74 | 15.64 | 10.70 |
| 20 | -1.90 | 22.08 | 17.29 | 12.43 |
| 21 | -2.00 | 23.43 | 19.01 | 14.33 |
| 22 | -2.10 | 24.80 | 20.82 | 16.42 |
| 23 | -2.20 | 26.19 | 22.70 | 18.69 |
| 24 | -2.30 | 27.60 | 24.67 | 21.16 |
| 25 | -2.40 | 29.03 | 26.71 | 23.84 |
| 26 | -2.50 | 30.48 | 28.83 | 26.73 |
| 27 | -2.60 | 31.95 | 31.03 | 29.85 |
| 28 | -2.70 | 33.43 | 33.31 | 33.19 |
| 29 | -2.80 | 34.94 | 35.67 | 36.77 |
| 30 | -2.90 | 36.46 | 38.11 | 40.60 |
| 31 | -3.00 | 38.01 | 40.63 | 44.68 |
| 32 | -3.10 | 39.57 | 43.22 | 49.03 |
| 33 | -3.20 | 41.15 | 45.90 | 53.64 |
| 34 | -3.30 | 42.75 | 48.65 | 58.53 |
| 35 | -3.40 | 44.37 | 51.49 | 63.70 |
| 36 | -3.50 | 46.01 | 54.40 | 69.17 |
| 37 | -3.60 | 47.67 | 57.39 | 74.94 |
| 38 | -3.70 | 49.35 | 60.46 | 81.03 |
| 39 | -3.80 | 51.04 | 63.61 | 87.42 |
| 40 | -3.90 | 52.76 | 66.84 | 94.15 |
| 41 | -4.00 | 54.49 | 70.15 | 101.21 |
| 42 | -4.10 | 56.24 | 73.53 | 108.60 |
| 43 | -4.20 | 58.02 | 77.00 | 116.35 |
| 44 | -4.30 | 59.81 | 80.54 | 124.46 |
| 45 | -4.40 | 61.62 | 84.17 | 132.93 |
| 46 | -4.50 | 63.45 | 87.87 | 141.77 |
| 47 | -4.60 | 65.30 | 91.65 | 151.00 |
| 48 | -4.70 | 67.17 | 95.51 | 160.62 |
| 49 | -4.80 | 69.05 | 99.45 | 170.63 |
| 50 | -4.90 | 70.96 | 103.47 | 181.05 |
| 51 | -5.00 | 72.88 | 107.57 | 191.88 |
| 52 | -5.10 | 74.83 | 111.74 | 203.13 |
| 53 | -5.20 | 76.79 | 116.00 | 214.81 |
| 54 | -5.30 | 78.77 | 120.33 | 226.93 |
| 55 | -5.40 | 80.78 | 124.75 | 239.49 |
| 56 | -5.50 | 82.80 | 129.24 | 252.51 |
| 57 | -5.60 | 84.84 | 133.81 | 265.99 |
| 58 | -5.70 | 86.89 | 138.46 | 279.94 |
| 59 | -5.80 | 88.97 | 143.19 | 294.36 |
| 60 | -5.90 | 91.07 | 148.00 | 309.27 |
| 61 | -6.00 | 93.18 | 152.89 | 324.67 |
| 62 | -6.10 | 95.32 | 157.86 | 340.58 |
| 63 | -6.20 | 97.47 | 162.90 | 356.99 |
| 64 | -6.30 | 99.65 | 168.03 | 373.92 |
| 65 | -6.40 | 101.84 | 173.23 | 391.37 |
| 66 | -6.50 | 104.05 | 178.51 | 409.36 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.16 | 0.01 |
| 3 | -0.20 | 2.00 | 0.40 | 0.04 |
| 4 | -0.30 | 3.03 | 0.71 | 0.11 |
| 5 | -0.40 | 4.08 | 1.08 | 0.21 |
| 6 | -0.50 | 5.14 | 1.53 | 0.36 |
| 7 | -0.60 | 6.23 | 2.06 | 0.56 |
| 8 | -0.70 | 7.33 | 2.65 | 0.82 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 9 | -0.80 | 8.46 | 3.34 | 1.15 |
| 10 | -0.90 | 9.60 | 4.10 | 1.56 |
| 11 | -1.00 | 10.76 | 4.95 | 2.05 |
| 12 | -1.10 | 11.94 | 5.88 | 2.63 |
| 13 | -1.20 | 13.14 | 6.89 | 3.32 |
| 14 | -1.30 | 14.36 | 7.97 | 4.12 |
| 15 | -1.40 | 15.60 | 9.12 | 5.03 |
| 16 | -1.50 | 16.86 | 10.34 | 6.06 |
| 17 | -1.60 | 18.13 | 11.64 | 7.23 |
| 18 | -1.70 | 19.43 | 13.01 | 8.53 |
| 19 | -1.80 | 20.74 | 14.44 | 9.98 |
| 20 | -1.90 | 22.08 | 15.96 | 11.59 |
| 21 | -2.00 | 23.43 | 17.54 | 13.35 |
| 22 | -2.10 | 24.80 | 19.19 | 15.28 |
| 23 | -2.20 | 26.19 | 20.92 | 17.38 |
| 24 | -2.30 | 27.60 | 22.72 | 19.67 |
| 25 | -2.40 | 29.03 | 24.59 | 22.15 |
| 26 | -2.50 | 30.48 | 26.53 | 24.82 |
| 27 | -2.60 | 31.95 | 28.54 | 27.69 |
| 28 | -2.70 | 33.43 | 30.63 | 30.78 |
| 29 | -2.80 | 34.94 | 32.79 | 34.08 |
| 30 | -2.90 | 36.46 | 35.01 | 37.61 |
| 31 | -3.00 | 38.01 | 37.31 | 41.37 |
| 32 | -3.10 | 39.57 | 39.69 | 45.37 |
| 33 | -3.20 | 41.15 | 42.13 | 49.62 |
| 34 | -3.30 | 42.75 | 44.64 | 54.12 |
| 35 | -3.40 | 44.37 | 47.23 | 58.88 |
| 36 | -3.50 | 46.01 | 49.89 | 63.91 |
| 37 | -3.60 | 47.67 | 52.62 | 69.22 |
| 38 | -3.70 | 49.35 | 55.42 | 74.81 |
| 39 | -3.80 | 51.04 | 58.29 | 80.69 |
| 40 | -3.90 | 52.76 | 61.24 | 86.87 |
| 41 | -4.00 | 54.49 | 64.26 | 93.35 |
| 42 | -4.10 | 56.24 | 67.34 | 100.15 |
| 43 | -4.20 | 58.02 | 70.50 | 107.26 |
| 44 | -4.30 | 59.81 | 73.74 | 114.70 |
| 45 | -4.40 | 61.62 | 77.04 | 122.47 |
| 46 | -4.50 | 63.45 | 80.41 | 130.59 |
| 47 | -4.60 | 65.30 | 83.86 | 139.05 |
| 48 | -4.70 | 67.17 | 87.38 | 147.87 |
| 49 | -4.80 | 69.05 | 90.97 | 157.05 |
| 50 | -4.90 | 70.96 | 94.63 | 166.61 |
| 51 | -5.00 | 72.88 | 98.36 | 176.54 |
| 52 | -5.10 | 74.83 | 102.17 | 186.85 |
| 53 | -5.20 | 76.79 | 106.04 | 197.55 |
| 54 | -5.30 | 78.77 | 109.99 | 208.66 |
| 55 | -5.40 | 80.78 | 114.01 | 220.17 |
| 56 | -5.50 | 82.80 | 118.10 | 232.09 |
| 57 | -5.60 | 84.84 | 122.27 | 244.43 |
| 58 | -5.70 | 86.89 | 126.50 | 257.21 |
| 59 | -5.80 | 88.97 | 130.81 | 270.41 |
| 60 | -5.90 | 91.07 | 135.18 | 284.06 |
| 61 | -6.00 | 93.18 | 139.63 | 298.16 |
| 62 | -6.10 | 95.32 | 144.15 | 312.72 |
| 63 | -6.20 | 97.47 | 148.75 | 327.74 |
| 64 | -6.30 | 99.65 | 153.41 | 343.23 |
| 65 | -6.40 | 101.84 | 158.15 | 359.20 |
| 66 | -6.50 | 104.05 | 162.96 | 375.65 |

Combinazione n° 10 - SLER

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
|----|----------|-----------|-----------|------------|

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.03 | 0.00 |
| 3 | -0.20 | 2.00 | 0.12 | 0.02 |
| 4 | -0.30 | 3.03 | 0.26 | 0.04 |
| 5 | -0.40 | 4.08 | 0.46 | 0.09 |
| 6 | -0.50 | 5.14 | 0.71 | 0.17 |
| 7 | -0.60 | 6.23 | 1.03 | 0.28 |
| 8 | -0.70 | 7.33 | 1.40 | 0.42 |
| 9 | -0.80 | 8.46 | 1.85 | 0.62 |
| 10 | -0.90 | 9.60 | 2.36 | 0.86 |
| 11 | -1.00 | 10.76 | 2.95 | 1.17 |
| 12 | -1.10 | 11.94 | 3.59 | 1.54 |
| 13 | -1.20 | 13.14 | 4.30 | 1.98 |
| 14 | -1.30 | 14.36 | 5.07 | 2.50 |
| 15 | -1.40 | 15.60 | 5.90 | 3.11 |
| 16 | -1.50 | 16.86 | 6.78 | 3.81 |
| 17 | -1.60 | 18.13 | 7.72 | 4.60 |
| 18 | -1.70 | 19.43 | 8.72 | 5.49 |
| 19 | -1.80 | 20.74 | 9.78 | 6.50 |
| 20 | -1.90 | 22.08 | 10.89 | 7.61 |
| 21 | -2.00 | 23.43 | 12.06 | 8.85 |
| 22 | -2.10 | 24.80 | 13.28 | 10.21 |
| 23 | -2.20 | 26.19 | 14.57 | 11.70 |
| 24 | -2.30 | 27.60 | 15.91 | 13.33 |
| 25 | -2.40 | 29.03 | 17.31 | 15.10 |
| 26 | -2.50 | 30.48 | 18.76 | 17.02 |
| 27 | -2.60 | 31.95 | 20.27 | 19.09 |
| 28 | -2.70 | 33.43 | 21.84 | 21.32 |
| 29 | -2.80 | 34.94 | 23.47 | 23.72 |
| 30 | -2.90 | 36.46 | 25.15 | 26.29 |
| 31 | -3.00 | 38.01 | 26.89 | 29.04 |
| 32 | -3.10 | 39.57 | 28.69 | 31.97 |
| 33 | -3.20 | 41.15 | 30.54 | 35.08 |
| 34 | -3.30 | 42.75 | 32.45 | 38.40 |
| 35 | -3.40 | 44.37 | 34.42 | 41.91 |
| 36 | -3.50 | 46.01 | 36.44 | 45.63 |
| 37 | -3.60 | 47.67 | 38.53 | 49.56 |
| 38 | -3.70 | 49.35 | 40.66 | 53.70 |
| 39 | -3.80 | 51.04 | 42.86 | 58.08 |
| 40 | -3.90 | 52.76 | 45.11 | 62.68 |
| 41 | -4.00 | 54.49 | 47.42 | 67.51 |
| 42 | -4.10 | 56.24 | 49.79 | 72.59 |
| 43 | -4.20 | 58.02 | 52.21 | 77.91 |
| 44 | -4.30 | 59.81 | 54.69 | 83.48 |
| 45 | -4.40 | 61.62 | 57.23 | 89.31 |
| 46 | -4.50 | 63.45 | 59.82 | 95.41 |
| 47 | -4.60 | 65.30 | 62.48 | 101.77 |
| 48 | -4.70 | 67.17 | 65.18 | 108.41 |
| 49 | -4.80 | 69.05 | 67.95 | 115.34 |
| 50 | -4.90 | 70.96 | 70.77 | 122.54 |
| 51 | -5.00 | 72.88 | 73.65 | 130.04 |
| 52 | -5.10 | 74.83 | 76.59 | 137.84 |
| 53 | -5.20 | 76.79 | 79.58 | 145.95 |
| 54 | -5.30 | 78.77 | 82.63 | 154.36 |
| 55 | -5.40 | 80.78 | 85.74 | 163.09 |
| 56 | -5.50 | 82.80 | 88.90 | 172.14 |
| 57 | -5.60 | 84.84 | 92.12 | 181.51 |
| 58 | -5.70 | 86.89 | 95.40 | 191.22 |
| 59 | -5.80 | 88.97 | 98.77 | 201.27 |
| 60 | -5.90 | 91.07 | 102.30 | 211.67 |
| 61 | -6.00 | 93.18 | 106.00 | 222.45 |
| 62 | -6.10 | 95.32 | 109.88 | 233.61 |
| 63 | -6.20 | 97.47 | 113.89 | 245.17 |
| 64 | -6.30 | 99.65 | 117.99 | 257.15 |
| 65 | -6.40 | 101.84 | 122.17 | 269.54 |
| 66 | -6.50 | 104.05 | 126.43 | 282.37 |

Combinazione n° 11 - SLEF

| n° | X | N | T | M |
|----|-------|-------|--------|--------|
| | [m] | [kN] | [kN] | [kNm] |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.03 | 0.00 |
| 3 | -0.20 | 2.00 | 0.12 | 0.02 |
| 4 | -0.30 | 3.03 | 0.26 | 0.04 |
| 5 | -0.40 | 4.08 | 0.46 | 0.09 |
| 6 | -0.50 | 5.14 | 0.71 | 0.17 |
| 7 | -0.60 | 6.23 | 1.03 | 0.28 |
| 8 | -0.70 | 7.33 | 1.40 | 0.42 |
| 9 | -0.80 | 8.46 | 1.85 | 0.62 |
| 10 | -0.90 | 9.60 | 2.36 | 0.86 |
| 11 | -1.00 | 10.76 | 2.95 | 1.17 |
| 12 | -1.10 | 11.94 | 3.59 | 1.54 |
| 13 | -1.20 | 13.14 | 4.30 | 1.98 |
| 14 | -1.30 | 14.36 | 5.07 | 2.50 |
| 15 | -1.40 | 15.60 | 5.90 | 3.11 |
| 16 | -1.50 | 16.86 | 6.78 | 3.81 |
| 17 | -1.60 | 18.13 | 7.72 | 4.60 |
| 18 | -1.70 | 19.43 | 8.72 | 5.49 |
| 19 | -1.80 | 20.74 | 9.78 | 6.50 |
| 20 | -1.90 | 22.08 | 10.89 | 7.61 |
| 21 | -2.00 | 23.43 | 12.06 | 8.85 |
| 22 | -2.10 | 24.80 | 13.28 | 10.21 |
| 23 | -2.20 | 26.19 | 14.57 | 11.70 |
| 24 | -2.30 | 27.60 | 15.91 | 13.33 |
| 25 | -2.40 | 29.03 | 17.31 | 15.10 |
| 26 | -2.50 | 30.48 | 18.76 | 17.02 |
| 27 | -2.60 | 31.95 | 20.27 | 19.09 |
| 28 | -2.70 | 33.43 | 21.84 | 21.32 |
| 29 | -2.80 | 34.94 | 23.47 | 23.72 |
| 30 | -2.90 | 36.46 | 25.15 | 26.29 |
| 31 | -3.00 | 38.01 | 26.89 | 29.04 |
| 32 | -3.10 | 39.57 | 28.69 | 31.97 |
| 33 | -3.20 | 41.15 | 30.54 | 35.08 |
| 34 | -3.30 | 42.75 | 32.45 | 38.40 |
| 35 | -3.40 | 44.37 | 34.42 | 41.91 |
| 36 | -3.50 | 46.01 | 36.44 | 45.63 |
| 37 | -3.60 | 47.67 | 38.53 | 49.56 |
| 38 | -3.70 | 49.35 | 40.66 | 53.70 |
| 39 | -3.80 | 51.04 | 42.86 | 58.08 |
| 40 | -3.90 | 52.76 | 45.11 | 62.68 |
| 41 | -4.00 | 54.49 | 47.42 | 67.51 |
| 42 | -4.10 | 56.24 | 49.79 | 72.59 |
| 43 | -4.20 | 58.02 | 52.21 | 77.91 |
| 44 | -4.30 | 59.81 | 54.69 | 83.48 |
| 45 | -4.40 | 61.62 | 57.23 | 89.31 |
| 46 | -4.50 | 63.45 | 59.82 | 95.41 |
| 47 | -4.60 | 65.30 | 62.48 | 101.77 |
| 48 | -4.70 | 67.17 | 65.18 | 108.41 |
| 49 | -4.80 | 69.05 | 67.95 | 115.34 |
| 50 | -4.90 | 70.96 | 70.77 | 122.54 |
| 51 | -5.00 | 72.88 | 73.65 | 130.04 |
| 52 | -5.10 | 74.83 | 76.59 | 137.84 |
| 53 | -5.20 | 76.79 | 79.58 | 145.95 |
| 54 | -5.30 | 78.77 | 82.63 | 154.36 |
| 55 | -5.40 | 80.78 | 85.74 | 163.09 |
| 56 | -5.50 | 82.80 | 88.90 | 172.14 |
| 57 | -5.60 | 84.84 | 92.12 | 181.51 |
| 58 | -5.70 | 86.89 | 95.40 | 191.22 |
| 59 | -5.80 | 88.97 | 98.77 | 201.27 |
| 60 | -5.90 | 91.07 | 102.30 | 211.67 |
| 61 | -6.00 | 93.18 | 106.00 | 222.45 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 62 | -6.10 | 95.32 | 109.88 | 233.61 |
| 63 | -6.20 | 97.47 | 113.89 | 245.17 |
| 64 | -6.30 | 99.65 | 117.99 | 257.15 |
| 65 | -6.40 | 101.84 | 122.17 | 269.54 |
| 66 | -6.50 | 104.05 | 126.43 | 282.37 |

Combinazione n° 12 - SLEQ

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.03 | 0.00 |
| 3 | -0.20 | 2.00 | 0.12 | 0.02 |
| 4 | -0.30 | 3.03 | 0.26 | 0.04 |
| 5 | -0.40 | 4.08 | 0.46 | 0.09 |
| 6 | -0.50 | 5.14 | 0.71 | 0.17 |
| 7 | -0.60 | 6.23 | 1.03 | 0.28 |
| 8 | -0.70 | 7.33 | 1.40 | 0.42 |
| 9 | -0.80 | 8.46 | 1.85 | 0.62 |
| 10 | -0.90 | 9.60 | 2.36 | 0.86 |
| 11 | -1.00 | 10.76 | 2.95 | 1.17 |
| 12 | -1.10 | 11.94 | 3.59 | 1.54 |
| 13 | -1.20 | 13.14 | 4.30 | 1.98 |
| 14 | -1.30 | 14.36 | 5.07 | 2.50 |
| 15 | -1.40 | 15.60 | 5.90 | 3.11 |
| 16 | -1.50 | 16.86 | 6.78 | 3.81 |
| 17 | -1.60 | 18.13 | 7.72 | 4.60 |
| 18 | -1.70 | 19.43 | 8.72 | 5.49 |
| 19 | -1.80 | 20.74 | 9.78 | 6.50 |
| 20 | -1.90 | 22.08 | 10.89 | 7.61 |
| 21 | -2.00 | 23.43 | 12.06 | 8.85 |
| 22 | -2.10 | 24.80 | 13.28 | 10.21 |
| 23 | -2.20 | 26.19 | 14.57 | 11.70 |
| 24 | -2.30 | 27.60 | 15.91 | 13.33 |
| 25 | -2.40 | 29.03 | 17.31 | 15.10 |
| 26 | -2.50 | 30.48 | 18.76 | 17.02 |
| 27 | -2.60 | 31.95 | 20.27 | 19.09 |
| 28 | -2.70 | 33.43 | 21.84 | 21.32 |
| 29 | -2.80 | 34.94 | 23.47 | 23.72 |
| 30 | -2.90 | 36.46 | 25.15 | 26.29 |
| 31 | -3.00 | 38.01 | 26.89 | 29.04 |
| 32 | -3.10 | 39.57 | 28.69 | 31.97 |
| 33 | -3.20 | 41.15 | 30.54 | 35.08 |
| 34 | -3.30 | 42.75 | 32.45 | 38.40 |
| 35 | -3.40 | 44.37 | 34.42 | 41.91 |
| 36 | -3.50 | 46.01 | 36.44 | 45.63 |
| 37 | -3.60 | 47.67 | 38.53 | 49.56 |
| 38 | -3.70 | 49.35 | 40.66 | 53.70 |
| 39 | -3.80 | 51.04 | 42.86 | 58.08 |
| 40 | -3.90 | 52.76 | 45.11 | 62.68 |
| 41 | -4.00 | 54.49 | 47.42 | 67.51 |
| 42 | -4.10 | 56.24 | 49.79 | 72.59 |
| 43 | -4.20 | 58.02 | 52.21 | 77.91 |
| 44 | -4.30 | 59.81 | 54.69 | 83.48 |
| 45 | -4.40 | 61.62 | 57.23 | 89.31 |
| 46 | -4.50 | 63.45 | 59.82 | 95.41 |
| 47 | -4.60 | 65.30 | 62.48 | 101.77 |
| 48 | -4.70 | 67.17 | 65.18 | 108.41 |
| 49 | -4.80 | 69.05 | 67.95 | 115.34 |
| 50 | -4.90 | 70.96 | 70.77 | 122.54 |
| 51 | -5.00 | 72.88 | 73.65 | 130.04 |
| 52 | -5.10 | 74.83 | 76.59 | 137.84 |
| 53 | -5.20 | 76.79 | 79.58 | 145.95 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 54 | -5.30 | 78.77 | 82.63 | 154.36 |
| 55 | -5.40 | 80.78 | 85.74 | 163.09 |
| 56 | -5.50 | 82.80 | 88.90 | 172.14 |
| 57 | -5.60 | 84.84 | 92.12 | 181.51 |
| 58 | -5.70 | 86.89 | 95.40 | 191.22 |
| 59 | -5.80 | 88.97 | 98.77 | 201.27 |
| 60 | -5.90 | 91.07 | 102.30 | 211.67 |
| 61 | -6.00 | 93.18 | 106.00 | 222.45 |
| 62 | -6.10 | 95.32 | 109.88 | 233.61 |
| 63 | -6.20 | 97.47 | 113.89 | 245.17 |
| 64 | -6.30 | 99.65 | 117.99 | 257.15 |
| 65 | -6.40 | 101.84 | 122.17 | 269.54 |
| 66 | -6.50 | 104.05 | 126.43 | 282.37 |

Combinazione n° 13 - SLEQ H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.11 | 0.01 |
| 3 | -0.20 | 2.00 | 0.29 | 0.03 |
| 4 | -0.30 | 3.03 | 0.55 | 0.08 |
| 5 | -0.40 | 4.08 | 0.87 | 0.17 |
| 6 | -0.50 | 5.14 | 1.26 | 0.29 |
| 7 | -0.60 | 6.23 | 1.73 | 0.46 |
| 8 | -0.70 | 7.33 | 2.27 | 0.69 |
| 9 | -0.80 | 8.46 | 2.90 | 0.98 |
| 10 | -0.90 | 9.60 | 3.61 | 1.34 |
| 11 | -1.00 | 10.76 | 4.40 | 1.78 |
| 12 | -1.10 | 11.94 | 5.28 | 2.30 |
| 13 | -1.20 | 13.14 | 6.23 | 2.93 |
| 14 | -1.30 | 14.36 | 7.25 | 3.65 |
| 15 | -1.40 | 15.60 | 8.34 | 4.49 |
| 16 | -1.50 | 16.86 | 9.50 | 5.45 |
| 17 | -1.60 | 18.13 | 10.74 | 6.53 |
| 18 | -1.70 | 19.43 | 12.05 | 7.74 |
| 19 | -1.80 | 20.74 | 13.43 | 9.09 |
| 20 | -1.90 | 22.08 | 14.88 | 10.59 |
| 21 | -2.00 | 23.43 | 16.40 | 12.24 |
| 22 | -2.10 | 24.80 | 18.00 | 14.05 |
| 23 | -2.20 | 26.19 | 19.66 | 16.03 |
| 24 | -2.30 | 27.60 | 21.40 | 18.19 |
| 25 | -2.40 | 29.03 | 23.21 | 20.53 |
| 26 | -2.50 | 30.48 | 25.09 | 23.06 |
| 27 | -2.60 | 31.95 | 27.04 | 25.79 |
| 28 | -2.70 | 33.43 | 29.06 | 28.72 |
| 29 | -2.80 | 34.94 | 31.16 | 31.87 |
| 30 | -2.90 | 36.46 | 33.32 | 35.23 |
| 31 | -3.00 | 38.01 | 35.56 | 38.82 |
| 32 | -3.10 | 39.57 | 37.87 | 42.64 |
| 33 | -3.20 | 41.15 | 40.24 | 46.70 |
| 34 | -3.30 | 42.75 | 42.69 | 51.01 |
| 35 | -3.40 | 44.37 | 45.22 | 55.57 |
| 36 | -3.50 | 46.01 | 47.81 | 60.40 |
| 37 | -3.60 | 47.67 | 50.47 | 65.50 |
| 38 | -3.70 | 49.35 | 53.21 | 70.87 |
| 39 | -3.80 | 51.04 | 56.02 | 76.52 |
| 40 | -3.90 | 52.76 | 58.89 | 82.47 |
| 41 | -4.00 | 54.49 | 61.84 | 88.72 |
| 42 | -4.10 | 56.24 | 64.86 | 95.27 |
| 43 | -4.20 | 58.02 | 67.95 | 102.13 |
| 44 | -4.30 | 59.81 | 71.12 | 109.31 |
| 45 | -4.40 | 61.62 | 74.35 | 116.82 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 46 | -4.50 | 63.45 | 77.66 | 124.66 |
| 47 | -4.60 | 65.30 | 81.03 | 132.85 |
| 48 | -4.70 | 67.17 | 84.48 | 141.38 |
| 49 | -4.80 | 69.05 | 88.00 | 150.27 |
| 50 | -4.90 | 70.96 | 91.59 | 159.52 |
| 51 | -5.00 | 72.88 | 95.26 | 169.14 |
| 52 | -5.10 | 74.83 | 98.99 | 179.14 |
| 53 | -5.20 | 76.79 | 102.79 | 189.52 |
| 54 | -5.30 | 78.77 | 106.67 | 200.30 |
| 55 | -5.40 | 80.78 | 110.62 | 211.47 |
| 56 | -5.50 | 82.80 | 114.63 | 223.05 |
| 57 | -5.60 | 84.84 | 118.72 | 235.05 |
| 58 | -5.70 | 86.89 | 122.89 | 247.46 |
| 59 | -5.80 | 88.97 | 127.16 | 260.30 |
| 60 | -5.90 | 91.07 | 131.60 | 273.59 |
| 61 | -6.00 | 93.18 | 136.22 | 287.34 |
| 62 | -6.10 | 95.32 | 141.04 | 301.57 |
| 63 | -6.20 | 97.47 | 146.01 | 316.29 |
| 64 | -6.30 | 99.65 | 151.08 | 331.53 |
| 65 | -6.40 | 101.84 | 156.24 | 347.29 |
| 66 | -6.50 | 104.05 | 161.50 | 363.57 |

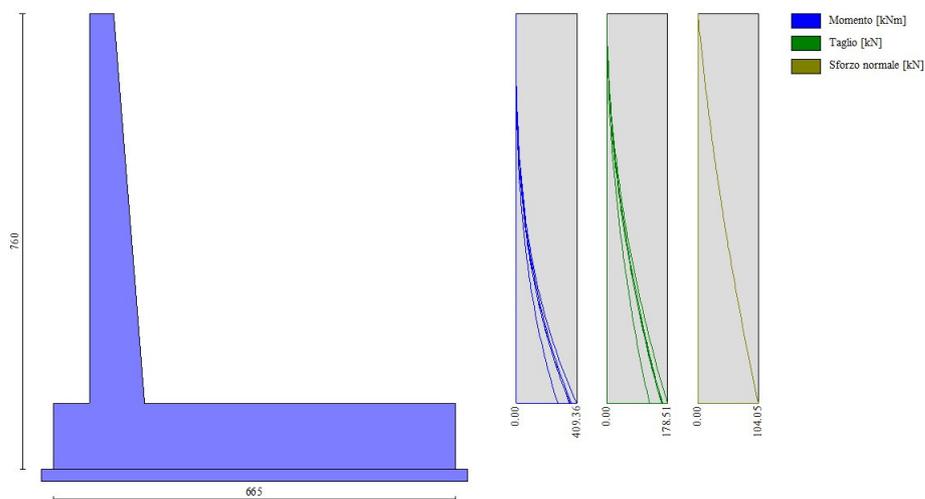


Fig. 8 - Paramento (Inviluppo)

Fondazione

Combinazione n° 1 - STR (A1-M1-R3)

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
|----|----------|-----------|-----------|------------|

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 19.37 | 0.97 |
| 3 | -0.80 | 0.00 | 38.53 | 3.87 |
| 4 | -0.70 | 0.00 | 57.49 | 8.67 |
| 5 | -0.60 | 0.00 | 76.24 | 15.36 |
| 6 | -0.50 | 0.00 | 94.78 | 23.91 |
| 7 | -0.40 | 0.00 | 113.12 | 34.31 |
| 8 | 0.51 | 0.00 | -324.94 | -1068.78 |
| 9 | 0.60 | 0.00 | -324.85 | -1039.26 |
| 10 | 0.70 | 0.00 | -324.55 | -1009.76 |
| 11 | 0.80 | 0.00 | -324.05 | -980.30 |
| 12 | 0.90 | 0.00 | -323.35 | -950.90 |
| 13 | 1.00 | 0.00 | -322.45 | -921.57 |
| 14 | 1.10 | 0.00 | -321.35 | -892.35 |
| 15 | 1.20 | 0.00 | -320.05 | -863.24 |
| 16 | 1.30 | 0.00 | -318.54 | -834.28 |
| 17 | 1.40 | 0.00 | -316.83 | -805.47 |
| 18 | 1.49 | 0.00 | -314.93 | -776.84 |
| 19 | 1.59 | 0.00 | -312.81 | -748.41 |
| 20 | 1.69 | 0.00 | -310.50 | -720.20 |
| 21 | 1.79 | 0.00 | -307.99 | -692.23 |
| 22 | 1.89 | 0.00 | -305.27 | -664.52 |
| 23 | 1.99 | 0.00 | -302.35 | -637.08 |
| 24 | 2.09 | 0.00 | -299.23 | -609.94 |
| 25 | 2.19 | 0.00 | -295.91 | -583.12 |
| 26 | 2.29 | 0.00 | -292.39 | -556.64 |
| 27 | 2.38 | 0.00 | -288.66 | -530.52 |
| 28 | 2.48 | 0.00 | -284.73 | -504.78 |
| 29 | 2.58 | 0.00 | -280.61 | -479.43 |
| 30 | 2.68 | 0.00 | -276.27 | -454.50 |
| 31 | 2.78 | 0.00 | -271.74 | -430.01 |
| 32 | 2.88 | 0.00 | -267.01 | -405.98 |
| 33 | 2.98 | 0.00 | -262.07 | -382.43 |
| 34 | 3.08 | 0.00 | -256.93 | -359.37 |
| 35 | 3.17 | 0.00 | -251.60 | -336.83 |
| 36 | 3.27 | 0.00 | -246.05 | -314.83 |
| 37 | 3.37 | 0.00 | -240.31 | -293.39 |
| 38 | 3.47 | 0.00 | -234.37 | -272.53 |
| 39 | 3.57 | 0.00 | -228.22 | -252.26 |
| 40 | 3.67 | 0.00 | -221.87 | -232.61 |
| 41 | 3.77 | 0.00 | -213.49 | -211.88 |
| 42 | 3.87 | 0.00 | -204.07 | -191.24 |
| 43 | 3.97 | 0.00 | -194.45 | -171.54 |
| 44 | 4.06 | 0.00 | -184.63 | -152.80 |
| 45 | 4.16 | 0.00 | -174.60 | -135.05 |
| 46 | 4.26 | 0.00 | -164.37 | -118.29 |
| 47 | 4.36 | 0.00 | -153.94 | -102.56 |
| 48 | 4.46 | 0.00 | -143.31 | -87.87 |
| 49 | 4.56 | 0.00 | -132.48 | -74.23 |
| 50 | 4.66 | 0.00 | -121.44 | -61.68 |
| 51 | 4.76 | 0.00 | -110.21 | -50.23 |
| 52 | 4.86 | 0.00 | -98.77 | -39.90 |
| 53 | 4.95 | 0.00 | -87.13 | -30.71 |
| 54 | 5.05 | 0.00 | -75.29 | -22.68 |
| 55 | 5.15 | 0.00 | -63.24 | -15.84 |
| 56 | 5.25 | 0.00 | -51.00 | -10.19 |
| 57 | 5.35 | 0.00 | -38.55 | -5.76 |
| 58 | 5.45 | 0.00 | -25.90 | -2.57 |
| 59 | 5.55 | 0.00 | -13.05 | -0.65 |
| 60 | 5.65 | 0.00 | 0.00 | 0.00 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 23.80 | 1.19 |
| 3 | -0.80 | 0.00 | 47.26 | 4.75 |
| 4 | -0.70 | 0.00 | 70.39 | 10.63 |
| 5 | -0.60 | 0.00 | 93.18 | 18.82 |
| 6 | -0.50 | 0.00 | 115.64 | 29.26 |
| 7 | -0.40 | 0.00 | 137.76 | 41.93 |
| 8 | 0.51 | 0.00 | -124.75 | -700.79 |
| 9 | 0.60 | 0.00 | -130.87 | -688.54 |
| 10 | 0.70 | 0.00 | -136.67 | -675.70 |
| 11 | 0.80 | 0.00 | -142.13 | -662.30 |
| 12 | 0.90 | 0.00 | -147.27 | -648.38 |
| 13 | 1.00 | 0.00 | -152.07 | -633.97 |
| 14 | 1.10 | 0.00 | -156.55 | -619.09 |
| 15 | 1.20 | 0.00 | -160.71 | -603.80 |
| 16 | 1.30 | 0.00 | -164.53 | -588.10 |
| 17 | 1.40 | 0.00 | -168.02 | -572.05 |
| 18 | 1.49 | 0.00 | -171.19 | -555.67 |
| 19 | 1.59 | 0.00 | -174.03 | -538.99 |
| 20 | 1.69 | 0.00 | -176.54 | -522.04 |
| 21 | 1.79 | 0.00 | -178.72 | -504.87 |
| 22 | 1.89 | 0.00 | -180.57 | -487.49 |
| 23 | 1.99 | 0.00 | -182.10 | -469.95 |
| 24 | 2.09 | 0.00 | -183.30 | -452.27 |
| 25 | 2.19 | 0.00 | -184.16 | -434.49 |
| 26 | 2.29 | 0.00 | -184.71 | -416.64 |
| 27 | 2.38 | 0.00 | -184.92 | -398.76 |
| 28 | 2.48 | 0.00 | -184.80 | -380.87 |
| 29 | 2.58 | 0.00 | -184.36 | -363.01 |
| 30 | 2.68 | 0.00 | -183.59 | -345.20 |
| 31 | 2.78 | 0.00 | -182.48 | -327.49 |
| 32 | 2.88 | 0.00 | -181.06 | -309.91 |
| 33 | 2.98 | 0.00 | -179.30 | -292.48 |
| 34 | 3.08 | 0.00 | -177.21 | -275.24 |
| 35 | 3.17 | 0.00 | -174.80 | -258.23 |
| 36 | 3.27 | 0.00 | -172.06 | -241.46 |
| 37 | 3.37 | 0.00 | -168.99 | -224.99 |
| 38 | 3.47 | 0.00 | -165.59 | -208.84 |
| 39 | 3.57 | 0.00 | -161.86 | -193.04 |
| 40 | 3.67 | 0.00 | -157.81 | -177.62 |
| 41 | 3.77 | 0.00 | -153.15 | -162.36 |
| 42 | 3.87 | 0.00 | -148.05 | -147.47 |
| 43 | 3.97 | 0.00 | -142.61 | -133.11 |
| 44 | 4.06 | 0.00 | -136.85 | -119.29 |
| 45 | 4.16 | 0.00 | -130.76 | -106.06 |
| 46 | 4.26 | 0.00 | -124.34 | -93.45 |
| 47 | 4.36 | 0.00 | -117.59 | -81.49 |
| 48 | 4.46 | 0.00 | -110.52 | -70.22 |
| 49 | 4.56 | 0.00 | -103.11 | -59.66 |
| 50 | 4.66 | 0.00 | -95.38 | -49.84 |
| 51 | 4.76 | 0.00 | -87.32 | -40.81 |
| 52 | 4.86 | 0.00 | -78.93 | -32.59 |
| 53 | 4.95 | 0.00 | -70.21 | -25.22 |
| 54 | 5.05 | 0.00 | -61.17 | -18.72 |
| 55 | 5.15 | 0.00 | -51.79 | -13.14 |
| 56 | 5.25 | 0.00 | -42.09 | -8.49 |
| 57 | 5.35 | 0.00 | -32.06 | -4.83 |
| 58 | 5.45 | 0.00 | -21.70 | -2.17 |
| 59 | 5.55 | 0.00 | -11.01 | -0.55 |
| 60 | 5.65 | 0.00 | 0.00 | 0.00 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 21.54 | 1.08 |
| 3 | -0.80 | 0.00 | 42.75 | 4.30 |
| 4 | -0.70 | 0.00 | 63.64 | 9.62 |
| 5 | -0.60 | 0.00 | 84.20 | 17.01 |
| 6 | -0.50 | 0.00 | 104.44 | 26.45 |
| 7 | -0.40 | 0.00 | 124.36 | 37.89 |
| 8 | 0.51 | 0.00 | -217.44 | -926.10 |
| 9 | 0.60 | 0.00 | -221.49 | -904.79 |
| 10 | 0.70 | 0.00 | -225.23 | -883.10 |
| 11 | 0.80 | 0.00 | -228.65 | -861.05 |
| 12 | 0.90 | 0.00 | -231.75 | -838.67 |
| 13 | 1.00 | 0.00 | -234.54 | -816.01 |
| 14 | 1.10 | 0.00 | -237.01 | -793.09 |
| 15 | 1.20 | 0.00 | -239.16 | -769.94 |
| 16 | 1.30 | 0.00 | -241.00 | -746.59 |
| 17 | 1.40 | 0.00 | -242.51 | -723.07 |
| 18 | 1.49 | 0.00 | -243.71 | -699.42 |
| 19 | 1.59 | 0.00 | -244.60 | -675.67 |
| 20 | 1.69 | 0.00 | -245.16 | -651.85 |
| 21 | 1.79 | 0.00 | -245.41 | -627.98 |
| 22 | 1.89 | 0.00 | -245.35 | -604.11 |
| 23 | 1.99 | 0.00 | -244.96 | -580.26 |
| 24 | 2.09 | 0.00 | -244.26 | -556.46 |
| 25 | 2.19 | 0.00 | -243.24 | -532.75 |
| 26 | 2.29 | 0.00 | -241.90 | -509.16 |
| 27 | 2.38 | 0.00 | -240.25 | -485.71 |
| 28 | 2.48 | 0.00 | -238.28 | -462.44 |
| 29 | 2.58 | 0.00 | -235.99 | -439.38 |
| 30 | 2.68 | 0.00 | -233.39 | -416.57 |
| 31 | 2.78 | 0.00 | -230.46 | -394.03 |
| 32 | 2.88 | 0.00 | -227.23 | -371.79 |
| 33 | 2.98 | 0.00 | -223.67 | -349.88 |
| 34 | 3.08 | 0.00 | -219.80 | -328.35 |
| 35 | 3.17 | 0.00 | -215.61 | -307.21 |
| 36 | 3.27 | 0.00 | -211.10 | -286.51 |
| 37 | 3.37 | 0.00 | -206.27 | -266.26 |
| 38 | 3.47 | 0.00 | -201.13 | -246.51 |
| 39 | 3.57 | 0.00 | -195.67 | -227.28 |
| 40 | 3.67 | 0.00 | -189.90 | -208.60 |
| 41 | 3.77 | 0.00 | -183.53 | -190.26 |
| 42 | 3.87 | 0.00 | -176.73 | -172.45 |
| 43 | 3.97 | 0.00 | -169.60 | -155.33 |
| 44 | 4.06 | 0.00 | -162.17 | -138.93 |
| 45 | 4.16 | 0.00 | -154.41 | -123.29 |
| 46 | 4.26 | 0.00 | -146.33 | -108.42 |
| 47 | 4.36 | 0.00 | -137.94 | -94.37 |
| 48 | 4.46 | 0.00 | -129.23 | -81.16 |
| 49 | 4.56 | 0.00 | -120.21 | -68.83 |
| 50 | 4.66 | 0.00 | -110.87 | -57.41 |
| 51 | 4.76 | 0.00 | -101.21 | -46.92 |
| 52 | 4.86 | 0.00 | -91.23 | -37.41 |
| 53 | 4.95 | 0.00 | -80.94 | -28.90 |
| 54 | 5.05 | 0.00 | -70.33 | -21.42 |
| 55 | 5.15 | 0.00 | -59.40 | -15.00 |
| 56 | 5.25 | 0.00 | -48.15 | -9.69 |
| 57 | 5.35 | 0.00 | -36.59 | -5.50 |
| 58 | 5.45 | 0.00 | -24.71 | -2.46 |
| 59 | 5.55 | 0.00 | -12.51 | -0.62 |
| 60 | 5.65 | 0.00 | 0.00 | 0.00 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 16.93 | 0.85 |
| 3 | -0.80 | 0.00 | 33.71 | 3.38 |
| 4 | -0.70 | 0.00 | 50.35 | 7.58 |
| 5 | -0.60 | 0.00 | 66.86 | 13.45 |
| 6 | -0.50 | 0.00 | 83.22 | 20.95 |
| 7 | -0.40 | 0.00 | 99.44 | 30.09 |
| 8 | 0.51 | 0.00 | -104.70 | -428.05 |
| 9 | 0.60 | 0.00 | -106.94 | -419.51 |
| 10 | 0.70 | 0.00 | -109.04 | -410.76 |
| 11 | 0.80 | 0.00 | -111.00 | -401.81 |
| 12 | 0.90 | 0.00 | -112.82 | -392.67 |
| 13 | 1.00 | 0.00 | -114.50 | -383.36 |
| 14 | 1.10 | 0.00 | -116.05 | -373.88 |
| 15 | 1.20 | 0.00 | -117.46 | -364.27 |
| 16 | 1.30 | 0.00 | -118.74 | -354.51 |
| 17 | 1.40 | 0.00 | -119.87 | -344.64 |
| 18 | 1.49 | 0.00 | -120.87 | -334.67 |
| 19 | 1.59 | 0.00 | -121.74 | -324.60 |
| 20 | 1.69 | 0.00 | -122.46 | -314.45 |
| 21 | 1.79 | 0.00 | -123.05 | -304.24 |
| 22 | 1.89 | 0.00 | -123.50 | -293.98 |
| 23 | 1.99 | 0.00 | -123.81 | -283.68 |
| 24 | 2.09 | 0.00 | -123.99 | -273.35 |
| 25 | 2.19 | 0.00 | -124.03 | -263.02 |
| 26 | 2.29 | 0.00 | -123.93 | -252.68 |
| 27 | 2.38 | 0.00 | -123.69 | -242.37 |
| 28 | 2.48 | 0.00 | -123.32 | -232.08 |
| 29 | 2.58 | 0.00 | -122.81 | -221.84 |
| 30 | 2.68 | 0.00 | -122.16 | -211.65 |
| 31 | 2.78 | 0.00 | -121.38 | -201.54 |
| 32 | 2.88 | 0.00 | -120.46 | -191.51 |
| 33 | 2.98 | 0.00 | -119.40 | -181.58 |
| 34 | 3.08 | 0.00 | -118.20 | -171.76 |
| 35 | 3.17 | 0.00 | -116.87 | -162.06 |
| 36 | 3.27 | 0.00 | -115.40 | -152.51 |
| 37 | 3.37 | 0.00 | -113.79 | -143.10 |
| 38 | 3.47 | 0.00 | -112.04 | -133.86 |
| 39 | 3.57 | 0.00 | -110.16 | -124.80 |
| 40 | 3.67 | 0.00 | -108.14 | -115.94 |
| 41 | 3.77 | 0.00 | -104.63 | -106.00 |
| 42 | 3.87 | 0.00 | -100.35 | -95.87 |
| 43 | 3.97 | 0.00 | -95.95 | -86.17 |
| 44 | 4.06 | 0.00 | -91.40 | -76.91 |
| 45 | 4.16 | 0.00 | -86.72 | -68.10 |
| 46 | 4.26 | 0.00 | -81.90 | -59.77 |
| 47 | 4.36 | 0.00 | -76.94 | -51.92 |
| 48 | 4.46 | 0.00 | -71.84 | -44.56 |
| 49 | 4.56 | 0.00 | -66.61 | -37.72 |
| 50 | 4.66 | 0.00 | -61.24 | -31.40 |
| 51 | 4.76 | 0.00 | -55.74 | -25.62 |
| 52 | 4.86 | 0.00 | -50.09 | -20.38 |
| 53 | 4.95 | 0.00 | -44.31 | -15.72 |
| 54 | 5.05 | 0.00 | -38.39 | -11.63 |
| 55 | 5.15 | 0.00 | -32.34 | -8.13 |
| 56 | 5.25 | 0.00 | -26.14 | -5.24 |
| 57 | 5.35 | 0.00 | -19.81 | -2.97 |
| 58 | 5.45 | 0.00 | -13.35 | -1.33 |
| 59 | 5.55 | 0.00 | -6.74 | -0.33 |
| 60 | 5.65 | 0.00 | 0.00 | 0.00 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 16.93 | 0.85 |
| 3 | -0.80 | 0.00 | 33.71 | 3.38 |
| 4 | -0.70 | 0.00 | 50.35 | 7.58 |
| 5 | -0.60 | 0.00 | 66.86 | 13.45 |
| 6 | -0.50 | 0.00 | 83.22 | 20.95 |
| 7 | -0.40 | 0.00 | 99.44 | 30.09 |
| 8 | 0.51 | 0.00 | -104.70 | -428.05 |
| 9 | 0.60 | 0.00 | -106.94 | -419.51 |
| 10 | 0.70 | 0.00 | -109.04 | -410.76 |
| 11 | 0.80 | 0.00 | -111.00 | -401.81 |
| 12 | 0.90 | 0.00 | -112.82 | -392.67 |
| 13 | 1.00 | 0.00 | -114.50 | -383.36 |
| 14 | 1.10 | 0.00 | -116.05 | -373.88 |
| 15 | 1.20 | 0.00 | -117.46 | -364.27 |
| 16 | 1.30 | 0.00 | -118.74 | -354.51 |
| 17 | 1.40 | 0.00 | -119.87 | -344.64 |
| 18 | 1.49 | 0.00 | -120.87 | -334.67 |
| 19 | 1.59 | 0.00 | -121.74 | -324.60 |
| 20 | 1.69 | 0.00 | -122.46 | -314.45 |
| 21 | 1.79 | 0.00 | -123.05 | -304.24 |
| 22 | 1.89 | 0.00 | -123.50 | -293.98 |
| 23 | 1.99 | 0.00 | -123.81 | -283.68 |
| 24 | 2.09 | 0.00 | -123.99 | -273.35 |
| 25 | 2.19 | 0.00 | -124.03 | -263.02 |
| 26 | 2.29 | 0.00 | -123.93 | -252.68 |
| 27 | 2.38 | 0.00 | -123.69 | -242.37 |
| 28 | 2.48 | 0.00 | -123.32 | -232.08 |
| 29 | 2.58 | 0.00 | -122.81 | -221.84 |
| 30 | 2.68 | 0.00 | -122.16 | -211.65 |
| 31 | 2.78 | 0.00 | -121.38 | -201.54 |
| 32 | 2.88 | 0.00 | -120.46 | -191.51 |
| 33 | 2.98 | 0.00 | -119.40 | -181.58 |
| 34 | 3.08 | 0.00 | -118.20 | -171.76 |
| 35 | 3.17 | 0.00 | -116.87 | -162.06 |
| 36 | 3.27 | 0.00 | -115.40 | -152.51 |
| 37 | 3.37 | 0.00 | -113.79 | -143.10 |
| 38 | 3.47 | 0.00 | -112.04 | -133.86 |
| 39 | 3.57 | 0.00 | -110.16 | -124.80 |
| 40 | 3.67 | 0.00 | -108.14 | -115.94 |
| 41 | 3.77 | 0.00 | -104.63 | -106.00 |
| 42 | 3.87 | 0.00 | -100.35 | -95.87 |
| 43 | 3.97 | 0.00 | -95.95 | -86.17 |
| 44 | 4.06 | 0.00 | -91.40 | -76.91 |
| 45 | 4.16 | 0.00 | -86.72 | -68.10 |
| 46 | 4.26 | 0.00 | -81.90 | -59.77 |
| 47 | 4.36 | 0.00 | -76.94 | -51.92 |
| 48 | 4.46 | 0.00 | -71.84 | -44.56 |
| 49 | 4.56 | 0.00 | -66.61 | -37.72 |
| 50 | 4.66 | 0.00 | -61.24 | -31.40 |
| 51 | 4.76 | 0.00 | -55.74 | -25.62 |
| 52 | 4.86 | 0.00 | -50.09 | -20.38 |
| 53 | 4.95 | 0.00 | -44.31 | -15.72 |
| 54 | 5.05 | 0.00 | -38.39 | -11.63 |
| 55 | 5.15 | 0.00 | -32.34 | -8.13 |
| 56 | 5.25 | 0.00 | -26.14 | -5.24 |
| 57 | 5.35 | 0.00 | -19.81 | -2.97 |
| 58 | 5.45 | 0.00 | -13.35 | -1.33 |
| 59 | 5.55 | 0.00 | -6.74 | -0.33 |
| 60 | 5.65 | 0.00 | 0.00 | 0.00 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 16.93 | 0.85 |
| 3 | -0.80 | 0.00 | 33.71 | 3.38 |
| 4 | -0.70 | 0.00 | 50.35 | 7.58 |
| 5 | -0.60 | 0.00 | 66.86 | 13.45 |
| 6 | -0.50 | 0.00 | 83.22 | 20.95 |
| 7 | -0.40 | 0.00 | 99.44 | 30.09 |
| 8 | 0.51 | 0.00 | -104.70 | -428.05 |
| 9 | 0.60 | 0.00 | -106.94 | -419.51 |
| 10 | 0.70 | 0.00 | -109.04 | -410.76 |
| 11 | 0.80 | 0.00 | -111.00 | -401.81 |
| 12 | 0.90 | 0.00 | -112.82 | -392.67 |
| 13 | 1.00 | 0.00 | -114.50 | -383.36 |
| 14 | 1.10 | 0.00 | -116.05 | -373.88 |
| 15 | 1.20 | 0.00 | -117.46 | -364.27 |
| 16 | 1.30 | 0.00 | -118.74 | -354.51 |
| 17 | 1.40 | 0.00 | -119.87 | -344.64 |
| 18 | 1.49 | 0.00 | -120.87 | -334.67 |
| 19 | 1.59 | 0.00 | -121.74 | -324.60 |
| 20 | 1.69 | 0.00 | -122.46 | -314.45 |
| 21 | 1.79 | 0.00 | -123.05 | -304.24 |
| 22 | 1.89 | 0.00 | -123.50 | -293.98 |
| 23 | 1.99 | 0.00 | -123.81 | -283.68 |
| 24 | 2.09 | 0.00 | -123.99 | -273.35 |
| 25 | 2.19 | 0.00 | -124.03 | -263.02 |
| 26 | 2.29 | 0.00 | -123.93 | -252.68 |
| 27 | 2.38 | 0.00 | -123.69 | -242.37 |
| 28 | 2.48 | 0.00 | -123.32 | -232.08 |
| 29 | 2.58 | 0.00 | -122.81 | -221.84 |
| 30 | 2.68 | 0.00 | -122.16 | -211.65 |
| 31 | 2.78 | 0.00 | -121.38 | -201.54 |
| 32 | 2.88 | 0.00 | -120.46 | -191.51 |
| 33 | 2.98 | 0.00 | -119.40 | -181.58 |
| 34 | 3.08 | 0.00 | -118.20 | -171.76 |
| 35 | 3.17 | 0.00 | -116.87 | -162.06 |
| 36 | 3.27 | 0.00 | -115.40 | -152.51 |
| 37 | 3.37 | 0.00 | -113.79 | -143.10 |
| 38 | 3.47 | 0.00 | -112.04 | -133.86 |
| 39 | 3.57 | 0.00 | -110.16 | -124.80 |
| 40 | 3.67 | 0.00 | -108.14 | -115.94 |
| 41 | 3.77 | 0.00 | -104.63 | -106.00 |
| 42 | 3.87 | 0.00 | -100.35 | -95.87 |
| 43 | 3.97 | 0.00 | -95.95 | -86.17 |
| 44 | 4.06 | 0.00 | -91.40 | -76.91 |
| 45 | 4.16 | 0.00 | -86.72 | -68.10 |
| 46 | 4.26 | 0.00 | -81.90 | -59.77 |
| 47 | 4.36 | 0.00 | -76.94 | -51.92 |
| 48 | 4.46 | 0.00 | -71.84 | -44.56 |
| 49 | 4.56 | 0.00 | -66.61 | -37.72 |
| 50 | 4.66 | 0.00 | -61.24 | -31.40 |
| 51 | 4.76 | 0.00 | -55.74 | -25.62 |
| 52 | 4.86 | 0.00 | -50.09 | -20.38 |
| 53 | 4.95 | 0.00 | -44.31 | -15.72 |
| 54 | 5.05 | 0.00 | -38.39 | -11.63 |
| 55 | 5.15 | 0.00 | -32.34 | -8.13 |
| 56 | 5.25 | 0.00 | -26.14 | -5.24 |
| 57 | 5.35 | 0.00 | -19.81 | -2.97 |
| 58 | 5.45 | 0.00 | -13.35 | -1.33 |
| 59 | 5.55 | 0.00 | -6.74 | -0.33 |
| 60 | 5.65 | 0.00 | 0.00 | 0.00 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 22.31 | 1.12 |
| 3 | -0.80 | 0.00 | 44.33 | 4.45 |
| 4 | -0.70 | 0.00 | 66.06 | 9.97 |
| 5 | -0.60 | 0.00 | 87.51 | 17.65 |
| 6 | -0.50 | 0.00 | 108.66 | 27.47 |
| 7 | -0.40 | 0.00 | 129.53 | 39.38 |
| 8 | 0.51 | 0.00 | -132.44 | -665.79 |
| 9 | 0.60 | 0.00 | -137.80 | -654.36 |
| 10 | 0.70 | 0.00 | -142.89 | -642.41 |
| 11 | 0.80 | 0.00 | -147.69 | -629.97 |
| 12 | 0.90 | 0.00 | -152.22 | -617.07 |
| 13 | 1.00 | 0.00 | -156.46 | -603.73 |
| 14 | 1.10 | 0.00 | -160.42 | -589.99 |
| 15 | 1.20 | 0.00 | -164.10 | -575.87 |
| 16 | 1.30 | 0.00 | -167.50 | -561.40 |
| 17 | 1.40 | 0.00 | -170.62 | -546.61 |
| 18 | 1.49 | 0.00 | -173.46 | -531.53 |
| 19 | 1.59 | 0.00 | -176.01 | -516.18 |
| 20 | 1.69 | 0.00 | -178.29 | -500.59 |
| 21 | 1.79 | 0.00 | -180.28 | -484.79 |
| 22 | 1.89 | 0.00 | -182.00 | -468.80 |
| 23 | 1.99 | 0.00 | -183.43 | -452.67 |
| 24 | 2.09 | 0.00 | -184.58 | -436.40 |
| 25 | 2.19 | 0.00 | -185.45 | -420.03 |
| 26 | 2.29 | 0.00 | -186.04 | -403.59 |
| 27 | 2.38 | 0.00 | -186.35 | -387.11 |
| 28 | 2.48 | 0.00 | -186.38 | -370.61 |
| 29 | 2.58 | 0.00 | -186.13 | -354.12 |
| 30 | 2.68 | 0.00 | -185.59 | -337.67 |
| 31 | 2.78 | 0.00 | -184.78 | -321.28 |
| 32 | 2.88 | 0.00 | -183.68 | -304.99 |
| 33 | 2.98 | 0.00 | -182.30 | -288.83 |
| 34 | 3.08 | 0.00 | -180.65 | -272.81 |
| 35 | 3.17 | 0.00 | -178.71 | -256.97 |
| 36 | 3.27 | 0.00 | -176.49 | -241.34 |
| 37 | 3.37 | 0.00 | -173.99 | -225.94 |
| 38 | 3.47 | 0.00 | -171.21 | -210.80 |
| 39 | 3.57 | 0.00 | -168.14 | -195.95 |
| 40 | 3.67 | 0.00 | -164.80 | -181.41 |
| 41 | 3.77 | 0.00 | -159.82 | -165.95 |
| 42 | 3.87 | 0.00 | -153.94 | -150.44 |
| 43 | 3.97 | 0.00 | -147.77 | -135.53 |
| 44 | 4.06 | 0.00 | -141.33 | -121.24 |
| 45 | 4.16 | 0.00 | -134.60 | -107.60 |
| 46 | 4.26 | 0.00 | -127.59 | -94.64 |
| 47 | 4.36 | 0.00 | -120.31 | -82.38 |
| 48 | 4.46 | 0.00 | -112.74 | -70.86 |
| 49 | 4.56 | 0.00 | -104.89 | -60.10 |
| 50 | 4.66 | 0.00 | -96.76 | -50.14 |
| 51 | 4.76 | 0.00 | -88.35 | -40.98 |
| 52 | 4.86 | 0.00 | -79.65 | -32.68 |
| 53 | 4.95 | 0.00 | -70.68 | -25.25 |
| 54 | 5.05 | 0.00 | -61.43 | -18.72 |
| 55 | 5.15 | 0.00 | -51.89 | -13.11 |
| 56 | 5.25 | 0.00 | -42.08 | -8.47 |
| 57 | 5.35 | 0.00 | -31.98 | -4.80 |
| 58 | 5.45 | 0.00 | -21.60 | -2.15 |
| 59 | 5.55 | 0.00 | -10.94 | -0.54 |
| 60 | 5.65 | 0.00 | 0.00 | 0.00 |

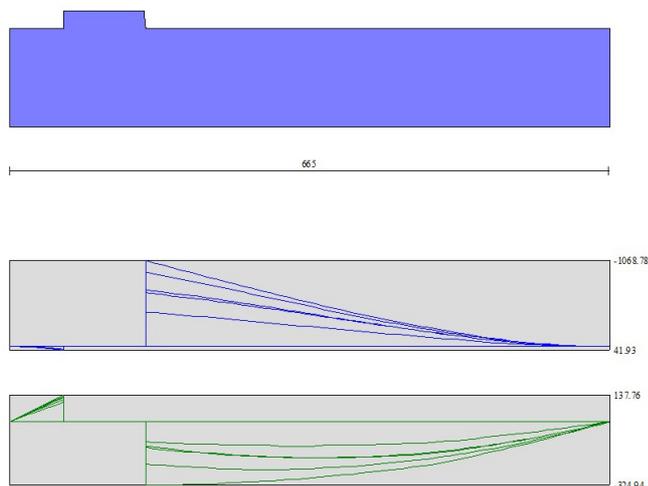


Fig. 9 - Fondazione (Inviluppo)

Verifiche strutturali

Verifiche a flessione

Elementi calcolati a trave

Simbologia adottata

| | |
|-----|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Afi | area ferri inferiori espresso in [cmq] |
| Afs | area ferri superiori espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| N | sforzo normale agente espressa in [kN] |
| Mu | momento ultimi espresso in [kNm] |
| Nu | sforzo normale ultimo espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione ultima e sollecitazione agente) |

Paramento

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
NM25 03 D 26 CL NV 24 05 001 A 92 di 314

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|-------|
| 60 | -5.90 | 100 | 86 | 26.55 | 53.09 | 273.93 | 91.07 | 1740.27 | 578.55 | 6.353 |
| 61 | -6.00 | 100 | 87 | 26.55 | 53.09 | 287.90 | 93.18 | 1754.55 | 567.90 | 6.094 |
| 62 | -6.10 | 100 | 87 | 26.55 | 53.09 | 302.37 | 95.32 | 1768.88 | 557.63 | 5.850 |
| 63 | -6.20 | 100 | 88 | 26.55 | 53.09 | 317.37 | 97.47 | 1783.27 | 547.70 | 5.619 |
| 64 | -6.30 | 100 | 89 | 26.55 | 53.09 | 332.91 | 99.65 | 1797.69 | 538.09 | 5.400 |
| 65 | -6.40 | 100 | 90 | 26.55 | 53.09 | 349.00 | 101.84 | 1812.16 | 528.80 | 5.192 |
| 66 | -6.50 | 100 | 91 | 26.55 | 53.09 | 365.65 | 104.05 | 1826.68 | 519.81 | 4.996 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | 0.00 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | -0.10 | 100 | 41 | 26.55 | 53.09 | 0.01 | 0.99 | 0.00 | 0.00 | 100000.000 |
| 3 | -0.20 | 100 | 42 | 26.55 | 53.09 | 0.04 | 2.00 | 189.30 | 8639.50 | 4320.783 |
| 4 | -0.30 | 100 | 42 | 26.55 | 53.09 | 0.11 | 3.03 | 295.04 | 8075.92 | 2667.168 |
| 5 | -0.40 | 100 | 43 | 26.55 | 53.09 | 0.22 | 4.08 | 401.14 | 7500.38 | 1840.421 |
| 6 | -0.50 | 100 | 44 | 26.55 | 53.09 | 0.37 | 5.14 | 502.90 | 6918.75 | 1345.561 |
| 7 | -0.60 | 100 | 45 | 26.55 | 53.09 | 0.59 | 6.23 | 598.24 | 6358.19 | 1020.982 |
| 8 | -0.70 | 100 | 45 | 26.55 | 53.09 | 0.86 | 7.33 | 686.55 | 5834.70 | 795.762 |
| 9 | -0.80 | 100 | 46 | 26.55 | 53.09 | 1.21 | 8.46 | 768.28 | 5355.38 | 633.322 |
| 10 | -0.90 | 100 | 47 | 26.55 | 53.09 | 1.65 | 9.60 | 845.37 | 4929.78 | 513.580 |
| 11 | -1.00 | 100 | 48 | 26.55 | 53.09 | 2.17 | 10.76 | 917.46 | 4547.67 | 422.614 |
| 12 | -1.10 | 100 | 49 | 26.55 | 53.09 | 2.80 | 11.94 | 986.60 | 4212.52 | 352.753 |
| 13 | -1.20 | 100 | 49 | 26.55 | 53.09 | 3.53 | 13.14 | 1051.32 | 3911.40 | 297.627 |
| 14 | -1.30 | 100 | 50 | 26.55 | 53.09 | 4.39 | 14.36 | 1113.25 | 3645.44 | 253.841 |
| 15 | -1.40 | 100 | 51 | 26.55 | 53.09 | 5.36 | 15.60 | 1172.93 | 3410.58 | 218.636 |
| 16 | -1.50 | 100 | 52 | 26.55 | 53.09 | 6.48 | 16.86 | 1206.58 | 3139.79 | 186.263 |
| 17 | -1.60 | 100 | 52 | 26.55 | 53.09 | 7.73 | 18.13 | 1225.32 | 2873.35 | 158.458 |
| 18 | -1.70 | 100 | 53 | 26.55 | 53.09 | 9.14 | 19.43 | 1236.93 | 2629.97 | 135.366 |
| 19 | -1.80 | 100 | 54 | 26.55 | 53.09 | 10.70 | 20.74 | 1248.51 | 2420.27 | 116.678 |
| 20 | -1.90 | 100 | 55 | 26.55 | 53.09 | 12.43 | 22.08 | 1255.77 | 2230.49 | 101.033 |
| 21 | -2.00 | 100 | 56 | 26.55 | 53.09 | 14.33 | 23.43 | 1265.38 | 2068.60 | 88.290 |
| 22 | -2.10 | 100 | 56 | 26.55 | 53.09 | 16.42 | 24.80 | 1271.17 | 1920.40 | 77.431 |
| 23 | -2.20 | 100 | 57 | 26.55 | 53.09 | 18.69 | 26.19 | 1277.79 | 1790.58 | 68.363 |
| 24 | -2.30 | 100 | 58 | 26.55 | 53.09 | 21.16 | 27.60 | 1286.30 | 1677.62 | 60.778 |
| 25 | -2.40 | 100 | 59 | 26.55 | 53.09 | 23.84 | 29.03 | 1294.48 | 1576.23 | 54.294 |
| 26 | -2.50 | 100 | 59 | 26.55 | 53.09 | 26.73 | 30.48 | 1300.56 | 1482.75 | 48.648 |
| 27 | -2.60 | 100 | 60 | 26.55 | 53.09 | 29.85 | 31.95 | 1308.60 | 1400.60 | 43.842 |
| 28 | -2.70 | 100 | 61 | 26.55 | 53.09 | 33.19 | 33.43 | 1317.78 | 1327.35 | 39.702 |
| 29 | -2.80 | 100 | 62 | 26.55 | 53.09 | 36.77 | 34.94 | 1327.95 | 1261.68 | 36.111 |
| 30 | -2.90 | 100 | 63 | 26.55 | 53.09 | 40.60 | 36.46 | 1339.07 | 1202.59 | 32.981 |
| 31 | -3.00 | 100 | 63 | 26.55 | 53.09 | 44.68 | 38.01 | 1347.29 | 1145.99 | 30.153 |
| 32 | -3.10 | 100 | 64 | 26.55 | 53.09 | 49.03 | 39.57 | 1355.09 | 1093.71 | 27.641 |
| 33 | -3.20 | 100 | 65 | 26.55 | 53.09 | 53.64 | 41.15 | 1363.79 | 1046.29 | 25.426 |
| 34 | -3.30 | 100 | 66 | 26.55 | 53.09 | 58.53 | 42.75 | 1373.29 | 1003.11 | 23.464 |
| 35 | -3.40 | 100 | 66 | 26.55 | 53.09 | 63.70 | 44.37 | 1383.50 | 963.64 | 21.718 |
| 36 | -3.50 | 100 | 67 | 26.55 | 53.09 | 69.17 | 46.01 | 1394.34 | 927.43 | 20.157 |
| 37 | -3.60 | 100 | 68 | 26.55 | 53.09 | 74.94 | 47.67 | 1405.76 | 894.13 | 18.757 |
| 38 | -3.70 | 100 | 69 | 26.55 | 53.09 | 81.03 | 49.35 | 1417.69 | 863.39 | 17.497 |
| 39 | -3.80 | 100 | 70 | 26.55 | 53.09 | 87.42 | 51.04 | 1430.10 | 834.95 | 16.358 |
| 40 | -3.90 | 100 | 70 | 26.55 | 53.09 | 94.15 | 52.76 | 1442.94 | 808.57 | 15.326 |
| 41 | -4.00 | 100 | 71 | 26.55 | 53.09 | 101.21 | 54.49 | 1455.40 | 783.62 | 14.381 |
| 42 | -4.10 | 100 | 72 | 26.55 | 53.09 | 108.60 | 56.24 | 1467.55 | 760.02 | 13.513 |
| 43 | -4.20 | 100 | 73 | 26.55 | 53.09 | 116.35 | 58.02 | 1479.96 | 737.95 | 12.720 |
| 44 | -4.30 | 100 | 73 | 26.55 | 53.09 | 124.46 | 59.81 | 1492.60 | 717.27 | 11.993 |
| 45 | -4.40 | 100 | 74 | 26.55 | 53.09 | 132.93 | 61.62 | 1505.47 | 697.86 | 11.325 |
| 46 | -4.50 | 100 | 75 | 26.55 | 53.09 | 141.77 | 63.45 | 1518.53 | 679.60 | 10.711 |
| 47 | -4.60 | 100 | 76 | 26.55 | 53.09 | 151.00 | 65.30 | 1531.78 | 662.40 | 10.144 |
| 48 | -4.70 | 100 | 77 | 26.55 | 53.09 | 160.62 | 67.17 | 1545.19 | 646.17 | 9.620 |
| 49 | -4.80 | 100 | 77 | 26.55 | 53.09 | 170.63 | 69.05 | 1558.76 | 630.83 | 9.135 |

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|-------|
| 50 | -4.90 | 100 | 78 | 26.55 | 53.09 | 181.05 | 70.96 | 1572.47 | 616.31 | 8.686 |
| 51 | -5.00 | 100 | 79 | 26.55 | 53.09 | 191.88 | 72.88 | 1586.32 | 602.56 | 8.267 |
| 52 | -5.10 | 100 | 80 | 26.55 | 53.09 | 203.13 | 74.83 | 1600.28 | 589.51 | 7.878 |
| 53 | -5.20 | 100 | 80 | 26.55 | 53.09 | 214.81 | 76.79 | 1614.36 | 577.11 | 7.515 |
| 54 | -5.30 | 100 | 81 | 26.55 | 53.09 | 226.93 | 78.77 | 1628.54 | 565.32 | 7.176 |
| 55 | -5.40 | 100 | 82 | 26.55 | 53.09 | 239.49 | 80.78 | 1642.82 | 554.08 | 6.860 |
| 56 | -5.50 | 100 | 83 | 26.55 | 53.09 | 252.51 | 82.80 | 1657.19 | 543.38 | 6.563 |
| 57 | -5.60 | 100 | 84 | 26.55 | 53.09 | 265.99 | 84.84 | 1671.65 | 533.16 | 6.285 |
| 58 | -5.70 | 100 | 84 | 26.55 | 53.09 | 279.94 | 86.89 | 1686.19 | 523.41 | 6.023 |
| 59 | -5.80 | 100 | 85 | 26.55 | 53.09 | 294.36 | 88.97 | 1700.80 | 514.08 | 5.778 |
| 60 | -5.90 | 100 | 86 | 26.55 | 53.09 | 309.27 | 91.07 | 1715.48 | 505.15 | 5.547 |
| 61 | -6.00 | 100 | 87 | 26.55 | 53.09 | 324.67 | 93.18 | 1730.22 | 496.60 | 5.329 |
| 62 | -6.10 | 100 | 87 | 26.55 | 53.09 | 340.58 | 95.32 | 1745.03 | 488.40 | 5.124 |
| 63 | -6.20 | 100 | 88 | 26.55 | 53.09 | 356.99 | 97.47 | 1759.90 | 480.53 | 4.930 |
| 64 | -6.30 | 100 | 89 | 26.55 | 53.09 | 373.92 | 99.65 | 1774.82 | 472.98 | 4.747 |
| 65 | -6.40 | 100 | 90 | 26.55 | 53.09 | 391.37 | 101.84 | 1789.79 | 465.73 | 4.573 |
| 66 | -6.50 | 100 | 91 | 26.55 | 53.09 | 409.36 | 104.05 | 1804.82 | 458.75 | 4.409 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | 0.00 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | -0.10 | 100 | 41 | 26.55 | 53.09 | 0.01 | 0.99 | 0.00 | 0.00 | 100000.000 |
| 3 | -0.20 | 100 | 42 | 26.55 | 53.09 | 0.04 | 2.00 | 185.62 | 8665.54 | 4333.806 |
| 4 | -0.30 | 100 | 42 | 26.55 | 53.09 | 0.11 | 3.03 | 288.00 | 8126.52 | 2683.877 |
| 5 | -0.40 | 100 | 43 | 26.55 | 53.09 | 0.21 | 4.08 | 390.82 | 7580.75 | 1860.142 |
| 6 | -0.50 | 100 | 44 | 26.55 | 53.09 | 0.36 | 5.14 | 489.93 | 7028.80 | 1366.965 |
| 7 | -0.60 | 100 | 45 | 26.55 | 53.09 | 0.56 | 6.23 | 583.29 | 6493.09 | 1042.644 |
| 8 | -0.70 | 100 | 45 | 26.55 | 53.09 | 0.82 | 7.33 | 669.87 | 5984.93 | 816.250 |
| 9 | -0.80 | 100 | 46 | 26.55 | 53.09 | 1.15 | 8.46 | 751.05 | 5521.30 | 652.944 |
| 10 | -0.90 | 100 | 47 | 26.55 | 53.09 | 1.56 | 9.60 | 827.61 | 5103.62 | 531.690 |
| 11 | -1.00 | 100 | 48 | 26.55 | 53.09 | 2.05 | 10.76 | 899.50 | 4725.84 | 439.171 |
| 12 | -1.10 | 100 | 49 | 26.55 | 53.09 | 2.63 | 11.94 | 968.32 | 4390.92 | 367.692 |
| 13 | -1.20 | 100 | 49 | 26.55 | 53.09 | 3.32 | 13.14 | 1033.88 | 4092.22 | 311.386 |
| 14 | -1.30 | 100 | 50 | 26.55 | 53.09 | 4.12 | 14.36 | 1095.91 | 3823.76 | 266.258 |
| 15 | -1.40 | 100 | 51 | 26.55 | 53.09 | 5.03 | 15.60 | 1155.76 | 3585.78 | 229.867 |
| 16 | -1.50 | 100 | 52 | 26.55 | 53.09 | 6.06 | 16.86 | 1213.74 | 3374.21 | 200.170 |
| 17 | -1.60 | 100 | 52 | 26.55 | 53.09 | 7.23 | 18.13 | 1233.43 | 3093.48 | 170.598 |
| 18 | -1.70 | 100 | 53 | 26.55 | 53.09 | 8.53 | 19.43 | 1250.30 | 2846.22 | 146.496 |
| 19 | -1.80 | 100 | 54 | 26.55 | 53.09 | 9.98 | 20.74 | 1263.25 | 2624.38 | 126.517 |
| 20 | -1.90 | 100 | 55 | 26.55 | 53.09 | 11.59 | 22.08 | 1274.23 | 2427.70 | 109.966 |
| 21 | -2.00 | 100 | 56 | 26.55 | 53.09 | 13.35 | 23.43 | 1282.67 | 2251.08 | 96.078 |
| 22 | -2.10 | 100 | 56 | 26.55 | 53.09 | 15.28 | 24.80 | 1293.19 | 2099.01 | 84.633 |
| 23 | -2.20 | 100 | 57 | 26.55 | 53.09 | 17.38 | 26.19 | 1299.28 | 1957.56 | 74.738 |
| 24 | -2.30 | 100 | 58 | 26.55 | 53.09 | 19.67 | 27.60 | 1306.60 | 1833.47 | 66.424 |
| 25 | -2.40 | 100 | 59 | 26.55 | 53.09 | 22.15 | 29.03 | 1315.65 | 1724.75 | 59.410 |
| 26 | -2.50 | 100 | 59 | 26.55 | 53.09 | 24.82 | 30.48 | 1324.82 | 1627.13 | 53.384 |
| 27 | -2.60 | 100 | 60 | 26.55 | 53.09 | 27.69 | 31.95 | 1331.45 | 1536.07 | 48.082 |
| 28 | -2.70 | 100 | 61 | 26.55 | 53.09 | 30.78 | 33.43 | 1339.56 | 1455.20 | 43.526 |
| 29 | -2.80 | 100 | 62 | 26.55 | 53.09 | 34.08 | 34.94 | 1348.83 | 1382.83 | 39.579 |
| 30 | -2.90 | 100 | 63 | 26.55 | 53.09 | 37.61 | 36.46 | 1359.16 | 1317.78 | 36.140 |
| 31 | -3.00 | 100 | 63 | 26.55 | 53.09 | 41.37 | 38.01 | 1370.39 | 1259.02 | 33.126 |
| 32 | -3.10 | 100 | 64 | 26.55 | 53.09 | 45.37 | 39.57 | 1380.25 | 1203.80 | 30.423 |
| 33 | -3.20 | 100 | 65 | 26.55 | 53.09 | 49.62 | 41.15 | 1388.02 | 1151.20 | 27.975 |
| 34 | -3.30 | 100 | 66 | 26.55 | 53.09 | 54.12 | 42.75 | 1396.69 | 1103.35 | 25.808 |
| 35 | -3.40 | 100 | 66 | 26.55 | 53.09 | 58.88 | 44.37 | 1406.14 | 1059.65 | 23.881 |
| 36 | -3.50 | 100 | 67 | 26.55 | 53.09 | 63.91 | 46.01 | 1416.30 | 1019.61 | 22.160 |
| 37 | -3.60 | 100 | 68 | 26.55 | 53.09 | 69.22 | 47.67 | 1427.10 | 982.79 | 20.617 |
| 38 | -3.70 | 100 | 69 | 26.55 | 53.09 | 74.81 | 49.35 | 1438.46 | 948.84 | 19.228 |
| 39 | -3.80 | 100 | 70 | 26.55 | 53.09 | 80.69 | 51.04 | 1450.34 | 917.44 | 17.974 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|-----------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 94 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|--------|
| 40 | -3.90 | 100 | 70 | 26.55 | 53.09 | 86.87 | 52.76 | 1462.69 | 888.33 | 16.838 |
| 41 | -4.00 | 100 | 71 | 26.55 | 53.09 | 93.35 | 54.49 | 1475.48 | 861.28 | 15.806 |
| 42 | -4.10 | 100 | 72 | 26.55 | 53.09 | 100.15 | 56.24 | 1488.54 | 836.01 | 14.864 |
| 43 | -4.20 | 100 | 73 | 26.55 | 53.09 | 107.26 | 58.02 | 1500.57 | 811.67 | 13.990 |
| 44 | -4.30 | 100 | 73 | 26.55 | 53.09 | 114.70 | 59.81 | 1512.87 | 788.87 | 13.190 |
| 45 | -4.40 | 100 | 74 | 26.55 | 53.09 | 122.47 | 61.62 | 1525.41 | 767.47 | 12.455 |
| 46 | -4.50 | 100 | 75 | 26.55 | 53.09 | 130.59 | 63.45 | 1538.18 | 747.35 | 11.779 |
| 47 | -4.60 | 100 | 76 | 26.55 | 53.09 | 139.05 | 65.30 | 1551.14 | 728.40 | 11.155 |
| 48 | -4.70 | 100 | 77 | 26.55 | 53.09 | 147.87 | 67.17 | 1564.30 | 710.53 | 10.579 |
| 49 | -4.80 | 100 | 77 | 26.55 | 53.09 | 157.05 | 69.05 | 1577.62 | 693.64 | 10.045 |
| 50 | -4.90 | 100 | 78 | 26.55 | 53.09 | 166.61 | 70.96 | 1591.10 | 677.66 | 9.550 |
| 51 | -5.00 | 100 | 79 | 26.55 | 53.09 | 176.54 | 72.88 | 1604.73 | 662.53 | 9.090 |
| 52 | -5.10 | 100 | 80 | 26.55 | 53.09 | 186.85 | 74.83 | 1618.49 | 648.17 | 8.662 |
| 53 | -5.20 | 100 | 80 | 26.55 | 53.09 | 197.55 | 76.79 | 1632.38 | 634.53 | 8.263 |
| 54 | -5.30 | 100 | 81 | 26.55 | 53.09 | 208.66 | 78.77 | 1646.39 | 621.56 | 7.890 |
| 55 | -5.40 | 100 | 82 | 26.55 | 53.09 | 220.17 | 80.78 | 1660.50 | 609.21 | 7.542 |
| 56 | -5.50 | 100 | 83 | 26.55 | 53.09 | 232.09 | 82.80 | 1674.71 | 597.44 | 7.216 |
| 57 | -5.60 | 100 | 84 | 26.55 | 53.09 | 244.43 | 84.84 | 1689.02 | 586.21 | 6.910 |
| 58 | -5.70 | 100 | 84 | 26.55 | 53.09 | 257.21 | 86.89 | 1703.42 | 575.48 | 6.623 |
| 59 | -5.80 | 100 | 85 | 26.55 | 53.09 | 270.41 | 88.97 | 1717.90 | 565.23 | 6.353 |
| 60 | -5.90 | 100 | 86 | 26.55 | 53.09 | 284.06 | 91.07 | 1732.45 | 555.42 | 6.099 |
| 61 | -6.00 | 100 | 87 | 26.55 | 53.09 | 298.16 | 93.18 | 1747.08 | 546.02 | 5.860 |
| 62 | -6.10 | 100 | 87 | 26.55 | 53.09 | 312.72 | 95.32 | 1761.78 | 537.01 | 5.634 |
| 63 | -6.20 | 100 | 88 | 26.55 | 53.09 | 327.74 | 97.47 | 1776.54 | 528.37 | 5.421 |
| 64 | -6.30 | 100 | 89 | 26.55 | 53.09 | 343.23 | 99.65 | 1791.36 | 520.08 | 5.219 |
| 65 | -6.40 | 100 | 90 | 26.55 | 53.09 | 359.20 | 101.84 | 1806.24 | 512.11 | 5.029 |
| 66 | -6.50 | 100 | 91 | 26.55 | 53.09 | 375.65 | 104.05 | 1821.18 | 504.44 | 4.848 |

Fondazione

Combinazione n° 1 - STR (A1-M1-R3)

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | -1.00 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | -0.90 | 100 | 110 | 45.24 | 22.62 | 0.97 | 0.00 | 1737.61 | 0.00 | 1791.050 |
| 3 | -0.80 | 100 | 110 | 45.24 | 22.62 | 3.87 | 0.00 | 1737.61 | 0.00 | 449.357 |
| 4 | -0.70 | 100 | 110 | 45.24 | 22.62 | 8.67 | 0.00 | 1737.61 | 0.00 | 200.428 |
| 5 | -0.60 | 100 | 110 | 45.24 | 22.62 | 15.36 | 0.00 | 1737.61 | 0.00 | 113.145 |
| 6 | -0.50 | 100 | 110 | 45.24 | 22.62 | 23.91 | 0.00 | 1737.61 | 0.00 | 72.673 |
| 7 | -0.40 | 100 | 110 | 45.24 | 22.62 | 34.31 | 0.00 | 1737.61 | 0.00 | 50.650 |
| 8 | 0.51 | 100 | 110 | 22.62 | 45.24 | -1068.78 | 0.00 | -1737.61 | 0.00 | 1.626 |
| 9 | 0.60 | 100 | 110 | 22.62 | 45.24 | -1039.26 | 0.00 | -1737.61 | 0.00 | 1.672 |
| 10 | 0.70 | 100 | 110 | 22.62 | 45.24 | -1009.76 | 0.00 | -1737.61 | 0.00 | 1.721 |
| 11 | 0.80 | 100 | 110 | 22.62 | 45.24 | -980.30 | 0.00 | -1737.61 | 0.00 | 1.773 |
| 12 | 0.90 | 100 | 110 | 22.62 | 45.24 | -950.90 | 0.00 | -1737.61 | 0.00 | 1.827 |
| 13 | 1.00 | 100 | 110 | 22.62 | 45.24 | -921.57 | 0.00 | -1737.61 | 0.00 | 1.885 |
| 14 | 1.10 | 100 | 110 | 22.62 | 45.24 | -892.35 | 0.00 | -1737.61 | 0.00 | 1.947 |
| 15 | 1.20 | 100 | 110 | 22.62 | 45.24 | -863.24 | 0.00 | -1737.61 | 0.00 | 2.013 |
| 16 | 1.30 | 100 | 110 | 22.62 | 45.24 | -834.28 | 0.00 | -1737.61 | 0.00 | 2.083 |
| 17 | 1.40 | 100 | 110 | 22.62 | 45.24 | -805.47 | 0.00 | -1737.61 | 0.00 | 2.157 |
| 18 | 1.49 | 100 | 110 | 22.62 | 45.24 | -776.84 | 0.00 | -1737.61 | 0.00 | 2.237 |
| 19 | 1.59 | 100 | 110 | 22.62 | 45.24 | -748.41 | 0.00 | -1737.61 | 0.00 | 2.322 |
| 20 | 1.69 | 100 | 110 | 22.62 | 45.24 | -720.20 | 0.00 | -1737.61 | 0.00 | 2.413 |
| 21 | 1.79 | 100 | 110 | 22.62 | 45.24 | -692.23 | 0.00 | -1737.61 | 0.00 | 2.510 |
| 22 | 1.89 | 100 | 110 | 22.62 | 45.24 | -664.52 | 0.00 | -1737.61 | 0.00 | 2.615 |
| 23 | 1.99 | 100 | 110 | 22.62 | 45.24 | -637.08 | 0.00 | -1737.61 | 0.00 | 2.727 |
| 24 | 2.09 | 100 | 110 | 22.62 | 45.24 | -609.94 | 0.00 | -1737.61 | 0.00 | 2.849 |
| 25 | 2.19 | 100 | 110 | 22.62 | 45.24 | -583.12 | 0.00 | -1737.61 | 0.00 | 2.980 |

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
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| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 26 | 2.29 | 100 | 110 | 22.62 | 45.24 | -556.64 | 0.00 | -1737.61 | 0.00 | 3.122 |
| 27 | 2.38 | 100 | 110 | 22.62 | 45.24 | -530.52 | 0.00 | -1737.61 | 0.00 | 3.275 |
| 28 | 2.48 | 100 | 110 | 22.62 | 45.24 | -504.78 | 0.00 | -1737.61 | 0.00 | 3.442 |
| 29 | 2.58 | 100 | 110 | 22.62 | 45.24 | -479.43 | 0.00 | -1737.61 | 0.00 | 3.624 |
| 30 | 2.68 | 100 | 110 | 22.62 | 45.24 | -454.50 | 0.00 | -1737.61 | 0.00 | 3.823 |
| 31 | 2.78 | 100 | 110 | 22.62 | 45.24 | -430.01 | 0.00 | -1737.61 | 0.00 | 4.041 |
| 32 | 2.88 | 100 | 110 | 22.62 | 45.24 | -405.98 | 0.00 | -1737.61 | 0.00 | 4.280 |
| 33 | 2.98 | 100 | 110 | 22.62 | 45.24 | -382.43 | 0.00 | -1737.61 | 0.00 | 4.544 |
| 34 | 3.08 | 100 | 110 | 22.62 | 45.24 | -359.37 | 0.00 | -1737.61 | 0.00 | 4.835 |
| 35 | 3.17 | 100 | 110 | 22.62 | 45.24 | -336.83 | 0.00 | -1737.61 | 0.00 | 5.159 |
| 36 | 3.27 | 100 | 110 | 22.62 | 45.24 | -314.83 | 0.00 | -1737.61 | 0.00 | 5.519 |
| 37 | 3.37 | 100 | 110 | 22.62 | 45.24 | -293.39 | 0.00 | -1737.61 | 0.00 | 5.923 |
| 38 | 3.47 | 100 | 110 | 22.62 | 45.24 | -272.53 | 0.00 | -1737.61 | 0.00 | 6.376 |
| 39 | 3.57 | 100 | 110 | 22.62 | 45.24 | -252.26 | 0.00 | -1737.61 | 0.00 | 6.888 |
| 40 | 3.67 | 100 | 110 | 22.62 | 45.24 | -232.61 | 0.00 | -1737.61 | 0.00 | 7.470 |
| 41 | 3.77 | 100 | 110 | 22.62 | 45.24 | -211.88 | 0.00 | -1737.61 | 0.00 | 8.201 |
| 42 | 3.87 | 100 | 110 | 22.62 | 45.24 | -191.24 | 0.00 | -1737.61 | 0.00 | 9.086 |
| 43 | 3.97 | 100 | 110 | 22.62 | 45.24 | -171.54 | 0.00 | -1737.61 | 0.00 | 10.129 |
| 44 | 4.06 | 100 | 110 | 22.62 | 45.24 | -152.80 | 0.00 | -1737.61 | 0.00 | 11.372 |
| 45 | 4.16 | 100 | 110 | 22.62 | 45.24 | -135.05 | 0.00 | -1737.61 | 0.00 | 12.867 |
| 46 | 4.26 | 100 | 110 | 22.62 | 45.24 | -118.29 | 0.00 | -1737.61 | 0.00 | 14.689 |
| 47 | 4.36 | 100 | 110 | 22.62 | 45.24 | -102.56 | 0.00 | -1737.61 | 0.00 | 16.942 |
| 48 | 4.46 | 100 | 110 | 22.62 | 45.24 | -87.87 | 0.00 | -1737.61 | 0.00 | 19.776 |
| 49 | 4.56 | 100 | 110 | 22.62 | 45.24 | -74.23 | 0.00 | -1737.61 | 0.00 | 23.407 |
| 50 | 4.66 | 100 | 110 | 22.62 | 45.24 | -61.68 | 0.00 | -1737.61 | 0.00 | 28.170 |
| 51 | 4.76 | 100 | 110 | 22.62 | 45.24 | -50.23 | 0.00 | -1737.61 | 0.00 | 34.591 |
| 52 | 4.86 | 100 | 110 | 22.62 | 45.24 | -39.90 | 0.00 | -1737.61 | 0.00 | 43.546 |
| 53 | 4.95 | 100 | 110 | 22.62 | 45.24 | -30.71 | 0.00 | -1737.61 | 0.00 | 56.575 |
| 54 | 5.05 | 100 | 110 | 22.62 | 45.24 | -22.68 | 0.00 | -1737.61 | 0.00 | 76.599 |
| 55 | 5.15 | 100 | 110 | 22.62 | 45.24 | -15.84 | 0.00 | -1737.61 | 0.00 | 109.723 |
| 56 | 5.25 | 100 | 110 | 22.62 | 45.24 | -10.19 | 0.00 | -1737.61 | 0.00 | 170.547 |
| 57 | 5.35 | 100 | 110 | 22.62 | 45.24 | -5.76 | 0.00 | -1737.61 | 0.00 | 301.621 |
| 58 | 5.45 | 100 | 110 | 22.62 | 45.24 | -2.57 | 0.00 | -1737.61 | 0.00 | 675.142 |
| 59 | 5.55 | 100 | 110 | 22.62 | 45.24 | -0.65 | 0.00 | -1737.61 | 0.00 | 2686.687 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | -1.00 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | -0.90 | 100 | 110 | 45.24 | 22.62 | 1.19 | 0.00 | 1737.61 | 0.00 | 1456.802 |
| 3 | -0.80 | 100 | 110 | 45.24 | 22.62 | 4.75 | 0.00 | 1737.61 | 0.00 | 365.918 |
| 4 | -0.70 | 100 | 110 | 45.24 | 22.62 | 10.63 | 0.00 | 1737.61 | 0.00 | 163.401 |
| 5 | -0.60 | 100 | 110 | 45.24 | 22.62 | 18.82 | 0.00 | 1737.61 | 0.00 | 92.351 |
| 6 | -0.50 | 100 | 110 | 45.24 | 22.62 | 29.26 | 0.00 | 1737.61 | 0.00 | 59.387 |
| 7 | -0.40 | 100 | 110 | 45.24 | 22.62 | 41.93 | 0.00 | 1737.61 | 0.00 | 41.439 |
| 8 | 0.51 | 100 | 110 | 22.62 | 45.24 | -700.79 | 0.00 | -1737.61 | 0.00 | 2.480 |
| 9 | 0.60 | 100 | 110 | 22.62 | 45.24 | -688.54 | 0.00 | -1737.61 | 0.00 | 2.524 |
| 10 | 0.70 | 100 | 110 | 22.62 | 45.24 | -675.70 | 0.00 | -1737.61 | 0.00 | 2.572 |
| 11 | 0.80 | 100 | 110 | 22.62 | 45.24 | -662.30 | 0.00 | -1737.61 | 0.00 | 2.624 |
| 12 | 0.90 | 100 | 110 | 22.62 | 45.24 | -648.38 | 0.00 | -1737.61 | 0.00 | 2.680 |
| 13 | 1.00 | 100 | 110 | 22.62 | 45.24 | -633.97 | 0.00 | -1737.61 | 0.00 | 2.741 |
| 14 | 1.10 | 100 | 110 | 22.62 | 45.24 | -619.09 | 0.00 | -1737.61 | 0.00 | 2.807 |
| 15 | 1.20 | 100 | 110 | 22.62 | 45.24 | -603.80 | 0.00 | -1737.61 | 0.00 | 2.878 |
| 16 | 1.30 | 100 | 110 | 22.62 | 45.24 | -588.10 | 0.00 | -1737.61 | 0.00 | 2.955 |
| 17 | 1.40 | 100 | 110 | 22.62 | 45.24 | -572.05 | 0.00 | -1737.61 | 0.00 | 3.038 |
| 18 | 1.49 | 100 | 110 | 22.62 | 45.24 | -555.67 | 0.00 | -1737.61 | 0.00 | 3.127 |
| 19 | 1.59 | 100 | 110 | 22.62 | 45.24 | -538.99 | 0.00 | -1737.61 | 0.00 | 3.224 |
| 20 | 1.69 | 100 | 110 | 22.62 | 45.24 | -522.04 | 0.00 | -1737.61 | 0.00 | 3.328 |
| 21 | 1.79 | 100 | 110 | 22.62 | 45.24 | -504.87 | 0.00 | -1737.61 | 0.00 | 3.442 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|-----------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 96 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 22 | 1.89 | 100 | 110 | 22.62 | 45.24 | -487.49 | 0.00 | -1737.61 | 0.00 | 3.564 |
| 23 | 1.99 | 100 | 110 | 22.62 | 45.24 | -469.95 | 0.00 | -1737.61 | 0.00 | 3.697 |
| 24 | 2.09 | 100 | 110 | 22.62 | 45.24 | -452.27 | 0.00 | -1737.61 | 0.00 | 3.842 |
| 25 | 2.19 | 100 | 110 | 22.62 | 45.24 | -434.49 | 0.00 | -1737.61 | 0.00 | 3.999 |
| 26 | 2.29 | 100 | 110 | 22.62 | 45.24 | -416.64 | 0.00 | -1737.61 | 0.00 | 4.170 |
| 27 | 2.38 | 100 | 110 | 22.62 | 45.24 | -398.76 | 0.00 | -1737.61 | 0.00 | 4.358 |
| 28 | 2.48 | 100 | 110 | 22.62 | 45.24 | -380.87 | 0.00 | -1737.61 | 0.00 | 4.562 |
| 29 | 2.58 | 100 | 110 | 22.62 | 45.24 | -363.01 | 0.00 | -1737.61 | 0.00 | 4.787 |
| 30 | 2.68 | 100 | 110 | 22.62 | 45.24 | -345.20 | 0.00 | -1737.61 | 0.00 | 5.034 |
| 31 | 2.78 | 100 | 110 | 22.62 | 45.24 | -327.49 | 0.00 | -1737.61 | 0.00 | 5.306 |
| 32 | 2.88 | 100 | 110 | 22.62 | 45.24 | -309.91 | 0.00 | -1737.61 | 0.00 | 5.607 |
| 33 | 2.98 | 100 | 110 | 22.62 | 45.24 | -292.48 | 0.00 | -1737.61 | 0.00 | 5.941 |
| 34 | 3.08 | 100 | 110 | 22.62 | 45.24 | -275.24 | 0.00 | -1737.61 | 0.00 | 6.313 |
| 35 | 3.17 | 100 | 110 | 22.62 | 45.24 | -258.23 | 0.00 | -1737.61 | 0.00 | 6.729 |
| 36 | 3.27 | 100 | 110 | 22.62 | 45.24 | -241.46 | 0.00 | -1737.61 | 0.00 | 7.196 |
| 37 | 3.37 | 100 | 110 | 22.62 | 45.24 | -224.99 | 0.00 | -1737.61 | 0.00 | 7.723 |
| 38 | 3.47 | 100 | 110 | 22.62 | 45.24 | -208.84 | 0.00 | -1737.61 | 0.00 | 8.320 |
| 39 | 3.57 | 100 | 110 | 22.62 | 45.24 | -193.04 | 0.00 | -1737.61 | 0.00 | 9.002 |
| 40 | 3.67 | 100 | 110 | 22.62 | 45.24 | -177.62 | 0.00 | -1737.61 | 0.00 | 9.783 |
| 41 | 3.77 | 100 | 110 | 22.62 | 45.24 | -162.36 | 0.00 | -1737.61 | 0.00 | 10.702 |
| 42 | 3.87 | 100 | 110 | 22.62 | 45.24 | -147.47 | 0.00 | -1737.61 | 0.00 | 11.782 |
| 43 | 3.97 | 100 | 110 | 22.62 | 45.24 | -133.11 | 0.00 | -1737.61 | 0.00 | 13.054 |
| 44 | 4.06 | 100 | 110 | 22.62 | 45.24 | -119.29 | 0.00 | -1737.61 | 0.00 | 14.566 |
| 45 | 4.16 | 100 | 110 | 22.62 | 45.24 | -106.06 | 0.00 | -1737.61 | 0.00 | 16.383 |
| 46 | 4.26 | 100 | 110 | 22.62 | 45.24 | -93.45 | 0.00 | -1737.61 | 0.00 | 18.594 |
| 47 | 4.36 | 100 | 110 | 22.62 | 45.24 | -81.49 | 0.00 | -1737.61 | 0.00 | 21.322 |
| 48 | 4.46 | 100 | 110 | 22.62 | 45.24 | -70.22 | 0.00 | -1737.61 | 0.00 | 24.747 |
| 49 | 4.56 | 100 | 110 | 22.62 | 45.24 | -59.66 | 0.00 | -1737.61 | 0.00 | 29.127 |
| 50 | 4.66 | 100 | 110 | 22.62 | 45.24 | -49.84 | 0.00 | -1737.61 | 0.00 | 34.862 |
| 51 | 4.76 | 100 | 110 | 22.62 | 45.24 | -40.81 | 0.00 | -1737.61 | 0.00 | 42.577 |
| 52 | 4.86 | 100 | 110 | 22.62 | 45.24 | -32.59 | 0.00 | -1737.61 | 0.00 | 53.315 |
| 53 | 4.95 | 100 | 110 | 22.62 | 45.24 | -25.22 | 0.00 | -1737.61 | 0.00 | 68.904 |
| 54 | 5.05 | 100 | 110 | 22.62 | 45.24 | -18.72 | 0.00 | -1737.61 | 0.00 | 92.811 |
| 55 | 5.15 | 100 | 110 | 22.62 | 45.24 | -13.14 | 0.00 | -1737.61 | 0.00 | 132.272 |
| 56 | 5.25 | 100 | 110 | 22.62 | 45.24 | -8.49 | 0.00 | -1737.61 | 0.00 | 204.570 |
| 57 | 5.35 | 100 | 110 | 22.62 | 45.24 | -4.83 | 0.00 | -1737.61 | 0.00 | 360.012 |
| 58 | 5.45 | 100 | 110 | 22.62 | 45.24 | -2.17 | 0.00 | -1737.61 | 0.00 | 801.941 |
| 59 | 5.55 | 100 | 110 | 22.62 | 45.24 | -0.55 | 0.00 | -1737.61 | 0.00 | 3176.058 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | -1.00 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | -0.90 | 100 | 110 | 45.24 | 22.62 | 1.08 | 0.00 | 1737.61 | 0.00 | 1609.512 |
| 3 | -0.80 | 100 | 110 | 45.24 | 22.62 | 4.30 | 0.00 | 1737.61 | 0.00 | 404.404 |
| 4 | -0.70 | 100 | 110 | 45.24 | 22.62 | 9.62 | 0.00 | 1737.61 | 0.00 | 180.645 |
| 5 | -0.60 | 100 | 110 | 45.24 | 22.62 | 17.01 | 0.00 | 1737.61 | 0.00 | 102.130 |
| 6 | -0.50 | 100 | 110 | 45.24 | 22.62 | 26.45 | 0.00 | 1737.61 | 0.00 | 65.697 |
| 7 | -0.40 | 100 | 110 | 45.24 | 22.62 | 37.89 | 0.00 | 1737.61 | 0.00 | 45.858 |
| 8 | 0.51 | 100 | 110 | 22.62 | 45.24 | -926.10 | 0.00 | -1737.61 | 0.00 | 1.876 |
| 9 | 0.60 | 100 | 110 | 22.62 | 45.24 | -904.79 | 0.00 | -1737.61 | 0.00 | 1.920 |
| 10 | 0.70 | 100 | 110 | 22.62 | 45.24 | -883.10 | 0.00 | -1737.61 | 0.00 | 1.968 |
| 11 | 0.80 | 100 | 110 | 22.62 | 45.24 | -861.05 | 0.00 | -1737.61 | 0.00 | 2.018 |
| 12 | 0.90 | 100 | 110 | 22.62 | 45.24 | -838.67 | 0.00 | -1737.61 | 0.00 | 2.072 |
| 13 | 1.00 | 100 | 110 | 22.62 | 45.24 | -816.01 | 0.00 | -1737.61 | 0.00 | 2.129 |
| 14 | 1.10 | 100 | 110 | 22.62 | 45.24 | -793.09 | 0.00 | -1737.61 | 0.00 | 2.191 |
| 15 | 1.20 | 100 | 110 | 22.62 | 45.24 | -769.94 | 0.00 | -1737.61 | 0.00 | 2.257 |
| 16 | 1.30 | 100 | 110 | 22.62 | 45.24 | -746.59 | 0.00 | -1737.61 | 0.00 | 2.327 |
| 17 | 1.40 | 100 | 110 | 22.62 | 45.24 | -723.07 | 0.00 | -1737.61 | 0.00 | 2.403 |

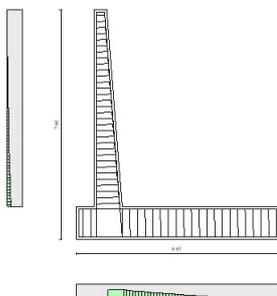


Fig. 10 - Paramento (Inviluppo)

Verifiche a taglio

Simbologia adottata

| | |
|--------------|---|
| I_s | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| A_{sw} | area ferri a taglio espresso in [cm ²] |
| $\cot\theta$ | inclinazione delle bielle compresse, θ inclinazione dei puntoni di calcestruzzo |
| V_{Rcd} | resistenza di progetto a 'taglio compressione' espressa in [kN] |
| V_{Rsd} | resistenza di progetto a 'taglio trazione' espressa in [kN] |
| V_{Rd} | resistenza di progetto a taglio espresso in [kN]. Per elementi con armature trasversali resistenti al taglio ($A_{sw}>0.0$) $V_{Rd}=\min(V_{Rcd}, V_{Rsd})$. |
| T | taglio agente espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione resistente e sollecitazione agente) |

Paramento

Combinazione n° 1 - STR (A1-M1-R3)

| n° | Y | B | H | A_{sw} | s | $\cot\theta$ | V_{Rcd} | V_{Rsd} | V_{Rd} | T | FS |
|----|---|---|---|----------|---|--------------|-----------|-----------|----------|---|----|
|----|---|---|---|----------|---|--------------|-----------|-----------|----------|---|----|

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 291.33 | 0.00 | 100.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 296.72 | 0.17 | 1775.521 |
| 3 | -0.20 | 100 | 42 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 302.10 | 0.41 | 729.799 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 307.47 | 0.74 | 415.646 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 312.83 | 1.14 | 273.497 |
| 6 | -0.50 | 100 | 44 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 318.18 | 1.63 | 195.612 |
| 7 | -0.60 | 100 | 45 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 323.51 | 2.19 | 147.832 |
| 8 | -0.70 | 100 | 45 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 328.83 | 2.84 | 115.977 |
| 9 | -0.80 | 100 | 46 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 334.13 | 3.57 | 93.545 |
| 10 | -0.90 | 100 | 47 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 337.26 | 4.40 | 76.649 |
| 11 | -1.00 | 100 | 48 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 340.37 | 5.32 | 63.966 |
| 12 | -1.10 | 100 | 49 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 343.45 | 6.33 | 54.271 |
| 13 | -1.20 | 100 | 49 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 346.52 | 7.42 | 46.709 |
| 14 | -1.30 | 100 | 50 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 349.58 | 8.59 | 40.697 |
| 15 | -1.40 | 100 | 51 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 352.61 | 9.84 | 35.832 |
| 16 | -1.50 | 100 | 52 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 355.63 | 11.17 | 31.835 |
| 17 | -1.60 | 100 | 52 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 358.63 | 12.58 | 28.507 |
| 18 | -1.70 | 100 | 53 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 361.61 | 14.07 | 25.702 |
| 19 | -1.80 | 100 | 54 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 364.58 | 15.64 | 23.314 |
| 20 | -1.90 | 100 | 55 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 367.53 | 17.29 | 21.263 |
| 21 | -2.00 | 100 | 56 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 370.47 | 19.01 | 19.486 |
| 22 | -2.10 | 100 | 56 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 373.39 | 20.82 | 17.936 |
| 23 | -2.20 | 100 | 57 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 376.30 | 22.70 | 16.575 |
| 24 | -2.30 | 100 | 58 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 379.20 | 24.67 | 15.373 |
| 25 | -2.40 | 100 | 59 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 382.08 | 26.71 | 14.305 |
| 26 | -2.50 | 100 | 59 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 384.95 | 28.83 | 13.352 |
| 27 | -2.60 | 100 | 60 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 387.81 | 31.03 | 12.497 |
| 28 | -2.70 | 100 | 61 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 390.66 | 33.31 | 11.727 |
| 29 | -2.80 | 100 | 62 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 393.49 | 35.67 | 11.031 |
| 30 | -2.90 | 100 | 63 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 396.31 | 38.11 | 10.399 |
| 31 | -3.00 | 100 | 63 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 399.12 | 40.63 | 9.824 |
| 32 | -3.10 | 100 | 64 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 401.92 | 43.22 | 9.298 |
| 33 | -3.20 | 100 | 65 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 404.71 | 45.90 | 8.817 |
| 34 | -3.30 | 100 | 66 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 407.48 | 48.65 | 8.375 |
| 35 | -3.40 | 100 | 66 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 410.25 | 51.49 | 7.968 |
| 36 | -3.50 | 100 | 67 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 413.01 | 54.40 | 7.592 |
| 37 | -3.60 | 100 | 68 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 415.75 | 57.39 | 7.244 |
| 38 | -3.70 | 100 | 69 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 418.49 | 60.46 | 6.922 |
| 39 | -3.80 | 100 | 70 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 421.22 | 63.61 | 6.622 |
| 40 | -3.90 | 100 | 70 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 423.94 | 66.84 | 6.343 |
| 41 | -4.00 | 100 | 71 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 426.65 | 70.15 | 6.082 |
| 42 | -4.10 | 100 | 72 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 429.35 | 73.53 | 5.839 |
| 43 | -4.20 | 100 | 73 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 432.04 | 77.00 | 5.611 |
| 44 | -4.30 | 100 | 73 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 434.73 | 80.54 | 5.397 |
| 45 | -4.40 | 100 | 74 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 437.41 | 84.17 | 5.197 |
| 46 | -4.50 | 100 | 75 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 440.07 | 87.87 | 5.008 |
| 47 | -4.60 | 100 | 76 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 442.74 | 91.65 | 4.831 |
| 48 | -4.70 | 100 | 77 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 445.39 | 95.51 | 4.663 |
| 49 | -4.80 | 100 | 77 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 448.03 | 99.45 | 4.505 |
| 50 | -4.90 | 100 | 78 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 450.67 | 103.47 | 4.356 |
| 51 | -5.00 | 100 | 79 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 453.30 | 107.57 | 4.214 |
| 52 | -5.10 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 455.93 | 111.74 | 4.080 |
| 53 | -5.20 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 458.55 | 116.00 | 3.953 |
| 54 | -5.30 | 100 | 81 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 461.16 | 120.33 | 3.832 |
| 55 | -5.40 | 100 | 82 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 463.76 | 124.75 | 3.718 |
| 56 | -5.50 | 100 | 83 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 466.36 | 129.24 | 3.608 |
| 57 | -5.60 | 100 | 84 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 468.95 | 133.81 | 3.505 |
| 58 | -5.70 | 100 | 84 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 471.54 | 138.46 | 3.406 |
| 59 | -5.80 | 100 | 85 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 474.12 | 143.19 | 3.311 |
| 60 | -5.90 | 100 | 86 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 476.69 | 148.00 | 3.221 |
| 61 | -6.00 | 100 | 87 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 479.26 | 152.89 | 3.135 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 101 di 314 |

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|-------|
| 62 | -6.10 | 100 | 87 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.82 | 157.86 | 3.052 |
| 63 | -6.20 | 100 | 88 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 484.38 | 162.90 | 2.973 |
| 64 | -6.30 | 100 | 89 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 486.93 | 168.03 | 2.898 |
| 65 | -6.40 | 100 | 90 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 489.48 | 173.23 | 2.826 |
| 66 | -6.50 | 100 | 91 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 492.02 | 178.51 | 2.756 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 291.33 | 0.00 | 100.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 296.72 | 0.16 | 1815.522 |
| 3 | -0.20 | 100 | 42 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 302.10 | 0.40 | 756.722 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 307.47 | 0.71 | 435.139 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 312.83 | 1.08 | 288.348 |
| 6 | -0.50 | 100 | 44 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 318.18 | 1.53 | 207.346 |
| 7 | -0.60 | 100 | 45 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 323.51 | 2.06 | 157.364 |
| 8 | -0.70 | 100 | 45 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 328.83 | 2.65 | 123.858 |
| 9 | -0.80 | 100 | 46 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 334.13 | 3.34 | 100.152 |
| 10 | -0.90 | 100 | 47 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 337.26 | 4.10 | 82.222 |
| 11 | -1.00 | 100 | 48 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 340.37 | 4.95 | 68.722 |
| 12 | -1.10 | 100 | 49 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 343.45 | 5.88 | 58.381 |
| 13 | -1.20 | 100 | 49 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 346.52 | 6.89 | 50.304 |
| 14 | -1.30 | 100 | 50 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 349.58 | 7.97 | 43.875 |
| 15 | -1.40 | 100 | 51 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 352.61 | 9.12 | 38.668 |
| 16 | -1.50 | 100 | 52 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 355.63 | 10.34 | 34.385 |
| 17 | -1.60 | 100 | 52 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 358.63 | 11.64 | 30.815 |
| 18 | -1.70 | 100 | 53 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 361.61 | 13.01 | 27.805 |
| 19 | -1.80 | 100 | 54 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 364.58 | 14.44 | 25.239 |
| 20 | -1.90 | 100 | 55 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 367.53 | 15.96 | 23.034 |
| 21 | -2.00 | 100 | 56 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 370.47 | 17.54 | 21.123 |
| 22 | -2.10 | 100 | 56 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 373.39 | 19.19 | 19.454 |
| 23 | -2.20 | 100 | 57 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 376.30 | 20.92 | 17.987 |
| 24 | -2.30 | 100 | 58 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 379.20 | 22.72 | 16.691 |
| 25 | -2.40 | 100 | 59 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 382.08 | 24.59 | 15.539 |
| 26 | -2.50 | 100 | 59 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 384.95 | 26.53 | 14.510 |
| 27 | -2.60 | 100 | 60 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 387.81 | 28.54 | 13.586 |
| 28 | -2.70 | 100 | 61 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 390.66 | 30.63 | 12.754 |
| 29 | -2.80 | 100 | 62 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 393.49 | 32.79 | 12.002 |
| 30 | -2.90 | 100 | 63 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 396.31 | 35.01 | 11.319 |
| 31 | -3.00 | 100 | 63 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 399.12 | 37.31 | 10.696 |
| 32 | -3.10 | 100 | 64 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 401.92 | 39.69 | 10.127 |
| 33 | -3.20 | 100 | 65 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 404.71 | 42.13 | 9.606 |
| 34 | -3.30 | 100 | 66 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 407.48 | 44.64 | 9.127 |
| 35 | -3.40 | 100 | 66 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 410.25 | 47.23 | 8.686 |
| 36 | -3.50 | 100 | 67 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 413.01 | 49.89 | 8.278 |
| 37 | -3.60 | 100 | 68 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 415.75 | 52.62 | 7.901 |
| 38 | -3.70 | 100 | 69 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 418.49 | 55.42 | 7.551 |
| 39 | -3.80 | 100 | 70 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 421.22 | 58.29 | 7.226 |
| 40 | -3.90 | 100 | 70 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 423.94 | 61.24 | 6.923 |
| 41 | -4.00 | 100 | 71 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 426.65 | 64.26 | 6.640 |
| 42 | -4.10 | 100 | 72 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 429.35 | 67.34 | 6.375 |
| 43 | -4.20 | 100 | 73 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 432.04 | 70.50 | 6.128 |
| 44 | -4.30 | 100 | 73 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 434.73 | 73.74 | 5.896 |
| 45 | -4.40 | 100 | 74 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 437.41 | 77.04 | 5.678 |
| 46 | -4.50 | 100 | 75 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 440.07 | 80.41 | 5.473 |
| 47 | -4.60 | 100 | 76 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 442.74 | 83.86 | 5.279 |
| 48 | -4.70 | 100 | 77 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 445.39 | 87.38 | 5.097 |
| 49 | -4.80 | 100 | 77 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 448.03 | 90.97 | 4.925 |
| 50 | -4.90 | 100 | 78 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 450.67 | 94.63 | 4.762 |
| 51 | -5.00 | 100 | 79 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 453.30 | 98.36 | 4.608 |
| 52 | -5.10 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 455.93 | 102.17 | 4.463 |
| 53 | -5.20 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 458.55 | 106.04 | 4.324 |

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
NM25 03 D 26 CL NV 24 05 001 A 102 di 314

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|-------|
| 54 | -5.30 | 100 | 81 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 461.16 | 109.99 | 4.193 |
| 55 | -5.40 | 100 | 82 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 463.76 | 114.01 | 4.068 |
| 56 | -5.50 | 100 | 83 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 466.36 | 118.10 | 3.949 |
| 57 | -5.60 | 100 | 84 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 468.95 | 122.27 | 3.836 |
| 58 | -5.70 | 100 | 84 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 471.54 | 126.50 | 3.728 |
| 59 | -5.80 | 100 | 85 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 474.12 | 130.81 | 3.625 |
| 60 | -5.90 | 100 | 86 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 476.69 | 135.18 | 3.526 |
| 61 | -6.00 | 100 | 87 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 479.26 | 139.63 | 3.432 |
| 62 | -6.10 | 100 | 87 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.82 | 144.15 | 3.342 |
| 63 | -6.20 | 100 | 88 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 484.38 | 148.75 | 3.256 |
| 64 | -6.30 | 100 | 89 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 486.93 | 153.41 | 3.174 |
| 65 | -6.40 | 100 | 90 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 489.48 | 158.15 | 3.095 |
| 66 | -6.50 | 100 | 91 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 492.02 | 162.96 | 3.019 |

Fondazione

Combinazione n° 1 - STR (A1-M1-R3)

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 1 | -1.00 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | 0.00 | 100.000 |
| 2 | -0.90 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -19.37 | 24.843 |
| 3 | -0.80 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -38.53 | 12.488 |
| 4 | -0.70 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -57.49 | 8.370 |
| 5 | -0.60 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -76.24 | 6.312 |
| 6 | -0.50 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -94.78 | 5.077 |
| 7 | -0.40 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -113.12 | 4.254 |
| 8 | 0.51 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -324.94 | 1.481 |
| 9 | 0.60 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -324.85 | 1.481 |
| 10 | 0.70 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -324.55 | 1.483 |
| 11 | 0.80 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -324.05 | 1.485 |
| 12 | 0.90 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -323.35 | 1.488 |
| 13 | 1.00 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -322.45 | 1.492 |
| 14 | 1.10 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -321.35 | 1.497 |
| 15 | 1.20 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -320.05 | 1.503 |
| 16 | 1.30 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -318.54 | 1.511 |
| 17 | 1.40 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -316.83 | 1.519 |
| 18 | 1.49 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -314.93 | 1.528 |
| 19 | 1.59 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -312.81 | 1.538 |
| 20 | 1.69 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -310.50 | 1.550 |
| 21 | 1.79 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -307.99 | 1.562 |
| 22 | 1.89 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -305.27 | 1.576 |
| 23 | 1.99 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -302.35 | 1.591 |
| 24 | 2.09 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -299.23 | 1.608 |
| 25 | 2.19 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -295.91 | 1.626 |
| 26 | 2.29 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -292.39 | 1.646 |
| 27 | 2.38 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -288.66 | 1.667 |
| 28 | 2.48 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -284.73 | 1.690 |
| 29 | 2.58 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -280.61 | 1.715 |
| 30 | 2.68 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -276.27 | 1.742 |
| 31 | 2.78 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -271.74 | 1.771 |
| 32 | 2.88 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -267.01 | 1.802 |
| 33 | 2.98 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -262.07 | 1.836 |
| 34 | 3.08 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -256.93 | 1.873 |
| 35 | 3.17 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -251.60 | 1.912 |
| 36 | 3.27 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -246.05 | 1.956 |
| 37 | 3.37 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -240.31 | 2.002 |
| 38 | 3.47 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -234.37 | 2.053 |
| 39 | 3.57 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -228.22 | 2.108 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 103 di 314 |

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 40 | 3.67 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -221.87 | 2.169 |
| 41 | 3.77 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -213.49 | 2.254 |
| 42 | 3.87 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -204.07 | 2.358 |
| 43 | 3.97 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -194.45 | 2.475 |
| 44 | 4.06 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -184.63 | 2.606 |
| 45 | 4.16 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -174.60 | 2.756 |
| 46 | 4.26 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -164.37 | 2.927 |
| 47 | 4.36 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -153.94 | 3.126 |
| 48 | 4.46 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -143.31 | 3.358 |
| 49 | 4.56 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -132.48 | 3.632 |
| 50 | 4.66 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -121.44 | 3.962 |
| 51 | 4.76 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -110.21 | 4.366 |
| 52 | 4.86 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -98.77 | 4.872 |
| 53 | 4.95 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -87.13 | 5.523 |
| 54 | 5.05 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -75.29 | 6.391 |
| 55 | 5.15 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -63.24 | 7.608 |
| 56 | 5.25 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -51.00 | 9.435 |
| 57 | 5.35 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -38.55 | 12.481 |
| 58 | 5.45 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -25.90 | 18.576 |
| 59 | 5.55 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -13.05 | 36.865 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 341.04 | 0.00 | 100.000 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 1 | -1.00 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | 0.00 | 100.000 |
| 2 | -0.90 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -23.80 | 20.218 |
| 3 | -0.80 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -47.26 | 10.181 |
| 4 | -0.70 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -70.39 | 6.836 |
| 5 | -0.60 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -93.18 | 5.164 |
| 6 | -0.50 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -115.64 | 4.161 |
| 7 | -0.40 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -137.76 | 3.493 |
| 8 | 0.51 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -124.75 | 3.857 |
| 9 | 0.60 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -130.87 | 3.677 |
| 10 | 0.70 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -136.67 | 3.521 |
| 11 | 0.80 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -142.13 | 3.385 |
| 12 | 0.90 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -147.27 | 3.267 |
| 13 | 1.00 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -152.07 | 3.164 |
| 14 | 1.10 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -156.55 | 3.074 |
| 15 | 1.20 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -160.71 | 2.994 |
| 16 | 1.30 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -164.53 | 2.925 |
| 17 | 1.40 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -168.02 | 2.864 |
| 18 | 1.49 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -171.19 | 2.811 |
| 19 | 1.59 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -174.03 | 2.765 |
| 20 | 1.69 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -176.54 | 2.726 |
| 21 | 1.79 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -178.72 | 2.692 |
| 22 | 1.89 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -180.57 | 2.665 |
| 23 | 1.99 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -182.10 | 2.642 |
| 24 | 2.09 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -183.30 | 2.625 |
| 25 | 2.19 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -184.16 | 2.613 |
| 26 | 2.29 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -184.71 | 2.605 |
| 27 | 2.38 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -184.92 | 2.602 |
| 28 | 2.48 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -184.80 | 2.604 |
| 29 | 2.58 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -184.36 | 2.610 |
| 30 | 2.68 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -183.59 | 2.621 |
| 31 | 2.78 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -182.48 | 2.637 |
| 32 | 2.88 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -181.06 | 2.658 |
| 33 | 2.98 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -179.30 | 2.684 |
| 34 | 3.08 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -177.21 | 2.715 |
| 35 | 3.17 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -174.80 | 2.753 |
| 36 | 3.27 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -172.06 | 2.797 |
| 37 | 3.37 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -168.99 | 2.847 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 104 di 314 |

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 38 | 3.47 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -165.59 | 2.906 |
| 39 | 3.57 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -161.86 | 2.973 |
| 40 | 3.67 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -157.81 | 3.049 |
| 41 | 3.77 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -153.15 | 3.142 |
| 42 | 3.87 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -148.05 | 3.250 |
| 43 | 3.97 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -142.61 | 3.374 |
| 44 | 4.06 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -136.85 | 3.516 |
| 45 | 4.16 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -130.76 | 3.680 |
| 46 | 4.26 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -124.34 | 3.870 |
| 47 | 4.36 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -117.59 | 4.092 |
| 48 | 4.46 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -110.52 | 4.354 |
| 49 | 4.56 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -103.11 | 4.667 |
| 50 | 4.66 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -95.38 | 5.045 |
| 51 | 4.76 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -87.32 | 5.511 |
| 52 | 4.86 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -78.93 | 6.096 |
| 53 | 4.95 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -70.21 | 6.853 |
| 54 | 5.05 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -61.17 | 7.867 |
| 55 | 5.15 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -51.79 | 9.291 |
| 56 | 5.25 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -42.09 | 11.432 |
| 57 | 5.35 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -32.06 | 15.009 |
| 58 | 5.45 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -21.70 | 22.172 |
| 59 | 5.55 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -11.01 | 43.684 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 341.04 | 0.00 | 100.000 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 1 | -1.00 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | 0.00 | 100.000 |
| 2 | -0.90 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -21.54 | 22.341 |
| 3 | -0.80 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -42.75 | 11.255 |
| 4 | -0.70 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -63.64 | 7.561 |
| 5 | -0.60 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -84.20 | 5.714 |
| 6 | -0.50 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -104.44 | 4.607 |
| 7 | -0.40 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -124.36 | 3.869 |
| 8 | 0.51 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -217.44 | 2.213 |
| 9 | 0.60 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -221.49 | 2.172 |
| 10 | 0.70 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -225.23 | 2.136 |
| 11 | 0.80 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -228.65 | 2.104 |
| 12 | 0.90 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -231.75 | 2.076 |
| 13 | 1.00 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -234.54 | 2.052 |
| 14 | 1.10 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -237.01 | 2.030 |
| 15 | 1.20 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -239.16 | 2.012 |
| 16 | 1.30 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -241.00 | 1.997 |
| 17 | 1.40 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -242.51 | 1.984 |
| 18 | 1.49 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -243.71 | 1.974 |
| 19 | 1.59 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -244.60 | 1.967 |
| 20 | 1.69 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -245.16 | 1.963 |
| 21 | 1.79 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -245.41 | 1.961 |
| 22 | 1.89 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -245.35 | 1.961 |
| 23 | 1.99 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -244.96 | 1.964 |
| 24 | 2.09 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -244.26 | 1.970 |
| 25 | 2.19 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -243.24 | 1.978 |
| 26 | 2.29 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -241.90 | 1.989 |
| 27 | 2.38 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -240.25 | 2.003 |
| 28 | 2.48 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -238.28 | 2.019 |
| 29 | 2.58 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -235.99 | 2.039 |
| 30 | 2.68 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -233.39 | 2.062 |
| 31 | 2.78 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -230.46 | 2.088 |
| 32 | 2.88 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -227.23 | 2.118 |
| 33 | 2.98 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -223.67 | 2.151 |
| 34 | 3.08 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -219.80 | 2.189 |
| 35 | 3.17 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -215.61 | 2.232 |

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 36 | 3.27 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -211.10 | 2.279 |
| 37 | 3.37 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -206.27 | 2.333 |
| 38 | 3.47 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -201.13 | 2.392 |
| 39 | 3.57 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -195.67 | 2.459 |
| 40 | 3.67 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -189.90 | 2.534 |
| 41 | 3.77 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -183.53 | 2.622 |
| 42 | 3.87 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -176.73 | 2.723 |
| 43 | 3.97 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -169.60 | 2.837 |
| 44 | 4.06 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -162.17 | 2.967 |
| 45 | 4.16 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -154.41 | 3.116 |
| 46 | 4.26 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -146.33 | 3.288 |
| 47 | 4.36 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -137.94 | 3.488 |
| 48 | 4.46 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -129.23 | 3.723 |
| 49 | 4.56 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -120.21 | 4.003 |
| 50 | 4.66 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -110.87 | 4.340 |
| 51 | 4.76 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -101.21 | 4.754 |
| 52 | 4.86 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -91.23 | 5.274 |
| 53 | 4.95 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -80.94 | 5.945 |
| 54 | 5.05 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -70.33 | 6.842 |
| 55 | 5.15 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -59.40 | 8.101 |
| 56 | 5.25 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -48.15 | 9.993 |
| 57 | 5.35 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -36.59 | 13.151 |
| 58 | 5.45 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -24.71 | 19.473 |
| 59 | 5.55 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -12.51 | 38.452 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 341.04 | 0.00 | 100.000 |

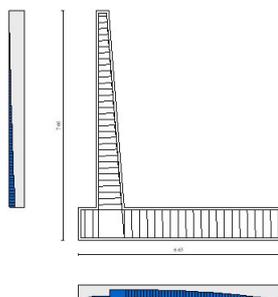


Fig. 11 - Paramento (Inviluppo)

Verifica delle tensioni

Simbologia adottata

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
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| | |
|---------------|---|
| n° | indice sezione |
| Y | ordinata sezione, espressa in [m] |
| B | larghezza sezione, espresso in [cm] |
| H | altezza sezione, espressa in [cm] |
| Afi | area ferri inferiori, espresso in [cmq] |
| Afs | area ferri superiori, espressa in [cmq] |
| M | momento agente, espressa in [kNm] |
| N | sforzo normale agente, espressa in [kN] |
| σ_c | tensione di compressione nel cls, espressa in [kPa] |
| σ_{fi} | tensione nei ferri inferiori, espressa in [kPa] |
| σ_{fs} | tensione nei ferri superiori, espressa in [kPa] |

Combinazioni SLER

Paramento

Combinazione n° 10 - SLER

| | | |
|---|--------|-------|
| Tensione massima di compressione nel calcestruzzo | 19920 | [kPa] |
| Tensione massima di trazione dell'acciaio | 360000 | [kPa] |

| n° | Y | B | H | Afi | Afs | M | N | σ_c | σ_{fi} | σ_{fs} |
|----|-------|------|------|-------|-------|-------|-------|------------|---------------|---------------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
| 1 | 0.00 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.10 | 100 | 41 | 26.55 | 53.09 | 0.00 | 0.99 | 2 | 25 | 32 |
| 3 | -0.20 | 100 | 42 | 26.55 | 53.09 | 0.02 | 2.00 | 5 | 47 | 66 |
| 4 | -0.30 | 100 | 42 | 26.55 | 53.09 | 0.04 | 3.03 | 7 | 66 | 104 |
| 5 | -0.40 | 100 | 43 | 26.55 | 53.09 | 0.09 | 4.08 | 11 | 80 | 147 |
| 6 | -0.50 | 100 | 44 | 26.55 | 53.09 | 0.17 | 5.14 | 14 | 89 | 195 |
| 7 | -0.60 | 100 | 45 | 26.55 | 53.09 | 0.28 | 6.23 | 19 | 91 | 251 |
| 8 | -0.70 | 100 | 45 | 26.55 | 53.09 | 0.42 | 7.33 | 24 | 86 | 313 |
| 9 | -0.80 | 100 | 46 | 26.55 | 53.09 | 0.62 | 8.46 | 30 | 73 | 385 |
| 10 | -0.90 | 100 | 47 | 26.55 | 53.09 | 0.86 | 9.60 | 36 | 50 | 466 |
| 11 | -1.00 | 100 | 48 | 26.55 | 53.09 | 1.17 | 10.76 | 44 | 9 | 560 |
| 12 | -1.10 | 100 | 49 | 26.55 | 53.09 | 1.54 | 11.94 | 53 | 56 | 668 |
| 13 | -1.20 | 100 | 49 | 26.55 | 53.09 | 1.98 | 13.14 | 64 | 149 | 791 |
| 14 | -1.30 | 100 | 50 | 26.55 | 53.09 | 2.50 | 14.36 | 76 | 272 | 929 |
| 15 | -1.40 | 100 | 51 | 26.55 | 53.09 | 3.11 | 15.60 | 89 | 427 | 1081 |
| 16 | -1.50 | 100 | 52 | 26.55 | 53.09 | 3.81 | 16.86 | 104 | 616 | 1248 |
| 17 | -1.60 | 100 | 52 | 26.55 | 53.09 | 4.60 | 18.13 | 120 | 839 | 1430 |
| 18 | -1.70 | 100 | 53 | 26.55 | 53.09 | 5.49 | 19.43 | 137 | 1098 | 1626 |
| 19 | -1.80 | 100 | 54 | 26.55 | 53.09 | 6.50 | 20.74 | 156 | 1393 | 1837 |
| 20 | -1.90 | 100 | 55 | 26.55 | 53.09 | 7.61 | 22.08 | 176 | 1724 | 2062 |
| 21 | -2.00 | 100 | 56 | 26.55 | 53.09 | 8.85 | 23.43 | 197 | 2091 | 2302 |
| 22 | -2.10 | 100 | 56 | 26.55 | 53.09 | 10.21 | 24.80 | 220 | 2496 | 2557 |

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 23 | -2.20 | 100 | 57 | 26.55 | 53.09 | 11.70 | 26.19 | 244 | 2939 | 2826 |
| 24 | -2.30 | 100 | 58 | 26.55 | 53.09 | 13.33 | 27.60 | 269 | 3420 | 3109 |
| 25 | -2.40 | 100 | 59 | 26.55 | 53.09 | 15.10 | 29.03 | 296 | 3939 | 3408 |
| 26 | -2.50 | 100 | 59 | 26.55 | 53.09 | 17.02 | 30.48 | 323 | 4497 | 3721 |
| 27 | -2.60 | 100 | 60 | 26.55 | 53.09 | 19.09 | 31.95 | 352 | 5095 | 4049 |
| 28 | -2.70 | 100 | 61 | 26.55 | 53.09 | 21.32 | 33.43 | 382 | 5733 | 4391 |
| 29 | -2.80 | 100 | 62 | 26.55 | 53.09 | 23.72 | 34.94 | 414 | 6410 | 4748 |
| 30 | -2.90 | 100 | 63 | 26.55 | 53.09 | 26.29 | 36.46 | 446 | 7128 | 5120 |
| 31 | -3.00 | 100 | 63 | 26.55 | 53.09 | 29.04 | 38.01 | 480 | 7887 | 5507 |
| 32 | -3.10 | 100 | 64 | 26.55 | 53.09 | 31.97 | 39.57 | 515 | 8687 | 5908 |
| 33 | -3.20 | 100 | 65 | 26.55 | 53.09 | 35.08 | 41.15 | 551 | 9528 | 6324 |
| 34 | -3.30 | 100 | 66 | 26.55 | 53.09 | 38.40 | 42.75 | 589 | 10411 | 6754 |
| 35 | -3.40 | 100 | 66 | 26.55 | 53.09 | 41.91 | 44.37 | 627 | 11335 | 7199 |
| 36 | -3.50 | 100 | 67 | 26.55 | 53.09 | 45.63 | 46.01 | 667 | 12302 | 7658 |
| 37 | -3.60 | 100 | 68 | 26.55 | 53.09 | 49.56 | 47.67 | 708 | 13311 | 8131 |
| 38 | -3.70 | 100 | 69 | 26.55 | 53.09 | 53.70 | 49.35 | 750 | 14362 | 8619 |
| 39 | -3.80 | 100 | 70 | 26.55 | 53.09 | 58.08 | 51.04 | 793 | 15456 | 9121 |
| 40 | -3.90 | 100 | 70 | 26.55 | 53.09 | 62.68 | 52.76 | 837 | 16593 | 9637 |
| 41 | -4.00 | 100 | 71 | 26.55 | 53.09 | 67.51 | 54.49 | 882 | 17773 | 10168 |
| 42 | -4.10 | 100 | 72 | 26.55 | 53.09 | 72.59 | 56.24 | 929 | 18996 | 10712 |
| 43 | -4.20 | 100 | 73 | 26.55 | 53.09 | 77.91 | 58.02 | 976 | 20263 | 11270 |
| 44 | -4.30 | 100 | 73 | 26.55 | 53.09 | 83.48 | 59.81 | 1025 | 21573 | 11842 |
| 45 | -4.40 | 100 | 74 | 26.55 | 53.09 | 89.31 | 61.62 | 1074 | 22927 | 12428 |
| 46 | -4.50 | 100 | 75 | 26.55 | 53.09 | 95.41 | 63.45 | 1125 | 24325 | 13028 |
| 47 | -4.60 | 100 | 76 | 26.55 | 53.09 | 101.77 | 65.30 | 1176 | 25767 | 13641 |
| 48 | -4.70 | 100 | 77 | 26.55 | 53.09 | 108.41 | 67.17 | 1229 | 27253 | 14267 |
| 49 | -4.80 | 100 | 77 | 26.55 | 53.09 | 115.34 | 69.05 | 1283 | 28783 | 14908 |
| 50 | -4.90 | 100 | 78 | 26.55 | 53.09 | 122.54 | 70.96 | 1337 | 30358 | 15561 |
| 51 | -5.00 | 100 | 79 | 26.55 | 53.09 | 130.04 | 72.88 | 1393 | 31977 | 16228 |
| 52 | -5.10 | 100 | 80 | 26.55 | 53.09 | 137.84 | 74.83 | 1450 | 33641 | 16908 |
| 53 | -5.20 | 100 | 80 | 26.55 | 53.09 | 145.95 | 76.79 | 1507 | 35349 | 17601 |
| 54 | -5.30 | 100 | 81 | 26.55 | 53.09 | 154.36 | 78.77 | 1566 | 37102 | 18307 |
| 55 | -5.40 | 100 | 82 | 26.55 | 53.09 | 163.09 | 80.78 | 1625 | 38900 | 19026 |
| 56 | -5.50 | 100 | 83 | 26.55 | 53.09 | 172.14 | 82.80 | 1686 | 40743 | 19758 |
| 57 | -5.60 | 100 | 84 | 26.55 | 53.09 | 181.51 | 84.84 | 1747 | 42631 | 20503 |
| 58 | -5.70 | 100 | 84 | 26.55 | 53.09 | 191.22 | 86.89 | 1810 | 44564 | 21260 |
| 59 | -5.80 | 100 | 85 | 26.55 | 53.09 | 201.27 | 88.97 | 1873 | 46542 | 22030 |
| 60 | -5.90 | 100 | 86 | 26.55 | 53.09 | 211.67 | 91.07 | 1937 | 48568 | 22814 |
| 61 | -6.00 | 100 | 87 | 26.55 | 53.09 | 222.45 | 93.18 | 2003 | 50644 | 23612 |
| 62 | -6.10 | 100 | 87 | 26.55 | 53.09 | 233.61 | 95.32 | 2069 | 52774 | 24425 |
| 63 | -6.20 | 100 | 88 | 26.55 | 53.09 | 245.17 | 97.47 | 2137 | 54959 | 25254 |
| 64 | -6.30 | 100 | 89 | 26.55 | 53.09 | 257.15 | 99.65 | 2206 | 57201 | 26100 |
| 65 | -6.40 | 100 | 90 | 26.55 | 53.09 | 269.54 | 101.84 | 2276 | 59501 | 26962 |
| 66 | -6.50 | 100 | 91 | 26.55 | 53.09 | 282.37 | 104.05 | 2348 | 61857 | 27840 |

Fondazione

Combinazione n° 10 - SLER

Tensione massima di compressione nel calcestruzzo 17430 [kPa]

Tensione massima di trazione dell'acciaio 360000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | -1.00 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.90 | 100 | 110 | 45.24 | 22.62 | 0.85 | 0.00 | 5 | 199 | 61 |
| 3 | -0.80 | 100 | 110 | 45.24 | 22.62 | 3.38 | 0.00 | 21 | 792 | 243 |
| 4 | -0.70 | 100 | 110 | 45.24 | 22.62 | 7.58 | 0.00 | 47 | 1777 | 545 |
| 5 | -0.60 | 100 | 110 | 45.24 | 22.62 | 13.45 | 0.00 | 83 | 3150 | 967 |
| 6 | -0.50 | 100 | 110 | 45.24 | 22.62 | 20.95 | 0.00 | 129 | 4908 | 1507 |
| 7 | -0.40 | 100 | 110 | 45.24 | 22.62 | 30.09 | 0.00 | 185 | 7047 | 2163 |
| 8 | 0.51 | 100 | 110 | 22.62 | 45.24 | -428.05 | 0.00 | 2627 | 30780 | 100265 |
| 9 | 0.60 | 100 | 110 | 22.62 | 45.24 | -419.51 | 0.00 | 2575 | 30166 | 98265 |
| 10 | 0.70 | 100 | 110 | 22.62 | 45.24 | -410.76 | 0.00 | 2521 | 29536 | 96215 |
| 11 | 0.80 | 100 | 110 | 22.62 | 45.24 | -401.81 | 0.00 | 2466 | 28893 | 94118 |
| 12 | 0.90 | 100 | 110 | 22.62 | 45.24 | -392.67 | 0.00 | 2410 | 28235 | 91978 |
| 13 | 1.00 | 100 | 110 | 22.62 | 45.24 | -383.36 | 0.00 | 2353 | 27566 | 89796 |
| 14 | 1.10 | 100 | 110 | 22.62 | 45.24 | -373.88 | 0.00 | 2295 | 26885 | 87577 |
| 15 | 1.20 | 100 | 110 | 22.62 | 45.24 | -364.27 | 0.00 | 2236 | 26193 | 85324 |
| 16 | 1.30 | 100 | 110 | 22.62 | 45.24 | -354.51 | 0.00 | 2176 | 25492 | 83040 |
| 17 | 1.40 | 100 | 110 | 22.62 | 45.24 | -344.64 | 0.00 | 2115 | 24782 | 80728 |
| 18 | 1.49 | 100 | 110 | 22.62 | 45.24 | -334.67 | 0.00 | 2054 | 24065 | 78391 |
| 19 | 1.59 | 100 | 110 | 22.62 | 45.24 | -324.60 | 0.00 | 1992 | 23341 | 76033 |
| 20 | 1.69 | 100 | 110 | 22.62 | 45.24 | -314.45 | 0.00 | 1930 | 22611 | 73656 |
| 21 | 1.79 | 100 | 110 | 22.62 | 45.24 | -304.24 | 0.00 | 1867 | 21877 | 71264 |
| 22 | 1.89 | 100 | 110 | 22.62 | 45.24 | -293.98 | 0.00 | 1804 | 21139 | 68860 |
| 23 | 1.99 | 100 | 110 | 22.62 | 45.24 | -283.68 | 0.00 | 1741 | 20398 | 66447 |
| 24 | 2.09 | 100 | 110 | 22.62 | 45.24 | -273.35 | 0.00 | 1678 | 19656 | 64029 |
| 25 | 2.19 | 100 | 110 | 22.62 | 45.24 | -263.02 | 0.00 | 1614 | 18913 | 61608 |
| 26 | 2.29 | 100 | 110 | 22.62 | 45.24 | -252.68 | 0.00 | 1551 | 18170 | 59188 |
| 27 | 2.38 | 100 | 110 | 22.62 | 45.24 | -242.37 | 0.00 | 1488 | 17428 | 56771 |
| 28 | 2.48 | 100 | 110 | 22.62 | 45.24 | -232.08 | 0.00 | 1424 | 16688 | 54362 |
| 29 | 2.58 | 100 | 110 | 22.62 | 45.24 | -221.84 | 0.00 | 1362 | 15952 | 51963 |
| 30 | 2.68 | 100 | 110 | 22.62 | 45.24 | -211.65 | 0.00 | 1299 | 15219 | 49577 |
| 31 | 2.78 | 100 | 110 | 22.62 | 45.24 | -201.54 | 0.00 | 1237 | 14492 | 47208 |
| 32 | 2.88 | 100 | 110 | 22.62 | 45.24 | -191.51 | 0.00 | 1175 | 13771 | 44859 |
| 33 | 2.98 | 100 | 110 | 22.62 | 45.24 | -181.58 | 0.00 | 1114 | 13057 | 42532 |
| 34 | 3.08 | 100 | 110 | 22.62 | 45.24 | -171.76 | 0.00 | 1054 | 12350 | 40232 |
| 35 | 3.17 | 100 | 110 | 22.62 | 45.24 | -162.06 | 0.00 | 995 | 11653 | 37961 |
| 36 | 3.27 | 100 | 110 | 22.62 | 45.24 | -152.51 | 0.00 | 936 | 10966 | 35722 |
| 37 | 3.37 | 100 | 110 | 22.62 | 45.24 | -143.10 | 0.00 | 878 | 10290 | 33519 |
| 38 | 3.47 | 100 | 110 | 22.62 | 45.24 | -133.86 | 0.00 | 822 | 9626 | 31355 |
| 39 | 3.57 | 100 | 110 | 22.62 | 45.24 | -124.80 | 0.00 | 766 | 8974 | 29233 |
| 40 | 3.67 | 100 | 110 | 22.62 | 45.24 | -115.94 | 0.00 | 712 | 8337 | 27156 |
| 41 | 3.77 | 100 | 110 | 22.62 | 45.24 | -106.00 | 0.00 | 651 | 7622 | 24830 |
| 42 | 3.87 | 100 | 110 | 22.62 | 45.24 | -95.87 | 0.00 | 588 | 6894 | 22456 |
| 43 | 3.97 | 100 | 110 | 22.62 | 45.24 | -86.17 | 0.00 | 529 | 6196 | 20184 |
| 44 | 4.06 | 100 | 110 | 22.62 | 45.24 | -76.91 | 0.00 | 472 | 5530 | 18015 |
| 45 | 4.16 | 100 | 110 | 22.62 | 45.24 | -68.10 | 0.00 | 418 | 4897 | 15952 |
| 46 | 4.26 | 100 | 110 | 22.62 | 45.24 | -59.77 | 0.00 | 367 | 4298 | 14000 |
| 47 | 4.36 | 100 | 110 | 22.62 | 45.24 | -51.92 | 0.00 | 319 | 3733 | 12161 |
| 48 | 4.46 | 100 | 110 | 22.62 | 45.24 | -44.56 | 0.00 | 274 | 3204 | 10438 |
| 49 | 4.56 | 100 | 110 | 22.62 | 45.24 | -37.72 | 0.00 | 232 | 2712 | 8835 |
| 50 | 4.66 | 100 | 110 | 22.62 | 45.24 | -31.40 | 0.00 | 193 | 2258 | 7355 |
| 51 | 4.76 | 100 | 110 | 22.62 | 45.24 | -25.62 | 0.00 | 157 | 1842 | 6000 |
| 52 | 4.86 | 100 | 110 | 22.62 | 45.24 | -20.38 | 0.00 | 125 | 1466 | 4775 |
| 53 | 4.95 | 100 | 110 | 22.62 | 45.24 | -15.72 | 0.00 | 96 | 1130 | 3682 |
| 54 | 5.05 | 100 | 110 | 22.62 | 45.24 | -11.63 | 0.00 | 71 | 836 | 2724 |
| 55 | 5.15 | 100 | 110 | 22.62 | 45.24 | -8.13 | 0.00 | 50 | 585 | 1905 |
| 56 | 5.25 | 100 | 110 | 22.62 | 45.24 | -5.24 | 0.00 | 32 | 377 | 1228 |
| 57 | 5.35 | 100 | 110 | 22.62 | 45.24 | -2.97 | 0.00 | 18 | 213 | 695 |
| 58 | 5.45 | 100 | 110 | 22.62 | 45.24 | -1.33 | 0.00 | 8 | 96 | 311 |
| 59 | 5.55 | 100 | 110 | 22.62 | 45.24 | -0.33 | 0.00 | 2 | 24 | 78 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

Combinazioni SLEF

Paramento

Combinazione n° 11 - SLEF

Tensione massima di compressione nel calcestruzzo 33200 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y | B | H | Afi | Afs | M | N | σc | σfi | σfs |
|----|-------|------|------|-------|-------|--------|-------|-------|-------|-------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
| 1 | 0.00 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.10 | 100 | 41 | 26.55 | 53.09 | 0.00 | 0.99 | 2 | 25 | 32 |
| 3 | -0.20 | 100 | 42 | 26.55 | 53.09 | 0.02 | 2.00 | 5 | 47 | 66 |
| 4 | -0.30 | 100 | 42 | 26.55 | 53.09 | 0.04 | 3.03 | 7 | 66 | 104 |
| 5 | -0.40 | 100 | 43 | 26.55 | 53.09 | 0.09 | 4.08 | 11 | 80 | 147 |
| 6 | -0.50 | 100 | 44 | 26.55 | 53.09 | 0.17 | 5.14 | 14 | 89 | 195 |
| 7 | -0.60 | 100 | 45 | 26.55 | 53.09 | 0.28 | 6.23 | 19 | 91 | 251 |
| 8 | -0.70 | 100 | 45 | 26.55 | 53.09 | 0.42 | 7.33 | 24 | 86 | 313 |
| 9 | -0.80 | 100 | 46 | 26.55 | 53.09 | 0.62 | 8.46 | 30 | 73 | 385 |
| 10 | -0.90 | 100 | 47 | 26.55 | 53.09 | 0.86 | 9.60 | 36 | 50 | 466 |
| 11 | -1.00 | 100 | 48 | 26.55 | 53.09 | 1.17 | 10.76 | 44 | 9 | 560 |
| 12 | -1.10 | 100 | 49 | 26.55 | 53.09 | 1.54 | 11.94 | 53 | 56 | 668 |
| 13 | -1.20 | 100 | 49 | 26.55 | 53.09 | 1.98 | 13.14 | 64 | 149 | 791 |
| 14 | -1.30 | 100 | 50 | 26.55 | 53.09 | 2.50 | 14.36 | 76 | 272 | 929 |
| 15 | -1.40 | 100 | 51 | 26.55 | 53.09 | 3.11 | 15.60 | 89 | 427 | 1081 |
| 16 | -1.50 | 100 | 52 | 26.55 | 53.09 | 3.81 | 16.86 | 104 | 616 | 1248 |
| 17 | -1.60 | 100 | 52 | 26.55 | 53.09 | 4.60 | 18.13 | 120 | 839 | 1430 |
| 18 | -1.70 | 100 | 53 | 26.55 | 53.09 | 5.49 | 19.43 | 137 | 1098 | 1626 |
| 19 | -1.80 | 100 | 54 | 26.55 | 53.09 | 6.50 | 20.74 | 156 | 1393 | 1837 |
| 20 | -1.90 | 100 | 55 | 26.55 | 53.09 | 7.61 | 22.08 | 176 | 1724 | 2062 |
| 21 | -2.00 | 100 | 56 | 26.55 | 53.09 | 8.85 | 23.43 | 197 | 2091 | 2302 |
| 22 | -2.10 | 100 | 56 | 26.55 | 53.09 | 10.21 | 24.80 | 220 | 2496 | 2557 |
| 23 | -2.20 | 100 | 57 | 26.55 | 53.09 | 11.70 | 26.19 | 244 | 2939 | 2826 |
| 24 | -2.30 | 100 | 58 | 26.55 | 53.09 | 13.33 | 27.60 | 269 | 3420 | 3109 |
| 25 | -2.40 | 100 | 59 | 26.55 | 53.09 | 15.10 | 29.03 | 296 | 3939 | 3408 |
| 26 | -2.50 | 100 | 59 | 26.55 | 53.09 | 17.02 | 30.48 | 323 | 4497 | 3721 |
| 27 | -2.60 | 100 | 60 | 26.55 | 53.09 | 19.09 | 31.95 | 352 | 5095 | 4049 |
| 28 | -2.70 | 100 | 61 | 26.55 | 53.09 | 21.32 | 33.43 | 382 | 5733 | 4391 |
| 29 | -2.80 | 100 | 62 | 26.55 | 53.09 | 23.72 | 34.94 | 414 | 6410 | 4748 |
| 30 | -2.90 | 100 | 63 | 26.55 | 53.09 | 26.29 | 36.46 | 446 | 7128 | 5120 |
| 31 | -3.00 | 100 | 63 | 26.55 | 53.09 | 29.04 | 38.01 | 480 | 7887 | 5507 |
| 32 | -3.10 | 100 | 64 | 26.55 | 53.09 | 31.97 | 39.57 | 515 | 8687 | 5908 |
| 33 | -3.20 | 100 | 65 | 26.55 | 53.09 | 35.08 | 41.15 | 551 | 9528 | 6324 |
| 34 | -3.30 | 100 | 66 | 26.55 | 53.09 | 38.40 | 42.75 | 589 | 10411 | 6754 |
| 35 | -3.40 | 100 | 66 | 26.55 | 53.09 | 41.91 | 44.37 | 627 | 11335 | 7199 |
| 36 | -3.50 | 100 | 67 | 26.55 | 53.09 | 45.63 | 46.01 | 667 | 12302 | 7658 |
| 37 | -3.60 | 100 | 68 | 26.55 | 53.09 | 49.56 | 47.67 | 708 | 13311 | 8131 |
| 38 | -3.70 | 100 | 69 | 26.55 | 53.09 | 53.70 | 49.35 | 750 | 14362 | 8619 |
| 39 | -3.80 | 100 | 70 | 26.55 | 53.09 | 58.08 | 51.04 | 793 | 15456 | 9121 |
| 40 | -3.90 | 100 | 70 | 26.55 | 53.09 | 62.68 | 52.76 | 837 | 16593 | 9637 |
| 41 | -4.00 | 100 | 71 | 26.55 | 53.09 | 67.51 | 54.49 | 882 | 17773 | 10168 |
| 42 | -4.10 | 100 | 72 | 26.55 | 53.09 | 72.59 | 56.24 | 929 | 18996 | 10712 |
| 43 | -4.20 | 100 | 73 | 26.55 | 53.09 | 77.91 | 58.02 | 976 | 20263 | 11270 |
| 44 | -4.30 | 100 | 73 | 26.55 | 53.09 | 83.48 | 59.81 | 1025 | 21573 | 11842 |
| 45 | -4.40 | 100 | 74 | 26.55 | 53.09 | 89.31 | 61.62 | 1074 | 22927 | 12428 |
| 46 | -4.50 | 100 | 75 | 26.55 | 53.09 | 95.41 | 63.45 | 1125 | 24325 | 13028 |
| 47 | -4.60 | 100 | 76 | 26.55 | 53.09 | 101.77 | 65.30 | 1176 | 25767 | 13641 |

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
NM25 03 D 26 CL NV 24 05 001 A 110 di 314

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 48 | -4.70 | 100 | 77 | 26.55 | 53.09 | 108.41 | 67.17 | 1229 | 27253 | 14267 |
| 49 | -4.80 | 100 | 77 | 26.55 | 53.09 | 115.34 | 69.05 | 1283 | 28783 | 14908 |
| 50 | -4.90 | 100 | 78 | 26.55 | 53.09 | 122.54 | 70.96 | 1337 | 30358 | 15561 |
| 51 | -5.00 | 100 | 79 | 26.55 | 53.09 | 130.04 | 72.88 | 1393 | 31977 | 16228 |
| 52 | -5.10 | 100 | 80 | 26.55 | 53.09 | 137.84 | 74.83 | 1450 | 33641 | 16908 |
| 53 | -5.20 | 100 | 80 | 26.55 | 53.09 | 145.95 | 76.79 | 1507 | 35349 | 17601 |
| 54 | -5.30 | 100 | 81 | 26.55 | 53.09 | 154.36 | 78.77 | 1566 | 37102 | 18307 |
| 55 | -5.40 | 100 | 82 | 26.55 | 53.09 | 163.09 | 80.78 | 1625 | 38900 | 19026 |
| 56 | -5.50 | 100 | 83 | 26.55 | 53.09 | 172.14 | 82.80 | 1686 | 40743 | 19758 |
| 57 | -5.60 | 100 | 84 | 26.55 | 53.09 | 181.51 | 84.84 | 1747 | 42631 | 20503 |
| 58 | -5.70 | 100 | 84 | 26.55 | 53.09 | 191.22 | 86.89 | 1810 | 44564 | 21260 |
| 59 | -5.80 | 100 | 85 | 26.55 | 53.09 | 201.27 | 88.97 | 1873 | 46542 | 22030 |
| 60 | -5.90 | 100 | 86 | 26.55 | 53.09 | 211.67 | 91.07 | 1937 | 48568 | 22814 |
| 61 | -6.00 | 100 | 87 | 26.55 | 53.09 | 222.45 | 93.18 | 2003 | 50644 | 23612 |
| 62 | -6.10 | 100 | 87 | 26.55 | 53.09 | 233.61 | 95.32 | 2069 | 52774 | 24425 |
| 63 | -6.20 | 100 | 88 | 26.55 | 53.09 | 245.17 | 97.47 | 2137 | 54959 | 25254 |
| 64 | -6.30 | 100 | 89 | 26.55 | 53.09 | 257.15 | 99.65 | 2206 | 57201 | 26100 |
| 65 | -6.40 | 100 | 90 | 26.55 | 53.09 | 269.54 | 101.84 | 2276 | 59501 | 26962 |
| 66 | -6.50 | 100 | 91 | 26.55 | 53.09 | 282.37 | 104.05 | 2348 | 61857 | 27840 |

Fondazione

Combinazione n° 11 - SLEF

Tensione massima di compressione nel calcestruzzo 29050 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | -1.00 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.90 | 100 | 110 | 45.24 | 22.62 | 0.85 | 0.00 | 5 | 199 | 61 |
| 3 | -0.80 | 100 | 110 | 45.24 | 22.62 | 3.38 | 0.00 | 21 | 792 | 243 |
| 4 | -0.70 | 100 | 110 | 45.24 | 22.62 | 7.58 | 0.00 | 47 | 1777 | 545 |
| 5 | -0.60 | 100 | 110 | 45.24 | 22.62 | 13.45 | 0.00 | 83 | 3150 | 967 |
| 6 | -0.50 | 100 | 110 | 45.24 | 22.62 | 20.95 | 0.00 | 129 | 4908 | 1507 |
| 7 | -0.40 | 100 | 110 | 45.24 | 22.62 | 30.09 | 0.00 | 185 | 7047 | 2163 |
| 8 | 0.51 | 100 | 110 | 22.62 | 45.24 | -428.05 | 0.00 | 2627 | 30780 | 100265 |
| 9 | 0.60 | 100 | 110 | 22.62 | 45.24 | -419.51 | 0.00 | 2575 | 30166 | 98265 |
| 10 | 0.70 | 100 | 110 | 22.62 | 45.24 | -410.76 | 0.00 | 2521 | 29536 | 96215 |
| 11 | 0.80 | 100 | 110 | 22.62 | 45.24 | -401.81 | 0.00 | 2466 | 28893 | 94118 |
| 12 | 0.90 | 100 | 110 | 22.62 | 45.24 | -392.67 | 0.00 | 2410 | 28235 | 91978 |
| 13 | 1.00 | 100 | 110 | 22.62 | 45.24 | -383.36 | 0.00 | 2353 | 27566 | 89796 |
| 14 | 1.10 | 100 | 110 | 22.62 | 45.24 | -373.88 | 0.00 | 2295 | 26885 | 87577 |
| 15 | 1.20 | 100 | 110 | 22.62 | 45.24 | -364.27 | 0.00 | 2236 | 26193 | 85324 |
| 16 | 1.30 | 100 | 110 | 22.62 | 45.24 | -354.51 | 0.00 | 2176 | 25492 | 83040 |
| 17 | 1.40 | 100 | 110 | 22.62 | 45.24 | -344.64 | 0.00 | 2115 | 24782 | 80728 |
| 18 | 1.49 | 100 | 110 | 22.62 | 45.24 | -334.67 | 0.00 | 2054 | 24065 | 78391 |
| 19 | 1.59 | 100 | 110 | 22.62 | 45.24 | -324.60 | 0.00 | 1992 | 23341 | 76033 |
| 20 | 1.69 | 100 | 110 | 22.62 | 45.24 | -314.45 | 0.00 | 1930 | 22611 | 73656 |
| 21 | 1.79 | 100 | 110 | 22.62 | 45.24 | -304.24 | 0.00 | 1867 | 21877 | 71264 |
| 22 | 1.89 | 100 | 110 | 22.62 | 45.24 | -293.98 | 0.00 | 1804 | 21139 | 68860 |
| 23 | 1.99 | 100 | 110 | 22.62 | 45.24 | -283.68 | 0.00 | 1741 | 20398 | 66447 |
| 24 | 2.09 | 100 | 110 | 22.62 | 45.24 | -273.35 | 0.00 | 1678 | 19656 | 64029 |
| 25 | 2.19 | 100 | 110 | 22.62 | 45.24 | -263.02 | 0.00 | 1614 | 18913 | 61608 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 111 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 26 | 2.29 | 100 | 110 | 22.62 | 45.24 | -252.68 | 0.00 | 1551 | 18170 | 59188 |
| 27 | 2.38 | 100 | 110 | 22.62 | 45.24 | -242.37 | 0.00 | 1488 | 17428 | 56771 |
| 28 | 2.48 | 100 | 110 | 22.62 | 45.24 | -232.08 | 0.00 | 1424 | 16688 | 54362 |
| 29 | 2.58 | 100 | 110 | 22.62 | 45.24 | -221.84 | 0.00 | 1362 | 15952 | 51963 |
| 30 | 2.68 | 100 | 110 | 22.62 | 45.24 | -211.65 | 0.00 | 1299 | 15219 | 49577 |
| 31 | 2.78 | 100 | 110 | 22.62 | 45.24 | -201.54 | 0.00 | 1237 | 14492 | 47208 |
| 32 | 2.88 | 100 | 110 | 22.62 | 45.24 | -191.51 | 0.00 | 1175 | 13771 | 44859 |
| 33 | 2.98 | 100 | 110 | 22.62 | 45.24 | -181.58 | 0.00 | 1114 | 13057 | 42532 |
| 34 | 3.08 | 100 | 110 | 22.62 | 45.24 | -171.76 | 0.00 | 1054 | 12350 | 40232 |
| 35 | 3.17 | 100 | 110 | 22.62 | 45.24 | -162.06 | 0.00 | 995 | 11653 | 37961 |
| 36 | 3.27 | 100 | 110 | 22.62 | 45.24 | -152.51 | 0.00 | 936 | 10966 | 35722 |
| 37 | 3.37 | 100 | 110 | 22.62 | 45.24 | -143.10 | 0.00 | 878 | 10290 | 33519 |
| 38 | 3.47 | 100 | 110 | 22.62 | 45.24 | -133.86 | 0.00 | 822 | 9626 | 31355 |
| 39 | 3.57 | 100 | 110 | 22.62 | 45.24 | -124.80 | 0.00 | 766 | 8974 | 29233 |
| 40 | 3.67 | 100 | 110 | 22.62 | 45.24 | -115.94 | 0.00 | 712 | 8337 | 27156 |
| 41 | 3.77 | 100 | 110 | 22.62 | 45.24 | -106.00 | 0.00 | 651 | 7622 | 24830 |
| 42 | 3.87 | 100 | 110 | 22.62 | 45.24 | -95.87 | 0.00 | 588 | 6894 | 22456 |
| 43 | 3.97 | 100 | 110 | 22.62 | 45.24 | -86.17 | 0.00 | 529 | 6196 | 20184 |
| 44 | 4.06 | 100 | 110 | 22.62 | 45.24 | -76.91 | 0.00 | 472 | 5530 | 18015 |
| 45 | 4.16 | 100 | 110 | 22.62 | 45.24 | -68.10 | 0.00 | 418 | 4897 | 15952 |
| 46 | 4.26 | 100 | 110 | 22.62 | 45.24 | -59.77 | 0.00 | 367 | 4298 | 14000 |
| 47 | 4.36 | 100 | 110 | 22.62 | 45.24 | -51.92 | 0.00 | 319 | 3733 | 12161 |
| 48 | 4.46 | 100 | 110 | 22.62 | 45.24 | -44.56 | 0.00 | 274 | 3204 | 10438 |
| 49 | 4.56 | 100 | 110 | 22.62 | 45.24 | -37.72 | 0.00 | 232 | 2712 | 8835 |
| 50 | 4.66 | 100 | 110 | 22.62 | 45.24 | -31.40 | 0.00 | 193 | 2258 | 7355 |
| 51 | 4.76 | 100 | 110 | 22.62 | 45.24 | -25.62 | 0.00 | 157 | 1842 | 6000 |
| 52 | 4.86 | 100 | 110 | 22.62 | 45.24 | -20.38 | 0.00 | 125 | 1466 | 4775 |
| 53 | 4.95 | 100 | 110 | 22.62 | 45.24 | -15.72 | 0.00 | 96 | 1130 | 3682 |
| 54 | 5.05 | 100 | 110 | 22.62 | 45.24 | -11.63 | 0.00 | 71 | 836 | 2724 |
| 55 | 5.15 | 100 | 110 | 22.62 | 45.24 | -8.13 | 0.00 | 50 | 585 | 1905 |
| 56 | 5.25 | 100 | 110 | 22.62 | 45.24 | -5.24 | 0.00 | 32 | 377 | 1228 |
| 57 | 5.35 | 100 | 110 | 22.62 | 45.24 | -2.97 | 0.00 | 18 | 213 | 695 |
| 58 | 5.45 | 100 | 110 | 22.62 | 45.24 | -1.33 | 0.00 | 8 | 96 | 311 |
| 59 | 5.55 | 100 | 110 | 22.62 | 45.24 | -0.33 | 0.00 | 2 | 24 | 78 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

Combinazioni SLEQ

Paramento

Combinazione n° 12 - SLEQ

Tensione massima di compressione nel calcestruzzo 14940 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | 0.00 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.10 | 100 | 41 | 26.55 | 53.09 | 0.00 | 0.99 | 2 | 25 | 32 |
| 3 | -0.20 | 100 | 42 | 26.55 | 53.09 | 0.02 | 2.00 | 5 | 47 | 66 |
| 4 | -0.30 | 100 | 42 | 26.55 | 53.09 | 0.04 | 3.03 | 7 | 66 | 104 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 112 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 5 | -0.40 | 100 | 43 | 26.55 | 53.09 | 0.09 | 4.08 | 11 | 80 | 147 |
| 6 | -0.50 | 100 | 44 | 26.55 | 53.09 | 0.17 | 5.14 | 14 | 89 | 195 |
| 7 | -0.60 | 100 | 45 | 26.55 | 53.09 | 0.28 | 6.23 | 19 | 91 | 251 |
| 8 | -0.70 | 100 | 45 | 26.55 | 53.09 | 0.42 | 7.33 | 24 | 86 | 313 |
| 9 | -0.80 | 100 | 46 | 26.55 | 53.09 | 0.62 | 8.46 | 30 | 73 | 385 |
| 10 | -0.90 | 100 | 47 | 26.55 | 53.09 | 0.86 | 9.60 | 36 | 50 | 466 |
| 11 | -1.00 | 100 | 48 | 26.55 | 53.09 | 1.17 | 10.76 | 44 | 9 | 560 |
| 12 | -1.10 | 100 | 49 | 26.55 | 53.09 | 1.54 | 11.94 | 53 | 56 | 668 |
| 13 | -1.20 | 100 | 49 | 26.55 | 53.09 | 1.98 | 13.14 | 64 | 149 | 791 |
| 14 | -1.30 | 100 | 50 | 26.55 | 53.09 | 2.50 | 14.36 | 76 | 272 | 929 |
| 15 | -1.40 | 100 | 51 | 26.55 | 53.09 | 3.11 | 15.60 | 89 | 427 | 1081 |
| 16 | -1.50 | 100 | 52 | 26.55 | 53.09 | 3.81 | 16.86 | 104 | 616 | 1248 |
| 17 | -1.60 | 100 | 52 | 26.55 | 53.09 | 4.60 | 18.13 | 120 | 839 | 1430 |
| 18 | -1.70 | 100 | 53 | 26.55 | 53.09 | 5.49 | 19.43 | 137 | 1098 | 1626 |
| 19 | -1.80 | 100 | 54 | 26.55 | 53.09 | 6.50 | 20.74 | 156 | 1393 | 1837 |
| 20 | -1.90 | 100 | 55 | 26.55 | 53.09 | 7.61 | 22.08 | 176 | 1724 | 2062 |
| 21 | -2.00 | 100 | 56 | 26.55 | 53.09 | 8.85 | 23.43 | 197 | 2091 | 2302 |
| 22 | -2.10 | 100 | 56 | 26.55 | 53.09 | 10.21 | 24.80 | 220 | 2496 | 2557 |
| 23 | -2.20 | 100 | 57 | 26.55 | 53.09 | 11.70 | 26.19 | 244 | 2939 | 2826 |
| 24 | -2.30 | 100 | 58 | 26.55 | 53.09 | 13.33 | 27.60 | 269 | 3420 | 3109 |
| 25 | -2.40 | 100 | 59 | 26.55 | 53.09 | 15.10 | 29.03 | 296 | 3939 | 3408 |
| 26 | -2.50 | 100 | 59 | 26.55 | 53.09 | 17.02 | 30.48 | 323 | 4497 | 3721 |
| 27 | -2.60 | 100 | 60 | 26.55 | 53.09 | 19.09 | 31.95 | 352 | 5095 | 4049 |
| 28 | -2.70 | 100 | 61 | 26.55 | 53.09 | 21.32 | 33.43 | 382 | 5733 | 4391 |
| 29 | -2.80 | 100 | 62 | 26.55 | 53.09 | 23.72 | 34.94 | 414 | 6410 | 4748 |
| 30 | -2.90 | 100 | 63 | 26.55 | 53.09 | 26.29 | 36.46 | 446 | 7128 | 5120 |
| 31 | -3.00 | 100 | 63 | 26.55 | 53.09 | 29.04 | 38.01 | 480 | 7887 | 5507 |
| 32 | -3.10 | 100 | 64 | 26.55 | 53.09 | 31.97 | 39.57 | 515 | 8687 | 5908 |
| 33 | -3.20 | 100 | 65 | 26.55 | 53.09 | 35.08 | 41.15 | 551 | 9528 | 6324 |
| 34 | -3.30 | 100 | 66 | 26.55 | 53.09 | 38.40 | 42.75 | 589 | 10411 | 6754 |
| 35 | -3.40 | 100 | 66 | 26.55 | 53.09 | 41.91 | 44.37 | 627 | 11335 | 7199 |
| 36 | -3.50 | 100 | 67 | 26.55 | 53.09 | 45.63 | 46.01 | 667 | 12302 | 7658 |
| 37 | -3.60 | 100 | 68 | 26.55 | 53.09 | 49.56 | 47.67 | 708 | 13311 | 8131 |
| 38 | -3.70 | 100 | 69 | 26.55 | 53.09 | 53.70 | 49.35 | 750 | 14362 | 8619 |
| 39 | -3.80 | 100 | 70 | 26.55 | 53.09 | 58.08 | 51.04 | 793 | 15456 | 9121 |
| 40 | -3.90 | 100 | 70 | 26.55 | 53.09 | 62.68 | 52.76 | 837 | 16593 | 9637 |
| 41 | -4.00 | 100 | 71 | 26.55 | 53.09 | 67.51 | 54.49 | 882 | 17773 | 10168 |
| 42 | -4.10 | 100 | 72 | 26.55 | 53.09 | 72.59 | 56.24 | 929 | 18996 | 10712 |
| 43 | -4.20 | 100 | 73 | 26.55 | 53.09 | 77.91 | 58.02 | 976 | 20263 | 11270 |
| 44 | -4.30 | 100 | 73 | 26.55 | 53.09 | 83.48 | 59.81 | 1025 | 21573 | 11842 |
| 45 | -4.40 | 100 | 74 | 26.55 | 53.09 | 89.31 | 61.62 | 1074 | 22927 | 12428 |
| 46 | -4.50 | 100 | 75 | 26.55 | 53.09 | 95.41 | 63.45 | 1125 | 24325 | 13028 |
| 47 | -4.60 | 100 | 76 | 26.55 | 53.09 | 101.77 | 65.30 | 1176 | 25767 | 13641 |
| 48 | -4.70 | 100 | 77 | 26.55 | 53.09 | 108.41 | 67.17 | 1229 | 27253 | 14267 |
| 49 | -4.80 | 100 | 77 | 26.55 | 53.09 | 115.34 | 69.05 | 1283 | 28783 | 14908 |
| 50 | -4.90 | 100 | 78 | 26.55 | 53.09 | 122.54 | 70.96 | 1337 | 30358 | 15561 |
| 51 | -5.00 | 100 | 79 | 26.55 | 53.09 | 130.04 | 72.88 | 1393 | 31977 | 16228 |
| 52 | -5.10 | 100 | 80 | 26.55 | 53.09 | 137.84 | 74.83 | 1450 | 33641 | 16908 |
| 53 | -5.20 | 100 | 80 | 26.55 | 53.09 | 145.95 | 76.79 | 1507 | 35349 | 17601 |
| 54 | -5.30 | 100 | 81 | 26.55 | 53.09 | 154.36 | 78.77 | 1566 | 37102 | 18307 |
| 55 | -5.40 | 100 | 82 | 26.55 | 53.09 | 163.09 | 80.78 | 1625 | 38900 | 19026 |
| 56 | -5.50 | 100 | 83 | 26.55 | 53.09 | 172.14 | 82.80 | 1686 | 40743 | 19758 |
| 57 | -5.60 | 100 | 84 | 26.55 | 53.09 | 181.51 | 84.84 | 1747 | 42631 | 20503 |
| 58 | -5.70 | 100 | 84 | 26.55 | 53.09 | 191.22 | 86.89 | 1810 | 44564 | 21260 |
| 59 | -5.80 | 100 | 85 | 26.55 | 53.09 | 201.27 | 88.97 | 1873 | 46542 | 22030 |
| 60 | -5.90 | 100 | 86 | 26.55 | 53.09 | 211.67 | 91.07 | 1937 | 48568 | 22814 |
| 61 | -6.00 | 100 | 87 | 26.55 | 53.09 | 222.45 | 93.18 | 2003 | 50644 | 23612 |
| 62 | -6.10 | 100 | 87 | 26.55 | 53.09 | 233.61 | 95.32 | 2069 | 52774 | 24425 |
| 63 | -6.20 | 100 | 88 | 26.55 | 53.09 | 245.17 | 97.47 | 2137 | 54959 | 25254 |
| 64 | -6.30 | 100 | 89 | 26.55 | 53.09 | 257.15 | 99.65 | 2206 | 57201 | 26100 |
| 65 | -6.40 | 100 | 90 | 26.55 | 53.09 | 269.54 | 101.84 | 2276 | 59501 | 26962 |
| 66 | -6.50 | 100 | 91 | 26.55 | 53.09 | 282.37 | 104.05 | 2348 | 61857 | 27840 |

Tensione massima di compressione nel calcestruzzo 14940 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | 0.00 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.10 | 100 | 41 | 26.55 | 53.09 | 0.01 | 0.99 | 2 | 24 | 33 |
| 3 | -0.20 | 100 | 42 | 26.55 | 53.09 | 0.03 | 2.00 | 5 | 43 | 71 |
| 4 | -0.30 | 100 | 42 | 26.55 | 53.09 | 0.08 | 3.03 | 8 | 57 | 115 |
| 5 | -0.40 | 100 | 43 | 26.55 | 53.09 | 0.17 | 4.08 | 13 | 63 | 166 |
| 6 | -0.50 | 100 | 44 | 26.55 | 53.09 | 0.29 | 5.14 | 17 | 62 | 226 |
| 7 | -0.60 | 100 | 45 | 26.55 | 53.09 | 0.46 | 6.23 | 23 | 51 | 296 |
| 8 | -0.70 | 100 | 45 | 26.55 | 53.09 | 0.69 | 7.33 | 30 | 27 | 378 |
| 9 | -0.80 | 100 | 46 | 26.55 | 53.09 | 0.98 | 8.46 | 38 | 19 | 474 |
| 10 | -0.90 | 100 | 47 | 26.55 | 53.09 | 1.34 | 9.60 | 48 | 94 | 587 |
| 11 | -1.00 | 100 | 48 | 26.55 | 53.09 | 1.78 | 10.76 | 59 | 202 | 716 |
| 12 | -1.10 | 100 | 49 | 26.55 | 53.09 | 2.30 | 11.94 | 72 | 346 | 863 |
| 13 | -1.20 | 100 | 49 | 26.55 | 53.09 | 2.93 | 13.14 | 87 | 529 | 1027 |
| 14 | -1.30 | 100 | 50 | 26.55 | 53.09 | 3.65 | 14.36 | 103 | 752 | 1209 |
| 15 | -1.40 | 100 | 51 | 26.55 | 53.09 | 4.49 | 15.60 | 121 | 1016 | 1408 |
| 16 | -1.50 | 100 | 52 | 26.55 | 53.09 | 5.45 | 16.86 | 141 | 1324 | 1625 |
| 17 | -1.60 | 100 | 52 | 26.55 | 53.09 | 6.53 | 18.13 | 162 | 1674 | 1860 |
| 18 | -1.70 | 100 | 53 | 26.55 | 53.09 | 7.74 | 19.43 | 185 | 2069 | 2112 |
| 19 | -1.80 | 100 | 54 | 26.55 | 53.09 | 9.09 | 20.74 | 210 | 2508 | 2383 |
| 20 | -1.90 | 100 | 55 | 26.55 | 53.09 | 10.59 | 22.08 | 236 | 2994 | 2672 |
| 21 | -2.00 | 100 | 56 | 26.55 | 53.09 | 12.24 | 23.43 | 264 | 3525 | 2979 |
| 22 | -2.10 | 100 | 56 | 26.55 | 53.09 | 14.05 | 24.80 | 293 | 4104 | 3305 |
| 23 | -2.20 | 100 | 57 | 26.55 | 53.09 | 16.03 | 26.19 | 324 | 4731 | 3649 |
| 24 | -2.30 | 100 | 58 | 26.55 | 53.09 | 18.19 | 27.60 | 357 | 5406 | 4011 |
| 25 | -2.40 | 100 | 59 | 26.55 | 53.09 | 20.53 | 29.03 | 391 | 6129 | 4392 |
| 26 | -2.50 | 100 | 59 | 26.55 | 53.09 | 23.06 | 30.48 | 426 | 6902 | 4792 |
| 27 | -2.60 | 100 | 60 | 26.55 | 53.09 | 25.79 | 31.95 | 464 | 7725 | 5210 |
| 28 | -2.70 | 100 | 61 | 26.55 | 53.09 | 28.72 | 33.43 | 503 | 8599 | 5647 |
| 29 | -2.80 | 100 | 62 | 26.55 | 53.09 | 31.87 | 34.94 | 543 | 9523 | 6102 |
| 30 | -2.90 | 100 | 63 | 26.55 | 53.09 | 35.23 | 36.46 | 585 | 10498 | 6575 |
| 31 | -3.00 | 100 | 63 | 26.55 | 53.09 | 38.82 | 38.01 | 628 | 11525 | 7067 |
| 32 | -3.10 | 100 | 64 | 26.55 | 53.09 | 42.64 | 39.57 | 673 | 12604 | 7577 |
| 33 | -3.20 | 100 | 65 | 26.55 | 53.09 | 46.70 | 41.15 | 719 | 13735 | 8106 |
| 34 | -3.30 | 100 | 66 | 26.55 | 53.09 | 51.01 | 42.75 | 767 | 14919 | 8652 |
| 35 | -3.40 | 100 | 66 | 26.55 | 53.09 | 55.57 | 44.37 | 816 | 16155 | 9217 |
| 36 | -3.50 | 100 | 67 | 26.55 | 53.09 | 60.40 | 46.01 | 867 | 17445 | 9800 |
| 37 | -3.60 | 100 | 68 | 26.55 | 53.09 | 65.50 | 47.67 | 919 | 18789 | 10401 |
| 38 | -3.70 | 100 | 69 | 26.55 | 53.09 | 70.87 | 49.35 | 972 | 20186 | 11020 |
| 39 | -3.80 | 100 | 70 | 26.55 | 53.09 | 76.52 | 51.04 | 1027 | 21637 | 11657 |
| 40 | -3.90 | 100 | 70 | 26.55 | 53.09 | 82.47 | 52.76 | 1084 | 23142 | 12311 |
| 41 | -4.00 | 100 | 71 | 26.55 | 53.09 | 88.72 | 54.49 | 1141 | 24702 | 12983 |
| 42 | -4.10 | 100 | 72 | 26.55 | 53.09 | 95.27 | 56.24 | 1200 | 26316 | 13672 |
| 43 | -4.20 | 100 | 73 | 26.55 | 53.09 | 102.13 | 58.02 | 1260 | 27986 | 14379 |
| 44 | -4.30 | 100 | 73 | 26.55 | 53.09 | 109.31 | 59.81 | 1322 | 29710 | 15103 |
| 45 | -4.40 | 100 | 74 | 26.55 | 53.09 | 116.82 | 61.62 | 1385 | 31490 | 15844 |
| 46 | -4.50 | 100 | 75 | 26.55 | 53.09 | 124.66 | 63.45 | 1449 | 33324 | 16603 |
| 47 | -4.60 | 100 | 76 | 26.55 | 53.09 | 132.85 | 65.30 | 1515 | 35215 | 17378 |
| 48 | -4.70 | 100 | 77 | 26.55 | 53.09 | 141.38 | 67.17 | 1582 | 37161 | 18171 |
| 49 | -4.80 | 100 | 77 | 26.55 | 53.09 | 150.27 | 69.05 | 1650 | 39163 | 18980 |
| 50 | -4.90 | 100 | 78 | 26.55 | 53.09 | 159.52 | 70.96 | 1719 | 41221 | 19806 |
| 51 | -5.00 | 100 | 79 | 26.55 | 53.09 | 169.14 | 72.88 | 1789 | 43335 | 20648 |
| 52 | -5.10 | 100 | 80 | 26.55 | 53.09 | 179.14 | 74.83 | 1861 | 45505 | 21507 |
| 53 | -5.20 | 100 | 80 | 26.55 | 53.09 | 189.52 | 76.79 | 1934 | 47732 | 22382 |
| 54 | -5.30 | 100 | 81 | 26.55 | 53.09 | 200.30 | 78.77 | 2008 | 50015 | 23273 |
| 55 | -5.40 | 100 | 82 | 26.55 | 53.09 | 211.47 | 80.78 | 2084 | 52355 | 24181 |
| 56 | -5.50 | 100 | 83 | 26.55 | 53.09 | 223.05 | 82.80 | 2160 | 54751 | 25104 |
| 57 | -5.60 | 100 | 84 | 26.55 | 53.09 | 235.05 | 84.84 | 2238 | 57204 | 26044 |

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
NM25 03 D 26 CL NV 24 05 001 A 114 di 314

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 58 | -5.70 | 100 | 84 | 26.55 | 53.09 | 247.46 | 86.89 | 2317 | 59714 | 26999 |
| 59 | -5.80 | 100 | 85 | 26.55 | 53.09 | 260.30 | 88.97 | 2397 | 62281 | 27970 |
| 60 | -5.90 | 100 | 86 | 26.55 | 53.09 | 273.59 | 91.07 | 2478 | 64907 | 28958 |
| 61 | -6.00 | 100 | 87 | 26.55 | 53.09 | 287.34 | 93.18 | 2561 | 67596 | 29963 |
| 62 | -6.10 | 100 | 87 | 26.55 | 53.09 | 301.57 | 95.32 | 2645 | 70349 | 30986 |
| 63 | -6.20 | 100 | 88 | 26.55 | 53.09 | 316.29 | 97.47 | 2730 | 73170 | 32028 |
| 64 | -6.30 | 100 | 89 | 26.55 | 53.09 | 331.53 | 99.65 | 2817 | 76060 | 33090 |
| 65 | -6.40 | 100 | 90 | 26.55 | 53.09 | 347.29 | 101.84 | 2905 | 79019 | 34171 |
| 66 | -6.50 | 100 | 91 | 26.55 | 53.09 | 363.57 | 104.05 | 2995 | 82047 | 35272 |

Fondazione

Combinazione n° 12 - SLEQ

Tensione massima di compressione nel calcestruzzo 13073 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | -1.00 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.90 | 100 | 110 | 45.24 | 22.62 | 0.85 | 0.00 | 5 | 199 | 61 |
| 3 | -0.80 | 100 | 110 | 45.24 | 22.62 | 3.38 | 0.00 | 21 | 792 | 243 |
| 4 | -0.70 | 100 | 110 | 45.24 | 22.62 | 7.58 | 0.00 | 47 | 1777 | 545 |
| 5 | -0.60 | 100 | 110 | 45.24 | 22.62 | 13.45 | 0.00 | 83 | 3150 | 967 |
| 6 | -0.50 | 100 | 110 | 45.24 | 22.62 | 20.95 | 0.00 | 129 | 4908 | 1507 |
| 7 | -0.40 | 100 | 110 | 45.24 | 22.62 | 30.09 | 0.00 | 185 | 7047 | 2163 |
| 8 | 0.51 | 100 | 110 | 22.62 | 45.24 | -428.05 | 0.00 | 2627 | 30780 | 100265 |
| 9 | 0.60 | 100 | 110 | 22.62 | 45.24 | -419.51 | 0.00 | 2575 | 30166 | 98265 |
| 10 | 0.70 | 100 | 110 | 22.62 | 45.24 | -410.76 | 0.00 | 2521 | 29536 | 96215 |
| 11 | 0.80 | 100 | 110 | 22.62 | 45.24 | -401.81 | 0.00 | 2466 | 28893 | 94118 |
| 12 | 0.90 | 100 | 110 | 22.62 | 45.24 | -392.67 | 0.00 | 2410 | 28235 | 91978 |
| 13 | 1.00 | 100 | 110 | 22.62 | 45.24 | -383.36 | 0.00 | 2353 | 27566 | 89796 |
| 14 | 1.10 | 100 | 110 | 22.62 | 45.24 | -373.88 | 0.00 | 2295 | 26885 | 87577 |
| 15 | 1.20 | 100 | 110 | 22.62 | 45.24 | -364.27 | 0.00 | 2236 | 26193 | 85324 |
| 16 | 1.30 | 100 | 110 | 22.62 | 45.24 | -354.51 | 0.00 | 2176 | 25492 | 83040 |
| 17 | 1.40 | 100 | 110 | 22.62 | 45.24 | -344.64 | 0.00 | 2115 | 24782 | 80728 |
| 18 | 1.49 | 100 | 110 | 22.62 | 45.24 | -334.67 | 0.00 | 2054 | 24065 | 78391 |
| 19 | 1.59 | 100 | 110 | 22.62 | 45.24 | -324.60 | 0.00 | 1992 | 23341 | 76033 |
| 20 | 1.69 | 100 | 110 | 22.62 | 45.24 | -314.45 | 0.00 | 1930 | 22611 | 73656 |
| 21 | 1.79 | 100 | 110 | 22.62 | 45.24 | -304.24 | 0.00 | 1867 | 21877 | 71264 |
| 22 | 1.89 | 100 | 110 | 22.62 | 45.24 | -293.98 | 0.00 | 1804 | 21139 | 68860 |
| 23 | 1.99 | 100 | 110 | 22.62 | 45.24 | -283.68 | 0.00 | 1741 | 20398 | 66447 |
| 24 | 2.09 | 100 | 110 | 22.62 | 45.24 | -273.35 | 0.00 | 1678 | 19656 | 64029 |
| 25 | 2.19 | 100 | 110 | 22.62 | 45.24 | -263.02 | 0.00 | 1614 | 18913 | 61608 |
| 26 | 2.29 | 100 | 110 | 22.62 | 45.24 | -252.68 | 0.00 | 1551 | 18170 | 59188 |
| 27 | 2.38 | 100 | 110 | 22.62 | 45.24 | -242.37 | 0.00 | 1488 | 17428 | 56771 |
| 28 | 2.48 | 100 | 110 | 22.62 | 45.24 | -232.08 | 0.00 | 1424 | 16688 | 54362 |
| 29 | 2.58 | 100 | 110 | 22.62 | 45.24 | -221.84 | 0.00 | 1362 | 15952 | 51963 |
| 30 | 2.68 | 100 | 110 | 22.62 | 45.24 | -211.65 | 0.00 | 1299 | 15219 | 49577 |
| 31 | 2.78 | 100 | 110 | 22.62 | 45.24 | -201.54 | 0.00 | 1237 | 14492 | 47208 |
| 32 | 2.88 | 100 | 110 | 22.62 | 45.24 | -191.51 | 0.00 | 1175 | 13771 | 44859 |
| 33 | 2.98 | 100 | 110 | 22.62 | 45.24 | -181.58 | 0.00 | 1114 | 13057 | 42532 |
| 34 | 3.08 | 100 | 110 | 22.62 | 45.24 | -171.76 | 0.00 | 1054 | 12350 | 40232 |
| 35 | 3.17 | 100 | 110 | 22.62 | 45.24 | -162.06 | 0.00 | 995 | 11653 | 37961 |

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 36 | 3.27 | 100 | 110 | 22.62 | 45.24 | -152.51 | 0.00 | 936 | 10966 | 35722 |
| 37 | 3.37 | 100 | 110 | 22.62 | 45.24 | -143.10 | 0.00 | 878 | 10290 | 33519 |
| 38 | 3.47 | 100 | 110 | 22.62 | 45.24 | -133.86 | 0.00 | 822 | 9626 | 31355 |
| 39 | 3.57 | 100 | 110 | 22.62 | 45.24 | -124.80 | 0.00 | 766 | 8974 | 29233 |
| 40 | 3.67 | 100 | 110 | 22.62 | 45.24 | -115.94 | 0.00 | 712 | 8337 | 27156 |
| 41 | 3.77 | 100 | 110 | 22.62 | 45.24 | -106.00 | 0.00 | 651 | 7622 | 24830 |
| 42 | 3.87 | 100 | 110 | 22.62 | 45.24 | -95.87 | 0.00 | 588 | 6894 | 22456 |
| 43 | 3.97 | 100 | 110 | 22.62 | 45.24 | -86.17 | 0.00 | 529 | 6196 | 20184 |
| 44 | 4.06 | 100 | 110 | 22.62 | 45.24 | -76.91 | 0.00 | 472 | 5530 | 18015 |
| 45 | 4.16 | 100 | 110 | 22.62 | 45.24 | -68.10 | 0.00 | 418 | 4897 | 15952 |
| 46 | 4.26 | 100 | 110 | 22.62 | 45.24 | -59.77 | 0.00 | 367 | 4298 | 14000 |
| 47 | 4.36 | 100 | 110 | 22.62 | 45.24 | -51.92 | 0.00 | 319 | 3733 | 12161 |
| 48 | 4.46 | 100 | 110 | 22.62 | 45.24 | -44.56 | 0.00 | 274 | 3204 | 10438 |
| 49 | 4.56 | 100 | 110 | 22.62 | 45.24 | -37.72 | 0.00 | 232 | 2712 | 8835 |
| 50 | 4.66 | 100 | 110 | 22.62 | 45.24 | -31.40 | 0.00 | 193 | 2258 | 7355 |
| 51 | 4.76 | 100 | 110 | 22.62 | 45.24 | -25.62 | 0.00 | 157 | 1842 | 6000 |
| 52 | 4.86 | 100 | 110 | 22.62 | 45.24 | -20.38 | 0.00 | 125 | 1466 | 4775 |
| 53 | 4.95 | 100 | 110 | 22.62 | 45.24 | -15.72 | 0.00 | 96 | 1130 | 3682 |
| 54 | 5.05 | 100 | 110 | 22.62 | 45.24 | -11.63 | 0.00 | 71 | 836 | 2724 |
| 55 | 5.15 | 100 | 110 | 22.62 | 45.24 | -8.13 | 0.00 | 50 | 585 | 1905 |
| 56 | 5.25 | 100 | 110 | 22.62 | 45.24 | -5.24 | 0.00 | 32 | 377 | 1228 |
| 57 | 5.35 | 100 | 110 | 22.62 | 45.24 | -2.97 | 0.00 | 18 | 213 | 695 |
| 58 | 5.45 | 100 | 110 | 22.62 | 45.24 | -1.33 | 0.00 | 8 | 96 | 311 |
| 59 | 5.55 | 100 | 110 | 22.62 | 45.24 | -0.33 | 0.00 | 2 | 24 | 78 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

Combinazione n° 13 - SLEQ H + V

Tensione massima di compressione nel calcestruzzo 13073 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | -1.00 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.90 | 100 | 110 | 45.24 | 22.62 | 1.12 | 0.00 | 7 | 262 | 80 |
| 3 | -0.80 | 100 | 110 | 45.24 | 22.62 | 4.45 | 0.00 | 27 | 1043 | 320 |
| 4 | -0.70 | 100 | 110 | 45.24 | 22.62 | 9.97 | 0.00 | 61 | 2336 | 717 |
| 5 | -0.60 | 100 | 110 | 45.24 | 22.62 | 17.65 | 0.00 | 108 | 4135 | 1269 |
| 6 | -0.50 | 100 | 110 | 45.24 | 22.62 | 27.47 | 0.00 | 169 | 6433 | 1975 |
| 7 | -0.40 | 100 | 110 | 45.24 | 22.62 | 39.38 | 0.00 | 242 | 9224 | 2831 |
| 8 | 0.51 | 100 | 110 | 22.62 | 45.24 | -665.79 | 0.00 | 4086 | 47875 | 155953 |
| 9 | 0.60 | 100 | 110 | 22.62 | 45.24 | -654.36 | 0.00 | 4016 | 47052 | 153275 |
| 10 | 0.70 | 100 | 110 | 22.62 | 45.24 | -642.41 | 0.00 | 3943 | 46193 | 150475 |
| 11 | 0.80 | 100 | 110 | 22.62 | 45.24 | -629.97 | 0.00 | 3866 | 45299 | 147561 |
| 12 | 0.90 | 100 | 110 | 22.62 | 45.24 | -617.07 | 0.00 | 3787 | 44371 | 144539 |
| 13 | 1.00 | 100 | 110 | 22.62 | 45.24 | -603.73 | 0.00 | 3705 | 43412 | 141416 |
| 14 | 1.10 | 100 | 110 | 22.62 | 45.24 | -589.99 | 0.00 | 3621 | 42424 | 138197 |
| 15 | 1.20 | 100 | 110 | 22.62 | 45.24 | -575.87 | 0.00 | 3534 | 41409 | 134890 |
| 16 | 1.30 | 100 | 110 | 22.62 | 45.24 | -561.40 | 0.00 | 3446 | 40368 | 131501 |
| 17 | 1.40 | 100 | 110 | 22.62 | 45.24 | -546.61 | 0.00 | 3355 | 39305 | 128037 |
| 18 | 1.49 | 100 | 110 | 22.62 | 45.24 | -531.53 | 0.00 | 3262 | 38220 | 124504 |
| 19 | 1.59 | 100 | 110 | 22.62 | 45.24 | -516.18 | 0.00 | 3168 | 37117 | 120908 |
| 20 | 1.69 | 100 | 110 | 22.62 | 45.24 | -500.59 | 0.00 | 3072 | 35996 | 117256 |
| 21 | 1.79 | 100 | 110 | 22.62 | 45.24 | -484.79 | 0.00 | 2975 | 34859 | 113555 |
| 22 | 1.89 | 100 | 110 | 22.62 | 45.24 | -468.80 | 0.00 | 2877 | 33710 | 109811 |
| 23 | 1.99 | 100 | 110 | 22.62 | 45.24 | -452.67 | 0.00 | 2778 | 32549 | 106031 |
| 24 | 2.09 | 100 | 110 | 22.62 | 45.24 | -436.40 | 0.00 | 2678 | 31380 | 102220 |
| 25 | 2.19 | 100 | 110 | 22.62 | 45.24 | -420.03 | 0.00 | 2578 | 30203 | 98387 |

| n° | Y | B | H | Afi | Afs | M | N | σ_c | σ_{fi} | σ_{fs} |
|----|------|------|------|-------|-------|---------|------|------------|---------------|---------------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
| 26 | 2.29 | 100 | 110 | 22.62 | 45.24 | -403.59 | 0.00 | 2477 | 29021 | 94536 |
| 27 | 2.38 | 100 | 110 | 22.62 | 45.24 | -387.11 | 0.00 | 2376 | 27835 | 90675 |
| 28 | 2.48 | 100 | 110 | 22.62 | 45.24 | -370.61 | 0.00 | 2275 | 26649 | 86810 |
| 29 | 2.58 | 100 | 110 | 22.62 | 45.24 | -354.12 | 0.00 | 2173 | 25463 | 82947 |
| 30 | 2.68 | 100 | 110 | 22.62 | 45.24 | -337.67 | 0.00 | 2072 | 24280 | 79094 |
| 31 | 2.78 | 100 | 110 | 22.62 | 45.24 | -321.28 | 0.00 | 1972 | 23102 | 75256 |
| 32 | 2.88 | 100 | 110 | 22.62 | 45.24 | -304.99 | 0.00 | 1872 | 21931 | 71441 |
| 33 | 2.98 | 100 | 110 | 22.62 | 45.24 | -288.83 | 0.00 | 1773 | 20768 | 67654 |
| 34 | 3.08 | 100 | 110 | 22.62 | 45.24 | -272.81 | 0.00 | 1674 | 19617 | 63902 |
| 35 | 3.17 | 100 | 110 | 22.62 | 45.24 | -256.97 | 0.00 | 1577 | 18478 | 60192 |
| 36 | 3.27 | 100 | 110 | 22.62 | 45.24 | -241.34 | 0.00 | 1481 | 17354 | 56530 |
| 37 | 3.37 | 100 | 110 | 22.62 | 45.24 | -225.94 | 0.00 | 1387 | 16246 | 52923 |
| 38 | 3.47 | 100 | 110 | 22.62 | 45.24 | -210.80 | 0.00 | 1294 | 15158 | 49376 |
| 39 | 3.57 | 100 | 110 | 22.62 | 45.24 | -195.95 | 0.00 | 1203 | 14090 | 45898 |
| 40 | 3.67 | 100 | 110 | 22.62 | 45.24 | -181.41 | 0.00 | 1113 | 13045 | 42493 |
| 41 | 3.77 | 100 | 110 | 22.62 | 45.24 | -166.95 | 0.00 | 1019 | 11933 | 38872 |
| 42 | 3.87 | 100 | 110 | 22.62 | 45.24 | -150.44 | 0.00 | 923 | 10818 | 35239 |
| 43 | 3.97 | 100 | 110 | 22.62 | 45.24 | -135.53 | 0.00 | 832 | 9745 | 31745 |
| 44 | 4.06 | 100 | 110 | 22.62 | 45.24 | -121.24 | 0.00 | 744 | 8718 | 28398 |
| 45 | 4.16 | 100 | 110 | 22.62 | 45.24 | -107.60 | 0.00 | 660 | 7737 | 25203 |
| 46 | 4.26 | 100 | 110 | 22.62 | 45.24 | -94.64 | 0.00 | 581 | 6805 | 22167 |
| 47 | 4.36 | 100 | 110 | 22.62 | 45.24 | -82.38 | 0.00 | 506 | 5924 | 19297 |
| 48 | 4.46 | 100 | 110 | 22.62 | 45.24 | -70.86 | 0.00 | 435 | 5095 | 16598 |
| 49 | 4.56 | 100 | 110 | 22.62 | 45.24 | -60.10 | 0.00 | 369 | 4322 | 14079 |
| 50 | 4.66 | 100 | 110 | 22.62 | 45.24 | -50.14 | 0.00 | 308 | 3605 | 11744 |
| 51 | 4.76 | 100 | 110 | 22.62 | 45.24 | -40.98 | 0.00 | 252 | 2947 | 9600 |
| 52 | 4.86 | 100 | 110 | 22.62 | 45.24 | -32.68 | 0.00 | 201 | 2350 | 7655 |
| 53 | 4.95 | 100 | 110 | 22.62 | 45.24 | -25.25 | 0.00 | 155 | 1815 | 5914 |
| 54 | 5.05 | 100 | 110 | 22.62 | 45.24 | -18.72 | 0.00 | 115 | 1346 | 4384 |
| 55 | 5.15 | 100 | 110 | 22.62 | 45.24 | -13.11 | 0.00 | 80 | 943 | 3071 |
| 56 | 5.25 | 100 | 110 | 22.62 | 45.24 | -8.47 | 0.00 | 52 | 609 | 1983 |
| 57 | 5.35 | 100 | 110 | 22.62 | 45.24 | -4.80 | 0.00 | 29 | 345 | 1125 |
| 58 | 5.45 | 100 | 110 | 22.62 | 45.24 | -2.15 | 0.00 | 13 | 155 | 504 |
| 59 | 5.55 | 100 | 110 | 22.62 | 45.24 | -0.54 | 0.00 | 3 | 39 | 127 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

Verifica a fessurazione

Simbologia adottata

| | |
|------------|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Af | area ferri zona tesa espresso in [cmq] |
| Aeff | area efficace espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| Mpf | momento di prima fessurazione espressa in [kNm] |
| ϵ | deformazione espresso in % |
| Sm | spaziatura tra le fessure espressa in [mm] |
| w | apertura delle fessure espressa in [mm] |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 117 di 314 |

Combinazioni SLER

Paramento

Combinazione n° 10 - SLER

Apertura limite fessure $w_{lim}=0.20$

| n° | Y | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|-------|------|------|-------|---------|--------|---------|----------|------|-------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | 0.00 | 5.81 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.20 | 100 | 42 | 0.00 | 0.00 | 0.02 | 16.80 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | 0.04 | 35.28 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | 0.09 | 65.88 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.50 | 100 | 44 | 0.00 | 0.00 | 0.17 | 118.89 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.60 | 100 | 45 | 0.00 | 0.00 | 0.28 | 222.15 | 0.000000 | 0.00 | 0.000 |
| 8 | -0.70 | 100 | 45 | 0.00 | 0.00 | 0.42 | 484.78 | 0.000000 | 0.00 | 0.000 |
| 9 | -0.80 | 100 | 46 | 0.00 | 0.00 | 0.62 | 2201.91 | 0.000000 | 0.00 | 0.000 |
| 10 | -0.90 | 100 | 47 | 0.00 | 0.00 | 0.86 | 1546.90 | 0.000000 | 0.00 | 0.000 |
| 11 | -1.00 | 100 | 48 | 0.00 | 0.00 | 1.17 | 704.98 | 0.000000 | 0.00 | 0.000 |
| 12 | -1.10 | 100 | 49 | 53.09 | 1600.00 | 1.54 | 508.13 | 0.000000 | 0.00 | 0.000 |
| 13 | -1.20 | 100 | 49 | 53.09 | 1600.00 | 1.98 | 423.46 | 0.000000 | 0.00 | 0.000 |
| 14 | -1.30 | 100 | 50 | 53.09 | 1600.00 | 2.50 | 378.29 | 0.000000 | 0.00 | 0.000 |
| 15 | -1.40 | 100 | 51 | 53.09 | 1600.00 | 3.11 | 351.57 | 0.000000 | 0.00 | 0.000 |
| 16 | -1.50 | 100 | 52 | 53.09 | 1600.00 | 3.81 | 334.94 | 0.000000 | 0.00 | 0.000 |
| 17 | -1.60 | 100 | 52 | 53.09 | 1600.00 | 4.60 | 324.43 | 0.000000 | 0.00 | 0.000 |
| 18 | -1.70 | 100 | 53 | 53.09 | 1600.00 | 5.49 | 317.91 | 0.000000 | 0.00 | 0.000 |
| 19 | -1.80 | 100 | 54 | 53.09 | 1600.00 | 6.50 | 314.14 | 0.000000 | 0.00 | 0.000 |
| 20 | -1.90 | 100 | 55 | 53.09 | 1600.00 | 7.61 | 312.36 | 0.000000 | 0.00 | 0.000 |
| 21 | -2.00 | 100 | 56 | 53.09 | 1600.00 | 8.85 | 312.06 | 0.000000 | 0.00 | 0.000 |
| 22 | -2.10 | 100 | 56 | 53.09 | 1600.00 | 10.21 | 312.89 | 0.000000 | 0.00 | 0.000 |
| 23 | -2.20 | 100 | 57 | 53.09 | 1600.00 | 11.70 | 314.62 | 0.000000 | 0.00 | 0.000 |
| 24 | -2.30 | 100 | 58 | 53.09 | 1600.00 | 13.33 | 317.08 | 0.000000 | 0.00 | 0.000 |
| 25 | -2.40 | 100 | 59 | 53.09 | 1600.00 | 15.10 | 320.12 | 0.000000 | 0.00 | 0.000 |
| 26 | -2.50 | 100 | 59 | 53.09 | 1600.00 | 17.02 | 323.66 | 0.000000 | 0.00 | 0.000 |
| 27 | -2.60 | 100 | 60 | 53.09 | 1600.00 | 19.09 | 327.62 | 0.000000 | 0.00 | 0.000 |
| 28 | -2.70 | 100 | 61 | 53.09 | 1600.00 | 21.32 | 331.94 | 0.000000 | 0.00 | 0.000 |
| 29 | -2.80 | 100 | 62 | 53.09 | 1600.00 | 23.72 | 336.58 | 0.000000 | 0.00 | 0.000 |
| 30 | -2.90 | 100 | 63 | 53.09 | 1600.00 | 26.29 | 341.49 | 0.000000 | 0.00 | 0.000 |
| 31 | -3.00 | 100 | 63 | 53.09 | 1600.00 | 29.04 | 346.65 | 0.000000 | 0.00 | 0.000 |
| 32 | -3.10 | 100 | 64 | 53.09 | 1600.00 | 31.97 | 352.03 | 0.000000 | 0.00 | 0.000 |
| 33 | -3.20 | 100 | 65 | 53.09 | 1600.00 | 35.08 | 357.61 | 0.000000 | 0.00 | 0.000 |
| 34 | -3.30 | 100 | 66 | 53.09 | 1600.00 | 38.40 | 363.38 | 0.000000 | 0.00 | 0.000 |
| 35 | -3.40 | 100 | 66 | 53.09 | 1600.00 | 41.91 | 369.31 | 0.000000 | 0.00 | 0.000 |
| 36 | -3.50 | 100 | 67 | 53.09 | 1600.00 | 45.63 | 375.40 | 0.000000 | 0.00 | 0.000 |
| 37 | -3.60 | 100 | 68 | 53.09 | 1600.00 | 49.56 | 381.64 | 0.000000 | 0.00 | 0.000 |
| 38 | -3.70 | 100 | 69 | 53.09 | 1600.00 | 53.70 | 388.02 | 0.000000 | 0.00 | 0.000 |
| 39 | -3.80 | 100 | 70 | 53.09 | 1600.00 | 58.08 | 394.53 | 0.000000 | 0.00 | 0.000 |
| 40 | -3.90 | 100 | 70 | 53.09 | 1600.00 | 62.68 | 401.16 | 0.000000 | 0.00 | 0.000 |
| 41 | -4.00 | 100 | 71 | 53.09 | 1600.00 | 67.51 | 407.91 | 0.000000 | 0.00 | 0.000 |
| 42 | -4.10 | 100 | 72 | 53.09 | 1600.00 | 72.59 | 414.78 | 0.000000 | 0.00 | 0.000 |
| 43 | -4.20 | 100 | 73 | 53.09 | 1600.00 | 77.91 | 421.75 | 0.000000 | 0.00 | 0.000 |
| 44 | -4.30 | 100 | 73 | 53.09 | 1600.00 | 83.48 | 428.82 | 0.000000 | 0.00 | 0.000 |
| 45 | -4.40 | 100 | 74 | 53.09 | 1600.00 | 89.31 | 436.00 | 0.000000 | 0.00 | 0.000 |
| 46 | -4.50 | 100 | 75 | 53.09 | 1600.00 | 95.41 | 443.27 | 0.000000 | 0.00 | 0.000 |
| 47 | -4.60 | 100 | 76 | 53.09 | 1600.00 | 101.77 | 450.64 | 0.000000 | 0.00 | 0.000 |
| 48 | -4.70 | 100 | 77 | 53.09 | 1600.00 | 108.41 | 458.10 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
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| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 49 | -4.80 | 100 | 77 | 53.09 | 1600.00 | 115.34 | 465.65 | 0.000000 | 0.00 | 0.000 |
| 50 | -4.90 | 100 | 78 | 53.09 | 1600.00 | 122.54 | 473.29 | 0.000000 | 0.00 | 0.000 |
| 51 | -5.00 | 100 | 79 | 53.09 | 1600.00 | 130.04 | 481.02 | 0.000000 | 0.00 | 0.000 |
| 52 | -5.10 | 100 | 80 | 53.09 | 1600.00 | 137.84 | 488.83 | 0.000000 | 0.00 | 0.000 |
| 53 | -5.20 | 100 | 80 | 53.09 | 1600.00 | 145.95 | 496.73 | 0.000000 | 0.00 | 0.000 |
| 54 | -5.30 | 100 | 81 | 53.09 | 1600.00 | 154.36 | 504.70 | 0.000000 | 0.00 | 0.000 |
| 55 | -5.40 | 100 | 82 | 53.09 | 1600.00 | 163.09 | 512.76 | 0.000000 | 0.00 | 0.000 |
| 56 | -5.50 | 100 | 83 | 53.09 | 1600.00 | 172.14 | 520.90 | 0.000000 | 0.00 | 0.000 |
| 57 | -5.60 | 100 | 84 | 53.09 | 1600.00 | 181.51 | 529.12 | 0.000000 | 0.00 | 0.000 |
| 58 | -5.70 | 100 | 84 | 53.09 | 1600.00 | 191.22 | 537.41 | 0.000000 | 0.00 | 0.000 |
| 59 | -5.80 | 100 | 85 | 53.09 | 1600.00 | 201.27 | 545.78 | 0.000000 | 0.00 | 0.000 |
| 60 | -5.90 | 100 | 86 | 53.09 | 1600.00 | 211.67 | 554.23 | 0.000000 | 0.00 | 0.000 |
| 61 | -6.00 | 100 | 87 | 53.09 | 1600.00 | 222.45 | 562.75 | 0.000000 | 0.00 | 0.000 |
| 62 | -6.10 | 100 | 87 | 53.09 | 1600.00 | 233.61 | 571.33 | 0.000000 | 0.00 | 0.000 |
| 63 | -6.20 | 100 | 88 | 53.09 | 1600.00 | 245.17 | 579.99 | 0.000000 | 0.00 | 0.000 |
| 64 | -6.30 | 100 | 89 | 53.09 | 1600.00 | 257.15 | 588.72 | 0.000000 | 0.00 | 0.000 |
| 65 | -6.40 | 100 | 90 | 53.09 | 1600.00 | 269.54 | 597.51 | 0.000000 | 0.00 | 0.000 |
| 66 | -6.50 | 100 | 91 | 53.09 | 1600.00 | 282.37 | 606.37 | 0.000000 | 0.00 | 0.000 |

Fondazione

Combinazione n° 10 - SLER

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | -1.00 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.90 | 100 | 110 | 45.24 | 1600.00 | 0.85 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.80 | 100 | 110 | 45.24 | 1600.00 | 3.38 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.70 | 100 | 110 | 45.24 | 1600.00 | 7.58 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.60 | 100 | 110 | 45.24 | 1600.00 | 13.45 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.50 | 100 | 110 | 45.24 | 1600.00 | 20.95 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.40 | 100 | 110 | 45.24 | 1600.00 | 30.09 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 8 | 0.51 | 100 | 110 | 45.24 | 1600.00 | -428.05 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 9 | 0.60 | 100 | 110 | 45.24 | 1600.00 | -419.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 10 | 0.70 | 100 | 110 | 45.24 | 1600.00 | -410.76 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 11 | 0.80 | 100 | 110 | 45.24 | 1600.00 | -401.81 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 12 | 0.90 | 100 | 110 | 45.24 | 1600.00 | -392.67 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 13 | 1.00 | 100 | 110 | 45.24 | 1600.00 | -383.36 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 14 | 1.10 | 100 | 110 | 45.24 | 1600.00 | -373.88 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 15 | 1.20 | 100 | 110 | 45.24 | 1600.00 | -364.27 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 16 | 1.30 | 100 | 110 | 45.24 | 1600.00 | -354.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 17 | 1.40 | 100 | 110 | 45.24 | 1600.00 | -344.64 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 18 | 1.49 | 100 | 110 | 45.24 | 1600.00 | -334.67 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 19 | 1.59 | 100 | 110 | 45.24 | 1600.00 | -324.60 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 20 | 1.69 | 100 | 110 | 45.24 | 1600.00 | -314.45 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 21 | 1.79 | 100 | 110 | 45.24 | 1600.00 | -304.24 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 22 | 1.89 | 100 | 110 | 45.24 | 1600.00 | -293.98 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 23 | 1.99 | 100 | 110 | 45.24 | 1600.00 | -283.68 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 24 | 2.09 | 100 | 110 | 45.24 | 1600.00 | -273.35 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 25 | 2.19 | 100 | 110 | 45.24 | 1600.00 | -263.02 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 26 | 2.29 | 100 | 110 | 45.24 | 1600.00 | -252.68 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 27 | 2.38 | 100 | 110 | 45.24 | 1600.00 | -242.37 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 28 | 2.48 | 100 | 110 | 45.24 | 1600.00 | -232.08 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 29 | 2.58 | 100 | 110 | 45.24 | 1600.00 | -221.84 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 30 | 2.68 | 100 | 110 | 45.24 | 1600.00 | -211.65 | -719.00 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
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| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 31 | 2.78 | 100 | 110 | 45.24 | 1600.00 | -201.54 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 32 | 2.88 | 100 | 110 | 45.24 | 1600.00 | -191.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 33 | 2.98 | 100 | 110 | 45.24 | 1600.00 | -181.58 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 34 | 3.08 | 100 | 110 | 45.24 | 1600.00 | -171.76 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 35 | 3.17 | 100 | 110 | 45.24 | 1600.00 | -162.06 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 36 | 3.27 | 100 | 110 | 45.24 | 1600.00 | -152.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 37 | 3.37 | 100 | 110 | 45.24 | 1600.00 | -143.10 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 38 | 3.47 | 100 | 110 | 45.24 | 1600.00 | -133.86 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 39 | 3.57 | 100 | 110 | 45.24 | 1600.00 | -124.80 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 40 | 3.67 | 100 | 110 | 45.24 | 1600.00 | -115.94 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 41 | 3.77 | 100 | 110 | 45.24 | 1600.00 | -106.00 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 42 | 3.87 | 100 | 110 | 45.24 | 1600.00 | -95.87 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 43 | 3.97 | 100 | 110 | 45.24 | 1600.00 | -86.17 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 44 | 4.06 | 100 | 110 | 45.24 | 1600.00 | -76.91 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 45 | 4.16 | 100 | 110 | 45.24 | 1600.00 | -68.10 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 46 | 4.26 | 100 | 110 | 45.24 | 1600.00 | -59.77 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 47 | 4.36 | 100 | 110 | 45.24 | 1600.00 | -51.92 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 48 | 4.46 | 100 | 110 | 45.24 | 1600.00 | -44.56 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 49 | 4.56 | 100 | 110 | 45.24 | 1600.00 | -37.72 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 50 | 4.66 | 100 | 110 | 45.24 | 1600.00 | -31.40 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 51 | 4.76 | 100 | 110 | 45.24 | 1600.00 | -25.62 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 52 | 4.86 | 100 | 110 | 45.24 | 1600.00 | -20.38 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 53 | 4.95 | 100 | 110 | 45.24 | 1600.00 | -15.72 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 54 | 5.05 | 100 | 110 | 45.24 | 1600.00 | -11.63 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 55 | 5.15 | 100 | 110 | 45.24 | 1600.00 | -8.13 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 56 | 5.25 | 100 | 110 | 45.24 | 1600.00 | -5.24 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 57 | 5.35 | 100 | 110 | 45.24 | 1600.00 | -2.97 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 58 | 5.45 | 100 | 110 | 45.24 | 1600.00 | -1.33 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 59 | 5.55 | 100 | 110 | 45.24 | 1600.00 | -0.33 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |

Combinazioni SLEF

Paramento

Combinazione n° 11 - SLEF

Apertura limite fessure $w_{lim}=0.30$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | 0.00 | 5.81 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.20 | 100 | 42 | 0.00 | 0.00 | 0.02 | 16.80 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | 0.04 | 35.28 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | 0.09 | 65.88 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.50 | 100 | 44 | 0.00 | 0.00 | 0.17 | 118.89 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.60 | 100 | 45 | 0.00 | 0.00 | 0.28 | 222.15 | 0.000000 | 0.00 | 0.000 |
| 8 | -0.70 | 100 | 45 | 0.00 | 0.00 | 0.42 | 484.78 | 0.000000 | 0.00 | 0.000 |
| 9 | -0.80 | 100 | 46 | 0.00 | 0.00 | 0.62 | 2201.91 | 0.000000 | 0.00 | 0.000 |
| 10 | -0.90 | 100 | 47 | 0.00 | 0.00 | 0.86 | 1546.90 | 0.000000 | 0.00 | 0.000 |
| 11 | -1.00 | 100 | 48 | 0.00 | 0.00 | 1.17 | 704.98 | 0.000000 | 0.00 | 0.000 |
| 12 | -1.10 | 100 | 49 | 53.09 | 1600.00 | 1.54 | 508.13 | 0.000000 | 0.00 | 0.000 |
| 13 | -1.20 | 100 | 49 | 53.09 | 1600.00 | 1.98 | 423.46 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 120 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 14 | -1.30 | 100 | 50 | 53.09 | 1600.00 | 2.50 | 378.29 | 0.000000 | 0.00 | 0.000 |
| 15 | -1.40 | 100 | 51 | 53.09 | 1600.00 | 3.11 | 351.57 | 0.000000 | 0.00 | 0.000 |
| 16 | -1.50 | 100 | 52 | 53.09 | 1600.00 | 3.81 | 334.94 | 0.000000 | 0.00 | 0.000 |
| 17 | -1.60 | 100 | 52 | 53.09 | 1600.00 | 4.60 | 324.43 | 0.000000 | 0.00 | 0.000 |
| 18 | -1.70 | 100 | 53 | 53.09 | 1600.00 | 5.49 | 317.91 | 0.000000 | 0.00 | 0.000 |
| 19 | -1.80 | 100 | 54 | 53.09 | 1600.00 | 6.50 | 314.14 | 0.000000 | 0.00 | 0.000 |
| 20 | -1.90 | 100 | 55 | 53.09 | 1600.00 | 7.61 | 312.36 | 0.000000 | 0.00 | 0.000 |
| 21 | -2.00 | 100 | 56 | 53.09 | 1600.00 | 8.85 | 312.06 | 0.000000 | 0.00 | 0.000 |
| 22 | -2.10 | 100 | 56 | 53.09 | 1600.00 | 10.21 | 312.89 | 0.000000 | 0.00 | 0.000 |
| 23 | -2.20 | 100 | 57 | 53.09 | 1600.00 | 11.70 | 314.62 | 0.000000 | 0.00 | 0.000 |
| 24 | -2.30 | 100 | 58 | 53.09 | 1600.00 | 13.33 | 317.08 | 0.000000 | 0.00 | 0.000 |
| 25 | -2.40 | 100 | 59 | 53.09 | 1600.00 | 15.10 | 320.12 | 0.000000 | 0.00 | 0.000 |
| 26 | -2.50 | 100 | 59 | 53.09 | 1600.00 | 17.02 | 323.66 | 0.000000 | 0.00 | 0.000 |
| 27 | -2.60 | 100 | 60 | 53.09 | 1600.00 | 19.09 | 327.62 | 0.000000 | 0.00 | 0.000 |
| 28 | -2.70 | 100 | 61 | 53.09 | 1600.00 | 21.32 | 331.94 | 0.000000 | 0.00 | 0.000 |
| 29 | -2.80 | 100 | 62 | 53.09 | 1600.00 | 23.72 | 336.58 | 0.000000 | 0.00 | 0.000 |
| 30 | -2.90 | 100 | 63 | 53.09 | 1600.00 | 26.29 | 341.49 | 0.000000 | 0.00 | 0.000 |
| 31 | -3.00 | 100 | 63 | 53.09 | 1600.00 | 29.04 | 346.65 | 0.000000 | 0.00 | 0.000 |
| 32 | -3.10 | 100 | 64 | 53.09 | 1600.00 | 31.97 | 352.03 | 0.000000 | 0.00 | 0.000 |
| 33 | -3.20 | 100 | 65 | 53.09 | 1600.00 | 35.08 | 357.61 | 0.000000 | 0.00 | 0.000 |
| 34 | -3.30 | 100 | 66 | 53.09 | 1600.00 | 38.40 | 363.38 | 0.000000 | 0.00 | 0.000 |
| 35 | -3.40 | 100 | 66 | 53.09 | 1600.00 | 41.91 | 369.31 | 0.000000 | 0.00 | 0.000 |
| 36 | -3.50 | 100 | 67 | 53.09 | 1600.00 | 45.63 | 375.40 | 0.000000 | 0.00 | 0.000 |
| 37 | -3.60 | 100 | 68 | 53.09 | 1600.00 | 49.56 | 381.64 | 0.000000 | 0.00 | 0.000 |
| 38 | -3.70 | 100 | 69 | 53.09 | 1600.00 | 53.70 | 388.02 | 0.000000 | 0.00 | 0.000 |
| 39 | -3.80 | 100 | 70 | 53.09 | 1600.00 | 58.08 | 394.53 | 0.000000 | 0.00 | 0.000 |
| 40 | -3.90 | 100 | 70 | 53.09 | 1600.00 | 62.68 | 401.16 | 0.000000 | 0.00 | 0.000 |
| 41 | -4.00 | 100 | 71 | 53.09 | 1600.00 | 67.51 | 407.91 | 0.000000 | 0.00 | 0.000 |
| 42 | -4.10 | 100 | 72 | 53.09 | 1600.00 | 72.59 | 414.78 | 0.000000 | 0.00 | 0.000 |
| 43 | -4.20 | 100 | 73 | 53.09 | 1600.00 | 77.91 | 421.75 | 0.000000 | 0.00 | 0.000 |
| 44 | -4.30 | 100 | 73 | 53.09 | 1600.00 | 83.48 | 428.82 | 0.000000 | 0.00 | 0.000 |
| 45 | -4.40 | 100 | 74 | 53.09 | 1600.00 | 89.31 | 436.00 | 0.000000 | 0.00 | 0.000 |
| 46 | -4.50 | 100 | 75 | 53.09 | 1600.00 | 95.41 | 443.27 | 0.000000 | 0.00 | 0.000 |
| 47 | -4.60 | 100 | 76 | 53.09 | 1600.00 | 101.77 | 450.64 | 0.000000 | 0.00 | 0.000 |
| 48 | -4.70 | 100 | 77 | 53.09 | 1600.00 | 108.41 | 458.10 | 0.000000 | 0.00 | 0.000 |
| 49 | -4.80 | 100 | 77 | 53.09 | 1600.00 | 115.34 | 465.65 | 0.000000 | 0.00 | 0.000 |
| 50 | -4.90 | 100 | 78 | 53.09 | 1600.00 | 122.54 | 473.29 | 0.000000 | 0.00 | 0.000 |
| 51 | -5.00 | 100 | 79 | 53.09 | 1600.00 | 130.04 | 481.02 | 0.000000 | 0.00 | 0.000 |
| 52 | -5.10 | 100 | 80 | 53.09 | 1600.00 | 137.84 | 488.83 | 0.000000 | 0.00 | 0.000 |
| 53 | -5.20 | 100 | 80 | 53.09 | 1600.00 | 145.95 | 496.73 | 0.000000 | 0.00 | 0.000 |
| 54 | -5.30 | 100 | 81 | 53.09 | 1600.00 | 154.36 | 504.70 | 0.000000 | 0.00 | 0.000 |
| 55 | -5.40 | 100 | 82 | 53.09 | 1600.00 | 163.09 | 512.76 | 0.000000 | 0.00 | 0.000 |
| 56 | -5.50 | 100 | 83 | 53.09 | 1600.00 | 172.14 | 520.90 | 0.000000 | 0.00 | 0.000 |
| 57 | -5.60 | 100 | 84 | 53.09 | 1600.00 | 181.51 | 529.12 | 0.000000 | 0.00 | 0.000 |
| 58 | -5.70 | 100 | 84 | 53.09 | 1600.00 | 191.22 | 537.41 | 0.000000 | 0.00 | 0.000 |
| 59 | -5.80 | 100 | 85 | 53.09 | 1600.00 | 201.27 | 545.78 | 0.000000 | 0.00 | 0.000 |
| 60 | -5.90 | 100 | 86 | 53.09 | 1600.00 | 211.67 | 554.23 | 0.000000 | 0.00 | 0.000 |
| 61 | -6.00 | 100 | 87 | 53.09 | 1600.00 | 222.45 | 562.75 | 0.000000 | 0.00 | 0.000 |
| 62 | -6.10 | 100 | 87 | 53.09 | 1600.00 | 233.61 | 571.33 | 0.000000 | 0.00 | 0.000 |
| 63 | -6.20 | 100 | 88 | 53.09 | 1600.00 | 245.17 | 579.99 | 0.000000 | 0.00 | 0.000 |
| 64 | -6.30 | 100 | 89 | 53.09 | 1600.00 | 257.15 | 588.72 | 0.000000 | 0.00 | 0.000 |
| 65 | -6.40 | 100 | 90 | 53.09 | 1600.00 | 269.54 | 597.51 | 0.000000 | 0.00 | 0.000 |
| 66 | -6.50 | 100 | 91 | 53.09 | 1600.00 | 282.37 | 606.37 | 0.000000 | 0.00 | 0.000 |

Fondazione

Combinazione n° 11 - SLEF

Apertura limite fessure $w_{lim}=0.30$

| n° | Y | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|-------|------|------|-------|---------|---------|---------|----------|------|-------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 1 | -1.00 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.90 | 100 | 110 | 45.24 | 1600.00 | 0.85 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.80 | 100 | 110 | 45.24 | 1600.00 | 3.38 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.70 | 100 | 110 | 45.24 | 1600.00 | 7.58 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.60 | 100 | 110 | 45.24 | 1600.00 | 13.45 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.50 | 100 | 110 | 45.24 | 1600.00 | 20.95 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.40 | 100 | 110 | 45.24 | 1600.00 | 30.09 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 8 | 0.51 | 100 | 110 | 45.24 | 1600.00 | -428.05 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 9 | 0.60 | 100 | 110 | 45.24 | 1600.00 | -419.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 10 | 0.70 | 100 | 110 | 45.24 | 1600.00 | -410.76 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 11 | 0.80 | 100 | 110 | 45.24 | 1600.00 | -401.81 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 12 | 0.90 | 100 | 110 | 45.24 | 1600.00 | -392.67 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 13 | 1.00 | 100 | 110 | 45.24 | 1600.00 | -383.36 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 14 | 1.10 | 100 | 110 | 45.24 | 1600.00 | -373.88 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 15 | 1.20 | 100 | 110 | 45.24 | 1600.00 | -364.27 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 16 | 1.30 | 100 | 110 | 45.24 | 1600.00 | -354.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 17 | 1.40 | 100 | 110 | 45.24 | 1600.00 | -344.64 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 18 | 1.49 | 100 | 110 | 45.24 | 1600.00 | -334.67 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 19 | 1.59 | 100 | 110 | 45.24 | 1600.00 | -324.60 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 20 | 1.69 | 100 | 110 | 45.24 | 1600.00 | -314.45 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 21 | 1.79 | 100 | 110 | 45.24 | 1600.00 | -304.24 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 22 | 1.89 | 100 | 110 | 45.24 | 1600.00 | -293.98 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 23 | 1.99 | 100 | 110 | 45.24 | 1600.00 | -283.68 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 24 | 2.09 | 100 | 110 | 45.24 | 1600.00 | -273.35 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 25 | 2.19 | 100 | 110 | 45.24 | 1600.00 | -263.02 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 26 | 2.29 | 100 | 110 | 45.24 | 1600.00 | -252.68 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 27 | 2.38 | 100 | 110 | 45.24 | 1600.00 | -242.37 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 28 | 2.48 | 100 | 110 | 45.24 | 1600.00 | -232.08 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 29 | 2.58 | 100 | 110 | 45.24 | 1600.00 | -221.84 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 30 | 2.68 | 100 | 110 | 45.24 | 1600.00 | -211.65 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 31 | 2.78 | 100 | 110 | 45.24 | 1600.00 | -201.54 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 32 | 2.88 | 100 | 110 | 45.24 | 1600.00 | -191.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 33 | 2.98 | 100 | 110 | 45.24 | 1600.00 | -181.58 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 34 | 3.08 | 100 | 110 | 45.24 | 1600.00 | -171.76 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 35 | 3.17 | 100 | 110 | 45.24 | 1600.00 | -162.06 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 36 | 3.27 | 100 | 110 | 45.24 | 1600.00 | -152.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 37 | 3.37 | 100 | 110 | 45.24 | 1600.00 | -143.10 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 38 | 3.47 | 100 | 110 | 45.24 | 1600.00 | -133.86 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 39 | 3.57 | 100 | 110 | 45.24 | 1600.00 | -124.80 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 40 | 3.67 | 100 | 110 | 45.24 | 1600.00 | -115.94 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 41 | 3.77 | 100 | 110 | 45.24 | 1600.00 | -106.00 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 42 | 3.87 | 100 | 110 | 45.24 | 1600.00 | -95.87 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 43 | 3.97 | 100 | 110 | 45.24 | 1600.00 | -86.17 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 44 | 4.06 | 100 | 110 | 45.24 | 1600.00 | -76.91 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 45 | 4.16 | 100 | 110 | 45.24 | 1600.00 | -68.10 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 46 | 4.26 | 100 | 110 | 45.24 | 1600.00 | -59.77 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 47 | 4.36 | 100 | 110 | 45.24 | 1600.00 | -51.92 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 48 | 4.46 | 100 | 110 | 45.24 | 1600.00 | -44.56 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 49 | 4.56 | 100 | 110 | 45.24 | 1600.00 | -37.72 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 50 | 4.66 | 100 | 110 | 45.24 | 1600.00 | -31.40 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 51 | 4.76 | 100 | 110 | 45.24 | 1600.00 | -25.62 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 52 | 4.86 | 100 | 110 | 45.24 | 1600.00 | -20.38 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 53 | 4.95 | 100 | 110 | 45.24 | 1600.00 | -15.72 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 54 | 5.05 | 100 | 110 | 45.24 | 1600.00 | -11.63 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 55 | 5.15 | 100 | 110 | 45.24 | 1600.00 | -8.13 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 56 | 5.25 | 100 | 110 | 45.24 | 1600.00 | -5.24 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 57 | 5.35 | 100 | 110 | 45.24 | 1600.00 | -2.97 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 58 | 5.45 | 100 | 110 | 45.24 | 1600.00 | -1.33 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 59 | 5.55 | 100 | 110 | 45.24 | 1600.00 | -0.33 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |

Paramento

Combinazione n° 12 - SLEQ

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | 0.00 | 5.81 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.20 | 100 | 42 | 0.00 | 0.00 | 0.02 | 16.80 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | 0.04 | 35.28 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | 0.09 | 65.88 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.50 | 100 | 44 | 0.00 | 0.00 | 0.17 | 118.89 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.60 | 100 | 45 | 0.00 | 0.00 | 0.28 | 222.15 | 0.000000 | 0.00 | 0.000 |
| 8 | -0.70 | 100 | 45 | 0.00 | 0.00 | 0.42 | 484.78 | 0.000000 | 0.00 | 0.000 |
| 9 | -0.80 | 100 | 46 | 0.00 | 0.00 | 0.62 | 2201.91 | 0.000000 | 0.00 | 0.000 |
| 10 | -0.90 | 100 | 47 | 0.00 | 0.00 | 0.86 | 1546.90 | 0.000000 | 0.00 | 0.000 |
| 11 | -1.00 | 100 | 48 | 0.00 | 0.00 | 1.17 | 704.98 | 0.000000 | 0.00 | 0.000 |
| 12 | -1.10 | 100 | 49 | 53.09 | 1600.00 | 1.54 | 508.13 | 0.000000 | 0.00 | 0.000 |
| 13 | -1.20 | 100 | 49 | 53.09 | 1600.00 | 1.98 | 423.46 | 0.000000 | 0.00 | 0.000 |
| 14 | -1.30 | 100 | 50 | 53.09 | 1600.00 | 2.50 | 378.29 | 0.000000 | 0.00 | 0.000 |
| 15 | -1.40 | 100 | 51 | 53.09 | 1600.00 | 3.11 | 351.57 | 0.000000 | 0.00 | 0.000 |
| 16 | -1.50 | 100 | 52 | 53.09 | 1600.00 | 3.81 | 334.94 | 0.000000 | 0.00 | 0.000 |
| 17 | -1.60 | 100 | 52 | 53.09 | 1600.00 | 4.60 | 324.43 | 0.000000 | 0.00 | 0.000 |
| 18 | -1.70 | 100 | 53 | 53.09 | 1600.00 | 5.49 | 317.91 | 0.000000 | 0.00 | 0.000 |
| 19 | -1.80 | 100 | 54 | 53.09 | 1600.00 | 6.50 | 314.14 | 0.000000 | 0.00 | 0.000 |
| 20 | -1.90 | 100 | 55 | 53.09 | 1600.00 | 7.61 | 312.36 | 0.000000 | 0.00 | 0.000 |
| 21 | -2.00 | 100 | 56 | 53.09 | 1600.00 | 8.85 | 312.06 | 0.000000 | 0.00 | 0.000 |
| 22 | -2.10 | 100 | 56 | 53.09 | 1600.00 | 10.21 | 312.89 | 0.000000 | 0.00 | 0.000 |
| 23 | -2.20 | 100 | 57 | 53.09 | 1600.00 | 11.70 | 314.62 | 0.000000 | 0.00 | 0.000 |
| 24 | -2.30 | 100 | 58 | 53.09 | 1600.00 | 13.33 | 317.08 | 0.000000 | 0.00 | 0.000 |
| 25 | -2.40 | 100 | 59 | 53.09 | 1600.00 | 15.10 | 320.12 | 0.000000 | 0.00 | 0.000 |
| 26 | -2.50 | 100 | 59 | 53.09 | 1600.00 | 17.02 | 323.66 | 0.000000 | 0.00 | 0.000 |
| 27 | -2.60 | 100 | 60 | 53.09 | 1600.00 | 19.09 | 327.62 | 0.000000 | 0.00 | 0.000 |
| 28 | -2.70 | 100 | 61 | 53.09 | 1600.00 | 21.32 | 331.94 | 0.000000 | 0.00 | 0.000 |
| 29 | -2.80 | 100 | 62 | 53.09 | 1600.00 | 23.72 | 336.58 | 0.000000 | 0.00 | 0.000 |
| 30 | -2.90 | 100 | 63 | 53.09 | 1600.00 | 26.29 | 341.49 | 0.000000 | 0.00 | 0.000 |
| 31 | -3.00 | 100 | 63 | 53.09 | 1600.00 | 29.04 | 346.65 | 0.000000 | 0.00 | 0.000 |
| 32 | -3.10 | 100 | 64 | 53.09 | 1600.00 | 31.97 | 352.03 | 0.000000 | 0.00 | 0.000 |
| 33 | -3.20 | 100 | 65 | 53.09 | 1600.00 | 35.08 | 357.61 | 0.000000 | 0.00 | 0.000 |
| 34 | -3.30 | 100 | 66 | 53.09 | 1600.00 | 38.40 | 363.38 | 0.000000 | 0.00 | 0.000 |
| 35 | -3.40 | 100 | 66 | 53.09 | 1600.00 | 41.91 | 369.31 | 0.000000 | 0.00 | 0.000 |
| 36 | -3.50 | 100 | 67 | 53.09 | 1600.00 | 45.63 | 375.40 | 0.000000 | 0.00 | 0.000 |
| 37 | -3.60 | 100 | 68 | 53.09 | 1600.00 | 49.56 | 381.64 | 0.000000 | 0.00 | 0.000 |
| 38 | -3.70 | 100 | 69 | 53.09 | 1600.00 | 53.70 | 388.02 | 0.000000 | 0.00 | 0.000 |
| 39 | -3.80 | 100 | 70 | 53.09 | 1600.00 | 58.08 | 394.53 | 0.000000 | 0.00 | 0.000 |
| 40 | -3.90 | 100 | 70 | 53.09 | 1600.00 | 62.68 | 401.16 | 0.000000 | 0.00 | 0.000 |
| 41 | -4.00 | 100 | 71 | 53.09 | 1600.00 | 67.51 | 407.91 | 0.000000 | 0.00 | 0.000 |
| 42 | -4.10 | 100 | 72 | 53.09 | 1600.00 | 72.59 | 414.78 | 0.000000 | 0.00 | 0.000 |
| 43 | -4.20 | 100 | 73 | 53.09 | 1600.00 | 77.91 | 421.75 | 0.000000 | 0.00 | 0.000 |
| 44 | -4.30 | 100 | 73 | 53.09 | 1600.00 | 83.48 | 428.82 | 0.000000 | 0.00 | 0.000 |
| 45 | -4.40 | 100 | 74 | 53.09 | 1600.00 | 89.31 | 436.00 | 0.000000 | 0.00 | 0.000 |
| 46 | -4.50 | 100 | 75 | 53.09 | 1600.00 | 95.41 | 443.27 | 0.000000 | 0.00 | 0.000 |
| 47 | -4.60 | 100 | 76 | 53.09 | 1600.00 | 101.77 | 450.64 | 0.000000 | 0.00 | 0.000 |
| 48 | -4.70 | 100 | 77 | 53.09 | 1600.00 | 108.41 | 458.10 | 0.000000 | 0.00 | 0.000 |
| 49 | -4.80 | 100 | 77 | 53.09 | 1600.00 | 115.34 | 465.65 | 0.000000 | 0.00 | 0.000 |
| 50 | -4.90 | 100 | 78 | 53.09 | 1600.00 | 122.54 | 473.29 | 0.000000 | 0.00 | 0.000 |
| 51 | -5.00 | 100 | 79 | 53.09 | 1600.00 | 130.04 | 481.02 | 0.000000 | 0.00 | 0.000 |
| 52 | -5.10 | 100 | 80 | 53.09 | 1600.00 | 137.84 | 488.83 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 123 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 53 | -5.20 | 100 | 80 | 53.09 | 1600.00 | 145.95 | 496.73 | 0.000000 | 0.00 | 0.000 |
| 54 | -5.30 | 100 | 81 | 53.09 | 1600.00 | 154.36 | 504.70 | 0.000000 | 0.00 | 0.000 |
| 55 | -5.40 | 100 | 82 | 53.09 | 1600.00 | 163.09 | 512.76 | 0.000000 | 0.00 | 0.000 |
| 56 | -5.50 | 100 | 83 | 53.09 | 1600.00 | 172.14 | 520.90 | 0.000000 | 0.00 | 0.000 |
| 57 | -5.60 | 100 | 84 | 53.09 | 1600.00 | 181.51 | 529.12 | 0.000000 | 0.00 | 0.000 |
| 58 | -5.70 | 100 | 84 | 53.09 | 1600.00 | 191.22 | 537.41 | 0.000000 | 0.00 | 0.000 |
| 59 | -5.80 | 100 | 85 | 53.09 | 1600.00 | 201.27 | 545.78 | 0.000000 | 0.00 | 0.000 |
| 60 | -5.90 | 100 | 86 | 53.09 | 1600.00 | 211.67 | 554.23 | 0.000000 | 0.00 | 0.000 |
| 61 | -6.00 | 100 | 87 | 53.09 | 1600.00 | 222.45 | 562.75 | 0.000000 | 0.00 | 0.000 |
| 62 | -6.10 | 100 | 87 | 53.09 | 1600.00 | 233.61 | 571.33 | 0.000000 | 0.00 | 0.000 |
| 63 | -6.20 | 100 | 88 | 53.09 | 1600.00 | 245.17 | 579.99 | 0.000000 | 0.00 | 0.000 |
| 64 | -6.30 | 100 | 89 | 53.09 | 1600.00 | 257.15 | 588.72 | 0.000000 | 0.00 | 0.000 |
| 65 | -6.40 | 100 | 90 | 53.09 | 1600.00 | 269.54 | 597.51 | 0.000000 | 0.00 | 0.000 |
| 66 | -6.50 | 100 | 91 | 53.09 | 1600.00 | 282.37 | 606.37 | 0.000000 | 0.00 | 0.000 |

Combinazione n° 13 - SLEQ H + V

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | 0.01 | 14.66 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.20 | 100 | 42 | 0.00 | 0.00 | 0.03 | 40.58 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | 0.08 | 88.30 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | 0.17 | 189.00 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.50 | 100 | 44 | 0.00 | 0.00 | 0.29 | 491.90 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.60 | 100 | 45 | 0.00 | 0.00 | 0.46 | 11073.41 | 0.000000 | 0.00 | 0.000 |
| 8 | -0.70 | 100 | 45 | 0.00 | 0.00 | 0.69 | 874.79 | 0.000000 | 0.00 | 0.000 |
| 9 | -0.80 | 100 | 46 | 53.09 | 1600.00 | 0.98 | 510.03 | 0.000000 | 0.00 | 0.000 |
| 10 | -0.90 | 100 | 47 | 53.09 | 1600.00 | 1.34 | 397.38 | 0.000000 | 0.00 | 0.000 |
| 11 | -1.00 | 100 | 48 | 53.09 | 1600.00 | 1.78 | 344.91 | 0.000000 | 0.00 | 0.000 |
| 12 | -1.10 | 100 | 49 | 53.09 | 1600.00 | 2.30 | 316.14 | 0.000000 | 0.00 | 0.000 |
| 13 | -1.20 | 100 | 49 | 53.09 | 1600.00 | 2.93 | 299.18 | 0.000000 | 0.00 | 0.000 |
| 14 | -1.30 | 100 | 50 | 53.09 | 1600.00 | 3.65 | 288.95 | 0.000000 | 0.00 | 0.000 |
| 15 | -1.40 | 100 | 51 | 53.09 | 1600.00 | 4.49 | 282.92 | 0.000000 | 0.00 | 0.000 |
| 16 | -1.50 | 100 | 52 | 53.09 | 1600.00 | 5.45 | 279.69 | 0.000000 | 0.00 | 0.000 |
| 17 | -1.60 | 100 | 52 | 53.09 | 1600.00 | 6.53 | 278.43 | 0.000000 | 0.00 | 0.000 |
| 18 | -1.70 | 100 | 53 | 53.09 | 1600.00 | 7.74 | 278.60 | 0.000000 | 0.00 | 0.000 |
| 19 | -1.80 | 100 | 54 | 53.09 | 1600.00 | 9.09 | 279.86 | 0.000000 | 0.00 | 0.000 |
| 20 | -1.90 | 100 | 55 | 53.09 | 1600.00 | 10.59 | 281.96 | 0.000000 | 0.00 | 0.000 |
| 21 | -2.00 | 100 | 56 | 53.09 | 1600.00 | 12.24 | 284.73 | 0.000000 | 0.00 | 0.000 |
| 22 | -2.10 | 100 | 56 | 53.09 | 1600.00 | 14.05 | 288.05 | 0.000000 | 0.00 | 0.000 |
| 23 | -2.20 | 100 | 57 | 53.09 | 1600.00 | 16.03 | 291.81 | 0.000000 | 0.00 | 0.000 |
| 24 | -2.30 | 100 | 58 | 53.09 | 1600.00 | 18.19 | 295.96 | 0.000000 | 0.00 | 0.000 |
| 25 | -2.40 | 100 | 59 | 53.09 | 1600.00 | 20.53 | 300.43 | 0.000000 | 0.00 | 0.000 |
| 26 | -2.50 | 100 | 59 | 53.09 | 1600.00 | 23.06 | 305.19 | 0.000000 | 0.00 | 0.000 |
| 27 | -2.60 | 100 | 60 | 53.09 | 1600.00 | 25.79 | 310.20 | 0.000000 | 0.00 | 0.000 |
| 28 | -2.70 | 100 | 61 | 53.09 | 1600.00 | 28.72 | 315.43 | 0.000000 | 0.00 | 0.000 |
| 29 | -2.80 | 100 | 62 | 53.09 | 1600.00 | 31.87 | 320.85 | 0.000000 | 0.00 | 0.000 |
| 30 | -2.90 | 100 | 63 | 53.09 | 1600.00 | 35.23 | 326.46 | 0.000000 | 0.00 | 0.000 |
| 31 | -3.00 | 100 | 63 | 53.09 | 1600.00 | 38.82 | 332.24 | 0.000000 | 0.00 | 0.000 |
| 32 | -3.10 | 100 | 64 | 53.09 | 1600.00 | 42.64 | 338.17 | 0.000000 | 0.00 | 0.000 |
| 33 | -3.20 | 100 | 65 | 53.09 | 1600.00 | 46.70 | 344.24 | 0.000000 | 0.00 | 0.000 |
| 34 | -3.30 | 100 | 66 | 53.09 | 1600.00 | 51.01 | 350.44 | 0.000000 | 0.00 | 0.000 |
| 35 | -3.40 | 100 | 66 | 53.09 | 1600.00 | 55.57 | 356.77 | 0.000000 | 0.00 | 0.000 |
| 36 | -3.50 | 100 | 67 | 53.09 | 1600.00 | 60.40 | 363.22 | 0.000000 | 0.00 | 0.000 |
| 37 | -3.60 | 100 | 68 | 53.09 | 1600.00 | 65.50 | 369.79 | 0.000000 | 0.00 | 0.000 |
| 38 | -3.70 | 100 | 69 | 53.09 | 1600.00 | 70.87 | 376.46 | 0.000000 | 0.00 | 0.000 |
| 39 | -3.80 | 100 | 70 | 53.09 | 1600.00 | 76.52 | 383.23 | 0.000000 | 0.00 | 0.000 |
| 40 | -3.90 | 100 | 70 | 53.09 | 1600.00 | 82.47 | 390.11 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 41 | -4.00 | 100 | 71 | 53.09 | 1600.00 | 88.72 | 397.08 | 0.000000 | 0.00 | 0.000 |
| 42 | -4.10 | 100 | 72 | 53.09 | 1600.00 | 95.27 | 404.15 | 0.000000 | 0.00 | 0.000 |
| 43 | -4.20 | 100 | 73 | 53.09 | 1600.00 | 102.13 | 411.31 | 0.000000 | 0.00 | 0.000 |
| 44 | -4.30 | 100 | 73 | 53.09 | 1600.00 | 109.31 | 418.56 | 0.000000 | 0.00 | 0.000 |
| 45 | -4.40 | 100 | 74 | 53.09 | 1600.00 | 116.82 | 425.89 | 0.000000 | 0.00 | 0.000 |
| 46 | -4.50 | 100 | 75 | 53.09 | 1600.00 | 124.66 | 433.31 | 0.000000 | 0.00 | 0.000 |
| 47 | -4.60 | 100 | 76 | 53.09 | 1600.00 | 132.85 | 440.82 | 0.000000 | 0.00 | 0.000 |
| 48 | -4.70 | 100 | 77 | 53.09 | 1600.00 | 141.38 | 448.40 | 0.000000 | 0.00 | 0.000 |
| 49 | -4.80 | 100 | 77 | 53.09 | 1600.00 | 150.27 | 456.07 | 0.000000 | 0.00 | 0.000 |
| 50 | -4.90 | 100 | 78 | 53.09 | 1600.00 | 159.52 | 463.82 | 0.000000 | 0.00 | 0.000 |
| 51 | -5.00 | 100 | 79 | 53.09 | 1600.00 | 169.14 | 471.64 | 0.000000 | 0.00 | 0.000 |
| 52 | -5.10 | 100 | 80 | 53.09 | 1600.00 | 179.14 | 479.54 | 0.000000 | 0.00 | 0.000 |
| 53 | -5.20 | 100 | 80 | 53.09 | 1600.00 | 189.52 | 487.52 | 0.000000 | 0.00 | 0.000 |
| 54 | -5.30 | 100 | 81 | 53.09 | 1600.00 | 200.30 | 495.58 | 0.000000 | 0.00 | 0.000 |
| 55 | -5.40 | 100 | 82 | 53.09 | 1600.00 | 211.47 | 503.71 | 0.000000 | 0.00 | 0.000 |
| 56 | -5.50 | 100 | 83 | 53.09 | 1600.00 | 223.05 | 511.91 | 0.000000 | 0.00 | 0.000 |
| 57 | -5.60 | 100 | 84 | 53.09 | 1600.00 | 235.05 | 520.19 | 0.000000 | 0.00 | 0.000 |
| 58 | -5.70 | 100 | 84 | 53.09 | 1600.00 | 247.46 | 528.54 | 0.000000 | 0.00 | 0.000 |
| 59 | -5.80 | 100 | 85 | 53.09 | 1600.00 | 260.30 | 536.97 | 0.000000 | 0.00 | 0.000 |
| 60 | -5.90 | 100 | 86 | 53.09 | 1600.00 | 273.59 | 545.46 | 0.000000 | 0.00 | 0.000 |
| 61 | -6.00 | 100 | 87 | 53.09 | 1600.00 | 287.34 | 554.02 | 0.000000 | 0.00 | 0.000 |
| 62 | -6.10 | 100 | 87 | 53.09 | 1600.00 | 301.57 | 562.66 | 0.000000 | 0.00 | 0.000 |
| 63 | -6.20 | 100 | 88 | 53.09 | 1600.00 | 316.29 | 571.36 | 0.000000 | 0.00 | 0.000 |
| 64 | -6.30 | 100 | 89 | 53.09 | 1600.00 | 331.53 | 580.12 | 0.000000 | 0.00 | 0.000 |
| 65 | -6.40 | 100 | 90 | 53.09 | 1600.00 | 347.29 | 588.96 | 0.000000 | 0.00 | 0.000 |
| 66 | -6.50 | 100 | 91 | 53.09 | 1600.00 | 363.57 | 597.86 | 0.000000 | 0.00 | 0.000 |

Fondazione

Combinazione n° 12 - SLEQ

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | -1.00 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.90 | 100 | 110 | 45.24 | 1600.00 | 0.85 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.80 | 100 | 110 | 45.24 | 1600.00 | 3.38 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.70 | 100 | 110 | 45.24 | 1600.00 | 7.58 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.60 | 100 | 110 | 45.24 | 1600.00 | 13.45 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.50 | 100 | 110 | 45.24 | 1600.00 | 20.95 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.40 | 100 | 110 | 45.24 | 1600.00 | 30.09 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 8 | 0.51 | 100 | 110 | 45.24 | 1600.00 | -428.05 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 9 | 0.60 | 100 | 110 | 45.24 | 1600.00 | -419.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 10 | 0.70 | 100 | 110 | 45.24 | 1600.00 | -410.76 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 11 | 0.80 | 100 | 110 | 45.24 | 1600.00 | -401.81 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 12 | 0.90 | 100 | 110 | 45.24 | 1600.00 | -392.67 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 13 | 1.00 | 100 | 110 | 45.24 | 1600.00 | -383.36 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 14 | 1.10 | 100 | 110 | 45.24 | 1600.00 | -373.88 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 15 | 1.20 | 100 | 110 | 45.24 | 1600.00 | -364.27 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 16 | 1.30 | 100 | 110 | 45.24 | 1600.00 | -354.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 17 | 1.40 | 100 | 110 | 45.24 | 1600.00 | -344.64 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 18 | 1.49 | 100 | 110 | 45.24 | 1600.00 | -334.67 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 19 | 1.59 | 100 | 110 | 45.24 | 1600.00 | -324.60 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 20 | 1.69 | 100 | 110 | 45.24 | 1600.00 | -314.45 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 21 | 1.79 | 100 | 110 | 45.24 | 1600.00 | -304.24 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 22 | 1.89 | 100 | 110 | 45.24 | 1600.00 | -293.98 | -719.00 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
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| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 23 | 1.99 | 100 | 110 | 45.24 | 1600.00 | -283.68 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 24 | 2.09 | 100 | 110 | 45.24 | 1600.00 | -273.35 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 25 | 2.19 | 100 | 110 | 45.24 | 1600.00 | -263.02 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 26 | 2.29 | 100 | 110 | 45.24 | 1600.00 | -252.68 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 27 | 2.38 | 100 | 110 | 45.24 | 1600.00 | -242.37 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 28 | 2.48 | 100 | 110 | 45.24 | 1600.00 | -232.08 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 29 | 2.58 | 100 | 110 | 45.24 | 1600.00 | -221.84 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 30 | 2.68 | 100 | 110 | 45.24 | 1600.00 | -211.65 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 31 | 2.78 | 100 | 110 | 45.24 | 1600.00 | -201.54 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 32 | 2.88 | 100 | 110 | 45.24 | 1600.00 | -191.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 33 | 2.98 | 100 | 110 | 45.24 | 1600.00 | -181.58 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 34 | 3.08 | 100 | 110 | 45.24 | 1600.00 | -171.76 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 35 | 3.17 | 100 | 110 | 45.24 | 1600.00 | -162.06 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 36 | 3.27 | 100 | 110 | 45.24 | 1600.00 | -152.51 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 37 | 3.37 | 100 | 110 | 45.24 | 1600.00 | -143.10 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 38 | 3.47 | 100 | 110 | 45.24 | 1600.00 | -133.86 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 39 | 3.57 | 100 | 110 | 45.24 | 1600.00 | -124.80 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 40 | 3.67 | 100 | 110 | 45.24 | 1600.00 | -115.94 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 41 | 3.77 | 100 | 110 | 45.24 | 1600.00 | -106.00 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 42 | 3.87 | 100 | 110 | 45.24 | 1600.00 | -95.87 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 43 | 3.97 | 100 | 110 | 45.24 | 1600.00 | -86.17 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 44 | 4.06 | 100 | 110 | 45.24 | 1600.00 | -76.91 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 45 | 4.16 | 100 | 110 | 45.24 | 1600.00 | -68.10 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 46 | 4.26 | 100 | 110 | 45.24 | 1600.00 | -59.77 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 47 | 4.36 | 100 | 110 | 45.24 | 1600.00 | -51.92 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 48 | 4.46 | 100 | 110 | 45.24 | 1600.00 | -44.56 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 49 | 4.56 | 100 | 110 | 45.24 | 1600.00 | -37.72 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 50 | 4.66 | 100 | 110 | 45.24 | 1600.00 | -31.40 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 51 | 4.76 | 100 | 110 | 45.24 | 1600.00 | -25.62 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 52 | 4.86 | 100 | 110 | 45.24 | 1600.00 | -20.38 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 53 | 4.95 | 100 | 110 | 45.24 | 1600.00 | -15.72 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 54 | 5.05 | 100 | 110 | 45.24 | 1600.00 | -11.63 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 55 | 5.15 | 100 | 110 | 45.24 | 1600.00 | -8.13 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 56 | 5.25 | 100 | 110 | 45.24 | 1600.00 | -5.24 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 57 | 5.35 | 100 | 110 | 45.24 | 1600.00 | -2.97 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 58 | 5.45 | 100 | 110 | 45.24 | 1600.00 | -1.33 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 59 | 5.55 | 100 | 110 | 45.24 | 1600.00 | -0.33 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 60 | 5.65 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |

Combinazione n° 13 - SLEQ_H + V

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | -1.00 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.90 | 100 | 110 | 45.24 | 1600.00 | 1.12 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.80 | 100 | 110 | 45.24 | 1600.00 | 4.45 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.70 | 100 | 110 | 45.24 | 1600.00 | 9.97 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.60 | 100 | 110 | 45.24 | 1600.00 | 17.65 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.50 | 100 | 110 | 45.24 | 1600.00 | 27.47 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.40 | 100 | 110 | 45.24 | 1600.00 | 39.38 | 719.00 | 0.000000 | 0.00 | 0.000 |
| 8 | 0.51 | 100 | 110 | 45.24 | 1600.00 | -665.79 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 9 | 0.60 | 100 | 110 | 45.24 | 1600.00 | -654.36 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 10 | 0.70 | 100 | 110 | 45.24 | 1600.00 | -642.41 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 11 | 0.80 | 100 | 110 | 45.24 | 1600.00 | -629.97 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 12 | 0.90 | 100 | 110 | 45.24 | 1600.00 | -617.07 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 13 | 1.00 | 100 | 110 | 45.24 | 1600.00 | -603.73 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 14 | 1.10 | 100 | 110 | 45.24 | 1600.00 | -589.99 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 15 | 1.20 | 100 | 110 | 45.24 | 1600.00 | -575.87 | -719.00 | 0.000000 | 0.00 | 0.000 |
| 16 | 1.30 | 100 | 110 | 45.24 | 1600.00 | -561.40 | -719.00 | 0.000000 | 0.00 | 0.000 |

P_x, P_y Coordinata X ed Y del punto di applicazione dell'azione, espressa in [m]

| Ic | A | V | I | C _x | C _y | P _x | P _y |
|----|---|--------|------|----------------|----------------|----------------|----------------|
| | | [kN] | [°] | [kN] | [kN] | [m] | [m] |
| 1 | Spinta statica | 255.10 | 0.00 | 255.10 | 0.00 | 5.65 | -4.76 |
| | Peso/Inerzia muro | | | 0.00 | 283.28/0.00 | 1.45 | -5.81 |
| | Peso/Inerzia terrapieno | | | 0.00 | 734.00/0.00 | 2.96 | -3.20 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |

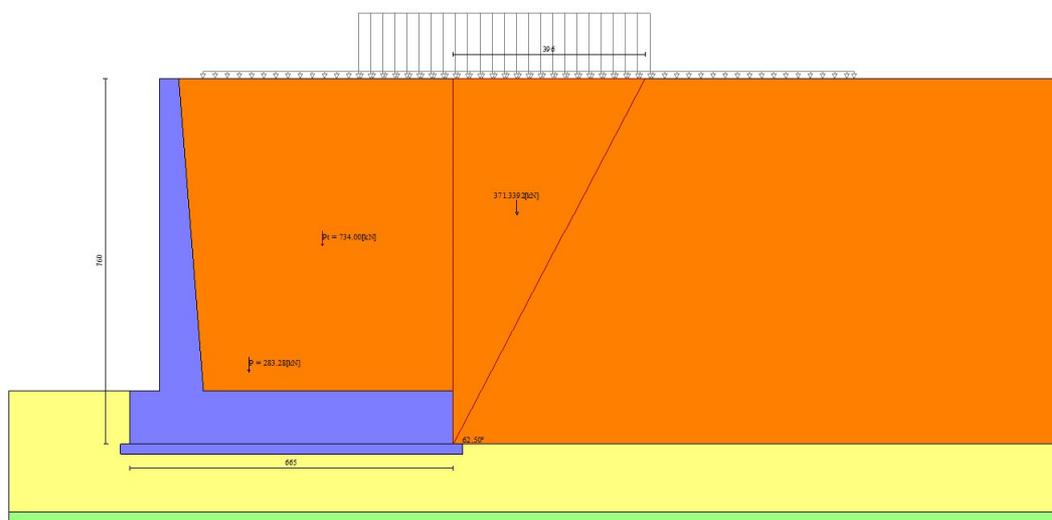


Fig. 12 - Cuneo di spinta (combinazione statica) (Combinazione n° 1)

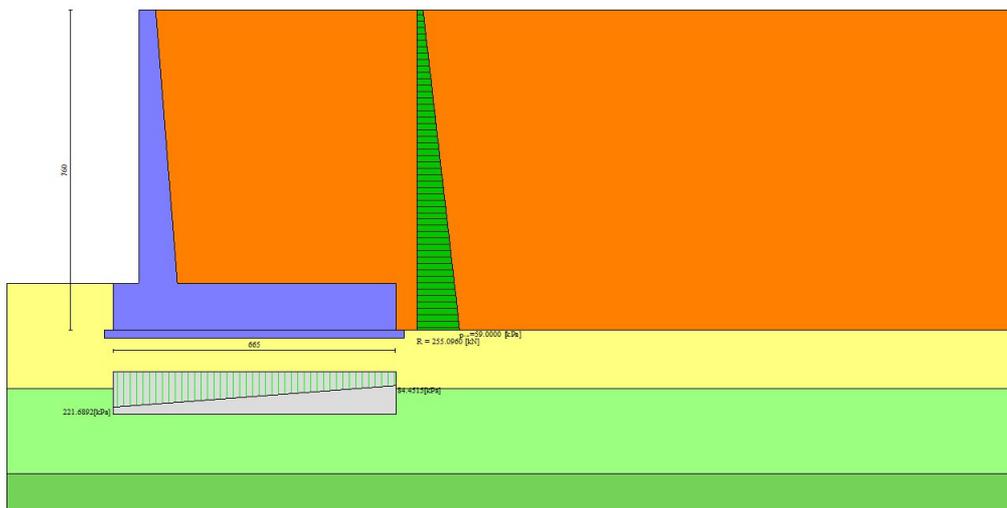


Fig. 13 - Diagramma delle pressioni (combinazione statica) (Combinazione n° 1)

Risultanti globali

Simbologia adottata

| | |
|----------------|---|
| Cmb | Indice/Tipo combinazione |
| N | Componente normale al piano di posa, espressa in [kN] |
| T | Componente parallela al piano di posa, espressa in [kN] |
| M _r | Momento ribaltante, espresso in [kNm] |
| M _s | Momento stabilizzante, espresso in [kNm] |
| ecc | Eccentricità risultante, espressa in [m] |

| Ic | N [kN] | T [kN] | M _r [kNm] | M _s [kNm] | ecc [m] |
|--------------------|-----------|-----------|-------------------------|-------------------------|------------|
| 1 - STR (A1-M1-R3) | 1017.28 | 255.10 | 724.52 | 3599.76 | 0.497 |
| 2 - STR (A1-M1-R3) | 1030.15 | 340.00 | 1015.40 | 3616.76 | 0.798 |
| 3 - STR (A1-M1-R3) | 904.62 | 319.70 | 1184.33 | 3396.39 | 0.878 |
| 4 - GEO (A2-M2-R2) | 1007.44 | 254.18 | 731.09 | 3559.65 | 0.515 |
| 5 - GEO (A2-M2-R2) | 1030.15 | 340.00 | 1015.40 | 3616.76 | 0.798 |
| 6 - GEO (A2-M2-R2) | 904.62 | 319.70 | 1184.33 | 3396.39 | 0.878 |
| 7 - EQU (A1-M1-R3) | 1017.28 | 255.10 | 724.52 | 3599.76 | 0.497 |
| 8 - EQU (A1-M1-R3) | 1049.97 | 398.20 | 1206.53 | 3686.35 | 0.961 |
| 9 - EQU (A1-M1-R3) | 884.80 | 372.22 | 1430.68 | 3396.39 | 1.101 |
| 10 - SLEF | 998.52 | 194.01 | 548.90 | 3523.28 | 0.344 |
| 11 - SLEF | 998.52 | 194.01 | 548.90 | 3523.28 | 0.344 |
| 12 - SLEQ | 998.52 | 194.01 | 548.90 | 3523.28 | 0.344 |
| 13 - SLEQ | 1036.26 | 305.59 | 916.47 | 3656.47 | 0.679 |

Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

| | |
|--------------------|--|
| Cmb | Indice/Tipo combinazione |
| S | Sisma (H: componente orizzontale, V: componente verticale) |
| FS _{SCO} | Coeff. di sicurezza allo scorrimento |
| FS _{RIB} | Coeff. di sicurezza al ribaltamento |
| FS _{QLIM} | Coeff. di sicurezza a carico limite |
| FS _{STAB} | Coeff. di sicurezza a stabilità globale |
| FS _{HYD} | Coeff. di sicurezza a sifonamento |
| FS _{SUPL} | Coeff. di sicurezza a sollevamento |

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{SUPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|--------------------|
| 1 - STR (A1-M1-R3) | | 1.860 | | 1.790 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.413 | | 1.236 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.319 | | 1.277 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.380 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.383 | | |
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.332 | | |
| 7 - EQU (A1-M1-R3) | | | 4.968 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 3.055 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.374 | | | | |

Verifica a scorrimento fondazione

Simbologia adottata

| | |
|-----------------|---|
| n° | Indice combinazione |
| R _{sa} | Resistenza allo scorrimento per attrito, espresso in [kN] |
| R _{pt} | Resistenza passiva terreno antistante, espresso in [kN] |
| R _{ps} | Resistenza passiva sperone, espresso in [kN] |
| R _p | Resistenza a carichi orizzontali pali (solo per fondazione mista), espresso in [kN] |
| R _t | Resistenza a carichi orizzontali tiranti (solo se presenti), espresso in [kN] |
| R | Resistenza allo scorrimento (somma di R _{sa} +R _{pt} +R _{ps} +R _p), espresso in [kN] |
| T | Carico parallelo al piano di posa, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto R/T) |

| n° | R _{sa} | R _{pt} | R _{ps} | R _p | R _t | R | T | FS |
|--------------------------|-----------------|-----------------|-----------------|----------------|----------------|--------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | |
| 3 - STR (A1-M1-R3) H - V | 421.83 | 0.00 | 0.00 | -- | -- | 421.83 | 319.70 | 1.319 |

Verifica a carico limite

Simbologia adottata

| | |
|----|---|
| n° | Indice combinazione |
| N | Carico normale totale al piano di posa, espresso in [kN] |
| Qu | carico limite del terreno, espresso in [kN] |
| Qd | Portanza di progetto, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto tra il carico limite e carico agente al piano di posa) |

| n° | N | Qu | Qd | FS |
|--------------------------|---------|---------|---------|-------|
| | [kN] | [kN] | [kN] | |
| 2 - STR (A1-M1-R3) H + V | 1030.15 | 1273.69 | 1061.41 | 1.236 |

Dettagli calcolo portanza

Simbologia adottata

| | |
|---------------------------|--|
| n° | Indice combinazione |
| Nc, Nq, Ny | Fattori di capacità portante |
| ic, iq, iy | Fattori di inclinazione del carico |
| dc, dq, dy | Fattori di profondità del piano di posa |
| gc, gq, gy | Fattori di inclinazione del profilo topografico |
| bc, bq, by | Fattori di inclinazione del piano di posa |
| sc, sq, sy | Fattori di forma della fondazione |
| pc, pq, py | Fattori di riduzione per punzonamento secondo Vesic |
| Re | Fattore di riduzione capacità portante per eccentricità secondo Meyerhof |
| Ir, Irc | Indici di rigidità per punzonamento secondo Vesic |
| r _y fattore | Fattori per tener conto dell'effetto piastra. Per fondazioni che hanno larghezza maggiore di 2 m, il terzo termine della formula trinomia 0.5B _y N _y viene moltiplicato per questo fattore |
| D | Affondamento del piano di posa, espresso in [m] |
| B' | Larghezza fondazione ridotta, espresso in [m] |
| H | Altezza del cuneo di rottura, espresso in [m] |
| γ | Peso di volume del terreno medio, espresso in [kN/mc] |
| φ | Angolo di attrito del terreno medio, espresso in [°] |
| c | Coesione del terreno medio, espresso in [kPa] |

Per i coeff. che in tabella sono indicati con il simbolo '-' sono coeff. non presenti nel metodo scelto (Meyerhof).

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 131 di 314 |

| n° | Nc Nq Ny | ic iq iy | dc dq dy | gc gq gy | bc bq by | sc sq sy | pc pq py | Ir | Irc | Re | ry |
|----|----------------------------|-------------------------|-------------------------|----------------|----------------|----------------|----------------|----|-----|----|-------|
| 2 | 27.101 15.802 12.464 | 0.635 0.635 0.131 | 1.056 1.028 1.028 | -- -- -- | -- -- -- | -- -- -- | -- -- -- | -- | -- | -- | 0.870 |

| n° | D | B' | H | γ | ϕ | c |
|----|------|------|------|----------|---------|-------|
| | [m] | [m] | [m] | [°] | [kN/mc] | [kPa] |
| 2 | 1.10 | 5.05 | 5.60 | 9.89 | 28.64 | 0 |

Verifica a ribaltamento

Simbologia adottata

- n° Indice combinazione
- Ms Momento stabilizzante, espresso in [kNm]
- Mr Momento ribaltante, espresso in [kNm]
- FS Fattore di sicurezza (rapporto tra momento stabilizzante e momento ribaltante)

La verifica viene eseguita rispetto allo spigolo inferiore esterno della fondazione

| n° | Ms | Mr | FS |
|--------------------------|---------|---------|-------|
| | [kNm] | [kNm] | |
| 9 - EQU (A1-M1-R3) H - V | 3396.39 | 1430.68 | 2.374 |

Verifica stabilità globale muro + terreno

Simbologia adottata

- Ic Indice/Tipo combinazione
- C Centro superficie di scorrimento, espresso in [m]
- R Raggio, espresso in [m]
- FS Fattore di sicurezza

| Ic | C | R | FS |
|--------------------------|------------|-------|-------|
| | [m] | [m] | |
| 6 - GEO (A2-M2-R2) H - V | 0.00; 4.00 | 12.91 | 1.332 |

Dettagli strisce verifiche stabilità

Simbologia adottata

Le ascisse X sono considerate positive verso monte

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOLGIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 132 di 314 |

Le ordinate Y sono considerate positive verso l'alto

Origine in testa al muro (spigolo contro terra)

- W peso della striscia espresso in [kN]
 Qy carico sulla striscia espresso in [kN]
 α angolo fra la base della striscia e l'orizzontale espresso in [°] (positivo antiorario)
 ϕ angolo d'attrito del terreno lungo la base della striscia
 c coesione del terreno lungo la base della striscia espressa in [kPa]
 b larghezza della striscia espressa in [m]
 u pressione neutra lungo la base della striscia espressa in [kPa]
 Tx; Ty Resistenza al taglio fornita dai tiranti in direzione X ed Y espressa in [kPa]

| n° | W [kN] | Qy [kN] | b [m] | α [°] | ϕ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|-----------------|---------------|------------|------------|----------------|
| 1 | 14.16 | 1.58 | 12.29 - 0.79 | 67.155 | 35.000 | 0 | 0.0 | |
| 2 | 38.43 | 1.58 | 0.79 | 59.441 | 35.000 | 0 | 0.0 | |
| 3 | 56.47 | 1.58 | 0.79 | 53.054 | 35.000 | 0 | 0.0 | |
| 4 | 70.92 | 3.92 | 0.79 | 47.522 | 35.000 | 0 | 0.0 | |
| 5 | 82.91 | 4.75 | 0.79 | 42.531 | 35.000 | 0 | 0.0 | |
| 6 | 93.03 | 4.75 | 0.79 | 37.914 | 35.000 | 0 | 0.0 | |
| 7 | 101.63 | 4.75 | 0.79 | 33.574 | 35.000 | 0 | 0.0 | |
| 8 | 108.96 | 4.75 | 0.79 | 29.443 | 35.000 | 0 | 0.0 | |
| 9 | 118.16 | 4.75 | 0.79 | 25.475 | 25.000 | 0 | 0.0 | |
| 10 | 125.19 | 4.75 | 0.79 | 21.635 | 25.000 | 0 | 0.0 | |
| 11 | 129.48 | 4.23 | 0.79 | 17.895 | 25.000 | 0 | 2.7 | |
| 12 | 132.92 | 1.58 | 0.79 | 14.232 | 25.000 | 0 | 5.0 | |
| 13 | 135.56 | 1.58 | 0.79 | 10.628 | 25.000 | 0 | 6.7 | |
| 14 | 137.42 | 1.58 | 0.79 | 7.067 | 25.000 | 0 | 7.9 | |
| 15 | 138.93 | 1.38 | 0.79 | 3.533 | 25.000 | 0 | 8.6 | |
| 16 | 161.67 | 0.00 | 0.79 | 0.012 | 25.000 | 0 | 8.9 | |
| 17 | 40.55 | 0.00 | 0.79 | -3.509 | 25.000 | 0 | 8.6 | |
| 18 | 34.74 | 0.00 | 0.79 | -7.043 | 25.000 | 0 | 7.9 | |
| 19 | 32.89 | 0.00 | 0.79 | -10.604 | 25.000 | 0 | 6.7 | |
| 20 | 30.26 | 0.00 | 0.79 | -14.208 | 25.000 | 0 | 5.0 | |
| 21 | 26.83 | 0.00 | 0.79 | -17.870 | 25.000 | 0 | 2.8 | |
| 22 | 22.54 | 0.00 | 0.79 | -21.610 | 25.000 | 0 | 0.0 | |
| 23 | 17.34 | 0.00 | 0.79 | -25.449 | 25.000 | 0 | 0.0 | |
| 24 | 11.13 | 0.00 | 0.79 | -29.416 | 25.000 | 0 | 0.0 | |
| 25 | 3.81 | 0.00 | -7.53 - 0.79 | -33.072 | 25.000 | 0 | 0.0 | |

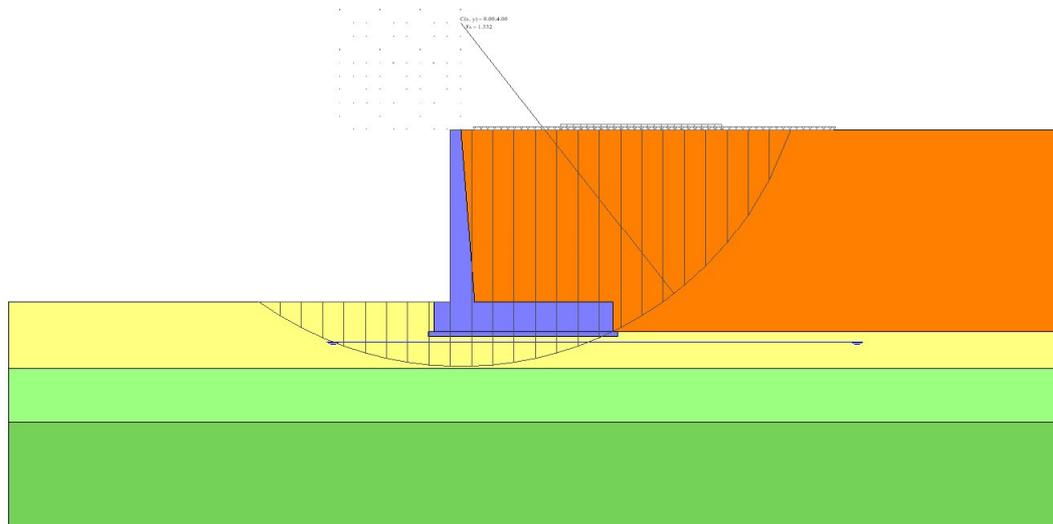


Fig. 14 - Stabilità fronte di scavo - Cerchio critico (Combinazione n° 6)

Sollecitazioni

Elementi calcolati a trave

Simbologia adottata

- N Sforzo normale, espresso in [kN]. Positivo se di compressione.
 T Taglio, espresso in [kN]. Positivo se diretto da monte verso valle
 M Momento, espresso in [kNm]. Positivo se tende le fibre contro terra (a monte)

Paramento

| n° | X [m] | N _{min} [kN] | N _{max} [kN] | T _{min} [kN] | T _{max} [kN] | M _{min} [kNm] | M _{max} [kNm] |
|----|----------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|---------------------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.99 | 0.03 | 0.17 | 0.00 | 0.01 |
| 3 | -0.20 | 2.00 | 2.00 | 0.12 | 0.41 | 0.02 | 0.04 |
| 4 | -0.30 | 3.03 | 3.03 | 0.26 | 0.74 | 0.04 | 0.11 |
| 5 | -0.40 | 4.08 | 4.08 | 0.46 | 1.14 | 0.09 | 0.22 |
| 6 | -0.50 | 5.14 | 5.14 | 0.71 | 1.63 | 0.17 | 0.37 |
| 7 | -0.60 | 6.23 | 6.23 | 1.03 | 2.19 | 0.28 | 0.59 |
| 8 | -0.70 | 7.33 | 7.33 | 1.40 | 2.84 | 0.42 | 0.86 |
| 9 | -0.80 | 8.46 | 8.46 | 1.85 | 3.57 | 0.62 | 1.21 |
| 10 | -0.90 | 9.60 | 9.60 | 2.36 | 4.40 | 0.86 | 1.65 |
| 11 | -1.00 | 10.76 | 10.76 | 2.95 | 5.32 | 1.17 | 2.17 |
| 12 | -1.10 | 11.94 | 11.94 | 3.59 | 6.33 | 1.54 | 2.80 |
| 13 | -1.20 | 13.14 | 13.14 | 4.30 | 7.42 | 1.98 | 3.53 |
| 14 | -1.30 | 14.36 | 14.36 | 5.07 | 8.59 | 2.50 | 4.39 |
| 15 | -1.40 | 15.60 | 15.60 | 5.90 | 9.84 | 3.11 | 5.36 |

| n° | X [m] | Nmin [kN] | Nmax [kN] | Tmin [kN] | Tmax [kN] | Mmin [kNm] | Mmax [kNm] |
|----|----------|--------------|--------------|--------------|--------------|---------------|---------------|
| 16 | -1.50 | 16.86 | 16.86 | 6.78 | 11.17 | 3.81 | 6.48 |
| 17 | -1.60 | 18.13 | 18.13 | 7.72 | 12.58 | 4.60 | 7.73 |
| 18 | -1.70 | 19.43 | 19.43 | 8.72 | 14.07 | 5.49 | 9.14 |
| 19 | -1.80 | 20.74 | 20.74 | 9.78 | 15.64 | 6.50 | 10.70 |
| 20 | -1.90 | 22.08 | 22.08 | 10.89 | 17.29 | 7.61 | 12.43 |
| 21 | -2.00 | 23.43 | 23.43 | 12.06 | 19.01 | 8.85 | 14.33 |
| 22 | -2.10 | 24.80 | 24.80 | 13.28 | 20.82 | 10.21 | 16.42 |
| 23 | -2.20 | 26.19 | 26.19 | 14.57 | 22.70 | 11.70 | 18.69 |
| 24 | -2.30 | 27.60 | 27.60 | 15.91 | 24.67 | 13.33 | 21.16 |
| 25 | -2.40 | 29.03 | 29.03 | 17.31 | 26.71 | 15.10 | 23.84 |
| 26 | -2.50 | 30.48 | 30.48 | 18.76 | 28.83 | 17.02 | 26.73 |
| 27 | -2.60 | 31.95 | 31.95 | 20.27 | 31.03 | 19.09 | 29.85 |
| 28 | -2.70 | 33.43 | 33.43 | 21.84 | 33.31 | 21.32 | 33.19 |
| 29 | -2.80 | 34.94 | 34.94 | 23.47 | 35.67 | 23.72 | 36.77 |
| 30 | -2.90 | 36.46 | 36.46 | 25.15 | 38.11 | 26.29 | 40.60 |
| 31 | -3.00 | 38.01 | 38.01 | 26.89 | 40.63 | 29.04 | 44.68 |
| 32 | -3.10 | 39.57 | 39.57 | 28.69 | 43.22 | 31.97 | 49.03 |
| 33 | -3.20 | 41.15 | 41.15 | 30.54 | 45.90 | 35.08 | 53.64 |
| 34 | -3.30 | 42.75 | 42.75 | 32.45 | 48.65 | 38.40 | 58.53 |
| 35 | -3.40 | 44.37 | 44.37 | 34.42 | 51.49 | 41.91 | 63.70 |
| 36 | -3.50 | 46.01 | 46.01 | 36.44 | 54.40 | 45.63 | 69.17 |
| 37 | -3.60 | 47.67 | 47.67 | 38.53 | 57.39 | 49.56 | 74.94 |
| 38 | -3.70 | 49.35 | 49.35 | 40.66 | 60.46 | 53.70 | 81.03 |
| 39 | -3.80 | 51.04 | 51.04 | 42.86 | 63.61 | 58.08 | 87.42 |
| 40 | -3.90 | 52.76 | 52.76 | 45.11 | 66.84 | 62.68 | 94.15 |
| 41 | -4.00 | 54.49 | 54.49 | 47.42 | 70.15 | 67.51 | 101.21 |
| 42 | -4.10 | 56.24 | 56.24 | 49.79 | 73.53 | 72.59 | 108.60 |
| 43 | -4.20 | 58.02 | 58.02 | 52.21 | 77.00 | 77.91 | 116.35 |
| 44 | -4.30 | 59.81 | 59.81 | 54.69 | 80.54 | 83.48 | 124.46 |
| 45 | -4.40 | 61.62 | 61.62 | 57.23 | 84.17 | 89.31 | 132.93 |
| 46 | -4.50 | 63.45 | 63.45 | 59.82 | 87.87 | 95.41 | 141.77 |
| 47 | -4.60 | 65.30 | 65.30 | 62.48 | 91.65 | 101.77 | 151.00 |
| 48 | -4.70 | 67.17 | 67.17 | 65.18 | 95.51 | 108.41 | 160.62 |
| 49 | -4.80 | 69.05 | 69.05 | 67.95 | 99.45 | 115.34 | 170.63 |
| 50 | -4.90 | 70.96 | 70.96 | 70.77 | 103.47 | 122.54 | 181.05 |
| 51 | -5.00 | 72.88 | 72.88 | 73.65 | 107.57 | 130.04 | 191.88 |
| 52 | -5.10 | 74.83 | 74.83 | 76.59 | 111.74 | 137.84 | 203.13 |
| 53 | -5.20 | 76.79 | 76.79 | 79.58 | 116.00 | 145.95 | 214.81 |
| 54 | -5.30 | 78.77 | 78.77 | 82.63 | 120.33 | 154.36 | 226.93 |
| 55 | -5.40 | 80.78 | 80.78 | 85.74 | 124.75 | 163.09 | 239.49 |
| 56 | -5.50 | 82.80 | 82.80 | 88.90 | 129.24 | 172.14 | 252.51 |
| 57 | -5.60 | 84.84 | 84.84 | 92.12 | 133.81 | 181.51 | 265.99 |
| 58 | -5.70 | 86.89 | 86.89 | 95.40 | 138.46 | 191.22 | 279.94 |
| 59 | -5.80 | 88.97 | 88.97 | 98.77 | 143.19 | 201.27 | 294.36 |
| 60 | -5.90 | 91.07 | 91.07 | 102.30 | 148.00 | 211.67 | 309.27 |
| 61 | -6.00 | 93.18 | 93.18 | 106.00 | 152.89 | 222.45 | 324.67 |
| 62 | -6.10 | 95.32 | 95.32 | 109.88 | 157.86 | 233.61 | 340.58 |
| 63 | -6.20 | 97.47 | 97.47 | 113.89 | 162.90 | 245.17 | 356.99 |
| 64 | -6.30 | 99.65 | 99.65 | 117.99 | 168.03 | 257.15 | 373.92 |
| 65 | -6.40 | 101.84 | 101.84 | 122.17 | 173.23 | 269.54 | 391.37 |
| 66 | -6.50 | 104.05 | 104.05 | 126.43 | 178.51 | 282.37 | 409.36 |

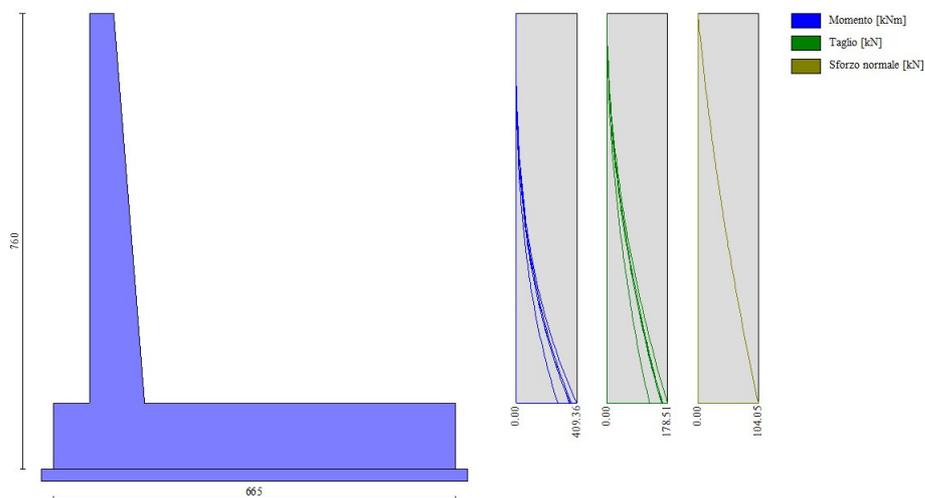


Fig. 15 - Paramento

Fondazione

| n° | X [m] | Nmin [kN] | Nmax [kN] | Tmin [kN] | Tmax [kN] | Mmin [kNm] | Mmax [kNm] |
|----|----------|--------------|--------------|--------------|--------------|---------------|---------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 0.00 | 16.93 | 23.80 | 0.85 | 1.19 |
| 3 | -0.80 | 0.00 | 0.00 | 33.71 | 47.26 | 3.38 | 4.75 |
| 4 | -0.70 | 0.00 | 0.00 | 50.35 | 70.39 | 7.58 | 10.63 |
| 5 | -0.60 | 0.00 | 0.00 | 66.86 | 93.18 | 13.45 | 18.82 |
| 6 | -0.50 | 0.00 | 0.00 | 83.22 | 115.64 | 20.95 | 29.26 |
| 7 | -0.40 | 0.00 | 0.00 | 99.44 | 137.76 | 30.09 | 41.93 |
| 8 | 0.51 | 0.00 | 0.00 | -324.94 | -104.70 | -1068.78 | -428.05 |
| 9 | 0.60 | 0.00 | 0.00 | -324.85 | -106.94 | -1039.26 | -419.51 |
| 10 | 0.70 | 0.00 | 0.00 | -324.55 | -109.04 | -1009.76 | -410.76 |
| 11 | 0.80 | 0.00 | 0.00 | -324.05 | -111.00 | -980.30 | -401.81 |
| 12 | 0.90 | 0.00 | 0.00 | -323.35 | -112.82 | -950.90 | -392.67 |
| 13 | 1.00 | 0.00 | 0.00 | -322.45 | -114.50 | -921.57 | -383.36 |
| 14 | 1.10 | 0.00 | 0.00 | -321.35 | -116.05 | -892.35 | -373.88 |
| 15 | 1.20 | 0.00 | 0.00 | -320.05 | -117.46 | -863.24 | -364.27 |
| 16 | 1.30 | 0.00 | 0.00 | -318.54 | -118.74 | -834.28 | -354.51 |
| 17 | 1.40 | 0.00 | 0.00 | -316.83 | -119.87 | -805.47 | -344.64 |
| 18 | 1.49 | 0.00 | 0.00 | -314.93 | -120.87 | -776.84 | -334.67 |
| 19 | 1.59 | 0.00 | 0.00 | -312.81 | -121.74 | -748.41 | -324.60 |
| 20 | 1.69 | 0.00 | 0.00 | -310.50 | -122.46 | -720.20 | -314.45 |
| 21 | 1.79 | 0.00 | 0.00 | -307.99 | -123.05 | -692.23 | -304.24 |
| 22 | 1.89 | 0.00 | 0.00 | -305.27 | -123.50 | -664.52 | -293.98 |
| 23 | 1.99 | 0.00 | 0.00 | -302.35 | -123.81 | -637.08 | -283.68 |
| 24 | 2.09 | 0.00 | 0.00 | -299.23 | -123.99 | -609.94 | -273.35 |
| 25 | 2.19 | 0.00 | 0.00 | -295.91 | -124.03 | -583.12 | -263.02 |
| 26 | 2.29 | 0.00 | 0.00 | -292.39 | -123.93 | -556.64 | -252.68 |
| 27 | 2.38 | 0.00 | 0.00 | -288.66 | -123.69 | -530.52 | -242.37 |
| 28 | 2.48 | 0.00 | 0.00 | -284.73 | -123.32 | -504.78 | -232.08 |
| 29 | 2.58 | 0.00 | 0.00 | -280.61 | -122.81 | -479.43 | -221.84 |
| 30 | 2.68 | 0.00 | 0.00 | -276.27 | -122.16 | -454.50 | -211.65 |
| 31 | 2.78 | 0.00 | 0.00 | -271.74 | -121.38 | -430.01 | -201.54 |
| 32 | 2.88 | 0.00 | 0.00 | -267.01 | -120.46 | -405.98 | -191.51 |

| n° | X [m] | Nmin [kN] | Nmax [kN] | Tmin [kN] | Tmax [kN] | Mmin [kNm] | Mmax [kNm] |
|----|----------|--------------|--------------|--------------|--------------|---------------|---------------|
| 33 | 2.98 | 0.00 | 0.00 | -262.07 | -119.40 | -382.43 | -181.58 |
| 34 | 3.08 | 0.00 | 0.00 | -256.93 | -118.20 | -359.37 | -171.76 |
| 35 | 3.17 | 0.00 | 0.00 | -251.60 | -116.87 | -336.83 | -162.06 |
| 36 | 3.27 | 0.00 | 0.00 | -246.05 | -115.40 | -314.83 | -152.51 |
| 37 | 3.37 | 0.00 | 0.00 | -240.31 | -113.79 | -293.39 | -143.10 |
| 38 | 3.47 | 0.00 | 0.00 | -234.37 | -112.04 | -272.53 | -133.86 |
| 39 | 3.57 | 0.00 | 0.00 | -228.22 | -110.16 | -252.26 | -124.80 |
| 40 | 3.67 | 0.00 | 0.00 | -221.87 | -108.14 | -232.61 | -115.94 |
| 41 | 3.77 | 0.00 | 0.00 | -213.49 | -104.63 | -211.88 | -106.00 |
| 42 | 3.87 | 0.00 | 0.00 | -204.07 | -100.35 | -191.24 | -95.87 |
| 43 | 3.97 | 0.00 | 0.00 | -194.45 | -95.95 | -171.54 | -86.17 |
| 44 | 4.06 | 0.00 | 0.00 | -184.63 | -91.40 | -152.80 | -76.91 |
| 45 | 4.16 | 0.00 | 0.00 | -174.60 | -86.72 | -135.05 | -68.10 |
| 46 | 4.26 | 0.00 | 0.00 | -164.37 | -81.90 | -118.29 | -59.77 |
| 47 | 4.36 | 0.00 | 0.00 | -153.94 | -76.94 | -102.56 | -51.92 |
| 48 | 4.46 | 0.00 | 0.00 | -143.31 | -71.84 | -87.87 | -44.56 |
| 49 | 4.56 | 0.00 | 0.00 | -132.48 | -66.61 | -74.23 | -37.72 |
| 50 | 4.66 | 0.00 | 0.00 | -121.44 | -61.24 | -61.68 | -31.40 |
| 51 | 4.76 | 0.00 | 0.00 | -110.21 | -55.74 | -50.23 | -25.62 |
| 52 | 4.86 | 0.00 | 0.00 | -98.77 | -50.09 | -39.90 | -20.38 |
| 53 | 4.95 | 0.00 | 0.00 | -87.13 | -44.31 | -30.71 | -15.72 |
| 54 | 5.05 | 0.00 | 0.00 | -75.29 | -38.39 | -22.68 | -11.63 |
| 55 | 5.15 | 0.00 | 0.00 | -63.24 | -32.34 | -15.84 | -8.13 |
| 56 | 5.25 | 0.00 | 0.00 | -51.00 | -26.14 | -10.19 | -5.24 |
| 57 | 5.35 | 0.00 | 0.00 | -38.55 | -19.81 | -5.76 | -2.97 |
| 58 | 5.45 | 0.00 | 0.00 | -25.90 | -13.35 | -2.57 | -1.33 |
| 59 | 5.55 | 0.00 | 0.00 | -13.05 | -6.74 | -0.65 | -0.33 |
| 60 | 5.65 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

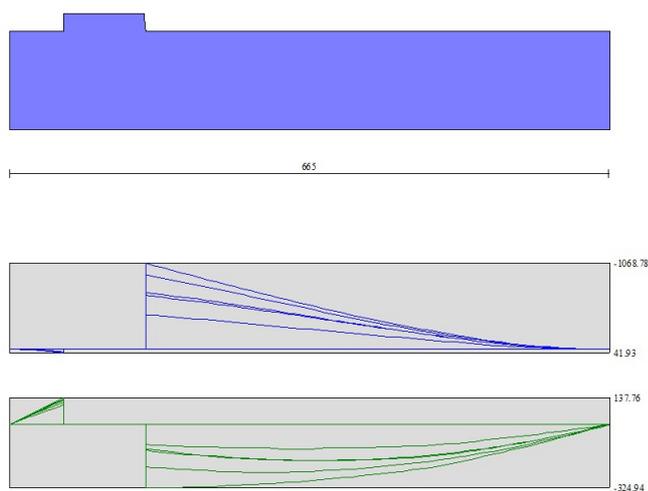


Fig. 16 - Fondazione

Verifiche a flessione

Elementi calcolati a trave

Simbologia adottata

| | |
|-----|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Afi | area ferri inferiori espresso in [cmq] |
| Afs | area ferri superiori espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| N | sforzio normale agente espressa in [kN] |
| Mu | momento ultimi espresso in [kNm] |
| Nu | sforzio normale ultimo espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione ultima e sollecitazione agente) |

Paramento

| n° | B | H | Afi | Afs | M | N | Mu | Nu | FS |
|----|------|------|-------|-------|-------|-------|---------|---------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kNm] | [kN] | |
| 1 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | 100 | 41 | 26.55 | 53.09 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 3 | 100 | 42 | 26.55 | 53.09 | 0.04 | 2.00 | 189.30 | 8639.50 | 4320.783 |
| 4 | 100 | 42 | 26.55 | 53.09 | 0.11 | 3.03 | 295.04 | 8075.92 | 2667.168 |
| 5 | 100 | 43 | 26.55 | 53.09 | 0.22 | 4.08 | 401.14 | 7500.38 | 1840.421 |
| 6 | 100 | 44 | 26.55 | 53.09 | 0.37 | 5.14 | 502.90 | 6918.75 | 1345.561 |
| 7 | 100 | 45 | 26.55 | 53.09 | 0.59 | 6.23 | 598.24 | 6358.19 | 1020.982 |
| 8 | 100 | 45 | 26.55 | 53.09 | 0.86 | 7.33 | 686.55 | 5834.70 | 795.762 |
| 9 | 100 | 46 | 26.55 | 53.09 | 1.21 | 8.46 | 768.28 | 5355.38 | 633.322 |
| 10 | 100 | 47 | 26.55 | 53.09 | 1.65 | 9.60 | 845.37 | 4929.78 | 513.580 |
| 11 | 100 | 48 | 26.55 | 53.09 | 2.17 | 10.76 | 917.46 | 4547.67 | 422.614 |
| 12 | 100 | 49 | 26.55 | 53.09 | 2.80 | 11.94 | 986.60 | 4212.52 | 352.753 |
| 13 | 100 | 49 | 26.55 | 53.09 | 3.53 | 13.14 | 1051.32 | 3911.40 | 297.627 |
| 14 | 100 | 50 | 26.55 | 53.09 | 4.39 | 14.36 | 1113.25 | 3645.44 | 253.841 |
| 15 | 100 | 51 | 26.55 | 53.09 | 5.36 | 15.60 | 1172.93 | 3410.58 | 218.636 |
| 16 | 100 | 52 | 26.55 | 53.09 | 6.48 | 16.86 | 1206.58 | 3139.79 | 186.263 |
| 17 | 100 | 52 | 26.55 | 53.09 | 7.73 | 18.13 | 1225.32 | 2873.35 | 158.458 |
| 18 | 100 | 53 | 26.55 | 53.09 | 9.14 | 19.43 | 1236.93 | 2629.97 | 135.366 |
| 19 | 100 | 54 | 26.55 | 53.09 | 10.70 | 20.74 | 1248.51 | 2420.27 | 116.678 |
| 20 | 100 | 55 | 26.55 | 53.09 | 12.43 | 22.08 | 1255.77 | 2230.49 | 101.033 |
| 21 | 100 | 56 | 26.55 | 53.09 | 14.33 | 23.43 | 1265.38 | 2068.60 | 88.290 |
| 22 | 100 | 56 | 26.55 | 53.09 | 16.42 | 24.80 | 1271.17 | 1920.40 | 77.431 |
| 23 | 100 | 57 | 26.55 | 53.09 | 18.69 | 26.19 | 1277.79 | 1790.58 | 68.363 |
| 24 | 100 | 58 | 26.55 | 53.09 | 21.16 | 27.60 | 1286.30 | 1677.62 | 60.778 |
| 25 | 100 | 59 | 26.55 | 53.09 | 23.84 | 29.03 | 1294.48 | 1576.23 | 54.294 |
| 26 | 100 | 59 | 26.55 | 53.09 | 26.73 | 30.48 | 1300.56 | 1482.75 | 48.648 |
| 27 | 100 | 60 | 26.55 | 53.09 | 29.85 | 31.95 | 1308.60 | 1400.60 | 43.842 |

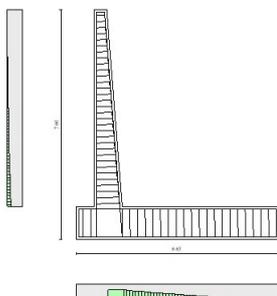


Fig. 17 - Paramento (Inviluppo)

Verifiche a taglio

Simbologia adottata

| | |
|--------------|---|
| I_s | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| A_{sw} | area ferri a taglio espresso in [cmq] |
| $\cot\theta$ | inclinazione delle bielle compresse, θ inclinazione dei puntoni di calcestruzzo |
| V_{Rcd} | resistenza di progetto a 'taglio compressione' espressa in [kN] |
| V_{Rsd} | resistenza di progetto a 'taglio trazione' espressa in [kN] |
| V_{Rd} | resistenza di progetto a taglio espresso in [kN]. Per elementi con armature trasversali resistenti al taglio ($A_{sw}>0.0$) $V_{Rd}=\min(V_{Rcd}, V_{Rsd})$. |
| T | taglio agente espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione resistente e sollecitazione agente) |

Paramento

| n° | B [cm] | H [cm] | A_{sw} [cmq] | $\cot\theta$ | V_{Rcd} [kN] | V_{Rsd} [kN] | V_{Rd} [kN] | T [kN] | FS |
|----|-----------|-----------|-------------------|--------------|-------------------|-------------------|------------------|-----------|----------|
| 1 | 100 | 40 | 0.00 | -- | 0.00 | 0.00 | 291.33 | 0.00 | 100.000 |
| 2 | 100 | 41 | 0.00 | -- | 0.00 | 0.00 | 296.72 | 0.17 | 1775.521 |
| 3 | 100 | 42 | 0.00 | -- | 0.00 | 0.00 | 302.10 | 0.41 | 729.799 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 141 di 314 |

| n° | B [cm] | H [cm] | A _{sw} [cmq] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|-----------|-----------|--------------------------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 4 | 100 | 42 | 0.00 | -- | 0.00 | 0.00 | 307.47 | 0.74 | 415.646 |
| 5 | 100 | 43 | 0.00 | -- | 0.00 | 0.00 | 312.83 | 1.14 | 273.497 |
| 6 | 100 | 44 | 0.00 | -- | 0.00 | 0.00 | 318.18 | 1.63 | 195.612 |
| 7 | 100 | 45 | 0.00 | -- | 0.00 | 0.00 | 323.51 | 2.19 | 147.832 |
| 8 | 100 | 45 | 0.00 | -- | 0.00 | 0.00 | 328.83 | 2.84 | 115.977 |
| 9 | 100 | 46 | 0.00 | -- | 0.00 | 0.00 | 334.13 | 3.57 | 93.545 |
| 10 | 100 | 47 | 0.00 | -- | 0.00 | 0.00 | 337.26 | 4.40 | 76.649 |
| 11 | 100 | 48 | 0.00 | -- | 0.00 | 0.00 | 340.37 | 5.32 | 63.966 |
| 12 | 100 | 49 | 0.00 | -- | 0.00 | 0.00 | 343.45 | 6.33 | 54.271 |
| 13 | 100 | 49 | 0.00 | -- | 0.00 | 0.00 | 346.52 | 7.42 | 46.709 |
| 14 | 100 | 50 | 0.00 | -- | 0.00 | 0.00 | 349.58 | 8.59 | 40.697 |
| 15 | 100 | 51 | 0.00 | -- | 0.00 | 0.00 | 352.61 | 9.84 | 35.832 |
| 16 | 100 | 52 | 0.00 | -- | 0.00 | 0.00 | 355.63 | 11.17 | 31.835 |
| 17 | 100 | 52 | 0.00 | -- | 0.00 | 0.00 | 358.63 | 12.58 | 28.507 |
| 18 | 100 | 53 | 0.00 | -- | 0.00 | 0.00 | 361.61 | 14.07 | 25.702 |
| 19 | 100 | 54 | 0.00 | -- | 0.00 | 0.00 | 364.58 | 15.64 | 23.314 |
| 20 | 100 | 55 | 0.00 | -- | 0.00 | 0.00 | 367.53 | 17.29 | 21.263 |
| 21 | 100 | 56 | 0.00 | -- | 0.00 | 0.00 | 370.47 | 19.01 | 19.486 |
| 22 | 100 | 56 | 0.00 | -- | 0.00 | 0.00 | 373.39 | 20.82 | 17.936 |
| 23 | 100 | 57 | 0.00 | -- | 0.00 | 0.00 | 376.30 | 22.70 | 16.575 |
| 24 | 100 | 58 | 0.00 | -- | 0.00 | 0.00 | 379.20 | 24.67 | 15.373 |
| 25 | 100 | 59 | 0.00 | -- | 0.00 | 0.00 | 382.08 | 26.71 | 14.305 |
| 26 | 100 | 59 | 0.00 | -- | 0.00 | 0.00 | 384.95 | 28.83 | 13.352 |
| 27 | 100 | 60 | 0.00 | -- | 0.00 | 0.00 | 387.81 | 31.03 | 12.497 |
| 28 | 100 | 61 | 0.00 | -- | 0.00 | 0.00 | 390.66 | 33.31 | 11.727 |
| 29 | 100 | 62 | 0.00 | -- | 0.00 | 0.00 | 393.49 | 35.67 | 11.031 |
| 30 | 100 | 63 | 0.00 | -- | 0.00 | 0.00 | 396.31 | 38.11 | 10.399 |
| 31 | 100 | 63 | 0.00 | -- | 0.00 | 0.00 | 399.12 | 40.63 | 9.824 |
| 32 | 100 | 64 | 0.00 | -- | 0.00 | 0.00 | 401.92 | 43.22 | 9.298 |
| 33 | 100 | 65 | 0.00 | -- | 0.00 | 0.00 | 404.71 | 45.90 | 8.817 |
| 34 | 100 | 66 | 0.00 | -- | 0.00 | 0.00 | 407.48 | 48.65 | 8.375 |
| 35 | 100 | 66 | 0.00 | -- | 0.00 | 0.00 | 410.25 | 51.49 | 7.968 |
| 36 | 100 | 67 | 0.00 | -- | 0.00 | 0.00 | 413.01 | 54.40 | 7.592 |
| 37 | 100 | 68 | 0.00 | -- | 0.00 | 0.00 | 415.75 | 57.39 | 7.244 |
| 38 | 100 | 69 | 0.00 | -- | 0.00 | 0.00 | 418.49 | 60.46 | 6.922 |
| 39 | 100 | 70 | 0.00 | -- | 0.00 | 0.00 | 421.22 | 63.61 | 6.622 |
| 40 | 100 | 70 | 0.00 | -- | 0.00 | 0.00 | 423.94 | 66.84 | 6.343 |
| 41 | 100 | 71 | 0.00 | -- | 0.00 | 0.00 | 426.65 | 70.15 | 6.082 |
| 42 | 100 | 72 | 0.00 | -- | 0.00 | 0.00 | 429.35 | 73.53 | 5.839 |
| 43 | 100 | 73 | 0.00 | -- | 0.00 | 0.00 | 432.04 | 77.00 | 5.611 |
| 44 | 100 | 73 | 0.00 | -- | 0.00 | 0.00 | 434.73 | 80.54 | 5.397 |
| 45 | 100 | 74 | 0.00 | -- | 0.00 | 0.00 | 437.41 | 84.17 | 5.197 |
| 46 | 100 | 75 | 0.00 | -- | 0.00 | 0.00 | 440.07 | 87.87 | 5.008 |
| 47 | 100 | 76 | 0.00 | -- | 0.00 | 0.00 | 442.74 | 91.65 | 4.831 |
| 48 | 100 | 77 | 0.00 | -- | 0.00 | 0.00 | 445.39 | 95.51 | 4.663 |
| 49 | 100 | 77 | 0.00 | -- | 0.00 | 0.00 | 448.03 | 99.45 | 4.505 |
| 50 | 100 | 78 | 0.00 | -- | 0.00 | 0.00 | 450.67 | 103.47 | 4.356 |
| 51 | 100 | 79 | 0.00 | -- | 0.00 | 0.00 | 453.30 | 107.57 | 4.214 |
| 52 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 455.93 | 111.74 | 4.080 |
| 53 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 458.55 | 116.00 | 3.953 |
| 54 | 100 | 81 | 0.00 | -- | 0.00 | 0.00 | 461.16 | 120.33 | 3.832 |
| 55 | 100 | 82 | 0.00 | -- | 0.00 | 0.00 | 463.76 | 124.75 | 3.718 |
| 56 | 100 | 83 | 0.00 | -- | 0.00 | 0.00 | 466.36 | 129.24 | 3.608 |
| 57 | 100 | 84 | 0.00 | -- | 0.00 | 0.00 | 468.95 | 133.81 | 3.505 |
| 58 | 100 | 84 | 0.00 | -- | 0.00 | 0.00 | 471.54 | 138.46 | 3.406 |
| 59 | 100 | 85 | 0.00 | -- | 0.00 | 0.00 | 474.12 | 143.19 | 3.311 |
| 60 | 100 | 86 | 0.00 | -- | 0.00 | 0.00 | 476.69 | 148.00 | 3.221 |
| 61 | 100 | 87 | 0.00 | -- | 0.00 | 0.00 | 479.26 | 152.89 | 3.135 |
| 62 | 100 | 87 | 0.00 | -- | 0.00 | 0.00 | 481.82 | 157.86 | 3.052 |
| 63 | 100 | 88 | 0.00 | -- | 0.00 | 0.00 | 484.38 | 162.90 | 2.973 |
| 64 | 100 | 89 | 0.00 | -- | 0.00 | 0.00 | 486.93 | 168.03 | 2.898 |
| 65 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 489.48 | 173.23 | 2.826 |
| 66 | 100 | 91 | 0.00 | -- | 0.00 | 0.00 | 492.02 | 178.51 | 2.756 |

Fondazione

| n° | B [cm] | H [cm] | A _{sw} [cmq] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|-----------|-----------|--------------------------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 1 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | 0.00 | 100.000 |
| 2 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -23.80 | 20.218 |
| 3 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -47.26 | 10.181 |
| 4 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -70.39 | 6.836 |
| 5 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -93.18 | 5.164 |
| 6 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -115.64 | 4.161 |
| 7 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -137.76 | 3.493 |
| 8 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -324.94 | 1.481 |
| 9 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -324.85 | 1.481 |
| 10 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -324.55 | 1.483 |
| 11 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -324.05 | 1.485 |
| 12 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -323.35 | 1.488 |
| 13 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -322.45 | 1.492 |
| 14 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -321.35 | 1.497 |
| 15 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -320.05 | 1.503 |
| 16 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -318.54 | 1.511 |
| 17 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -316.83 | 1.519 |
| 18 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -314.93 | 1.528 |
| 19 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -312.81 | 1.538 |
| 20 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -310.50 | 1.550 |
| 21 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -307.99 | 1.562 |
| 22 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -305.27 | 1.576 |
| 23 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -302.35 | 1.591 |
| 24 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -299.23 | 1.608 |
| 25 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -295.91 | 1.626 |
| 26 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -292.39 | 1.646 |
| 27 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -288.66 | 1.667 |
| 28 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -284.73 | 1.690 |
| 29 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -280.61 | 1.715 |
| 30 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -276.27 | 1.742 |
| 31 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -271.74 | 1.771 |
| 32 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -267.01 | 1.802 |
| 33 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -262.07 | 1.836 |
| 34 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -256.93 | 1.873 |
| 35 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -251.60 | 1.912 |
| 36 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -246.05 | 1.956 |
| 37 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -240.31 | 2.002 |
| 38 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -234.37 | 2.053 |
| 39 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -228.22 | 2.108 |
| 40 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -221.87 | 2.169 |
| 41 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -213.49 | 2.254 |
| 42 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -204.07 | 2.358 |
| 43 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -194.45 | 2.475 |
| 44 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -184.63 | 2.606 |
| 45 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -174.60 | 2.756 |
| 46 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -164.37 | 2.927 |
| 47 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -153.94 | 3.126 |
| 48 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -143.31 | 3.358 |
| 49 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -132.48 | 3.632 |
| 50 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -121.44 | 3.962 |
| 51 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -110.21 | 4.366 |
| 52 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -98.77 | 4.872 |
| 53 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -87.13 | 5.523 |
| 54 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -75.29 | 6.391 |
| 55 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -63.24 | 7.608 |
| 56 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -51.00 | 9.435 |
| 57 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -38.55 | 12.481 |
| 58 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -25.90 | 18.576 |
| 59 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 481.18 | -13.05 | 36.865 |
| 60 | 100 | 110 | 0.00 | -- | 0.00 | 0.00 | 341.04 | 0.00 | 100.000 |

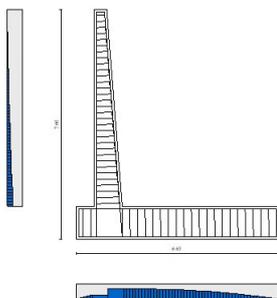


Fig. 18 - Paramento (Inviluppo)

Verifica delle tensioni

Simbologia adottata

| | |
|---------------|---|
| n° | indice sezione |
| Y | ordinata sezione, espressa in [m] |
| B | larghezza sezione, espresso in [cm] |
| H | altezza sezione, espressa in [cm] |
| A_{fi} | area ferri inferiori, espresso in [cmq] |
| A_{fs} | area ferri superiori, espressa in [cmq] |
| M | momento agente, espressa in [kNm] |
| N | sfuerzo normale agente, espressa in [kN] |
| σ_c | tensione di compressione nel cls, espressa in [kPa] |
| σ_{fi} | tensione nei ferri inferiori, espressa in [kPa] |
| σ_{fs} | tensione nei ferri superiori, espressa in [kPa] |

Combinazioni SLER

Paramento

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 58 | 100 | 84 | 26.55 | 53.09 | 191.22 | 86.89 | 1810 (10) | 44564 (10) | 21260 (10) |
| 59 | 100 | 85 | 26.55 | 53.09 | 201.27 | 88.97 | 1873 (10) | 46542 (10) | 22030 (10) |
| 60 | 100 | 86 | 26.55 | 53.09 | 211.67 | 91.07 | 1937 (10) | 48568 (10) | 22814 (10) |
| 61 | 100 | 87 | 26.55 | 53.09 | 222.45 | 93.18 | 2003 (10) | 50644 (10) | 23612 (10) |
| 62 | 100 | 87 | 26.55 | 53.09 | 233.61 | 95.32 | 2069 (10) | 52774 (10) | 24425 (10) |
| 63 | 100 | 88 | 26.55 | 53.09 | 245.17 | 97.47 | 2137 (10) | 54959 (10) | 25254 (10) |
| 64 | 100 | 89 | 26.55 | 53.09 | 257.15 | 99.65 | 2206 (10) | 57201 (10) | 26100 (10) |
| 65 | 100 | 90 | 26.55 | 53.09 | 269.54 | 101.84 | 2276 (10) | 59501 (10) | 26962 (10) |
| 66 | 100 | 91 | 26.55 | 53.09 | 282.37 | 104.05 | 2348 (10) | 61857 (10) | 27840 (10) |

Fondazione

Tensione massima di compressione nel calcestruzzo 17430 [kPa]

Tensione massima di trazione dell'acciaio 360000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0 (10) | 0 (10) | 0 (10) |
| 2 | 100 | 110 | 45.24 | 22.62 | 0.85 | 0.00 | 5 (10) | 199 (10) | 61 (10) |
| 3 | 100 | 110 | 45.24 | 22.62 | 3.38 | 0.00 | 21 (10) | 792 (10) | 243 (10) |
| 4 | 100 | 110 | 45.24 | 22.62 | 7.58 | 0.00 | 47 (10) | 1777 (10) | 545 (10) |
| 5 | 100 | 110 | 45.24 | 22.62 | 13.45 | 0.00 | 83 (10) | 3150 (10) | 967 (10) |
| 6 | 100 | 110 | 45.24 | 22.62 | 20.95 | 0.00 | 129 (10) | 4908 (10) | 1507 (10) |
| 7 | 100 | 110 | 45.24 | 22.62 | 30.09 | 0.00 | 185 (10) | 7047 (10) | 2163 (10) |
| 8 | 100 | 110 | 22.62 | 45.24 | -428.05 | 0.00 | 2627 (10) | 30780 (10) | 100265 (10) |
| 9 | 100 | 110 | 22.62 | 45.24 | -419.51 | 0.00 | 2575 (10) | 30166 (10) | 98265 (10) |
| 10 | 100 | 110 | 22.62 | 45.24 | -410.76 | 0.00 | 2521 (10) | 29536 (10) | 96215 (10) |
| 11 | 100 | 110 | 22.62 | 45.24 | -401.81 | 0.00 | 2466 (10) | 28893 (10) | 94118 (10) |
| 12 | 100 | 110 | 22.62 | 45.24 | -392.67 | 0.00 | 2410 (10) | 28235 (10) | 91978 (10) |
| 13 | 100 | 110 | 22.62 | 45.24 | -383.36 | 0.00 | 2353 (10) | 27566 (10) | 89796 (10) |
| 14 | 100 | 110 | 22.62 | 45.24 | -373.88 | 0.00 | 2295 (10) | 26885 (10) | 87577 (10) |
| 15 | 100 | 110 | 22.62 | 45.24 | -364.27 | 0.00 | 2236 (10) | 26193 (10) | 85324 (10) |
| 16 | 100 | 110 | 22.62 | 45.24 | -354.51 | 0.00 | 2176 (10) | 25492 (10) | 83040 (10) |
| 17 | 100 | 110 | 22.62 | 45.24 | -344.64 | 0.00 | 2115 (10) | 24782 (10) | 80728 (10) |
| 18 | 100 | 110 | 22.62 | 45.24 | -334.67 | 0.00 | 2054 (10) | 24065 (10) | 78391 (10) |
| 19 | 100 | 110 | 22.62 | 45.24 | -324.60 | 0.00 | 1992 (10) | 23341 (10) | 76033 (10) |
| 20 | 100 | 110 | 22.62 | 45.24 | -314.45 | 0.00 | 1930 (10) | 22611 (10) | 73656 (10) |
| 21 | 100 | 110 | 22.62 | 45.24 | -304.24 | 0.00 | 1867 (10) | 21877 (10) | 71264 (10) |
| 22 | 100 | 110 | 22.62 | 45.24 | -293.98 | 0.00 | 1804 (10) | 21139 (10) | 68860 (10) |
| 23 | 100 | 110 | 22.62 | 45.24 | -283.68 | 0.00 | 1741 (10) | 20398 (10) | 66447 (10) |
| 24 | 100 | 110 | 22.62 | 45.24 | -273.35 | 0.00 | 1678 (10) | 19656 (10) | 64029 (10) |
| 25 | 100 | 110 | 22.62 | 45.24 | -263.02 | 0.00 | 1614 (10) | 18913 (10) | 61608 (10) |
| 26 | 100 | 110 | 22.62 | 45.24 | -252.68 | 0.00 | 1551 (10) | 18170 (10) | 59188 (10) |
| 27 | 100 | 110 | 22.62 | 45.24 | -242.37 | 0.00 | 1488 (10) | 17428 (10) | 56771 (10) |
| 28 | 100 | 110 | 22.62 | 45.24 | -232.08 | 0.00 | 1424 (10) | 16688 (10) | 54362 (10) |
| 29 | 100 | 110 | 22.62 | 45.24 | -221.84 | 0.00 | 1362 (10) | 15952 (10) | 51963 (10) |
| 30 | 100 | 110 | 22.62 | 45.24 | -211.65 | 0.00 | 1299 (10) | 15219 (10) | 49577 (10) |
| 31 | 100 | 110 | 22.62 | 45.24 | -201.54 | 0.00 | 1237 (10) | 14492 (10) | 47208 (10) |
| 32 | 100 | 110 | 22.62 | 45.24 | -191.51 | 0.00 | 1175 (10) | 13771 (10) | 44859 (10) |
| 33 | 100 | 110 | 22.62 | 45.24 | -181.58 | 0.00 | 1114 (10) | 13057 (10) | 42532 (10) |
| 34 | 100 | 110 | 22.62 | 45.24 | -171.76 | 0.00 | 1054 (10) | 12350 (10) | 40232 (10) |
| 35 | 100 | 110 | 22.62 | 45.24 | -162.06 | 0.00 | 995 (10) | 11653 (10) | 37961 (10) |
| 36 | 100 | 110 | 22.62 | 45.24 | -152.51 | 0.00 | 936 (10) | 10966 (10) | 35722 (10) |
| 37 | 100 | 110 | 22.62 | 45.24 | -143.10 | 0.00 | 878 (10) | 10290 (10) | 33519 (10) |
| 38 | 100 | 110 | 22.62 | 45.24 | -133.86 | 0.00 | 822 (10) | 9626 (10) | 31355 (10) |
| 39 | 100 | 110 | 22.62 | 45.24 | -124.80 | 0.00 | 766 (10) | 8974 (10) | 29233 (10) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
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| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 40 | 100 | 110 | 22.62 | 45.24 | -115.94 | 0.00 | 712 (10) | 8337 (10) | 27156 (10) |
| 41 | 100 | 110 | 22.62 | 45.24 | -106.00 | 0.00 | 651 (10) | 7622 (10) | 24830 (10) |
| 42 | 100 | 110 | 22.62 | 45.24 | -95.87 | 0.00 | 588 (10) | 6894 (10) | 22456 (10) |
| 43 | 100 | 110 | 22.62 | 45.24 | -86.17 | 0.00 | 529 (10) | 6196 (10) | 20184 (10) |
| 44 | 100 | 110 | 22.62 | 45.24 | -76.91 | 0.00 | 472 (10) | 5530 (10) | 18015 (10) |
| 45 | 100 | 110 | 22.62 | 45.24 | -68.10 | 0.00 | 418 (10) | 4897 (10) | 15952 (10) |
| 46 | 100 | 110 | 22.62 | 45.24 | -59.77 | 0.00 | 367 (10) | 4298 (10) | 14000 (10) |
| 47 | 100 | 110 | 22.62 | 45.24 | -51.92 | 0.00 | 319 (10) | 3733 (10) | 12161 (10) |
| 48 | 100 | 110 | 22.62 | 45.24 | -44.56 | 0.00 | 274 (10) | 3204 (10) | 10438 (10) |
| 49 | 100 | 110 | 22.62 | 45.24 | -37.72 | 0.00 | 232 (10) | 2712 (10) | 8835 (10) |
| 50 | 100 | 110 | 22.62 | 45.24 | -31.40 | 0.00 | 193 (10) | 2258 (10) | 7355 (10) |
| 51 | 100 | 110 | 22.62 | 45.24 | -25.62 | 0.00 | 157 (10) | 1842 (10) | 6000 (10) |
| 52 | 100 | 110 | 22.62 | 45.24 | -20.38 | 0.00 | 125 (10) | 1466 (10) | 4775 (10) |
| 53 | 100 | 110 | 22.62 | 45.24 | -15.72 | 0.00 | 96 (10) | 1130 (10) | 3682 (10) |
| 54 | 100 | 110 | 22.62 | 45.24 | -11.63 | 0.00 | 71 (10) | 836 (10) | 2724 (10) |
| 55 | 100 | 110 | 22.62 | 45.24 | -8.13 | 0.00 | 50 (10) | 585 (10) | 1905 (10) |
| 56 | 100 | 110 | 22.62 | 45.24 | -5.24 | 0.00 | 32 (10) | 377 (10) | 1228 (10) |
| 57 | 100 | 110 | 22.62 | 45.24 | -2.97 | 0.00 | 18 (10) | 213 (10) | 695 (10) |
| 58 | 100 | 110 | 22.62 | 45.24 | -1.33 | 0.00 | 8 (10) | 96 (10) | 311 (10) |
| 59 | 100 | 110 | 22.62 | 45.24 | -0.33 | 0.00 | 2 (10) | 24 (10) | 78 (10) |
| 60 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | 0 (10) | 0 (10) | 0 (10) |

Combinazioni SLEF

Paramento

Tensione massima di compressione nel calcestruzzo 33200 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0 (11) | 0 (11) | 0 (11) |
| 2 | 100 | 41 | 26.55 | 53.09 | 0.00 | 0.99 | 2 (11) | 25 (11) | 32 (11) |
| 3 | 100 | 42 | 26.55 | 53.09 | 0.02 | 2.00 | 5 (11) | 47 (11) | 66 (11) |
| 4 | 100 | 42 | 26.55 | 53.09 | 0.04 | 3.03 | 7 (11) | 66 (11) | 104 (11) |
| 5 | 100 | 43 | 26.55 | 53.09 | 0.09 | 4.08 | 11 (11) | 80 (11) | 147 (11) |
| 6 | 100 | 44 | 26.55 | 53.09 | 0.17 | 5.14 | 14 (11) | 89 (11) | 195 (11) |
| 7 | 100 | 45 | 26.55 | 53.09 | 0.28 | 6.23 | 19 (11) | 91 (11) | 251 (11) |
| 8 | 100 | 45 | 26.55 | 53.09 | 0.42 | 7.33 | 24 (11) | 86 (11) | 313 (11) |
| 9 | 100 | 46 | 26.55 | 53.09 | 0.62 | 8.46 | 30 (11) | 73 (11) | 385 (11) |
| 10 | 100 | 47 | 26.55 | 53.09 | 0.86 | 9.60 | 36 (11) | 50 (11) | 466 (11) |
| 11 | 100 | 48 | 26.55 | 53.09 | 1.17 | 10.76 | 44 (11) | 9 (11) | 560 (11) |
| 12 | 100 | 49 | 26.55 | 53.09 | 1.54 | 11.94 | 53 (11) | 56 (11) | 668 (11) |
| 13 | 100 | 49 | 26.55 | 53.09 | 1.98 | 13.14 | 64 (11) | 149 (11) | 791 (11) |
| 14 | 100 | 50 | 26.55 | 53.09 | 2.50 | 14.36 | 76 (11) | 272 (11) | 929 (11) |
| 15 | 100 | 51 | 26.55 | 53.09 | 3.11 | 15.60 | 89 (11) | 427 (11) | 1081 (11) |
| 16 | 100 | 52 | 26.55 | 53.09 | 3.81 | 16.86 | 104 (11) | 616 (11) | 1248 (11) |
| 17 | 100 | 52 | 26.55 | 53.09 | 4.60 | 18.13 | 120 (11) | 839 (11) | 1430 (11) |
| 18 | 100 | 53 | 26.55 | 53.09 | 5.49 | 19.43 | 137 (11) | 1098 (11) | 1626 (11) |
| 19 | 100 | 54 | 26.55 | 53.09 | 6.50 | 20.74 | 156 (11) | 1393 (11) | 1837 (11) |
| 20 | 100 | 55 | 26.55 | 53.09 | 7.61 | 22.08 | 176 (11) | 1724 (11) | 2062 (11) |
| 21 | 100 | 56 | 26.55 | 53.09 | 8.85 | 23.43 | 197 (11) | 2091 (11) | 2302 (11) |
| 22 | 100 | 56 | 26.55 | 53.09 | 10.21 | 24.80 | 220 (11) | 2496 (11) | 2557 (11) |

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 23 | 100 | 57 | 26.55 | 53.09 | 11.70 | 26.19 | 244 (11) | 2939 (11) | 2826 (11) |
| 24 | 100 | 58 | 26.55 | 53.09 | 13.33 | 27.60 | 269 (11) | 3420 (11) | 3109 (11) |
| 25 | 100 | 59 | 26.55 | 53.09 | 15.10 | 29.03 | 296 (11) | 3939 (11) | 3408 (11) |
| 26 | 100 | 59 | 26.55 | 53.09 | 17.02 | 30.48 | 323 (11) | 4497 (11) | 3721 (11) |
| 27 | 100 | 60 | 26.55 | 53.09 | 19.09 | 31.95 | 352 (11) | 5095 (11) | 4049 (11) |
| 28 | 100 | 61 | 26.55 | 53.09 | 21.32 | 33.43 | 382 (11) | 5733 (11) | 4391 (11) |
| 29 | 100 | 62 | 26.55 | 53.09 | 23.72 | 34.94 | 414 (11) | 6410 (11) | 4748 (11) |
| 30 | 100 | 63 | 26.55 | 53.09 | 26.29 | 36.46 | 446 (11) | 7128 (11) | 5120 (11) |
| 31 | 100 | 63 | 26.55 | 53.09 | 29.04 | 38.01 | 480 (11) | 7887 (11) | 5507 (11) |
| 32 | 100 | 64 | 26.55 | 53.09 | 31.97 | 39.57 | 515 (11) | 8687 (11) | 5908 (11) |
| 33 | 100 | 65 | 26.55 | 53.09 | 35.08 | 41.15 | 551 (11) | 9528 (11) | 6324 (11) |
| 34 | 100 | 66 | 26.55 | 53.09 | 38.40 | 42.75 | 589 (11) | 10411 (11) | 6754 (11) |
| 35 | 100 | 66 | 26.55 | 53.09 | 41.91 | 44.37 | 627 (11) | 11335 (11) | 7199 (11) |
| 36 | 100 | 67 | 26.55 | 53.09 | 45.63 | 46.01 | 667 (11) | 12302 (11) | 7658 (11) |
| 37 | 100 | 68 | 26.55 | 53.09 | 49.56 | 47.67 | 708 (11) | 13311 (11) | 8131 (11) |
| 38 | 100 | 69 | 26.55 | 53.09 | 53.70 | 49.35 | 750 (11) | 14362 (11) | 8619 (11) |
| 39 | 100 | 70 | 26.55 | 53.09 | 58.08 | 51.04 | 793 (11) | 15456 (11) | 9121 (11) |
| 40 | 100 | 70 | 26.55 | 53.09 | 62.68 | 52.76 | 837 (11) | 16593 (11) | 9637 (11) |
| 41 | 100 | 71 | 26.55 | 53.09 | 67.51 | 54.49 | 882 (11) | 17773 (11) | 10168 (11) |
| 42 | 100 | 72 | 26.55 | 53.09 | 72.59 | 56.24 | 929 (11) | 18996 (11) | 10712 (11) |
| 43 | 100 | 73 | 26.55 | 53.09 | 77.91 | 58.02 | 976 (11) | 20263 (11) | 11270 (11) |
| 44 | 100 | 73 | 26.55 | 53.09 | 83.48 | 59.81 | 1025 (11) | 21573 (11) | 11842 (11) |
| 45 | 100 | 74 | 26.55 | 53.09 | 89.31 | 61.62 | 1074 (11) | 22927 (11) | 12428 (11) |
| 46 | 100 | 75 | 26.55 | 53.09 | 95.41 | 63.45 | 1125 (11) | 24325 (11) | 13028 (11) |
| 47 | 100 | 76 | 26.55 | 53.09 | 101.77 | 65.30 | 1176 (11) | 25767 (11) | 13641 (11) |
| 48 | 100 | 77 | 26.55 | 53.09 | 108.41 | 67.17 | 1229 (11) | 27253 (11) | 14267 (11) |
| 49 | 100 | 77 | 26.55 | 53.09 | 115.34 | 69.05 | 1283 (11) | 28783 (11) | 14908 (11) |
| 50 | 100 | 78 | 26.55 | 53.09 | 122.54 | 70.96 | 1337 (11) | 30358 (11) | 15561 (11) |
| 51 | 100 | 79 | 26.55 | 53.09 | 130.04 | 72.88 | 1393 (11) | 31977 (11) | 16228 (11) |
| 52 | 100 | 80 | 26.55 | 53.09 | 137.84 | 74.83 | 1450 (11) | 33641 (11) | 16908 (11) |
| 53 | 100 | 80 | 26.55 | 53.09 | 145.95 | 76.79 | 1507 (11) | 35349 (11) | 17601 (11) |
| 54 | 100 | 81 | 26.55 | 53.09 | 154.36 | 78.77 | 1566 (11) | 37102 (11) | 18307 (11) |
| 55 | 100 | 82 | 26.55 | 53.09 | 163.09 | 80.78 | 1625 (11) | 38900 (11) | 19026 (11) |
| 56 | 100 | 83 | 26.55 | 53.09 | 172.14 | 82.80 | 1686 (11) | 40743 (11) | 19758 (11) |
| 57 | 100 | 84 | 26.55 | 53.09 | 181.51 | 84.84 | 1747 (11) | 42631 (11) | 20503 (11) |
| 58 | 100 | 84 | 26.55 | 53.09 | 191.22 | 86.89 | 1810 (11) | 44564 (11) | 21260 (11) |
| 59 | 100 | 85 | 26.55 | 53.09 | 201.27 | 88.97 | 1873 (11) | 46542 (11) | 22030 (11) |
| 60 | 100 | 86 | 26.55 | 53.09 | 211.67 | 91.07 | 1937 (11) | 48568 (11) | 22814 (11) |
| 61 | 100 | 87 | 26.55 | 53.09 | 222.45 | 93.18 | 2003 (11) | 50644 (11) | 23612 (11) |
| 62 | 100 | 87 | 26.55 | 53.09 | 233.61 | 95.32 | 2069 (11) | 52774 (11) | 24425 (11) |
| 63 | 100 | 88 | 26.55 | 53.09 | 245.17 | 97.47 | 2137 (11) | 54959 (11) | 25254 (11) |
| 64 | 100 | 89 | 26.55 | 53.09 | 257.15 | 99.65 | 2206 (11) | 57201 (11) | 26100 (11) |
| 65 | 100 | 90 | 26.55 | 53.09 | 269.54 | 101.84 | 2276 (11) | 59501 (11) | 26962 (11) |
| 66 | 100 | 91 | 26.55 | 53.09 | 282.37 | 104.05 | 2348 (11) | 61857 (11) | 27840 (11) |

Fondazione

Tensione massima di compressione nel calcestruzzo 29050 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 1 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0 (11) | 0 (11) | 0 (11) |
| 2 | 100 | 110 | 45.24 | 22.62 | 0.85 | 0.00 | 5 (11) | 199 (11) | 61 (11) |
| 3 | 100 | 110 | 45.24 | 22.62 | 3.38 | 0.00 | 21 (11) | 792 (11) | 243 (11) |
| 4 | 100 | 110 | 45.24 | 22.62 | 7.58 | 0.00 | 47 (11) | 1777 (11) | 545 (11) |

Tensione massima di compressione nel calcestruzzo 14940 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 1 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0 (12) | 0 (12) | 0 (12) |
| 2 | 100 | 41 | 26.55 | 53.09 | 0.01 | 0.99 | 2 (13) | 25 (12) | 33 (13) |
| 3 | 100 | 42 | 26.55 | 53.09 | 0.03 | 2.00 | 5 (13) | 47 (12) | 71 (13) |
| 4 | 100 | 42 | 26.55 | 53.09 | 0.08 | 3.03 | 8 (13) | 66 (12) | 115 (13) |
| 5 | 100 | 43 | 26.55 | 53.09 | 0.17 | 4.08 | 13 (13) | 80 (12) | 166 (13) |
| 6 | 100 | 44 | 26.55 | 53.09 | 0.29 | 5.14 | 17 (13) | 89 (12) | 226 (13) |
| 7 | 100 | 45 | 26.55 | 53.09 | 0.46 | 6.23 | 23 (13) | 91 (12) | 296 (13) |
| 8 | 100 | 45 | 26.55 | 53.09 | 0.69 | 7.33 | 30 (13) | 86 (12) | 378 (13) |
| 9 | 100 | 46 | 26.55 | 53.09 | 0.98 | 8.46 | 38 (13) | 73 (12) | 474 (13) |
| 10 | 100 | 47 | 26.55 | 53.09 | 1.34 | 9.60 | 48 (13) | 94 (13) | 587 (13) |
| 11 | 100 | 48 | 26.55 | 53.09 | 1.78 | 10.76 | 59 (13) | 202 (13) | 716 (13) |
| 12 | 100 | 49 | 26.55 | 53.09 | 2.30 | 11.94 | 72 (13) | 346 (13) | 863 (13) |
| 13 | 100 | 49 | 26.55 | 53.09 | 2.93 | 13.14 | 87 (13) | 529 (13) | 1027 (13) |
| 14 | 100 | 50 | 26.55 | 53.09 | 3.65 | 14.36 | 103 (13) | 752 (13) | 1209 (13) |
| 15 | 100 | 51 | 26.55 | 53.09 | 4.49 | 15.60 | 121 (13) | 1016 (13) | 1408 (13) |
| 16 | 100 | 52 | 26.55 | 53.09 | 5.45 | 16.86 | 141 (13) | 1324 (13) | 1625 (13) |
| 17 | 100 | 52 | 26.55 | 53.09 | 6.53 | 18.13 | 162 (13) | 1674 (13) | 1860 (13) |
| 18 | 100 | 53 | 26.55 | 53.09 | 7.74 | 19.43 | 185 (13) | 2069 (13) | 2112 (13) |
| 19 | 100 | 54 | 26.55 | 53.09 | 9.09 | 20.74 | 210 (13) | 2508 (13) | 2383 (13) |
| 20 | 100 | 55 | 26.55 | 53.09 | 10.59 | 22.08 | 236 (13) | 2994 (13) | 2672 (13) |
| 21 | 100 | 56 | 26.55 | 53.09 | 12.24 | 23.43 | 264 (13) | 3525 (13) | 2979 (13) |
| 22 | 100 | 56 | 26.55 | 53.09 | 14.05 | 24.80 | 293 (13) | 4104 (13) | 3305 (13) |
| 23 | 100 | 57 | 26.55 | 53.09 | 16.03 | 26.19 | 324 (13) | 4731 (13) | 3649 (13) |
| 24 | 100 | 58 | 26.55 | 53.09 | 18.19 | 27.60 | 357 (13) | 5406 (13) | 4011 (13) |
| 25 | 100 | 59 | 26.55 | 53.09 | 20.53 | 29.03 | 391 (13) | 6129 (13) | 4392 (13) |
| 26 | 100 | 59 | 26.55 | 53.09 | 23.06 | 30.48 | 426 (13) | 6902 (13) | 4792 (13) |
| 27 | 100 | 60 | 26.55 | 53.09 | 25.79 | 31.95 | 464 (13) | 7725 (13) | 5210 (13) |
| 28 | 100 | 61 | 26.55 | 53.09 | 28.72 | 33.43 | 503 (13) | 8599 (13) | 5647 (13) |
| 29 | 100 | 62 | 26.55 | 53.09 | 31.87 | 34.94 | 543 (13) | 9523 (13) | 6102 (13) |
| 30 | 100 | 63 | 26.55 | 53.09 | 35.23 | 36.46 | 585 (13) | 10498 (13) | 6575 (13) |
| 31 | 100 | 63 | 26.55 | 53.09 | 38.82 | 38.01 | 628 (13) | 11525 (13) | 7067 (13) |
| 32 | 100 | 64 | 26.55 | 53.09 | 42.64 | 39.57 | 673 (13) | 12604 (13) | 7577 (13) |
| 33 | 100 | 65 | 26.55 | 53.09 | 46.70 | 41.15 | 719 (13) | 13735 (13) | 8106 (13) |
| 34 | 100 | 66 | 26.55 | 53.09 | 51.01 | 42.75 | 767 (13) | 14919 (13) | 8652 (13) |
| 35 | 100 | 66 | 26.55 | 53.09 | 55.57 | 44.37 | 816 (13) | 16155 (13) | 9217 (13) |
| 36 | 100 | 67 | 26.55 | 53.09 | 60.40 | 46.01 | 867 (13) | 17445 (13) | 9800 (13) |
| 37 | 100 | 68 | 26.55 | 53.09 | 65.50 | 47.67 | 919 (13) | 18789 (13) | 10401 (13) |
| 38 | 100 | 69 | 26.55 | 53.09 | 70.87 | 49.35 | 972 (13) | 20186 (13) | 11020 (13) |
| 39 | 100 | 70 | 26.55 | 53.09 | 76.52 | 51.04 | 1027 (13) | 21637 (13) | 11657 (13) |
| 40 | 100 | 70 | 26.55 | 53.09 | 82.47 | 52.76 | 1084 (13) | 23142 (13) | 12311 (13) |
| 41 | 100 | 71 | 26.55 | 53.09 | 88.72 | 54.49 | 1141 (13) | 24702 (13) | 12983 (13) |
| 42 | 100 | 72 | 26.55 | 53.09 | 95.27 | 56.24 | 1200 (13) | 26316 (13) | 13672 (13) |
| 43 | 100 | 73 | 26.55 | 53.09 | 102.13 | 58.02 | 1260 (13) | 27986 (13) | 14379 (13) |
| 44 | 100 | 73 | 26.55 | 53.09 | 109.31 | 59.81 | 1322 (13) | 29710 (13) | 15103 (13) |
| 45 | 100 | 74 | 26.55 | 53.09 | 116.82 | 61.62 | 1385 (13) | 31490 (13) | 15844 (13) |
| 46 | 100 | 75 | 26.55 | 53.09 | 124.66 | 63.45 | 1449 (13) | 33324 (13) | 16603 (13) |
| 47 | 100 | 76 | 26.55 | 53.09 | 132.85 | 65.30 | 1515 (13) | 35215 (13) | 17378 (13) |
| 48 | 100 | 77 | 26.55 | 53.09 | 141.38 | 67.17 | 1582 (13) | 37161 (13) | 18171 (13) |
| 49 | 100 | 77 | 26.55 | 53.09 | 150.27 | 69.05 | 1650 (13) | 39163 (13) | 18980 (13) |
| 50 | 100 | 78 | 26.55 | 53.09 | 159.52 | 70.96 | 1719 (13) | 41221 (13) | 19806 (13) |
| 51 | 100 | 79 | 26.55 | 53.09 | 169.14 | 72.88 | 1789 (13) | 43335 (13) | 20648 (13) |
| 52 | 100 | 80 | 26.55 | 53.09 | 179.14 | 74.83 | 1861 (13) | 45505 (13) | 21507 (13) |
| 53 | 100 | 80 | 26.55 | 53.09 | 189.52 | 76.79 | 1934 (13) | 47732 (13) | 22382 (13) |
| 54 | 100 | 81 | 26.55 | 53.09 | 200.30 | 78.77 | 2008 (13) | 50015 (13) | 23273 (13) |
| 55 | 100 | 82 | 26.55 | 53.09 | 211.47 | 80.78 | 2084 (13) | 52355 (13) | 24181 (13) |
| 56 | 100 | 83 | 26.55 | 53.09 | 223.05 | 82.80 | 2160 (13) | 54751 (13) | 25104 (13) |
| 57 | 100 | 84 | 26.55 | 53.09 | 235.05 | 84.84 | 2238 (13) | 57204 (13) | 26044 (13) |

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 58 | 100 | 84 | 26.55 | 53.09 | 247.46 | 86.89 | 2317 (13) | 59714 (13) | 26999 (13) |
| 59 | 100 | 85 | 26.55 | 53.09 | 260.30 | 88.97 | 2397 (13) | 62281 (13) | 27970 (13) |
| 60 | 100 | 86 | 26.55 | 53.09 | 273.59 | 91.07 | 2478 (13) | 64907 (13) | 28958 (13) |
| 61 | 100 | 87 | 26.55 | 53.09 | 287.34 | 93.18 | 2561 (13) | 67596 (13) | 29963 (13) |
| 62 | 100 | 87 | 26.55 | 53.09 | 301.57 | 95.32 | 2645 (13) | 70349 (13) | 30986 (13) |
| 63 | 100 | 88 | 26.55 | 53.09 | 316.29 | 97.47 | 2730 (13) | 73170 (13) | 32028 (13) |
| 64 | 100 | 89 | 26.55 | 53.09 | 331.53 | 99.65 | 2817 (13) | 76060 (13) | 33090 (13) |
| 65 | 100 | 90 | 26.55 | 53.09 | 347.29 | 101.84 | 2905 (13) | 79019 (13) | 34171 (13) |
| 66 | 100 | 91 | 26.55 | 53.09 | 363.57 | 104.05 | 2995 (13) | 82047 (13) | 35272 (13) |

Fondazione

Tensione massima di compressione nel calcestruzzo 13073 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | 100 | 110 | 45.24 | 22.62 | 0.00 | 0.00 | 0 (12) | 0 (12) | 0 (12) |
| 2 | 100 | 110 | 45.24 | 22.62 | 1.12 | 0.00 | 7 (13) | 262 (13) | 80 (13) |
| 3 | 100 | 110 | 45.24 | 22.62 | 4.45 | 0.00 | 27 (13) | 1043 (13) | 320 (13) |
| 4 | 100 | 110 | 45.24 | 22.62 | 9.97 | 0.00 | 61 (13) | 2336 (13) | 717 (13) |
| 5 | 100 | 110 | 45.24 | 22.62 | 17.65 | 0.00 | 108 (13) | 4135 (13) | 1269 (13) |
| 6 | 100 | 110 | 45.24 | 22.62 | 27.47 | 0.00 | 169 (13) | 6433 (13) | 1975 (13) |
| 7 | 100 | 110 | 45.24 | 22.62 | 39.38 | 0.00 | 242 (13) | 9224 (13) | 2831 (13) |
| 8 | 100 | 110 | 22.62 | 45.24 | -665.79 | 0.00 | 4086 (13) | 47875 (13) | 155953 (13) |
| 9 | 100 | 110 | 22.62 | 45.24 | -654.36 | 0.00 | 4016 (13) | 47052 (13) | 153275 (13) |
| 10 | 100 | 110 | 22.62 | 45.24 | -642.41 | 0.00 | 3943 (13) | 46193 (13) | 150475 (13) |
| 11 | 100 | 110 | 22.62 | 45.24 | -629.97 | 0.00 | 3866 (13) | 45299 (13) | 147561 (13) |
| 12 | 100 | 110 | 22.62 | 45.24 | -617.07 | 0.00 | 3787 (13) | 44371 (13) | 144539 (13) |
| 13 | 100 | 110 | 22.62 | 45.24 | -603.73 | 0.00 | 3705 (13) | 43412 (13) | 141416 (13) |
| 14 | 100 | 110 | 22.62 | 45.24 | -589.99 | 0.00 | 3621 (13) | 42424 (13) | 138197 (13) |
| 15 | 100 | 110 | 22.62 | 45.24 | -575.87 | 0.00 | 3534 (13) | 41409 (13) | 134890 (13) |
| 16 | 100 | 110 | 22.62 | 45.24 | -561.40 | 0.00 | 3446 (13) | 40368 (13) | 131501 (13) |
| 17 | 100 | 110 | 22.62 | 45.24 | -546.61 | 0.00 | 3355 (13) | 39305 (13) | 128037 (13) |
| 18 | 100 | 110 | 22.62 | 45.24 | -531.53 | 0.00 | 3262 (13) | 38220 (13) | 124504 (13) |
| 19 | 100 | 110 | 22.62 | 45.24 | -516.18 | 0.00 | 3168 (13) | 37117 (13) | 120908 (13) |
| 20 | 100 | 110 | 22.62 | 45.24 | -500.59 | 0.00 | 3072 (13) | 35996 (13) | 117256 (13) |
| 21 | 100 | 110 | 22.62 | 45.24 | -484.79 | 0.00 | 2975 (13) | 34859 (13) | 113555 (13) |
| 22 | 100 | 110 | 22.62 | 45.24 | -468.80 | 0.00 | 2877 (13) | 33710 (13) | 109811 (13) |
| 23 | 100 | 110 | 22.62 | 45.24 | -452.67 | 0.00 | 2778 (13) | 32549 (13) | 106031 (13) |
| 24 | 100 | 110 | 22.62 | 45.24 | -436.40 | 0.00 | 2678 (13) | 31380 (13) | 102220 (13) |
| 25 | 100 | 110 | 22.62 | 45.24 | -420.03 | 0.00 | 2578 (13) | 30203 (13) | 98387 (13) |
| 26 | 100 | 110 | 22.62 | 45.24 | -403.59 | 0.00 | 2477 (13) | 29021 (13) | 94536 (13) |
| 27 | 100 | 110 | 22.62 | 45.24 | -387.11 | 0.00 | 2376 (13) | 27835 (13) | 90675 (13) |
| 28 | 100 | 110 | 22.62 | 45.24 | -370.61 | 0.00 | 2275 (13) | 26649 (13) | 86810 (13) |
| 29 | 100 | 110 | 22.62 | 45.24 | -354.12 | 0.00 | 2173 (13) | 25463 (13) | 82947 (13) |
| 30 | 100 | 110 | 22.62 | 45.24 | -337.67 | 0.00 | 2072 (13) | 24280 (13) | 79094 (13) |
| 31 | 100 | 110 | 22.62 | 45.24 | -321.28 | 0.00 | 1972 (13) | 23102 (13) | 75256 (13) |
| 32 | 100 | 110 | 22.62 | 45.24 | -304.99 | 0.00 | 1872 (13) | 21931 (13) | 71441 (13) |
| 33 | 100 | 110 | 22.62 | 45.24 | -288.83 | 0.00 | 1773 (13) | 20768 (13) | 67654 (13) |
| 34 | 100 | 110 | 22.62 | 45.24 | -272.81 | 0.00 | 1674 (13) | 19617 (13) | 63902 (13) |
| 35 | 100 | 110 | 22.62 | 45.24 | -256.97 | 0.00 | 1577 (13) | 18478 (13) | 60192 (13) |
| 36 | 100 | 110 | 22.62 | 45.24 | -241.34 | 0.00 | 1481 (13) | 17354 (13) | 56530 (13) |
| 37 | 100 | 110 | 22.62 | 45.24 | -225.94 | 0.00 | 1387 (13) | 16246 (13) | 52923 (13) |
| 38 | 100 | 110 | 22.62 | 45.24 | -210.80 | 0.00 | 1294 (13) | 15158 (13) | 49376 (13) |
| 39 | 100 | 110 | 22.62 | 45.24 | -195.95 | 0.00 | 1203 (13) | 14090 (13) | 45898 (13) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 151 di 314 |

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 40 | 100 | 110 | 22.62 | 45.24 | -181.41 | 0.00 | 1113 (13) | 13045 (13) | 42493 (13) |
| 41 | 100 | 110 | 22.62 | 45.24 | -165.95 | 0.00 | 1019 (13) | 11933 (13) | 38872 (13) |
| 42 | 100 | 110 | 22.62 | 45.24 | -150.44 | 0.00 | 923 (13) | 10818 (13) | 35239 (13) |
| 43 | 100 | 110 | 22.62 | 45.24 | -135.53 | 0.00 | 832 (13) | 9745 (13) | 31745 (13) |
| 44 | 100 | 110 | 22.62 | 45.24 | -121.24 | 0.00 | 744 (13) | 8718 (13) | 28398 (13) |
| 45 | 100 | 110 | 22.62 | 45.24 | -107.60 | 0.00 | 660 (13) | 7737 (13) | 25203 (13) |
| 46 | 100 | 110 | 22.62 | 45.24 | -94.64 | 0.00 | 581 (13) | 6805 (13) | 22167 (13) |
| 47 | 100 | 110 | 22.62 | 45.24 | -82.38 | 0.00 | 506 (13) | 5924 (13) | 19297 (13) |
| 48 | 100 | 110 | 22.62 | 45.24 | -70.86 | 0.00 | 435 (13) | 5095 (13) | 16598 (13) |
| 49 | 100 | 110 | 22.62 | 45.24 | -60.10 | 0.00 | 369 (13) | 4322 (13) | 14079 (13) |
| 50 | 100 | 110 | 22.62 | 45.24 | -50.14 | 0.00 | 308 (13) | 3605 (13) | 11744 (13) |
| 51 | 100 | 110 | 22.62 | 45.24 | -40.98 | 0.00 | 252 (13) | 2947 (13) | 9600 (13) |
| 52 | 100 | 110 | 22.62 | 45.24 | -32.68 | 0.00 | 201 (13) | 2350 (13) | 7655 (13) |
| 53 | 100 | 110 | 22.62 | 45.24 | -25.25 | 0.00 | 155 (13) | 1815 (13) | 5914 (13) |
| 54 | 100 | 110 | 22.62 | 45.24 | -18.72 | 0.00 | 115 (13) | 1346 (13) | 4384 (13) |
| 55 | 100 | 110 | 22.62 | 45.24 | -13.11 | 0.00 | 80 (13) | 943 (13) | 3071 (13) |
| 56 | 100 | 110 | 22.62 | 45.24 | -8.47 | 0.00 | 52 (13) | 609 (13) | 1983 (13) |
| 57 | 100 | 110 | 22.62 | 45.24 | -4.80 | 0.00 | 29 (13) | 345 (13) | 1125 (13) |
| 58 | 100 | 110 | 22.62 | 45.24 | -2.15 | 0.00 | 13 (13) | 155 (13) | 504 (13) |
| 59 | 100 | 110 | 22.62 | 45.24 | -0.54 | 0.00 | 3 (13) | 39 (13) | 127 (13) |
| 60 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | 0 (12) | 0 (12) | 0 (12) |

Verifica a fessurazione

Simbologia adottata

| | |
|------------|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Af | area ferri zona tesa espresso in [cmq] |
| Aeff | area efficace espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| Mpf | momento di prima fessurazione espressa in [kNm] |
| ϵ | deformazione espresso in % |
| Sm | spaziatura tra le fessure espressa in [mm] |
| w | apertura delle fessure espressa in [mm] |

Combinazioni SLER

Paramento

Apertura limite fessure $w_{lim}=0.20$

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 153 di 314 |

| n° | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|------|------|-------|---------|--------|--------|----------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 66 | 100 | 91 | 53.09 | 1600.00 | 282.37 | 606.37 | 0.000000 | 0.00 | 0.000 (10) |

Fondazione

Apertura limite fessure $w_{lim}=0.20$

| n° | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|------|------|-------|---------|---------|---------|----------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 1 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (10) |
| 2 | 100 | 110 | 45.24 | 1600.00 | 0.85 | 719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 3 | 100 | 110 | 45.24 | 1600.00 | 3.38 | 719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 4 | 100 | 110 | 45.24 | 1600.00 | 7.58 | 719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 5 | 100 | 110 | 45.24 | 1600.00 | 13.45 | 719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 6 | 100 | 110 | 45.24 | 1600.00 | 20.95 | 719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 7 | 100 | 110 | 45.24 | 1600.00 | 30.09 | 719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 8 | 100 | 110 | 45.24 | 1600.00 | -428.05 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 9 | 100 | 110 | 45.24 | 1600.00 | -419.51 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 10 | 100 | 110 | 45.24 | 1600.00 | -410.76 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 11 | 100 | 110 | 45.24 | 1600.00 | -401.81 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 12 | 100 | 110 | 45.24 | 1600.00 | -392.67 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 13 | 100 | 110 | 45.24 | 1600.00 | -383.36 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 14 | 100 | 110 | 45.24 | 1600.00 | -373.88 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 15 | 100 | 110 | 45.24 | 1600.00 | -364.27 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 16 | 100 | 110 | 45.24 | 1600.00 | -354.51 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 17 | 100 | 110 | 45.24 | 1600.00 | -344.64 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 18 | 100 | 110 | 45.24 | 1600.00 | -334.67 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 19 | 100 | 110 | 45.24 | 1600.00 | -324.60 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 20 | 100 | 110 | 45.24 | 1600.00 | -314.45 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 21 | 100 | 110 | 45.24 | 1600.00 | -304.24 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 22 | 100 | 110 | 45.24 | 1600.00 | -293.98 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 23 | 100 | 110 | 45.24 | 1600.00 | -283.68 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 24 | 100 | 110 | 45.24 | 1600.00 | -273.35 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 25 | 100 | 110 | 45.24 | 1600.00 | -263.02 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 26 | 100 | 110 | 45.24 | 1600.00 | -252.68 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 27 | 100 | 110 | 45.24 | 1600.00 | -242.37 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 28 | 100 | 110 | 45.24 | 1600.00 | -232.08 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 29 | 100 | 110 | 45.24 | 1600.00 | -221.84 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 30 | 100 | 110 | 45.24 | 1600.00 | -211.65 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 31 | 100 | 110 | 45.24 | 1600.00 | -201.54 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 32 | 100 | 110 | 45.24 | 1600.00 | -191.51 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 33 | 100 | 110 | 45.24 | 1600.00 | -181.58 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 34 | 100 | 110 | 45.24 | 1600.00 | -171.76 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 35 | 100 | 110 | 45.24 | 1600.00 | -162.06 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 36 | 100 | 110 | 45.24 | 1600.00 | -152.51 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 37 | 100 | 110 | 45.24 | 1600.00 | -143.10 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 38 | 100 | 110 | 45.24 | 1600.00 | -133.86 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 39 | 100 | 110 | 45.24 | 1600.00 | -124.80 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 40 | 100 | 110 | 45.24 | 1600.00 | -115.94 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 41 | 100 | 110 | 45.24 | 1600.00 | -106.00 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 42 | 100 | 110 | 45.24 | 1600.00 | -95.87 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 43 | 100 | 110 | 45.24 | 1600.00 | -86.17 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 44 | 100 | 110 | 45.24 | 1600.00 | -76.91 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 45 | 100 | 110 | 45.24 | 1600.00 | -68.10 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 46 | 100 | 110 | 45.24 | 1600.00 | -59.77 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 47 | 100 | 110 | 45.24 | 1600.00 | -51.92 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 48 | 100 | 110 | 45.24 | 1600.00 | -44.56 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 49 | 100 | 110 | 45.24 | 1600.00 | -37.72 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 50 | 100 | 110 | 45.24 | 1600.00 | -31.40 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 51 | 100 | 110 | 45.24 | 1600.00 | -25.62 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 154 di 314 |

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 52 | 100 | 110 | 45.24 | 1600.00 | -20.38 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 53 | 100 | 110 | 45.24 | 1600.00 | -15.72 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 54 | 100 | 110 | 45.24 | 1600.00 | -11.63 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 55 | 100 | 110 | 45.24 | 1600.00 | -8.13 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 56 | 100 | 110 | 45.24 | 1600.00 | -5.24 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 57 | 100 | 110 | 45.24 | 1600.00 | -2.97 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 58 | 100 | 110 | 45.24 | 1600.00 | -1.33 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 59 | 100 | 110 | 45.24 | 1600.00 | -0.33 | -719.00 | 0.000000 | 0.00 | 0.000 (10) |
| 60 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (10) |

Combinazioni SLEF

Paramento

Apertura limite fessure $w_{lim}=0.30$

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 1 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (11) |
| 2 | 100 | 41 | 0.00 | 0.00 | 0.00 | 5.81 | 0.000000 | 0.00 | 0.000 (11) |
| 3 | 100 | 42 | 0.00 | 0.00 | 0.02 | 16.80 | 0.000000 | 0.00 | 0.000 (11) |
| 4 | 100 | 42 | 0.00 | 0.00 | 0.04 | 35.28 | 0.000000 | 0.00 | 0.000 (11) |
| 5 | 100 | 43 | 0.00 | 0.00 | 0.09 | 65.88 | 0.000000 | 0.00 | 0.000 (11) |
| 6 | 100 | 44 | 0.00 | 0.00 | 0.17 | 118.89 | 0.000000 | 0.00 | 0.000 (11) |
| 7 | 100 | 45 | 0.00 | 0.00 | 0.28 | 222.15 | 0.000000 | 0.00 | 0.000 (11) |
| 8 | 100 | 45 | 0.00 | 0.00 | 0.42 | 484.78 | 0.000000 | 0.00 | 0.000 (11) |
| 9 | 100 | 46 | 0.00 | 0.00 | 0.62 | 2201.91 | 0.000000 | 0.00 | 0.000 (11) |
| 10 | 100 | 47 | 0.00 | 0.00 | 0.86 | 1546.90 | 0.000000 | 0.00 | 0.000 (11) |
| 11 | 100 | 48 | 0.00 | 0.00 | 1.17 | 704.98 | 0.000000 | 0.00 | 0.000 (11) |
| 12 | 100 | 49 | 53.09 | 1600.00 | 1.54 | 508.13 | 0.000000 | 0.00 | 0.000 (11) |
| 13 | 100 | 49 | 53.09 | 1600.00 | 1.98 | 423.46 | 0.000000 | 0.00 | 0.000 (11) |
| 14 | 100 | 50 | 53.09 | 1600.00 | 2.50 | 378.29 | 0.000000 | 0.00 | 0.000 (11) |
| 15 | 100 | 51 | 53.09 | 1600.00 | 3.11 | 351.57 | 0.000000 | 0.00 | 0.000 (11) |
| 16 | 100 | 52 | 53.09 | 1600.00 | 3.81 | 334.94 | 0.000000 | 0.00 | 0.000 (11) |
| 17 | 100 | 52 | 53.09 | 1600.00 | 4.60 | 324.43 | 0.000000 | 0.00 | 0.000 (11) |
| 18 | 100 | 53 | 53.09 | 1600.00 | 5.49 | 317.91 | 0.000000 | 0.00 | 0.000 (11) |
| 19 | 100 | 54 | 53.09 | 1600.00 | 6.50 | 314.14 | 0.000000 | 0.00 | 0.000 (11) |
| 20 | 100 | 55 | 53.09 | 1600.00 | 7.61 | 312.36 | 0.000000 | 0.00 | 0.000 (11) |
| 21 | 100 | 56 | 53.09 | 1600.00 | 8.85 | 312.06 | 0.000000 | 0.00 | 0.000 (11) |
| 22 | 100 | 56 | 53.09 | 1600.00 | 10.21 | 312.89 | 0.000000 | 0.00 | 0.000 (11) |
| 23 | 100 | 57 | 53.09 | 1600.00 | 11.70 | 314.62 | 0.000000 | 0.00 | 0.000 (11) |
| 24 | 100 | 58 | 53.09 | 1600.00 | 13.33 | 317.08 | 0.000000 | 0.00 | 0.000 (11) |
| 25 | 100 | 59 | 53.09 | 1600.00 | 15.10 | 320.12 | 0.000000 | 0.00 | 0.000 (11) |
| 26 | 100 | 59 | 53.09 | 1600.00 | 17.02 | 323.66 | 0.000000 | 0.00 | 0.000 (11) |
| 27 | 100 | 60 | 53.09 | 1600.00 | 19.09 | 327.62 | 0.000000 | 0.00 | 0.000 (11) |
| 28 | 100 | 61 | 53.09 | 1600.00 | 21.32 | 331.94 | 0.000000 | 0.00 | 0.000 (11) |
| 29 | 100 | 62 | 53.09 | 1600.00 | 23.72 | 336.58 | 0.000000 | 0.00 | 0.000 (11) |
| 30 | 100 | 63 | 53.09 | 1600.00 | 26.29 | 341.49 | 0.000000 | 0.00 | 0.000 (11) |
| 31 | 100 | 63 | 53.09 | 1600.00 | 29.04 | 346.65 | 0.000000 | 0.00 | 0.000 (11) |
| 32 | 100 | 64 | 53.09 | 1600.00 | 31.97 | 352.03 | 0.000000 | 0.00 | 0.000 (11) |
| 33 | 100 | 65 | 53.09 | 1600.00 | 35.08 | 357.61 | 0.000000 | 0.00 | 0.000 (11) |
| 34 | 100 | 66 | 53.09 | 1600.00 | 38.40 | 363.38 | 0.000000 | 0.00 | 0.000 (11) |
| 35 | 100 | 66 | 53.09 | 1600.00 | 41.91 | 369.31 | 0.000000 | 0.00 | 0.000 (11) |
| 36 | 100 | 67 | 53.09 | 1600.00 | 45.63 | 375.40 | 0.000000 | 0.00 | 0.000 (11) |
| 37 | 100 | 68 | 53.09 | 1600.00 | 49.56 | 381.64 | 0.000000 | 0.00 | 0.000 (11) |
| 38 | 100 | 69 | 53.09 | 1600.00 | 53.70 | 388.02 | 0.000000 | 0.00 | 0.000 (11) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 155 di 314 |

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 39 | 100 | 70 | 53.09 | 1600.00 | 58.08 | 394.53 | 0.000000 | 0.00 | 0.000 (11) |
| 40 | 100 | 70 | 53.09 | 1600.00 | 62.68 | 401.16 | 0.000000 | 0.00 | 0.000 (11) |
| 41 | 100 | 71 | 53.09 | 1600.00 | 67.51 | 407.91 | 0.000000 | 0.00 | 0.000 (11) |
| 42 | 100 | 72 | 53.09 | 1600.00 | 72.59 | 414.78 | 0.000000 | 0.00 | 0.000 (11) |
| 43 | 100 | 73 | 53.09 | 1600.00 | 77.91 | 421.75 | 0.000000 | 0.00 | 0.000 (11) |
| 44 | 100 | 73 | 53.09 | 1600.00 | 83.48 | 428.82 | 0.000000 | 0.00 | 0.000 (11) |
| 45 | 100 | 74 | 53.09 | 1600.00 | 89.31 | 436.00 | 0.000000 | 0.00 | 0.000 (11) |
| 46 | 100 | 75 | 53.09 | 1600.00 | 95.41 | 443.27 | 0.000000 | 0.00 | 0.000 (11) |
| 47 | 100 | 76 | 53.09 | 1600.00 | 101.77 | 450.64 | 0.000000 | 0.00 | 0.000 (11) |
| 48 | 100 | 77 | 53.09 | 1600.00 | 108.41 | 458.10 | 0.000000 | 0.00 | 0.000 (11) |
| 49 | 100 | 77 | 53.09 | 1600.00 | 115.34 | 465.65 | 0.000000 | 0.00 | 0.000 (11) |
| 50 | 100 | 78 | 53.09 | 1600.00 | 122.54 | 473.29 | 0.000000 | 0.00 | 0.000 (11) |
| 51 | 100 | 79 | 53.09 | 1600.00 | 130.04 | 481.02 | 0.000000 | 0.00 | 0.000 (11) |
| 52 | 100 | 80 | 53.09 | 1600.00 | 137.84 | 488.83 | 0.000000 | 0.00 | 0.000 (11) |
| 53 | 100 | 80 | 53.09 | 1600.00 | 145.95 | 496.73 | 0.000000 | 0.00 | 0.000 (11) |
| 54 | 100 | 81 | 53.09 | 1600.00 | 154.36 | 504.70 | 0.000000 | 0.00 | 0.000 (11) |
| 55 | 100 | 82 | 53.09 | 1600.00 | 163.09 | 512.76 | 0.000000 | 0.00 | 0.000 (11) |
| 56 | 100 | 83 | 53.09 | 1600.00 | 172.14 | 520.90 | 0.000000 | 0.00 | 0.000 (11) |
| 57 | 100 | 84 | 53.09 | 1600.00 | 181.51 | 529.12 | 0.000000 | 0.00 | 0.000 (11) |
| 58 | 100 | 84 | 53.09 | 1600.00 | 191.22 | 537.41 | 0.000000 | 0.00 | 0.000 (11) |
| 59 | 100 | 85 | 53.09 | 1600.00 | 201.27 | 545.78 | 0.000000 | 0.00 | 0.000 (11) |
| 60 | 100 | 86 | 53.09 | 1600.00 | 211.67 | 554.23 | 0.000000 | 0.00 | 0.000 (11) |
| 61 | 100 | 87 | 53.09 | 1600.00 | 222.45 | 562.75 | 0.000000 | 0.00 | 0.000 (11) |
| 62 | 100 | 87 | 53.09 | 1600.00 | 233.61 | 571.33 | 0.000000 | 0.00 | 0.000 (11) |
| 63 | 100 | 88 | 53.09 | 1600.00 | 245.17 | 579.99 | 0.000000 | 0.00 | 0.000 (11) |
| 64 | 100 | 89 | 53.09 | 1600.00 | 257.15 | 588.72 | 0.000000 | 0.00 | 0.000 (11) |
| 65 | 100 | 90 | 53.09 | 1600.00 | 269.54 | 597.51 | 0.000000 | 0.00 | 0.000 (11) |
| 66 | 100 | 91 | 53.09 | 1600.00 | 282.37 | 606.37 | 0.000000 | 0.00 | 0.000 (11) |

Fondazione

Apertura limite fessure $w_{lim}=0.30$

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 1 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (11) |
| 2 | 100 | 110 | 45.24 | 1600.00 | 0.85 | 719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 3 | 100 | 110 | 45.24 | 1600.00 | 3.38 | 719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 4 | 100 | 110 | 45.24 | 1600.00 | 7.58 | 719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 5 | 100 | 110 | 45.24 | 1600.00 | 13.45 | 719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 6 | 100 | 110 | 45.24 | 1600.00 | 20.95 | 719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 7 | 100 | 110 | 45.24 | 1600.00 | 30.09 | 719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 8 | 100 | 110 | 45.24 | 1600.00 | -428.05 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 9 | 100 | 110 | 45.24 | 1600.00 | -419.51 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 10 | 100 | 110 | 45.24 | 1600.00 | -410.76 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 11 | 100 | 110 | 45.24 | 1600.00 | -401.81 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 12 | 100 | 110 | 45.24 | 1600.00 | -392.67 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 13 | 100 | 110 | 45.24 | 1600.00 | -383.36 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 14 | 100 | 110 | 45.24 | 1600.00 | -373.88 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 15 | 100 | 110 | 45.24 | 1600.00 | -364.27 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 16 | 100 | 110 | 45.24 | 1600.00 | -354.51 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 17 | 100 | 110 | 45.24 | 1600.00 | -344.64 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 18 | 100 | 110 | 45.24 | 1600.00 | -334.67 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 19 | 100 | 110 | 45.24 | 1600.00 | -324.60 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 20 | 100 | 110 | 45.24 | 1600.00 | -314.45 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 21 | 100 | 110 | 45.24 | 1600.00 | -304.24 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 22 | 100 | 110 | 45.24 | 1600.00 | -293.98 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 23 | 100 | 110 | 45.24 | 1600.00 | -283.68 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 24 | 100 | 110 | 45.24 | 1600.00 | -273.35 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 156 di 314 |

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 25 | 100 | 110 | 45.24 | 1600.00 | -263.02 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 26 | 100 | 110 | 45.24 | 1600.00 | -252.68 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 27 | 100 | 110 | 45.24 | 1600.00 | -242.37 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 28 | 100 | 110 | 45.24 | 1600.00 | -232.08 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 29 | 100 | 110 | 45.24 | 1600.00 | -221.84 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 30 | 100 | 110 | 45.24 | 1600.00 | -211.65 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 31 | 100 | 110 | 45.24 | 1600.00 | -201.54 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 32 | 100 | 110 | 45.24 | 1600.00 | -191.51 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 33 | 100 | 110 | 45.24 | 1600.00 | -181.58 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 34 | 100 | 110 | 45.24 | 1600.00 | -171.76 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 35 | 100 | 110 | 45.24 | 1600.00 | -162.06 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 36 | 100 | 110 | 45.24 | 1600.00 | -152.51 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 37 | 100 | 110 | 45.24 | 1600.00 | -143.10 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 38 | 100 | 110 | 45.24 | 1600.00 | -133.86 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 39 | 100 | 110 | 45.24 | 1600.00 | -124.80 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 40 | 100 | 110 | 45.24 | 1600.00 | -115.94 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 41 | 100 | 110 | 45.24 | 1600.00 | -106.00 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 42 | 100 | 110 | 45.24 | 1600.00 | -95.87 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 43 | 100 | 110 | 45.24 | 1600.00 | -86.17 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 44 | 100 | 110 | 45.24 | 1600.00 | -76.91 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 45 | 100 | 110 | 45.24 | 1600.00 | -68.10 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 46 | 100 | 110 | 45.24 | 1600.00 | -59.77 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 47 | 100 | 110 | 45.24 | 1600.00 | -51.92 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 48 | 100 | 110 | 45.24 | 1600.00 | -44.56 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 49 | 100 | 110 | 45.24 | 1600.00 | -37.72 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 50 | 100 | 110 | 45.24 | 1600.00 | -31.40 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 51 | 100 | 110 | 45.24 | 1600.00 | -25.62 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 52 | 100 | 110 | 45.24 | 1600.00 | -20.38 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 53 | 100 | 110 | 45.24 | 1600.00 | -15.72 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 54 | 100 | 110 | 45.24 | 1600.00 | -11.63 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 55 | 100 | 110 | 45.24 | 1600.00 | -8.13 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 56 | 100 | 110 | 45.24 | 1600.00 | -5.24 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 57 | 100 | 110 | 45.24 | 1600.00 | -2.97 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 58 | 100 | 110 | 45.24 | 1600.00 | -1.33 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 59 | 100 | 110 | 45.24 | 1600.00 | -0.33 | -719.00 | 0.000000 | 0.00 | 0.000 (11) |
| 60 | 100 | 110 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (11) |

Combinazioni SLEQ

Paramento

Apertura limite fessure $w_{lim}=0.20$

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 1 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (12) |
| 2 | 100 | 41 | 0.00 | 0.00 | 0.00 | 5.81 | 0.000000 | 0.00 | 0.000 (12) |
| 3 | 100 | 42 | 0.00 | 0.00 | 0.02 | 16.80 | 0.000000 | 0.00 | 0.000 (12) |
| 4 | 100 | 42 | 0.00 | 0.00 | 0.04 | 35.28 | 0.000000 | 0.00 | 0.000 (12) |
| 5 | 100 | 43 | 0.00 | 0.00 | 0.09 | 65.88 | 0.000000 | 0.00 | 0.000 (12) |
| 6 | 100 | 44 | 0.00 | 0.00 | 0.17 | 118.89 | 0.000000 | 0.00 | 0.000 (12) |
| 7 | 100 | 45 | 0.00 | 0.00 | 0.28 | 222.15 | 0.000000 | 0.00 | 0.000 (12) |
| 8 | 100 | 45 | 0.00 | 0.00 | 0.42 | 484.78 | 0.000000 | 0.00 | 0.000 (12) |
| 9 | 100 | 46 | 0.00 | 0.00 | 0.62 | 2201.91 | 0.000000 | 0.00 | 0.000 (12) |
| 10 | 100 | 47 | 0.00 | 0.00 | 0.86 | 1546.90 | 0.000000 | 0.00 | 0.000 (12) |
| 11 | 100 | 48 | 0.00 | 0.00 | 1.17 | 704.98 | 0.000000 | 0.00 | 0.000 (12) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 157 di 314 |

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 12 | 100 | 49 | 53.09 | 1600.00 | 1.54 | 508.13 | 0.000000 | 0.00 | 0.000 (12) |
| 13 | 100 | 49 | 53.09 | 1600.00 | 1.98 | 423.46 | 0.000000 | 0.00 | 0.000 (12) |
| 14 | 100 | 50 | 53.09 | 1600.00 | 2.50 | 378.29 | 0.000000 | 0.00 | 0.000 (12) |
| 15 | 100 | 51 | 53.09 | 1600.00 | 3.11 | 351.57 | 0.000000 | 0.00 | 0.000 (12) |
| 16 | 100 | 52 | 53.09 | 1600.00 | 3.81 | 334.94 | 0.000000 | 0.00 | 0.000 (12) |
| 17 | 100 | 52 | 53.09 | 1600.00 | 4.60 | 324.43 | 0.000000 | 0.00 | 0.000 (12) |
| 18 | 100 | 53 | 53.09 | 1600.00 | 5.49 | 317.91 | 0.000000 | 0.00 | 0.000 (12) |
| 19 | 100 | 54 | 53.09 | 1600.00 | 6.50 | 314.14 | 0.000000 | 0.00 | 0.000 (12) |
| 20 | 100 | 55 | 53.09 | 1600.00 | 7.61 | 312.36 | 0.000000 | 0.00 | 0.000 (12) |
| 21 | 100 | 56 | 53.09 | 1600.00 | 8.85 | 312.06 | 0.000000 | 0.00 | 0.000 (12) |
| 22 | 100 | 56 | 53.09 | 1600.00 | 10.21 | 312.89 | 0.000000 | 0.00 | 0.000 (12) |
| 23 | 100 | 57 | 53.09 | 1600.00 | 11.70 | 314.62 | 0.000000 | 0.00 | 0.000 (12) |
| 24 | 100 | 58 | 53.09 | 1600.00 | 13.33 | 317.08 | 0.000000 | 0.00 | 0.000 (12) |
| 25 | 100 | 59 | 53.09 | 1600.00 | 15.10 | 320.12 | 0.000000 | 0.00 | 0.000 (12) |
| 26 | 100 | 59 | 53.09 | 1600.00 | 17.02 | 323.66 | 0.000000 | 0.00 | 0.000 (12) |
| 27 | 100 | 60 | 53.09 | 1600.00 | 19.09 | 327.62 | 0.000000 | 0.00 | 0.000 (12) |
| 28 | 100 | 61 | 53.09 | 1600.00 | 21.32 | 331.94 | 0.000000 | 0.00 | 0.000 (12) |
| 29 | 100 | 62 | 53.09 | 1600.00 | 23.72 | 336.58 | 0.000000 | 0.00 | 0.000 (12) |
| 30 | 100 | 63 | 53.09 | 1600.00 | 26.29 | 341.49 | 0.000000 | 0.00 | 0.000 (12) |
| 31 | 100 | 63 | 53.09 | 1600.00 | 29.04 | 346.65 | 0.000000 | 0.00 | 0.000 (12) |
| 32 | 100 | 64 | 53.09 | 1600.00 | 31.97 | 352.03 | 0.000000 | 0.00 | 0.000 (12) |
| 33 | 100 | 65 | 53.09 | 1600.00 | 35.08 | 357.61 | 0.000000 | 0.00 | 0.000 (12) |
| 34 | 100 | 66 | 53.09 | 1600.00 | 38.40 | 363.38 | 0.000000 | 0.00 | 0.000 (12) |
| 35 | 100 | 66 | 53.09 | 1600.00 | 41.91 | 369.31 | 0.000000 | 0.00 | 0.000 (12) |
| 36 | 100 | 67 | 53.09 | 1600.00 | 45.63 | 375.40 | 0.000000 | 0.00 | 0.000 (12) |
| 37 | 100 | 68 | 53.09 | 1600.00 | 49.56 | 381.64 | 0.000000 | 0.00 | 0.000 (12) |
| 38 | 100 | 69 | 53.09 | 1600.00 | 53.70 | 388.02 | 0.000000 | 0.00 | 0.000 (12) |
| 39 | 100 | 70 | 53.09 | 1600.00 | 58.08 | 394.53 | 0.000000 | 0.00 | 0.000 (12) |
| 40 | 100 | 70 | 53.09 | 1600.00 | 62.68 | 401.16 | 0.000000 | 0.00 | 0.000 (12) |
| 41 | 100 | 71 | 53.09 | 1600.00 | 67.51 | 407.91 | 0.000000 | 0.00 | 0.000 (12) |
| 42 | 100 | 72 | 53.09 | 1600.00 | 72.59 | 414.78 | 0.000000 | 0.00 | 0.000 (12) |
| 43 | 100 | 73 | 53.09 | 1600.00 | 77.91 | 421.75 | 0.000000 | 0.00 | 0.000 (12) |
| 44 | 100 | 73 | 53.09 | 1600.00 | 83.48 | 428.82 | 0.000000 | 0.00 | 0.000 (12) |
| 45 | 100 | 74 | 53.09 | 1600.00 | 89.31 | 436.00 | 0.000000 | 0.00 | 0.000 (12) |
| 46 | 100 | 75 | 53.09 | 1600.00 | 95.41 | 443.27 | 0.000000 | 0.00 | 0.000 (12) |
| 47 | 100 | 76 | 53.09 | 1600.00 | 101.77 | 450.64 | 0.000000 | 0.00 | 0.000 (12) |
| 48 | 100 | 77 | 53.09 | 1600.00 | 108.41 | 458.10 | 0.000000 | 0.00 | 0.000 (12) |
| 49 | 100 | 77 | 53.09 | 1600.00 | 115.34 | 465.65 | 0.000000 | 0.00 | 0.000 (12) |
| 50 | 100 | 78 | 53.09 | 1600.00 | 122.54 | 473.29 | 0.000000 | 0.00 | 0.000 (12) |
| 51 | 100 | 79 | 53.09 | 1600.00 | 130.04 | 481.02 | 0.000000 | 0.00 | 0.000 (12) |
| 52 | 100 | 80 | 53.09 | 1600.00 | 137.84 | 488.83 | 0.000000 | 0.00 | 0.000 (12) |
| 53 | 100 | 80 | 53.09 | 1600.00 | 145.95 | 496.73 | 0.000000 | 0.00 | 0.000 (12) |
| 54 | 100 | 81 | 53.09 | 1600.00 | 154.36 | 504.70 | 0.000000 | 0.00 | 0.000 (12) |
| 55 | 100 | 82 | 53.09 | 1600.00 | 163.09 | 512.76 | 0.000000 | 0.00 | 0.000 (12) |
| 56 | 100 | 83 | 53.09 | 1600.00 | 172.14 | 520.90 | 0.000000 | 0.00 | 0.000 (12) |
| 57 | 100 | 84 | 53.09 | 1600.00 | 181.51 | 529.12 | 0.000000 | 0.00 | 0.000 (12) |
| 58 | 100 | 84 | 53.09 | 1600.00 | 191.22 | 537.41 | 0.000000 | 0.00 | 0.000 (12) |
| 59 | 100 | 85 | 53.09 | 1600.00 | 201.27 | 545.78 | 0.000000 | 0.00 | 0.000 (12) |
| 60 | 100 | 86 | 53.09 | 1600.00 | 211.67 | 554.23 | 0.000000 | 0.00 | 0.000 (12) |
| 61 | 100 | 87 | 53.09 | 1600.00 | 222.45 | 562.75 | 0.000000 | 0.00 | 0.000 (12) |
| 62 | 100 | 87 | 53.09 | 1600.00 | 233.61 | 571.33 | 0.000000 | 0.00 | 0.000 (12) |
| 63 | 100 | 88 | 53.09 | 1600.00 | 245.17 | 579.99 | 0.000000 | 0.00 | 0.000 (12) |
| 64 | 100 | 89 | 53.09 | 1600.00 | 257.15 | 588.72 | 0.000000 | 0.00 | 0.000 (12) |
| 65 | 100 | 90 | 53.09 | 1600.00 | 269.54 | 597.51 | 0.000000 | 0.00 | 0.000 (12) |
| 66 | 100 | 91 | 53.09 | 1600.00 | 282.37 | 606.37 | 0.000000 | 0.00 | 0.000 (12) |

Fondazione

Apertura limite fessure $w_{lim}=0.20$

13. TABULATI DI CALCOLO CONCIO 2

13.1 RISULTATI PER COMBINAZIONE

Spinta e forze

Simbologia adottata

| | |
|--------|--|
| Ic | Indice della combinazione |
| A | Tipo azione |
| I | Inclinazione della spinta, espressa in [°] |
| V | Valore dell'azione, espressa in [kN] |
| Cx, Cy | Componente in direzione X ed Y dell'azione, espressa in [kN] |
| Px, Py | Coordinata X ed Y del punto di applicazione dell'azione, espressa in [m] |

| Ic | A | V [kN] | I [°] | Cx [kN] | Cy [kN] | Px [m] | Py [m] |
|----|---|-----------|----------|------------|---------------|-----------|-----------|
| 1 | Spinta statica | 164.47 | 0.00 | 164.47 | 0.00 | 4.10 | -3.65 |
| | Peso/Inerzia muro | | | 0.00 | 185.91/0.00 | 0.90 | -4.39 |
| | Peso/Inerzia terrapieno | | | 0.00 | 391.94/0.00 | 2.15 | -2.46 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 2 | Spinta statica | 99.21 | 0.00 | 99.21 | 0.00 | 4.10 | -3.84 |
| | Incremento di spinta sismica | | 33.94 | 33.94 | 0.00 | 4.10 | -3.93 |
| | Peso/Inerzia muro | | | 24.12 | 185.91/12.06 | 0.90 | -4.39 |
| | Peso/Inerzia terrapieno | | | 49.21 | 379.19/24.60 | 2.15 | -2.46 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 3 | Spinta statica | 99.21 | 0.00 | 99.21 | 0.00 | 4.10 | -3.84 |
| | Incremento di spinta sismica | | 21.49 | 21.49 | 0.00 | 4.10 | -3.93 |
| | Peso/Inerzia muro | | | 24.12 | 185.91/-12.06 | 0.90 | -4.39 |
| | Peso/Inerzia terrapieno | | | 49.21 | 379.19/-24.60 | 2.15 | -2.46 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 10 | Spinta statica | 124.79 | 0.00 | 124.79 | 0.00 | 4.10 | -3.66 |
| | Peso/Inerzia muro | | | 0.00 | 185.91/0.00 | 0.90 | -4.39 |
| | Peso/Inerzia terrapieno | | | 0.00 | 385.55/0.00 | 2.15 | -2.46 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 11 | Spinta statica | 124.79 | 0.00 | 124.79 | 0.00 | 4.10 | -3.66 |
| | Peso/Inerzia muro | | | 0.00 | 185.91/0.00 | 0.90 | -4.39 |
| | Peso/Inerzia terrapieno | | | 0.00 | 385.55/0.00 | 2.15 | -2.46 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 12 | Spinta statica | 124.79 | 0.00 | 124.79 | 0.00 | 4.10 | -3.66 |
| | Peso/Inerzia muro | | | 0.00 | 185.91/0.00 | 0.90 | -4.39 |
| | Peso/Inerzia terrapieno | | | 0.00 | 385.55/0.00 | 2.15 | -2.46 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 13 | Spinta statica | 124.79 | 0.00 | 124.79 | 0.00 | 4.10 | -3.66 |
| | Incremento di spinta sismica | | 24.01 | 24.01 | 0.00 | 4.10 | -3.93 |
| | Peso/Inerzia muro | | | 14.06 | 185.91/7.03 | 0.90 | -4.39 |
| | Peso/Inerzia terrapieno | | | 29.15 | 385.55/14.57 | 2.15 | -2.46 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |

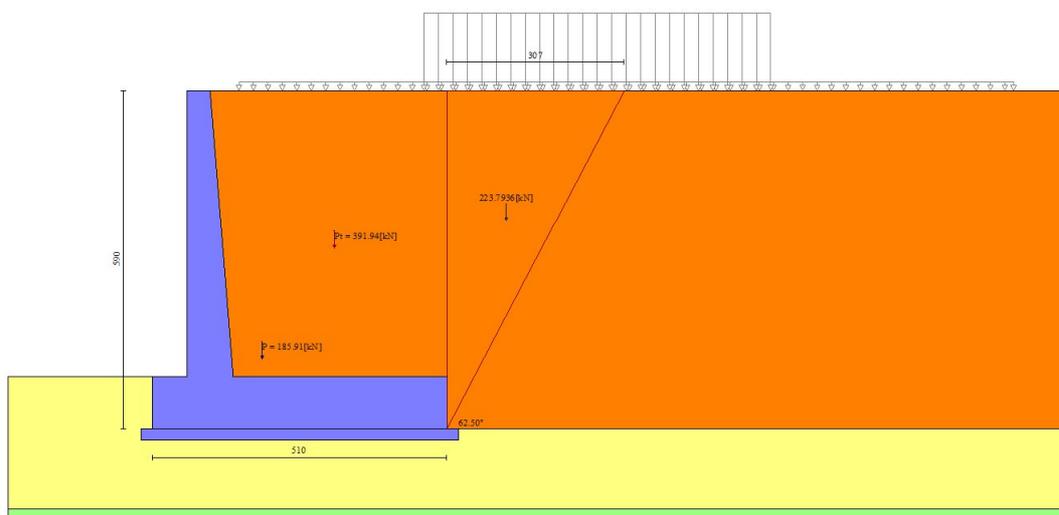


Fig. 3 - Cuneo di spinta (combinazione statica) (Combinazione n° 1)

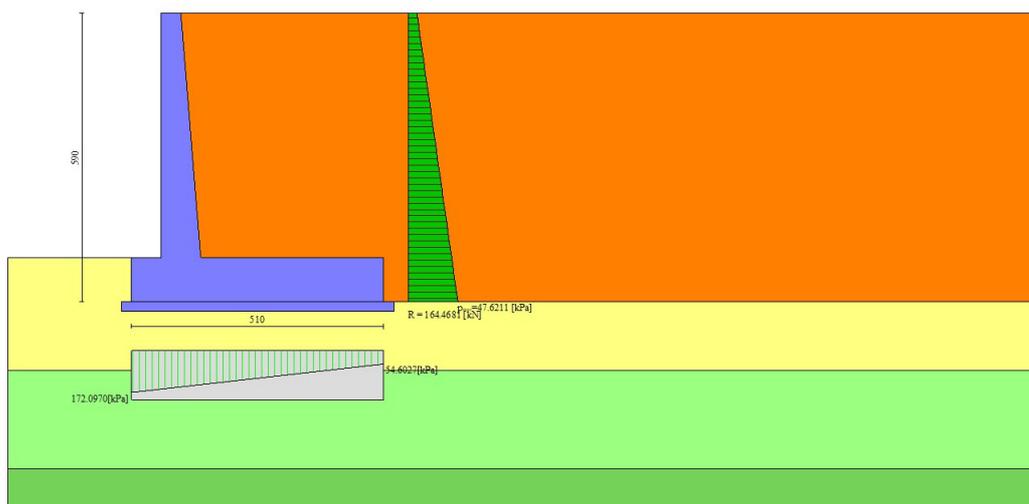


Fig. 4 - Diagramma delle pressioni (combinazione statica) (Combinazione n° 1)

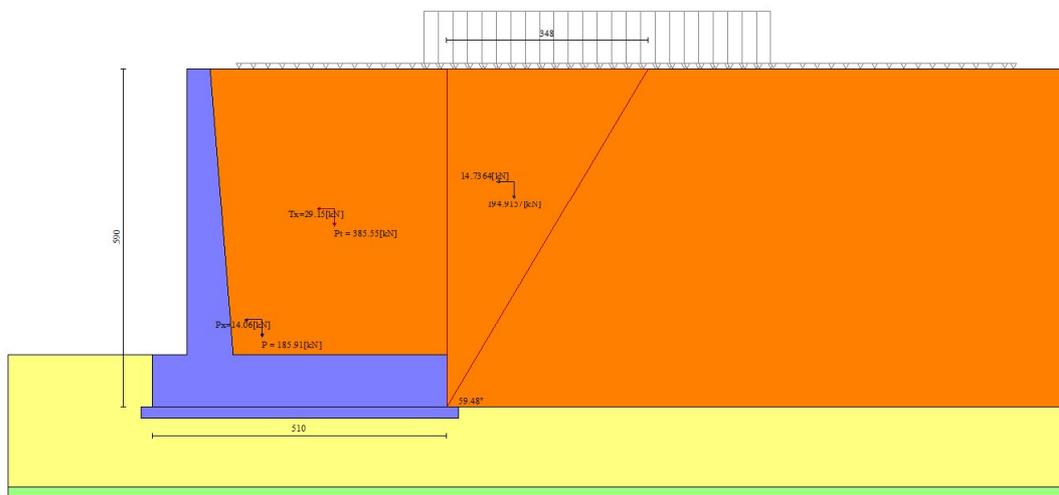


Fig. 5 - Cuneo di spinta (combinazione sismica) (Combinazione n° 13)

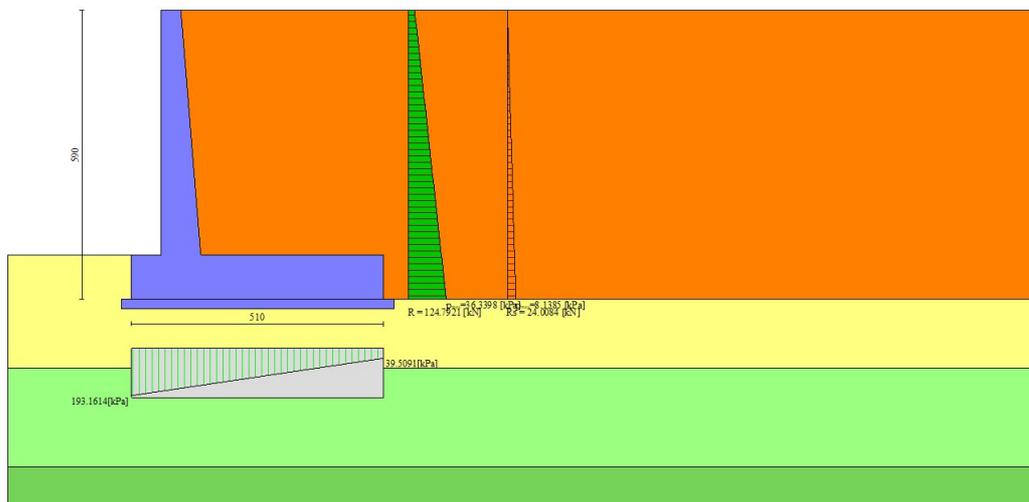


Fig. 6 - Diagramma delle pressioni (combinazione sismica) (Combinazione n° 13)

Risultanti globali

Simbologia adottata

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
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Cmb Indice/Tipo combinazione

N Componente normale al piano di posa, espressa in [kN]

T Componente parallela al piano di posa, espressa in [kN]

Mr Momento ribaltante, espresso in [kNm]

Ms Momento stabilizzante, espresso in [kNm]

ecc Eccentricità risultante, espressa in [m]

| Ic | N | T | Mr | Ms | ecc |
|--------------------|--------|--------|--------|---------|-------|
| | [kN] | [kN] | [kNm] | [kNm] | [m] |
| 1 - STR (A1-M1-R3) | 577.85 | 164.47 | 370.63 | 1589.07 | 0.440 |
| 2 - STR (A1-M1-R3) | 601.76 | 206.48 | 476.97 | 1648.08 | 0.603 |
| 3 - STR (A1-M1-R3) | 528.43 | 194.03 | 552.91 | 1547.66 | 0.666 |
| 4 - GEO (A2-M2-R2) | 574.82 | 165.45 | 376.41 | 1579.23 | 0.456 |
| 5 - GEO (A2-M2-R2) | 601.76 | 206.48 | 476.97 | 1648.08 | 0.603 |
| 6 - GEO (A2-M2-R2) | 528.43 | 194.03 | 552.91 | 1547.66 | 0.666 |
| 7 - EQU (A1-M1-R3) | 577.85 | 164.47 | 370.63 | 1589.07 | 0.440 |
| 8 - EQU (A1-M1-R3) | 613.34 | 241.56 | 565.36 | 1679.79 | 0.732 |
| 9 - EQU (A1-M1-R3) | 516.85 | 225.67 | 666.25 | 1547.66 | 0.844 |
| 10 - SLER | 571.46 | 124.79 | 280.02 | 1568.34 | 0.295 |
| 11 - SLEF | 571.46 | 124.79 | 280.02 | 1568.34 | 0.295 |
| 12 - SLEQ | 571.46 | 124.79 | 280.02 | 1568.34 | 0.295 |
| 13 - SLEQ | 593.07 | 192.01 | 448.70 | 1627.63 | 0.561 |

Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

Cmb Indice/Tipo combinazione

S Sisma (H: componente orizzontale, V: componente verticale)

FS_{SCO} Coeff. di sicurezza allo scorrimento

FS_{RIB} Coeff. di sicurezza al ribaltamento

FS_{QLIM} Coeff. di sicurezza a carico limite

FS_{STAB} Coeff. di sicurezza a stabilità globale

FS_{HYD} Coeff. di sicurezza a sifonamento

FS_{SUPL} Coeff. di sicurezza a sollevamento

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{SUPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|--------------------|
| 1 - STR (A1-M1-R3) | | 1.638 | | 1.872 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.359 | | 1.387 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.270 | | 1.427 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.263 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.321 | | |
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.273 | | |
| 7 - EQU (A1-M1-R3) | | | 4.287 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 2.971 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.323 | | | | |

Verifica a scorrimento fondazione

Simbologia adottata

| | |
|-----|---|
| n° | Indice combinazione |
| Rsa | Resistenza allo scorrimento per attrito, espresso in [kN] |
| Rpt | Resistenza passiva terreno antistante, espresso in [kN] |
| Rps | Resistenza passiva sperone, espresso in [kN] |
| Rp | Resistenza a carichi orizzontali pali (solo per fondazione mista), espresso in [kN] |
| Rt | Resistenza a carichi orizzontali tiranti (solo se presenti), espresso in [kN] |
| R | Resistenza allo scorrimento (somma di Rsa+Rpt+Rps+Rp), espresso in [kN] |
| T | Carico parallelo al piano di posa, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto R/T) |

| n° | Rsa | Rpt | Rps | Rp | Rt | R | T | FS |
|--------------------------|--------|------|------|------|------|--------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | |
| 1 - STR (A1-M1-R3) | 269.45 | 0.00 | 0.00 | -- | -- | 269.45 | 164.47 | 1.638 |
| 2 - STR (A1-M1-R3) H + V | 280.61 | 0.00 | 0.00 | -- | -- | 280.61 | 206.48 | 1.359 |
| 3 - STR (A1-M1-R3) H - V | 246.41 | 0.00 | 0.00 | -- | -- | 246.41 | 194.03 | 1.270 |

Verifica a carico limite

Simbologia adottata

| | |
|----|--|
| n° | Indice combinazione |
| N | Carico normale totale al piano di posa, espresso in [kN] |
| Qu | carico limite del terreno, espresso in [kN] |
| Qd | Portanza di progetto, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto tra il carico limie e carico agente al piano di posa) |

| n° | N | Qu | Qd | FS |
|--------------------------|--------|---------|--------|-------|
| | [kN] | [kN] | [kN] | |
| 1 - STR (A1-M1-R3) | 577.85 | 1081.62 | 772.59 | 1.872 |
| 2 - STR (A1-M1-R3) H + V | 601.76 | 834.45 | 695.37 | 1.387 |
| 3 - STR (A1-M1-R3) H - V | 528.43 | 753.92 | 628.26 | 1.427 |

Dettagli calcolo portanza

Simbologia adottata

| | |
|----|---------------------|
| n° | Indice combinazione |
|----|---------------------|

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
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| | |
|---------------|--|
| Nc, Nq, Ny | Fattori di capacità portante |
| ic, iq, iy | Fattori di inclinazione del carico |
| dc, dq, dy | Fattori di profondità del piano di posa |
| gc, gq, gy | Fattori di inclinazione del profilo topografico |
| bc, bq, by | Fattori di inclinazione del piano di posa |
| sc, sq, sy | Fattori di forma della fondazione |
| pc, pq, py | Fattori di riduzione per punzonamento secondo Vesic |
| Re | Fattore di riduzione capacità portante per eccentricità secondo Meyerhof |
| Ir, Irc | Indici di rigidità per punzonamento secondo Vesic |
| ry fattore | Fattori per tener conto dell'effetto piastra. Per fondazioni che hanno larghezza maggiore di 2 m, il terzo termine della formula trinomia $0.5B\gamma N_c$ viene moltiplicato per questo fattore |
| D | Affondamento del piano di posa, espresso in [m] |
| B' | Larghezza fondazione ridotta, espresso in [m] |
| H | Altezza del cuneo di rottura, espresso in [m] |
| γ | Peso di volume del terreno medio, espresso in [kN/mc] |
| ϕ | Angolo di attrito del terreno medio, espresso in [°] |
| c | Coesione del terreno medio, espresso in [kPa] |

Per i coeff. che in tabella sono indicati con il simbolo '-' sono coeff. non presenti nel metodo scelto (Meyerhof).

| n° | Nc Nq Ny | ic iq iy | dc dq dy | gc gq gy | bc bq by | sc sq sy | pc pq py | Ir | Irc | Re | ry |
|----|----------------------------|-------------------------|-------------------------|----------------|----------------|----------------|----------------|----|-----|----|-------|
| 1 | 28.123 16.666 13.508 | 0.678 0.678 0.206 | 1.060 1.030 1.030 | -- -- -- | -- -- -- | -- -- -- | -- -- -- | -- | -- | -- | 0.898 |
| 2 | 28.123 16.666 13.508 | 0.623 0.623 0.122 | 1.060 1.030 1.030 | -- -- -- | -- -- -- | -- -- -- | -- -- -- | -- | -- | -- | 0.898 |
| 3 | 28.123 16.666 13.508 | 0.602 0.602 0.095 | 1.060 1.030 1.030 | -- -- -- | -- -- -- | -- -- -- | -- -- -- | -- | -- | -- | 0.898 |

| n° | D [m] | B' [m] | H [m] | γ [°] | ϕ [kN/mc] | c [kPa] |
|----|----------|-----------|----------|-----------------|-------------------|------------|
| 1 | 0.90 | 4.22 | 4.34 | 10.55 | 29.12 | 0 |
| 2 | 0.90 | 3.89 | 4.34 | 10.55 | 29.12 | 0 |
| 3 | 0.90 | 3.76 | 4.34 | 10.55 | 29.12 | 0 |

Verifica a ribaltamento

Simbologia adottata

| | |
|----|--|
| n° | Indice combinazione |
| Ms | Momento stabilizzante, espresso in [kNm] |
| Mr | Momento ribaltante, espresso in [kNm] |
| FS | Fattore di sicurezza (rapporto tra momento stabilizzante e momento ribaltante) |

La verifica viene eseguita rispetto allo spigolo inferiore esterno della fondazione

| n° | Ms [kNm] | Mr [kNm] | FS |
|--------------------------|-------------|-------------|-------|
| 7 - EQU (A1-M1-R3) | 1589.07 | 370.63 | 4.287 |
| 8 - EQU (A1-M1-R3) H + V | 1679.79 | 565.36 | 2.971 |
| 9 - EQU (A1-M1-R3) H - V | 1547.66 | 666.25 | 2.323 |

Verifica stabilità globale muro + terreno

Simbologia adottata

Ic Indice/Tipo combinazione

C Centro superficie di scorrimento, espresso in [m]

R Raggio, espresso in [m]

FS Fattore di sicurezza

| Ic | C [m] | R [m] | FS |
|--------------------------|-------------|----------|-------|
| 4 - GEO (A2-M2-R2) | -1.00; 3.00 | 10.27 | 1.263 |
| 5 - GEO (A2-M2-R2) H + V | -1.00; 3.00 | 10.27 | 1.321 |
| 6 - GEO (A2-M2-R2) H - V | -1.00; 3.00 | 10.27 | 1.273 |

Dettagli strisce verifiche stabilità

Simbologia adottata

Le ascisse X sono considerate positive verso monte

Le ordinate Y sono considerate positive verso l'alto

Origine in testa al muro (spigolo contro terra)

W peso della striscia espresso in [kN]

Qy carico sulla striscia espresso in [kN]

α angolo fra la base della striscia e l'orizzontale espresso in [°] (positivo antiorario)

ϕ angolo d'attrito del terreno lungo la base della striscia

c coesione del terreno lungo la base della striscia espressa in [kPa]

b larghezza della striscia espressa in [m]

u pressione neutra lungo la base della striscia espressa in [kPa]

Tx; Ty Resistenza al taglio fornita dai tiranti in direzione X ed Y espressa in [kPa]

Combinazione n° 4 - GEO (A2-M2-R2)

| n° | W [kN] | Qy [kN] | b [m] | α [°] | ϕ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|-------------|-----------------|---------------|------------|------------|----------------|
| 1 | 9.90 | 16.67 | 8.83 - 0.65 | 67.871 | 29.256 | 0 | 0.0 | |

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | W [kN] | Qy [kN] | b [m] | α [°] | φ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|----------|----------|------------|------------|----------------|
| 2 | 26.71 | 16.67 | 0.65 | 59.765 | 29.256 | 0 | 0.0 | |
| 3 | 38.99 | 16.67 | 0.65 | 53.126 | 29.256 | 0 | 0.0 | |
| 4 | 48.74 | 16.67 | 0.65 | 47.412 | 29.256 | 0 | 0.0 | |
| 5 | 56.78 | 16.67 | 0.65 | 42.271 | 29.256 | 0 | 0.0 | |
| 6 | 63.53 | 16.67 | 0.65 | 37.524 | 29.256 | 0 | 0.0 | |
| 7 | 69.24 | 16.67 | 0.65 | 33.065 | 29.256 | 0 | 0.0 | |
| 8 | 76.45 | 14.84 | 0.65 | 28.823 | 20.458 | 0 | 0.0 | |
| 9 | 81.38 | 1.69 | 0.65 | 24.748 | 20.458 | 0 | 0.0 | |
| 10 | 84.77 | 1.69 | 0.65 | 20.804 | 20.458 | 0 | 0.9 | |
| 11 | 87.53 | 1.69 | 0.65 | 16.960 | 20.458 | 0 | 3.1 | |
| 12 | 89.70 | 1.69 | 0.65 | 13.195 | 20.458 | 0 | 4.8 | |
| 13 | 91.35 | 1.34 | 0.65 | 9.486 | 20.458 | 0 | 6.1 | |
| 14 | 105.72 | 0.00 | 0.65 | 5.818 | 20.458 | 0 | 6.9 | |
| 15 | 38.77 | 0.00 | 0.65 | 2.173 | 20.458 | 0 | 7.4 | |
| 16 | 28.25 | 0.00 | 0.65 | -1.462 | 20.458 | 0 | 7.4 | |
| 17 | 27.47 | 0.00 | 0.65 | -5.104 | 20.458 | 0 | 7.1 | |
| 18 | 26.49 | 0.00 | 0.65 | -8.767 | 20.458 | 0 | 6.3 | |
| 19 | 24.98 | 0.00 | 0.65 | -12.466 | 20.458 | 0 | 5.1 | |
| 20 | 22.92 | 0.00 | 0.65 | -16.219 | 20.458 | 0 | 3.5 | |
| 21 | 20.28 | 0.00 | 0.65 | -20.045 | 20.458 | 0 | 1.4 | |
| 22 | 17.02 | 0.00 | 0.65 | -23.968 | 20.458 | 0 | 0.0 | |
| 23 | 13.08 | 0.00 | 0.65 | -28.014 | 20.458 | 0 | 0.0 | |
| 24 | 8.41 | 0.00 | 0.65 | -32.220 | 20.458 | 0 | 0.0 | |
| 25 | 2.87 | 0.00 | -7.45 - 0.65 | -36.078 | 20.458 | 0 | 0.0 | |

Combinazione n° 5 - GEO (A2-M2-R2) H + V

| n° | W [kN] | Qy [kN] | b [m] | α [°] | φ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|----------|----------|------------|------------|----------------|
| 1 | 9.90 | 3.91 | 8.83 - 0.65 | 67.871 | 35.000 | 0 | 0.0 | |
| 2 | 26.71 | 3.91 | 0.65 | 59.765 | 35.000 | 0 | 0.0 | |
| 3 | 38.99 | 3.91 | 0.65 | 53.126 | 35.000 | 0 | 0.0 | |
| 4 | 48.74 | 3.91 | 0.65 | 47.412 | 35.000 | 0 | 0.0 | |
| 5 | 56.78 | 3.91 | 0.65 | 42.271 | 35.000 | 0 | 0.0 | |
| 6 | 63.53 | 3.91 | 0.65 | 37.524 | 35.000 | 0 | 0.0 | |
| 7 | 69.24 | 3.91 | 0.65 | 33.065 | 35.000 | 0 | 0.0 | |
| 8 | 76.45 | 3.59 | 0.65 | 28.823 | 25.000 | 0 | 0.0 | |
| 9 | 81.38 | 1.30 | 0.65 | 24.748 | 25.000 | 0 | 0.0 | |
| 10 | 84.77 | 1.30 | 0.65 | 20.804 | 25.000 | 0 | 0.9 | |
| 11 | 87.53 | 1.30 | 0.65 | 16.960 | 25.000 | 0 | 3.1 | |
| 12 | 89.70 | 1.30 | 0.65 | 13.195 | 25.000 | 0 | 4.8 | |
| 13 | 91.35 | 1.03 | 0.65 | 9.486 | 25.000 | 0 | 6.1 | |
| 14 | 105.72 | 0.00 | 0.65 | 5.818 | 25.000 | 0 | 6.9 | |
| 15 | 38.77 | 0.00 | 0.65 | 2.173 | 25.000 | 0 | 7.4 | |
| 16 | 28.25 | 0.00 | 0.65 | -1.462 | 25.000 | 0 | 7.4 | |
| 17 | 27.47 | 0.00 | 0.65 | -5.104 | 25.000 | 0 | 7.1 | |
| 18 | 26.49 | 0.00 | 0.65 | -8.767 | 25.000 | 0 | 6.3 | |
| 19 | 24.98 | 0.00 | 0.65 | -12.466 | 25.000 | 0 | 5.1 | |
| 20 | 22.92 | 0.00 | 0.65 | -16.219 | 25.000 | 0 | 3.5 | |
| 21 | 20.28 | 0.00 | 0.65 | -20.045 | 25.000 | 0 | 1.4 | |
| 22 | 17.02 | 0.00 | 0.65 | -23.968 | 25.000 | 0 | 0.0 | |
| 23 | 13.08 | 0.00 | 0.65 | -28.014 | 25.000 | 0 | 0.0 | |
| 24 | 8.41 | 0.00 | 0.65 | -32.220 | 25.000 | 0 | 0.0 | |
| 25 | 2.87 | 0.00 | -7.45 - 0.65 | -36.078 | 25.000 | 0 | 0.0 | |

Combinazione n° 6 - GEO (A2-M2-R2) H - V

| n° | W [kN] | Qy [kN] | b [m] | α [°] | φ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|----------|----------|----------|------------|------------|----------------|
|----|-----------|------------|----------|----------|----------|------------|------------|----------------|

| n° | W [kN] | Qy [kN] | b [m] | α [°] | ϕ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|-----------------|---------------|------------|------------|----------------|
| 1 | 9.90 | 3.91 | 8.83 - 0.65 | 67.871 | 35.000 | 0 | 0.0 | |
| 2 | 26.71 | 3.91 | 0.65 | 59.765 | 35.000 | 0 | 0.0 | |
| 3 | 38.99 | 3.91 | 0.65 | 53.126 | 35.000 | 0 | 0.0 | |
| 4 | 48.74 | 3.91 | 0.65 | 47.412 | 35.000 | 0 | 0.0 | |
| 5 | 56.78 | 3.91 | 0.65 | 42.271 | 35.000 | 0 | 0.0 | |
| 6 | 63.53 | 3.91 | 0.65 | 37.524 | 35.000 | 0 | 0.0 | |
| 7 | 69.24 | 3.91 | 0.65 | 33.065 | 35.000 | 0 | 0.0 | |
| 8 | 76.45 | 3.59 | 0.65 | 28.823 | 25.000 | 0 | 0.0 | |
| 9 | 81.38 | 1.30 | 0.65 | 24.748 | 25.000 | 0 | 0.0 | |
| 10 | 84.77 | 1.30 | 0.65 | 20.804 | 25.000 | 0 | 0.9 | |
| 11 | 87.53 | 1.30 | 0.65 | 16.960 | 25.000 | 0 | 3.1 | |
| 12 | 89.70 | 1.30 | 0.65 | 13.195 | 25.000 | 0 | 4.8 | |
| 13 | 91.35 | 1.03 | 0.65 | 9.486 | 25.000 | 0 | 6.1 | |
| 14 | 105.72 | 0.00 | 0.65 | 5.818 | 25.000 | 0 | 6.9 | |
| 15 | 38.77 | 0.00 | 0.65 | 2.173 | 25.000 | 0 | 7.4 | |
| 16 | 28.25 | 0.00 | 0.65 | -1.462 | 25.000 | 0 | 7.4 | |
| 17 | 27.47 | 0.00 | 0.65 | -5.104 | 25.000 | 0 | 7.1 | |
| 18 | 26.49 | 0.00 | 0.65 | -8.767 | 25.000 | 0 | 6.3 | |
| 19 | 24.98 | 0.00 | 0.65 | -12.466 | 25.000 | 0 | 5.1 | |
| 20 | 22.92 | 0.00 | 0.65 | -16.219 | 25.000 | 0 | 3.5 | |
| 21 | 20.28 | 0.00 | 0.65 | -20.045 | 25.000 | 0 | 1.4 | |
| 22 | 17.02 | 0.00 | 0.65 | -23.968 | 25.000 | 0 | 0.0 | |
| 23 | 13.08 | 0.00 | 0.65 | -28.014 | 25.000 | 0 | 0.0 | |
| 24 | 8.41 | 0.00 | 0.65 | -32.220 | 25.000 | 0 | 0.0 | |
| 25 | 2.87 | 0.00 | -7.45 - 0.65 | -36.078 | 25.000 | 0 | 0.0 | |

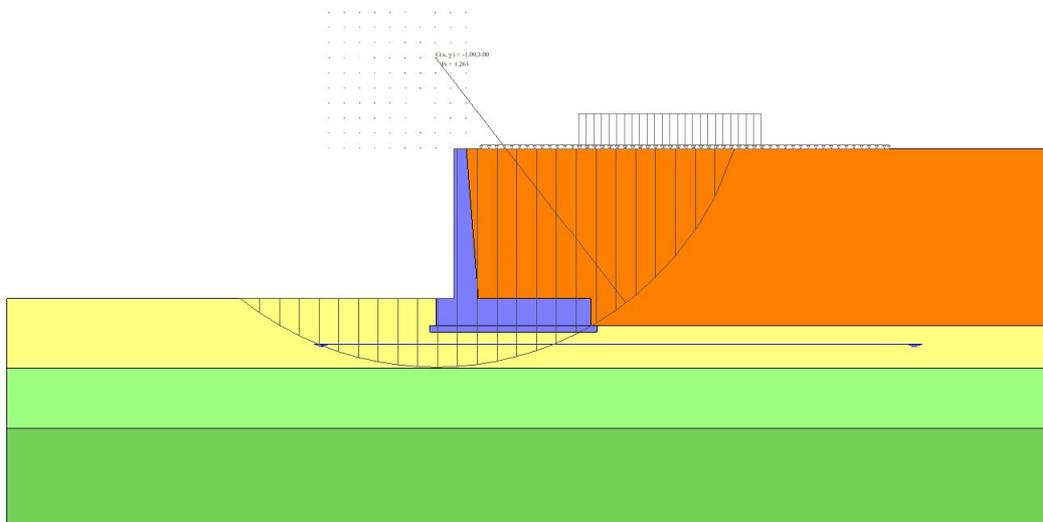


Fig. 7 - Stabilità fronte di scavo - Cerchio critico (Combinazione n° 4)

Spostamenti

Simbologia adottata

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 168 di 314 |

Cmb Tipo combinazione
 $a_{g,crit}$ accelerazione critica, espressa in $[m/s^2]$
Dmax Spostamento orizzontale massimo, espressa in [cm]

| Cmb | $a_{g,crit}$ [m/s^2] | Dmax [cm] |
|-----------------|-----------------------------|--------------|
| 13 - SLEQ H + V | 1.7818 | 0.0014 |

Sollecitazioni

Elementi calcolati a trave

Simbologia adottata

N Sforzo normale, espresso in [kN]. Positivo se di compressione.
T Taglio, espresso in [kN]. Positivo se diretto da monte verso valle
M Momento, espresso in [kNm]. Positivo se tende le fibre contro terra (a monte)

Paramento

Combinazione n° 1 - STR (A1-M1-R3)

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.04 | 0.00 |
| 3 | -0.20 | 2.00 | 0.15 | 0.02 |
| 4 | -0.30 | 3.03 | 0.34 | 0.05 |
| 5 | -0.40 | 4.08 | 0.60 | 0.11 |
| 6 | -0.50 | 5.15 | 0.93 | 0.21 |
| 7 | -0.60 | 6.24 | 1.34 | 0.34 |
| 8 | -0.70 | 7.34 | 1.83 | 0.53 |
| 9 | -0.80 | 8.47 | 2.41 | 0.77 |
| 10 | -0.90 | 9.62 | 3.09 | 1.08 |
| 11 | -1.00 | 10.78 | 3.86 | 1.47 |
| 12 | -1.10 | 11.97 | 4.72 | 1.94 |
| 13 | -1.20 | 13.17 | 5.65 | 2.51 |
| 14 | -1.30 | 14.40 | 6.67 | 3.18 |
| 15 | -1.40 | 15.64 | 7.75 | 3.96 |
| 16 | -1.50 | 16.91 | 8.91 | 4.86 |
| 17 | -1.60 | 18.19 | 10.15 | 5.88 |
| 18 | -1.70 | 19.49 | 11.46 | 7.03 |
| 19 | -1.80 | 20.81 | 12.85 | 8.33 |
| 20 | -1.90 | 22.15 | 14.31 | 9.77 |
| 21 | -2.00 | 23.52 | 15.84 | 11.37 |
| 22 | -2.10 | 24.90 | 17.45 | 13.13 |
| 23 | -2.20 | 26.30 | 19.14 | 15.06 |
| 24 | -2.30 | 27.72 | 20.90 | 17.17 |
| 25 | -2.40 | 29.16 | 22.73 | 19.46 |
| 26 | -2.50 | 30.61 | 24.64 | 21.95 |
| 27 | -2.60 | 32.09 | 26.62 | 24.64 |
| 28 | -2.70 | 33.59 | 28.67 | 27.53 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 29 | -2.80 | 35.11 | 30.80 | 30.64 |
| 30 | -2.90 | 36.64 | 33.01 | 33.97 |
| 31 | -3.00 | 38.20 | 35.29 | 37.54 |
| 32 | -3.10 | 39.78 | 37.64 | 41.34 |
| 33 | -3.20 | 41.37 | 40.06 | 45.38 |
| 34 | -3.30 | 42.99 | 42.57 | 49.68 |
| 35 | -3.40 | 44.62 | 45.14 | 54.24 |
| 36 | -3.50 | 46.27 | 47.79 | 59.07 |
| 37 | -3.60 | 47.95 | 50.51 | 64.17 |
| 38 | -3.70 | 49.64 | 53.31 | 69.55 |
| 39 | -3.80 | 51.35 | 56.18 | 75.23 |
| 40 | -3.90 | 53.08 | 59.13 | 81.20 |
| 41 | -4.00 | 54.84 | 62.15 | 87.48 |
| 42 | -4.10 | 56.61 | 65.25 | 94.07 |
| 43 | -4.20 | 58.40 | 68.42 | 100.98 |
| 44 | -4.30 | 60.21 | 71.66 | 108.22 |
| 45 | -4.40 | 62.04 | 74.98 | 115.80 |
| 46 | -4.50 | 63.89 | 78.37 | 123.71 |
| 47 | -4.60 | 65.75 | 81.83 | 131.98 |
| 48 | -4.70 | 67.64 | 85.37 | 140.61 |
| 49 | -4.80 | 69.55 | 88.99 | 149.60 |
| 50 | -4.90 | 71.48 | 92.68 | 158.96 |
| 51 | -5.00 | 73.42 | 96.44 | 168.70 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.17 | 0.01 |
| 3 | -0.20 | 2.00 | 0.41 | 0.04 |
| 4 | -0.30 | 3.03 | 0.74 | 0.11 |
| 5 | -0.40 | 4.08 | 1.14 | 0.22 |
| 6 | -0.50 | 5.15 | 1.62 | 0.37 |
| 7 | -0.60 | 6.24 | 2.18 | 0.59 |
| 8 | -0.70 | 7.34 | 2.82 | 0.86 |
| 9 | -0.80 | 8.47 | 3.56 | 1.21 |
| 10 | -0.90 | 9.62 | 4.38 | 1.64 |
| 11 | -1.00 | 10.78 | 5.30 | 2.17 |
| 12 | -1.10 | 11.97 | 6.30 | 2.79 |
| 13 | -1.20 | 13.17 | 7.38 | 3.52 |
| 14 | -1.30 | 14.40 | 8.55 | 4.38 |
| 15 | -1.40 | 15.64 | 9.79 | 5.35 |
| 16 | -1.50 | 16.91 | 11.11 | 6.46 |
| 17 | -1.60 | 18.19 | 12.52 | 7.71 |
| 18 | -1.70 | 19.49 | 14.00 | 9.11 |
| 19 | -1.80 | 20.81 | 15.56 | 10.67 |
| 20 | -1.90 | 22.15 | 17.19 | 12.39 |
| 21 | -2.00 | 23.52 | 18.91 | 14.29 |
| 22 | -2.10 | 24.90 | 20.71 | 16.36 |
| 23 | -2.20 | 26.30 | 22.58 | 18.63 |
| 24 | -2.30 | 27.72 | 24.53 | 21.09 |
| 25 | -2.40 | 29.16 | 26.56 | 23.76 |
| 26 | -2.50 | 30.61 | 28.67 | 26.64 |
| 27 | -2.60 | 32.09 | 30.86 | 29.74 |
| 28 | -2.70 | 33.59 | 33.13 | 33.07 |
| 29 | -2.80 | 35.11 | 35.48 | 36.64 |
| 30 | -2.90 | 36.64 | 37.90 | 40.45 |
| 31 | -3.00 | 38.20 | 40.40 | 44.51 |
| 32 | -3.10 | 39.78 | 42.98 | 48.83 |
| 33 | -3.20 | 41.37 | 45.64 | 53.43 |
| 34 | -3.30 | 42.99 | 48.38 | 58.29 |
| 35 | -3.40 | 44.62 | 51.20 | 63.45 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 36 | -3.50 | 46.27 | 54.09 | 68.89 |
| 37 | -3.60 | 47.95 | 57.06 | 74.64 |
| 38 | -3.70 | 49.64 | 60.12 | 80.69 |
| 39 | -3.80 | 51.35 | 63.25 | 87.06 |
| 40 | -3.90 | 53.08 | 66.46 | 93.75 |
| 41 | -4.00 | 54.84 | 69.74 | 100.77 |
| 42 | -4.10 | 56.61 | 73.11 | 108.14 |
| 43 | -4.20 | 58.40 | 76.55 | 115.85 |
| 44 | -4.30 | 60.21 | 80.08 | 123.91 |
| 45 | -4.40 | 62.04 | 83.68 | 132.34 |
| 46 | -4.50 | 63.89 | 87.36 | 141.15 |
| 47 | -4.60 | 65.75 | 91.12 | 150.33 |
| 48 | -4.70 | 67.64 | 94.95 | 159.90 |
| 49 | -4.80 | 69.55 | 98.87 | 169.86 |
| 50 | -4.90 | 71.48 | 102.86 | 180.23 |
| 51 | -5.00 | 73.42 | 106.93 | 191.00 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.16 | 0.01 |
| 3 | -0.20 | 2.00 | 0.40 | 0.04 |
| 4 | -0.30 | 3.03 | 0.70 | 0.11 |
| 5 | -0.40 | 4.08 | 1.08 | 0.21 |
| 6 | -0.50 | 5.15 | 1.53 | 0.36 |
| 7 | -0.60 | 6.24 | 2.05 | 0.56 |
| 8 | -0.70 | 7.34 | 2.64 | 0.82 |
| 9 | -0.80 | 8.47 | 3.32 | 1.15 |
| 10 | -0.90 | 9.62 | 4.08 | 1.55 |
| 11 | -1.00 | 10.78 | 4.92 | 2.04 |
| 12 | -1.10 | 11.97 | 5.85 | 2.63 |
| 13 | -1.20 | 13.17 | 6.85 | 3.31 |
| 14 | -1.30 | 14.40 | 7.92 | 4.10 |
| 15 | -1.40 | 15.64 | 9.06 | 5.01 |
| 16 | -1.50 | 16.91 | 10.28 | 6.04 |
| 17 | -1.60 | 18.19 | 11.56 | 7.20 |
| 18 | -1.70 | 19.49 | 12.92 | 8.50 |
| 19 | -1.80 | 20.81 | 14.35 | 9.94 |
| 20 | -1.90 | 22.15 | 15.85 | 11.54 |
| 21 | -2.00 | 23.52 | 17.42 | 13.29 |
| 22 | -2.10 | 24.90 | 19.06 | 15.21 |
| 23 | -2.20 | 26.30 | 20.78 | 17.31 |
| 24 | -2.30 | 27.72 | 22.56 | 19.58 |
| 25 | -2.40 | 29.16 | 24.42 | 22.04 |
| 26 | -2.50 | 30.61 | 26.35 | 24.70 |
| 27 | -2.60 | 32.09 | 28.34 | 27.56 |
| 28 | -2.70 | 33.59 | 30.41 | 30.63 |
| 29 | -2.80 | 35.11 | 32.55 | 33.91 |
| 30 | -2.90 | 36.64 | 34.77 | 37.42 |
| 31 | -3.00 | 38.20 | 37.05 | 41.16 |
| 32 | -3.10 | 39.78 | 39.40 | 45.13 |
| 33 | -3.20 | 41.37 | 41.83 | 49.36 |
| 34 | -3.30 | 42.99 | 44.32 | 53.83 |
| 35 | -3.40 | 44.62 | 46.89 | 58.57 |
| 36 | -3.50 | 46.27 | 49.53 | 63.57 |
| 37 | -3.60 | 47.95 | 52.24 | 68.84 |
| 38 | -3.70 | 49.64 | 55.02 | 74.40 |
| 39 | -3.80 | 51.35 | 57.87 | 80.24 |
| 40 | -3.90 | 53.08 | 60.79 | 86.38 |
| 41 | -4.00 | 54.84 | 63.78 | 92.83 |
| 42 | -4.10 | 56.61 | 66.85 | 99.58 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 43 | -4.20 | 58.40 | 69.98 | 106.65 |
| 44 | -4.30 | 60.21 | 73.19 | 114.04 |
| 45 | -4.40 | 62.04 | 76.47 | 121.77 |
| 46 | -4.50 | 63.89 | 79.81 | 129.83 |
| 47 | -4.60 | 65.75 | 83.23 | 138.24 |
| 48 | -4.70 | 67.64 | 86.72 | 147.00 |
| 49 | -4.80 | 69.55 | 90.29 | 156.13 |
| 50 | -4.90 | 71.48 | 93.92 | 165.62 |
| 51 | -5.00 | 73.42 | 97.62 | 175.48 |

Combinazione n° 10 - SLER

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.03 | 0.00 |
| 3 | -0.20 | 2.00 | 0.12 | 0.02 |
| 4 | -0.30 | 3.03 | 0.26 | 0.04 |
| 5 | -0.40 | 4.08 | 0.46 | 0.09 |
| 6 | -0.50 | 5.15 | 0.72 | 0.17 |
| 7 | -0.60 | 6.24 | 1.03 | 0.28 |
| 8 | -0.70 | 7.34 | 1.41 | 0.43 |
| 9 | -0.80 | 8.47 | 1.85 | 0.62 |
| 10 | -0.90 | 9.62 | 2.37 | 0.87 |
| 11 | -1.00 | 10.78 | 2.95 | 1.17 |
| 12 | -1.10 | 11.97 | 3.60 | 1.55 |
| 13 | -1.20 | 13.17 | 4.31 | 1.99 |
| 14 | -1.30 | 14.40 | 5.08 | 2.52 |
| 15 | -1.40 | 15.64 | 5.91 | 3.13 |
| 16 | -1.50 | 16.91 | 6.80 | 3.82 |
| 17 | -1.60 | 18.19 | 7.74 | 4.62 |
| 18 | -1.70 | 19.49 | 8.74 | 5.52 |
| 19 | -1.80 | 20.81 | 9.80 | 6.53 |
| 20 | -1.90 | 22.15 | 10.91 | 7.65 |
| 21 | -2.00 | 23.52 | 12.08 | 8.89 |
| 22 | -2.10 | 24.90 | 13.31 | 10.25 |
| 23 | -2.20 | 26.30 | 14.60 | 11.75 |
| 24 | -2.30 | 27.72 | 15.94 | 13.38 |
| 25 | -2.40 | 29.16 | 17.34 | 15.16 |
| 26 | -2.50 | 30.61 | 18.80 | 17.09 |
| 27 | -2.60 | 32.09 | 20.32 | 19.17 |
| 28 | -2.70 | 33.59 | 21.89 | 21.41 |
| 29 | -2.80 | 35.11 | 23.52 | 23.81 |
| 30 | -2.90 | 36.64 | 25.20 | 26.39 |
| 31 | -3.00 | 38.20 | 26.95 | 29.15 |
| 32 | -3.10 | 39.78 | 28.75 | 32.09 |
| 33 | -3.20 | 41.37 | 30.61 | 35.22 |
| 34 | -3.30 | 42.99 | 32.52 | 38.54 |
| 35 | -3.40 | 44.62 | 34.49 | 42.06 |
| 36 | -3.50 | 46.27 | 36.52 | 45.79 |
| 37 | -3.60 | 47.95 | 38.61 | 49.74 |
| 38 | -3.70 | 49.64 | 40.75 | 53.90 |
| 39 | -3.80 | 51.35 | 42.95 | 58.29 |
| 40 | -3.90 | 53.08 | 45.21 | 62.90 |
| 41 | -4.00 | 54.84 | 47.52 | 67.75 |
| 42 | -4.10 | 56.61 | 49.89 | 72.84 |
| 43 | -4.20 | 58.40 | 52.32 | 78.18 |
| 44 | -4.30 | 60.21 | 54.81 | 83.77 |
| 45 | -4.40 | 62.04 | 57.35 | 89.62 |
| 46 | -4.50 | 63.89 | 59.95 | 95.74 |
| 47 | -4.60 | 65.75 | 62.61 | 102.13 |
| 48 | -4.70 | 67.64 | 65.32 | 108.79 |
| 49 | -4.80 | 69.55 | 68.09 | 115.73 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 50 | -4.90 | 71.48 | 70.92 | 122.96 |
| 51 | -5.00 | 73.42 | 73.80 | 130.48 |

Combinazione n° 11 - SLEF

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.03 | 0.00 |
| 3 | -0.20 | 2.00 | 0.12 | 0.02 |
| 4 | -0.30 | 3.03 | 0.26 | 0.04 |
| 5 | -0.40 | 4.08 | 0.46 | 0.09 |
| 6 | -0.50 | 5.15 | 0.72 | 0.17 |
| 7 | -0.60 | 6.24 | 1.03 | 0.28 |
| 8 | -0.70 | 7.34 | 1.41 | 0.43 |
| 9 | -0.80 | 8.47 | 1.85 | 0.62 |
| 10 | -0.90 | 9.62 | 2.37 | 0.87 |
| 11 | -1.00 | 10.78 | 2.95 | 1.17 |
| 12 | -1.10 | 11.97 | 3.60 | 1.55 |
| 13 | -1.20 | 13.17 | 4.31 | 1.99 |
| 14 | -1.30 | 14.40 | 5.08 | 2.52 |
| 15 | -1.40 | 15.64 | 5.91 | 3.13 |
| 16 | -1.50 | 16.91 | 6.80 | 3.82 |
| 17 | -1.60 | 18.19 | 7.74 | 4.62 |
| 18 | -1.70 | 19.49 | 8.74 | 5.52 |
| 19 | -1.80 | 20.81 | 9.80 | 6.53 |
| 20 | -1.90 | 22.15 | 10.91 | 7.65 |
| 21 | -2.00 | 23.52 | 12.08 | 8.89 |
| 22 | -2.10 | 24.90 | 13.31 | 10.25 |
| 23 | -2.20 | 26.30 | 14.60 | 11.75 |
| 24 | -2.30 | 27.72 | 15.94 | 13.38 |
| 25 | -2.40 | 29.16 | 17.34 | 15.16 |
| 26 | -2.50 | 30.61 | 18.80 | 17.09 |
| 27 | -2.60 | 32.09 | 20.32 | 19.17 |
| 28 | -2.70 | 33.59 | 21.89 | 21.41 |
| 29 | -2.80 | 35.11 | 23.52 | 23.81 |
| 30 | -2.90 | 36.64 | 25.20 | 26.39 |
| 31 | -3.00 | 38.20 | 26.95 | 29.15 |
| 32 | -3.10 | 39.78 | 28.75 | 32.09 |
| 33 | -3.20 | 41.37 | 30.61 | 35.22 |
| 34 | -3.30 | 42.99 | 32.52 | 38.54 |
| 35 | -3.40 | 44.62 | 34.49 | 42.06 |
| 36 | -3.50 | 46.27 | 36.52 | 45.79 |
| 37 | -3.60 | 47.95 | 38.61 | 49.74 |
| 38 | -3.70 | 49.64 | 40.75 | 53.90 |
| 39 | -3.80 | 51.35 | 42.95 | 58.29 |
| 40 | -3.90 | 53.08 | 45.21 | 62.90 |
| 41 | -4.00 | 54.84 | 47.52 | 67.75 |
| 42 | -4.10 | 56.61 | 49.89 | 72.84 |
| 43 | -4.20 | 58.40 | 52.32 | 78.18 |
| 44 | -4.30 | 60.21 | 54.81 | 83.77 |
| 45 | -4.40 | 62.04 | 57.35 | 89.62 |
| 46 | -4.50 | 63.89 | 59.95 | 95.74 |
| 47 | -4.60 | 65.75 | 62.61 | 102.13 |
| 48 | -4.70 | 67.64 | 65.32 | 108.79 |
| 49 | -4.80 | 69.55 | 68.09 | 115.73 |
| 50 | -4.90 | 71.48 | 70.92 | 122.96 |
| 51 | -5.00 | 73.42 | 73.80 | 130.48 |

Combinazione n° 12 - SLEQ

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.03 | 0.00 |
| 3 | -0.20 | 2.00 | 0.12 | 0.02 |
| 4 | -0.30 | 3.03 | 0.26 | 0.04 |
| 5 | -0.40 | 4.08 | 0.46 | 0.09 |
| 6 | -0.50 | 5.15 | 0.72 | 0.17 |
| 7 | -0.60 | 6.24 | 1.03 | 0.28 |
| 8 | -0.70 | 7.34 | 1.41 | 0.43 |
| 9 | -0.80 | 8.47 | 1.85 | 0.62 |
| 10 | -0.90 | 9.62 | 2.37 | 0.87 |
| 11 | -1.00 | 10.78 | 2.95 | 1.17 |
| 12 | -1.10 | 11.97 | 3.60 | 1.55 |
| 13 | -1.20 | 13.17 | 4.31 | 1.99 |
| 14 | -1.30 | 14.40 | 5.08 | 2.52 |
| 15 | -1.40 | 15.64 | 5.91 | 3.13 |
| 16 | -1.50 | 16.91 | 6.80 | 3.82 |
| 17 | -1.60 | 18.19 | 7.74 | 4.62 |
| 18 | -1.70 | 19.49 | 8.74 | 5.52 |
| 19 | -1.80 | 20.81 | 9.80 | 6.53 |
| 20 | -1.90 | 22.15 | 10.91 | 7.65 |
| 21 | -2.00 | 23.52 | 12.08 | 8.89 |
| 22 | -2.10 | 24.90 | 13.31 | 10.25 |
| 23 | -2.20 | 26.30 | 14.60 | 11.75 |
| 24 | -2.30 | 27.72 | 15.94 | 13.38 |
| 25 | -2.40 | 29.16 | 17.34 | 15.16 |
| 26 | -2.50 | 30.61 | 18.80 | 17.09 |
| 27 | -2.60 | 32.09 | 20.32 | 19.17 |
| 28 | -2.70 | 33.59 | 21.89 | 21.41 |
| 29 | -2.80 | 35.11 | 23.52 | 23.81 |
| 30 | -2.90 | 36.64 | 25.20 | 26.39 |
| 31 | -3.00 | 38.20 | 26.95 | 29.15 |
| 32 | -3.10 | 39.78 | 28.75 | 32.09 |
| 33 | -3.20 | 41.37 | 30.61 | 35.22 |
| 34 | -3.30 | 42.99 | 32.52 | 38.54 |
| 35 | -3.40 | 44.62 | 34.49 | 42.06 |
| 36 | -3.50 | 46.27 | 36.52 | 45.79 |
| 37 | -3.60 | 47.95 | 38.61 | 49.74 |
| 38 | -3.70 | 49.64 | 40.75 | 53.90 |
| 39 | -3.80 | 51.35 | 42.95 | 58.29 |
| 40 | -3.90 | 53.08 | 45.21 | 62.90 |
| 41 | -4.00 | 54.84 | 47.52 | 67.75 |
| 42 | -4.10 | 56.61 | 49.89 | 72.84 |
| 43 | -4.20 | 58.40 | 52.32 | 78.18 |
| 44 | -4.30 | 60.21 | 54.81 | 83.77 |
| 45 | -4.40 | 62.04 | 57.35 | 89.62 |
| 46 | -4.50 | 63.89 | 59.95 | 95.74 |
| 47 | -4.60 | 65.75 | 62.61 | 102.13 |
| 48 | -4.70 | 67.64 | 65.32 | 108.79 |
| 49 | -4.80 | 69.55 | 68.09 | 115.73 |
| 50 | -4.90 | 71.48 | 70.92 | 122.96 |
| 51 | -5.00 | 73.42 | 73.80 | 130.48 |

Combinazione n° 13 - SLEQ H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.11 | 0.01 |
| 3 | -0.20 | 2.00 | 0.29 | 0.03 |
| 4 | -0.30 | 3.03 | 0.54 | 0.08 |
| 5 | -0.40 | 4.08 | 0.85 | 0.17 |
| 6 | -0.50 | 5.15 | 1.24 | 0.29 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 7 | -0.60 | 6.24 | 1.69 | 0.46 |
| 8 | -0.70 | 7.34 | 2.22 | 0.68 |
| 9 | -0.80 | 8.47 | 2.83 | 0.96 |
| 10 | -0.90 | 9.62 | 3.52 | 1.32 |
| 11 | -1.00 | 10.78 | 4.30 | 1.75 |
| 12 | -1.10 | 11.97 | 5.15 | 2.26 |
| 13 | -1.20 | 13.17 | 6.08 | 2.87 |
| 14 | -1.30 | 14.40 | 7.07 | 3.59 |
| 15 | -1.40 | 15.64 | 8.14 | 4.41 |
| 16 | -1.50 | 16.91 | 9.27 | 5.34 |
| 17 | -1.60 | 18.19 | 10.47 | 6.40 |
| 18 | -1.70 | 19.49 | 11.75 | 7.58 |
| 19 | -1.80 | 20.81 | 13.09 | 8.90 |
| 20 | -1.90 | 22.15 | 14.50 | 10.37 |
| 21 | -2.00 | 23.52 | 15.99 | 11.98 |
| 22 | -2.10 | 24.90 | 17.54 | 13.75 |
| 23 | -2.20 | 26.30 | 19.16 | 15.69 |
| 24 | -2.30 | 27.72 | 20.85 | 17.80 |
| 25 | -2.40 | 29.16 | 22.61 | 20.08 |
| 26 | -2.50 | 30.61 | 24.44 | 22.55 |
| 27 | -2.60 | 32.09 | 26.33 | 25.22 |
| 28 | -2.70 | 33.59 | 28.30 | 28.08 |
| 29 | -2.80 | 35.11 | 30.34 | 31.15 |
| 30 | -2.90 | 36.64 | 32.44 | 34.43 |
| 31 | -3.00 | 38.20 | 34.62 | 37.93 |
| 32 | -3.10 | 39.78 | 36.86 | 41.66 |
| 33 | -3.20 | 41.37 | 39.17 | 45.62 |
| 34 | -3.30 | 42.99 | 41.56 | 49.82 |
| 35 | -3.40 | 44.62 | 44.01 | 54.28 |
| 36 | -3.50 | 46.27 | 46.53 | 58.98 |
| 37 | -3.60 | 47.95 | 49.12 | 63.95 |
| 38 | -3.70 | 49.64 | 51.78 | 69.19 |
| 39 | -3.80 | 51.35 | 54.50 | 74.70 |
| 40 | -3.90 | 53.08 | 57.30 | 80.50 |
| 41 | -4.00 | 54.84 | 60.17 | 86.59 |
| 42 | -4.10 | 56.61 | 63.10 | 92.97 |
| 43 | -4.20 | 58.40 | 66.11 | 99.66 |
| 44 | -4.30 | 60.21 | 69.18 | 106.66 |
| 45 | -4.40 | 62.04 | 72.33 | 113.98 |
| 46 | -4.50 | 63.89 | 75.54 | 121.62 |
| 47 | -4.60 | 65.75 | 78.82 | 129.60 |
| 48 | -4.70 | 67.64 | 82.17 | 137.91 |
| 49 | -4.80 | 69.55 | 85.59 | 146.57 |
| 50 | -4.90 | 71.48 | 89.08 | 155.59 |
| 51 | -5.00 | 73.42 | 92.64 | 164.96 |

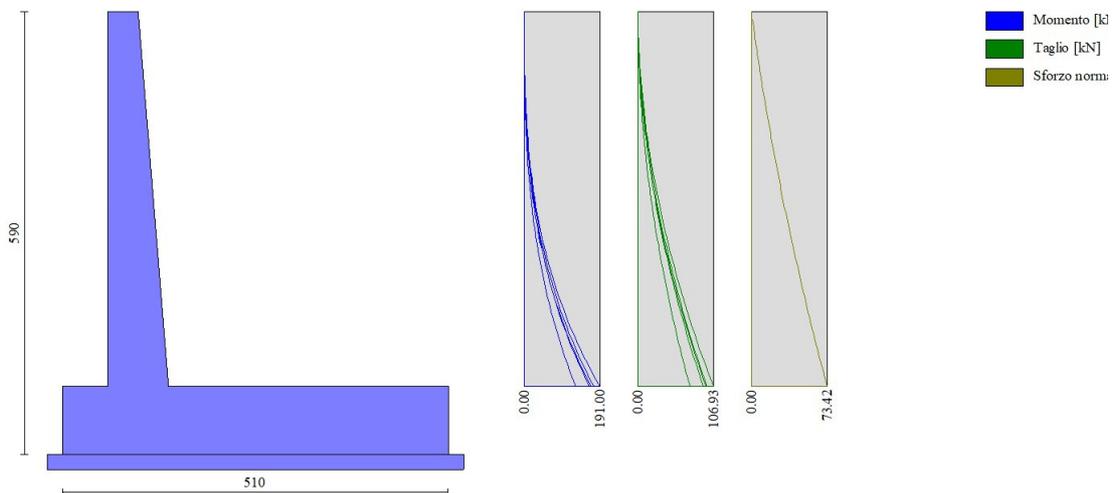


Fig. 8 - Paramento (Inviluppo)

Fondazione

Combinazione n° 1 - STR (A1-M1-R3)

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 14.89 | 0.75 |
| 3 | -0.80 | 0.00 | 29.55 | 2.97 |
| 4 | -0.70 | 0.00 | 43.97 | 6.65 |
| 5 | -0.60 | 0.00 | 58.17 | 11.76 |
| 6 | -0.50 | 0.00 | 72.13 | 18.27 |
| 7 | -0.40 | 0.00 | 85.87 | 26.18 |
| 8 | 0.40 | 0.00 | -200.34 | -467.91 |
| 9 | 0.50 | 0.00 | -199.65 | -448.99 |
| 10 | 0.60 | 0.00 | -198.45 | -429.63 |
| 11 | 0.70 | 0.00 | -197.00 | -410.39 |
| 12 | 0.80 | 0.00 | -195.33 | -391.31 |
| 13 | 0.90 | 0.00 | -193.42 | -372.41 |
| 14 | 1.00 | 0.00 | -191.28 | -353.71 |
| 15 | 1.10 | 0.00 | -188.92 | -335.23 |
| 16 | 1.20 | 0.00 | -186.32 | -317.01 |
| 17 | 1.30 | 0.00 | -183.49 | -299.05 |
| 18 | 1.40 | 0.00 | -180.43 | -281.39 |
| 19 | 1.50 | 0.00 | -177.15 | -264.05 |
| 20 | 1.60 | 0.00 | -173.63 | -247.04 |
| 21 | 1.70 | 0.00 | -169.88 | -230.40 |
| 22 | 1.80 | 0.00 | -165.90 | -214.15 |
| 23 | 1.90 | 0.00 | -161.69 | -198.31 |
| 24 | 2.00 | 0.00 | -157.24 | -182.89 |
| 25 | 2.10 | 0.00 | -152.57 | -167.94 |
| 26 | 2.20 | 0.00 | -147.67 | -153.46 |
| 27 | 2.30 | 0.00 | -142.54 | -139.49 |
| 28 | 2.40 | 0.00 | -137.18 | -126.04 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 29 | 2.50 | 0.00 | -131.58 | -113.13 |
| 30 | 2.60 | 0.00 | -125.76 | -100.80 |
| 31 | 2.70 | 0.00 | -119.70 | -89.06 |
| 32 | 2.80 | 0.00 | -113.42 | -77.94 |
| 33 | 2.90 | 0.00 | -106.90 | -67.46 |
| 34 | 3.00 | 0.00 | -100.16 | -57.64 |
| 35 | 3.10 | 0.00 | -93.18 | -48.51 |
| 36 | 3.20 | 0.00 | -85.98 | -40.09 |
| 37 | 3.30 | 0.00 | -78.54 | -32.40 |
| 38 | 3.40 | 0.00 | -70.87 | -25.46 |
| 39 | 3.50 | 0.00 | -62.97 | -19.31 |
| 40 | 3.60 | 0.00 | -54.84 | -13.95 |
| 41 | 3.70 | 0.00 | -46.48 | -9.42 |
| 42 | 3.80 | 0.00 | -35.25 | -5.34 |
| 43 | 3.90 | 0.00 | -23.73 | -2.39 |
| 44 | 4.00 | 0.00 | -11.98 | -0.60 |
| 45 | 4.10 | 0.00 | 0.00 | 0.00 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 17.81 | 0.89 |
| 3 | -0.80 | 0.00 | 35.29 | 3.55 |
| 4 | -0.70 | 0.00 | 52.44 | 7.94 |
| 5 | -0.60 | 0.00 | 69.26 | 14.03 |
| 6 | -0.50 | 0.00 | 85.75 | 21.78 |
| 7 | -0.40 | 0.00 | 101.92 | 31.17 |
| 8 | 0.40 | 0.00 | -90.15 | -305.46 |
| 9 | 0.50 | 0.00 | -93.86 | -296.69 |
| 10 | 0.60 | 0.00 | -97.05 | -287.23 |
| 11 | 0.70 | 0.00 | -99.91 | -277.46 |
| 12 | 0.80 | 0.00 | -102.44 | -267.42 |
| 13 | 0.90 | 0.00 | -104.64 | -257.14 |
| 14 | 1.00 | 0.00 | -106.51 | -246.66 |
| 15 | 1.10 | 0.00 | -108.06 | -236.01 |
| 16 | 1.20 | 0.00 | -109.27 | -225.22 |
| 17 | 1.30 | 0.00 | -110.16 | -214.33 |
| 18 | 1.40 | 0.00 | -110.72 | -203.36 |
| 19 | 1.50 | 0.00 | -110.95 | -192.35 |
| 20 | 1.60 | 0.00 | -110.85 | -181.34 |
| 21 | 1.70 | 0.00 | -110.42 | -170.35 |
| 22 | 1.80 | 0.00 | -109.66 | -159.43 |
| 23 | 1.90 | 0.00 | -108.58 | -148.59 |
| 24 | 2.00 | 0.00 | -107.17 | -137.88 |
| 25 | 2.10 | 0.00 | -105.42 | -127.33 |
| 26 | 2.20 | 0.00 | -103.35 | -116.97 |
| 27 | 2.30 | 0.00 | -100.96 | -106.83 |
| 28 | 2.40 | 0.00 | -98.23 | -96.95 |
| 29 | 2.50 | 0.00 | -95.17 | -87.35 |
| 30 | 2.60 | 0.00 | -91.79 | -78.08 |
| 31 | 2.70 | 0.00 | -88.07 | -69.16 |
| 32 | 2.80 | 0.00 | -84.03 | -60.64 |
| 33 | 2.90 | 0.00 | -79.66 | -52.53 |
| 34 | 3.00 | 0.00 | -74.96 | -44.87 |
| 35 | 3.10 | 0.00 | -69.94 | -37.71 |
| 36 | 3.20 | 0.00 | -64.58 | -31.06 |
| 37 | 3.30 | 0.00 | -58.90 | -24.96 |
| 38 | 3.40 | 0.00 | -52.88 | -19.45 |
| 39 | 3.50 | 0.00 | -46.54 | -14.55 |
| 40 | 3.60 | 0.00 | -39.87 | -10.31 |
| 41 | 3.70 | 0.00 | -32.87 | -6.75 |

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 42 | 3.80 | 0.00 | -25.15 | -3.85 |
| 43 | 3.90 | 0.00 | -17.10 | -1.73 |
| 44 | 4.00 | 0.00 | -8.71 | -0.44 |
| 45 | 4.10 | 0.00 | 0.00 | 0.00 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 16.13 | 0.81 |
| 3 | -0.80 | 0.00 | 31.94 | 3.22 |
| 4 | -0.70 | 0.00 | 47.44 | 7.19 |
| 5 | -0.60 | 0.00 | 62.61 | 12.69 |
| 6 | -0.50 | 0.00 | 77.46 | 19.70 |
| 7 | -0.40 | 0.00 | 92.00 | 28.17 |
| 8 | 0.40 | 0.00 | -140.90 | -395.31 |
| 9 | 0.50 | 0.00 | -143.07 | -381.55 |
| 10 | 0.60 | 0.00 | -144.72 | -367.24 |
| 11 | 0.70 | 0.00 | -146.06 | -352.78 |
| 12 | 0.80 | 0.00 | -147.07 | -338.20 |
| 13 | 0.90 | 0.00 | -147.77 | -323.54 |
| 14 | 1.00 | 0.00 | -148.14 | -308.82 |
| 15 | 1.10 | 0.00 | -148.20 | -294.08 |
| 16 | 1.20 | 0.00 | -147.94 | -279.35 |
| 17 | 1.30 | 0.00 | -147.36 | -264.66 |
| 18 | 1.40 | 0.00 | -146.46 | -250.04 |
| 19 | 1.50 | 0.00 | -145.24 | -235.54 |
| 20 | 1.60 | 0.00 | -143.70 | -221.17 |
| 21 | 1.70 | 0.00 | -141.85 | -206.97 |
| 22 | 1.80 | 0.00 | -139.67 | -192.97 |
| 23 | 1.90 | 0.00 | -137.18 | -179.20 |
| 24 | 2.00 | 0.00 | -134.36 | -165.70 |
| 25 | 2.10 | 0.00 | -131.23 | -152.50 |
| 26 | 2.20 | 0.00 | -127.78 | -139.62 |
| 27 | 2.30 | 0.00 | -124.01 | -127.11 |
| 28 | 2.40 | 0.00 | -119.92 | -114.99 |
| 29 | 2.50 | 0.00 | -115.51 | -103.30 |
| 30 | 2.60 | 0.00 | -110.78 | -92.06 |
| 31 | 2.70 | 0.00 | -105.74 | -81.31 |
| 32 | 2.80 | 0.00 | -100.37 | -71.08 |
| 33 | 2.90 | 0.00 | -94.69 | -61.41 |
| 34 | 3.00 | 0.00 | -88.68 | -52.31 |
| 35 | 3.10 | 0.00 | -82.36 | -43.84 |
| 36 | 3.20 | 0.00 | -75.72 | -36.01 |
| 37 | 3.30 | 0.00 | -68.76 | -28.86 |
| 38 | 3.40 | 0.00 | -61.48 | -22.43 |
| 39 | 3.50 | 0.00 | -53.88 | -16.74 |
| 40 | 3.60 | 0.00 | -45.96 | -11.82 |
| 41 | 3.70 | 0.00 | -37.73 | -7.72 |
| 42 | 3.80 | 0.00 | -28.78 | -4.39 |
| 43 | 3.90 | 0.00 | -19.51 | -1.97 |
| 44 | 4.00 | 0.00 | -9.91 | -0.50 |
| 45 | 4.10 | 0.00 | 0.00 | 0.00 |

Combinazione n° 10 - SLER

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
|----|----------|-----------|-----------|------------|

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 12.81 | 0.64 |
| 3 | -0.80 | 0.00 | 25.47 | 2.56 |
| 4 | -0.70 | 0.00 | 37.98 | 5.73 |
| 5 | -0.60 | 0.00 | 50.34 | 10.15 |
| 6 | -0.50 | 0.00 | 62.54 | 15.79 |
| 7 | -0.40 | 0.00 | 74.59 | 22.65 |
| 8 | 0.40 | 0.00 | -72.96 | -199.32 |
| 9 | 0.50 | 0.00 | -74.14 | -192.72 |
| 10 | 0.60 | 0.00 | -74.97 | -185.67 |
| 11 | 0.70 | 0.00 | -75.65 | -178.54 |
| 12 | 0.80 | 0.00 | -76.17 | -171.34 |
| 13 | 0.90 | 0.00 | -76.55 | -164.10 |
| 14 | 1.00 | 0.00 | -76.77 | -156.83 |
| 15 | 1.10 | 0.00 | -76.83 | -149.55 |
| 16 | 1.20 | 0.00 | -76.75 | -142.27 |
| 17 | 1.30 | 0.00 | -76.51 | -135.00 |
| 18 | 1.40 | 0.00 | -76.12 | -127.77 |
| 19 | 1.50 | 0.00 | -75.58 | -120.58 |
| 20 | 1.60 | 0.00 | -74.88 | -113.45 |
| 21 | 1.70 | 0.00 | -74.03 | -106.40 |
| 22 | 1.80 | 0.00 | -73.03 | -99.45 |
| 23 | 1.90 | 0.00 | -71.88 | -92.60 |
| 24 | 2.00 | 0.00 | -70.58 | -85.87 |
| 25 | 2.10 | 0.00 | -69.12 | -79.28 |
| 26 | 2.20 | 0.00 | -67.51 | -72.85 |
| 27 | 2.30 | 0.00 | -65.75 | -66.58 |
| 28 | 2.40 | 0.00 | -63.83 | -60.50 |
| 29 | 2.50 | 0.00 | -61.77 | -54.62 |
| 30 | 2.60 | 0.00 | -59.55 | -48.95 |
| 31 | 2.70 | 0.00 | -57.17 | -43.51 |
| 32 | 2.80 | 0.00 | -54.65 | -38.31 |
| 33 | 2.90 | 0.00 | -51.97 | -33.38 |
| 34 | 3.00 | 0.00 | -49.14 | -28.72 |
| 35 | 3.10 | 0.00 | -46.16 | -24.35 |
| 36 | 3.20 | 0.00 | -43.03 | -20.29 |
| 37 | 3.30 | 0.00 | -39.74 | -16.55 |
| 38 | 3.40 | 0.00 | -36.30 | -13.14 |
| 39 | 3.50 | 0.00 | -32.71 | -10.09 |
| 40 | 3.60 | 0.00 | -28.97 | -7.40 |
| 41 | 3.70 | 0.00 | -25.07 | -5.10 |
| 42 | 3.80 | 0.00 | -19.06 | -2.89 |
| 43 | 3.90 | 0.00 | -12.86 | -1.30 |
| 44 | 4.00 | 0.00 | -6.51 | -0.33 |
| 45 | 4.10 | 0.00 | 0.00 | 0.00 |

Combinazione n° 11 - SLEF

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 12.81 | 0.64 |
| 3 | -0.80 | 0.00 | 25.47 | 2.56 |
| 4 | -0.70 | 0.00 | 37.98 | 5.73 |
| 5 | -0.60 | 0.00 | 50.34 | 10.15 |
| 6 | -0.50 | 0.00 | 62.54 | 15.79 |
| 7 | -0.40 | 0.00 | 74.59 | 22.65 |
| 8 | 0.40 | 0.00 | -72.96 | -199.32 |
| 9 | 0.50 | 0.00 | -74.14 | -192.72 |
| 10 | 0.60 | 0.00 | -74.97 | -185.67 |
| 11 | 0.70 | 0.00 | -75.65 | -178.54 |
| 12 | 0.80 | 0.00 | -76.17 | -171.34 |
| 13 | 0.90 | 0.00 | -76.55 | -164.10 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 14 | 1.00 | 0.00 | -76.77 | -156.83 |
| 15 | 1.10 | 0.00 | -76.83 | -149.55 |
| 16 | 1.20 | 0.00 | -76.75 | -142.27 |
| 17 | 1.30 | 0.00 | -76.51 | -135.00 |
| 18 | 1.40 | 0.00 | -76.12 | -127.77 |
| 19 | 1.50 | 0.00 | -75.58 | -120.58 |
| 20 | 1.60 | 0.00 | -74.88 | -113.45 |
| 21 | 1.70 | 0.00 | -74.03 | -106.40 |
| 22 | 1.80 | 0.00 | -73.03 | -99.45 |
| 23 | 1.90 | 0.00 | -71.88 | -92.60 |
| 24 | 2.00 | 0.00 | -70.58 | -85.87 |
| 25 | 2.10 | 0.00 | -69.12 | -79.28 |
| 26 | 2.20 | 0.00 | -67.51 | -72.85 |
| 27 | 2.30 | 0.00 | -65.75 | -66.58 |
| 28 | 2.40 | 0.00 | -63.83 | -60.50 |
| 29 | 2.50 | 0.00 | -61.77 | -54.62 |
| 30 | 2.60 | 0.00 | -59.55 | -48.95 |
| 31 | 2.70 | 0.00 | -57.17 | -43.51 |
| 32 | 2.80 | 0.00 | -54.65 | -38.31 |
| 33 | 2.90 | 0.00 | -51.97 | -33.38 |
| 34 | 3.00 | 0.00 | -49.14 | -28.72 |
| 35 | 3.10 | 0.00 | -46.16 | -24.35 |
| 36 | 3.20 | 0.00 | -43.03 | -20.29 |
| 37 | 3.30 | 0.00 | -39.74 | -16.55 |
| 38 | 3.40 | 0.00 | -36.30 | -13.14 |
| 39 | 3.50 | 0.00 | -32.71 | -10.09 |
| 40 | 3.60 | 0.00 | -28.97 | -7.40 |
| 41 | 3.70 | 0.00 | -25.07 | -5.10 |
| 42 | 3.80 | 0.00 | -19.06 | -2.89 |
| 43 | 3.90 | 0.00 | -12.86 | -1.30 |
| 44 | 4.00 | 0.00 | -6.51 | -0.33 |
| 45 | 4.10 | 0.00 | 0.00 | 0.00 |

Combinazione n° 12 - SLEQ

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 12.81 | 0.64 |
| 3 | -0.80 | 0.00 | 25.47 | 2.56 |
| 4 | -0.70 | 0.00 | 37.98 | 5.73 |
| 5 | -0.60 | 0.00 | 50.34 | 10.15 |
| 6 | -0.50 | 0.00 | 62.54 | 15.79 |
| 7 | -0.40 | 0.00 | 74.59 | 22.65 |
| 8 | 0.40 | 0.00 | -72.96 | -199.32 |
| 9 | 0.50 | 0.00 | -74.14 | -192.72 |
| 10 | 0.60 | 0.00 | -74.97 | -185.67 |
| 11 | 0.70 | 0.00 | -75.65 | -178.54 |
| 12 | 0.80 | 0.00 | -76.17 | -171.34 |
| 13 | 0.90 | 0.00 | -76.55 | -164.10 |
| 14 | 1.00 | 0.00 | -76.77 | -156.83 |
| 15 | 1.10 | 0.00 | -76.83 | -149.55 |
| 16 | 1.20 | 0.00 | -76.75 | -142.27 |
| 17 | 1.30 | 0.00 | -76.51 | -135.00 |
| 18 | 1.40 | 0.00 | -76.12 | -127.77 |
| 19 | 1.50 | 0.00 | -75.58 | -120.58 |
| 20 | 1.60 | 0.00 | -74.88 | -113.45 |
| 21 | 1.70 | 0.00 | -74.03 | -106.40 |
| 22 | 1.80 | 0.00 | -73.03 | -99.45 |
| 23 | 1.90 | 0.00 | -71.88 | -92.60 |
| 24 | 2.00 | 0.00 | -70.58 | -85.87 |
| 25 | 2.10 | 0.00 | -69.12 | -79.28 |
| 26 | 2.20 | 0.00 | -67.51 | -72.85 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 180 di 314 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 27 | 2.30 | 0.00 | -65.75 | -66.58 |
| 28 | 2.40 | 0.00 | -63.83 | -60.50 |
| 29 | 2.50 | 0.00 | -61.77 | -54.62 |
| 30 | 2.60 | 0.00 | -59.55 | -48.95 |
| 31 | 2.70 | 0.00 | -57.17 | -43.51 |
| 32 | 2.80 | 0.00 | -54.65 | -38.31 |
| 33 | 2.90 | 0.00 | -51.97 | -33.38 |
| 34 | 3.00 | 0.00 | -49.14 | -28.72 |
| 35 | 3.10 | 0.00 | -46.16 | -24.35 |
| 36 | 3.20 | 0.00 | -43.03 | -20.29 |
| 37 | 3.30 | 0.00 | -39.74 | -16.55 |
| 38 | 3.40 | 0.00 | -36.30 | -13.14 |
| 39 | 3.50 | 0.00 | -32.71 | -10.09 |
| 40 | 3.60 | 0.00 | -28.97 | -7.40 |
| 41 | 3.70 | 0.00 | -25.07 | -5.10 |
| 42 | 3.80 | 0.00 | -19.06 | -2.89 |
| 43 | 3.90 | 0.00 | -12.86 | -1.30 |
| 44 | 4.00 | 0.00 | -6.51 | -0.33 |
| 45 | 4.10 | 0.00 | 0.00 | 0.00 |

Combinazione n° 13 - SLEQ H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -1.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 16.96 | 0.85 |
| 3 | -0.80 | 0.00 | 33.62 | 3.38 |
| 4 | -0.70 | 0.00 | 49.97 | 7.56 |
| 5 | -0.60 | 0.00 | 66.03 | 13.37 |
| 6 | -0.50 | 0.00 | 81.78 | 20.76 |
| 7 | -0.40 | 0.00 | 97.23 | 29.71 |
| 8 | 0.40 | 0.00 | -95.80 | -304.46 |
| 9 | 0.50 | 0.00 | -99.05 | -295.47 |
| 10 | 0.60 | 0.00 | -101.80 | -285.83 |
| 11 | 0.70 | 0.00 | -104.24 | -275.92 |
| 12 | 0.80 | 0.00 | -106.38 | -265.79 |
| 13 | 0.90 | 0.00 | -108.22 | -255.45 |
| 14 | 1.00 | 0.00 | -109.76 | -244.95 |
| 15 | 1.10 | 0.00 | -111.00 | -234.31 |
| 16 | 1.20 | 0.00 | -111.93 | -223.56 |
| 17 | 1.30 | 0.00 | -112.57 | -212.73 |
| 18 | 1.40 | 0.00 | -112.90 | -201.85 |
| 19 | 1.50 | 0.00 | -112.93 | -190.95 |
| 20 | 1.60 | 0.00 | -112.66 | -180.07 |
| 21 | 1.70 | 0.00 | -112.09 | -169.23 |
| 22 | 1.80 | 0.00 | -111.22 | -158.46 |
| 23 | 1.90 | 0.00 | -110.04 | -147.79 |
| 24 | 2.00 | 0.00 | -108.57 | -137.26 |
| 25 | 2.10 | 0.00 | -106.79 | -126.88 |
| 26 | 2.20 | 0.00 | -104.71 | -116.70 |
| 27 | 2.30 | 0.00 | -102.33 | -106.75 |
| 28 | 2.40 | 0.00 | -99.65 | -97.04 |
| 29 | 2.50 | 0.00 | -96.67 | -87.62 |
| 30 | 2.60 | 0.00 | -93.38 | -78.52 |
| 31 | 2.70 | 0.00 | -89.80 | -69.75 |
| 32 | 2.80 | 0.00 | -85.91 | -61.36 |
| 33 | 2.90 | 0.00 | -81.72 | -53.37 |
| 34 | 3.00 | 0.00 | -77.23 | -45.82 |
| 35 | 3.10 | 0.00 | -72.44 | -38.73 |
| 36 | 3.20 | 0.00 | -67.35 | -32.14 |
| 37 | 3.30 | 0.00 | -61.96 | -26.07 |
| 38 | 3.40 | 0.00 | -56.26 | -20.55 |
| 39 | 3.50 | 0.00 | -50.27 | -15.62 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 40 | 3.60 | 0.00 | -43.97 | -11.31 |
| 41 | 3.70 | 0.00 | -37.37 | -7.63 |
| 42 | 3.80 | 0.00 | -28.51 | -4.34 |
| 43 | 3.90 | 0.00 | -19.31 | -1.95 |
| 44 | 4.00 | 0.00 | -9.80 | -0.49 |
| 45 | 4.10 | 0.00 | 0.00 | 0.00 |

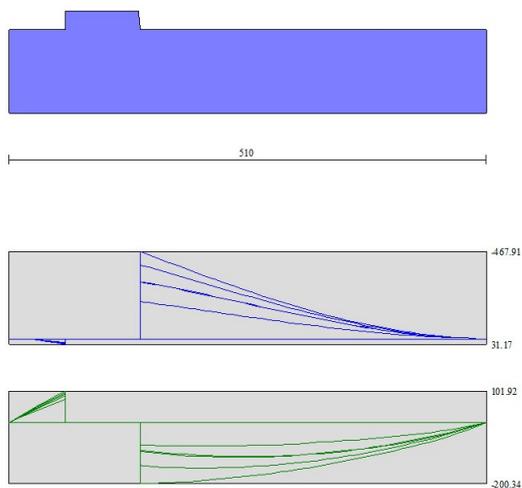


Fig. 9 - Fondazione (Inviluppo)

Verifiche strutturali

Verifiche a flessione

Elementi calcolati a trave

Simbologia adottata

| | |
|-----|--|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Afi | area ferri inferiori espresso in [cmq] |
| Afs | area ferri superiori espressa in [cmq] |

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 15 | 1.10 | 100 | 90 | 22.62 | 45.24 | -294.08 | 0.00 | -1388.66 | 0.00 | 4.722 |
| 16 | 1.20 | 100 | 90 | 22.62 | 45.24 | -279.35 | 0.00 | -1388.66 | 0.00 | 4.971 |
| 17 | 1.30 | 100 | 90 | 22.62 | 45.24 | -264.66 | 0.00 | -1388.66 | 0.00 | 5.247 |
| 18 | 1.40 | 100 | 90 | 22.62 | 45.24 | -250.04 | 0.00 | -1388.66 | 0.00 | 5.554 |
| 19 | 1.50 | 100 | 90 | 22.62 | 45.24 | -235.54 | 0.00 | -1388.66 | 0.00 | 5.896 |
| 20 | 1.60 | 100 | 90 | 22.62 | 45.24 | -221.17 | 0.00 | -1388.66 | 0.00 | 6.279 |
| 21 | 1.70 | 100 | 90 | 22.62 | 45.24 | -206.97 | 0.00 | -1388.66 | 0.00 | 6.710 |
| 22 | 1.80 | 100 | 90 | 22.62 | 45.24 | -192.97 | 0.00 | -1388.66 | 0.00 | 7.196 |
| 23 | 1.90 | 100 | 90 | 22.62 | 45.24 | -179.20 | 0.00 | -1388.66 | 0.00 | 7.749 |
| 24 | 2.00 | 100 | 90 | 22.62 | 45.24 | -165.70 | 0.00 | -1388.66 | 0.00 | 8.381 |
| 25 | 2.10 | 100 | 90 | 22.62 | 45.24 | -152.50 | 0.00 | -1388.66 | 0.00 | 9.106 |
| 26 | 2.20 | 100 | 90 | 22.62 | 45.24 | -139.62 | 0.00 | -1388.66 | 0.00 | 9.946 |
| 27 | 2.30 | 100 | 90 | 22.62 | 45.24 | -127.11 | 0.00 | -1388.66 | 0.00 | 10.925 |
| 28 | 2.40 | 100 | 90 | 22.62 | 45.24 | -114.99 | 0.00 | -1388.66 | 0.00 | 12.076 |
| 29 | 2.50 | 100 | 90 | 22.62 | 45.24 | -103.30 | 0.00 | -1388.66 | 0.00 | 13.443 |
| 30 | 2.60 | 100 | 90 | 22.62 | 45.24 | -92.06 | 0.00 | -1388.66 | 0.00 | 15.084 |
| 31 | 2.70 | 100 | 90 | 22.62 | 45.24 | -81.31 | 0.00 | -1388.66 | 0.00 | 17.079 |
| 32 | 2.80 | 100 | 90 | 22.62 | 45.24 | -71.08 | 0.00 | -1388.66 | 0.00 | 19.536 |
| 33 | 2.90 | 100 | 90 | 22.62 | 45.24 | -61.41 | 0.00 | -1388.66 | 0.00 | 22.614 |
| 34 | 3.00 | 100 | 90 | 22.62 | 45.24 | -52.31 | 0.00 | -1388.66 | 0.00 | 26.545 |
| 35 | 3.10 | 100 | 90 | 22.62 | 45.24 | -43.84 | 0.00 | -1388.66 | 0.00 | 31.676 |
| 36 | 3.20 | 100 | 90 | 22.62 | 45.24 | -36.01 | 0.00 | -1388.66 | 0.00 | 38.561 |
| 37 | 3.30 | 100 | 90 | 22.62 | 45.24 | -28.86 | 0.00 | -1388.66 | 0.00 | 48.109 |
| 38 | 3.40 | 100 | 90 | 22.62 | 45.24 | -22.43 | 0.00 | -1388.66 | 0.00 | 61.912 |
| 39 | 3.50 | 100 | 90 | 22.62 | 45.24 | -16.74 | 0.00 | -1388.66 | 0.00 | 82.962 |
| 40 | 3.60 | 100 | 90 | 22.62 | 45.24 | -11.82 | 0.00 | -1388.66 | 0.00 | 117.452 |
| 41 | 3.70 | 100 | 90 | 22.62 | 45.24 | -7.72 | 0.00 | -1388.66 | 0.00 | 179.981 |
| 42 | 3.80 | 100 | 90 | 22.62 | 45.24 | -4.39 | 0.00 | -1388.66 | 0.00 | 316.408 |
| 43 | 3.90 | 100 | 90 | 22.62 | 45.24 | -1.97 | 0.00 | -1388.66 | 0.00 | 704.241 |
| 44 | 4.00 | 100 | 90 | 22.62 | 45.24 | -0.50 | 0.00 | -1388.66 | 0.00 | 2786.905 |
| 45 | 4.10 | 100 | 90 | 22.62 | 45.24 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |

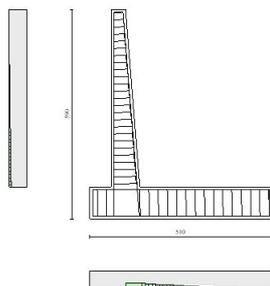


Fig. 10 - Paramento (Inviluppo)

Verifiche a taglio

Simbologia adottata

| | |
|------------------|---|
| Is | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| A _{sw} | area ferri a taglio espresso in [cm ²] |
| cotθ | inclinazione delle bielle compresse, θ inclinazione dei puntoni di calcestruzzo |
| V _{Rcd} | resistenza di progetto a 'taglio compressione' espressa in [kN] |
| V _{Rsd} | resistenza di progetto a 'taglio trazione' espressa in [kN] |
| V _{Rd} | resistenza di progetto a taglio espresso in [kN]. Per elementi con armature trasversali resistenti al taglio (A _{sw} >0.0) V _{Rd} =min(V _{Rcd} , V _{Rsd}). |
| T | taglio agente espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione resistente e sollecitazione agente) |

Paramento

Combinazione n° 1 - STR (A1-M1-R3)

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cm ²] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|---------------------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 291.33 | 0.00 | 100.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 296.84 | 0.04 | 7903.093 |
| 3 | -0.20 | 100 | 42 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 302.34 | 0.15 | 2012.382 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 307.83 | 0.34 | 913.120 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 313.30 | 0.60 | 524.562 |
| 6 | -0.50 | 100 | 44 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 318.76 | 0.93 | 342.336 |
| 7 | -0.60 | 100 | 45 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 324.21 | 1.34 | 242.092 |
| 8 | -0.70 | 100 | 46 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 329.65 | 1.83 | 180.101 |
| 9 | -0.80 | 100 | 46 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 334.67 | 2.41 | 138.666 |
| 10 | -0.90 | 100 | 47 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 337.86 | 3.09 | 109.341 |
| 11 | -1.00 | 100 | 48 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 341.03 | 3.86 | 88.323 |
| 12 | -1.10 | 100 | 49 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 344.18 | 4.72 | 72.942 |
| 13 | -1.20 | 100 | 50 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 347.31 | 5.65 | 61.432 |
| 14 | -1.30 | 100 | 50 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 350.43 | 6.67 | 52.576 |
| 15 | -1.40 | 100 | 51 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 353.52 | 7.75 | 45.603 |
| 16 | -1.50 | 100 | 52 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 356.59 | 8.91 | 40.004 |
| 17 | -1.60 | 100 | 53 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 359.65 | 10.15 | 35.431 |
| 18 | -1.70 | 100 | 54 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 362.69 | 11.46 | 31.642 |
| 19 | -1.80 | 100 | 54 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 365.72 | 12.85 | 28.464 |
| 20 | -1.90 | 100 | 55 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 368.73 | 14.31 | 25.769 |
| 21 | -2.00 | 100 | 56 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 371.72 | 15.84 | 23.461 |
| 22 | -2.10 | 100 | 57 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 374.70 | 17.45 | 21.468 |
| 23 | -2.20 | 100 | 58 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 377.66 | 19.14 | 19.734 |
| 24 | -2.30 | 100 | 58 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 380.61 | 20.90 | 18.215 |
| 25 | -2.40 | 100 | 59 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 383.55 | 22.73 | 16.875 |
| 26 | -2.50 | 100 | 60 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 386.47 | 24.64 | 15.687 |
| 27 | -2.60 | 100 | 61 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 389.38 | 26.62 | 14.629 |
| 28 | -2.70 | 100 | 61 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 392.28 | 28.67 | 13.681 |
| 29 | -2.80 | 100 | 62 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 395.17 | 30.80 | 12.829 |

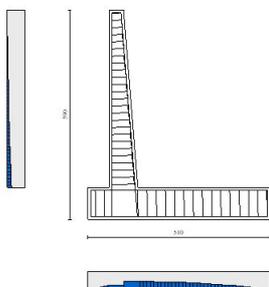


Fig. 11 - Paramento (Inviluppo)

Verifica delle tensioni

Simbologia adottata

| | |
|---------------|--|
| n° | indice sezione |
| Y | ordinata sezione, espressa in [m] |
| B | larghezza sezione, espresso in [cm] |
| H | altezza sezione, espressa in [cm] |
| A_{fi} | area ferri inferiori, espresso in [cm ²] |
| A_{fs} | area ferri superiori, espressa in [cm ²] |
| M | momento agente, espressa in [kNm] |
| N | sfuerzo normale agente, espressa in [kN] |
| σ_c | tensione di compressione nel cls, espressa in [kPa] |
| σ_{fi} | tensione nei ferri inferiori, espressa in [kPa] |
| σ_{fs} | tensione nei ferri superiori, espressa in [kPa] |

Combinazioni SLER

Paramento

| n° | Y | B | H | Afi | Afs | M | N | σ_c | σ_{fi} | σ_{fs} |
|----|------|------|------|-------|-------|--------|------|------------|---------------|---------------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
| 32 | 2.80 | 100 | 90 | 22.62 | 45.24 | -61.36 | 0.00 | 530 | 5963 | 17986 |
| 33 | 2.90 | 100 | 90 | 22.62 | 45.24 | -53.37 | 0.00 | 461 | 5187 | 15645 |
| 34 | 3.00 | 100 | 90 | 22.62 | 45.24 | -45.82 | 0.00 | 396 | 4453 | 13431 |
| 35 | 3.10 | 100 | 90 | 22.62 | 45.24 | -38.73 | 0.00 | 334 | 3764 | 11353 |
| 36 | 3.20 | 100 | 90 | 22.62 | 45.24 | -32.14 | 0.00 | 278 | 3123 | 9420 |
| 37 | 3.30 | 100 | 90 | 22.62 | 45.24 | -26.07 | 0.00 | 225 | 2533 | 7641 |
| 38 | 3.40 | 100 | 90 | 22.62 | 45.24 | -20.55 | 0.00 | 177 | 1997 | 6024 |
| 39 | 3.50 | 100 | 90 | 22.62 | 45.24 | -15.62 | 0.00 | 135 | 1518 | 4579 |
| 40 | 3.60 | 100 | 90 | 22.62 | 45.24 | -11.31 | 0.00 | 98 | 1099 | 3314 |
| 41 | 3.70 | 100 | 90 | 22.62 | 45.24 | -7.63 | 0.00 | 66 | 742 | 2238 |
| 42 | 3.80 | 100 | 90 | 22.62 | 45.24 | -4.34 | 0.00 | 38 | 422 | 1273 |
| 43 | 3.90 | 100 | 90 | 22.62 | 45.24 | -1.95 | 0.00 | 17 | 190 | 572 |
| 44 | 4.00 | 100 | 90 | 22.62 | 45.24 | -0.49 | 0.00 | 4 | 48 | 144 |
| 45 | 4.10 | 100 | 90 | 22.62 | 45.24 | 0.00 | 0.00 | 0 | 0 | 0 |

Verifica a fessurazione

Simbologia adottata

| | |
|------------|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Af | area ferri zona tesa espresso in [cmq] |
| Aeff | area efficace espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| Mpf | momento di prima fessurazione espressa in [kNm] |
| ϵ | deformazione espresso in % |
| Sm | spaziatura tra le fessure espressa in [mm] |
| w | apertura delle fessure espressa in [mm] |

Combinazioni SLER

Paramento

Combinazione n° 10 - SLER

Apertura limite fessure $w_{lim}=0.20$

| n° | Y | B | H | Af | Aeff | M | Mpf | ϵ | Sm | w |
|----|-----|------|------|-------|-------|-------|-------|------------|------|------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 212 di 314 |

| Ic | A | V [kN] | I [°] | Cx [kN] | Cy [kN] | Px [m] | Py [m] |
|----|---|-----------|----------|------------|-------------|-----------|-----------|
| 1 | Spinta statica | 164.47 | 0.00 | 164.47 | 0.00 | 4.10 | -3.65 |
| | Peso/Inerzia muro | | | 0.00 | 185.91/0.00 | 0.90 | -4.39 |
| | Peso/Inerzia terrapieno | | | 0.00 | 391.94/0.00 | 2.15 | -2.46 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |

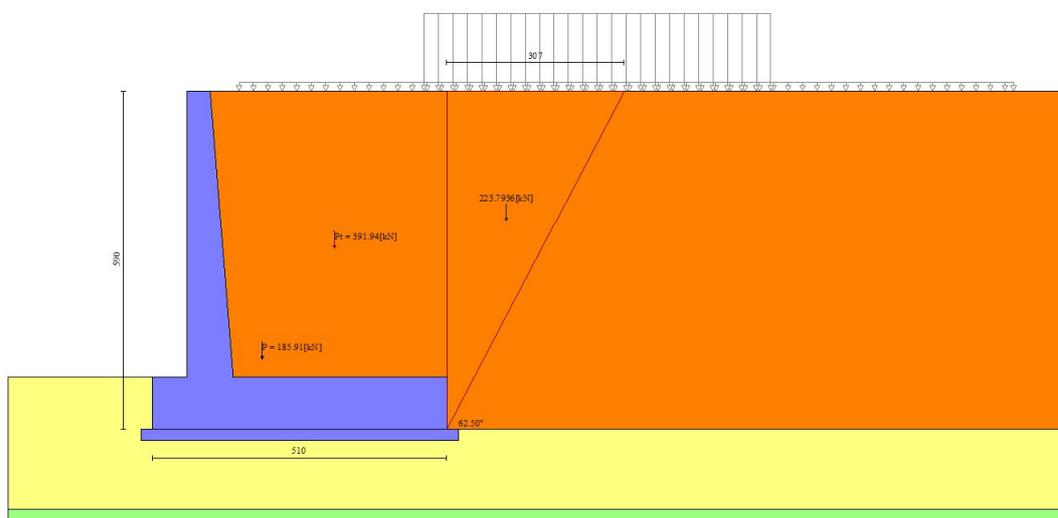


Fig. 12 - Cuneo di spinta (combinazione statica) (Combinazione n° 1)

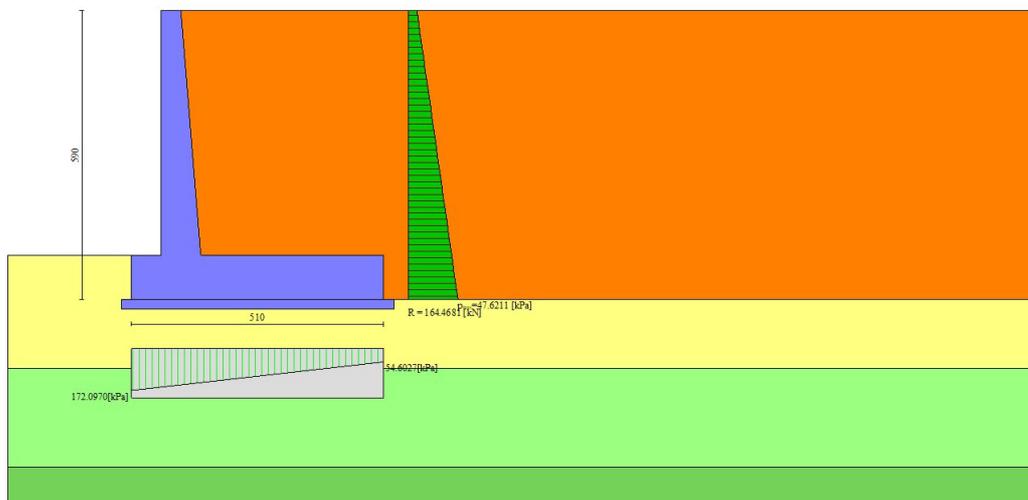


Fig. 13 - Diagramma delle pressioni (combinazione statica) (Combinazione n° 1)

Risultanti globali

Simbologia adottata

| | |
|----------------|---|
| Cmb | Indice/Tipo combinazione |
| N | Componente normale al piano di posa, espressa in [kN] |
| T | Componente parallela al piano di posa, espressa in [kN] |
| M _r | Momento ribaltante, espresso in [kNm] |
| M _s | Momento stabilizzante, espresso in [kNm] |
| ecc | Eccentricità risultante, espressa in [m] |

| Ic | N [kN] | T [kN] | M _r [kNm] | M _s [kNm] | ecc [m] |
|--------------------|-----------|-----------|-------------------------|-------------------------|------------|
| 1 - STR (A1-M1-R3) | 577.85 | 164.47 | 370.63 | 1589.07 | 0.440 |
| 2 - STR (A1-M1-R3) | 601.76 | 206.48 | 476.97 | 1648.08 | 0.603 |
| 3 - STR (A1-M1-R3) | 528.43 | 194.03 | 552.91 | 1547.66 | 0.666 |
| 4 - GEO (A2-M2-R2) | 574.82 | 165.45 | 376.41 | 1579.23 | 0.456 |
| 5 - GEO (A2-M2-R2) | 601.76 | 206.48 | 476.97 | 1648.08 | 0.603 |
| 6 - GEO (A2-M2-R2) | 528.43 | 194.03 | 552.91 | 1547.66 | 0.666 |
| 7 - EQU (A1-M1-R3) | 577.85 | 164.47 | 370.63 | 1589.07 | 0.440 |
| 8 - EQU (A1-M1-R3) | 613.34 | 241.56 | 565.36 | 1679.79 | 0.732 |
| 9 - EQU (A1-M1-R3) | 516.85 | 225.67 | 666.25 | 1547.66 | 0.844 |
| 10 - SLER | 571.46 | 124.79 | 280.02 | 1568.34 | 0.295 |
| 11 - SLEF | 571.46 | 124.79 | 280.02 | 1568.34 | 0.295 |
| 12 - SLEQ | 571.46 | 124.79 | 280.02 | 1568.34 | 0.295 |
| 13 - SLEQ | 593.07 | 192.01 | 448.70 | 1627.63 | 0.561 |

Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

| | |
|--------------------|--|
| Cmb | Indice/Tipo combinazione |
| S | Sisma (H: componente orizzontale, V: componente verticale) |
| FS _{SCO} | Coeff. di sicurezza allo scorrimento |
| FS _{RIB} | Coeff. di sicurezza al ribaltamento |
| FS _{QLIM} | Coeff. di sicurezza a carico limite |
| FS _{STAB} | Coeff. di sicurezza a stabilità globale |
| FS _{HYD} | Coeff. di sicurezza a sifonamento |
| FS _{UPL} | Coeff. di sicurezza a sollevamento |

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{UPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|-------------------|
| 1 - STR (A1-M1-R3) | | 1.638 | | 1.872 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.359 | | 1.387 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.270 | | 1.427 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.263 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.321 | | |
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.273 | | |
| 7 - EQU (A1-M1-R3) | | | 4.287 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 2.971 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.323 | | | | |

Verifica a scorrimento fondazione

Simbologia adottata

| | |
|-----|---|
| n° | Indice combinazione |
| Rsa | Resistenza allo scorrimento per attrito, espresso in [kN] |
| Rpt | Resistenza passiva terreno antistante, espresso in [kN] |
| Rps | Resistenza passiva sperone, espresso in [kN] |
| Rp | Resistenza a carichi orizzontali pali (solo per fondazione mista), espresso in [kN] |
| Rt | Resistenza a carichi orizzontali tiranti (solo se presenti), espresso in [kN] |
| R | Resistenza allo scorrimento (somma di Rsa+Rpt+Rps+Rp), espresso in [kN] |
| T | Carico parallelo al piano di posa, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto R/T) |

| n° | Rsa | Rpt | Rps | Rp | Rt | R | T | FS |
|--------------------------|--------|------|------|------|------|--------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | |
| 3 - STR (A1-M1-R3) H - V | 246.41 | 0.00 | 0.00 | -- | -- | 246.41 | 194.03 | 1.270 |

Verifica a carico limite

Simbologia adottata

| | |
|----|---|
| n° | Indice combinazione |
| N | Carico normale totale al piano di posa, espresso in [kN] |
| Qu | carico limite del terreno, espresso in [kN] |
| Qd | Portanza di progetto, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto tra il carico limite e carico agente al piano di posa) |

| n° | N | Qu | Qd | FS |
|--------------------------|--------|--------|--------|-------|
| | [kN] | [kN] | [kN] | |
| 2 - STR (A1-M1-R3) H + V | 601.76 | 834.45 | 695.37 | 1.387 |

Dettagli calcolo portanza

Simbologia adottata

| | |
|-----------------------|--|
| n° | Indice combinazione |
| N_c, N_q, N_γ | Fattori di capacità portante |
| i_c, i_q, i_γ | Fattori di inclinazione del carico |
| d_c, d_q, d_γ | Fattori di profondità del piano di posa |
| g_c, g_q, g_γ | Fattori di inclinazione del profilo topografico |
| b_c, b_q, b_γ | Fattori di inclinazione del piano di posa |
| s_c, s_q, s_γ | Fattori di forma della fondazione |
| p_c, p_q, p_γ | Fattori di riduzione per punzonamento secondo Vesic |
| R_e | Fattore di riduzione capacità portante per eccentricità secondo Meyerhof |
| I_r, I_{rc} | Indici di rigidità per punzonamento secondo Vesic |
| r_γ fattore | Fattori per tener conto dell'effetto piastra. Per fondazioni che hanno larghezza maggiore di 2 m, il terzo termine della formula trinomia $0.5B_\gamma N_\gamma$ viene moltiplicato per questo fattore |
| D | Affondamento del piano di posa, espresso in [m] |
| B' | Larghezza fondazione ridotta, espresso in [m] |
| H | Altezza del cuneo di rottura, espresso in [m] |
| γ | Peso di volume del terreno medio, espresso in [kN/mc] |
| ϕ | Angolo di attrito del terreno medio, espresso in [°] |
| c | Coesione del terreno medio, espresso in [kPa] |

Per i coeff. che in tabella sono indicati con il simbolo "--" sono coeff. non presenti nel metodo scelto (Meyerhof).

| n° | N_c N_q N_γ | i_c i_q i_γ | d_c d_q d_γ | g_c g_q g_γ | b_c b_q b_γ | s_c s_q s_γ | p_c p_q p_γ | I_r | I_{rc} | R_e | r_γ |
|-----------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|-------|----------|-------|------------|
| 2 | 28.123 16.666 13.508 | 0.623 0.623 0.122 | 1.060 1.030 1.030 | -- -- -- | -- -- -- | -- -- -- | -- -- -- | -- | -- | -- | 0.898 |

| n° | D | B' | H | γ | ϕ | c |
|-----------|------|------|------|----------|---------|-------|
| | [m] | [m] | [m] | [°] | [kN/mc] | [kPa] |
| 2 | 0.90 | 3.89 | 4.34 | 10.55 | 29.12 | 0 |

Verifica a ribaltamento

Simbologia adottata

| | |
|-----------|--|
| n° | Indice combinazione |
| M_s | Momento stabilizzante, espresso in [kNm] |
| M_r | Momento ribaltante, espresso in [kNm] |
| FS | Fattore di sicurezza (rapporto tra momento stabilizzante e momento ribaltante) |

La verifica viene eseguita rispetto allo spigolo inferiore esterno della fondazione

| n° | Ms | Mr | FS |
|--------------------------|---------|--------|-------|
| | [kNm] | [kNm] | |
| 9 - EQU (A1-M1-R3) H - V | 1547.66 | 666.25 | 2.323 |

Verifica stabilità globale muro + terreno

Simbologia adottata

Ic Indice/Tipo combinazione

C Centro superficie di scorrimento, espresso in [m]

R Raggio, espresso in [m]

FS Fattore di sicurezza

| Ic | C | R | FS |
|--------------------|-------------|-------|-------|
| | [m] | [m] | |
| 4 - GEO (A2-M2-R2) | -1.00; 3.00 | 10.27 | 1.263 |

Dettagli strisce verifiche stabilità

Simbologia adottata

Le ascisse X sono considerate positive verso monte

Le ordinate Y sono considerate positive verso l'alto

Origine in testa al muro (spigolo contro terra)

W peso della striscia espresso in [kN]

Qy carico sulla striscia espresso in [kN]

α angolo fra la base della striscia e l'orizzontale espresso in [°] (positivo antiorario)

ϕ angolo d'attrito del terreno lungo la base della striscia

c coesione del terreno lungo la base della striscia espressa in [kPa]

b larghezza della striscia espressa in [m]

u pressione neutra lungo la base della striscia espressa in [kPa]

Tx; Ty Resistenza al taglio fornita dai tiranti in direzione X ed Y espressa in [kPa]

| n° | W | Qy | b | α | ϕ | c | u | Tx; Ty |
|----|-------|-------|-------------|----------|--------|-------|-------|--------|
| | [kN] | [kN] | [m] | [°] | [°] | [kPa] | [kPa] | [kN] |
| 1 | 9.90 | 16.67 | 8.83 - 0.65 | 67.871 | 29.256 | 0 | 0.0 | |
| 2 | 26.71 | 16.67 | 0.65 | 59.765 | 29.256 | 0 | 0.0 | |
| 3 | 38.99 | 16.67 | 0.65 | 53.126 | 29.256 | 0 | 0.0 | |
| 4 | 48.74 | 16.67 | 0.65 | 47.412 | 29.256 | 0 | 0.0 | |
| 5 | 56.78 | 16.67 | 0.65 | 42.271 | 29.256 | 0 | 0.0 | |
| 6 | 63.53 | 16.67 | 0.65 | 37.524 | 29.256 | 0 | 0.0 | |
| 7 | 69.24 | 16.67 | 0.65 | 33.065 | 29.256 | 0 | 0.0 | |

| n° | W [kN] | Qy [kN] | b [m] | α [°] | ϕ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|-----------------|---------------|------------|------------|----------------|
| 8 | 76.45 | 14.84 | 0.65 | 28.823 | 20.458 | 0 | 0.0 | |
| 9 | 81.38 | 1.69 | 0.65 | 24.748 | 20.458 | 0 | 0.0 | |
| 10 | 84.77 | 1.69 | 0.65 | 20.804 | 20.458 | 0 | 0.9 | |
| 11 | 87.53 | 1.69 | 0.65 | 16.960 | 20.458 | 0 | 3.1 | |
| 12 | 89.70 | 1.69 | 0.65 | 13.195 | 20.458 | 0 | 4.8 | |
| 13 | 91.35 | 1.34 | 0.65 | 9.486 | 20.458 | 0 | 6.1 | |
| 14 | 105.72 | 0.00 | 0.65 | 5.818 | 20.458 | 0 | 6.9 | |
| 15 | 38.77 | 0.00 | 0.65 | 2.173 | 20.458 | 0 | 7.4 | |
| 16 | 28.25 | 0.00 | 0.65 | -1.462 | 20.458 | 0 | 7.4 | |
| 17 | 27.47 | 0.00 | 0.65 | -5.104 | 20.458 | 0 | 7.1 | |
| 18 | 26.49 | 0.00 | 0.65 | -8.767 | 20.458 | 0 | 6.3 | |
| 19 | 24.98 | 0.00 | 0.65 | -12.466 | 20.458 | 0 | 5.1 | |
| 20 | 22.92 | 0.00 | 0.65 | -16.219 | 20.458 | 0 | 3.5 | |
| 21 | 20.28 | 0.00 | 0.65 | -20.045 | 20.458 | 0 | 1.4 | |
| 22 | 17.02 | 0.00 | 0.65 | -23.968 | 20.458 | 0 | 0.0 | |
| 23 | 13.08 | 0.00 | 0.65 | -28.014 | 20.458 | 0 | 0.0 | |
| 24 | 8.41 | 0.00 | 0.65 | -32.220 | 20.458 | 0 | 0.0 | |
| 25 | 2.87 | 0.00 | -7.45 - 0.65 | -36.078 | 20.458 | 0 | 0.0 | |

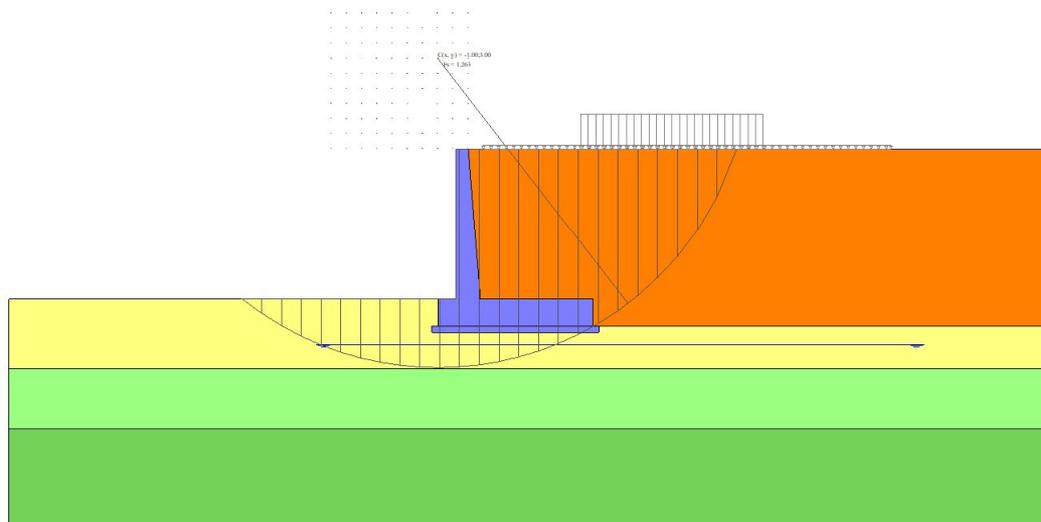


Fig. 14 - Stabilità fronte di scavo - Cerchio critico (Combinazione n° 4)

Sollecitazioni

Elementi calcolati a trave

Simbologia adottata

- N Sforzo normale, espresso in [kN]. Positivo se di compressione.
T Taglio, espresso in [kN]. Positivo se diretto da monte verso valle

M Momento, espresso in [kNm]. Positivo se tende le fibre contro terra (a monte)

Paramento

| n° | X | Nmin | Nmax | Tmin | Tmax | Mmin | Mmax |
|----|-------|-------|-------|-------|--------|--------|--------|
| | [m] | [kN] | [kN] | [kN] | [kN] | [kNm] | [kNm] |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.99 | 0.99 | 0.03 | 0.17 | 0.00 | 0.01 |
| 3 | -0.20 | 2.00 | 2.00 | 0.12 | 0.41 | 0.02 | 0.04 |
| 4 | -0.30 | 3.03 | 3.03 | 0.26 | 0.74 | 0.04 | 0.11 |
| 5 | -0.40 | 4.08 | 4.08 | 0.46 | 1.14 | 0.09 | 0.22 |
| 6 | -0.50 | 5.15 | 5.15 | 0.72 | 1.62 | 0.17 | 0.37 |
| 7 | -0.60 | 6.24 | 6.24 | 1.03 | 2.18 | 0.28 | 0.59 |
| 8 | -0.70 | 7.34 | 7.34 | 1.41 | 2.82 | 0.43 | 0.86 |
| 9 | -0.80 | 8.47 | 8.47 | 1.85 | 3.56 | 0.62 | 1.21 |
| 10 | -0.90 | 9.62 | 9.62 | 2.37 | 4.38 | 0.87 | 1.64 |
| 11 | -1.00 | 10.78 | 10.78 | 2.95 | 5.30 | 1.17 | 2.17 |
| 12 | -1.10 | 11.97 | 11.97 | 3.60 | 6.30 | 1.55 | 2.79 |
| 13 | -1.20 | 13.17 | 13.17 | 4.31 | 7.38 | 1.99 | 3.52 |
| 14 | -1.30 | 14.40 | 14.40 | 5.08 | 8.55 | 2.52 | 4.38 |
| 15 | -1.40 | 15.64 | 15.64 | 5.91 | 9.79 | 3.13 | 5.35 |
| 16 | -1.50 | 16.91 | 16.91 | 6.80 | 11.11 | 3.82 | 6.46 |
| 17 | -1.60 | 18.19 | 18.19 | 7.74 | 12.52 | 4.62 | 7.71 |
| 18 | -1.70 | 19.49 | 19.49 | 8.74 | 14.00 | 5.52 | 9.11 |
| 19 | -1.80 | 20.81 | 20.81 | 9.80 | 15.56 | 6.53 | 10.67 |
| 20 | -1.90 | 22.15 | 22.15 | 10.91 | 17.19 | 7.65 | 12.39 |
| 21 | -2.00 | 23.52 | 23.52 | 12.08 | 18.91 | 8.89 | 14.29 |
| 22 | -2.10 | 24.90 | 24.90 | 13.31 | 20.71 | 10.25 | 16.36 |
| 23 | -2.20 | 26.30 | 26.30 | 14.60 | 22.58 | 11.75 | 18.63 |
| 24 | -2.30 | 27.72 | 27.72 | 15.94 | 24.53 | 13.38 | 21.09 |
| 25 | -2.40 | 29.16 | 29.16 | 17.34 | 26.56 | 15.16 | 23.76 |
| 26 | -2.50 | 30.61 | 30.61 | 18.80 | 28.67 | 17.09 | 26.64 |
| 27 | -2.60 | 32.09 | 32.09 | 20.32 | 30.86 | 19.17 | 29.74 |
| 28 | -2.70 | 33.59 | 33.59 | 21.89 | 33.13 | 21.41 | 33.07 |
| 29 | -2.80 | 35.11 | 35.11 | 23.52 | 35.48 | 23.81 | 36.64 |
| 30 | -2.90 | 36.64 | 36.64 | 25.20 | 37.90 | 26.39 | 40.45 |
| 31 | -3.00 | 38.20 | 38.20 | 26.95 | 40.40 | 29.15 | 44.51 |
| 32 | -3.10 | 39.78 | 39.78 | 28.75 | 42.98 | 32.09 | 48.83 |
| 33 | -3.20 | 41.37 | 41.37 | 30.61 | 45.64 | 35.22 | 53.43 |
| 34 | -3.30 | 42.99 | 42.99 | 32.52 | 48.38 | 38.54 | 58.29 |
| 35 | -3.40 | 44.62 | 44.62 | 34.49 | 51.20 | 42.06 | 63.45 |
| 36 | -3.50 | 46.27 | 46.27 | 36.52 | 54.09 | 45.79 | 68.89 |
| 37 | -3.60 | 47.95 | 47.95 | 38.61 | 57.06 | 49.74 | 74.64 |
| 38 | -3.70 | 49.64 | 49.64 | 40.75 | 60.12 | 53.90 | 80.69 |
| 39 | -3.80 | 51.35 | 51.35 | 42.95 | 63.25 | 58.29 | 87.06 |
| 40 | -3.90 | 53.08 | 53.08 | 45.21 | 66.46 | 62.90 | 93.75 |
| 41 | -4.00 | 54.84 | 54.84 | 47.52 | 69.74 | 67.75 | 100.77 |
| 42 | -4.10 | 56.61 | 56.61 | 49.89 | 73.11 | 72.84 | 108.14 |
| 43 | -4.20 | 58.40 | 58.40 | 52.32 | 76.55 | 78.18 | 115.85 |
| 44 | -4.30 | 60.21 | 60.21 | 54.81 | 80.08 | 83.77 | 123.91 |
| 45 | -4.40 | 62.04 | 62.04 | 57.35 | 83.68 | 89.62 | 132.34 |
| 46 | -4.50 | 63.89 | 63.89 | 59.95 | 87.36 | 95.74 | 141.15 |
| 47 | -4.60 | 65.75 | 65.75 | 62.61 | 91.12 | 102.13 | 150.33 |
| 48 | -4.70 | 67.64 | 67.64 | 65.32 | 94.95 | 108.79 | 159.90 |
| 49 | -4.80 | 69.55 | 69.55 | 68.09 | 98.87 | 115.73 | 169.86 |
| 50 | -4.90 | 71.48 | 71.48 | 70.92 | 102.86 | 122.96 | 180.23 |
| 51 | -5.00 | 73.42 | 73.42 | 73.80 | 106.93 | 130.48 | 191.00 |

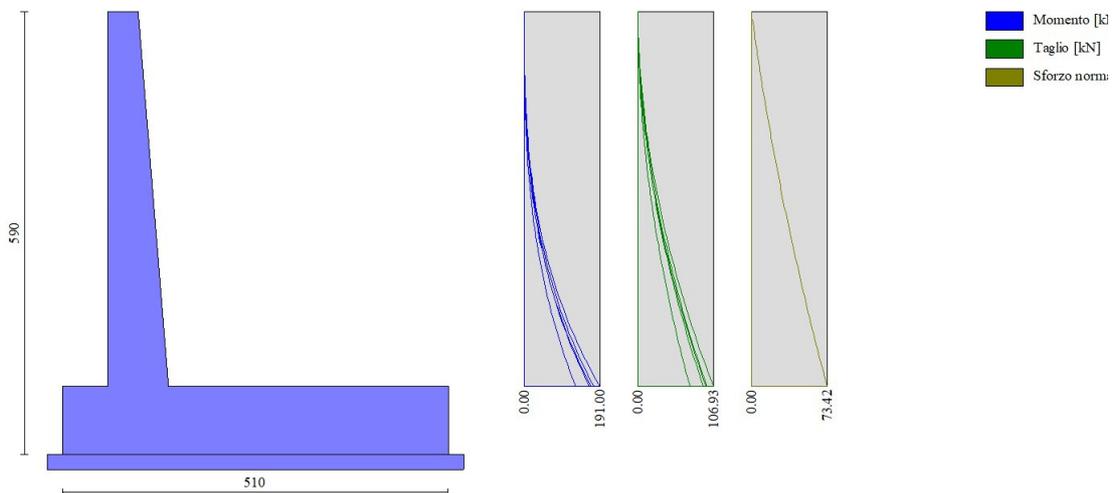


Fig. 15 - Paramento

Fondazione

| n° | X | Nmin | Nmax | Tmin | Tmax | Mmin | Mmax |
|----|-------|------|------|---------|--------|---------|---------|
| | [m] | [kN] | [kN] | [kN] | [kN] | [kNm] | [kNm] |
| 1 | -1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.90 | 0.00 | 0.00 | 12.81 | 17.81 | 0.64 | 0.89 |
| 3 | -0.80 | 0.00 | 0.00 | 25.47 | 35.29 | 2.56 | 3.55 |
| 4 | -0.70 | 0.00 | 0.00 | 37.98 | 52.44 | 5.73 | 7.94 |
| 5 | -0.60 | 0.00 | 0.00 | 50.34 | 69.26 | 10.15 | 14.03 |
| 6 | -0.50 | 0.00 | 0.00 | 62.54 | 85.75 | 15.79 | 21.78 |
| 7 | -0.40 | 0.00 | 0.00 | 74.59 | 101.92 | 22.65 | 31.17 |
| 8 | 0.40 | 0.00 | 0.00 | -200.34 | -72.96 | -467.91 | -199.32 |
| 9 | 0.50 | 0.00 | 0.00 | -199.65 | -74.14 | -448.99 | -192.72 |
| 10 | 0.60 | 0.00 | 0.00 | -198.45 | -74.97 | -429.63 | -185.67 |
| 11 | 0.70 | 0.00 | 0.00 | -197.00 | -75.65 | -410.39 | -178.54 |
| 12 | 0.80 | 0.00 | 0.00 | -195.33 | -76.17 | -391.31 | -171.34 |
| 13 | 0.90 | 0.00 | 0.00 | -193.42 | -76.55 | -372.41 | -164.10 |
| 14 | 1.00 | 0.00 | 0.00 | -191.28 | -76.77 | -353.71 | -156.83 |
| 15 | 1.10 | 0.00 | 0.00 | -188.92 | -76.83 | -335.23 | -149.55 |
| 16 | 1.20 | 0.00 | 0.00 | -186.32 | -76.75 | -317.01 | -142.27 |
| 17 | 1.30 | 0.00 | 0.00 | -183.49 | -76.51 | -299.05 | -135.00 |
| 18 | 1.40 | 0.00 | 0.00 | -180.43 | -76.12 | -281.39 | -127.77 |
| 19 | 1.50 | 0.00 | 0.00 | -177.15 | -75.58 | -264.05 | -120.58 |
| 20 | 1.60 | 0.00 | 0.00 | -173.63 | -74.88 | -247.04 | -113.45 |
| 21 | 1.70 | 0.00 | 0.00 | -169.88 | -74.03 | -230.40 | -106.40 |
| 22 | 1.80 | 0.00 | 0.00 | -165.90 | -73.03 | -214.15 | -99.45 |
| 23 | 1.90 | 0.00 | 0.00 | -161.69 | -71.88 | -198.31 | -92.60 |
| 24 | 2.00 | 0.00 | 0.00 | -157.24 | -70.58 | -182.89 | -85.87 |
| 25 | 2.10 | 0.00 | 0.00 | -152.57 | -69.12 | -167.94 | -79.28 |
| 26 | 2.20 | 0.00 | 0.00 | -147.67 | -67.51 | -153.46 | -72.85 |
| 27 | 2.30 | 0.00 | 0.00 | -142.54 | -65.75 | -139.49 | -66.58 |
| 28 | 2.40 | 0.00 | 0.00 | -137.18 | -63.83 | -126.04 | -60.50 |
| 29 | 2.50 | 0.00 | 0.00 | -131.58 | -61.77 | -113.13 | -54.62 |
| 30 | 2.60 | 0.00 | 0.00 | -125.76 | -59.55 | -100.80 | -48.95 |
| 31 | 2.70 | 0.00 | 0.00 | -119.70 | -57.17 | -89.06 | -43.51 |
| 32 | 2.80 | 0.00 | 0.00 | -113.42 | -54.65 | -77.94 | -38.31 |

| n° | X [m] | N _{min} [kN] | N _{max} [kN] | T _{min} [kN] | T _{max} [kN] | M _{min} [kNm] | M _{max} [kNm] |
|----|----------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|---------------------------|
| 33 | 2.90 | 0.00 | 0.00 | -106.90 | -51.97 | -67.46 | -33.38 |
| 34 | 3.00 | 0.00 | 0.00 | -100.16 | -49.14 | -57.64 | -28.72 |
| 35 | 3.10 | 0.00 | 0.00 | -93.18 | -46.16 | -48.51 | -24.35 |
| 36 | 3.20 | 0.00 | 0.00 | -85.98 | -43.03 | -40.09 | -20.29 |
| 37 | 3.30 | 0.00 | 0.00 | -78.54 | -39.74 | -32.40 | -16.55 |
| 38 | 3.40 | 0.00 | 0.00 | -70.87 | -36.30 | -25.46 | -13.14 |
| 39 | 3.50 | 0.00 | 0.00 | -62.97 | -32.71 | -19.31 | -10.09 |
| 40 | 3.60 | 0.00 | 0.00 | -54.84 | -28.97 | -13.95 | -7.40 |
| 41 | 3.70 | 0.00 | 0.00 | -46.48 | -25.07 | -9.42 | -5.10 |
| 42 | 3.80 | 0.00 | 0.00 | -35.25 | -19.06 | -5.34 | -2.89 |
| 43 | 3.90 | 0.00 | 0.00 | -23.73 | -12.86 | -2.39 | -1.30 |
| 44 | 4.00 | 0.00 | 0.00 | -11.98 | -6.51 | -0.60 | -0.33 |
| 45 | 4.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

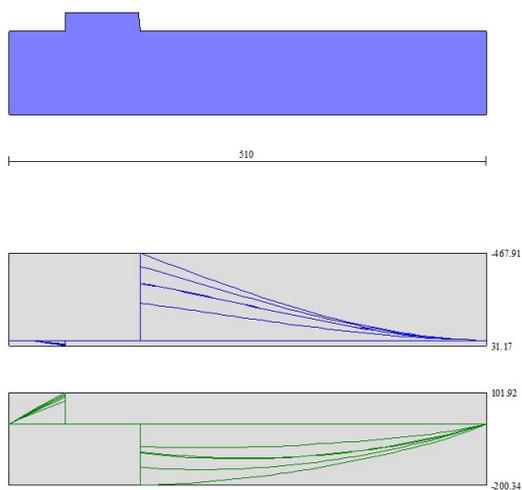


Fig. 16 - Fondazione

Verifiche strutturali

Verifiche a flessione

Elementi calcolati a trave

Simbologia adottata

n° indice sezione

Y ordinata sezione espressa in [m]

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 221 di 314 |

B larghezza sezione espresso in [cm]
H altezza sezione espressa in [cm]
Afi area ferri inferiori espresso in [cmq]
Afs area ferri superiori espressa in [cmq]
M momento agente espressa in [kNm]
N sforzo normale agente espressa in [kN]
Mu momento ultimi espresso in [kNm]
Nu sforzo normale ultimo espressa in [kN]
FS fattore di sicurezza (rapporto tra sollecitazione ultima e sollecitazione agente)

Paramento

| n° | B | H | Afi | Afs | M | N | Mu | Nu | FS |
|----|------|------|-------|-------|--------|-------|---------|---------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kNm] | [kN] | |
| 1 | 100 | 40 | 26.55 | 53.09 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | 100 | 41 | 26.55 | 53.09 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 3 | 100 | 42 | 26.55 | 53.09 | 0.04 | 2.00 | 189.78 | 8643.99 | 4321.170 |
| 4 | 100 | 42 | 26.55 | 53.09 | 0.11 | 3.03 | 295.63 | 8084.71 | 2668.362 |
| 5 | 100 | 43 | 26.55 | 53.09 | 0.22 | 4.08 | 401.87 | 7514.22 | 1842.259 |
| 6 | 100 | 44 | 26.55 | 53.09 | 0.37 | 5.15 | 503.89 | 6937.95 | 1347.885 |
| 7 | 100 | 45 | 26.55 | 53.09 | 0.59 | 6.24 | 599.63 | 6382.56 | 1023.621 |
| 8 | 100 | 46 | 26.55 | 53.09 | 0.86 | 7.34 | 688.39 | 5863.12 | 798.488 |
| 9 | 100 | 46 | 26.55 | 53.09 | 1.21 | 8.47 | 770.77 | 5387.70 | 636.108 |
| 10 | 100 | 47 | 26.55 | 53.09 | 1.64 | 9.62 | 848.63 | 4965.08 | 516.319 |
| 11 | 100 | 48 | 26.55 | 53.09 | 2.17 | 10.78 | 921.51 | 4584.81 | 425.215 |
| 12 | 100 | 49 | 26.55 | 53.09 | 2.79 | 11.97 | 991.51 | 4250.97 | 355.198 |
| 13 | 100 | 50 | 26.55 | 53.09 | 3.52 | 13.17 | 1057.22 | 3951.00 | 299.934 |
| 14 | 100 | 50 | 26.55 | 53.09 | 4.38 | 14.40 | 1120.06 | 3685.48 | 255.980 |
| 15 | 100 | 51 | 26.55 | 53.09 | 5.35 | 15.64 | 1180.69 | 3450.87 | 220.622 |
| 16 | 100 | 52 | 26.55 | 53.09 | 6.46 | 16.91 | 1217.61 | 3185.83 | 188.453 |
| 17 | 100 | 53 | 26.55 | 53.09 | 7.71 | 18.19 | 1237.74 | 2919.20 | 160.499 |
| 18 | 100 | 54 | 26.55 | 53.09 | 9.11 | 19.49 | 1249.84 | 2673.51 | 137.167 |
| 19 | 100 | 54 | 26.55 | 53.09 | 10.67 | 20.81 | 1262.65 | 2463.15 | 118.347 |
| 20 | 100 | 55 | 26.55 | 53.09 | 12.39 | 22.15 | 1270.27 | 2271.11 | 102.512 |
| 21 | 100 | 56 | 26.55 | 53.09 | 14.29 | 23.52 | 1280.28 | 2107.29 | 89.612 |
| 22 | 100 | 57 | 26.55 | 53.09 | 16.36 | 24.90 | 1287.04 | 1958.16 | 78.653 |
| 23 | 100 | 58 | 26.55 | 53.09 | 18.63 | 26.30 | 1293.96 | 1826.52 | 69.459 |
| 24 | 100 | 58 | 26.55 | 53.09 | 21.09 | 27.72 | 1302.80 | 1711.98 | 61.768 |
| 25 | 100 | 59 | 26.55 | 53.09 | 23.76 | 29.16 | 1311.90 | 1609.86 | 55.217 |
| 26 | 100 | 60 | 26.55 | 53.09 | 26.64 | 30.61 | 1318.32 | 1515.02 | 49.488 |
| 27 | 100 | 61 | 26.55 | 53.09 | 29.74 | 32.09 | 1326.57 | 1431.48 | 44.605 |
| 28 | 100 | 61 | 26.55 | 53.09 | 33.07 | 33.59 | 1335.95 | 1356.95 | 40.398 |
| 29 | 100 | 62 | 26.55 | 53.09 | 36.64 | 35.11 | 1346.44 | 1290.25 | 36.752 |
| 30 | 100 | 63 | 26.55 | 53.09 | 40.45 | 36.64 | 1357.90 | 1230.22 | 33.572 |
| 31 | 100 | 64 | 26.55 | 53.09 | 44.51 | 38.20 | 1366.81 | 1173.04 | 30.708 |
| 32 | 100 | 65 | 26.55 | 53.09 | 48.83 | 39.78 | 1374.85 | 1119.83 | 28.154 |
| 33 | 100 | 65 | 26.55 | 53.09 | 53.43 | 41.37 | 1383.81 | 1071.57 | 25.901 |
| 34 | 100 | 66 | 26.55 | 53.09 | 58.29 | 42.99 | 1393.59 | 1027.63 | 23.906 |
| 35 | 100 | 67 | 26.55 | 53.09 | 63.45 | 44.62 | 1404.09 | 987.46 | 22.130 |
| 36 | 100 | 68 | 26.55 | 53.09 | 68.89 | 46.27 | 1415.25 | 950.62 | 20.543 |
| 37 | 100 | 69 | 26.55 | 53.09 | 74.64 | 47.95 | 1427.00 | 916.73 | 19.120 |
| 38 | 100 | 69 | 26.55 | 53.09 | 80.69 | 49.64 | 1439.28 | 885.46 | 17.838 |
| 39 | 100 | 70 | 26.55 | 53.09 | 87.06 | 51.35 | 1452.04 | 856.52 | 16.679 |
| 40 | 100 | 71 | 26.55 | 53.09 | 93.75 | 53.08 | 1465.25 | 829.68 | 15.629 |
| 41 | 100 | 72 | 26.55 | 53.09 | 100.77 | 54.84 | 1477.93 | 804.22 | 14.666 |
| 42 | 100 | 73 | 26.55 | 53.09 | 108.14 | 56.61 | 1490.37 | 780.17 | 13.782 |

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
NM25 03 D 26 CL NV 24 05 001 A 222 di 314

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|--------|
| 43 | 100 | 73 | 26.55 | 53.09 | 115.85 | 58.40 | 1503.07 | 757.67 | 12.975 |
| 44 | 100 | 74 | 26.55 | 53.09 | 123.91 | 60.21 | 1516.02 | 736.59 | 12.234 |
| 45 | 100 | 75 | 26.55 | 53.09 | 132.34 | 62.04 | 1529.19 | 716.80 | 11.555 |
| 46 | 100 | 76 | 26.55 | 53.09 | 141.15 | 63.89 | 1542.56 | 698.19 | 10.929 |
| 47 | 100 | 77 | 26.55 | 53.09 | 150.33 | 65.75 | 1556.12 | 680.65 | 10.352 |
| 48 | 100 | 77 | 26.55 | 53.09 | 159.90 | 67.64 | 1569.86 | 664.10 | 9.818 |
| 49 | 100 | 78 | 26.55 | 53.09 | 169.86 | 69.55 | 1583.75 | 648.47 | 9.324 |
| 50 | 100 | 79 | 26.55 | 53.09 | 180.23 | 71.48 | 1597.78 | 633.67 | 8.865 |
| 51 | 100 | 80 | 26.55 | 53.09 | 191.00 | 73.42 | 1611.96 | 619.64 | 8.439 |

Fondazione

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | 100 | 90 | 45.24 | 22.62 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | 100 | 90 | 45.24 | 22.62 | 0.89 | 0.00 | 1388.66 | 0.00 | 1554.803 |
| 3 | 100 | 90 | 45.24 | 22.62 | 3.55 | 0.00 | 1388.66 | 0.00 | 391.099 |
| 4 | 100 | 90 | 45.24 | 22.62 | 7.94 | 0.00 | 1388.66 | 0.00 | 174.901 |
| 5 | 100 | 90 | 45.24 | 22.62 | 14.03 | 0.00 | 1388.66 | 0.00 | 98.996 |
| 6 | 100 | 90 | 45.24 | 22.62 | 21.78 | 0.00 | 1388.66 | 0.00 | 63.756 |
| 7 | 100 | 90 | 45.24 | 22.62 | 31.17 | 0.00 | 1388.66 | 0.00 | 44.555 |
| 8 | 100 | 90 | 22.62 | 45.24 | -467.91 | 0.00 | -1388.66 | 0.00 | 2.968 |
| 9 | 100 | 90 | 22.62 | 45.24 | -448.99 | 0.00 | -1388.66 | 0.00 | 3.093 |
| 10 | 100 | 90 | 22.62 | 45.24 | -429.63 | 0.00 | -1388.66 | 0.00 | 3.232 |
| 11 | 100 | 90 | 22.62 | 45.24 | -410.39 | 0.00 | -1388.66 | 0.00 | 3.384 |
| 12 | 100 | 90 | 22.62 | 45.24 | -391.31 | 0.00 | -1388.66 | 0.00 | 3.549 |
| 13 | 100 | 90 | 22.62 | 45.24 | -372.41 | 0.00 | -1388.66 | 0.00 | 3.729 |
| 14 | 100 | 90 | 22.62 | 45.24 | -353.71 | 0.00 | -1388.66 | 0.00 | 3.926 |
| 15 | 100 | 90 | 22.62 | 45.24 | -335.23 | 0.00 | -1388.66 | 0.00 | 4.142 |
| 16 | 100 | 90 | 22.62 | 45.24 | -317.01 | 0.00 | -1388.66 | 0.00 | 4.381 |
| 17 | 100 | 90 | 22.62 | 45.24 | -299.05 | 0.00 | -1388.66 | 0.00 | 4.644 |
| 18 | 100 | 90 | 22.62 | 45.24 | -281.39 | 0.00 | -1388.66 | 0.00 | 4.935 |
| 19 | 100 | 90 | 22.62 | 45.24 | -264.05 | 0.00 | -1388.66 | 0.00 | 5.259 |
| 20 | 100 | 90 | 22.62 | 45.24 | -247.04 | 0.00 | -1388.66 | 0.00 | 5.621 |
| 21 | 100 | 90 | 22.62 | 45.24 | -230.40 | 0.00 | -1388.66 | 0.00 | 6.027 |
| 22 | 100 | 90 | 22.62 | 45.24 | -214.15 | 0.00 | -1388.66 | 0.00 | 6.485 |
| 23 | 100 | 90 | 22.62 | 45.24 | -198.31 | 0.00 | -1388.66 | 0.00 | 7.003 |
| 24 | 100 | 90 | 22.62 | 45.24 | -182.89 | 0.00 | -1388.66 | 0.00 | 7.593 |
| 25 | 100 | 90 | 22.62 | 45.24 | -167.94 | 0.00 | -1388.66 | 0.00 | 8.269 |
| 26 | 100 | 90 | 22.62 | 45.24 | -153.46 | 0.00 | -1388.66 | 0.00 | 9.049 |
| 27 | 100 | 90 | 22.62 | 45.24 | -139.49 | 0.00 | -1388.66 | 0.00 | 9.956 |
| 28 | 100 | 90 | 22.62 | 45.24 | -126.04 | 0.00 | -1388.66 | 0.00 | 11.018 |
| 29 | 100 | 90 | 22.62 | 45.24 | -113.13 | 0.00 | -1388.66 | 0.00 | 12.275 |
| 30 | 100 | 90 | 22.62 | 45.24 | -100.80 | 0.00 | -1388.66 | 0.00 | 13.776 |
| 31 | 100 | 90 | 22.62 | 45.24 | -89.06 | 0.00 | -1388.66 | 0.00 | 15.592 |
| 32 | 100 | 90 | 22.62 | 45.24 | -77.94 | 0.00 | -1388.66 | 0.00 | 17.817 |
| 33 | 100 | 90 | 22.62 | 45.24 | -67.46 | 0.00 | -1388.66 | 0.00 | 20.585 |
| 34 | 100 | 90 | 22.62 | 45.24 | -57.64 | 0.00 | -1388.66 | 0.00 | 24.091 |
| 35 | 100 | 90 | 22.62 | 45.24 | -48.51 | 0.00 | -1388.66 | 0.00 | 28.625 |
| 36 | 100 | 90 | 22.62 | 45.24 | -40.09 | 0.00 | -1388.66 | 0.00 | 34.639 |
| 37 | 100 | 90 | 22.62 | 45.24 | -32.40 | 0.00 | -1388.66 | 0.00 | 42.862 |
| 38 | 100 | 90 | 22.62 | 45.24 | -25.46 | 0.00 | -1388.66 | 0.00 | 54.536 |
| 39 | 100 | 90 | 22.62 | 45.24 | -19.31 | 0.00 | -1388.66 | 0.00 | 71.927 |
| 40 | 100 | 90 | 22.62 | 45.24 | -13.95 | 0.00 | -1388.66 | 0.00 | 99.539 |
| 41 | 100 | 90 | 22.62 | 45.24 | -9.42 | 0.00 | -1388.66 | 0.00 | 147.419 |
| 42 | 100 | 90 | 22.62 | 45.24 | -5.34 | 0.00 | -1388.66 | 0.00 | 260.069 |
| 43 | 100 | 90 | 22.62 | 45.24 | -2.39 | 0.00 | -1388.66 | 0.00 | 581.390 |
| 44 | 100 | 90 | 22.62 | 45.24 | -0.60 | 0.00 | -1388.66 | 0.00 | 2310.696 |
| 45 | 100 | 90 | 22.62 | 45.24 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |

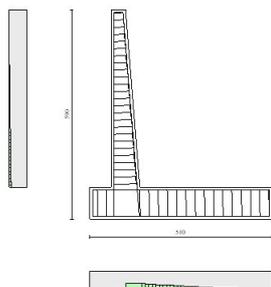


Fig. 17 - Paramento (Inviluppo)

Verifiche a taglio

Simbologia adottata

| | |
|--------------|---|
| I_s | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| A_{sw} | area ferri a taglio espresso in [cm ²] |
| $\cot\theta$ | inclinazione delle bielle compresse, θ inclinazione dei puntoni di calcestruzzo |
| V_{Rcd} | resistenza di progetto a 'taglio compressione' espressa in [kN] |
| V_{Rsd} | resistenza di progetto a 'taglio trazione' espressa in [kN] |
| V_{Rd} | resistenza di progetto a taglio espresso in [kN]. Per elementi con armature trasversali resistenti al taglio ($A_{sw}>0.0$) $V_{Rd}=\min(V_{Rcd}, V_{Rsd})$. |
| T | taglio agente espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione resistente e sollecitazione agente) |

Paramento

| | | | | | | | | | |
|-----------|----------|----------|-----------------------|-------------|------------------------|------------------------|-----------------------|----------|-----------|
| n° | B | H | A_{sw} | cotθ | V_{Rcd} | V_{Rsd} | V_{Rd} | T | FS |
|-----------|----------|----------|-----------------------|-------------|------------------------|------------------------|-----------------------|----------|-----------|

| n° | B [cm] | H [cm] | A _{sw} [cmq] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|-----------|-----------|--------------------------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 8 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -200.34 | 2.154 |
| 9 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -199.65 | 2.161 |
| 10 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -198.45 | 2.174 |
| 11 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -197.00 | 2.190 |
| 12 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -195.33 | 2.209 |
| 13 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -193.42 | 2.231 |
| 14 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -191.28 | 2.256 |
| 15 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -188.92 | 2.284 |
| 16 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -186.32 | 2.316 |
| 17 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -183.49 | 2.351 |
| 18 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -180.43 | 2.391 |
| 19 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -177.15 | 2.436 |
| 20 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -173.63 | 2.485 |
| 21 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -169.88 | 2.540 |
| 22 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -165.90 | 2.601 |
| 23 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -161.69 | 2.669 |
| 24 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -157.24 | 2.744 |
| 25 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -152.57 | 2.828 |
| 26 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -147.67 | 2.922 |
| 27 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -142.54 | 3.027 |
| 28 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -137.18 | 3.145 |
| 29 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -131.58 | 3.279 |
| 30 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -125.76 | 3.431 |
| 31 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -119.70 | 3.605 |
| 32 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -113.42 | 3.804 |
| 33 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -106.90 | 4.036 |
| 34 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -100.16 | 4.308 |
| 35 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -93.18 | 4.630 |
| 36 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -85.98 | 5.019 |
| 37 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -78.54 | 5.494 |
| 38 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -70.87 | 6.088 |
| 39 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -62.97 | 6.852 |
| 40 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -54.84 | 7.867 |
| 41 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -46.48 | 9.282 |
| 42 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -35.25 | 12.240 |
| 43 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -23.73 | 18.182 |
| 44 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | -11.98 | 36.013 |
| 45 | 100 | 90 | 0.00 | -- | 0.00 | 0.00 | 431.48 | 0.00 | 100.000 |

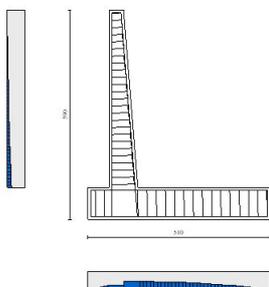


Fig. 18 - Paramento (Inviluppo)

Verifica delle tensioni

Simbologia adottata

| | |
|---------------|---|
| n° | indice sezione |
| Y | ordinata sezione, espressa in [m] |
| B | larghezza sezione, espresso in [cm] |
| H | altezza sezione, espressa in [cm] |
| A_{fi} | area ferri inferiori, espresso in [cmq] |
| A_{fs} | area ferri superiori, espressa in [cmq] |
| M | momento agente, espressa in [kNm] |
| N | sfuerzo normale agente, espressa in [kN] |
| σ_c | tensione di compressione nel cls, espressa in [kPa] |
| σ_{fi} | tensione nei ferri inferiori, espressa in [kPa] |
| σ_{fs} | tensione nei ferri superiori, espressa in [kPa] |

Combinazioni SLER

Paramento

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 233 di 314 |

B larghezza sezione espresso in [cm]
H altezza sezione espressa in [cm]
Af area ferri zona tesa espresso in [cmq]
Aeff area efficace espressa in [cmq]
M momento agente espressa in [kNm]
Mpf momento di prima fessurazione espressa in [kNm]
ε deformazione espresso in %
Sm spaziatura tra le fessure espressa in [mm]
w apertura delle fessure espressa in [mm]

Combinazioni SLER

Paramento

Apertura limite fessure $w_{lim}=0.20$

| n° | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|------|------|-------|---------|-------|---------|----------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 1 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (10) |
| 2 | 100 | 41 | 0.00 | 0.00 | 0.00 | 5.90 | 0.000000 | 0.00 | 0.000 (10) |
| 3 | 100 | 42 | 0.00 | 0.00 | 0.02 | 17.03 | 0.000000 | 0.00 | 0.000 (10) |
| 4 | 100 | 42 | 0.00 | 0.00 | 0.04 | 35.74 | 0.000000 | 0.00 | 0.000 (10) |
| 5 | 100 | 43 | 0.00 | 0.00 | 0.09 | 66.70 | 0.000000 | 0.00 | 0.000 (10) |
| 6 | 100 | 44 | 0.00 | 0.00 | 0.17 | 120.39 | 0.000000 | 0.00 | 0.000 (10) |
| 7 | 100 | 45 | 0.00 | 0.00 | 0.28 | 225.07 | 0.000000 | 0.00 | 0.000 (10) |
| 8 | 100 | 46 | 0.00 | 0.00 | 0.43 | 491.79 | 0.000000 | 0.00 | 0.000 (10) |
| 9 | 100 | 46 | 0.00 | 0.00 | 0.62 | 2252.78 | 0.000000 | 0.00 | 0.000 (10) |
| 10 | 100 | 47 | 0.00 | 0.00 | 0.87 | 1553.66 | 0.000000 | 0.00 | 0.000 (10) |
| 11 | 100 | 48 | 0.00 | 0.00 | 1.17 | 711.18 | 0.000000 | 0.00 | 0.000 (10) |
| 12 | 100 | 49 | 53.09 | 1600.00 | 1.55 | 513.20 | 0.000000 | 0.00 | 0.000 (10) |
| 13 | 100 | 50 | 53.09 | 1600.00 | 1.99 | 427.98 | 0.000000 | 0.00 | 0.000 (10) |
| 14 | 100 | 50 | 53.09 | 1600.00 | 2.52 | 382.54 | 0.000000 | 0.00 | 0.000 (10) |
| 15 | 100 | 51 | 53.09 | 1600.00 | 3.13 | 355.69 | 0.000000 | 0.00 | 0.000 (10) |
| 16 | 100 | 52 | 53.09 | 1600.00 | 3.82 | 339.01 | 0.000000 | 0.00 | 0.000 (10) |
| 17 | 100 | 53 | 53.09 | 1600.00 | 4.62 | 328.51 | 0.000000 | 0.00 | 0.000 (10) |
| 18 | 100 | 54 | 53.09 | 1600.00 | 5.52 | 322.03 | 0.000000 | 0.00 | 0.000 (10) |
| 19 | 100 | 54 | 53.09 | 1600.00 | 6.53 | 318.34 | 0.000000 | 0.00 | 0.000 (10) |
| 20 | 100 | 55 | 53.09 | 1600.00 | 7.65 | 316.65 | 0.000000 | 0.00 | 0.000 (10) |
| 21 | 100 | 56 | 53.09 | 1600.00 | 8.89 | 316.45 | 0.000000 | 0.00 | 0.000 (10) |
| 22 | 100 | 57 | 53.09 | 1600.00 | 10.25 | 317.41 | 0.000000 | 0.00 | 0.000 (10) |
| 23 | 100 | 58 | 53.09 | 1600.00 | 11.75 | 319.27 | 0.000000 | 0.00 | 0.000 (10) |
| 24 | 100 | 58 | 53.09 | 1600.00 | 13.38 | 321.86 | 0.000000 | 0.00 | 0.000 (10) |
| 25 | 100 | 59 | 53.09 | 1600.00 | 15.16 | 325.06 | 0.000000 | 0.00 | 0.000 (10) |
| 26 | 100 | 60 | 53.09 | 1600.00 | 17.09 | 328.76 | 0.000000 | 0.00 | 0.000 (10) |
| 27 | 100 | 61 | 53.09 | 1600.00 | 19.17 | 332.88 | 0.000000 | 0.00 | 0.000 (10) |
| 28 | 100 | 61 | 53.09 | 1600.00 | 21.41 | 337.37 | 0.000000 | 0.00 | 0.000 (10) |
| 29 | 100 | 62 | 53.09 | 1600.00 | 23.81 | 342.18 | 0.000000 | 0.00 | 0.000 (10) |
| 30 | 100 | 63 | 53.09 | 1600.00 | 26.39 | 347.27 | 0.000000 | 0.00 | 0.000 (10) |
| 31 | 100 | 64 | 53.09 | 1600.00 | 29.15 | 352.62 | 0.000000 | 0.00 | 0.000 (10) |
| 32 | 100 | 65 | 53.09 | 1600.00 | 32.09 | 358.19 | 0.000000 | 0.00 | 0.000 (10) |
| 33 | 100 | 65 | 53.09 | 1600.00 | 35.22 | 363.96 | 0.000000 | 0.00 | 0.000 (10) |
| 34 | 100 | 66 | 53.09 | 1600.00 | 38.54 | 369.93 | 0.000000 | 0.00 | 0.000 (10) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
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| n° | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|------|------|-------|---------|-------|---------|----------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 42 | 100 | 90 | 45.24 | 1600.00 | -2.89 | -496.13 | 0.000000 | 0.00 | 0.000 (12) |
| 43 | 100 | 90 | 45.24 | 1600.00 | -1.30 | -496.13 | 0.000000 | 0.00 | 0.000 (12) |
| 44 | 100 | 90 | 45.24 | 1600.00 | -0.33 | -496.13 | 0.000000 | 0.00 | 0.000 (12) |
| 45 | 100 | 90 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (12) |

14. TABULATI DI CALCOLO CONCIO 3

14.1 RISULTATI PER COMBINAZIONE

Spinta e forze

Simbologia adottata

| | |
|---------------------------------|--|
| Ic | Indice della combinazione |
| A | Tipo azione |
| I | Inclinazione della spinta, espressa in [°] |
| V | Valore dell'azione, espressa in [kN] |
| C _x , C _y | Componente in direzione X ed Y dell'azione, espressa in [kN] |
| P _x , P _y | Coordinata X ed Y del punto di applicazione dell'azione, espressa in [m] |

| Ic | A | V | I | C _x | C _y | P _x | P _y |
|----|---|--------|-------|----------------|----------------|----------------|----------------|
| | | [kN] | [°] | [kN] | [kN] | [m] | [m] |
| 1 | Spinta statica | 120.81 | 0.00 | 120.81 | 0.00 | 3.60 | -3.06 |
| | Peso/Inerzia muro | | | 0.00 | 142.66/0.00 | 0.80 | -3.65 |
| | Peso/Inerzia terrapieno | | | 0.00 | 280.87/0.00 | 1.88 | -2.05 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 2 | Spinta statica | 70.92 | 0.00 | 70.92 | 0.00 | 3.60 | -3.22 |
| | Incremento di spinta sismica | | 24.32 | 24.32 | 0.00 | 3.60 | -3.30 |
| | Peso/Inerzia muro | | | 18.51 | 142.66/9.26 | 0.80 | -3.65 |
| | Peso/Inerzia terrapieno | | | 36.05 | 277.77/18.02 | 1.88 | -2.04 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 3 | Spinta statica | 70.92 | 0.00 | 70.92 | 0.00 | 3.60 | -3.22 |
| | Incremento di spinta sismica | | 15.42 | 15.42 | 0.00 | 3.60 | -3.30 |
| | Peso/Inerzia muro | | | 18.51 | 142.66/-9.26 | 0.80 | -3.65 |
| | Peso/Inerzia terrapieno | | | 36.05 | 277.77/-18.02 | 1.88 | -2.04 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 10 | Spinta statica | 91.53 | 0.00 | 91.53 | 0.00 | 3.60 | -3.07 |
| | Peso/Inerzia muro | | | 0.00 | 142.66/0.00 | 0.80 | -3.65 |
| | Peso/Inerzia terrapieno | | | 0.00 | 277.77/0.00 | 1.88 | -2.04 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 11 | Spinta statica | 91.53 | 0.00 | 91.53 | 0.00 | 3.60 | -3.07 |
| | Peso/Inerzia muro | | | 0.00 | 142.66/0.00 | 0.80 | -3.65 |
| | Peso/Inerzia terrapieno | | | 0.00 | 277.77/0.00 | 1.88 | -2.04 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 12 | Spinta statica | 91.53 | 0.00 | 91.53 | 0.00 | 3.60 | -3.07 |
| | Peso/Inerzia muro | | | 0.00 | 142.66/0.00 | 0.80 | -3.65 |
| | Peso/Inerzia terrapieno | | | 0.00 | 277.77/0.00 | 1.88 | -2.04 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |
| 13 | Spinta statica | 91.53 | 0.00 | 91.53 | 0.00 | 3.60 | -3.07 |
| | Incremento di spinta sismica | | 17.77 | 17.77 | 0.00 | 3.60 | -3.30 |
| | Peso/Inerzia muro | | | 10.79 | 142.66/5.39 | 0.80 | -3.65 |
| | Peso/Inerzia terrapieno | | | 21.00 | 277.77/10.50 | 1.88 | -2.04 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |

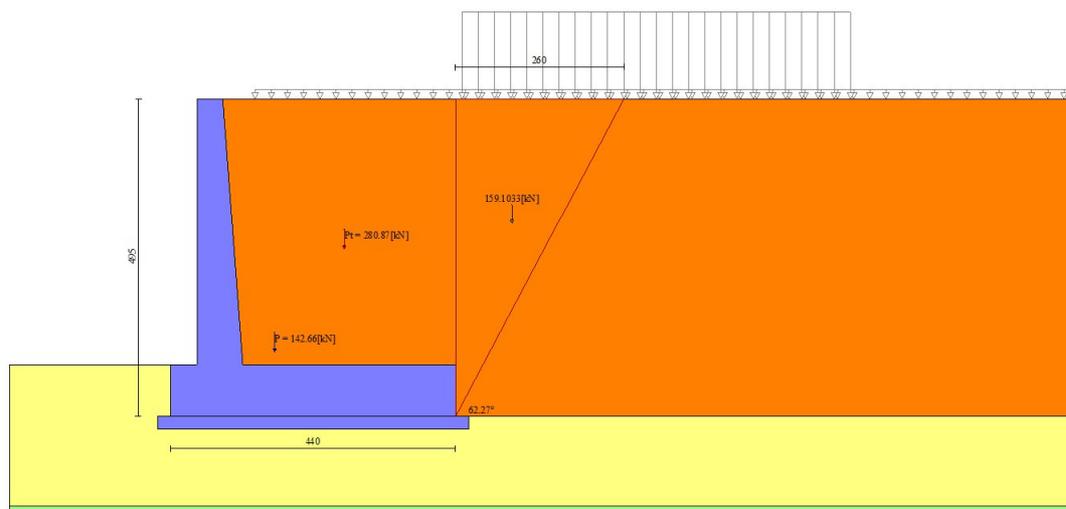


Fig. 3 - Cuneo di spinta (combinazione statica) (Combinazione n° 1)

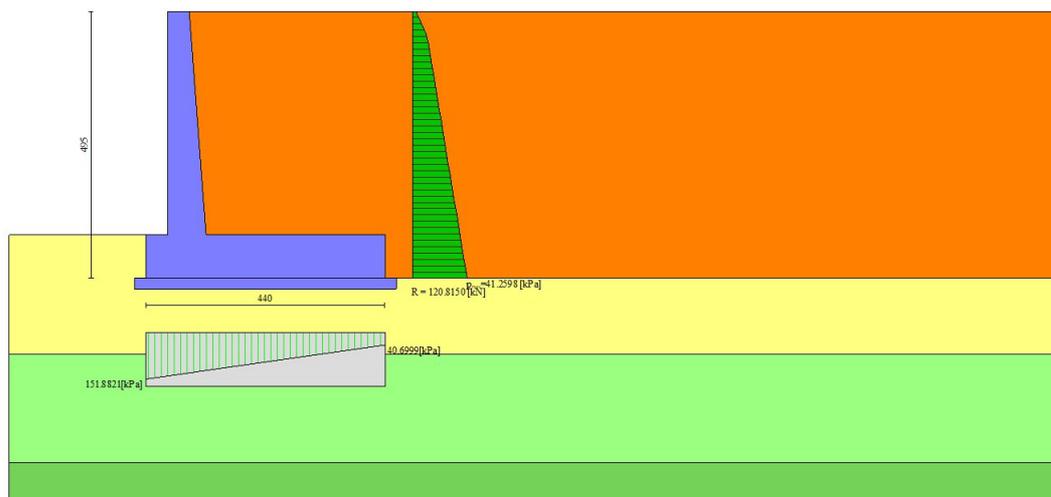


Fig. 4 - Diagramma delle pressioni (combinazione statica) (Combinazione n° 1)

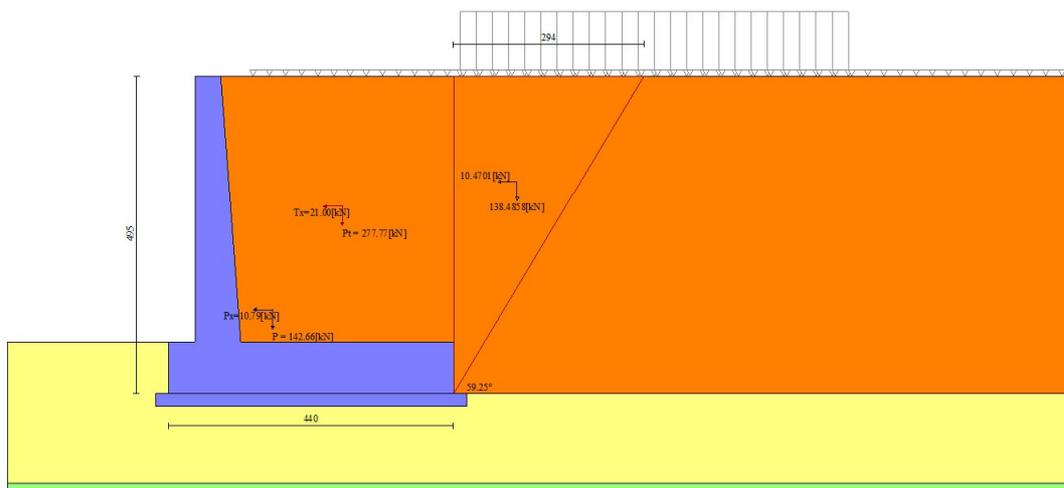


Fig. 5 - Cuneo di spinta (combinazione sismica) (Combinazione n° 13)

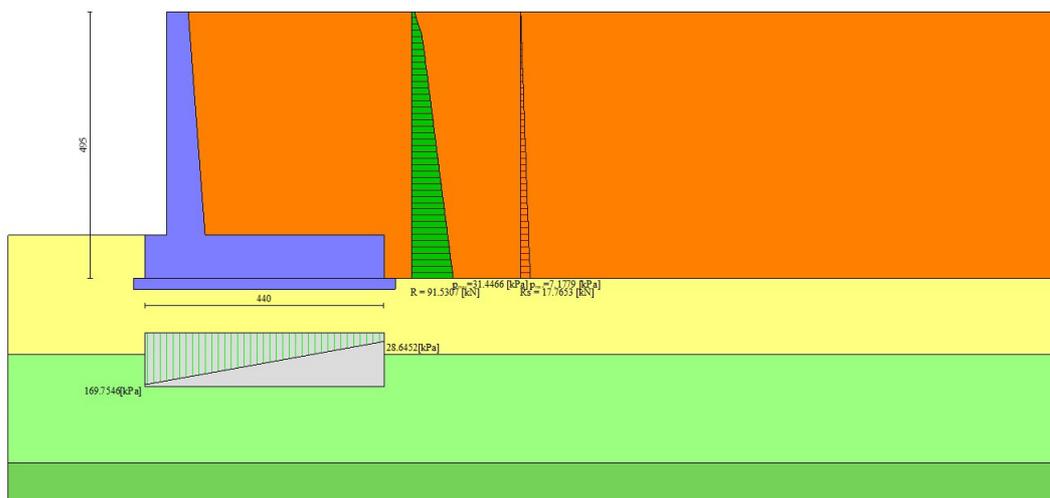


Fig. 6 - Diagramma delle pressioni (combinazione sismica) (Combinazione n° 13)

Risultanti globali

Simbologia adottata

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
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Cmb Indice/Tipo combinazione

N Componente normale al piano di posa, espressa in [kN]

T Componente parallela al piano di posa, espressa in [kN]

Mr Momento ribaltante, espresso in [kNm]

Ms Momento stabilizzante, espresso in [kNm]

ecc Eccentricità risultante, espressa in [m]

| Ic | N | T | Mr | Ms | ecc |
|--------------------|--------|--------|--------|---------|-------|
| | [kN] | [kN] | [kNm] | [kNm] | [m] |
| 1 - STR (A1-M1-R3) | 423.53 | 120.81 | 228.23 | 980.40 | 0.423 |
| 2 - STR (A1-M1-R3) | 447.71 | 149.79 | 291.95 | 1034.93 | 0.540 |
| 3 - STR (A1-M1-R3) | 393.15 | 140.90 | 340.33 | 971.87 | 0.593 |
| 4 - GEO (A2-M2-R2) | 422.29 | 122.11 | 233.28 | 976.99 | 0.438 |
| 5 - GEO (A2-M2-R2) | 447.71 | 149.79 | 291.95 | 1034.93 | 0.540 |
| 6 - GEO (A2-M2-R2) | 393.15 | 140.90 | 340.33 | 971.87 | 0.593 |
| 7 - EQU (A1-M1-R3) | 423.53 | 120.81 | 228.23 | 980.40 | 0.423 |
| 8 - EQU (A1-M1-R3) | 456.32 | 175.56 | 346.73 | 1054.84 | 0.647 |
| 9 - EQU (A1-M1-R3) | 384.53 | 164.21 | 410.97 | 971.87 | 0.741 |
| 10 - SLER | 420.43 | 91.53 | 172.17 | 971.87 | 0.297 |
| 11 - SLEF | 420.43 | 91.53 | 172.17 | 971.87 | 0.297 |
| 12 - SLEQ | 420.43 | 91.53 | 172.17 | 971.87 | 0.297 |
| 13 - SLEQ | 436.32 | 141.08 | 276.54 | 1008.61 | 0.521 |

Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

Cmb Indice/Tipo combinazione

S Sisma (H: componente orizzontale, V: componente verticale)

FS_{SCO} Coeff. di sicurezza allo scorrimento

FS_{RIB} Coeff. di sicurezza al ribaltamento

FS_{QLIM} Coeff. di sicurezza a carico limite

FS_{STAB} Coeff. di sicurezza a stabilità globale

FS_{HYD} Coeff. di sicurezza a sifonamento

FS_{SUPL} Coeff. di sicurezza a sollevamento

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{SUPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|--------------------|
| 1 - STR (A1-M1-R3) | | 1.635 | | 2.015 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.394 | | 1.525 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.301 | | 1.567 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.298 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.366 | | |
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.314 | | |
| 7 - EQU (A1-M1-R3) | | | 4.296 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 3.042 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.365 | | | | |

Verifica a scorrimento fondazione

Simbologia adottata

| | |
|-----|---|
| n° | Indice combinazione |
| Rsa | Resistenza allo scorrimento per attrito, espresso in [kN] |
| Rpt | Resistenza passiva terreno antistante, espresso in [kN] |
| Rps | Resistenza passiva sperone, espresso in [kN] |
| Rp | Resistenza a carichi orizzontali pali (solo per fondazione mista), espresso in [kN] |
| Rt | Resistenza a carichi orizzontali tiranti (solo se presenti), espresso in [kN] |
| R | Resistenza allo scorrimento (somma di Rsa+Rpt+Rps+Rp), espresso in [kN] |
| T | Carico parallelo al piano di posa, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto R/T) |

| n° | Rsa | Rpt | Rps | Rp | Rt | R | T | FS |
|--------------------------|--------|------|------|------|------|--------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | |
| 1 - STR (A1-M1-R3) | 197.49 | 0.00 | 0.00 | -- | -- | 197.49 | 120.81 | 1.635 |
| 2 - STR (A1-M1-R3) H + V | 208.77 | 0.00 | 0.00 | -- | -- | 208.77 | 149.79 | 1.394 |
| 3 - STR (A1-M1-R3) H - V | 183.33 | 0.00 | 0.00 | -- | -- | 183.33 | 140.90 | 1.301 |

Verifica a carico limite

Simbologia adottata

| | |
|----|---|
| n° | Indice combinazione |
| N | Carico normale totale al piano di posa, espresso in [kN] |
| Qu | carico limite del terreno, espresso in [kN] |
| Qd | Portanza di progetto, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto tra il carico limite e carico agente al piano di posa) |

| n° | N | Qu | Qd | FS |
|--------------------------|--------|--------|--------|-------|
| | [kN] | [kN] | [kN] | |
| 1 - STR (A1-M1-R3) | 423.53 | 853.34 | 609.53 | 2.015 |
| 2 - STR (A1-M1-R3) H + V | 447.71 | 682.64 | 568.87 | 1.525 |
| 3 - STR (A1-M1-R3) H - V | 393.15 | 615.93 | 513.28 | 1.567 |

Dettagli calcolo portanza

Simbologia adottata

| | |
|----|---------------------|
| n° | Indice combinazione |
|----|---------------------|

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
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| | |
|---------------|--|
| Nc, Nq, Ny | Fattori di capacità portante |
| ic, iq, iy | Fattori di inclinazione del carico |
| dc, dq, dy | Fattori di profondità del piano di posa |
| gc, gq, gy | Fattori di inclinazione del profilo topografico |
| bc, bq, by | Fattori di inclinazione del piano di posa |
| sc, sq, sy | Fattori di forma della fondazione |
| pc, pq, py | Fattori di riduzione per punzonamento secondo Vesic |
| Re | Fattore di riduzione capacità portante per eccentricità secondo Meyerhof |
| Ir, Irc | Indici di rigidezza per punzonamento secondo Vesic |
| ry fattore | Fattori per tener conto dell'effetto piastra. Per fondazioni che hanno larghezza maggiore di 2 m, il terzo termine della formula trinomia $0.5B\gamma N_c$ viene moltiplicato per questo fattore |
| D | Affondamento del piano di posa, espresso in [m] |
| B' | Larghezza fondazione ridotta, espresso in [m] |
| H | Altezza del cuneo di rottura, espresso in [m] |
| γ | Peso di volume del terreno medio, espresso in [kN/mc] |
| ϕ | Angolo di attrito del terreno medio, espresso in [°] |
| c | Coesione del terreno medio, espresso in [kPa] |

Per i coeff. che in tabella sono indicati con il simbolo '-' sono coeff. non presenti nel metodo scelto (Meyerhof).

| n° | Nc Nq Ny | ic iq iy | dc dq dy | gc gq gy | bc bq by | sc sq sy | pc pq py | Ir | Irc | Re | ry |
|----|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----|-----|----|-------|
| 1 | 28.838 | 0.677 | 1.062 | -- | -- | -- | -- | -- | -- | -- | 0.914 |
| | 17.277 | 0.677 | 1.031 | -- | -- | -- | -- | -- | -- | | |
| | 14.259 | 0.211 | 1.031 | -- | -- | -- | -- | -- | -- | | |
| 2 | 28.838 | 0.631 | 1.062 | -- | -- | -- | -- | -- | -- | -- | 0.914 |
| | 17.277 | 0.631 | 1.031 | -- | -- | -- | -- | -- | -- | | |
| | 14.259 | 0.138 | 1.031 | -- | -- | -- | -- | -- | -- | | |
| 3 | 28.838 | 0.610 | 1.062 | -- | -- | -- | -- | -- | -- | -- | 0.914 |
| | 17.277 | 0.610 | 1.031 | -- | -- | -- | -- | -- | -- | | |
| | 14.259 | 0.109 | 1.031 | -- | -- | -- | -- | -- | -- | | |

| n° | D [m] | B' [m] | H [m] | γ [°] | ϕ [kN/mc] | c [kPa] |
|----|----------|-----------|----------|-----------------|-------------------|------------|
| 1 | 0.80 | 3.55 | 3.77 | 11.28 | 29.44 | 0 |
| 2 | 0.80 | 3.32 | 3.77 | 11.28 | 29.44 | 0 |
| 3 | 0.80 | 3.21 | 3.77 | 11.28 | 29.44 | 0 |

Verifica a ribaltamento

Simbologia adottata

| | |
|----|--|
| n° | Indice combinazione |
| Ms | Momento stabilizzante, espresso in [kNm] |
| Mr | Momento ribaltante, espresso in [kNm] |
| FS | Fattore di sicurezza (rapporto tra momento stabilizzante e momento ribaltante) |

La verifica viene eseguita rispetto allo spigolo inferiore esterno della fondazione

| n° | Ms [kNm] | Mr [kNm] | FS |
|--------------------------|-------------|-------------|-------|
| 7 - EQU (A1-M1-R3) | 980.40 | 228.23 | 4.296 |
| 8 - EQU (A1-M1-R3) H + V | 1054.84 | 346.73 | 3.042 |
| 9 - EQU (A1-M1-R3) H - V | 971.87 | 410.97 | 2.365 |

Verifica stabilità globale muro + terreno

Simbologia adottata

Ic Indice/Tipo combinazione

C Centro superficie di scorrimento, espresso in [m]

R Raggio, espresso in [m]

FS Fattore di sicurezza

| Ic | C [m] | R [m] | FS |
|--------------------------|-------------|----------|-------|
| 4 - GEO (A2-M2-R2) | -1.00; 2.00 | 8.34 | 1.298 |
| 5 - GEO (A2-M2-R2) H + V | -1.00; 3.50 | 9.63 | 1.366 |
| 6 - GEO (A2-M2-R2) H - V | -1.50; 4.50 | 10.75 | 1.314 |

Dettagli strisce verifiche stabilità

Simbologia adottata

Le ascisse X sono considerate positive verso monte

Le ordinate Y sono considerate positive verso l'alto

Origine in testa al muro (spigolo contro terra)

W peso della striscia espresso in [kN]

Qy carico sulla striscia espresso in [kN]

α angolo fra la base della striscia e l'orizzontale espresso in [°] (positivo antiorario)

ϕ angolo d'attrito del terreno lungo la base della striscia

c coesione del terreno lungo la base della striscia espressa in [kPa]

b larghezza della striscia espressa in [m]

u pressione neutra lungo la base della striscia espressa in [kPa]

Tx; Ty Resistenza al taglio fornita dai tiranti in direzione X ed Y espressa in [kPa]

Combinazione n° 4 - GEO (A2-M2-R2)

| n° | W [kN] | Qy [kN] | b [m] | α [°] | ϕ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|-------------|-----------------|---------------|------------|------------|----------------|
| 1 | 8.00 | 14.09 | 7.11 - 0.55 | 70.210 | 29.256 | 0 | 0.0 | |

| n° | W [kN] | Qy [kN] | b [m] | α [°] | ϕ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|-----------------|---------------|------------|------------|----------------|
| 1 | 7.24 | 3.88 | 8.27 - 0.65 | 61.262 | 35.000 | 0 | 0.0 | |
| 2 | 20.18 | 3.88 | 0.65 | 55.089 | 35.000 | 0 | 0.0 | |
| 3 | 30.50 | 3.88 | 0.65 | 49.426 | 35.000 | 0 | 0.0 | |
| 4 | 39.02 | 3.88 | 0.65 | 44.364 | 35.000 | 0 | 0.0 | |
| 5 | 46.21 | 3.88 | 0.65 | 39.712 | 35.000 | 0 | 0.0 | |
| 6 | 52.32 | 3.88 | 0.65 | 35.357 | 35.000 | 0 | 0.0 | |
| 7 | 57.55 | 3.88 | 0.65 | 31.228 | 35.000 | 0 | 0.0 | |
| 8 | 64.21 | 1.47 | 0.65 | 27.273 | 25.000 | 0 | 0.0 | |
| 9 | 68.63 | 1.29 | 0.65 | 23.455 | 25.000 | 0 | 0.0 | |
| 10 | 71.78 | 1.29 | 0.65 | 19.744 | 25.000 | 0 | 0.0 | |
| 11 | 74.35 | 1.29 | 0.65 | 16.119 | 25.000 | 0 | 0.7 | |
| 12 | 76.38 | 1.29 | 0.65 | 12.559 | 25.000 | 0 | 2.3 | |
| 13 | 84.50 | 0.03 | 0.65 | 9.047 | 25.000 | 0 | 3.5 | |
| 14 | 55.00 | 0.00 | 0.65 | 5.570 | 25.000 | 0 | 4.3 | |
| 15 | 25.70 | 0.00 | 0.65 | 2.114 | 25.000 | 0 | 4.8 | |
| 16 | 25.67 | 0.00 | 0.65 | -1.335 | 25.000 | 0 | 4.8 | |
| 17 | 25.25 | 0.00 | 0.65 | -4.789 | 25.000 | 0 | 4.5 | |
| 18 | 24.34 | 0.00 | 0.65 | -8.261 | 25.000 | 0 | 3.7 | |
| 19 | 22.93 | 0.00 | 0.65 | -11.763 | 25.000 | 0 | 2.6 | |
| 20 | 21.02 | 0.00 | 0.65 | -15.311 | 25.000 | 0 | 1.1 | |
| 21 | 18.57 | 0.00 | 0.65 | -18.920 | 25.000 | 0 | 0.0 | |
| 22 | 15.56 | 0.00 | 0.65 | -22.609 | 25.000 | 0 | 0.0 | |
| 23 | 11.93 | 0.00 | 0.65 | -26.401 | 25.000 | 0 | 0.0 | |
| 24 | 7.64 | 0.00 | 0.65 | -30.322 | 25.000 | 0 | 0.0 | |
| 25 | 2.59 | 0.00 | -7.89 - 0.65 | -33.787 | 25.000 | 0 | 0.0 | |

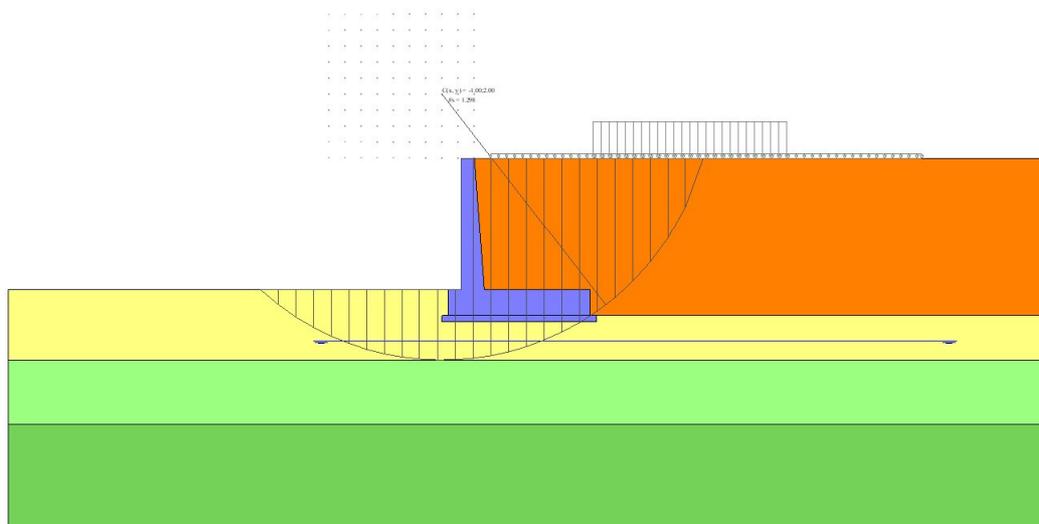


Fig. 7 - Stabilità fronte di scavo - Cerchio critico (Combinazione n° 4)

Spostamenti

Simbologia adottata

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
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Cmb Tipo combinazione
 $a_{g,crit}$ accelerazione critica, espressa in $[m/s^2]$
Dmax Spostamento orizzontale massimo, espressa in [cm]

| Cmb | $a_{g,crit}$ [m/s^2] | Dmax [cm] |
|-----------------|-----------------------------|--------------|
| 13 - SLEQ H + V | 1.7814 | 0.0014 |

Sollecitazioni

Elementi calcolati a trave

Simbologia adottata

N Sforzo normale, espresso in [kN]. Positivo se di compressione.
T Taglio, espresso in [kN]. Positivo se diretto da monte verso valle
M Momento, espresso in [kNm]. Positivo se tende le fibre contro terra (a monte)

Paramento

Combinazione n° 1 - STR (A1-M1-R3)

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.98 | 0.04 | 0.00 |
| 3 | -0.20 | 1.97 | 0.15 | 0.02 |
| 4 | -0.30 | 2.99 | 0.33 | 0.05 |
| 5 | -0.40 | 4.02 | 0.58 | 0.11 |
| 6 | -0.49 | 5.07 | 0.90 | 0.20 |
| 7 | -0.59 | 6.13 | 1.30 | 0.32 |
| 8 | -0.69 | 7.22 | 1.78 | 0.50 |
| 9 | -0.79 | 8.32 | 2.34 | 0.73 |
| 10 | -0.89 | 9.44 | 2.99 | 1.03 |
| 11 | -0.99 | 10.58 | 3.74 | 1.39 |
| 12 | -1.09 | 11.74 | 4.57 | 1.85 |
| 13 | -1.19 | 12.91 | 5.48 | 2.39 |
| 14 | -1.28 | 14.10 | 6.46 | 3.03 |
| 15 | -1.38 | 15.31 | 7.52 | 3.77 |
| 16 | -1.48 | 16.54 | 8.64 | 4.63 |
| 17 | -1.58 | 17.78 | 9.84 | 5.60 |
| 18 | -1.68 | 19.04 | 11.12 | 6.70 |
| 19 | -1.78 | 20.32 | 12.46 | 7.94 |
| 20 | -1.88 | 21.62 | 13.88 | 9.32 |
| 21 | -1.98 | 22.94 | 15.37 | 10.84 |
| 22 | -2.08 | 24.27 | 16.93 | 12.53 |
| 23 | -2.17 | 25.62 | 18.57 | 14.37 |
| 24 | -2.27 | 26.99 | 20.28 | 16.39 |
| 25 | -2.37 | 28.38 | 22.06 | 18.58 |
| 26 | -2.47 | 29.78 | 23.91 | 20.96 |
| 27 | -2.57 | 31.21 | 25.83 | 23.53 |
| 28 | -2.67 | 32.65 | 27.83 | 26.29 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 29 | -2.77 | 34.11 | 29.89 | 29.27 |
| 30 | -2.87 | 35.58 | 32.03 | 32.45 |
| 31 | -2.96 | 37.07 | 34.24 | 35.86 |
| 32 | -3.06 | 38.59 | 36.53 | 39.49 |
| 33 | -3.16 | 40.12 | 38.88 | 43.36 |
| 34 | -3.26 | 41.66 | 41.31 | 47.48 |
| 35 | -3.36 | 43.23 | 43.81 | 51.84 |
| 36 | -3.46 | 44.81 | 46.38 | 56.45 |
| 37 | -3.56 | 46.41 | 49.02 | 61.33 |
| 38 | -3.66 | 48.03 | 51.74 | 66.48 |
| 39 | -3.75 | 49.67 | 54.53 | 71.91 |
| 40 | -3.85 | 51.32 | 57.39 | 77.63 |
| 41 | -3.95 | 52.99 | 60.32 | 83.63 |
| 42 | -4.05 | 54.68 | 63.32 | 89.94 |
| 43 | -4.15 | 56.39 | 66.40 | 96.55 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.98 | 0.16 | 0.01 |
| 3 | -0.20 | 1.97 | 0.41 | 0.04 |
| 4 | -0.30 | 2.99 | 0.72 | 0.11 |
| 5 | -0.40 | 4.02 | 1.12 | 0.21 |
| 6 | -0.49 | 5.07 | 1.58 | 0.36 |
| 7 | -0.59 | 6.13 | 2.13 | 0.56 |
| 8 | -0.69 | 7.22 | 2.76 | 0.83 |
| 9 | -0.79 | 8.32 | 3.47 | 1.16 |
| 10 | -0.89 | 9.44 | 4.27 | 1.58 |
| 11 | -0.99 | 10.58 | 5.16 | 2.08 |
| 12 | -1.09 | 11.74 | 6.14 | 2.68 |
| 13 | -1.19 | 12.91 | 7.19 | 3.38 |
| 14 | -1.28 | 14.10 | 8.32 | 4.20 |
| 15 | -1.38 | 15.31 | 9.53 | 5.13 |
| 16 | -1.48 | 16.54 | 10.82 | 6.19 |
| 17 | -1.58 | 17.78 | 12.19 | 7.39 |
| 18 | -1.68 | 19.04 | 13.63 | 8.74 |
| 19 | -1.78 | 20.32 | 15.14 | 10.23 |
| 20 | -1.88 | 21.62 | 16.74 | 11.88 |
| 21 | -1.98 | 22.94 | 18.41 | 13.70 |
| 22 | -2.08 | 24.27 | 20.15 | 15.69 |
| 23 | -2.17 | 25.62 | 21.98 | 17.86 |
| 24 | -2.27 | 26.99 | 23.88 | 20.22 |
| 25 | -2.37 | 28.38 | 25.85 | 22.78 |
| 26 | -2.47 | 29.78 | 27.90 | 25.54 |
| 27 | -2.57 | 31.21 | 30.03 | 28.52 |
| 28 | -2.67 | 32.65 | 32.23 | 31.71 |
| 29 | -2.77 | 34.11 | 34.51 | 35.13 |
| 30 | -2.87 | 35.58 | 36.87 | 38.78 |
| 31 | -2.96 | 37.07 | 39.30 | 42.68 |
| 32 | -3.06 | 38.59 | 41.81 | 46.82 |
| 33 | -3.16 | 40.12 | 44.40 | 51.23 |
| 34 | -3.26 | 41.66 | 47.06 | 55.90 |
| 35 | -3.36 | 43.23 | 49.80 | 60.84 |
| 36 | -3.46 | 44.81 | 52.61 | 66.06 |
| 37 | -3.56 | 46.41 | 55.50 | 71.56 |
| 38 | -3.66 | 48.03 | 58.47 | 77.37 |
| 39 | -3.75 | 49.67 | 61.51 | 83.47 |
| 40 | -3.85 | 51.32 | 64.63 | 89.89 |
| 41 | -3.95 | 52.99 | 67.83 | 96.63 |
| 42 | -4.05 | 54.68 | 71.10 | 103.69 |
| 43 | -4.15 | 56.39 | 74.45 | 111.08 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | X | N | T | M |
|----|-------|-------|-------|--------|
| | [m] | [kN] | [kN] | [kNm] |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.98 | 0.16 | 0.01 |
| 3 | -0.20 | 1.97 | 0.39 | 0.04 |
| 4 | -0.30 | 2.99 | 0.69 | 0.10 |
| 5 | -0.40 | 4.02 | 1.06 | 0.20 |
| 6 | -0.49 | 5.07 | 1.49 | 0.34 |
| 7 | -0.59 | 6.13 | 2.00 | 0.54 |
| 8 | -0.69 | 7.22 | 2.58 | 0.79 |
| 9 | -0.79 | 8.32 | 3.24 | 1.10 |
| 10 | -0.89 | 9.44 | 3.98 | 1.49 |
| 11 | -0.99 | 10.58 | 4.80 | 1.96 |
| 12 | -1.09 | 11.74 | 5.70 | 2.52 |
| 13 | -1.19 | 12.91 | 6.67 | 3.17 |
| 14 | -1.28 | 14.10 | 7.71 | 3.93 |
| 15 | -1.38 | 15.31 | 8.82 | 4.80 |
| 16 | -1.48 | 16.54 | 10.01 | 5.79 |
| 17 | -1.58 | 17.78 | 11.26 | 6.90 |
| 18 | -1.68 | 19.04 | 12.58 | 8.15 |
| 19 | -1.78 | 20.32 | 13.97 | 9.53 |
| 20 | -1.88 | 21.62 | 15.43 | 11.06 |
| 21 | -1.98 | 22.94 | 16.96 | 12.74 |
| 22 | -2.08 | 24.27 | 18.55 | 14.58 |
| 23 | -2.17 | 25.62 | 20.22 | 16.59 |
| 24 | -2.27 | 26.99 | 21.96 | 18.77 |
| 25 | -2.37 | 28.38 | 23.76 | 21.13 |
| 26 | -2.47 | 29.78 | 25.63 | 23.67 |
| 27 | -2.57 | 31.21 | 27.58 | 26.41 |
| 28 | -2.67 | 32.65 | 29.59 | 29.36 |
| 29 | -2.77 | 34.11 | 31.67 | 32.50 |
| 30 | -2.87 | 35.58 | 33.82 | 35.87 |
| 31 | -2.96 | 37.07 | 36.04 | 39.45 |
| 32 | -3.06 | 38.59 | 38.33 | 43.26 |
| 33 | -3.16 | 40.12 | 40.68 | 47.31 |
| 34 | -3.26 | 41.66 | 43.11 | 51.60 |
| 35 | -3.36 | 43.23 | 45.60 | 56.14 |
| 36 | -3.46 | 44.81 | 48.17 | 60.93 |
| 37 | -3.56 | 46.41 | 50.80 | 65.99 |
| 38 | -3.66 | 48.03 | 53.50 | 71.31 |
| 39 | -3.75 | 49.67 | 56.27 | 76.91 |
| 40 | -3.85 | 51.32 | 59.11 | 82.80 |
| 41 | -3.95 | 52.99 | 62.02 | 88.98 |
| 42 | -4.05 | 54.68 | 65.00 | 95.45 |
| 43 | -4.15 | 56.39 | 68.04 | 102.22 |

Combinazione n° 10 - SLER

| n° | X | N | T | M |
|----|-------|------|------|-------|
| | [m] | [kN] | [kN] | [kNm] |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.98 | 0.03 | 0.00 |
| 3 | -0.20 | 1.97 | 0.11 | 0.01 |
| 4 | -0.30 | 2.99 | 0.25 | 0.04 |
| 5 | -0.40 | 4.02 | 0.45 | 0.09 |
| 6 | -0.49 | 5.07 | 0.69 | 0.16 |
| 7 | -0.59 | 6.13 | 1.00 | 0.26 |
| 8 | -0.69 | 7.22 | 1.36 | 0.41 |
| 9 | -0.79 | 8.32 | 1.80 | 0.59 |
| 10 | -0.89 | 9.44 | 2.29 | 0.82 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 11 | -0.99 | 10.58 | 2.86 | 1.11 |
| 12 | -1.09 | 11.74 | 3.49 | 1.47 |
| 13 | -1.19 | 12.91 | 4.18 | 1.89 |
| 14 | -1.28 | 14.10 | 4.93 | 2.39 |
| 15 | -1.38 | 15.31 | 5.73 | 2.97 |
| 16 | -1.48 | 16.54 | 6.59 | 3.64 |
| 17 | -1.58 | 17.78 | 7.51 | 4.40 |
| 18 | -1.68 | 19.04 | 8.48 | 5.25 |
| 19 | -1.78 | 20.32 | 9.50 | 6.21 |
| 20 | -1.88 | 21.62 | 10.59 | 7.28 |
| 21 | -1.98 | 22.94 | 11.72 | 8.47 |
| 22 | -2.08 | 24.27 | 12.92 | 9.77 |
| 23 | -2.17 | 25.62 | 14.17 | 11.20 |
| 24 | -2.27 | 26.99 | 15.47 | 12.76 |
| 25 | -2.37 | 28.38 | 16.83 | 14.46 |
| 26 | -2.47 | 29.78 | 18.24 | 16.30 |
| 27 | -2.57 | 31.21 | 19.71 | 18.28 |
| 28 | -2.67 | 32.65 | 21.24 | 20.42 |
| 29 | -2.77 | 34.11 | 22.82 | 22.72 |
| 30 | -2.87 | 35.58 | 24.46 | 25.18 |
| 31 | -2.96 | 37.07 | 26.15 | 27.82 |
| 32 | -3.06 | 38.59 | 27.90 | 30.63 |
| 33 | -3.16 | 40.12 | 29.70 | 33.62 |
| 34 | -3.26 | 41.66 | 31.56 | 36.79 |
| 35 | -3.36 | 43.23 | 33.47 | 40.16 |
| 36 | -3.46 | 44.81 | 35.44 | 43.73 |
| 37 | -3.56 | 46.41 | 37.47 | 47.50 |
| 38 | -3.66 | 48.03 | 39.55 | 51.47 |
| 39 | -3.75 | 49.67 | 41.68 | 55.67 |
| 40 | -3.85 | 51.32 | 43.87 | 60.08 |
| 41 | -3.95 | 52.99 | 46.12 | 64.71 |
| 42 | -4.05 | 54.68 | 48.42 | 69.58 |
| 43 | -4.15 | 56.39 | 50.78 | 74.69 |

Combinazione n° 11 - SLEF

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.98 | 0.03 | 0.00 |
| 3 | -0.20 | 1.97 | 0.11 | 0.01 |
| 4 | -0.30 | 2.99 | 0.25 | 0.04 |
| 5 | -0.40 | 4.02 | 0.45 | 0.09 |
| 6 | -0.49 | 5.07 | 0.69 | 0.16 |
| 7 | -0.59 | 6.13 | 1.00 | 0.26 |
| 8 | -0.69 | 7.22 | 1.36 | 0.41 |
| 9 | -0.79 | 8.32 | 1.80 | 0.59 |
| 10 | -0.89 | 9.44 | 2.29 | 0.82 |
| 11 | -0.99 | 10.58 | 2.86 | 1.11 |
| 12 | -1.09 | 11.74 | 3.49 | 1.47 |
| 13 | -1.19 | 12.91 | 4.18 | 1.89 |
| 14 | -1.28 | 14.10 | 4.93 | 2.39 |
| 15 | -1.38 | 15.31 | 5.73 | 2.97 |
| 16 | -1.48 | 16.54 | 6.59 | 3.64 |
| 17 | -1.58 | 17.78 | 7.51 | 4.40 |
| 18 | -1.68 | 19.04 | 8.48 | 5.25 |
| 19 | -1.78 | 20.32 | 9.50 | 6.21 |
| 20 | -1.88 | 21.62 | 10.59 | 7.28 |
| 21 | -1.98 | 22.94 | 11.72 | 8.47 |
| 22 | -2.08 | 24.27 | 12.92 | 9.77 |
| 23 | -2.17 | 25.62 | 14.17 | 11.20 |
| 24 | -2.27 | 26.99 | 15.47 | 12.76 |
| 25 | -2.37 | 28.38 | 16.83 | 14.46 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 26 | -2.47 | 29.78 | 18.24 | 16.30 |
| 27 | -2.57 | 31.21 | 19.71 | 18.28 |
| 28 | -2.67 | 32.65 | 21.24 | 20.42 |
| 29 | -2.77 | 34.11 | 22.82 | 22.72 |
| 30 | -2.87 | 35.58 | 24.46 | 25.18 |
| 31 | -2.96 | 37.07 | 26.15 | 27.82 |
| 32 | -3.06 | 38.59 | 27.90 | 30.63 |
| 33 | -3.16 | 40.12 | 29.70 | 33.62 |
| 34 | -3.26 | 41.66 | 31.56 | 36.79 |
| 35 | -3.36 | 43.23 | 33.47 | 40.16 |
| 36 | -3.46 | 44.81 | 35.44 | 43.73 |
| 37 | -3.56 | 46.41 | 37.47 | 47.50 |
| 38 | -3.66 | 48.03 | 39.55 | 51.47 |
| 39 | -3.75 | 49.67 | 41.68 | 55.67 |
| 40 | -3.85 | 51.32 | 43.87 | 60.08 |
| 41 | -3.95 | 52.99 | 46.12 | 64.71 |
| 42 | -4.05 | 54.68 | 48.42 | 69.58 |
| 43 | -4.15 | 56.39 | 50.78 | 74.69 |

Combinazione n° 12 - SLEQ

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.98 | 0.03 | 0.00 |
| 3 | -0.20 | 1.97 | 0.11 | 0.01 |
| 4 | -0.30 | 2.99 | 0.25 | 0.04 |
| 5 | -0.40 | 4.02 | 0.45 | 0.09 |
| 6 | -0.49 | 5.07 | 0.69 | 0.16 |
| 7 | -0.59 | 6.13 | 1.00 | 0.26 |
| 8 | -0.69 | 7.22 | 1.36 | 0.41 |
| 9 | -0.79 | 8.32 | 1.80 | 0.59 |
| 10 | -0.89 | 9.44 | 2.29 | 0.82 |
| 11 | -0.99 | 10.58 | 2.86 | 1.11 |
| 12 | -1.09 | 11.74 | 3.49 | 1.47 |
| 13 | -1.19 | 12.91 | 4.18 | 1.89 |
| 14 | -1.28 | 14.10 | 4.93 | 2.39 |
| 15 | -1.38 | 15.31 | 5.73 | 2.97 |
| 16 | -1.48 | 16.54 | 6.59 | 3.64 |
| 17 | -1.58 | 17.78 | 7.51 | 4.40 |
| 18 | -1.68 | 19.04 | 8.48 | 5.25 |
| 19 | -1.78 | 20.32 | 9.50 | 6.21 |
| 20 | -1.88 | 21.62 | 10.59 | 7.28 |
| 21 | -1.98 | 22.94 | 11.72 | 8.47 |
| 22 | -2.08 | 24.27 | 12.92 | 9.77 |
| 23 | -2.17 | 25.62 | 14.17 | 11.20 |
| 24 | -2.27 | 26.99 | 15.47 | 12.76 |
| 25 | -2.37 | 28.38 | 16.83 | 14.46 |
| 26 | -2.47 | 29.78 | 18.24 | 16.30 |
| 27 | -2.57 | 31.21 | 19.71 | 18.28 |
| 28 | -2.67 | 32.65 | 21.24 | 20.42 |
| 29 | -2.77 | 34.11 | 22.82 | 22.72 |
| 30 | -2.87 | 35.58 | 24.46 | 25.18 |
| 31 | -2.96 | 37.07 | 26.15 | 27.82 |
| 32 | -3.06 | 38.59 | 27.90 | 30.63 |
| 33 | -3.16 | 40.12 | 29.70 | 33.62 |
| 34 | -3.26 | 41.66 | 31.56 | 36.79 |
| 35 | -3.36 | 43.23 | 33.47 | 40.16 |
| 36 | -3.46 | 44.81 | 35.44 | 43.73 |
| 37 | -3.56 | 46.41 | 37.47 | 47.50 |
| 38 | -3.66 | 48.03 | 39.55 | 51.47 |
| 39 | -3.75 | 49.67 | 41.68 | 55.67 |
| 40 | -3.85 | 51.32 | 43.87 | 60.08 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 41 | -3.95 | 52.99 | 46.12 | 64.71 |
| 42 | -4.05 | 54.68 | 48.42 | 69.58 |
| 43 | -4.15 | 56.39 | 50.78 | 74.69 |

Combinazione n° 13 - SLEQ_H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.98 | 0.11 | 0.01 |
| 3 | -0.20 | 1.97 | 0.28 | 0.03 |
| 4 | -0.30 | 2.99 | 0.52 | 0.08 |
| 5 | -0.40 | 4.02 | 0.83 | 0.16 |
| 6 | -0.49 | 5.07 | 1.21 | 0.28 |
| 7 | -0.59 | 6.13 | 1.65 | 0.44 |
| 8 | -0.69 | 7.22 | 2.17 | 0.65 |
| 9 | -0.79 | 8.32 | 2.76 | 0.92 |
| 10 | -0.89 | 9.44 | 3.43 | 1.26 |
| 11 | -0.99 | 10.58 | 4.18 | 1.67 |
| 12 | -1.09 | 11.74 | 5.01 | 2.16 |
| 13 | -1.19 | 12.91 | 5.91 | 2.75 |
| 14 | -1.28 | 14.10 | 6.88 | 3.43 |
| 15 | -1.38 | 15.31 | 7.91 | 4.21 |
| 16 | -1.48 | 16.54 | 9.01 | 5.11 |
| 17 | -1.58 | 17.78 | 10.19 | 6.12 |
| 18 | -1.68 | 19.04 | 11.42 | 7.25 |
| 19 | -1.78 | 20.32 | 12.73 | 8.52 |
| 20 | -1.88 | 21.62 | 14.10 | 9.92 |
| 21 | -1.98 | 22.94 | 15.54 | 11.47 |
| 22 | -2.08 | 24.27 | 17.05 | 13.16 |
| 23 | -2.17 | 25.62 | 18.63 | 15.02 |
| 24 | -2.27 | 26.99 | 20.27 | 17.03 |
| 25 | -2.37 | 28.38 | 21.98 | 19.22 |
| 26 | -2.47 | 29.78 | 23.76 | 21.59 |
| 27 | -2.57 | 31.21 | 25.60 | 24.14 |
| 28 | -2.67 | 32.65 | 27.51 | 26.88 |
| 29 | -2.77 | 34.11 | 29.49 | 29.82 |
| 30 | -2.87 | 35.58 | 31.53 | 32.96 |
| 31 | -2.96 | 37.07 | 33.65 | 36.31 |
| 32 | -3.06 | 38.59 | 35.83 | 39.88 |
| 33 | -3.16 | 40.12 | 38.07 | 43.68 |
| 34 | -3.26 | 41.66 | 40.39 | 47.70 |
| 35 | -3.36 | 43.23 | 42.77 | 51.97 |
| 36 | -3.46 | 44.81 | 45.22 | 56.47 |
| 37 | -3.56 | 46.41 | 47.73 | 61.23 |
| 38 | -3.66 | 48.03 | 50.32 | 66.25 |
| 39 | -3.75 | 49.67 | 52.97 | 71.53 |
| 40 | -3.85 | 51.32 | 55.69 | 77.09 |
| 41 | -3.95 | 52.99 | 58.47 | 82.92 |
| 42 | -4.05 | 54.68 | 61.32 | 89.03 |
| 43 | -4.15 | 56.39 | 64.24 | 95.44 |

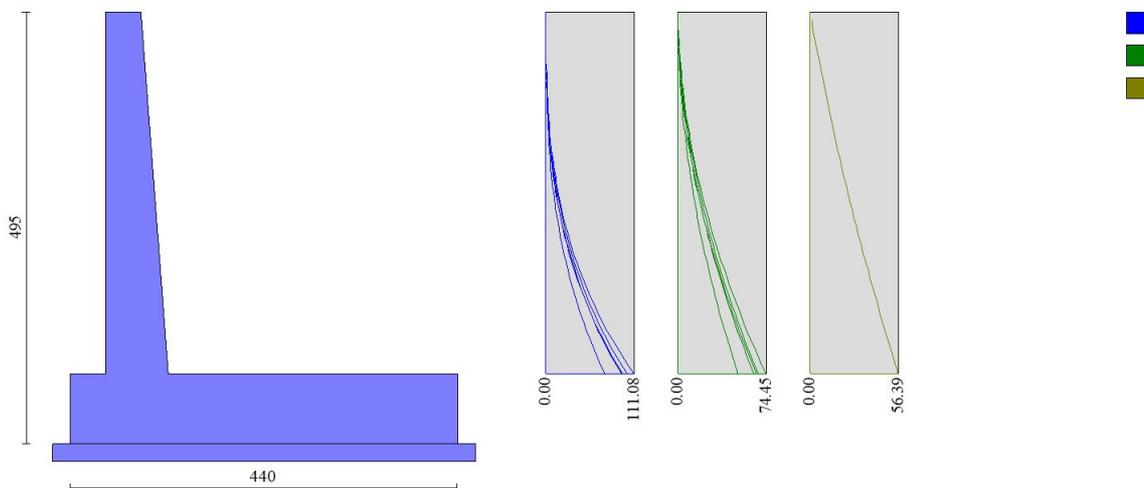


Fig. 8 - Paramento (Inviluppo)

Fondazione

Combinazione n° 1 - STR (A1-M1-R3)

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -0.80 | 0.00 | 0.00 | 0.00 |
| 2 | -0.70 | 0.00 | 13.10 | 0.66 |
| 3 | -0.60 | 0.00 | 25.95 | 2.61 |
| 4 | -0.50 | 0.00 | 38.54 | 5.84 |
| 5 | -0.40 | 0.00 | 50.89 | 10.31 |
| 6 | 0.31 | 0.00 | -140.36 | -305.90 |
| 7 | 0.41 | 0.00 | -140.41 | -292.37 |
| 8 | 0.51 | 0.00 | -140.18 | -278.81 |
| 9 | 0.61 | 0.00 | -139.43 | -264.87 |
| 10 | 0.71 | 0.00 | -138.42 | -251.01 |
| 11 | 0.81 | 0.00 | -137.17 | -237.27 |
| 12 | 0.91 | 0.00 | -135.66 | -223.67 |
| 13 | 1.01 | 0.00 | -133.90 | -210.23 |
| 14 | 1.11 | 0.00 | -131.89 | -196.98 |
| 15 | 1.21 | 0.00 | -129.63 | -183.94 |
| 16 | 1.31 | 0.00 | -127.12 | -171.14 |
| 17 | 1.41 | 0.00 | -124.36 | -158.60 |
| 18 | 1.50 | 0.00 | -121.34 | -146.35 |
| 19 | 1.60 | 0.00 | -118.08 | -134.42 |
| 20 | 1.70 | 0.00 | -114.56 | -122.82 |
| 21 | 1.80 | 0.00 | -110.79 | -111.58 |
| 22 | 1.90 | 0.00 | -106.77 | -100.74 |
| 23 | 2.00 | 0.00 | -102.50 | -90.30 |
| 24 | 2.10 | 0.00 | -97.98 | -80.31 |
| 25 | 2.20 | 0.00 | -93.21 | -70.77 |
| 26 | 2.30 | 0.00 | -88.18 | -61.73 |
| 27 | 2.40 | 0.00 | -82.91 | -53.20 |
| 28 | 2.50 | 0.00 | -77.38 | -45.21 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 29 | 2.60 | 0.00 | -71.60 | -37.78 |
| 30 | 2.70 | 0.00 | -65.57 | -30.94 |
| 31 | 2.80 | 0.00 | -59.29 | -24.71 |
| 32 | 2.90 | 0.00 | -52.76 | -19.13 |
| 33 | 3.00 | 0.00 | -45.98 | -14.20 |
| 34 | 3.10 | 0.00 | -38.94 | -9.97 |
| 35 | 3.20 | 0.00 | -31.66 | -6.45 |
| 36 | 3.30 | 0.00 | -24.12 | -3.66 |
| 37 | 3.40 | 0.00 | -16.33 | -1.64 |
| 38 | 3.50 | 0.00 | -8.29 | -0.42 |
| 39 | 3.60 | 0.00 | 0.00 | 0.00 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -0.80 | 0.00 | 0.00 | 0.00 |
| 2 | -0.70 | 0.00 | 15.54 | 0.78 |
| 3 | -0.60 | 0.00 | 30.74 | 3.10 |
| 4 | -0.50 | 0.00 | 45.60 | 6.92 |
| 5 | -0.40 | 0.00 | 60.12 | 12.21 |
| 6 | 0.31 | 0.00 | -57.39 | -195.52 |
| 7 | 0.41 | 0.00 | -61.25 | -189.91 |
| 8 | 0.51 | 0.00 | -64.77 | -183.91 |
| 9 | 0.61 | 0.00 | -67.76 | -177.30 |
| 10 | 0.71 | 0.00 | -70.41 | -170.41 |
| 11 | 0.81 | 0.00 | -72.72 | -163.27 |
| 12 | 0.91 | 0.00 | -74.70 | -155.92 |
| 13 | 1.01 | 0.00 | -76.34 | -148.39 |
| 14 | 1.11 | 0.00 | -77.63 | -140.71 |
| 15 | 1.21 | 0.00 | -78.59 | -132.92 |
| 16 | 1.31 | 0.00 | -79.21 | -125.05 |
| 17 | 1.41 | 0.00 | -79.49 | -117.14 |
| 18 | 1.50 | 0.00 | -79.44 | -109.21 |
| 19 | 1.60 | 0.00 | -79.04 | -101.31 |
| 20 | 1.70 | 0.00 | -78.31 | -93.46 |
| 21 | 1.80 | 0.00 | -77.23 | -85.71 |
| 22 | 1.90 | 0.00 | -75.82 | -78.08 |
| 23 | 2.00 | 0.00 | -74.07 | -70.60 |
| 24 | 2.10 | 0.00 | -71.98 | -63.32 |
| 25 | 2.20 | 0.00 | -69.55 | -56.26 |
| 26 | 2.30 | 0.00 | -66.79 | -49.46 |
| 27 | 2.40 | 0.00 | -63.68 | -42.95 |
| 28 | 2.50 | 0.00 | -60.24 | -36.77 |
| 29 | 2.60 | 0.00 | -56.45 | -30.96 |
| 30 | 2.70 | 0.00 | -52.33 | -25.53 |
| 31 | 2.80 | 0.00 | -47.87 | -20.53 |
| 32 | 2.90 | 0.00 | -43.07 | -16.00 |
| 33 | 3.00 | 0.00 | -37.94 | -11.95 |
| 34 | 3.10 | 0.00 | -32.46 | -8.44 |
| 35 | 3.20 | 0.00 | -26.65 | -5.49 |
| 36 | 3.30 | 0.00 | -20.49 | -3.14 |
| 37 | 3.40 | 0.00 | -14.00 | -1.42 |
| 38 | 3.50 | 0.00 | -7.17 | -0.36 |
| 39 | 3.60 | 0.00 | 0.00 | 0.00 |

Combinazione n° 3 - STR (A1-M1-R3) H - V

| n° | X | N | T | M |
|----|---|---|---|---|
|----|---|---|---|---|

| | [m] | [kN] | [kN] | [kNm] |
|----|-------|------|---------|---------|
| 1 | -0.80 | 0.00 | 0.00 | 0.00 |
| 2 | -0.70 | 0.00 | 14.04 | 0.70 |
| 3 | -0.60 | 0.00 | 27.75 | 2.80 |
| 4 | -0.50 | 0.00 | 41.14 | 6.24 |
| 5 | -0.40 | 0.00 | 54.19 | 11.01 |
| 6 | 0.31 | 0.00 | -96.00 | -255.46 |
| 7 | 0.41 | 0.00 | -98.50 | -246.07 |
| 8 | 0.51 | 0.00 | -100.67 | -236.42 |
| 9 | 0.61 | 0.00 | -102.32 | -226.30 |
| 10 | 0.71 | 0.00 | -103.65 | -216.03 |
| 11 | 0.81 | 0.00 | -104.65 | -205.65 |
| 12 | 0.91 | 0.00 | -105.32 | -195.18 |
| 13 | 1.01 | 0.00 | -105.67 | -184.66 |
| 14 | 1.11 | 0.00 | -105.69 | -174.12 |
| 15 | 1.21 | 0.00 | -105.38 | -163.60 |
| 16 | 1.31 | 0.00 | -104.75 | -153.12 |
| 17 | 1.41 | 0.00 | -103.79 | -142.72 |
| 18 | 1.50 | 0.00 | -102.50 | -132.43 |
| 19 | 1.60 | 0.00 | -100.88 | -122.29 |
| 20 | 1.70 | 0.00 | -98.94 | -112.33 |
| 21 | 1.80 | 0.00 | -96.68 | -102.58 |
| 22 | 1.90 | 0.00 | -94.08 | -93.06 |
| 23 | 2.00 | 0.00 | -91.16 | -83.83 |
| 24 | 2.10 | 0.00 | -87.92 | -74.90 |
| 25 | 2.20 | 0.00 | -84.34 | -66.31 |
| 26 | 2.30 | 0.00 | -80.44 | -58.09 |
| 27 | 2.40 | 0.00 | -76.21 | -50.28 |
| 28 | 2.50 | 0.00 | -71.66 | -42.91 |
| 29 | 2.60 | 0.00 | -66.78 | -36.00 |
| 30 | 2.70 | 0.00 | -61.57 | -29.60 |
| 31 | 2.80 | 0.00 | -56.04 | -23.74 |
| 32 | 2.90 | 0.00 | -50.17 | -18.44 |
| 33 | 3.00 | 0.00 | -43.99 | -13.74 |
| 34 | 3.10 | 0.00 | -37.47 | -9.68 |
| 35 | 3.20 | 0.00 | -30.63 | -6.28 |
| 36 | 3.30 | 0.00 | -23.46 | -3.58 |
| 37 | 3.40 | 0.00 | -15.97 | -1.61 |
| 38 | 3.50 | 0.00 | -8.15 | -0.41 |
| 39 | 3.60 | 0.00 | 0.00 | 0.00 |

Combinazione n° 10 - SLER

| n° | X | N | T | M |
|----|-------|------|--------|---------|
| | [m] | [kN] | [kN] | [kNm] |
| 1 | -0.80 | 0.00 | 0.00 | 0.00 |
| 2 | -0.70 | 0.00 | 11.38 | 0.57 |
| 3 | -0.60 | 0.00 | 22.59 | 2.27 |
| 4 | -0.50 | 0.00 | 33.62 | 5.08 |
| 5 | -0.40 | 0.00 | 44.48 | 8.99 |
| 6 | 0.31 | 0.00 | -47.78 | -130.87 |
| 7 | 0.41 | 0.00 | -49.32 | -126.34 |
| 8 | 0.51 | 0.00 | -50.67 | -121.64 |
| 9 | 0.61 | 0.00 | -51.66 | -116.54 |
| 10 | 0.71 | 0.00 | -52.48 | -111.34 |
| 11 | 0.81 | 0.00 | -53.12 | -106.08 |
| 12 | 0.91 | 0.00 | -53.59 | -100.76 |
| 13 | 1.01 | 0.00 | -53.88 | -95.40 |
| 14 | 1.11 | 0.00 | -54.00 | -90.02 |
| 15 | 1.21 | 0.00 | -53.94 | -84.64 |
| 16 | 1.31 | 0.00 | -53.70 | -79.27 |
| 17 | 1.41 | 0.00 | -53.29 | -73.93 |
| 18 | 1.50 | 0.00 | -52.71 | -68.65 |
| 19 | 1.60 | 0.00 | -51.95 | -63.43 |
| 20 | 1.70 | 0.00 | -51.02 | -58.30 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 21 | 1.80 | 0.00 | -49.91 | -53.26 |
| 22 | 1.90 | 0.00 | -48.62 | -48.35 |
| 23 | 2.00 | 0.00 | -47.16 | -43.57 |
| 24 | 2.10 | 0.00 | -45.53 | -38.95 |
| 25 | 2.20 | 0.00 | -43.72 | -34.50 |
| 26 | 2.30 | 0.00 | -41.73 | -30.24 |
| 27 | 2.40 | 0.00 | -39.57 | -26.19 |
| 28 | 2.50 | 0.00 | -37.24 | -22.36 |
| 29 | 2.60 | 0.00 | -34.73 | -18.77 |
| 30 | 2.70 | 0.00 | -32.04 | -15.44 |
| 31 | 2.80 | 0.00 | -29.18 | -12.38 |
| 32 | 2.90 | 0.00 | -26.15 | -9.62 |
| 33 | 3.00 | 0.00 | -22.94 | -7.18 |
| 34 | 3.10 | 0.00 | -19.55 | -5.06 |
| 35 | 3.20 | 0.00 | -15.99 | -3.28 |
| 36 | 3.30 | 0.00 | -12.26 | -1.87 |
| 37 | 3.40 | 0.00 | -8.35 | -0.84 |
| 38 | 3.50 | 0.00 | -4.26 | -0.21 |
| 39 | 3.60 | 0.00 | 0.00 | 0.00 |

Combinazione n° 11 - SLEF

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 1 | -0.80 | 0.00 | 0.00 | 0.00 |
| 2 | -0.70 | 0.00 | 11.38 | 0.57 |
| 3 | -0.60 | 0.00 | 22.59 | 2.27 |
| 4 | -0.50 | 0.00 | 33.62 | 5.08 |
| 5 | -0.40 | 0.00 | 44.48 | 8.99 |
| 6 | 0.31 | 0.00 | -47.78 | -130.87 |
| 7 | 0.41 | 0.00 | -49.32 | -126.34 |
| 8 | 0.51 | 0.00 | -50.67 | -121.64 |
| 9 | 0.61 | 0.00 | -51.66 | -116.54 |
| 10 | 0.71 | 0.00 | -52.48 | -111.34 |
| 11 | 0.81 | 0.00 | -53.12 | -106.08 |
| 12 | 0.91 | 0.00 | -53.59 | -100.76 |
| 13 | 1.01 | 0.00 | -53.88 | -95.40 |
| 14 | 1.11 | 0.00 | -54.00 | -90.02 |
| 15 | 1.21 | 0.00 | -53.94 | -84.64 |
| 16 | 1.31 | 0.00 | -53.70 | -79.27 |
| 17 | 1.41 | 0.00 | -53.29 | -73.93 |
| 18 | 1.50 | 0.00 | -52.71 | -68.65 |
| 19 | 1.60 | 0.00 | -51.95 | -63.43 |
| 20 | 1.70 | 0.00 | -51.02 | -58.30 |
| 21 | 1.80 | 0.00 | -49.91 | -53.26 |
| 22 | 1.90 | 0.00 | -48.62 | -48.35 |
| 23 | 2.00 | 0.00 | -47.16 | -43.57 |
| 24 | 2.10 | 0.00 | -45.53 | -38.95 |
| 25 | 2.20 | 0.00 | -43.72 | -34.50 |
| 26 | 2.30 | 0.00 | -41.73 | -30.24 |
| 27 | 2.40 | 0.00 | -39.57 | -26.19 |
| 28 | 2.50 | 0.00 | -37.24 | -22.36 |
| 29 | 2.60 | 0.00 | -34.73 | -18.77 |
| 30 | 2.70 | 0.00 | -32.04 | -15.44 |
| 31 | 2.80 | 0.00 | -29.18 | -12.38 |
| 32 | 2.90 | 0.00 | -26.15 | -9.62 |
| 33 | 3.00 | 0.00 | -22.94 | -7.18 |
| 34 | 3.10 | 0.00 | -19.55 | -5.06 |
| 35 | 3.20 | 0.00 | -15.99 | -3.28 |
| 36 | 3.30 | 0.00 | -12.26 | -1.87 |
| 37 | 3.40 | 0.00 | -8.35 | -0.84 |
| 38 | 3.50 | 0.00 | -4.26 | -0.21 |
| 39 | 3.60 | 0.00 | 0.00 | 0.00 |

Combinazione n° 12 - SLEQ

| n° | X | N | T | M |
|----|-------|------|--------|---------|
| | [m] | [kN] | [kN] | [kNm] |
| 1 | -0.80 | 0.00 | 0.00 | 0.00 |
| 2 | -0.70 | 0.00 | 11.38 | 0.57 |
| 3 | -0.60 | 0.00 | 22.59 | 2.27 |
| 4 | -0.50 | 0.00 | 33.62 | 5.08 |
| 5 | -0.40 | 0.00 | 44.48 | 8.99 |
| 6 | 0.31 | 0.00 | -47.78 | -130.87 |
| 7 | 0.41 | 0.00 | -49.32 | -126.34 |
| 8 | 0.51 | 0.00 | -50.67 | -121.64 |
| 9 | 0.61 | 0.00 | -51.66 | -116.54 |
| 10 | 0.71 | 0.00 | -52.48 | -111.34 |
| 11 | 0.81 | 0.00 | -53.12 | -106.08 |
| 12 | 0.91 | 0.00 | -53.59 | -100.76 |
| 13 | 1.01 | 0.00 | -53.88 | -95.40 |
| 14 | 1.11 | 0.00 | -54.00 | -90.02 |
| 15 | 1.21 | 0.00 | -53.94 | -84.64 |
| 16 | 1.31 | 0.00 | -53.70 | -79.27 |
| 17 | 1.41 | 0.00 | -53.29 | -73.93 |
| 18 | 1.50 | 0.00 | -52.71 | -68.65 |
| 19 | 1.60 | 0.00 | -51.95 | -63.43 |
| 20 | 1.70 | 0.00 | -51.02 | -58.30 |
| 21 | 1.80 | 0.00 | -49.91 | -53.26 |
| 22 | 1.90 | 0.00 | -48.62 | -48.35 |
| 23 | 2.00 | 0.00 | -47.16 | -43.57 |
| 24 | 2.10 | 0.00 | -45.53 | -38.95 |
| 25 | 2.20 | 0.00 | -43.72 | -34.50 |
| 26 | 2.30 | 0.00 | -41.73 | -30.24 |
| 27 | 2.40 | 0.00 | -39.57 | -26.19 |
| 28 | 2.50 | 0.00 | -37.24 | -22.36 |
| 29 | 2.60 | 0.00 | -34.73 | -18.77 |
| 30 | 2.70 | 0.00 | -32.04 | -15.44 |
| 31 | 2.80 | 0.00 | -29.18 | -12.38 |
| 32 | 2.90 | 0.00 | -26.15 | -9.62 |
| 33 | 3.00 | 0.00 | -22.94 | -7.18 |
| 34 | 3.10 | 0.00 | -19.55 | -5.06 |
| 35 | 3.20 | 0.00 | -15.99 | -3.28 |
| 36 | 3.30 | 0.00 | -12.26 | -1.87 |
| 37 | 3.40 | 0.00 | -8.35 | -0.84 |
| 38 | 3.50 | 0.00 | -4.26 | -0.21 |
| 39 | 3.60 | 0.00 | 0.00 | 0.00 |

Combinazione n° 13 - SLEQ H + V

| n° | X | N | T | M |
|----|-------|------|--------|---------|
| | [m] | [kN] | [kN] | [kNm] |
| 1 | -0.80 | 0.00 | 0.00 | 0.00 |
| 2 | -0.70 | 0.00 | 14.85 | 0.75 |
| 3 | -0.60 | 0.00 | 29.39 | 2.96 |
| 4 | -0.50 | 0.00 | 43.60 | 6.61 |
| 5 | -0.40 | 0.00 | 57.49 | 11.67 |
| 6 | 0.31 | 0.00 | -62.27 | -197.64 |
| 7 | 0.41 | 0.00 | -65.67 | -191.57 |
| 8 | 0.51 | 0.00 | -68.74 | -185.15 |
| 9 | 0.61 | 0.00 | -71.31 | -178.17 |
| 10 | 0.71 | 0.00 | -73.55 | -170.94 |
| 11 | 0.81 | 0.00 | -75.48 | -163.51 |
| 12 | 0.91 | 0.00 | -77.09 | -155.90 |
| 13 | 1.01 | 0.00 | -78.38 | -148.15 |
| 14 | 1.11 | 0.00 | -79.35 | -140.28 |

| n° | X [m] | N [kN] | T [kN] | M [kNm] |
|----|----------|-----------|-----------|------------|
| 15 | 1.21 | 0.00 | -80.00 | -132.34 |
| 16 | 1.31 | 0.00 | -80.34 | -124.34 |
| 17 | 1.41 | 0.00 | -80.35 | -116.33 |
| 18 | 1.50 | 0.00 | -80.05 | -108.33 |
| 19 | 1.60 | 0.00 | -79.43 | -100.38 |
| 20 | 1.70 | 0.00 | -78.48 | -92.51 |
| 21 | 1.80 | 0.00 | -77.22 | -84.74 |
| 22 | 1.90 | 0.00 | -75.64 | -77.12 |
| 23 | 2.00 | 0.00 | -73.74 | -69.67 |
| 24 | 2.10 | 0.00 | -71.53 | -62.42 |
| 25 | 2.20 | 0.00 | -68.99 | -55.42 |
| 26 | 2.30 | 0.00 | -66.14 | -48.68 |
| 27 | 2.40 | 0.00 | -62.96 | -42.24 |
| 28 | 2.50 | 0.00 | -59.47 | -36.13 |
| 29 | 2.60 | 0.00 | -55.66 | -30.39 |
| 30 | 2.70 | 0.00 | -51.53 | -25.05 |
| 31 | 2.80 | 0.00 | -47.08 | -20.13 |
| 32 | 2.90 | 0.00 | -42.31 | -15.67 |
| 33 | 3.00 | 0.00 | -37.22 | -11.70 |
| 34 | 3.10 | 0.00 | -31.81 | -8.26 |
| 35 | 3.20 | 0.00 | -26.09 | -5.37 |
| 36 | 3.30 | 0.00 | -20.05 | -3.07 |
| 37 | 3.40 | 0.00 | -13.68 | -1.39 |
| 38 | 3.50 | 0.00 | -7.00 | -0.35 |
| 39 | 3.60 | 0.00 | 0.00 | 0.00 |

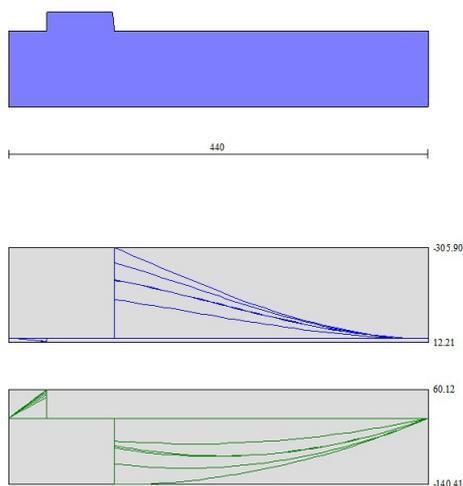


Fig. 9 - Fondazione (Inviluppo)

Verifiche a flessione

Elementi calcolati a trave

Simbologia adottata

| | |
|-----|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Afi | area ferri inferiori espresso in [cmq] |
| Afs | area ferri superiori espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| N | sforzo normale agente espressa in [kN] |
| Mu | momento ultimi espresso in [kNm] |
| Nu | sforzo normale ultimo espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione ultima e sollecitazione agente) |

Paramento

Combinazione n° 1 - STR (A1-M1-R3)

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | 0.00 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | -0.10 | 100 | 41 | 15.71 | 15.71 | 0.00 | 0.98 | 0.00 | 0.00 | 100000.000 |
| 3 | -0.20 | 100 | 41 | 15.71 | 15.71 | 0.02 | 1.97 | 63.61 | 7470.61 | 3785.296 |
| 4 | -0.30 | 100 | 42 | 15.71 | 15.71 | 0.05 | 2.99 | 123.56 | 7581.13 | 2537.987 |
| 5 | -0.40 | 100 | 43 | 15.71 | 15.71 | 0.11 | 4.02 | 202.41 | 7691.64 | 1914.140 |
| 6 | -0.49 | 100 | 44 | 15.71 | 15.71 | 0.20 | 5.07 | 291.96 | 7583.52 | 1496.537 |
| 7 | -0.59 | 100 | 44 | 15.71 | 15.71 | 0.32 | 6.13 | 378.08 | 7160.70 | 1167.336 |
| 8 | -0.69 | 100 | 45 | 15.71 | 15.71 | 0.50 | 7.22 | 462.48 | 6682.89 | 925.755 |
| 9 | -0.79 | 100 | 46 | 15.71 | 15.71 | 0.73 | 8.32 | 541.19 | 6163.46 | 740.688 |
| 10 | -0.89 | 100 | 47 | 15.71 | 15.71 | 1.03 | 9.44 | 611.36 | 5626.02 | 595.884 |
| 11 | -0.99 | 100 | 47 | 15.71 | 15.71 | 1.39 | 10.58 | 671.97 | 5097.44 | 481.824 |
| 12 | -1.09 | 100 | 48 | 15.71 | 15.71 | 1.85 | 11.74 | 723.50 | 4600.48 | 392.023 |
| 13 | -1.19 | 100 | 49 | 15.71 | 15.71 | 2.39 | 12.91 | 765.89 | 4142.60 | 320.912 |
| 14 | -1.28 | 100 | 50 | 15.71 | 15.71 | 3.03 | 14.10 | 762.09 | 3551.86 | 251.902 |
| 15 | -1.38 | 100 | 50 | 15.71 | 15.71 | 3.77 | 15.31 | 739.90 | 3005.27 | 196.303 |
| 16 | -1.48 | 100 | 51 | 15.71 | 18.85 | 4.63 | 16.54 | 766.90 | 2741.76 | 165.803 |
| 17 | -1.58 | 100 | 52 | 15.71 | 18.85 | 5.60 | 17.78 | 735.60 | 2335.18 | 131.330 |
| 18 | -1.68 | 100 | 52 | 15.71 | 18.85 | 6.70 | 19.04 | 699.86 | 1988.11 | 104.398 |
| 19 | -1.78 | 100 | 53 | 15.71 | 18.85 | 7.94 | 20.32 | 670.13 | 1715.21 | 84.394 |
| 20 | -1.88 | 100 | 54 | 15.71 | 18.85 | 9.32 | 21.62 | 638.54 | 1481.62 | 68.524 |
| 21 | -1.98 | 100 | 55 | 15.71 | 18.85 | 10.84 | 22.94 | 614.26 | 1299.20 | 56.640 |
| 22 | -2.08 | 100 | 55 | 15.71 | 18.85 | 12.53 | 24.27 | 592.47 | 1147.93 | 47.296 |
| 23 | -2.17 | 100 | 56 | 15.71 | 18.85 | 14.37 | 25.62 | 575.20 | 1025.49 | 40.022 |
| 24 | -2.27 | 100 | 57 | 15.71 | 18.85 | 16.39 | 26.99 | 562.24 | 926.09 | 34.310 |
| 25 | -2.37 | 100 | 58 | 15.71 | 18.85 | 18.58 | 28.38 | 552.49 | 843.89 | 29.736 |
| 26 | -2.47 | 100 | 58 | 15.71 | 18.85 | 20.96 | 29.78 | 545.21 | 774.87 | 26.017 |

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | -0.80 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | -0.70 | 100 | 80 | 18.85 | 18.85 | 0.66 | 0.00 | 520.00 | 0.00 | 791.323 |
| 3 | -0.60 | 100 | 80 | 18.85 | 18.85 | 2.61 | 0.00 | 520.00 | 0.00 | 199.107 |
| 4 | -0.50 | 100 | 80 | 18.85 | 18.85 | 5.84 | 0.00 | 520.00 | 0.00 | 89.067 |
| 5 | -0.40 | 100 | 80 | 18.85 | 18.85 | 10.31 | 0.00 | 520.00 | 0.00 | 50.428 |
| 6 | 0.31 | 100 | 80 | 18.85 | 18.85 | -305.90 | 0.00 | -520.00 | 0.00 | 1.700 |
| 7 | 0.41 | 100 | 80 | 18.85 | 18.85 | -292.37 | 0.00 | -520.00 | 0.00 | 1.779 |
| 8 | 0.51 | 100 | 80 | 18.85 | 18.85 | -278.81 | 0.00 | -520.00 | 0.00 | 1.865 |
| 9 | 0.61 | 100 | 80 | 18.85 | 18.85 | -264.87 | 0.00 | -520.00 | 0.00 | 1.963 |
| 10 | 0.71 | 100 | 80 | 18.85 | 18.85 | -251.01 | 0.00 | -520.00 | 0.00 | 2.072 |
| 11 | 0.81 | 100 | 80 | 18.85 | 18.85 | -237.27 | 0.00 | -520.00 | 0.00 | 2.192 |
| 12 | 0.91 | 100 | 80 | 18.85 | 18.85 | -223.67 | 0.00 | -520.00 | 0.00 | 2.325 |
| 13 | 1.01 | 100 | 80 | 18.85 | 18.85 | -210.23 | 0.00 | -520.00 | 0.00 | 2.473 |
| 14 | 1.11 | 100 | 80 | 18.85 | 18.85 | -196.98 | 0.00 | -520.00 | 0.00 | 2.640 |
| 15 | 1.21 | 100 | 80 | 18.85 | 18.85 | -183.94 | 0.00 | -520.00 | 0.00 | 2.827 |
| 16 | 1.31 | 100 | 80 | 18.85 | 18.85 | -171.14 | 0.00 | -520.00 | 0.00 | 3.038 |
| 17 | 1.41 | 100 | 80 | 18.85 | 18.85 | -158.60 | 0.00 | -520.00 | 0.00 | 3.279 |
| 18 | 1.50 | 100 | 80 | 18.85 | 18.85 | -146.35 | 0.00 | -520.00 | 0.00 | 3.553 |
| 19 | 1.60 | 100 | 80 | 18.85 | 18.85 | -134.42 | 0.00 | -520.00 | 0.00 | 3.869 |
| 20 | 1.70 | 100 | 80 | 18.85 | 18.85 | -122.82 | 0.00 | -520.00 | 0.00 | 4.234 |
| 21 | 1.80 | 100 | 80 | 18.85 | 18.85 | -111.58 | 0.00 | -520.00 | 0.00 | 4.660 |
| 22 | 1.90 | 100 | 80 | 18.85 | 18.85 | -100.74 | 0.00 | -520.00 | 0.00 | 5.162 |
| 23 | 2.00 | 100 | 80 | 18.85 | 18.85 | -90.30 | 0.00 | -520.00 | 0.00 | 5.758 |
| 24 | 2.10 | 100 | 80 | 18.85 | 18.85 | -80.31 | 0.00 | -520.00 | 0.00 | 6.475 |
| 25 | 2.20 | 100 | 80 | 18.85 | 18.85 | -70.77 | 0.00 | -520.00 | 0.00 | 7.347 |
| 26 | 2.30 | 100 | 80 | 18.85 | 18.85 | -61.73 | 0.00 | -520.00 | 0.00 | 8.424 |
| 27 | 2.40 | 100 | 80 | 18.85 | 18.85 | -53.20 | 0.00 | -520.00 | 0.00 | 9.775 |
| 28 | 2.50 | 100 | 80 | 18.85 | 18.85 | -45.21 | 0.00 | -520.00 | 0.00 | 11.503 |
| 29 | 2.60 | 100 | 80 | 18.85 | 18.85 | -37.78 | 0.00 | -520.00 | 0.00 | 13.764 |
| 30 | 2.70 | 100 | 80 | 18.85 | 18.85 | -30.94 | 0.00 | -520.00 | 0.00 | 16.807 |
| 31 | 2.80 | 100 | 80 | 18.85 | 18.85 | -24.71 | 0.00 | -520.00 | 0.00 | 21.042 |
| 32 | 2.90 | 100 | 80 | 18.85 | 18.85 | -19.13 | 0.00 | -520.00 | 0.00 | 27.189 |
| 33 | 3.00 | 100 | 80 | 18.85 | 18.85 | -14.20 | 0.00 | -520.00 | 0.00 | 36.616 |
| 34 | 3.10 | 100 | 80 | 18.85 | 18.85 | -9.97 | 0.00 | -520.00 | 0.00 | 52.174 |
| 35 | 3.20 | 100 | 80 | 18.85 | 18.85 | -6.45 | 0.00 | -520.00 | 0.00 | 80.677 |
| 36 | 3.30 | 100 | 80 | 18.85 | 18.85 | -3.66 | 0.00 | -520.00 | 0.00 | 141.955 |
| 37 | 3.40 | 100 | 80 | 18.85 | 18.85 | -1.64 | 0.00 | -520.00 | 0.00 | 316.157 |
| 38 | 3.50 | 100 | 80 | 18.85 | 18.85 | -0.42 | 0.00 | -520.00 | 0.00 | 1251.916 |
| 39 | 3.60 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 1 | -0.80 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | -0.70 | 100 | 80 | 18.85 | 18.85 | 0.78 | 0.00 | 520.00 | 0.00 | 666.775 |
| 3 | -0.60 | 100 | 80 | 18.85 | 18.85 | 3.10 | 0.00 | 520.00 | 0.00 | 167.917 |
| 4 | -0.50 | 100 | 80 | 18.85 | 18.85 | 6.92 | 0.00 | 520.00 | 0.00 | 75.181 |
| 5 | -0.40 | 100 | 80 | 18.85 | 18.85 | 12.21 | 0.00 | 520.00 | 0.00 | 42.604 |
| 6 | 0.31 | 100 | 80 | 18.85 | 18.85 | -195.52 | 0.00 | -520.00 | 0.00 | 2.660 |
| 7 | 0.41 | 100 | 80 | 18.85 | 18.85 | -189.91 | 0.00 | -520.00 | 0.00 | 2.738 |
| 8 | 0.51 | 100 | 80 | 18.85 | 18.85 | -183.91 | 0.00 | -520.00 | 0.00 | 2.827 |
| 9 | 0.61 | 100 | 80 | 18.85 | 18.85 | -177.30 | 0.00 | -520.00 | 0.00 | 2.933 |
| 10 | 0.71 | 100 | 80 | 18.85 | 18.85 | -170.41 | 0.00 | -520.00 | 0.00 | 3.051 |
| 11 | 0.81 | 100 | 80 | 18.85 | 18.85 | -163.27 | 0.00 | -520.00 | 0.00 | 3.185 |
| 12 | 0.91 | 100 | 80 | 18.85 | 18.85 | -155.92 | 0.00 | -520.00 | 0.00 | 3.335 |
| 13 | 1.01 | 100 | 80 | 18.85 | 18.85 | -148.39 | 0.00 | -520.00 | 0.00 | 3.504 |
| 14 | 1.11 | 100 | 80 | 18.85 | 18.85 | -140.71 | 0.00 | -520.00 | 0.00 | 3.696 |
| 15 | 1.21 | 100 | 80 | 18.85 | 18.85 | -132.92 | 0.00 | -520.00 | 0.00 | 3.912 |

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 33 | 3.00 | 100 | 80 | 18.85 | 18.85 | -13.74 | 0.00 | -520.00 | 0.00 | 37.839 |
| 34 | 3.10 | 100 | 80 | 18.85 | 18.85 | -9.68 | 0.00 | -520.00 | 0.00 | 53.724 |
| 35 | 3.20 | 100 | 80 | 18.85 | 18.85 | -6.28 | 0.00 | -520.00 | 0.00 | 82.784 |
| 36 | 3.30 | 100 | 80 | 18.85 | 18.85 | -3.58 | 0.00 | -520.00 | 0.00 | 145.163 |
| 37 | 3.40 | 100 | 80 | 18.85 | 18.85 | -1.61 | 0.00 | -520.00 | 0.00 | 322.223 |
| 38 | 3.50 | 100 | 80 | 18.85 | 18.85 | -0.41 | 0.00 | -520.00 | 0.00 | 1271.779 |
| 39 | 3.60 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |

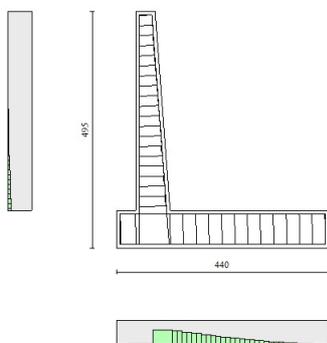


Fig. 10 - Paramento (Inviluppo)

Verifiche a taglio

Simbologia adottata

| | |
|---------------|---|
| I_s | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espressa in [cm] |
| H | altezza sezione espressa in [cm] |
| A_{sw} | area ferri a taglio espresso in [cmq] |
| $\cotg\theta$ | inclinazione delle bielle compresse, θ inclinazione dei puntoni di calcestruzzo |
| V_{Rcd} | resistenza di progetto a 'taglio compressione' espressa in [kN] |
| V_{Rsd} | resistenza di progetto a 'taglio trazione' espressa in [kN] |
| V_{Rd} | resistenza di progetto a taglio espresso in [kN]. Per elementi con armature trasversali resistenti al taglio ($A_{sw} > 0.0$) $V_{Rd} = \min(V_{Rcd}, V_{Rsd})$. |



RADDOPPIO LINEA CODOGNO – CREMONA – MANTOVA
 TRATTA PIADENA - MANTOVA

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
|----------|---------|----------|--------------|------|------------|
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 267 di 314 |

T taglio agente espressa in [kN]

FS fattore di sicurezza (rapporto tra sollecitazione resistente e sollecitazione agente)

Paramento

Combinazione n° 1 - STR (A1-M1-R3)

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 226.71 | 0.00 | 100.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 229.03 | 0.04 | 6284.150 |
| 3 | -0.20 | 100 | 41 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 231.35 | 0.15 | 1586.890 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 233.64 | 0.33 | 714.259 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 235.92 | 0.58 | 407.105 |
| 6 | -0.49 | 100 | 44 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 238.19 | 0.90 | 263.644 |
| 7 | -0.59 | 100 | 44 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 240.44 | 1.30 | 185.044 |
| 8 | -0.69 | 100 | 45 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 242.68 | 1.78 | 136.693 |
| 9 | -0.79 | 100 | 46 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 244.90 | 2.34 | 104.683 |
| 10 | -0.89 | 100 | 47 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 247.11 | 2.99 | 82.545 |
| 11 | -0.99 | 100 | 47 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 249.31 | 3.74 | 66.662 |
| 12 | -1.09 | 100 | 48 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 251.50 | 4.57 | 55.026 |
| 13 | -1.19 | 100 | 49 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 253.68 | 5.48 | 46.309 |
| 14 | -1.28 | 100 | 50 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 255.84 | 6.46 | 39.604 |
| 15 | -1.38 | 100 | 50 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 258.00 | 7.52 | 34.330 |
| 16 | -1.48 | 100 | 51 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 268.47 | 8.64 | 31.060 |
| 17 | -1.58 | 100 | 52 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 270.66 | 9.84 | 27.495 |
| 18 | -1.68 | 100 | 52 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 272.85 | 11.12 | 24.542 |
| 19 | -1.78 | 100 | 53 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 275.03 | 12.46 | 22.067 |
| 20 | -1.88 | 100 | 54 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 277.19 | 13.88 | 19.969 |
| 21 | -1.98 | 100 | 55 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 279.35 | 15.37 | 18.173 |
| 22 | -2.08 | 100 | 55 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 281.50 | 16.93 | 16.623 |
| 23 | -2.17 | 100 | 56 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 283.64 | 18.57 | 15.275 |
| 24 | -2.27 | 100 | 57 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 285.77 | 20.28 | 14.094 |
| 25 | -2.37 | 100 | 58 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 287.89 | 22.06 | 13.053 |
| 26 | -2.47 | 100 | 58 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 290.01 | 23.91 | 12.131 |
| 27 | -2.57 | 100 | 59 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 292.11 | 25.83 | 11.309 |
| 28 | -2.67 | 100 | 60 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 294.21 | 27.83 | 10.574 |
| 29 | -2.77 | 100 | 61 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 296.30 | 29.89 | 9.912 |
| 30 | -2.87 | 100 | 61 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 315.20 | 32.03 | 9.840 |
| 31 | -2.96 | 100 | 62 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 317.38 | 34.24 | 9.268 |
| 32 | -3.06 | 100 | 63 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 319.56 | 36.53 | 8.749 |
| 33 | -3.16 | 100 | 63 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 321.72 | 38.88 | 8.274 |
| 34 | -3.26 | 100 | 64 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 323.88 | 41.31 | 7.840 |
| 35 | -3.36 | 100 | 65 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 326.04 | 43.81 | 7.442 |
| 36 | -3.46 | 100 | 66 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 328.19 | 46.38 | 7.076 |
| 37 | -3.56 | 100 | 66 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 330.33 | 49.02 | 6.738 |
| 38 | -3.66 | 100 | 67 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 332.46 | 51.74 | 6.426 |
| 39 | -3.75 | 100 | 68 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 334.59 | 54.53 | 6.136 |
| 40 | -3.85 | 100 | 69 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 336.71 | 57.39 | 5.867 |
| 41 | -3.95 | 100 | 69 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 338.83 | 60.32 | 5.617 |
| 42 | -4.05 | 100 | 70 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 340.94 | 63.32 | 5.384 |
| 43 | -4.15 | 100 | 71 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 343.04 | 66.40 | 5.166 |

Combinazione n° 2 - STR (A1-M1-R3) H + V

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 226.71 | 0.00 | 100.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
|----------|---------|----------|--------------|------|------------|
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 271 di 314 |

| n° | Y [m] | B [cm] | H [cm] | A _{sw} [cmq] | s [cm] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|----------|-----------|-----------|--------------------------|-----------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 1 | -0.80 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | 0.00 | 100.000 |
| 2 | -0.70 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -14.04 | 23.737 |
| 3 | -0.60 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -27.75 | 12.009 |
| 4 | -0.50 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -41.14 | 8.102 |
| 5 | -0.40 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -54.19 | 6.150 |
| 6 | 0.31 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -96.00 | 3.472 |
| 7 | 0.41 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -98.50 | 3.384 |
| 8 | 0.51 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -100.67 | 3.311 |
| 9 | 0.61 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -102.32 | 3.257 |
| 10 | 0.71 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -103.65 | 3.216 |
| 11 | 0.81 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -104.65 | 3.185 |
| 12 | 0.91 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -105.32 | 3.165 |
| 13 | 1.01 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -105.67 | 3.154 |
| 14 | 1.11 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -105.69 | 3.154 |
| 15 | 1.21 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -105.38 | 3.163 |
| 16 | 1.31 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -104.75 | 3.182 |
| 17 | 1.41 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -103.79 | 3.212 |
| 18 | 1.50 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -102.50 | 3.252 |
| 19 | 1.60 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -100.88 | 3.304 |
| 20 | 1.70 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -98.94 | 3.369 |
| 21 | 1.80 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -96.68 | 3.448 |
| 22 | 1.90 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -94.08 | 3.543 |
| 23 | 2.00 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -91.16 | 3.656 |
| 24 | 2.10 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -87.92 | 3.791 |
| 25 | 2.20 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -84.34 | 3.952 |
| 26 | 2.30 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -80.44 | 4.144 |
| 27 | 2.40 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -76.21 | 4.373 |
| 28 | 2.50 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -71.66 | 4.651 |
| 29 | 2.60 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -66.78 | 4.991 |
| 30 | 2.70 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -61.57 | 5.413 |
| 31 | 2.80 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -56.04 | 5.948 |
| 32 | 2.90 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -50.17 | 6.643 |
| 33 | 3.00 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -43.99 | 7.577 |
| 34 | 3.10 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -37.47 | 8.895 |
| 35 | 3.20 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -30.63 | 10.881 |
| 36 | 3.30 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -23.46 | 14.205 |
| 37 | 3.40 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -15.97 | 20.872 |
| 38 | 3.50 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -8.15 | 40.907 |
| 39 | 3.60 | 100 | 80 | 0.00 | 0.00 | -- | 0.00 | 0.00 | 333.31 | 0.00 | 100.000 |

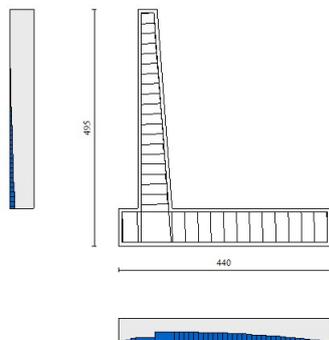


Fig. 11 - Paramento (Inviluppo)

Verifica delle tensioni

Simbologia adottata

| | |
|---------------|---|
| n° | indice sezione |
| Y | ordinata sezione, espressa in [m] |
| B | larghezza sezione, espresso in [cm] |
| H | altezza sezione, espressa in [cm] |
| A_{fi} | area ferri inferiori, espresso in [cmq] |
| A_{fs} | area ferri superiori, espressa in [cmq] |
| M | momento agente, espressa in [kNm] |
| N | sfuerzo normale agente, espressa in [kN] |
| σ_c | tensione di compressione nel cls, espressa in [kPa] |
| σ_{fi} | tensione nei ferri inferiori, espressa in [kPa] |
| σ_{fs} | tensione nei ferri superiori, espressa in [kPa] |

Combinazioni SLER

Paramento

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 273 di 314 |

Combinazione n° 10 - SLER

Tensione massima di compressione nel calcestruzzo 19920 [kPa]
Tensione massima di trazione dell'acciaio 360000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | oc [kPa] | ofi [kPa] | ofs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | 0.00 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.10 | 100 | 41 | 15.71 | 15.71 | 0.00 | 0.98 | 2 | 31 | 33 |
| 3 | -0.20 | 100 | 41 | 15.71 | 15.71 | 0.01 | 1.97 | 5 | 60 | 69 |
| 4 | -0.30 | 100 | 42 | 15.71 | 15.71 | 0.04 | 2.99 | 8 | 83 | 108 |
| 5 | -0.40 | 100 | 43 | 15.71 | 15.71 | 0.09 | 4.02 | 11 | 100 | 153 |
| 6 | -0.49 | 100 | 44 | 15.71 | 15.71 | 0.16 | 5.07 | 15 | 111 | 204 |
| 7 | -0.59 | 100 | 44 | 15.71 | 15.71 | 0.26 | 6.13 | 19 | 113 | 262 |
| 8 | -0.69 | 100 | 45 | 15.71 | 15.71 | 0.41 | 7.22 | 25 | 106 | 329 |
| 9 | -0.79 | 100 | 46 | 15.71 | 15.71 | 0.59 | 8.32 | 31 | 89 | 405 |
| 10 | -0.89 | 100 | 47 | 15.71 | 15.71 | 0.82 | 9.44 | 38 | 60 | 491 |
| 11 | -0.99 | 100 | 47 | 15.71 | 15.71 | 1.11 | 10.58 | 47 | 4 | 594 |
| 12 | -1.09 | 100 | 48 | 15.71 | 15.71 | 1.47 | 11.74 | 57 | 99 | 718 |
| 13 | -1.19 | 100 | 49 | 15.71 | 15.71 | 1.89 | 12.91 | 71 | 270 | 865 |
| 14 | -1.28 | 100 | 50 | 15.71 | 15.71 | 2.39 | 14.10 | 87 | 533 | 1037 |
| 15 | -1.38 | 100 | 50 | 15.71 | 15.71 | 2.97 | 15.31 | 105 | 904 | 1232 |
| 16 | -1.48 | 100 | 51 | 15.71 | 18.85 | 3.64 | 16.54 | 124 | 1241 | 1429 |
| 17 | -1.58 | 100 | 52 | 15.71 | 18.85 | 4.40 | 17.78 | 147 | 1765 | 1658 |
| 18 | -1.68 | 100 | 52 | 15.71 | 18.85 | 5.25 | 19.04 | 171 | 2390 | 1906 |
| 19 | -1.78 | 100 | 53 | 15.71 | 18.85 | 6.21 | 20.32 | 198 | 3116 | 2173 |
| 20 | -1.88 | 100 | 54 | 15.71 | 18.85 | 7.28 | 21.62 | 228 | 3944 | 2457 |
| 21 | -1.98 | 100 | 55 | 15.71 | 18.85 | 8.47 | 22.94 | 259 | 4874 | 2760 |
| 22 | -2.08 | 100 | 55 | 15.71 | 18.85 | 9.77 | 24.27 | 292 | 5906 | 3081 |
| 23 | -2.17 | 100 | 56 | 15.71 | 18.85 | 11.20 | 25.62 | 327 | 7041 | 3421 |
| 24 | -2.27 | 100 | 57 | 15.71 | 18.85 | 12.76 | 26.99 | 364 | 8280 | 3780 |
| 25 | -2.37 | 100 | 58 | 15.71 | 18.85 | 14.46 | 28.38 | 403 | 9625 | 4157 |
| 26 | -2.47 | 100 | 58 | 15.71 | 18.85 | 16.30 | 29.78 | 444 | 11076 | 4554 |
| 27 | -2.57 | 100 | 59 | 15.71 | 18.85 | 18.28 | 31.21 | 487 | 12635 | 4970 |
| 28 | -2.67 | 100 | 60 | 15.71 | 18.85 | 20.42 | 32.65 | 532 | 14302 | 5406 |
| 29 | -2.77 | 100 | 61 | 15.71 | 18.85 | 22.72 | 34.11 | 579 | 16077 | 5861 |
| 30 | -2.87 | 100 | 61 | 15.71 | 25.13 | 25.18 | 35.58 | 575 | 13837 | 6094 |
| 31 | -2.96 | 100 | 62 | 15.71 | 25.13 | 27.82 | 37.07 | 620 | 15358 | 6568 |
| 32 | -3.06 | 100 | 63 | 15.71 | 25.13 | 30.63 | 38.59 | 668 | 16963 | 7060 |
| 33 | -3.16 | 100 | 63 | 15.71 | 25.13 | 33.62 | 40.12 | 717 | 18655 | 7572 |
| 34 | -3.26 | 100 | 64 | 15.71 | 25.13 | 36.79 | 41.66 | 768 | 20432 | 8102 |
| 35 | -3.36 | 100 | 65 | 15.71 | 25.13 | 40.16 | 43.23 | 820 | 22295 | 8651 |
| 36 | -3.46 | 100 | 66 | 15.71 | 25.13 | 43.73 | 44.81 | 874 | 24246 | 9219 |
| 37 | -3.56 | 100 | 66 | 15.71 | 25.13 | 47.50 | 46.41 | 930 | 26285 | 9805 |
| 38 | -3.66 | 100 | 67 | 15.71 | 25.13 | 51.47 | 48.03 | 987 | 28411 | 10411 |
| 39 | -3.75 | 100 | 68 | 15.71 | 25.13 | 55.67 | 49.67 | 1046 | 30626 | 11035 |
| 40 | -3.85 | 100 | 69 | 15.71 | 25.13 | 60.08 | 51.32 | 1106 | 32930 | 11678 |
| 41 | -3.95 | 100 | 69 | 15.71 | 25.13 | 64.71 | 52.99 | 1168 | 35324 | 12339 |
| 42 | -4.05 | 100 | 70 | 15.71 | 25.13 | 69.58 | 54.68 | 1232 | 37807 | 13020 |
| 43 | -4.15 | 100 | 71 | 15.71 | 25.13 | 74.69 | 56.39 | 1297 | 40381 | 13718 |

Fondazione

Combinazione n° 10 - SLER

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 274 di 314 |

Tensione massima di compressione nel calcestruzzo 17430 [kPa]

Tensione massima di trazione dell'acciaio 360000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|---------------------|----------------------|----------------------|
| 1 | -0.80 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.70 | 100 | 80 | 18.85 | 18.85 | 0.57 | 0.00 | 8 | 444 | 78 |
| 3 | -0.60 | 100 | 80 | 18.85 | 18.85 | 2.27 | 0.00 | 34 | 1766 | 312 |
| 4 | -0.50 | 100 | 80 | 18.85 | 18.85 | 5.08 | 0.00 | 75 | 3953 | 699 |
| 5 | -0.40 | 100 | 80 | 18.85 | 18.85 | 8.99 | 0.00 | 133 | 6991 | 1236 |
| 6 | 0.31 | 100 | 80 | 18.85 | 18.85 | -130.87 | 0.00 | 1932 | 17989 | 101780 |
| 7 | 0.41 | 100 | 80 | 18.85 | 18.85 | -126.34 | 0.00 | 1865 | 17366 | 98254 |
| 8 | 0.51 | 100 | 80 | 18.85 | 18.85 | -121.64 | 0.00 | 1795 | 16720 | 94598 |
| 9 | 0.61 | 100 | 80 | 18.85 | 18.85 | -116.54 | 0.00 | 1720 | 16018 | 90629 |
| 10 | 0.71 | 100 | 80 | 18.85 | 18.85 | -111.34 | 0.00 | 1643 | 15305 | 86591 |
| 11 | 0.81 | 100 | 80 | 18.85 | 18.85 | -106.08 | 0.00 | 1566 | 14581 | 82496 |
| 12 | 0.91 | 100 | 80 | 18.85 | 18.85 | -100.76 | 0.00 | 1487 | 13849 | 78358 |
| 13 | 1.01 | 100 | 80 | 18.85 | 18.85 | -95.40 | 0.00 | 1408 | 13113 | 74190 |
| 14 | 1.11 | 100 | 80 | 18.85 | 18.85 | -90.02 | 0.00 | 1329 | 12374 | 70007 |
| 15 | 1.21 | 100 | 80 | 18.85 | 18.85 | -84.64 | 0.00 | 1249 | 11634 | 65822 |
| 16 | 1.31 | 100 | 80 | 18.85 | 18.85 | -79.27 | 0.00 | 1170 | 10896 | 61648 |
| 17 | 1.41 | 100 | 80 | 18.85 | 18.85 | -73.93 | 0.00 | 1091 | 10163 | 57499 |
| 18 | 1.50 | 100 | 80 | 18.85 | 18.85 | -68.65 | 0.00 | 1013 | 9436 | 53388 |
| 19 | 1.60 | 100 | 80 | 18.85 | 18.85 | -63.43 | 0.00 | 936 | 8719 | 49330 |
| 20 | 1.70 | 100 | 80 | 18.85 | 18.85 | -58.30 | 0.00 | 860 | 8013 | 45337 |
| 21 | 1.80 | 100 | 80 | 18.85 | 18.85 | -53.26 | 0.00 | 786 | 7321 | 41423 |
| 22 | 1.90 | 100 | 80 | 18.85 | 18.85 | -48.35 | 0.00 | 714 | 6646 | 37602 |
| 23 | 2.00 | 100 | 80 | 18.85 | 18.85 | -43.57 | 0.00 | 643 | 5990 | 33888 |
| 24 | 2.10 | 100 | 80 | 18.85 | 18.85 | -38.95 | 0.00 | 575 | 5354 | 30293 |
| 25 | 2.20 | 100 | 80 | 18.85 | 18.85 | -34.50 | 0.00 | 509 | 4743 | 26832 |
| 26 | 2.30 | 100 | 80 | 18.85 | 18.85 | -30.24 | 0.00 | 446 | 4157 | 23518 |
| 27 | 2.40 | 100 | 80 | 18.85 | 18.85 | -26.19 | 0.00 | 386 | 3599 | 20365 |
| 28 | 2.50 | 100 | 80 | 18.85 | 18.85 | -22.36 | 0.00 | 330 | 3073 | 17386 |
| 29 | 2.60 | 100 | 80 | 18.85 | 18.85 | -18.77 | 0.00 | 277 | 2580 | 14595 |
| 30 | 2.70 | 100 | 80 | 18.85 | 18.85 | -15.44 | 0.00 | 228 | 2122 | 12005 |
| 31 | 2.80 | 100 | 80 | 18.85 | 18.85 | -12.38 | 0.00 | 183 | 1702 | 9630 |
| 32 | 2.90 | 100 | 80 | 18.85 | 18.85 | -9.62 | 0.00 | 142 | 1323 | 7484 |
| 33 | 3.00 | 100 | 80 | 18.85 | 18.85 | -7.18 | 0.00 | 106 | 986 | 5580 |
| 34 | 3.10 | 100 | 80 | 18.85 | 18.85 | -5.06 | 0.00 | 75 | 695 | 3932 |
| 35 | 3.20 | 100 | 80 | 18.85 | 18.85 | -3.28 | 0.00 | 48 | 451 | 2552 |
| 36 | 3.30 | 100 | 80 | 18.85 | 18.85 | -1.87 | 0.00 | 28 | 257 | 1456 |
| 37 | 3.40 | 100 | 80 | 18.85 | 18.85 | -0.84 | 0.00 | 12 | 116 | 656 |
| 38 | 3.50 | 100 | 80 | 18.85 | 18.85 | -0.21 | 0.00 | 3 | 29 | 166 |
| 39 | 3.60 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 | 0 | 0 |

Combinazioni SLEF

Paramento

Combinazione n° 11 - SLEF

Tensione massima di compressione nel calcestruzzo 33200 [kPa]

Tensione massima di trazione dell'acciaio

450000 [kPa]

| n° | Y | B | H | Afi | Afs | M | N | oc | ofi | ofs |
|----|-------|------|------|-------|-------|-------|-------|-------|-------|-------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
| 1 | 0.00 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.10 | 100 | 41 | 15.71 | 15.71 | 0.00 | 0.98 | 2 | 31 | 33 |
| 3 | -0.20 | 100 | 41 | 15.71 | 15.71 | 0.01 | 1.97 | 5 | 60 | 69 |
| 4 | -0.30 | 100 | 42 | 15.71 | 15.71 | 0.04 | 2.99 | 8 | 83 | 108 |
| 5 | -0.40 | 100 | 43 | 15.71 | 15.71 | 0.09 | 4.02 | 11 | 100 | 153 |
| 6 | -0.49 | 100 | 44 | 15.71 | 15.71 | 0.16 | 5.07 | 15 | 111 | 204 |
| 7 | -0.59 | 100 | 44 | 15.71 | 15.71 | 0.26 | 6.13 | 19 | 113 | 262 |
| 8 | -0.69 | 100 | 45 | 15.71 | 15.71 | 0.41 | 7.22 | 25 | 106 | 329 |
| 9 | -0.79 | 100 | 46 | 15.71 | 15.71 | 0.59 | 8.32 | 31 | 89 | 405 |
| 10 | -0.89 | 100 | 47 | 15.71 | 15.71 | 0.82 | 9.44 | 38 | 60 | 491 |
| 11 | -0.99 | 100 | 47 | 15.71 | 15.71 | 1.11 | 10.58 | 47 | 4 | 594 |
| 12 | -1.09 | 100 | 48 | 15.71 | 15.71 | 1.47 | 11.74 | 57 | 99 | 718 |
| 13 | -1.19 | 100 | 49 | 15.71 | 15.71 | 1.89 | 12.91 | 71 | 270 | 865 |
| 14 | -1.28 | 100 | 50 | 15.71 | 15.71 | 2.39 | 14.10 | 87 | 533 | 1037 |
| 15 | -1.38 | 100 | 50 | 15.71 | 15.71 | 2.97 | 15.31 | 105 | 904 | 1232 |
| 16 | -1.48 | 100 | 51 | 15.71 | 18.85 | 3.64 | 16.54 | 124 | 1241 | 1429 |
| 17 | -1.58 | 100 | 52 | 15.71 | 18.85 | 4.40 | 17.78 | 147 | 1765 | 1658 |
| 18 | -1.68 | 100 | 52 | 15.71 | 18.85 | 5.25 | 19.04 | 171 | 2390 | 1906 |
| 19 | -1.78 | 100 | 53 | 15.71 | 18.85 | 6.21 | 20.32 | 198 | 3116 | 2173 |
| 20 | -1.88 | 100 | 54 | 15.71 | 18.85 | 7.28 | 21.62 | 228 | 3944 | 2457 |
| 21 | -1.98 | 100 | 55 | 15.71 | 18.85 | 8.47 | 22.94 | 259 | 4874 | 2760 |
| 22 | -2.08 | 100 | 55 | 15.71 | 18.85 | 9.77 | 24.27 | 292 | 5906 | 3081 |
| 23 | -2.17 | 100 | 56 | 15.71 | 18.85 | 11.20 | 25.62 | 327 | 7041 | 3421 |
| 24 | -2.27 | 100 | 57 | 15.71 | 18.85 | 12.76 | 26.99 | 364 | 8280 | 3780 |
| 25 | -2.37 | 100 | 58 | 15.71 | 18.85 | 14.46 | 28.38 | 403 | 9625 | 4157 |
| 26 | -2.47 | 100 | 58 | 15.71 | 18.85 | 16.30 | 29.78 | 444 | 11076 | 4554 |
| 27 | -2.57 | 100 | 59 | 15.71 | 18.85 | 18.28 | 31.21 | 487 | 12635 | 4970 |
| 28 | -2.67 | 100 | 60 | 15.71 | 18.85 | 20.42 | 32.65 | 532 | 14302 | 5406 |
| 29 | -2.77 | 100 | 61 | 15.71 | 18.85 | 22.72 | 34.11 | 579 | 16077 | 5861 |
| 30 | -2.87 | 100 | 61 | 15.71 | 25.13 | 25.18 | 35.58 | 575 | 13837 | 6094 |
| 31 | -2.96 | 100 | 62 | 15.71 | 25.13 | 27.82 | 37.07 | 620 | 15358 | 6568 |
| 32 | -3.06 | 100 | 63 | 15.71 | 25.13 | 30.63 | 38.59 | 668 | 16963 | 7060 |
| 33 | -3.16 | 100 | 63 | 15.71 | 25.13 | 33.62 | 40.12 | 717 | 18655 | 7572 |
| 34 | -3.26 | 100 | 64 | 15.71 | 25.13 | 36.79 | 41.66 | 768 | 20432 | 8102 |
| 35 | -3.36 | 100 | 65 | 15.71 | 25.13 | 40.16 | 43.23 | 820 | 22295 | 8651 |
| 36 | -3.46 | 100 | 66 | 15.71 | 25.13 | 43.73 | 44.81 | 874 | 24246 | 9219 |
| 37 | -3.56 | 100 | 66 | 15.71 | 25.13 | 47.50 | 46.41 | 930 | 26285 | 9805 |
| 38 | -3.66 | 100 | 67 | 15.71 | 25.13 | 51.47 | 48.03 | 987 | 28411 | 10411 |
| 39 | -3.75 | 100 | 68 | 15.71 | 25.13 | 55.67 | 49.67 | 1046 | 30626 | 11035 |
| 40 | -3.85 | 100 | 69 | 15.71 | 25.13 | 60.08 | 51.32 | 1106 | 32930 | 11678 |
| 41 | -3.95 | 100 | 69 | 15.71 | 25.13 | 64.71 | 52.99 | 1168 | 35324 | 12339 |
| 42 | -4.05 | 100 | 70 | 15.71 | 25.13 | 69.58 | 54.68 | 1232 | 37807 | 13020 |
| 43 | -4.15 | 100 | 71 | 15.71 | 25.13 | 74.69 | 56.39 | 1297 | 40381 | 13718 |

Fondazione

Combinazione n° 11 - SLEF

Tensione massima di compressione nel calcestruzzo 29050 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 276 di 314 |

| n° | Y | B | H | Afi | Afs | M | N | σ_c | σ_{fi} | σ_{fs} |
|----|-------|------|------|-------|-------|---------|------|------------|---------------|---------------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
| 1 | -0.80 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.70 | 100 | 80 | 18.85 | 18.85 | 0.57 | 0.00 | 8 | 444 | 78 |
| 3 | -0.60 | 100 | 80 | 18.85 | 18.85 | 2.27 | 0.00 | 34 | 1766 | 312 |
| 4 | -0.50 | 100 | 80 | 18.85 | 18.85 | 5.08 | 0.00 | 75 | 3953 | 699 |
| 5 | -0.40 | 100 | 80 | 18.85 | 18.85 | 8.99 | 0.00 | 133 | 6991 | 1236 |
| 6 | 0.31 | 100 | 80 | 18.85 | 18.85 | -130.87 | 0.00 | 1932 | 17989 | 101780 |
| 7 | 0.41 | 100 | 80 | 18.85 | 18.85 | -126.34 | 0.00 | 1865 | 17366 | 98254 |
| 8 | 0.51 | 100 | 80 | 18.85 | 18.85 | -121.64 | 0.00 | 1795 | 16720 | 94598 |
| 9 | 0.61 | 100 | 80 | 18.85 | 18.85 | -116.54 | 0.00 | 1720 | 16018 | 90629 |
| 10 | 0.71 | 100 | 80 | 18.85 | 18.85 | -111.34 | 0.00 | 1643 | 15305 | 86591 |
| 11 | 0.81 | 100 | 80 | 18.85 | 18.85 | -106.08 | 0.00 | 1566 | 14581 | 82496 |
| 12 | 0.91 | 100 | 80 | 18.85 | 18.85 | -100.76 | 0.00 | 1487 | 13849 | 78358 |
| 13 | 1.01 | 100 | 80 | 18.85 | 18.85 | -95.40 | 0.00 | 1408 | 13113 | 74190 |
| 14 | 1.11 | 100 | 80 | 18.85 | 18.85 | -90.02 | 0.00 | 1329 | 12374 | 70007 |
| 15 | 1.21 | 100 | 80 | 18.85 | 18.85 | -84.64 | 0.00 | 1249 | 11634 | 65822 |
| 16 | 1.31 | 100 | 80 | 18.85 | 18.85 | -79.27 | 0.00 | 1170 | 10896 | 61648 |
| 17 | 1.41 | 100 | 80 | 18.85 | 18.85 | -73.93 | 0.00 | 1091 | 10163 | 57499 |
| 18 | 1.50 | 100 | 80 | 18.85 | 18.85 | -68.65 | 0.00 | 1013 | 9436 | 53388 |
| 19 | 1.60 | 100 | 80 | 18.85 | 18.85 | -63.43 | 0.00 | 936 | 8719 | 49330 |
| 20 | 1.70 | 100 | 80 | 18.85 | 18.85 | -58.30 | 0.00 | 860 | 8013 | 45337 |
| 21 | 1.80 | 100 | 80 | 18.85 | 18.85 | -53.26 | 0.00 | 786 | 7321 | 41423 |
| 22 | 1.90 | 100 | 80 | 18.85 | 18.85 | -48.35 | 0.00 | 714 | 6646 | 37602 |
| 23 | 2.00 | 100 | 80 | 18.85 | 18.85 | -43.57 | 0.00 | 643 | 5990 | 33888 |
| 24 | 2.10 | 100 | 80 | 18.85 | 18.85 | -38.95 | 0.00 | 575 | 5354 | 30293 |
| 25 | 2.20 | 100 | 80 | 18.85 | 18.85 | -34.50 | 0.00 | 509 | 4743 | 26832 |
| 26 | 2.30 | 100 | 80 | 18.85 | 18.85 | -30.24 | 0.00 | 446 | 4157 | 23518 |
| 27 | 2.40 | 100 | 80 | 18.85 | 18.85 | -26.19 | 0.00 | 386 | 3599 | 20365 |
| 28 | 2.50 | 100 | 80 | 18.85 | 18.85 | -22.36 | 0.00 | 330 | 3073 | 17386 |
| 29 | 2.60 | 100 | 80 | 18.85 | 18.85 | -18.77 | 0.00 | 277 | 2580 | 14595 |
| 30 | 2.70 | 100 | 80 | 18.85 | 18.85 | -15.44 | 0.00 | 228 | 2122 | 12005 |
| 31 | 2.80 | 100 | 80 | 18.85 | 18.85 | -12.38 | 0.00 | 183 | 1702 | 9630 |
| 32 | 2.90 | 100 | 80 | 18.85 | 18.85 | -9.62 | 0.00 | 142 | 1323 | 7484 |
| 33 | 3.00 | 100 | 80 | 18.85 | 18.85 | -7.18 | 0.00 | 106 | 986 | 5580 |
| 34 | 3.10 | 100 | 80 | 18.85 | 18.85 | -5.06 | 0.00 | 75 | 695 | 3932 |
| 35 | 3.20 | 100 | 80 | 18.85 | 18.85 | -3.28 | 0.00 | 48 | 451 | 2552 |
| 36 | 3.30 | 100 | 80 | 18.85 | 18.85 | -1.87 | 0.00 | 28 | 257 | 1456 |
| 37 | 3.40 | 100 | 80 | 18.85 | 18.85 | -0.84 | 0.00 | 12 | 116 | 656 |
| 38 | 3.50 | 100 | 80 | 18.85 | 18.85 | -0.21 | 0.00 | 3 | 29 | 166 |
| 39 | 3.60 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 | 0 | 0 |

Combinazioni SLEQ

Paramento

Combinazione n° 12 - SLEQ

Tensione massima di compressione nel calcestruzzo 14940 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y | B | H | Afi | Afs | M | N | σ_c | σ_{fi} | σ_{fs} |
|----|---|---|---|-----|-----|---|---|------------|---------------|---------------|
|----|---|---|---|-----|-----|---|---|------------|---------------|---------------|

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 277 di 314 |

| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
|----|-------|------|------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 0.00 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.10 | 100 | 41 | 15.71 | 15.71 | 0.00 | 0.98 | 2 | 31 | 33 |
| 3 | -0.20 | 100 | 41 | 15.71 | 15.71 | 0.01 | 1.97 | 5 | 60 | 69 |
| 4 | -0.30 | 100 | 42 | 15.71 | 15.71 | 0.04 | 2.99 | 8 | 83 | 108 |
| 5 | -0.40 | 100 | 43 | 15.71 | 15.71 | 0.09 | 4.02 | 11 | 100 | 153 |
| 6 | -0.49 | 100 | 44 | 15.71 | 15.71 | 0.16 | 5.07 | 15 | 111 | 204 |
| 7 | -0.59 | 100 | 44 | 15.71 | 15.71 | 0.26 | 6.13 | 19 | 113 | 262 |
| 8 | -0.69 | 100 | 45 | 15.71 | 15.71 | 0.41 | 7.22 | 25 | 106 | 329 |
| 9 | -0.79 | 100 | 46 | 15.71 | 15.71 | 0.59 | 8.32 | 31 | 89 | 405 |
| 10 | -0.89 | 100 | 47 | 15.71 | 15.71 | 0.82 | 9.44 | 38 | 60 | 491 |
| 11 | -0.99 | 100 | 47 | 15.71 | 15.71 | 1.11 | 10.58 | 47 | 4 | 594 |
| 12 | -1.09 | 100 | 48 | 15.71 | 15.71 | 1.47 | 11.74 | 57 | 99 | 718 |
| 13 | -1.19 | 100 | 49 | 15.71 | 15.71 | 1.89 | 12.91 | 71 | 270 | 865 |
| 14 | -1.28 | 100 | 50 | 15.71 | 15.71 | 2.39 | 14.10 | 87 | 533 | 1037 |
| 15 | -1.38 | 100 | 50 | 15.71 | 15.71 | 2.97 | 15.31 | 105 | 904 | 1232 |
| 16 | -1.48 | 100 | 51 | 15.71 | 18.85 | 3.64 | 16.54 | 124 | 1241 | 1429 |
| 17 | -1.58 | 100 | 52 | 15.71 | 18.85 | 4.40 | 17.78 | 147 | 1765 | 1658 |
| 18 | -1.68 | 100 | 52 | 15.71 | 18.85 | 5.25 | 19.04 | 171 | 2390 | 1906 |
| 19 | -1.78 | 100 | 53 | 15.71 | 18.85 | 6.21 | 20.32 | 198 | 3116 | 2173 |
| 20 | -1.88 | 100 | 54 | 15.71 | 18.85 | 7.28 | 21.62 | 228 | 3944 | 2457 |
| 21 | -1.98 | 100 | 55 | 15.71 | 18.85 | 8.47 | 22.94 | 259 | 4874 | 2760 |
| 22 | -2.08 | 100 | 55 | 15.71 | 18.85 | 9.77 | 24.27 | 292 | 5906 | 3081 |
| 23 | -2.17 | 100 | 56 | 15.71 | 18.85 | 11.20 | 25.62 | 327 | 7041 | 3421 |
| 24 | -2.27 | 100 | 57 | 15.71 | 18.85 | 12.76 | 26.99 | 364 | 8280 | 3780 |
| 25 | -2.37 | 100 | 58 | 15.71 | 18.85 | 14.46 | 28.38 | 403 | 9625 | 4157 |
| 26 | -2.47 | 100 | 58 | 15.71 | 18.85 | 16.30 | 29.78 | 444 | 11076 | 4554 |
| 27 | -2.57 | 100 | 59 | 15.71 | 18.85 | 18.28 | 31.21 | 487 | 12635 | 4970 |
| 28 | -2.67 | 100 | 60 | 15.71 | 18.85 | 20.42 | 32.65 | 532 | 14302 | 5406 |
| 29 | -2.77 | 100 | 61 | 15.71 | 18.85 | 22.72 | 34.11 | 579 | 16077 | 5861 |
| 30 | -2.87 | 100 | 61 | 15.71 | 25.13 | 25.18 | 35.58 | 575 | 13837 | 6094 |
| 31 | -2.96 | 100 | 62 | 15.71 | 25.13 | 27.82 | 37.07 | 620 | 15358 | 6568 |
| 32 | -3.06 | 100 | 63 | 15.71 | 25.13 | 30.63 | 38.59 | 668 | 16963 | 7060 |
| 33 | -3.16 | 100 | 63 | 15.71 | 25.13 | 33.62 | 40.12 | 717 | 18655 | 7572 |
| 34 | -3.26 | 100 | 64 | 15.71 | 25.13 | 36.79 | 41.66 | 768 | 20432 | 8102 |
| 35 | -3.36 | 100 | 65 | 15.71 | 25.13 | 40.16 | 43.23 | 820 | 22295 | 8651 |
| 36 | -3.46 | 100 | 66 | 15.71 | 25.13 | 43.73 | 44.81 | 874 | 24246 | 9219 |
| 37 | -3.56 | 100 | 66 | 15.71 | 25.13 | 47.50 | 46.41 | 930 | 26285 | 9805 |
| 38 | -3.66 | 100 | 67 | 15.71 | 25.13 | 51.47 | 48.03 | 987 | 28411 | 10411 |
| 39 | -3.75 | 100 | 68 | 15.71 | 25.13 | 55.67 | 49.67 | 1046 | 30626 | 11035 |
| 40 | -3.85 | 100 | 69 | 15.71 | 25.13 | 60.08 | 51.32 | 1106 | 32930 | 11678 |
| 41 | -3.95 | 100 | 69 | 15.71 | 25.13 | 64.71 | 52.99 | 1168 | 35324 | 12339 |
| 42 | -4.05 | 100 | 70 | 15.71 | 25.13 | 69.58 | 54.68 | 1232 | 37807 | 13020 |
| 43 | -4.15 | 100 | 71 | 15.71 | 25.13 | 74.69 | 56.39 | 1297 | 40381 | 13718 |

Combinazione n° 13 - SLEQ H + V

Tensione massima di compressione nel calcestruzzo 14940 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y | B | H | Afi | Afs | M | N | σc | σfi | σfs |
|----|-------|------|------|-------|-------|-------|------|-------|-------|-------|
| | [m] | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
| 1 | 0.00 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.10 | 100 | 41 | 15.71 | 15.71 | 0.01 | 0.98 | 2 | 30 | 34 |
| 3 | -0.20 | 100 | 41 | 15.71 | 15.71 | 0.03 | 1.97 | 5 | 54 | 74 |
| 4 | -0.30 | 100 | 42 | 15.71 | 15.71 | 0.08 | 2.99 | 9 | 71 | 120 |
| 5 | -0.40 | 100 | 43 | 15.71 | 15.71 | 0.16 | 4.02 | 13 | 79 | 174 |
| 6 | -0.49 | 100 | 44 | 15.71 | 15.71 | 0.28 | 5.07 | 18 | 77 | 237 |
| 7 | -0.59 | 100 | 44 | 15.71 | 15.71 | 0.44 | 6.13 | 24 | 64 | 311 |
| 8 | -0.69 | 100 | 45 | 15.71 | 15.71 | 0.65 | 7.22 | 31 | 36 | 397 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
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| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 9 | -0.79 | 100 | 46 | 15.71 | 15.71 | 0.92 | 8.32 | 40 | 28 | 502 |
| 10 | -0.89 | 100 | 47 | 15.71 | 15.71 | 1.26 | 9.44 | 51 | 152 | 631 |
| 11 | -0.99 | 100 | 47 | 15.71 | 15.71 | 1.67 | 10.58 | 66 | 365 | 786 |
| 12 | -1.09 | 100 | 48 | 15.71 | 15.71 | 2.16 | 11.74 | 84 | 692 | 967 |
| 13 | -1.19 | 100 | 49 | 15.71 | 15.71 | 2.75 | 12.91 | 105 | 1147 | 1173 |
| 14 | -1.28 | 100 | 50 | 15.71 | 15.71 | 3.43 | 14.10 | 128 | 1738 | 1402 |
| 15 | -1.38 | 100 | 50 | 15.71 | 15.71 | 4.21 | 15.31 | 155 | 2467 | 1652 |
| 16 | -1.48 | 100 | 51 | 15.71 | 18.85 | 5.11 | 16.54 | 177 | 2881 | 1888 |
| 17 | -1.58 | 100 | 52 | 15.71 | 18.85 | 6.12 | 17.78 | 207 | 3732 | 2174 |
| 18 | -1.68 | 100 | 52 | 15.71 | 18.85 | 7.25 | 19.04 | 239 | 4701 | 2481 |
| 19 | -1.78 | 100 | 53 | 15.71 | 18.85 | 8.52 | 20.32 | 274 | 5789 | 2811 |
| 20 | -1.88 | 100 | 54 | 15.71 | 18.85 | 9.92 | 21.62 | 312 | 6998 | 3163 |
| 21 | -1.98 | 100 | 55 | 15.71 | 18.85 | 11.47 | 22.94 | 352 | 8329 | 3537 |
| 22 | -2.08 | 100 | 55 | 15.71 | 18.85 | 13.16 | 24.27 | 394 | 9784 | 3935 |
| 23 | -2.17 | 100 | 56 | 15.71 | 18.85 | 15.02 | 25.62 | 439 | 11365 | 4355 |
| 24 | -2.27 | 100 | 57 | 15.71 | 18.85 | 17.03 | 26.99 | 486 | 13073 | 4799 |
| 25 | -2.37 | 100 | 58 | 15.71 | 18.85 | 19.22 | 28.38 | 536 | 14910 | 5267 |
| 26 | -2.47 | 100 | 58 | 15.71 | 18.85 | 21.59 | 29.78 | 587 | 16876 | 5758 |
| 27 | -2.57 | 100 | 59 | 15.71 | 18.85 | 24.14 | 31.21 | 642 | 18975 | 6273 |
| 28 | -2.67 | 100 | 60 | 15.71 | 18.85 | 26.88 | 32.65 | 698 | 21206 | 6813 |
| 29 | -2.77 | 100 | 61 | 15.71 | 18.85 | 29.82 | 34.11 | 757 | 23571 | 7377 |
| 30 | -2.87 | 100 | 61 | 15.71 | 25.13 | 32.96 | 35.58 | 746 | 19977 | 7678 |
| 31 | -2.96 | 100 | 62 | 15.71 | 25.13 | 36.31 | 37.07 | 803 | 21982 | 8266 |
| 32 | -3.06 | 100 | 63 | 15.71 | 25.13 | 39.88 | 38.59 | 862 | 24092 | 8876 |
| 33 | -3.16 | 100 | 63 | 15.71 | 25.13 | 43.68 | 40.12 | 924 | 26307 | 9510 |
| 34 | -3.26 | 100 | 64 | 15.71 | 25.13 | 47.70 | 41.66 | 987 | 28627 | 10166 |
| 35 | -3.36 | 100 | 65 | 15.71 | 25.13 | 51.97 | 43.23 | 1053 | 31053 | 10846 |
| 36 | -3.46 | 100 | 66 | 15.71 | 25.13 | 56.47 | 44.81 | 1120 | 33586 | 11548 |
| 37 | -3.56 | 100 | 66 | 15.71 | 25.13 | 61.23 | 46.41 | 1189 | 36227 | 12274 |
| 38 | -3.66 | 100 | 67 | 15.71 | 25.13 | 66.25 | 48.03 | 1261 | 38976 | 13022 |
| 39 | -3.75 | 100 | 68 | 15.71 | 25.13 | 71.53 | 49.67 | 1334 | 41833 | 13794 |
| 40 | -3.85 | 100 | 69 | 15.71 | 25.13 | 77.09 | 51.32 | 1409 | 44800 | 14588 |
| 41 | -3.95 | 100 | 69 | 15.71 | 25.13 | 82.92 | 52.99 | 1486 | 47877 | 15405 |
| 42 | -4.05 | 100 | 70 | 15.71 | 25.13 | 89.03 | 54.68 | 1565 | 51063 | 16244 |
| 43 | -4.15 | 100 | 71 | 15.71 | 25.13 | 95.44 | 56.39 | 1646 | 54360 | 17106 |

Fondazione

Combinazione n° 12 - SLEQ

Tensione massima di compressione nel calcestruzzo 13073 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | -0.80 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.70 | 100 | 80 | 18.85 | 18.85 | 0.57 | 0.00 | 8 | 444 | 78 |
| 3 | -0.60 | 100 | 80 | 18.85 | 18.85 | 2.27 | 0.00 | 34 | 1766 | 312 |
| 4 | -0.50 | 100 | 80 | 18.85 | 18.85 | 5.08 | 0.00 | 75 | 3953 | 699 |
| 5 | -0.40 | 100 | 80 | 18.85 | 18.85 | 8.99 | 0.00 | 133 | 6991 | 1236 |
| 6 | 0.31 | 100 | 80 | 18.85 | 18.85 | -130.87 | 0.00 | 1932 | 17989 | 101780 |
| 7 | 0.41 | 100 | 80 | 18.85 | 18.85 | -126.34 | 0.00 | 1865 | 17366 | 98254 |
| 8 | 0.51 | 100 | 80 | 18.85 | 18.85 | -121.64 | 0.00 | 1795 | 16720 | 94598 |
| 9 | 0.61 | 100 | 80 | 18.85 | 18.85 | -116.54 | 0.00 | 1720 | 16018 | 90629 |

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 10 | 0.71 | 100 | 80 | 18.85 | 18.85 | -111.34 | 0.00 | 1643 | 15305 | 86591 |
| 11 | 0.81 | 100 | 80 | 18.85 | 18.85 | -106.08 | 0.00 | 1566 | 14581 | 82496 |
| 12 | 0.91 | 100 | 80 | 18.85 | 18.85 | -100.76 | 0.00 | 1487 | 13849 | 78358 |
| 13 | 1.01 | 100 | 80 | 18.85 | 18.85 | -95.40 | 0.00 | 1408 | 13113 | 74190 |
| 14 | 1.11 | 100 | 80 | 18.85 | 18.85 | -90.02 | 0.00 | 1329 | 12374 | 70007 |
| 15 | 1.21 | 100 | 80 | 18.85 | 18.85 | -84.64 | 0.00 | 1249 | 11634 | 65822 |
| 16 | 1.31 | 100 | 80 | 18.85 | 18.85 | -79.27 | 0.00 | 1170 | 10896 | 61648 |
| 17 | 1.41 | 100 | 80 | 18.85 | 18.85 | -73.93 | 0.00 | 1091 | 10163 | 57499 |
| 18 | 1.50 | 100 | 80 | 18.85 | 18.85 | -68.65 | 0.00 | 1013 | 9436 | 53388 |
| 19 | 1.60 | 100 | 80 | 18.85 | 18.85 | -63.43 | 0.00 | 936 | 8719 | 49330 |
| 20 | 1.70 | 100 | 80 | 18.85 | 18.85 | -58.30 | 0.00 | 860 | 8013 | 45337 |
| 21 | 1.80 | 100 | 80 | 18.85 | 18.85 | -53.26 | 0.00 | 786 | 7321 | 41423 |
| 22 | 1.90 | 100 | 80 | 18.85 | 18.85 | -48.35 | 0.00 | 714 | 6646 | 37602 |
| 23 | 2.00 | 100 | 80 | 18.85 | 18.85 | -43.57 | 0.00 | 643 | 5990 | 33888 |
| 24 | 2.10 | 100 | 80 | 18.85 | 18.85 | -38.95 | 0.00 | 575 | 5354 | 30293 |
| 25 | 2.20 | 100 | 80 | 18.85 | 18.85 | -34.50 | 0.00 | 509 | 4743 | 26832 |
| 26 | 2.30 | 100 | 80 | 18.85 | 18.85 | -30.24 | 0.00 | 446 | 4157 | 23518 |
| 27 | 2.40 | 100 | 80 | 18.85 | 18.85 | -26.19 | 0.00 | 386 | 3599 | 20365 |
| 28 | 2.50 | 100 | 80 | 18.85 | 18.85 | -22.36 | 0.00 | 330 | 3073 | 17386 |
| 29 | 2.60 | 100 | 80 | 18.85 | 18.85 | -18.77 | 0.00 | 277 | 2580 | 14595 |
| 30 | 2.70 | 100 | 80 | 18.85 | 18.85 | -15.44 | 0.00 | 228 | 2122 | 12005 |
| 31 | 2.80 | 100 | 80 | 18.85 | 18.85 | -12.38 | 0.00 | 183 | 1702 | 9630 |
| 32 | 2.90 | 100 | 80 | 18.85 | 18.85 | -9.62 | 0.00 | 142 | 1323 | 7484 |
| 33 | 3.00 | 100 | 80 | 18.85 | 18.85 | -7.18 | 0.00 | 106 | 986 | 5580 |
| 34 | 3.10 | 100 | 80 | 18.85 | 18.85 | -5.06 | 0.00 | 75 | 695 | 3932 |
| 35 | 3.20 | 100 | 80 | 18.85 | 18.85 | -3.28 | 0.00 | 48 | 451 | 2552 |
| 36 | 3.30 | 100 | 80 | 18.85 | 18.85 | -1.87 | 0.00 | 28 | 257 | 1456 |
| 37 | 3.40 | 100 | 80 | 18.85 | 18.85 | -0.84 | 0.00 | 12 | 116 | 656 |
| 38 | 3.50 | 100 | 80 | 18.85 | 18.85 | -0.21 | 0.00 | 3 | 29 | 166 |
| 39 | 3.60 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 | 0 | 0 |

Combinazione n° 13 - SLEQ_H + V

Tensione massima di compressione nel calcestruzzo 13073 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 1 | -0.80 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 | 0 | 0 |
| 2 | -0.70 | 100 | 80 | 18.85 | 18.85 | 0.75 | 0.00 | 11 | 580 | 102 |
| 3 | -0.60 | 100 | 80 | 18.85 | 18.85 | 2.96 | 0.00 | 44 | 2302 | 407 |
| 4 | -0.50 | 100 | 80 | 18.85 | 18.85 | 6.61 | 0.00 | 98 | 5142 | 909 |
| 5 | -0.40 | 100 | 80 | 18.85 | 18.85 | 11.67 | 0.00 | 172 | 9075 | 1604 |
| 6 | 0.31 | 100 | 80 | 18.85 | 18.85 | -197.64 | 0.00 | 2917 | 27167 | 153704 |
| 7 | 0.41 | 100 | 80 | 18.85 | 18.85 | -191.57 | 0.00 | 2827 | 26332 | 148983 |
| 8 | 0.51 | 100 | 80 | 18.85 | 18.85 | -185.15 | 0.00 | 2733 | 25450 | 143991 |
| 9 | 0.61 | 100 | 80 | 18.85 | 18.85 | -178.17 | 0.00 | 2630 | 24490 | 138559 |
| 10 | 0.71 | 100 | 80 | 18.85 | 18.85 | -170.94 | 0.00 | 2523 | 23497 | 132942 |
| 11 | 0.81 | 100 | 80 | 18.85 | 18.85 | -163.51 | 0.00 | 2413 | 22475 | 127162 |
| 12 | 0.91 | 100 | 80 | 18.85 | 18.85 | -155.90 | 0.00 | 2301 | 21430 | 121245 |
| 13 | 1.01 | 100 | 80 | 18.85 | 18.85 | -148.15 | 0.00 | 2187 | 20364 | 115216 |
| 14 | 1.11 | 100 | 80 | 18.85 | 18.85 | -140.28 | 0.00 | 2070 | 19283 | 109099 |
| 15 | 1.21 | 100 | 80 | 18.85 | 18.85 | -132.34 | 0.00 | 1953 | 18191 | 102919 |
| 16 | 1.31 | 100 | 80 | 18.85 | 18.85 | -124.34 | 0.00 | 1835 | 17092 | 96701 |
| 17 | 1.41 | 100 | 80 | 18.85 | 18.85 | -116.33 | 0.00 | 1717 | 15990 | 90469 |
| 18 | 1.50 | 100 | 80 | 18.85 | 18.85 | -108.33 | 0.00 | 1599 | 14891 | 84249 |
| 19 | 1.60 | 100 | 80 | 18.85 | 18.85 | -100.38 | 0.00 | 1482 | 13798 | 78065 |
| 20 | 1.70 | 100 | 80 | 18.85 | 18.85 | -92.51 | 0.00 | 1365 | 12715 | 71941 |

Relazione di calcolo muro di sostegno sede stradale-NV24

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| n° | Y [m] | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|----------|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 21 | 1.80 | 100 | 80 | 18.85 | 18.85 | -84.74 | 0.00 | 1251 | 11648 | 65902 |
| 22 | 1.90 | 100 | 80 | 18.85 | 18.85 | -77.12 | 0.00 | 1138 | 10600 | 59974 |
| 23 | 2.00 | 100 | 80 | 18.85 | 18.85 | -69.67 | 0.00 | 1028 | 9576 | 54181 |
| 24 | 2.10 | 100 | 80 | 18.85 | 18.85 | -62.42 | 0.00 | 921 | 8581 | 48547 |
| 25 | 2.20 | 100 | 80 | 18.85 | 18.85 | -55.42 | 0.00 | 818 | 7617 | 43098 |
| 26 | 2.30 | 100 | 80 | 18.85 | 18.85 | -48.68 | 0.00 | 718 | 6691 | 37857 |
| 27 | 2.40 | 100 | 80 | 18.85 | 18.85 | -42.24 | 0.00 | 623 | 5806 | 32850 |
| 28 | 2.50 | 100 | 80 | 18.85 | 18.85 | -36.13 | 0.00 | 533 | 4967 | 28102 |
| 29 | 2.60 | 100 | 80 | 18.85 | 18.85 | -30.39 | 0.00 | 449 | 4178 | 23637 |
| 30 | 2.70 | 100 | 80 | 18.85 | 18.85 | -25.05 | 0.00 | 370 | 3443 | 19480 |
| 31 | 2.80 | 100 | 80 | 18.85 | 18.85 | -20.13 | 0.00 | 297 | 2767 | 15655 |
| 32 | 2.90 | 100 | 80 | 18.85 | 18.85 | -15.67 | 0.00 | 231 | 2154 | 12188 |
| 33 | 3.00 | 100 | 80 | 18.85 | 18.85 | -11.70 | 0.00 | 173 | 1609 | 9103 |
| 34 | 3.10 | 100 | 80 | 18.85 | 18.85 | -8.26 | 0.00 | 122 | 1135 | 6424 |
| 35 | 3.20 | 100 | 80 | 18.85 | 18.85 | -5.37 | 0.00 | 79 | 738 | 4177 |
| 36 | 3.30 | 100 | 80 | 18.85 | 18.85 | -3.07 | 0.00 | 45 | 422 | 2387 |
| 37 | 3.40 | 100 | 80 | 18.85 | 18.85 | -1.39 | 0.00 | 20 | 190 | 1077 |
| 38 | 3.50 | 100 | 80 | 18.85 | 18.85 | -0.35 | 0.00 | 5 | 48 | 273 |
| 39 | 3.60 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 | 0 | 0 |

Verifica a fessurazione

Simbologia adottata

| | |
|------------|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Af | area ferri zona tesa espresso in [cmq] |
| Aeff | area efficace espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| Mpf | momento di prima fessurazione espressa in [kNm] |
| ϵ | deformazione espresso in % |
| Sm | spaziatura tra le fessure espressa in [mm] |
| w | apertura delle fessure espressa in [mm] |

Combinazioni SLER

Paramento

Combinazione n° 10 - SLER

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 281 di 314 |

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ϵ [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|-------------------|------------|-----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | 0.00 | 4.10 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.20 | 100 | 41 | 0.00 | 0.00 | 0.01 | 11.89 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | 0.04 | 24.90 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | 0.09 | 46.10 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.49 | 100 | 44 | 0.00 | 0.00 | 0.16 | 81.86 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.59 | 100 | 44 | 0.00 | 0.00 | 0.26 | 148.17 | 0.000000 | 0.00 | 0.000 |
| 8 | -0.69 | 100 | 45 | 0.00 | 0.00 | 0.41 | 299.26 | 0.000000 | 0.00 | 0.000 |
| 9 | -0.79 | 100 | 46 | 0.00 | 0.00 | 0.59 | 914.46 | 0.000000 | 0.00 | 0.000 |
| 10 | -0.89 | 100 | 47 | 0.00 | 0.00 | 0.82 | 2240.61 | 0.000000 | 0.00 | 0.000 |
| 11 | -0.99 | 100 | 47 | 0.00 | 0.00 | 1.11 | 654.18 | 0.000000 | 0.00 | 0.000 |
| 12 | -1.09 | 100 | 48 | 15.71 | 1550.00 | 1.47 | 434.45 | 0.000000 | 0.00 | 0.000 |
| 13 | -1.19 | 100 | 49 | 15.71 | 1550.00 | 1.89 | 349.89 | 0.000000 | 0.00 | 0.000 |
| 14 | -1.28 | 100 | 50 | 15.71 | 1550.00 | 2.39 | 306.82 | 0.000000 | 0.00 | 0.000 |
| 15 | -1.38 | 100 | 50 | 15.71 | 1550.00 | 2.97 | 281.88 | 0.000000 | 0.00 | 0.000 |
| 16 | -1.48 | 100 | 51 | 18.85 | 1550.00 | 3.64 | 270.61 | 0.000000 | 0.00 | 0.000 |
| 17 | -1.58 | 100 | 52 | 18.85 | 1550.00 | 4.40 | 260.84 | 0.000000 | 0.00 | 0.000 |
| 18 | -1.68 | 100 | 52 | 18.85 | 1550.00 | 5.25 | 254.68 | 0.000000 | 0.00 | 0.000 |
| 19 | -1.78 | 100 | 53 | 18.85 | 1550.00 | 6.21 | 250.97 | 0.000000 | 0.00 | 0.000 |
| 20 | -1.88 | 100 | 54 | 18.85 | 1550.00 | 7.28 | 249.01 | 0.000000 | 0.00 | 0.000 |
| 21 | -1.98 | 100 | 55 | 18.85 | 1550.00 | 8.47 | 248.34 | 0.000000 | 0.00 | 0.000 |
| 22 | -2.08 | 100 | 55 | 18.85 | 1550.00 | 9.77 | 248.66 | 0.000000 | 0.00 | 0.000 |
| 23 | -2.17 | 100 | 56 | 18.85 | 1550.00 | 11.20 | 249.76 | 0.000000 | 0.00 | 0.000 |
| 24 | -2.27 | 100 | 57 | 18.85 | 1550.00 | 12.76 | 251.48 | 0.000000 | 0.00 | 0.000 |
| 25 | -2.37 | 100 | 58 | 18.85 | 1550.00 | 14.46 | 253.70 | 0.000000 | 0.00 | 0.000 |
| 26 | -2.47 | 100 | 58 | 18.85 | 1550.00 | 16.30 | 256.35 | 0.000000 | 0.00 | 0.000 |
| 27 | -2.57 | 100 | 59 | 18.85 | 1550.00 | 18.28 | 259.37 | 0.000000 | 0.00 | 0.000 |
| 28 | -2.67 | 100 | 60 | 18.85 | 1550.00 | 20.42 | 262.69 | 0.000000 | 0.00 | 0.000 |
| 29 | -2.77 | 100 | 61 | 18.85 | 1550.00 | 22.72 | 266.27 | 0.000000 | 0.00 | 0.000 |
| 30 | -2.87 | 100 | 61 | 25.13 | 1550.00 | 25.18 | 279.38 | 0.000000 | 0.00 | 0.000 |
| 31 | -2.96 | 100 | 62 | 25.13 | 1550.00 | 27.82 | 283.53 | 0.000000 | 0.00 | 0.000 |
| 32 | -3.06 | 100 | 63 | 25.13 | 1550.00 | 30.63 | 287.87 | 0.000000 | 0.00 | 0.000 |
| 33 | -3.16 | 100 | 63 | 25.13 | 1550.00 | 33.62 | 292.39 | 0.000000 | 0.00 | 0.000 |
| 34 | -3.26 | 100 | 64 | 25.13 | 1550.00 | 36.79 | 297.06 | 0.000000 | 0.00 | 0.000 |
| 35 | -3.36 | 100 | 65 | 25.13 | 1550.00 | 40.16 | 301.89 | 0.000000 | 0.00 | 0.000 |
| 36 | -3.46 | 100 | 66 | 25.13 | 1550.00 | 43.73 | 306.84 | 0.000000 | 0.00 | 0.000 |
| 37 | -3.56 | 100 | 66 | 25.13 | 1550.00 | 47.50 | 311.93 | 0.000000 | 0.00 | 0.000 |
| 38 | -3.66 | 100 | 67 | 25.13 | 1550.00 | 51.47 | 317.13 | 0.000000 | 0.00 | 0.000 |
| 39 | -3.75 | 100 | 68 | 25.13 | 1550.00 | 55.67 | 322.45 | 0.000000 | 0.00 | 0.000 |
| 40 | -3.85 | 100 | 69 | 25.13 | 1550.00 | 60.08 | 327.88 | 0.000000 | 0.00 | 0.000 |
| 41 | -3.95 | 100 | 69 | 25.13 | 1550.00 | 64.71 | 333.41 | 0.000000 | 0.00 | 0.000 |
| 42 | -4.05 | 100 | 70 | 25.13 | 1550.00 | 69.58 | 339.03 | 0.000000 | 0.00 | 0.000 |
| 43 | -4.15 | 100 | 71 | 25.13 | 1550.00 | 74.69 | 344.75 | 0.000000 | 0.00 | 0.000 |

Fondazione

Combinazione n° 10 - SLER

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ϵ [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|-------------------|------------|-----------|
| 1 | -0.80 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.70 | 100 | 80 | 18.85 | 1550.00 | 0.57 | 351.49 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 282 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 3 | -0.60 | 100 | 80 | 18.85 | 1550.00 | 2.27 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.50 | 100 | 80 | 18.85 | 1550.00 | 5.08 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 80 | 18.85 | 1550.00 | 8.99 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 6 | 0.31 | 100 | 80 | 18.85 | 1550.00 | -130.87 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 7 | 0.41 | 100 | 80 | 18.85 | 1550.00 | -126.34 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 8 | 0.51 | 100 | 80 | 18.85 | 1550.00 | -121.64 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 9 | 0.61 | 100 | 80 | 18.85 | 1550.00 | -116.54 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 10 | 0.71 | 100 | 80 | 18.85 | 1550.00 | -111.34 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 11 | 0.81 | 100 | 80 | 18.85 | 1550.00 | -106.08 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 12 | 0.91 | 100 | 80 | 18.85 | 1550.00 | -100.76 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 13 | 1.01 | 100 | 80 | 18.85 | 1550.00 | -95.40 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 14 | 1.11 | 100 | 80 | 18.85 | 1550.00 | -90.02 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 15 | 1.21 | 100 | 80 | 18.85 | 1550.00 | -84.64 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 16 | 1.31 | 100 | 80 | 18.85 | 1550.00 | -79.27 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 17 | 1.41 | 100 | 80 | 18.85 | 1550.00 | -73.93 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 18 | 1.50 | 100 | 80 | 18.85 | 1550.00 | -68.65 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 19 | 1.60 | 100 | 80 | 18.85 | 1550.00 | -63.43 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 20 | 1.70 | 100 | 80 | 18.85 | 1550.00 | -58.30 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 21 | 1.80 | 100 | 80 | 18.85 | 1550.00 | -53.26 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 22 | 1.90 | 100 | 80 | 18.85 | 1550.00 | -48.35 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 23 | 2.00 | 100 | 80 | 18.85 | 1550.00 | -43.57 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 24 | 2.10 | 100 | 80 | 18.85 | 1550.00 | -38.95 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 25 | 2.20 | 100 | 80 | 18.85 | 1550.00 | -34.50 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 26 | 2.30 | 100 | 80 | 18.85 | 1550.00 | -30.24 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 27 | 2.40 | 100 | 80 | 18.85 | 1550.00 | -26.19 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 28 | 2.50 | 100 | 80 | 18.85 | 1550.00 | -22.36 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 29 | 2.60 | 100 | 80 | 18.85 | 1550.00 | -18.77 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 30 | 2.70 | 100 | 80 | 18.85 | 1550.00 | -15.44 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 31 | 2.80 | 100 | 80 | 18.85 | 1550.00 | -12.38 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 32 | 2.90 | 100 | 80 | 18.85 | 1550.00 | -9.62 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 33 | 3.00 | 100 | 80 | 18.85 | 1550.00 | -7.18 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 34 | 3.10 | 100 | 80 | 18.85 | 1550.00 | -5.06 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 35 | 3.20 | 100 | 80 | 18.85 | 1550.00 | -3.28 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 36 | 3.30 | 100 | 80 | 18.85 | 1550.00 | -1.87 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 37 | 3.40 | 100 | 80 | 18.85 | 1550.00 | -0.84 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 38 | 3.50 | 100 | 80 | 18.85 | 1550.00 | -0.21 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 39 | 3.60 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |

Combinazioni SLEF

Paramento

Combinazione n° 11 - SLEF

 Apertura limite fessure $w_{lim}=0.30$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | 0.00 | 4.10 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.20 | 100 | 41 | 0.00 | 0.00 | 0.01 | 11.89 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | 0.04 | 24.90 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | 0.09 | 46.10 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.49 | 100 | 44 | 0.00 | 0.00 | 0.16 | 81.86 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 283 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 7 | -0.59 | 100 | 44 | 0.00 | 0.00 | 0.26 | 148.17 | 0.000000 | 0.00 | 0.000 |
| 8 | -0.69 | 100 | 45 | 0.00 | 0.00 | 0.41 | 299.26 | 0.000000 | 0.00 | 0.000 |
| 9 | -0.79 | 100 | 46 | 0.00 | 0.00 | 0.59 | 914.46 | 0.000000 | 0.00 | 0.000 |
| 10 | -0.89 | 100 | 47 | 0.00 | 0.00 | 0.82 | 2240.61 | 0.000000 | 0.00 | 0.000 |
| 11 | -0.99 | 100 | 47 | 0.00 | 0.00 | 1.11 | 654.18 | 0.000000 | 0.00 | 0.000 |
| 12 | -1.09 | 100 | 48 | 15.71 | 1550.00 | 1.47 | 434.45 | 0.000000 | 0.00 | 0.000 |
| 13 | -1.19 | 100 | 49 | 15.71 | 1550.00 | 1.89 | 349.89 | 0.000000 | 0.00 | 0.000 |
| 14 | -1.28 | 100 | 50 | 15.71 | 1550.00 | 2.39 | 306.82 | 0.000000 | 0.00 | 0.000 |
| 15 | -1.38 | 100 | 50 | 15.71 | 1550.00 | 2.97 | 281.88 | 0.000000 | 0.00 | 0.000 |
| 16 | -1.48 | 100 | 51 | 18.85 | 1550.00 | 3.64 | 270.61 | 0.000000 | 0.00 | 0.000 |
| 17 | -1.58 | 100 | 52 | 18.85 | 1550.00 | 4.40 | 260.84 | 0.000000 | 0.00 | 0.000 |
| 18 | -1.68 | 100 | 52 | 18.85 | 1550.00 | 5.25 | 254.68 | 0.000000 | 0.00 | 0.000 |
| 19 | -1.78 | 100 | 53 | 18.85 | 1550.00 | 6.21 | 250.97 | 0.000000 | 0.00 | 0.000 |
| 20 | -1.88 | 100 | 54 | 18.85 | 1550.00 | 7.28 | 249.01 | 0.000000 | 0.00 | 0.000 |
| 21 | -1.98 | 100 | 55 | 18.85 | 1550.00 | 8.47 | 248.34 | 0.000000 | 0.00 | 0.000 |
| 22 | -2.08 | 100 | 55 | 18.85 | 1550.00 | 9.77 | 248.66 | 0.000000 | 0.00 | 0.000 |
| 23 | -2.17 | 100 | 56 | 18.85 | 1550.00 | 11.20 | 249.76 | 0.000000 | 0.00 | 0.000 |
| 24 | -2.27 | 100 | 57 | 18.85 | 1550.00 | 12.76 | 251.48 | 0.000000 | 0.00 | 0.000 |
| 25 | -2.37 | 100 | 58 | 18.85 | 1550.00 | 14.46 | 253.70 | 0.000000 | 0.00 | 0.000 |
| 26 | -2.47 | 100 | 58 | 18.85 | 1550.00 | 16.30 | 256.35 | 0.000000 | 0.00 | 0.000 |
| 27 | -2.57 | 100 | 59 | 18.85 | 1550.00 | 18.28 | 259.37 | 0.000000 | 0.00 | 0.000 |
| 28 | -2.67 | 100 | 60 | 18.85 | 1550.00 | 20.42 | 262.69 | 0.000000 | 0.00 | 0.000 |
| 29 | -2.77 | 100 | 61 | 18.85 | 1550.00 | 22.72 | 266.27 | 0.000000 | 0.00 | 0.000 |
| 30 | -2.87 | 100 | 61 | 25.13 | 1550.00 | 25.18 | 279.38 | 0.000000 | 0.00 | 0.000 |
| 31 | -2.96 | 100 | 62 | 25.13 | 1550.00 | 27.82 | 283.53 | 0.000000 | 0.00 | 0.000 |
| 32 | -3.06 | 100 | 63 | 25.13 | 1550.00 | 30.63 | 287.87 | 0.000000 | 0.00 | 0.000 |
| 33 | -3.16 | 100 | 63 | 25.13 | 1550.00 | 33.62 | 292.39 | 0.000000 | 0.00 | 0.000 |
| 34 | -3.26 | 100 | 64 | 25.13 | 1550.00 | 36.79 | 297.06 | 0.000000 | 0.00 | 0.000 |
| 35 | -3.36 | 100 | 65 | 25.13 | 1550.00 | 40.16 | 301.89 | 0.000000 | 0.00 | 0.000 |
| 36 | -3.46 | 100 | 66 | 25.13 | 1550.00 | 43.73 | 306.84 | 0.000000 | 0.00 | 0.000 |
| 37 | -3.56 | 100 | 66 | 25.13 | 1550.00 | 47.50 | 311.93 | 0.000000 | 0.00 | 0.000 |
| 38 | -3.66 | 100 | 67 | 25.13 | 1550.00 | 51.47 | 317.13 | 0.000000 | 0.00 | 0.000 |
| 39 | -3.75 | 100 | 68 | 25.13 | 1550.00 | 55.67 | 322.45 | 0.000000 | 0.00 | 0.000 |
| 40 | -3.85 | 100 | 69 | 25.13 | 1550.00 | 60.08 | 327.88 | 0.000000 | 0.00 | 0.000 |
| 41 | -3.95 | 100 | 69 | 25.13 | 1550.00 | 64.71 | 333.41 | 0.000000 | 0.00 | 0.000 |
| 42 | -4.05 | 100 | 70 | 25.13 | 1550.00 | 69.58 | 339.03 | 0.000000 | 0.00 | 0.000 |
| 43 | -4.15 | 100 | 71 | 25.13 | 1550.00 | 74.69 | 344.75 | 0.000000 | 0.00 | 0.000 |

Fondazione

Combinazione n° 11 - SLEF

Apertura limite fessure $w_{lim}=0.30$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | -0.80 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.70 | 100 | 80 | 18.85 | 1550.00 | 0.57 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.60 | 100 | 80 | 18.85 | 1550.00 | 2.27 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.50 | 100 | 80 | 18.85 | 1550.00 | 5.08 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 80 | 18.85 | 1550.00 | 8.99 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 6 | 0.31 | 100 | 80 | 18.85 | 1550.00 | -130.87 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 7 | 0.41 | 100 | 80 | 18.85 | 1550.00 | -126.34 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 8 | 0.51 | 100 | 80 | 18.85 | 1550.00 | -121.64 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 9 | 0.61 | 100 | 80 | 18.85 | 1550.00 | -116.54 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 10 | 0.71 | 100 | 80 | 18.85 | 1550.00 | -111.34 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 11 | 0.81 | 100 | 80 | 18.85 | 1550.00 | -106.08 | -351.49 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 284 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 12 | 0.91 | 100 | 80 | 18.85 | 1550.00 | -100.76 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 13 | 1.01 | 100 | 80 | 18.85 | 1550.00 | -95.40 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 14 | 1.11 | 100 | 80 | 18.85 | 1550.00 | -90.02 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 15 | 1.21 | 100 | 80 | 18.85 | 1550.00 | -84.64 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 16 | 1.31 | 100 | 80 | 18.85 | 1550.00 | -79.27 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 17 | 1.41 | 100 | 80 | 18.85 | 1550.00 | -73.93 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 18 | 1.50 | 100 | 80 | 18.85 | 1550.00 | -68.65 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 19 | 1.60 | 100 | 80 | 18.85 | 1550.00 | -63.43 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 20 | 1.70 | 100 | 80 | 18.85 | 1550.00 | -58.30 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 21 | 1.80 | 100 | 80 | 18.85 | 1550.00 | -53.26 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 22 | 1.90 | 100 | 80 | 18.85 | 1550.00 | -48.35 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 23 | 2.00 | 100 | 80 | 18.85 | 1550.00 | -43.57 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 24 | 2.10 | 100 | 80 | 18.85 | 1550.00 | -38.95 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 25 | 2.20 | 100 | 80 | 18.85 | 1550.00 | -34.50 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 26 | 2.30 | 100 | 80 | 18.85 | 1550.00 | -30.24 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 27 | 2.40 | 100 | 80 | 18.85 | 1550.00 | -26.19 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 28 | 2.50 | 100 | 80 | 18.85 | 1550.00 | -22.36 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 29 | 2.60 | 100 | 80 | 18.85 | 1550.00 | -18.77 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 30 | 2.70 | 100 | 80 | 18.85 | 1550.00 | -15.44 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 31 | 2.80 | 100 | 80 | 18.85 | 1550.00 | -12.38 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 32 | 2.90 | 100 | 80 | 18.85 | 1550.00 | -9.62 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 33 | 3.00 | 100 | 80 | 18.85 | 1550.00 | -7.18 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 34 | 3.10 | 100 | 80 | 18.85 | 1550.00 | -5.06 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 35 | 3.20 | 100 | 80 | 18.85 | 1550.00 | -3.28 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 36 | 3.30 | 100 | 80 | 18.85 | 1550.00 | -1.87 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 37 | 3.40 | 100 | 80 | 18.85 | 1550.00 | -0.84 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 38 | 3.50 | 100 | 80 | 18.85 | 1550.00 | -0.21 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 39 | 3.60 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |

Combinazioni SLEQ

Paramento

Combinazione n° 12 - SLEQ

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | 0.00 | 4.10 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.20 | 100 | 41 | 0.00 | 0.00 | 0.01 | 11.89 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | 0.04 | 24.90 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | 0.09 | 46.10 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.49 | 100 | 44 | 0.00 | 0.00 | 0.16 | 81.86 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.59 | 100 | 44 | 0.00 | 0.00 | 0.26 | 148.17 | 0.000000 | 0.00 | 0.000 |
| 8 | -0.69 | 100 | 45 | 0.00 | 0.00 | 0.41 | 299.26 | 0.000000 | 0.00 | 0.000 |
| 9 | -0.79 | 100 | 46 | 0.00 | 0.00 | 0.59 | 914.46 | 0.000000 | 0.00 | 0.000 |
| 10 | -0.89 | 100 | 47 | 0.00 | 0.00 | 0.82 | 2240.61 | 0.000000 | 0.00 | 0.000 |
| 11 | -0.99 | 100 | 47 | 0.00 | 0.00 | 1.11 | 654.18 | 0.000000 | 0.00 | 0.000 |
| 12 | -1.09 | 100 | 48 | 15.71 | 1550.00 | 1.47 | 434.45 | 0.000000 | 0.00 | 0.000 |
| 13 | -1.19 | 100 | 49 | 15.71 | 1550.00 | 1.89 | 349.89 | 0.000000 | 0.00 | 0.000 |
| 14 | -1.28 | 100 | 50 | 15.71 | 1550.00 | 2.39 | 306.82 | 0.000000 | 0.00 | 0.000 |
| 15 | -1.38 | 100 | 50 | 15.71 | 1550.00 | 2.97 | 281.88 | 0.000000 | 0.00 | 0.000 |

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 16 | -1.48 | 100 | 51 | 18.85 | 1550.00 | 3.64 | 270.61 | 0.000000 | 0.00 | 0.000 |
| 17 | -1.58 | 100 | 52 | 18.85 | 1550.00 | 4.40 | 260.84 | 0.000000 | 0.00 | 0.000 |
| 18 | -1.68 | 100 | 52 | 18.85 | 1550.00 | 5.25 | 254.68 | 0.000000 | 0.00 | 0.000 |
| 19 | -1.78 | 100 | 53 | 18.85 | 1550.00 | 6.21 | 250.97 | 0.000000 | 0.00 | 0.000 |
| 20 | -1.88 | 100 | 54 | 18.85 | 1550.00 | 7.28 | 249.01 | 0.000000 | 0.00 | 0.000 |
| 21 | -1.98 | 100 | 55 | 18.85 | 1550.00 | 8.47 | 248.34 | 0.000000 | 0.00 | 0.000 |
| 22 | -2.08 | 100 | 55 | 18.85 | 1550.00 | 9.77 | 248.66 | 0.000000 | 0.00 | 0.000 |
| 23 | -2.17 | 100 | 56 | 18.85 | 1550.00 | 11.20 | 249.76 | 0.000000 | 0.00 | 0.000 |
| 24 | -2.27 | 100 | 57 | 18.85 | 1550.00 | 12.76 | 251.48 | 0.000000 | 0.00 | 0.000 |
| 25 | -2.37 | 100 | 58 | 18.85 | 1550.00 | 14.46 | 253.70 | 0.000000 | 0.00 | 0.000 |
| 26 | -2.47 | 100 | 58 | 18.85 | 1550.00 | 16.30 | 256.35 | 0.000000 | 0.00 | 0.000 |
| 27 | -2.57 | 100 | 59 | 18.85 | 1550.00 | 18.28 | 259.37 | 0.000000 | 0.00 | 0.000 |
| 28 | -2.67 | 100 | 60 | 18.85 | 1550.00 | 20.42 | 262.69 | 0.000000 | 0.00 | 0.000 |
| 29 | -2.77 | 100 | 61 | 18.85 | 1550.00 | 22.72 | 266.27 | 0.000000 | 0.00 | 0.000 |
| 30 | -2.87 | 100 | 61 | 25.13 | 1550.00 | 25.18 | 279.38 | 0.000000 | 0.00 | 0.000 |
| 31 | -2.96 | 100 | 62 | 25.13 | 1550.00 | 27.82 | 283.53 | 0.000000 | 0.00 | 0.000 |
| 32 | -3.06 | 100 | 63 | 25.13 | 1550.00 | 30.63 | 287.87 | 0.000000 | 0.00 | 0.000 |
| 33 | -3.16 | 100 | 63 | 25.13 | 1550.00 | 33.62 | 292.39 | 0.000000 | 0.00 | 0.000 |
| 34 | -3.26 | 100 | 64 | 25.13 | 1550.00 | 36.79 | 297.06 | 0.000000 | 0.00 | 0.000 |
| 35 | -3.36 | 100 | 65 | 25.13 | 1550.00 | 40.16 | 301.89 | 0.000000 | 0.00 | 0.000 |
| 36 | -3.46 | 100 | 66 | 25.13 | 1550.00 | 43.73 | 306.84 | 0.000000 | 0.00 | 0.000 |
| 37 | -3.56 | 100 | 66 | 25.13 | 1550.00 | 47.50 | 311.93 | 0.000000 | 0.00 | 0.000 |
| 38 | -3.66 | 100 | 67 | 25.13 | 1550.00 | 51.47 | 317.13 | 0.000000 | 0.00 | 0.000 |
| 39 | -3.75 | 100 | 68 | 25.13 | 1550.00 | 55.67 | 322.45 | 0.000000 | 0.00 | 0.000 |
| 40 | -3.85 | 100 | 69 | 25.13 | 1550.00 | 60.08 | 327.88 | 0.000000 | 0.00 | 0.000 |
| 41 | -3.95 | 100 | 69 | 25.13 | 1550.00 | 64.71 | 333.41 | 0.000000 | 0.00 | 0.000 |
| 42 | -4.05 | 100 | 70 | 25.13 | 1550.00 | 69.58 | 339.03 | 0.000000 | 0.00 | 0.000 |
| 43 | -4.15 | 100 | 71 | 25.13 | 1550.00 | 74.69 | 344.75 | 0.000000 | 0.00 | 0.000 |

Combinazione n° 13 - SLEQ H + V

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | 0.00 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.10 | 100 | 41 | 0.00 | 0.00 | 0.01 | 10.47 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.20 | 100 | 41 | 0.00 | 0.00 | 0.03 | 28.52 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.30 | 100 | 42 | 0.00 | 0.00 | 0.08 | 60.50 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 43 | 0.00 | 0.00 | 0.16 | 123.44 | 0.000000 | 0.00 | 0.000 |
| 6 | -0.49 | 100 | 44 | 0.00 | 0.00 | 0.28 | 283.05 | 0.000000 | 0.00 | 0.000 |
| 7 | -0.59 | 100 | 44 | 0.00 | 0.00 | 0.44 | 1255.52 | 0.000000 | 0.00 | 0.000 |
| 8 | -0.69 | 100 | 45 | 0.00 | 0.00 | 0.65 | 1052.56 | 0.000000 | 0.00 | 0.000 |
| 9 | -0.79 | 100 | 46 | 15.71 | 1550.00 | 0.92 | 472.78 | 0.000000 | 0.00 | 0.000 |
| 10 | -0.89 | 100 | 47 | 15.71 | 1550.00 | 1.26 | 343.20 | 0.000000 | 0.00 | 0.000 |
| 11 | -0.99 | 100 | 47 | 15.71 | 1550.00 | 1.67 | 288.21 | 0.000000 | 0.00 | 0.000 |
| 12 | -1.09 | 100 | 48 | 15.71 | 1550.00 | 2.16 | 259.19 | 0.000000 | 0.00 | 0.000 |
| 13 | -1.19 | 100 | 49 | 15.71 | 1550.00 | 2.75 | 242.27 | 0.000000 | 0.00 | 0.000 |
| 14 | -1.28 | 100 | 50 | 15.71 | 1550.00 | 3.43 | 231.99 | 0.000000 | 0.00 | 0.000 |
| 15 | -1.38 | 100 | 50 | 15.71 | 1550.00 | 4.21 | 225.72 | 0.000000 | 0.00 | 0.000 |
| 16 | -1.48 | 100 | 51 | 18.85 | 1550.00 | 5.11 | 225.95 | 0.000000 | 0.00 | 0.000 |
| 17 | -1.58 | 100 | 52 | 18.85 | 1550.00 | 6.12 | 224.16 | 0.000000 | 0.00 | 0.000 |
| 18 | -1.68 | 100 | 52 | 18.85 | 1550.00 | 7.25 | 223.69 | 0.000000 | 0.00 | 0.000 |
| 19 | -1.78 | 100 | 53 | 18.85 | 1550.00 | 8.52 | 224.20 | 0.000000 | 0.00 | 0.000 |
| 20 | -1.88 | 100 | 54 | 18.85 | 1550.00 | 9.92 | 225.47 | 0.000000 | 0.00 | 0.000 |
| 21 | -1.98 | 100 | 55 | 18.85 | 1550.00 | 11.47 | 227.34 | 0.000000 | 0.00 | 0.000 |
| 22 | -2.08 | 100 | 55 | 18.85 | 1550.00 | 13.16 | 229.70 | 0.000000 | 0.00 | 0.000 |
| 23 | -2.17 | 100 | 56 | 18.85 | 1550.00 | 15.02 | 232.46 | 0.000000 | 0.00 | 0.000 |
| 24 | -2.27 | 100 | 57 | 18.85 | 1550.00 | 17.03 | 235.55 | 0.000000 | 0.00 | 0.000 |
| 25 | -2.37 | 100 | 58 | 18.85 | 1550.00 | 19.22 | 238.93 | 0.000000 | 0.00 | 0.000 |
| 26 | -2.47 | 100 | 58 | 18.85 | 1550.00 | 21.59 | 242.57 | 0.000000 | 0.00 | 0.000 |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|-------------|----------------|-----------|---------------------|----------|-------------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 286 di 314 |

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 27 | -2.57 | 100 | 59 | 18.85 | 1550.00 | 24.14 | 246.42 | 0.000000 | 0.00 | 0.000 |
| 28 | -2.67 | 100 | 60 | 18.85 | 1550.00 | 26.88 | 250.46 | 0.000000 | 0.00 | 0.000 |
| 29 | -2.77 | 100 | 61 | 18.85 | 1550.00 | 29.82 | 254.68 | 0.000000 | 0.00 | 0.000 |
| 30 | -2.87 | 100 | 61 | 25.13 | 1550.00 | 32.96 | 268.08 | 0.000000 | 0.00 | 0.000 |
| 31 | -2.96 | 100 | 62 | 25.13 | 1550.00 | 36.31 | 272.73 | 0.000000 | 0.00 | 0.000 |
| 32 | -3.06 | 100 | 63 | 25.13 | 1550.00 | 39.88 | 277.52 | 0.000000 | 0.00 | 0.000 |
| 33 | -3.16 | 100 | 63 | 25.13 | 1550.00 | 43.68 | 282.43 | 0.000000 | 0.00 | 0.000 |
| 34 | -3.26 | 100 | 64 | 25.13 | 1550.00 | 47.70 | 287.46 | 0.000000 | 0.00 | 0.000 |
| 35 | -3.36 | 100 | 65 | 25.13 | 1550.00 | 51.97 | 292.60 | 0.000000 | 0.00 | 0.000 |
| 36 | -3.46 | 100 | 66 | 25.13 | 1550.00 | 56.47 | 297.84 | 0.000000 | 0.00 | 0.000 |
| 37 | -3.56 | 100 | 66 | 25.13 | 1550.00 | 61.23 | 303.19 | 0.000000 | 0.00 | 0.000 |
| 38 | -3.66 | 100 | 67 | 25.13 | 1550.00 | 66.25 | 308.63 | 0.000000 | 0.00 | 0.000 |
| 39 | -3.75 | 100 | 68 | 25.13 | 1550.00 | 71.53 | 314.16 | 0.000000 | 0.00 | 0.000 |
| 40 | -3.85 | 100 | 69 | 25.13 | 1550.00 | 77.09 | 319.79 | 0.000000 | 0.00 | 0.000 |
| 41 | -3.95 | 100 | 69 | 25.13 | 1550.00 | 82.92 | 325.49 | 0.000000 | 0.00 | 0.000 |
| 42 | -4.05 | 100 | 70 | 25.13 | 1550.00 | 89.03 | 331.28 | 0.000000 | 0.00 | 0.000 |
| 43 | -4.15 | 100 | 71 | 25.13 | 1550.00 | 95.44 | 337.15 | 0.000000 | 0.00 | 0.000 |

Fondazione

Combinazione n° 12 - SLEQ

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | -0.80 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.70 | 100 | 80 | 18.85 | 1550.00 | 0.57 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.60 | 100 | 80 | 18.85 | 1550.00 | 2.27 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.50 | 100 | 80 | 18.85 | 1550.00 | 5.08 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 80 | 18.85 | 1550.00 | 8.99 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 6 | 0.31 | 100 | 80 | 18.85 | 1550.00 | -130.87 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 7 | 0.41 | 100 | 80 | 18.85 | 1550.00 | -126.34 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 8 | 0.51 | 100 | 80 | 18.85 | 1550.00 | -121.64 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 9 | 0.61 | 100 | 80 | 18.85 | 1550.00 | -116.54 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 10 | 0.71 | 100 | 80 | 18.85 | 1550.00 | -111.34 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 11 | 0.81 | 100 | 80 | 18.85 | 1550.00 | -106.08 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 12 | 0.91 | 100 | 80 | 18.85 | 1550.00 | -100.76 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 13 | 1.01 | 100 | 80 | 18.85 | 1550.00 | -95.40 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 14 | 1.11 | 100 | 80 | 18.85 | 1550.00 | -90.02 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 15 | 1.21 | 100 | 80 | 18.85 | 1550.00 | -84.64 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 16 | 1.31 | 100 | 80 | 18.85 | 1550.00 | -79.27 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 17 | 1.41 | 100 | 80 | 18.85 | 1550.00 | -73.93 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 18 | 1.50 | 100 | 80 | 18.85 | 1550.00 | -68.65 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 19 | 1.60 | 100 | 80 | 18.85 | 1550.00 | -63.43 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 20 | 1.70 | 100 | 80 | 18.85 | 1550.00 | -58.30 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 21 | 1.80 | 100 | 80 | 18.85 | 1550.00 | -53.26 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 22 | 1.90 | 100 | 80 | 18.85 | 1550.00 | -48.35 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 23 | 2.00 | 100 | 80 | 18.85 | 1550.00 | -43.57 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 24 | 2.10 | 100 | 80 | 18.85 | 1550.00 | -38.95 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 25 | 2.20 | 100 | 80 | 18.85 | 1550.00 | -34.50 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 26 | 2.30 | 100 | 80 | 18.85 | 1550.00 | -30.24 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 27 | 2.40 | 100 | 80 | 18.85 | 1550.00 | -26.19 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 28 | 2.50 | 100 | 80 | 18.85 | 1550.00 | -22.36 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 29 | 2.60 | 100 | 80 | 18.85 | 1550.00 | -18.77 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 30 | 2.70 | 100 | 80 | 18.85 | 1550.00 | -15.44 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 31 | 2.80 | 100 | 80 | 18.85 | 1550.00 | -12.38 | -351.49 | 0.000000 | 0.00 | 0.000 |

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 32 | 2.90 | 100 | 80 | 18.85 | 1550.00 | -9.62 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 33 | 3.00 | 100 | 80 | 18.85 | 1550.00 | -7.18 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 34 | 3.10 | 100 | 80 | 18.85 | 1550.00 | -5.06 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 35 | 3.20 | 100 | 80 | 18.85 | 1550.00 | -3.28 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 36 | 3.30 | 100 | 80 | 18.85 | 1550.00 | -1.87 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 37 | 3.40 | 100 | 80 | 18.85 | 1550.00 | -0.84 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 38 | 3.50 | 100 | 80 | 18.85 | 1550.00 | -0.21 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 39 | 3.60 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |

Combinazione n° 13 - SLEQ H + V

Apertura limite fessure $w_{lim}=0.20$

| n° | Y [m] | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|----------|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|-----------|
| 1 | -0.80 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |
| 2 | -0.70 | 100 | 80 | 18.85 | 1550.00 | 0.75 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 3 | -0.60 | 100 | 80 | 18.85 | 1550.00 | 2.96 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 4 | -0.50 | 100 | 80 | 18.85 | 1550.00 | 6.61 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 5 | -0.40 | 100 | 80 | 18.85 | 1550.00 | 11.67 | 351.49 | 0.000000 | 0.00 | 0.000 |
| 6 | 0.31 | 100 | 80 | 18.85 | 1550.00 | -197.64 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 7 | 0.41 | 100 | 80 | 18.85 | 1550.00 | -191.57 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 8 | 0.51 | 100 | 80 | 18.85 | 1550.00 | -185.15 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 9 | 0.61 | 100 | 80 | 18.85 | 1550.00 | -178.17 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 10 | 0.71 | 100 | 80 | 18.85 | 1550.00 | -170.94 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 11 | 0.81 | 100 | 80 | 18.85 | 1550.00 | -163.51 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 12 | 0.91 | 100 | 80 | 18.85 | 1550.00 | -155.90 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 13 | 1.01 | 100 | 80 | 18.85 | 1550.00 | -148.15 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 14 | 1.11 | 100 | 80 | 18.85 | 1550.00 | -140.28 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 15 | 1.21 | 100 | 80 | 18.85 | 1550.00 | -132.34 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 16 | 1.31 | 100 | 80 | 18.85 | 1550.00 | -124.34 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 17 | 1.41 | 100 | 80 | 18.85 | 1550.00 | -116.33 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 18 | 1.50 | 100 | 80 | 18.85 | 1550.00 | -108.33 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 19 | 1.60 | 100 | 80 | 18.85 | 1550.00 | -100.38 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 20 | 1.70 | 100 | 80 | 18.85 | 1550.00 | -92.51 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 21 | 1.80 | 100 | 80 | 18.85 | 1550.00 | -84.74 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 22 | 1.90 | 100 | 80 | 18.85 | 1550.00 | -77.12 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 23 | 2.00 | 100 | 80 | 18.85 | 1550.00 | -69.67 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 24 | 2.10 | 100 | 80 | 18.85 | 1550.00 | -62.42 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 25 | 2.20 | 100 | 80 | 18.85 | 1550.00 | -55.42 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 26 | 2.30 | 100 | 80 | 18.85 | 1550.00 | -48.68 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 27 | 2.40 | 100 | 80 | 18.85 | 1550.00 | -42.24 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 28 | 2.50 | 100 | 80 | 18.85 | 1550.00 | -36.13 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 29 | 2.60 | 100 | 80 | 18.85 | 1550.00 | -30.39 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 30 | 2.70 | 100 | 80 | 18.85 | 1550.00 | -25.05 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 31 | 2.80 | 100 | 80 | 18.85 | 1550.00 | -20.13 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 32 | 2.90 | 100 | 80 | 18.85 | 1550.00 | -15.67 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 33 | 3.00 | 100 | 80 | 18.85 | 1550.00 | -11.70 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 34 | 3.10 | 100 | 80 | 18.85 | 1550.00 | -8.26 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 35 | 3.20 | 100 | 80 | 18.85 | 1550.00 | -5.37 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 36 | 3.30 | 100 | 80 | 18.85 | 1550.00 | -3.07 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 37 | 3.40 | 100 | 80 | 18.85 | 1550.00 | -1.39 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 38 | 3.50 | 100 | 80 | 18.85 | 1550.00 | -0.35 | -351.49 | 0.000000 | 0.00 | 0.000 |
| 39 | 3.60 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 |

14.2 RISULTATI PER INVILUPPO

Spinta e forze

Simbologia adottata

| | |
|--------|--|
| Ic | Indice della combinazione |
| A | Tipo azione |
| I | Inclinazione della spinta, espressa in [°] |
| V | Valore dell'azione, espressa in [kN] |
| Cx, Cy | Componente in direzione X ed Y dell'azione, espressa in [kN] |
| Px, Py | Coordinata X ed Y del punto di applicazione dell'azione, espressa in [m] |

| Ic | A | V | I | Cx | Cy | Px | Py |
|----|---|--------|------|--------|-------------|------|-------|
| | | [kN] | [°] | [kN] | [kN] | [m] | [m] |
| 1 | Spinta statica | 120.81 | 0.00 | 120.81 | 0.00 | 3.60 | -3.06 |
| | Peso/Inerzia muro | | | 0.00 | 142.66/0.00 | 0.80 | -3.65 |
| | Peso/Inerzia terrapieno | | | 0.00 | 280.87/0.00 | 1.88 | -2.05 |
| | Peso dell'acqua sulla fondazione di valle | | | | 0.00 | 0.00 | 0.00 |

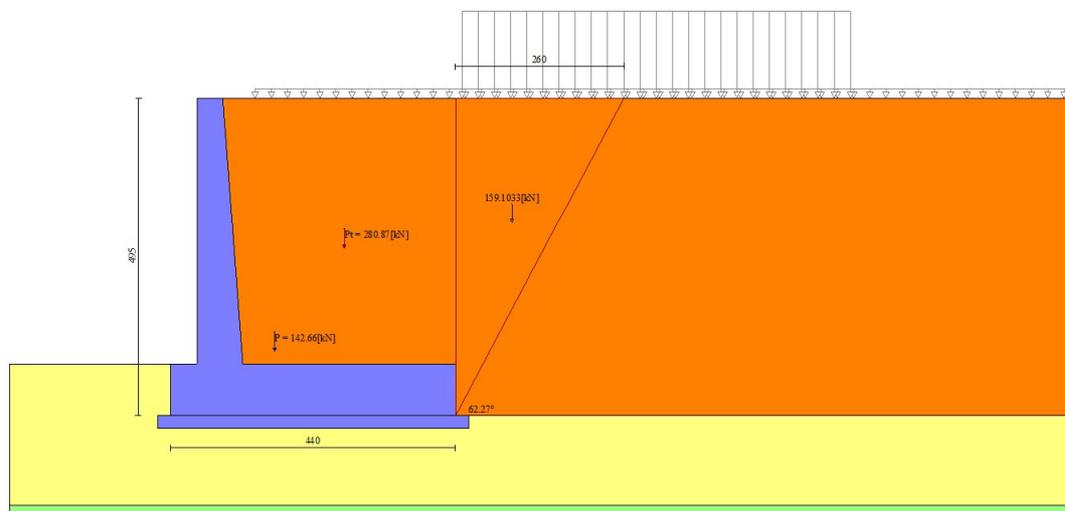


Fig. 12 - Cuneo di spinta (combinazione statica) (Combinazione n° 1)

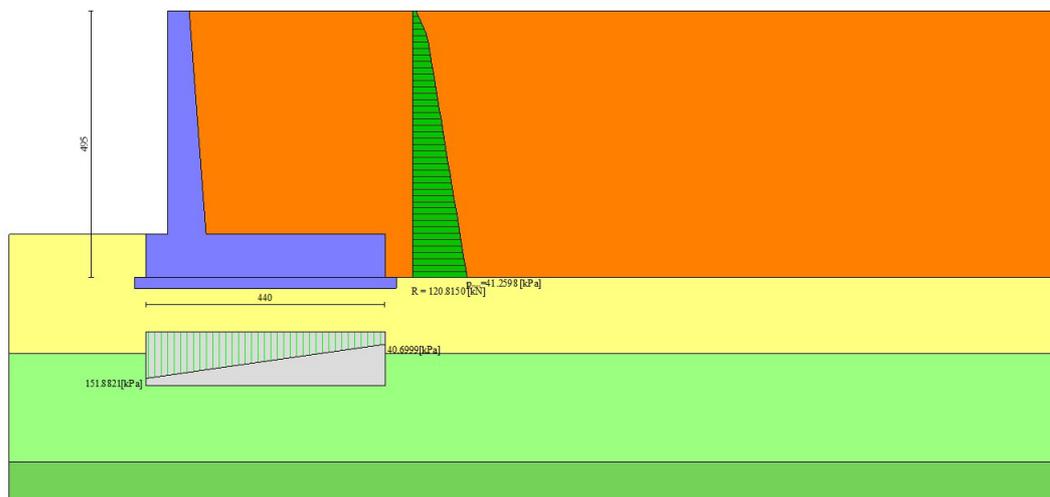


Fig. 13 - Diagramma delle pressioni (combinazione statica) (Combinazione n° 1)

Risultanti globali

Simbologia adottata

| | |
|----------------|---|
| Cmb | Indice/Tipo combinazione |
| N | Componente normale al piano di posa, espressa in [kN] |
| T | Componente parallela al piano di posa, espressa in [kN] |
| M _r | Momento ribaltante, espresso in [kNm] |
| M _s | Momento stabilizzante, espresso in [kNm] |
| ecc | Eccentricità risultante, espressa in [m] |

| Ic | N | T | M _r | M _s | ecc |
|--------------------|--------|--------|----------------|----------------|-------|
| | [kN] | [kN] | [kNm] | [kNm] | [m] |
| 1 - STR (A1-M1-R3) | 423.53 | 120.81 | 228.23 | 980.40 | 0.423 |
| 2 - STR (A1-M1-R3) | 447.71 | 149.79 | 291.95 | 1034.93 | 0.540 |
| 3 - STR (A1-M1-R3) | 393.15 | 140.90 | 340.33 | 971.87 | 0.593 |
| 4 - GEO (A2-M2-R2) | 422.29 | 122.11 | 233.28 | 976.99 | 0.438 |
| 5 - GEO (A2-M2-R2) | 447.71 | 149.79 | 291.95 | 1034.93 | 0.540 |
| 6 - GEO (A2-M2-R2) | 393.15 | 140.90 | 340.33 | 971.87 | 0.593 |
| 7 - EQU (A1-M1-R3) | 423.53 | 120.81 | 228.23 | 980.40 | 0.423 |
| 8 - EQU (A1-M1-R3) | 456.32 | 175.56 | 346.73 | 1054.84 | 0.647 |
| 9 - EQU (A1-M1-R3) | 384.53 | 164.21 | 410.97 | 971.87 | 0.741 |
| 10 - SLEP | 420.43 | 91.53 | 172.17 | 971.87 | 0.297 |
| 11 - SLEF | 420.43 | 91.53 | 172.17 | 971.87 | 0.297 |
| 12 - SLEQ | 420.43 | 91.53 | 172.17 | 971.87 | 0.297 |
| 13 - SLEQ | 436.32 | 141.08 | 276.54 | 1008.61 | 0.521 |

Verifiche geotecniche

Quadro riassuntivo coeff. di sicurezza calcolati

Simbologia adottata

| | |
|--------------------|--|
| Cmb | Indice/Tipo combinazione |
| S | Sisma (H: componente orizzontale, V: componente verticale) |
| FS _{SCO} | Coeff. di sicurezza allo scorrimento |
| FS _{RIB} | Coeff. di sicurezza al ribaltamento |
| FS _{QLIM} | Coeff. di sicurezza a carico limite |
| FS _{STAB} | Coeff. di sicurezza a stabilità globale |
| FS _{HYD} | Coeff. di sicurezza a sifonamento |
| FS _{SUPL} | Coeff. di sicurezza a sollevamento |

| Cmb | Sismica | FS _{SCO} | FS _{RIB} | FS _{QLIM} | FS _{STAB} | FS _{HYD} | FS _{SUPL} |
|--------------------|---------|-------------------|-------------------|--------------------|--------------------|-------------------|--------------------|
| 1 - STR (A1-M1-R3) | | 1.635 | | 2.015 | | | |
| 2 - STR (A1-M1-R3) | H + V | 1.394 | | 1.525 | | | |
| 3 - STR (A1-M1-R3) | H - V | 1.301 | | 1.567 | | | |
| 4 - GEO (A2-M2-R2) | | | | | 1.298 | | |
| 5 - GEO (A2-M2-R2) | H + V | | | | 1.366 | | |
| 6 - GEO (A2-M2-R2) | H - V | | | | 1.314 | | |
| 7 - EQU (A1-M1-R3) | | | 4.296 | | | | |
| 8 - EQU (A1-M1-R3) | H + V | | 3.042 | | | | |
| 9 - EQU (A1-M1-R3) | H - V | | 2.365 | | | | |

Verifica a scorrimento fondazione

Simbologia adottata

| | |
|-----------------|---|
| n° | Indice combinazione |
| R _{sa} | Resistenza allo scorrimento per attrito, espresso in [kN] |
| R _{pt} | Resistenza passiva terreno antistante, espresso in [kN] |
| R _{ps} | Resistenza passiva sperone, espresso in [kN] |
| R _p | Resistenza a carichi orizzontali pali (solo per fondazione mista), espresso in [kN] |
| R _t | Resistenza a carichi orizzontali tiranti (solo se presenti), espresso in [kN] |
| R | Resistenza allo scorrimento (somma di R _{sa} +R _{pt} +R _{ps} +R _p), espresso in [kN] |
| T | Carico parallelo al piano di posa, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto R/T) |

| n° | R _{sa} | R _{pt} | R _{ps} | R _p | R _t | R | T | FS |
|--------------------------|-----------------|-----------------|-----------------|----------------|----------------|--------|--------|-------|
| | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | [kN] | |
| 3 - STR (A1-M1-R3) H - V | 183.33 | 0.00 | 0.00 | -- | -- | 183.33 | 140.90 | 1.301 |

Verifica a carico limite

Simbologia adottata

| | |
|----|---|
| n° | Indice combinazione |
| N | Carico normale totale al piano di posa, espresso in [kN] |
| Qu | carico limite del terreno, espresso in [kN] |
| Qd | Portanza di progetto, espresso in [kN] |
| FS | Fattore di sicurezza (rapporto tra il carico limite e carico agente al piano di posa) |

| n° | N [kN] | Qu [kN] | Qd [kN] | FS |
|--------------------------|-----------|------------|------------|-------|
| 2 - STR (A1-M1-R3) H + V | 447.71 | 682.64 | 568.87 | 1.525 |

Dettagli calcolo portanza

Simbologia adottata

| | |
|---------------------------|--|
| n° | Indice combinazione |
| Nc, Nq, Ny | Fattori di capacità portante |
| ic, iq, iy | Fattori di inclinazione del carico |
| dc, dq, dy | Fattori di profondità del piano di posa |
| gc, gq, gy | Fattori di inclinazione del profilo topografico |
| bc, bq, by | Fattori di inclinazione del piano di posa |
| sc, sq, sy | Fattori di forma della fondazione |
| pc, pq, py | Fattori di riduzione per punzonamento secondo Vesic |
| Re | Fattore di riduzione capacità portante per eccentricità secondo Meyerhof |
| Ir, Irc | Indici di rigidità per punzonamento secondo Vesic |
| r _y fattore | Fattori per tener conto dell'effetto piastra. Per fondazioni che hanno larghezza maggiore di 2 m, il terzo termine della formula trinomia 0.5B _y N _y viene moltiplicato per questo fattore |
| D | Affondamento del piano di posa, espresso in [m] |
| B' | Larghezza fondazione ridotta, espresso in [m] |
| H | Altezza del cuneo di rottura, espresso in [m] |
| γ | Peso di volume del terreno medio, espresso in [kN/mc] |
| φ | Angolo di attrito del terreno medio, espresso in [°] |
| c | Coesione del terreno medio, espresso in [kPa] |

Per i coeff. che in tabella sono indicati con il simbolo '-' sono coeff. non presenti nel metodo scelto (Meyerhof).

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 292 di 314 |

| n° | Nc Nq Ny | ic iq iy | dc dq dy | gc gq gy | bc bq by | sc sq sy | pc pq py | Ir | Irc | Re | ry |
|----|----------------------------|-------------------------|-------------------------|----------------|----------------|----------------|----------------|----|-----|----|-------|
| 2 | 28.838 17.277 14.259 | 0.631 0.631 0.138 | 1.062 1.031 1.031 | -- -- -- | -- -- -- | -- -- -- | -- -- -- | -- | -- | -- | 0.914 |

| n° | D | B' | H | γ | ϕ | c |
|----|------|------|------|----------|---------|-------|
| | [m] | [m] | [m] | [°] | [kN/mc] | [kPa] |
| 2 | 0.80 | 3.32 | 3.77 | 11.28 | 29.44 | 0 |

Verifica a ribaltamento

Simbologia adottata

- n° Indice combinazione
- Ms Momento stabilizzante, espresso in [kNm]
- Mr Momento ribaltante, espresso in [kNm]
- FS Fattore di sicurezza (rapporto tra momento stabilizzante e momento ribaltante)

La verifica viene eseguita rispetto allo spigolo inferiore esterno della fondazione

| n° | Ms | Mr | FS |
|--------------------------|--------|--------|-------|
| | [kNm] | [kNm] | |
| 9 - EQU (A1-M1-R3) H - V | 971.87 | 410.97 | 2.365 |

Verifica stabilità globale muro + terreno

Simbologia adottata

- Ic Indice/Tipo combinazione
- C Centro superficie di scorrimento, espresso in [m]
- R Raggio, espresso in [m]
- FS Fattore di sicurezza

| Ic | C | R | FS |
|--------------------|-------------|------|-------|
| | [m] | [m] | |
| 4 - GEO (A2-M2-R2) | -1.00; 2.00 | 8.34 | 1.298 |

Dettagli strisce verifiche stabilità

Simbologia adottata

Le ascisse X sono considerate positive verso monte

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 293 di 314 |

Le ordinate Y sono considerate positive verso l'alto

Origine in testa al muro (spigolo contro terra)

- W peso della striscia espresso in [kN]
 Qy carico sulla striscia espresso in [kN]
 α angolo fra la base della striscia e l'orizzontale espresso in [°] (positivo antiorario)
 ϕ angolo d'attrito del terreno lungo la base della striscia
 c coesione del terreno lungo la base della striscia espressa in [kPa]
 b larghezza della striscia espressa in [m]
 u pressione neutra lungo la base della striscia espressa in [kPa]
 Tx; Ty Resistenza al taglio fornita dai tiranti in direzione X ed Y espressa in [kPa]

| n° | W [kN] | Qy [kN] | b [m] | α [°] | ϕ [°] | c [kPa] | u [kPa] | Tx; Ty [kN] |
|----|-----------|------------|--------------|-----------------|---------------|------------|------------|----------------|
| 1 | 8.00 | 14.09 | 7.11 - 0.55 | 70.210 | 29.256 | 0 | 0.0 | |
| 2 | 21.20 | 14.09 | 0.55 | 61.065 | 29.256 | 0 | 0.0 | |
| 3 | 30.36 | 14.09 | 0.55 | 53.944 | 29.256 | 0 | 0.0 | |
| 4 | 37.50 | 14.09 | 0.55 | 47.911 | 29.256 | 0 | 0.0 | |
| 5 | 43.32 | 14.09 | 0.55 | 42.526 | 29.256 | 0 | 0.0 | |
| 6 | 48.17 | 14.09 | 0.55 | 37.576 | 29.256 | 0 | 0.0 | |
| 7 | 53.75 | 3.92 | 0.55 | 32.939 | 20.458 | 0 | 0.0 | |
| 8 | 58.11 | 1.43 | 0.55 | 28.535 | 20.458 | 0 | 0.0 | |
| 9 | 60.98 | 1.43 | 0.55 | 24.309 | 20.458 | 0 | 0.0 | |
| 10 | 63.33 | 1.43 | 0.55 | 20.221 | 20.458 | 0 | 0.7 | |
| 11 | 65.23 | 1.43 | 0.55 | 16.238 | 20.458 | 0 | 2.5 | |
| 12 | 66.70 | 1.43 | 0.55 | 12.335 | 20.458 | 0 | 3.9 | |
| 13 | 72.30 | 0.02 | 0.55 | 8.489 | 20.458 | 0 | 4.9 | |
| 14 | 61.23 | 0.00 | 0.55 | 4.682 | 20.458 | 0 | 5.5 | |
| 15 | 23.79 | 0.00 | 0.55 | 0.895 | 20.458 | 0 | 5.8 | |
| 16 | 22.78 | 0.00 | 0.55 | -2.887 | 20.458 | 0 | 5.7 | |
| 17 | 22.30 | 0.00 | 0.55 | -6.683 | 20.458 | 0 | 5.2 | |
| 18 | 21.43 | 0.00 | 0.55 | -10.508 | 20.458 | 0 | 4.4 | |
| 19 | 20.15 | 0.00 | 0.55 | -14.382 | 20.458 | 0 | 3.2 | |
| 20 | 18.46 | 0.00 | 0.55 | -18.324 | 20.458 | 0 | 1.6 | |
| 21 | 16.33 | 0.00 | 0.55 | -22.359 | 20.458 | 0 | 0.0 | |
| 22 | 13.71 | 0.00 | 0.55 | -26.515 | 20.458 | 0 | 0.0 | |
| 23 | 10.55 | 0.00 | 0.55 | -30.828 | 20.458 | 0 | 0.0 | |
| 24 | 6.80 | 0.00 | 0.55 | -35.347 | 20.458 | 0 | 0.0 | |
| 25 | 2.33 | 0.00 | -6.65 - 0.55 | -39.568 | 20.458 | 0 | 0.0 | |

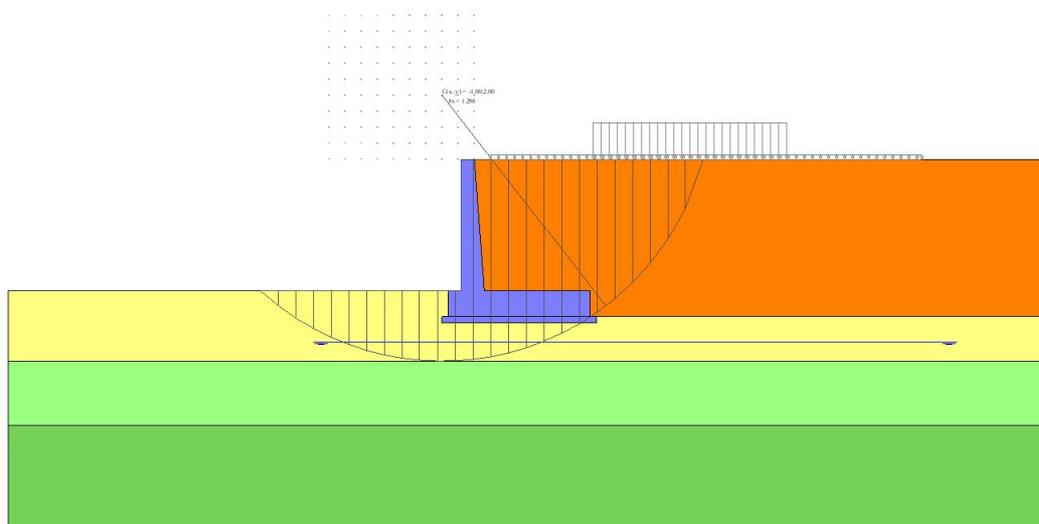


Fig. 14 - Stabilità fronte di scavo - Cerchio critico (Combinazione n° 4)

Sollecitazioni

Elementi calcolati a trave

Simbologia adottata

- N Sforzo normale, espresso in [kN]. Positivo se di compressione.
T Taglio, espresso in [kN]. Positivo se diretto da monte verso valle
M Momento, espresso in [kNm]. Positivo se tende le fibre contro terra (a monte)

Paramento

| n° | X [m] | N _{min} [kN] | N _{max} [kN] | T _{min} [kN] | T _{max} [kN] | M _{min} [kNm] | M _{max} [kNm] |
|----|----------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|---------------------------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.10 | 0.98 | 0.98 | 0.03 | 0.16 | 0.00 | 0.01 |
| 3 | -0.20 | 1.97 | 1.97 | 0.11 | 0.41 | 0.01 | 0.04 |
| 4 | -0.30 | 2.99 | 2.99 | 0.25 | 0.72 | 0.04 | 0.11 |
| 5 | -0.40 | 4.02 | 4.02 | 0.45 | 1.12 | 0.09 | 0.21 |
| 6 | -0.49 | 5.07 | 5.07 | 0.69 | 1.58 | 0.16 | 0.36 |
| 7 | -0.59 | 6.13 | 6.13 | 1.00 | 2.13 | 0.26 | 0.56 |
| 8 | -0.69 | 7.22 | 7.22 | 1.36 | 2.76 | 0.41 | 0.83 |
| 9 | -0.79 | 8.32 | 8.32 | 1.80 | 3.47 | 0.59 | 1.16 |
| 10 | -0.89 | 9.44 | 9.44 | 2.29 | 4.27 | 0.82 | 1.58 |
| 11 | -0.99 | 10.58 | 10.58 | 2.86 | 5.16 | 1.11 | 2.08 |
| 12 | -1.09 | 11.74 | 11.74 | 3.49 | 6.14 | 1.47 | 2.68 |
| 13 | -1.19 | 12.91 | 12.91 | 4.18 | 7.19 | 1.89 | 3.38 |
| 14 | -1.28 | 14.10 | 14.10 | 4.93 | 8.32 | 2.39 | 4.20 |
| 15 | -1.38 | 15.31 | 15.31 | 5.73 | 9.53 | 2.97 | 5.13 |

| n° | X [m] | Nmin [kN] | Nmax [kN] | Tmin [kN] | Tmax [kN] | Mmin [kNm] | Mmax [kNm] |
|----|----------|--------------|--------------|--------------|--------------|---------------|---------------|
| 16 | -1.48 | 16.54 | 16.54 | 6.59 | 10.82 | 3.64 | 6.19 |
| 17 | -1.58 | 17.78 | 17.78 | 7.51 | 12.19 | 4.40 | 7.39 |
| 18 | -1.68 | 19.04 | 19.04 | 8.48 | 13.63 | 5.25 | 8.74 |
| 19 | -1.78 | 20.32 | 20.32 | 9.50 | 15.14 | 6.21 | 10.23 |
| 20 | -1.88 | 21.62 | 21.62 | 10.59 | 16.74 | 7.28 | 11.88 |
| 21 | -1.98 | 22.94 | 22.94 | 11.72 | 18.41 | 8.47 | 13.70 |
| 22 | -2.08 | 24.27 | 24.27 | 12.92 | 20.15 | 9.77 | 15.69 |
| 23 | -2.17 | 25.62 | 25.62 | 14.17 | 21.98 | 11.20 | 17.86 |
| 24 | -2.27 | 26.99 | 26.99 | 15.47 | 23.88 | 12.76 | 20.22 |
| 25 | -2.37 | 28.38 | 28.38 | 16.83 | 25.85 | 14.46 | 22.78 |
| 26 | -2.47 | 29.78 | 29.78 | 18.24 | 27.90 | 16.30 | 25.54 |
| 27 | -2.57 | 31.21 | 31.21 | 19.71 | 30.03 | 18.28 | 28.52 |
| 28 | -2.67 | 32.65 | 32.65 | 21.24 | 32.23 | 20.42 | 31.71 |
| 29 | -2.77 | 34.11 | 34.11 | 22.82 | 34.51 | 22.72 | 35.13 |
| 30 | -2.87 | 35.58 | 35.58 | 24.46 | 36.87 | 25.18 | 38.78 |
| 31 | -2.96 | 37.07 | 37.07 | 26.15 | 39.30 | 27.82 | 42.68 |
| 32 | -3.06 | 38.59 | 38.59 | 27.90 | 41.81 | 30.63 | 46.82 |
| 33 | -3.16 | 40.12 | 40.12 | 29.70 | 44.40 | 33.62 | 51.23 |
| 34 | -3.26 | 41.66 | 41.66 | 31.56 | 47.06 | 36.79 | 55.90 |
| 35 | -3.36 | 43.23 | 43.23 | 33.47 | 49.80 | 40.16 | 60.84 |
| 36 | -3.46 | 44.81 | 44.81 | 35.44 | 52.61 | 43.73 | 66.06 |
| 37 | -3.56 | 46.41 | 46.41 | 37.47 | 55.50 | 47.50 | 71.56 |
| 38 | -3.66 | 48.03 | 48.03 | 39.55 | 58.47 | 51.47 | 77.37 |
| 39 | -3.75 | 49.67 | 49.67 | 41.68 | 61.51 | 55.67 | 83.47 |
| 40 | -3.85 | 51.32 | 51.32 | 43.87 | 64.63 | 60.08 | 89.89 |
| 41 | -3.95 | 52.99 | 52.99 | 46.12 | 67.83 | 64.71 | 96.63 |
| 42 | -4.05 | 54.68 | 54.68 | 48.42 | 71.10 | 69.58 | 103.69 |
| 43 | -4.15 | 56.39 | 56.39 | 50.78 | 74.45 | 74.69 | 111.08 |

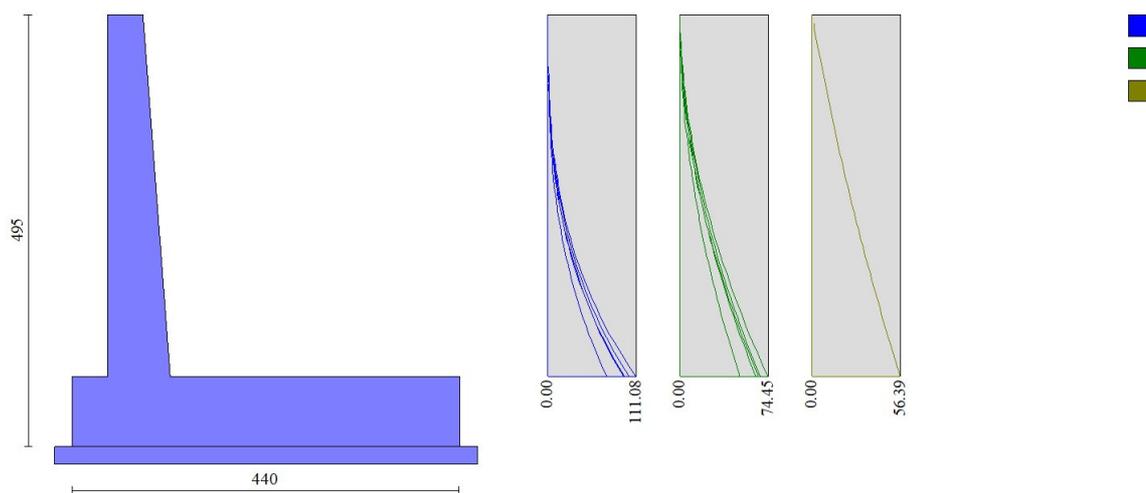


Fig. 15 - Paramento

| n° | X | Nmin | Nmax | Tmin | Tmax | Mmin | Mmax |
|----|-------|------|------|---------|--------|---------|---------|
| | [m] | [kN] | [kN] | [kN] | [kN] | [kNm] | [kNm] |
| 1 | -0.80 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | -0.70 | 0.00 | 0.00 | 11.38 | 15.54 | 0.57 | 0.78 |
| 3 | -0.60 | 0.00 | 0.00 | 22.59 | 30.74 | 2.27 | 3.10 |
| 4 | -0.50 | 0.00 | 0.00 | 33.62 | 45.60 | 5.08 | 6.92 |
| 5 | -0.40 | 0.00 | 0.00 | 44.48 | 60.12 | 8.99 | 12.21 |
| 6 | 0.31 | 0.00 | 0.00 | -140.36 | -47.78 | -305.90 | -130.87 |
| 7 | 0.41 | 0.00 | 0.00 | -140.41 | -49.32 | -292.37 | -126.34 |
| 8 | 0.51 | 0.00 | 0.00 | -140.18 | -50.67 | -278.81 | -121.64 |
| 9 | 0.61 | 0.00 | 0.00 | -139.43 | -51.66 | -264.87 | -116.54 |
| 10 | 0.71 | 0.00 | 0.00 | -138.42 | -52.48 | -251.01 | -111.34 |
| 11 | 0.81 | 0.00 | 0.00 | -137.17 | -53.12 | -237.27 | -106.08 |
| 12 | 0.91 | 0.00 | 0.00 | -135.66 | -53.59 | -223.67 | -100.76 |
| 13 | 1.01 | 0.00 | 0.00 | -133.90 | -53.88 | -210.23 | -95.40 |
| 14 | 1.11 | 0.00 | 0.00 | -131.89 | -54.00 | -196.98 | -90.02 |
| 15 | 1.21 | 0.00 | 0.00 | -129.63 | -53.94 | -183.94 | -84.64 |
| 16 | 1.31 | 0.00 | 0.00 | -127.12 | -53.70 | -171.14 | -79.27 |
| 17 | 1.41 | 0.00 | 0.00 | -124.36 | -53.29 | -158.60 | -73.93 |
| 18 | 1.50 | 0.00 | 0.00 | -121.34 | -52.71 | -146.35 | -68.65 |
| 19 | 1.60 | 0.00 | 0.00 | -118.08 | -51.95 | -134.42 | -63.43 |
| 20 | 1.70 | 0.00 | 0.00 | -114.56 | -51.02 | -122.82 | -58.30 |
| 21 | 1.80 | 0.00 | 0.00 | -110.79 | -49.91 | -111.58 | -53.26 |
| 22 | 1.90 | 0.00 | 0.00 | -106.77 | -48.62 | -100.74 | -48.35 |
| 23 | 2.00 | 0.00 | 0.00 | -102.50 | -47.16 | -90.30 | -43.57 |
| 24 | 2.10 | 0.00 | 0.00 | -97.98 | -45.53 | -80.31 | -38.95 |
| 25 | 2.20 | 0.00 | 0.00 | -93.21 | -43.72 | -70.77 | -34.50 |
| 26 | 2.30 | 0.00 | 0.00 | -88.18 | -41.73 | -61.73 | -30.24 |
| 27 | 2.40 | 0.00 | 0.00 | -82.91 | -39.57 | -53.20 | -26.19 |
| 28 | 2.50 | 0.00 | 0.00 | -77.38 | -37.24 | -45.21 | -22.36 |
| 29 | 2.60 | 0.00 | 0.00 | -71.60 | -34.73 | -37.78 | -18.77 |
| 30 | 2.70 | 0.00 | 0.00 | -65.57 | -32.04 | -30.94 | -15.44 |
| 31 | 2.80 | 0.00 | 0.00 | -59.29 | -29.18 | -24.71 | -12.38 |
| 32 | 2.90 | 0.00 | 0.00 | -52.76 | -26.15 | -19.13 | -9.62 |
| 33 | 3.00 | 0.00 | 0.00 | -45.98 | -22.94 | -14.20 | -7.18 |
| 34 | 3.10 | 0.00 | 0.00 | -38.94 | -19.55 | -9.97 | -5.06 |
| 35 | 3.20 | 0.00 | 0.00 | -31.66 | -15.99 | -6.45 | -3.28 |
| 36 | 3.30 | 0.00 | 0.00 | -24.12 | -12.26 | -3.66 | -1.87 |
| 37 | 3.40 | 0.00 | 0.00 | -16.33 | -8.35 | -1.64 | -0.84 |
| 38 | 3.50 | 0.00 | 0.00 | -8.29 | -4.26 | -0.42 | -0.21 |
| 39 | 3.60 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

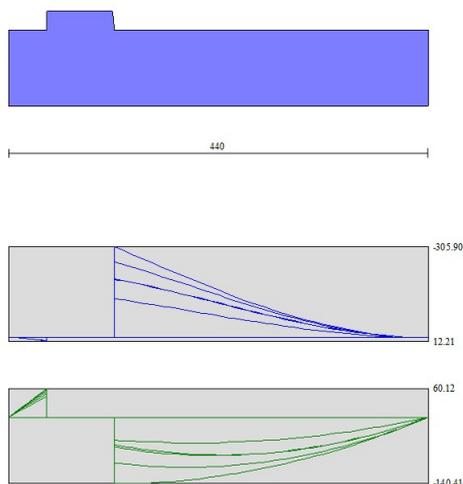


Fig. 16 - Fondazione

Verifiche strutturali

Verifiche a flessione

Elementi calcolati a trave

Simbologia adottata

| | |
|-----|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Afi | area ferri inferiori espresso in [cmq] |
| Afs | area ferri superiori espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| N | sforzo normale agente espressa in [kN] |
| Mu | momento ultimi espresso in [kNm] |
| Nu | sforzo normale ultimo espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione ultima e sollecitazione agente) |

Paramento

| n° | B | H | Afi | Afs | M | N | Mu | Nu | FS |
|----|------|------|-------|-------|--------|-------|--------|---------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kNm] | [kN] | |
| 1 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | 100 | 41 | 15.71 | 15.71 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 3 | 100 | 41 | 15.71 | 15.71 | 0.04 | 1.97 | 159.68 | 7470.61 | 3785.296 |
| 4 | 100 | 42 | 15.71 | 15.71 | 0.11 | 2.99 | 264.37 | 7422.37 | 2484.839 |
| 5 | 100 | 43 | 15.71 | 15.71 | 0.21 | 4.02 | 359.95 | 6906.09 | 1718.647 |
| 6 | 100 | 44 | 15.71 | 15.71 | 0.36 | 5.07 | 449.23 | 6343.28 | 1251.787 |
| 7 | 100 | 44 | 15.71 | 15.71 | 0.56 | 6.13 | 528.11 | 5761.64 | 939.262 |
| 8 | 100 | 45 | 15.71 | 15.71 | 0.83 | 7.22 | 594.86 | 5190.15 | 718.972 |
| 9 | 100 | 46 | 15.71 | 15.71 | 1.16 | 8.32 | 650.22 | 4653.64 | 559.247 |
| 10 | 100 | 47 | 15.71 | 15.71 | 1.58 | 9.44 | 695.89 | 4166.82 | 441.331 |
| 11 | 100 | 47 | 15.71 | 15.71 | 2.08 | 10.58 | 713.26 | 3630.24 | 343.141 |
| 12 | 100 | 48 | 15.71 | 15.71 | 2.68 | 11.74 | 698.69 | 3062.93 | 261.003 |
| 13 | 100 | 49 | 15.71 | 15.71 | 3.38 | 12.91 | 667.02 | 2547.58 | 197.352 |
| 14 | 100 | 50 | 15.71 | 15.71 | 4.20 | 14.10 | 627.12 | 2107.71 | 149.481 |
| 15 | 100 | 50 | 15.71 | 15.71 | 5.13 | 15.31 | 584.23 | 1743.18 | 113.864 |
| 16 | 100 | 51 | 15.71 | 18.85 | 6.19 | 16.54 | 627.67 | 1675.56 | 101.327 |
| 17 | 100 | 52 | 15.71 | 18.85 | 7.39 | 17.78 | 599.70 | 1442.21 | 81.110 |
| 18 | 100 | 52 | 15.71 | 18.85 | 8.74 | 19.04 | 575.96 | 1255.53 | 65.930 |
| 19 | 100 | 53 | 15.71 | 18.85 | 10.23 | 20.32 | 556.19 | 1105.09 | 54.374 |
| 20 | 100 | 54 | 15.71 | 18.85 | 11.88 | 21.62 | 539.90 | 982.59 | 45.444 |
| 21 | 100 | 55 | 15.71 | 18.85 | 13.70 | 22.94 | 527.85 | 883.90 | 38.535 |
| 22 | 100 | 55 | 15.71 | 18.85 | 15.69 | 24.27 | 518.95 | 802.82 | 33.077 |
| 23 | 100 | 56 | 15.71 | 18.85 | 17.86 | 25.62 | 512.44 | 735.11 | 28.690 |
| 24 | 100 | 57 | 15.71 | 18.85 | 20.22 | 26.99 | 507.80 | 677.78 | 25.110 |
| 25 | 100 | 58 | 15.71 | 18.85 | 22.78 | 28.38 | 504.64 | 628.66 | 22.152 |
| 26 | 100 | 58 | 15.71 | 18.85 | 25.54 | 29.78 | 502.67 | 586.15 | 19.680 |
| 27 | 100 | 59 | 15.71 | 18.85 | 28.52 | 31.21 | 501.69 | 549.03 | 17.593 |
| 28 | 100 | 60 | 15.71 | 18.85 | 31.71 | 32.65 | 501.51 | 516.35 | 15.816 |
| 29 | 100 | 61 | 15.71 | 18.85 | 35.13 | 34.11 | 502.02 | 487.40 | 14.291 |
| 30 | 100 | 61 | 15.71 | 25.13 | 38.78 | 35.58 | 654.72 | 600.67 | 16.882 |
| 31 | 100 | 62 | 15.71 | 25.13 | 42.68 | 37.07 | 656.67 | 570.45 | 15.387 |
| 32 | 100 | 63 | 15.71 | 25.13 | 46.82 | 38.59 | 659.18 | 543.21 | 14.078 |
| 33 | 100 | 63 | 15.71 | 25.13 | 51.23 | 40.12 | 662.16 | 518.53 | 12.926 |
| 34 | 100 | 64 | 15.71 | 25.13 | 55.90 | 41.66 | 665.56 | 496.09 | 11.907 |
| 35 | 100 | 65 | 15.71 | 25.13 | 60.84 | 43.23 | 669.33 | 475.60 | 11.002 |
| 36 | 100 | 66 | 15.71 | 25.13 | 66.06 | 44.81 | 673.41 | 456.82 | 10.195 |
| 37 | 100 | 66 | 15.71 | 25.13 | 71.56 | 46.41 | 677.79 | 439.56 | 9.471 |
| 38 | 100 | 67 | 15.71 | 25.13 | 77.37 | 48.03 | 682.42 | 423.64 | 8.820 |
| 39 | 100 | 68 | 15.71 | 25.13 | 83.47 | 49.67 | 687.28 | 408.91 | 8.233 |
| 40 | 100 | 69 | 15.71 | 25.13 | 89.89 | 51.32 | 692.34 | 395.26 | 7.702 |
| 41 | 100 | 69 | 15.71 | 25.13 | 96.63 | 52.99 | 697.60 | 382.57 | 7.220 |
| 42 | 100 | 70 | 15.71 | 25.13 | 103.69 | 54.68 | 703.02 | 370.75 | 6.780 |
| 43 | 100 | 71 | 15.71 | 25.13 | 111.08 | 56.39 | 708.60 | 359.70 | 6.379 |

Fondazione

| n° | B | H | Afi | Afs | M | N | Mu | Nu | FS |
|----|------|------|-------|-------|---------|------|---------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kNm] | [kN] | |
| 1 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |
| 2 | 100 | 80 | 18.85 | 18.85 | 0.78 | 0.00 | 520.00 | 0.00 | 666.775 |
| 3 | 100 | 80 | 18.85 | 18.85 | 3.10 | 0.00 | 520.00 | 0.00 | 167.917 |
| 4 | 100 | 80 | 18.85 | 18.85 | 6.92 | 0.00 | 520.00 | 0.00 | 75.181 |
| 5 | 100 | 80 | 18.85 | 18.85 | 12.21 | 0.00 | 520.00 | 0.00 | 42.604 |
| 6 | 100 | 80 | 18.85 | 18.85 | -305.90 | 0.00 | -520.00 | 0.00 | 1.700 |
| 7 | 100 | 80 | 18.85 | 18.85 | -292.37 | 0.00 | -520.00 | 0.00 | 1.779 |
| 8 | 100 | 80 | 18.85 | 18.85 | -278.81 | 0.00 | -520.00 | 0.00 | 1.865 |
| 9 | 100 | 80 | 18.85 | 18.85 | -264.87 | 0.00 | -520.00 | 0.00 | 1.963 |
| 10 | 100 | 80 | 18.85 | 18.85 | -251.01 | 0.00 | -520.00 | 0.00 | 2.072 |

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | Mu [kNm] | Nu [kN] | FS |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|------------|------------|
| 11 | 100 | 80 | 18.85 | 18.85 | -237.27 | 0.00 | -520.00 | 0.00 | 2.192 |
| 12 | 100 | 80 | 18.85 | 18.85 | -223.67 | 0.00 | -520.00 | 0.00 | 2.325 |
| 13 | 100 | 80 | 18.85 | 18.85 | -210.23 | 0.00 | -520.00 | 0.00 | 2.473 |
| 14 | 100 | 80 | 18.85 | 18.85 | -196.98 | 0.00 | -520.00 | 0.00 | 2.640 |
| 15 | 100 | 80 | 18.85 | 18.85 | -183.94 | 0.00 | -520.00 | 0.00 | 2.827 |
| 16 | 100 | 80 | 18.85 | 18.85 | -171.14 | 0.00 | -520.00 | 0.00 | 3.038 |
| 17 | 100 | 80 | 18.85 | 18.85 | -158.60 | 0.00 | -520.00 | 0.00 | 3.279 |
| 18 | 100 | 80 | 18.85 | 18.85 | -146.35 | 0.00 | -520.00 | 0.00 | 3.553 |
| 19 | 100 | 80 | 18.85 | 18.85 | -134.42 | 0.00 | -520.00 | 0.00 | 3.869 |
| 20 | 100 | 80 | 18.85 | 18.85 | -122.82 | 0.00 | -520.00 | 0.00 | 4.234 |
| 21 | 100 | 80 | 18.85 | 18.85 | -111.58 | 0.00 | -520.00 | 0.00 | 4.660 |
| 22 | 100 | 80 | 18.85 | 18.85 | -100.74 | 0.00 | -520.00 | 0.00 | 5.162 |
| 23 | 100 | 80 | 18.85 | 18.85 | -90.30 | 0.00 | -520.00 | 0.00 | 5.758 |
| 24 | 100 | 80 | 18.85 | 18.85 | -80.31 | 0.00 | -520.00 | 0.00 | 6.475 |
| 25 | 100 | 80 | 18.85 | 18.85 | -70.77 | 0.00 | -520.00 | 0.00 | 7.347 |
| 26 | 100 | 80 | 18.85 | 18.85 | -61.73 | 0.00 | -520.00 | 0.00 | 8.424 |
| 27 | 100 | 80 | 18.85 | 18.85 | -53.20 | 0.00 | -520.00 | 0.00 | 9.775 |
| 28 | 100 | 80 | 18.85 | 18.85 | -45.21 | 0.00 | -520.00 | 0.00 | 11.503 |
| 29 | 100 | 80 | 18.85 | 18.85 | -37.78 | 0.00 | -520.00 | 0.00 | 13.764 |
| 30 | 100 | 80 | 18.85 | 18.85 | -30.94 | 0.00 | -520.00 | 0.00 | 16.807 |
| 31 | 100 | 80 | 18.85 | 18.85 | -24.71 | 0.00 | -520.00 | 0.00 | 21.042 |
| 32 | 100 | 80 | 18.85 | 18.85 | -19.13 | 0.00 | -520.00 | 0.00 | 27.189 |
| 33 | 100 | 80 | 18.85 | 18.85 | -14.20 | 0.00 | -520.00 | 0.00 | 36.616 |
| 34 | 100 | 80 | 18.85 | 18.85 | -9.97 | 0.00 | -520.00 | 0.00 | 52.174 |
| 35 | 100 | 80 | 18.85 | 18.85 | -6.45 | 0.00 | -520.00 | 0.00 | 80.677 |
| 36 | 100 | 80 | 18.85 | 18.85 | -3.66 | 0.00 | -520.00 | 0.00 | 141.955 |
| 37 | 100 | 80 | 18.85 | 18.85 | -1.64 | 0.00 | -520.00 | 0.00 | 316.157 |
| 38 | 100 | 80 | 18.85 | 18.85 | -0.42 | 0.00 | -520.00 | 0.00 | 1251.916 |
| 39 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0.00 | 0.00 | 100000.000 |

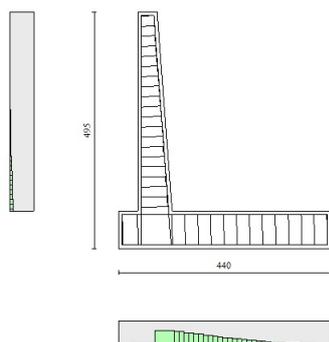


Fig. 17 - Paramento (Inviluppo)

Verifiche a taglio

Simbologia adottata

| | |
|------------------|---|
| Is | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| A _{sw} | area ferri a taglio espresso in [cmq] |
| cotθ | inclinazione delle bielle compresse, θ inclinazione dei puntoni di calcestruzzo |
| V _{Rcd} | resistenza di progetto a 'taglio compressione' espressa in [kN] |
| V _{Rsd} | resistenza di progetto a 'taglio trazione' espressa in [kN] |
| V _{Rd} | resistenza di progetto a taglio espresso in [kN]. Per elementi con armature trasversali resistenti al taglio (A _{sw} >0.0) V _{Rd} =min(V _{Rcd} , V _{Rsd}). |
| T | taglio agente espressa in [kN] |
| FS | fattore di sicurezza (rapporto tra sollecitazione resistente e sollecitazione agente) |

Paramento

| n° | B [cm] | H [cm] | A _{sw} [cmq] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|-----------|-----------|--------------------------|------|--------------------------|--------------------------|-------------------------|-----------|----------|
| 1 | 100 | 40 | 0.00 | -- | 0.00 | 0.00 | 226.71 | 0.00 | 100.000 |
| 2 | 100 | 41 | 0.00 | -- | 0.00 | 0.00 | 229.03 | 0.16 | 1394.827 |
| 3 | 100 | 41 | 0.00 | -- | 0.00 | 0.00 | 231.35 | 0.41 | 570.768 |
| 4 | 100 | 42 | 0.00 | -- | 0.00 | 0.00 | 233.64 | 0.72 | 323.305 |
| 5 | 100 | 43 | 0.00 | -- | 0.00 | 0.00 | 235.92 | 1.12 | 211.489 |
| 6 | 100 | 44 | 0.00 | -- | 0.00 | 0.00 | 238.19 | 1.58 | 150.346 |
| 7 | 100 | 44 | 0.00 | -- | 0.00 | 0.00 | 240.44 | 2.13 | 112.924 |
| 8 | 100 | 45 | 0.00 | -- | 0.00 | 0.00 | 242.68 | 2.76 | 88.070 |
| 9 | 100 | 46 | 0.00 | -- | 0.00 | 0.00 | 244.90 | 3.47 | 70.612 |
| 10 | 100 | 47 | 0.00 | -- | 0.00 | 0.00 | 247.11 | 4.27 | 57.884 |
| 11 | 100 | 47 | 0.00 | -- | 0.00 | 0.00 | 249.31 | 5.16 | 48.319 |
| 12 | 100 | 48 | 0.00 | -- | 0.00 | 0.00 | 251.50 | 6.14 | 40.994 |
| 13 | 100 | 49 | 0.00 | -- | 0.00 | 0.00 | 253.68 | 7.19 | 35.280 |
| 14 | 100 | 50 | 0.00 | -- | 0.00 | 0.00 | 255.84 | 8.32 | 30.735 |
| 15 | 100 | 50 | 0.00 | -- | 0.00 | 0.00 | 258.00 | 9.53 | 27.058 |
| 16 | 100 | 51 | 0.00 | -- | 0.00 | 0.00 | 268.47 | 10.82 | 24.807 |
| 17 | 100 | 52 | 0.00 | -- | 0.00 | 0.00 | 270.66 | 12.19 | 22.210 |
| 18 | 100 | 52 | 0.00 | -- | 0.00 | 0.00 | 272.85 | 13.63 | 20.023 |
| 19 | 100 | 53 | 0.00 | -- | 0.00 | 0.00 | 275.03 | 15.14 | 18.161 |
| 20 | 100 | 54 | 0.00 | -- | 0.00 | 0.00 | 277.19 | 16.74 | 16.561 |
| 21 | 100 | 55 | 0.00 | -- | 0.00 | 0.00 | 279.35 | 18.41 | 15.176 |
| 22 | 100 | 55 | 0.00 | -- | 0.00 | 0.00 | 281.50 | 20.15 | 13.967 |
| 23 | 100 | 56 | 0.00 | -- | 0.00 | 0.00 | 283.64 | 21.98 | 12.906 |
| 24 | 100 | 57 | 0.00 | -- | 0.00 | 0.00 | 285.77 | 23.88 | 11.969 |
| 25 | 100 | 58 | 0.00 | -- | 0.00 | 0.00 | 287.89 | 25.85 | 11.137 |
| 26 | 100 | 58 | 0.00 | -- | 0.00 | 0.00 | 290.01 | 27.90 | 10.394 |
| 27 | 100 | 59 | 0.00 | -- | 0.00 | 0.00 | 292.11 | 30.03 | 9.727 |
| 28 | 100 | 60 | 0.00 | -- | 0.00 | 0.00 | 294.21 | 32.23 | 9.127 |
| 29 | 100 | 61 | 0.00 | -- | 0.00 | 0.00 | 296.30 | 34.51 | 8.585 |
| 30 | 100 | 61 | 0.00 | -- | 0.00 | 0.00 | 315.20 | 36.87 | 8.549 |
| 31 | 100 | 62 | 0.00 | -- | 0.00 | 0.00 | 317.38 | 39.30 | 8.075 |
| 32 | 100 | 63 | 0.00 | -- | 0.00 | 0.00 | 319.56 | 41.81 | 7.642 |
| 33 | 100 | 63 | 0.00 | -- | 0.00 | 0.00 | 321.72 | 44.40 | 7.246 |
| 34 | 100 | 64 | 0.00 | -- | 0.00 | 0.00 | 323.88 | 47.06 | 6.882 |

| n° | B [cm] | H [cm] | A _{sw} [cmq] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|-----------|-----------|--------------------------|------|--------------------------|--------------------------|-------------------------|-----------|-------|
| 35 | 100 | 65 | 0.00 | -- | 0.00 | 0.00 | 326.04 | 49.80 | 6.547 |
| 36 | 100 | 66 | 0.00 | -- | 0.00 | 0.00 | 328.19 | 52.61 | 6.238 |
| 37 | 100 | 66 | 0.00 | -- | 0.00 | 0.00 | 330.33 | 55.50 | 5.952 |
| 38 | 100 | 67 | 0.00 | -- | 0.00 | 0.00 | 332.46 | 58.47 | 5.686 |
| 39 | 100 | 68 | 0.00 | -- | 0.00 | 0.00 | 334.59 | 61.51 | 5.439 |
| 40 | 100 | 69 | 0.00 | -- | 0.00 | 0.00 | 336.71 | 64.63 | 5.210 |
| 41 | 100 | 69 | 0.00 | -- | 0.00 | 0.00 | 338.83 | 67.83 | 4.996 |
| 42 | 100 | 70 | 0.00 | -- | 0.00 | 0.00 | 340.94 | 71.10 | 4.795 |
| 43 | 100 | 71 | 0.00 | -- | 0.00 | 0.00 | 343.04 | 74.45 | 4.608 |

Fondazione

| n° | B [cm] | H [cm] | A _{sw} [cmq] | cotθ | V _{Rcd} [kN] | V _{Rsd} [kN] | V _{Rd} [kN] | T [kN] | FS |
|----|-----------|-----------|--------------------------|------|--------------------------|--------------------------|-------------------------|-----------|---------|
| 1 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | 0.00 | 100.000 |
| 2 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -15.54 | 21.447 |
| 3 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -30.74 | 10.843 |
| 4 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -45.60 | 7.309 |
| 5 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -60.12 | 5.544 |
| 6 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -140.36 | 2.375 |
| 7 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -140.41 | 2.374 |
| 8 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -140.18 | 2.378 |
| 9 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -139.43 | 2.391 |
| 10 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -138.42 | 2.408 |
| 11 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -137.17 | 2.430 |
| 12 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -135.66 | 2.457 |
| 13 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -133.90 | 2.489 |
| 14 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -131.89 | 2.527 |
| 15 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -129.63 | 2.571 |
| 16 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -127.12 | 2.622 |
| 17 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -124.36 | 2.680 |
| 18 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -121.34 | 2.747 |
| 19 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -118.08 | 2.823 |
| 20 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -114.56 | 2.909 |
| 21 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -110.79 | 3.008 |
| 22 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -106.77 | 3.122 |
| 23 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -102.50 | 3.252 |
| 24 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -97.98 | 3.402 |
| 25 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -93.21 | 3.576 |
| 26 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -88.18 | 3.780 |
| 27 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -82.91 | 4.020 |
| 28 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -77.38 | 4.307 |
| 29 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -71.60 | 4.655 |
| 30 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -65.57 | 5.083 |
| 31 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -59.29 | 5.622 |
| 32 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -52.76 | 6.318 |
| 33 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -45.98 | 7.250 |
| 34 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -38.94 | 8.559 |
| 35 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -31.66 | 10.529 |
| 36 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -24.12 | 13.820 |
| 37 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -16.33 | 20.411 |
| 38 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | -8.29 | 40.203 |
| 39 | 100 | 80 | 0.00 | -- | 0.00 | 0.00 | 333.31 | 0.00 | 100.000 |

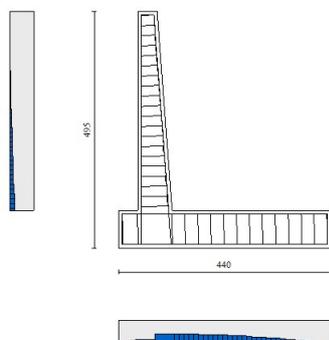


Fig. 18 - Paramento (Inviluppo)

Verifica delle tensioni

Simbologia adottata

| | |
|---------------|---|
| n° | indice sezione |
| Y | ordinata sezione, espressa in [m] |
| B | larghezza sezione, espressa in [cm] |
| H | altezza sezione, espressa in [cm] |
| A_{fi} | area ferri inferiori, espresso in [cmq] |
| A_{fs} | area ferri superiori, espressa in [cmq] |
| M | momento agente, espressa in [kNm] |
| N | sfuerzo normale agente, espressa in [kN] |
| σ_c | tensione di compressione nel cls, espressa in [kPa] |
| σ_{fi} | tensione nei ferri inferiori, espressa in [kPa] |
| σ_{fs} | tensione nei ferri superiori, espressa in [kPa] |

Combinazioni SLER

Paramento

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 303 di 314 |

Tensione massima di compressione nel calcestruzzo 19920 [kPa]

Tensione massima di trazione dell'acciaio 360000 [kPa]

| n° | B | H | Afi | Afs | M | N | σc | σfi | σfs |
|----|------|------|-------|-------|-------|-------|-----------|------------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kN] | [kPa] | [kPa] | [kPa] |
| 1 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0 (10) | 0 (10) | 0 (10) |
| 2 | 100 | 41 | 15.71 | 15.71 | 0.00 | 0.98 | 2 (10) | 31 (10) | 33 (10) |
| 3 | 100 | 41 | 15.71 | 15.71 | 0.01 | 1.97 | 5 (10) | 60 (10) | 69 (10) |
| 4 | 100 | 42 | 15.71 | 15.71 | 0.04 | 2.99 | 8 (10) | 83 (10) | 108 (10) |
| 5 | 100 | 43 | 15.71 | 15.71 | 0.09 | 4.02 | 11 (10) | 100 (10) | 153 (10) |
| 6 | 100 | 44 | 15.71 | 15.71 | 0.16 | 5.07 | 15 (10) | 111 (10) | 204 (10) |
| 7 | 100 | 44 | 15.71 | 15.71 | 0.26 | 6.13 | 19 (10) | 113 (10) | 262 (10) |
| 8 | 100 | 45 | 15.71 | 15.71 | 0.41 | 7.22 | 25 (10) | 106 (10) | 329 (10) |
| 9 | 100 | 46 | 15.71 | 15.71 | 0.59 | 8.32 | 31 (10) | 89 (10) | 405 (10) |
| 10 | 100 | 47 | 15.71 | 15.71 | 0.82 | 9.44 | 38 (10) | 60 (10) | 491 (10) |
| 11 | 100 | 47 | 15.71 | 15.71 | 1.11 | 10.58 | 47 (10) | 4 (10) | 594 (10) |
| 12 | 100 | 48 | 15.71 | 15.71 | 1.47 | 11.74 | 57 (10) | 99 (10) | 718 (10) |
| 13 | 100 | 49 | 15.71 | 15.71 | 1.89 | 12.91 | 71 (10) | 270 (10) | 865 (10) |
| 14 | 100 | 50 | 15.71 | 15.71 | 2.39 | 14.10 | 87 (10) | 533 (10) | 1037 (10) |
| 15 | 100 | 50 | 15.71 | 15.71 | 2.97 | 15.31 | 105 (10) | 904 (10) | 1232 (10) |
| 16 | 100 | 51 | 15.71 | 18.85 | 3.64 | 16.54 | 124 (10) | 1241 (10) | 1429 (10) |
| 17 | 100 | 52 | 15.71 | 18.85 | 4.40 | 17.78 | 147 (10) | 1765 (10) | 1658 (10) |
| 18 | 100 | 52 | 15.71 | 18.85 | 5.25 | 19.04 | 171 (10) | 2390 (10) | 1906 (10) |
| 19 | 100 | 53 | 15.71 | 18.85 | 6.21 | 20.32 | 198 (10) | 3116 (10) | 2173 (10) |
| 20 | 100 | 54 | 15.71 | 18.85 | 7.28 | 21.62 | 228 (10) | 3944 (10) | 2457 (10) |
| 21 | 100 | 55 | 15.71 | 18.85 | 8.47 | 22.94 | 259 (10) | 4874 (10) | 2760 (10) |
| 22 | 100 | 55 | 15.71 | 18.85 | 9.77 | 24.27 | 292 (10) | 5906 (10) | 3081 (10) |
| 23 | 100 | 56 | 15.71 | 18.85 | 11.20 | 25.62 | 327 (10) | 7041 (10) | 3421 (10) |
| 24 | 100 | 57 | 15.71 | 18.85 | 12.76 | 26.99 | 364 (10) | 8280 (10) | 3780 (10) |
| 25 | 100 | 58 | 15.71 | 18.85 | 14.46 | 28.38 | 403 (10) | 9625 (10) | 4157 (10) |
| 26 | 100 | 58 | 15.71 | 18.85 | 16.30 | 29.78 | 444 (10) | 11076 (10) | 4554 (10) |
| 27 | 100 | 59 | 15.71 | 18.85 | 18.28 | 31.21 | 487 (10) | 12635 (10) | 4970 (10) |
| 28 | 100 | 60 | 15.71 | 18.85 | 20.42 | 32.65 | 532 (10) | 14302 (10) | 5406 (10) |
| 29 | 100 | 61 | 15.71 | 18.85 | 22.72 | 34.11 | 579 (10) | 16077 (10) | 5861 (10) |
| 30 | 100 | 61 | 15.71 | 25.13 | 25.18 | 35.58 | 575 (10) | 13837 (10) | 6094 (10) |
| 31 | 100 | 62 | 15.71 | 25.13 | 27.82 | 37.07 | 620 (10) | 15358 (10) | 6568 (10) |
| 32 | 100 | 63 | 15.71 | 25.13 | 30.63 | 38.59 | 668 (10) | 16963 (10) | 7060 (10) |
| 33 | 100 | 63 | 15.71 | 25.13 | 33.62 | 40.12 | 717 (10) | 18655 (10) | 7572 (10) |
| 34 | 100 | 64 | 15.71 | 25.13 | 36.79 | 41.66 | 768 (10) | 20432 (10) | 8102 (10) |
| 35 | 100 | 65 | 15.71 | 25.13 | 40.16 | 43.23 | 820 (10) | 22295 (10) | 8651 (10) |
| 36 | 100 | 66 | 15.71 | 25.13 | 43.73 | 44.81 | 874 (10) | 24246 (10) | 9219 (10) |
| 37 | 100 | 66 | 15.71 | 25.13 | 47.50 | 46.41 | 930 (10) | 26285 (10) | 9805 (10) |
| 38 | 100 | 67 | 15.71 | 25.13 | 51.47 | 48.03 | 987 (10) | 28411 (10) | 10411 (10) |
| 39 | 100 | 68 | 15.71 | 25.13 | 55.67 | 49.67 | 1046 (10) | 30626 (10) | 11035 (10) |
| 40 | 100 | 69 | 15.71 | 25.13 | 60.08 | 51.32 | 1106 (10) | 32930 (10) | 11678 (10) |
| 41 | 100 | 69 | 15.71 | 25.13 | 64.71 | 52.99 | 1168 (10) | 35324 (10) | 12339 (10) |
| 42 | 100 | 70 | 15.71 | 25.13 | 69.58 | 54.68 | 1232 (10) | 37807 (10) | 13020 (10) |
| 43 | 100 | 71 | 15.71 | 25.13 | 74.69 | 56.39 | 1297 (10) | 40381 (10) | 13718 (10) |

Fondazione

Tensione massima di compressione nel calcestruzzo 17430 [kPa]

Tensione massima di trazione dell'acciaio 360000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 1 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 (10) | 0 (10) | 0 (10) |
| 2 | 100 | 80 | 18.85 | 18.85 | 0.57 | 0.00 | 8 (10) | 444 (10) | 78 (10) |
| 3 | 100 | 80 | 18.85 | 18.85 | 2.27 | 0.00 | 34 (10) | 1766 (10) | 312 (10) |
| 4 | 100 | 80 | 18.85 | 18.85 | 5.08 | 0.00 | 75 (10) | 3953 (10) | 699 (10) |
| 5 | 100 | 80 | 18.85 | 18.85 | 8.99 | 0.00 | 133 (10) | 6991 (10) | 1236 (10) |
| 6 | 100 | 80 | 18.85 | 18.85 | -130.87 | 0.00 | 1932 (10) | 17989 (10) | 101780 (10) |
| 7 | 100 | 80 | 18.85 | 18.85 | -126.34 | 0.00 | 1865 (10) | 17366 (10) | 98254 (10) |
| 8 | 100 | 80 | 18.85 | 18.85 | -121.64 | 0.00 | 1795 (10) | 16720 (10) | 94598 (10) |
| 9 | 100 | 80 | 18.85 | 18.85 | -116.54 | 0.00 | 1720 (10) | 16018 (10) | 90629 (10) |
| 10 | 100 | 80 | 18.85 | 18.85 | -111.34 | 0.00 | 1643 (10) | 15305 (10) | 86591 (10) |
| 11 | 100 | 80 | 18.85 | 18.85 | -106.08 | 0.00 | 1566 (10) | 14581 (10) | 82496 (10) |
| 12 | 100 | 80 | 18.85 | 18.85 | -100.76 | 0.00 | 1487 (10) | 13849 (10) | 78358 (10) |
| 13 | 100 | 80 | 18.85 | 18.85 | -95.40 | 0.00 | 1408 (10) | 13113 (10) | 74190 (10) |
| 14 | 100 | 80 | 18.85 | 18.85 | -90.02 | 0.00 | 1329 (10) | 12374 (10) | 70007 (10) |
| 15 | 100 | 80 | 18.85 | 18.85 | -84.64 | 0.00 | 1249 (10) | 11634 (10) | 65822 (10) |
| 16 | 100 | 80 | 18.85 | 18.85 | -79.27 | 0.00 | 1170 (10) | 10896 (10) | 61648 (10) |
| 17 | 100 | 80 | 18.85 | 18.85 | -73.93 | 0.00 | 1091 (10) | 10163 (10) | 57499 (10) |
| 18 | 100 | 80 | 18.85 | 18.85 | -68.65 | 0.00 | 1013 (10) | 9436 (10) | 53388 (10) |
| 19 | 100 | 80 | 18.85 | 18.85 | -63.43 | 0.00 | 936 (10) | 8719 (10) | 49330 (10) |
| 20 | 100 | 80 | 18.85 | 18.85 | -58.30 | 0.00 | 860 (10) | 8013 (10) | 45337 (10) |
| 21 | 100 | 80 | 18.85 | 18.85 | -53.26 | 0.00 | 786 (10) | 7321 (10) | 41423 (10) |
| 22 | 100 | 80 | 18.85 | 18.85 | -48.35 | 0.00 | 714 (10) | 6646 (10) | 37602 (10) |
| 23 | 100 | 80 | 18.85 | 18.85 | -43.57 | 0.00 | 643 (10) | 5990 (10) | 33888 (10) |
| 24 | 100 | 80 | 18.85 | 18.85 | -38.95 | 0.00 | 575 (10) | 5354 (10) | 30293 (10) |
| 25 | 100 | 80 | 18.85 | 18.85 | -34.50 | 0.00 | 509 (10) | 4743 (10) | 26832 (10) |
| 26 | 100 | 80 | 18.85 | 18.85 | -30.24 | 0.00 | 446 (10) | 4157 (10) | 23518 (10) |
| 27 | 100 | 80 | 18.85 | 18.85 | -26.19 | 0.00 | 386 (10) | 3599 (10) | 20365 (10) |
| 28 | 100 | 80 | 18.85 | 18.85 | -22.36 | 0.00 | 330 (10) | 3073 (10) | 17386 (10) |
| 29 | 100 | 80 | 18.85 | 18.85 | -18.77 | 0.00 | 277 (10) | 2580 (10) | 14595 (10) |
| 30 | 100 | 80 | 18.85 | 18.85 | -15.44 | 0.00 | 228 (10) | 2122 (10) | 12005 (10) |
| 31 | 100 | 80 | 18.85 | 18.85 | -12.38 | 0.00 | 183 (10) | 1702 (10) | 9630 (10) |
| 32 | 100 | 80 | 18.85 | 18.85 | -9.62 | 0.00 | 142 (10) | 1323 (10) | 7484 (10) |
| 33 | 100 | 80 | 18.85 | 18.85 | -7.18 | 0.00 | 106 (10) | 986 (10) | 5580 (10) |
| 34 | 100 | 80 | 18.85 | 18.85 | -5.06 | 0.00 | 75 (10) | 695 (10) | 3932 (10) |
| 35 | 100 | 80 | 18.85 | 18.85 | -3.28 | 0.00 | 48 (10) | 451 (10) | 2552 (10) |
| 36 | 100 | 80 | 18.85 | 18.85 | -1.87 | 0.00 | 28 (10) | 257 (10) | 1456 (10) |
| 37 | 100 | 80 | 18.85 | 18.85 | -0.84 | 0.00 | 12 (10) | 116 (10) | 656 (10) |
| 38 | 100 | 80 | 18.85 | 18.85 | -0.21 | 0.00 | 3 (10) | 29 (10) | 166 (10) |
| 39 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 (10) | 0 (10) | 0 (10) |

Combinazioni SLEF

Paramento

Tensione massima di compressione nel calcestruzzo 33200 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 1 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0 (11) | 0 (11) | 0 (11) |
| 2 | 100 | 41 | 15.71 | 15.71 | 0.00 | 0.98 | 2 (11) | 31 (11) | 33 (11) |
| 3 | 100 | 41 | 15.71 | 15.71 | 0.01 | 1.97 | 5 (11) | 60 (11) | 69 (11) |
| 4 | 100 | 42 | 15.71 | 15.71 | 0.04 | 2.99 | 8 (11) | 83 (11) | 108 (11) |

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 5 | 100 | 43 | 15.71 | 15.71 | 0.09 | 4.02 | 11 (11) | 100 (11) | 153 (11) |
| 6 | 100 | 44 | 15.71 | 15.71 | 0.16 | 5.07 | 15 (11) | 111 (11) | 204 (11) |
| 7 | 100 | 44 | 15.71 | 15.71 | 0.26 | 6.13 | 19 (11) | 113 (11) | 262 (11) |
| 8 | 100 | 45 | 15.71 | 15.71 | 0.41 | 7.22 | 25 (11) | 106 (11) | 329 (11) |
| 9 | 100 | 46 | 15.71 | 15.71 | 0.59 | 8.32 | 31 (11) | 89 (11) | 405 (11) |
| 10 | 100 | 47 | 15.71 | 15.71 | 0.82 | 9.44 | 38 (11) | 60 (11) | 491 (11) |
| 11 | 100 | 47 | 15.71 | 15.71 | 1.11 | 10.58 | 47 (11) | 0 (1) | 594 (11) |
| 12 | 100 | 48 | 15.71 | 15.71 | 1.47 | 11.74 | 57 (11) | 99 (11) | 718 (11) |
| 13 | 100 | 49 | 15.71 | 15.71 | 1.89 | 12.91 | 71 (11) | 270 (11) | 865 (11) |
| 14 | 100 | 50 | 15.71 | 15.71 | 2.39 | 14.10 | 87 (11) | 533 (11) | 1037 (11) |
| 15 | 100 | 50 | 15.71 | 15.71 | 2.97 | 15.31 | 105 (11) | 904 (11) | 1232 (11) |
| 16 | 100 | 51 | 15.71 | 18.85 | 3.64 | 16.54 | 124 (11) | 1241 (11) | 1429 (11) |
| 17 | 100 | 52 | 15.71 | 18.85 | 4.40 | 17.78 | 147 (11) | 1765 (11) | 1658 (11) |
| 18 | 100 | 52 | 15.71 | 18.85 | 5.25 | 19.04 | 171 (11) | 2390 (11) | 1906 (11) |
| 19 | 100 | 53 | 15.71 | 18.85 | 6.21 | 20.32 | 198 (11) | 3116 (11) | 2173 (11) |
| 20 | 100 | 54 | 15.71 | 18.85 | 7.28 | 21.62 | 228 (11) | 3944 (11) | 2457 (11) |
| 21 | 100 | 55 | 15.71 | 18.85 | 8.47 | 22.94 | 259 (11) | 4874 (11) | 2760 (11) |
| 22 | 100 | 55 | 15.71 | 18.85 | 9.77 | 24.27 | 292 (11) | 5906 (11) | 3081 (11) |
| 23 | 100 | 56 | 15.71 | 18.85 | 11.20 | 25.62 | 327 (11) | 7041 (11) | 3421 (11) |
| 24 | 100 | 57 | 15.71 | 18.85 | 12.76 | 26.99 | 364 (11) | 8280 (11) | 3780 (11) |
| 25 | 100 | 58 | 15.71 | 18.85 | 14.46 | 28.38 | 403 (11) | 9625 (11) | 4157 (11) |
| 26 | 100 | 58 | 15.71 | 18.85 | 16.30 | 29.78 | 444 (11) | 11076 (11) | 4554 (11) |
| 27 | 100 | 59 | 15.71 | 18.85 | 18.28 | 31.21 | 487 (11) | 12635 (11) | 4970 (11) |
| 28 | 100 | 60 | 15.71 | 18.85 | 20.42 | 32.65 | 532 (11) | 14302 (11) | 5406 (11) |
| 29 | 100 | 61 | 15.71 | 18.85 | 22.72 | 34.11 | 579 (11) | 16077 (11) | 5861 (11) |
| 30 | 100 | 61 | 15.71 | 25.13 | 25.18 | 35.58 | 575 (11) | 13837 (11) | 6094 (11) |
| 31 | 100 | 62 | 15.71 | 25.13 | 27.82 | 37.07 | 620 (11) | 15358 (11) | 6568 (11) |
| 32 | 100 | 63 | 15.71 | 25.13 | 30.63 | 38.59 | 668 (11) | 16963 (11) | 7060 (11) |
| 33 | 100 | 63 | 15.71 | 25.13 | 33.62 | 40.12 | 717 (11) | 18655 (11) | 7572 (11) |
| 34 | 100 | 64 | 15.71 | 25.13 | 36.79 | 41.66 | 768 (11) | 20432 (11) | 8102 (11) |
| 35 | 100 | 65 | 15.71 | 25.13 | 40.16 | 43.23 | 820 (11) | 22295 (11) | 8651 (11) |
| 36 | 100 | 66 | 15.71 | 25.13 | 43.73 | 44.81 | 874 (11) | 24246 (11) | 9219 (11) |
| 37 | 100 | 66 | 15.71 | 25.13 | 47.50 | 46.41 | 930 (11) | 26285 (11) | 9805 (11) |
| 38 | 100 | 67 | 15.71 | 25.13 | 51.47 | 48.03 | 987 (11) | 28411 (11) | 10411 (11) |
| 39 | 100 | 68 | 15.71 | 25.13 | 55.67 | 49.67 | 1046 (11) | 30626 (11) | 11035 (11) |
| 40 | 100 | 69 | 15.71 | 25.13 | 60.08 | 51.32 | 1106 (11) | 32930 (11) | 11678 (11) |
| 41 | 100 | 69 | 15.71 | 25.13 | 64.71 | 52.99 | 1168 (11) | 35324 (11) | 12339 (11) |
| 42 | 100 | 70 | 15.71 | 25.13 | 69.58 | 54.68 | 1232 (11) | 37807 (11) | 13020 (11) |
| 43 | 100 | 71 | 15.71 | 25.13 | 74.69 | 56.39 | 1297 (11) | 40381 (11) | 13718 (11) |

Fondazione

Tensione massima di compressione nel calcestruzzo 29050 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 1 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 (11) | 0 (11) | 0 (11) |
| 2 | 100 | 80 | 18.85 | 18.85 | 0.57 | 0.00 | 8 (11) | 444 (11) | 78 (11) |
| 3 | 100 | 80 | 18.85 | 18.85 | 2.27 | 0.00 | 34 (11) | 1766 (11) | 312 (11) |
| 4 | 100 | 80 | 18.85 | 18.85 | 5.08 | 0.00 | 75 (11) | 3953 (11) | 699 (11) |
| 5 | 100 | 80 | 18.85 | 18.85 | 8.99 | 0.00 | 133 (11) | 6991 (11) | 1236 (11) |
| 6 | 100 | 80 | 18.85 | 18.85 | -130.87 | 0.00 | 1932 (11) | 17989 (11) | 101780 (11) |
| 7 | 100 | 80 | 18.85 | 18.85 | -126.34 | 0.00 | 1865 (11) | 17366 (11) | 98254 (11) |
| 8 | 100 | 80 | 18.85 | 18.85 | -121.64 | 0.00 | 1795 (11) | 16720 (11) | 94598 (11) |
| 9 | 100 | 80 | 18.85 | 18.85 | -116.54 | 0.00 | 1720 (11) | 16018 (11) | 90629 (11) |

Relazione di calcolo muro di sostegno sede stradale-NV24

COMMESSA LOTTO CODIFICA DOCUMENTO REV. FOGLIO
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| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 10 | 100 | 80 | 18.85 | 18.85 | -111.34 | 0.00 | 1643 (11) | 15305 (11) | 86591 (11) |
| 11 | 100 | 80 | 18.85 | 18.85 | -106.08 | 0.00 | 1566 (11) | 14581 (11) | 82496 (11) |
| 12 | 100 | 80 | 18.85 | 18.85 | -100.76 | 0.00 | 1487 (11) | 13849 (11) | 78358 (11) |
| 13 | 100 | 80 | 18.85 | 18.85 | -95.40 | 0.00 | 1408 (11) | 13113 (11) | 74190 (11) |
| 14 | 100 | 80 | 18.85 | 18.85 | -90.02 | 0.00 | 1329 (11) | 12374 (11) | 70007 (11) |
| 15 | 100 | 80 | 18.85 | 18.85 | -84.64 | 0.00 | 1249 (11) | 11634 (11) | 65822 (11) |
| 16 | 100 | 80 | 18.85 | 18.85 | -79.27 | 0.00 | 1170 (11) | 10896 (11) | 61648 (11) |
| 17 | 100 | 80 | 18.85 | 18.85 | -73.93 | 0.00 | 1091 (11) | 10163 (11) | 57499 (11) |
| 18 | 100 | 80 | 18.85 | 18.85 | -68.65 | 0.00 | 1013 (11) | 9436 (11) | 53388 (11) |
| 19 | 100 | 80 | 18.85 | 18.85 | -63.43 | 0.00 | 936 (11) | 8719 (11) | 49330 (11) |
| 20 | 100 | 80 | 18.85 | 18.85 | -58.30 | 0.00 | 860 (11) | 8013 (11) | 45337 (11) |
| 21 | 100 | 80 | 18.85 | 18.85 | -53.26 | 0.00 | 786 (11) | 7321 (11) | 41423 (11) |
| 22 | 100 | 80 | 18.85 | 18.85 | -48.35 | 0.00 | 714 (11) | 6646 (11) | 37602 (11) |
| 23 | 100 | 80 | 18.85 | 18.85 | -43.57 | 0.00 | 643 (11) | 5990 (11) | 33888 (11) |
| 24 | 100 | 80 | 18.85 | 18.85 | -38.95 | 0.00 | 575 (11) | 5354 (11) | 30293 (11) |
| 25 | 100 | 80 | 18.85 | 18.85 | -34.50 | 0.00 | 509 (11) | 4743 (11) | 26832 (11) |
| 26 | 100 | 80 | 18.85 | 18.85 | -30.24 | 0.00 | 446 (11) | 4157 (11) | 23518 (11) |
| 27 | 100 | 80 | 18.85 | 18.85 | -26.19 | 0.00 | 386 (11) | 3599 (11) | 20365 (11) |
| 28 | 100 | 80 | 18.85 | 18.85 | -22.36 | 0.00 | 330 (11) | 3073 (11) | 17386 (11) |
| 29 | 100 | 80 | 18.85 | 18.85 | -18.77 | 0.00 | 277 (11) | 2580 (11) | 14595 (11) |
| 30 | 100 | 80 | 18.85 | 18.85 | -15.44 | 0.00 | 228 (11) | 2122 (11) | 12005 (11) |
| 31 | 100 | 80 | 18.85 | 18.85 | -12.38 | 0.00 | 183 (11) | 1702 (11) | 9630 (11) |
| 32 | 100 | 80 | 18.85 | 18.85 | -9.62 | 0.00 | 142 (11) | 1323 (11) | 7484 (11) |
| 33 | 100 | 80 | 18.85 | 18.85 | -7.18 | 0.00 | 106 (11) | 986 (11) | 5580 (11) |
| 34 | 100 | 80 | 18.85 | 18.85 | -5.06 | 0.00 | 75 (11) | 695 (11) | 3932 (11) |
| 35 | 100 | 80 | 18.85 | 18.85 | -3.28 | 0.00 | 48 (11) | 451 (11) | 2552 (11) |
| 36 | 100 | 80 | 18.85 | 18.85 | -1.87 | 0.00 | 28 (11) | 257 (11) | 1456 (11) |
| 37 | 100 | 80 | 18.85 | 18.85 | -0.84 | 0.00 | 12 (11) | 116 (11) | 656 (11) |
| 38 | 100 | 80 | 18.85 | 18.85 | -0.21 | 0.00 | 3 (11) | 29 (11) | 166 (11) |
| 39 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 (11) | 0 (11) | 0 (11) |

Combinazioni SLEQ

Paramento

Tensione massima di compressione nel calcestruzzo 14940 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σc [kPa] | σfi [kPa] | σfs [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|-------------|--------------|--------------|
| 1 | 100 | 40 | 15.71 | 15.71 | 0.00 | 0.00 | 0 (12) | 0 (12) | 0 (12) |
| 2 | 100 | 41 | 15.71 | 15.71 | 0.01 | 0.98 | 2 (13) | 31 (12) | 34 (13) |
| 3 | 100 | 41 | 15.71 | 15.71 | 0.03 | 1.97 | 5 (13) | 60 (12) | 74 (13) |
| 4 | 100 | 42 | 15.71 | 15.71 | 0.08 | 2.99 | 9 (13) | 83 (12) | 120 (13) |
| 5 | 100 | 43 | 15.71 | 15.71 | 0.16 | 4.02 | 13 (13) | 100 (12) | 174 (13) |
| 6 | 100 | 44 | 15.71 | 15.71 | 0.28 | 5.07 | 18 (13) | 111 (12) | 237 (13) |
| 7 | 100 | 44 | 15.71 | 15.71 | 0.44 | 6.13 | 24 (13) | 113 (12) | 311 (13) |
| 8 | 100 | 45 | 15.71 | 15.71 | 0.65 | 7.22 | 31 (13) | 106 (12) | 397 (13) |
| 9 | 100 | 46 | 15.71 | 15.71 | 0.92 | 8.32 | 40 (13) | 89 (12) | 502 (13) |
| 10 | 100 | 47 | 15.71 | 15.71 | 1.26 | 9.44 | 51 (13) | 152 (13) | 631 (13) |
| 11 | 100 | 47 | 15.71 | 15.71 | 1.67 | 10.58 | 66 (13) | 365 (13) | 786 (13) |
| 12 | 100 | 48 | 15.71 | 15.71 | 2.16 | 11.74 | 84 (13) | 692 (13) | 967 (13) |
| 13 | 100 | 49 | 15.71 | 15.71 | 2.75 | 12.91 | 105 (13) | 1147 (13) | 1173 (13) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 307 di 314 |

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 14 | 100 | 50 | 15.71 | 15.71 | 3.43 | 14.10 | 128 (13) | 1738 (13) | 1402 (13) |
| 15 | 100 | 50 | 15.71 | 15.71 | 4.21 | 15.31 | 155 (13) | 2467 (13) | 1652 (13) |
| 16 | 100 | 51 | 15.71 | 18.85 | 5.11 | 16.54 | 177 (13) | 2881 (13) | 1888 (13) |
| 17 | 100 | 52 | 15.71 | 18.85 | 6.12 | 17.78 | 207 (13) | 3732 (13) | 2174 (13) |
| 18 | 100 | 52 | 15.71 | 18.85 | 7.25 | 19.04 | 239 (13) | 4701 (13) | 2481 (13) |
| 19 | 100 | 53 | 15.71 | 18.85 | 8.52 | 20.32 | 274 (13) | 5789 (13) | 2811 (13) |
| 20 | 100 | 54 | 15.71 | 18.85 | 9.92 | 21.62 | 312 (13) | 6998 (13) | 3163 (13) |
| 21 | 100 | 55 | 15.71 | 18.85 | 11.47 | 22.94 | 352 (13) | 8329 (13) | 3537 (13) |
| 22 | 100 | 55 | 15.71 | 18.85 | 13.16 | 24.27 | 394 (13) | 9784 (13) | 3935 (13) |
| 23 | 100 | 56 | 15.71 | 18.85 | 15.02 | 25.62 | 439 (13) | 11365 (13) | 4355 (13) |
| 24 | 100 | 57 | 15.71 | 18.85 | 17.03 | 26.99 | 486 (13) | 13073 (13) | 4799 (13) |
| 25 | 100 | 58 | 15.71 | 18.85 | 19.22 | 28.38 | 536 (13) | 14910 (13) | 5267 (13) |
| 26 | 100 | 58 | 15.71 | 18.85 | 21.59 | 29.78 | 587 (13) | 16876 (13) | 5758 (13) |
| 27 | 100 | 59 | 15.71 | 18.85 | 24.14 | 31.21 | 642 (13) | 18975 (13) | 6273 (13) |
| 28 | 100 | 60 | 15.71 | 18.85 | 26.88 | 32.65 | 698 (13) | 21206 (13) | 6813 (13) |
| 29 | 100 | 61 | 15.71 | 18.85 | 29.82 | 34.11 | 757 (13) | 23571 (13) | 7377 (13) |
| 30 | 100 | 61 | 15.71 | 25.13 | 32.96 | 35.58 | 746 (13) | 19977 (13) | 7678 (13) |
| 31 | 100 | 62 | 15.71 | 25.13 | 36.31 | 37.07 | 803 (13) | 21982 (13) | 8266 (13) |
| 32 | 100 | 63 | 15.71 | 25.13 | 39.88 | 38.59 | 862 (13) | 24092 (13) | 8876 (13) |
| 33 | 100 | 63 | 15.71 | 25.13 | 43.68 | 40.12 | 924 (13) | 26307 (13) | 9510 (13) |
| 34 | 100 | 64 | 15.71 | 25.13 | 47.70 | 41.66 | 987 (13) | 28627 (13) | 10166 (13) |
| 35 | 100 | 65 | 15.71 | 25.13 | 51.97 | 43.23 | 1053 (13) | 31053 (13) | 10846 (13) |
| 36 | 100 | 66 | 15.71 | 25.13 | 56.47 | 44.81 | 1120 (13) | 33586 (13) | 11548 (13) |
| 37 | 100 | 66 | 15.71 | 25.13 | 61.23 | 46.41 | 1189 (13) | 36227 (13) | 12274 (13) |
| 38 | 100 | 67 | 15.71 | 25.13 | 66.25 | 48.03 | 1261 (13) | 38976 (13) | 13022 (13) |
| 39 | 100 | 68 | 15.71 | 25.13 | 71.53 | 49.67 | 1334 (13) | 41833 (13) | 13794 (13) |
| 40 | 100 | 69 | 15.71 | 25.13 | 77.09 | 51.32 | 1409 (13) | 44800 (13) | 14588 (13) |
| 41 | 100 | 69 | 15.71 | 25.13 | 82.92 | 52.99 | 1486 (13) | 47877 (13) | 15405 (13) |
| 42 | 100 | 70 | 15.71 | 25.13 | 89.03 | 54.68 | 1565 (13) | 51063 (13) | 16244 (13) |
| 43 | 100 | 71 | 15.71 | 25.13 | 95.44 | 56.39 | 1646 (13) | 54360 (13) | 17106 (13) |

Fondazione

Tensione massima di compressione nel calcestruzzo 13073 [kPa]

Tensione massima di trazione dell'acciaio 450000 [kPa]

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 1 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 (12) | 0 (12) | 0 (12) |
| 2 | 100 | 80 | 18.85 | 18.85 | 0.75 | 0.00 | 11 (13) | 580 (13) | 102 (13) |
| 3 | 100 | 80 | 18.85 | 18.85 | 2.96 | 0.00 | 44 (13) | 2302 (13) | 407 (13) |
| 4 | 100 | 80 | 18.85 | 18.85 | 6.61 | 0.00 | 98 (13) | 5142 (13) | 909 (13) |
| 5 | 100 | 80 | 18.85 | 18.85 | 11.67 | 0.00 | 172 (13) | 9075 (13) | 1604 (13) |
| 6 | 100 | 80 | 18.85 | 18.85 | -197.64 | 0.00 | 2917 (13) | 27167 (13) | 153704 (13) |
| 7 | 100 | 80 | 18.85 | 18.85 | -191.57 | 0.00 | 2827 (13) | 26332 (13) | 148983 (13) |
| 8 | 100 | 80 | 18.85 | 18.85 | -185.15 | 0.00 | 2733 (13) | 25450 (13) | 143991 (13) |
| 9 | 100 | 80 | 18.85 | 18.85 | -178.17 | 0.00 | 2630 (13) | 24490 (13) | 138559 (13) |
| 10 | 100 | 80 | 18.85 | 18.85 | -170.94 | 0.00 | 2523 (13) | 23497 (13) | 132942 (13) |
| 11 | 100 | 80 | 18.85 | 18.85 | -163.51 | 0.00 | 2413 (13) | 22475 (13) | 127162 (13) |
| 12 | 100 | 80 | 18.85 | 18.85 | -155.90 | 0.00 | 2301 (13) | 21430 (13) | 121245 (13) |
| 13 | 100 | 80 | 18.85 | 18.85 | -148.15 | 0.00 | 2187 (13) | 20364 (13) | 115216 (13) |
| 14 | 100 | 80 | 18.85 | 18.85 | -140.28 | 0.00 | 2070 (13) | 19283 (13) | 109099 (13) |
| 15 | 100 | 80 | 18.85 | 18.85 | -132.34 | 0.00 | 1953 (13) | 18191 (13) | 102919 (13) |
| 16 | 100 | 80 | 18.85 | 18.85 | -124.34 | 0.00 | 1835 (13) | 17092 (13) | 96701 (13) |
| 17 | 100 | 80 | 18.85 | 18.85 | -116.33 | 0.00 | 1717 (13) | 15990 (13) | 90469 (13) |
| 18 | 100 | 80 | 18.85 | 18.85 | -108.33 | 0.00 | 1599 (13) | 14891 (13) | 84249 (13) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| | | | | | |
|----------|---------|----------|--------------|------|------------|
| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 308 di 314 |

| n° | B [cm] | H [cm] | Afi [cmq] | Afs [cmq] | M [kNm] | N [kN] | σ_c [kPa] | σ_{fi} [kPa] | σ_{fs} [kPa] |
|----|-----------|-----------|--------------|--------------|------------|-----------|---------------------|------------------------|------------------------|
| 19 | 100 | 80 | 18.85 | 18.85 | -100.38 | 0.00 | 1482 (13) | 13798 (13) | 78065 (13) |
| 20 | 100 | 80 | 18.85 | 18.85 | -92.51 | 0.00 | 1365 (13) | 12715 (13) | 71941 (13) |
| 21 | 100 | 80 | 18.85 | 18.85 | -84.74 | 0.00 | 1251 (13) | 11648 (13) | 65902 (13) |
| 22 | 100 | 80 | 18.85 | 18.85 | -77.12 | 0.00 | 1138 (13) | 10600 (13) | 59974 (13) |
| 23 | 100 | 80 | 18.85 | 18.85 | -69.67 | 0.00 | 1028 (13) | 9576 (13) | 54181 (13) |
| 24 | 100 | 80 | 18.85 | 18.85 | -62.42 | 0.00 | 921 (13) | 8581 (13) | 48547 (13) |
| 25 | 100 | 80 | 18.85 | 18.85 | -55.42 | 0.00 | 818 (13) | 7617 (13) | 43098 (13) |
| 26 | 100 | 80 | 18.85 | 18.85 | -48.68 | 0.00 | 718 (13) | 6691 (13) | 37857 (13) |
| 27 | 100 | 80 | 18.85 | 18.85 | -42.24 | 0.00 | 623 (13) | 5806 (13) | 32850 (13) |
| 28 | 100 | 80 | 18.85 | 18.85 | -36.13 | 0.00 | 533 (13) | 4967 (13) | 28102 (13) |
| 29 | 100 | 80 | 18.85 | 18.85 | -30.39 | 0.00 | 449 (13) | 4178 (13) | 23637 (13) |
| 30 | 100 | 80 | 18.85 | 18.85 | -25.05 | 0.00 | 370 (13) | 3443 (13) | 19480 (13) |
| 31 | 100 | 80 | 18.85 | 18.85 | -20.13 | 0.00 | 297 (13) | 2767 (13) | 15655 (13) |
| 32 | 100 | 80 | 18.85 | 18.85 | -15.67 | 0.00 | 231 (13) | 2154 (13) | 12188 (13) |
| 33 | 100 | 80 | 18.85 | 18.85 | -11.70 | 0.00 | 173 (13) | 1609 (13) | 9103 (13) |
| 34 | 100 | 80 | 18.85 | 18.85 | -8.26 | 0.00 | 122 (13) | 1135 (13) | 6424 (13) |
| 35 | 100 | 80 | 18.85 | 18.85 | -5.37 | 0.00 | 79 (13) | 738 (13) | 4177 (13) |
| 36 | 100 | 80 | 18.85 | 18.85 | -3.07 | 0.00 | 45 (13) | 422 (13) | 2387 (13) |
| 37 | 100 | 80 | 18.85 | 18.85 | -1.39 | 0.00 | 20 (13) | 190 (13) | 1077 (13) |
| 38 | 100 | 80 | 18.85 | 18.85 | -0.35 | 0.00 | 5 (13) | 48 (13) | 273 (13) |
| 39 | 100 | 80 | 18.85 | 18.85 | 0.00 | 0.00 | 0 (12) | 0 (12) | 0 (12) |

Verifica a fessurazione

Simbologia adottata

| | |
|------------|---|
| n° | indice sezione |
| Y | ordinata sezione espressa in [m] |
| B | larghezza sezione espresso in [cm] |
| H | altezza sezione espressa in [cm] |
| Af | area ferri zona tesa espresso in [cmq] |
| Aeff | area efficace espressa in [cmq] |
| M | momento agente espressa in [kNm] |
| Mpf | momento di prima fessurazione espressa in [kNm] |
| ϵ | deformazione espresso in % |
| Sm | spaziatura tra le fessure espressa in [mm] |
| w | apertura delle fessure espressa in [mm] |

Combinazioni SLER

Paramento

Apertura limite fessure $w_{lim}=0.20$

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 1 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (10) |
| 2 | 100 | 41 | 0.00 | 0.00 | 0.00 | 4.10 | 0.000000 | 0.00 | 0.000 (10) |
| 3 | 100 | 41 | 0.00 | 0.00 | 0.01 | 11.89 | 0.000000 | 0.00 | 0.000 (10) |
| 4 | 100 | 42 | 0.00 | 0.00 | 0.04 | 24.90 | 0.000000 | 0.00 | 0.000 (10) |
| 5 | 100 | 43 | 0.00 | 0.00 | 0.09 | 46.10 | 0.000000 | 0.00 | 0.000 (10) |
| 6 | 100 | 44 | 0.00 | 0.00 | 0.16 | 81.86 | 0.000000 | 0.00 | 0.000 (10) |
| 7 | 100 | 44 | 0.00 | 0.00 | 0.26 | 148.17 | 0.000000 | 0.00 | 0.000 (10) |
| 8 | 100 | 45 | 0.00 | 0.00 | 0.41 | 299.26 | 0.000000 | 0.00 | 0.000 (10) |
| 9 | 100 | 46 | 0.00 | 0.00 | 0.59 | 914.46 | 0.000000 | 0.00 | 0.000 (10) |
| 10 | 100 | 47 | 0.00 | 0.00 | 0.82 | 2240.61 | 0.000000 | 0.00 | 0.000 (10) |
| 11 | 100 | 47 | 0.00 | 0.00 | 1.11 | 654.18 | 0.000000 | 0.00 | 0.000 (10) |
| 12 | 100 | 48 | 15.71 | 1550.00 | 1.47 | 434.45 | 0.000000 | 0.00 | 0.000 (10) |
| 13 | 100 | 49 | 15.71 | 1550.00 | 1.89 | 349.89 | 0.000000 | 0.00 | 0.000 (10) |
| 14 | 100 | 50 | 15.71 | 1550.00 | 2.39 | 306.82 | 0.000000 | 0.00 | 0.000 (10) |
| 15 | 100 | 50 | 15.71 | 1550.00 | 2.97 | 281.88 | 0.000000 | 0.00 | 0.000 (10) |
| 16 | 100 | 51 | 18.85 | 1550.00 | 3.64 | 270.61 | 0.000000 | 0.00 | 0.000 (10) |
| 17 | 100 | 52 | 18.85 | 1550.00 | 4.40 | 260.84 | 0.000000 | 0.00 | 0.000 (10) |
| 18 | 100 | 52 | 18.85 | 1550.00 | 5.25 | 254.68 | 0.000000 | 0.00 | 0.000 (10) |
| 19 | 100 | 53 | 18.85 | 1550.00 | 6.21 | 250.97 | 0.000000 | 0.00 | 0.000 (10) |
| 20 | 100 | 54 | 18.85 | 1550.00 | 7.28 | 249.01 | 0.000000 | 0.00 | 0.000 (10) |
| 21 | 100 | 55 | 18.85 | 1550.00 | 8.47 | 248.34 | 0.000000 | 0.00 | 0.000 (10) |
| 22 | 100 | 55 | 18.85 | 1550.00 | 9.77 | 248.66 | 0.000000 | 0.00 | 0.000 (10) |
| 23 | 100 | 56 | 18.85 | 1550.00 | 11.20 | 249.76 | 0.000000 | 0.00 | 0.000 (10) |
| 24 | 100 | 57 | 18.85 | 1550.00 | 12.76 | 251.48 | 0.000000 | 0.00 | 0.000 (10) |
| 25 | 100 | 58 | 18.85 | 1550.00 | 14.46 | 253.70 | 0.000000 | 0.00 | 0.000 (10) |
| 26 | 100 | 58 | 18.85 | 1550.00 | 16.30 | 256.35 | 0.000000 | 0.00 | 0.000 (10) |
| 27 | 100 | 59 | 18.85 | 1550.00 | 18.28 | 259.37 | 0.000000 | 0.00 | 0.000 (10) |
| 28 | 100 | 60 | 18.85 | 1550.00 | 20.42 | 262.69 | 0.000000 | 0.00 | 0.000 (10) |
| 29 | 100 | 61 | 18.85 | 1550.00 | 22.72 | 266.27 | 0.000000 | 0.00 | 0.000 (10) |
| 30 | 100 | 61 | 25.13 | 1550.00 | 25.18 | 279.38 | 0.000000 | 0.00 | 0.000 (10) |
| 31 | 100 | 62 | 25.13 | 1550.00 | 27.82 | 283.53 | 0.000000 | 0.00 | 0.000 (10) |
| 32 | 100 | 63 | 25.13 | 1550.00 | 30.63 | 287.87 | 0.000000 | 0.00 | 0.000 (10) |
| 33 | 100 | 63 | 25.13 | 1550.00 | 33.62 | 292.39 | 0.000000 | 0.00 | 0.000 (10) |
| 34 | 100 | 64 | 25.13 | 1550.00 | 36.79 | 297.06 | 0.000000 | 0.00 | 0.000 (10) |
| 35 | 100 | 65 | 25.13 | 1550.00 | 40.16 | 301.89 | 0.000000 | 0.00 | 0.000 (10) |
| 36 | 100 | 66 | 25.13 | 1550.00 | 43.73 | 306.84 | 0.000000 | 0.00 | 0.000 (10) |
| 37 | 100 | 66 | 25.13 | 1550.00 | 47.50 | 311.93 | 0.000000 | 0.00 | 0.000 (10) |
| 38 | 100 | 67 | 25.13 | 1550.00 | 51.47 | 317.13 | 0.000000 | 0.00 | 0.000 (10) |
| 39 | 100 | 68 | 25.13 | 1550.00 | 55.67 | 322.45 | 0.000000 | 0.00 | 0.000 (10) |
| 40 | 100 | 69 | 25.13 | 1550.00 | 60.08 | 327.88 | 0.000000 | 0.00 | 0.000 (10) |
| 41 | 100 | 69 | 25.13 | 1550.00 | 64.71 | 333.41 | 0.000000 | 0.00 | 0.000 (10) |
| 42 | 100 | 70 | 25.13 | 1550.00 | 69.58 | 339.03 | 0.000000 | 0.00 | 0.000 (10) |
| 43 | 100 | 71 | 25.13 | 1550.00 | 74.69 | 344.75 | 0.000000 | 0.00 | 0.000 (10) |

Fondazione

Apertura limite fessure $w_{lim}=0.20$

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 1 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (10) |
| 2 | 100 | 80 | 18.85 | 1550.00 | 0.57 | 351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 3 | 100 | 80 | 18.85 | 1550.00 | 2.27 | 351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 4 | 100 | 80 | 18.85 | 1550.00 | 5.08 | 351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 5 | 100 | 80 | 18.85 | 1550.00 | 8.99 | 351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 6 | 100 | 80 | 18.85 | 1550.00 | -130.87 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 7 | 100 | 80 | 18.85 | 1550.00 | -126.34 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 8 | 100 | 80 | 18.85 | 1550.00 | -121.64 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 9 | 100 | 80 | 18.85 | 1550.00 | -116.54 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 10 | 100 | 80 | 18.85 | 1550.00 | -111.34 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 11 | 100 | 80 | 18.85 | 1550.00 | -106.08 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 12 | 100 | 80 | 18.85 | 1550.00 | -100.76 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 13 | 100 | 80 | 18.85 | 1550.00 | -95.40 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 14 | 100 | 80 | 18.85 | 1550.00 | -90.02 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 15 | 100 | 80 | 18.85 | 1550.00 | -84.64 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 16 | 100 | 80 | 18.85 | 1550.00 | -79.27 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 17 | 100 | 80 | 18.85 | 1550.00 | -73.93 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 18 | 100 | 80 | 18.85 | 1550.00 | -68.65 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 19 | 100 | 80 | 18.85 | 1550.00 | -63.43 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 20 | 100 | 80 | 18.85 | 1550.00 | -58.30 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 21 | 100 | 80 | 18.85 | 1550.00 | -53.26 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 22 | 100 | 80 | 18.85 | 1550.00 | -48.35 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 23 | 100 | 80 | 18.85 | 1550.00 | -43.57 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 24 | 100 | 80 | 18.85 | 1550.00 | -38.95 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 25 | 100 | 80 | 18.85 | 1550.00 | -34.50 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 26 | 100 | 80 | 18.85 | 1550.00 | -30.24 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 27 | 100 | 80 | 18.85 | 1550.00 | -26.19 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 28 | 100 | 80 | 18.85 | 1550.00 | -22.36 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 29 | 100 | 80 | 18.85 | 1550.00 | -18.77 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 30 | 100 | 80 | 18.85 | 1550.00 | -15.44 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 31 | 100 | 80 | 18.85 | 1550.00 | -12.38 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 32 | 100 | 80 | 18.85 | 1550.00 | -9.62 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 33 | 100 | 80 | 18.85 | 1550.00 | -7.18 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 34 | 100 | 80 | 18.85 | 1550.00 | -5.06 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 35 | 100 | 80 | 18.85 | 1550.00 | -3.28 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 36 | 100 | 80 | 18.85 | 1550.00 | -1.87 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 37 | 100 | 80 | 18.85 | 1550.00 | -0.84 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 38 | 100 | 80 | 18.85 | 1550.00 | -0.21 | -351.49 | 0.000000 | 0.00 | 0.000 (10) |
| 39 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (10) |

Combinazioni SLEF

Paramento

Apertura limite fessure $w_{lim}=0.30$

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 1 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (11) |
| 2 | 100 | 41 | 0.00 | 0.00 | 0.00 | 4.10 | 0.000000 | 0.00 | 0.000 (11) |
| 3 | 100 | 41 | 0.00 | 0.00 | 0.01 | 11.89 | 0.000000 | 0.00 | 0.000 (11) |
| 4 | 100 | 42 | 0.00 | 0.00 | 0.04 | 24.90 | 0.000000 | 0.00 | 0.000 (11) |
| 5 | 100 | 43 | 0.00 | 0.00 | 0.09 | 46.10 | 0.000000 | 0.00 | 0.000 (11) |
| 6 | 100 | 44 | 0.00 | 0.00 | 0.16 | 81.86 | 0.000000 | 0.00 | 0.000 (11) |
| 7 | 100 | 44 | 0.00 | 0.00 | 0.26 | 148.17 | 0.000000 | 0.00 | 0.000 (11) |
| 8 | 100 | 45 | 0.00 | 0.00 | 0.41 | 299.26 | 0.000000 | 0.00 | 0.000 (11) |
| 9 | 100 | 46 | 0.00 | 0.00 | 0.59 | 914.46 | 0.000000 | 0.00 | 0.000 (11) |
| 10 | 100 | 47 | 0.00 | 0.00 | 0.82 | 2240.61 | 0.000000 | 0.00 | 0.000 (11) |
| 11 | 100 | 47 | 0.00 | 0.00 | 1.11 | 654.18 | 0.000000 | 0.00 | 0.000 (11) |
| 12 | 100 | 48 | 15.71 | 1550.00 | 1.47 | 434.45 | 0.000000 | 0.00 | 0.000 (11) |
| 13 | 100 | 49 | 15.71 | 1550.00 | 1.89 | 349.89 | 0.000000 | 0.00 | 0.000 (11) |
| 14 | 100 | 50 | 15.71 | 1550.00 | 2.39 | 306.82 | 0.000000 | 0.00 | 0.000 (11) |
| 15 | 100 | 50 | 15.71 | 1550.00 | 2.97 | 281.88 | 0.000000 | 0.00 | 0.000 (11) |
| 16 | 100 | 51 | 18.85 | 1550.00 | 3.64 | 270.61 | 0.000000 | 0.00 | 0.000 (11) |

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 17 | 100 | 52 | 18.85 | 1550.00 | 4.40 | 260.84 | 0.000000 | 0.00 | 0.000 (11) |
| 18 | 100 | 52 | 18.85 | 1550.00 | 5.25 | 254.68 | 0.000000 | 0.00 | 0.000 (11) |
| 19 | 100 | 53 | 18.85 | 1550.00 | 6.21 | 250.97 | 0.000000 | 0.00 | 0.000 (11) |
| 20 | 100 | 54 | 18.85 | 1550.00 | 7.28 | 249.01 | 0.000000 | 0.00 | 0.000 (11) |
| 21 | 100 | 55 | 18.85 | 1550.00 | 8.47 | 248.34 | 0.000000 | 0.00 | 0.000 (11) |
| 22 | 100 | 55 | 18.85 | 1550.00 | 9.77 | 248.66 | 0.000000 | 0.00 | 0.000 (11) |
| 23 | 100 | 56 | 18.85 | 1550.00 | 11.20 | 249.76 | 0.000000 | 0.00 | 0.000 (11) |
| 24 | 100 | 57 | 18.85 | 1550.00 | 12.76 | 251.48 | 0.000000 | 0.00 | 0.000 (11) |
| 25 | 100 | 58 | 18.85 | 1550.00 | 14.46 | 253.70 | 0.000000 | 0.00 | 0.000 (11) |
| 26 | 100 | 58 | 18.85 | 1550.00 | 16.30 | 256.35 | 0.000000 | 0.00 | 0.000 (11) |
| 27 | 100 | 59 | 18.85 | 1550.00 | 18.28 | 259.37 | 0.000000 | 0.00 | 0.000 (11) |
| 28 | 100 | 60 | 18.85 | 1550.00 | 20.42 | 262.69 | 0.000000 | 0.00 | 0.000 (11) |
| 29 | 100 | 61 | 18.85 | 1550.00 | 22.72 | 266.27 | 0.000000 | 0.00 | 0.000 (11) |
| 30 | 100 | 61 | 25.13 | 1550.00 | 25.18 | 279.38 | 0.000000 | 0.00 | 0.000 (11) |
| 31 | 100 | 62 | 25.13 | 1550.00 | 27.82 | 283.53 | 0.000000 | 0.00 | 0.000 (11) |
| 32 | 100 | 63 | 25.13 | 1550.00 | 30.63 | 287.87 | 0.000000 | 0.00 | 0.000 (11) |
| 33 | 100 | 63 | 25.13 | 1550.00 | 33.62 | 292.39 | 0.000000 | 0.00 | 0.000 (11) |
| 34 | 100 | 64 | 25.13 | 1550.00 | 36.79 | 297.06 | 0.000000 | 0.00 | 0.000 (11) |
| 35 | 100 | 65 | 25.13 | 1550.00 | 40.16 | 301.89 | 0.000000 | 0.00 | 0.000 (11) |
| 36 | 100 | 66 | 25.13 | 1550.00 | 43.73 | 306.84 | 0.000000 | 0.00 | 0.000 (11) |
| 37 | 100 | 66 | 25.13 | 1550.00 | 47.50 | 311.93 | 0.000000 | 0.00 | 0.000 (11) |
| 38 | 100 | 67 | 25.13 | 1550.00 | 51.47 | 317.13 | 0.000000 | 0.00 | 0.000 (11) |
| 39 | 100 | 68 | 25.13 | 1550.00 | 55.67 | 322.45 | 0.000000 | 0.00 | 0.000 (11) |
| 40 | 100 | 69 | 25.13 | 1550.00 | 60.08 | 327.88 | 0.000000 | 0.00 | 0.000 (11) |
| 41 | 100 | 69 | 25.13 | 1550.00 | 64.71 | 333.41 | 0.000000 | 0.00 | 0.000 (11) |
| 42 | 100 | 70 | 25.13 | 1550.00 | 69.58 | 339.03 | 0.000000 | 0.00 | 0.000 (11) |
| 43 | 100 | 71 | 25.13 | 1550.00 | 74.69 | 344.75 | 0.000000 | 0.00 | 0.000 (11) |

Fondazione

Apertura limite fessure $w_{lim}=0.30$

| n° | B [cm] | H [cm] | Af [cmq] | Aeff [cmq] | M [kNm] | Mpf [kNm] | ε [%] | Sm [mm] | w [mm] |
|----|-----------|-----------|-------------|---------------|------------|--------------|----------|------------|------------|
| 1 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (11) |
| 2 | 100 | 80 | 18.85 | 1550.00 | 0.57 | 351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 3 | 100 | 80 | 18.85 | 1550.00 | 2.27 | 351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 4 | 100 | 80 | 18.85 | 1550.00 | 5.08 | 351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 5 | 100 | 80 | 18.85 | 1550.00 | 8.99 | 351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 6 | 100 | 80 | 18.85 | 1550.00 | -130.87 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 7 | 100 | 80 | 18.85 | 1550.00 | -126.34 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 8 | 100 | 80 | 18.85 | 1550.00 | -121.64 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 9 | 100 | 80 | 18.85 | 1550.00 | -116.54 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 10 | 100 | 80 | 18.85 | 1550.00 | -111.34 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 11 | 100 | 80 | 18.85 | 1550.00 | -106.08 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 12 | 100 | 80 | 18.85 | 1550.00 | -100.76 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 13 | 100 | 80 | 18.85 | 1550.00 | -95.40 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 14 | 100 | 80 | 18.85 | 1550.00 | -90.02 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 15 | 100 | 80 | 18.85 | 1550.00 | -84.64 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 16 | 100 | 80 | 18.85 | 1550.00 | -79.27 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 17 | 100 | 80 | 18.85 | 1550.00 | -73.93 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 18 | 100 | 80 | 18.85 | 1550.00 | -68.65 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 19 | 100 | 80 | 18.85 | 1550.00 | -63.43 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 20 | 100 | 80 | 18.85 | 1550.00 | -58.30 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 21 | 100 | 80 | 18.85 | 1550.00 | -53.26 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 22 | 100 | 80 | 18.85 | 1550.00 | -48.35 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 23 | 100 | 80 | 18.85 | 1550.00 | -43.57 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 24 | 100 | 80 | 18.85 | 1550.00 | -38.95 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 25 | 100 | 80 | 18.85 | 1550.00 | -34.50 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
|----------|---------|----------|--------------|------|------------|
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 312 di 314 |

| n° | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|------|------|-------|---------|--------|---------|----------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 26 | 100 | 80 | 18.85 | 1550.00 | -30.24 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 27 | 100 | 80 | 18.85 | 1550.00 | -26.19 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 28 | 100 | 80 | 18.85 | 1550.00 | -22.36 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 29 | 100 | 80 | 18.85 | 1550.00 | -18.77 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 30 | 100 | 80 | 18.85 | 1550.00 | -15.44 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 31 | 100 | 80 | 18.85 | 1550.00 | -12.38 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 32 | 100 | 80 | 18.85 | 1550.00 | -9.62 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 33 | 100 | 80 | 18.85 | 1550.00 | -7.18 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 34 | 100 | 80 | 18.85 | 1550.00 | -5.06 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 35 | 100 | 80 | 18.85 | 1550.00 | -3.28 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 36 | 100 | 80 | 18.85 | 1550.00 | -1.87 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 37 | 100 | 80 | 18.85 | 1550.00 | -0.84 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 38 | 100 | 80 | 18.85 | 1550.00 | -0.21 | -351.49 | 0.000000 | 0.00 | 0.000 (11) |
| 39 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (11) |

Combinazioni SLEQ

Paramento

 Apertura limite fessure $w_{lim}=0.20$

| n° | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|------|------|-------|---------|-------|---------|----------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 1 | 100 | 40 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (12) |
| 2 | 100 | 41 | 0.00 | 0.00 | 0.00 | 4.10 | 0.000000 | 0.00 | 0.000 (12) |
| 3 | 100 | 41 | 0.00 | 0.00 | 0.01 | 11.89 | 0.000000 | 0.00 | 0.000 (12) |
| 4 | 100 | 42 | 0.00 | 0.00 | 0.04 | 24.90 | 0.000000 | 0.00 | 0.000 (12) |
| 5 | 100 | 43 | 0.00 | 0.00 | 0.09 | 46.10 | 0.000000 | 0.00 | 0.000 (12) |
| 6 | 100 | 44 | 0.00 | 0.00 | 0.16 | 81.86 | 0.000000 | 0.00 | 0.000 (12) |
| 7 | 100 | 44 | 0.00 | 0.00 | 0.26 | 148.17 | 0.000000 | 0.00 | 0.000 (12) |
| 8 | 100 | 45 | 0.00 | 0.00 | 0.41 | 299.26 | 0.000000 | 0.00 | 0.000 (12) |
| 9 | 100 | 46 | 0.00 | 0.00 | 0.59 | 914.46 | 0.000000 | 0.00 | 0.000 (12) |
| 10 | 100 | 47 | 0.00 | 0.00 | 0.82 | 2240.61 | 0.000000 | 0.00 | 0.000 (12) |
| 11 | 100 | 47 | 0.00 | 0.00 | 1.11 | 654.18 | 0.000000 | 0.00 | 0.000 (12) |
| 12 | 100 | 48 | 15.71 | 1550.00 | 1.47 | 434.45 | 0.000000 | 0.00 | 0.000 (12) |
| 13 | 100 | 49 | 15.71 | 1550.00 | 1.89 | 349.89 | 0.000000 | 0.00 | 0.000 (12) |
| 14 | 100 | 50 | 15.71 | 1550.00 | 2.39 | 306.82 | 0.000000 | 0.00 | 0.000 (12) |
| 15 | 100 | 50 | 15.71 | 1550.00 | 2.97 | 281.88 | 0.000000 | 0.00 | 0.000 (12) |
| 16 | 100 | 51 | 18.85 | 1550.00 | 3.64 | 270.61 | 0.000000 | 0.00 | 0.000 (12) |
| 17 | 100 | 52 | 18.85 | 1550.00 | 4.40 | 260.84 | 0.000000 | 0.00 | 0.000 (12) |
| 18 | 100 | 52 | 18.85 | 1550.00 | 5.25 | 254.68 | 0.000000 | 0.00 | 0.000 (12) |
| 19 | 100 | 53 | 18.85 | 1550.00 | 6.21 | 250.97 | 0.000000 | 0.00 | 0.000 (12) |
| 20 | 100 | 54 | 18.85 | 1550.00 | 7.28 | 249.01 | 0.000000 | 0.00 | 0.000 (12) |
| 21 | 100 | 55 | 18.85 | 1550.00 | 8.47 | 248.34 | 0.000000 | 0.00 | 0.000 (12) |
| 22 | 100 | 55 | 18.85 | 1550.00 | 9.77 | 248.66 | 0.000000 | 0.00 | 0.000 (12) |
| 23 | 100 | 56 | 18.85 | 1550.00 | 11.20 | 249.76 | 0.000000 | 0.00 | 0.000 (12) |
| 24 | 100 | 57 | 18.85 | 1550.00 | 12.76 | 251.48 | 0.000000 | 0.00 | 0.000 (12) |
| 25 | 100 | 58 | 18.85 | 1550.00 | 14.46 | 253.70 | 0.000000 | 0.00 | 0.000 (12) |
| 26 | 100 | 58 | 18.85 | 1550.00 | 16.30 | 256.35 | 0.000000 | 0.00 | 0.000 (12) |
| 27 | 100 | 59 | 18.85 | 1550.00 | 18.28 | 259.37 | 0.000000 | 0.00 | 0.000 (12) |
| 28 | 100 | 60 | 18.85 | 1550.00 | 20.42 | 262.69 | 0.000000 | 0.00 | 0.000 (12) |
| 29 | 100 | 61 | 18.85 | 1550.00 | 22.72 | 266.27 | 0.000000 | 0.00 | 0.000 (12) |
| 30 | 100 | 61 | 25.13 | 1550.00 | 25.18 | 279.38 | 0.000000 | 0.00 | 0.000 (12) |
| 31 | 100 | 62 | 25.13 | 1550.00 | 27.82 | 283.53 | 0.000000 | 0.00 | 0.000 (12) |
| 32 | 100 | 63 | 25.13 | 1550.00 | 30.63 | 287.87 | 0.000000 | 0.00 | 0.000 (12) |
| 33 | 100 | 63 | 25.13 | 1550.00 | 33.62 | 292.39 | 0.000000 | 0.00 | 0.000 (12) |

| n° | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|------|------|-------|---------|-------|--------|----------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 34 | 100 | 64 | 25.13 | 1550.00 | 36.79 | 297.06 | 0.000000 | 0.00 | 0.000 (12) |
| 35 | 100 | 65 | 25.13 | 1550.00 | 40.16 | 301.89 | 0.000000 | 0.00 | 0.000 (12) |
| 36 | 100 | 66 | 25.13 | 1550.00 | 43.73 | 306.84 | 0.000000 | 0.00 | 0.000 (12) |
| 37 | 100 | 66 | 25.13 | 1550.00 | 47.50 | 311.93 | 0.000000 | 0.00 | 0.000 (12) |
| 38 | 100 | 67 | 25.13 | 1550.00 | 51.47 | 317.13 | 0.000000 | 0.00 | 0.000 (12) |
| 39 | 100 | 68 | 25.13 | 1550.00 | 55.67 | 322.45 | 0.000000 | 0.00 | 0.000 (12) |
| 40 | 100 | 69 | 25.13 | 1550.00 | 60.08 | 327.88 | 0.000000 | 0.00 | 0.000 (12) |
| 41 | 100 | 69 | 25.13 | 1550.00 | 64.71 | 333.41 | 0.000000 | 0.00 | 0.000 (12) |
| 42 | 100 | 70 | 25.13 | 1550.00 | 69.58 | 339.03 | 0.000000 | 0.00 | 0.000 (12) |
| 43 | 100 | 71 | 25.13 | 1550.00 | 74.69 | 344.75 | 0.000000 | 0.00 | 0.000 (12) |

Fondazione

Apertura limite fessure $w_{lim}=0.20$

| n° | B | H | Af | Aeff | M | Mpf | ε | Sm | w |
|----|------|------|-------|---------|---------|---------|----------|------|------------|
| | [cm] | [cm] | [cmq] | [cmq] | [kNm] | [kNm] | [%] | [mm] | [mm] |
| 1 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (12) |
| 2 | 100 | 80 | 18.85 | 1550.00 | 0.57 | 351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 3 | 100 | 80 | 18.85 | 1550.00 | 2.27 | 351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 4 | 100 | 80 | 18.85 | 1550.00 | 5.08 | 351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 5 | 100 | 80 | 18.85 | 1550.00 | 8.99 | 351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 6 | 100 | 80 | 18.85 | 1550.00 | -130.87 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 7 | 100 | 80 | 18.85 | 1550.00 | -126.34 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 8 | 100 | 80 | 18.85 | 1550.00 | -121.64 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 9 | 100 | 80 | 18.85 | 1550.00 | -116.54 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 10 | 100 | 80 | 18.85 | 1550.00 | -111.34 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 11 | 100 | 80 | 18.85 | 1550.00 | -106.08 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 12 | 100 | 80 | 18.85 | 1550.00 | -100.76 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 13 | 100 | 80 | 18.85 | 1550.00 | -95.40 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 14 | 100 | 80 | 18.85 | 1550.00 | -90.02 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 15 | 100 | 80 | 18.85 | 1550.00 | -84.64 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 16 | 100 | 80 | 18.85 | 1550.00 | -79.27 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 17 | 100 | 80 | 18.85 | 1550.00 | -73.93 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 18 | 100 | 80 | 18.85 | 1550.00 | -68.65 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 19 | 100 | 80 | 18.85 | 1550.00 | -63.43 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 20 | 100 | 80 | 18.85 | 1550.00 | -58.30 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 21 | 100 | 80 | 18.85 | 1550.00 | -53.26 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 22 | 100 | 80 | 18.85 | 1550.00 | -48.35 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 23 | 100 | 80 | 18.85 | 1550.00 | -43.57 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 24 | 100 | 80 | 18.85 | 1550.00 | -38.95 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 25 | 100 | 80 | 18.85 | 1550.00 | -34.50 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 26 | 100 | 80 | 18.85 | 1550.00 | -30.24 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 27 | 100 | 80 | 18.85 | 1550.00 | -26.19 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 28 | 100 | 80 | 18.85 | 1550.00 | -22.36 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 29 | 100 | 80 | 18.85 | 1550.00 | -18.77 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 30 | 100 | 80 | 18.85 | 1550.00 | -15.44 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 31 | 100 | 80 | 18.85 | 1550.00 | -12.38 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 32 | 100 | 80 | 18.85 | 1550.00 | -9.62 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 33 | 100 | 80 | 18.85 | 1550.00 | -7.18 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 34 | 100 | 80 | 18.85 | 1550.00 | -5.06 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 35 | 100 | 80 | 18.85 | 1550.00 | -3.28 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 36 | 100 | 80 | 18.85 | 1550.00 | -1.87 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 37 | 100 | 80 | 18.85 | 1550.00 | -0.84 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 38 | 100 | 80 | 18.85 | 1550.00 | -0.21 | -351.49 | 0.000000 | 0.00 | 0.000 (12) |
| 39 | 100 | 80 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | 0.000 (12) |



**RADDOPPIO LINEA CODOGNO – CREMONA – MANTOVA
TRATTA PIADENA - MANTOVA**

Relazione di calcolo muro di sostegno sede stradale-NV24

| COMMESSA | LOTTO | CODIFICA | DOCUMENTO | REV. | FOGLIO |
|----------|---------|----------|--------------|------|------------|
| NM25 | 03 D 26 | CL | NV 24 05 001 | A | 314 di 314 |