

COMMITTENTE:



PROGETTAZIONE:



## U.O. INFRASTRUTTURE NORD

### PROGETTO DEFINITIVO

#### DIRETTRICE FERROVIARIA MESSINA – CATANIA – PALERMO NUOVO COLLEGAMENTO PALERMO – CATANIA

#### RADDOPPIO TRATTA FIUME TORTO – LERCARA DIRAMAZIONE LOTTO 1 + 2

#### FABBRICATI STAZIONE

FV03 - Stazione di Lercara dir - km 29+147

Relazione di calcolo strutturale fondazioni pile ponte pedonale

SCALA:

-

COMMESSA	LOTTO	FASE	ENTE	TIPO DOC.	OPERA/DISCIPLINA	PROGR.	REV.
RS3Z	00	D	26	CL	FV0300	009	B

Rev.	Descrizione	Redatto	Data	Verificato	Data	Approvato	Data	Autorizzato	Data
A	EMISSIONE ESECUTIVA	C. INTEGRA	Gennaio 2020	F. COPPINI	Gennaio 2020	A. BARRECA	Gennaio 2020	F. COPPINI Maggio 2020 ITALFERR - UO INFRASTRUTTURE NORD Det. Ing. Francesco Giamberini Ordine degli Ingegneri della Provincia di Roma n. 25372/Str	
B	1° AGG. A CONSEGNA CSLLPP	C. INTEGRA	Maggio 2020	F. COPPINI	Maggio 2020	A. BARRECA	Maggio 2020		

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## 1 PREMESSA

L'oggetto della presente relazione è la struttura di collegamento ed accesso ai diversi binari della stazione di Lercara (PA).

Si tratta di una struttura metallica mono-piano di lunghezza complessiva pari a circa 44,05 m e larghezza 9,45 m appoggiata su:

- 4 pile in c.a. di altezza pari a 7.85 m, con sezione cava, posizionate su 2 allineamenti fondati su pali;
- pareti in c.a che costituiscono il fabbricato viaggiatori (non trattate in questo documento, di cui si tiene conto tramite il sistema di vincoli adottato).

La struttura metallica è composta da 2 travi principali continue, disposte longitudinalmente alla struttura, di tipo laminato a caldo con altezza pari a 800 mm e piattabanda di larghezza 300 mm. Su tali travi si innestano perpendicolarmente delle travi secondarie IPE 500, anche esse con schema statico di trave continua. Le travi secondarie sono, infine, collegate a profili tubolari di dimensione 500x300x6 mm che realizzano i portali trasversali che costituiscono la copertura.

**In questo documento sono riportate le verifiche strutturali delle fondazioni delle pile.**

## 2 NORMATIVE DI RIFERIMENTO

La progettazione è conforme alle normative vigenti nonché alle Istruzioni dell'Ente FF.SS.

I calcoli e le disposizioni esecutive sono conformi alle norme attualmente in vigore e di seguito elencate:

- Decreto Ministeriale 17 gennaio 2018: Aggiornamento delle Norme tecniche per le costruzioni;
- Circolare 21 gennaio 2019, n.7 C.S.LL.PP.: Istruzioni per l'applicazione dell'“Aggiornamento delle Norme tecniche per le costruzioni di cui al D.M. 17 gennaio 2018;
- Circolare 15 ottobre 1996, n.252 AA.GG./S.T.C.: Istruzioni per l'applicazione delle “Nuove norme tecniche per il calcolo, l'esecuzione ed il collaudo delle opere in cemento armato normale e precompresso e per le strutture metalliche” di cui al decreto ministeriale 9 gennaio 1996;
- RFI DTC SI MA IFS 001 B: “Manuale di progettazione delle opere civili” del 22/12/2017.
- RFI DTC SI PS MA IFS 001 B: Sezione 2 – Ponti e Strutture
- RFI DTC SI CS MA IFS 002 B: Manuale di Progettazione delle Opere Civili - Parte II - Sezione 5 – Prescrizioni per marciapiedi e pensiline delle stazioni ferroviarie a servizio dei viaggiatori
- Regolamento (UE) N.1299/2014 della Commissione del 18 novembre 2014 relativo alle specifiche tecniche di interoperabilità per il sottosistema “infrastruttura” del sistema ferroviario dell'Unione europea
- Eurocodice 3: Progettazione delle strutture di acciaio – Parte 1.1: Regole generali e regole per gli edifici
- UNI EN 11104 marzo 2004: “Calcestruzzo: specificazione. prestazione. produzione e conformità” Istruzioni complementari per l'applicazione delle EN 206-1
- UNI EN 206-1 ottobre 2006: “Calcestruzzo: specificazione. prestazione. produzione e conformità”
- UNI EN 1992-1-1 (Eurocodice 2) novembre 2005: “Progettazione delle strutture di calcestruzzo Parte 1: Regole generali e regole per edifici”
- UNI EN 1998-5 (Eurocodice 8) gennaio 2005: “Progettazione delle strutture per la resistenza sismica – Parte 5: Fondazioni. strutture di contenimento ed aspetti geotecnici”
- UIC CODE 777-2:2002: Structures built over railways lines – Construction requirements in the track zone.

Riferimenti STI:

- Regolamento (UE) N. 1299/2014 della Commissione del 18 novembre 2014 relativo alle specifiche tecniche di interoperabilità per il sottosistema “infrastruttura” del sistema ferroviario dell'Unione europea, modificato dal Regolamento di esecuzione (UE) N° 2019/776 della Commissione del 16 maggio 2019.

### 3 CARATTERISTICHE DEI MATERIALI

- CALCESTRUZZO PER STRUTTURE DI FONDAZIONE (PALI E PLATEE): C25/30

<b>Rck 30</b>		= classe di resistenza
$f_{ck} =$	24.9 MPa	= resistenza cilindrica caratteristica a compressione
$\alpha_{cc} =$	<b>0.85</b>	= coefficiente riduttivo per le resistenze di lunga durata
$\gamma_c =$	<b>1.5</b>	= coefficiente parziale di sicurezza
$f_{cd} = \alpha_{cc} f_{ck} / \gamma_c =$	14.11 MPa	= resistenza cilindrica di calcolo a compressione
$f_{cm} = f_{ck} + 8 =$	32.9 MPa	= resistenza cilindrica media a compressione
$f_{ctm} = 0,30 f_{ck}^{2/3}$ per classi $\leq$ C50/60	2.56 MPa	= resistenza media a trazione
$f_{ctm} = 2,12 \ln[1+f_{cm}/10]$ per classi $>$ C50/60		
$f_{ctk} = 0,7 f_{ctm} =$	1.79 MPa	= resistenza caratteristica a trazione
$f_{ctd} = f_{ctk} / \gamma_c =$	1.19 MPa	= resistenzadi calcolo a trazione
$E_c = 22000 [(f_{ck}+8)/10]^{0.3} =$	31447 MPa	= modulo elastico

- ACCIAIO PER CEMENTO ARMATO: B450C

#### **B450C**

$f_{tk} \geq$	540 MPa	= tensione caratteristica di rottura
$f_{yk} \geq$	450 MPa	= tensione caratteristica di snervamento
$\gamma_s =$	<b>1.15</b>	= coefficiente parziale di sicurezza
$f_{yd} = f_{yk} / \gamma_s =$	391.3 MPa	= resistenza di calcolo
$E_s =$	<b>200000</b> MPa	= modulo elastico

#### **4 PARAMETRI GEOTECNICI DEL SITO**

Contenuta nel documento RS3Z00D26CLFV0300006.

#### **5 UBICAZIONE DELL'INTERVENTO**

Contenuta nel documento RS3Z00D26CLFV0300006.

#### **6 ANALISI DEI CARICHI**

Contenuta nel documento RS3Z00D26CLFV0300006.

#### **7 COMBINAZIONI DI CARICO**

Contenuta nel documento RS3Z00D26CLFV0300006.

#### **8 MODELLAZIONE STRUTTURALE**

Contenuta nel documento RS3Z00D26CLFV0300006.

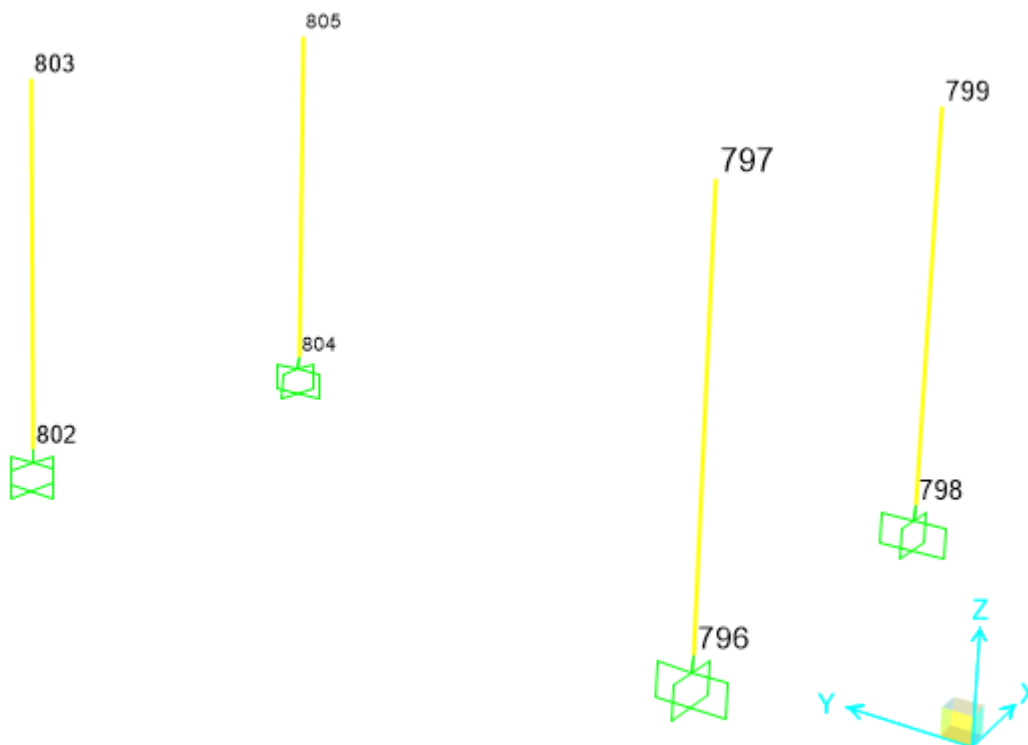
## 9 VERIFICHE STRUTTURALI DELLE OPERE DI FONDAZIONE

Nel presente paragrafo sono riportate le verifiche strutturali dei plinti di fondazione e dei pali.

### 9.1 Sollecitazioni di calcolo

Al fine di dimensionare le opere di fondazione, sono state estrapolate dal modello di calcolo le sollecitazioni alla base delle pile, ovvero le reazioni vincolari d'incastro, e sono state ripartite in modo rigido sui pali di fondazione.

Di seguito viene riportata una vista del modello di calcolo dalla quale si possono evincere i nomi dei nodi di interesse e la tabella con le reazioni vincolari in detti nodi.



*Figura 1: Joints labels*

*Relazione di calcolo strutturale  
fondazioni pile ponte pedonale*

COMMESSA	LOTTO	FASE-ENTE	DOCUMENTO	REV.	FOGLIO
RS3Z	00	D 26	CLFV0300009	B	6 di 34

Joint	OutputCase	CaseType	StepType	F1	F2	F3	M1	M2	M3
Text	Text	Text	Text	KN	KN	KN	KN-m	KN-m	KN-m
796	SLU (q1)	Combination		-36.5	0.0	2367.3	0.0	-1058.6	0.0
796	SLU (q2)	Combination		36.5	0.0	2454.8	0.0	-860.6	0.0
796	SLU (q3)	Combination		0.0	-43.5	2418.3	167.6	-966.5	0.0
796	SLU (q4)	Combination		0.0	43.5	2474.7	-167.5	-1020.0	0.0
796	SLU (n1)	Combination		-36.5	0.0	1973.6	0.0	-684.6	0.0
796	SLU (n2)	Combination		36.5	0.0	2061.2	0.0	-486.6	0.0
796	SLU (n3)	Combination		0.0	-43.5	2024.6	167.6	-592.5	0.0
796	SLU (n4)	Combination		0.0	43.5	2081.0	-167.5	-646.0	0.0
796	SLU (v1)	Combination		-60.9	0.0	1863.8	0.0	-674.0	0.0
796	SLU (v2)	Combination		60.9	0.0	2009.7	0.0	-344.0	0.0
796	SLU (v3)	Combination		0.0	-72.5	1948.8	279.3	-520.5	0.0
796	SLU (v4)	Combination		0.0	72.5	2042.9	-279.3	-609.8	0.0
796	SLU (T1)	Combination		-36.5	0.0	1935.2	0.0	-648.1	0.0
796	SLU (T2)	Combination		36.5	0.0	2022.8	0.0	-450.1	0.0
796	SLU (T3)	Combination		0.0	-43.5	1986.3	167.6	-556.0	0.0
796	SLU (T4)	Combination		0.0	43.5	2042.7	-167.5	-609.6	0.0
796	SLU_URTO X	Combination		0.0	0.0	1501.5	0.0	-402.6	0.0
796	SLU_URTO Y	Combination		0.0	0.0	1501.0	0.0	-402.2	0.0
796	Comb. SLVx (q=1)	Combination	Max	112.6	34.0	1608.9	262.2	490.8	2.5
796	Comb. SLVx (q=1)	Combination	Min	-112.6	-34.1	1393.4	-262.2	-1295.3	-2.5
796	Comb. SLVy (q=1)	Combination	Max	35.4	113.5	1589.1	873.9	-69.7	8.4
796	Comb. SLVy (q=1)	Combination	Min	-35.4	-113.5	1413.2	-873.9	-734.8	-8.4
798	SLU (q1)	Combination		-117.0	0.0	2453.6	0.0	203.1	0.0
798	SLU (q2)	Combination		155.5	0.0	2366.2	0.0	2026.9	0.0
798	SLU (q3)	Combination		22.0	-43.5	2417.3	167.6	1145.1	0.0
798	SLU (q4)	Combination		20.5	43.5	2473.8	-167.5	1186.6	0.0
798	SLU (n1)	Combination		-126.9	0.0	2060.3	0.0	-250.7	0.0
798	SLU (n2)	Combination		145.6	0.0	1973.0	0.0	1573.1	0.0
798	SLU (n3)	Combination		12.2	-43.5	2024.1	167.6	691.3	0.0
798	SLU (n4)	Combination		10.7	43.5	2080.6	-167.5	732.8	0.0
798	SLU (v1)	Combination		-219.8	0.0	2008.7	0.0	-952.2	0.0
798	SLU (v2)	Combination		234.4	0.0	1863.1	0.0	2087.5	0.0
798	SLU (v3)	Combination		12.0	-72.5	1948.3	279.3	617.8	0.0
798	SLU (v4)	Combination		9.5	72.5	2042.4	-279.2	686.9	0.0
798	SLU (T1)	Combination		-132.7	0.0	2021.8	0.0	-334.9	0.0
798	SLU (T2)	Combination		139.8	0.0	1934.5	0.0	1488.8	0.0



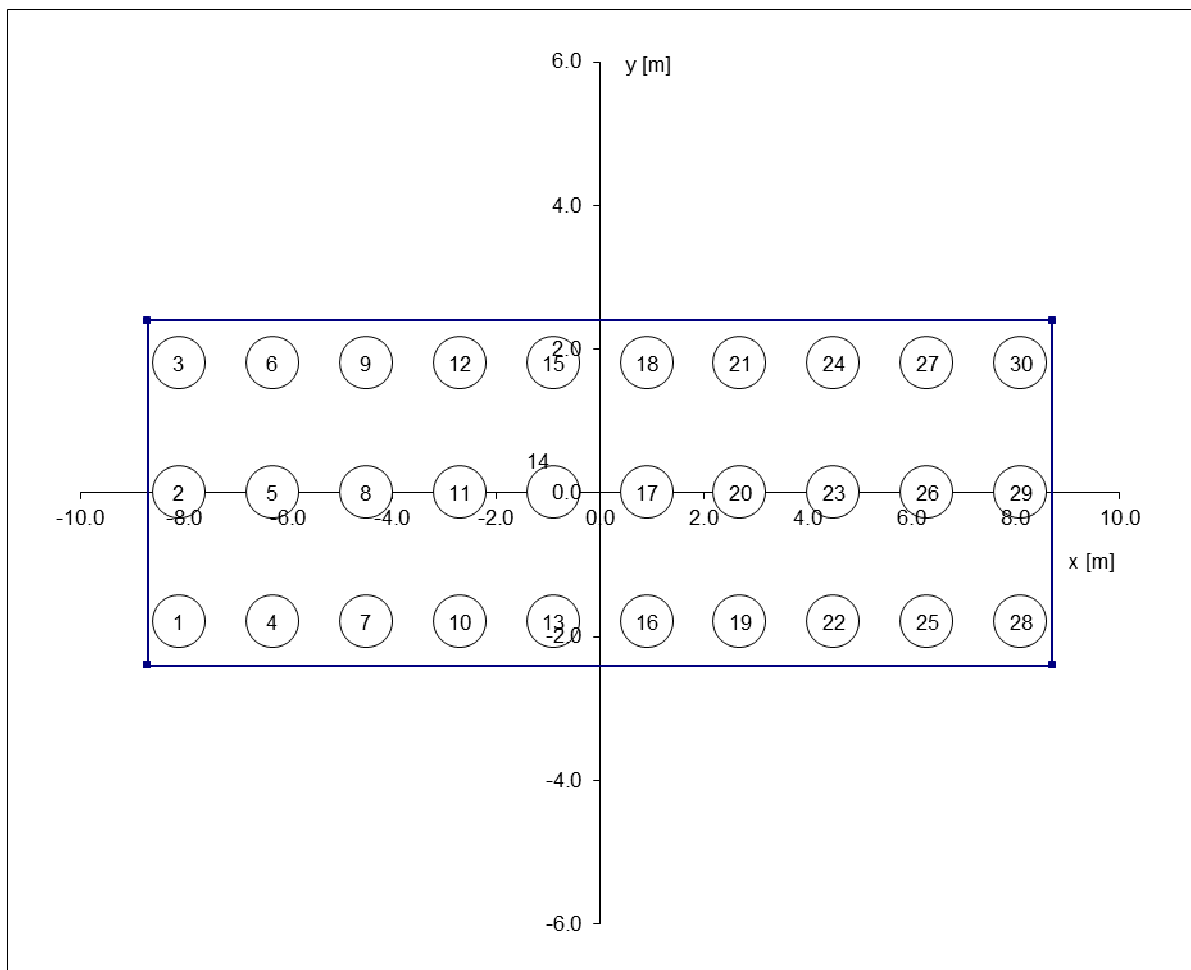
Joint	OutputCase	CaseType	StepType	F1	F2	F3	M1	M2	M3
Text	Text	Text	Text	KN	KN	KN	KN-m	KN-m	KN-m
798	SLU (T3)	Combination		6.3	-43.5	1985.6	167.6	607.1	0.0
798	SLU (T4)	Combination		4.8	43.5	2042.1	-167.5	648.5	0.0
798	SLU_URTO X	Combination		-260.8	0.0	1500.4	0.0	-1723.8	0.0
798	SLU_URTO Y	Combination		-28.3	0.0	1501.0	0.0	171.3	0.0
798	Comb. SLVx (q=1)	Combination	Max	390.2	34.0	1606.9	262.2	3555.3	2.5
798	Comb. SLVx (q=1)	Combination	Min	-368.2	-34.1	1394.9	-262.2	-2572.6	-2.5
798	Comb. SLVy (q=1)	Combination	Max	146.9	113.5	1591.9	873.9	1605.6	8.4
798	Comb. SLVy (q=1)	Combination	Min	-125.0	-113.5	1409.9	-873.9	-623.0	-8.4
802	SLU (q1)	Combination		-36.5	-8.9	2690.8	72.7	-1366.0	-8.5
802	SLU (q2)	Combination		36.5	-31.2	2794.4	254.4	-1183.1	-29.7
802	SLU (q3)	Combination		0.0	-91.3	2825.8	556.8	-1353.6	-45.4
802	SLU (q4)	Combination		0.0	49.5	2823.9	-216.1	-1351.8	5.7
802	SLU (n1)	Combination		-36.5	-0.2	2167.2	1.5	-868.5	-0.2
802	SLU (n2)	Combination		36.5	-22.5	2270.7	183.2	-685.6	-21.4
802	SLU (n3)	Combination		0.0	-82.5	2302.1	485.5	-856.1	-37.1
802	SLU (n4)	Combination		0.0	58.2	2300.2	-287.4	-854.3	14.0
802	SLU (v1)	Combination		-60.9	9.0	2020.1	-73.5	-822.5	8.6
802	SLU (v2)	Combination		60.9	-28.1	2192.7	229.3	-517.8	-26.7
802	SLU (v3)	Combination		0.0	-128.2	2245.1	733.2	-801.9	-52.9
802	SLU (v4)	Combination		0.0	106.4	2241.9	-554.9	-798.9	32.1
802	SLU (T1)	Combination		-36.5	2.3	2087.3	-19.0	-792.6	2.2
802	SLU (T2)	Combination		36.5	-20.0	2190.8	162.7	-609.7	-19.0
802	SLU (T3)	Combination		0.0	-80.0	2222.3	465.0	-780.2	-34.7
802	SLU (T4)	Combination		0.0	60.7	2220.4	-307.9	-778.4	16.4
802	SLU_URTO X	Combination		0.0	12.3	1653.0	-99.9	-546.5	11.6
802	SLU_URTO Y	Combination		0.0	-193.0	1653.7	1572.9	-547.2	-183.3
802	Comb. SLVx (q=1)	Combination	Max	112.1	197.0	1755.9	1739.0	341.9	149.3
802	Comb. SLVx (q=1)	Combination	Min	-112.1	-215.9	1551.5	-1584.7	-1436.3	-167.3
802	Comb. SLVy (q=1)	Combination	Max	34.8	530.1	1736.3	4423.9	-222.6	406.5
802	Comb. SLVy (q=1)	Combination	Min	-34.8	-549.1	1571.0	-4269.6	-871.7	-424.5
804	SLU (q1)	Combination		-178.6	8.9	2803.4	-72.7	34.0	-8.5
804	SLU (q2)	Combination		62.7	31.2	2699.1	-254.4	1587.1	-29.7
804	SLU (q3)	Combination		-64.3	-50.4	2834.7	223.7	837.8	6.5
804	SLU (q4)	Combination		-62.1	92.2	2832.6	-564.4	854.1	-46.3
804	SLU (n1)	Combination		-150.7	0.2	2276.0	-1.5	-239.7	-0.2
804	SLU (n2)	Combination		90.6	22.5	2171.8	-183.2	1313.4	-21.4

Joint	OutputCase	CaseType	StepType	F1	F2	F3	M1	M2	M3
Text	Text	Text	Text	KN	KN	KN	KN-m	KN-m	KN-m
804	SLU (n3)	Combination		-36.4	-59.2	2307.4	295.0	564.1	14.9
804	SLU (n4)	Combination		-34.2	83.5	2305.3	-493.2	580.4	-38.0
804	SLU (v1)	Combination		-225.1	-9.0	2198.0	73.5	-815.4	8.6
804	SLU (v2)	Combination		177.0	28.1	2024.2	-229.4	1773.1	-26.7
804	SLU (v3)	Combination		-34.7	-107.9	2250.3	567.6	524.4	33.6
804	SLU (v4)	Combination		-30.9	129.8	2246.7	-746.0	551.5	-54.4
804	SLU (T1)	Combination		-136.7	-2.3	2196.3	19.0	-201.7	2.2
804	SLU (T2)	Combination		104.5	20.0	2092.0	-162.7	1351.4	-19.0
804	SLU (T3)	Combination		-22.5	-61.7	2227.6	315.5	602.1	17.2
804	SLU (T4)	Combination		-20.2	81.0	2225.5	-472.7	618.4	-35.6
804	SLU_URTO X	Combination		-3452.8	-12.3	1658.1	99.9	-10188.5	11.6
804	SLU_URTO Y	Combination		-37.7	-1307.0	1657.0	4127.1	243.1	-183.3
804	Comb. SLV <sub>x</sub> (q=1)	Combination	Max	215.6	233.8	1759.1	1669.1	2175.1	168.4
804	Comb. SLV <sub>x</sub> (q=1)	Combination	Min	-277.7	-214.9	1555.1	-1823.4	-1580.5	-186.4
804	Comb. SLV <sub>y</sub> (q=1)	Combination	Max	57.3	564.8	1749.6	4272.2	966.9	437.4
804	Comb. SLV <sub>y</sub> (q=1)	Combination	Min	-119.4	-545.9	1564.6	-4426.5	-372.3	-455.4

## 9.2 Verifiche Strutturali sui pali di fondazione

I pali avranno diametro pari a 600 mm ad interasse 1.8 m ed una lunghezza pari a 25 m.

Si riporta di seguito la disposizione dei pali e la numerazione adottata.



*Figura 2: Schema pali*

Il calcolo delle sollecitazioni agenti sul singolo palo è stato effettuato con il metodo del plinto rigido.

Il calcolo delle sollecitazioni sui singoli pali è stato effettuato assumendo le seguenti ipotesi:

- Plinto rigido;
- Vincolo di incastro tra pali e plinto;
- Pali costituenti la palificata verticali;
- Rotazione del plinto e della testa dei pali impedita.

Per un gruppo di n pali, sottoposto a forze verticali, orizzontali e di momento esterne (agenti alla quota testa pali ed in corrispondenza del baricentro della palificata) i carichi agenti alla testa di ciascun palo sono stimabili con le seguenti espressioni:

$$Q_{ti} = \frac{N}{n} \pm \frac{[M_x + M_{inc,x}] \cdot y_i}{\sum_1^n y_i^2} \pm \frac{[M_y + M_{inc,y}] \cdot x_i}{\sum_1^n x_i^2};$$

$$H_{tix} = \frac{H_x}{n};$$

$$H_{tiy} = \frac{H_y}{n};$$

essendo :

- N = forza verticale esterna;
- $M_x = M_{long}$  = momento esterno attorno all'asse x, accoppiato con  $H_y$ ;
- $H_y = T_{long}$  = forza orizzontale esterna nella direzione y;
- $M_y = M_{trasv}$  = momento esterno attorno all'asse y, accoppiato con  $H_x$ ;
- $H_x = T_{trasv}$  = forza orizzontale esterna nella direzione x;
- $Q_{ti}$  = forza verticale agente alla testa del palo i-esimo;
- $H_{tix} = T_{trasv\_i}$  = forza orizzontale agente alla testa del palo i-esimo nella direzione x;
- $H_{tiy} = T_{long\_i}$  = forza orizzontale agente alla testa del palo i-esimo nella direzione y;
- $M_{inc,x} = M_{long\_inc} = \sum M_{tix}$  = momento di incastro risultante che i pali esercitano sul plinto per effetto del vincolo di rotazione impedita nella direzione x;
- $M_{tix} = M_{long\_inc\_i}$  = momento di incastro alla testa del palo i-esimo per effetto del vincolo di rotazione impedita nella direzione x;
- $M_{inc,y} = M_{trasv\_inc} = \sum M_{tiy}$  = momento di incastro risultante che i pali esercitano sul plinto per effetto del vincolo di rotazione impedita nella direzione y;

-  $M_{tiy} = M_{trasv\_inc\_i}$  = momento di incastro alla testa del palo i-esimo per effetto del vincolo di rotazione impedita nella direzione y;

-  $y_i$  = distanza del palo i-esimo dall'asse baricentrico della palificata nella direzione y;

-  $x_i$  = distanza del palo i-esimo dall'asse baricentrico della palificata nella direzione x.

I valori di N, T ed M esterni considerati sono quelli ottenuti dal modello allo spiccato delle fondazioni.

In tutte le tabelle di seguito riportate le unità di misura sono i kN per sforzi normali e tagli e i kN×m per i momenti.

Gli sforzi normali positivi si intendono di compressione mentre i momenti positivi seguono la regola della mano destra.

Le tensioni positive sono di compressione e quelle negative di trazione.

In base alle convenzioni sui segni su indicate, per ogni palo sono riportati i massimi e i minimi sforzi assiali e la condizione di carico N–M più gravosa in termini di massima tensione nel calcestruzzo e di minima tensione nelle armature. Per le tensioni tangenziali è stato considerato il taglio massimo T agente in sommità del palo (anche non contemporaneo ad N–M).

Di seguito vengono riportate le sollecitazioni agenti sui pali, calcolate a partire dalle reazioni vincolari alla base delle pile sommando, ai momenti sollecitanti, i momenti calcolati in accordo alla teoria elastica di Matlock e Reese utilizzando la relazione:

$$M = C_M H \lambda,$$

in cui:

$H = T$  = taglio agente;

$C_M$  = coefficiente funzione di  $L/\lambda$ ;

$\lambda = (E_p J / n_h)^{1/5}$ ;

$n_h = E_{MR}/D$ , ove:

per i **terreni coesivi**:  $E_{MR} = \xi c_u$ , con  $\xi = 300\div 450$  assunto, nel caso specifico, pari a 450

$n_h$	$E_{MR}$	$E_{cls}$	$J_{palo}$
(kN/m <sup>3</sup> )	(kPa)	(kPa)	(m <sup>4</sup> )
75000.00	45000.00	31447000.00	0.01

ID	Nodo	Combinazione	N	Mt	Ml	Tt	Tl	n
-	-	-	[kN]	[kNm]	[kNm]	[kN]	[kN]	[-]
1	796	SLU (q1)	2367.3	0.0	-1057.2	0.0	-36.5	30
2	796	SLU (q2)	2454.8	0.0	-861.9	0.0	36.5	30
3	796	SLU (q3)	2418.3	-165.9	-966.5	-43.5	0.0	30
4	796	SLU (q4)	2474.7	165.9	-1020.0	43.5	0.0	30
5	796	SLU (n1)	1973.6	0.0	-683.2	0.0	-36.5	30
6	796	SLU (n2)	2061.2	0.0	-487.9	0.0	36.5	30
7	796	SLU (n3)	2024.6	-165.9	-592.5	-43.5	0.0	30
8	796	SLU (n4)	2081.0	165.9	-646.0	43.5	0.0	30
9	796	SLU (v1)	1863.8	0.0	-671.7	0.0	-60.9	30
10	796	SLU (v2)	2009.7	0.0	-346.3	0.0	60.9	30
11	796	SLU (v3)	1948.8	-276.5	-520.5	-72.5	0.0	30
12	796	SLU (v4)	2042.9	276.5	-609.8	72.5	0.0	30
13	796	SLU (T1)	1935.2	0.0	-646.7	0.0	-36.5	30
14	796	SLU (T2)	2022.8	0.0	-451.5	0.0	36.5	30
15	796	SLU (T3)	1986.3	-165.9	-556.0	-43.5	0.0	30
16	796	SLU (T4)	2042.7	165.9	-609.6	43.5	0.0	30
17	796	SLU_URTO X	1501.5	0.0	-402.6	0.0	0.0	30
18	796	SLU_URTO Y	1501.0	0.0	-402.2	0.0	0.0	30
19	796	Comb. SLVx (q=1)	1608.9	-263.5	486.5	34.0	112.6	30
20	796	Comb. SLVx (q=1)	1393.4	263.5	-1291.1	-34.1	-112.6	30
21	796	Comb. SLVy (q=1)	1589.1	-878.2	-71.1	113.5	35.4	30
22	796	Comb. SLVy (q=1)	1413.2	878.2	-733.5	-113.5	-35.4	30
23	798	SLU (q1)	2453.6	0.0	207.5	0.0	-117.0	30
24	798	SLU (q2)	2366.2	0.0	2021.0	0.0	155.5	30
25	798	SLU (q3)	2417.3	-165.9	1144.3	-43.5	22.0	30
26	798	SLU (q4)	2473.8	165.9	1185.8	43.5	20.5	30
27	798	SLU (n1)	2060.3	0.0	-245.9	0.0	-126.9	30
28	798	SLU (n2)	1973.0	0.0	1567.6	0.0	145.6	30
29	798	SLU (n3)	2024.1	-165.9	690.9	-43.5	12.2	30
30	798	SLU (n4)	2080.6	165.9	732.4	43.5	10.7	30
31	798	SLU (v1)	2008.7	0.0	-943.9	0.0	-219.8	30
32	798	SLU (v2)	1863.1	0.0	2078.6	0.0	234.4	30
33	798	SLU (v3)	1948.3	-276.5	617.4	-72.5	12.0	30
34	798	SLU (v4)	2042.4	276.5	686.6	72.5	9.5	30
35	798	SLU (T1)	2021.8	0.0	-329.9	0.0	-132.7	30
36	798	SLU (T2)	1934.5	0.0	1483.6	0.0	139.8	30
37	798	SLU (T3)	1985.6	-165.9	606.8	-43.5	6.3	30
38	798	SLU (T4)	2042.1	165.9	648.3	43.5	4.8	30
39	798	SLU_URTO X	1500.4	0.0	-1714.0	0.0	-260.8	30
40	798	SLU_URTO Y	1501.0	0.0	172.4	0.0	-28.3	30

ID	Nodo	Combinazione	N	Mt	Ml	Tt	Tl	n
-	-	-	[kN]	[kNm]	[kNm]	[kN]	[kN]	[-]
41	798	Comb. SLVx (q=1)	1606.9	-263.5	3540.6	34.0	390.2	30
42	798	Comb. SLVx (q=1)	1394.9	263.5	-2558.7	-34.1	-368.2	30
43	798	Comb. SLVy (q=1)	1591.9	-878.2	1600.1	113.5	146.9	30
44	798	Comb. SLVy (q=1)	1409.9	878.2	-618.2	-113.5	-125.0	30
45	802	SLU (q1)	2690.8	-72.4	-1364.6	-8.9	-36.5	30
46	802	SLU (q2)	2794.4	-253.2	-1184.5	-31.2	36.5	30
47	802	SLU (q3)	2825.8	-553.3	-1353.6	-91.3	0.0	30
48	802	SLU (q4)	2823.9	214.3	-1351.8	49.5	0.0	30
49	802	SLU (n1)	2167.2	-1.5	-867.1	-0.2	-36.5	30
50	802	SLU (n2)	2270.7	-182.4	-687.0	-22.5	36.5	30
51	802	SLU (n3)	2302.1	-482.4	-856.1	-82.5	0.0	30
52	802	SLU (n4)	2300.2	285.2	-854.3	58.2	0.0	30
53	802	SLU (v1)	2020.1	73.2	-820.2	9.0	-60.9	30
54	802	SLU (v2)	2192.7	-228.3	-520.1	-28.1	60.9	30
55	802	SLU (v3)	2245.1	-728.4	-801.9	-128.2	0.0	30
56	802	SLU (v4)	2241.9	550.9	-798.9	106.4	0.0	30
57	802	SLU (T1)	2087.3	18.9	-791.2	2.3	-36.5	30
58	802	SLU (T2)	2190.8	-161.9	-611.1	-20.0	36.5	30
59	802	SLU (T3)	2222.3	-462.0	-780.2	-80.0	0.0	30
60	802	SLU (T4)	2220.4	305.6	-778.4	60.7	0.0	30
61	802	SLU_URTO X	1653.0	99.4	-546.5	12.3	0.0	30
62	802	SLU_URTO Y	1653.7	-1565.7	-547.2	-193.0	0.0	30
63	802	Comb. SLVx (q=1)	1755.9	-1746.4	337.7	197.0	112.1	30
64	802	Comb. SLVx (q=1)	1551.5	1592.8	-1432.1	-215.9	-112.1	30
65	802	Comb. SLVy (q=1)	1736.3	-4443.9	-223.9	530.1	34.8	30
66	802	Comb. SLVy (q=1)	1571.0	4290.3	-870.4	-549.1	-34.8	30
67	804	SLU (q1)	2803.4	72.4	40.7	8.9	-178.6	30
68	804	SLU (q2)	2699.1	253.3	1584.7	31.2	62.7	30
69	804	SLU (q3)	2834.7	-221.8	840.3	-50.4	-64.3	30
70	804	SLU (q4)	2832.6	560.9	856.5	92.2	-62.1	30
71	804	SLU (n1)	2276.0	1.5	-234.0	0.2	-150.7	30
72	804	SLU (n2)	2171.8	182.4	1310.0	22.5	90.6	30
73	804	SLU (n3)	2307.4	-292.7	565.5	-59.2	-36.4	30
74	804	SLU (n4)	2305.3	490.0	581.7	83.5	-34.2	30
75	804	SLU (v1)	2198.0	-73.2	-806.9	-9.0	-225.1	30
76	804	SLU (v2)	2024.2	228.3	1766.4	28.1	177.0	30
77	804	SLU (v3)	2250.3	-563.6	525.7	-107.9	-34.7	30
78	804	SLU (v4)	2246.7	741.1	552.7	129.8	-30.9	30
79	804	SLU (T1)	2196.3	-18.9	-196.5	-2.3	-136.7	30
80	804	SLU (T2)	2092.0	161.9	1347.4	20.0	104.5	30
81	804	SLU (T3)	2227.6	-313.2	603.0	-61.7	-22.5	30
82	804	SLU (T4)	2225.5	469.6	619.2	81.0	-20.2	30

*Relazione di calcolo strutturale  
fondazioni pile ponte pedonale*

COMMESSA	LOTTO	FASE-ENTE	DOCUMENTO	REV.	FOGLIO
RS3Z	00	D 26	CLFV0300009	B	14 di 34

ID	Nodo	Combinazione	N	Mt	Ml	Tt	Tl	n
-	-	-	[kN]	[kNm]	[kNm]	[kN]	[kN]	[-]
83	804	SLU_URTO X	1658.1	-99.4	-10058.3	-12.3	-3452.8	30
84	804	SLU_URTO Y	1657.0	-4077.8	244.5	-1307.0	-37.7	30
85	804	Comb. SLVx (q=1)	1759.1	-1677.9	2167.0	233.8	215.6	30
86	804	Comb. SLVx (q=1)	1555.1	1831.5	-1570.0	-214.9	-277.7	30
87	804	Comb. SLVy (q=1)	1749.6	-4293.5	964.7	564.8	57.3	30
88	804	Comb. SLVy (q=1)	1564.6	4447.1	-367.8	-545.9	-119.4	30

Palo1		Palo2		Palo3		Palo4		Palo5		Palo6		Palo7		Palo8		Palo9	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
89.6	1.2	89.6	1.2	89.6	1.2	87.2	1.2	87.2	1.2	87.2	1.2	84.8	1.2	84.8	1.2	84.8	1.2
90.5	1.2	90.5	1.2	90.5	1.2	88.6	1.2	88.6	1.2	88.6	1.2	86.7	1.2	86.7	1.2	86.7	1.2
95.0	1.5	90.4	1.5	85.8	1.5	92.8	1.5	88.2	1.5	83.6	1.5	90.6	1.5	86.0	1.5	81.4	1.5
88.2	1.5	92.8	1.5	97.4	1.5	85.9	1.5	90.5	1.5	95.1	1.5	83.6	1.5	88.2	1.5	92.8	1.5
72.7	1.2	72.7	1.2	72.7	1.2	71.2	1.2	71.2	1.2	71.2	1.2	69.6	1.2	69.6	1.2	69.6	1.2
73.6	1.2	73.6	1.2	73.6	1.2	72.5	1.2	72.5	1.2	72.5	1.2	71.4	1.2	71.4	1.2	71.4	1.2
78.1	1.5	73.5	1.5	68.9	1.5	76.8	1.5	72.1	1.5	67.5	1.5	75.4	1.5	70.8	1.5	66.2	1.5
71.3	1.5	75.9	1.5	80.5	1.5	69.8	1.5	74.4	1.5	79.1	1.5	68.4	1.5	73.0	1.5	77.6	1.5
68.9	2.0	68.9	2.0	68.9	2.0	67.4	2.0	67.4	2.0	67.4	2.0	65.9	2.0	65.9	2.0	65.9	2.0
70.5	2.0	70.5	2.0	70.5	2.0	69.7	2.0	69.7	2.0	69.7	2.0	68.9	2.0	68.9	2.0	68.9	2.0
77.9	2.4	70.2	2.4	62.5	2.4	76.7	2.4	69.1	2.4	61.4	2.4	75.6	2.4	67.9	2.4	60.2	2.4
66.6	2.4	74.3	2.4	81.9	2.4	65.2	2.4	72.9	2.4	80.6	2.4	63.8	2.4	71.5	2.4	79.2	2.4
71.0	1.2	71.0	1.2	71.0	1.2	69.6	1.2	69.6	1.2	69.6	1.2	68.1	1.2	68.1	1.2	68.1	1.2
72.0	1.2	72.0	1.2	72.0	1.2	71.0	1.2	71.0	1.2	71.0	1.2	70.0	1.2	70.0	1.2	70.0	1.2
76.4	1.5	71.8	1.5	67.2	1.5	75.2	1.5	70.6	1.5	66.0	1.5	73.9	1.5	69.3	1.5	64.7	1.5
69.6	1.5	74.2	1.5	78.9	1.5	68.3	1.5	72.9	1.5	77.5	1.5	66.9	1.5	71.5	1.5	76.1	1.5
54.1	0.0	54.1	0.0	54.1	0.0	53.2	0.0	53.2	0.0	53.2	0.0	52.3	0.0	52.3	0.0	52.3	0.0
54.1	0.0	54.1	0.0	54.1	0.0	53.2	0.0	53.2	0.0	53.2	0.0	52.3	0.0	52.3	0.0	52.3	0.0
56.0	3.9	48.7	3.9	41.4	3.9	57.1	3.9	49.8	3.9	42.5	3.9	58.2	3.9	50.9	3.9	43.6	3.9
52.2	3.9	59.5	3.9	66.8	3.9	49.3	3.9	56.6	3.9	63.9	3.9	46.4	3.9	53.7	3.9	61.0	3.9
78.1	4.0	53.7	4.0	29.3	4.0	77.9	4.0	53.5	4.0	29.1	4.0	77.8	4.0	53.4	4.0	29.0	4.0
30.1	4.0	54.5	4.0	78.9	4.0	28.5	4.0	52.9	4.0	77.3	4.0	26.8	4.0	51.2	4.0	75.6	4.0
79.7	3.9	79.7	3.9	79.7	3.9	80.2	3.9	80.2	3.9	80.2	3.9	80.6	3.9	80.6	3.9	80.6	3.9
58.5	5.2	58.5	5.2	58.5	5.2	63.0	5.2	63.0	5.2	63.0	5.2	67.5	5.2	67.5	5.2	67.5	5.2
73.6	1.6	69.0	1.6	64.4	1.6	76.2	1.6	71.6	1.6	67.0	1.6	78.8	1.6	74.2	1.6	69.5	1.6
65.9	1.6	70.5	1.6	75.1	1.6	68.5	1.6	73.1	1.6	77.8	1.6	71.2	1.6	75.8	1.6	80.4	1.6
71.2	4.2	71.2	4.2	71.2	4.2	70.6	4.2	70.6	4.2	70.6	4.2	70.1	4.2	70.1	4.2	70.1	4.2
49.9	4.9	49.9	4.9	49.9	4.9	53.5	4.9	53.4	4.9	53.4	4.9	57.0	4.9	57.0	4.9	57.0	4.9
65.1	1.5	60.5	1.5	55.9	1.5	66.7	1.5	62.0	1.5	57.4	1.5	68.2	1.5	63.6	1.5	59.0	1.5
57.3	1.5	62.0	1.5	66.6	1.5	59.0	1.5	63.6	1.5	68.2	1.5	60.6	1.5	65.2	1.5	69.9	1.5
76.5	7.3	76.5	7.3	76.5	7.3	74.4	7.3	74.4	7.3	74.4	7.3	72.3	7.3	72.3	7.3	72.3	7.3



Palo1		Palo2		Palo3		Palo4		Palo5		Palo6		Palo7		Palo8		Palo9	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
41.1	7.8	41.1	7.8	41.1	7.8	45.8	7.8	45.8	7.8	45.8	7.8	50.4	7.8	50.4	7.8	50.4	7.8
66.4	2.5	58.7	2.5	51.0	2.5	67.8	2.5	60.1	2.5	52.4	2.5	69.2	2.5	61.5	2.5	53.8	2.5
53.5	2.4	61.1	2.4	68.8	2.4	55.0	2.4	62.7	2.4	70.4	2.4	56.5	2.4	64.2	2.4	71.9	2.4
70.7	4.4	70.7	4.4	70.7	4.4	70.0	4.4	70.0	4.4	70.0	4.4	69.2	4.4	69.2	4.4	69.2	4.4
49.5	4.7	49.5	4.7	49.5	4.7	52.8	4.7	52.8	4.7	52.8	4.7	56.2	4.7	56.2	4.7	56.2	4.7
64.7	1.5	60.1	1.5	55.4	1.5	66.0	1.5	61.4	1.5	56.8	1.5	67.4	1.5	62.8	1.5	58.2	1.5
56.9	1.5	61.5	1.5	66.1	1.5	58.4	1.5	63.0	1.5	67.6	1.5	59.8	1.5	64.4	1.5	69.0	1.5
67.3	8.7	67.3	8.7	67.3	8.7	63.5	8.7	63.5	8.7	63.5	8.7	59.6	8.7	59.6	8.7	59.6	8.7
48.3	0.9	48.3	0.9	48.3	0.9	48.7	0.9	48.7	0.9	48.7	0.9	49.1	0.9	49.1	0.9	49.1	0.9
25.1	13.1	17.8	13.1	10.5	13.1	33.1	13.1	25.7	13.1	18.4	13.1	41.0	13.1	33.7	13.1	26.4	13.1
65.0	12.3	72.3	12.3	79.7	12.3	59.3	12.3	66.6	12.3	73.9	12.3	53.5	12.3	60.9	12.3	68.2	12.3
61.3	6.2	36.9	6.2	12.5	6.2	64.9	6.2	40.5	6.2	16.1	6.2	68.5	6.2	44.1	6.2	19.7	6.2
28.8	5.6	53.2	5.6	77.6	5.6	27.5	5.6	51.9	5.6	76.2	5.6	26.1	5.6	50.5	5.6	74.9	5.6
105.5	1.3	103.5	1.3	101.5	1.3	102.4	1.3	100.4	1.3	98.4	1.3	99.4	1.3	97.4	1.3	95.3	1.3
112.1	1.6	105.1	1.6	98.1	1.6	109.5	1.6	102.5	1.6	95.4	1.6	106.8	1.6	99.8	1.6	92.8	1.6
123.2	3.0	107.9	3.0	92.5	3.0	120.2	3.0	104.8	3.0	89.5	3.0	117.2	3.0	101.8	3.0	86.4	3.0
101.8	1.6	107.8	1.6	113.7	1.6	98.8	1.6	104.7	1.6	110.7	1.6	95.8	1.6	101.7	1.6	107.7	1.6
81.0	1.2	81.0	1.2	81.0	1.2	79.1	1.2	79.1	1.2	79.0	1.2	77.1	1.2	77.1	1.2	77.1	1.2
87.7	1.4	82.6	1.4	77.6	1.4	86.2	1.4	81.1	1.4	76.0	1.4	84.6	1.4	79.5	1.4	74.5	1.4
98.8	2.8	85.4	2.8	72.0	2.8	96.9	2.8	83.5	2.8	70.1	2.8	94.9	2.8	81.5	2.8	68.1	2.8
77.4	1.9	85.3	1.9	93.2	1.9	75.5	1.9	83.4	1.9	91.3	1.9	73.5	1.9	81.5	1.9	89.4	1.9
73.6	2.1	75.6	2.1	77.7	2.1	71.7	2.1	73.8	2.1	75.8	2.1	69.9	2.1	71.9	2.1	74.0	2.1
84.7	2.2	78.3	2.2	72.0	2.2	83.5	2.2	77.2	2.2	70.8	2.2	82.3	2.2	76.0	2.2	69.7	2.2
103.2	4.3	82.9	4.3	62.7	4.3	101.4	4.3	81.1	4.3	60.9	4.3	99.6	4.3	79.3	4.3	59.1	4.3
67.5	3.5	82.8	3.5	98.1	3.5	65.7	3.5	81.0	3.5	96.3	3.5	63.9	3.5	79.2	3.5	94.5	3.5
77.0	1.2	77.6	1.2	78.1	1.2	75.3	1.2	75.8	1.2	76.3	1.2	73.5	1.2	74.0	1.2	74.5	1.2
83.7	1.4	79.2	1.4	74.7	1.4	82.3	1.4	77.8	1.4	73.3	1.4	81.0	1.4	76.5	1.4	72.0	1.4
94.8	2.7	82.0	2.7	69.1	2.7	93.0	2.7	80.2	2.7	67.4	2.7	91.3	2.7	78.5	2.7	65.6	2.7
73.4	2.0	81.9	2.0	90.4	2.0	71.6	2.0	80.1	2.0	88.6	2.0	69.9	2.0	78.4	2.0	86.9	2.0
57.9	0.4	60.6	0.4	63.4	0.4	56.6	0.4	59.4	0.4	62.2	0.4	55.4	0.4	58.2	0.4	60.9	0.4
104.1	6.4	60.7	6.4	17.2	6.4	102.9	6.4	59.4	6.4	15.9	6.4	101.7	6.4	58.2	6.4	14.7	6.4
103.6	7.6	55.1	7.6	6.6	7.6	104.4	7.6	55.9	7.6	7.4	7.6	105.1	7.6	56.6	7.6	8.1	7.6
21.9	8.1	66.2	8.1	110.4	8.1	18.7	8.1	63.0	8.1	107.2	8.1	15.5	8.1	59.8	8.1	104.0	8.1
183.6	17.7	60.1	17.7	-63.3	17.7	183.1	17.7	59.6	17.7	-63.8	17.7	182.6	17.7	59.1	17.7	-64.3	17.7
-58.0	18.3	61.2	18.3	180.3	18.3	-60.0	18.3	59.2	18.3	178.4	18.3	-61.9	18.3	57.3	18.3	176.4	18.3
91.0	6.0	93.0	6.0	95.0	6.0	91.1	6.0	93.1	6.0	95.1	6.0	91.2	6.0	93.2	6.0	95.2	6.0
66.9	2.3	74.0	2.3	81.0	2.3	70.5	2.3	77.5	2.3	84.6	2.3	74.0	2.3	81.1	2.3	88.1	2.3
92.2	2.7	86.0	2.7	79.8	2.7	94.1	2.7	87.9	2.7	81.7	2.7	95.9	2.7	89.8	2.7	83.6	2.7
70.2	3.7	85.8	3.7	101.3	3.7	72.1	3.7	87.7	3.7	103.3	3.7	74.0	3.7	89.6	3.7	105.2	3.7
78.2	5.0	78.2	5.0	78.3	5.0	77.7	5.0	77.7	5.0	77.7	5.0	77.1	5.0	77.2	5.0	77.2	5.0
54.1	3.1	59.2	3.1	64.2	3.1	57.0	3.1	62.1	3.1	67.2	3.1	60.0	3.1	65.0	3.1	70.1	3.1

Palo1		Palo2		Palo3		Palo4		Palo5		Palo6		Palo7		Palo8		Palo9	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
79.3	2.3	71.2	2.3	63.1	2.3	80.6	2.3	72.5	2.3	64.3	2.3	81.9	2.3	73.7	2.3	65.6	2.3
57.4	3.0	71.0	3.0	84.6	3.0	58.7	3.0	72.3	3.0	85.9	3.0	60.0	3.0	73.6	3.0	87.2	3.0
83.4	7.5	81.4	7.5	79.4	7.5	81.6	7.5	79.6	7.5	77.6	7.5	79.8	7.5	77.8	7.5	75.8	7.5
43.3	6.0	49.6	6.0	56.0	6.0	47.3	6.0	53.6	6.0	59.9	6.0	51.2	6.0	57.6	6.0	63.9	6.0
85.4	3.8	69.7	3.8	54.0	3.8	86.5	3.8	70.9	3.8	55.2	3.8	87.7	3.8	72.1	3.8	56.4	3.8
48.7	4.4	69.3	4.4	89.9	4.4	50.0	4.4	70.5	4.4	91.1	4.4	51.2	4.4	71.8	4.4	92.4	4.4
75.7	4.6	75.2	4.6	74.7	4.6	75.3	4.6	74.8	4.6	74.2	4.6	74.8	4.6	74.3	4.6	73.8	4.6
51.6	3.5	56.1	3.5	60.6	3.5	54.6	3.5	59.1	3.5	63.6	3.5	57.7	3.5	62.2	3.5	66.7	3.5
76.9	2.2	68.2	2.2	59.5	2.2	78.2	2.2	69.5	2.2	60.8	2.2	79.6	2.2	70.9	2.2	62.2	2.2
54.9	2.8	67.9	2.8	81.0	2.8	56.3	2.8	69.3	2.8	82.4	2.8	57.7	2.8	70.7	2.8	83.8	2.8
159.6	115.1	156.9	115.1	154.1	115.1	137.1	115.1	134.3	115.1	131.5	115.1	114.5	115.1	111.7	115.1	109.0	115.1
166.0	43.6	52.8	43.6	-60.5	43.6	166.6	43.6	53.3	43.6	-60.0	43.6	167.1	43.6	53.9	43.6	-59.4	43.6
83.4	10.6	36.7	10.6	-9.9	10.6	88.2	10.6	41.6	10.6	-5.0	10.6	93.1	10.6	46.5	10.6	-0.1	10.6
16.8	11.7	67.7	11.7	118.6	11.7	13.3	11.7	64.2	11.7	115.0	11.7	9.8	11.7	60.6	11.7	111.5	11.7
167.8	18.9	48.6	18.9	-70.7	18.9	170.0	18.9	50.7	18.9	-68.5	18.9	172.2	18.9	52.9	18.9	-66.4	18.9
-67.7	18.6	55.9	18.6	179.4	18.6	-68.5	18.6	55.0	18.6	178.6	18.6	-69.3	18.6	54.2	18.6	177.7	18.6

Palo10		Palo11		Palo12		Palo13		Palo14		Palo15		Palo16		Palo17		Palo18	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
82.5	1.2	82.5	1.2	82.5	1.2	80.1	1.2	80.1	1.2	80.1	1.2	77.7	1.2	77.7	1.2	77.7	1.2
84.7	1.2	84.7	1.2	84.7	1.2	82.8	1.2	82.8	1.2	82.8	1.2	80.9	1.2	80.9	1.2	80.9	1.2
88.5	1.5	83.9	1.5	79.3	1.5	86.3	1.5	81.7	1.5	77.1	1.5	84.1	1.5	79.5	1.5	74.9	1.5
81.3	1.5	85.9	1.5	90.5	1.5	79.0	1.5	83.6	1.5	88.2	1.5	76.7	1.5	81.3	1.5	86.0	1.5
68.1	1.2	68.1	1.2	68.1	1.2	66.6	1.2	66.6	1.2	66.6	1.2	65.0	1.2	65.0	1.2	65.0	1.2
70.3	1.2	70.3	1.2	70.3	1.2	69.3	1.2	69.3	1.2	69.3	1.2	68.2	1.2	68.2	1.2	68.2	1.2
74.1	1.5	69.5	1.5	64.9	1.5	72.8	1.5	68.2	1.5	63.5	1.5	71.4	1.5	66.8	1.5	62.2	1.5
66.9	1.5	71.5	1.5	76.2	1.5	65.5	1.5	70.1	1.5	74.7	1.5	64.0	1.5	68.6	1.5	73.3	1.5
64.4	2.0	64.4	2.0	64.4	2.0	62.9	2.0	62.9	2.0	62.9	2.0	61.4	2.0	61.4	2.0	61.4	2.0
68.2	2.0	68.2	2.0	68.2	2.0	67.4	2.0	67.4	2.0	67.4	2.0	66.6	2.0	66.6	2.0	66.6	2.0
74.4	2.4	66.7	2.4	59.0	2.4	73.2	2.4	65.5	2.4	57.9	2.4	72.1	2.4	64.4	2.4	56.7	2.4
62.5	2.4	70.1	2.4	77.8	2.4	61.1	2.4	68.8	2.4	76.5	2.4	59.7	2.4	67.4	2.4	75.1	2.4
66.7	1.2	66.7	1.2	66.7	1.2	65.2	1.2	65.2	1.2	65.2	1.2	63.8	1.2	63.8	1.2	63.8	1.2
68.9	1.2	68.9	1.2	68.9	1.2	67.9	1.2	67.9	1.2	67.9	1.2	66.9	1.2	66.9	1.2	66.9	1.2
72.7	1.5	68.1	1.5	63.5	1.5	71.4	1.5	66.8	1.5	62.2	1.5	70.2	1.5	65.6	1.5	61.0	1.5
65.5	1.5	70.1	1.5	74.7	1.5	64.2	1.5	68.8	1.5	73.4	1.5	62.8	1.5	67.4	1.5	72.0	1.5
51.4	0.0	51.4	0.0	51.4	0.0	50.5	0.0	50.5	0.0	50.5	0.0	49.6	0.0	49.6	0.0	49.6	0.0
51.4	0.0	51.4	0.0	51.4	0.0	50.5	0.0	50.5	0.0	50.5	0.0	49.6	0.0	49.6	0.0	49.6	0.0
59.3	3.9	52.0	3.9	44.7	3.9	60.4	3.9	53.1	3.9	45.8	3.9	61.5	3.9	54.2	3.9	46.9	3.9
43.5	3.9	50.8	3.9	58.1	3.9	40.6	3.9	47.9	3.9	55.2	3.9	37.7	3.9	45.0	3.9	52.3	3.9

*Relazione di calcolo strutturale  
fondazioni pile ponte pedonale*

COMMESSA	LOTTO	FASE-ENTE	DOCUMENTO	REV.	FOGLIO
RS3Z	00	D 26	CLFV0300009	B	17 di 34

Palo10		Palo11		Palo12		Palo13		Palo14		Palo15		Palo16		Palo17		Palo18	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
77.6	4.0	53.2	4.0	28.8	4.0	77.4	4.0	53.0	4.0	28.7	4.0	77.3	4.0	52.9	4.0	28.5	4.0
25.2	4.0	49.6	4.0	74.0	4.0	23.5	4.0	47.9	4.0	72.3	4.0	21.9	4.0	46.3	4.0	70.7	4.0
81.1	3.9	81.1	3.9	81.1	3.9	81.6	3.9	81.6	3.9	81.6	3.9	82.0	3.9	82.0	3.9	82.0	3.9
72.1	5.2	72.1	5.2	72.1	5.2	76.6	5.2	76.6	5.2	76.6	5.2	81.1	5.2	81.1	5.2	81.1	5.2
81.3	1.6	76.7	1.6	72.1	1.6	83.9	1.6	79.3	1.6	74.7	1.6	86.5	1.6	81.9	1.6	77.3	1.6
73.9	1.6	78.5	1.6	83.1	1.6	76.5	1.6	81.1	1.6	85.7	1.6	79.2	1.6	83.8	1.6	88.4	1.6
69.5	4.2	69.5	4.2	69.5	4.2	69.0	4.2	69.0	4.2	69.0	4.2	68.4	4.2	68.4	4.2	68.4	4.2
60.5	4.9	60.5	4.9	60.5	4.9	64.0	4.9	64.0	4.9	64.0	4.9	67.5	4.9	67.5	4.9	67.5	4.9
69.8	1.5	65.1	1.5	60.5	1.5	71.3	1.5	66.7	1.5	62.1	1.5	72.9	1.5	68.2	1.5	63.6	1.5
62.3	1.5	66.9	1.5	71.5	1.5	63.9	1.5	68.5	1.5	73.1	1.5	65.6	1.5	70.2	1.5	74.8	1.5
70.1	7.3	70.1	7.3	70.1	7.3	68.0	7.3	68.0	7.3	68.0	7.3	65.9	7.3	65.9	7.3	65.9	7.3
55.1	7.8	55.1	7.8	55.1	7.8	59.8	7.8	59.8	7.8	59.8	7.8	64.4	7.8	64.4	7.8	64.4	7.8
70.5	2.5	62.9	2.5	55.2	2.5	71.9	2.5	64.2	2.5	56.6	2.5	73.3	2.5	65.6	2.5	58.0	2.5
58.1	2.4	65.8	2.4	73.4	2.4	59.6	2.4	67.3	2.4	75.0	2.4	61.2	2.4	68.9	2.4	76.5	2.4
68.5	4.4	68.5	4.4	68.5	4.4	67.8	4.4	67.8	4.4	67.8	4.4	67.0	4.4	67.0	4.4	67.0	4.4
59.5	4.7	59.5	4.7	59.5	4.7	62.8	4.7	62.8	4.7	62.8	4.7	66.1	4.7	66.1	4.7	66.1	4.7
68.8	1.5	64.1	1.5	59.5	1.5	70.1	1.5	65.5	1.5	60.9	1.5	71.5	1.5	66.9	1.5	62.3	1.5
61.3	1.5	65.9	1.5	70.5	1.5	62.7	1.5	67.3	1.5	71.9	1.5	64.2	1.5	68.8	1.5	73.4	1.5
55.8	8.7	55.8	8.7	55.8	8.7	51.9	8.7	51.9	8.7	51.9	8.7	48.1	8.7	48.1	8.7	48.1	8.7
49.5	0.9	49.5	0.9	49.5	0.9	49.8	0.9	49.8	0.9	49.8	0.9	50.2	0.9	50.2	0.9	50.2	0.9
49.0	13.1	41.6	13.1	34.3	13.1	56.9	13.1	49.6	13.1	42.3	13.1	64.9	13.1	57.5	13.1	50.2	13.1
47.8	12.3	55.1	12.3	62.4	12.3	42.0	12.3	49.4	12.3	56.7	12.3	36.3	12.3	43.6	12.3	50.9	12.3
72.1	6.2	47.7	6.2	23.3	6.2	75.7	6.2	51.3	6.2	26.9	6.2	79.3	6.2	54.9	6.2	30.5	6.2
24.7	5.6	49.1	5.6	73.5	5.6	23.3	5.6	47.7	5.6	72.1	5.6	21.9	5.6	46.3	5.6	70.7	5.6
96.3	1.3	94.3	1.3	92.3	1.3	93.2	1.3	91.2	1.3	89.2	1.3	90.2	1.3	88.2	1.3	86.2	1.3
104.2	1.6	97.1	1.6	90.1	1.6	101.5	1.6	94.5	1.6	87.4	1.6	98.9	1.6	91.8	1.6	84.8	1.6
114.1	3.0	98.8	3.0	83.4	3.0	111.1	3.0	95.7	3.0	80.3	3.0	108.0	3.0	92.7	3.0	77.3	3.0
92.7	1.6	98.7	1.6	104.6	1.6	89.7	1.6	95.6	1.6	101.6	1.6	86.7	1.6	92.6	1.6	98.6	1.6
75.2	1.2	75.2	1.2	75.1	1.2	73.3	1.2	73.2	1.2	73.2	1.2	71.3	1.2	71.3	1.2	71.2	1.2
83.1	1.4	78.0	1.4	72.9	1.4	81.5	1.4	76.5	1.4	71.4	1.4	80.0	1.4	74.9	1.4	69.9	1.4
93.0	2.8	79.6	2.8	66.2	2.8	91.1	2.8	77.7	2.8	64.3	2.8	89.2	2.8	75.8	2.8	62.4	2.8
71.6	1.9	79.6	1.9	87.5	1.9	69.7	1.9	77.6	1.9	85.6	1.9	67.8	1.9	75.7	1.9	83.6	1.9
68.1	2.1	70.1	2.1	72.1	2.1	66.2	2.1	68.3	2.1	70.3	2.1	64.4	2.1	66.4	2.1	68.4	2.1
81.2	2.2	74.8	2.2	68.5	2.2	80.0	2.2	73.7	2.2	67.3	2.2	78.8	2.2	72.5	2.2	66.2	2.2
97.8	4.3	77.5	4.3	57.3	4.3	96.0	4.3	75.7	4.3	55.5	4.3	94.2	4.3	73.9	4.3	53.7	4.3
62.1	3.5	77.4	3.5	92.7	3.5	60.3	3.5	75.6	3.5	90.9	3.5	58.5	3.5	73.8	3.5	89.1	3.5
71.7	1.2	72.2	1.2	72.8	1.2	69.9	1.2	70.5	1.2	71.0	1.2	68.2	1.2	68.7	1.2	69.2	1.2
79.6	1.4	75.1	1.4	70.6	1.4	78.2	1.4	73.7	1.4	69.2	1.4	76.8	1.4	72.3	1.4	67.8	1.4
89.5	2.7	76.7	2.7	63.9	2.7	87.8	2.7	75.0	2.7	62.1	2.7	86.0	2.7	73.2	2.7	60.4	2.7
68.1	2.0	76.6	2.0	85.1	2.0	66.4	2.0	74.9	2.0	83.4	2.0	64.6	2.0	73.1	2.0	81.6	2.0
54.2	0.4	56.9	0.4	59.7	0.4	53.0	0.4	55.7	0.4	58.5	0.4	51.7	0.4	54.5	0.4	57.2	0.4

Palo10		Palo11		Palo12		Palo13		Palo14		Palo15		Palo16		Palo17		Palo18	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
100.5	6.4	57.0	6.4	13.5	6.4	99.2	6.4	55.7	6.4	12.2	6.4	98.0	6.4	54.5	6.4	11.0	6.4
105.9	7.6	57.4	7.6	8.9	7.6	106.7	7.6	58.1	7.6	9.6	7.6	107.4	7.6	58.9	7.6	10.4	7.6
12.3	8.1	56.5	8.1	100.8	8.1	9.1	8.1	53.3	8.1	97.6	8.1	5.9	8.1	50.1	8.1	94.4	8.1
182.1	17.7	58.6	17.7	-64.8	17.7	181.6	17.7	58.1	17.7	-65.3	17.7	181.1	17.7	57.6	17.7	-65.8	17.7
-63.9	18.3	55.3	18.3	174.5	18.3	-65.8	18.3	53.3	18.3	172.5	18.3	-67.8	18.3	51.4	18.3	170.6	18.3
91.3	6.0	93.3	6.0	95.3	6.0	91.4	6.0	93.4	6.0	95.4	6.0	91.5	6.0	93.5	6.0	95.5	6.0
77.6	2.3	84.6	2.3	91.7	2.3	81.2	2.3	88.2	2.3	95.2	2.3	84.7	2.3	91.7	2.3	98.8	2.3
97.8	2.7	91.7	2.7	85.5	2.7	99.7	2.7	93.5	2.7	87.4	2.7	101.6	2.7	95.4	2.7	89.3	2.7
76.0	3.7	91.5	3.7	107.1	3.7	77.9	3.7	93.5	3.7	109.0	3.7	79.8	3.7	95.4	3.7	111.0	3.7
76.6	5.0	76.7	5.0	76.7	5.0	76.1	5.0	76.1	5.0	76.2	5.0	75.6	5.0	75.6	5.0	75.6	5.0
62.9	3.1	68.0	3.1	73.0	3.1	65.9	3.1	70.9	3.1	76.0	3.1	68.8	3.1	73.9	3.1	78.9	3.1
83.1	2.3	75.0	2.3	66.9	2.3	84.4	2.3	76.3	2.3	68.1	2.3	85.7	2.3	77.5	2.3	69.4	2.3
61.3	3.0	74.9	3.0	88.5	3.0	62.6	3.0	76.2	3.0	89.8	3.0	63.9	3.0	77.5	3.0	91.1	3.0
78.0	7.5	76.0	7.5	74.0	7.5	76.2	7.5	74.2	7.5	72.1	7.5	74.4	7.5	72.4	7.5	70.3	7.5
55.2	6.0	61.5	6.0	67.9	6.0	59.1	6.0	65.5	6.0	71.8	6.0	63.1	6.0	69.5	6.0	75.8	6.0
88.9	3.8	73.2	3.8	57.6	3.8	90.1	3.8	74.4	3.8	58.8	3.8	91.3	3.8	75.6	3.8	59.9	3.8
52.4	4.4	73.0	4.4	93.6	4.4	53.7	4.4	74.3	4.4	94.9	4.4	54.9	4.4	75.5	4.4	96.1	4.4
74.4	4.6	73.9	4.6	73.3	4.6	74.0	4.6	73.4	4.6	72.9	4.6	73.5	4.6	73.0	4.6	72.5	4.6
60.7	3.5	65.2	3.5	69.7	3.5	63.7	3.5	68.2	3.5	72.7	3.5	66.7	3.5	71.2	3.5	75.7	3.5
80.9	2.2	72.2	2.2	63.5	2.2	82.3	2.2	73.6	2.2	64.9	2.2	83.6	2.2	74.9	2.2	66.2	2.2
59.1	2.8	72.1	2.8	85.1	2.8	60.4	2.8	73.5	2.8	86.5	2.8	61.8	2.8	74.9	2.8	87.9	2.8
91.9	115.1	89.1	115.1	86.4	115.1	69.3	115.1	66.6	115.1	63.8	115.1	46.7	115.1	44.0	115.1	41.2	115.1
167.7	43.6	54.4	43.6	-58.9	43.6	168.2	43.6	55.0	43.6	-58.3	43.6	168.8	43.6	55.5	43.6	-57.8	43.6
97.9	10.6	51.3	10.6	4.7	10.6	102.8	10.6	56.2	10.6	9.6	10.6	107.7	10.6	61.1	10.6	14.5	10.6
6.2	11.7	57.1	11.7	108.0	11.7	2.7	11.7	53.6	11.7	104.5	11.7	-0.8	11.7	50.1	11.7	100.9	11.7
174.3	18.9	55.1	18.9	-64.2	18.9	176.5	18.9	57.2	18.9	-62.0	18.9	178.7	18.9	59.4	18.9	-59.9	18.9
-70.1	18.6	53.4	18.6	176.9	18.6	-71.0	18.6	52.6	18.6	176.1	18.6	-71.8	18.6	51.7	18.6	175.3	18.6

Palo19		Palo20		Palo21		Palo22		Palo23		Palo24		Palo25		Palo26		Palo27	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
75.3	1.2	75.3	1.2	75.3	1.2	73.0	1.2	73.0	1.2	73.0	1.2	70.6	1.2	70.6	1.2	70.6	1.2
78.9	1.2	78.9	1.2	78.9	1.2	77.0	1.2	77.0	1.2	77.0	1.2	75.1	1.2	75.1	1.2	75.1	1.2
82.0	1.5	77.4	1.5	72.7	1.5	79.8	1.5	75.2	1.5	70.6	1.5	77.6	1.5	73.0	1.5	68.4	1.5
74.4	1.5	79.1	1.5	83.7	1.5	72.2	1.5	76.8	1.5	81.4	1.5	69.9	1.5	74.5	1.5	79.1	1.5
63.5	1.2	63.5	1.2	63.5	1.2	62.0	1.2	62.0	1.2	62.0	1.2	60.4	1.2	60.4	1.2	60.4	1.2
67.1	1.2	67.1	1.2	67.1	1.2	66.0	1.2	66.0	1.2	66.0	1.2	64.9	1.2	64.9	1.2	64.9	1.2
70.1	1.5	65.5	1.5	60.9	1.5	68.8	1.5	64.2	1.5	59.6	1.5	67.4	1.5	62.8	1.5	58.2	1.5

Palo19		Palo20		Palo21		Palo22		Palo23		Palo24		Palo25		Palo26		Palo27	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
62.6	1.5	67.2	1.5	71.8	1.5	61.1	1.5	65.7	1.5	70.4	1.5	59.7	1.5	64.3	1.5	68.9	1.5
59.9	2.0	59.9	2.0	59.9	2.0	58.4	2.0	58.4	2.0	58.4	2.0	56.8	2.0	56.8	2.0	56.8	2.0
65.8	2.0	65.8	2.0	65.8	2.0	65.0	2.0	65.0	2.0	65.0	2.0	64.3	2.0	64.3	2.0	64.3	2.0
70.9	2.4	63.2	2.4	55.5	2.4	69.7	2.4	62.0	2.4	54.4	2.4	68.6	2.4	60.9	2.4	53.2	2.4
58.4	2.4	66.0	2.4	73.7	2.4	57.0	2.4	64.7	2.4	72.4	2.4	55.6	2.4	63.3	2.4	71.0	2.4
62.3	1.2	62.3	1.2	62.3	1.2	60.9	1.2	60.9	1.2	60.9	1.2	59.4	1.2	59.4	1.2	59.4	1.2
65.9	1.2	65.9	1.2	65.9	1.2	64.9	1.2	64.9	1.2	64.9	1.2	63.9	1.2	63.9	1.2	63.9	1.2
68.9	1.5	64.3	1.5	59.7	1.5	67.7	1.5	63.1	1.5	58.5	1.5	66.4	1.5	61.8	1.5	57.2	1.5
61.4	1.5	66.0	1.5	70.6	1.5	60.1	1.5	64.7	1.5	69.3	1.5	58.7	1.5	63.3	1.5	67.9	1.5
48.7	0.0	48.7	0.0	48.7	0.0	47.8	0.0	47.8	0.0	47.8	0.0	46.9	0.0	46.9	0.0	46.9	0.0
48.7	0.0	48.7	0.0	48.7	0.0	47.8	0.0	47.8	0.0	47.8	0.0	46.9	0.0	46.9	0.0	46.9	0.0
62.6	3.9	55.3	3.9	47.9	3.9	63.7	3.9	56.4	3.9	49.0	3.9	64.8	3.9	57.5	3.9	50.1	3.9
34.8	3.9	42.1	3.9	49.4	3.9	31.9	3.9	39.2	3.9	46.5	3.9	29.0	3.9	36.3	3.9	43.6	3.9
77.1	4.0	52.7	4.0	28.3	4.0	77.0	4.0	52.6	4.0	28.2	4.0	76.8	4.0	52.4	4.0	28.0	4.0
20.2	4.0	44.6	4.0	69.0	4.0	18.6	4.0	43.0	4.0	67.4	4.0	16.9	4.0	41.3	4.0	65.7	4.0
82.5	3.9	82.5	3.9	82.5	3.9	83.0	3.9	83.0	3.9	83.0	3.9	83.4	3.9	83.4	3.9	83.4	3.9
85.7	5.2	85.7	5.2	85.7	5.2	90.2	5.2	90.2	5.2	90.2	5.2	94.8	5.2	94.8	5.2	94.8	5.2
89.0	1.6	84.4	1.6	79.8	1.6	91.6	1.6	87.0	1.6	82.4	1.6	94.2	1.6	89.6	1.6	85.0	1.6
81.8	1.6	86.5	1.6	91.1	1.6	84.5	1.6	89.1	1.6	93.7	1.6	87.2	1.6	91.8	1.6	96.4	1.6
67.9	4.2	67.8	4.2	67.8	4.2	67.3	4.2	67.3	4.2	67.3	4.2	66.7	4.2	66.7	4.2	66.7	4.2
71.0	4.9	71.0	4.9	71.0	4.9	74.6	4.9	74.6	4.9	74.6	4.9	78.1	4.9	78.1	4.9	78.1	4.9
74.4	1.5	69.8	1.5	65.2	1.5	76.0	1.5	71.3	1.5	66.7	1.5	77.5	1.5	72.9	1.5	68.3	1.5
67.2	1.5	71.8	1.5	76.4	1.5	68.9	1.5	73.5	1.5	78.1	1.5	70.5	1.5	75.1	1.5	79.7	1.5
63.8	7.3	63.8	7.3	63.8	7.3	61.7	7.3	61.7	7.3	61.7	7.3	59.5	7.3	59.5	7.3	59.5	7.3
69.1	7.8	69.1	7.8	69.1	7.8	73.8	7.8	73.8	7.8	73.8	7.8	78.4	7.8	78.4	7.8	78.4	7.8
74.7	2.5	67.0	2.5	59.3	2.5	76.1	2.5	68.4	2.5	60.7	2.5	77.5	2.5	69.8	2.5	62.1	2.5
62.7	2.4	70.4	2.4	78.1	2.4	64.3	2.4	71.9	2.4	79.6	2.4	65.8	2.4	73.5	2.4	81.2	2.4
66.3	4.4	66.3	4.4	66.3	4.4	65.5	4.4	65.5	4.4	65.5	4.4	64.8	4.4	64.8	4.4	64.8	4.4
69.5	4.7	69.5	4.7	69.5	4.7	72.8	4.7	72.8	4.7	72.8	4.7	76.1	4.7	76.1	4.7	76.1	4.7
72.8	1.5	68.2	1.5	63.6	1.5	74.2	1.5	69.6	1.5	65.0	1.5	75.6	1.5	71.0	1.5	66.3	1.5
65.6	1.5	70.3	1.5	74.9	1.5	67.1	1.5	71.7	1.5	76.3	1.5	68.6	1.5	73.2	1.5	77.8	1.5
44.2	8.7	44.2	8.7	44.2	8.7	40.4	8.7	40.4	8.7	40.4	8.7	36.5	8.7	36.5	8.7	36.5	8.7
50.6	0.9	50.6	0.9	50.6	0.9	51.0	0.9	51.0	0.9	51.0	0.9	51.4	0.9	51.4	0.9	51.4	0.9
72.8	13.1	65.5	13.1	58.2	13.1	80.7	13.1	73.4	13.1	66.1	13.1	88.7	13.1	81.4	13.1	74.1	13.1
30.6	12.3	37.9	12.3	45.2	12.3	24.8	12.3	32.1	12.3	39.5	12.3	19.1	12.3	26.4	12.3	33.7	12.3
82.8	6.2	58.4	6.2	34.1	6.2	86.4	6.2	62.0	6.2	37.6	6.2	90.0	6.2	65.6	6.2	41.2	6.2
20.5	5.6	44.9	5.6	69.3	5.6	19.1	5.6	43.5	5.6	67.9	5.6	17.7	5.6	42.1	5.6	66.5	5.6
87.1	1.3	85.1	1.3	83.1	1.3	84.0	1.3	82.0	1.3	80.0	1.3	81.0	1.3	79.0	1.3	77.0	1.3
96.2	1.6	89.2	1.6	82.1	1.6	93.5	1.6	86.5	1.6	79.5	1.6	90.9	1.6	83.8	1.6	76.8	1.6
105.0	3.0	89.6	3.0	74.3	3.0	102.0	3.0	86.6	3.0	71.2	3.0	98.9	3.0	83.6	3.0	68.2	3.0
83.6	1.6	89.6	1.6	95.5	1.6	80.6	1.6	86.5	1.6	92.5	1.6	77.6	1.6	83.5	1.6	89.5	1.6

Palo19		Palo20		Palo21		Palo22		Palo23		Palo24		Palo25		Palo26		Palo27	
Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V	Q	V
[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]	[kN]
69.4	1.2	69.3	1.2	69.3	1.2	67.4	1.2	67.4	1.2	67.3	1.2	65.5	1.2	65.4	1.2	65.4	1.2
78.4	1.4	73.4	1.4	68.3	1.4	76.9	1.4	71.8	1.4	66.8	1.4	75.4	1.4	70.3	1.4	65.2	1.4
87.3	2.8	73.9	2.8	60.5	2.8	85.3	2.8	71.9	2.8	58.5	2.8	83.4	2.8	70.0	2.8	56.6	2.8
65.9	1.9	73.8	1.9	81.7	1.9	64.0	1.9	71.9	1.9	79.8	1.9	62.0	1.9	70.0	1.9	77.9	1.9
62.5	2.1	64.6	2.1	66.6	2.1	60.7	2.1	62.7	2.1	64.8	2.1	58.9	2.1	60.9	2.1	62.9	2.1
77.7	2.2	71.3	2.2	65.0	2.2	76.5	2.2	70.2	2.2	63.8	2.2	75.3	2.2	69.0	2.2	62.7	2.2
92.4	4.3	72.1	4.3	51.9	4.3	90.6	4.3	70.3	4.3	50.1	4.3	88.8	4.3	68.5	4.3	48.3	4.3
56.7	3.5	72.0	3.5	87.3	3.5	54.9	3.5	70.2	3.5	85.6	3.5	53.2	3.5	68.5	3.5	83.8	3.5
66.4	1.2	66.9	1.2	67.4	1.2	64.6	1.2	65.1	1.2	65.7	1.2	62.8	1.2	63.4	1.2	63.9	1.2
75.5	1.4	71.0	1.4	66.5	1.4	74.1	1.4	69.6	1.4	65.1	1.4	72.7	1.4	68.2	1.4	63.7	1.4
84.3	2.7	71.4	2.7	58.6	2.7	82.5	2.7	69.7	2.7	56.9	2.7	80.8	2.7	67.9	2.7	55.1	2.7
62.9	2.0	71.4	2.0	79.9	2.0	61.2	2.0	69.6	2.0	78.1	2.0	59.4	2.0	67.9	2.0	76.4	2.0
50.5	0.4	53.3	0.4	56.0	0.4	49.3	0.4	52.0	0.4	54.8	0.4	48.0	0.4	50.8	0.4	53.6	0.4
96.8	6.4	53.3	6.4	9.8	6.4	95.5	6.4	52.1	6.4	8.6	6.4	94.3	6.4	50.8	6.4	7.3	6.4
108.2	7.6	59.7	7.6	11.2	7.6	108.9	7.6	60.4	7.6	11.9	7.6	109.7	7.6	61.2	7.6	12.7	7.6
2.6	8.1	46.9	8.1	91.1	8.1	-0.6	8.1	43.7	8.1	87.9	8.1	-3.8	8.1	40.5	8.1	84.7	8.1
180.6	17.7	57.1	17.7	-66.3	17.7	180.1	17.7	56.6	17.7	-66.8	17.7	179.6	17.7	56.1	17.7	-67.3	17.7
-69.7	18.3	49.4	18.3	168.6	18.3	-71.7	18.3	47.5	18.3	166.7	18.3	-73.6	18.3	45.5	18.3	164.7	18.3
91.6	6.0	93.6	6.0	95.6	6.0	91.7	6.0	93.7	6.0	95.7	6.0	91.8	6.0	93.8	6.0	95.8	6.0
88.3	2.3	95.3	2.3	102.3	2.3	91.8	2.3	98.9	2.3	105.9	2.3	95.4	2.3	102.4	2.3	109.5	2.3
103.5	2.7	97.3	2.7	91.2	2.7	105.4	2.7	99.2	2.7	93.0	2.7	107.3	2.7	101.1	2.7	94.9	2.7
81.7	3.7	97.3	3.7	112.9	3.7	83.6	3.7	99.2	3.7	114.8	3.7	85.6	3.7	101.1	3.7	116.7	3.7
75.0	5.0	75.1	5.0	75.1	5.0	74.5	5.0	74.6	5.0	74.6	5.0	74.0	5.0	74.0	5.0	74.1	5.0
71.7	3.1	76.8	3.1	81.9	3.1	74.7	3.1	79.7	3.1	84.8	3.1	77.6	3.1	82.7	3.1	87.7	3.1
86.9	2.3	78.8	2.3	70.7	2.3	88.2	2.3	80.1	2.3	72.0	2.3	89.5	2.3	81.4	2.3	73.2	2.3
65.2	3.0	78.8	3.0	92.4	3.0	66.5	3.0	80.1	3.0	93.7	3.0	67.8	3.0	81.4	3.0	95.0	3.0
72.6	7.5	70.5	7.5	68.5	7.5	70.8	7.5	68.7	7.5	66.7	7.5	69.0	7.5	66.9	7.5	64.9	7.5
67.1	6.0	73.4	6.0	79.8	6.0	71.0	6.0	77.4	6.0	83.7	6.0	75.0	6.0	81.4	6.0	87.7	6.0
92.4	3.8	76.8	3.8	61.1	3.8	93.6	3.8	78.0	3.8	62.3	3.8	94.8	3.8	79.1	3.8	63.5	3.8
56.2	4.4	76.8	4.4	97.3	4.4	57.4	4.4	78.0	4.4	98.6	4.4	58.6	4.4	79.2	4.4	99.8	4.4
73.1	4.6	72.5	4.6	72.0	4.6	72.6	4.6	72.1	4.6	71.6	4.6	72.2	4.6	71.7	4.6	71.1	4.6
69.8	3.5	74.3	3.5	78.8	3.5	72.8	3.5	77.3	3.5	81.8	3.5	75.8	3.5	80.3	3.5	84.8	3.5
85.0	2.2	76.3	2.2	67.6	2.2	86.3	2.2	77.6	2.2	68.9	2.2	87.7	2.2	79.0	2.2	70.3	2.2
63.2	2.8	76.3	2.8	89.3	2.8	64.6	2.8	77.7	2.8	90.7	2.8	66.0	2.8	79.0	2.8	92.1	2.8
24.2	115.1	21.4	115.1	18.6	115.1	1.6	115.1	-1.2	115.1	-3.9	115.1	-21.0	115.1	-23.8	115.1	-26.5	115.1
169.3	43.6	56.1	43.6	-57.2	43.6	169.9	43.6	56.6	43.6	-56.7	43.6	170.4	43.6	57.2	43.6	-56.1	43.6
112.5	10.6	65.9	10.6	19.3	10.6	117.4	10.6	70.8	10.6	24.2	10.6	122.3	10.6	75.7	10.6	29.1	10.6
-4.3	11.7	46.5	11.7	97.4	11.7	-7.9	11.7	43.0	11.7	93.9	11.7	-11.4	11.7	39.5	11.7	90.4	11.7
180.8	18.9	61.6	18.9	-57.7	18.9	183.0	18.9	63.7	18.9	-55.5	18.9	185.2	18.9	65.9	18.9	-53.4	18.9
-72.6	18.6	50.9	18.6	174.4	18.6	-73.4	18.6	50.1	18.6	173.6	18.6	-74.3	18.6	49.3	18.6	172.8	18.6

Palo28		Palo29		Palo30	
Q [kN]	V [kN]	Q [kN]	V [kN]	Q [kN]	V [kN]
68.2	1.2	68.2	1.2	68.2	1.2
73.1	1.2	73.1	1.2	73.1	1.2
75.5	1.5	70.8	1.5	66.2	1.5
67.6	1.5	72.2	1.5	76.8	1.5
58.9	1.2	58.9	1.2	58.9	1.2
63.8	1.2	63.8	1.2	63.8	1.2
66.1	1.5	61.5	1.5	56.9	1.5
58.2	1.5	62.8	1.5	67.5	1.5
55.3	2.0	55.3	2.0	55.3	2.0
63.5	2.0	63.5	2.0	63.5	2.0
67.4	2.4	59.7	2.4	52.0	2.4
54.3	2.4	61.9	2.4	69.6	2.4
58.0	1.2	58.0	1.2	58.0	1.2
62.9	1.2	62.9	1.2	62.9	1.2
65.2	1.5	60.6	1.5	56.0	1.5
57.3	1.5	61.9	1.5	66.5	1.5
46.0	0.0	46.0	0.0	46.0	0.0
46.0	0.0	46.0	0.0	46.0	0.0
65.9	3.9	58.5	3.9	51.2	3.9
26.1	3.9	33.4	3.9	40.7	3.9
76.6	4.0	52.3	4.0	27.9	4.0
15.3	4.0	39.7	4.0	64.1	4.0
83.9	3.9	83.9	3.9	83.9	3.9
99.3	5.2	99.3	5.2	99.3	5.2
96.7	1.6	92.1	1.6	87.5	1.6
89.8	1.6	94.4	1.6	99.0	1.6
66.2	4.2	66.2	4.2	66.2	4.2
81.6	4.9	81.6	4.9	81.6	4.9
79.1	1.5	74.4	1.5	69.8	1.5
72.1	1.5	76.8	1.5	81.4	1.5
57.4	7.3	57.4	7.3	57.4	7.3
83.1	7.8	83.1	7.8	83.1	7.8
78.9	2.5	71.2	2.5	63.5	2.5
67.3	2.4	75.0	2.4	82.7	2.4
64.1	4.4	64.1	4.4	64.1	4.4
79.5	4.7	79.5	4.7	79.5	4.7
76.9	1.5	72.3	1.5	67.7	1.5
70.0	1.5	74.6	1.5	79.2	1.5
32.7	8.7	32.7	8.7	32.7	8.7
51.8	0.9	51.8	0.9	51.8	0.9
96.6	13.1	89.3	13.1	82.0	13.1

Palo28		Palo29		Palo30	
Q [kN]	V [kN]	Q [kN]	V [kN]	Q [kN]	V [kN]
13.3	12.3	20.6	12.3	28.0	12.3
93.6	6.2	69.2	6.2	44.8	6.2
16.4	5.6	40.8	5.6	65.1	5.6
77.9	1.3	75.9	1.3	73.9	1.3
88.2	1.6	81.2	1.6	74.1	1.6
95.9	3.0	80.5	3.0	65.2	3.0
74.5	1.6	80.5	1.6	86.4	1.6
63.5	1.2	63.5	1.2	63.4	1.2
73.8	1.4	68.8	1.4	63.7	1.4
81.5	2.8	68.1	2.8	54.7	2.8
60.1	1.9	68.0	1.9	76.0	1.9
57.0	2.1	59.1	2.1	61.1	2.1
74.2	2.2	67.8	2.2	61.5	2.2
87.0	4.3	66.7	4.3	46.5	4.3
51.4	3.5	66.7	3.5	82.0	3.5
61.1	1.2	61.6	1.2	62.1	1.2
71.4	1.4	66.9	1.4	62.4	1.4
79.0	2.7	66.2	2.7	53.4	2.7
57.7	2.0	66.1	2.0	74.6	2.0
46.8	0.4	49.6	0.4	52.3	0.4
93.1	6.4	49.6	6.4	6.1	6.4
110.5	7.6	61.9	7.6	13.4	7.6
-7.0	8.1	37.3	8.1	81.5	8.1
179.1	17.7	55.6	17.7	-67.8	17.7
-75.6	18.3	43.6	18.3	162.8	18.3
91.8	6.0	93.9	6.0	95.9	6.0
98.9	2.3	106.0	2.3	113.0	2.3
109.1	2.7	103.0	2.7	96.8	2.7
87.5	3.7	103.1	3.7	118.7	3.7
73.5	5.0	73.5	5.0	73.5	5.0
80.6	3.1	85.6	3.1	90.7	3.1
90.8	2.3	82.6	2.3	74.5	2.3
69.1	3.0	82.7	3.0	96.3	3.0
67.1	7.5	65.1	7.5	63.1	7.5
79.0	6.0	85.3	6.0	91.7	6.0
96.0	3.8	80.3	3.8	64.7	3.8
59.9	4.4	80.5	4.4	101.1	4.4
71.7	4.6	71.2	4.6	70.7	4.6
78.8	3.5	83.3	3.5	87.8	3.5
89.0	2.2	80.3	2.2	71.6	2.2
67.4	2.8	80.4	2.8	93.5	2.8



Palo28		Palo29		Palo30	
Q [kN]	V [kN]	Q [kN]	V [kN]	Q [kN]	V [kN]
-43.6	115.1	-46.3	115.1	-49.1	115.1
171.0	43.6	57.7	43.6	-55.6	43.6
127.1	10.6	80.5	10.6	33.9	10.6
-14.9	11.7	36.0	11.7	86.9	11.7
187.3	18.9	68.1	18.9	-51.2	18.9
-75.1	18.6	48.4	18.6	172.0	18.6

Per ogni combinazione di calcolo e per ogni palo, sono state valutate le sollecitazioni massime e minime agenti. Nella tabella seguente sono riportati detti valori su ogni palo e la combinazione corrispondente.

Palo	Combinazione	Q <sub>MAX</sub> [kN]	T [kN]	M [kN m]
1	SLVy (q=1)	183.6	17.7	-20.0
2	SLU_URTO X	156.9	115.1	-130.2
3	SLVy (q=1)	180.3	18.3	-20.8
4	SLVy (q=1)	183.1	17.7	-20.0
5	SLU_URTO X	134.3	115.1	-130.2
6	SLVy (q=1)	178.6	18.6	-21.1
7	SLVy (q=1)	182.6	17.7	-20.0
8	SLU_URTO X	111.7	115.1	-130.2
9	SLVy (q=1)	177.7	18.6	-21.1
10	SLVy (q=1)	182.1	17.7	-20.0
11	SLU (q3)	98.8	3.0	-3.4
12	SLVy (q=1)	176.9	18.6	-21.1
13	SLVy (q=1)	181.6	17.7	-20.0
14	SLU (q3)	95.7	3.0	-3.4
15	SLVy (q=1)	176.1	18.6	-21.1
16	SLVy (q=1)	181.1	17.7	-20.0
17	SLU (q3)	95.4	2.7	-3.1
18	SLVy (q=1)	175.3	18.6	-21.1
19	SLVy (q=1)	180.8	18.9	-21.4
20	SLU (q3)	97.3	2.7	-3.1
21	SLVy (q=1)	174.4	18.6	-21.1
22	SLVy (q=1)	183.0	18.9	-21.4
23	SLU (q4)	99.2	3.7	-4.2
24	SLVy (q=1)	173.6	18.6	-21.1
25	SLVy (q=1)	185.2	18.9	-21.4
26	SLU (q2)	102.4	2.3	-2.6
27	SLVy (q=1)	172.8	18.6	-21.1
28	SLVy (q=1)	187.3	18.9	-21.4
29	SLU (q2)	106.0	2.3	-2.6
30	SLVy (q=1)	172.0	18.6	-21.1

Palo	Combinazione	$Q_{MIN}$ [kN]	T [kN]	M [kN m]
1	SLVy (q=1)	-67.7	18.6	-21.1
2	SLVx (q=1)	17.8	13.1	-14.8
3	SLVy (q=1)	-70.7	18.9	-21.4
4	SLVy (q=1)	-68.5	18.6	-21.1
5	SLVx (q=1)	25.7	13.1	-14.8
6	SLVy (q=1)	-68.5	18.9	-21.4
7	SLVy (q=1)	-69.3	18.6	-21.1
8	SLVx (q=1)	33.7	13.1	-14.8
9	SLVy (q=1)	-66.4	18.9	-21.4
10	SLVy (q=1)	-70.1	18.6	-21.1
11	SLVx (q=1)	41.6	13.1	-14.8
12	SLVy (q=1)	-64.8	17.7	-20.0
13	SLVy (q=1)	-71.0	18.6	-21.1
14	SLVy (q=1)	47.7	5.6	-6.4
15	SLVy (q=1)	-65.3	17.7	-20.0
16	SLVy (q=1)	-71.8	18.6	-21.1
17	SLVx (q=1)	43.6	12.3	-13.9
18	SLVy (q=1)	-65.8	17.7	-20.0
19	SLVy (q=1)	-72.6	18.6	-21.1
20	SLU_URTO X	21.4	115.1	-130.2
21	SLVy (q=1)	-66.3	17.7	-20.0
22	SLVy (q=1)	-73.4	18.6	-21.1
23	SLU_URTO X	-1.2	115.1	-130.2
24	SLVy (q=1)	-66.8	17.7	-20.0
25	SLVy (q=1)	-74.3	18.6	-21.1
26	SLU_URTO X	-23.8	115.1	-130.2
27	SLVy (q=1)	-67.3	17.7	-20.0
28	SLVy (q=1)	-75.6	18.3	-20.8
29	SLU_URTO X	-46.3	115.1	-130.2
30	SLVy (q=1)	-67.8	17.7	-20.0

## Dimensionamento delle armature

Diametro = 600 (mm)

Raggio = 300 (mm)

Sforzo Normale = 21 (kN)

### Caratteristiche dei Materiali

calcestruzzo

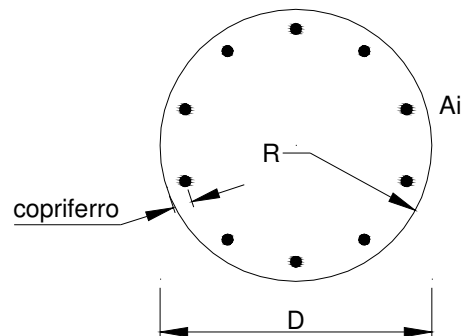
Rck = 30 (Mpa)

fck = 25 (Mpa)

$\gamma_c$  = 1.5

$\alpha_{cc}$  = 0.85

$f_{cd} = \alpha_{cc} f_{ck} / \gamma_c = 14.17$  (Mpa)



### Acciaio

tipo di acciaio

fyk = 450 (Mpa)

$\gamma_s$  = 1.15

$f_{yd} = f_{yk} / \gamma_s = 391.3$  (Mpa)

Es = 206000 (Mpa)

$\epsilon_{ys}$  = 0.190%

$\epsilon_{uk}$  = 10.000%

### Armature

numero	diametro (mm)	area (mm <sup>2</sup> )	copriferro (mm)
24	$\phi$ 22	9123	60
0	$\phi$ 0	0	120
0	$\phi$ 0	0	30

Calcolo

### Momento di Plasticizzazione

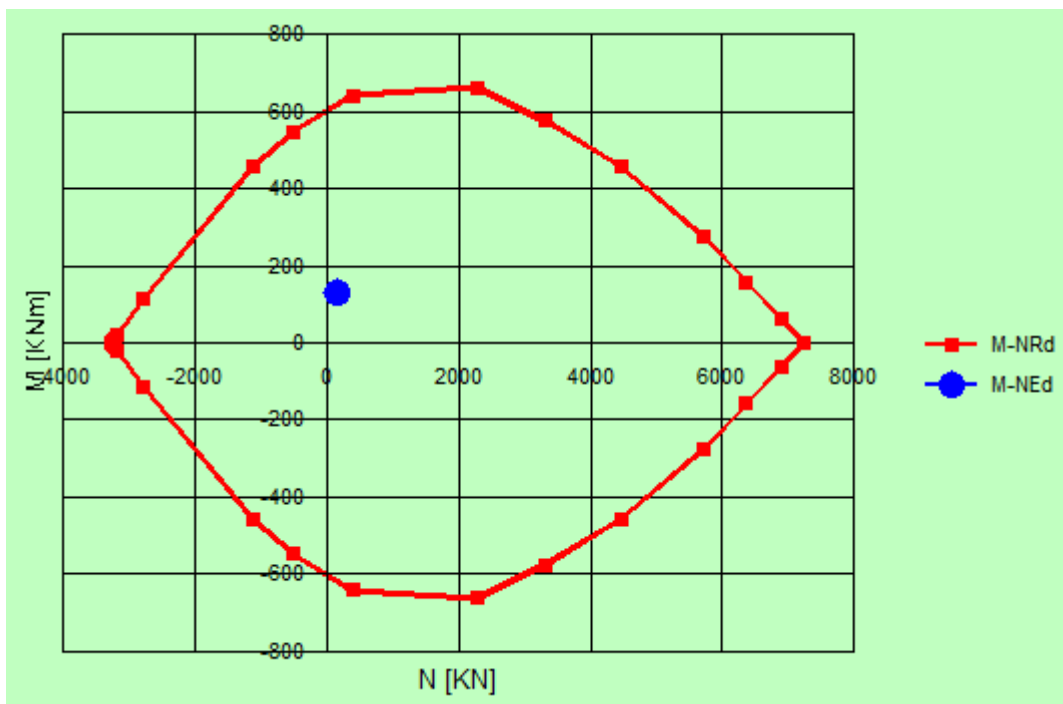
My = 660.9 (kN m)

Inserisci

### 9.3 Verifiche a pressoflessione sui Pali

Si riportano di seguito le sollecitazioni adottate per il calcolo strutturale dei pali e le verifiche a pressoflessione eseguite tramite l'applicativo VcaSlu.

Palo	Combinazione	Q [kN]	M [kN m]
2	SLU_URTO X	156.9	-130.2



*Relazione di calcolo strutturale  
fondazioni pile ponte pedonale*

COMMESSA  
RS3Z

LOTTO  
00

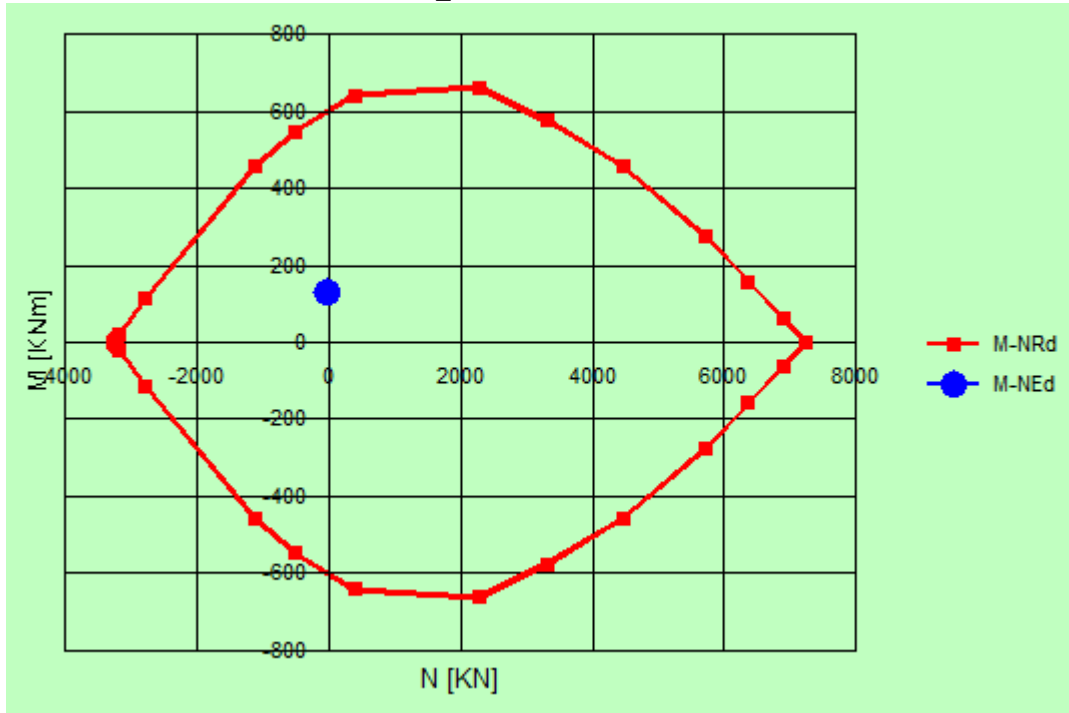
FASE-ENTE  
D 26

DOCUMENTO  
CLFV0300009

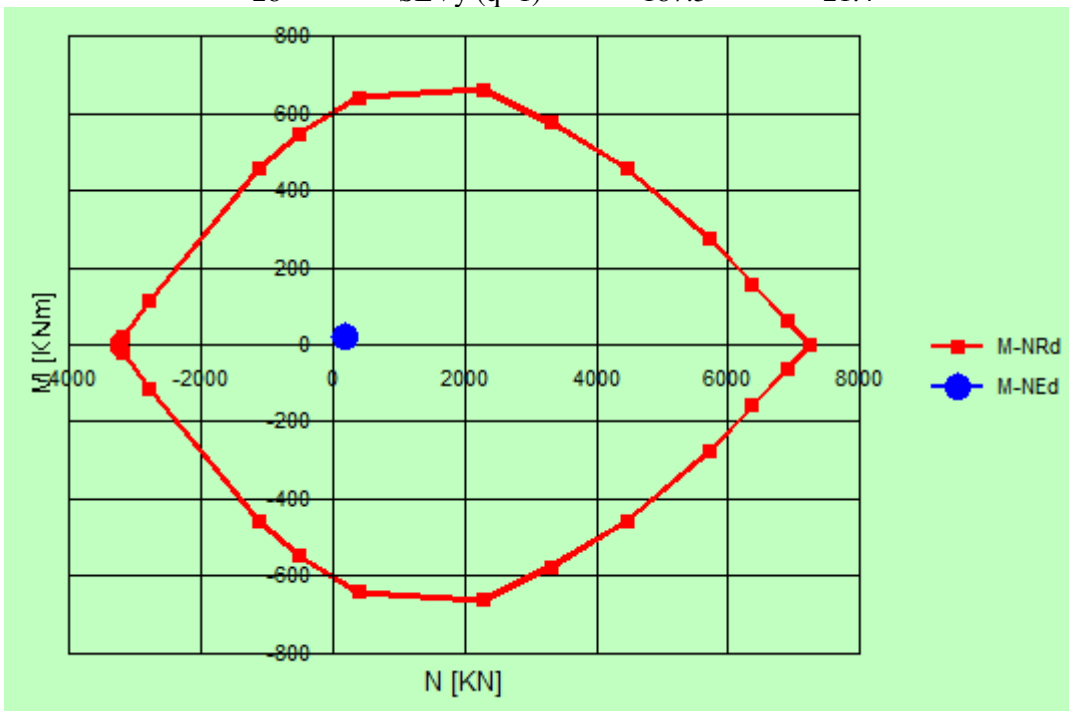
REV.  
B

FOGLIO  
27 di 34

Palo 29      Combinazione SLU\_URTO X      Q [kN] -46.3      M [kN m] -130.2



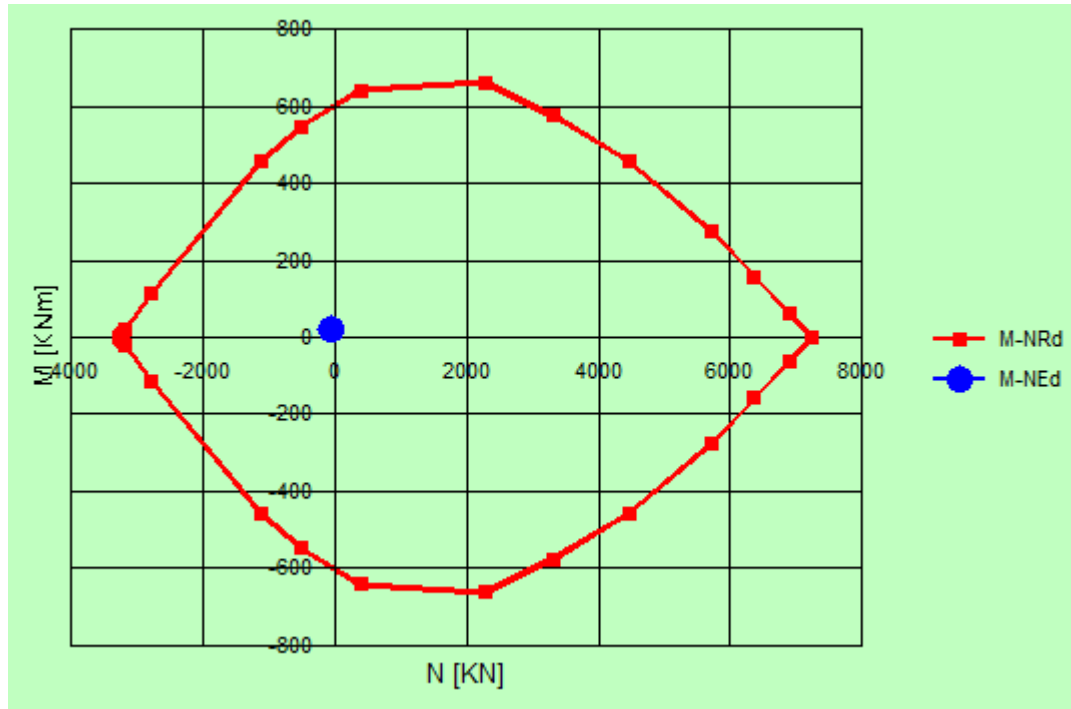
Palo 28      Combinazione SLV<sub>y</sub> (q=1)      Q [kN] 187.3      M [kN m] -21.4



*Relazione di calcolo strutturale  
fondazioni pile ponte pedonale*

COMMESSA	LOTTO	FASE-ENTE	DOCUMENTO	REV.	FOGLIO
RS3Z	00	D 26	CLFV0300009	B	28 di 34

Palo	Combinazione	Q [kN]	M [kN m]
28	SLVy (q=1)	-75.6	-20.8



**Verifiche a taglio SLU sui pali**

$V_{Ed} = T_{SLU}$	115.1	kN
$V_{Ed} = T_{SLU}$	115100	N
$\phi$	12	mm
$A_{\phi}$	113.0973	mm <sup>2</sup>
bracci	2	-
$A_{sw}$	226.1947	mm <sup>2</sup>
s	200	mm
$f_{ywd}$	391.3043	MPa
$\cot \theta$	1	-
$\alpha_c$	1	-
$z = 0.9d$	394.3318	mm
v	0.54024	-
$V_{Rd,s}$	174513.4	N
$V_{Rd,s \max}$	894298.4	N
$V_{Rd,c \text{ effettivo}}$	174513.4	N
<b>Verifica</b>	<b>OK</b>	
T.S.	0.6595	
C.S.	1.51619	

**La verifica a taglio risulta soddisfatta per armatura fi 12 con passo 200 mm.**

#### 9.4 Verifiche Strutturali sulla platea di fondazione

In base alle azioni di calcolo riportate nei paragrafi precedenti, è stata eseguita la verifica della platea assumendo l'ipotesi di mensola tozza.

##### Direzione lunga

Dimensioni mensola		
hc	1.2	m
b	4.8	m
copriferro netto	0.055	m
ac	1.2	m
d	1.125	m

Azione di calcolo		
Ped	474.56	kN

l	1425.00	[mm]	Armatura verticale posizionata			
$\lambda$	1.41	[mm]	$\Phi$	n	As (mm <sup>2</sup> )	
P <sub>Rs</sub>	2096.31	TS	0.86	20	24	7539.822
c	1.5					
P <sub>Rc</sub>	21558.00	check	OK			

AICAP pag286 se ac>hc/2		
Verifica meccanismo	ac>hc/2	Si
z	0.900	m
(6.60 EC2)		
$\sigma_{Rd2}$	16.46	Mpa
$\sigma_{Rd1}$	13.99	Mpa
x2	0.01	m
a	1.20	m
Ft	634.33	kN
As estradosso	1621.07	mm <sup>2</sup>
Verifica ferri estradosso	<b>Si</b>	
Fwd	264.70	kN
As staffe vert	676.46	mm <sup>2</sup>

Armatura orizzontale posizionata		
$\Phi$	n	As (mm <sup>2</sup> )
20	24	7539.82
0	0	0
0	0	0
As tot (mm <sup>2</sup> )		7539.82

Armatura verticale posizionata			
$\Phi$	n	n bracci	As (mm <sup>2</sup> )
20	7	2	4398.23
			0



Relazione di calcolo strutturale  
fondazioni pile ponte pedonale

COMMESSA	LOTTO	FASE-ENTE	DOCUMENTO	REV.	FOGLIO
RS3Z	00	D 26	CLFV0300009	B	31 di 34

Verifica staffe vert	<b>Si</b>	0	0	0	0
				As tot (mm2)	4398.23
y2	0.23	m			
$\sigma_2$	0.29	MPa			
Verifica nodo 2	<b>Si</b>	<b>0.02</b>	Limitazione armatura		
				As staffe > 0.5 As	<b>Si</b>
$\sigma_1$	0.26	MPa			
Verifica nodo 1	<b>Si</b>	<b>0.08</b>			

**Direzione corta**

Dimensioni mensola		
hc	1.2	m
b	17.4	m
copriferro netto	0.055	m
ac	1.2	m
d	1.123	m

Azione di calcolo		
Ped	1807.63	kN

l	1424.60	[mm]	Armatura verticale posizionata		
$\lambda$	1.41	[mm]	$\Phi$	n	As (mm2)
P <sub>Rs</sub>	3265.35	TS	<b>24</b>	<b>26</b>	7539.822
c	1.5				
P <sub>Rc</sub>	77853.54	check	<b>OK</b>		

AICAP pag286 se ac>hc/2					
Verifica meccanismo	ac>hc/2	<b>Si</b>			
z	0.898	m	Armatura orizzontale posizionata		
(6.60 EC2)			$\Phi$	n	As (mm2)
$\sigma_{Rd2}$	16.46	Mpa	<b>20</b>	<b>87</b>	27331.86
$\sigma_{Rd1}$	13.99	Mpa	0	0	0
x2	0.01	m	0	0	0
a	1.20	m			
Ft	2420.81	kN	As tot (mm2)		27331.86

As estradosso	6186.53	mm <sup>2</sup>
Verifica ferri estradosso	<b>Si</b>	
Fwd	1011.33	kN
As staffe vert	2584.52	mm <sup>2</sup>
Verifica staffe vert	<b>Si</b>	
y <sub>2</sub>	0.22	m
σ <sub>2</sub>	0.31	MPa
Verifica nodo 2	<b>Si</b>	
σ <sub>1</sub>	0.30	MPa
Verifica nodo 1	<b>Si</b>	

**0.02**

**0.02**

Armatura verticale posizionata			
Φ	n	n bracci	As (mm <sup>2</sup> )
20	7	2	4398.23
			0
0	0	0	0
As tot (mm <sup>2</sup> )			4398.23

Limitazione armatura	
As staffe > 0.5 As	<b>Si</b>