

S.G.C. E78 GROSSETO - FANO

Tratto Selci Lama (E45) - S. Stefano di Gaifa.
Adeguamento a 2 corsie del tratto della Variante di Urbania

PROGETTO DEFINITIVO

ANAS - DIREZIONE PROGETTAZIONE E REALIZZAZIONE LAVORI

| | | |
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OPERE D'ARTE MAGGIORI

Gallerie

Elaborati generali

Relazione di calcolo galleria artificiale

| CODICE PROGETTO | | | NOME FILE | REVISIONE | SCALA |
|-----------------|-------------|------|-----------------------------|-----------|------------|
| PROGETTO | LIV.PROG. | ANNO | T00GA00OSTRE01_A | | |
| DPAN247 | D | 22 | CODICE ELAB. T00GA00OSTRE01 | A | - |
| D | | | | | |
| C | | | | | |
| B | | | | | |
| A | Emissione | | Ottobre '21 | Ragnacci | Panfilì |
| REV. | DESCRIZIONE | | DATA | REDATTO | VERIFICATO |
| | | | | | APPROVATO |

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1. PREMESSA

La presente opera rientra nell'ambito del Progetto Definitivo del 7° lotto della E78 Grosseto Fano tronco Selci Lama - S.Stefano di Gaifa

La presente relazione tecnica e di calcolo, tratta l'analisi e le verifiche del tratto di galleria artificiale e dei muri di prolungamento di essa per gli imbocchi delle gallerie "Il Monte", "Urbania 1", "Urbania 2" e "Urbania 3".

Per ogni imbocco la galleria è caratterizzata da un giunto strutturale atto a separare la galleria dai muri d'invito. Quest'ultimo presenta altezza variabile con lo sviluppo in modo da garantire una certa continuità architettonica dell'imbocco.

L'analisi della galleria artificiale si ritiene valida per tutti gli imbocchi in quanto tutte le gallerie artificiali, nella sezione più sfavorevole poggiano sullo stesso tipo di roccia. Verranno tuttavia prese in considerazione le due condizioni di ricoprimento peggiori.

Per il muro d'invito verranno considerati due casi: tratto di muro con massima altezza e muro poggiate sul terreno con le caratteristiche più scadenti.

Vengono riportate nel seguito le analisi statiche e pseudo-statiche condotte e le relative verifiche ai fini del rispetto delle normative vigenti. Tali verifiche sono state condotte secondo quanto previsto dalla Normativa vigente sia agli stati limite ultimi che di esercizio.

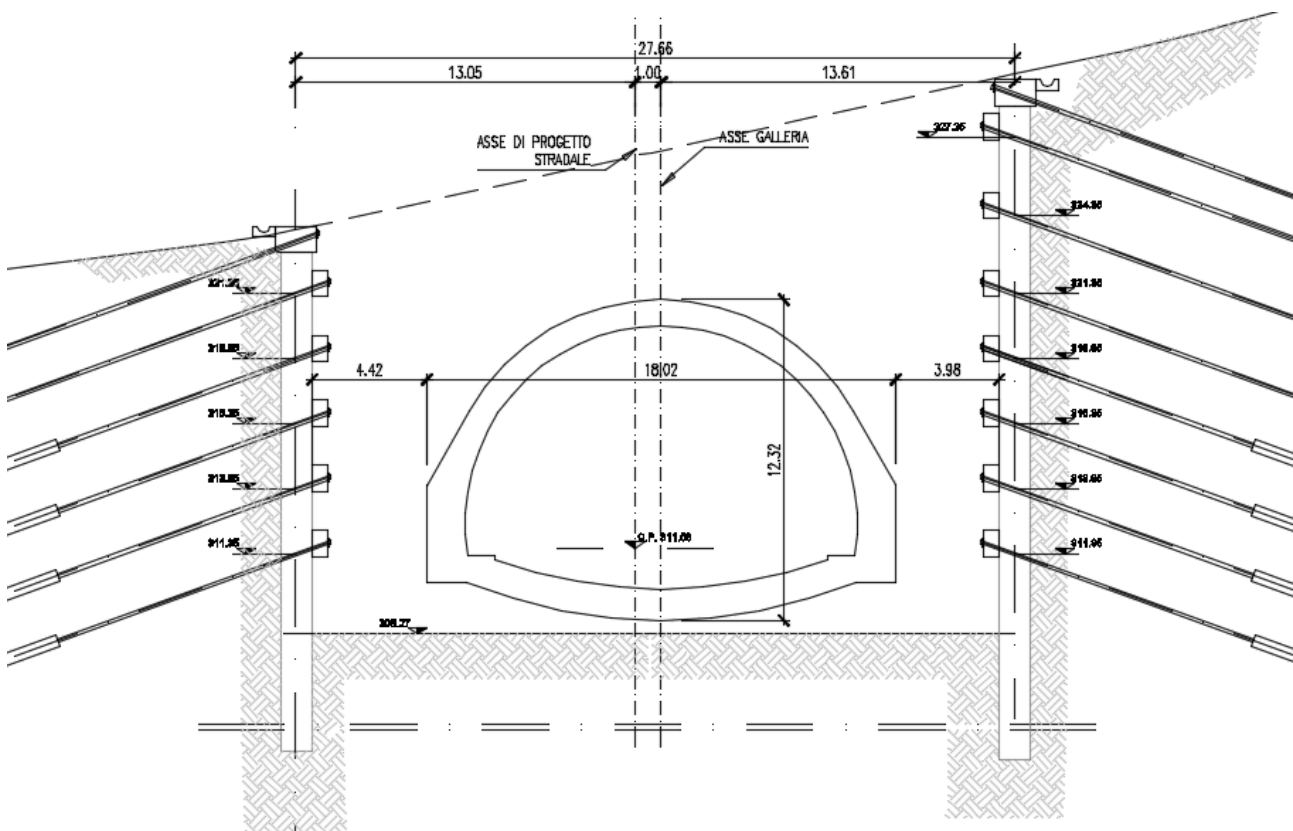


Figura 1.1 Sezione tipo galleria artificiale

PROGETTAZIONE ATI:

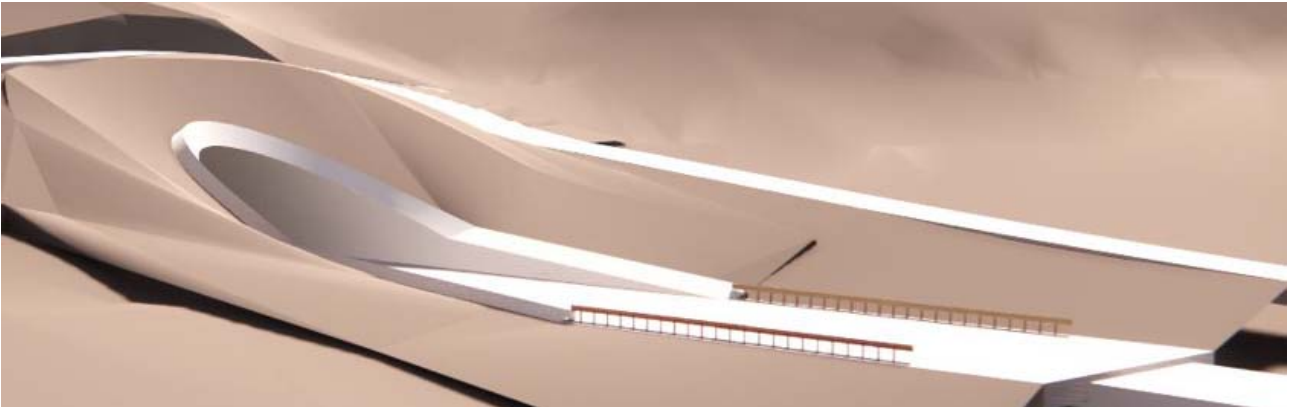


Figura 1.2 Rappresentazione imbocco galleria

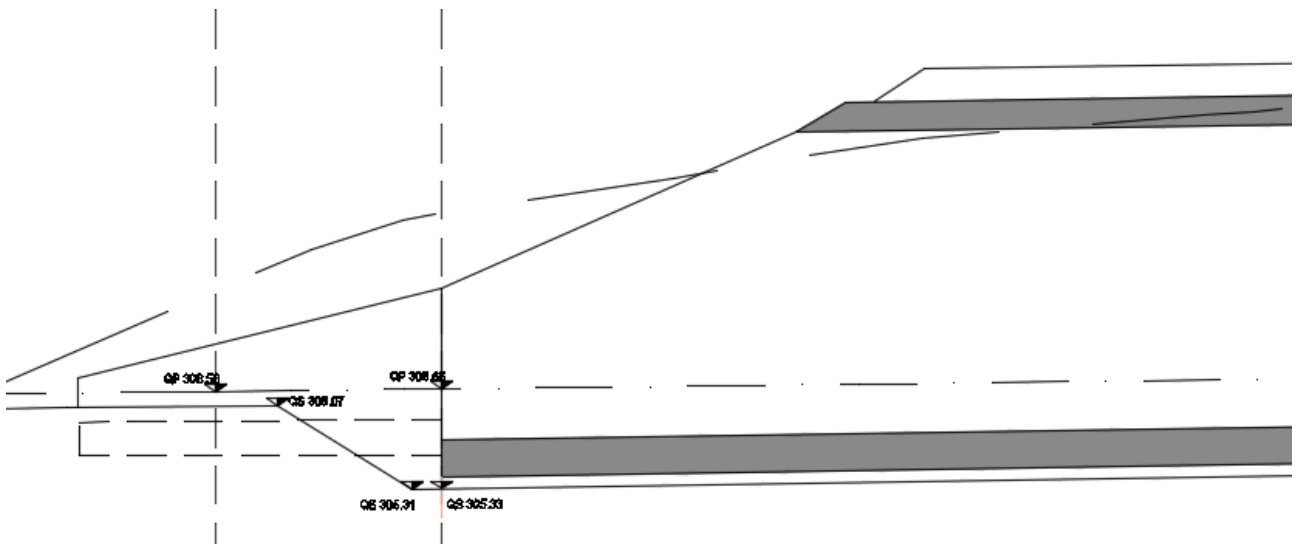


Figura 1.3 Profilo imbocco galleria

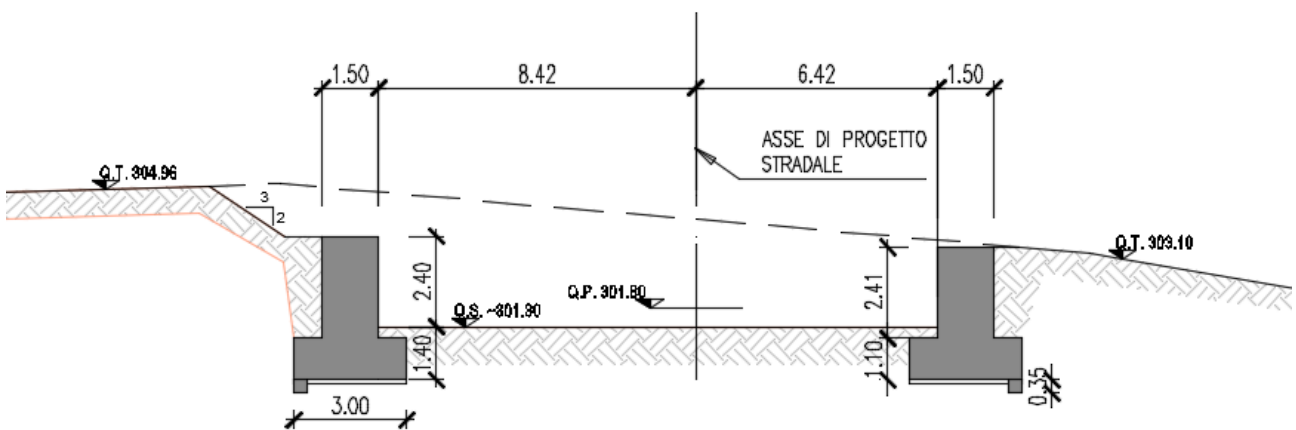


Figura 1.4 Sezione tipo muri d'invito

PROGETTAZIONE ATI:

2. NORMATIVA DI RIFERIMENTO

- [1] Decreto Ministero delle Infrastrutture e Trasporti 17/01/2018, Aggiornamento delle “Norme tecniche per le costruzioni”;
- [2] Circolare del 21/01/2019 n.7, “Istruzioni per l’applicazione dell’«Aggiornamento delle “Norme tecniche per le costruzioni”» di cui al decreto ministeriale 17 gennaio 2018”.
- [3] UNI EN 1992-1-1 EUROCODICE 2- Progettazione delle strutture in calcestruzzo armato - Parte 1-1: Regole generali e regole per gli edifici
- [4] UNI EN 1997-1: EUROCODICE 7 – Progettazione Geotecnica – Parte 1: Regole Generali
- [5] UNI EN 1998-5 EUROCODICE 8: Progettazione delle strutture per la resistenza sismica – Parte 5 - Fondazioni, strutture di contenimento ed aspetti geotecnici;

PROGETTAZIONE ATI:

3. CONDIZIONI GEOLOGICHE E GEOTECNICHE

3.1. INQUADRAMENTO GEOLOGICO E IDROGEOLOGICO GALLERIA

A causa della notevole variabilità della profondità del substrato roccioso e dell'altrettanto rilevante sviluppo longitudinale dell'opera, nelle analisi sono state considerate le due sezioni con le condizioni più sfavorevoli, ovvero quella avente il massimo spessore uniforme (progressiva Km 0+737.85) con uno spessore di ricoprimento in calotta di 4.5m, e quella con il ricoprimento asimmetrico peggiore (progressiva km 1+800) con ricoprimento, rispetto al livello della chiave dell'arco superiore, di 2.5m su un piedritto e di 8.5 m per l'altro.

Si considera un materiale di riempimento di tipo granulometrico con caratteristiche meccaniche riportate nel paragrafo 3.3; il letto di fondazione invece risulta composto da un substrato Marnoso Arenaceo le cui caratteristiche sono state rilevate dal profilo geotecnico a cui si rimanda

La falda di progetto mostra un affondamento minimo di 3.6m. A favore di sicurezza si considera una falda di progetto con una profondità di 2.6m da piano campagna.

3.2. INQUADRAMENTO GEOLOGICO E IDROGEOLOGICO MURO

A causa della notevole variabilità dello sviluppo longitudinale dell'opera, nelle analisi sono state considerate le due sezioni con le condizioni più sfavorevoli, ovvero quella avente la massima altezza e quella in cui la fondazione poggia sullo strato più scadente.

Si considera un materiale di riempimento di tipo granulometrico con caratteristiche meccaniche riportate nel paragrafo 3.4; il letto di fondazione invece risulta, per il muro con altezza maggiore, composto da un terreno con granulometria sottile, mentre quello più scadente risulta quello componente il corpo di frana.

La presenza di un materiale di riporto con permeabilità molto alta permette di trascurare la spinta dell'acqua a tergo del muro e per questo si considera la falda coincidente con il piano di fondazione.

3.3. STRATIGRAFIA DI PROGETTO GALLERIA

Di seguito si riportano i valori caratteristici dei terreni presenti in sito, utilizzati per le successive analisi della galleria:

| Descrizione | Unità | γ_{sat} [kN/m ³] | ϕ' [°] | c' [kPa] | C_u [kPa] | E_{medio} [MPa] | z |
|----------------------------|-------|--|----------------|---------------|----------------|----------------------|------------------|
| Materiale di riempimento | R | 22 | 35 | 0 | 0 | 45 | 0 m-fondo scavo |
| Substrato marnoso-arenaceo | SUB | 23 | 30 | 27 | 300 | 500 | Fondo scavo-50 m |

Si riporta nel seguito una sintesi della parametrizzazione geotecnica utilizzata per la definizione del quadro geomeccanico che caratterizza le analisi condotte per le gallerie artificiali oggetto della presente relazione.

PROGETTAZIONE ATI:

- Piedritti (formulazione Bowles-Winkler) $K_h = 49450 \text{ kN/m}^3$
- Arco inferiore (formulazione Galerkin - R=19m) $K_v = 20242.91 \text{ kN/m}^3$
- Arco superiore (formulazione Galerkin) $K_v = 6315 \text{ kN/m}^3$

3.4. STRATIGRAFIA DI PROGETTO MURO D'INVITO

Di seguito si riportano i valori caratteristici dei terreni presenti in sito, utilizzati per le analisi del muro d'invito con la massima altezza.

| Descrizione | Unità | γ_{sat} [kN/m ³] | ϕ' [°] | c' [kPa] | C_u [kPa] | E_{medio} [MPa] | z |
|----------------------------|-------|--|----------------|---------------|----------------|----------------------|-----------------|
| Materiale di riempimento | R | 20 | 35 | 0 | 0 | 45 | 0 m-fondo scavo |
| Depositi eluvio colluviali | E/C | 19 | 23 | 10 | 100 | 12.5 | Fondo scavo |

Per il muro poggiate sullo strato di terreno più scadente invece le caratteristiche del terreno risultano:

| Descrizione | Unità | γ_{sat} [kN/m ³] | ϕ' [°] | c' [kPa] | C_u [kPa] | E_{medio} [MPa] | z |
|--------------------------|-------|--|----------------|---------------|----------------|----------------------|-----------------|
| Materiale di riempimento | R | 20 | 35 | 0 | 0 | 45 | 0 m-fondo scavo |
| Corpo di Frana | CdF | 18 | 18 | 0 | 80 | 10 | Fondo scavo |

I valori considerati per gli angoli d'attrito sono i valori medi risultanti dalle prove eseguite in laboratorio.

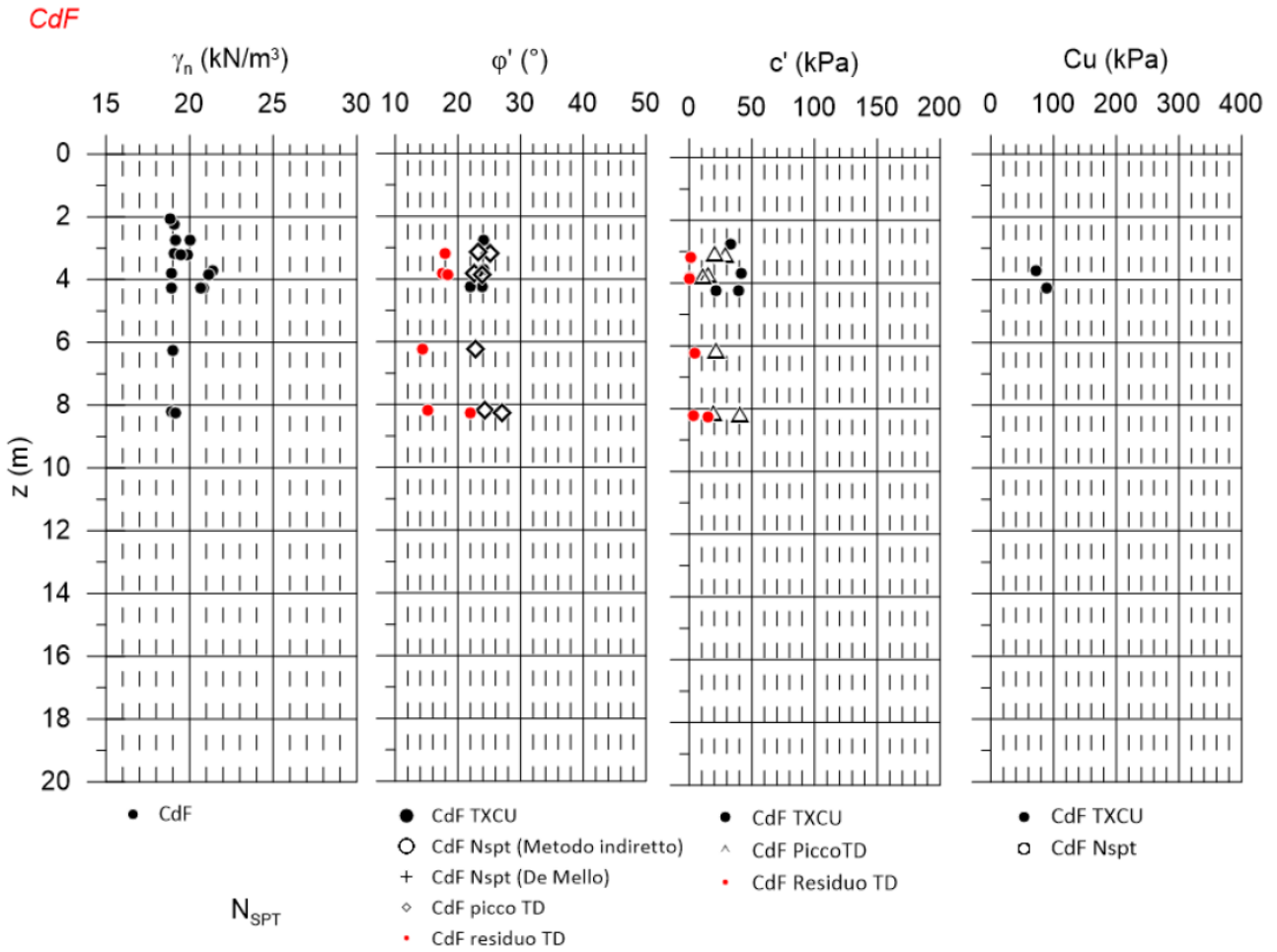


Figura 3.1 Prove di laboratorio frana.

4. CARATTERISTICHE DEI MATERIALI STRUTTURALI

4.1. CALCESTRUZZO

- Calcestruzzo per magrone

| | | |
|------------------------------|-----------|--------|
| Classe di resistenza minima: | C_{min} | C12/15 |
|------------------------------|-----------|--------|

- Calcestruzzo per getto: pali, trave di coronamento e ripartizione

| | | |
|---|------|--------|
| Conforme alla norma UNI EN 206-1/UNI11104 | | |
| Classe di resistenza minima: | Cmin | C28/35 |
| Classe di esposizione: | | XC3 |
| Classe di consistenza: | S | S5 |
| Dimensione massima aggregati [mm] | Dmax | 20 |
| Copriferro [mm] | c | 40 |

Per garantire la durabilità delle strutture in calcestruzzo e per la definizione della classe di resistenza di queste ultime in funzione delle condizioni ambientali, si farà riferimento alle indicazioni contenute nelle norme UNI EN 206-1 ed UNI 11104.

4.2. ACCIAIO

- Acciaio per armature ordinarie

| | | |
|--|----------|------------------|
| Acciaio in barre ad aderenza migliorata tipo B450C controllato in stabilimento | | |
| Tensione caratteristica di snervamento: | f_{yk} | $\geq 450N/mm^2$ |
| Tensione caratteristica di rottura | f_{tk} | $\geq 540N/mm^2$ |

4.3. ULTERIORI SPECIFICHE RELATIVE AI MATERIALI

4.3.1. CALCESTRUZZI

La prescrizione del calcestruzzo all'atto del progetto deve essere caratterizzata almeno mediante la classe di resistenza, la classe di consistenza al getto ed il diametro massimo dell'aggregato, nonché la classe di esposizione ambientale, di cui alla norma UNI EN 206:2016.

Per le caratteristiche dei calcestruzzi si fa riferimento alle formule indicate di seguito:

- resistenza a compressione cubica: R_{ck}
- resistenza a compressione cilindrica: $f_{ck} = 0,83 \cdot R_{ck}$
- resistenza a compressione cilindrica media: $f_{cm} = f_{ck} + 8 [N/mm^2]$
- resistenza media a trazione semplice per classi <C50/60: $f_{ctm} = 0,30 \cdot f_{ck}^{2/3}$
- modulo elastico: $E_{cm} = 22.000 \cdot [f_{cm}/10]^{0,3} [N/mm^2]$
- coefficiente di Poisson: 0,20

PROGETTAZIONE ATI:

5. CARATTERISTICHE GEOMETRICHE GALLERIA

L'opera completa presenta le superfici più interne coincidenti con quelle della galleria naturale; a differenza di quest'ultima, il tratto di galleria oggetto di studio presenta dei piedritti con spessore 1.50m a cui si raccordano l'arco inferiore e superiore. L'arco inferiore si raccorda attraverso una ciabatta di fondazione di sezione rettangolare mentre quello superiore si raccorda al piedritto nel piano dei reni con una sezione a spessore variabile.

Qui di seguito viene riportata la sezione finale.

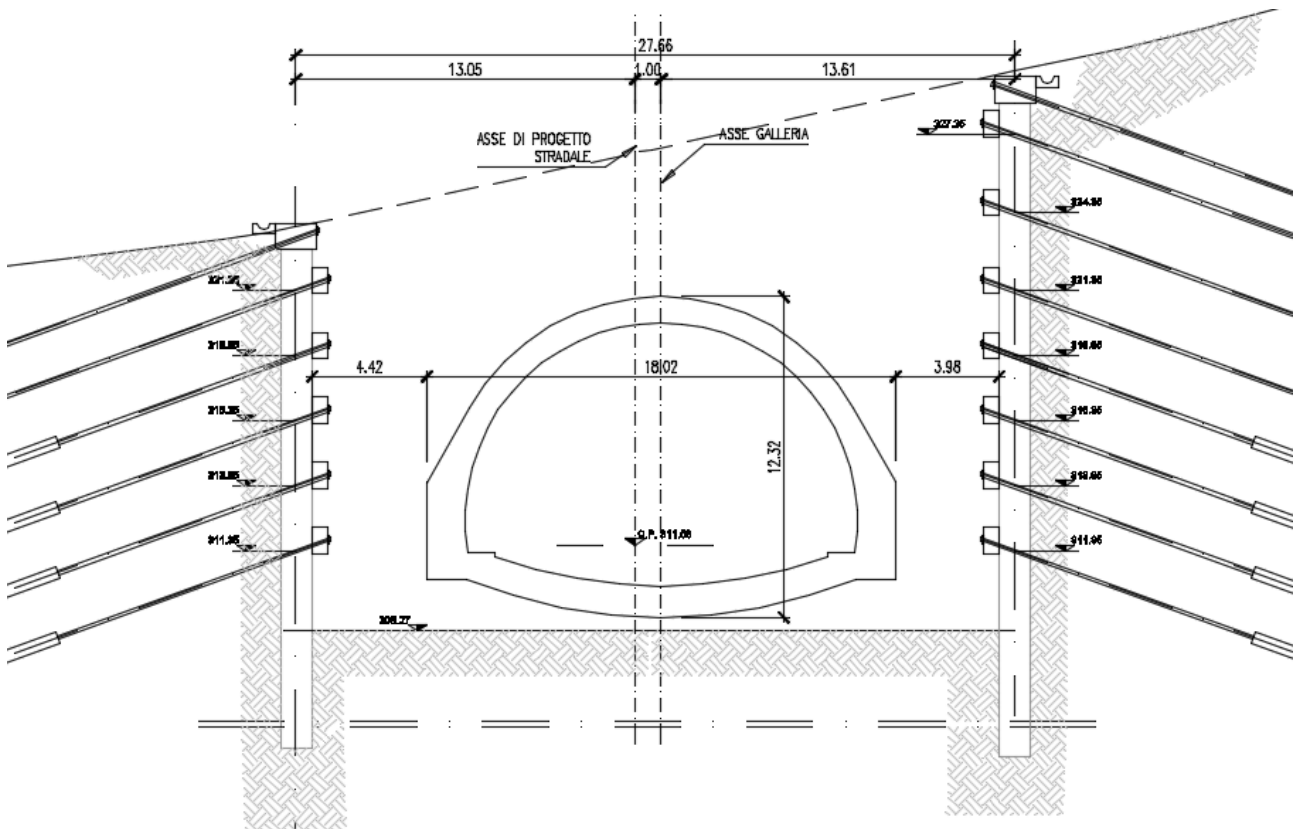
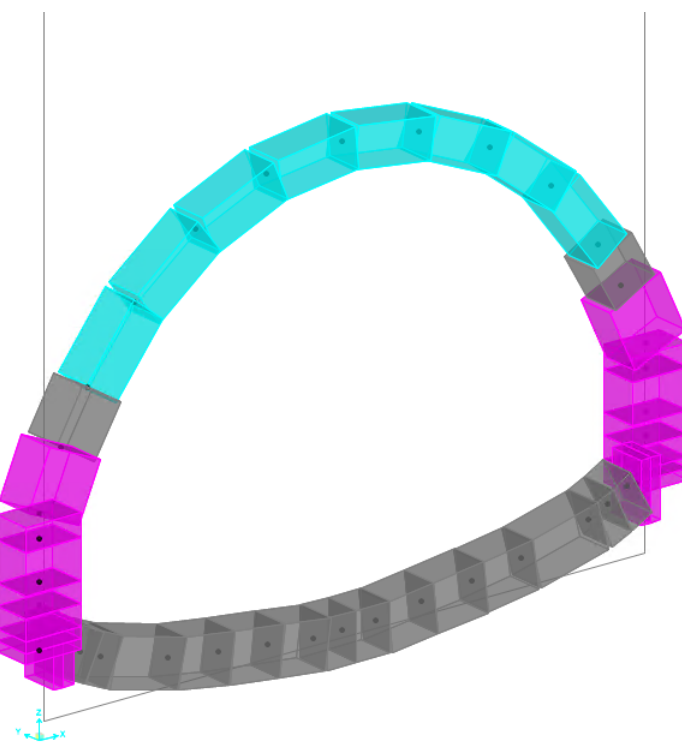
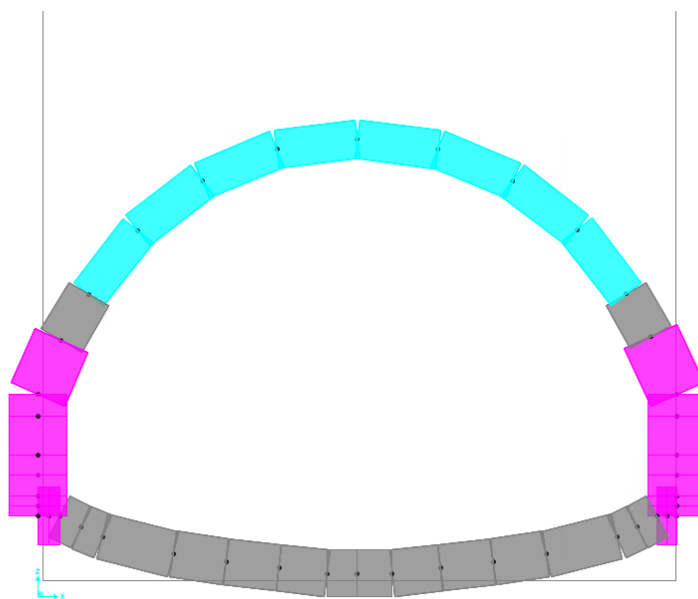


Figura 5.1 Sezione dell'opera in esame

Nell'analisi si considera una sezione di galleria di larghezza unitaria ($B=1$ m) e viene quindi definito un modello della struttura schematizzato in elementi beam. In funzione della variabilità degli elementi strutturali si sono individuate le seguenti sezioni tipologiche:

- Arco rovescio (1.20 m)
- Arco superiore (1.00 m)
- Rene (1.20 m)
- Piedritto (1.50 m)

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA



PROGETTAZIONE ATI:

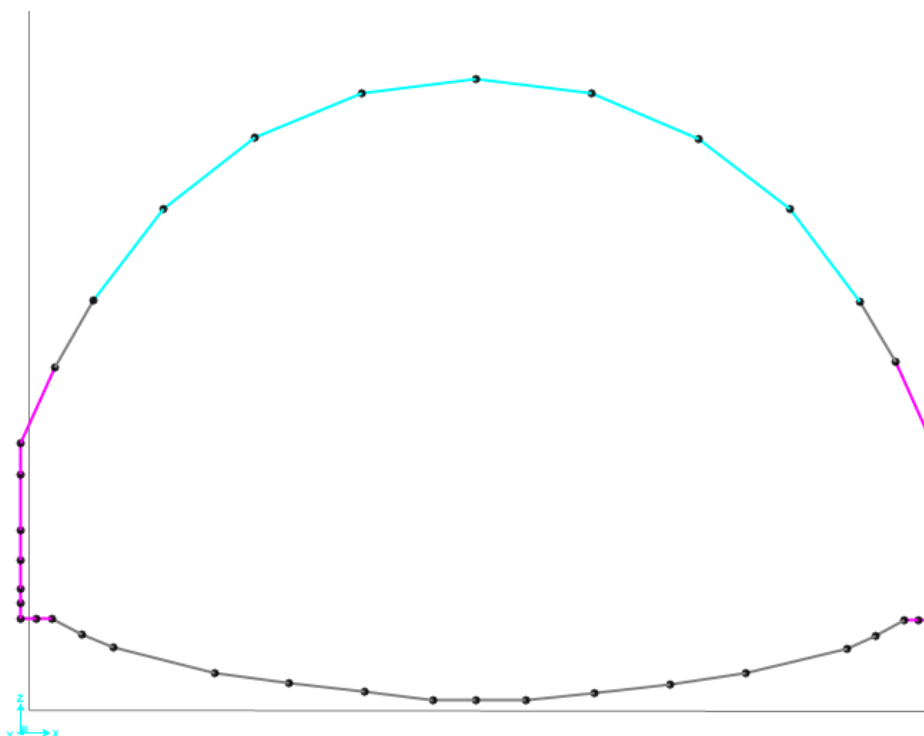


Figura 5.2 Modellazione geometrica galleria

PROGETTAZIONE ATI:

6. CARATTERISTICHE GEOMETRICHE MURO D'INVITO

Il muro d'invito presenta dimensioni variabili lungo il suo sviluppo e per questo nel calcolo viene considerata una sezione di spessore medio con altezza pari a quella massima.

In particolare per il muro con altezza massima l'altezza di calcolo considerata risulta con un'altezza di 4.90m dall'estradosso della fondazione e spessore di 1.50m, con fondazione larga 3 metri e alta 1.10m.

Il muro poggianti sul terreno con caratteristiche più scadenti presenta un'altezza di 4.00m dall'estradosso della fondazione e spessore di 1.50m, con una fondazione larga 3 metri e alta 1.10m. In più alla base della fondazione di questa tipologia di muro si considera la presenza di un "dente" 35x35cm utile ad per aumentare l'attrito della fondazione nei confronti delle spinte laterali.

Il muro è considerabile quindi come un blocco rigido e per questo sarà verificato come un muro a gravità e l'armatura risulterà utile principalmente a limitare le fessurazioni del calcestruzzo.

PROGETTAZIONE ATI:

7. DEFINIZIONE DELL'AZIONE SISMICA

Le azioni sismiche di progetto, in base alle quali valutare il rispetto dei diversi stati limite considerati, si definiscono a partire dalla "pericolosità sismica di base" del sito di costruzione. Essa costituisce l'elemento di conoscenza primario per la determinazione delle azioni sismiche.

La pericolosità sismica è definita in termini di accelerazione orizzontale massima attesa a_g in condizioni di campo libero su sito di riferimento rigido con superficie topografica orizzontale, nonché di ordinate dello spettro di risposta elastico in accelerazione ad essa corrispondente $S_e(T)$, con riferimento a prefissate probabilità di eccedenza P_{VR} , nel periodo di riferimento V_R .

Ai fini della normativa vigente le forme spettrali sono definite, per ciascuna delle probabilità di superamento nel periodo di riferimento P_{VR} , a partire dai valori dei seguenti parametri su sito di riferimento rigido orizzontale:

- a_g accelerazione orizzontale massima al sito;
- F_0 valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;
- T_C^* periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale.

Ai fini delle verifiche strutturali, in accordo con la normativa vigente, si considera lo Stato Limite di Salvaguardia della Vita (SLV). Non verrà considerato lo Stato Limite di Danno (SLD) in quanto la struttura risulta provvisoria.

Per la definizione del tempo di ritorno del sisma, è stata considerata una vita nominale della struttura pari a 50 anni e classe d'uso IV ($c_u = 2$), cosicché il periodo di riferimento dell'azione sismica risulta essere:

$$V_R = V_N \cdot c_u = 100 \text{ anni}$$

7.1. CATEGORIE DI SOTTOSUOLO E CONDIZIONI TOPOGRAFICHE

Ai fini della definizione dell'azione sismica di progetto, si rende necessario valutare l'effetto della risposta sismica locale sulla base dell'individuazione di categorie di sottosuolo (Tab.3.2.IV del D.M. 17/01/2018) e topografiche (Tab.3.2.V del D.M. 17/01/2018) di riferimento (in assenza di specifiche analisi).

A livello di categoria di suolo di fondazione si assume un terreno di categoria B: "Rocce tenere e depositi di terreni a grana grossa molto addensati o terreni a grana fina molto consistenti".

Per quanto concerne invece le condizioni topografiche, il sito in oggetto è attribuibile alla Categoria T2: "Pendii con inclinazione media $i > 15^\circ$ ".

7.2. DEFINIZIONE DELL'ACCELERAZIONE SISMICA DI PROGETTO

Sulla base di quanto mostrato in precedenza sono riportati i parametri per la definizione dell'azione sismica massima di progetto la quale sarà necessaria per la definizione della forza pseudo-statica sismica.

PROGETTAZIONE ATI:

Vengono qui di seguito riportati i principali parametri, oltre che l'azione sismica presente nella locazione specifica dei manufatti, sia allo Stato Limite di Salvaguardia della Vita che allo Stato Limite di Danno.

Parametri indipendenti

| STATO LIMITE | SLV |
|--------------|---------|
| a_d | 0,225 g |
| F_e | 2,507 |
| T_c^* | 0,329 s |
| S_s | 1,175 |
| C_c | 1,374 |
| S_T | 1,200 |
| q | 1,000 |

Parametri dipendenti

| | |
|--------|---------|
| S | 1,410 |
| η | 1,000 |
| T_B | 0,151 s |
| T_C | 0,452 s |
| T_D | 2,498 s |

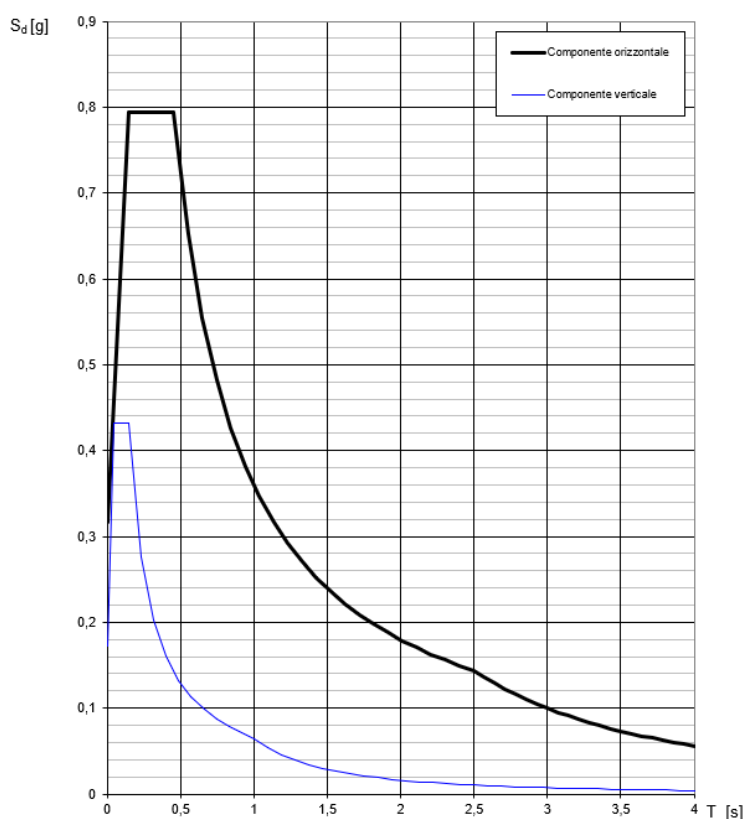


Figura 7.1 Definizione accelerazione sismica SLV

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

Parametri indipendenti

| STATO LIMITE | SLD |
|--------------|---------|
| a_g | 0,097 g |
| F_o | 2,456 |
| T_c^* | 0,297 s |
| S_S | 1,200 |
| C_C | 1,403 |
| S_T | 1,200 |
| q | 1,000 |

Parametri dipendenti

| | |
|--------|---------|
| S | 1,440 |
| η | 1,000 |
| T_B | 0,139 s |
| T_C | 0,416 s |
| T_D | 1,989 s |

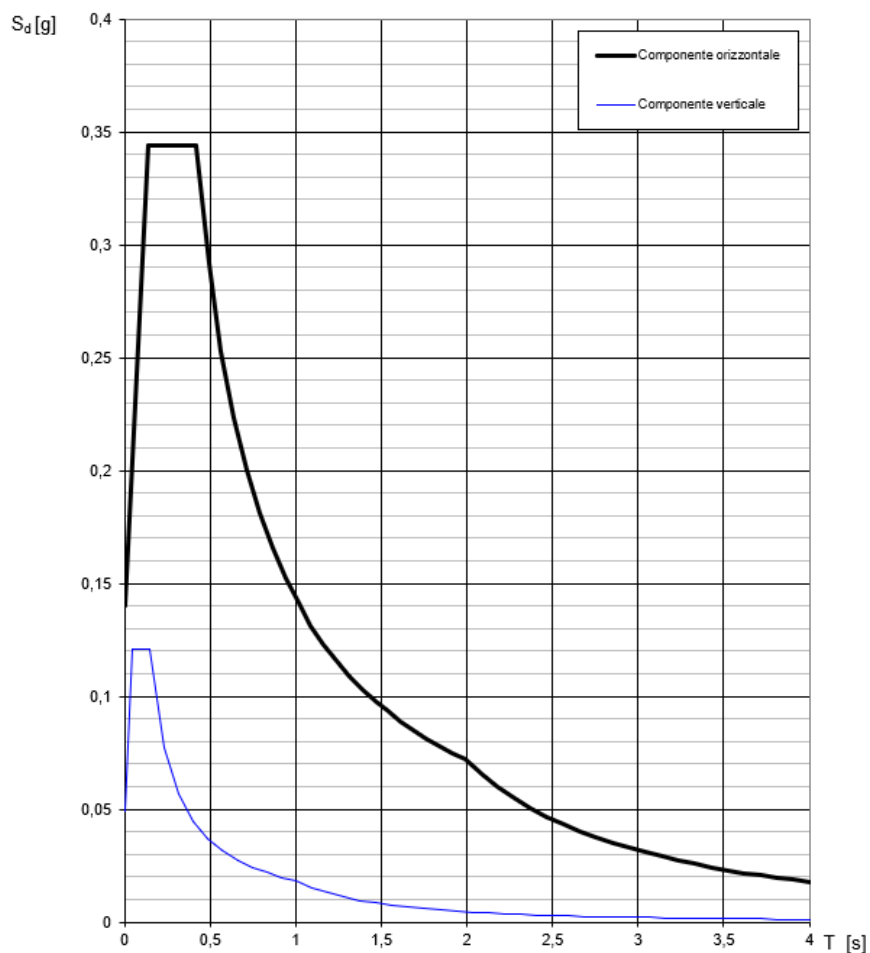


Figura 7.2 Definizione accelerazione sismica SLD

PROGETTAZIONE ATI:

8. CRITERI DI VERIFICA E CALCOLO

8.1. PREMESSA NORMATIVA DI CALCOLO

Le verifiche contenute nel presente documento fanno riferimento a quanto prescritto per i sistemi fondazionali nelle NTC2018 e successiva circolare esplicativa.

Le verifiche strutturali sono eseguite nei confronti degli Stati Limite Ultimi (SLU) e degli Stati Limite di Salvaguardia della Vita (SLV) riferiti allo sviluppo di meccanismi di collasso determinati dalla mobilitazione della resistenza del terreno e al raggiungimento della resistenza degli elementi strutturali che compongono la fondazione.

Gli stati limite di esercizio esaminati per il soddisfacimento delle prestazioni richieste ai manufatti sono:

- danneggiamenti locali che possono ridurre la durabilità della struttura, la sua efficienza o il suo aspetto (controllo delle tensioni massime e della fessurazione del calcestruzzo con verifiche sezionali);
- eccessive deformazioni che possono limitare l'uso della costruzione, la sua efficienza e il suo aspetto (verifica dei rapporti limite deformazione massima o spessore /luce di calcolo).

Per ogni stato limite deve essere rispettata la condizione:

$$E_d \leq R_d \quad (\text{eq. 6.2.1 delle NTC2018})$$

dove

E_d valore di progetto dell'azione o dell'effetto dell'azione;

R_d valore di progetto della resistenza del sistema geotecnico.

8.2. COMBINAZIONE DELLE AZIONI (CAP. 2.5.3 D.M. 17/01/2018)

- Combinazione fondamentale, generalmente impiegata per gli stati limite ultimi (SLU):

$$\sum_{j \geq 1} \gamma_{G,j} G_{k,j} + \gamma_P P + \gamma_{Q,1} Q_{k,1} + \sum_{i \geq 2} \gamma_{Q,i} \psi_{0,i} Q_{k,i}$$

- Combinazione caratteristica (rara), generalmente impiegata per gli stati limite di esercizio (SLE) irreversibili, da utilizzarsi nelle verifiche alle tensioni ammissibili:

$$\sum_{j \geq 1} G_{k,j} + P + Q_{k,1} + \sum_{i \geq 2} \psi_{0,i} Q_{k,i}$$

- Combinazione frequente, generalmente impiegata per gli stati limite di esercizio (SLE) reversibili:

$$\sum_{j \geq 1} G_{k,j} + P + \psi_{1,1} Q_{k,1} + \sum_{i \geq 1} \psi_{2,i} Q_{k,i}$$

- Combinazione quasi permanente (SLE), generalmente impiegata per gli effetti a lungo termine:

$$\sum_{j \geq 1} G_{k,j} + P + \sum_{i \geq 1} \psi_{2,i} Q_{k,i}$$

- Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica:

$$\sum_{j \geq 1} G_{k,j} + P + A_{Ed} + \sum_{i \geq 1} \psi_{2,i} Q_{k,i}$$

La progettazione e verifica degli elementi strutturali è condotta in conformità alla normativa vigente Norme Tecniche per le Costruzioni 2018 (DM 17/01/2018). Le verifiche tensionali degli elementi strutturali sono eseguite col metodo degli stati limite. Ai fini del dimensionamento e delle verifiche sono stati presi in esame i seguenti approcci di calcolo, secondo quanto specificato in NTC 2018:

SLU approccio 1:

- Combinazione Fondamentale
- Combinazione sismica

SLE:

- Combinazione Rara (SLE-R)
- Combinazione sismica (SLD)
- Combinazione Frequente (SLE-F)
- Combinazione Quasi Permanente (SLE- Q)

Per ognuno degli stati limite sopra definiti si adotteranno le combinazioni di carico definite precedentemente. Si rimanda all'allegato per la definizione delle combinazioni di carico.

8.3. COEFFICIENTI DELLE AZIONI AGLI STATI LIMITE

Per la verifica agli SLU si adottano i valori dei coefficienti parziali della tabella sotto riportata (rif. Tab. 6.2.1 delle NTC 2018):

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

Tab. 6.2.I – Coefficienti parziali per le azioni o per l'effetto delle azioni

| | Effetto | Coefficiente Parziale γ_F (o γ_E) | EQU | (A1) | (A2) |
|--------------------------------|-------------|---|-----|------|------|
| Carichi permanenti G_1 | Favorevole | γ_{G1} | 0,9 | 1,0 | 1,0 |
| | Sfavorevole | | 1,1 | 1,3 | 1,0 |
| Carichi permanenti $G_2^{(1)}$ | Favorevole | γ_{G2} | 0,8 | 0,8 | 0,8 |
| | Sfavorevole | | 1,5 | 1,5 | 1,3 |
| Azioni variabili Q | Favorevole | γ_{Qi} | 0,0 | 0,0 | 0,0 |
| | Sfavorevole | | 1,5 | 1,5 | 1,3 |

⁽¹⁾ Per i carichi permanenti G_2 si applica quanto indicato alla Tabella 2.6.I. Per la spinta delle terre si fa riferimento ai coefficienti γ_{G1}

I coefficienti di combinazione dei carichi, applicati secondo le varie combinazioni, sono riferiti alla Tab. 2.5.I delle NTC 2018:

Tab. 2.5.I – Valori dei coefficienti di combinazione

| Categoria/Azione variabile | ψ_{0j} | ψ_{1j} | ψ_{2j} |
|---|----------------------------|-------------|-------------|
| Categoria A - Ambienti ad uso residenziale | 0,7 | 0,5 | 0,3 |
| Categoria B - Uffici | 0,7 | 0,5 | 0,3 |
| Categoria C - Ambienti suscettibili di affollamento | 0,7 | 0,7 | 0,6 |
| Categoria D - Ambienti ad uso commerciale | 0,7 | 0,7 | 0,6 |
| Categoria E - Aree per immagazzinamento, uso commerciale e uso industriale Biblioteche, archivi, magazzini e ambienti ad uso industriale | 1,0 | 0,9 | 0,8 |
| Categoria F - Rimesse, parcheggi ed aree per il traffico di veicoli (per autoveicoli di peso ≤ 30 kN) | 0,7 | 0,7 | 0,6 |
| Categoria G - Rimesse, parcheggi ed aree per il traffico di veicoli (per autoveicoli di peso > 30 kN) | 0,7 | 0,5 | 0,3 |
| Categoria H - Coperture accessibili per sola manutenzione | 0,0 | 0,0 | 0,0 |
| Categoria I - Coperture praticabili | da valutarsi caso per caso | | |
| Categoria K - Coperture per usi speciali (impianti, eliporti, ...) | da valutarsi caso per caso | | |
| Vento | 0,6 | 0,2 | 0,0 |
| Neve (a quota ≤ 1000 m s.l.m.) | 0,5 | 0,2 | 0,0 |
| Neve (a quota > 1000 m s.l.m.) | 0,7 | 0,5 | 0,2 |
| Variazioni termiche | 0,6 | 0,5 | 0,0 |

8.4. VERIFICHE AGLI STATI LIMITE (SLU)

Per ogni stato limite ultimo **SLU** deve essere rispettata la condizione:

$$E_d \leq R_d$$

Dove E_d è il valore di progetto delle azioni e R_d il valore di progetto della resistenza del sistema.

Effetto delle azioni sono espresse in funzione delle azioni di progetto $E_d = F_k \cdot \gamma_E$, dei parametri di progetto X_k / γ_M e della geometria di progetto. Nella formulazione della resistenza appare esplicitamente il coefficiente γ_R che opera direttamente sulla resistenza.

| Combinazioni per analisi statiche SLU | | | | | | | |
|---------------------------------------|-----------------------|------------|-------------|------------|--------------------------------------|------|-------|
| | Azioni (γ_F) | | | | Proprietà del terreno (γ_M) | | |
| | Permanenti | | Variabili | | tan φ' | c' | c_u |
| | Sfavorevoli | Favorevoli | Sfavorevoli | Favorevoli | | | |
| STR (A1 + M1) | 1.30 | 1.00 | 1.50 | 0.00 | 1.00 | 1.00 | 1.00 |
| GEO (A2 + M2) | 1.00 | 1.00 | 1.30 | 0.00 | 1.25 | 1.25 | 1.40 |

8.4.1. SLU (STR)

Per quanto concerne le verifiche agli stati limite ultimo per il dimensionamento strutturale (STR) le analisi saranno eseguite facendo riferimento alla Combinazione 1 (A1+M1+R1) in cui le azioni permanenti e variabili sono amplificate mediante i coefficienti parziali del gruppo A1, applicati direttamente sulle sollecitazioni caratteristiche.

In questo caso le verifiche a cui far riferimento sono le seguenti:

- Resistenza a pressoflessione.
- Resistenza a taglio

8.4.2. CONDIZIONI SISMICHE

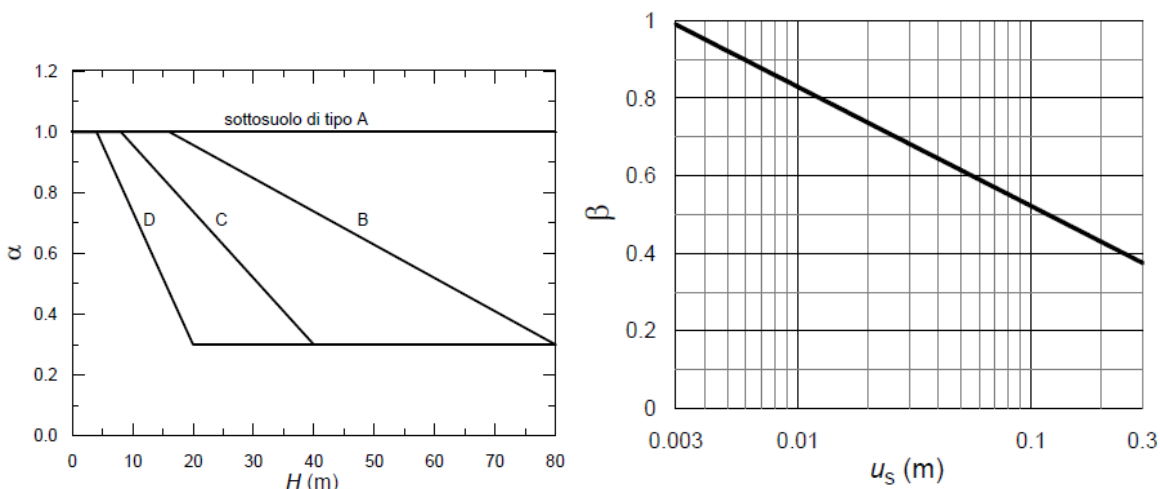
Come prescritto dalle NTC2018 Al Par. 7.11.1, le verifiche si eseguono con coefficienti parziali unitari sulle azioni e sui parametri geotecnici e considerando le variazioni della spinta delle terre sulle superfici laterali della galleria.

In accordo con il Capitolo 7.11.6.3.1 delle NTC2018, l'analisi della spinta delle terre in condizioni sismiche può essere effettuata seguendo un metodo pseudo-statico.

Questa tipologia di analisi consente di considerare l'azione dinamica indotta dal sisma attraverso una statica equivalente: essa è pari al prodotto delle forze di gravità per un opportuno coefficiente sismico. Nelle verifiche allo Stato Limite Ultimo (SLV) l'accelerazione laterale di progetto può essere calcolata mediante la seguente espressione:

$$k_h = \alpha \cdot \beta \frac{a_{\max}}{g}$$

Dove il coefficiente α è funzione della deformabilità dei terreni interagenti con la struttura e dell'altezza dell'opera, mentre β dipende dalla capacità della struttura di subire spostamenti. Tali coefficienti possono essere dedotti a partire dalle Figure 7.11.2 e 7.11.3 presenti nelle NTC2018 e di seguito riportate.



PROGETTAZIONE ATI:

Nel caso della galleria, data la notevole rigidità dell'opera si terrà conto delle forze inerziali derivanti dalla spinta del terreno sono state considerate con una forza pseudo-statica valutata attraverso il noto metodo di Wood; metodo applicabile in quanto si di un'opera rigida completamente vincolata.

Nel caso del muro a gravità invece si dovrà tenere in conto della libertà di muoversi del muro: se questo non è libero di muoversi, ad esempio per la presenza di pali allora si farà riferimento alla spinta di Wood, altrimenti si farà riferimento alla spinta di Mononobe-Okabe.

Tale metodo si rifà all'analisi dell'equilibrio limite di un cuneo di terreno instabile a contatto con l'opera di sostegno; in più, però, il metodo tiene conto della forza d'inerzia della massa del cuneo instabile, considerata applicata nel baricentro del cuneo stesso, derivante dall'accelerazione sismica.

A tale scopo, nella definizione del coefficiente di spinta attiva, il metodo considera un angolo di rotazione addizionale:

$$\psi = \arctan\left(\frac{k_h}{1 \mp k_v}\right)$$

dove k_h e k_v sono i coefficienti sismici, rispettivamente orizzontale e verticale definiti al paragrafo 7.2.

L'espressione del coefficiente di spinta attiva si modifica, pertanto, come segue:

$$K_{a,s} = \frac{\sin^2(\varphi' - \beta - \psi)}{\cos\psi \cdot \cos^2\beta \cdot \sin(\beta + \delta + \psi) \cdot \left[\left(1 + \sqrt{\frac{\sin(\varphi' + \delta) \cdot \sin(\varphi' - i - \psi)}{\sin(\beta + \delta + \psi) \cdot \sin(\beta - i)}} \right) \right]^2}$$

Dove i è l'inclinazione del terreno a tergo dell'opera di sostegno.

La spinta del terreno a tergo del muro in condizioni sismiche, pertanto, si valuta semplicemente sostituendo al coefficiente di spinta attiva in condizioni statiche k_a il coefficiente $K_{a,s}$ sopra definito:
 $P_A = 0,5 \cdot \gamma' \cdot K_{a,s} \cdot H^2 (1 \mp k_v)$.

8.5. VERIFICHE AGLI STATI LIMITE (SLE)

Le opere ed i sistemi geotecnici devono essere verificati nei confronti degli stati limite di esercizio. Per ciascuno stato limite di esercizio deve essere rispettata la condizione:

$$E_d \leq C_d$$

Dove E_d è sempre il valore di progetto dell'effetto delle azioni e C_d è il prescritto valore limite dell'effetto delle azioni.

Per gli Stati Limite di Esercizio occorre verificare che l'ampiezza delle fessure w_k , per gli elementi con armature lente, sia al di sotto del valore limite fissato per le classi di esposizione in oggetto. In particolare, devono essere rispettati i seguenti limiti:

PROGETTAZIONE ATI:

- Combinazione di carico quasi permanente: $w_k = 0.2mm$;
- Combinazione di carico frequente: $w_k = 0.3mm$;

Tab. 4.1.III – Descrizione delle condizioni ambientali

| Condizioni ambientali | Classe di esposizione |
|-----------------------|-----------------------------------|
| Ordinarie | X0, XC1, XC2, XC3, XF1 |
| Aggressive | XC4, XD1, XS1, XA1, XA2, XF2, XF3 |
| Molto aggressive | XD2, XD3, XS2, XS3, XA3, XF4 |

| Gruppi di Esigenze | Condizioni ambientali | Combinazione di azioni | Armatura | | | |
|--------------------|-----------------------|------------------------|--------------------|------------|------------------|------------|
| | | | Sensibile | | Poco sensibile | |
| | | | Stato limite | w_k | Stato limite | w_k |
| A | Ordinarie | frequente | apertura fessure | $\leq w_2$ | apertura fessure | $\leq w_3$ |
| | | quasi permanente | apertura fessure | $\leq w_1$ | apertura fessure | $\leq w_2$ |
| B | Aggressive | frequente | apertura fessure | $\leq w_1$ | apertura fessure | $\leq w_2$ |
| | | quasi permanente | decompressione | - | apertura fessure | $\leq w_1$ |
| C | Molto aggressive | frequente | formazione fessure | - | apertura fessure | $\leq w_1$ |
| | | quasi permanente | decompressione | - | apertura fessure | $\leq w_1$ |

Allo Stato Limite di Danno (SLD) è necessario invece verificare, sia la resistenza come indicato dalle NTC18 per strutture con classe d'uso IV, anche che la struttura rimanga prevalentemente elastica come da definizione di SLD. Per fare questo viene eseguita una verifica tensionale e in particolare che le tensioni siano comprese entro certi limiti:

- $\sigma_c < 0.6 \cdot f_{ck}$
- $\sigma_s < 0.8 \cdot f_{yk}$

9. ANALISI DEI CARICHI

Si considerano i seguenti carichi nel calcolo delle sollecitazioni agenti sulle paratie:

- Carichi permanenti G_1 :
 - Peso proprio del terreno (simmetrico e asimmetrico);
 - Peso proprio delle strutture (valutato direttamente dal software).
 - Spinta dell'acqua;
 - Spinta delle terre (simmetriche e asimmetriche);
- Carichi variabili Q :
 - Sovraccarico da traffico stimato come 20 kPa uniformemente distribuito;
- Azione del sisma E :
 - Componente inerziale della spinta delle terre;

Poiché il modello di calcolo utilizzato per l'analisi strutturale schematizza una striscia di paratia profonda 1.0 m (sviluppo in direzione longitudinale) nel seguito i carichi e le sollecitazioni si intendono riferiti a detta striscia unitaria.

9.1. CARICHI PERMANENTI

Le pressioni nel terreno sono determinate sulla base dei pesi specifici delle stratigrafie relative al manufatto.

Le pressioni totali ed efficaci sono riferite al livello di falda posto in evidenza nel capitolo 3 e calcolate sia per il caso simmetrico che asimmetrico.

La spinta delle terre viene valutata a partire dallo stato di sforzo verticale con le seguenti formulazioni:

- Spinta del terreno a riposo: formula di Jacky

$$K_0 = 1 - \sin \phi'$$

- Spinta attiva e passiva: Il calcolo può essere condotto con varie formulazioni come Coulomb o Rankine e viene valutato direttamente dal software di calcolo per le varie fasi di cantiere. Il coefficiente di spinta passiva K_p viene valutata automaticamente dal software attraverso la reazione delle molle poste nel contorno dell'opera.

$$K_A = \tan^2 \left(\frac{\pi}{4} - \frac{\phi'}{2} \right) = \tan^2(\beta)$$

L'angolo di attrito tra il muro e il terreno viene posto pari a $\delta = 0 \cdot \phi'$

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| 5,15 | S_PSX | | | S_PCEN | | | S_PDX | | |
|----------------------|------------------------|----------------------------------|----------------------------------|-------------------------|----------------------------------|----------------------------------|------------------------|----------------------------------|----------------------------------|
| | h _{ricopr} 10 | | | h _{ricopr} 4,5 | | | h _{ricopr} 10 | | |
| altezza ricoprimento | σ'_v | σ'_h [kPa] K ₀ | σ'_h [kPa] K _A | σ'_v | σ'_h [kPa] K ₀ | σ'_h [kPa] K _A | σ'_v | σ'_h [kPa] K ₀ | σ'_h [kPa] K _A |
| z [m] | | | | | | | | | |
| 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 |
| 1,00 | 17,00 | 8,50 | 5,67 | 17,00 | 8,50 | 5,67 | 17,00 | 8,50 | 5,67 |
| 2,00 | 34,00 | 17,00 | 11,33 | 34,00 | 17,00 | 11,33 | 34,00 | 17,00 | 11,33 |
| 3,00 | 49,08 | 24,54 | 16,36 | 49,08 | 24,54 | 16,36 | 49,08 | 24,54 | 16,36 |
| 4,50 | 67,37 | 33,68 | 22,46 | 67,37 | 33,68 | 22,46 | 67,37 | 33,68 | 22,46 |
| 5,00 | 73,47 | 36,73 | 24,49 | 0,00 | 0,00 | 0,00 | 73,47 | 36,73 | 24,49 |
| 6,00 | 85,66 | 42,83 | 28,55 | 0,00 | 0,00 | 0,00 | 85,66 | 42,83 | 28,55 |
| 7,00 | 97,85 | 48,93 | 32,62 | 0,00 | 0,00 | 0,00 | 97,85 | 48,93 | 32,62 |
| 8,00 | 110,05 | 55,02 | 36,68 | 0,00 | 0,00 | 0,00 | 110,05 | 55,02 | 36,68 |
| 9,00 | 122,24 | 61,12 | 40,75 | 0,00 | 0,00 | 0,00 | 122,24 | 61,12 | 40,75 |
| 10,00 | 134,44 | 67,22 | 44,81 | 0,00 | 0,00 | 0,00 | 134,44 | 67,22 | 44,81 |
| 11,00 | 146,63 | 73,31 | 48,88 | 0,00 | 0,00 | 0,00 | 146,63 | 73,31 | 48,88 |
| 12,00 | 158,82 | 79,41 | 52,94 | 0,00 | 0,00 | 0,00 | 158,82 | 79,41 | 52,94 |
| 13,00 | 171,02 | 85,51 | 57,01 | 0,00 | 0,00 | 0,00 | 171,02 | 85,51 | 57,01 |
| 14,00 | 183,21 | 91,61 | 61,07 | 0,00 | 0,00 | 0,00 | 183,21 | 91,61 | 61,07 |
| 15,15 | 197,23 | 98,62 | 65,74 | 0,00 | 0,00 | 0,00 | 197,23 | 98,62 | 65,74 |
| 16,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 |

| | A_PSX | | | A_PCEN | | | A_PDX | | |
|----------------------|--------------------------|----------------------------------|----------------------------------|--------------------------|----------------------------------|----------------------------------|---------------------------|----------------------------------|----------------------------------|
| | h _{ricopr} 8,12 | | | h _{ricopr} 5,62 | | | h _{ricopr} 14,37 | | |
| altezza ricoprimento | σ'_v | σ'_h [kPa] K ₀ | σ'_h [kPa] K _A | σ'_v | σ'_h [kPa] K ₀ | σ'_h [kPa] K _A | σ'_v | σ'_h [kPa] K ₀ | σ'_h [kPa] K _A |
| z [m] | | | | | | | | | |
| 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 |
| 1,00 | 12,19 | 6,10 | 4,06 | 17,00 | 8,50 | 5,67 | 17,00 | 8,50 | 5,67 |
| 2,00 | 24,39 | 12,19 | 8,13 | 34,00 | 17,00 | 11,33 | 34,00 | 17,00 | 11,33 |
| 3,00 | 36,58 | 18,29 | 12,19 | 49,08 | 24,54 | 16,36 | 51,00 | 25,50 | 17,00 |
| 4,50 | 54,87 | 27,44 | 18,29 | 67,37 | 33,68 | 22,46 | 76,50 | 38,25 | 25,50 |
| 5,00 | 60,97 | 30,49 | 20,32 | 73,47 | 36,73 | 24,49 | 85,00 | 42,50 | 28,33 |
| 6,00 | 73,16 | 36,58 | 24,39 | 0,00 | 0,00 | 0,00 | 101,04 | 50,52 | 33,68 |
| 7,00 | 85,36 | 42,68 | 28,45 | 0,00 | 0,00 | 0,00 | 113,23 | 56,62 | 37,74 |
| 8,00 | 97,55 | 48,78 | 32,52 | 0,00 | 0,00 | 0,00 | 125,43 | 62,71 | 41,81 |
| 9,00 | 109,75 | 54,87 | 36,58 | 0,00 | 0,00 | 0,00 | 137,62 | 68,81 | 45,87 |
| 10,00 | 121,94 | 60,97 | 40,65 | 0,00 | 0,00 | 0,00 | 149,81 | 74,91 | 49,94 |
| 11,00 | 134,13 | 67,07 | 44,71 | 0,00 | 0,00 | 0,00 | 162,01 | 81,00 | 54,00 |
| 12,00 | 146,33 | 73,16 | 48,78 | 0,00 | 0,00 | 0,00 | 174,20 | 87,10 | 58,07 |
| 13,00 | 158,52 | 79,26 | 52,84 | 0,00 | 0,00 | 0,00 | 186,40 | 93,20 | 62,13 |
| 14,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 198,59 | 99,30 | 66,20 |
| 15,15 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 212,61 | 106,31 | 70,87 |
| 16,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 0,00 | 222,98 | 111,49 | 74,33 |
| 17,00 | | | | | | | 235,17 | 117,59 | 78,39 |
| 18,00 | | | | | | | 247,37 | 123,68 | 82,46 |
| 19,00 | | | | | | | 259,56 | 129,78 | 86,52 |
| 20,00 | | | | | | | 0,00 | 0,00 | 0,00 |

Figura 9.1 Spinte terre

PROGETTAZIONE ATI:

9.2. AZIONE SISMICA GALLERIA

Nel caso in esame, data la notevole rigidità dell'opera si terrà conto delle forze inerziali derivanti dalla spinta del terreno sono state considerate con una forza pseudo-statica valutata attraverso il noto metodo di Wood; metodo applicabile in quanto si di un'opera rigida completamente vincolata. La spinta ΔP_d agente sulla galleria è pertanto così definita:

$$\Delta P_d = (a_g / g) \times S \times \gamma_t \times H^2$$

$a_g/g \times S = k_h$ (coefficiente sismico da applicare alla massa di terreno)

$\gamma_t = 22.0 \text{ kN/m}^3$ (peso specifico del terreno)

$H = 11.00 \text{ m}$ (altezza dell'opera)

SLV:

$$\Delta P_{d,SLV} = 69.00 \text{ kN/m}$$

SLD:

$$\Delta P_{d,SLD} = 30.95 \text{ kN/m}$$

Trascurando la variazione delle pressioni interstiziali ed essendo la traslazione differenziale tra acqua e terreno impedita, il contributo dell'acqua sarà legato unicamente alla componente idrostatica.

9.3. AZIONE SISMICA MURO

Nel caso di un muro di sostegno la scelta del tipo di azione dipende dalla possibilità o meno di movimento della struttura. Visto che il muro presenta una fondazione diretta è facile ipotizzare che risulta libero di muoversi e quindi l'azione sismica sarà considerata attraverso il metodo di Mononobe-Okabe.

PROGETTAZIONE ATI:

10. SOFTWARE DI CALCOLO E IPOTESI DI MODELLAZIONE

I calcoli progettuali sono stati svolti con l'ausilio del codice di calcolo **SAP2000**.

La simulazione avviene analizzando il problema piano XZ (considerando una profondità unitaria in direzione Y), dove i gradi di libertà attivi sono lo spostamento laterale, verticale e la rotazione attorno all'asse Y. In tale codice la schematizzazione dell'interazione tra galleria e terreno avviene considerando:

- La galleria come una serie di elementi il cui comportamento è caratterizzato dalla rigidezza flessionale EJ e dalla rigidezza assiale EA;
- Il terreno come una serie di molle di tipo elastiche a comportamento bi-lineare distribuito lungo lo sviluppo dell'elemento.

Il comportamento bi-lineare consiste nel modellare le molle con un comportamento elastico a compressione, con rigidezza pari a quella stimata in precedenza, e a trazione rigidezza e resistenza uguale a zero.

Questo modello numerico consente una simulazione del comportamento del terreno adeguata agli scopi progettuali. In particolare, permetterà di stimare l'interazione completa tra terreno e struttura in maniera accettabile e con un onere di calcolo relativamente basso.

Il difetto di questo approccio è la necessità di dover risolvere un problema non-lineare per ogni combinazione di calcolo stimata. Tuttavia, dato il basso numero di carichi e combinazioni presenti questo problema passa in secondo piano.

10.1. ALTRI SOFTWARE

Le verifiche delle sezioni in c.a. sono state eseguite con l'ausilio del freeware "VCASlu" distribuito dal Prof. Piero Gelfi dell'Università di Brescia e attraverso fogli Excel opportunamente predisposti.

11. CRITERI GENERALI DI VERIFICA DELLE SEZIONI IN C.A.

Per le sezioni in cemento armato si effettuano:

- Verifiche per gli Stati Limite Ultimi a presso-flessione ed a taglio;
- Verifiche per gli Stati Limite di Esercizio per la fessurazione.

11.1. VERIFICA AGLI STATI LIMITE ULTIMO

11.1.1. VERIFICA A PRESSOFLESSIONE

La verifica alle sollecitazioni che provocano tensioni normali (sforzo normale, flessione semplice e flessione composta) è stata fatta con uno specifico programma in cui, inserendo le caratteristiche geometriche della sezione, delle armature e delle sollecitazioni desunte dai precitati tabulati di calcolo, si ottiene, per i materiali ipotizzati, il momento resistente che dovrà risultare maggiore del momento agente.

Con riferimento alla sezione pressoinflessa retta, la capacità, in termini di resistenza e duttilità, si determina in base alle ipotesi di calcolo e ai modelli $\sigma - \varepsilon$:

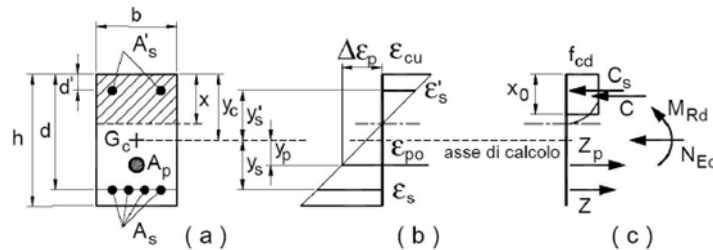


Figura 11.1 Schema verifica a pressoflessione

Le verifiche a flessione vengono condotte confrontando le resistenze ultime e le sollecitazioni massime agenti, valutando il corrispondente fattore di sicurezza (FS) come rapporto tra la sollecitazione resistente e la massima agente.

$$FS = \frac{M_{Rd}}{M_{Ed}} \geq 1$$

Le verifiche a pressoflessione, invece, vengono condotte definendo un dominio di interazione N-M funzione delle caratteristiche meccaniche, geometriche e dal quantitativo d'armatura della sezione: per ogni combinazione si valuta che la coppia (N_{Ed}, M_{Ed}) agente risulti interna a tale dominio.

In particolare, per quanto concerne quest'ultima, si fa riferimento alle 4 combinazioni più gravose: le due con azione assiale minima (max compressione) e massima (max trazione o min compressione) e le due con momento minimo e massimo.

11.1.2. VERIFICA A TAGLIO

Per la verifica di resistenza agli SLU, con riferimento alle sollecitazioni taglianti, deve risultare:

PROGETTAZIONE ATI:

$$FS = \frac{V_{Rd}}{V_{Ed}} \geq 1$$

Per il valore resistente si fa riferimento ai seguenti valori qui di seguito riportato, tenendo conto di sezioni armate o non armate a taglio:

- $V_{Rd,c} = \max \left\{ \left[\frac{0.18}{\gamma_c} \cdot k \cdot (100 \cdot \rho_I \cdot f_{ck})^{\frac{1}{3}} + k_1 \cdot \sigma_{cp} \right] \cdot b_w \cdot d; (v_{\min} + 0.15 \cdot \sigma_{cp}) \cdot b_w \cdot d \right\}$
resistenza di calcolo dell'elemento privo di armatura a taglio;
- $V_{Rd,s} = 0.9 \cdot d \cdot \frac{A_{sw}}{s} \cdot f_{yd} \cdot (ctg(\alpha) + ctg(\theta)) \cdot \sin \alpha$, valore di progetto della forza di taglio che può essere sopportato dall'armatura a taglio alla tensione di snervamento delle armature;
- $V_{Rd,max} = 0.9 \cdot d \cdot b_w \cdot f'_{cd} \cdot \frac{ctg(\alpha) + ctg(\theta)}{1 + ctg^2(\theta)}$, Valore di progetto della massima forza di taglio che può essere sopportato dall'elemento, limitato dalla rottura delle bielle compresse.

Nelle espressioni precedenti, i simboli hanno i seguenti significati:

- $k = 1 + \sqrt{\frac{200}{d}} \leq 2.0$, con d espresso in mm;
- $\rho_I = \frac{A_{SI}}{b_w \cdot d} \leq 0.02$ è il rapporto geometrico di armatura longitudinale;
- A_{SI} è l'area dell'armatura tesa;
- b_w è la larghezza minima della sezione in zona tesa;
- $\sigma_{cp} = \frac{N_{Ed}}{A_c} < 0.2 \cdot f_{cd}$ è la tensione media di compressione della sezione;
- A_c è l'area della sezione in calcestruzzo;
- $v_{\min} = 0.035 \cdot k^{3/2} \cdot f_{ck}^{1/2}$;
- A_{sw} è l'area della sezione trasversale dell'armatura a taglio;
- s è il passo delle staffe;
- f_{yd} è la tensione di snervamento di progetto dell'armatura a taglio
- α è l'inclinazione dell'armatura resistente a taglio rispetto all'asse dell'elemento;
- θ è l'inclinazione della biella di calcestruzzo compressa e deve essere $1 \leq \cot \theta \leq 2.5$

11.2. VERIFICA AGLI STATI LIMITE DI ESERCIZIO

Per gli Stati Limite di Esercizio occorre verificare che l'ampiezza delle fessure w_k , per gli elementi con armature lente, sia al di sotto del valore limite fissato per le classi di esposizione in oggetto.

In particolare, devono essere rispettati i seguenti limiti:

- Combinazione di carico quasi permanente: $w_k = 0.2mm$;
- Combinazione di carico frequente: $w_k = 0.3mm$;

L'ampiezza caratteristica w_k delle lesioni si valuta attraverso l'espressione:

$$w_k = s_{r,max} (\varepsilon_{sm} - \varepsilon_{cm})$$

Dove:

$s_{r,max}$ è il massimo interasse tra le fessure;

ε_{sm} è il valor medio della deformazione nell'acciaio.

ε_{cm} è il valor medio della deformazione nel calcestruzzo fra le fessure.

La differenza $\varepsilon_{sm} - \varepsilon_{cm}$ può valutarsi attraverso l'espressione:

$$\varepsilon_{sm} - \varepsilon_{cm} = \frac{\sigma_s - \frac{k_t}{\rho_{p,eff}} (1 + \alpha_e \rho_{p,eff})}{E_s} \geq 0.6 \frac{\sigma_s}{E_s}$$

Dove:

σ_s è la tensione nell'acciaio calcolata in sezione parzializzata;

E_s è il modulo elastico dell'acciaio;

$\rho_{p,eff}$ è il rapporto tra l'area dell'armatura tesa e l'area effettiva di calcestruzzo in trazione;

α_e è il rapporto tra il modulo elastico dell'acciaio e quello del calcestruzzo

$k_t=0.4$ (carico di lunga durata).

Detta s la distanza massima tra le barre di armatura, il massimo interasse tra le fessure si può valutare attraverso la seguente espressione:

$$\begin{cases} s_{r,max} = k_3 c + k_1 k_2 k_4 \frac{\phi}{\rho_{p,eff}} & \text{se } s \leq 5(c + \phi/2) \\ s_{r,max} = 1.3 * (H - y_n) & \text{se } s > 5(c + \phi/2) \end{cases}$$

Dove:

c è il copriferro (distanza tra bordo del calcestruzzo e l'armatura; assunto uguale a 4cm);

y_n è la distanza dell'asse neutro dal lembo superiore;

ϕ è il diametro delle barre;

H è l'altezza della sezione;

$k_1=0.8$ (per barre ad aderenza migliorata);

$k_2=0.5$ (per flessione);

$k_3=3.4$ (valore consigliato);

$k_4=0.425$ (valore consigliato).

11.3. VERIFICA AGLI STATI LIMITE GEOTECNICI (MURO)

11.3.1. VERIFICA A SCORRIMENTO

La risultante delle azioni orizzontali agenti sul muro deve essere non superiore alla resistenza per attrito disponibile sul piano di imposta. Quest'ultima è pari al prodotto della risultante delle azioni verticali (azioni ortogonali al piano di imposta) per il coefficiente di attrito fondazione-terreno.

Deve essere quindi:

PROGETTAZIONE ATI:

$$\frac{Q_V \cdot \tan(\phi')}{Q_H} \geq 1,1 \quad (\geq 1,0 \text{ con sisma})$$

Dove:

- Q_V è la risultante delle azioni caratteristiche ortogonali al piano di posa;
- Q_H è la risultante delle azioni di progetto parallele al piano di posa;
- $\mu = \tan(\phi')$ coefficiente di attrito fondazione-terreno.

A meno di situazioni particolari, la resistenza passiva offerta dal terreno presente a valle del muro deve essere trascurata. Infatti, questa viene considerata solo nel caso in cui sia presente il dente in fondazione; in questo caso viene considerato solo il 50% della spinta, come indicato nelle NTC 18, in quanto per potere considerare il 100% della spinta passiva è necessario mobilitare di molto il terreno a valle.

11.3.2. VERIFICA A RIBALTAMENTO

La somma dei momenti delle forze esterne agenti sul muro (spinta del terrapieno, sovraccarichi, ...), valutati rispetto allo spigolo di valle della platea di fondazione, deve risultare non superiore alla somma dei momenti dovuti ai pesi propri della struttura (muro in c.a.), del terreno gravante sulla mensola di monte e delle masse eventualmente collegate al muro (ad es. barriere di sicurezza o antirumore), valutati rispetto allo stesso spigolo.

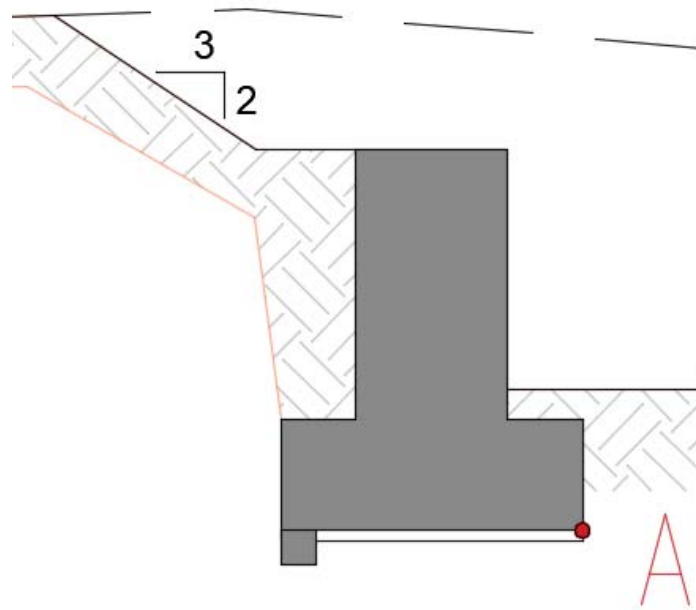


Figura 11.2 Schema verifica a ribaltamento

Dunque, con riferimento al punto A evidenziato in figura, M_{rib} è la risultante dei momenti ribaltanti di progetto, M_{stab} è la risultante dei momenti stabilizzanti di progetto e la verifica al ribaltamento è soddisfatta se, per ogni combinazione di carico, risulta:

$$\frac{M_{stab}}{M_{rib}} \geq 1,15 \quad (\geq 1,0 \text{ con sisma})$$

PROGETTAZIONE ATI:

La verifica verrà eseguita solo nel punto A in quanto l'armatura del muro non permette il ribaltamento della sola mensola.

11.3.3. COLLASSO PER CARICO LIMITE DEL COMPLESSO FONDAZIONE-TERRENO

Vista la natura dei terreni, la valutazione della capacità portante della fondazione del muro di sostegno viene condotta in condizioni non drenate. La formula generale risulta essere:

$$q_{lim} = s_u \cdot N_c \cdot s_c \cdot d_c \cdot i_c \cdot b_c \cdot g_c + q$$

Con:

| | |
|-----------------|--|
| $N_c = 2 + \pi$ | fattori di capacità portante |
| s_c | fattori correttivi che tengono conto della forma della fondazione; |
| d_c | fattori correttivi che tengono conto della profondità del piano di posa; |
| i_c | fattori correttivi che tengono conto dell'inclinazione dei carichi; |
| g_c | fattori correttivi che tengono conto dell'inclinazione del piano campagna; |
| b_c | fattori correttivi che tengono conto dell'inclinazione del piano di posa; |
| q | tensione verticale efficace agente al piano di posa della fondazione; |

Inoltre, si definisce efficace la parte di fondazione reale rispetto alla quale la risultante dei carichi verticali di progetto Q_V risulta centrata. Per fondazioni rettangolari di larghezza B e lunghezza L , indicate con e_B ed e_L le componenti della eccentricità del carico rispettivamente in direzione B e L , le corrispondenti dimensioni efficaci sono:

$$B' = B - 2 e_B \qquad L' = L - 2 e_L$$

Nella figura seguente sono mostrati i valori dei coefficienti sopra citati:

| | <p>Table of inclination, ground, and base factors for the Hansen (1970) equations. See Table 4-5c for equivalent Vesic equations.</p> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|--|---------------|--|--------------------------------------|--|--------------------|--|----------------------------|-----------------------|------------------------------------|--|----------------|--|---|--|-------------------|----------------|--|--|----------------------------------|--|--|--|---------------------|--------------------------------|---|--|---------------------------------------|---|--|--|--|-----------------------------------|---|--|--|---|--|--------------------------------|--|---------------------------------------|--|-------------------|
| <p>Shape and depth factors for use in either the Hansen (1970) or Vesic (1973, 1975b) bearing-capacity equations of Table 4-1. Use s'_c, d'_c when $\phi = 0$ only for Hansen equations. Subscripts H, V for Hansen, Vesic, respectively.</p> <table border="1"> <thead> <tr> <th>Shape factors</th> <th>Depth factors</th> </tr> </thead> <tbody> <tr> <td>$s'_{c(H)} = 0.2 \frac{B'}{L'} \quad (\phi = 0^\circ)$</td> <td>$d'_c = 0.4k \quad (\phi = 0^\circ)$</td> </tr> <tr> <td>$s_{c(H)} = 1.0 + \frac{N_q}{N_c} \cdot \frac{B'}{L'}$</td> <td>$d_c = 1.0 + 0.4k$</td> </tr> <tr> <td>$s_{c(V)} = 1.0 + \frac{N_q}{N_c} \cdot \frac{B}{L}$</td> <td>$k = D/B$ for $D/B \leq 1$</td> </tr> <tr> <td>$s_c = 1.0$ for strip</td> <td>$k = \tan^{-1}(D/B)$ for $D/B > 1$</td> </tr> <tr> <td></td> <td>k in radians</td> </tr> <tr> <td>$s_{q(H)} = 1.0 + \frac{B'}{L'} \sin \phi$</td> <td>$d_q = 1 + 2 \tan \phi (1 - \sin \phi)^2 k$</td> </tr> <tr> <td>$s_{q(V)} = 1.0 + \frac{B}{L} \tan \phi$</td> <td>$k$ defined above</td> </tr> <tr> <td>for all ϕ</td> <td></td> </tr> <tr> <td>$s_{\gamma(H)} = 1.0 - 0.4 \frac{B'}{L'} \geq 0.6$</td> <td>$d_\gamma = 1.00$ for all ϕ</td> </tr> <tr> <td>$s_{\gamma(V)} = 1.0 - 0.4 \frac{B}{L} \geq 0.6$</td> <td></td> </tr> </tbody> </table> | Shape factors | Depth factors | $s'_{c(H)} = 0.2 \frac{B'}{L'} \quad (\phi = 0^\circ)$ | $d'_c = 0.4k \quad (\phi = 0^\circ)$ | $s_{c(H)} = 1.0 + \frac{N_q}{N_c} \cdot \frac{B'}{L'}$ | $d_c = 1.0 + 0.4k$ | $s_{c(V)} = 1.0 + \frac{N_q}{N_c} \cdot \frac{B}{L}$ | $k = D/B$ for $D/B \leq 1$ | $s_c = 1.0$ for strip | $k = \tan^{-1}(D/B)$ for $D/B > 1$ | | k in radians | $s_{q(H)} = 1.0 + \frac{B'}{L'} \sin \phi$ | $d_q = 1 + 2 \tan \phi (1 - \sin \phi)^2 k$ | $s_{q(V)} = 1.0 + \frac{B}{L} \tan \phi$ | k defined above | for all ϕ | | $s_{\gamma(H)} = 1.0 - 0.4 \frac{B'}{L'} \geq 0.6$ | $d_\gamma = 1.00$ for all ϕ | $s_{\gamma(V)} = 1.0 - 0.4 \frac{B}{L} \geq 0.6$ | | <table border="1"> <thead> <tr> <th>Inclination factors</th> <th>Ground factors (base on slope)</th> </tr> </thead> <tbody> <tr> <td>$i'_c = 0.5 - \sqrt{1 - \frac{H_i}{A_f c_a}}$</td> <td>$g'_c = \frac{\beta^\circ}{147^\circ}$</td> </tr> <tr> <td>$i_c = i_q - \frac{1 - i_q}{N_q - 1}$</td> <td>$g_c = 1.0 - \frac{\beta^\circ}{147^\circ}$</td> </tr> <tr> <td>$i_q = \left[1 - \frac{0.5 H_i}{V + A_f c_a \cot \phi} \right]^{2.1}$ $2 \leq \alpha_1 \leq 5$</td> <td>$g_q = g_\gamma = (1 - 0.5 \tan \beta)^\delta$</td> </tr> <tr> <td></td> <td>Base factors (tilted base)</td> </tr> <tr> <td>$i_\gamma = \left[1 - \frac{0.7 H_i}{V + A_f c_a \cot \phi} \right]^{2.2}$</td> <td>$b'_c = \frac{\eta^\circ}{147^\circ} \quad (\phi = 0)$</td> </tr> <tr> <td>$i_\gamma = \left[1 - \frac{(0.7 - \eta^\circ/450^\circ) H_i}{V + A_f c_a \cot \phi} \right]^{2.2}$ $2 \leq \alpha_2 \leq 5$</td> <td>$b_c = 1 - \frac{\eta^\circ}{147^\circ} \quad (\phi > 0)$</td> </tr> <tr> <td></td> <td>$b_q = \exp(-2\eta \tan \phi)$</td> </tr> <tr> <td></td> <td>$b_\gamma = \exp(-2.7\eta \tan \phi)$</td> </tr> <tr> <td></td> <td>η in radians</td> </tr> </tbody> </table> <p>$A_f = B' \cdot L'$</p> | Inclination factors | Ground factors (base on slope) | $i'_c = 0.5 - \sqrt{1 - \frac{H_i}{A_f c_a}}$ | $g'_c = \frac{\beta^\circ}{147^\circ}$ | $i_c = i_q - \frac{1 - i_q}{N_q - 1}$ | $g_c = 1.0 - \frac{\beta^\circ}{147^\circ}$ | $i_q = \left[1 - \frac{0.5 H_i}{V + A_f c_a \cot \phi} \right]^{2.1}$ $2 \leq \alpha_1 \leq 5$ | $g_q = g_\gamma = (1 - 0.5 \tan \beta)^\delta$ | | Base factors (tilted base) | $i_\gamma = \left[1 - \frac{0.7 H_i}{V + A_f c_a \cot \phi} \right]^{2.2}$ | $b'_c = \frac{\eta^\circ}{147^\circ} \quad (\phi = 0)$ | $i_\gamma = \left[1 - \frac{(0.7 - \eta^\circ/450^\circ) H_i}{V + A_f c_a \cot \phi} \right]^{2.2}$ $2 \leq \alpha_2 \leq 5$ | $b_c = 1 - \frac{\eta^\circ}{147^\circ} \quad (\phi > 0)$ | | $b_q = \exp(-2\eta \tan \phi)$ | | $b_\gamma = \exp(-2.7\eta \tan \phi)$ | | η in radians |
| Shape factors | Depth factors | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $s'_{c(H)} = 0.2 \frac{B'}{L'} \quad (\phi = 0^\circ)$ | $d'_c = 0.4k \quad (\phi = 0^\circ)$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $s_{c(H)} = 1.0 + \frac{N_q}{N_c} \cdot \frac{B'}{L'}$ | $d_c = 1.0 + 0.4k$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $s_{c(V)} = 1.0 + \frac{N_q}{N_c} \cdot \frac{B}{L}$ | $k = D/B$ for $D/B \leq 1$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $s_c = 1.0$ for strip | $k = \tan^{-1}(D/B)$ for $D/B > 1$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | k in radians | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $s_{q(H)} = 1.0 + \frac{B'}{L'} \sin \phi$ | $d_q = 1 + 2 \tan \phi (1 - \sin \phi)^2 k$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $s_{q(V)} = 1.0 + \frac{B}{L} \tan \phi$ | k defined above | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| for all ϕ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $s_{\gamma(H)} = 1.0 - 0.4 \frac{B'}{L'} \geq 0.6$ | $d_\gamma = 1.00$ for all ϕ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| Inclination factors | Ground factors (base on slope) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $i'_c = 0.5 - \sqrt{1 - \frac{H_i}{A_f c_a}}$ | $g'_c = \frac{\beta^\circ}{147^\circ}$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| $i_c = i_q - \frac{1 - i_q}{N_q - 1}$ | $g_c = 1.0 - \frac{\beta^\circ}{147^\circ}$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | $b_q = \exp(-2\eta \tan \phi)$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | $b_\gamma = \exp(-2.7\eta \tan \phi)$ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | η in radians | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <p>Notes:</p> <ol style="list-style-type: none"> Note use of "effective" base dimensions B', L' by Hansen but not by Vesic. The values above are consistent with either a vertical load or a vertical load accompanied by a horizontal load H_B. With a vertical load and a load H_L (and either $H_B = 0$ or $H_B > 0$) you may have to compute two sets of shape s_i and d_i as $s_{i,B}, s_{i,L}$ and $d_{i,B}, d_{i,L}$. For i, L subscripts of Eq. (4-2), presented in Sec. 4-6, use ratio L'/B' or D/L'. | <p>Notes:</p> <ol style="list-style-type: none"> Use H_i as either H_B or H_L, or both if $H_L > 0$. Hansen (1970) did not give an i_c for $\phi > 0$. The value above is from Hansen (1961) and also used by Vesic. Variable c_a = base adhesion, on the order of 0.6 to 1.0 \times base cohesion. Refer to sketch for identification of angles η and β, footing depth D, location of H_i (parallel and at top of base slab; usually also produces eccentricity). Especially note V = force normal to base and is not the resultant R from combining V and H_i. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Figura 11.3 Parametri per la valutazione della capacit  portante

12. RISULTATI DELL'ANALISI

Si riportano nel seguito i risultati per le varie combinazioni nei diversi elementi strutturali.

12.1. SLU

Nel presente capitolo sono riportati i risultati principali relativi alla distribuzione delle azioni interne, in termini di azione assiale, taglio e momento flettente per varie combinazioni di calcolo allo Stato Limite ultimo.

Di seguito si riportano i diagrammi delle azioni interne:

PROGETTAZIONE ATI:

- SLU/SLV – Momento Flettente

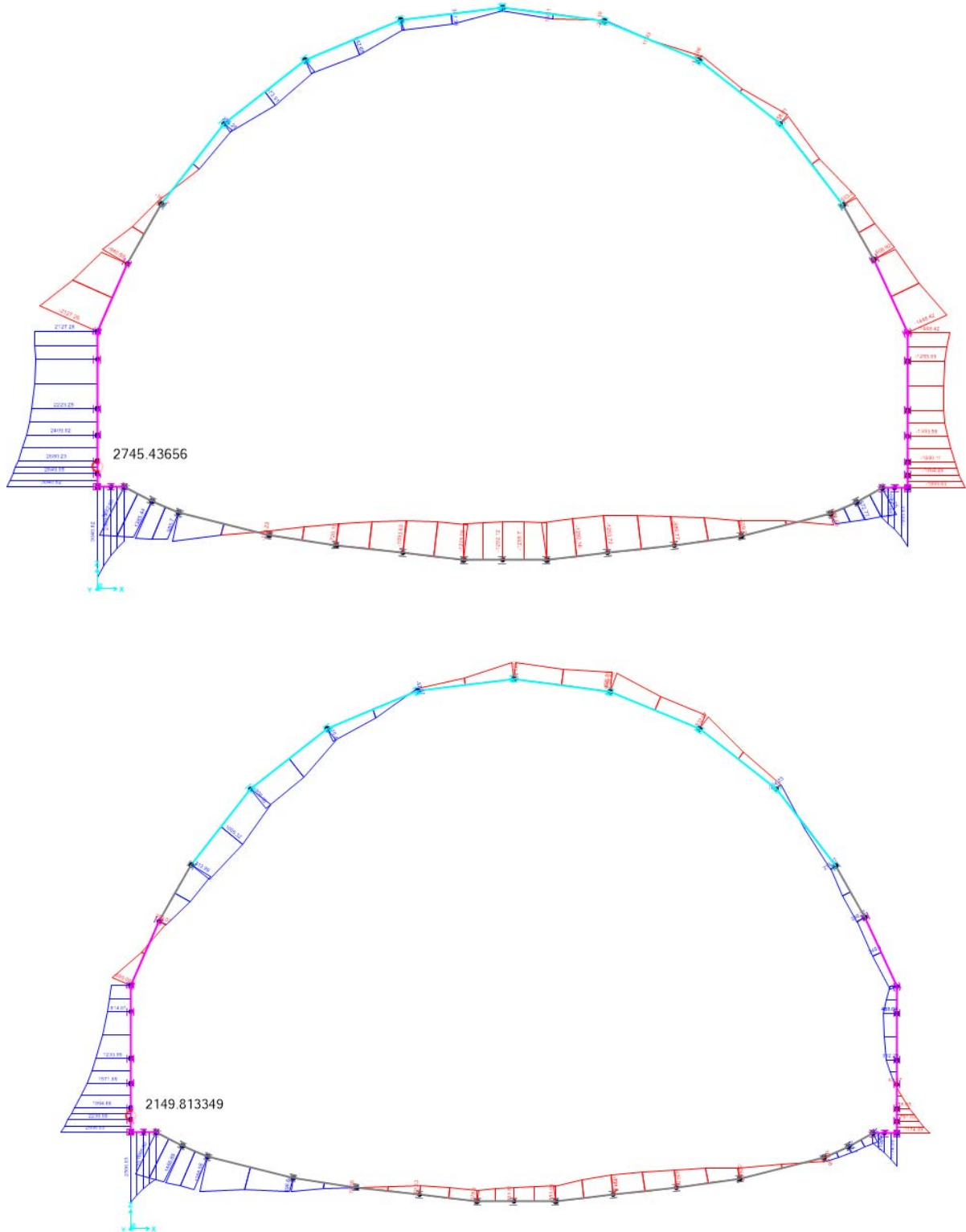


Figura 12.1 Momenti carico asimmetrico - SLU/SLV

PROGETTAZIONE ATI:

- SLU/SLV – Taglio

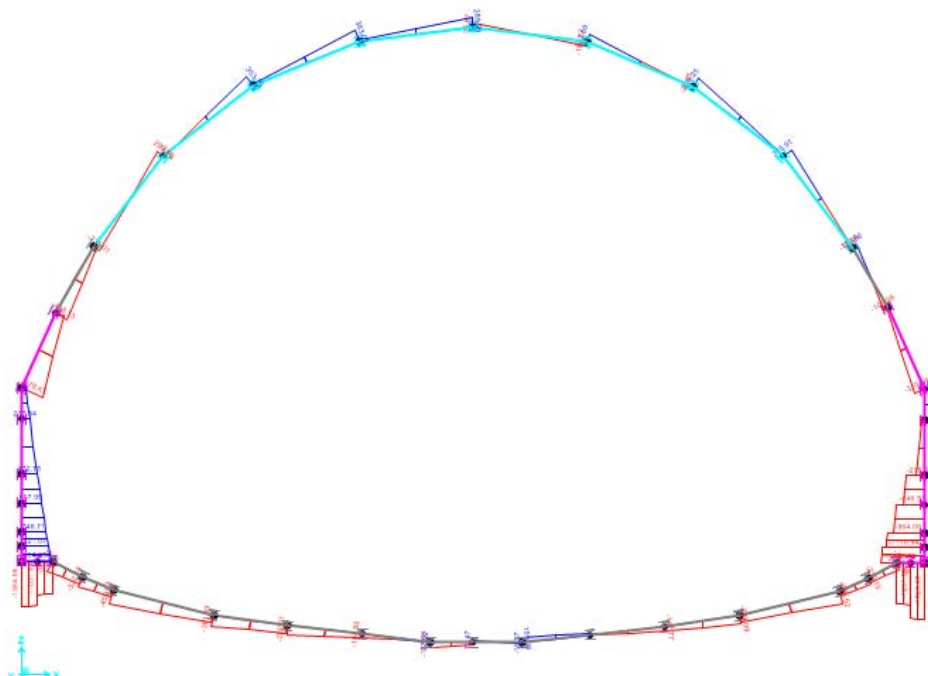
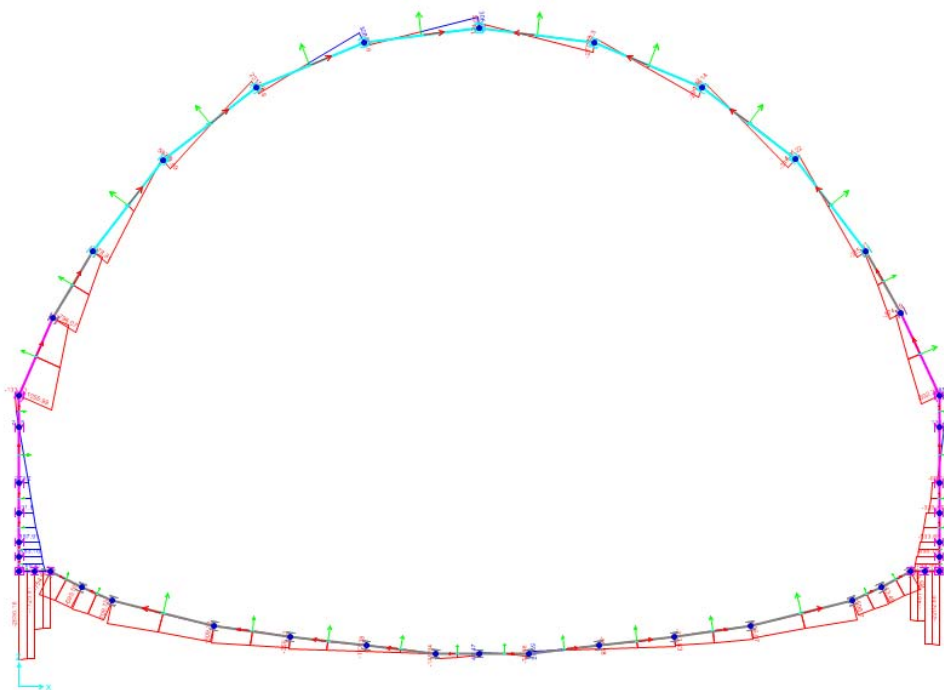


Figura 12.2 Taglio – SLU/SLV

PROGETTAZIONE ATI:

- SLU – Azione assiale

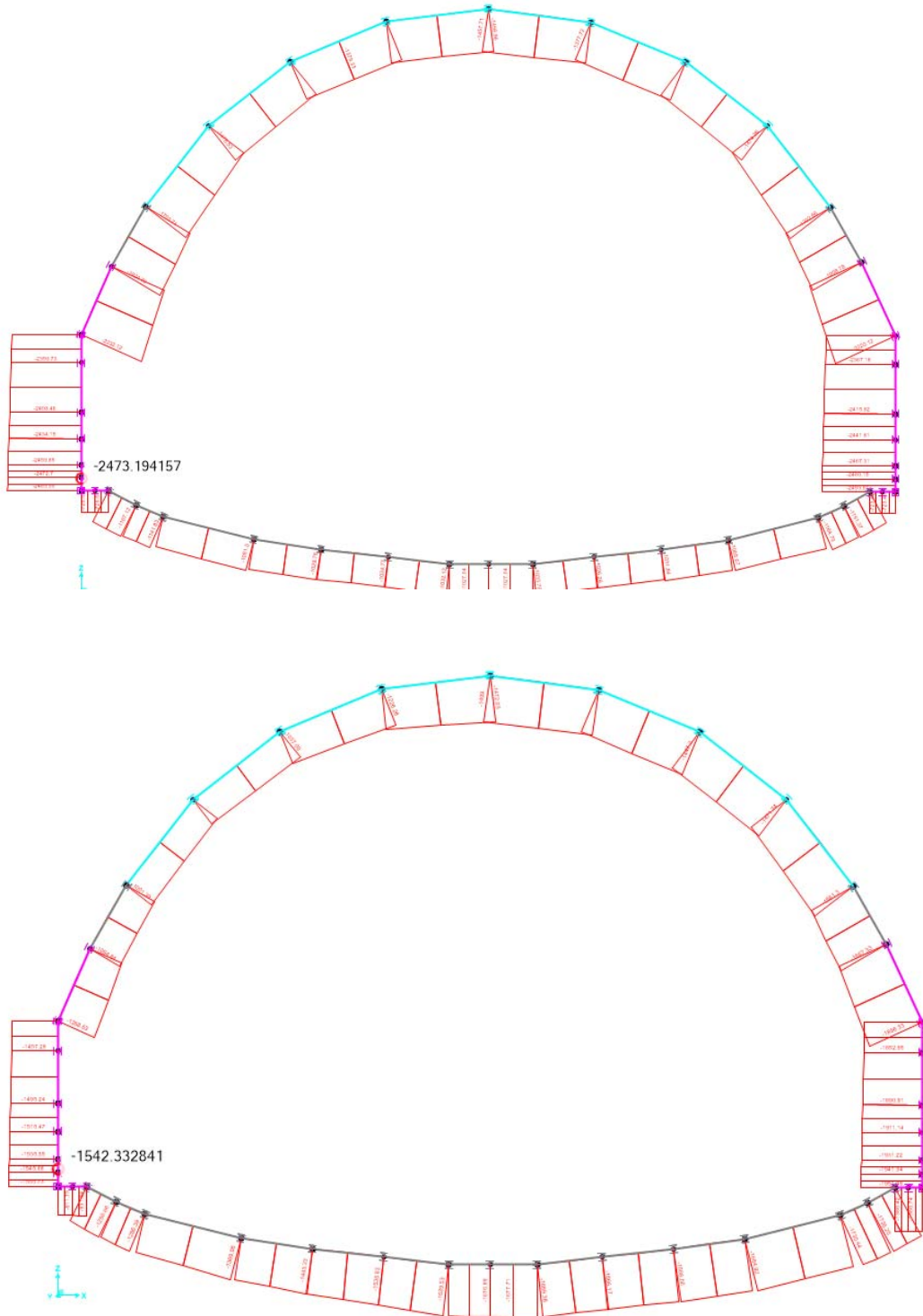


Figura 12.3 Azione assiale carico uniforme -SLU/SLV

PROGETTAZIONE ATI:

- SLE- Rara/SLD – Momento

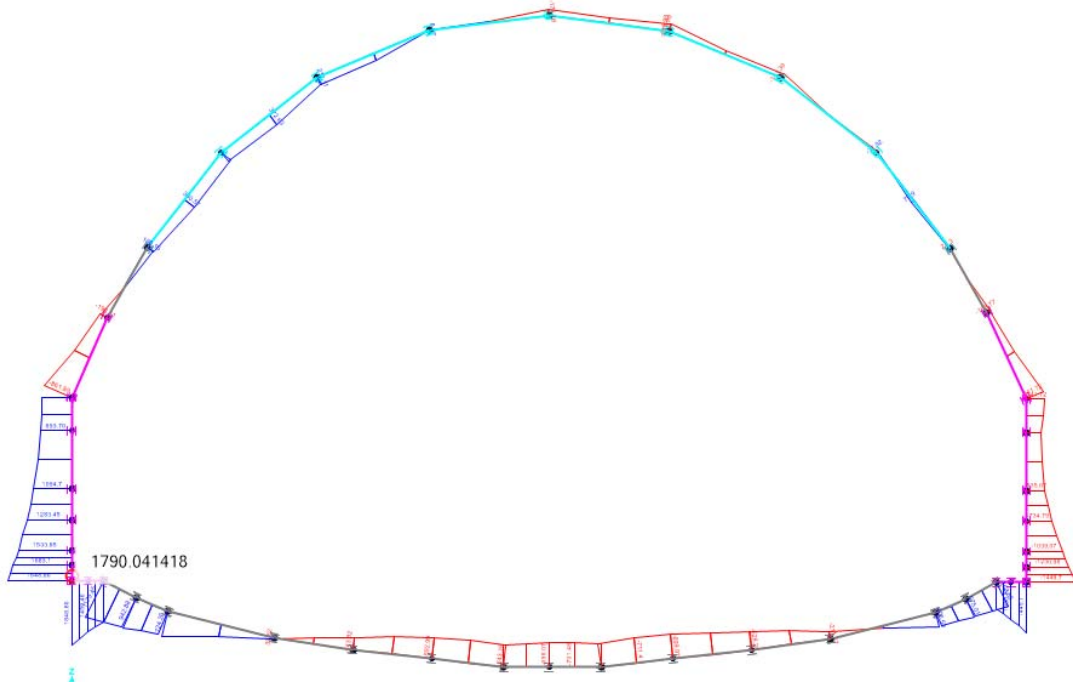


Figura 12.4 Momento – SLE rara/SLD

- SLE- Rara/SLD – azione assiale

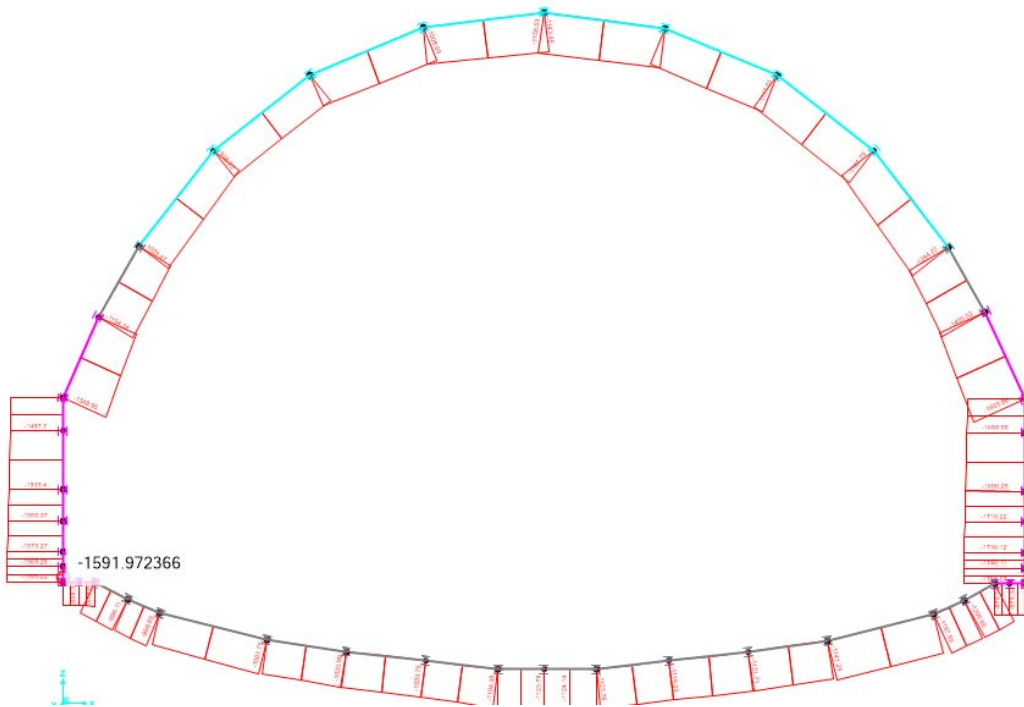


Figura 12.5 azione assiale– SLE rara/SLD

PROGETTAZIONE ATI:

- SLE- Rara/SLD – spostamento

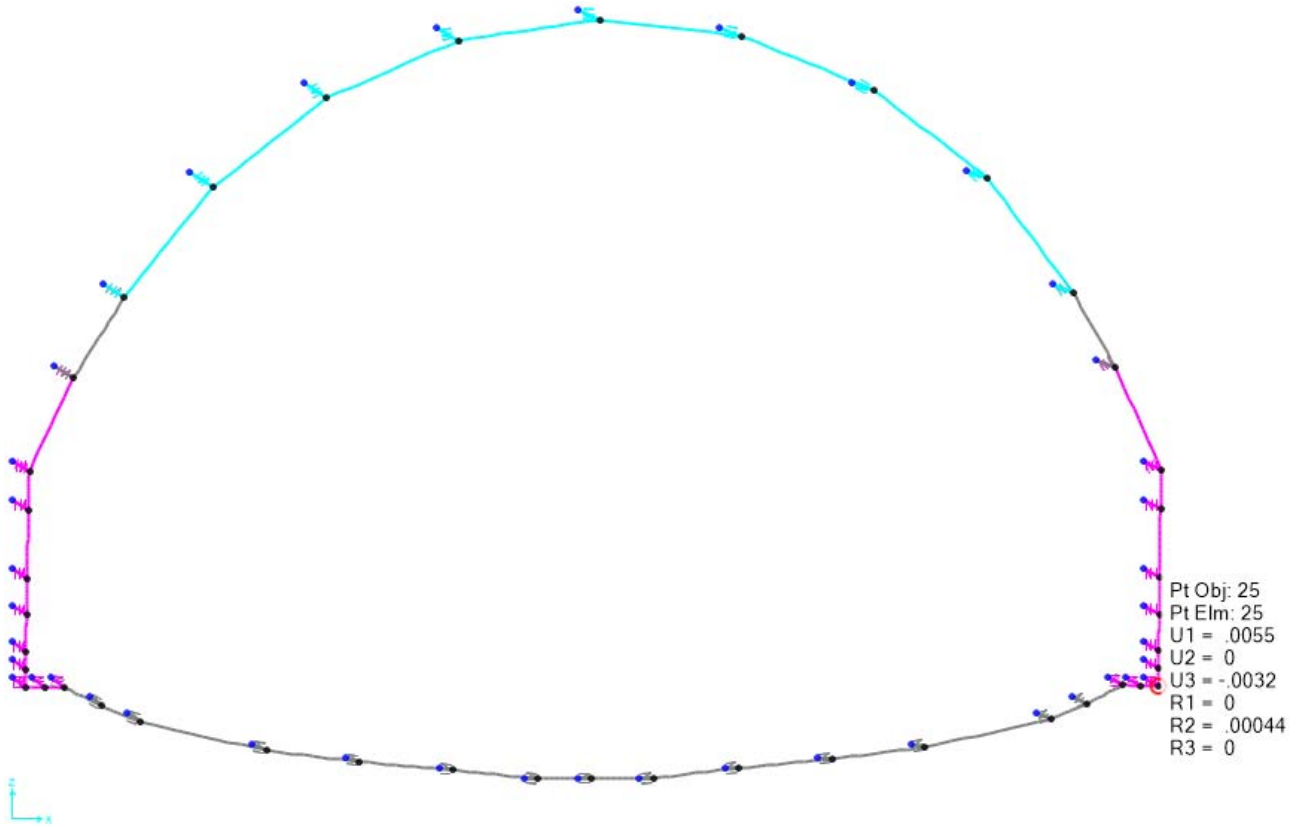


Figura 12.6 Spostamento – SLE rara

- SLE- Frequente – Momento

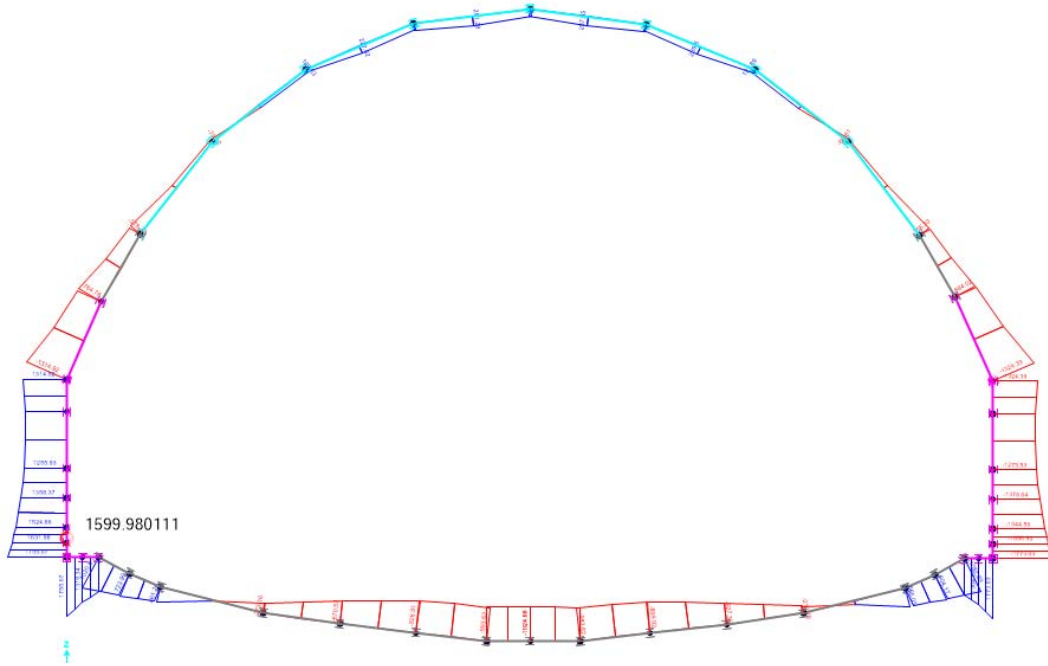


Figura 12.7 Momento – SLE Freq

- SLE Frequente - Azione assiale

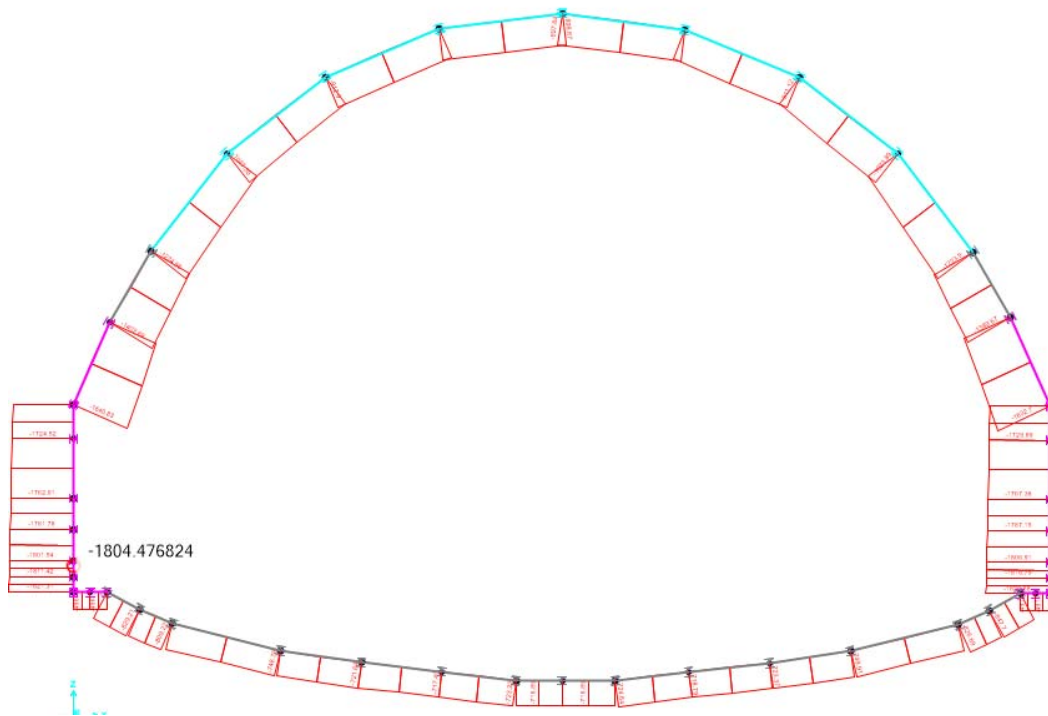


Figura 12.8 Azione Assiale – SLE Freq

PROGETTAZIONE ATI:

- SLE- Frequente – Spostamento

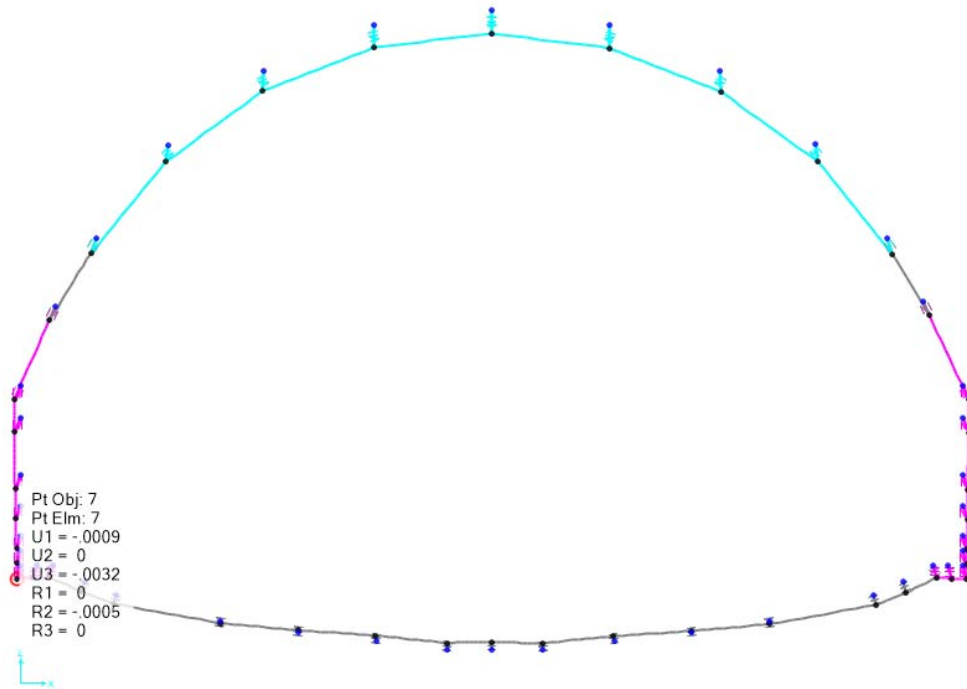


Figura 12.9 Spostamento – SLE Freq

- SLE- Quasi permanente – Momento

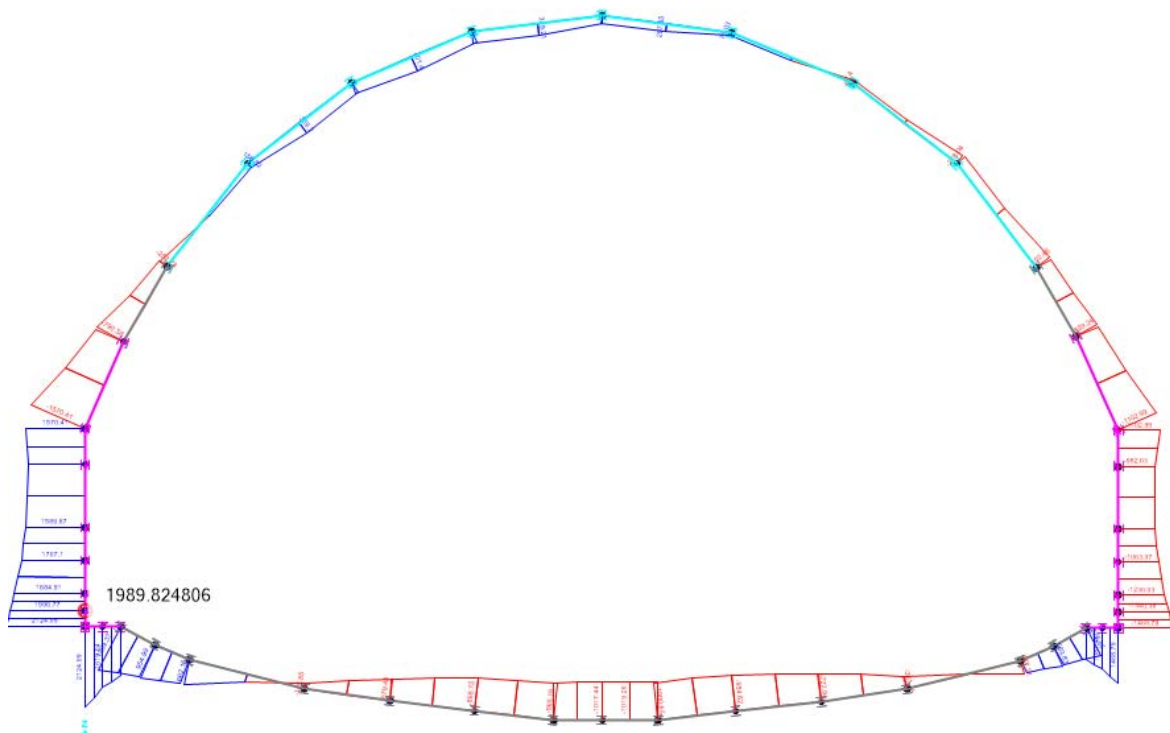


Figura 12.10 Momento – SLE Quasi Permanente

PROGETTAZIONE ATI:

- SLE- Quasi permanente – Azione assiale

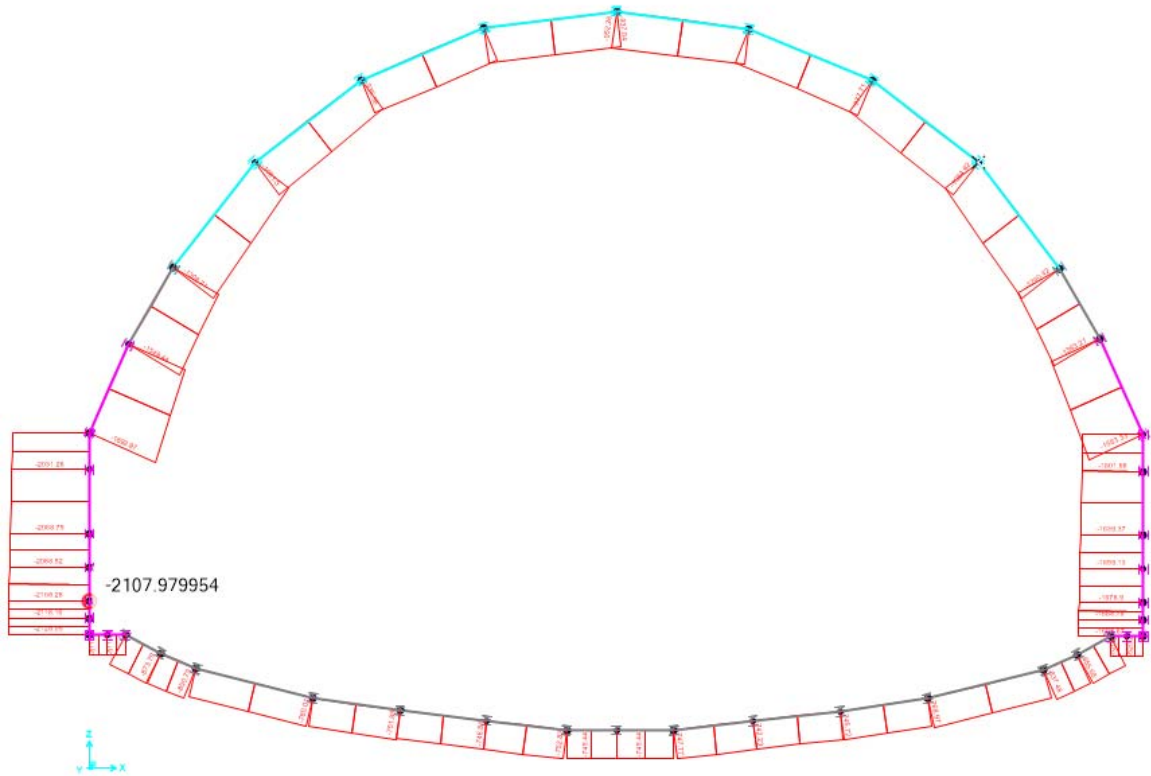


Figura 12.11 Azione assiale – SLE Quasi Permanente

- SLE- Quasi permanente – Spostamento

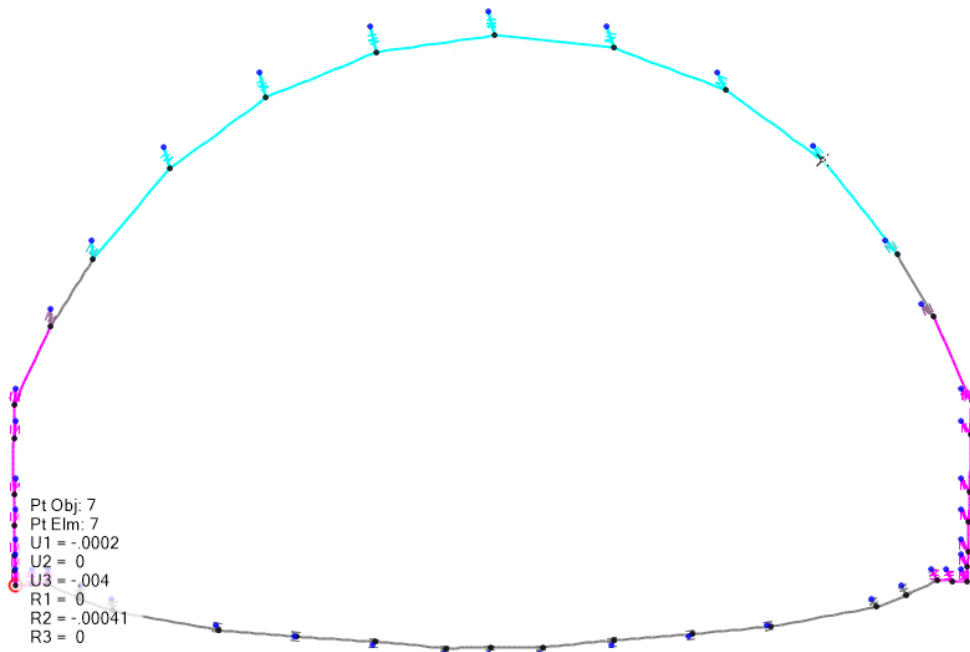


Figura 12.12 Spostamento – SLE Quasi Permanente

PROGETTAZIONE ATI:

13. VERIFICHE GALLERIA

13.1. VERIFICHE SLU

Il momento e il taglio resistente vengono valutati attraverso le formule riportati al capitolo 11.

Per ottimizzare l'armatura di taglio si farà riferimento per la verifica, al puntone ad inclinazione variabile e si valuterà l'inclinazione del puntone tale che: $V_{Rd,s} = V_{Rd,max}$

Di seguito verranno riportate le 4 combinazioni più gravose precedentemente valutate per le 4 sezioni: Arco inferiore, arco superiore, piedritto e reni.

| SEZ CALOTTA h=1.00m | | |
|---------------------|-----------------|--------------------|
| b | 1000 | [mm] |
| h | 1000 | [mm] |
| As | 1900,66 | [mm ²] |
| ϕ_{base} | 22 | 200 |
| ϕ_{rinf} | 0 | 200 |
| STATO LIMITE ULTIMO | N max | |
| | N _{Ed} | -925,314 kN |
| | M _{Ed} | 230,5079 kNm |
| | N min | |
| | N _{Ed} | -1963,713 kN |
| | M _{Ed} | -483,5171 kNm |
| | M max | |
| | N _{Ed} | -1194,768 kN |
| | M _{Ed} | 1007,9418 kNm |
| | M min | |
| | N _{Ed} | -1875,523 kN |
| | M _{Ed} | -738,6444 kNm |

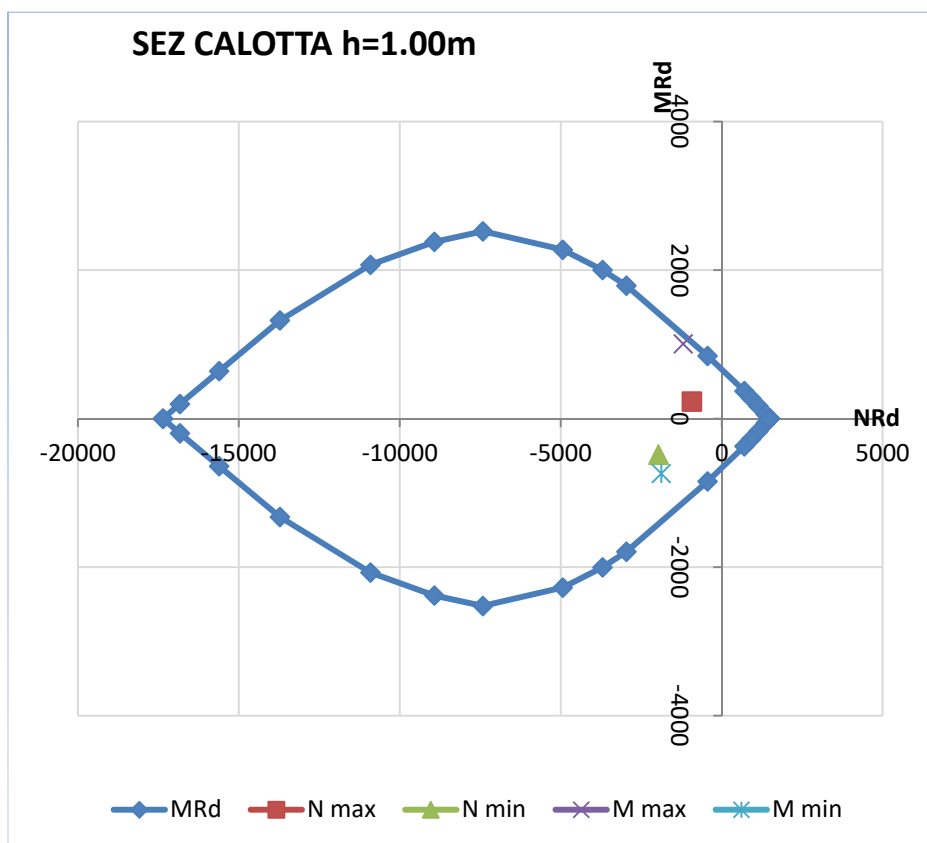


Figura 13.1 Dominio Arco superiore

| SEZ RENI h=1.20m | | |
|---------------------|-----------------|--------------------|
| b | 1000 | [mm] |
| h | 1200 | [mm] |
| As | 2654,65 | [mm ²] |
| ϕ_{base} | 26 | 200 |
| ϕ_{rinf} | 0 | 200 |
| STATO LIMITE ULTIMO | N max | |
| | N _{Ed} | -1016,476 kN |
| | M _{Ed} | 647,9404 kNm |
| | N min | |
| | N _{Ed} | -2312,55 kN |
| | M _{Ed} | -1251,9025 kNm |
| | M max | |
| | N _{Ed} | -1274,102 kN |
| | M _{Ed} | 817,2634 kNm |
| | M min | |
| | N _{Ed} | -2312,55 kN |
| | M _{Ed} | -1251,9025 kNm |

PROGETTAZIONE ATI:

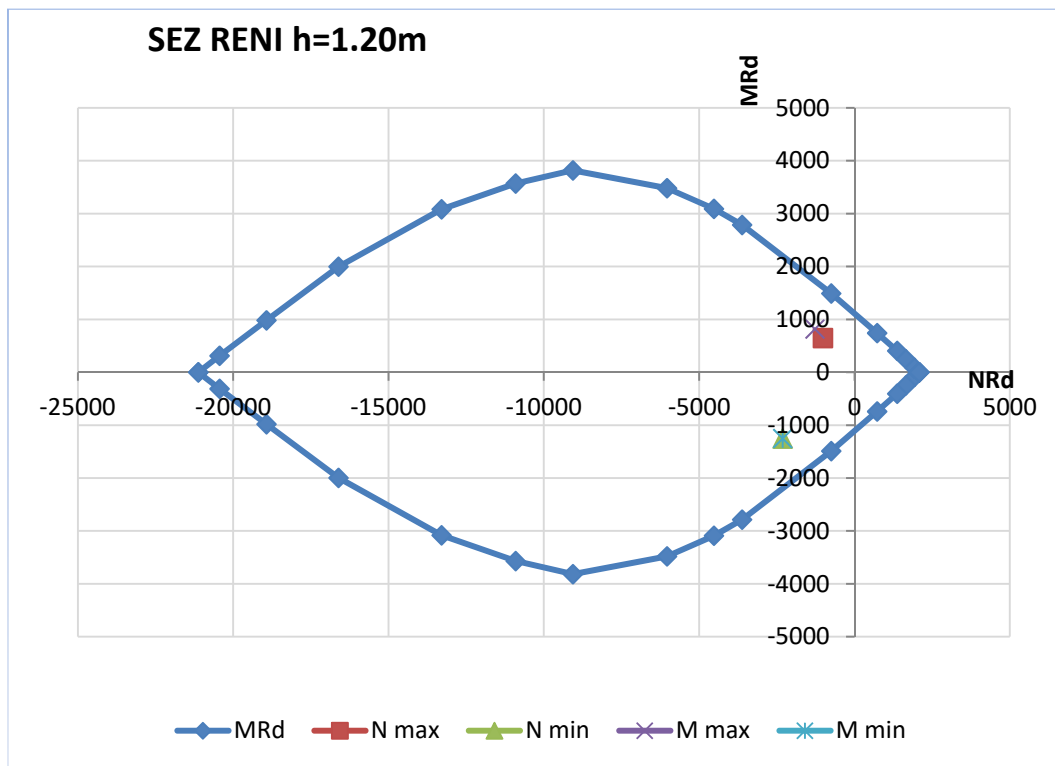


Figura 13.2 Dominio Reni

| SEZ PIEDRITTI h=1.50m | | |
|-----------------------|------------|--------------------|
| b | 1000 | [mm] |
| h | 1500 | [mm] |
| As | 5309,29 | [mm ²] |
| ϕ_{base} | 26 | 200 |
| ϕ_{rinf} | 26 | 200 |
| N max | | |
| N _{Ed} | -1131,182 | kN |
| M _{Ed} | 270,6065 | kNm |
| N min | | |
| N _{Ed} | -3091,871 | kN |
| M _{Ed} | 2750,0539 | kNm |
| M max | | |
| N _{Ed} | -3076,174 | kN |
| M _{Ed} | 2849,0513 | kNm |
| M min | | |
| N _{Ed} | -2800,929 | kN |
| M _{Ed} | -2342,6476 | kNm |

STATO LIMITE ULTIMO

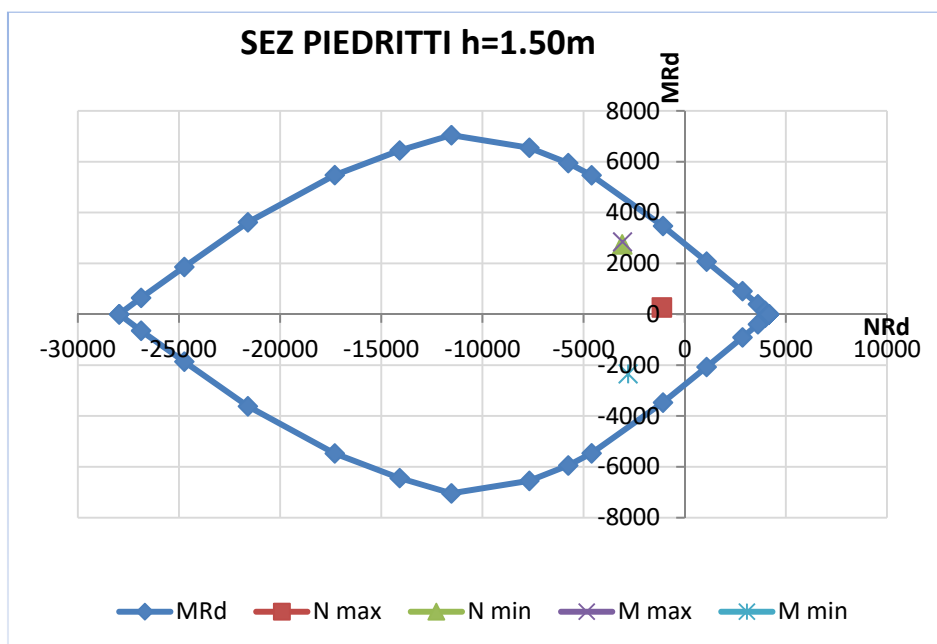


Figura 13.3 Dominio Piedritti

Si riportano di seguito le verifiche a taglio:

- Arco superiore

| Dati di input | |
|--|--|
| Rck | 35 N/mm ² |
| fck | 27 N/mm ² |
| Valore medio della resistenza a trazione | $f_{ctm} = 2,7 \text{ N/mm}^2 = 0.3 \times f_{ck}^{2/3}$ |
| Coefficiente sicurezza cls | $\gamma_c = 1,5$ Fattore di confidenza FC = |
| Coefficiente carichi lunga durata | $\alpha_{cc} = 0,85$ |
| fcd=resistenza di calcolo del cls | $f_{cd} = 15,33 \text{ N/mm}^2 = \alpha_{cc} \times f_{ck} / \gamma_c$ |
| Resistenza caratteristica di snervamento acciaio | $f_{yk} = 450 \text{ N/mm}^2$ |
| Coefficiente sicurezza acciaio | $\gamma_s = 1,15$ |
| Snervamento di calcolo acciaio | $f_{yd} = 391 \text{ N/mm}^2 = f_{yk} / \gamma_s$ |
| Forza di taglio di calcolo | $V_{sd} = 599,2 \text{ kN}$ |
| Forza assiale di calcolo | $N_{sd} = 925,31 \text{ kN}$ |
| Larghezza sezione | $b_w = 100 \text{ cm} = 1000 \text{ mm}$ |
| altezza della sezione | $H = 100 \text{ cm} = 1000 \text{ mm}$ |
| Copriferro | $c = 5 \text{ cm}$ |
| Diametro barre superiori | $\phi_2 = 22 \text{ mm}$ (armatura compressa) |
| Diametro barre inferiori | $\phi_1 = 22 \text{ mm}$ (armatura tesa) |
| Diametro staffe | $\phi_{st} = 12 \text{ mm}$ |
| Numero di barre superiori | $N_2 = 5$ |
| Numero di barre inferiori | $N_1 = 5$ |
| altezza utile della sezione | $d = 92,7 \text{ cm} = 927 \text{ mm}$ |

| | | |
|--|--|--|
| Resistenza di calcolo dell'elemento con armatura a taglio | | (rif. cap. 4.1.2.1.3.2 del D.M. 2008) |
| Verifica delle bielle compresse: Vr_{cd} | | |
| Vr _{cd} = [0.9 x d x b _w x α _c x f _{cd} x (cotgα + cotgθ)] / [1 + (cotgθ) ²] | | |
| Definizione del coefficiente maggiorativo α _c | α _{cp} < 0,00 => α _c = 1 | membrature non compresse |
| 0,00 =< α _{cp} < 3,83 => α _c = 0,94 | | |
| 3,83 =< α _{cp} <= 7,66 => α _c = 1,25 | | |
| 7,66 < α _{cp} < 15,33 => α _c = 2,65 | | membrature fortemente compresse |
| Essendo α _{cp} = -0,93 N/mm ² | si assume quindi | α _c = 1 |
| Resistenza a compressione ridotta | f _{cd} = 7,66 N/mm ² | = 0.5 x f _{cd} |
| Angolo di inclinazione dell'armatura a taglio | α = 90° | (45° per ferri piegati e 90° per staffe) |
| | α = 1,57 rad | |
| Angolo di inclinazione dei puntoni compressi | θ = 45° | (compreso tra 21.8° e 45°) |
| | θ = 0,79 rad | |
| Vr_{cd} = 3197,11 kN | | OK - VERIFICA SODDISFATTA |
| Verifica dell'armatura a taglio: Vr_{sd} | | |
| Vr _{sd} = 0.9 x d x (A _{sw} / s) x f _{yd} x (cotgα + cotgθ) x sinα | | |
| Passo delle staffe | s = 20 cm | 200 mm |
| Diametro staffe | φ _{st} = 12 mm | |
| Braccia resistenti | n = 4 | |
| Area armatura a taglio | A _{sw} = 4,52 cm ² | 452 mm ² |
| Percentuale minima di armatura | ρ _{w,min} = 0,0009 | = 0.08 x (F _{ck} ^{0.5}) / F _{yk} |
| Area minima di armatura a taglio | A _{w,min} = 184,92 mm ² | = ρ _{w,min} x s x B _w x senα (EC2-Par.9.2.2) |

- **Rene**

| | | |
|--|---|--|
| Dati di input | | |
| R _{ck} | 35 N/mm ² | |
| f _{ck} | 27 N/mm ² | |
| Valore medio della resistenza a trazione | f _{ctm} = 2,7 N/mm ² | = 0.3 x f _{ck} ^(2/3) |
| Coefficiente sicurezza cls | γ _c = 1,5 | Fattore di confidenza FC = 1 |
| Coefficiente carichi lunga durata | α _{cc} = 0,85 | |
| f _{cd} =resistenza di calcolo del cls | f _{cd} = 15,33 N/mm ² | = α _{cc} x f _{ck} / γ _c |
| Resistenza caratteristica di snervamento acciaio | f _{yk} = 450 N/mm ² | |
| Coefficiente sicurezza acciaio | γ _s = 1,15 | |
| Snervamento di calcolo acciaio | f _{yd} = 391 N/mm ² | = f _{yk} / γ _s |
| Forza di taglio di calcolo | V _{sd} = 796,1 kN | |
| Forza assiale di calcolo | N _{sd} = 1061 kN | |
| Larghezza sezione | b _w = 100 cm | = 1000 mm |
| altezza della sezione | H = 120 cm | = 1200 mm |
| Copriferro | c = 5 cm | |
| Diametro barre superiori | φ ₂ = 26 mm | (armatura compressa) |
| Diametro barre inferiori | φ ₁ = 26 mm | (armatura tesa) |
| Diametro staffe | φ _{st} = 12 mm | |
| Numero di barre superiori | N ₂ = 5 | |
| Numero di barre inferiori | N ₁ = 5 | |
| altezza utile della sezione | d = 112,5 cm | = 1125 mm |

| | | | |
|--|--|--|----------|
| Resistenza di calcolo dell'elemento con armatura a taglio | | (rif. cap. 4.1.2.1.3.2 del D.M. 2008) | |
| Verifica delle bielle compresse: Vr_{cd} | | | |
| Vr _{cd} = [0.9 x d x b _w x α _c x f _{cd} x (cotgα + cotgθ)] / [1 + (cotgθ) ²] | | | |
| Definizione del coefficiente maggiorativo α _c | α _{cp} < 0,00 => α _c = 1 | 1 membrature non compresse | |
| 0,00 =< α _{cp} < 3,83 => α _c = 0,94 | 3,83 =< α _{cp} <= 7,66 => α _c = 1,25 | ↓ | |
| 7,66 < α _{cp} < 15,33 => α _c = 2,64 | membrature fortemente compresse | | |
| Essendo α _{cp} = -0,88 N/mm ² | si assume quindi α _c = | | 1 |
| Resistenza a compressione ridotta | f _{cd} = 7,66 N/mm ² | = 0.5 x f _{cd} | |
| Angolo di inclinazione dell'armatura a taglio | α = 90° | (45° per ferri piegati e 90° per staffe) | |
| | α = 1,57 rad | | |
| Angolo di inclinazione dei puntoni compressi | θ = 45° | (compreso tra 21.8° e 45°) | |
| | θ = 0,79 rad | | |
| Vr_{cd} = 3879,98 kN | | OK - VERIFICA SODDISFATTA | |
| Verifica dell'armatura a taglio: Vr_{sd} | | | |
| Vr _{sd} = 0.9 x d x (A _{sw} / s) x f _{yd} x (cotgα + cotgθ) x sinα | | | |
| Passo delle staffe | s = 20 cm | 200 mm | |
| Diametro staffe | φ _{st} = 12 mm | | |
| Braccia resistenti | n = 4 | | |
| Area armatura a taglio | A _{sw} = 4,52 cm ² | 452 mm ² | |
| Percentuale minima di armatura | ρ _{w,min} = 0,0009 mm | = 0.08 x (F _{ck} ^{0.5}) / F _{yk} | |
| Area minima di armatura a taglio | A _{w,min} = 184,92 mm ² | = ρ _{w,min} x s x B _w x senα (EC2-Par.9.2.2) | |
| Vr_{sd} = 896,17 kN | | OK - VERIFICA SODDISFATTA | |

- Piedritto

| | | | |
|--|---|--|--|
| Dati di input | | | |
| R _{ck} | 35 N/mm ² | | |
| f _{ck} | 27 N/mm ² | | |
| Valore medio della resistenza a trazione | f _{ctm} = 2,7 N/mm ² | = 0.3 x f _{ck} ^(2/3) | |
| Coefficiente sicurezza cls | γ _c = 1,5 | Fattore di confidenza FC = 1 | |
| Coefficiente carichi lunga durata | α _{cc} = 0,85 | | |
| f _{cd} =resistenza di calcolo del cls | f _{cd} = 15,33 N/mm ² | = α _{cc} x f _{ck} / γ _c | |
| Resistenza caratteristica di snervamento acciaio | f _{yk} = 450 N/mm ² | | |
| Coefficiente sicurezza acciaio | γ _s = 1,15 | | |
| Snervamento di calcolo acciaio | f _{yd} = 391 N/mm ² | = f _{yd} / γ _s | |
| Forza di taglio di calcolo | V _{sd} = 1056,0 kN | | |
| Forza assiale di calcolo | N _{sd} = 1131,18 kN | | |
| Larghezza sezione | b _w = 100 cm | = 1000 mm | |
| altezza della sezione | H = 150 cm | = 1500 mm | |
| Copriferro | c = 5 cm | | |
| Diametro barre superiori | φ ₂ = 26 mm | (armatura compressa) | |
| Diametro barre inferiori | φ ₁ = 26 mm | (armatura tesa) | |
| Diametro staffe | φ _{st} = 12 mm | | |
| Numero di barre superiori | N ₂ = 10 | | |
| Numero di barre inferiori | N ₁ = 10 | | |
| altezza utile della sezione | d = 142,5 cm | = 1425 mm | |

| | | |
|--|---|--|
| Resistenza di calcolo dell'elemento con armatura a taglio | | (rif. cap. 4.1.2.1.3.2 del D.M. 2008) |
| Verifica delle bielle compresse: Vr_{cd} | | |
| Vr _{cd} = [0.9 x d x b _w x α _c x f _{cd} x (cotgα + cotgθ)] / [1 + (cotgθ) ²] | | |
| Definizione del coefficiente maggiorativo α _c | α _{cp} < 0,00 => α _c = 1 membrature non compresse | |
| | 0,00 =< α _{cp} < 3,83 => α _c = 0,95 | |
| | 3,83 =< α _{cp} <= 7,66 => α _c = 1,25 | |
| | 7,66 < α _{cp} < 15,33 => α _c = 2,62 membrature fortemente compresse | |
| Essendo | α _{cp} = -0,75 N/mm ² | si assume quindi α _c = 1 |
| Resistenza a compressione ridotta | f _{cd} = 7,66 N/mm ² | = 0.5 x f _{cd} |
| Angolo di inclinazione dell'armatura a taglio | α = 90° | (45° per ferri piegati e 90° per staffe) |
| | α = 1,57 rad | |
| Angolo di inclinazione dei puntoni compressi | θ = 45° | (compreso tra 21.8° e 45°) |
| | θ = 0,79 rad | |
| Vr_{cd} = 4914,65 kN | | OK - VERIFICA SODDISFATTA |
| Verifica dell'armatura a taglio: Vr_{sd} | | |
| Vr _{sd} = 0.9 x d x (A _{sw} / s) x f _{yd} x (cotgα + cotgθ) x sinα | | |
| Passo delle staffe | s = 20 cm | 200 mm |
| Diametro staffe | φ _{st} = 12 mm | |
| Braccia resistenti | n = 4 | |
| Area armatura a taglio | A _{sw} = 4,52 cm ² | 452 mm ² |
| Percentuale minima di armatura | ρ _{w,min} = 0,0009 mm | = 0.08 x (F _{ck} ^{0.5}) / F _{yk} |
| Area minima di armatura a taglio | A _{w,min} = 184,92 mm ² | = ρ _{w,min} x s x B _w x senα (EC2-Par.9.2.2) |
| Vr_{sd} = 1135,15 kN | | OK - VERIFICA SODDISFATTA |

- Arco inferiore

| | | |
|--|---|--|
| Dati di input | | |
| R _{ck} | 35 N/mm ² | |
| f _{ck} | 27 N/mm ² | |
| Valore medio della resistenza a trazione | f _{ctm} = 2,7 N/mm ² | = 0.3 x f _{ck} ^(2/3) |
| Coefficiente sicurezza cls | γ _c = 1,5 | Fattore di confidenza FC = 1 |
| Coefficiente carichi lunga durata | α _{cc} = 0,85 | |
| f _{cd} =resistenza di calcolo del cls | f _{cd} = 15,33 N/mm ² | = α _{cc} x f _{ck} / γ _c |
| Resistenza caratteristica di snervamento acciaio | f _{yk} = 450 N/mm ² | |
| Coefficiente sicurezza acciaio | γ _s = 1,15 | |
| Snervamento di calcolo acciaio | f _{yd} = 391 N/mm ² | = f _{yd} / γ _s |
| Forza di taglio di calcolo | V _{sd} = 784,0 kN | |
| Forza assiale di calcolo | N _{sd} = 921 kN | |
| Larghezza sezione | b _w = 100 cm | = 1000 mm |
| altezza della sezione | H = 120 cm | = 1200 mm |
| Copriferro | c = 5 cm | |
| Diametro barre superiori | φ ₂ = 26 mm | (armatura compressa) |
| Diametro barre inferiori | φ ₁ = 26 mm | (armatura tesa) |
| Diametro staffe | φ _{st} = 12 mm | |
| Numero di barre superiori | N ₂ = 10 | |
| Numero di barre inferiori | N ₁ = 10 | |
| altezza utile della sezione | d = 112,5 cm | = 1125 mm |

| | | | |
|--|--|--|---|
| Resistenza di calcolo dell'elemento con armatura a taglio | | (rif. cap. 4.1.2.1.3.2 del D.M. 2008) | |
| Verifica delle bielle compresse: Vr_{cd} | | | |
| $Vr_{cd} = [0.9 \times d \times b_w \times \alpha_c \times f_{cd} \times (\cotg\alpha + \cotg\theta)] / [1 + (\cotg\theta)^2]$ | | | |
| Definizione del coefficiente maggiorativo α_c | $\alpha_{cp} < 0,00 \Rightarrow \alpha_c = 1$ membrature non compresse | $0,00 = \alpha_{cp} < 3,83 \Rightarrow \alpha_c = 0,95$ | ↓ |
| | $3,83 = \alpha_{cp} < 7,66 \Rightarrow \alpha_c = 1,25$ | $7,66 < \alpha_{cp} < 15,33 \Rightarrow \alpha_c = 2,63$ membrature fortemente compresse | |
| Essendo $\alpha_{cp} = -0,77$ N/mm ² | si assume quindi $\alpha_c = 1$ | | |
| Resistenza a compressione ridotta | $f_{cd} = 7,66$ N/mm ² | = 0.5 x f _{cd} | |
| Angolo di inclinazione dell'armatura a taglio | $\alpha = 90^\circ$ | (45° per ferri piegati e 90° per staffe) | |
| | $\alpha = 1,57$ rad | | |
| Angolo di inclinazione dei puntoni compressi | $\theta = 45^\circ$ | (compreso tra 21.8° e 45°) | |
| | $\theta = 0,79$ rad | | |
| Vr_{cd} = 3879,98 kN | | OK - VERIFICA SODDISFATTA | |
| Verifica dell'armatura a taglio: Vr_{sd} | | | |
| $Vr_{sd} = 0.9 \times d \times (A_{sw} / s) \times f_{yd} \times (\cotg\alpha + \cotg\theta) \times \sin\alpha$ | | | |
| Passo delle staffe | $s = 20$ cm | 200 mm | |
| Diametro staffe | $\phi_{st} = 12$ mm | | |
| Braccia resistenti | $n = 4$ | | |
| Area armatura a taglio | $A_{sw} = 4,52$ cm ² | 452 mm ² | |
| Percentuale minima di armatura | $\rho_{w,min} = 0,0009$ mm | = 0.08 x (F _{ck} ^{0.5}) / F _{yk} | |
| Area minima di armatura a taglio | $A_{w,min} = 184,92$ mm ² | = $\rho_{w,min} \times s \times B_w \times \sin\alpha$ (EC2-Par.9.2.2) | |
| Vr_{sd} = 896,17 kN | | OK - VERIFICA SODDISFATTA | |

13.1. VERIFICA SLE

13.1.1. VERIFICA SFORZI SLD

Nel seguente capitolo verrà riassunta la valutazione degli sforzi della galleria allo SLD e si verificherà che tali sforzi siano contenuti entro i limiti dettati dalla norma e precedentemente riassunti nei criteri generali di verifica.

La valutazione degli sforzi viene eseguita con l'ausilio di VCASlu e poi riassunto nelle tabelle successive.

| SEZ CALOTTA h=1.00m | | |
|---------------------|-----------------|--------------|
| SLD | N max | |
| | N _{Ed} | -925,314 kN |
| | M _{Ed} | 230,5079 kNm |
| | N min | |
| | N _{Ed} | -1497,38 kN |
| | M _{Ed} | -50,2531 kNm |
| | M max | |
| | N _{Ed} | -1109,94 kN |
| | M _{Ed} | 627,6867 kNm |
| | M min | |
| | N _{Ed} | -1337,99 kN |
| | M _{Ed} | -385,129 kNm |

| N max | | | |
|------------------|--------|-----|--------------------------------------|
| $\sigma_{c,max}$ | 4,35 | MPa | F _{S_{CLS}} = 3,86 |
| $\sigma_{s,max}$ | 39,98 | MPa | F _{S_{ACC}} = 9,00 |
| N min | | | |
| $\sigma_{c,max}$ | 1,09 | MPa | F _{S_{CLS}} = 15,37 |
| $\sigma_{s,max}$ | 6,60 | MPa | F _{S_{ACC}} = 54,55 |
| M max | | | |
| $\sigma_{c,max}$ | 6,64 | MPa | F _{S_{CLS}} = 2,53 |
| $\sigma_{s,max}$ | 140,60 | MPa | F _{S_{ACC}} = 2,56 |
| M min | | | |
| $\sigma_{c,max}$ | 3,62 | MPa | F _{S_{CLS}} = 4,64 |
| $\sigma_{s,max}$ | 14,95 | MPa | F _{S_{ACC}} = 24,08 |

PROGETTAZIONE ATI:

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| SEZ RENI h=1.20m | | | |
|------------------|-----------------|----------|-----|
| SLD | N max | | |
| | N _{Ed} | -1051,73 | kN |
| | M _{Ed} | 187,873 | kNm |
| | N min | | |
| | N _{Ed} | -1592,66 | kN |
| | M _{Ed} | -75,1656 | kNm |
| | M max | | |
| | N _{Ed} | -1306,31 | kN |
| | M _{Ed} | 372,2576 | kNm |
| | M min | | |
| | N _{Ed} | -1154,35 | kN |
| | M _{Ed} | -198,315 | kNm |

| N max | | | | |
|------------------|------|-----|---------------------|--------|
| $\sigma_{c,max}$ | 1,51 | MPa | F _{SCLS} = | 11,13 |
| $\sigma_{s,max}$ | 7,00 | MPa | F _{SACC} = | 51,43 |
| N min | | | | |
| $\sigma_{c,max}$ | 1,51 | MPa | F _{SCLS} = | 11,13 |
| $\sigma_{s,max}$ | 7,00 | MPa | F _{SACC} = | 51,43 |
| M max | | | | |
| $\sigma_{c,max}$ | 2,44 | MPa | F _{SCLS} = | 6,90 |
| $\sigma_{s,max}$ | 3,34 | MPa | F _{SACC} = | 107,95 |
| M min | | | | |
| $\sigma_{c,max}$ | 1,76 | MPa | F _{SCLS} = | 9,55 |
| $\sigma_{s,max}$ | 8,00 | MPa | F _{SACC} = | 45,00 |

| SEZ PIEDRITTI h=1.50m | | | |
|-----------------------|-----------------|----------|-----|
| SLD | N max | | |
| | N _{Ed} | -1192,08 | kN |
| | M _{Ed} | -195,907 | kNm |
| | N min | | |
| | N _{Ed} | -2063,84 | kN |
| | M _{Ed} | 2123,376 | kNm |
| | M max | | |
| | N _{Ed} | -2063,84 | kN |
| | M _{Ed} | 2123,376 | kNm |
| | M min | | |
| | N _{Ed} | -1740,44 | kN |
| | M _{Ed} | -1232,46 | kNm |

| N max | | | | |
|------------------|--------|-----|---------------------|-------|
| $\sigma_{c,max}$ | 1,18 | MPa | F _{SCLS} = | 14,24 |
| $\sigma_{s,max}$ | 6,80 | MPa | F _{SACC} = | 52,94 |
| N min | | | | |
| $\sigma_{c,max}$ | 7,67 | MPa | F _{SCLS} = | 2,19 |
| $\sigma_{s,max}$ | 148,50 | MPa | F _{SACC} = | 2,42 |
| M max | | | | |
| $\sigma_{c,max}$ | 7,67 | MPa | F _{SCLS} = | 2,19 |
| $\sigma_{s,max}$ | 148,50 | MPa | F _{SACC} = | 2,42 |
| M min | | | | |
| $\sigma_{c,max}$ | 4,44 | MPa | F _{SCLS} = | 3,78 |
| $\sigma_{s,max}$ | 53,98 | MPa | F _{SACC} = | 6,67 |

| SEZ ARCO INF h=1.20m | | | |
|----------------------|-----------------|----------|-----|
| SLD | N max | | |
| | N _{Ed} | -931,942 | kN |
| | M _{Ed} | 724,2605 | kNm |
| | N min | | |
| | N _{Ed} | -1371,78 | kN |
| | M _{Ed} | 354,4638 | kNm |
| | M max | | |
| | N _{Ed} | -1169,41 | kN |
| | M _{Ed} | 1494,471 | kNm |
| | M min | | |
| | N _{Ed} | -1290,99 | kN |
| | M _{Ed} | -783,98 | kNm |

| N max | | | | |
|------------------|--------|-----|---------------------|--------|
| $\sigma_{c,max}$ | 3,87 | MPa | F _{SCLS} = | 4,35 |
| $\sigma_{s,max}$ | 63,16 | MPa | F _{SACC} = | 5,70 |
| N min | | | | |
| $\sigma_{c,max}$ | 2,17 | MPa | F _{SCLS} = | 7,73 |
| $\sigma_{s,max}$ | 0,43 | MPa | F _{SACC} = | 833,33 |
| M max | | | | |
| $\sigma_{c,max}$ | 7,87 | MPa | F _{SCLS} = | 2,13 |
| $\sigma_{s,max}$ | 184,70 | MPa | F _{SACC} = | 1,95 |
| M min | | | | |
| $\sigma_{c,max}$ | 4,21 | MPa | F _{SCLS} = | 3,99 |
| $\sigma_{s,max}$ | 50,93 | MPa | F _{SACC} = | 7,07 |

PROGETTAZIONE ATI:

13.1.2. VERIFICA DELLA FESSURAZIONE – SLE FREQUENTE

Si riporta qui di seguito il calcolo della fessurazione con riferimento alle combinazioni frequenti:

- Arco superiore

| | | | |
|---------------|-----------------|------------|-----|
| SLE FREQUENTE | N max | | |
| | N _{Ed} | -879,162 | kN |
| | M _{Ed} | 212,1093 | kNm |
| | N min | | |
| | N _{Ed} | -1439,906 | kN |
| | M _{Ed} | -331,8051 | kNm |
| | M max | | |
| | N _{Ed} | -1066,8575 | kN |
| | M _{Ed} | 417,57895 | kNm |
| | M min | | |
| | N _{Ed} | -1371,909 | kN |
| | M _{Ed} | 417,57895 | kNm |

| | | | | |
|------------------|-------|-----|---------------------|---------|
| N max | | | | |
| $\sigma_{s,max}$ | 3,03 | MPa | w _k [mm] | 0,0001 |
| x | 818,7 | mm | Fs= | 3000,00 |
| N min | | | | |
| $\sigma_{s,max}$ | 3,031 | MPa | w _k [mm] | 0,0001 |
| x | 846,9 | mm | Fs= | 3000,00 |
| M max | | | | |
| $\sigma_{s,max}$ | 44,83 | MPa | w _k [mm] | 0,06 |
| x | 519,3 | mm | Fs= | 5,00 |
| M min | | | | |
| $\sigma_{s,max}$ | 20,28 | MPa | w _k [mm] | 0,02 |
| x | 669,6 | mm | Fs= | 15,00 |

- Reni

| | | | |
|---------------|-----------------|-----------|-----|
| SLE FREQUENTE | N max | | |
| | N _{Ed} | -1253,864 | kN |
| | M _{Ed} | -356,3238 | kNm |
| | N min | | |
| | N _{Ed} | -1698,581 | kN |
| | M _{Ed} | -902,584 | kNm |
| | M max | | |
| | N _{Ed} | -1480,677 | kN |
| | M _{Ed} | -91,7952 | kNm |
| | M min | | |
| | N _{Ed} | -1698,581 | kN |
| | M _{Ed} | -902,584 | kNm |

| | | | | |
|------------------|-------|-----|---------------------|----------|
| N max | | | | |
| $\sigma_{s,max}$ | 13,09 | MPa | w _k [mm] | 0,02 |
| x | 714 | mm | Fs= | 15,00 |
| N min | | | | |
| $\sigma_{s,max}$ | 80,12 | MPa | w _k [mm] | 0,11 |
| x | 578,7 | mm | Fs= | 2,73 |
| M max | | | | |
| $\sigma_{s,max}$ | 7 | MPa | w _k [mm] | 0,00001 |
| x | 1100 | mm | Fs= | 30000,00 |
| M min | | | | |
| $\sigma_{s,max}$ | 80,12 | MPa | w _k [mm] | 0,11 |
| x | 578,7 | mm | Fs= | 2,73 |

- Piedritti

| | | | |
|---------------|-----------------|------------|-----|
| SLE FREQUENTE | N max | | |
| | N _{Ed} | -1418,562 | kN |
| | M _{Ed} | -684,0176 | kNm |
| | N min | | |
| | N _{Ed} | -2287,293 | kN |
| | M _{Ed} | 2073,8984 | kNm |
| | M max | | |
| | N _{Ed} | -2272,9435 | kN |
| | M _{Ed} | 2107,24095 | kNm |
| | M min | | |
| | N _{Ed} | -2063,005 | kN |
| | M _{Ed} | -1720,9672 | kNm |

| | | | | |
|------------------|-------|-----|---------------------|-------|
| N max | | | | |
| $\sigma_{s,max}$ | 12,62 | MPa | w _k [mm] | 0,01 |
| x | 1047 | mm | Fs= | 30,00 |
| N min | | | | |
| $\sigma_{s,max}$ | 127,4 | MPa | w _k [mm] | 0,12 |
| x | 656,2 | mm | Fs= | 2,50 |
| M max | | | | |
| $\sigma_{s,max}$ | 132,6 | MPa | w _k [mm] | 0,13 |
| x | 647,6 | mm | Fs= | 2,31 |
| M min | | | | |
| $\sigma_{s,max}$ | 95,62 | MPa | w _k [mm] | 0,09 |
| x | 691,1 | mm | Fs= | 3,33 |

- Arco inferiore

| | | | |
|---------------|-----------------|------------|-----|
| SLE FREQUENTE | N max | | |
| | N _{Ed} | -712,989 | kN |
| | M _{Ed} | -670,5747 | kNm |
| | N min | | |
| | N _{Ed} | -978,8085 | kN |
| | M _{Ed} | 1141,41595 | kNm |
| | M max | | |
| | N _{Ed} | -972,467 | kN |
| | M _{Ed} | 1392,8037 | kNm |
| | M min | | |
| | N _{Ed} | -738,631 | kN |
| | M _{Ed} | -1065,7052 | kNm |

| | | | | |
|------------------|-------|-----|---------------------|------|
| N max | | | | |
| $\sigma_{s,max}$ | 68,83 | MPa | w _k [mm] | 0,06 |
| x | 480,3 | mm | F _S = | 5,00 |
| N min | | | | |
| $\sigma_{s,max}$ | 134,5 | MPa | w _k [mm] | 0,12 |
| x | 441 | mm | F _S = | 2,50 |
| M max | | | | |
| $\sigma_{s,max}$ | 181,3 | MPa | w _k [mm] | 0,19 |
| x | 412,6 | mm | F _S = | 1,58 |
| M min | | | | |
| $\sigma_{s,max}$ | 139,2 | MPa | w _k [mm] | 0,13 |
| x | 411,7 | mm | F _S = | 2,31 |

13.1.3. VERIFICA DELLA FESSURAZIONE – SLE QUASI PERMANENTE

Si riporta qui di seguito il calcolo della fessurazione con riferimento alle combinazioni quasi permanenti.

- Arco superiore

| | | | |
|-----------------|-----------------|-----------|-----|
| SLE QUASI PERM. | N max | | |
| | N _{Ed} | -785,283 | kN |
| | M _{Ed} | 171,5887 | kNm |
| | N min | | |
| | N _{Ed} | -1310,882 | kN |
| | M _{Ed} | -22,919 | kNm |
| | M max | | |
| | N _{Ed} | -1062,643 | kN |
| | M _{Ed} | 428,4135 | kNm |
| | M min | | |
| | N _{Ed} | -1240,422 | kN |
| | M _{Ed} | -452,4638 | kNm |

| | | | | |
|------------------|-------|-----|---------------------|----------|
| N max | | | | |
| $\sigma_{s,max}$ | 0,615 | MPa | w _k [mm] | 0,00001 |
| x | 878,7 | mm | F _S = | 20000,00 |
| N min | | | | |
| $\sigma_{s,max}$ | 6 | MPa | w _k [mm] | 0,00001 |
| x | 999 | mm | F _S = | 20000,00 |
| M max | | | | |
| $\sigma_{s,max}$ | 49,7 | MPa | w _k [mm] | 0,07 |
| x | 503,6 | mm | F _S = | 2,86 |
| M min | | | | |
| $\sigma_{s,max}$ | 39,98 | MPa | w _k [mm] | 0,07 |
| x | 558,1 | mm | F _S = | 2,86 |

- Reni

| | | | |
|-----------------|-----------------|-----------|-----|
| SLE QUASI PERM. | N max | | |
| | N _{Ed} | -1118,453 | kN |
| | M _{Ed} | -283,7246 | kNm |
| | N min | | |
| | N _{Ed} | -1549,445 | kN |
| | M _{Ed} | -790,3787 | kNm |
| | M max | | |
| | N _{Ed} | -1349,118 | kN |
| | M _{Ed} | -22,919 | kNm |
| | M min | | |
| | N _{Ed} | -1549,445 | kN |
| | M _{Ed} | -790,3787 | kNm |

| | | | | |
|------------------|--------|-----|---------------------|---------|
| N max | | | | |
| $\sigma_{s,max}$ | 0,2756 | MPa | w _k [mm] | 0,0001 |
| x | 1090 | mm | F _S = | 2000,00 |
| N min | | | | |
| $\sigma_{s,max}$ | 64,35 | MPa | w _k [mm] | 0,09 |
| x | 600,6 | mm | F _S = | 2,22 |
| M max | | | | |
| $\sigma_{s,max}$ | 0,01 | MPa | w _k [mm] | 0,0001 |
| x | 1200 | mm | F _S = | 2000,00 |
| M min | | | | |
| $\sigma_{s,max}$ | 64,35 | MPa | w _k [mm] | 0,09 |
| x | 600,6 | mm | F _S = | 2,22 |

PROGETTAZIONE ATI:

- Piedritti

| | | | |
|-----------------|-----------------|------------|-----|
| SLE QUASI PERM. | N max | | |
| | N _{Ed} | -1267,549 | kN |
| | M _{Ed} | 1996,7731 | kNm |
| | N min | | |
| | N _{Ed} | -2118,163 | kN |
| | M _{Ed} | 1996,7731 | kNm |
| | M max | | |
| | N _{Ed} | -2106,822 | kN |
| | M _{Ed} | 2047,3755 | kNm |
| | M min | | |
| | N _{Ed} | -1647,589 | kN |
| | M _{Ed} | -1581,2263 | kNm |

| | | | | |
|------------------|-------|-----|---------------------|------|
| N max | | | | |
| $\sigma_{s,max}$ | 188,1 | MPa | w _k [mm] | 0,20 |
| x | 507,6 | mm | F _s = | 1,00 |
| N min | | | | |
| $\sigma_{s,max}$ | 128 | MPa | w _k [mm] | 0,12 |
| x | 641,4 | mm | F _s = | 1,67 |
| M max | | | | |
| $\sigma_{s,max}$ | 135,4 | MPa | w _k [mm] | 0,13 |
| x | 630,4 | mm | F _s = | 1,54 |
| M min | | | | |
| $\sigma_{s,max}$ | 103,2 | MPa | w _k [mm] | 0,1 |
| x | 634,8 | mm | F _s = | 2,00 |

- Arco inferiore

| | | | |
|-----------------|-----------------|------------|-----|
| SLE QUASI PERM. | N max | | |
| | N _{Ed} | -721,171 | kN |
| | M _{Ed} | -628,2867 | kNm |
| | N min | | |
| | N _{Ed} | -989,362 | kN |
| | M _{Ed} | 1050,7241 | kNm |
| | M max | | |
| | N _{Ed} | -980,907 | kN |
| | M _{Ed} | 1360,1525 | kNm |
| | M min | | |
| | N _{Ed} | -745,443 | kN |
| | M _{Ed} | -1019,2624 | kNm |

| | | | | |
|------------------|-------|-----|---------------------|------|
| N max | | | | |
| $\sigma_{s,max}$ | 60,72 | MPa | w _k [mm] | 0,05 |
| x | 497,4 | mm | F _s = | 4,00 |
| N min | | | | |
| $\sigma_{s,max}$ | 117,2 | MPa | w _k [mm] | 0,1 |
| x | 456,7 | mm | F _s = | 2,00 |
| M max | | | | |
| $\sigma_{s,max}$ | 174,6 | MPa | w _k [mm] | 0,18 |
| x | 416,6 | mm | F _s = | 1,11 |
| M min | | | | |
| $\sigma_{s,max}$ | 130,1 | MPa | w _k [mm] | 0,12 |
| x | 418,4 | mm | F _s = | 1,67 |

14. VERIFICHE PROLUNGAMENTO GALLERIA

Le verifiche del muro d'invito sono le verifiche geotecniche di ribaltamento, scorrimento e capacità portante del sistema terreno-fondazione. Queste vengono eseguite per lo Stato Limite Ultimo e per lo Stato Limite di Salvaguardia della Vita.

Facendo riferimento ai parametri esposti nel capitolo dei criteri generali, vengono di seguito riassunte le verifiche eseguite per i tre stati limite per i due casi di progetto.

PROGETTAZIONE ATI:

14.1. VERIFICA MURO CON ALTEZZA MAGGIORE - SLU

| VERIFICA A RIBALTAMENTO MURO DI SOSTEGNO A GRAVITA' | | | | | | | | | | | | |
|---|----------------------|---------------------------|-------------------|--|------|-------------|------|--|---|----------------------|-----------|--|
| In accordo con D.M. 17/01/2018 | | | | | | | | | | | | |
| GEOMETRIA E CARATTERISTICHE TERRENO | | | | | | | | | | | | |
| Altezza della mensola (Hp) | Hp | 4.90 | m | | | | | | STATO LIMITE | SLU | | |
| Spessore sommità mensola (Bc-b) | S ₁ | 1.50 | m | | | | | | SPOSTAMENTO LATERALE | Libero | | |
| Larghezza totale soletta (B) | B | 3.00 | m | | | | | | β_M | 0 | | |
| Larghezza oltre la mensola (Bv) | Bv | 0.75 | m | | | | | | a_{max} | 0.264 | | |
| Altezza soletta (Hf) | S ₂ | 1.10 | m | | | | | | ANGOLI | | | |
| Altezza dente (Hd) | Hd | 0.00 | m | | | | | | ϕ' | 35.0 rad 0.6 | | |
| Larghezza dente (Bd) | Bd | 0.00 | m | | | | | | α | 90.0 rad 1.6 | | |
| Peso specifico del terreno di riporto | γ | 20.00 | kN/m ³ | | | | | | η | 90.0 rad 1.6 | | |
| Angolo di attrito del terreno di riporto | ϕ' | 35.00 | ° | | | | | | β | 0.0 rad 0.0 | | |
| Coesione in condizioni drenate | c' | 0.00 | kPa | | | | | | δ | 23.3 rad 0.4 | | |
| Carico dovuto da corsia 1 in sommità | no strada | q _{1,sup} | 0.00 kPa | z _{1,sup} | [m] | 1.21 | | | θ | 62.5 rad 1.1 | | |
| Carico dovuto da corsia 1 alla base | | q _{1,inf} | 0.00 kPa | z _{1,inf} | [m] | 4.90 | | | ξ | 0.0 rad 0.0 | | |
| Carico dovuto da corsia 1 fondazione | | q _{1,fond} | 0.00 kPa | z _{1,fond} | [m] | 6.00 | | | θ_k | 0.0 rad 0.00 | | |
| Carico dovuto da corsia 2 superiore | | q _{2,sup} | 0.00 kPa | z _{2,sup} | [m] | 2.94 | | | ζ | 0.0 rad 0.0 | | |
| Carico dovuto da corsia 2 alla base | | q _{2,inf} | 0.00 kPa | z _{2,inf} | [m] | 4.90 | | | | | | |
| Carico dovuto da corsia 2 fondazione | | q _{1,fond} | 0.00 kPa | z _{2,fond} | [m] | 6.00 | | | | | | |
| Sovraccarichi in superficie uniforme | | q | 20.00 kPa | | | | | | COEFFICIENTI PARZIALI - A1+M1+R3 | | | |
| Peso specifico calcestruzzo | γ_c | 25.00 | kN/m ³ | | | | | | | | | |
| Inclinazione interna mensola | α | 90.00 | ° | | | | | | | | | |
| Inclinazione esterna mensola | η | 90.00 | ° | | | | | | | | | |
| Inclinazione terreno | β | 0.00 | ° | | | | | | | | | |
| Angolo d'attrito muro-terreno | δ | 23.33 | fraz | 0.67 | | | | | | | | |
| Coefficiente di spinta attiva | KA | 0.24 | | | | | | | | | | |
| Parametri pseudo-statici | | k _H | 0.000 | | | | | | | | | |
| | | k _V | 0.000 | | | | | | | | | |
| Coefficiente di spinta attiva - Sismica (Mononobe & Okabe) | | K _{ae} | 0.000 | | | | | | | | | |
| | | | | | | | | | | | | |
| CARICHI PERMANENTI - CARATTERISTICI | | | | | | | | | | | | |
| Spinta attiva orizzontale totale | SAh | 107.72 | kN/m | CARICHI PERMANENTI - SISMICA (Mononobe&Okabe) | | | | | | S _{AE} | 0.00 kN/m | |
| Spinta verticale | S _v | 46.47 | kN/m | | | | | | | S _{AvE} | 0.00 kN/m | |
| Spinta orizzontale - terreno | S _{h,T} | 80.79 | kN/m | | | | | | | S _{ah,TE} | 0.00 kN/m | |
| Spinta orizzontale - sovraccarico costante | Terreno | S _{h,q} | 26.93 kN/m | | | | | | | S _{h,qE} | 0.00 kN/m | |
| Spinta orizzontale - sovr corsia 1 costante | | S _{h,q1} | 0.00 kN/m | | | | | | | S _{h,q1E} | 0.00 kN/m | |
| Spinta orizzontale - sovr corsia 1 triangolare | | S _{h,q1} | 0.00 kN/m | | | | | | | S _{h,q1E} | 0.00 kN/m | |
| Spinta orizzontale - sovr corsia 2 costante | | S _{h,q2} | 0.00 kN/m | | | | | | | S _{h,q2E} | 0.00 kN/m | |
| Spinta orizzontale - sovr corsia 2 triangolare | | S _{h,q2} | 0.00 kN/m | | | | | | | S _{h,q2E} | 0.00 kN/m | |
| Spinta verticale su soletta - sovraccarico | Presente | S _{v,q} | 15.00 kN/m | | | | | | | | | |
| Peso terreno sopra soletta | W _T | 73.50 | kN/m | | | | | | | | | |
| Peso soletta | W _S | 82.50 | kN/m | | | | | | | | | |
| Peso mensola | W _M | 183.75 | kN/m | | | | | | | | | |
| Peso dente | W _D | 0.00 | kN/m | | | | | | | | | |
| FORZE D'INERZIA ORIZZONTALI | | | | | | | | | | | | |
| Terreno sopra soletta | | 0 | kN/m | FORZE D'INERZIA VERTICALI | | | | | | | 0 kN/m | |
| Soletta | | 0 | kN/m | | | | | | | | 0 kN/m | |
| Mensola | | 0 | kN/m | | | | | | | | 0 kN/m | |
| Dente | | 0 | kN/m | | | | | | | | 0 kN/m | |
| CARICHI ORIZZONTALI CONCENTRATI - CARATTERISTICI | | | | | | | | | | | | |
| TIPO | Q - SFAV | F _{H1} | 0.00 kN/m | ψ_{01} | 0.60 | ψ_{21} | 0.00 | | | | | |
| TIPO | G1 - SFAV | F _{H2} | 0.00 kN/m | ψ_{02} | 0.00 | ψ_{22} | 0.00 | | | | | |
| TIPO | G1 - SFAV | F _{H3} | 0.00 kN/m | ψ_{03} | 0.00 | ψ_{23} | 0.00 | | | | | |
| TIPO | G1 - SFAV | F _{H4} | 0.00 kN/m | ψ_{04} | 0.00 | ψ_{24} | 0.00 | | | | | |
| BRACCI DELLE FORZE - CR PIEDE SOLETTA | | | | | | | | | | | | |
| Braccio spinta attiva verticale | b-S _{av} | 3.00 | m | BRACCI DELLE FORZE SISMICHE - CR PIEDE SOLETTA | | | | | | b-ΔS _{ae,h} | 2.00 m | |
| Braccio spinta attiva orizzontale - terreno | b-S _{ah,T} | 2.00 | m | | | | | | | b-W _{T,lin} | 3.55 m | |
| Braccio spinta orizzontale - sovraccarico | b-S _{ah,q} | 3.00 | m | | | | | | | b-W _{S,lin} | 0.55 m | |
| Braccio spinta orizzontale - corsia 1 cost | b-S _{ah,q1} | 2.39 | m | | | | | | | b-W _{M,lin} | 3.55 m | |
| Braccio spinta orizzontale - corsia 1 triang | b-S _{ah,q1} | 3.19 | m | | | | | | | | | |
| Braccio spinta orizzontale - corsia 2 cost | b-S _{ah,q2} | 1.53 | m | | | | | | | | | |
| Braccio spinta orizzontale - corsia 2 triang | b-S _{ah,q2} | 2.04 | m | | | | | | | | | |
| Braccio spinta verticale - sovraccarico su soletta | b-S _{av,q} | 2.63 | m | | | | | | | | | |
| Braccio Peso terreno sopra soletta | b-W _T | 2.63 | m | | | | | | | | | |
| Braccio Peso soletta | b-W _S | 1.50 | m | | | | | | | | | |
| Braccio Peso mensola | b-W _M | 1.50 | m | | | | | | | | | |
| Braccio peso dente | b-W _D | 3.00 | m | | | | | | | | | |
| Braccio carico orizzontale 1 | b-F _{H1} | 0.00 | m | | | | | | | | | |
| Braccio carico orizzontale 2 | b-F _{H2} | 0.00 | m | | | | | | | | | |
| Braccio carico orizzontale 3 | b-F _{H3} | 0.00 | m | | | | | | | | | |
| Braccio carico orizzontale 4 | b-F _{H4} | 0.00 | m | | | | | | | | | |
| COEFFICIENTE PARZIALE | | γ _R | 1.15 | | | | | | | | | |
| MOMENTO STABILIZZANTE | | M _{STAB} (kNm/m) | 724.00 | | | | | | | | | |
| MOMENTO INSTABILIZZANTE | | M _{INST} (kNm/m) | 315.09 | | | | | | | | | |
| FATTORE DI SICUREZZA | | F _S | 2.30 | VERIFICATO | | | | | | | | |

PROGETTAZIONE ATI:

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

VERIFICA A SCORRIMENTO MURO DI SOSTEGNO A GRAMMA'
In accordo con D.M. 17/01/2018

GEOMETRIA E CARATTERISTICHE TERRENO

| | | | | | | | | |
|--|---------------------|-------|-------------------|-------------------------|------|--|---|-----------------|
| Altezza della mensola | H | 4.90 | m | | | | STATO LIMITE | SLU |
| Spessore mensola | s ₁ | 1.50 | m | | | | SPOSTAMENTO LATERALE | Libero |
| Larghezza totale soletta | B | 3.00 | m | | | | β _M | 0 |
| Larghezza oltre la mensola | B* | 0.75 | m | | | | a _{max} | 0.264 |
| Altezza soletta | s ₂ | 1.10 | m | | | | ANGOLI | |
| Altezza dente (Hd) | Hd | 0.00 | m | | | | φ ₃ | 23.0 rad 0.6 |
| Larghezza dente (Bd) | Bd | 0.00 | m | | | | α | 90.0 rad 1.6 |
| Peso specifico del terreno di riporto | γ | 20.00 | kN/m ³ | | | | η | 90.0 rad 1.6 |
| Angolo di attrito del terreno di fondazione | φ' | 23.00 | ° | | | | β | 0.0 rad 0.0 |
| Coesione in condizioni drenate terreno di fondazione | c' | 0.00 | kPa | | | | φ' | 23.0 rad 0.4 |
| Carico dovuto da corsia 1 in sommità | q _{1,sup} | 0.00 | kPa | z _{1,sup} [m] | 1.21 | | θ | 62.5 rad 1.1 |
| Carico dovuto da corsia 1 alla base | q _{1,inf} | 0.00 | kPa | z _{1,inf} [m] | 4.90 | | ξ | 0.0 rad 0.0 |
| Carico dovuto da corsia 1 fondazione | q _{1,fond} | 0.00 | kPa | z _{1,fond} [m] | 6.00 | | θ _ξ | 0.0 rad 0.0 |
| Carico dovuto da corsia 2 superiore | q _{2,sup} | 0.00 | kPa | z _{2,sup} [m] | 2.94 | | ζ | 0.0 rad 0.0 |
| Carico dovuto da corsia 2 alla base | q _{2,inf} | 0.00 | kPa | z _{2,inf} [m] | 4.90 | | | |
| Carico dovuto da corsia 2 fondazione | q _{2,fond} | 0.00 | kPa | z _{2,fond} [m] | 6.00 | | | |
| Sovraccarichi in superficie uniforme | q | 20.00 | kPa | | | | COEFFICIENTI PARZIALI - A1+M1+R3 | |
| Peso specifico calcestruzzo | γ _c | 25.00 | kN/m ³ | | | | | FAV SFAV |
| Inclinazione interna mensola | α | 90.00 | ° | | | | A1 | G1 1.000 1.300 |
| Inclinazione esterna mensola | η | 90.00 | ° | | | | | G2 0.800 1.500 |
| Inclinazione terreno | β | 0.00 | ° | | | | | Q 0.000 1.500 |
| Angolo d'attrito muro-terreno (per calcolo azioni) | δ | 23.33 | fraz | 0.67 | | | | ECC 0.000 0.000 |
| Coefficiente di spinta attiva | KA | 0.24 | | | | | | |

| | | |
|--|-----------------|-------|
| Parametri pseudo-statici | k _H | 0.000 |
| | k _V | 0.000 |
| Coefficiente di spinta attiva - Sismica (Mononobe & Okabe) | K _{ae} | 0.000 |

↑ alto

CARICHI PERMANENTI

| | | | | | | | |
|--|-------|-------|------|---|--------|-----|------|
| Spinta attiva orizzontale totale | SAh | 107.7 | kN/m | ΔSpinta orizzontale | SAE | 0.0 | kN/m |
| Spinta verticale | Sv | 46.5 | kN/m | ΔSpinta verticale | SAVe | 0.0 | kN/m |
| Spinta orizzontale - terreno | Sh,T | 80.8 | kN/m | ΔSpinta orizzontale - terreno | Sah,TE | 0.0 | kN/m |
| Spinta orizzontale - sovraccarico costante | Sh,q | 26.9 | kN/m | ΔSpinta orizzontale - sovraccarico costante | Sh,qE | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 1 costante | Sh,q1 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 1 costante | Sh,q1E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 1 triangolare | Sh,q1 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 1 triangolare | Sh,q1E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 2 costante | Sh,q2 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 2 costante | Sh,q2E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 2 triangolare | Sh,q2 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 2 triangolare | Sh,q2E | 0.0 | kN/m |
| Spinta verticale su soletta - sovraccarico | Sv,q | 15.0 | kN/m | | | | |
| Peso terreno sopra soletta | WT | 73.5 | kN/m | | | | |
| Peso soletta | WS | 82.5 | kN/m | | | | |
| Peso mensola | WM | 183.8 | kN/m | | | | |
| Peso dente | WD | 0.0 | kN/m | | | | |
| Spinta passiva dente | SPD | 0.0 | kN/m | | | | |

FORZE D'INERZIA ORIZZONTALI

| | | | | | |
|-----------------------|---|------|-----------------------|---|------|
| Terreno sopra soletta | 0 | kN/m | Terreno sopra soletta | 0 | kN/m |
| Soletta | 0 | kN/m | Soletta | 0 | kN/m |
| Mensola | 0 | kN/m | Mensola | 0 | kN/m |
| Dente | 0 | kN/m | Dente | 0 | kN/m |

FORZE D'INERZIA VERTICALI

CARICHI ORIZZONTALI CONCENTRATI

| | | | | | | | | | |
|------|------|------|-----------------|------|------|-----------------|------|-----------------|------|
| TIPO | Q - | SFAV | F _{H1} | 0.00 | kN/m | ψ ₀₁ | 0.60 | ψ ₀₁ | 0.00 |
| TIPO | G1 - | SFAV | F _{H2} | 0.00 | kN/m | ψ ₀₂ | 0.00 | ψ ₀₂ | 0.00 |
| TIPO | G1 - | SFAV | F _{H3} | 0.00 | kN/m | ψ ₀₃ | 0.00 | ψ ₀₃ | 0.00 |
| TIPO | G1 - | SFAV | F _{H4} | 0.00 | kN/m | ψ ₀₄ | 0.00 | ψ ₀₄ | 0.00 |

COEFFICIENTE PARZIALE

| | | |
|-------------------------------|------------------------|--------|
| | Y _R | 1.10 |
| RISULTANTE VERTICALE | N (kNm/m) | 444.71 |
| AZIONE ORIZZONTALE RESISTENTE | T _{Rd} (kN/m) | 171.61 |
| AZIONE ORIZZONTALE AGENTE | T _{Ed} (kN/m) | 140.04 |
| FATTORE DI SICUREZZA | F _S | 1.23 |

VERIFICATO

PROGETTAZIONE ATI:

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| DETERMINAZIONE DELLA CAPACITA' PORTANTE LIMITE DI FONDAZIONI SUPERFICIALI RETTANGOLARI FORMULA GENERALE DI BRINCH - HANSEN (1970) | | | |
|--|-------------------|---|--------------|
| CONDIZIONI DRENATE | | $Q_{lim} = 0.5 \cdot \gamma \cdot B \cdot N_{\gamma} \cdot i_{\gamma} \cdot s_{\gamma} \cdot b_{\gamma} \cdot g_{\gamma} + q \cdot N_q \cdot d_q \cdot i_q \cdot s_q \cdot b_q \cdot g_q + c \cdot N_c \cdot d_c \cdot i_c \cdot s_c \cdot b_c \cdot g_c$ | |
| | | Fattori di capacità portante | |
| | | ϕ' | N_c |
| | | N_q | N_{γ} |
| | | 0 | 5.14 |
| | | 1 | 1.00 |
| | | 2 | 0.00 |
| | | 3 | 5.38 |
| | | 4 | 1.09 |
| | | 5 | 1.20 |
| | | 6 | 0.15 |
| | | 7 | 5.63 |
| | | 8 | 1.31 |
| | | 9 | 1.43 |
| | | 10 | 0.34 |
| | | 11 | 6.49 |
| | | 12 | 1.57 |
| | | 13 | 1.72 |
| | | 14 | 0.57 |
| | | 15 | 7.16 |
| | | 16 | 1.88 |
| | | 17 | 2.06 |
| | | 18 | 0.86 |
| | | 19 | 7.92 |
| | | 20 | 2.25 |
| | | 21 | 1.03 |
| | | 22 | 8.34 |
| | | 23 | 2.47 |
| | | 24 | 1.22 |
| | | 25 | 8.80 |
| | | 26 | 2.71 |
| | | 27 | 1.44 |
| | | 28 | 9.28 |
| | | 29 | 2.97 |
| | | 30 | 1.69 |
| | | 31 | 9.81 |
| | | 32 | 3.26 |
| | | 33 | 1.97 |
| | | 34 | 10.37 |
| | | 35 | 3.59 |
| | | 36 | 2.29 |
| | | 37 | 10.98 |
| | | 38 | 3.94 |
| | | 39 | 2.65 |
| | | 40 | 11.63 |
| | | 41 | 4.34 |
| | | 42 | 3.06 |
| | | 43 | 12.34 |
| | | 44 | 4.77 |
| | | 45 | 3.53 |
| | | 46 | 13.10 |
| | | 47 | 5.26 |
| | | 48 | 4.07 |
| | | 49 | 13.93 |
| | | 50 | 5.80 |
| | | | 4.68 |
| | | | 5.39 |
| | | | 6.20 |
| | | | 7.13 |
| | | | 8.20 |
| | | | 9.44 |
| | | | 10.88 |
| | | | 12.54 |
| | | | 14.47 |
| | | | 16.72 |
| | | | 19.34 |
| | | | 22.40 |
| | | | 25.99 |
| | | | 30.21 |
| | | | 35.19 |
| | | | 41.06 |
| | | | 48.03 |
| | | | 56.31 |
| | | | 66.19 |
| | | | 78.02 |
| | | | 92.25 |
| | | | 109.41 |
| | | | 130.21 |
| | | | 155.54 |
| | | | 186.53 |
| | | | 224.63 |
| | | | 271.75 |
| | | | 330.34 |
| | | | 403.65 |
| | | | 496.00 |
| | | | 613.14 |
| | | | 762.86 |
| Determinazione dei coefficienti | | | |
| Fattori correttivi dipendenti dall'inclinazione del carico | | | |
| $i_{\gamma} = 0.520$ | $i_q = 0.740$ | $i_c = 0.706$ | |
| Fattori correttivi dipendenti dalla profondità del piano di posa | | | |
| $d_{\gamma} = 1.000$ | | | |
| $d_q = 1.213$ | per $D/B' \leq 1$ | $d_q = 1.213$ | |
| $d_q = 11.743$ | per $D/B' > 1$ | | |
| $d_c = 1.271$ | per $D/B' \leq 1$ | $d_c = 1.271$ | |
| $d_c = 1.238$ | per $D/B' > 1$ | | |
| Fattori correttivi dipendenti dalla forma della fondazione | | | |
| $s_{\gamma} = 1.000$ | $s_q = 1.000$ | $s_c = 1.000$ | |
| Fattori correttivi dipendenti dall'inclinazione dell'intradosso fondazione | | | |
| $b_{\gamma} = 1.000$ | $b_q = 1.000$ | $b_c = 1.000$ | |
| Fattori correttivi dipendenti dall'inclinazione del piano campagna | | | |
| $g_{\gamma} = 1.000$ | $g_q = 1.000$ | $g_c = 1.000$ | |
| COEFFICIENTE PARZIALE $\gamma_R = 1.40$ | | | |
| CAPACITA' PORTANTE LIMITE $Q_{lim} \text{ (kPa)} = 235.09$ | | | |
| COEFFICIENTE DI SICUREZZA $FS = (Q_{lim}-q)/(Q_{es}-q) = 1.34$ | | VERIFICATO | |

User:
Peso efficace terreno
fondazione

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| CONDIZIONI NON DRENATE | | $Q_{lim} = cu \cdot (3.14 + 2) \cdot (dc \cdot ic \cdot sc \cdot bc \cdot gc) + q$ | |
|---|---------------------------------------|--|------------|
| Affondamento della fondazione | D (m) = | 1.7 | |
| Dim. minore fondazione efficace equivalente | B' (m) = | 2.5 | |
| Dim. maggiore fondazione efficace equivalente | L' (m) = | 1.0 | |
| Carico verticale agente sulla fondazione | N (kN) = | 442 | |
| Carico orizzontale agente sulla fondazione | H (kN) = | 140 | |
| Coesione in condizioni non drenate | cu (kN/m ²) = | 100.0 | # |
| Azione laterale stabilizzante | q (kN/m ²) = | 15.3 | |
| Inclinazione intradosso fondazione | α (°) = | 0.0 | |
| Inclinazione piano campagna | β (°) = | 0.0 | |
| sc = | 1.000 | ic = | 0.861 |
| dc = | 1.271 per D/B' <= 1 | quindi dc = | 1.271 # |
| dc = | 1.238 per D/B' > 1 | | |
| gc = | 1.000 | | |
| COEFFICIENTE PARZIALE | γ_R | 1.400 | |
| CAPACITA' PORTANTE LIMITE | Q_{lim} = | 412.596 | |
| COEFFICIENTE DI SICUREZZA | $FS = (Q_{lim} - q) / (Q_{es} - q) =$ | 2.35 | VERIFICATO |

Si riassumono di seguito i fattori di sicurezza allo SLU

| | | |
|--------|------|------------|
| RIB | 2.30 | VERIFICATO |
| SCOR | 1.23 | VERIFICATO |
| CAP DR | 1.34 | VERIFICATO |
| CAP ND | 2.35 | VERIFICATO |

14.2. VERIFICA MURO CON ALTEZZA MAGGIORE - SLV

PROGETTAZIONE ATI:

VERIFICA A RIBALTAMENTO MURO DI SOSTEGNO A GRAVITA'

In accordo con D.M. 17/01/2018

GEOMETRIA E CARATTERISTICHE TERRENO

| | | | |
|--|---------------------|--------------------|-------------------|
| Altezza della mensola (Hp) | Hp | 4.90 | m |
| Spessore sommità mensola (Bc-b) | s ₁ | 1.50 | m |
| Larghezza totale soletta (B) | B | 3.00 | m |
| Larghezza oltre la mensola (Bv) | Bv | 0.75 | m |
| Altezza soletta (Hf) | s ₂ | 1.10 | m |
| Altezza dente (Hd) | Hd | 0.00 | m |
| Larghezza dente (Bd) | Bd | 0.00 | m |
| Peso specifico del terreno di riporto | γ | 20.00 | kN/m ³ |
| Angolo di attrito del terreno di riporto | φ' | 35.00 | ° |
| Coesione in condizioni drenate | c' | 0.00 | kPa |
| Carico dovuto da corsia 1 in sommità | no strada | q _{1,sup} | 0.00 kPa |
| Carico dovuto da corsia 1 alla base | q _{1,inf} | 0.00 | kPa |
| Carico dovuto da corsia 1 fondazione | q _{1,fond} | 0.00 | kPa |
| Carico dovuto da corsia 2 superiore | q _{2,sup} | 0.00 | kPa |
| Carico dovuto da corsia 2 alla base | q _{2,inf} | 0.00 | kPa |
| Carico dovuto da corsia 2 fondazione | q _{2,fond} | 0.00 | kPa |
| Sovraccarichi in superficie uniforme | q | 20.00 | kPa |
| Peso specifico calcestruzzo | γ _c | 25.00 | kN/m ³ |
| Inclinazione interna mensola | α | 90.00 | ° |
| Inclinazione esterna mensola | η | 90.00 | ° |
| Inclinazione terreno | β | 0.00 | ° |
| Angolo d'attrito muro-terreno | δ | 23.33 | fraz |
| Coefficiente di spinta attiva | KA | 0.24 | |

STATO LIMITE

SLV

SPOSTAMENTO LATERALE

Libero

β_M 0.38

a_{max} 0.264

ANGOLI

| | | | |
|----------------|------|-----|------|
| φ | 35.0 | rad | 0.6 |
| α | 90.0 | rad | 1.6 |
| η | 90.0 | rad | 1.6 |
| β | 0.0 | rad | 0.0 |
| δ | 23.3 | rad | 0.4 |
| θ | 62.5 | rad | 1.1 |
| ξ | 0.0 | rad | 0.0 |
| θ _k | 6.0 | rad | 0.11 |
| ζ | 0.0 | rad | 0.0 |

COEFFICIENTI PARZIALI - A1+M1+R3

| | | | |
|----|-----|-------|-------|
| | | FAV | SFAV |
| A1 | G1 | 1.000 | 1.000 |
| | G2 | 1.000 | 1.000 |
| | Q | 0.000 | 1.000 |
| | ECC | 0.000 | 0.000 |

| | | |
|--|-----------------|--------|
| Parametri pseudo-statici | k _H | 0.100 |
| | k _V | -0.050 |
| Coefficiente di spinta attiva - Sismica (Mononobe & Okabe) | K _{ae} | 0.294 |

↑ alto

CARICHI PERMANENTI - CARATTERISTICI

| | | | |
|---|--------------------|--------|------|
| Spinta attiva orizzontale totale | S _{Ah} | 106.37 | kN/m |
| Spinta verticale | S _v | 45.88 | kN/m |
| Spinta orizzontale - terreno | S _{h,T} | 80.79 | kN/m |
| Spinta orizzontale - sovraccarico costante | S _{h,q} | 25.58 | kN/m |
| Spinta orizzontale - sov corsia 1 costante | S _{h,q1} | 0.00 | kN/m |
| Spinta orizzontale - sov corsia 1 triangolare | S _{h,q1E} | 0.00 | kN/m |
| Spinta orizzontale - sov corsia 2 costante | S _{h,q2} | 0.00 | kN/m |
| Spinta orizzontale - sov corsia 2 triangolare | S _{h,q2E} | 0.00 | kN/m |
| Spinta verticale su soletta - sovraccarico | S _{v,q} | 14.25 | kN/m |
| Peso terreno sopra soletta | W _T | 73.50 | kN/m |
| Peso soletta | W _S | 82.50 | kN/m |
| Peso mensola | W _M | 183.75 | kN/m |
| Peso dente | W _D | 0.00 | kN/m |

CARICHI PERMANENTI - SISMICA (Mononobe&Okabe)

| | | | |
|--|--------------------|-------|------|
| ΔSpinta orizzontale | S _{AE} | 22.06 | kN/m |
| ΔSpinta verticale | S _{AV,E} | 9.52 | kN/m |
| ΔSpinta orizzontale - terreno | S _{h,TE} | 16.55 | kN/m |
| ΔSpinta orizzontale - sovraccarico costante | S _{h,qE} | 5.52 | kN/m |
| ΔSpinta orizzontale - sov corsia 1 costante | S _{h,q1E} | 0.00 | kN/m |
| ΔSpinta orizzontale - sov corsia 1 triangolare | S _{h,q1E} | 0.00 | kN/m |
| ΔSpinta orizzontale - sov corsia 2 costante | S _{h,q2E} | 0.00 | kN/m |
| ΔSpinta orizzontale - sov corsia 2 triangolare | S _{h,q2E} | 0.00 | kN/m |

FORZE D'INERZIA ORIZZONTALI

| | | |
|-----------------------|----|------|
| Terreno sopra soletta | 7 | kN/m |
| Soletta | 8 | kN/m |
| Mensola | 18 | kN/m |
| Dente | 0 | kN/m |

FORZE D'INERZIA VERTICALI

| | | |
|-----------------------|----|------|
| Terreno sopra soletta | -4 | kN/m |
| Soletta | -4 | kN/m |
| Mensola | -9 | kN/m |
| Dente | 0 | kN/m |

CARICHI ORIZZONTALI CONCENTRATI - CARATTERISTICI

| | | | | | | | | |
|------|-----------|-----------------|------|------|-----------------|------|-----------------|------|
| TIPO | Q - SFAV | F _{H1} | 0.00 | kN/m | ψ ₀₁ | 0.60 | ψ ₂₁ | 0.00 |
| TIPO | G1 - SFAV | F _{H2} | 0.00 | kN/m | ψ ₀₂ | 0.00 | ψ ₂₂ | 0.00 |
| TIPO | G1 - SFAV | F _{H3} | 0.00 | kN/m | ψ ₀₃ | 0.00 | ψ ₂₃ | 0.00 |
| TIPO | G1 - SFAV | F _{H4} | 0.00 | kN/m | ψ ₀₄ | 0.00 | ψ ₂₄ | 0.00 |

BRACCI DELLE FORZE - CR PIEDE SOLETTA

| | | | |
|--|-----------------------|------|---|
| Braccio spinta attiva verticale | b-S _{av} | 3.00 | m |
| Braccio spinta attiva orizzontale - terreno | b-S _{ah,T} | 2.00 | m |
| Braccio spinta orizzontale - sovraccarico | b-S _{ah,q} | 3.00 | m |
| Braccio spinta orizzontale - corsia 1 cost | b-S _{ah,q1} | 2.39 | m |
| Braccio spinta orizzontale - corsia 1 triang | b-S _{ah,q1E} | 3.19 | m |
| Braccio spinta orizzontale - corsia 2 cost | b-S _{ah,q2} | 1.53 | m |
| Braccio spinta orizzontale - corsia 2 triang | b-S _{ah,q2E} | 2.04 | m |
| Braccio spinta verticale - sovraccarico su soletta | b-S _{av,q} | 2.63 | m |
| Braccio Peso terreno sopra soletta | b-W _T | 2.63 | m |
| Braccio Peso soletta | b-W _S | 1.50 | m |
| Braccio Peso mensola | b-W _M | 1.50 | m |
| Braccio peso dente | b-W _D | 3.00 | m |
| Braccio carico orizzontale 1 | b-F _{H1} | 0.00 | m |
| Braccio carico orizzontale 2 | b-F _{H2} | 0.00 | m |
| Braccio carico orizzontale 3 | b-F _{H3} | 0.00 | m |
| Braccio carico orizzontale 4 | b-F _{H4} | 0.00 | m |

BRACCI DELLE FORZE SISMICHE - CR PIEDE SOLETTA

| | | | |
|--|----------------------|------|---|
| Braccio Δ spinta attiva orizzontale | b-ΔS _{ae,h} | 2.00 | m |
| Peso terreno sopra soletta - orizzontale | b-W _{T,in} | 3.55 | m |
| Peso soletta - orizzontale | b-W _{S,in} | 0.55 | m |
| Peso mensola - orizzontale | b-W _{M,in} | 3.55 | m |

| | | |
|-------------------------|---------------------------|--------|
| COEFFICIENTE PARZIALE | Y _R | 1.00 |
| MOMENTO STABILIZZANTE | M _{STAB} (kNm/m) | 766.20 |
| MOMENTO INSTABILIZZANTE | M _{INST} (kNm/M) | 384.13 |
| FATTORE DI SICUREZZA | F _S | 1.99 |

VERIFICATO

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

VERIFICA A SCORRIMENTO MURO DI SOSTEGNO A GRAMITA'

In accordo con D.M. 17/01/2018

GEOMETRIA E CARATTERISTICHE TERRENO

| | | | | | | | |
|--|----------------|---------------------|-------------------------|-------------------------|------|---|-----------------|
| Altezza della mensola | H | 4.90 | m | | | STATO LIMITE | SLV |
| Spessore mensola | s ₁ | 1.50 | m | | | SPOSTAMENTO LATERALE | Libero |
| Larghezza totale soletta | B | 3.00 | m | | | β_M | 0.38 |
| Larghezza oltre la mensola | B* | 0.75 | m | | | a_{max} | 0.264 |
| Altezza soletta | s ₂ | 1.10 | m | | | ANGOLI | |
| Altezza dente (Hd) | Hd | 0.00 | m | | | φ ₃ | 23.0 rad 0.6 |
| Larghezza dente (Bd) | Bd | 0.00 | m | | | α | 90.0 rad 1.6 |
| Peso specifico del terreno di riporto | γ | 20.00 | kN/m ³ | | | η | 90.0 rad 1.6 |
| Angolo di attrito del terreno di fondazione | φ' | 23.00 | ° | | | β | 0.0 rad 0.0 |
| Coesione in condizioni drenate terreno di fondazione | c' | 0.00 | kPa | | | φ' | 23.0 rad 0.4 |
| Carico dovuto da corsia 1 in sommità | no strada | q _{1,sup} | 0.00 kPa | z _{1,sup} [m] | 1.21 | θ | 62.5 rad 1.1 |
| Carico dovuto da corsia 1 alla base | | q _{1,inf} | 0.00 kPa | z _{1,inf} [m] | 4.90 | ξ | 0.0 rad 0.0 |
| Carico dovuto da corsia 1 fondazione | | q _{1,fond} | 0.00 kPa | z _{1,fond} [m] | 6.00 | θ _x | 6.0 rad 0.1 |
| Carico dovuto da corsia 2 superiore | | q _{2,sup} | 0.00 kPa | z _{2,sup} [m] | 2.94 | ζ | 0.0 rad 0.0 |
| Carico dovuto da corsia 2 alla base | | q _{2,inf} | 0.00 kPa | z _{2,inf} [m] | 4.90 | | |
| Carico dovuto da corsia 2 fondazione | | q _{1,fond} | 0.00 kPa | z _{2,fond} [m] | 6.00 | | |
| Sovraccarichi in superficie uniforme | | q | 20.00 kPa | | | COEFFICIENTI PARZIALI - A1+M1+R3 | |
| Peso specifico calcestruzzo | | γ _c | 25.00 kN/m ³ | | | | FAV SFAV |
| Inclinazione interna mensola | | α | 90.00 ° | | | A1 | G1 1.000 1.000 |
| Inclinazione esterna mensola | | η | 90.00 ° | | | | G2 1.000 1.000 |
| Inclinazione terreno | | β | 0.00 ° | | | | Q 0.000 1.000 |
| Angolo d'attrito muro-terreno (per calcolo azioni) | | δ | 23.33 | fraz | 0.67 | | ECC 0.000 0.000 |
| Coefficiente di spinta attiva | | KA | 0.24 | | | | |

| | | | |
|---|-----------------|--------|--------|
| Parametri pseudo-statici | k _H | 0.100 | |
| | k _V | -0.050 | ↑ alto |
| Coefficiente di spinta attiva - Sismica (Mononobe & Okabe) | K _{ae} | 0.294 | |

CARICHI PERMANENTI

| | | | | | | | |
|--|----------|-------|-------|---|--------|------|------|
| Spinta attiva orizzontale totale | SAh | 106.4 | kN/m | ΔSpinta orizzontale | SAE | 22.1 | kN/m |
| Spinta verticale | Sv | 45.9 | kN/m | ΔSpinta verticale | SAvE | 9.5 | kN/m |
| Spinta orizzontale - terreno | Sh,T | 80.8 | kN/m | ΔSpinta orizzontale - terreno | Sah,TE | 16.5 | kN/m |
| Spinta orizzontale - sovraccarico costante | Sh,q | 25.6 | kN/m | ΔSpinta orizzontale - sovraccarico costante | Sh,qE | 5.5 | kN/m |
| Spinta orizzontale - sovr corsia 1 costante | Sh,q1 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 1 costante | Sh,q1E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 1 triangolare | Sh,q1 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 1 triangolare | Sh,q1E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 2 costante | Sh,q2 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 2 costante | Sh,q2E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 2 triangolare | Sh,q2 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 2 triangolare | Sh,q2E | 0.0 | kN/m |
| Spinta verticale su soletta - sovraccarico | Presente | Sv,q | 14.2 | kN/m | | | |
| Peso terreno sopra soletta | | WT | 73.5 | kN/m | | | |
| Peso soletta | | WS | 82.5 | kN/m | | | |
| Peso mensola | | WM | 183.8 | kN/m | | | |
| Peso dente | | WD | 0.0 | kN/m | | | |
| Spinta passiva dente | | SPD | 0.0 | kN/m | | | |

FORZE D'INERZIA ORIZZONTALI

| | | |
|-----------------------|----|------|
| Terreno sopra soletta | 7 | kN/m |
| Soletta | 8 | kN/m |
| Mensola | 18 | kN/m |
| Dente | 0 | kN/m |

FORZE D'INERZIA VERTICALI

| | | |
|-----------------------|----|------|
| Terreno sopra soletta | -4 | kN/m |
| Soletta | -4 | kN/m |
| Mensola | -9 | kN/m |
| Dente | 0 | kN/m |

CARICHI ORIZZONTALI CONCENTRATI

| | | | | | | | | | |
|------|------|------|-----------------|------|------|-----------------|------|-----------------|------|
| TIPO | Q - | SFAV | F _{H1} | 0.00 | kN/m | ψ ₀₁ | 0.60 | ψ ₀₁ | 0.00 |
| TIPO | G1 - | SFAV | F _{H2} | 0.00 | kN/m | ψ ₀₂ | 0.00 | ψ ₀₂ | 0.00 |
| TIPO | G1 - | SFAV | F _{H3} | 0.00 | kN/m | ψ ₀₃ | 0.00 | ψ ₀₃ | 0.00 |
| TIPO | G1 - | SFAV | F _{H4} | 0.00 | kN/m | ψ ₀₄ | 0.00 | ψ ₀₄ | 0.00 |

| | | |
|--------------------------------------|------------------------|--------|
| COEFFICIENTE PARZIALE | γ _R | 1.00 |
| RISULTANTE VERTICALE | N (kNm/m) | 392.36 |
| AZIONE ORIZZONTALE RESISTENTE | T _{Rd} (kN/m) | 166.55 |
| AZIONE ORIZZONTALE AGENTE | T _{Ed} (kN/m) | 162.52 |

| | | | |
|-----------------------------|----------------|------|-------------------|
| FATTORE DI SICUREZZA | F _s | 1.02 | VERIFICATO |
|-----------------------------|----------------|------|-------------------|

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| DETERMINAZIONE DELLA CAPACITA' PORTANTE LIMITE DI FONDAZIONI SUPERFICIALI RETTANGOLARI FORMULA GENERALE DI BRINCH - HANSEN (1970) | | | | | |
|--|--------|---|--------|------------|--------------|
| CONDIZIONI DRENATE | | $Q_{lim} = 0.5 \cdot \gamma \cdot B \cdot N_{\gamma} \cdot i_{\gamma} \cdot s_{\gamma} \cdot b_{\gamma} \cdot g_{\gamma} + q \cdot N_q \cdot d_q \cdot i_q \cdot s_q \cdot b_q \cdot g_q + c \cdot N_c \cdot d_c \cdot i_c \cdot s_c \cdot b_c \cdot g_c$ | | | |
| | | Fattori di capacità portante | | | |
| | | ϕ' | N_c | N_q | N_{γ} |
| | | 0 | 5.14 | 1.00 | 0.00 |
| | | 1 | 5.38 | 1.09 | 0.07 |
| | | 2 | 5.63 | 1.20 | 0.15 |
| | | 3 | 5.90 | 1.31 | 0.24 |
| | | 4 | 6.19 | 1.43 | 0.34 |
| | | 5 | 6.49 | 1.57 | 0.45 |
| | | 6 | 6.81 | 1.72 | 0.57 |
| | | 7 | 7.16 | 1.88 | 0.71 |
| | | 8 | 7.53 | 2.06 | 0.86 |
| | | 9 | 7.92 | 2.25 | 1.03 |
| | | 10 | 8.34 | 2.47 | 1.22 |
| | | 11 | 8.80 | 2.71 | 1.44 |
| | | 12 | 9.28 | 2.97 | 1.69 |
| | | 13 | 9.81 | 3.26 | 1.97 |
| | | 14 | 10.37 | 3.59 | 2.29 |
| | | 15 | 10.98 | 3.94 | 2.65 |
| | | 16 | 11.63 | 4.34 | 3.06 |
| | | 17 | 12.34 | 4.77 | 3.53 |
| | | 18 | 13.10 | 5.26 | 4.07 |
| | | 19 | 13.93 | 5.80 | 4.68 |
| | | 20 | 14.83 | 6.40 | 5.39 |
| | | 21 | 15.81 | 7.07 | 6.20 |
| | | 22 | 16.88 | 7.82 | 7.13 |
| | | 23 | 18.05 | 8.66 | 8.20 |
| | | 24 | 19.32 | 9.60 | 9.44 |
| | | 25 | 20.72 | 10.66 | 10.88 |
| | | 26 | 22.25 | 11.85 | 12.54 |
| | | 27 | 23.94 | 13.20 | 14.47 |
| | | 28 | 25.80 | 14.72 | 16.72 |
| | | 29 | 27.86 | 16.44 | 19.34 |
| | | 30 | 30.14 | 18.40 | 22.40 |
| | | 31 | 32.67 | 20.63 | 25.99 |
| | | 32 | 35.49 | 23.18 | 30.21 |
| | | 33 | 38.64 | 26.09 | 35.19 |
| | | 34 | 42.16 | 29.44 | 41.06 |
| | | 35 | 46.12 | 33.30 | 48.03 |
| | | 36 | 50.59 | 37.75 | 56.31 |
| | | 37 | 55.63 | 42.92 | 66.19 |
| | | 38 | 61.35 | 48.93 | 78.02 |
| | | 39 | 67.87 | 55.96 | 92.25 |
| | | 40 | 75.31 | 64.20 | 109.41 |
| | | 41 | 83.86 | 73.90 | 130.21 |
| | | 42 | 93.71 | 85.37 | 155.54 |
| | | 43 | 105.11 | 99.01 | 186.53 |
| | | 44 | 118.37 | 115.31 | 224.63 |
| | | 45 | 133.87 | 134.87 | 271.75 |
| | | 46 | 152.10 | 158.50 | 330.34 |
| | | 47 | 173.64 | 187.21 | 403.65 |
| | | 48 | 199.26 | 222.30 | 496.00 |
| | | 49 | 229.92 | 265.50 | 613.14 |
| | | 50 | 266.88 | 319.06 | 762.86 |
| Determinazione dei coefficienti | | | | | |
| Fattori correttivi dipendenti dall'inclinazione del carico | | | | | |
| $i_{\gamma} =$ | 0.406 | $i_q =$ | 0.664 | $i_c =$ | 0.620 |
| Fattori correttivi dipendenti dalla profondità del piano di posa | | | | | |
| $d_{\gamma} =$ | 1.000 | | | | |
| $d_q =$ | 1.275 | per $D/B' \leq 1$ | | | |
| quindi | | $d_q = 1.275$ | | | |
| $d_q =$ | 13.957 | per $D/B' > 1$ | | | |
| $d_c =$ | 1.349 | per $D/B' \leq 1$ | | | |
| quindi | | $d_c = 1.349$ | | | |
| $d_c =$ | 1.287 | per $D/B' > 1$ | | | |
| Fattori correttivi dipendenti dalla forma della fondazione | | | | | |
| $s_{\gamma} =$ | 1.000 | $s_q =$ | 1.000 | $s_c =$ | 1.000 |
| Fattori correttivi dipendenti dall'inclinazione dell'intradosso fondazione | | | | | |
| $b_{\gamma} =$ | 1.000 | $b_q =$ | 1.000 | $b_c =$ | 1.000 |
| Fattori correttivi dipendenti dall'inclinazione del piano campagna | | | | | |
| $g_{\gamma} =$ | 1.000 | $g_q =$ | 1.000 | $g_c =$ | 1.000 |
| COEFFICIENTE PARZIALE | | γ_{R} | 1.20 | | |
| CAPACITA' PORTANTE LIMITE | | Q_{lim} (kPa) = | 243.48 | | |
| COEFFICIENTE DI SICUREZZA | | $FS = (Q_{lim} - q) / (Q_{es} - q) =$ | 1.21 | VERIFICATO | |

User:
Peso efficace terreno
fondazione

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| CONDIZIONI NON DRENATE | | $Q_{lim} = cu \cdot (3.14 + 2) \cdot (dc \cdot ic \cdot sc \cdot bc \cdot gc) + q$ | |
|---|---------------------------------------|--|------------|
| Affondamento della fondazione | D (m) = | 1.7 | |
| Dim. minore fondazione efficace equivalente | B' (m) = | 1.9 | |
| Dim. maggiore fondazione efficace equivalente | L' (m) = | 1.0 | |
| Carico verticale agente sulla fondazione | N (kN) = | 392 | |
| Carico orizzontale agente sulla fondazione | H (kN) = | 163 | |
| Coesione in condizioni non drenate | cu (kN/m ²) = | 100.0 | # |
| Azione laterale stabilizzante | q (kN/m ²) = | 15.3 | |
| Inclinazione intradosso fondazione | α (°) = | 0.0 | |
| Inclinazione piano campagna | β (°) = | 0.0 | |
| sc = | 1.000 | ic = | 0.783 |
| dc = | 1.349 per D/B' <= 1 | quindi dc = | 1.349 # |
| dc = | 1.287 per D/B' > 1 | | |
| gc = | 1.000 | | |
| COEFFICIENTE PARZIALE | γ_R | 1.200 | |
| CAPACITA' PORTANTE LIMITE | Q_{lim} = | 465.170 | |
| COEFFICIENTE DI SICUREZZA | $FS = (Q_{lim} - q) / (Q_{es} - q) =$ | 2.31 | VERIFICATO |

Si riassumono i coefficienti di sicurezza allo SLV

| | | |
|--------|------|------------|
| RIB | 1.99 | VERIFICATO |
| SCOR | 1.02 | VERIFICATO |
| CAP DR | 1.21 | VERIFICATO |
| CAP ND | 2.31 | VERIFICATO |

PROGETTAZIONE ATI:

14.3. VERIFICA MURO SU TERRENO PEGGIORE - SLU

| VERIFICA A RIBALTAMENTO MURO DI SOSTEGNO A GRAVITA' | | | | | | | | | |
|--|----------------------|-----------------|-------------------|-------------------------|-----------------|------|-----------------|------|--|
| In accordo con D.M. 17/01/2018 | | | | | | | | | |
| GEOMETRIA E CARATTERISTICHE TERRENO | | | | | | | | | |
| Altezza della mensola (Hp) | Hp | 4.00 | m | | | | | | |
| Spessore sommità mensola (Bc-b) | s ₁ | 1.50 | m | | | | | | |
| Larghezza totale soletta (B) | B | 3.00 | m | | | | | | |
| Larghezza oltre la mensola (Bv) | Bv | 0.75 | m | | | | | | |
| Altezza soletta (Hf) | s ₂ | 1.10 | m | | | | | | |
| Altezza dente (Hd) | Hd | 0.35 | m | | | | | | |
| Larghezza dente (Bd) | Bd | 0.35 | m | | | | | | |
| Peso specifico del terreno di riporto | γ | 20.00 | kN/m ³ | | | | | | |
| Angolo di attrito del terreno di riporto | φ' | 35.00 | ° | | | | | | |
| Coesione in condizioni drenate | c' | 0.00 | kPa | | | | | | |
| Carico dovuto da corsia 1 in sommità | q _{1,sup} | 0.00 | kPa | Z _{1,sup} [m] | 1.21 | | | | |
| Carico dovuto da corsia 1 alla base | q _{1,inf} | 0.00 | kPa | Z _{1,inf} [m] | 4.00 | | | | |
| Carico dovuto da corsia 1 fondazione | q _{1,fond} | 0.00 | kPa | Z _{1,fond} [m] | 5.10 | | | | |
| Carico dovuto da corsia 2 superiore | q _{2,sup} | 0.00 | kPa | Z _{2,sup} [m] | 2.94 | | | | |
| Carico dovuto da corsia 2 alla base | q _{2,inf} | 0.00 | kPa | Z _{2,inf} [m] | 4.00 | | | | |
| Carico dovuto da corsia 2 fondazione | q _{2,fond} | 0.00 | kPa | Z _{2,fond} [m] | 5.10 | | | | |
| Sovraccarichi in superficie uniforme | q | 20.00 | kPa | | | | | | |
| Peso specifico calcestruzzo | γ _c | 25.00 | kN/m ³ | | | | | | |
| Inclinazione interna mensola | α | 90.00 | ° | | | | | | |
| Inclinazione esterna mensola | η | 90.00 | ° | | | | | | |
| Inclinazione terreno | β | 0.00 | ° | | | | | | |
| Angolo d'attrito muro-terreno | δ | 23.33 | fraz | 0.67 | | | | | |
| Coefficiente di spinta attiva | KA | 0.24 | | | | | | | |
| STATO LIMITE | | | | | | | | | |
| SPOSTAMENTO LATERALE | | | | | | | | | |
| β _M | | | | | | | | | |
| β _{M,max} | | | | | | | | | |
| ANGOLI | | | | | | | | | |
| φ | | 35.0 | rad | 0.6 | | | | | |
| α | | 90.0 | rad | 1.6 | | | | | |
| η | | 90.0 | rad | 1.6 | | | | | |
| β | | 0.0 | rad | 0.0 | | | | | |
| δ | | 23.3 | rad | 0.4 | | | | | |
| θ | | 62.5 | rad | 1.1 | | | | | |
| ξ | | 0.0 | rad | 0.0 | | | | | |
| θ _k | | 0.0 | rad | 0.00 | | | | | |
| ζ | | 0.0 | rad | 0.0 | | | | | |
| COEFFICIENTI PARZIALI - A1+M1+R3 | | | | | | | | | |
| FAV SFAV | | | | | | | | | |
| A1 | | | | | | | | | |
| G1 | | 1.000 | | 1.300 | | | | | |
| G2 | | 0.800 | | 1.500 | | | | | |
| Q | | 0.000 | | 1.500 | | | | | |
| ECC | | 0.000 | | 0.000 | | | | | |
| Parametri pseudo-statici | | | | | | | | | |
| k _H 0.000 | | | | | | | | | |
| k _V 0.000 | | | | | | | | | |
| ↑ alto | | | | | | | | | |
| Coefficiente di spinta attiva - Sismica (Mononobe & Okabe) | | | | | | | | | |
| K _{ae} 0.000 | | | | | | | | | |
| CARICHI PERMANENTI - CARATTERISTICI | | | | | | | | | |
| Spinta attiva orizzontale totale | S _{Ah} | 91.12 | kN/m | | | | | | |
| Spinta verticale | S _v | 39.31 | kN/m | | | | | | |
| Spinta orizzontale - terreno | S _{h,T} | 66.66 | kN/m | | | | | | |
| Spinta orizzontale - sovraccarico costante | S _{h,q} | 24.46 | kN/m | | | | | | |
| Spinta orizzontale - sovr corsia 1 costante | S _{h,q1} | 0.00 | kN/m | | | | | | |
| Spinta orizzontale - sovr corsia 1 triangolare | S _{h,q1} | 0.00 | kN/m | | | | | | |
| Spinta orizzontale - sovr corsia 2 costante | S _{h,q2} | 0.00 | kN/m | | | | | | |
| Spinta orizzontale - sovr corsia 2 triangolare | S _{h,q2} | 0.00 | kN/m | | | | | | |
| Spinta verticale su soletta - sovraccarico | S _{v,q} | 15.00 | kN/m | | | | | | |
| Peso terreno sopra soletta | W _T | 60.00 | kN/m | | | | | | |
| Peso soletta | W _S | 82.50 | kN/m | | | | | | |
| Peso mensola | W _M | 150.00 | kN/m | | | | | | |
| Peso dente | W _D | 3.06 | kN/m | | | | | | |
| CARICHI PERMANENTI - SISMICA (Mononobe & Okabe) | | | | | | | | | |
| ΔSpinta orizzontale | S _{AE} | 0.00 | kN/m | | | | | | |
| ΔSpinta verticale | S _{AV,E} | 0.00 | kN/m | | | | | | |
| ΔSpinta orizzontale - terreno | S _{ah,TE} | 0.00 | kN/m | | | | | | |
| ΔSpinta orizzontale - sovraccarico costante | S _{h,qE} | 0.00 | kN/m | | | | | | |
| ΔSpinta orizzontale - sovr corsia 1 costante | S _{h,q1E} | 0.00 | kN/m | | | | | | |
| ΔSpinta orizzontale - sovr corsia 1 triangolare | S _{h,q1E} | 0.00 | kN/m | | | | | | |
| ΔSpinta orizzontale - sovr corsia 2 costante | S _{h,q2E} | 0.00 | kN/m | | | | | | |
| ΔSpinta orizzontale - sovr corsia 2 triangolare | S _{h,q2E} | 0.00 | kN/m | | | | | | |
| FORZE D'INERZIA ORIZZONTALI | | | | | | | | | |
| Terreno sopra soletta | | 0 | kN/m | | | | | | |
| Soletta | | 0 | kN/m | | | | | | |
| Mensola | | 0 | kN/m | | | | | | |
| Dente | | 0 | kN/m | | | | | | |
| FORZE D'INERZIA VERTICALI | | | | | | | | | |
| Terreno sopra soletta | | 0 | kN/m | | | | | | |
| Soletta | | 0 | kN/m | | | | | | |
| Mensola | | 0 | kN/m | | | | | | |
| Dente | | 0 | kN/m | | | | | | |
| CARICHI ORIZZONTALI CONCENTRATI - CARATTERISTICI | | | | | | | | | |
| TIPO | Q - SFAV | F _{H1} | 0.00 | kN/m | ψ ₀₁ | 0.60 | ψ ₂₁ | 0.00 | |
| TIPO | G1 - SFAV | F _{H2} | 0.00 | kN/m | ψ ₀₂ | 0.00 | ψ ₂₂ | 0.00 | |
| TIPO | G1 - SFAV | F _{H3} | 0.00 | kN/m | ψ ₀₃ | 0.00 | ψ ₂₃ | 0.00 | |
| TIPO | G1 - SFAV | F _{H4} | 0.00 | kN/m | ψ ₀₄ | 0.00 | ψ ₂₄ | 0.00 | |
| BRACCI DELLE FORZE - CR PIEDE SOLETTA | | | | | | | | | |
| Braccio spinta attiva verticale | b-S _{av} | 3.00 | m | | | | | | |
| Braccio spinta attiva orizzontale - terreno | b-S _{ah,T} | 1.70 | m | | | | | | |
| Braccio spinta orizzontale - sovraccarico | b-S _{ah,q} | 2.55 | m | | | | | | |
| Braccio spinta orizzontale - corsia 1 cost | b-S _{ah,q1} | 1.94 | m | | | | | | |
| Braccio spinta orizzontale - corsia 1 triang | b-S _{ah,q1} | 2.59 | m | | | | | | |
| Braccio spinta orizzontale - corsia 2 cost | b-S _{ah,q2} | 1.08 | m | | | | | | |
| Braccio spinta orizzontale - corsia 2 triang | b-S _{ah,q2} | 1.44 | m | | | | | | |
| Braccio spinta verticale - sovraccarico su soletta | b-S _{av,q} | 2.63 | m | | | | | | |
| Braccio Peso terreno sopra soletta | b-W _T | 2.63 | m | | | | | | |
| Braccio Peso soletta | b-W _S | 1.50 | m | | | | | | |
| Braccio Peso mensola | b-W _M | 1.50 | m | | | | | | |
| Braccio peso dente | b-W _D | 2.83 | m | | | | | | |
| Braccio carico orizzontale 1 | b-F _{H1} | 0.00 | m | | | | | | |
| Braccio carico orizzontale 2 | b-F _{H2} | 0.00 | m | | | | | | |
| Braccio carico orizzontale 3 | b-F _{H3} | 0.00 | m | | | | | | |
| Braccio carico orizzontale 4 | b-F _{H4} | 0.00 | m | | | | | | |
| BRACCI DELLE FORZE SISMICHE - CR PIEDE SOLETTA | | | | | | | | | |
| Braccio Δ spinta attiva orizzontale | b-ΔS _{ah,h} | 1.70 | m | | | | | | |
| Peso terreno sopra soletta - orizzontale | b-W _{T,in} | 3.10 | m | | | | | | |
| Peso soletta - orizzontale | b-W _{S,in} | 0.55 | m | | | | | | |
| Peso mensola - orizzontale | b-W _{M,in} | 3.10 | m | | | | | | |
| COEFFICIENTE PARZIALE | | | | | | | | | |
| γ _R 1.15 | | | | | | | | | |
| MOMENTO STABILIZZANTE | | | | | | | | | |
| M _{STAB} (kNm/m) 632.40 | | | | | | | | | |
| MOMENTO INSTABILIZZANTE | | | | | | | | | |
| M _{INST} (kNm/M) 228.41 | | | | | | | | | |
| FATTORE DI SICUREZZA | | | | | | | | | |
| F _S 2.77 VERIFICATO | | | | | | | | | |

PROGETTAZIONE ATI:

VERIFICA A SCORRIMENTO MURO DI SOSTEGNO A GRAVITA'

In accordo con D.M. 17/01/2018

GEOMETRIA E CARATTERISTICHE TERRENO

| | | | | | |
|--|----------------|---------------------|-------------------|------|------------------------------|
| Altezza della mensola | H | 4.00 | m | | |
| Spessore mensola | s ₁ | 1.50 | m | | |
| Larghezza totale soletta | B | 3.00 | m | | |
| Larghezza oltre la mensola | B* | 0.75 | m | | |
| Altezza soletta | s ₂ | 1.10 | m | | |
| Altezza dente (Hd) | Hd | 0.35 | m | | |
| Larghezza dente (Bd) | Bd | 0.35 | m | | |
| Peso specifico del terreno di riporto | γ | 20.00 | kN/m ³ | | |
| Angolo di attrito del terreno di fondazione | φ' | 18.00 | ° | | |
| Coesione in condizioni drenate terreno di fondazione | c' | 0.00 | kPa | | |
| Carico dovuto da corsia 1 in sommità | no strada | q _{1,sup} | 0.00 | kPa | z _{1,sup} [m] 1.21 |
| Carico dovuto da corsia 1 alla base | | q _{1,inf} | 0.00 | kPa | z _{1,inf} [m] 4.00 |
| Carico dovuto da corsia 1 fondazione | | q _{1,fond} | 0.00 | kPa | z _{1,fond} [m] 5.10 |
| Carico dovuto da corsia 2 superiore | | q _{2,sup} | 0.00 | kPa | z _{2,sup} [m] 2.94 |
| Carico dovuto da corsia 2 alla base | | q _{2,inf} | 0.00 | kPa | z _{2,inf} [m] 4.00 |
| Carico dovuto da corsia 2 fondazione | | q _{2,fond} | 0.00 | kPa | z _{2,fond} [m] 5.10 |
| Sovraccarichi in superficie uniforme | q | 20.00 | kPa | | |
| Peso specifico calcestruzzo | γ _c | 25.00 | kN/m ³ | | |
| Inclinazione interna mensola | α | 90.00 | ° | | |
| Inclinazione esterna mensola | η | 90.00 | ° | | |
| Inclinazione terreno | β | 0.00 | ° | | |
| Angolo d'attrito muro-terreno (per calcolo azioni) | δ | 23.33 | fraz | 0.67 | |
| Coefficiente di spinta attiva | KA | 0.24 | | | |

| | |
|-----------------------------|---------------|
| STATO LIMITE | SLU |
| SPOSTAMENTO LATERALE | Libero |
| β _M | 0 |
| a _{max} | 0.264 |

| ANGOLI | | | |
|----------------|------|-----|-----|
| φ ₃ | 18.0 | rad | 0.6 |
| α | 90.0 | rad | 1.6 |
| η | 90.0 | rad | 1.6 |
| β | 0.0 | rad | 0.0 |
| φ' | 18.0 | rad | 0.3 |
| θ | 62.5 | rad | 1.1 |
| ξ | 0.0 | rad | 0.0 |
| θ _k | 0.0 | rad | 0.0 |
| ζ | 0.0 | rad | 0.0 |

| COEFFICIENTI PARZIALI - A1+M1+R3 | | | |
|---|-----|-------|-------|
| | | FAV | SFAV |
| A1 | G1 | 1.000 | 1.300 |
| | G2 | 0.800 | 1.500 |
| | Q | 0.000 | 1.500 |
| | ECC | 0.000 | 0.000 |

| | | | |
|---|-----------------|-------|--------|
| Parametri pseudo-statici | k _h | 0.000 | |
| | k _v | 0.000 | ↑ alto |
| Coefficiente di spinta attiva - Sismica (Mononobe & Okabe) | K _{ae} | 0.000 | |

CARICHI PERMANENTI

| | | | | | | | | |
|--|----------|-------|-------|-------------------------------|---|--------|------|------|
| Spinta attiva orizzontale totale | SAh | 91.1 | kN/m | ΔSpinta orizzontale | SAE | 0.0 | kN/m | |
| Spinta verticale | Sv | 39.3 | kN/m | ΔSpinta verticale | SAVe | 0.0 | kN/m | |
| Spinta orizzontale - terreno | Sh,T | 66.7 | kN/m | Δspinta orizzontale - terreno | Sah,TE | 0.0 | kN/m | |
| Spinta orizzontale - sovraccarico costante | Terreno | Sh,q | 24.5 | kN/m | ΔSpinta orizzontale - sovraccarico costante | Sh,qE | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 1 costante | | Sh,q1 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 1 costante | Sh,q1E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 1 triangolare | | Sh,q1 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 1 triangolare | Sh,q1E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 2 costante | | Sh,q2 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 2 costante | Sh,q2E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 2 triangolare | | Sh,q2 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 2 triangolare | Sh,q2E | 0.0 | kN/m |
| Spinta verticale su soletta - sovraccarico | Presente | Sv,q | 15.0 | kN/m | | | | |
| Peso terreno sopra soletta | | WT | 60.0 | kN/m | | | | |
| Peso soletta | | WS | 82.5 | kN/m | | | | |
| Peso mensola | | WM | 150.0 | kN/m | | | | |
| Peso dente | | WD | 3.1 | kN/m | | | | |
| Spinta passiva dente | | SPD | 35.0 | kN/m | | | | |

FORZE D'INERZIA ORIZZONTALI

| | | |
|-----------------------|---|------|
| Terreno sopra soletta | 0 | kN/m |
| Soletta | 0 | kN/m |
| Mensola | 0 | kN/m |
| Dente | 0 | kN/m |

FORZE D'INERZIA VERTICALI

| | | |
|-----------------------|---|------|
| Terreno sopra soletta | 0 | kN/m |
| Soletta | 0 | kN/m |
| Mensola | 0 | kN/m |
| Dente | 0 | kN/m |

CARICHI ORIZZONTALI CONCENTRATI

| | | | | | | | | | |
|------|------|------|-----------------|------|------|-----------------|------|-----------------|------|
| TIPO | Q - | SFAV | F _{H1} | 0.00 | kN/m | ψ ₀₁ | 0.60 | ψ ₀₁ | 0.00 |
| TIPO | G1 - | SFAV | F _{H2} | 0.00 | kN/m | ψ ₀₂ | 0.00 | ψ ₀₂ | 0.00 |
| TIPO | G1 - | SFAV | F _{H3} | 0.00 | kN/m | ψ ₀₃ | 0.00 | ψ ₀₃ | 0.00 |
| TIPO | G1 - | SFAV | F _{H4} | 0.00 | kN/m | ψ ₀₄ | 0.00 | ψ ₀₄ | 0.00 |

| | | |
|--------------------------------------|------------------------|--------|
| COEFFICIENTE PARZIALE | γ _R | 1.10 |
| RISULTANTE VERTICALE | N (kNm/m) | 387.16 |
| AZIONE ORIZZONTALE RESISTENTE | T _{Rd} (kN/m) | 146.16 |
| AZIONE ORIZZONTALE AGENTE | T _{Ed} (kN/m) | 118.46 |

| | | | |
|-----------------------------|----------------|------|-------------------|
| FATTORE DI SICUREZZA | F _s | 1.23 | VERIFICATO |
|-----------------------------|----------------|------|-------------------|

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| DETERMINAZIONE DELLA CAPACITA' PORTANTE LIMITE DI FONDAZIONI SUPERFICIALI RETTANGOLARI FORMULA GENERALE DI BRINCH - HANSEN (1970) | | | | | |
|--|--------|---|---------|------------|--------------|
| CONDIZIONI DRENATE | | $Q_{lim} = 0.5 \cdot \gamma \cdot B \cdot N_{\gamma} \cdot i_{\gamma} \cdot s_{\gamma} \cdot b_{\gamma} \cdot g_{\gamma} + q \cdot N_q \cdot d_q \cdot i_q \cdot s_q \cdot b_q \cdot g_q + c \cdot N_c \cdot d_c \cdot i_c \cdot s_c \cdot b_c \cdot g_c$ | | | |
| | | Fattori di capacità portante | | | |
| | | ϕ' | N_c | N_q | N_{γ} |
| | | 0 | 5.14 | 1.00 | 0.00 |
| | | 1 | 5.38 | 1.09 | 0.07 |
| | | 2 | 5.63 | 1.20 | 0.15 |
| | | 3 | 5.90 | 1.31 | 0.24 |
| | | 4 | 6.19 | 1.43 | 0.34 |
| | | 5 | 6.49 | 1.57 | 0.45 |
| | | 6 | 6.81 | 1.72 | 0.57 |
| | | 7 | 7.16 | 1.88 | 0.71 |
| | | 8 | 7.53 | 2.06 | 0.86 |
| | | 9 | 7.92 | 2.25 | 1.03 |
| | | 10 | 8.34 | 2.47 | 1.22 |
| | | 11 | 8.80 | 2.71 | 1.44 |
| | | 12 | 9.28 | 2.97 | 1.69 |
| | | 13 | 9.81 | 3.26 | 1.97 |
| | | 14 | 10.37 | 3.59 | 2.29 |
| | | 15 | 10.98 | 3.94 | 2.65 |
| | | 16 | 11.63 | 4.34 | 3.06 |
| | | 17 | 12.34 | 4.77 | 3.53 |
| | | 18 | 13.10 | 5.26 | 4.07 |
| | | 19 | 13.93 | 5.80 | 4.68 |
| | | 20 | 14.83 | 6.40 | 5.39 |
| | | 21 | 15.81 | 7.07 | 6.20 |
| | | 22 | 16.88 | 7.82 | 7.13 |
| | | 23 | 18.05 | 8.66 | 8.20 |
| | | 24 | 19.32 | 9.60 | 9.44 |
| | | 25 | 20.72 | 10.66 | 10.88 |
| | | 26 | 22.25 | 11.85 | 12.54 |
| | | 27 | 23.94 | 13.20 | 14.47 |
| | | 28 | 25.80 | 14.72 | 16.72 |
| | | 29 | 27.86 | 16.44 | 19.34 |
| | | 30 | 30.14 | 18.40 | 22.40 |
| | | 31 | 32.67 | 20.63 | 25.99 |
| | | 32 | 35.49 | 23.18 | 30.21 |
| | | 33 | 38.64 | 26.09 | 35.19 |
| | | 34 | 42.16 | 29.44 | 41.06 |
| | | 35 | 46.12 | 33.30 | 48.03 |
| | | 36 | 50.59 | 37.75 | 56.31 |
| | | 37 | 55.63 | 42.92 | 66.19 |
| | | 38 | 61.35 | 48.93 | 78.02 |
| | | 39 | 67.87 | 55.96 | 92.25 |
| | | 40 | 75.31 | 64.20 | 109.41 |
| | | 41 | 83.86 | 73.90 | 130.21 |
| | | 42 | 93.71 | 85.37 | 155.54 |
| | | 43 | 105.11 | 99.01 | 186.53 |
| | | 44 | 118.37 | 115.31 | 224.63 |
| | | 45 | 133.87 | 134.87 | 271.75 |
| | | 46 | 152.10 | 158.50 | 330.34 |
| | | 47 | 173.64 | 187.21 | 403.65 |
| | | 48 | 199.26 | 222.30 | 496.00 |
| | | 49 | 229.92 | 265.50 | 613.14 |
| | | 50 | 266.88 | 319.06 | 762.86 |
| Determinazione dei coefficienti | | | | | |
| Fattori correttivi dipendenti dall'inclinazione del carico | | | | | |
| $i_{\gamma} =$ | 0.479 | $i_q =$ | 0.713 | $i_c =$ | 0.646 |
| Fattori correttivi dipendenti dalla profondità del piano di posa | | | | | |
| $d_{\gamma} =$ | 1.000 | | | | |
| $d_q =$ | 1.227 | per $D/B' \leq 1$ | | | |
| | | quindi | $d_q =$ | 1.227 | |
| $d_q =$ | 12.236 | per $D/B' > 1$ | | | |
| $d_c =$ | 1.293 | per $D/B' \leq 1$ | | | |
| | | quindi | $d_c =$ | 1.293 | |
| $d_c =$ | 1.253 | per $D/B' > 1$ | | | |
| Fattori correttivi dipendenti dalla forma della fondazione | | | | | |
| $s_{\gamma} =$ | 1.000 | $s_q =$ | 1.000 | $s_c =$ | 1.000 |
| Fattori correttivi dipendenti dall'inclinazione dell'intradosso fondazione | | | | | |
| $b_{\gamma} =$ | 1.000 | $b_q =$ | 1.000 | $b_c =$ | 1.000 |
| Fattori correttivi dipendenti dall'inclinazione del piano campagna | | | | | |
| $g_{\gamma} =$ | 1.000 | $g_q =$ | 1.000 | $g_c =$ | 1.000 |
| COEFFICIENTE PARZIALE | | $\gamma_R =$ | 1.40 | | |
| CAPACITA' PORTANTE LIMITE | | $Q_{lim} \text{ (kPa)} =$ | 152.55 | | |
| COEFFICIENTE DI SICUREZZA | | $FS = (Q_{lim}-q)/(Q_{es}-q) =$ | 1.09 | VERIFICATO | |

User:
Peso efficace terreno
fondazione

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| CONDIZIONI NON DRENATE | | $Q_{lim} = cu \cdot (3.14 + 2) \cdot (dc \cdot ic \cdot sc \cdot bc \cdot gc) + q$ | |
|---|---------------------------------------|--|------------|
| Affondamento della fondazione | D (m) = | 2.0 | |
| Dim. minore fondazione efficace equivalente | B' (m) = | 2.7 | |
| Dim. maggiore fondazione efficace equivalente | L' (m) = | 1.0 | |
| Carico verticale agente sulla fondazione | N (kN) = | 381 | |
| Carico orizzontale agente sulla fondazione | H (kN) = | 118 | |
| Coesione in condizioni non drenate | cu (kN/m ²) = | 80.0 | # |
| Azione laterale stabilizzante | q (kN/m ²) = | 36.0 | |
| Inclinazione intradosso fondazione | α (°) = | 0.0 | |
| Inclinazione piano campagna | β (°) = | 0.0 | |
| sc = | 1.000 | ic = | 0.866 |
| dc = | 1.293 per D/B' <= 1 | quindi dc = | 1.293 # |
| dc = | 1.253 per D/B' > 1 | | |
| gc = | 1.000 | | |
| COEFFICIENTE PARZIALE | γ_R | 1.400 | |
| CAPACITA' PORTANTE LIMITE | Q_{lim} = | 354.788 | |
| COEFFICIENTE DI SICUREZZA | $FS = (Q_{lim} - q) / (Q_{es} - q) =$ | 2.54 | VERIFICATO |

Si riassumono le verifiche geotecniche allo SLU

| | | |
|--------|------|------------|
| RIB | 2.77 | VERIFICATO |
| SCOR | 1.23 | VERIFICATO |
| CAP DR | 1.09 | VERIFICATO |
| CAP ND | 2.54 | VERIFICATO |

PROGETTAZIONE ATI:

14.4. VERIFICA MURO SU TERRENO PEGGIORE - SLV

VERIFICA A RIBALTAMENTO MURO DI SOSTEGNO A GRAVITA'

In accordo con D.M. 17/01/2018

GEOMETRIA E CARATTERISTICHE TERRENO

| | | | |
|--|---------------------|-------|-------------------|
| Altezza della mensola (Hp) | Hp | 4.00 | m |
| Spessore sommità mensola (Bc-b) | S ₁ | 1.50 | m |
| Larghezza totale soletta (B) | B | 3.00 | m |
| Larghezza oltre la mensola (Bv) | Bv | 0.75 | m |
| Altezza soletta (Hf) | S ₂ | 1.10 | m |
| Altezza dente (Hd) | Hd | 0.35 | m |
| Larghezza dente (Bd) | Bd | 0.35 | m |
| Peso specifico del terreno di riporto | γ | 20.00 | kN/m ³ |
| Angolo di attrito del terreno di riporto | φ' | 35.00 | ° |
| Coesione in condizioni drenate | c' | 0.00 | kPa |
| Carico dovuto da corsia 1 in sommità | q _{1,sup} | 0.00 | kPa |
| Carico dovuto da corsia 1 alla base | q _{1,inf} | 0.00 | kPa |
| Carico dovuto da corsia 1 fondazione | q _{1,fond} | 0.00 | kPa |
| Carico dovuto da corsia 2 superiore | q _{2,sup} | 0.00 | kPa |
| Carico dovuto da corsia 2 alla base | q _{2,inf} | 0.00 | kPa |
| Carico dovuto da corsia 2 fondazione | q _{2,fond} | 0.00 | kPa |
| Sovaccarichi in superficie uniforme | q | 20.00 | kPa |
| Peso specifico calcestruzzo | γ _C | 25.00 | kN/m ³ |
| Inclinazione interna mensola | α | 90.00 | ° |
| Inclinazione esterna mensola | η | 90.00 | ° |
| Inclinazione terreno | β | 0.00 | ° |
| Angolo d'attrito muro-terreno | δ | 23.33 | fraz |
| Coefficiente di spinta attiva | KA | 0.24 | |

STATO LIMITE **SLV**

SPOSTAMENTO LATERALE **Libero**

β_M **0.38**

a_{max} **0.264**

ANGOLI

| | | | |
|----------------|------|-----|------|
| φ | 35.0 | rad | 0.6 |
| α | 90.0 | rad | 1.6 |
| η | 90.0 | rad | 1.6 |
| β | 0.0 | rad | 0.0 |
| δ | 23.3 | rad | 0.4 |
| θ | 62.5 | rad | 1.1 |
| ξ | 0.0 | rad | 0.0 |
| θ _k | 6.0 | rad | 0.11 |
| ζ | 0.0 | rad | 0.0 |

COEFFICIENTI PARZIALI - A1+M1+R3

| | | | |
|----|-----|-------|-------|
| | | FAV | SFAV |
| A1 | G1 | 1.000 | 1.000 |
| | G2 | 1.000 | 1.000 |
| | Q | 0.000 | 1.000 |
| | ECC | 0.000 | 0.000 |
| | | | |

| | | |
|--|-----------------|--------|
| Parametri pseudo-statici | k _H | 0.100 |
| | k _V | -0.050 |
| Coefficiente di spinta attiva - Sismica (Mononobe & Okabe) | K _{ae} | 0.294 |

↑ alto

CARICHI PERMANENTI - CARATTERISTICI

| | | | |
|--|--------------------|--------|------|
| Spinta attiva orizzontale totale | S _{Ah} | 89.89 | kN/m |
| Spinta verticale | S _v | 38.78 | kN/m |
| Spinta orizzontale - terreno | S _{h,T} | 66.66 | kN/m |
| Spinta orizzontale - sovraccarico costante | S _{h,q} | 23.23 | kN/m |
| Spinta orizzontale - sovr corsia 1 costante | S _{h,q1} | 0.00 | kN/m |
| Spinta orizzontale - sovr corsia 1 triangolare | S _{h,q1E} | 0.00 | kN/m |
| Spinta orizzontale - sovr corsia 2 costante | S _{h,q2} | 0.00 | kN/m |
| Spinta orizzontale - sovr corsia 2 triangolare | S _{h,q2E} | 0.00 | kN/m |
| Spinta verticale su soletta - sovraccarico | S _{v,q} | 14.25 | kN/m |
| Peso terreno sopra soletta | W _T | 60.00 | kN/m |
| Peso soletta | W _S | 82.50 | kN/m |
| Peso mensola | W _M | 150.00 | kN/m |
| Peso dente | W _D | 3.06 | kN/m |

CARICHI PERMANENTI - SISMICA (Mononobe&Okabe)

| | | | |
|---|---------------------|-------|------|
| ΔSpinta orizzontale | S _{AE} | 18.66 | kN/m |
| ΔSpinta verticale | S _{AV,E} | 8.05 | kN/m |
| Δspinta orizzontale - terreno | S _{ah,TE} | 13.65 | kN/m |
| ΔSpinta orizzontale - sovraccarico costante | S _{h,qE} | 5.01 | kN/m |
| ΔSpinta orizzontale - sovr corsia 1 costante | S _{h,q1E} | 0.00 | kN/m |
| ΔSpinta orizzontale - sovr corsia 1 triangolare | S _{h,q1EE} | 0.00 | kN/m |
| ΔSpinta orizzontale - sovr corsia 2 costante | S _{h,q2E} | 0.00 | kN/m |
| ΔSpinta orizzontale - sovr corsia 2 triangolare | S _{h,q2EE} | 0.00 | kN/m |

FORZE D'INERZIA ORIZZONTALI

| | | |
|-----------------------|----|------|
| Terreno sopra soletta | 6 | kN/m |
| Soletta | 8 | kN/m |
| Mensola | 15 | kN/m |
| Dente | 0 | kN/m |

FORZE D'INERZIA VERTICALI

| | | |
|-----------------------|----|------|
| Terreno sopra soletta | -3 | kN/m |
| Soletta | -4 | kN/m |
| Mensola | -8 | kN/m |
| Dente | 0 | kN/m |

CARICHI ORIZZONTALI CONCENTRATI - CARATTERISTICI

| | | | | | | | | |
|------|-----------|-----------------|------|------|-----------------|------|-----------------|------|
| TIPO | Q - SFAV | F _{H1} | 0.00 | kN/m | ψ ₀₁ | 0.60 | ψ ₂₁ | 0.00 |
| TIPO | G1 - SFAV | F _{H2} | 0.00 | kN/m | ψ ₀₂ | 0.00 | ψ ₂₂ | 0.00 |
| TIPO | G1 - SFAV | F _{H3} | 0.00 | kN/m | ψ ₀₃ | 0.00 | ψ ₂₃ | 0.00 |
| TIPO | G1 - SFAV | F _{H4} | 0.00 | kN/m | ψ ₀₄ | 0.00 | ψ ₂₄ | 0.00 |

BRACCI DELLE FORZE - CR PIEDE SOLETTA

| | | | |
|--|-----------------------|------|---|
| Braccio spinta attiva verticale | b-S _{av} | 3.00 | m |
| Braccio spinta attiva orizzontale - terreno | b-S _{ah,T} | 1.70 | m |
| Braccio spinta orizzontale - sovraccarico | b-S _{ah,q} | 2.55 | m |
| Braccio spinta orizzontale - corsia 1 cost | b-S _{ah,q1} | 1.94 | m |
| Braccio spinta orizzontale - corsia 1 triang | b-S _{ah,q1E} | 2.59 | m |
| Braccio spinta orizzontale - corsia 2 cost | b-S _{ah,q2} | 1.08 | m |
| Braccio spinta orizzontale - corsia 2 triang | b-S _{ah,q2E} | 1.44 | m |
| Braccio spinta verticale - sovraccarico su soletta | b-S _{av,q} | 2.63 | m |
| Braccio Peso terreno sopra soletta | b-W _T | 2.63 | m |
| Braccio Peso soletta | b-W _S | 1.50 | m |
| Braccio Peso mensola | b-W _M | 1.50 | m |
| Braccio peso dente | b-W _D | 2.83 | m |
| Braccio carico orizzontale 1 | b-F _{H,1} | 0.00 | m |
| Braccio carico orizzontale 2 | b-F _{H,2} | 0.00 | m |
| Braccio carico orizzontale 3 | b-F _{H,3} | 0.00 | m |
| Braccio carico orizzontale 4 | b-F _{H,4} | 0.00 | m |

BRACCI DELLE FORZE SISMICHE - CR PIEDE SOLETTA

| | | | |
|--|----------------------|------|---|
| Braccio Δ spinta attiva orizzontale | b-ΔS _{av,h} | 1.70 | m |
| Peso terreno sopra soletta - orizzontale | b-W _{T,ih} | 3.10 | m |
| Peso soletta - orizzontale | b-W _{S,ih} | 0.55 | m |
| Peso mensola - orizzontale | b-W _{M,ih} | 3.10 | m |

| | | |
|-------------------------|---------------------------|--------|
| COEFFICIENTE PARZIALE | γ _R | 1.00 |
| MOMENTO STABILIZZANTE | M _{STAB} (kNm/m) | 666.95 |
| MOMENTO INSTABILIZZANTE | M _{INST} (kNm/M) | 278.41 |
| FATTORE DI SICUREZZA | F _S | 2.40 |

VERIFICATO

PROGETTAZIONE ATI:

VERIFICA A SCORRIMENTO MURO DI SOSTEGNO A GRAVITA'

In accordo con D.M. 17/01/2018

GEOMETRIA E CARATTERISTICHE TERRENO

| | | | | | | | | | |
|--|----------------|---------------------|-------------------|-------------------------|------|--|--|---|---------------|
| Altezza della mensola | H | 4.00 | m | | | | | STATO LIMITE | SLV |
| Spessore mensola | s ₁ | 1.50 | m | | | | | SPOSTAMENTO LATERALE | Libero |
| Larghezza totale soletta | B | 3.00 | m | | | | | β_M | 0.38 |
| Larghezza oltre la mensola | B* | 0.75 | m | | | | | a_{max} | 0.264 |
| Altezza soletta | s ₂ | 1.10 | m | | | | | ANGOLI | |
| Altezza dente (Hd) | Hd | 0.35 | m | | | | | φ ₃ | 18.0 rad 0.6 |
| Larghezza dente (Bd) | Bd | 0.35 | m | | | | | α | 90.0 rad 1.6 |
| Peso specifico del terreno di riporto | γ | 20.00 | kN/m ³ | | | | | η | 90.0 rad 1.6 |
| Angolo di attrito del terreno di fondazione | φ' | 18.00 | ° | | | | | β | 0.0 rad 0.0 |
| Coesione in condizioni drenate terreno di fondazione | c' | 0.00 | kPa | | | | | φ' | 18.0 rad 0.3 |
| Carico dovuto da corsia 1 in sommità | no strada | q _{1,sup} | 0.00 kPa | z _{1,sup} [m] | 1.21 | | | θ | 62.5 rad 1.1 |
| Carico dovuto da corsia 1 alla base | | q _{1,inf} | 0.00 kPa | z _{1,inf} [m] | 4.00 | | | ξ | 0.0 rad 0.0 |
| Carico dovuto da corsia 1 fondazione | | q _{1,fond} | 0.00 kPa | z _{1,fond} [m] | 5.10 | | | θ _k | 6.0 rad 0.1 |
| Carico dovuto da corsia 2 superiore | | q _{2,sup} | 0.00 kPa | z _{2,sup} [m] | 2.94 | | | ζ | 0.0 rad 0.0 |
| Carico dovuto da corsia 2 alla base | | q _{2,inf} | 0.00 kPa | z _{2,inf} [m] | 4.00 | | | | |
| Carico dovuto da corsia 2 fondazione | | q _{2,fond} | 0.00 kPa | z _{2,fond} [m] | 5.10 | | | | |
| Sovraccarichi in superficie uniforme | | q | 20.00 kPa | | | | | COEFFICIENTI PARZIALI - A1+M1+R3 | |
| Peso specifico calcestruzzo | γ _C | 25.00 | kN/m ³ | | | | | | |
| Inclinazione interna mensola | α | 90.00 | ° | | | | | | |
| Inclinazione esterna mensola | η | 90.00 | ° | | | | | | |
| Inclinazione terreno | β | 0.00 | ° | | | | | | |
| Angolo d'attrito muro-terreno (per calcolo azioni) | δ | 23.33 | fraz | 0.67 | | | | | |
| Coefficiente di spinta attiva | K _A | 0.24 | | | | | | | |

| | | |
|---|-----------------|--------|
| Parametri pseudo-statici | k _H | 0.100 |
| | k _V | -0.050 |
| Coefficiente di spinta attiva - Sismica (Mononobe & Okabe) | K _{ae} | 0.294 |

CARICHI PERMANENTI

| | | | | | | | | |
|--|----------|-------|-------|-------------------------------|---|--------|------|------|
| Spinta attiva orizzontale totale | SAh | 89.9 | kN/m | ΔSpinta orizzontale | SAE | 18.7 | kN/m | |
| Spinta verticale | Sv | 38.8 | kN/m | ΔSpinta verticale | SAV | 8.0 | kN/m | |
| Spinta orizzontale - terreno | Sh,T | 66.7 | kN/m | ΔSpinta orizzontale - terreno | Sah,TE | 13.7 | kN/m | |
| Spinta orizzontale - sovraccarico costante | Terreno | Sh,q | 23.2 | kN/m | ΔSpinta orizzontale - sovraccarico costante | Sh,qE | 5.0 | kN/m |
| Spinta orizzontale - sovr corsia 1 costante | | Sh,q1 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 1 costante | Sh,q1E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 1 triangolare | | Sh,q1 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 1 triangolare | Sh,q1E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 2 costante | | Sh,q2 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 2 costante | Sh,q2E | 0.0 | kN/m |
| Spinta orizzontale - sovr corsia 2 triangolare | | Sh,q2 | 0.0 | kN/m | ΔSpinta orizzontale - sovr corsia 2 triangolare | Sh,q2E | 0.0 | kN/m |
| Spinta verticale su soletta - sovraccarico | Presente | Sv,q | 14.2 | kN/m | | | | |
| Peso terreno sopra soletta | | WT | 60.0 | kN/m | | | | |
| Peso soletta | | WS | 82.5 | kN/m | | | | |
| Peso mensola | | WM | 150.0 | kN/m | | | | |
| Peso dente | | WD | 3.1 | kN/m | | | | |
| Spinta passiva dente | | SPD | 35.0 | kN/m | | | | |

FORZE D'INERZIA ORIZZONTALI

| | | |
|-----------------------|----|------|
| Terreno sopra soletta | 6 | kN/m |
| Soletta | 8 | kN/m |
| Mensola | 15 | kN/m |
| Dente | 0 | kN/m |

FORZE D'INERZIA VERTICALI

| | | |
|-----------------------|----|------|
| Terreno sopra soletta | -3 | kN/m |
| Soletta | -4 | kN/m |
| Mensola | -8 | kN/m |
| Dente | 0 | kN/m |

CARICHI ORIZZONTALI CONCENTRATI

| | | | | | | | | | |
|------|------|------|-----------------|------|------|-----------------|------|-----------------|------|
| TIPO | Q - | SFAV | F _{H1} | 0.00 | kN/m | ψ ₀₁ | 0.60 | ψ ₀₁ | 0.00 |
| TIPO | G1 - | SFAV | F _{H2} | 0.00 | kN/m | ψ ₀₂ | 0.00 | ψ ₀₂ | 0.00 |
| TIPO | G1 - | SFAV | F _{H3} | 0.00 | kN/m | ψ ₀₃ | 0.00 | ψ ₀₃ | 0.00 |
| TIPO | G1 - | SFAV | F _{H4} | 0.00 | kN/m | ψ ₀₄ | 0.00 | ψ ₀₄ | 0.00 |

| | | |
|--------------------------------------|------------------------|--------|
| COEFFICIENTE PARZIALE | γ _R | 1.00 |
| RISULTANTE VERTICALE | N (kNm/m) | 341.81 |
| AZIONE ORIZZONTALE RESISTENTE | T _{Rd} (kN/m) | 146.04 |
| AZIONE ORIZZONTALE AGENTE | T _{Ed} (kN/m) | 138.21 |
| FATTORE DI SICUREZZA | F _S | 1.06 |

VERIFICATO

PROGETTAZIONE ATI:

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| DETERMINAZIONE DELLA CAPACITA' PORTANTE LIMITE DI FONDAZIONI SUPERFICIALI RETTANGOLARI | | | | Fattori di capacità portante | | | |
|---|--|--|--|------------------------------|--------|--------|------------|
| FORMULA GENERALE DI BRINCH - HANSEN (1970) | | | | ϕ' | Nc | Nq | N_γ |
| CONDIZIONI DRENATE $Q_{lim} = 0.5 \cdot \gamma \cdot B \cdot N_\gamma \cdot i_\gamma \cdot s_\gamma \cdot b_\gamma \cdot g_\gamma + q \cdot N_q \cdot d_q \cdot i_q \cdot s_q \cdot b_q \cdot g_q + c \cdot N_c \cdot d_c \cdot i_c \cdot s_c \cdot b_c \cdot g_c$ | | | | 0 | 5.14 | 1.00 | 0.00 |
| | | | | 1 | 5.38 | 1.09 | 0.07 |
| | | | | 2 | 5.63 | 1.20 | 0.15 |
| | | | | 3 | 5.90 | 1.31 | 0.24 |
| | | | | 4 | 6.19 | 1.43 | 0.34 |
| | | | | 5 | 6.49 | 1.57 | 0.45 |
| | | | | 6 | 6.81 | 1.72 | 0.57 |
| | | | | 7 | 7.16 | 1.88 | 0.71 |
| | | | | 8 | 7.53 | 2.06 | 0.86 |
| | | | | 9 | 7.92 | 2.25 | 1.03 |
| | | | | 10 | 8.34 | 2.47 | 1.22 |
| | | | | 11 | 8.80 | 2.71 | 1.44 |
| | | | | 12 | 9.28 | 2.97 | 1.69 |
| | | | | 13 | 9.81 | 3.26 | 1.97 |
| | | | | 14 | 10.37 | 3.59 | 2.29 |
| | | | | 15 | 10.98 | 3.94 | 2.65 |
| | | | | 16 | 11.63 | 4.34 | 3.06 |
| | | | | 17 | 12.34 | 4.77 | 3.53 |
| | | | | 18 | 13.10 | 5.26 | 4.07 |
| | | | | 19 | 13.93 | 5.80 | 4.68 |
| | | | | 20 | 14.83 | 6.40 | 5.39 |
| | | | | 21 | 15.81 | 7.07 | 6.20 |
| | | | | 22 | 16.88 | 7.82 | 7.13 |
| | | | | 23 | 18.05 | 8.66 | 8.20 |
| | | | | 24 | 19.32 | 9.60 | 9.44 |
| | | | | 25 | 20.72 | 10.66 | 10.88 |
| | | | | 26 | 22.25 | 11.85 | 12.54 |
| | | | | 27 | 23.94 | 13.20 | 14.47 |
| | | | | 28 | 25.80 | 14.72 | 16.72 |
| | | | | 29 | 27.86 | 16.44 | 19.34 |
| | | | | 30 | 30.14 | 18.40 | 22.40 |
| | | | | 31 | 32.67 | 20.63 | 25.99 |
| | | | | 32 | 35.49 | 23.18 | 30.21 |
| | | | | 33 | 38.64 | 26.09 | 35.19 |
| | | | | 34 | 42.16 | 29.44 | 41.06 |
| | | | | 35 | 46.12 | 33.30 | 48.03 |
| | | | | 36 | 50.59 | 37.75 | 56.31 |
| | | | | 37 | 55.63 | 42.92 | 66.19 |
| | | | | 38 | 61.35 | 48.93 | 78.02 |
| | | | | 39 | 67.87 | 55.96 | 92.25 |
| | | | | 40 | 75.31 | 64.20 | 109.41 |
| | | | | 41 | 83.86 | 73.90 | 130.21 |
| | | | | 42 | 93.71 | 85.37 | 155.54 |
| | | | | 43 | 105.11 | 99.01 | 186.53 |
| | | | | 44 | 118.37 | 115.31 | 224.63 |
| | | | | 45 | 133.87 | 134.87 | 271.75 |
| | | | | 46 | 152.10 | 158.50 | 330.34 |
| | | | | 47 | 173.64 | 187.21 | 403.65 |
| | | | | 48 | 199.26 | 222.30 | 496.00 |
| | | | | 49 | 229.92 | 265.50 | 613.14 |
| | | | | 50 | 266.88 | 319.06 | 762.86 |
| Determinazione dei coefficienti | | | | | | | |
| Fattori correttivi dipendenti dall'inclinazione del carico | | | | | | | |
| $i_\gamma = 0.365$ $i_q = 0.634$ $i_c = 0.548$ | | | | | | | |
| Fattori correttivi dipendenti dalla profondità del piano di posa | | | | | | | |
| $d_\gamma = 1.000$ | | | | | | | |
| $d_q = 1.277$ per $D/B' \leq 1$ | | | | | | | |
| quindi $d_q = 1.277$ | | | | | | | |
| $d_q = 13.941$ per $D/B' > 1$ | | | | | | | |
| $d_c = 1.356$ per $D/B' \leq 1$ | | | | | | | |
| quindi $d_c = 1.356$ | | | | | | | |
| $d_c = 1.291$ per $D/B' > 1$ | | | | | | | |
| Fattori correttivi dipendenti dalla forma della fondazione | | | | | | | |
| $s_\gamma = 1.000$ $s_q = 1.000$ $s_c = 1.000$ | | | | | | | |
| Fattori correttivi dipendenti dall'inclinazione dell'intradosso fondazione | | | | | | | |
| $b_\gamma = 1.000$ $b_q = 1.000$ $b_c = 1.000$ | | | | | | | |
| Fattori correttivi dipendenti dall'inclinazione del piano campagna | | | | | | | |
| $g_\gamma = 1.000$ $g_q = 1.000$ $g_c = 1.000$ | | | | | | | |
| COEFFICIENTE PARZIALE $\gamma_R = 1.20$ | | | | | | | |
| CAPACITA' PORTANTE LIMITE $Q_{lim} \text{ (kPa)} = 152.53$ | | | | | | | |
| COEFFICIENTE DI SICUREZZA $FS = (Q_{lim}-q)/(Q_{es}-q) = 1.01$ | | | | VERIFICATO | | | |

User:
Peso efficace terreno
fondazione

RELAZIONE DI CALCOLO GALLERIA ARTIFICIALE E PROLUNGAMENTO GALLERIA

| CONDIZIONI NON DRENATE | | $Q_{lim} = cu \cdot (3.14 + 2) \cdot (dc \cdot ic \cdot sc \cdot bc \cdot gc) + q$ | |
|---|---------------------------------|--|--------------|
| Affondamento della fondazione | D (m) = | 2.0 | |
| Dim. minore fondazione efficace equivalente | B' (m) = | 2.2 | |
| Dim. maggiore fondazione efficace equivalente | L' (m) = | 1.0 | |
| Carico verticale agente sulla fondazione | N (kN) = | 339 | |
| Carico orizzontale agente sulla fondazione | H (kN) = | 138 | |
| Coesione in condizioni non drenate | cu (kN/m ²) = | 80.0 | # |
| Azione laterale stabilizzante | q (kN/m ²) = | 36.0 | |
| Inclinazione intradosso fondazione | α (°) = | 0.0 | |
| Inclinazione piano campagna | β (°) = | 0.0 | |
| sc = | 1.000 | ic = | 0.804 |
| dc = | 1.356 | per D/B' <= 1 | |
| | | quindi | dc = 1.356 # |
| dc = | 1.291 | per D/B' > 1 | |
| gc = | 1.000 | | |
| COEFFICIENTE PARZIALE | γ_R | 1.200 | |
| CAPACITA' PORTANTE LIMITE | Q_{lim} = | 403.890 | |
| COEFFICIENTE DI SICUREZZA | $FS = (Q_{lim}-q)/(Q_{es}-q) =$ | 2.68 | VERIFICATO |

Di seguito si riassumono i coefficienti di sicurezza ottenuti

| | | |
|--------|------|------------|
| RIB | 2.40 | VERIFICATO |
| SCOR | 1.06 | VERIFICATO |
| CAP DR | 1.01 | VERIFICATO |
| CAP ND | 2.68 | VERIFICATO |

PROGETTAZIONE ATI:

15. CONCLUSIONI

Oggetto della presente relazione sono state le analisi per la valutazione della sicurezza delle gallerie artificiali d'imbocco e dei muri d'invito inseriti all'interno del progetto della E78 Grosseto – Fano, Tronco Selci Lama – S. Stefano di Gaifa – Lotto 7.

L'opera è stata studiata e verificata in tutte le combinazioni più sfavorevoli tra quelle presenti nella tratta di progetto risultando quindi sicura ai sensi delle NTC18.

PROGETTAZIONE ATI:

ALLEGATO DI CALCOLO: OUTPUT SAP2000

Table: Material Properties 01 - General, Part 1 of 2

Table: Material Properties 01 - General, Part 1 of 2

| Material | Type | Grade | SymType | TempDepend | Color | GUID |
|----------|----------|--------|-----------|------------|---------|--------------------------------------|
| B450C | Rebar | B450C | Uniaxial | No | Green | e6729f9e-31fd-4c43-b854-c0f6561a273c |
| C28/35 | Concrete | C28/35 | Isotropic | No | Yellow | 61f11988-1fd0-4fb1-8cd1-9631d17302b4 |
| S355 | Steel | S355 | Isotropic | No | Magenta | |
| Tendon | Tendon | | Uniaxial | No | Magenta | 02967ba4-25dc-438b-8e22-bf5885592edf |

Table: Material Properties 01 - General, Part 2 of 2

Table: Material Properties 01 - General, Part 2 of 2

| Material | Notes |
|----------|---|
| B450C | NTC2008 B450C 27/09/2021 15:29:38 |
| C28/35 | UNI EN 206-1:2006 e UNI 11104:2004 C28/35 27/09/2021 14:55:10 |
| S355 | NTC2008 S355 27/09/2021 14:55:10 |
| Tendon | Tendon added 28/09/2021 09:15:32 |

Table: Material Properties 02 - Basic Mechanical Properties

Table: Material Properties 02 - Basic Mechanical Properties

| Material | UnitWeight KN/m3 | UnitMass KN-s2/m4 | E1 KN/m2 | G12 KN/m2 | U12 | A1 1/C |
|----------|---------------------|----------------------|-----------------|-----------------|-----|------------|
| B450C | 7.6973E+01 | 7.8490E+00 | 210000000 | | | 1.1700E-05 |
| C28/35 | 2.4993E+01 | 2.5485E+00 | 32308000. | 13461666. 67 | 0.2 | 1.0000E-05 |
| S355 | 7.6973E+01 | 7.8490E+00 | 210000000 | 80769230. 77 | 0.3 | 1.1700E-05 |
| Tendon | 7.6973E+01 | 7.8490E+00 | 196500599. 9 | | | 1.1700E-05 |

PROGETTAZIONE ATI:

Table: Load Pattern Definitions

Table: Load Pattern Definitions

| LoadPat | DesignType | SelfWtMult | AutoLoad |
|-------------------------|------------|------------|----------|
| DEAD | Dead | 1. | |
| TERR_SIMM | Live | 0. | |
| TERR_A--SIMM | Live | 0. | |
| SIMM_KA | Live | 0. | |
| SIMM_K0 | Live | 0. | |
| A--SIMM_KA | Live | 0. | |
| A--SIMM_K0 | Live | 0. | |
| SIMM_SOVR_K A | Live | 0. | |
| SIMM_SOVR_K 0 | Live | 0. | |
| A-- SIMM_SOVR_K A | Live | 0. | |
| A-- SIMM_SOVR_K 0 | Live | 0. | |
| SOVR | Live | 0. | |
| SISMA WOOD | Live | 0. | |
| iDROSTATICA | Live | 0. | |
| SISMA WOOD SLD | Live | 0. | |

Table: Load Case Definitions, Part 1 of 2

Table: Load Case Definitions, Part 1 of 2

| Case | Type | InitialCond | ModalCase | BaseCase | MassSource | DesActOpt |
|-------------------------|-----------|-------------|-----------|----------|------------|-----------|
| DEAD | LinStatic | Zero | | | | Prog Det |
| MODAL | LinModal | Zero | | | | Prog Det |
| SIMM_KA | LinStatic | Zero | | | | Prog Det |
| SIMM_K0 | LinStatic | Zero | | | | Prog Det |
| A--SIMM_KA | LinStatic | Zero | | | | Prog Det |
| A--SIMM_K0 | LinStatic | Zero | | | | Prog Det |
| A-- SIMM_SOVR_K A | LinStatic | Zero | | | | Prog Det |
| A-- SIMM_SOVR_K 0 | LinStatic | Zero | | | | Prog Det |
| SIMM_SOVR_K 0 | LinStatic | Zero | | | | Prog Det |
| SIMM_SOVR_K A | LinStatic | Zero | | | | Prog Det |
| SOVR | LinStatic | Zero | | | | Prog Det |
| TERR_SIMM | LinStatic | Zero | | | | Prog Det |
| TERR_A--SIMM | LinStatic | Zero | | | | Prog Det |
| INERZIA H SLV | LinStatic | Zero | | | | Prog Det |
| INERZIA V + SLV | LinStatic | Zero | | | | Prog Det |
| INERZIA V - SLV | LinStatic | Zero | | | | Prog Det |
| SISMA WOOD SLV | LinStatic | Zero | | | | Prog Det |
| iDROSTATICA | LinStatic | Zero | | | | Prog Det |

PROGETTAZIONE ATI:

Table: Load Case Definitions, Part 1 of 2

| Case | Type | InitialCond | ModalCase | BaseCase | MassSource | DesActOpt |
|---------------------|-----------|-------------|-----------|----------|------------|-----------|
| SISMA WOOD SLD | LinStatic | Zero | | | | Prog Det |
| INERZIA H SLD | LinStatic | Zero | | | | Prog Det |
| INERZIA V + SLD | LinStatic | Zero | | | | Prog Det |
| INERZIA V SLD | LinStatic | Zero | | | | Prog Det |
| INERZIA V -1 | LinStatic | Zero | | | | Prog Det |
| SLU_1 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLU_2 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLU_3 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLU_4 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLE_F1 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLE_F2 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLE_F3 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLE_F4 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLE_QP1 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLE_QP2 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLE_QP3 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLE_QP4 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLV_1 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLV_2 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLV_3 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLV_4 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLD_1 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLD_2 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLD_3 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLD_4 | NonStatic | Zero | | | MSSSRC1 | Prog Det |
| SLU_IDR_1 | NonStatic | Zero | | | | Prog Det |
| SLU_IDR_2 | NonStatic | Zero | | | | Prog Det |
| SISMA WOOD SLV-1 | NonStatic | Zero | | | | Prog Det |
| DEAD-1 | NonStatic | Zero | | | MSSSRC1 | Prog Det |

Table: Load Case Definitions, Part 2 of 2

Table: Load Case Definitions,
Part 2 of 2

| Case | DesignAct |
|---------------------|----------------------|
| DEAD | Non-Composite |
| MODAL | Other |
| SIMM_KA | Short-Term Composite |
| SIMM_K0 | Short-Term Composite |
| A--SIMM_KA | Short-Term Composite |
| A--SIMM_K0 | Short-Term Composite |
| A--SIMM_SOVR_K A | Short-Term Composite |
| A--SIMM_SOVR_K 0 | Short-Term Composite |

PROGETTAZIONE ATI:

**Table: Load Case Definitions,
Part 2 of 2**

| Case | DesignAct |
|--------------------|-------------------------|
| SIMM_SOVR_K 0 | Short-Term Composite |
| SIMM_SOVR_K A | Short-Term Composite |
| SOVR | Short-Term Composite |
| TERR_SIMM | Short-Term Composite |
| TERR_A--SIMM | Short-Term Composite |
| INERZIA H SLV | Short-Term Composite |
| INERZIA V + SLV | Short-Term Composite |
| INERZIA V - SLV | Short-Term Composite |
| SISMA WOOD SLV | Short-Term Composite |
| IDROSTATICA | Short-Term Composite |
| SISMA WOOD SLD | Short-Term Composite |
| INERZIA H SLD | Short-Term Composite |
| INERZIA V + SLD | Short-Term Composite |
| INERZIA V SLD | Short-Term Composite |
| INERZIA V -1 | Short-Term Composite |
| SLU_1 | Non- Composite |
| SLU_2 | Non- Composite |
| SLU_3 | Non- Composite |
| SLU_4 | Non- Composite |
| SLE_F1 | Non- Composite |
| SLE_F2 | Non- Composite |
| SLE_F3 | Non- Composite |
| SLE_F4 | Non- Composite |
| SLE_QP1 | Non- Composite |
| SLE_QP2 | Non- Composite |
| SLE_QP3 | Non- Composite |
| SLE_QP4 | Non- Composite |
| SLV_1 | Non- Composite |
| SLV_2 | Non- Composite |
| SLV_3 | Non- Composite |

PROGETTAZIONE ATI:

Table: Load Case Definitions, Part 2 of 2

| Case | DesignAct |
|------------------|----------------------|
| SLV_4 | Non-Composite |
| SLD_1 | Non-Composite |
| SLD_2 | Non-Composite |
| SLD_3 | Non-Composite |
| SLD_4 | Non-Composite |
| SLU_IDR_1 | Non-Composite |
| SLU_IDR_2 | Non-Composite |
| SISMA WOOD SLV-1 | Short-Term Composite |
| DEAD-1 | Non-Composite |

Table: Frame Section Properties 01 - General, Part 1 of 4

Table: Frame Section Properties 01 - General, Part 1 of 4

| SectionName | Material | Shape | t3 m | t2 m | Area m2 | TorsConst m4 | I33 m4 | I22 m4 |
|-------------|----------|-------------|---------|---------|------------|-----------------|-----------|-----------|
| 100x100 | C28/35 | Rectangular | 1. | 1. | 1. | 0.140833 | 0.083333 | 0.083333 |
| 100x120 | C28/35 | Rectangular | 1.2 | 1. | 1.2 | 0.198439 | 0.144 | 0.1 |
| 100x150 | C28/35 | Rectangular | 1.5 | 1. | 1.5 | 0.293457 | 0.28125 | 0.125 |

Table: Frame Section Properties 01 - General, Part 2 of 4

Table: Frame Section Properties 01 - General, Part 2 of 4

| SectionName | I23 m4 | AS2 m2 | AS3 m2 |
|-------------|-----------|-----------|-----------|
| 100x100 | 0. | 0.833333 | 0.833333 |
| 100x120 | 0. | 1. | 1. |
| 100x150 | 0. | 1.25 | 1.25 |

Table: Frame Section Properties 01 - General, Part 3 of 4

Table: Frame Section Properties 01 - General, Part 3 of 4

| SectionName | S33 m3 | S22 m3 | Z33 m3 | Z22 m3 | R33 m | R22 m |
|-------------|-----------|-----------|-----------|-----------|----------|----------|
| 100x100 | 0.166667 | 0.166667 | 0.25 | 0.25 | 0.288675 | 0.288675 |
| 100x120 | 0.24 | 0.2 | 0.36 | 0.3 | 0.34641 | 0.288675 |
| 100x150 | 0.375 | 0.25 | 0.5625 | 0.375 | 0.433013 | 0.288675 |

Table: Frame Section Properties 01 - General, Part 4 of 4

Table: Frame Section Properties 01 - General, Part 4 of 4

| SectionName | AMod | A2Mod | A3Mod | JMod | I2Mod | I3Mod | MMod | WMod |
|-------------|------|-------|-------|------|-------|-------|------|------|
| 100x100 | 1. | 1. | 1. | 1. | 1. | 1. | 1. | 1. |

PROGETTAZIONE ATI:

Table: Frame Section Properties 01 - General, Part 4 of 4

| SectionName | AMod | A2Mod | A3Mod | JMod | I2Mod | I3Mod | MMod | WMod |
|-------------|------|-------|-------|------|-------|-------|------|------|
| 100x120 | 1. | 1. | 1. | 1. | 1. | 1. | 1. | 1. |
| 100x150 | 1. | 1. | 1. | 1. | 1. | 1. | 1. | 1. |

Table: Frame Section Properties 02 - Concrete Column, Part 1 of 2

Table: Frame Section Properties 02 - Concrete Column, Part 1 of 2

| SectionName | RebarMatL | RebarMatC | ReinfConfig | LatReinf | Cover | NumBars3D ir | NumBars2D ir |
|-------------|-----------|-----------|-------------|----------|-------|-----------------|-----------------|
| 100x100 | B450C | B450C | Rectangular | Ties | 0.04 | 3 | 3 |
| 100x120 | B450C | B450C | Rectangular | Ties | 0.04 | 3 | 3 |
| 100x150 | B450C | B450C | Rectangular | Ties | 0.04 | 3 | 3 |

Table: Frame Section Properties 02 - Concrete Column, Part 2 of 2

Table: Frame Section Properties 02 - Concrete Column, Part 2 of 2

| SectionName | BarSizeL | BarSizeC | SpacingC m | NumCBars2 | NumCBars3 |
|-------------|----------|----------|---------------|-----------|-----------|
| 100x100 | #9 | #4 | 0.15 | 3 | 3 |
| 100x120 | #9 | #4 | 0.15 | 3 | 3 |
| 100x150 | #9 | #4 | 0.15 | 3 | 3 |

Table: Frame Section Assignments

Table: Frame Section Assignments

| Frame | AnalSect | DesignSect | MatProp |
|-------|----------|------------|---------|
| 1 | 100x120 | 100x120 | Default |
| 2 | 100x120 | 100x120 | Default |
| 3 | 100x120 | 100x120 | Default |
| 4 | 100x120 | 100x120 | Default |
| 6 | 100x150 | 100x150 | Default |
| 7 | 100x150 | 100x150 | Default |
| 8 | 100x150 | 100x150 | Default |
| 9 | 100x120 | 100x120 | Default |
| 10 | 100x100 | 100x100 | Default |
| 11 | 100x100 | 100x100 | Default |
| 12 | 100x100 | 100x100 | Default |
| 13 | 100x100 | 100x100 | Default |
| 14 | 100x120 | 100x120 | Default |
| 16 | 100x120 | 100x120 | Default |
| 17 | 100x120 | 100x120 | Default |
| 19 | 100x150 | 100x150 | Default |
| 20 | 100x150 | 100x150 | Default |
| 21 | 100x150 | 100x150 | Default |
| 22 | 100x120 | 100x120 | Default |
| 23 | 100x100 | 100x100 | Default |
| 24 | 100x100 | 100x100 | Default |
| 25 | 100x100 | 100x100 | Default |
| 26 | 100x100 | 100x100 | Default |
| 27 | 100x120 | 100x120 | Default |
| 28 | 100x120 | 100x120 | Default |
| 29 | 100x120 | 100x120 | Default |

PROGETTAZIONE ATI:

Table: Frame Section Assignments

| Frame | AnalSect | DesignSect | MatProp |
|-------|----------|------------|---------|
| 30 | 100x120 | 100x120 | Default |
| 31 | 100x120 | 100x120 | Default |
| 34 | 100x120 | 100x120 | Default |
| 35 | 100x120 | 100x120 | Default |
| 38 | 100x150 | 100x150 | Default |
| 39 | 100x150 | 100x150 | Default |
| 41 | 100x150 | 100x150 | Default |
| 42 | 100x150 | 100x150 | Default |
| 43 | 100x150 | 100x150 | Default |
| 44 | 100x150 | 100x150 | Default |
| 45 | 100x150 | 100x150 | Default |
| 46 | 100x150 | 100x150 | Default |
| 47 | 100x150 | 100x150 | Default |
| 48 | 100x150 | 100x150 | Default |
| 49 | 100x150 | 100x150 | Default |
| 50 | 100x150 | 100x150 | Default |

Table: Frame Loads - Distributed, Part 1 of 3

Table: Frame Loads - Distributed, Part 1 of 3

| Frame | LoadPat | CoordSys | Type | Dir | DistType | RelDistA |
|-------|-----------------|----------|-------|---------|----------|----------|
| 2 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 2 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 2 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 3 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 3 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 3 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 6 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 6 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 6 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 6 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 6 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 6 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 6 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 7 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 7 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 7 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 7 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 7 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 7 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 7 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 8 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 8 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 8 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 8 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 8 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 8 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 8 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 8 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 8 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 8 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 8 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 8 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 1 of 3

| Frame | LoadPat | CoordSys | Type | Dir | DistType | RelDistA |
|-------|-----------------|----------|-------|---------|----------|----------|
| 8 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 8 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 9 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 9 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 9 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 9 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 9 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 9 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 9 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 9 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 9 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 9 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 9 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 9 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 9 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 9 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 10 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 10 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 10 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 10 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 10 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 10 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 10 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 10 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 10 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 10 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 10 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 10 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 10 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 10 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 11 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 11 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 11 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 11 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 11 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 11 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 11 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 11 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 11 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 11 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 11 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 11 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 11 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 11 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 12 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 12 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 12 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 12 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 12 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 12 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 12 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 12 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 12 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 12 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 12 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 1 of 3

| Frame | LoadPat | CoordSys | Type | Dir | DistType | RelDistA |
|-------|-----------------|----------|-------|---------|----------|----------|
| 12 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 12 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 12 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 13 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 13 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 13 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 13 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 13 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 13 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 13 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 13 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 13 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 13 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 13 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 13 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 13 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 13 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 14 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 14 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 14 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 16 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 16 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 16 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 17 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 17 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 17 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 19 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 19 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 19 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 19 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 19 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 20 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 20 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 20 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 20 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 20 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 21 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 21 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 21 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 21 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 21 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 21 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 21 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 21 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 21 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 21 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 21 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 21 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 22 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 22 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 22 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 22 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 22 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 22 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 22 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 1 of 3

| Frame | LoadPat | CoordSys | Type | Dir | DistType | RelDistA |
|-------|-----------------|----------|-------|---------|----------|----------|
| 22 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 22 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 22 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 22 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 22 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 23 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 23 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 23 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 23 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 23 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 23 | iDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 23 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 23 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 23 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 23 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 23 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 23 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 24 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 24 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 24 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 24 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 24 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 24 | iDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 24 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 24 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 24 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 24 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 24 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 24 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 25 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 25 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 25 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 25 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 25 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 25 | iDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 25 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 25 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 25 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 25 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 25 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 25 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 26 | SOVR | GLOBAL | Force | Gravity | RelDist | 0. |
| 26 | SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 26 | SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 26 | A--SIMM_SOVR_K0 | GLOBAL | Force | X | RelDist | 0. |
| 26 | A--SIMM_SOVR_KA | GLOBAL | Force | X | RelDist | 0. |
| 26 | iDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 26 | TERR_SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 26 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 26 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 26 | TERR_A--SIMM | GLOBAL | Force | Gravity | RelDist | 0. |
| 26 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 26 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 27 | iDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 28 | iDROSTATICA | Local | Force | 2 | RelDist | 0. |

PROGETTAZIONE ATI:

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Table: Frame Loads - Distributed, Part 1 of 3

| Frame | LoadPat | CoordSys | Type | Dir | DistType | RelDistA |
|-------|----------------|----------|-------|-----|----------|----------|
| 29 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 30 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 31 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 1 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 1 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 1 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 4 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 4 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 4 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 34 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 35 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 38 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 38 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 38 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 38 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 38 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 38 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 38 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 39 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 39 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 39 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 39 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 39 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 39 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 39 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 41 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 41 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 41 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 41 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 41 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 42 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 42 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 42 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 42 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 42 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 43 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 43 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 43 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 44 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 44 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 44 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 45 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 45 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 45 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 45 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 45 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 45 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 45 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |
| 46 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 46 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 46 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 46 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 46 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 46 | SISMA WOOD SLD | GLOBAL | Force | X | RelDist | 0. |
| 46 | SISMA WOOD | GLOBAL | Force | X | RelDist | 0. |

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Table: Frame Loads - Distributed, Part 1 of 3

| Frame | LoadPat | CoordSys | Type | Dir | DistType | RelDistA |
|-------|-------------|----------|-------|-----|----------|----------|
| 47 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 48 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 49 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 49 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 49 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 49 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 49 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 50 | IDROSTATICA | Local | Force | 2 | RelDist | 0. |
| 50 | SIMM_KA | GLOBAL | Force | X | RelDist | 0. |
| 50 | SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 50 | A--SIMM_K0 | GLOBAL | Force | X | RelDist | 0. |
| 50 | A--SIMM_KA | GLOBAL | Force | X | RelDist | 0. |

Table: Frame Loads - Distributed, Part 2 of 3

Table: Frame Loads - Distributed, Part 2 of 3

| Frame | LoadPat | RelDistB | AbsDistA | AbsDistB | FOverLA | FOverLB |
|-------|-----------------|----------|----------|----------|---------|---------|
| | | | m | m | KN/m | KN/m |
| 2 | IDROSTATICA | 1. | 0. | 1.37332 | 123.07 | 123.07 |
| 2 | SISMA WOOD SLD | 1. | 0. | 1.37332 | 30.8 | 30.8 |
| 2 | SISMA WOOD | 1. | 0. | 1.37332 | 69.74 | 69.74 |
| 3 | IDROSTATICA | 1. | 0. | 1.37601 | 123.07 | 123.07 |
| 3 | SISMA WOOD SLD | 1. | 0. | 1.37601 | 30.8 | 30.8 |
| 3 | SISMA WOOD | 1. | 0. | 1.37601 | 69.74 | 69.74 |
| 6 | IDROSTATICA | 1. | 0. | 1. | 106.8 | 86.4 |
| 6 | SIMM_KA | 1. | 0. | 1. | 48.71 | 41.92 |
| 6 | SIMM_K0 | 1. | 0. | 1. | 73.07 | 62.87 |
| 6 | A--SIMM_K0 | 1. | 0. | 1. | 117.59 | 106.21 |
| 6 | A--SIMM_KA | 1. | 0. | 1. | 74.33 | 70.87 |
| 6 | SISMA WOOD SLD | 1. | 0. | 1. | 30.8 | 30.8 |
| 6 | SISMA WOOD | 1. | 0. | 1. | 69.74 | 69.74 |
| 7 | IDROSTATICA | 1. | 0. | 0.5719 | 86.4 | 72.56 |
| 7 | SIMM_KA | 1. | 0. | 0.5719 | 41.92 | 38.52 |
| 7 | SIMM_K0 | 1. | 0. | 0.5719 | 62.87 | 57.78 |
| 7 | A--SIMM_K0 | 1. | 0. | 0.5719 | 106.21 | 99.3 |
| 7 | A--SIMM_KA | 1. | 0. | 0.5719 | 70.87 | 66.2 |
| 7 | SISMA WOOD SLD | 1. | 0. | 0.5719 | 30.8 | 30.8 |
| 7 | SISMA WOOD | 1. | 0. | 0.5719 | 69.74 | 69.74 |
| 8 | SOVR | 1. | 0. | 1.51312 | 20. | 20. |
| 8 | SIMM_SOVR_K0 | 1. | 0. | 1.51312 | 10. | 10. |
| 8 | SIMM_SOVR_KA | 1. | 0. | 1.51312 | 6.67 | 6.67 |
| 8 | A--SIMM_SOVR_K0 | 1. | 0. | 1.51312 | 10. | 10. |
| 8 | A--SIMM_SOVR_KA | 1. | 0. | 1.51312 | 6.67 | 6.67 |
| 8 | IDROSTATICA | 1. | 0. | 1.51312 | -72.56 | -72.56 |
| 8 | TERR_SIMM | 1. | 0. | 1.51312 | 115.55 | 105.36 |
| 8 | SIMM_KA | 1. | 0. | 1.51312 | 38.52 | 35.12 |
| 8 | SIMM_K0 | 1. | 0. | 1.51312 | 57.78 | 52.68 |
| 8 | TERR_A--SIMM | 1. | 0. | 1.51312 | 212.61 | 186.4 |
| 8 | A--SIMM_K0 | 1. | 0. | 1.51312 | 99.3 | 87.1 |
| 8 | A--SIMM_KA | 1. | 0. | 1.51312 | 66.2 | 58.07 |
| 8 | SISMA WOOD SLD | 1. | 0. | 1.51312 | 30.8 | 30.8 |
| 8 | SISMA WOOD | 1. | 0. | 1.51312 | 69.74 | 69.74 |
| 9 | SOVR | 1. | 0. | 1.39435 | 20. | 20. |
| 9 | SIMM_SOVR_K0 | 1. | 0. | 1.39435 | 10. | 10. |

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Table: Frame Loads - Distributed, Part 2 of 3

| Frame | LoadPat | RelDistB | AbsDistA | AbsDistB | FOverLA | FOverLB |
|-------|-----------------|----------|----------|----------|---------|---------|
| | | | m | m | KN/m | KN/m |
| 9 | SIMM_SOVR_KA | 1. | 0. | 1.39435 | 6.67 | 6.67 |
| 9 | A--SIMM_SOVR_K0 | 1. | 0. | 1.39435 | 10. | 10. |
| 9 | A--SIMM_SOVR_KA | 1. | 0. | 1.39435 | 6.67 | 6.67 |
| 9 | IDROSTATICA | 1. | 0. | 1.39435 | -72.56 | -62.76 |
| 9 | TERR_SIMM | 1. | 0. | 1.39435 | 105.36 | 95.16 |
| 9 | SIMM_KA | 1. | 0. | 1.39435 | 35.12 | 30.1 |
| 9 | SIMM_K0 | 1. | 0. | 1.39435 | 52.68 | 47.58 |
| 9 | TERR_A--SIMM | 1. | 0. | 1.39435 | 186.4 | 149.81 |
| 9 | A--SIMM_K0 | 1. | 0. | 1.39435 | 87.1 | 74.9 |
| 9 | A--SIMM_KA | 1. | 0. | 1.39435 | 58.07 | 49.94 |
| 9 | SISMA WOOD SLD | 1. | 0. | 1.39435 | 30.8 | 30.8 |
| 9 | SISMA WOOD | 1. | 0. | 1.39435 | 69.74 | 69.74 |
| 10 | SOVR | 1. | 0. | 2.07949 | 20. | 20. |
| 10 | SIMM_SOVR_K0 | 1. | 0. | 2.07949 | 10. | 10. |
| 10 | SIMM_SOVR_KA | 1. | 0. | 2.07949 | 6.67 | 6.67 |
| 10 | A--SIMM_SOVR_K0 | 1. | 0. | 2.07949 | 10. | 10. |
| 10 | A--SIMM_SOVR_KA | 1. | 0. | 2.07949 | 6.67 | 6.67 |
| 10 | IDROSTATICA | 1. | 0. | 2.07949 | -62.76 | -48. |
| 10 | TERR_SIMM | 1. | 0. | 2.07949 | 95.16 | 79.8 |
| 10 | SIMM_KA | 1. | 0. | 2.07949 | 30.1 | 24.93 |
| 10 | SIMM_K0 | 1. | 0. | 2.07949 | 47.58 | 39.3 |
| 10 | TERR_A--SIMM | 1. | 0. | 2.07949 | 149.81 | 131.5 |
| 10 | A--SIMM_K0 | 1. | 0. | 2.07949 | 74.9 | 65.8 |
| 10 | A--SIMM_KA | 1. | 0. | 2.07949 | 49.94 | 43.8 |
| 10 | SISMA WOOD SLD | 1. | 0. | 2.07949 | 30.8 | 30.8 |
| 10 | SISMA WOOD | 1. | 0. | 2.07949 | 69.74 | 69.74 |
| 11 | SOVR | 1. | 0. | 2.10446 | 20. | 20. |
| 11 | SIMM_SOVR_K0 | 1. | 0. | 2.10446 | 10. | 10. |
| 11 | SIMM_SOVR_KA | 1. | 0. | 2.10446 | 6.67 | 6.67 |
| 11 | A--SIMM_SOVR_K0 | 1. | 0. | 2.10446 | 10. | 10. |
| 11 | A--SIMM_SOVR_KA | 1. | 0. | 2.10446 | 6.67 | 6.67 |
| 11 | IDROSTATICA | 1. | 0. | 2.10446 | -48. | -33.34 |
| 11 | TERR_SIMM | 1. | 0. | 2.10446 | 79.8 | 64.58 |
| 11 | SIMM_KA | 1. | 0. | 2.10446 | 24.93 | 21.53 |
| 11 | SIMM_K0 | 1. | 0. | 2.10446 | 39.3 | 37.39 |
| 11 | TERR_A--SIMM | 1. | 0. | 2.10446 | 131.5 | 101.04 |
| 11 | A--SIMM_K0 | 1. | 0. | 2.10446 | 65.8 | 50.52 |
| 11 | A--SIMM_KA | 1. | 0. | 2.10446 | 43.8 | 33.68 |
| 11 | SISMA WOOD SLD | 1. | 0. | 2.10446 | 30.8 | 30.8 |
| 11 | SISMA WOOD | 1. | 0. | 2.10446 | 69.74 | 69.74 |
| 12 | SOVR | 1. | 0. | 2.09633 | 20. | 20. |
| 12 | SIMM_SOVR_K0 | 1. | 0. | 2.09633 | 10. | 10. |
| 12 | SIMM_SOVR_KA | 1. | 0. | 2.09633 | 6.67 | 6.67 |
| 12 | A--SIMM_SOVR_K0 | 1. | 0. | 2.09633 | 10. | 10. |
| 12 | A--SIMM_SOVR_KA | 1. | 0. | 2.09633 | 6.67 | 6.67 |
| 12 | IDROSTATICA | 1. | 0. | 2.09633 | -33.34 | -23.53 |
| 12 | TERR_SIMM | 1. | 0. | 2.09633 | 64.58 | 59.49 |
| 12 | SIMM_KA | 1. | 0. | 2.09633 | 21.53 | 19.93 |
| 12 | SIMM_K0 | 1. | 0. | 2.09633 | 37.39 | 32.29 |
| 12 | TERR_A--SIMM | 1. | 0. | 2.09633 | 101.04 | 85. |
| 12 | A--SIMM_K0 | 1. | 0. | 2.09633 | 50.52 | 42.5 |
| 12 | A--SIMM_KA | 1. | 0. | 2.09633 | 33.68 | 28.33 |
| 12 | SISMA WOOD SLD | 1. | 0. | 2.09633 | 30.8 | 30.8 |
| 12 | SISMA WOOD | 1. | 0. | 2.09633 | 69.74 | 69.74 |
| 13 | SOVR | 1. | 0. | 2.09228 | 20. | 20. |

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Table: Frame Loads - Distributed, Part 2 of 3

| Frame | LoadPat | RelDistB | AbsDistA | AbsDistB | FOverLA | FOverLB |
|-------|-----------------|----------|----------|----------|---------|---------|
| | | | m | m | KN/m | KN/m |
| 13 | SIMM_SOVR_K0 | 1. | 0. | 2.09228 | 10. | 10. |
| 13 | SIMM_SOVR_KA | 1. | 0. | 2.09228 | 6.67 | 6.67 |
| 13 | A--SIMM_SOVR_K0 | 1. | 0. | 2.09228 | 10. | 10. |
| 13 | A--SIMM_SOVR_KA | 1. | 0. | 2.09228 | 6.67 | 6.67 |
| 13 | IDROSTATICA | 1. | 0. | 2.09228 | -23.53 | -18.63 |
| 13 | TERR_SIMM | 1. | 0. | 2.09228 | 59.49 | 59.49 |
| 13 | SIMM_KA | 1. | 0. | 2.09228 | 19.93 | 19.93 |
| 13 | SIMM_K0 | 1. | 0. | 2.09228 | 32.29 | 29.74 |
| 13 | TERR_A--SIMM | 1. | 0. | 2.09228 | 85. | 73.47 |
| 13 | A--SIMM_K0 | 1. | 0. | 2.09228 | 42.5 | 36.73 |
| 13 | A--SIMM_KA | 1. | 0. | 2.09228 | 28.33 | 24.49 |
| 13 | SISMA WOOD SLD | 1. | 0. | 2.09228 | 30.8 | 30.8 |
| 13 | SISMA WOOD | 1. | 0. | 2.09228 | 69.74 | 69.74 |
| 14 | IDROSTATICA | 1. | 0. | 1.88301 | 123.07 | 123.07 |
| 14 | SISMA WOOD SLD | 1. | 0. | 1.88301 | 30.8 | 30.8 |
| 14 | SISMA WOOD | 1. | 0. | 1.88301 | 69.74 | 69.74 |
| 16 | IDROSTATICA | 1. | 0. | 0.7849 | 131.4 | 131.4 |
| 16 | SISMA WOOD SLD | 1. | 0. | 0.7849 | 30.8 | 30.8 |
| 16 | SISMA WOOD | 1. | 0. | 0.7849 | 69.74 | 69.74 |
| 17 | IDROSTATICA | 1. | 0. | 1.255 | 123.07 | 131.4 |
| 17 | SISMA WOOD SLD | 1. | 0. | 1.255 | 30.8 | 30.8 |
| 17 | SISMA WOOD | 1. | 0. | 1.255 | 69.74 | 69.74 |
| 19 | IDROSTATICA | 1. | 0. | 1. | -106.8 | -86.4 |
| 19 | SIMM_KA | 1. | 0. | 1. | -48.71 | -41.92 |
| 19 | SIMM_K0 | 1. | 0. | 1. | -73.07 | -62.87 |
| 19 | A--SIMM_K0 | 1. | 0. | 1. | -67.07 | -54.87 |
| 19 | A--SIMM_KA | 1. | 0. | 1. | -36.58 | -32.52 |
| 20 | IDROSTATICA | 1. | 0. | 0.5719 | -86.4 | -72.56 |
| 20 | SIMM_KA | 1. | 0. | 0.5719 | -41.92 | -38.52 |
| 20 | SIMM_K0 | 1. | 0. | 0.5719 | -62.87 | -57.78 |
| 20 | A--SIMM_K0 | 1. | 0. | 0.5719 | -54.87 | -48.78 |
| 20 | A--SIMM_KA | 1. | 0. | 0.5719 | -32.52 | -28.45 |
| 21 | SOVR | 1. | 0. | 1.63815 | 20. | 20. |
| 21 | SIMM_SOVR_K0 | 1. | 0. | 1.63815 | -10. | -10. |
| 21 | SIMM_SOVR_KA | 1. | 0. | 1.63815 | -6.67 | -6.67 |
| 21 | A--SIMM_SOVR_K0 | 1. | 0. | 1.63815 | -10. | -10. |
| 21 | A--SIMM_SOVR_KA | 1. | 0. | 1.63815 | -6.67 | -6.67 |
| 21 | IDROSTATICA | 1. | 0. | 1.63815 | -72.56 | -72.56 |
| 21 | TERR_SIMM | 1. | 0. | 1.63815 | 115.55 | 105.36 |
| 21 | SIMM_KA | 1. | 0. | 1.63815 | -38.52 | -35.12 |
| 21 | SIMM_K0 | 1. | 0. | 1.63815 | -57.78 | -52.68 |
| 21 | TERR_A--SIMM | 1. | 0. | 1.63815 | 97.55 | 85.36 |
| 21 | A--SIMM_K0 | 1. | 0. | 1.63815 | -48.78 | -42.68 |
| 21 | A--SIMM_KA | 1. | 0. | 1.63815 | -32.52 | -28.45 |
| 22 | SOVR | 1. | 0. | 1.26794 | 20. | 20. |
| 22 | SIMM_SOVR_K0 | 1. | 0. | 1.26794 | -10. | -10. |
| 22 | SIMM_SOVR_KA | 1. | 0. | 1.26794 | -6.67 | -6.67 |
| 22 | A--SIMM_SOVR_K0 | 1. | 0. | 1.26794 | -10. | -10. |
| 22 | A--SIMM_SOVR_KA | 1. | 0. | 1.26794 | -6.67 | -6.67 |
| 22 | IDROSTATICA | 1. | 0. | 1.26794 | -82.37 | -72.56 |
| 22 | TERR_SIMM | 1. | 0. | 1.26794 | 105.36 | 95.16 |
| 22 | SIMM_KA | 1. | 0. | 1.26794 | -35.12 | -30.1 |
| 22 | SIMM_K0 | 1. | 0. | 1.26794 | -52.68 | -47.58 |
| 22 | TERR_A--SIMM | 1. | 0. | 1.26794 | 85.36 | 73.47 |
| 22 | A--SIMM_K0 | 1. | 0. | 1.26794 | -42.68 | -36.73 |

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Table: Frame Loads - Distributed, Part 2 of 3

| Frame | LoadPat | RelDistB | AbsDistA | AbsDistB | FOverLA | FOverLB |
|-------|-----------------|----------|----------|----------|---------|---------|
| | | | m | m | KN/m | KN/m |
| 22 | A--SIMM_KA | 1. | 0. | 1.26794 | -28.45 | -24.49 |
| 23 | SOVR | 1. | 0. | 2.09321 | 20. | 20. |
| 23 | SIMM_SOVR_K0 | 1. | 0. | 2.09321 | -10. | -10. |
| 23 | SIMM_SOVR_KA | 1. | 0. | 2.09321 | -6.67 | -6.67 |
| 23 | A--SIMM_SOVR_K0 | 1. | 0. | 2.09321 | -10. | -10. |
| 23 | A--SIMM_SOVR_KA | 1. | 0. | 2.09321 | -6.67 | -6.67 |
| 23 | IDROSTATICA | 1. | 0. | 2.09321 | -62.76 | -48. |
| 23 | TERR_SIMM | 1. | 0. | 2.09321 | 95.16 | 79.8 |
| 23 | SIMM_KA | 1. | 0. | 2.09321 | -30.1 | -24.93 |
| 23 | SIMM_K0 | 1. | 0. | 2.09321 | -47.58 | -39.3 |
| 23 | TERR_A--SIMM | 1. | 0. | 2.09321 | 73.47 | 73.47 |
| 23 | A--SIMM_K0 | 1. | 0. | 2.09321 | -36.73 | -36.73 |
| 23 | A--SIMM_KA | 1. | 0. | 2.09321 | -24.49 | -24.49 |
| 24 | SOVR | 1. | 0. | 2.09341 | 20. | 20. |
| 24 | SIMM_SOVR_K0 | 1. | 0. | 2.09341 | -10. | -10. |
| 24 | SIMM_SOVR_KA | 1. | 0. | 2.09341 | -6.67 | -6.67 |
| 24 | A--SIMM_SOVR_K0 | 1. | 0. | 2.09341 | -10. | -10. |
| 24 | A--SIMM_SOVR_KA | 1. | 0. | 2.09341 | -6.67 | -6.67 |
| 24 | IDROSTATICA | 1. | 0. | 2.09341 | -48. | -33.34 |
| 24 | TERR_SIMM | 1. | 0. | 2.09341 | 79.8 | 64.58 |
| 24 | SIMM_KA | 1. | 0. | 2.09341 | -24.93 | -21.53 |
| 24 | SIMM_K0 | 1. | 0. | 2.09341 | -39.3 | -37.39 |
| 24 | TERR_A--SIMM | 1. | 0. | 2.09341 | 73.47 | 73.47 |
| 24 | A--SIMM_K0 | 1. | 0. | 2.09341 | -36.73 | -36.73 |
| 24 | A--SIMM_KA | 1. | 0. | 2.09341 | -24.49 | -24.49 |
| 25 | SOVR | 1. | 0. | 2.09331 | 20. | 20. |
| 25 | SIMM_SOVR_K0 | 1. | 0. | 2.09331 | -10. | -10. |
| 25 | SIMM_SOVR_KA | 1. | 0. | 2.09331 | -6.67 | -6.67 |
| 25 | A--SIMM_SOVR_K0 | 1. | 0. | 2.09331 | -10. | -10. |
| 25 | A--SIMM_SOVR_KA | 1. | 0. | 2.09331 | -6.67 | -6.67 |
| 25 | IDROSTATICA | 1. | 0. | 2.09331 | -33.34 | -23.53 |
| 25 | TERR_SIMM | 1. | 0. | 2.09331 | 64.58 | 59.49 |
| 25 | SIMM_KA | 1. | 0. | 2.09331 | -21.53 | -19.93 |
| 25 | SIMM_K0 | 1. | 0. | 2.09331 | -37.39 | -32.29 |
| 25 | TERR_A--SIMM | 1. | 0. | 2.09331 | 73.47 | 73.47 |
| 25 | A--SIMM_K0 | 1. | 0. | 2.09331 | -36.73 | -36.73 |
| 25 | A--SIMM_KA | 1. | 0. | 2.09331 | -24.49 | -24.49 |
| 26 | SOVR | 1. | 0. | 2.09332 | 20. | 20. |
| 26 | SIMM_SOVR_K0 | 1. | 0. | 2.09332 | -10. | -10. |
| 26 | SIMM_SOVR_KA | 1. | 0. | 2.09332 | -6.67 | -6.67 |
| 26 | A--SIMM_SOVR_K0 | 1. | 0. | 2.09332 | -10. | -10. |
| 26 | A--SIMM_SOVR_KA | 1. | 0. | 2.09332 | -6.67 | -6.67 |
| 26 | IDROSTATICA | 1. | 0. | 2.09332 | -23.53 | -18.63 |
| 26 | TERR_SIMM | 1. | 0. | 2.09332 | 59.49 | 59.49 |
| 26 | SIMM_KA | 1. | 0. | 2.09332 | -19.93 | -19.93 |
| 26 | SIMM_K0 | 1. | 0. | 2.09332 | -32.29 | -29.74 |
| 26 | TERR_A--SIMM | 1. | 0. | 2.09332 | 73.47 | 73.47 |
| 26 | A--SIMM_K0 | 1. | 0. | 2.09332 | -36.73 | -36.73 |
| 26 | A--SIMM_KA | 1. | 0. | 2.09332 | -24.49 | -24.49 |
| 27 | IDROSTATICA | 1. | 0. | 0.8977 | 131.4 | 131.4 |
| 28 | IDROSTATICA | 1. | 0. | 1.255 | 131.4 | 123.07 |
| 29 | IDROSTATICA | 1. | 0. | 1.37332 | 123.07 | 123.07 |
| 30 | IDROSTATICA | 1. | 0. | 1.37601 | 123.07 | 123.07 |
| 31 | IDROSTATICA | 1. | 0. | 1.88306 | 123.07 | 123.07 |
| 1 | IDROSTATICA | 1. | 0. | 0.60768 | 123.07 | 123.07 |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 2 of 3

| Frame | LoadPat | RelDistB | AbsDistA | AbsDistB | FOverLA | FOverLB |
|-------|----------------|----------|----------|----------|---------|---------|
| | | | m | m | KN/m | KN/m |
| 1 | SISMA WOOD SLD | 1. | 0. | 0.60768 | 30.8 | 30.8 |
| 1 | SISMA WOOD | 1. | 0. | 0.60768 | 69.74 | 69.74 |
| 4 | IDROSTATICA | 1. | 0. | 0.62502 | 123.07 | 123.07 |
| 4 | SISMA WOOD SLD | 1. | 0. | 0.62502 | 30.8 | 30.8 |
| 4 | SISMA WOOD | 1. | 0. | 0.62502 | 69.74 | 69.74 |
| 34 | IDROSTATICA | 1. | 0. | 0.57337 | 123.07 | 123.07 |
| 35 | IDROSTATICA | 1. | 0. | 0.59172 | 123.07 | 123.07 |
| 38 | IDROSTATICA | 1. | 0. | 0.5272 | 117.65 | 112.22 |
| 38 | SIMM_KA | 1. | 0. | 0.5272 | 56.02 | 52.11 |
| 38 | SIMM_K0 | 1. | 0. | 0.5272 | 84.03 | 78.16 |
| 38 | A--SIMM_K0 | 1. | 0. | 0.5272 | 129.78 | 123.68 |
| 38 | A--SIMM_KA | 1. | 0. | 0.5272 | 86.52 | 82.64 |
| 38 | SISMA WOOD SLD | 1. | 0. | 0.5272 | 30.8 | 30.8 |
| 38 | SISMA WOOD | 1. | 0. | 0.5272 | 69.74 | 69.74 |
| 39 | IDROSTATICA | 1. | 0. | 0.5272 | 112.22 | 106.8 |
| 39 | SIMM_KA | 1. | 0. | 0.5272 | 52.11 | 48.71 |
| 39 | SIMM_K0 | 1. | 0. | 0.5272 | 78.16 | 73.07 |
| 39 | A--SIMM_K0 | 1. | 0. | 0.5272 | 123.68 | 117.59 |
| 39 | A--SIMM_KA | 1. | 0. | 0.5272 | 82.64 | 74.33 |
| 39 | SISMA WOOD SLD | 1. | 0. | 0.5272 | 30.8 | 30.8 |
| 39 | SISMA WOOD | 1. | 0. | 0.5272 | 69.74 | 69.74 |
| 41 | IDROSTATICA | 1. | 0. | 0.5272 | -117.65 | -112.22 |
| 41 | SIMM_KA | 1. | 0. | 0.5272 | -56.02 | -52.11 |
| 41 | SIMM_K0 | 1. | 0. | 0.5272 | -84.03 | -78.16 |
| 41 | A--SIMM_K0 | 1. | 0. | 0.5272 | -79.26 | -73.76 |
| 41 | A--SIMM_KA | 1. | 0. | 0.5272 | -52.84 | -44.71 |
| 42 | IDROSTATICA | 1. | 0. | 0.5272 | -112.22 | -106.8 |
| 42 | SIMM_KA | 1. | 0. | 0.5272 | -52.11 | -48.71 |
| 42 | SIMM_K0 | 1. | 0. | 0.5272 | -78.16 | -73.07 |
| 42 | A--SIMM_K0 | 1. | 0. | 0.5272 | -73.76 | -67.07 |
| 42 | A--SIMM_KA | 1. | 0. | 0.5272 | -44.71 | -36.58 |
| 43 | IDROSTATICA | 1. | 0. | 0.27891 | 123.07 | 123.07 |
| 43 | SISMA WOOD SLD | 1. | 0. | 0.27891 | 30.8 | 30.8 |
| 43 | SISMA WOOD | 1. | 0. | 0.27891 | 69.74 | 69.74 |
| 44 | IDROSTATICA | 1. | 0. | 0.27891 | 123.07 | 123.07 |
| 44 | SISMA WOOD SLD | 1. | 0. | 0.27891 | 30.8 | 30.8 |
| 44 | SISMA WOOD | 1. | 0. | 0.27891 | 69.74 | 69.74 |
| 45 | IDROSTATICA | 1. | 0. | 0.2638 | 123.07 | 120.36 |
| 45 | SIMM_KA | 1. | 0. | 0.2638 | 56.02 | 56.02 |
| 45 | SIMM_K0 | 1. | 0. | 0.2638 | 84.03 | 84.03 |
| 45 | A--SIMM_K0 | 1. | 0. | 0.2638 | 129.78 | 129.78 |
| 45 | A--SIMM_KA | 1. | 0. | 0.2638 | 86.52 | 86.52 |
| 45 | SISMA WOOD SLD | 1. | 0. | 0.2638 | 30.8 | 30.8 |
| 45 | SISMA WOOD | 1. | 0. | 0.2638 | 69.74 | 69.74 |
| 46 | IDROSTATICA | 1. | 0. | 0.2636 | 120.36 | 117.65 |
| 46 | SIMM_KA | 1. | 0. | 0.2636 | 56.02 | 56.02 |
| 46 | SIMM_K0 | 1. | 0. | 0.2636 | 84.03 | 84.03 |
| 46 | A--SIMM_K0 | 1. | 0. | 0.2636 | 129.78 | 129.78 |
| 46 | A--SIMM_KA | 1. | 0. | 0.2636 | 86.52 | 86.52 |
| 46 | SISMA WOOD SLD | 1. | 0. | 0.2636 | 30.8 | 30.8 |
| 46 | SISMA WOOD | 1. | 0. | 0.2636 | 69.74 | 69.74 |
| 47 | IDROSTATICA | 1. | 0. | 0.26012 | 123.07 | 123.07 |
| 48 | IDROSTATICA | 1. | 0. | 0.26012 | 123.07 | 123.07 |
| 49 | IDROSTATICA | 1. | 0. | 0.2638 | -123.07 | -120.36 |
| 49 | SIMM_KA | 1. | 0. | 0.2638 | -56.02 | -56.02 |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 2 of 3

| Frame | LoadPat | RelDistB | AbsDistA | AbsDistB | FOverLA | FOverLB |
|-------|-------------|----------|----------|----------|---------|---------|
| | | | m | m | KN/m | KN/m |
| 49 | SIMM_K0 | 1. | 0. | 0.2638 | -84.03 | -84.03 |
| 49 | A--SIMM_K0 | 1. | 0. | 0.2638 | -79.26 | -79.26 |
| 49 | A--SIMM_KA | 1. | 0. | 0.2638 | -52.84 | -52.84 |
| 50 | IDROSTATICA | 1. | 0. | 0.2636 | -120.36 | -117.65 |
| 50 | SIMM_KA | 1. | 0. | 0.2636 | -56.02 | -56.02 |
| 50 | SIMM_K0 | 1. | 0. | 0.2636 | -84.03 | -84.03 |
| 50 | A--SIMM_K0 | 1. | 0. | 0.2636 | -79.26 | -79.26 |
| 50 | A--SIMM_KA | 1. | 0. | 0.2636 | -52.84 | -52.84 |

Table: Frame Loads - Distributed, Part 3 of 3

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|----------------|--------------------------------------|
| 2 | IDROSTATICA | 9c4d5735-76fc-4f3c-91a2-cf80bf206554 |
| 2 | SISMA WOOD SLD | 8d4d7f8c-753c-4052-af25-982463858e39 |
| 2 | SISMA WOOD | e8f39e97-e4a9-4c0f-819d-64dfe9f38857 |
| 3 | IDROSTATICA | dd106d7d-1328-4fe2-81b3-fa8efc095f10 |
| 3 | SISMA WOOD SLD | b755392b-7b12-4277-9ede-d2570d94b478 |
| 3 | SISMA WOOD | cfb93047-9b85-418f-a529-96069f7806e8 |
| 6 | IDROSTATICA | 1b9dfdc8-70e6-4272-9ea8-465315b470cf |
| 6 | SIMM_KA | dfcb88c5-8dc4-4794-a5fe-519694535ab6 |
| 6 | SIMM_K0 | 77cff551-b411-47f9-a7cd-e99790608866 |
| 6 | A--SIMM_K0 | e8375111-39d4-4462-bb88-80d2a34480a3 |
| 6 | A--SIMM_KA | 60b0dff3-35e3-4885-959d-2c0f0ea651ee |
| 6 | SISMA WOOD SLD | 64d784c4-902f-491d-85e5-2683c70d2b57 |
| 6 | SISMA WOOD | 80eb730b-1656-4505-927b-a14c4ccc13f1 |
| 7 | IDROSTATICA | 90d01087-10bb-407d-9f30-ff330629a39d |
| 7 | SIMM_KA | 013742cd-5ca7-498d-9b11-ba550d9a5b09 |
| 7 | SIMM_K0 | 61683c60-9a3d-4094-aa26-2e171587d301 |
| 7 | A--SIMM_K0 | 58eb8b09-cdca-4ce5-8775-574eaab2ad30 |
| 7 | A--SIMM_KA | ce8150c2-95ca-4c13-9024-a4a3f0242c0c |
| 7 | SISMA WOOD SLD | 2f0488d1-2711-414a-9dde-b2289e6dc250 |
| 7 | SISMA WOOD | ae0640cf-4f5a-4597-960e-f3fca39ba3e1 |
| 8 | SOVR | 7176155f-98ce-4fe6-8cef-2e9ba9f64ea2 |
| 8 | SIMM_SOVR_K0 | ee63ba91-9c68-4955-8b81-8e6eec6870be |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|-----------------|--------------------------------------|
| 8 | SIMM_SOVR_KA | ec9e155a-0237-482d-a7e1-a6cef1eedc4e |
| 8 | A--SIMM_SOVR_K0 | 657e2d6c-1f25-4e3f-b92f-b7a5b13dd7da |
| 8 | A--SIMM_SOVR_KA | 18656561-8a79-49ab-888c-791e26b19b84 |
| 8 | iDROSTATICA | 73a2efb0-0df9-4049-8bda-cf8c1818e92e |
| 8 | TERR_SIMM | 4cca39f0-837a-46a4-9020-777c4786c84e |
| 8 | SIMM_KA | 1ba94efd-d2dd-4be4-b568-28132abc5f4f |
| 8 | SIMM_K0 | 7e85b45a-ac78-4578-98a5-7096180ed8ee |
| 8 | TERR_A--SIMM | 607f7ab6-0bf8-48b2-aada-00753546c02d |
| 8 | A--SIMM_K0 | 56ea4440-2b53-42cd-8e99-5eff881a2cc2 |
| 8 | A--SIMM_KA | de0e9077-c5da-443e-baeb-ca1ff88ac5bd |
| 8 | SISMA WOOD SLD | 7e48c487-caaf-4e08-ac38-ed52846501cb |
| 8 | SISMA WOOD | f05eed7a-577a-4319-a515-283caac52cd1 |
| 9 | SOVR | 020c1490-68dc-42af-bdd5-9d20ce290fdd |
| 9 | SIMM_SOVR_K0 | 5595e3e8-4a2e-44f8-ab20-299c8e5bd507 |
| 9 | SIMM_SOVR_KA | b741b791-fde6-4eec-9519-210c5d28f7f1 |
| 9 | A--SIMM_SOVR_K0 | 960cd95e-c4de-4f92-8742-e886a68ecc88 |
| 9 | A--SIMM_SOVR_KA | 6a057cf2-9ae8-4fbd-b8b6-8808013caaa8 |
| 9 | iDROSTATICA | 14066c28-70e2-4208-bcc3-20bcc6aaa3c8 |
| 9 | TERR_SIMM | 79c04ae4-dc14-4b90-9112-7f55f0701286 |
| 9 | SIMM_KA | 0aeeb093-20a3-4292-a509-5d90c9b92c30 |
| 9 | SIMM_K0 | 360987a1-9e51-469d-9e5a-8867a702376b |
| 9 | TERR_A--SIMM | 1136b33b-5645-4183-8f71-8c423ee4784d |
| 9 | A--SIMM_K0 | 821d02ba-d4c3-47c1-a284-e719053fc439 |
| 9 | A--SIMM_KA | 161cbaa9-1845-49ad-a27f-9428b64c0bcf |
| 9 | SISMA WOOD SLD | b11f0ccd-c869-4da5-81c4-be6d14c1cad2 |
| 9 | SISMA WOOD | 99fe16f4-b573-4eb9-8521-aaaa3c07cb6d |
| 10 | SOVR | 88b903b0-bb3b-4980-aa42-9b536801e12e |
| 10 | SIMM_SOVR_K0 | 0debbb28-e922-476e-995e-a974f3843d0f |
| 10 | SIMM_SOVR_KA | 79606832-293a-4e15-90c3-1b2065395182 |
| 10 | A--SIMM_SOVR_K0 | abf53c7c-b64a-416f-b3e8-8f697d59113c |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|-----------------|--------------------------------------|
| 10 | A--SIMM_SOVR_KA | 8eff49bd-476d-4f0a-b949-3dd99d6e2050 |
| 10 | iDROSTATICA | 480c5eb3-689a-4a46-b2cb-c7cd35750485 |
| 10 | TERR_SIMM | 97022474-8556-40da-a295-3c1868da8120 |
| 10 | SIMM_KA | 36d8e519-4d50-4523-a77e-d1db4d34c1d2 |
| 10 | SIMM_K0 | 0bd47a37-45ed-415b-8ba5-9931b378f4c5 |
| 10 | TERR_A--SIMM | bba3382c-87aa-4a23-8317-b5acaaebd9b3 |
| 10 | A--SIMM_K0 | b36e1fd2-f1a5-4d29-9c2b-3be044ce0848 |
| 10 | A--SIMM_KA | 7450436b-4602-4803-a899-94aaf610fbe9 |
| 10 | SISMA WOOD SLD | 49cde15f-4413-4f21-9722-073aa526102e |
| 10 | SISMA WOOD | c47477c6-3b1a-4a2c-81b3-96e1efd2f245 |
| 11 | SOVR | 8de1a707-7f01-457c-a01d-2301d85795b4 |
| 11 | SIMM_SOVR_K0 | 7670fbe1-c350-4b16-9bdb-75a22cdc6783 |
| 11 | SIMM_SOVR_KA | 03fd50e1-48e1-4dc1-8fc4-a472a19ab437 |
| 11 | A--SIMM_SOVR_K0 | 9f382b31-b6f4-409c-81fb-b2310d25fb1b |
| 11 | A--SIMM_SOVR_KA | ace6a60c-d4c8-45d7-b0af-c5df5b223c7c |
| 11 | iDROSTATICA | 5cf603b5-bc74-4aa9-bce2-0420a92c8188 |
| 11 | TERR_SIMM | 711667b9-f09e-4515-9c15-4e0fd8e2c80c |
| 11 | SIMM_KA | 917df565-d0c5-4cc8-8aee-1ab53f91e8d4 |
| 11 | SIMM_K0 | 01015690-7852-4a9b-bfed-8cdf0246f760 |
| 11 | TERR_A--SIMM | f459a0a7-c5fc-419f-8959-4dfc27906e66 |
| 11 | A--SIMM_K0 | 99a9d0bf-16ed-4760-ac8b-90f77a573f11 |
| 11 | A--SIMM_KA | 03951dad-f37e-4428-b5db-8fc86765c2a0 |
| 11 | SISMA WOOD SLD | f9acaed6-c2b8-4c8c-b184-7cc3ce8bfcf2 |
| 11 | SISMA WOOD | 8111ed33-1b35-4e74-8fc6-7966227dc19c |
| 12 | SOVR | 5b90eb17-6126-4469-b046-f2eb7f654407 |
| 12 | SIMM_SOVR_K0 | 02c030cb-e87c-47c8-b2a4-4436c316295a |
| 12 | SIMM_SOVR_KA | 44f40cdf-9f6b-4bd5-b6c8-78f22109cec2 |
| 12 | A--SIMM_SOVR_K0 | c5ee8ecd-9fb4-448c-9e40-78a340a1d638 |
| 12 | A--SIMM_SOVR_KA | ce375f36-0f82-404b-9fa7-da4ba0fca22e |
| 12 | iDROSTATICA | 1457cf9c-82dd-4991-8858-80eec678c9cf |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|-----------------|--------------------------------------|
| 12 | TERR_SIMM | 702fbb79-3eed-4be5-a3e7-20a47ecf96ed |
| 12 | SIMM_KA | 729f7803-11e0-45d3-ad6d-7c168fe15a44 |
| 12 | SIMM_K0 | 874c512c-1feb-4ab7-84be-1a73578e073d |
| 12 | TERR_A--SIMM | b4459012-460c-4aa5-861c-f0d3abb0e654 |
| 12 | A--SIMM_K0 | 4711b555-ca21-4cda-9c07-d0b8632ece06 |
| 12 | A--SIMM_KA | 4d18a1e9-d61a-4c28-8683-dc01093f791f |
| 12 | SISMA WOOD SLD | 0996d711-d0c4-440a-9483-18e6caf8a46c |
| 12 | SISMA WOOD | 13d06d90-cb45-4271-813f-62c227f3d813 |
| 13 | SOVR | 58520a62-4a09-4a41-85c6-f2fb0f194fa |
| 13 | SIMM_SOVR_K0 | d0301497-2abc-42d9-a7d4-2830fbb6bd4c |
| 13 | SIMM_SOVR_KA | 5202838f-9dae-49de-b7bc-04950a15d49b |
| 13 | A--SIMM_SOVR_K0 | dd00b792-9b6c-4141-a1c8-ade5fd5c052f |
| 13 | A--SIMM_SOVR_KA | 76b860d0-8c23-4e9a-b9ef-bdd105ea5946 |
| 13 | IDROSTATICA | 841c323b-2023-42fb-8ff1-703f6709df49 |
| 13 | TERR_SIMM | f2bfa23a-9aee-4dd6-ab72-2b51681eceb7 |
| 13 | SIMM_KA | 017ee693-13a7-4d1a-97a2-69c784b707b6 |
| 13 | SIMM_K0 | dc5de510-6d2f-458c-89ed-40124c3ab689 |
| 13 | TERR_A--SIMM | 87935872-6653-4ffb-acdc-2840dec9a536 |
| 13 | A--SIMM_K0 | 287b6654-2449-45f4-b421-32dcd9cae1e6 |
| 13 | A--SIMM_KA | dc50a337-73b8-477b-9782-8994b8709d25 |
| 13 | SISMA WOOD SLD | 25c6f4c9-9f2c-4ea7-a70e-cf71ee8239ee |
| 13 | SISMA WOOD | a2fe1dee-7629-4b4c-8ebf-a9695fdf469e |
| 14 | IDROSTATICA | 9ce73f41-60b7-4850-a366-e6c06a1b54fb |
| 14 | SISMA WOOD SLD | d4136884-f4ab-459d-bc17-a0dcefea05d4 |
| 14 | SISMA WOOD | edc086f8-12c8-40c3-8650-921db37725a2 |
| 16 | IDROSTATICA | 6b97b621-723e-4dad-a2dd-75b7b35d6cb2 |
| 16 | SISMA WOOD SLD | 59949684-e034-4133-8d77-631251b21a9e |
| 16 | SISMA WOOD | bdc9cb65-0d62-484b-8e07-dc8ab80e3bba |
| 17 | IDROSTATICA | 9b908b60-7444-4b5c-bb3a-eb56bc92ede8 |
| 17 | SISMA WOOD SLD | 2563fdef-30d4-4fe6-8e46-5440ea8a7410 |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|-----------------|--------------------------------------|
| 17 | SISMA WOOD | fa4c2654-f3a2-4400-943e-c8475df8c8db |
| 19 | IDROSTATICA | 875bbe04-c0f6-44e3-8cae-d89363027025 |
| 19 | SIMM_KA | c850b731-3ae0-44e3-aafa-a8cbcb8353c8 |
| 19 | SIMM_K0 | d4491b9e-faa2-44ed-91c8-fce35d2dff10 |
| 19 | A--SIMM_K0 | 13a024af-c25f-4914-9784-8b87bee552d5 |
| 19 | A--SIMM_KA | c019fc45-1d47-4464-ad0d-534ba655b906 |
| 20 | IDROSTATICA | 0d3853ab-dbf9-4e28-885f-41dd76f3068c |
| 20 | SIMM_KA | 920cfb92-e906-4f9f-9278-cd26dcd8215e |
| 20 | SIMM_K0 | 347a0065-c5c9-42d3-863f-37f626d236c2 |
| 20 | A--SIMM_K0 | 002fd264-bb42-4a1d-a27b-1263ea067f8a |
| 20 | A--SIMM_KA | 75bcaf03-7ed1-4875-9643-84b31dc507f3 |
| 21 | SOVR | 5b766748-d98d-48a5-bc52-fda6ade503fa |
| 21 | SIMM_SOVR_K0 | 9700339f-598a-4533-a397-84987fb7df6 |
| 21 | SIMM_SOVR_KA | 603e6a19-4eff-4fc5-8482-0b1cea244543 |
| 21 | A--SIMM_SOVR_K0 | c7eeabf4-a5a7-4b43-8e21-fdbd6fef485f |
| 21 | A--SIMM_SOVR_KA | 8fd3214c-53ad-496d-9c99-d54918db5e02 |
| 21 | IDROSTATICA | 2078b62c-7afd-4b86-87bc-4d607599bd6f |
| 21 | TERR_SIMM | cbf511ea-ba07-4b8e-9272-1d44b20f455a |
| 21 | SIMM_KA | fc4f4987-b0ad-4c90-9af0-09c3029c9a68 |
| 21 | SIMM_K0 | 4f2bd682-d901-4a07-bbc9-caa763c9f153 |
| 21 | TERR_A--SIMM | 2a991a85-4cb8-4921-8109-46f816e608fc |
| 21 | A--SIMM_K0 | 998d2f7d-6a6a-4a5f-bcc4-f9fc8a25c31a |
| 21 | A--SIMM_KA | ce52a12e-646f-4f75-9ece-48ff9502ff94 |
| 22 | SOVR | ee5c00af-4f90-47db-878d-ccee3911e208 |
| 22 | SIMM_SOVR_K0 | 374267b6-d405-4756-8239-09f38aec56ba |
| 22 | SIMM_SOVR_KA | d410f455-54c6-4223-a5e2-ec75896f2ad0 |
| 22 | A--SIMM_SOVR_K0 | 67aac286-080c-4827-9fa4-e8d7364243d5 |
| 22 | A--SIMM_SOVR_KA | 74a885ba-9cd7-4e6e-9659-f319cf6de6b1 |
| 22 | IDROSTATICA | 25aa7b04-9f62-4a53-9d13-48b13a18a9af |
| 22 | TERR_SIMM | c7cbf8cf-1a87-4e3c-bda0-0783cfaaa8e6 |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|-----------------|--------------------------------------|
| 22 | SIMM_KA | 92cc5e50-59f3-4769-9788-15ce0e984658 |
| 22 | SIMM_K0 | 2f975304-64af-426a-9015-228694578c20 |
| 22 | TERR_A--SIMM | fde8c13d-39bf-4991-baf1-21b716c19c47 |
| 22 | A--SIMM_K0 | c16499ce-59ca-46f9-ba02-54f2e703865b |
| 22 | A--SIMM_KA | 0f408b16-bf5b-40d2-92c3-b9da010c778e |
| 23 | SOVR | 3637668e-f390-4762-87a3-1fd9cbf7582 |
| 23 | SIMM_SOVR_K0 | fbaacc49-f439-4d7a-bc3b-7e27f2a8d43b |
| 23 | SIMM_SOVR_KA | b6f6e79a-7258-4dbf-a3e8-0af0a34c5425 |
| 23 | A--SIMM_SOVR_K0 | af00f6e0-bd63-4599-83d9-ffa1871083d7 |
| 23 | A--SIMM_SOVR_KA | 582811ad-093d-43e2-8e22-0331571f2620 |
| 23 | IDROSTATICA | 1fa9a553-3b5e-4827-a661-a1758da5a27b |
| 23 | TERR_SIMM | e70891a1-eea3-4371-bf57-7817ec4b3a83 |
| 23 | SIMM_KA | e4db5ead-ab45-4148-9eff-9d4b934ca805 |
| 23 | SIMM_K0 | d5659fd0-6011-4673-a1de-428e0c78f7f4 |
| 23 | TERR_A--SIMM | af0be94f-cfa8-4392-8eee-2eb3e0fd9764 |
| 23 | A--SIMM_K0 | 5b806933-c5a2-44ce-b150-7ea1beb49709 |
| 23 | A--SIMM_KA | 33e16140-a338-42be-ae30-003e7903e96a |
| 24 | SOVR | 264f1778-a475-40e1-a1fb-67d03688a729 |
| 24 | SIMM_SOVR_K0 | b97a01de-796f-4a4e-abdc-e1df20fd1057 |
| 24 | SIMM_SOVR_KA | b428a930-6026-4b62-a8c8-e11cb9f24bb9 |
| 24 | A--SIMM_SOVR_K0 | 95e0461d-68be-48b3-96e8-d962e22bf77 |
| 24 | A--SIMM_SOVR_KA | ebd98086-1b1b-4697-bf59-aef3138394f2 |
| 24 | IDROSTATICA | fe0412fa-a201-4d31-a1b5-f07032234570 |
| 24 | TERR_SIMM | 1df4df4a-ac6d-4bc4-a994-1c66c84302c4 |
| 24 | SIMM_KA | 79088f76-b992-4142-a16f-bf9a8385fd8a |
| 24 | SIMM_K0 | e37b6afb-9fcb-438a-be60-5cf673aa217c |
| 24 | TERR_A--SIMM | a091840e-0a97-40b4-ad11-ac328a5f94f0 |
| 24 | A--SIMM_K0 | 04e96218-5d6c-47e7-9a85-b9786e40d2c5 |
| 24 | A--SIMM_KA | 9b8270c8-e7b4-43dd-a50b-b8ca2f589333 |
| 25 | SOVR | cd4fcf99-37dd-4b8b-a3d6-61c44416e445 |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|-----------------|--------------------------------------|
| 25 | SIMM_SOVR_K0 | 6ad751c5-92b0-4bbb-a7e2-990612945848 |
| 25 | SIMM_SOVR_KA | cef30f32-cfb1-4569-b0c7-6a4e2d75be7f |
| 25 | A--SIMM_SOVR_K0 | d81a2497-6b02-46ce-8dfa-3fed958805f8 |
| 25 | A--SIMM_SOVR_KA | 9722738a-23a7-413e-becf-3df3489d2a81 |
| 25 | iDROSTATICA | dd00a53f-8b0d-4d6d-b016-c10eccaffc0d |
| 25 | TERR_SIMM | c7384e95-5aff-48fa-89a1-63180f6402c6 |
| 25 | SIMM_KA | 8c51202e-4b58-4474-b02b-e8b32c7eb21a |
| 25 | SIMM_K0 | 0c7fd2b9-4486-436a-89bc-bbaedb99237e |
| 25 | TERR_A--SIMM | 99afa833-9537-4395-863b-416b6ac3ab7d |
| 25 | A--SIMM_K0 | 8a7b4f64-49b7-4b93-96d9-7fc42cae61e2 |
| 25 | A--SIMM_KA | 60d17ff2-7ffe-44b1-a1ba-6bfef2c747df |
| 26 | SOVR | 26e50500-79c3-440b-ba22-c4aa4902814f |
| 26 | SIMM_SOVR_K0 | 9d101c58-383b-44bf-a509-3d24b712371a |
| 26 | SIMM_SOVR_KA | 263cbf53-bd58-4d0a-880a-d7a67709952f |
| 26 | A--SIMM_SOVR_K0 | 86ac06db-e9be-48f9-a7b7-848545af3f12 |
| 26 | A--SIMM_SOVR_KA | 7bff0e34-572e-41a5-83bd-c184670c2a75 |
| 26 | iDROSTATICA | 40669899-f94f-447c-b665-52c0251dc643 |
| 26 | TERR_SIMM | 32f83f33-37be-47cb-935f-5e18e5bfb3f3 |
| 26 | SIMM_KA | c714fae7-520b-4a0d-bfc3-11322ed66ca5 |
| 26 | SIMM_K0 | fdee8309-abe5-4546-a1e7-e5f3f545c0de |
| 26 | TERR_A--SIMM | fd1648c7-02c4-425c-a5ab-68f8313d60d1 |
| 26 | A--SIMM_K0 | ea61006a-29b1-42e2-baac-32b162d36481 |
| 26 | A--SIMM_KA | 59a9602c-220e-4ec9-96bb-0e821610c163 |
| 27 | iDROSTATICA | 2c4bff4e-b205-4111-b898-80e954346255 |
| 28 | iDROSTATICA | fe671363-4314-4c56-8e27-3d695eed3043 |
| 29 | iDROSTATICA | 41e899c5-783c-4b4d-b17e-e82970488208 |
| 30 | iDROSTATICA | ebbc90f6-6fdd-449a-ab2a-fd7dd97fe334 |
| 31 | iDROSTATICA | a0a704bb-4c5f-49d8-abe8-9a5d88727671 |
| 1 | iDROSTATICA | 8a7ba2c4-c863-40f3-ae1-aa22464ccdc2 |
| 1 | SISMA WOOD SLD | 3726b007-8ec2-4c88-9ddd-584a2a8490cd |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|----------------|--------------------------------------|
| 1 | SISMA WOOD | 98ad64fb-8d06-4fa6-b32a-f6a13f187444 |
| 4 | IDROSTATICA | 8a7ba2c4-c863-40f3-ae1-aa22464ccdc2 |
| 4 | SISMA WOOD SLD | 9e9f0d25-7f71-43d8-9e31-56ed754e3683 |
| 4 | SISMA WOOD | 90e0b81f-98e1-4e1f-8976-ab5078693456 |
| 34 | IDROSTATICA | 66bd9133-300a-4251-b223-1172974aafd4 |
| 35 | IDROSTATICA | 66bd9133-300a-4251-b223-1172974aafd4 |
| 38 | IDROSTATICA | a61e5f41-c05b-4241-a8ab-4231a5f84376 |
| 38 | SIMM_KA | 070415e6-9004-4658-82d2-856a61a28f55 |
| 38 | SIMM_K0 | 693b7f6b-eb4-43b1-bacf-954932093601 |
| 38 | A--SIMM_K0 | 2b2a8ec9-f4cd-45fa-a33d-dfcee3210460 |
| 38 | A--SIMM_KA | 642b159f-5ec1-4ff2-82bb-158a31e00b6c |
| 38 | SISMA WOOD SLD | b59e8d6e-c0b0-435b-8cd7-93693c4281d5 |
| 38 | SISMA WOOD | 810f60a9-9adf-4e00-a379-ae4d4e9d66e4 |
| 39 | IDROSTATICA | a61e5f41-c05b-4241-a8ab-4231a5f84376 |
| 39 | SIMM_KA | 590c641e-87b8-4e46-8560-d667de229d6a |
| 39 | SIMM_K0 | 96fcfece-325e-415f-a227-8537cca26b59 |
| 39 | A--SIMM_K0 | 11743528-70a9-4392-abd1-95a6e0399702 |
| 39 | A--SIMM_KA | 344e4b39-5a4c-48b4-9ece-813c5ef4faba |
| 39 | SISMA WOOD SLD | 880029f5-e245-4de6-92e1-5876252e947d |
| 39 | SISMA WOOD | a0a6a40c-2461-4471-959d-dde977127bb4 |
| 41 | IDROSTATICA | fad49177-d433-4826-8650-86b28bc388ce |
| 41 | SIMM_KA | ae6e4998-471e-4735-bb32-60bcb0d9a29d |
| 41 | SIMM_K0 | 243f94b5-c4fc-470e-be35-f0e658a25d00 |
| 41 | A--SIMM_K0 | 739d100d-be64-4573-abb8-7073f149dba2 |
| 41 | A--SIMM_KA | a6586775-03e8-4286-92ce-f8216d4ee3a4 |
| 42 | IDROSTATICA | fad49177-d433-4826-8650-86b28bc388ce |
| 42 | SIMM_KA | a0604380-cf2b-4e48-822e-9f6a32a604bd |
| 42 | SIMM_K0 | 8c26bbb9-bcc6-4e01-bf26-839d5ff77ce0 |
| 42 | A--SIMM_K0 | 963c284a-8db2-476c-a51f-360e84981bef |
| 42 | A--SIMM_KA | 993a56be-8110-4ac0-b2d1-2e2aefca892b |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|----------------|--|
| 43 | IDROSTATICA | 8a7ba2c4-c863-40f3- aee1-aa22464ccdc2 |
| 43 | SISMA WOOD SLD | b013b73a-d8b8-4edb- 9a90-6029c317b5a7 |
| 43 | SISMA WOOD | 837333d6-2094-4399- 9948-f6c1dbcce964 |
| 44 | IDROSTATICA | 8a7ba2c4-c863-40f3- aee1-aa22464ccdc2 |
| 44 | SISMA WOOD SLD | 6a9d4ff3-508d-4883- a662-242b8c028c82 |
| 44 | SISMA WOOD | c0125a7d-c774-4b28- b579-e0f38ba85f65 |
| 45 | IDROSTATICA | a61e5f41-c05b-4241- a8ab-4231a5f84376 |
| 45 | SIMM_KA | 1229ca05-ce51-4618- 815b-9d219ef33bdb |
| 45 | SIMM_K0 | b185f63b-842c-4c7b- b2b4-f64449f39fc7 |
| 45 | A--SIMM_K0 | d3dc0aa0-9094-405f- 98a7-df51a6de4634 |
| 45 | A--SIMM_KA | a7e6b9ad-e9ce-4d4d- 9d02-c61df08efd46 |
| 45 | SISMA WOOD SLD | ab98f1e0-0c93-4083- 93d3-347efaf1c40c |
| 45 | SISMA WOOD | d5d63666-3197-4ca1- 8ee7-39f2b4c463be |
| 46 | IDROSTATICA | a61e5f41-c05b-4241- a8ab-4231a5f84376 |
| 46 | SIMM_KA | 4b8614c4-bd7f-47aa- 90e8-0702c5a1a6bf |
| 46 | SIMM_K0 | f5df4089-e986-428d- bd3a-289e694fe174 |
| 46 | A--SIMM_K0 | c790ad43-e8aa-4199- bbae-4a2d5fc4a1c1 |
| 46 | A--SIMM_KA | 7621d753-7a87-49cc- bcec-9dcf1404826e |
| 46 | SISMA WOOD SLD | 02a8e23e-65ff-4858- 9688-e7c00aeaf194 |
| 46 | SISMA WOOD | 9632d64d-c81d-412d- aece-4bd8c3c1b09c |
| 47 | IDROSTATICA | 66bd9133-300a-4251- b223-1172974aafd4 |
| 48 | IDROSTATICA | 66bd9133-300a-4251- b223-1172974aafd4 |
| 49 | IDROSTATICA | fad49177-d433-4826- 8650-86b28bc388ce |
| 49 | SIMM_KA | f792def4-af65-453c- 8780-71a269698ed0 |
| 49 | SIMM_K0 | 28746da8-d3f1-41cf- a166-dbc82ae4a97d |
| 49 | A--SIMM_K0 | d1a630b8-9326-45a6- b4be-7a64269a2f31 |
| 49 | A--SIMM_KA | 7648142d-ecaf-46bd- ad54-382cc514d8f9 |
| 50 | IDROSTATICA | fad49177-d433-4826- 8650-86b28bc388ce |
| 50 | SIMM_KA | b75732c3-0b5d-463f- 82d0-502ad79febcb |
| 50 | SIMM_K0 | 0be3dc16-27fc-491b- 8e23-9d530976e23c |

PROGETTAZIONE ATI:

Table: Frame Loads - Distributed, Part 3 of 3

| Frame | LoadPat | GUID |
|-------|------------|--------------------------------------|
| 50 | A--SIMM_K0 | 8a4a8a92-6651-42c7-b5b2-12f74517db2b |
| 50 | A--SIMM_KA | 663efe6c-3ec5-4b4a-8a47-7d4949f43213 |

Table: Combination Definitions

Table: Combination Definitions

| ComboName | ComboType | CaseName | ScaleFactor |
|-----------|------------|------------------|-------------|
| SLU_PROVA | Linear Add | DEAD | 1.3 |
| SLU_PROVA | | iDROSTATICA | 1.3 |
| SLU_PROVA | | TERR_SIMM | 1.3 |
| SLU_PROVA | | SIMM_K0 | 1.3 |
| SLU_PROVA | | SOVR | 1.5 |
| SLU_PROVA | | SIMM_SOVR_K 0 | 1.5 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Table: Element Forces - Frames, Part 1 of 2 | | | | | | |
|---|--------------|-------------------------|----------|----------|----------|----------|
| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
| 1 | 0. | DEAD | | 45.609 | 6.614 | 0. |
| 1 | 0.30384 | DEAD | | 49.224 | 14.978 | 0. |
| 1 | 0.60768 | DEAD | | 52.839 | 23.343 | 0. |
| 1 | 0. | SIMM_KA | | -145.959 | 23.382 | 0. |
| 1 | 0.30384 | SIMM_KA | | -145.959 | 23.382 | 0. |
| 1 | 0.60768 | SIMM_KA | | -145.959 | 23.382 | 0. |
| 1 | 0. | SIMM_K0 | | -220.417 | 34.689 | 0. |
| 1 | 0.30384 | SIMM_K0 | | -220.417 | 34.689 | 0. |
| 1 | 0.60768 | SIMM_K0 | | -220.417 | 34.689 | 0. |
| 1 | 0. | A--SIMM_KA | | -184.555 | 21.986 | 0. |
| 1 | 0.30384 | A--SIMM_KA | | -184.555 | 21.986 | 0. |
| 1 | 0.60768 | A--SIMM_KA | | -184.555 | 21.986 | 0. |
| 1 | 0. | A--SIMM_K0 | | -284.171 | 34.093 | 0. |
| 1 | 0.30384 | A--SIMM_K0 | | -284.171 | 34.093 | 0. |
| 1 | 0.60768 | A--SIMM_K0 | | -284.171 | 34.093 | 0. |
| 1 | 0. | A-- SIMM_SOVR_K A | | -9.272 | -0.56 | 0. |
| 1 | 0.30384 | A-- SIMM_SOVR_K A | | -9.272 | -0.56 | 0. |
| 1 | 0.60768 | A-- SIMM_SOVR_K A | | -9.272 | -0.56 | 0. |
| 1 | 0. | A-- SIMM_SOVR_K 0 | | -13.902 | -0.839 | 0. |
| 1 | 0.30384 | A-- SIMM_SOVR_K 0 | | -13.902 | -0.839 | 0. |
| 1 | 0.60768 | A-- SIMM_SOVR_K 0 | | -13.902 | -0.839 | 0. |
| 1 | 0. | SIMM_SOVR_K 0 | | -13.902 | -0.839 | 0. |
| 1 | 0.30384 | SIMM_SOVR_K 0 | | -13.902 | -0.839 | 0. |
| 1 | 0.60768 | SIMM_SOVR_K 0 | | -13.902 | -0.839 | 0. |
| 1 | 0. | SIMM_SOVR_K A | | -9.272 | -0.56 | 0. |
| 1 | 0.30384 | SIMM_SOVR_K A | | -9.272 | -0.56 | 0. |
| 1 | 0.60768 | SIMM_SOVR_K A | | -9.272 | -0.56 | 0. |
| 1 | 0. | SOVR | | 1.795 | -31.068 | 0. |
| 1 | 0.30384 | SOVR | | 1.795 | -31.068 | 0. |
| 1 | 0.60768 | SOVR | | 1.795 | -31.068 | 0. |
| 1 | 0. | TERR_SIMM | | -17.548 | -124.805 | 0. |
| 1 | 0.30384 | TERR_SIMM | | -17.548 | -124.805 | 0. |
| 1 | 0.60768 | TERR_SIMM | | -17.548 | -124.805 | 0. |
| 1 | 0. | TERR_A--SIMM | | -24.77 | -187.802 | 0. |
| 1 | 0.30384 | TERR_A--SIMM | | -24.77 | -187.802 | 0. |
| 1 | 0.60768 | TERR_A--SIMM | | -24.77 | -187.802 | 0. |
| 1 | 0. | INERZIA H SLV | | 6.416 | -0.968 | 0. |
| 1 | 0.30384 | INERZIA H SLV | | 6.416 | -0.968 | 0. |
| 1 | 0.60768 | INERZIA H SLV | | 6.416 | -0.968 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 1 | 0. | INERZIA V + SLV | | 0.777 | 0.251 | 0. |
| 1 | 0.30384 | INERZIA V + SLV | | 0.777 | 0.251 | 0. |
| 1 | 0.60768 | INERZIA V + SLV | | 0.777 | 0.251 | 0. |
| 1 | 0. | INERZIA V - SLV | | -0.777 | -0.251 | 0. |
| 1 | 0.30384 | INERZIA V - SLV | | -0.777 | -0.251 | 0. |
| 1 | 0.60768 | INERZIA V - SLV | | -0.777 | -0.251 | 0. |
| 1 | 0. | SISMA WOOD SLV | | 48.059 | -14.898 | 0. |
| 1 | 0.30384 | SISMA WOOD SLV | | 67.51 | -23.304 | 0. |
| 1 | 0.60768 | SISMA WOOD SLV | | 86.961 | -31.71 | 0. |
| 1 | 0. | IDROSTATICA | | -657.611 | -237.997 | 0. |
| 1 | 0.30384 | IDROSTATICA | | -657.611 | -275.39 | 0. |
| 1 | 0.60768 | IDROSTATICA | | -657.611 | -312.784 | 0. |
| 1 | 0. | SISMA WOOD SLD | | 21.225 | -6.579 | 0. |
| 1 | 0.30384 | SISMA WOOD SLD | | 29.815 | -10.292 | 0. |
| 1 | 0.60768 | SISMA WOOD SLD | | 38.405 | -14.004 | 0. |
| 1 | 0. | INERZIA H SLD | | 2.834 | -0.427 | 0. |
| 1 | 0.30384 | INERZIA H SLD | | 2.834 | -0.427 | 0. |
| 1 | 0.60768 | INERZIA H SLD | | 2.834 | -0.427 | 0. |
| 1 | 0. | INERZIA V + SLD | | 0.343 | 0.111 | 0. |
| 1 | 0.30384 | INERZIA V + SLD | | 0.343 | 0.111 | 0. |
| 1 | 0.60768 | INERZIA V + SLD | | 0.343 | 0.111 | 0. |
| 1 | 0. | INERZIA V SLD | | -0.343 | -0.111 | 0. |
| 1 | 0.30384 | INERZIA V SLD | | -0.343 | -0.111 | 0. |
| 1 | 0.60768 | INERZIA V SLD | | -0.343 | -0.111 | 0. |
| 1 | 0. | INERZIA V -1 | | -0.777 | -0.251 | 0. |
| 1 | 0.30384 | INERZIA V -1 | | -0.777 | -0.251 | 0. |
| 1 | 0.60768 | INERZIA V -1 | | -0.777 | -0.251 | 0. |
| 1 | 0. | SLU_1 | Max | -1141.835 | -513.949 | 0. |
| 1 | 0.30384 | SLU_1 | Max | -1137.135 | -551.686 | 0. |
| 1 | 0.60768 | SLU_1 | Max | -1132.436 | -589.423 | 0. |
| 1 | 0. | SLU_1 | Min | -1141.835 | -513.949 | 0. |
| 1 | 0.30384 | SLU_1 | Min | -1137.135 | -551.686 | 0. |
| 1 | 0.60768 | SLU_1 | Min | -1132.436 | -589.423 | 0. |
| 1 | 0. | SLU_2 | Max | -1048.924 | -540.091 | 0. |
| 1 | 0.30384 | SLU_2 | Max | -1044.225 | -577.828 | 0. |
| 1 | 0.60768 | SLU_2 | Max | -1039.525 | -615.565 | 0. |
| 1 | 0. | SLU_2 | Min | -1048.924 | -540.091 | 0. |
| 1 | 0.30384 | SLU_2 | Min | -1044.225 | -577.828 | 0. |
| 1 | 0.60768 | SLU_2 | Min | -1039.525 | -615.565 | 0. |
| 1 | 0. | SLU_3 | Max | -1238.249 | -620.074 | 0. |
| 1 | 0.30384 | SLU_3 | Max | -1233.55 | -657.812 | 0. |
| 1 | 0.60768 | SLU_3 | Max | -1228.85 | -695.549 | 0. |
| 1 | 0. | SLU_3 | Min | -1238.249 | -620.074 | 0. |
| 1 | 0.30384 | SLU_3 | Min | -1233.55 | -657.812 | 0. |
| 1 | 0.60768 | SLU_3 | Min | -1228.85 | -695.549 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 1 | 0. | SLU_4 | Max | -1101.616 | -638.63 | 0. |
| 1 | 0.30384 | SLU_4 | Max | -1096.916 | -676.367 | 0. |
| 1 | 0.60768 | SLU_4 | Max | -1092.217 | -714.104 | 0. |
| 1 | 0. | SLU_4 | Min | -1101.616 | -638.63 | 0. |
| 1 | 0.30384 | SLU_4 | Min | -1096.916 | -676.367 | 0. |
| 1 | 0.60768 | SLU_4 | Min | -1092.217 | -714.104 | 0. |
| 1 | 0. | SLE_F1 | Max | -877.981 | -383.416 | 0. |
| 1 | 0.30384 | SLE_F1 | Max | -874.366 | -412.445 | 0. |
| 1 | 0.60768 | SLE_F1 | Max | -870.751 | -441.474 | 0. |
| 1 | 0. | SLE_F1 | Min | -877.981 | -383.416 | 0. |
| 1 | 0.30384 | SLE_F1 | Min | -874.366 | -412.445 | 0. |
| 1 | 0.60768 | SLE_F1 | Min | -870.751 | -441.474 | 0. |
| 1 | 0. | SLE_F2 | Max | -809.223 | -403.518 | 0. |
| 1 | 0.30384 | SLE_F2 | Max | -805.608 | -432.547 | 0. |
| 1 | 0.60768 | SLE_F2 | Max | -801.993 | -461.576 | 0. |
| 1 | 0. | SLE_F2 | Min | -809.223 | -403.518 | 0. |
| 1 | 0.30384 | SLE_F2 | Min | -805.608 | -432.547 | 0. |
| 1 | 0.60768 | SLE_F2 | Min | -801.993 | -461.576 | 0. |
| 1 | 0. | SLE_F3 | Max | -848.571 | -477.811 | 0. |
| 1 | 0.30384 | SLE_F3 | Max | -844.956 | -506.84 | 0. |
| 1 | 0.60768 | SLE_F3 | Max | -841.341 | -535.869 | 0. |
| 1 | 0. | SLE_F3 | Min | -848.571 | -477.811 | 0. |
| 1 | 0.30384 | SLE_F3 | Min | -844.956 | -506.84 | 0. |
| 1 | 0.60768 | SLE_F3 | Min | -841.341 | -535.869 | 0. |
| 1 | 0. | SLE_F4 | Max | -957.502 | -461.021 | 0. |
| 1 | 0.30384 | SLE_F4 | Max | -953.887 | -490.05 | 0. |
| 1 | 0.60768 | SLE_F4 | Max | -950.272 | -519.078 | 0. |
| 1 | 0. | SLE_F4 | Min | -957.502 | -461.021 | 0. |
| 1 | 0.30384 | SLE_F4 | Min | -953.887 | -490.05 | 0. |
| 1 | 0.60768 | SLE_F4 | Min | -950.272 | -519.078 | 0. |
| 1 | 0. | SLE_QP1 | Max | -879.407 | -361.688 | 0. |
| 1 | 0.30384 | SLE_QP1 | Max | -875.792 | -390.716 | 0. |
| 1 | 0.60768 | SLE_QP1 | Max | -872.177 | -419.745 | 0. |
| 1 | 0. | SLE_QP1 | Min | -879.407 | -361.688 | 0. |
| 1 | 0.30384 | SLE_QP1 | Min | -875.792 | -390.716 | 0. |
| 1 | 0.60768 | SLE_QP1 | Min | -872.177 | -419.745 | 0. |
| 1 | 0. | SLE_QP2 | Max | -813.606 | -381.35 | 0. |
| 1 | 0.30384 | SLE_QP2 | Max | -809.991 | -410.379 | 0. |
| 1 | 0.60768 | SLE_QP2 | Max | -806.377 | -439.407 | 0. |
| 1 | 0. | SLE_QP2 | Min | -813.606 | -381.35 | 0. |
| 1 | 0.30384 | SLE_QP2 | Min | -809.991 | -410.379 | 0. |
| 1 | 0.60768 | SLE_QP2 | Min | -806.377 | -439.407 | 0. |
| 1 | 0. | SLE_QP3 | Max | -850.752 | -452.847 | 0. |
| 1 | 0.30384 | SLE_QP3 | Max | -847.137 | -481.876 | 0. |
| 1 | 0.60768 | SLE_QP3 | Max | -843.522 | -510.904 | 0. |
| 1 | 0. | SLE_QP3 | Min | -850.752 | -452.847 | 0. |
| 1 | 0.30384 | SLE_QP3 | Min | -847.137 | -481.876 | 0. |
| 1 | 0.60768 | SLE_QP3 | Min | -843.522 | -510.904 | 0. |
| 1 | 0. | SLE_QP4 | Max | -967.933 | -430.859 | 0. |
| 1 | 0.30384 | SLE_QP4 | Max | -964.318 | -459.887 | 0. |
| 1 | 0.60768 | SLE_QP4 | Max | -960.703 | -488.916 | 0. |
| 1 | 0. | SLE_QP4 | Min | -967.933 | -430.859 | 0. |
| 1 | 0.30384 | SLE_QP4 | Min | -964.318 | -459.887 | 0. |
| 1 | 0.60768 | SLE_QP4 | Min | -960.703 | -488.916 | 0. |
| 1 | 0. | SLV_1 | Max | -1286.388 | -246.782 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 1 | 0.30384 | SLV_1 | Max | -1263.322 | -284.217 | 0. |
| 1 | 0.60768 | SLV_1 | Max | -1240.256 | -321.651 | 0. |
| 1 | 0. | SLV_1 | Min | -1286.388 | -246.782 | 0. |
| 1 | 0.30384 | SLV_1 | Min | -1263.322 | -284.217 | 0. |
| 1 | 0.60768 | SLV_1 | Min | -1240.256 | -321.651 | 0. |
| 1 | 0. | SLV_2 | Max | -1288.856 | -247.267 | 0. |
| 1 | 0.30384 | SLV_2 | Max | -1265.79 | -284.702 | 0. |
| 1 | 0.60768 | SLV_2 | Max | -1242.724 | -322.137 | 0. |
| 1 | 0. | SLV_2 | Min | -1288.856 | -247.267 | 0. |
| 1 | 0.30384 | SLV_2 | Min | -1265.79 | -284.702 | 0. |
| 1 | 0.60768 | SLV_2 | Min | -1242.724 | -322.137 | 0. |
| 1 | 0. | SLV_3 | Max | -1482.889 | -292.199 | 0. |
| 1 | 0.30384 | SLV_3 | Max | -1459.823 | -329.634 | 0. |
| 1 | 0.60768 | SLV_3 | Max | -1436.757 | -367.068 | 0. |
| 1 | 0. | SLV_3 | Min | -1482.889 | -292.199 | 0. |
| 1 | 0.30384 | SLV_3 | Min | -1459.823 | -329.634 | 0. |
| 1 | 0.60768 | SLV_3 | Min | -1436.757 | -367.068 | 0. |
| 1 | 0. | SLV_4 | Max | -1485.108 | -292.042 | 0. |
| 1 | 0.30384 | SLV_4 | Max | -1462.042 | -329.477 | 0. |
| 1 | 0.60768 | SLV_4 | Max | -1438.976 | -366.912 | 0. |
| 1 | 0. | SLV_4 | Min | -1485.108 | -292.042 | 0. |
| 1 | 0.30384 | SLV_4 | Min | -1462.042 | -329.477 | 0. |
| 1 | 0.60768 | SLV_4 | Min | -1438.976 | -366.912 | 0. |
| 1 | 0. | SLD_1 | Max | -998.654 | -327.029 | 0. |
| 1 | 0.30384 | SLD_1 | Max | -986.448 | -359.77 | 0. |
| 1 | 0.60768 | SLD_1 | Max | -974.243 | -392.511 | 0. |
| 1 | 0. | SLD_1 | Min | -998.654 | -327.029 | 0. |
| 1 | 0.30384 | SLD_1 | Min | -986.448 | -359.77 | 0. |
| 1 | 0.60768 | SLD_1 | Min | -974.243 | -392.511 | 0. |
| 1 | 0. | SLD_2 | Max | -1000.069 | -327.469 | 0. |
| 1 | 0.30384 | SLD_2 | Max | -987.864 | -360.21 | 0. |
| 1 | 0.60768 | SLD_2 | Max | -975.658 | -392.951 | 0. |
| 1 | 0. | SLD_2 | Min | -1000.069 | -327.469 | 0. |
| 1 | 0.30384 | SLD_2 | Min | -987.864 | -360.21 | 0. |
| 1 | 0.60768 | SLD_2 | Min | -975.658 | -392.951 | 0. |
| 1 | 0. | SLD_3 | Max | -1194.43 | -365.993 | 0. |
| 1 | 0.30384 | SLD_3 | Max | -1182.225 | -398.734 | 0. |
| 1 | 0.60768 | SLD_3 | Max | -1170.019 | -431.475 | 0. |
| 1 | 0. | SLD_3 | Min | -1194.43 | -365.993 | 0. |
| 1 | 0.30384 | SLD_3 | Min | -1182.225 | -398.734 | 0. |
| 1 | 0.60768 | SLD_3 | Min | -1170.019 | -431.475 | 0. |
| 1 | 0. | SLD_4 | Max | -1195.369 | -366.001 | 0. |
| 1 | 0.30384 | SLD_4 | Max | -1183.164 | -398.742 | 0. |
| 1 | 0.60768 | SLD_4 | Max | -1170.959 | -431.483 | 0. |
| 1 | 0. | SLD_4 | Min | -1195.369 | -366.001 | 0. |
| 1 | 0.30384 | SLD_4 | Min | -1183.164 | -398.742 | 0. |
| 1 | 0.60768 | SLD_4 | Min | -1170.959 | -431.483 | 0. |
| 1 | 0. | SLU_IDR_1 | Max | -936.793 | -476.492 | 0. |
| 1 | 0.30384 | SLU_IDR_1 | Max | -933.54 | -510.096 | 0. |
| 1 | 0.60768 | SLU_IDR_1 | Max | -930.286 | -543.701 | 0. |
| 1 | 0. | SLU_IDR_1 | Min | -936.793 | -476.492 | 0. |
| 1 | 0.30384 | SLU_IDR_1 | Min | -933.54 | -510.096 | 0. |
| 1 | 0.60768 | SLU_IDR_1 | Min | -930.286 | -543.701 | 0. |
| 1 | 0. | SLU_IDR_2 | Max | -911.689 | -423.312 | 0. |
| 1 | 0.30384 | SLU_IDR_2 | Max | -908.436 | -456.917 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 1 | 0.60768 | SLU_IDR_2 | Max | -905.182 | -490.521 | 0. |
| 1 | 0. | SLU_IDR_2 | Min | -911.689 | -423.312 | 0. |
| 1 | 0.30384 | SLU_IDR_2 | Min | -908.436 | -456.917 | 0. |
| 1 | 0.60768 | SLU_IDR_2 | Min | -905.182 | -490.521 | 0. |
| 1 | 0. | SISMA WOOD SLV-1 | Max | -411.399 | 147.437 | 0. |
| 1 | 0.30384 | SISMA WOOD SLV-1 | Max | -391.948 | 139.031 | 0. |
| 1 | 0.60768 | SISMA WOOD SLV-1 | Max | -372.497 | 130.625 | 0. |
| 1 | 0. | SISMA WOOD SLV-1 | Min | -411.399 | 147.437 | 0. |
| 1 | 0.30384 | SISMA WOOD SLV-1 | Min | -391.948 | 139.031 | 0. |
| 1 | 0.60768 | SISMA WOOD SLV-1 | Min | -372.497 | 130.625 | 0. |
| 1 | 0. | DEAD-1 | Max | 48.459 | -3.549 | 0. |
| 1 | 0.30384 | DEAD-1 | Max | 52.074 | 4.816 | 0. |
| 1 | 0.60768 | DEAD-1 | Max | 55.689 | 13.181 | 0. |
| 1 | 0. | DEAD-1 | Min | 48.459 | -3.549 | 0. |
| 1 | 0.30384 | DEAD-1 | Min | 52.074 | 4.816 | 0. |
| 1 | 0.60768 | DEAD-1 | Min | 55.689 | 13.181 | 0. |
| 1 | 0. | SLU_PROVA | | -1123.118 | -465.81 | 0. |
| 1 | 0.30384 | SLU_PROVA | | -1118.419 | -503.547 | 0. |
| 1 | 0.60768 | SLU_PROVA | | -1113.719 | -541.284 | 0. |
| 2 | 0. | DEAD | | 16.661 | -10.794 | 0. |
| 2 | 0.68666 | DEAD | | 18.911 | 9.677 | 0. |
| 2 | 1.37332 | DEAD | | 21.16 | 30.147 | 0. |
| 2 | 0. | SIMM_KA | | -147.365 | -4.114 | 0. |
| 2 | 0.68666 | SIMM_KA | | -147.365 | -4.114 | 0. |
| 2 | 1.37332 | SIMM_KA | | -147.365 | -4.114 | 0. |
| 2 | 0. | SIMM_K0 | | -222.379 | -6.521 | 0. |
| 2 | 0.68666 | SIMM_K0 | | -222.379 | -6.521 | 0. |
| 2 | 1.37332 | SIMM_K0 | | -222.379 | -6.521 | 0. |
| 2 | 0. | A--SIMM_KA | | -182.98 | -20.194 | 0. |
| 2 | 0.68666 | A--SIMM_KA | | -182.98 | -20.194 | 0. |
| 2 | 1.37332 | A--SIMM_KA | | -182.98 | -20.194 | 0. |
| 2 | 0. | A--SIMM_K0 | | -281.918 | -30.203 | 0. |
| 2 | 0.68666 | A--SIMM_K0 | | -281.918 | -30.203 | 0. |
| 2 | 1.37332 | A--SIMM_K0 | | -281.918 | -30.203 | 0. |
| 2 | 0. | A-- SIMM_SOVR_K A | | -8.828 | -1.249 | 0. |
| 2 | 0.68666 | A-- SIMM_SOVR_K A | | -8.828 | -1.249 | 0. |
| 2 | 1.37332 | A-- SIMM_SOVR_K A | | -8.828 | -1.249 | 0. |
| 2 | 0. | A-- SIMM_SOVR_K 0 | | -13.235 | -1.873 | 0. |
| 2 | 0.68666 | A-- SIMM_SOVR_K 0 | | -13.235 | -1.873 | 0. |
| 2 | 1.37332 | A-- SIMM_SOVR_K 0 | | -13.235 | -1.873 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|----------|----------|
| 2 | 0. | SIMM_SOVR_K 0 | | -13.235 | -1.873 | 0. |
| 2 | 0.68666 | SIMM_SOVR_K 0 | | -13.235 | -1.873 | 0. |
| 2 | 1.37332 | SIMM_SOVR_K 0 | | -13.235 | -1.873 | 0. |
| 2 | 0. | SIMM_SOVR_K A | | -8.828 | -1.249 | 0. |
| 2 | 0.68666 | SIMM_SOVR_K A | | -8.828 | -1.249 | 0. |
| 2 | 1.37332 | SIMM_SOVR_K A | | -8.828 | -1.249 | 0. |
| 2 | 0. | SOVR | | 8.272 | -6.167 | 0. |
| 2 | 0.68666 | SOVR | | 8.272 | -6.167 | 0. |
| 2 | 1.37332 | SOVR | | 8.272 | -6.167 | 0. |
| 2 | 0. | TERR_SIMM | | 9.335 | -27.753 | 0. |
| 2 | 0.68666 | TERR_SIMM | | 9.335 | -27.753 | 0. |
| 2 | 1.37332 | TERR_SIMM | | 9.335 | -27.753 | 0. |
| 2 | 0. | TERR_A--SIMM | | 14.733 | -32.705 | 0. |
| 2 | 0.68666 | TERR_A--SIMM | | 14.733 | -32.705 | 0. |
| 2 | 1.37332 | TERR_A--SIMM | | 14.733 | -32.705 | 0. |
| 2 | 0. | INERZIA H SLV | | 2.553 | -0.445 | 0. |
| 2 | 0.68666 | INERZIA H SLV | | 2.553 | -0.445 | 0. |
| 2 | 1.37332 | INERZIA H SLV | | 2.553 | -0.445 | 0. |
| 2 | 0. | INERZIA V + SLV | | 0.285 | 0.158 | 0. |
| 2 | 0.68666 | INERZIA V + SLV | | 0.285 | 0.158 | 0. |
| 2 | 1.37332 | INERZIA V + SLV | | 0.285 | 0.158 | 0. |
| 2 | 0. | INERZIA V - SLV | | -0.285 | -0.158 | 0. |
| 2 | 0.68666 | INERZIA V - SLV | | -0.285 | -0.158 | 0. |
| 2 | 1.37332 | INERZIA V - SLV | | -0.285 | -0.158 | 0. |
| 2 | 0. | SISMA WOOD SLV | | -263.613 | -12.006 | 0. |
| 2 | 0.68666 | SISMA WOOD SLV | | -216.012 | -17.237 | 0. |
| 2 | 1.37332 | SISMA WOOD SLV | | -168.411 | -22.467 | 0. |
| 2 | 0. | iDROSTATICA | | -582.265 | -25.569 | 0. |
| 2 | 0.68666 | iDROSTATICA | | -582.265 | -110.076 | 0. |
| 2 | 1.37332 | iDROSTATICA | | -582.265 | -194.583 | 0. |
| 2 | 0. | SISMA WOOD SLD | | -116.422 | -5.302 | 0. |
| 2 | 0.68666 | SISMA WOOD SLD | | -95.4 | -7.612 | 0. |
| 2 | 1.37332 | SISMA WOOD SLD | | -74.377 | -9.922 | 0. |
| 2 | 0. | INERZIA H SLD | | 1.128 | -0.196 | 0. |
| 2 | 0.68666 | INERZIA H SLD | | 1.128 | -0.196 | 0. |
| 2 | 1.37332 | INERZIA H SLD | | 1.128 | -0.196 | 0. |
| 2 | 0. | INERZIA V + SLD | | 0.126 | 0.07 | 0. |
| 2 | 0.68666 | INERZIA V + SLD | | 0.126 | 0.07 | 0. |
| 2 | 1.37332 | INERZIA V + SLD | | 0.126 | 0.07 | 0. |
| 2 | 0. | INERZIA V SLD | | -0.126 | -0.07 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------|----------|-----------|----------|----------|
| 2 | 0.68666 | INERZIA V SLD | | -0.126 | -0.07 | 0. |
| 2 | 1.37332 | INERZIA V SLD | | -0.126 | -0.07 | 0. |
| 2 | 0. | INERZIA V -1 | | -0.285 | -0.158 | 0. |
| 2 | 0.68666 | INERZIA V -1 | | -0.285 | -0.158 | 0. |
| 2 | 1.37332 | INERZIA V -1 | | -0.285 | -0.158 | 0. |
| 2 | 0. | SLU_1 | Max | -1024.77 | -150.216 | 0. |
| 2 | 0.68666 | SLU_1 | Max | -1021.846 | -233.464 | 0. |
| 2 | 1.37332 | SLU_1 | Max | -1018.922 | -316.712 | 0. |
| 2 | 0. | SLU_1 | Min | -1024.77 | -150.216 | 0. |
| 2 | 0.68666 | SLU_1 | Min | -1021.846 | -233.464 | 0. |
| 2 | 1.37332 | SLU_1 | Min | -1018.922 | -316.712 | 0. |
| 2 | 0. | SLU_2 | Max | -927.008 | -159.931 | 0. |
| 2 | 0.68666 | SLU_2 | Max | -924.084 | -243.179 | 0. |
| 2 | 1.37332 | SLU_2 | Max | -921.16 | -326.426 | 0. |
| 2 | 0. | SLU_2 | Min | -927.008 | -159.931 | 0. |
| 2 | 0.68666 | SLU_2 | Min | -924.084 | -243.179 | 0. |
| 2 | 1.37332 | SLU_2 | Min | -921.16 | -326.426 | 0. |
| 2 | 0. | SLU_3 | Max | -1094.053 | -188.732 | 0. |
| 2 | 0.68666 | SLU_3 | Max | -1091.129 | -271.98 | 0. |
| 2 | 1.37332 | SLU_3 | Max | -1088.205 | -355.227 | 0. |
| 2 | 0. | SLU_3 | Min | -1094.053 | -188.732 | 0. |
| 2 | 0.68666 | SLU_3 | Min | -1091.129 | -271.98 | 0. |
| 2 | 1.37332 | SLU_3 | Min | -1088.205 | -355.227 | 0. |
| 2 | 0. | SLU_4 | Max | -957.023 | -189.109 | 0. |
| 2 | 0.68666 | SLU_4 | Max | -954.099 | -272.357 | 0. |
| 2 | 1.37332 | SLU_4 | Max | -951.175 | -355.604 | 0. |
| 2 | 0. | SLU_4 | Min | -957.023 | -189.109 | 0. |
| 2 | 0.68666 | SLU_4 | Min | -954.099 | -272.357 | 0. |
| 2 | 1.37332 | SLU_4 | Min | -951.175 | -355.604 | 0. |
| 2 | 0. | SLE_F1 | Max | -790.074 | -114.541 | 0. |
| 2 | 0.68666 | SLE_F1 | Max | -787.825 | -178.578 | 0. |
| 2 | 1.37332 | SLE_F1 | Max | -785.576 | -242.614 | 0. |
| 2 | 0. | SLE_F1 | Min | -790.074 | -114.541 | 0. |
| 2 | 0.68666 | SLE_F1 | Min | -787.825 | -178.578 | 0. |
| 2 | 1.37332 | SLE_F1 | Min | -785.576 | -242.614 | 0. |
| 2 | 0. | SLE_F2 | Max | -717.487 | -122.619 | 0. |
| 2 | 0.68666 | SLE_F2 | Max | -715.238 | -186.656 | 0. |
| 2 | 1.37332 | SLE_F2 | Max | -712.989 | -250.692 | 0. |
| 2 | 0. | SLE_F2 | Min | -717.487 | -122.619 | 0. |
| 2 | 0.68666 | SLE_F2 | Min | -715.238 | -186.656 | 0. |
| 2 | 1.37332 | SLE_F2 | Min | -712.989 | -250.692 | 0. |
| 2 | 0. | SLE_F3 | Max | -739.905 | -145.863 | 0. |
| 2 | 0.68666 | SLE_F3 | Max | -737.656 | -209.9 | 0. |
| 2 | 1.37332 | SLE_F3 | Max | -735.407 | -273.936 | 0. |
| 2 | 0. | SLE_F3 | Min | -739.905 | -145.863 | 0. |
| 2 | 0.68666 | SLE_F3 | Min | -737.656 | -209.9 | 0. |
| 2 | 1.37332 | SLE_F3 | Min | -735.407 | -273.936 | 0. |
| 2 | 0. | SLE_F4 | Max | -849.643 | -144.46 | 0. |
| 2 | 0.68666 | SLE_F4 | Max | -847.394 | -208.497 | 0. |
| 2 | 1.37332 | SLE_F4 | Max | -845.145 | -272.533 | 0. |
| 2 | 0. | SLE_F4 | Min | -849.643 | -144.46 | 0. |
| 2 | 0.68666 | SLE_F4 | Min | -847.394 | -208.497 | 0. |
| 2 | 1.37332 | SLE_F4 | Min | -845.145 | -272.533 | 0. |
| 2 | 0. | SLE_QP1 | Max | -795.221 | -114.086 | 0. |
| 2 | 0.68666 | SLE_QP1 | Max | -792.971 | -178.123 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 2 | 1.37332 | SLE_QP1 | Max | -790.722 | -242.159 | 0. |
| 2 | 0. | SLE_QP1 | Min | -795.221 | -114.086 | 0. |
| 2 | 0.68666 | SLE_QP1 | Min | -792.971 | -178.123 | 0. |
| 2 | 1.37332 | SLE_QP1 | Min | -790.722 | -242.159 | 0. |
| 2 | 0. | SLE_QP2 | Max | -725.669 | -121.866 | 0. |
| 2 | 0.68666 | SLE_QP2 | Max | -723.42 | -185.902 | 0. |
| 2 | 1.37332 | SLE_QP2 | Max | -721.171 | -249.939 | 0. |
| 2 | 0. | SLE_QP2 | Min | -725.669 | -121.866 | 0. |
| 2 | 0.68666 | SLE_QP2 | Min | -723.42 | -185.902 | 0. |
| 2 | 1.37332 | SLE_QP2 | Min | -721.171 | -249.939 | 0. |
| 2 | 0. | SLE_QP3 | Max | -746.839 | -146.596 | 0. |
| 2 | 0.68666 | SLE_QP3 | Max | -744.59 | -210.633 | 0. |
| 2 | 1.37332 | SLE_QP3 | Max | -742.34 | -274.669 | 0. |
| 2 | 0. | SLE_QP3 | Min | -746.839 | -146.596 | 0. |
| 2 | 0.68666 | SLE_QP3 | Min | -744.59 | -210.633 | 0. |
| 2 | 1.37332 | SLE_QP3 | Min | -742.34 | -274.669 | 0. |
| 2 | 0. | SLE_QP4 | Max | -865.853 | -142.974 | 0. |
| 2 | 0.68666 | SLE_QP4 | Max | -863.604 | -207.011 | 0. |
| 2 | 1.37332 | SLE_QP4 | Max | -861.355 | -271.047 | 0. |
| 2 | 0. | SLE_QP4 | Min | -865.853 | -142.974 | 0. |
| 2 | 0.68666 | SLE_QP4 | Min | -863.604 | -207.011 | 0. |
| 2 | 1.37332 | SLE_QP4 | Min | -861.355 | -271.047 | 0. |
| 2 | 0. | SLV_1 | Max | -1535.628 | -122.241 | 0. |
| 2 | 0.68666 | SLV_1 | Max | -1485.778 | -191.508 | 0. |
| 2 | 1.37332 | SLV_1 | Max | -1435.927 | -260.775 | 0. |
| 2 | 0. | SLV_1 | Min | -1535.628 | -122.241 | 0. |
| 2 | 0.68666 | SLV_1 | Min | -1485.778 | -191.508 | 0. |
| 2 | 1.37332 | SLV_1 | Min | -1435.927 | -260.775 | 0. |
| 2 | 0. | SLV_2 | Max | -1537.215 | -122.374 | 0. |
| 2 | 0.68666 | SLV_2 | Max | -1487.365 | -191.641 | 0. |
| 2 | 1.37332 | SLV_2 | Max | -1437.514 | -260.908 | 0. |
| 2 | 0. | SLV_2 | Min | -1537.215 | -122.374 | 0. |
| 2 | 0.68666 | SLV_2 | Min | -1487.365 | -191.641 | 0. |
| 2 | 1.37332 | SLV_2 | Min | -1437.514 | -260.908 | 0. |
| 2 | 0. | SLV_3 | Max | -1714.33 | -164.103 | 0. |
| 2 | 0.68666 | SLV_3 | Max | -1664.48 | -233.37 | 0. |
| 2 | 1.37332 | SLV_3 | Max | -1614.629 | -302.637 | 0. |
| 2 | 0. | SLV_3 | Min | -1714.33 | -164.103 | 0. |
| 2 | 0.68666 | SLV_3 | Min | -1664.48 | -233.37 | 0. |
| 2 | 1.37332 | SLV_3 | Min | -1614.629 | -302.637 | 0. |
| 2 | 0. | SLV_4 | Max | -1715.766 | -164.137 | 0. |
| 2 | 0.68666 | SLV_4 | Max | -1665.916 | -233.404 | 0. |
| 2 | 1.37332 | SLV_4 | Max | -1616.066 | -302.671 | 0. |
| 2 | 0. | SLV_4 | Min | -1715.766 | -164.137 | 0. |
| 2 | 0.68666 | SLV_4 | Min | -1665.916 | -233.404 | 0. |
| 2 | 1.37332 | SLV_4 | Min | -1616.066 | -302.671 | 0. |
| 2 | 0. | SLD_1 | Max | -1059.776 | -115.088 | 0. |
| 2 | 0.68666 | SLD_1 | Max | -1036.504 | -181.435 | 0. |
| 2 | 1.37332 | SLD_1 | Max | -1013.232 | -247.782 | 0. |
| 2 | 0. | SLD_1 | Min | -1059.776 | -115.088 | 0. |
| 2 | 0.68666 | SLD_1 | Min | -1036.504 | -181.435 | 0. |
| 2 | 1.37332 | SLD_1 | Min | -1013.232 | -247.782 | 0. |
| 2 | 0. | SLD_2 | Max | -1060.63 | -115.835 | 0. |
| 2 | 0.68666 | SLD_2 | Max | -1037.358 | -182.182 | 0. |
| 2 | 1.37332 | SLD_2 | Max | -1014.086 | -248.528 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 2 | 0. | SLD_2 | Min | -1060.63 | -115.835 | 0. |
| 2 | 0.68666 | SLD_2 | Min | -1037.358 | -182.182 | 0. |
| 2 | 1.37332 | SLD_2 | Min | -1014.086 | -248.528 | 0. |
| 2 | 0. | SLD_3 | Max | -1240.665 | -143.551 | 0. |
| 2 | 0.68666 | SLD_3 | Max | -1217.393 | -209.898 | 0. |
| 2 | 1.37332 | SLD_3 | Max | -1194.121 | -276.245 | 0. |
| 2 | 0. | SLD_3 | Min | -1240.665 | -143.551 | 0. |
| 2 | 0.68666 | SLD_3 | Min | -1217.393 | -209.898 | 0. |
| 2 | 1.37332 | SLD_3 | Min | -1194.121 | -276.245 | 0. |
| 2 | 0. | SLD_4 | Max | -1241.207 | -143.704 | 0. |
| 2 | 0.68666 | SLD_4 | Max | -1217.935 | -210.051 | 0. |
| 2 | 1.37332 | SLD_4 | Max | -1194.663 | -276.397 | 0. |
| 2 | 0. | SLD_4 | Min | -1241.207 | -143.704 | 0. |
| 2 | 0.68666 | SLD_4 | Min | -1217.935 | -210.051 | 0. |
| 2 | 1.37332 | SLD_4 | Min | -1194.663 | -276.397 | 0. |
| 2 | 0. | SLU_IDR_1 | Max | -818.837 | -169.526 | 0. |
| 2 | 0.68666 | SLU_IDR_1 | Max | -816.813 | -244.06 | 0. |
| 2 | 1.37332 | SLU_IDR_1 | Max | -814.789 | -318.594 | 0. |
| 2 | 0. | SLU_IDR_1 | Min | -818.837 | -169.526 | 0. |
| 2 | 0.68666 | SLU_IDR_1 | Min | -816.813 | -244.06 | 0. |
| 2 | 1.37332 | SLU_IDR_1 | Min | -814.789 | -318.594 | 0. |
| 2 | 0. | SLU_IDR_2 | Max | -805.667 | -144.782 | 0. |
| 2 | 0.68666 | SLU_IDR_2 | Max | -803.642 | -219.316 | 0. |
| 2 | 1.37332 | SLU_IDR_2 | Max | -801.618 | -293.85 | 0. |
| 2 | 0. | SLU_IDR_2 | Min | -805.667 | -144.782 | 0. |
| 2 | 0.68666 | SLU_IDR_2 | Min | -803.642 | -219.316 | 0. |
| 2 | 1.37332 | SLU_IDR_2 | Min | -801.618 | -293.85 | 0. |
| 2 | 0. | SISMA WOOD SLV-1 | Max | -757.692 | 55.226 | 0. |
| 2 | 0.68666 | SISMA WOOD SLV-1 | Max | -710.091 | 49.995 | 0. |
| 2 | 1.37332 | SISMA WOOD SLV-1 | Max | -662.49 | 44.765 | 0. |
| 2 | 0. | SISMA WOOD SLV-1 | Min | -757.692 | 55.226 | 0. |
| 2 | 0.68666 | SISMA WOOD SLV-1 | Min | -710.091 | 49.995 | 0. |
| 2 | 1.37332 | SISMA WOOD SLV-1 | Min | -662.49 | 44.765 | 0. |
| 2 | 0. | DEAD-1 | Max | 21.547 | -12.513 | 0. |
| 2 | 0.68666 | DEAD-1 | Max | 23.796 | 7.957 | 0. |
| 2 | 1.37332 | DEAD-1 | Max | 26.045 | 28.428 | 0. |
| 2 | 0. | DEAD-1 | Min | 21.547 | -12.513 | 0. |
| 2 | 0.68666 | DEAD-1 | Min | 23.796 | 7.957 | 0. |
| 2 | 1.37332 | DEAD-1 | Min | 26.045 | 28.428 | 0. |
| 2 | 0. | SLU_PROVA | | -1019.686 | -103.887 | 0. |
| 2 | 0.68666 | SLU_PROVA | | -1016.762 | -187.134 | 0. |
| 2 | 1.37332 | SLU_PROVA | | -1013.838 | -270.382 | 0. |
| 3 | 0. | DEAD | | 21.604 | -5.722 | 0. |
| 3 | 0.68801 | DEAD | | 24.603 | 14.693 | 0. |
| 3 | 1.37601 | DEAD | | 27.602 | 35.108 | 0. |
| 3 | 0. | SIMM_KA | | -147.568 | -6.996 | 0. |
| 3 | 0.68801 | SIMM_KA | | -147.568 | -6.996 | 0. |
| 3 | 1.37601 | SIMM_KA | | -147.568 | -6.996 | 0. |
| 3 | 0. | SIMM_K0 | | -222.698 | -11.004 | 0. |
| 3 | 0.68801 | SIMM_K0 | | -222.698 | -11.004 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 3 | 1.37601 | SIMM_K0 | | -222.698 | -11.004 | 0. |
| 3 | 0. | A--SIMM_KA | | -183.775 | -23.167 | 0. |
| 3 | 0.68801 | A--SIMM_KA | | -183.775 | -23.167 | 0. |
| 3 | 1.37601 | A--SIMM_KA | | -183.775 | -23.167 | 0. |
| 3 | 0. | A--SIMM_K0 | | -283.11 | -34.82 | 0. |
| 3 | 0.68801 | A--SIMM_K0 | | -283.11 | -34.82 | 0. |
| 3 | 1.37601 | A--SIMM_K0 | | -283.11 | -34.82 | 0. |
| 3 | 0. | A-- SIMM_SOVR_K A | | -8.885 | -1.875 | 0. |
| 3 | 0.68801 | A-- SIMM_SOVR_K A | | -8.885 | -1.875 | 0. |
| 3 | 1.37601 | A-- SIMM_SOVR_K A | | -8.885 | -1.875 | 0. |
| 3 | 0. | A-- SIMM_SOVR_K 0 | | -13.321 | -2.811 | 0. |
| 3 | 0.68801 | A-- SIMM_SOVR_K 0 | | -13.321 | -2.811 | 0. |
| 3 | 1.37601 | A-- SIMM_SOVR_K 0 | | -13.321 | -2.811 | 0. |
| 3 | 0. | SIMM_SOVR_K 0 | | -13.321 | -2.811 | 0. |
| 3 | 0.68801 | SIMM_SOVR_K 0 | | -13.321 | -2.811 | 0. |
| 3 | 1.37601 | SIMM_SOVR_K 0 | | -13.321 | -2.811 | 0. |
| 3 | 0. | SIMM_SOVR_K A | | -8.885 | -1.875 | 0. |
| 3 | 0.68801 | SIMM_SOVR_K A | | -8.885 | -1.875 | 0. |
| 3 | 1.37601 | SIMM_SOVR_K A | | -8.885 | -1.875 | 0. |
| 3 | 0. | SOVR | | 7.957 | -11.143 | 0. |
| 3 | 0.68801 | SOVR | | 7.957 | -11.143 | 0. |
| 3 | 1.37601 | SOVR | | 7.957 | -11.143 | 0. |
| 3 | 0. | TERR_SIMM | | 7.935 | -49.153 | 0. |
| 3 | 0.68801 | TERR_SIMM | | 7.935 | -49.153 | 0. |
| 3 | 1.37601 | TERR_SIMM | | 7.935 | -49.153 | 0. |
| 3 | 0. | TERR_A--SIMM | | 12.918 | -66.821 | 0. |
| 3 | 0.68801 | TERR_A--SIMM | | 12.918 | -66.821 | 0. |
| 3 | 1.37601 | TERR_A--SIMM | | 12.918 | -66.821 | 0. |
| 3 | 0. | INERZIA H SLV | | 3.859 | -0.374 | 0. |
| 3 | 0.68801 | INERZIA H SLV | | 3.859 | -0.374 | 0. |
| 3 | 1.37601 | INERZIA H SLV | | 3.859 | -0.374 | 0. |
| 3 | 0. | INERZIA V + SLV | | 0.377 | 0.24 | 0. |
| 3 | 0.68801 | INERZIA V + SLV | | 0.377 | 0.24 | 0. |
| 3 | 1.37601 | INERZIA V + SLV | | 0.377 | 0.24 | 0. |
| 3 | 0. | INERZIA V - SLV | | -0.377 | -0.24 | 0. |
| 3 | 0.68801 | INERZIA V - SLV | | -0.377 | -0.24 | 0. |
| 3 | 1.37601 | INERZIA V - SLV | | -0.377 | -0.24 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 3 | 0. | SISMA WOOD SLV | | -169.105 | -13.838 | 0. |
| 3 | 0.68801 | SISMA WOOD SLV | | -121.633 | -20.812 | 0. |
| 3 | 1.37601 | SISMA WOOD SLV | | -74.161 | -27.786 | 0. |
| 3 | 0. | iDROSTATICA | | -587.626 | -99.902 | 0. |
| 3 | 0.68801 | iDROSTATICA | | -587.626 | -184.575 | 0. |
| 3 | 1.37601 | iDROSTATICA | | -587.626 | -269.248 | 0. |
| 3 | 0. | SISMA WOOD SLD | | -74.684 | -6.112 | 0. |
| 3 | 0.68801 | SISMA WOOD SLD | | -53.718 | -9.192 | 0. |
| 3 | 1.37601 | SISMA WOOD SLD | | -32.752 | -12.272 | 0. |
| 3 | 0. | INERZIA H SLD | | 1.705 | -0.165 | 0. |
| 3 | 0.68801 | INERZIA H SLD | | 1.705 | -0.165 | 0. |
| 3 | 1.37601 | INERZIA H SLD | | 1.705 | -0.165 | 0. |
| 3 | 0. | INERZIA V + SLD | | 0.167 | 0.106 | 0. |
| 3 | 0.68801 | INERZIA V + SLD | | 0.167 | 0.106 | 0. |
| 3 | 1.37601 | INERZIA V + SLD | | 0.167 | 0.106 | 0. |
| 3 | 0. | INERZIA V SLD | | -0.167 | -0.106 | 0. |
| 3 | 0.68801 | INERZIA V SLD | | -0.167 | -0.106 | 0. |
| 3 | 1.37601 | INERZIA V SLD | | -0.167 | -0.106 | 0. |
| 3 | 0. | INERZIA V -1 | | -0.377 | -0.24 | 0. |
| 3 | 0.68801 | INERZIA V -1 | | -0.377 | -0.24 | 0. |
| 3 | 1.37601 | INERZIA V -1 | | -0.377 | -0.24 | 0. |
| 3 | 0. | SLU_1 | Max | -1029.779 | -279.398 | 0. |
| 3 | 0.68801 | SLU_1 | Max | -1025.88 | -362.933 | 0. |
| 3 | 1.37601 | SLU_1 | Max | -1021.981 | -446.469 | 0. |
| 3 | 0. | SLU_1 | Min | -1029.779 | -279.398 | 0. |
| 3 | 0.68801 | SLU_1 | Min | -1025.88 | -362.933 | 0. |
| 3 | 1.37601 | SLU_1 | Min | -1021.981 | -446.469 | 0. |
| 3 | 0. | SLU_2 | Max | -932.435 | -292.663 | 0. |
| 3 | 0.68801 | SLU_2 | Max | -928.537 | -376.198 | 0. |
| 3 | 1.37601 | SLU_2 | Max | -924.638 | -459.733 | 0. |
| 3 | 0. | SLU_2 | Min | -932.435 | -292.663 | 0. |
| 3 | 0.68801 | SLU_2 | Min | -928.537 | -376.198 | 0. |
| 3 | 1.37601 | SLU_2 | Min | -924.638 | -459.733 | 0. |
| 3 | 0. | SLU_3 | Max | -1100.92 | -342.248 | 0. |
| 3 | 0.68801 | SLU_3 | Max | -1097.021 | -425.783 | 0. |
| 3 | 1.37601 | SLU_3 | Max | -1093.122 | -509.318 | 0. |
| 3 | 0. | SLU_3 | Min | -1100.92 | -342.248 | 0. |
| 3 | 0.68801 | SLU_3 | Min | -1097.021 | -425.783 | 0. |
| 3 | 1.37601 | SLU_3 | Min | -1093.122 | -509.318 | 0. |
| 3 | 0. | SLU_4 | Max | -963.75 | -334.394 | 0. |
| 3 | 0.68801 | SLU_4 | Max | -959.851 | -417.929 | 0. |
| 3 | 1.37601 | SLU_4 | Max | -955.952 | -501.465 | 0. |
| 3 | 0. | SLU_4 | Min | -963.75 | -334.394 | 0. |
| 3 | 0.68801 | SLU_4 | Min | -959.851 | -417.929 | 0. |
| 3 | 1.37601 | SLU_4 | Min | -955.952 | -501.465 | 0. |
| 3 | 0. | SLE_F1 | Max | -793.889 | -213.846 | 0. |
| 3 | 0.68801 | SLE_F1 | Max | -790.89 | -278.104 | 0. |
| 3 | 1.37601 | SLE_F1 | Max | -787.891 | -342.362 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 3 | 0. | SLE_F1 | Min | -793.889 | -213.846 | 0. |
| 3 | 0.68801 | SLE_F1 | Min | -790.89 | -278.104 | 0. |
| 3 | 1.37601 | SLE_F1 | Min | -787.891 | -342.362 | 0. |
| 3 | 0. | SLE_F2 | Max | -721.644 | -224.559 | 0. |
| 3 | 0.68801 | SLE_F2 | Max | -718.645 | -288.817 | 0. |
| 3 | 1.37601 | SLE_F2 | Max | -715.646 | -353.075 | 0. |
| 3 | 0. | SLE_F2 | Min | -721.644 | -224.559 | 0. |
| 3 | 0.68801 | SLE_F2 | Min | -718.645 | -288.817 | 0. |
| 3 | 1.37601 | SLE_F2 | Min | -715.646 | -353.075 | 0. |
| 3 | 0. | SLE_F3 | Max | -745.032 | -254.242 | 0. |
| 3 | 0.68801 | SLE_F3 | Max | -742.033 | -318.5 | 0. |
| 3 | 1.37601 | SLE_F3 | Max | -739.034 | -382.758 | 0. |
| 3 | 0. | SLE_F3 | Min | -745.032 | -254.242 | 0. |
| 3 | 0.68801 | SLE_F3 | Min | -742.033 | -318.5 | 0. |
| 3 | 1.37601 | SLE_F3 | Min | -739.034 | -382.758 | 0. |
| 3 | 0. | SLE_F4 | Max | -854.839 | -259.211 | 0. |
| 3 | 0.68801 | SLE_F4 | Max | -851.84 | -323.469 | 0. |
| 3 | 1.37601 | SLE_F4 | Max | -848.841 | -387.727 | 0. |
| 3 | 0. | SLE_F4 | Min | -854.839 | -259.211 | 0. |
| 3 | 0.68801 | SLE_F4 | Min | -851.84 | -323.469 | 0. |
| 3 | 1.37601 | SLE_F4 | Min | -848.841 | -387.727 | 0. |
| 3 | 0. | SLE_QP1 | Max | -799.015 | -213.201 | 0. |
| 3 | 0.68801 | SLE_QP1 | Max | -796.016 | -277.459 | 0. |
| 3 | 1.37601 | SLE_QP1 | Max | -793.017 | -341.717 | 0. |
| 3 | 0. | SLE_QP1 | Min | -799.015 | -213.201 | 0. |
| 3 | 0.68801 | SLE_QP1 | Min | -796.016 | -277.459 | 0. |
| 3 | 1.37601 | SLE_QP1 | Min | -793.017 | -341.717 | 0. |
| 3 | 0. | SLE_QP2 | Max | -729.793 | -223.507 | 0. |
| 3 | 0.68801 | SLE_QP2 | Max | -726.794 | -287.765 | 0. |
| 3 | 1.37601 | SLE_QP2 | Max | -723.795 | -352.023 | 0. |
| 3 | 0. | SLE_QP2 | Min | -729.793 | -223.507 | 0. |
| 3 | 0.68801 | SLE_QP2 | Min | -726.794 | -287.765 | 0. |
| 3 | 1.37601 | SLE_QP2 | Min | -723.795 | -352.023 | 0. |
| 3 | 0. | SLE_QP3 | Max | -751.878 | -248.699 | 0. |
| 3 | 0.68801 | SLE_QP3 | Max | -748.879 | -312.957 | 0. |
| 3 | 1.37601 | SLE_QP3 | Max | -745.88 | -377.215 | 0. |
| 3 | 0. | SLE_QP3 | Min | -751.878 | -248.699 | 0. |
| 3 | 0.68801 | SLE_QP3 | Min | -748.879 | -312.957 | 0. |
| 3 | 1.37601 | SLE_QP3 | Min | -745.88 | -377.215 | 0. |
| 3 | 0. | SLE_QP4 | Max | -870.883 | -251.516 | 0. |
| 3 | 0.68801 | SLE_QP4 | Max | -867.884 | -315.774 | 0. |
| 3 | 1.37601 | SLE_QP4 | Max | -864.885 | -380.032 | 0. |
| 3 | 0. | SLE_QP4 | Min | -870.883 | -251.516 | 0. |
| 3 | 0.68801 | SLE_QP4 | Min | -867.884 | -315.774 | 0. |
| 3 | 1.37601 | SLE_QP4 | Min | -864.885 | -380.032 | 0. |
| 3 | 0. | SLV_1 | Max | -1443.333 | -219.002 | 0. |
| 3 | 0.68801 | SLV_1 | Max | -1392.862 | -290.234 | 0. |
| 3 | 1.37601 | SLV_1 | Max | -1342.39 | -361.466 | 0. |
| 3 | 0. | SLV_1 | Min | -1443.333 | -219.002 | 0. |
| 3 | 0.68801 | SLV_1 | Min | -1392.862 | -290.234 | 0. |
| 3 | 1.37601 | SLV_1 | Min | -1342.39 | -361.466 | 0. |
| 3 | 0. | SLV_2 | Max | -1445.092 | -219.022 | 0. |
| 3 | 0.68801 | SLV_2 | Max | -1394.621 | -290.254 | 0. |
| 3 | 1.37601 | SLV_2 | Max | -1344.15 | -361.486 | 0. |
| 3 | 0. | SLV_2 | Min | -1445.092 | -219.022 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 3 | 0.68801 | SLV_2 | Min | -1394.621 | -290.254 | 0. |
| 3 | 1.37601 | SLV_2 | Min | -1344.15 | -361.486 | 0. |
| 3 | 0. | SLV_3 | Max | -1623.847 | -275.626 | 0. |
| 3 | 0.68801 | SLV_3 | Max | -1573.376 | -346.858 | 0. |
| 3 | 1.37601 | SLV_3 | Max | -1522.905 | -418.09 | 0. |
| 3 | 0. | SLV_3 | Min | -1623.847 | -275.626 | 0. |
| 3 | 0.68801 | SLV_3 | Min | -1573.376 | -346.858 | 0. |
| 3 | 1.37601 | SLV_3 | Min | -1522.905 | -418.09 | 0. |
| 3 | 0. | SLV_4 | Max | -1625.455 | -275.703 | 0. |
| 3 | 0.68801 | SLV_4 | Max | -1574.984 | -346.935 | 0. |
| 3 | 1.37601 | SLV_4 | Max | -1524.513 | -418.167 | 0. |
| 3 | 0. | SLV_4 | Min | -1625.455 | -275.703 | 0. |
| 3 | 0.68801 | SLV_4 | Min | -1574.984 | -346.935 | 0. |
| 3 | 1.37601 | SLV_4 | Min | -1524.513 | -418.167 | 0. |
| 3 | 0. | SLD_1 | Max | -1020.992 | -211.471 | 0. |
| 3 | 0.68801 | SLD_1 | Max | -997.028 | -278.809 | 0. |
| 3 | 1.37601 | SLD_1 | Max | -973.063 | -346.147 | 0. |
| 3 | 0. | SLD_1 | Min | -1020.992 | -211.471 | 0. |
| 3 | 0.68801 | SLD_1 | Min | -997.028 | -278.809 | 0. |
| 3 | 1.37601 | SLD_1 | Min | -973.063 | -346.147 | 0. |
| 3 | 0. | SLD_2 | Max | -1021.945 | -212.413 | 0. |
| 3 | 0.68801 | SLD_2 | Max | -997.981 | -279.751 | 0. |
| 3 | 1.37601 | SLD_2 | Max | -974.016 | -347.089 | 0. |
| 3 | 0. | SLD_2 | Min | -1021.945 | -212.413 | 0. |
| 3 | 0.68801 | SLD_2 | Min | -997.981 | -279.751 | 0. |
| 3 | 1.37601 | SLD_2 | Min | -974.016 | -347.089 | 0. |
| 3 | 0. | SLD_3 | Max | -1203.254 | -256.662 | 0. |
| 3 | 0.68801 | SLD_3 | Max | -1179.289 | -324. | 0. |
| 3 | 1.37601 | SLD_3 | Max | -1155.324 | -391.338 | 0. |
| 3 | 0. | SLD_3 | Min | -1203.254 | -256.662 | 0. |
| 3 | 0.68801 | SLD_3 | Min | -1179.289 | -324. | 0. |
| 3 | 1.37601 | SLD_3 | Min | -1155.324 | -391.338 | 0. |
| 3 | 0. | SLD_4 | Max | -1203.876 | -256.841 | 0. |
| 3 | 0.68801 | SLD_4 | Max | -1179.911 | -324.179 | 0. |
| 3 | 1.37601 | SLD_4 | Max | -1155.947 | -391.517 | 0. |
| 3 | 0. | SLD_4 | Min | -1203.876 | -256.841 | 0. |
| 3 | 0.68801 | SLD_4 | Min | -1179.911 | -324.179 | 0. |
| 3 | 1.37601 | SLD_4 | Min | -1155.947 | -391.517 | 0. |
| 3 | 0. | SLU_IDR_1 | Max | -825.849 | -288.707 | 0. |
| 3 | 0.68801 | SLU_IDR_1 | Max | -823.15 | -363.473 | 0. |
| 3 | 1.37601 | SLU_IDR_1 | Max | -820.451 | -438.24 | 0. |
| 3 | 0. | SLU_IDR_1 | Min | -825.849 | -288.707 | 0. |
| 3 | 0.68801 | SLU_IDR_1 | Min | -823.15 | -363.473 | 0. |
| 3 | 1.37601 | SLU_IDR_1 | Min | -820.451 | -438.24 | 0. |
| 3 | 0. | SLU_IDR_2 | Max | -811.786 | -264.454 | 0. |
| 3 | 0.68801 | SLU_IDR_2 | Max | -809.087 | -339.221 | 0. |
| 3 | 1.37601 | SLU_IDR_2 | Max | -806.388 | -413.988 | 0. |
| 3 | 0. | SLU_IDR_2 | Min | -811.786 | -264.454 | 0. |
| 3 | 0.68801 | SLU_IDR_2 | Min | -809.087 | -339.221 | 0. |
| 3 | 1.37601 | SLU_IDR_2 | Min | -806.388 | -413.988 | 0. |
| 3 | 0. | SISMA WOOD SLV-1 | Max | -660.421 | 68.858 | 0. |
| 3 | 0.68801 | SISMA WOOD SLV-1 | Max | -612.949 | 61.884 | 0. |
| 3 | 1.37601 | SISMA WOOD SLV-1 | Max | -565.477 | 54.91 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|-----------|----------|
| 3 | 0. | SISMA WOOD SLV-1 | Min | -660.421 | 68.858 | 0. |
| 3 | 0.68801 | SISMA WOOD SLV-1 | Min | -612.949 | 61.884 | 0. |
| 3 | 1.37601 | SISMA WOOD SLV-1 | Min | -565.477 | 54.91 | 0. |
| 3 | 0. | DEAD-1 | Max | 26.4 | -8.936 | 0. |
| 3 | 0.68801 | DEAD-1 | Max | 29.399 | 11.479 | 0. |
| 3 | 1.37601 | DEAD-1 | Max | 32.398 | 31.894 | 0. |
| 3 | 0. | DEAD-1 | Min | 26.4 | -8.936 | 0. |
| 3 | 0.68801 | DEAD-1 | Min | 29.399 | 11.479 | 0. |
| 3 | 1.37601 | DEAD-1 | Min | 32.398 | 31.894 | 0. |
| 3 | 0. | SLU_PROVA | | -1023.067 | -236.447 | 0. |
| 3 | 0.68801 | SLU_PROVA | | -1019.168 | -319.982 | 0. |
| 3 | 1.37601 | SLU_PROVA | | -1015.27 | -403.517 | 0. |
| 4 | 0. | DEAD | | 53.687 | 4.868 | 0. |
| 4 | 0.31251 | DEAD | | 57.914 | 13.233 | 0. |
| 4 | 0.62502 | DEAD | | 62.142 | 21.598 | 0. |
| 4 | 0. | SIMM_KA | | -144.282 | 32.483 | 0. |
| 4 | 0.31251 | SIMM_KA | | -144.282 | 32.483 | 0. |
| 4 | 0.62502 | SIMM_KA | | -144.282 | 32.483 | 0. |
| 4 | 0. | SIMM_K0 | | -217.922 | 48.431 | 0. |
| 4 | 0.31251 | SIMM_K0 | | -217.922 | 48.431 | 0. |
| 4 | 0.62502 | SIMM_K0 | | -217.922 | 48.431 | 0. |
| 4 | 0. | A--SIMM_KA | | -182.788 | 37.125 | 0. |
| 4 | 0.31251 | A--SIMM_KA | | -182.788 | 37.125 | 0. |
| 4 | 0.62502 | A--SIMM_KA | | -182.788 | 37.125 | 0. |
| 4 | 0. | A--SIMM_K0 | | -281.445 | 57.066 | 0. |
| 4 | 0.31251 | A--SIMM_K0 | | -281.445 | 57.066 | 0. |
| 4 | 0.62502 | A--SIMM_K0 | | -281.445 | 57.066 | 0. |
| 4 | 0. | A-- SIMM_SOVR_K A | | -9.289 | 8.641E-03 | 0. |
| 4 | 0.31251 | A-- SIMM_SOVR_K A | | -9.289 | 8.641E-03 | 0. |
| 4 | 0.62502 | A-- SIMM_SOVR_K A | | -9.289 | 8.641E-03 | 0. |
| 4 | 0. | A-- SIMM_SOVR_K 0 | | -13.927 | 0.013 | 0. |
| 4 | 0.31251 | A-- SIMM_SOVR_K 0 | | -13.927 | 0.013 | 0. |
| 4 | 0.62502 | A-- SIMM_SOVR_K 0 | | -13.927 | 0.013 | 0. |
| 4 | 0. | SIMM_SOVR_K 0 | | -13.927 | 0.013 | 0. |
| 4 | 0.31251 | SIMM_SOVR_K 0 | | -13.927 | 0.013 | 0. |
| 4 | 0.62502 | SIMM_SOVR_K 0 | | -13.927 | 0.013 | 0. |
| 4 | 0. | SIMM_SOVR_K A | | -9.289 | 8.641E-03 | 0. |
| 4 | 0.31251 | SIMM_SOVR_K A | | -9.289 | 8.641E-03 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|-----------|----------|
| 4 | 0.62502 | SIMM_SOVR_K A | | -9.289 | 8.641E-03 | 0. |
| 4 | 0. | SOVR | | -0.238 | -36.652 | 0. |
| 4 | 0.31251 | SOVR | | -0.238 | -36.652 | 0. |
| 4 | 0.62502 | SOVR | | -0.238 | -36.652 | 0. |
| 4 | 0. | TERR_SIMM | | -25.663 | -145.497 | 0. |
| 4 | 0.31251 | TERR_SIMM | | -25.663 | -145.497 | 0. |
| 4 | 0.62502 | TERR_SIMM | | -25.663 | -145.497 | 0. |
| 4 | 0. | TERR_A--SIMM | | -37.029 | -220.432 | 0. |
| 4 | 0.31251 | TERR_A--SIMM | | -37.029 | -220.432 | 0. |
| 4 | 0.62502 | TERR_A--SIMM | | -37.029 | -220.432 | 0. |
| 4 | 0. | INERZIA H SLV | | 6.897 | -1.012 | 0. |
| 4 | 0.31251 | INERZIA H SLV | | 6.897 | -1.012 | 0. |
| 4 | 0.62502 | INERZIA H SLV | | 6.897 | -1.012 | 0. |
| 4 | 0. | INERZIA V + SLV | | 0.918 | 0.224 | 0. |
| 4 | 0.31251 | INERZIA V + SLV | | 0.918 | 0.224 | 0. |
| 4 | 0.62502 | INERZIA V + SLV | | 0.918 | 0.224 | 0. |
| 4 | 0. | INERZIA V - SLV | | -0.918 | -0.224 | 0. |
| 4 | 0.31251 | INERZIA V - SLV | | -0.918 | -0.224 | 0. |
| 4 | 0.62502 | INERZIA V - SLV | | -0.918 | -0.224 | 0. |
| 4 | 0. | SISMA WOOD SLV | | 85.533 | -14.29 | 0. |
| 4 | 0.31251 | SISMA WOOD SLV | | 104.984 | -24.121 | 0. |
| 4 | 0.62502 | SISMA WOOD SLV | | 124.435 | -33.952 | 0. |
| 4 | 0. | iDROSTATICA | | -674.834 | -260.743 | 0. |
| 4 | 0.31251 | iDROSTATICA | | -674.834 | -299.204 | 0. |
| 4 | 0.62502 | iDROSTATICA | | -674.834 | -337.664 | 0. |
| 4 | 0. | SISMA WOOD SLD | | 37.775 | -6.311 | 0. |
| 4 | 0.31251 | SISMA WOOD SLD | | 46.365 | -10.653 | 0. |
| 4 | 0.62502 | SISMA WOOD SLD | | 54.956 | -14.995 | 0. |
| 4 | 0. | INERZIA H SLD | | 3.046 | -0.447 | 0. |
| 4 | 0.31251 | INERZIA H SLD | | 3.046 | -0.447 | 0. |
| 4 | 0.62502 | INERZIA H SLD | | 3.046 | -0.447 | 0. |
| 4 | 0. | INERZIA V + SLD | | 0.405 | 0.099 | 0. |
| 4 | 0.31251 | INERZIA V + SLD | | 0.405 | 0.099 | 0. |
| 4 | 0.62502 | INERZIA V + SLD | | 0.405 | 0.099 | 0. |
| 4 | 0. | INERZIA V SLD | | -0.405 | -0.099 | 0. |
| 4 | 0.31251 | INERZIA V SLD | | -0.405 | -0.099 | 0. |
| 4 | 0.62502 | INERZIA V SLD | | -0.405 | -0.099 | 0. |
| 4 | 0. | INERZIA V -1 | | -0.918 | -0.224 | 0. |
| 4 | 0.31251 | INERZIA V -1 | | -0.918 | -0.224 | 0. |
| 4 | 0.62502 | INERZIA V -1 | | -0.918 | -0.224 | 0. |
| 4 | 0. | SLU_1 | Max | -1167.123 | -565.769 | 0. |
| 4 | 0.31251 | SLU_1 | Max | -1161.627 | -604.893 | 0. |
| 4 | 0.62502 | SLU_1 | Max | -1156.131 | -644.017 | 0. |
| 4 | 0. | SLU_1 | Min | -1167.123 | -565.769 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 4 | 0.31251 | SLU_1 | Min | -1161.627 | -604.893 | 0. |
| 4 | 0.62502 | SLU_1 | Min | -1156.131 | -644.017 | 0. |
| 4 | 0. | SLU_2 | Max | -1075.947 | -597.42 | 0. |
| 4 | 0.31251 | SLU_2 | Max | -1070.451 | -636.544 | 0. |
| 4 | 0.62502 | SLU_2 | Max | -1064.955 | -675.669 | 0. |
| 4 | 0. | SLU_2 | Min | -1075.947 | -597.42 | 0. |
| 4 | 0.31251 | SLU_2 | Min | -1070.451 | -636.544 | 0. |
| 4 | 0.62502 | SLU_2 | Min | -1064.955 | -675.669 | 0. |
| 4 | 0. | SLU_3 | Max | -1270.065 | -676.407 | 0. |
| 4 | 0.31251 | SLU_3 | Max | -1264.569 | -715.532 | 0. |
| 4 | 0.62502 | SLU_3 | Max | -1259.072 | -754.656 | 0. |
| 4 | 0. | SLU_3 | Min | -1270.065 | -676.407 | 0. |
| 4 | 0.31251 | SLU_3 | Min | -1264.569 | -715.532 | 0. |
| 4 | 0.62502 | SLU_3 | Min | -1259.072 | -754.656 | 0. |
| 4 | 0. | SLU_4 | Max | -1134.865 | -705.794 | 0. |
| 4 | 0.31251 | SLU_4 | Max | -1129.369 | -744.918 | 0. |
| 4 | 0.62502 | SLU_4 | Max | -1123.873 | -784.042 | 0. |
| 4 | 0. | SLU_4 | Min | -1134.865 | -705.794 | 0. |
| 4 | 0.31251 | SLU_4 | Min | -1129.369 | -744.918 | 0. |
| 4 | 0.62502 | SLU_4 | Min | -1123.873 | -784.042 | 0. |
| 4 | 0. | SLE_F1 | Max | -896.637 | -420.616 | 0. |
| 4 | 0.31251 | SLE_F1 | Max | -892.409 | -450.712 | 0. |
| 4 | 0.62502 | SLE_F1 | Max | -888.182 | -480.807 | 0. |
| 4 | 0. | SLE_F1 | Min | -896.637 | -420.616 | 0. |
| 4 | 0.31251 | SLE_F1 | Min | -892.409 | -450.712 | 0. |
| 4 | 0.62502 | SLE_F1 | Min | -888.182 | -480.807 | 0. |
| 4 | 0. | SLE_F2 | Max | -829.208 | -444.789 | 0. |
| 4 | 0.31251 | SLE_F2 | Max | -824.981 | -474.885 | 0. |
| 4 | 0.62502 | SLE_F2 | Max | -820.753 | -504.981 | 0. |
| 4 | 0. | SLE_F2 | Min | -829.208 | -444.789 | 0. |
| 4 | 0.31251 | SLE_F2 | Min | -824.981 | -474.885 | 0. |
| 4 | 0.62502 | SLE_F2 | Min | -820.753 | -504.981 | 0. |
| 4 | 0. | SLE_F3 | Max | -873.26 | -526.811 | 0. |
| 4 | 0.31251 | SLE_F3 | Max | -869.032 | -556.907 | 0. |
| 4 | 0.62502 | SLE_F3 | Max | -864.805 | -587.002 | 0. |
| 4 | 0. | SLE_F3 | Min | -873.26 | -526.811 | 0. |
| 4 | 0.31251 | SLE_F3 | Min | -869.032 | -556.907 | 0. |
| 4 | 0.62502 | SLE_F3 | Min | -864.805 | -587.002 | 0. |
| 4 | 0. | SLE_F4 | Max | -980.922 | -501.168 | 0. |
| 4 | 0.31251 | SLE_F4 | Max | -976.695 | -531.264 | 0. |
| 4 | 0.62502 | SLE_F4 | Max | -972.467 | -561.359 | 0. |
| 4 | 0. | SLE_F4 | Min | -980.922 | -501.168 | 0. |
| 4 | 0.31251 | SLE_F4 | Min | -976.695 | -531.264 | 0. |
| 4 | 0.62502 | SLE_F4 | Min | -972.467 | -561.359 | 0. |
| 4 | 0. | SLE_QP1 | Max | -896.606 | -393.799 | 0. |
| 4 | 0.31251 | SLE_QP1 | Max | -892.378 | -423.895 | 0. |
| 4 | 0.62502 | SLE_QP1 | Max | -888.15 | -453.99 | 0. |
| 4 | 0. | SLE_QP1 | Min | -896.606 | -393.799 | 0. |
| 4 | 0.31251 | SLE_QP1 | Min | -892.378 | -423.895 | 0. |
| 4 | 0.62502 | SLE_QP1 | Min | -888.15 | -453.99 | 0. |
| 4 | 0. | SLE_QP2 | Max | -832.103 | -417.368 | 0. |
| 4 | 0.31251 | SLE_QP2 | Max | -827.875 | -447.464 | 0. |
| 4 | 0.62502 | SLE_QP2 | Max | -823.647 | -477.56 | 0. |
| 4 | 0. | SLE_QP2 | Min | -832.103 | -417.368 | 0. |
| 4 | 0.31251 | SLE_QP2 | Min | -827.875 | -447.464 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 4 | 0.62502 | SLE_QP2 | Min | -823.647 | -477.56 | 0. |
| 4 | 0. | SLE_QP3 | Max | -873.793 | -496.898 | 0. |
| 4 | 0.31251 | SLE_QP3 | Max | -869.565 | -526.993 | 0. |
| 4 | 0.62502 | SLE_QP3 | Max | -865.337 | -557.089 | 0. |
| 4 | 0. | SLE_QP3 | Min | -873.793 | -496.898 | 0. |
| 4 | 0.31251 | SLE_QP3 | Min | -869.565 | -526.993 | 0. |
| 4 | 0.62502 | SLE_QP3 | Min | -865.337 | -557.089 | 0. |
| 4 | 0. | SLE_QP4 | Max | -989.362 | -464.977 | 0. |
| 4 | 0.31251 | SLE_QP4 | Max | -985.135 | -495.072 | 0. |
| 4 | 0.62502 | SLE_QP4 | Max | -980.907 | -525.168 | 0. |
| 4 | 0. | SLE_QP4 | Min | -989.362 | -464.977 | 0. |
| 4 | 0.31251 | SLE_QP4 | Min | -985.135 | -495.072 | 0. |
| 4 | 0.62502 | SLE_QP4 | Min | -980.907 | -525.168 | 0. |
| 4 | 0. | SLV_1 | Max | -1256.658 | -246.63 | 0. |
| 4 | 0.31251 | SLV_1 | Max | -1232.979 | -286.557 | 0. |
| 4 | 0.62502 | SLV_1 | Max | -1209.3 | -326.483 | 0. |
| 4 | 0. | SLV_1 | Min | -1256.658 | -246.63 | 0. |
| 4 | 0.31251 | SLV_1 | Min | -1232.979 | -286.557 | 0. |
| 4 | 0.62502 | SLV_1 | Min | -1209.3 | -326.483 | 0. |
| 4 | 0. | SLV_2 | Max | -1259.419 | -247.499 | 0. |
| 4 | 0.31251 | SLV_2 | Max | -1235.741 | -287.426 | 0. |
| 4 | 0.62502 | SLV_2 | Max | -1212.062 | -327.353 | 0. |
| 4 | 0. | SLV_2 | Min | -1259.419 | -247.499 | 0. |
| 4 | 0.31251 | SLV_2 | Min | -1235.741 | -287.426 | 0. |
| 4 | 0.62502 | SLV_2 | Min | -1212.062 | -327.353 | 0. |
| 4 | 0. | SLV_3 | Max | -1455.53 | -280.169 | 0. |
| 4 | 0.31251 | SLV_3 | Max | -1431.851 | -320.095 | 0. |
| 4 | 0.62502 | SLV_3 | Max | -1408.172 | -360.022 | 0. |
| 4 | 0. | SLV_3 | Min | -1455.53 | -280.169 | 0. |
| 4 | 0.31251 | SLV_3 | Min | -1431.851 | -320.095 | 0. |
| 4 | 0.62502 | SLV_3 | Min | -1408.172 | -360.022 | 0. |
| 4 | 0. | SLV_4 | Max | -1458.005 | -280.416 | 0. |
| 4 | 0.31251 | SLV_4 | Max | -1434.326 | -320.343 | 0. |
| 4 | 0.62502 | SLV_4 | Max | -1410.647 | -360.269 | 0. |
| 4 | 0. | SLV_4 | Min | -1458.005 | -280.416 | 0. |
| 4 | 0.31251 | SLV_4 | Min | -1434.326 | -320.343 | 0. |
| 4 | 0.62502 | SLV_4 | Min | -1410.647 | -360.269 | 0. |
| 4 | 0. | SLD_1 | Max | -996.106 | -344.053 | 0. |
| 4 | 0.31251 | SLD_1 | Max | -983.288 | -378.491 | 0. |
| 4 | 0.62502 | SLD_1 | Max | -970.47 | -412.928 | 0. |
| 4 | 0. | SLD_1 | Min | -996.106 | -344.053 | 0. |
| 4 | 0.31251 | SLD_1 | Min | -983.288 | -378.491 | 0. |
| 4 | 0.62502 | SLD_1 | Min | -970.47 | -412.928 | 0. |
| 4 | 0. | SLD_2 | Max | -997.656 | -344.373 | 0. |
| 4 | 0.31251 | SLD_2 | Max | -984.838 | -378.81 | 0. |
| 4 | 0.62502 | SLD_2 | Max | -972.02 | -413.247 | 0. |
| 4 | 0. | SLD_2 | Min | -997.656 | -344.373 | 0. |
| 4 | 0.31251 | SLD_2 | Min | -984.838 | -378.81 | 0. |
| 4 | 0.62502 | SLD_2 | Min | -972.02 | -413.247 | 0. |
| 4 | 0. | SLD_3 | Max | -1193.992 | -374.488 | 0. |
| 4 | 0.31251 | SLD_3 | Max | -1181.174 | -408.925 | 0. |
| 4 | 0.62502 | SLD_3 | Max | -1168.356 | -443.363 | 0. |
| 4 | 0. | SLD_3 | Min | -1193.992 | -374.488 | 0. |
| 4 | 0.31251 | SLD_3 | Min | -1181.174 | -408.925 | 0. |
| 4 | 0.62502 | SLD_3 | Min | -1168.356 | -443.363 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 4 | 0. | SLD_4 | Max | -1195.042 | -374.427 | 0. |
| 4 | 0.31251 | SLD_4 | Max | -1182.224 | -408.865 | 0. |
| 4 | 0.62502 | SLD_4 | Max | -1169.406 | -443.302 | 0. |
| 4 | 0. | SLD_4 | Min | -1195.042 | -374.427 | 0. |
| 4 | 0.31251 | SLD_4 | Min | -1182.224 | -408.865 | 0. |
| 4 | 0.62502 | SLD_4 | Min | -1169.406 | -443.302 | 0. |
| 4 | 0. | SLU_IDR_1 | Max | -962.141 | -516.886 | 0. |
| 4 | 0.31251 | SLU_IDR_1 | Max | -958.336 | -551.664 | 0. |
| 4 | 0.62502 | SLU_IDR_1 | Max | -954.531 | -586.442 | 0. |
| 4 | 0. | SLU_IDR_1 | Min | -962.141 | -516.886 | 0. |
| 4 | 0.31251 | SLU_IDR_1 | Min | -958.336 | -551.664 | 0. |
| 4 | 0.62502 | SLU_IDR_1 | Min | -954.531 | -586.442 | 0. |
| 4 | 0. | SLU_IDR_2 | Max | -933.585 | -455.364 | 0. |
| 4 | 0.31251 | SLU_IDR_2 | Max | -929.78 | -490.142 | 0. |
| 4 | 0.62502 | SLU_IDR_2 | Max | -925.975 | -524.92 | 0. |
| 4 | 0. | SLU_IDR_2 | Min | -933.585 | -455.364 | 0. |
| 4 | 0.31251 | SLU_IDR_2 | Min | -929.78 | -490.142 | 0. |
| 4 | 0.62502 | SLU_IDR_2 | Min | -925.975 | -524.92 | 0. |
| 4 | 0. | SISMA WOOD SLV-1 | Max | -363.986 | 152.747 | 0. |
| 4 | 0.31251 | SISMA WOOD SLV-1 | Max | -344.535 | 142.916 | 0. |
| 4 | 0.62502 | SISMA WOOD SLV-1 | Max | -325.084 | 133.085 | 0. |
| 4 | 0. | SISMA WOOD SLV-1 | Min | -363.986 | 152.747 | 0. |
| 4 | 0.31251 | SISMA WOOD SLV-1 | Min | -344.535 | 142.916 | 0. |
| 4 | 0.62502 | SISMA WOOD SLV-1 | Min | -325.084 | 133.085 | 0. |
| 4 | 0. | DEAD-1 | Max | 55.867 | -7.296 | 0. |
| 4 | 0.31251 | DEAD-1 | Max | 60.094 | 1.068 | 0. |
| 4 | 0.62502 | DEAD-1 | Max | 64.322 | 9.433 | 0. |
| 4 | 0. | DEAD-1 | Min | 55.867 | -7.296 | 0. |
| 4 | 0.31251 | DEAD-1 | Min | 60.094 | 1.068 | 0. |
| 4 | 0.62502 | DEAD-1 | Min | 64.322 | 9.433 | 0. |
| 4 | 0. | SLU_PROVA | | -1145.401 | -513.781 | 0. |
| 4 | 0.31251 | SLU_PROVA | | -1139.905 | -552.906 | 0. |
| 4 | 0.62502 | SLU_PROVA | | -1134.409 | -592.03 | 0. |
| 6 | 0. | DEAD | | -301.945 | -61.657 | 0. |
| 6 | 0.5 | DEAD | | -283.201 | -61.657 | 0. |
| 6 | 1. | DEAD | | -264.456 | -61.657 | 0. |
| 6 | 0. | SIMM_KA | | -12.661 | 86.754 | 0. |
| 6 | 0.5 | SIMM_KA | | -12.661 | 63.248 | 0. |
| 6 | 1. | SIMM_KA | | -12.661 | 41.439 | 0. |
| 6 | 0. | SIMM_K0 | | -19.338 | 132.128 | 0. |
| 6 | 0.5 | SIMM_K0 | | -19.338 | 96.868 | 0. |
| 6 | 1. | SIMM_K0 | | -19.338 | 64.158 | 0. |
| 6 | 0. | A--SIMM_KA | | 22.454 | 151.111 | 0. |
| 6 | 0.5 | A--SIMM_KA | | 22.454 | 114.378 | 0. |
| 6 | 1. | A--SIMM_KA | | 22.454 | 78.511 | 0. |
| 6 | 0. | A--SIMM_K0 | | 32.768 | 229.301 | 0. |
| 6 | 0.5 | A--SIMM_K0 | | 32.768 | 171.928 | 0. |
| 6 | 1. | A--SIMM_K0 | | 32.768 | 117.401 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 6 | 0. | A-- SIMM_SOVR_K A | | -1.65 | 11.645 | 0. |
| 6 | 0.5 | A-- SIMM_SOVR_K A | | -1.65 | 11.645 | 0. |
| 6 | 1. | A-- SIMM_SOVR_K A | | -1.65 | 11.645 | 0. |
| 6 | 0. | A-- SIMM_SOVR_K 0 | | -2.474 | 17.459 | 0. |
| 6 | 0.5 | A-- SIMM_SOVR_K 0 | | -2.474 | 17.459 | 0. |
| 6 | 1. | A-- SIMM_SOVR_K 0 | | -2.474 | 17.459 | 0. |
| 6 | 0. | SIMM_SOVR_K 0 | | -2.474 | 17.459 | 0. |
| 6 | 0.5 | SIMM_SOVR_K 0 | | -2.474 | 17.459 | 0. |
| 6 | 1. | SIMM_SOVR_K 0 | | -2.474 | 17.459 | 0. |
| 6 | 0. | SIMM_SOVR_K A | | -1.65 | 11.645 | 0. |
| 6 | 0.5 | SIMM_SOVR_K A | | -1.65 | 11.645 | 0. |
| 6 | 1. | SIMM_SOVR_K A | | -1.65 | 11.645 | 0. |
| 6 | 0. | SOVR | | -195.416 | -36.757 | 0. |
| 6 | 0.5 | SOVR | | -195.416 | -36.757 | 0. |
| 6 | 1. | SOVR | | -195.416 | -36.757 | 0. |
| 6 | 0. | TERR_SIMM | | -781.351 | -115.303 | 0. |
| 6 | 0.5 | TERR_SIMM | | -781.351 | -115.303 | 0. |
| 6 | 1. | TERR_SIMM | | -781.351 | -115.303 | 0. |
| 6 | 0. | TERR_A--SIMM | | -1243.062 | -160.603 | 0. |
| 6 | 0.5 | TERR_A--SIMM | | -1243.062 | -160.603 | 0. |
| 6 | 1. | TERR_A--SIMM | | -1243.062 | -160.603 | 0. |
| 6 | 0. | INERZIA H SLV | | 4.991 | 1.113 | 0. |
| 6 | 0.5 | INERZIA H SLV | | 4.991 | 1.113 | 0. |
| 6 | 1. | INERZIA H SLV | | 4.991 | 1.113 | 0. |
| 6 | 0. | INERZIA V + SLV | | -4.577 | -0.976 | 0. |
| 6 | 0.5 | INERZIA V + SLV | | -4.577 | -0.976 | 0. |
| 6 | 1. | INERZIA V + SLV | | -4.577 | -0.976 | 0. |
| 6 | 0. | INERZIA V - SLV | | 4.577 | 0.976 | 0. |
| 6 | 0.5 | INERZIA V - SLV | | 4.577 | 0.976 | 0. |
| 6 | 1. | INERZIA V - SLV | | 4.577 | 0.976 | 0. |
| 6 | 0. | SISMA WOOD SLV | | 191.868 | 151.77 | 0. |
| 6 | 0.5 | SISMA WOOD SLV | | 191.868 | 116.9 | 0. |
| 6 | 1. | SISMA WOOD SLV | | 191.868 | 82.03 | 0. |
| 6 | 0. | iDROSTATICA | | -362.043 | 231.096 | 0. |
| 6 | 0.5 | iDROSTATICA | | -362.043 | 180.246 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 6 | 1. | iDROSTATICA | | -362.043 | 134.496 | 0. |
| 6 | 0. | SISMA WOOD SLD | | 84.737 | 67.028 | 0. |
| 6 | 0.5 | SISMA WOOD SLD | | 84.737 | 51.628 | 0. |
| 6 | 1. | SISMA WOOD SLD | | 84.737 | 36.228 | 0. |
| 6 | 0. | INERZIA H SLD | | 2.204 | 0.492 | 0. |
| 6 | 0.5 | INERZIA H SLD | | 2.204 | 0.492 | 0. |
| 6 | 1. | INERZIA H SLD | | 2.204 | 0.492 | 0. |
| 6 | 0. | INERZIA V + SLD | | -2.021 | -0.431 | 0. |
| 6 | 0.5 | INERZIA V + SLD | | -2.021 | -0.431 | 0. |
| 6 | 1. | INERZIA V + SLD | | -2.021 | -0.431 | 0. |
| 6 | 0. | INERZIA V SLD | | 2.021 | 0.431 | 0. |
| 6 | 0.5 | INERZIA V SLD | | 2.021 | 0.431 | 0. |
| 6 | 1. | INERZIA V SLD | | 2.021 | 0.431 | 0. |
| 6 | 0. | INERZIA V -1 | | 4.577 | 0.976 | 0. |
| 6 | 0.5 | INERZIA V -1 | | 4.577 | 0.976 | 0. |
| 6 | 1. | INERZIA V -1 | | 4.577 | 0.976 | 0. |
| 6 | 0. | SLU_1 | Max | -2408.462 | 174.753 | 0. |
| 6 | 0.5 | SLU_1 | Max | -2384.094 | 62.81 | 0. |
| 6 | 1. | SLU_1 | Max | -2359.726 | -39.188 | 0. |
| 6 | 0. | SLU_1 | Min | -2408.462 | 174.753 | 0. |
| 6 | 0.5 | SLU_1 | Min | -2384.094 | 62.81 | 0. |
| 6 | 1. | SLU_1 | Min | -2359.726 | -39.188 | 0. |
| 6 | 0. | SLU_2 | Max | -2409.009 | 105.68 | 0. |
| 6 | 0.5 | SLU_2 | Max | -2384.641 | 9.017 | 0. |
| 6 | 1. | SLU_2 | Max | -2360.273 | -78.809 | 0. |
| 6 | 0. | SLU_2 | Min | -2409.009 | 105.68 | 0. |
| 6 | 0.5 | SLU_2 | Min | -2384.641 | 9.017 | 0. |
| 6 | 1. | SLU_2 | Min | -2360.273 | -78.809 | 0. |
| 6 | 0. | SLU_3 | Max | -3011.94 | 273.2 | 0. |
| 6 | 0.5 | SLU_3 | Max | -2987.573 | 132.511 | 0. |
| 6 | 1. | SLU_3 | Max | -2963.205 | 2.15 | 0. |
| 6 | 0. | SLU_3 | Min | -3011.94 | 273.2 | 0. |
| 6 | 0.5 | SLU_3 | Min | -2987.573 | 132.511 | 0. |
| 6 | 1. | SLU_3 | Min | -2963.205 | 2.15 | 0. |
| 6 | 0. | SLU_4 | Max | -3027.637 | 143.169 | 0. |
| 6 | 0.5 | SLU_4 | Max | -3003.27 | 29.312 | 0. |
| 6 | 1. | SLU_4 | Max | -2978.902 | -76.791 | 0. |
| 6 | 0. | SLU_4 | Min | -3027.637 | 143.169 | 0. |
| 6 | 0.5 | SLU_4 | Min | -3003.27 | 29.312 | 0. |
| 6 | 1. | SLU_4 | Min | -2978.902 | -76.791 | 0. |
| 6 | 0. | SLE_F1 | Max | -1761.642 | 146.878 | 0. |
| 6 | 0.5 | SLE_F1 | Max | -1742.898 | 60.768 | 0. |
| 6 | 1. | SLE_F1 | Max | -1724.153 | -17.692 | 0. |
| 6 | 0. | SLE_F1 | Min | -1761.642 | 146.878 | 0. |
| 6 | 0.5 | SLE_F1 | Min | -1742.898 | 60.768 | 0. |
| 6 | 1. | SLE_F1 | Min | -1724.153 | -17.692 | 0. |
| 6 | 0. | SLE_F2 | Max | -1762.012 | 96.77 | 0. |
| 6 | 0.5 | SLE_F2 | Max | -1743.268 | 22.414 | 0. |
| 6 | 1. | SLE_F2 | Max | -1724.523 | -45.145 | 0. |
| 6 | 0. | SLE_F2 | Min | -1762.012 | 96.77 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 6 | 0.5 | SLE_F2 | Min | -1743.268 | 22.414 | 0. |
| 6 | 1. | SLE_F2 | Min | -1724.523 | -45.145 | 0. |
| 6 | 0. | SLE_F3 | Max | -2237.882 | 125.01 | 0. |
| 6 | 0.5 | SLE_F3 | Max | -2219.138 | 37.427 | 0. |
| 6 | 1. | SLE_F3 | Max | -2200.393 | -44.19 | 0. |
| 6 | 0. | SLE_F3 | Min | -2237.882 | 125.01 | 0. |
| 6 | 0.5 | SLE_F3 | Min | -2219.138 | 37.427 | 0. |
| 6 | 1. | SLE_F3 | Min | -2200.393 | -44.19 | 0. |
| 6 | 0. | SLE_F4 | Max | -2226.004 | 224.083 | 0. |
| 6 | 0.5 | SLE_F4 | Max | -2207.259 | 115.86 | 0. |
| 6 | 1. | SLE_F4 | Max | -2188.515 | 15.583 | 0. |
| 6 | 0. | SLE_F4 | Min | -2226.004 | 224.083 | 0. |
| 6 | 0.5 | SLE_F4 | Min | -2207.259 | 115.86 | 0. |
| 6 | 1. | SLE_F4 | Min | -2188.515 | 15.583 | 0. |
| 6 | 0. | SLE_QP1 | Max | -1592.352 | 170.983 | 0. |
| 6 | 0.5 | SLE_QP1 | Max | -1573.608 | 84.873 | 0. |
| 6 | 1. | SLE_QP1 | Max | -1554.864 | 6.413 | 0. |
| 6 | 0. | SLE_QP1 | Min | -1592.352 | 170.983 | 0. |
| 6 | 0.5 | SLE_QP1 | Min | -1573.608 | 84.873 | 0. |
| 6 | 1. | SLE_QP1 | Min | -1554.864 | 6.413 | 0. |
| 6 | 0. | SLE_QP2 | Max | -1592.88 | 125.514 | 0. |
| 6 | 0.5 | SLE_QP2 | Max | -1574.135 | 51.158 | 0. |
| 6 | 1. | SLE_QP2 | Max | -1555.391 | -16.401 | 0. |
| 6 | 0. | SLE_QP2 | Min | -1592.88 | 125.514 | 0. |
| 6 | 0.5 | SLE_QP2 | Min | -1574.135 | 51.158 | 0. |
| 6 | 1. | SLE_QP2 | Min | -1555.391 | -16.401 | 0. |
| 6 | 0. | SLE_QP3 | Max | -2068.753 | 152.644 | 0. |
| 6 | 0.5 | SLE_QP3 | Max | -2050.009 | 65.061 | 0. |
| 6 | 1. | SLE_QP3 | Max | -2031.264 | -16.556 | 0. |
| 6 | 0. | SLE_QP3 | Min | -2068.753 | 152.644 | 0. |
| 6 | 0.5 | SLE_QP3 | Min | -2050.009 | 65.061 | 0. |
| 6 | 1. | SLE_QP3 | Min | -2031.264 | -16.556 | 0. |
| 6 | 0. | SLE_QP4 | Max | -2057.411 | 249.309 | 0. |
| 6 | 0.5 | SLE_QP4 | Max | -2038.667 | 141.086 | 0. |
| 6 | 1. | SLE_QP4 | Max | -2019.922 | 40.809 | 0. |
| 6 | 0. | SLE_QP4 | Min | -2057.411 | 249.309 | 0. |
| 6 | 0.5 | SLE_QP4 | Min | -2038.667 | 141.086 | 0. |
| 6 | 1. | SLE_QP4 | Min | -2019.922 | 40.809 | 0. |
| 6 | 0. | SLV_1 | Max | -1495.244 | 470.679 | 0. |
| 6 | 0.5 | SLV_1 | Max | -1476.499 | 349.699 | 0. |
| 6 | 1. | SLV_1 | Max | -1457.755 | 236.369 | 0. |
| 6 | 0. | SLV_1 | Min | -1495.244 | 470.679 | 0. |
| 6 | 0.5 | SLV_1 | Min | -1476.499 | 349.699 | 0. |
| 6 | 1. | SLV_1 | Min | -1457.755 | 236.369 | 0. |
| 6 | 0. | SLV_2 | Max | -1484.869 | 472.751 | 0. |
| 6 | 0.5 | SLV_2 | Max | -1466.125 | 351.771 | 0. |
| 6 | 1. | SLV_2 | Max | -1447.38 | 238.441 | 0. |
| 6 | 0. | SLV_2 | Min | -1484.869 | 472.751 | 0. |
| 6 | 0.5 | SLV_2 | Min | -1466.125 | 351.771 | 0. |
| 6 | 1. | SLV_2 | Min | -1447.38 | 238.441 | 0. |
| 6 | 0. | SLV_3 | Max | -1977.798 | 561.152 | 0. |
| 6 | 0.5 | SLV_3 | Max | -1959.053 | 418.059 | 0. |
| 6 | 1. | SLV_3 | Max | -1940.309 | 282.912 | 0. |
| 6 | 0. | SLV_3 | Min | -1977.798 | 561.152 | 0. |
| 6 | 0.5 | SLV_3 | Min | -1959.053 | 418.059 | 0. |
| 6 | 1. | SLV_3 | Min | -1940.309 | 282.912 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 6 | 1. | SLV_3 | Min | -1940.309 | 282.912 | 0. |
| 6 | 0. | SLV_4 | Max | -1967.164 | 563.249 | 0. |
| 6 | 0.5 | SLV_4 | Max | -1948.419 | 420.157 | 0. |
| 6 | 1. | SLV_4 | Max | -1929.675 | 285.009 | 0. |
| 6 | 0. | SLV_4 | Min | -1967.164 | 563.249 | 0. |
| 6 | 0.5 | SLV_4 | Min | -1948.419 | 420.157 | 0. |
| 6 | 1. | SLV_4 | Min | -1929.675 | 285.009 | 0. |
| 6 | 0. | SLD_1 | Max | -1535.397 | 301.179 | 0. |
| 6 | 0.5 | SLD_1 | Max | -1516.653 | 199.669 | 0. |
| 6 | 1. | SLD_1 | Max | -1497.908 | 105.809 | 0. |
| 6 | 0. | SLD_1 | Min | -1535.397 | 301.179 | 0. |
| 6 | 0.5 | SLD_1 | Min | -1516.653 | 199.669 | 0. |
| 6 | 1. | SLD_1 | Min | -1497.908 | 105.809 | 0. |
| 6 | 0. | SLD_2 | Max | -1530.53 | 302.481 | 0. |
| 6 | 0.5 | SLD_2 | Max | -1511.786 | 200.971 | 0. |
| 6 | 1. | SLD_2 | Max | -1493.042 | 107.111 | 0. |
| 6 | 0. | SLD_2 | Min | -1530.53 | 302.481 | 0. |
| 6 | 0.5 | SLD_2 | Min | -1511.786 | 200.971 | 0. |
| 6 | 1. | SLD_2 | Min | -1493.042 | 107.111 | 0. |
| 6 | 0. | SLD_3 | Max | -2013.983 | 391.804 | 0. |
| 6 | 0.5 | SLD_3 | Max | -1995.238 | 268.181 | 0. |
| 6 | 1. | SLD_3 | Max | -1976.494 | 152.504 | 0. |
| 6 | 0. | SLD_3 | Min | -2013.983 | 391.804 | 0. |
| 6 | 0.5 | SLD_3 | Min | -1995.238 | 268.181 | 0. |
| 6 | 1. | SLD_3 | Min | -1976.494 | 152.504 | 0. |
| 6 | 0. | SLD_4 | Max | -2009.208 | 392.826 | 0. |
| 6 | 0.5 | SLD_4 | Max | -1990.464 | 269.203 | 0. |
| 6 | 1. | SLD_4 | Max | -1971.719 | 153.526 | 0. |
| 6 | 0. | SLD_4 | Min | -2009.208 | 392.826 | 0. |
| 6 | 0.5 | SLD_4 | Min | -1990.464 | 269.203 | 0. |
| 6 | 1. | SLD_4 | Min | -1971.719 | 153.526 | 0. |
| 6 | 0. | SLU_IDR_1 | Max | -1928.149 | 200.988 | 0. |
| 6 | 0.5 | SLU_IDR_1 | Max | -1911.279 | 111.993 | 0. |
| 6 | 1. | SLU_IDR_1 | Max | -1894.409 | 29.388 | 0. |
| 6 | 0. | SLU_IDR_1 | Min | -1928.149 | 200.988 | 0. |
| 6 | 0.5 | SLU_IDR_1 | Min | -1911.279 | 111.993 | 0. |
| 6 | 1. | SLU_IDR_1 | Min | -1894.409 | 29.388 | 0. |
| 6 | 0. | SLU_IDR_2 | Max | -1500.869 | 180.998 | 0. |
| 6 | 0.5 | SLU_IDR_2 | Max | -1483.999 | 103.907 | 0. |
| 6 | 1. | SLU_IDR_2 | Max | -1467.129 | 33.954 | 0. |
| 6 | 0. | SLU_IDR_2 | Min | -1500.869 | 180.998 | 0. |
| 6 | 0.5 | SLU_IDR_2 | Min | -1483.999 | 103.907 | 0. |
| 6 | 1. | SLU_IDR_2 | Min | -1467.129 | 33.954 | 0. |
| 6 | 0. | SISMA WOOD SLV-1 | Max | -27.863 | 200.947 | 0. |
| 6 | 0.5 | SISMA WOOD SLV-1 | Max | -27.863 | 166.077 | 0. |
| 6 | 1. | SISMA WOOD SLV-1 | Max | -27.863 | 131.207 | 0. |
| 6 | 0. | SISMA WOOD SLV-1 | Min | -27.863 | 200.947 | 0. |
| 6 | 0.5 | SISMA WOOD SLV-1 | Min | -27.863 | 166.077 | 0. |
| 6 | 1. | SISMA WOOD SLV-1 | Min | -27.863 | 131.207 | 0. |
| 6 | 0. | DEAD-1 | Max | -366.636 | -76.858 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 6 | 0.5 | DEAD-1 | Max | -347.892 | -76.858 | 0. |
| 6 | 1. | DEAD-1 | Max | -329.148 | -76.858 | 0. |
| 6 | 0. | DEAD-1 | Min | -366.636 | -76.858 | 0. |
| 6 | 0.5 | DEAD-1 | Min | -347.892 | -76.858 | 0. |
| 6 | 1. | DEAD-1 | Min | -329.148 | -76.858 | 0. |
| 6 | 0. | SLU_PROVA | | -2200.914 | 213.196 | 0. |
| 6 | 0.5 | SLU_PROVA | | -2176.547 | 101.253 | 0. |
| 6 | 1. | SLU_PROVA | | -2152.179 | -0.745 | 0. |
| 7 | 0. | DEAD | | -264.456 | -69.904 | 0. |
| 7 | 0.28595 | DEAD | | -253.736 | -69.904 | 0. |
| 7 | 0.5719 | DEAD | | -243.016 | -69.904 | 0. |
| 7 | 0. | SIMM_KA | | -12.661 | 58.795 | 0. |
| 7 | 0.28595 | SIMM_KA | | -12.661 | 47.051 | 0. |
| 7 | 0.5719 | SIMM_KA | | -12.661 | 35.793 | 0. |
| 7 | 0. | SIMM_K0 | | -19.338 | 90.767 | 0. |
| 7 | 0.28595 | SIMM_K0 | | -19.338 | 73.153 | 0. |
| 7 | 0.5719 | SIMM_K0 | | -19.338 | 56.267 | 0. |
| 7 | 0. | A--SIMM_KA | | 22.454 | 131.814 | 0. |
| 7 | 0.28595 | A--SIMM_KA | | 22.454 | 111.883 | 0. |
| 7 | 0.5719 | A--SIMM_KA | | 22.454 | 92.619 | 0. |
| 7 | 0. | A--SIMM_K0 | | 32.768 | 196.44 | 0. |
| 7 | 0.28595 | A--SIMM_K0 | | 32.768 | 166.563 | 0. |
| 7 | 0.5719 | A--SIMM_K0 | | 32.768 | 137.674 | 0. |
| 7 | 0. | A-- SIMM_SOVR_K A | | -1.65 | 14.024 | 0. |
| 7 | 0.28595 | A-- SIMM_SOVR_K A | | -1.65 | 14.024 | 0. |
| 7 | 0.5719 | A-- SIMM_SOVR_K A | | -1.65 | 14.024 | 0. |
| 7 | 0. | A-- SIMM_SOVR_K 0 | | -2.474 | 21.025 | 0. |
| 7 | 0.28595 | A-- SIMM_SOVR_K 0 | | -2.474 | 21.025 | 0. |
| 7 | 0.5719 | A-- SIMM_SOVR_K 0 | | -2.474 | 21.025 | 0. |
| 7 | 0. | SIMM_SOVR_K 0 | | -2.474 | 21.025 | 0. |
| 7 | 0.28595 | SIMM_SOVR_K 0 | | -2.474 | 21.025 | 0. |
| 7 | 0.5719 | SIMM_SOVR_K 0 | | -2.474 | 21.025 | 0. |
| 7 | 0. | SIMM_SOVR_K A | | -1.65 | 14.024 | 0. |
| 7 | 0.28595 | SIMM_SOVR_K A | | -1.65 | 14.024 | 0. |
| 7 | 0.5719 | SIMM_SOVR_K A | | -1.65 | 14.024 | 0. |
| 7 | 0. | SOVR | | -195.416 | -47.659 | 0. |
| 7 | 0.28595 | SOVR | | -195.416 | -47.659 | 0. |
| 7 | 0.5719 | SOVR | | -195.416 | -47.659 | 0. |
| 7 | 0. | TERR_SIMM | | -781.351 | -152.493 | 0. |
| 7 | 0.28595 | TERR_SIMM | | -781.351 | -152.493 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 7 | 0.5719 | TERR_SIMM | | -781.351 | -152.493 | 0. |
| 7 | 0. | TERR_A--SIMM | | -1243.062 | -211.184 | 0. |
| 7 | 0.28595 | TERR_A--SIMM | | -1243.062 | -211.184 | 0. |
| 7 | 0.5719 | TERR_A--SIMM | | -1243.062 | -211.184 | 0. |
| 7 | 0. | INERZIA H SLV | | 4.991 | 4.635 | 0. |
| 7 | 0.28595 | INERZIA H SLV | | 4.991 | 4.635 | 0. |
| 7 | 0.5719 | INERZIA H SLV | | 4.991 | 4.635 | 0. |
| 7 | 0. | INERZIA V + SLV | | -4.101 | -1.11 | 0. |
| 7 | 0.28595 | INERZIA V + SLV | | -4.101 | -1.11 | 0. |
| 7 | 0.5719 | INERZIA V + SLV | | -4.101 | -1.11 | 0. |
| 7 | 0. | INERZIA V - SLV | | 4.101 | 1.11 | 0. |
| 7 | 0.28595 | INERZIA V - SLV | | 4.101 | 1.11 | 0. |
| 7 | 0.5719 | INERZIA V - SLV | | 4.101 | 1.11 | 0. |
| 7 | 0. | SISMA WOOD SLV | | 191.868 | 263.567 | 0. |
| 7 | 0.28595 | SISMA WOOD SLV | | 191.868 | 243.625 | 0. |
| 7 | 0.5719 | SISMA WOOD SLV | | 191.868 | 223.683 | 0. |
| 7 | 0. | iDROSTATICA | | -362.043 | 121.227 | 0. |
| 7 | 0.28595 | iDROSTATICA | | -362.043 | 97.511 | 0. |
| 7 | 0.5719 | iDROSTATICA | | -362.043 | 75.773 | 0. |
| 7 | 0. | SISMA WOOD SLD | | 84.737 | 116.402 | 0. |
| 7 | 0.28595 | SISMA WOOD SLD | | 84.737 | 107.595 | 0. |
| 7 | 0.5719 | SISMA WOOD SLD | | 84.737 | 98.787 | 0. |
| 7 | 0. | INERZIA H SLD | | 2.204 | 2.047 | 0. |
| 7 | 0.28595 | INERZIA H SLD | | 2.204 | 2.047 | 0. |
| 7 | 0.5719 | INERZIA H SLD | | 2.204 | 2.047 | 0. |
| 7 | 0. | INERZIA V + SLD | | -1.811 | -0.49 | 0. |
| 7 | 0.28595 | INERZIA V + SLD | | -1.811 | -0.49 | 0. |
| 7 | 0.5719 | INERZIA V + SLD | | -1.811 | -0.49 | 0. |
| 7 | 0. | INERZIA V SLD | | 1.811 | 0.49 | 0. |
| 7 | 0.28595 | INERZIA V SLD | | 1.811 | 0.49 | 0. |
| 7 | 0.5719 | INERZIA V SLD | | 1.811 | 0.49 | 0. |
| 7 | 0. | INERZIA V -1 | | 4.101 | 1.11 | 0. |
| 7 | 0.28595 | INERZIA V -1 | | 4.101 | 1.11 | 0. |
| 7 | 0.5719 | INERZIA V -1 | | 4.101 | 1.11 | 0. |
| 7 | 0. | SLU_1 | Max | -2359.726 | -110.064 | 0. |
| 7 | 0.28595 | SLU_1 | Max | -2345.79 | -163.794 | 0. |
| 7 | 0.5719 | SLU_1 | Max | -2331.854 | -214.005 | 0. |
| 7 | 0. | SLU_1 | Min | -2359.726 | -110.064 | 0. |
| 7 | 0.28595 | SLU_1 | Min | -2345.79 | -163.794 | 0. |
| 7 | 0.5719 | SLU_1 | Min | -2331.854 | -214.005 | 0. |
| 7 | 0. | SLU_2 | Max | -2360.273 | -167.206 | 0. |
| 7 | 0.28595 | SLU_2 | Max | -2346.337 | -213.305 | 0. |
| 7 | 0.5719 | SLU_2 | Max | -2332.401 | -256.199 | 0. |
| 7 | 0. | SLU_2 | Min | -2360.273 | -167.206 | 0. |
| 7 | 0.28595 | SLU_2 | Min | -2346.337 | -213.305 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 7 | 0.5719 | SLU_2 | Min | -2332.401 | -256.199 | 0. |
| 7 | 0. | SLU_3 | Max | -2963.205 | 2.154 | 0. |
| 7 | 0.28595 | SLU_3 | Max | -2949.269 | -67.517 | 0. |
| 7 | 0.5719 | SLU_3 | Max | -2935.333 | -133.332 | 0. |
| 7 | 0. | SLU_3 | Min | -2963.205 | 2.154 | 0. |
| 7 | 0.28595 | SLU_3 | Min | -2949.269 | -67.517 | 0. |
| 7 | 0.5719 | SLU_3 | Min | -2935.333 | -133.332 | 0. |
| 7 | 0. | SLU_4 | Max | -2978.902 | -119.448 | 0. |
| 7 | 0.28595 | SLU_4 | Max | -2964.966 | -176.19 | 0. |
| 7 | 0.5719 | SLU_4 | Max | -2951.03 | -229.493 | 0. |
| 7 | 0. | SLU_4 | Min | -2978.902 | -119.448 | 0. |
| 7 | 0.28595 | SLU_4 | Min | -2964.966 | -176.19 | 0. |
| 7 | 0.5719 | SLU_4 | Min | -2951.03 | -229.493 | 0. |
| 7 | 0. | SLE_F1 | Max | -1724.153 | -68.829 | 0. |
| 7 | 0.28595 | SLE_F1 | Max | -1713.433 | -110.16 | 0. |
| 7 | 0.5719 | SLE_F1 | Max | -1702.713 | -148.784 | 0. |
| 7 | 0. | SLE_F1 | Min | -1724.153 | -68.829 | 0. |
| 7 | 0.28595 | SLE_F1 | Min | -1713.433 | -110.16 | 0. |
| 7 | 0.5719 | SLE_F1 | Min | -1702.713 | -148.784 | 0. |
| 7 | 0. | SLE_F2 | Max | -1724.523 | -109.267 | 0. |
| 7 | 0.28595 | SLE_F2 | Max | -1713.803 | -144.728 | 0. |
| 7 | 0.5719 | SLE_F2 | Max | -1703.083 | -177.723 | 0. |
| 7 | 0. | SLE_F2 | Min | -1724.523 | -109.267 | 0. |
| 7 | 0.28595 | SLE_F2 | Min | -1713.803 | -144.728 | 0. |
| 7 | 0.5719 | SLE_F2 | Min | -1703.083 | -177.723 | 0. |
| 7 | 0. | SLE_F3 | Max | -2200.393 | -73.118 | 0. |
| 7 | 0.28595 | SLE_F3 | Max | -2189.673 | -116.766 | 0. |
| 7 | 0.5719 | SLE_F3 | Max | -2178.953 | -157.768 | 0. |
| 7 | 0. | SLE_F3 | Min | -2200.393 | -73.118 | 0. |
| 7 | 0.28595 | SLE_F3 | Min | -2189.673 | -116.766 | 0. |
| 7 | 0.5719 | SLE_F3 | Min | -2178.953 | -157.768 | 0. |
| 7 | 0. | SLE_F4 | Max | -2188.515 | 15.585 | 0. |
| 7 | 0.28595 | SLE_F4 | Max | -2177.795 | -38.008 | 0. |
| 7 | 0.5719 | SLE_F4 | Max | -2167.075 | -88.635 | 0. |
| 7 | 0. | SLE_F4 | Min | -2188.515 | 15.585 | 0. |
| 7 | 0.28595 | SLE_F4 | Min | -2177.795 | -38.008 | 0. |
| 7 | 0.5719 | SLE_F4 | Min | -2167.075 | -88.635 | 0. |
| 7 | 0. | SLE_QP1 | Max | -1554.864 | -38.692 | 0. |
| 7 | 0.28595 | SLE_QP1 | Max | -1544.144 | -80.023 | 0. |
| 7 | 0.5719 | SLE_QP1 | Max | -1533.424 | -118.647 | 0. |
| 7 | 0. | SLE_QP1 | Min | -1554.864 | -38.692 | 0. |
| 7 | 0.28595 | SLE_QP1 | Min | -1544.144 | -80.023 | 0. |
| 7 | 0.5719 | SLE_QP1 | Min | -1533.424 | -118.647 | 0. |
| 7 | 0. | SLE_QP2 | Max | -1555.391 | -73.327 | 0. |
| 7 | 0.28595 | SLE_QP2 | Max | -1544.671 | -108.787 | 0. |
| 7 | 0.5719 | SLE_QP2 | Max | -1533.951 | -141.783 | 0. |
| 7 | 0. | SLE_QP2 | Min | -1555.391 | -73.327 | 0. |
| 7 | 0.28595 | SLE_QP2 | Min | -1544.671 | -108.787 | 0. |
| 7 | 0.5719 | SLE_QP2 | Min | -1533.951 | -141.783 | 0. |
| 7 | 0. | SLE_QP3 | Max | -2031.264 | -38.269 | 0. |
| 7 | 0.28595 | SLE_QP3 | Max | -2020.544 | -81.917 | 0. |
| 7 | 0.5719 | SLE_QP3 | Max | -2009.824 | -122.919 | 0. |
| 7 | 0. | SLE_QP3 | Min | -2031.264 | -38.269 | 0. |
| 7 | 0.28595 | SLE_QP3 | Min | -2020.544 | -81.917 | 0. |
| 7 | 0.5719 | SLE_QP3 | Min | -2009.824 | -122.919 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 7 | 0. | SLE_QP4 | Max | -2019.922 | 40.814 | 0. |
| 7 | 0.28595 | SLE_QP4 | Max | -2009.202 | -12.78 | 0. |
| 7 | 0.5719 | SLE_QP4 | Max | -1998.482 | -63.406 | 0. |
| 7 | 0. | SLE_QP4 | Min | -2019.922 | 40.814 | 0. |
| 7 | 0.28595 | SLE_QP4 | Min | -2009.202 | -12.78 | 0. |
| 7 | 0.5719 | SLE_QP4 | Min | -1998.482 | -63.406 | 0. |
| 7 | 0. | SLV_1 | Max | -1457.279 | 235.469 | 0. |
| 7 | 0.28595 | SLV_1 | Max | -1446.559 | 174.197 | 0. |
| 7 | 0.5719 | SLV_1 | Max | -1435.839 | 115.63 | 0. |
| 7 | 0. | SLV_1 | Min | -1457.279 | 235.469 | 0. |
| 7 | 0.28595 | SLV_1 | Min | -1446.559 | 174.197 | 0. |
| 7 | 0.5719 | SLV_1 | Min | -1435.839 | 115.63 | 0. |
| 7 | 0. | SLV_2 | Max | -1447.856 | 237.542 | 0. |
| 7 | 0.28595 | SLV_2 | Max | -1437.136 | 176.269 | 0. |
| 7 | 0.5719 | SLV_2 | Max | -1426.416 | 117.703 | 0. |
| 7 | 0. | SLV_2 | Min | -1447.856 | 237.542 | 0. |
| 7 | 0.28595 | SLV_2 | Min | -1437.136 | 176.269 | 0. |
| 7 | 0.5719 | SLV_2 | Min | -1426.416 | 117.703 | 0. |
| 7 | 0. | SLV_3 | Max | -1939.833 | 282.026 | 0. |
| 7 | 0.28595 | SLV_3 | Max | -1929.113 | 208.491 | 0. |
| 7 | 0.5719 | SLV_3 | Max | -1918.393 | 137.922 | 0. |
| 7 | 0. | SLV_3 | Min | -1939.833 | 282.026 | 0. |
| 7 | 0.28595 | SLV_3 | Min | -1929.113 | 208.491 | 0. |
| 7 | 0.5719 | SLV_3 | Min | -1918.393 | 137.922 | 0. |
| 7 | 0. | SLV_4 | Max | -1930.151 | 284.124 | 0. |
| 7 | 0.28595 | SLV_4 | Max | -1919.431 | 210.588 | 0. |
| 7 | 0.5719 | SLV_4 | Max | -1908.711 | 140.019 | 0. |
| 7 | 0. | SLV_4 | Min | -1930.151 | 284.124 | 0. |
| 7 | 0.28595 | SLV_4 | Min | -1919.431 | 210.588 | 0. |
| 7 | 0.5719 | SLV_4 | Min | -1908.711 | 140.019 | 0. |
| 7 | 0. | SLD_1 | Max | -1497.698 | 105.417 | 0. |
| 7 | 0.28595 | SLD_1 | Max | -1486.978 | 55.28 | 0. |
| 7 | 0.5719 | SLD_1 | Max | -1476.258 | 7.848 | 0. |
| 7 | 0. | SLD_1 | Min | -1497.698 | 105.417 | 0. |
| 7 | 0.28595 | SLD_1 | Min | -1486.978 | 55.28 | 0. |
| 7 | 0.5719 | SLD_1 | Min | -1476.258 | 7.848 | 0. |
| 7 | 0. | SLD_2 | Max | -1493.252 | 106.719 | 0. |
| 7 | 0.28595 | SLD_2 | Max | -1482.532 | 56.581 | 0. |
| 7 | 0.5719 | SLD_2 | Max | -1471.812 | 9.15 | 0. |
| 7 | 0. | SLD_2 | Min | -1493.252 | 106.719 | 0. |
| 7 | 0.28595 | SLD_2 | Min | -1482.532 | 56.581 | 0. |
| 7 | 0.5719 | SLD_2 | Min | -1471.812 | 9.15 | 0. |
| 7 | 0. | SLD_3 | Max | -1976.284 | 152.139 | 0. |
| 7 | 0.28595 | SLD_3 | Max | -1965.564 | 89.738 | 0. |
| 7 | 0.5719 | SLD_3 | Max | -1954.844 | 30.304 | 0. |
| 7 | 0. | SLD_3 | Min | -1976.284 | 152.139 | 0. |
| 7 | 0.28595 | SLD_3 | Min | -1965.564 | 89.738 | 0. |
| 7 | 0.5719 | SLD_3 | Min | -1954.844 | 30.304 | 0. |
| 7 | 0. | SLD_4 | Max | -1971.93 | 153.161 | 0. |
| 7 | 0.28595 | SLD_4 | Max | -1961.21 | 90.76 | 0. |
| 7 | 0.5719 | SLD_4 | Max | -1950.49 | 31.326 | 0. |
| 7 | 0. | SLD_4 | Min | -1971.93 | 153.161 | 0. |
| 7 | 0.28595 | SLD_4 | Min | -1961.21 | 90.76 | 0. |
| 7 | 0.5719 | SLD_4 | Min | -1950.49 | 31.326 | 0. |
| 7 | 0. | SLU_IDR_1 | Max | -1894.409 | 2.303 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 7 | 0.28595 | SLU_IDR_1 | Max | -1884.761 | -41.723 | 0. |
| 7 | 0.5719 | SLU_IDR_1 | Max | -1875.113 | -82.972 | 0. |
| 7 | 0. | SLU_IDR_1 | Min | -1894.409 | 2.303 | 0. |
| 7 | 0.28595 | SLU_IDR_1 | Min | -1884.761 | -41.723 | 0. |
| 7 | 0.5719 | SLU_IDR_1 | Min | -1875.113 | -82.972 | 0. |
| 7 | 0. | SLU_IDR_2 | Max | -1467.129 | -24.608 | 0. |
| 7 | 0.28595 | SLU_IDR_2 | Max | -1457.481 | -61.266 | 0. |
| 7 | 0.5719 | SLU_IDR_2 | Max | -1447.833 | -95.309 | 0. |
| 7 | 0. | SLU_IDR_2 | Min | -1467.129 | -24.608 | 0. |
| 7 | 0.28595 | SLU_IDR_2 | Min | -1457.481 | -61.266 | 0. |
| 7 | 0.5719 | SLU_IDR_2 | Min | -1447.833 | -95.309 | 0. |
| 7 | 0. | SISMA WOOD SLV-1 | Max | -27.863 | 131.207 | 0. |
| 7 | 0.28595 | SISMA WOOD SLV-1 | Max | -27.863 | 111.264 | 0. |
| 7 | 0.5719 | SISMA WOOD SLV-1 | Max | -27.863 | 91.322 | 0. |
| 7 | 0. | SISMA WOOD SLV-1 | Min | -27.863 | 131.207 | 0. |
| 7 | 0.28595 | SISMA WOOD SLV-1 | Min | -27.863 | 111.264 | 0. |
| 7 | 0.5719 | SISMA WOOD SLV-1 | Min | -27.863 | 91.322 | 0. |
| 7 | 0. | DEAD-1 | Max | -329.148 | -89.392 | 0. |
| 7 | 0.28595 | DEAD-1 | Max | -318.428 | -89.392 | 0. |
| 7 | 0.5719 | DEAD-1 | Max | -307.708 | -89.392 | 0. |
| 7 | 0. | DEAD-1 | Min | -329.148 | -89.392 | 0. |
| 7 | 0.28595 | DEAD-1 | Min | -318.428 | -89.392 | 0. |
| 7 | 0.5719 | DEAD-1 | Min | -307.708 | -89.392 | 0. |
| 7 | 0. | SLU_PROVA | | -2152.179 | -53.474 | 0. |
| 7 | 0.28595 | SLU_PROVA | | -2138.243 | -107.203 | 0. |
| 7 | 0.5719 | SLU_PROVA | | -2124.307 | -157.415 | 0. |
| 8 | 0. | DEAD | | -251.987 | -32.07 | 0. |
| 8 | 0.75656 | DEAD | | -226.009 | -20.687 | 0. |
| 8 | 1.51312 | DEAD | | -200.031 | -9.303 | 0. |
| 8 | 0. | SIMM_KA | | 5.595 | -46.232 | 0. |
| 8 | 0.75656 | SIMM_KA | | -5.844 | -20.129 | 0. |
| 8 | 1.51312 | SIMM_KA | | -16.766 | 4.797 | 0. |
| 8 | 0. | SIMM_K0 | | 9.209 | -72.145 | 0. |
| 8 | 0.75656 | SIMM_K0 | | -7.949 | -32.99 | 0. |
| 8 | 1.51312 | SIMM_K0 | | -24.333 | 4.399 | 0. |
| 8 | 0. | A--SIMM_KA | | 66.244 | -101.06 | 0. |
| 8 | 0.75656 | A--SIMM_KA | | 46.76 | -56.595 | 0. |
| 8 | 1.51312 | A--SIMM_KA | | 28.51 | -14.947 | 0. |
| 8 | 0. | A--SIMM_K0 | | 97.9 | -150.413 | 0. |
| 8 | 0.75656 | A--SIMM_K0 | | 68.674 | -83.716 | 0. |
| 8 | 1.51312 | A--SIMM_K0 | | 41.299 | -21.247 | 0. |
| 8 | 0. | A-- SIMM_SOVR_K A | | 4.522 | -14.709 | 0. |
| 8 | 0.75656 | A-- SIMM_SOVR_K A | | 2.496 | -10.087 | 0. |
| 8 | 1.51312 | A-- SIMM_SOVR_K A | | 0.471 | -5.465 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 8 | 0. | A-- SIMM_SOVR_K 0 | | 6.779 | -22.053 | 0. |
| 8 | 0.75656 | A-- SIMM_SOVR_K 0 | | 3.742 | -15.123 | 0. |
| 8 | 1.51312 | A-- SIMM_SOVR_K 0 | | 0.706 | -8.194 | 0. |
| 8 | 0. | SIMM_SOVR_K 0 | | 6.779 | -22.053 | 0. |
| 8 | 0.75656 | SIMM_SOVR_K 0 | | 3.742 | -15.123 | 0. |
| 8 | 1.51312 | SIMM_SOVR_K 0 | | 0.706 | -8.194 | 0. |
| 8 | 0. | SIMM_SOVR_K A | | 4.522 | -14.709 | 0. |
| 8 | 0.75656 | SIMM_SOVR_K A | | 2.496 | -10.087 | 0. |
| 8 | 1.51312 | SIMM_SOVR_K A | | 0.471 | -5.465 | 0. |
| 8 | 0. | SOVR | | -199.84 | -30.592 | 0. |
| 8 | 0.75656 | SOVR | | -185.981 | -24.519 | 0. |
| 8 | 1.51312 | SOVR | | -172.122 | -18.446 | 0. |
| 8 | 0. | TERR_SIMM | | -782.675 | -160.381 | 0. |
| 8 | 0.75656 | TERR_SIMM | | -704.37 | -126.068 | 0. |
| 8 | 1.51312 | TERR_SIMM | | -629.596 | -93.302 | 0. |
| 8 | 0. | TERR_A--SIMM | | -1231.28 | -287.876 | 0. |
| 8 | 0.75656 | TERR_A--SIMM | | -1088.492 | -225.307 | 0. |
| 8 | 1.51312 | TERR_A--SIMM | | -954.786 | -166.717 | 0. |
| 8 | 0. | INERZIA H SLV | | 6.597 | -3.107 | 0. |
| 8 | 0.75656 | INERZIA H SLV | | 6.597 | -3.107 | 0. |
| 8 | 1.51312 | INERZIA H SLV | | 6.597 | -3.107 | 0. |
| 8 | 0. | INERZIA V + SLV | | -3.645 | -0.353 | 0. |
| 8 | 0.75656 | INERZIA V + SLV | | -3.645 | -0.353 | 0. |
| 8 | 1.51312 | INERZIA V + SLV | | -3.645 | -0.353 | 0. |
| 8 | 0. | INERZIA V - SLV | | 3.645 | 0.353 | 0. |
| 8 | 0.75656 | INERZIA V - SLV | | 3.645 | 0.353 | 0. |
| 8 | 1.51312 | INERZIA V - SLV | | 3.645 | 0.353 | 0. |
| 8 | 0. | SISMA WOOD SLV | | 293.316 | -211.023 | 0. |
| 8 | 0.75656 | SISMA WOOD SLV | | 272.14 | -162.697 | 0. |
| 8 | 1.51312 | SISMA WOOD SLV | | 250.963 | -114.37 | 0. |
| 8 | 0. | iDROSTATICA | | -302.899 | -207.796 | 0. |
| 8 | 0.75656 | iDROSTATICA | | -302.899 | -152.9 | 0. |
| 8 | 1.51312 | iDROSTATICA | | -302.899 | -98.004 | 0. |
| 8 | 0. | SISMA WOOD SLD | | 129.54 | -93.196 | 0. |
| 8 | 0.75656 | SISMA WOOD SLD | | 120.188 | -71.853 | 0. |
| 8 | 1.51312 | SISMA WOOD SLD | | 110.835 | -50.511 | 0. |
| 8 | 0. | INERZIA H SLD | | 2.913 | -1.372 | 0. |
| 8 | 0.75656 | INERZIA H SLD | | 2.913 | -1.372 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|-----------|----------|
| 8 | 1.51312 | INERZIA H SLD | | 2.913 | -1.372 | 0. |
| 8 | 0. | INERZIA V + SLD | | -1.61 | -0.156 | 0. |
| 8 | 0.75656 | INERZIA V + SLD | | -1.61 | -0.156 | 0. |
| 8 | 1.51312 | INERZIA V + SLD | | -1.61 | -0.156 | 0. |
| 8 | 0. | INERZIA V SLD | | 1.61 | 0.156 | 0. |
| 8 | 0.75656 | INERZIA V SLD | | 1.61 | 0.156 | 0. |
| 8 | 1.51312 | INERZIA V SLD | | 1.61 | 0.156 | 0. |
| 8 | 0. | INERZIA V -1 | | 3.645 | 0.353 | 0. |
| 8 | 0.75656 | INERZIA V -1 | | 3.645 | 0.353 | 0. |
| 8 | 1.51312 | INERZIA V -1 | | 3.645 | 0.353 | 0. |
| 8 | 0. | SLU_1 | Max | -2232.12 | -716.087 | 0. |
| 8 | 0.75656 | SLU_1 | Max | -2102.623 | -514.911 | 0. |
| 8 | 1.51312 | SLU_1 | Max | -1976.71 | -318.044 | 0. |
| 8 | 0. | SLU_1 | Min | -2232.12 | -716.087 | 0. |
| 8 | 0.75656 | SLU_1 | Min | -2102.623 | -514.911 | 0. |
| 8 | 1.51312 | SLU_1 | Min | -1976.71 | -318.044 | 0. |
| 8 | 0. | SLU_2 | Max | -2252.411 | -669.93 | 0. |
| 8 | 0.75656 | SLU_2 | Max | -2113.962 | -489.182 | 0. |
| 8 | 1.51312 | SLU_2 | Max | -1979.433 | -311.977 | 0. |
| 8 | 0. | SLU_2 | Min | -2252.411 | -669.93 | 0. |
| 8 | 0.75656 | SLU_2 | Min | -2113.962 | -489.182 | 0. |
| 8 | 1.51312 | SLU_2 | Min | -1979.433 | -311.977 | 0. |
| 8 | 0. | SLU_3 | Max | -2742.049 | -1055.995 | 0. |
| 8 | 0.75656 | SLU_3 | Max | -2544.415 | -782.282 | 0. |
| 8 | 1.51312 | SLU_3 | Max | -2356.178 | -519.238 | 0. |
| 8 | 0. | SLU_3 | Min | -2742.049 | -1055.995 | 0. |
| 8 | 0.75656 | SLU_3 | Min | -2544.415 | -782.282 | 0. |
| 8 | 1.51312 | SLU_3 | Min | -2356.178 | -519.238 | 0. |
| 8 | 0. | SLU_4 | Max | -2800.929 | -960.736 | 0. |
| 8 | 0.75656 | SLU_4 | Max | -2589.113 | -719.386 | 0. |
| 8 | 1.51312 | SLU_4 | Max | -2387.498 | -486.871 | 0. |
| 8 | 0. | SLU_4 | Min | -2800.929 | -960.736 | 0. |
| 8 | 0.75656 | SLU_4 | Min | -2589.113 | -719.386 | 0. |
| 8 | 1.51312 | SLU_4 | Min | -2387.498 | -486.871 | 0. |
| 8 | 0. | SLE_F1 | Max | -1626.769 | -530.003 | 0. |
| 8 | 0.75656 | SLE_F1 | Max | -1531.526 | -380.503 | 0. |
| 8 | 1.51312 | SLE_F1 | Max | -1439.041 | -234.318 | 0. |
| 8 | 0. | SLE_F1 | Min | -1626.769 | -530.003 | 0. |
| 8 | 0.75656 | SLE_F1 | Min | -1531.526 | -380.503 | 0. |
| 8 | 1.51312 | SLE_F1 | Min | -1439.041 | -234.318 | 0. |
| 8 | 0. | SLE_F2 | Max | -1640.831 | -497.856 | 0. |
| 8 | 0.75656 | SLE_F2 | Max | -1539.112 | -363.139 | 0. |
| 8 | 1.51312 | SLE_F2 | Max | -1440.406 | -231.147 | 0. |
| 8 | 0. | SLE_F2 | Min | -1640.831 | -497.856 | 0. |
| 8 | 0.75656 | SLE_F2 | Min | -1539.112 | -363.139 | 0. |
| 8 | 1.51312 | SLE_F2 | Min | -1440.406 | -231.147 | 0. |
| 8 | 0. | SLE_F3 | Max | -2063.005 | -721.06 | 0. |
| 8 | 0.75656 | SLE_F3 | Max | -1904.848 | -539.725 | 0. |
| 8 | 1.51312 | SLE_F3 | Max | -1754.539 | -365.187 | 0. |
| 8 | 0. | SLE_F3 | Min | -2063.005 | -721.06 | 0. |
| 8 | 0.75656 | SLE_F3 | Min | -1904.848 | -539.725 | 0. |
| 8 | 1.51312 | SLE_F3 | Min | -1754.539 | -365.187 | 0. |
| 8 | 0. | SLE_F4 | Max | -2020.445 | -788.588 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 8 | 0.75656 | SLE_F4 | Max | -1872.789 | -583.291 | 0. |
| 8 | 1.51312 | SLE_F4 | Max | -1732.362 | -386.2 | 0. |
| 8 | 0. | SLE_F4 | Min | -2020.445 | -788.588 | 0. |
| 8 | 0.75656 | SLE_F4 | Min | -1872.789 | -583.291 | 0. |
| 8 | 1.51312 | SLE_F4 | Min | -1732.362 | -386.2 | 0. |
| 8 | 0. | SLE_QP1 | Max | -1458.678 | -491.804 | 0. |
| 8 | 0.75656 | SLE_QP1 | Max | -1371.553 | -352.056 | 0. |
| 8 | 1.51312 | SLE_QP1 | Max | -1287.184 | -215.623 | 0. |
| 8 | 0. | SLE_QP1 | Min | -1458.678 | -491.804 | 0. |
| 8 | 0.75656 | SLE_QP1 | Min | -1371.553 | -352.056 | 0. |
| 8 | 1.51312 | SLE_QP1 | Min | -1287.184 | -215.623 | 0. |
| 8 | 0. | SLE_QP2 | Max | -1470.361 | -465.403 | 0. |
| 8 | 0.75656 | SLE_QP2 | Max | -1377.517 | -338.707 | 0. |
| 8 | 1.51312 | SLE_QP2 | Max | -1287.687 | -214.736 | 0. |
| 8 | 0. | SLE_QP2 | Min | -1470.361 | -465.403 | 0. |
| 8 | 0.75656 | SLE_QP2 | Min | -1377.517 | -338.707 | 0. |
| 8 | 1.51312 | SLE_QP2 | Min | -1287.687 | -214.736 | 0. |
| 8 | 0. | SLE_QP3 | Max | -1892.972 | -687.692 | 0. |
| 8 | 0.75656 | SLE_QP3 | Max | -1743.691 | -514.378 | 0. |
| 8 | 1.51312 | SLE_QP3 | Max | -1602.257 | -347.861 | 0. |
| 8 | 0. | SLE_QP3 | Min | -1892.972 | -687.692 | 0. |
| 8 | 0.75656 | SLE_QP3 | Min | -1743.691 | -514.378 | 0. |
| 8 | 1.51312 | SLE_QP3 | Min | -1602.257 | -347.861 | 0. |
| 8 | 0. | SLE_QP4 | Max | -1855.902 | -744.031 | 0. |
| 8 | 0.75656 | SLE_QP4 | Max | -1716.363 | -548.486 | 0. |
| 8 | 1.51312 | SLE_QP4 | Max | -1584.052 | -361.147 | 0. |
| 8 | 0. | SLE_QP4 | Min | -1855.902 | -744.031 | 0. |
| 8 | 0.75656 | SLE_QP4 | Min | -1716.363 | -548.486 | 0. |
| 8 | 1.51312 | SLE_QP4 | Min | -1584.052 | -361.147 | 0. |
| 8 | 0. | SLV_1 | Max | -1268.628 | -680.805 | 0. |
| 8 | 0.75656 | SLV_1 | Max | -1202.679 | -492.73 | 0. |
| 8 | 1.51312 | SLV_1 | Max | -1139.487 | -307.97 | 0. |
| 8 | 0. | SLV_1 | Min | -1268.628 | -680.805 | 0. |
| 8 | 0.75656 | SLV_1 | Min | -1202.679 | -492.73 | 0. |
| 8 | 1.51312 | SLV_1 | Min | -1139.487 | -307.97 | 0. |
| 8 | 0. | SLV_2 | Max | -1260.323 | -679.428 | 0. |
| 8 | 0.75656 | SLV_2 | Max | -1194.374 | -491.354 | 0. |
| 8 | 1.51312 | SLV_2 | Max | -1131.182 | -306.594 | 0. |
| 8 | 0. | SLV_2 | Min | -1260.323 | -679.428 | 0. |
| 8 | 0.75656 | SLV_2 | Min | -1194.374 | -491.354 | 0. |
| 8 | 1.51312 | SLV_2 | Min | -1131.182 | -306.594 | 0. |
| 8 | 0. | SLV_3 | Max | -1701.661 | -894.904 | 0. |
| 8 | 0.75656 | SLV_3 | Max | -1583.298 | -651.033 | 0. |
| 8 | 1.51312 | SLV_3 | Max | -1472.165 | -415.367 | 0. |
| 8 | 0. | SLV_3 | Min | -1701.661 | -894.904 | 0. |
| 8 | 0.75656 | SLV_3 | Min | -1583.298 | -651.033 | 0. |
| 8 | 1.51312 | SLV_3 | Min | -1472.165 | -415.367 | 0. |
| 8 | 0. | SLV_4 | Max | -1693.109 | -893.447 | 0. |
| 8 | 0.75656 | SLV_4 | Max | -1574.746 | -649.575 | 0. |
| 8 | 1.51312 | SLV_4 | Max | -1463.612 | -413.91 | 0. |
| 8 | 0. | SLV_4 | Min | -1693.109 | -893.447 | 0. |
| 8 | 0.75656 | SLV_4 | Min | -1574.746 | -649.575 | 0. |
| 8 | 1.51312 | SLV_4 | Min | -1463.612 | -413.91 | 0. |
| 8 | 0. | SLD_1 | Max | -1348.951 | -599.085 | 0. |
| 8 | 0.75656 | SLD_1 | Max | -1271.178 | -437.994 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 8 | 1.51312 | SLD_1 | Max | -1196.162 | -280.217 | 0. |
| 8 | 0. | SLD_1 | Min | -1348.951 | -599.085 | 0. |
| 8 | 0.75656 | SLD_1 | Min | -1271.178 | -437.994 | 0. |
| 8 | 1.51312 | SLD_1 | Min | -1196.162 | -280.217 | 0. |
| 8 | 0. | SLD_2 | Max | -1344.868 | -598.716 | 0. |
| 8 | 0.75656 | SLD_2 | Max | -1267.095 | -437.625 | 0. |
| 8 | 1.51312 | SLD_2 | Max | -1192.078 | -279.849 | 0. |
| 8 | 0. | SLD_2 | Min | -1344.868 | -598.716 | 0. |
| 8 | 0.75656 | SLD_2 | Min | -1267.095 | -437.625 | 0. |
| 8 | 1.51312 | SLD_2 | Min | -1192.078 | -279.849 | 0. |
| 8 | 0. | SLD_3 | Max | -1778.282 | -811.748 | 0. |
| 8 | 0.75656 | SLD_3 | Max | -1648.095 | -594.86 | 0. |
| 8 | 1.51312 | SLD_3 | Max | -1525.137 | -386.178 | 0. |
| 8 | 0. | SLD_3 | Min | -1778.282 | -811.748 | 0. |
| 8 | 0.75656 | SLD_3 | Min | -1648.095 | -594.86 | 0. |
| 8 | 1.51312 | SLD_3 | Min | -1525.137 | -386.178 | 0. |
| 8 | 0. | SLD_4 | Max | -1774.395 | -811.161 | 0. |
| 8 | 0.75656 | SLD_4 | Max | -1644.208 | -594.273 | 0. |
| 8 | 1.51312 | SLD_4 | Max | -1521.25 | -385.591 | 0. |
| 8 | 0. | SLD_4 | Min | -1774.395 | -811.161 | 0. |
| 8 | 0.75656 | SLD_4 | Min | -1644.208 | -594.273 | 0. |
| 8 | 1.51312 | SLD_4 | Min | -1521.25 | -385.591 | 0. |
| 8 | 0. | SLU_IDR_1 | Max | -1754.34 | -668.421 | 0. |
| 8 | 0.75656 | SLU_IDR_1 | Max | -1619.987 | -501.459 | 0. |
| 8 | 1.51312 | SLU_IDR_1 | Max | -1492.696 | -340.614 | 0. |
| 8 | 0. | SLU_IDR_1 | Min | -1754.34 | -668.421 | 0. |
| 8 | 0.75656 | SLU_IDR_1 | Min | -1619.987 | -501.459 | 0. |
| 8 | 1.51312 | SLU_IDR_1 | Min | -1492.696 | -340.614 | 0. |
| 8 | 0. | SLU_IDR_2 | Max | -1373.015 | -471.674 | 0. |
| 8 | 0.75656 | SLU_IDR_2 | Max | -1289.455 | -346.669 | 0. |
| 8 | 1.51312 | SLU_IDR_2 | Max | -1208.608 | -224.115 | 0. |
| 8 | 0. | SLU_IDR_2 | Min | -1373.015 | -471.674 | 0. |
| 8 | 0.75656 | SLU_IDR_2 | Min | -1289.455 | -346.669 | 0. |
| 8 | 1.51312 | SLU_IDR_2 | Min | -1208.608 | -224.115 | 0. |
| 8 | 0. | SISMA WOOD SLV-1 | Max | 11.132 | -94.827 | 0. |
| 8 | 0.75656 | SISMA WOOD SLV-1 | Max | -10.044 | -46.501 | 0. |
| 8 | 1.51312 | SISMA WOOD SLV-1 | Max | -31.221 | 1.825 | 0. |
| 8 | 0. | SISMA WOOD SLV-1 | Min | 11.132 | -94.827 | 0. |
| 8 | 0.75656 | SISMA WOOD SLV-1 | Min | -10.044 | -46.501 | 0. |
| 8 | 1.51312 | SISMA WOOD SLV-1 | Min | -31.221 | 1.825 | 0. |
| 8 | 0. | DEAD-1 | Max | -319.746 | -36.987 | 0. |
| 8 | 0.75656 | DEAD-1 | Max | -293.768 | -25.604 | 0. |
| 8 | 1.51312 | DEAD-1 | Max | -267.79 | -14.22 | 0. |
| 8 | 0. | DEAD-1 | Min | -319.746 | -36.987 | 0. |
| 8 | 0.75656 | DEAD-1 | Min | -293.768 | -25.604 | 0. |
| 8 | 1.51312 | DEAD-1 | Min | -267.79 | -14.22 | 0. |
| 8 | 0. | SLU_PROVA | | -2016.448 | -693.076 | 0. |
| 8 | 0.75656 | SLU_PROVA | | -1886.952 | -491.9 | 0. |
| 8 | 1.51312 | SLU_PROVA | | -1761.038 | -295.033 | 0. |
| 9 | 0. | DEAD | | -197.322 | -36.617 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 9 | 0.69717 | DEAD | | -179.307 | -26.005 | 0. |
| 9 | 1.39435 | DEAD | | -161.291 | -15.392 | 0. |
| 9 | 0. | SIMM_KA | | -16.937 | -1.592 | 0. |
| 9 | 0.69717 | SIMM_KA | | -28.92 | 18.751 | 0. |
| 9 | 1.39435 | SIMM_KA | | -40.015 | 37.586 | 0. |
| 9 | 0. | SIMM_K0 | | -24.249 | -5.253 | 0. |
| 9 | 0.69717 | SIMM_K0 | | -42.439 | 25.626 | 0. |
| 9 | 1.39435 | SIMM_K0 | | -59.726 | 54.973 | 0. |
| 9 | 0. | A--SIMM_KA | | 30.938 | -24.64 | 0. |
| 9 | 0.69717 | A--SIMM_KA | | 11.109 | 9.022 | 0. |
| 9 | 1.39435 | A--SIMM_KA | | -7.282 | 40.241 | 0. |
| 9 | 0. | A--SIMM_K0 | | 44.8 | -35.789 | 0. |
| 9 | 0.69717 | A--SIMM_K0 | | 15.059 | 14.7 | 0. |
| 9 | 1.39435 | A--SIMM_K0 | | -12.523 | 61.525 | 0. |
| 9 | 0. | A-- SIMM_SOVR_K A | | 1.164 | -6.081 | 0. |
| 9 | 0.69717 | A-- SIMM_SOVR_K A | | -1.196 | -2.074 | 0. |
| 9 | 1.39435 | A-- SIMM_SOVR_K A | | -3.557 | 1.933 | 0. |
| 9 | 0. | A-- SIMM_SOVR_K 0 | | 1.745 | -9.117 | 0. |
| 9 | 0.69717 | A-- SIMM_SOVR_K 0 | | -1.794 | -3.11 | 0. |
| 9 | 1.39435 | A-- SIMM_SOVR_K 0 | | -5.332 | 2.897 | 0. |
| 9 | 0. | SIMM_SOVR_K 0 | | 1.745 | -9.117 | 0. |
| 9 | 0.69717 | SIMM_SOVR_K 0 | | -1.794 | -3.11 | 0. |
| 9 | 1.39435 | SIMM_SOVR_K 0 | | -5.332 | 2.897 | 0. |
| 9 | 0. | SIMM_SOVR_K A | | 1.164 | -6.081 | 0. |
| 9 | 0.69717 | SIMM_SOVR_K A | | -1.196 | -2.074 | 0. |
| 9 | 1.39435 | SIMM_SOVR_K A | | -3.557 | 1.933 | 0. |
| 9 | 0. | SOVR | | -168.745 | -38.438 | 0. |
| 9 | 0.69717 | SOVR | | -156.731 | -31.361 | 0. |
| 9 | 1.39435 | SOVR | | -144.717 | -24.284 | 0. |
| 9 | 0. | TERR_SIMM | | -614.064 | -167.958 | 0. |
| 9 | 0.69717 | TERR_SIMM | | -552.306 | -131.578 | 0. |
| 9 | 1.39435 | TERR_SIMM | | -493.612 | -97.004 | 0. |
| 9 | 0. | TERR_A--SIMM | | -928.11 | -281.716 | 0. |
| 9 | 0.69717 | TERR_A--SIMM | | -821.635 | -218.995 | 0. |
| 9 | 1.39435 | TERR_A--SIMM | | -726.149 | -162.748 | 0. |
| 9 | 0. | INERZIA H SLV | | 6.175 | -1.913 | 0. |
| 9 | 0.69717 | INERZIA H SLV | | 6.175 | -1.913 | 0. |
| 9 | 1.39435 | INERZIA H SLV | | 6.175 | -1.913 | 0. |
| 9 | 0. | INERZIA V + SLV | | -2.888 | -0.438 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 9 | 0.69717 | INERZIA V + SLV | | -2.888 | -0.438 | 0. |
| 9 | 1.39435 | INERZIA V + SLV | | -2.888 | -0.438 | 0. |
| 9 | 0. | INERZIA V - SLV | | 2.888 | 0.438 | 0. |
| 9 | 0.69717 | INERZIA V - SLV | | 2.888 | 0.438 | 0. |
| 9 | 1.39435 | INERZIA V - SLV | | 2.888 | 0.438 | 0. |
| 9 | 0. | SISMA WOOD SLV | | 265.469 | -125.239 | 0. |
| 9 | 0.69717 | SISMA WOOD SLV | | 240.791 | -83.347 | 0. |
| 9 | 1.39435 | SISMA WOOD SLV | | 216.114 | -41.454 | 0. |
| 9 | 0. | iDROSTATICA | | -289.353 | -128.558 | 0. |
| 9 | 0.69717 | iDROSTATICA | | -289.353 | -79.679 | 0. |
| 9 | 1.39435 | iDROSTATICA | | -289.353 | -34.217 | 0. |
| 9 | 0. | SISMA WOOD SLD | | 117.242 | -55.311 | 0. |
| 9 | 0.69717 | SISMA WOOD SLD | | 106.343 | -36.809 | 0. |
| 9 | 1.39435 | SISMA WOOD SLD | | 95.445 | -18.308 | 0. |
| 9 | 0. | INERZIA H SLD | | 2.727 | -0.845 | 0. |
| 9 | 0.69717 | INERZIA H SLD | | 2.727 | -0.845 | 0. |
| 9 | 1.39435 | INERZIA H SLD | | 2.727 | -0.845 | 0. |
| 9 | 0. | INERZIA V + SLD | | -1.275 | -0.193 | 0. |
| 9 | 0.69717 | INERZIA V + SLD | | -1.275 | -0.193 | 0. |
| 9 | 1.39435 | INERZIA V + SLD | | -1.275 | -0.193 | 0. |
| 9 | 0. | INERZIA V SLD | | 1.275 | 0.193 | 0. |
| 9 | 0.69717 | INERZIA V SLD | | 1.275 | 0.193 | 0. |
| 9 | 1.39435 | INERZIA V SLD | | 1.275 | 0.193 | 0. |
| 9 | 0. | INERZIA V -1 | | 2.888 | 0.438 | 0. |
| 9 | 0.69717 | INERZIA V -1 | | 2.888 | 0.438 | 0. |
| 9 | 1.39435 | INERZIA V -1 | | 2.888 | 0.438 | 0. |
| 9 | 0. | SLU_1 | Max | -1924.784 | -551.124 | 0. |
| 9 | 0.69717 | SLU_1 | Max | -1832.012 | -366.724 | 0. |
| 9 | 1.39435 | SLU_1 | Max | -1742.049 | -191.102 | 0. |
| 9 | 0. | SLU_1 | Min | -1924.784 | -551.124 | 0. |
| 9 | 0.69717 | SLU_1 | Min | -1832.012 | -366.724 | 0. |
| 9 | 1.39435 | SLU_1 | Min | -1742.049 | -191.102 | 0. |
| 9 | 0. | SLU_2 | Max | -1928.265 | -544.967 | 0. |
| 9 | 0.69717 | SLU_2 | Max | -1825.657 | -377.265 | 0. |
| 9 | 1.39435 | SLU_2 | Max | -1725.876 | -218.309 | 0. |
| 9 | 0. | SLU_2 | Min | -1928.265 | -544.967 | 0. |
| 9 | 0.69717 | SLU_2 | Min | -1825.657 | -377.265 | 0. |
| 9 | 1.39435 | SLU_2 | Min | -1725.876 | -218.309 | 0. |
| 9 | 0. | SLU_3 | Max | -2277.599 | -796.072 | 0. |
| 9 | 0.69717 | SLU_3 | Max | -2141.71 | -551.935 | 0. |
| 9 | 1.39435 | SLU_3 | Max | -2017.302 | -325.418 | 0. |
| 9 | 0. | SLU_3 | Min | -2277.599 | -796.072 | 0. |
| 9 | 0.69717 | SLU_3 | Min | -2141.71 | -551.935 | 0. |
| 9 | 1.39435 | SLU_3 | Min | -2017.302 | -325.418 | 0. |
| 9 | 0. | SLU_4 | Max | -2312.55 | -767.662 | 0. |
| 9 | 0.69717 | SLU_4 | Max | -2162.008 | -548.4 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 9 | 1.39435 | SLU_4 | Max | -2023.883 | -345.17 | 0. |
| 9 | 0. | SLU_4 | Min | -2312.55 | -767.662 | 0. |
| 9 | 0.69717 | SLU_4 | Min | -2162.008 | -548.4 | 0. |
| 9 | 1.39435 | SLU_4 | Min | -2023.883 | -345.17 | 0. |
| 9 | 0. | SLE_F1 | Max | -1400.908 | -403.98 | 0. |
| 9 | 0.69717 | SLE_F1 | Max | -1332.967 | -267.417 | 0. |
| 9 | 1.39435 | SLE_F1 | Max | -1267.188 | -137.607 | 0. |
| 9 | 0. | SLE_F1 | Min | -1400.908 | -403.98 | 0. |
| 9 | 0.69717 | SLE_F1 | Min | -1332.967 | -267.417 | 0. |
| 9 | 1.39435 | SLE_F1 | Min | -1267.188 | -137.607 | 0. |
| 9 | 0. | SLE_F2 | Max | -1402.685 | -400.626 | 0. |
| 9 | 0.69717 | SLE_F2 | Max | -1327.654 | -276.1 | 0. |
| 9 | 1.39435 | SLE_F2 | Max | -1254.799 | -158.302 | 0. |
| 9 | 0. | SLE_F2 | Min | -1402.685 | -400.626 | 0. |
| 9 | 0.69717 | SLE_F2 | Min | -1327.654 | -276.1 | 0. |
| 9 | 1.39435 | SLE_F2 | Min | -1254.799 | -158.302 | 0. |
| 9 | 0. | SLE_F3 | Max | -1698.581 | -571.484 | 0. |
| 9 | 0.69717 | SLE_F3 | Max | -1586.678 | -407.297 | 0. |
| 9 | 1.39435 | SLE_F3 | Max | -1484.326 | -255.442 | 0. |
| 9 | 0. | SLE_F3 | Min | -1698.581 | -571.484 | 0. |
| 9 | 0.69717 | SLE_F3 | Min | -1586.678 | -407.297 | 0. |
| 9 | 1.39435 | SLE_F3 | Min | -1484.326 | -255.442 | 0. |
| 9 | 0. | SLE_F4 | Max | -1674.06 | -589.709 | 0. |
| 9 | 0.69717 | SLE_F4 | Max | -1572.953 | -407.195 | 0. |
| 9 | 1.39435 | SLE_F4 | Max | -1480.677 | -238.236 | 0. |
| 9 | 0. | SLE_F4 | Min | -1674.06 | -589.709 | 0. |
| 9 | 0.69717 | SLE_F4 | Min | -1572.953 | -407.195 | 0. |
| 9 | 1.39435 | SLE_F4 | Min | -1480.677 | -238.236 | 0. |
| 9 | 0. | SLE_QP1 | Max | -1252.356 | -367.345 | 0. |
| 9 | 0.69717 | SLE_QP1 | Max | -1190.772 | -240.596 | 0. |
| 9 | 1.39435 | SLE_QP1 | Max | -1131.35 | -120.599 | 0. |
| 9 | 0. | SLE_QP1 | Min | -1252.356 | -367.345 | 0. |
| 9 | 0.69717 | SLE_QP1 | Min | -1190.772 | -240.596 | 0. |
| 9 | 1.39435 | SLE_QP1 | Min | -1131.35 | -120.599 | 0. |
| 9 | 0. | SLE_QP2 | Max | -1253.009 | -366.118 | 0. |
| 9 | 0.69717 | SLE_QP2 | Max | -1185.219 | -249.905 | 0. |
| 9 | 1.39435 | SLE_QP2 | Max | -1119.604 | -140.421 | 0. |
| 9 | 0. | SLE_QP2 | Min | -1253.009 | -366.118 | 0. |
| 9 | 0.69717 | SLE_QP2 | Min | -1185.219 | -249.905 | 0. |
| 9 | 1.39435 | SLE_QP2 | Min | -1119.604 | -140.421 | 0. |
| 9 | 0. | SLE_QP3 | Max | -1549.445 | -536.15 | 0. |
| 9 | 0.69717 | SLE_QP3 | Max | -1444.782 | -380.277 | 0. |
| 9 | 1.39435 | SLE_QP3 | Max | -1349.671 | -236.735 | 0. |
| 9 | 0. | SLE_QP3 | Min | -1549.445 | -536.15 | 0. |
| 9 | 0.69717 | SLE_QP3 | Min | -1444.782 | -380.277 | 0. |
| 9 | 1.39435 | SLE_QP3 | Min | -1349.671 | -236.735 | 0. |
| 9 | 0. | SLE_QP4 | Max | -1529.787 | -547.177 | 0. |
| 9 | 0.69717 | SLE_QP4 | Max | -1435.037 | -374.476 | 0. |
| 9 | 1.39435 | SLE_QP4 | Max | -1349.118 | -215.33 | 0. |
| 9 | 0. | SLE_QP4 | Min | -1529.787 | -547.177 | 0. |
| 9 | 0.69717 | SLE_QP4 | Min | -1435.037 | -374.476 | 0. |
| 9 | 1.39435 | SLE_QP4 | Min | -1349.118 | -215.33 | 0. |
| 9 | 0. | SLV_1 | Max | -1094.837 | -439.681 | 0. |
| 9 | 0.69717 | SLV_1 | Max | -1057.93 | -271.038 | 0. |
| 9 | 1.39435 | SLV_1 | Max | -1023.185 | -109.149 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 9 | 0. | SLV_1 | Min | -1094.837 | -439.681 | 0. |
| 9 | 0.69717 | SLV_1 | Min | -1057.93 | -271.038 | 0. |
| 9 | 1.39435 | SLV_1 | Min | -1023.185 | -109.149 | 0. |
| 9 | 0. | SLV_2 | Max | -1088.127 | -438.134 | 0. |
| 9 | 0.69717 | SLV_2 | Max | -1051.221 | -269.492 | 0. |
| 9 | 1.39435 | SLV_2 | Max | -1016.476 | -107.602 | 0. |
| 9 | 0. | SLV_2 | Min | -1088.127 | -438.134 | 0. |
| 9 | 0.69717 | SLV_2 | Min | -1051.221 | -269.492 | 0. |
| 9 | 1.39435 | SLV_2 | Min | -1016.476 | -107.602 | 0. |
| 9 | 0. | SLV_3 | Max | -1412.362 | -585.925 | 0. |
| 9 | 0.69717 | SLV_3 | Max | -1342.289 | -371.332 | 0. |
| 9 | 1.39435 | SLV_3 | Max | -1281.048 | -170.292 | 0. |
| 9 | 0. | SLV_3 | Min | -1412.362 | -585.925 | 0. |
| 9 | 0.69717 | SLV_3 | Min | -1342.289 | -371.332 | 0. |
| 9 | 1.39435 | SLV_3 | Min | -1281.048 | -170.292 | 0. |
| 9 | 0. | SLV_4 | Max | -1405.416 | -584.268 | 0. |
| 9 | 0.69717 | SLV_4 | Max | -1335.343 | -369.674 | 0. |
| 9 | 1.39435 | SLV_4 | Max | -1274.102 | -168.635 | 0. |
| 9 | 0. | SLV_4 | Min | -1405.416 | -584.268 | 0. |
| 9 | 0.69717 | SLV_4 | Min | -1335.343 | -369.674 | 0. |
| 9 | 1.39435 | SLV_4 | Min | -1274.102 | -168.635 | 0. |
| 9 | 0. | SLD_1 | Max | -1154.345 | -419.861 | 0. |
| 9 | 0.69717 | SLD_1 | Max | -1103.66 | -274.61 | 0. |
| 9 | 1.39435 | SLD_1 | Max | -1055.135 | -136.111 | 0. |
| 9 | 0. | SLD_1 | Min | -1154.345 | -419.861 | 0. |
| 9 | 0.69717 | SLD_1 | Min | -1103.66 | -274.61 | 0. |
| 9 | 1.39435 | SLD_1 | Min | -1055.135 | -136.111 | 0. |
| 9 | 0. | SLD_2 | Max | -1150.941 | -419.366 | 0. |
| 9 | 0.69717 | SLD_2 | Max | -1100.255 | -274.115 | 0. |
| 9 | 1.39435 | SLD_2 | Max | -1051.731 | -135.616 | 0. |
| 9 | 0. | SLD_2 | Min | -1150.941 | -419.366 | 0. |
| 9 | 0.69717 | SLD_2 | Min | -1100.255 | -274.115 | 0. |
| 9 | 1.39435 | SLD_2 | Min | -1051.731 | -135.616 | 0. |
| 9 | 0. | SLD_3 | Max | -1468.364 | -564.243 | 0. |
| 9 | 0.69717 | SLD_3 | Max | -1384.513 | -373.04 | 0. |
| 9 | 1.39435 | SLD_3 | Max | -1309.492 | -195.392 | 0. |
| 9 | 0. | SLD_3 | Min | -1468.364 | -564.243 | 0. |
| 9 | 0.69717 | SLD_3 | Min | -1384.513 | -373.04 | 0. |
| 9 | 1.39435 | SLD_3 | Min | -1309.492 | -195.392 | 0. |
| 9 | 0. | SLD_4 | Max | -1465.181 | -563.554 | 0. |
| 9 | 0.69717 | SLD_4 | Max | -1381.329 | -372.351 | 0. |
| 9 | 1.39435 | SLD_4 | Max | -1306.309 | -194.703 | 0. |
| 9 | 0. | SLD_4 | Min | -1465.181 | -563.554 | 0. |
| 9 | 0.69717 | SLD_4 | Min | -1381.329 | -372.351 | 0. |
| 9 | 1.39435 | SLD_4 | Min | -1306.309 | -194.703 | 0. |
| 9 | 0. | SLU_IDR_1 | Max | -1441.526 | -515.911 | 0. |
| 9 | 0.69717 | SLU_IDR_1 | Max | -1347.33 | -365.849 | 0. |
| 9 | 1.39435 | SLU_IDR_1 | Max | -1261.73 | -227.568 | 0. |
| 9 | 0. | SLU_IDR_1 | Min | -1441.526 | -515.911 | 0. |
| 9 | 0.69717 | SLU_IDR_1 | Min | -1347.33 | -365.849 | 0. |
| 9 | 1.39435 | SLU_IDR_1 | Min | -1261.73 | -227.568 | 0. |
| 9 | 0. | SLU_IDR_2 | Max | -1173.521 | -364.695 | 0. |
| 9 | 0.69717 | SLU_IDR_2 | Max | -1112.51 | -250.327 | 0. |
| 9 | 1.39435 | SLU_IDR_2 | Max | -1053.456 | -142.699 | 0. |
| 9 | 0. | SLU_IDR_2 | Min | -1173.521 | -364.695 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 9 | 0.69717 | SLU_IDR_2 | Min | -1112.51 | -250.327 | 0. |
| 9 | 1.39435 | SLU_IDR_2 | Min | -1053.456 | -142.699 | 0. |
| 9 | 0. | SISMA WOOD SLV-1 | Max | -31.216 | -1.905 | 0. |
| 9 | 0.69717 | SISMA WOOD SLV-1 | Max | -55.894 | 39.988 | 0. |
| 9 | 1.39435 | SISMA WOOD SLV-1 | Max | -80.571 | 81.881 | 0. |
| 9 | 0. | SISMA WOOD SLV-1 | Min | -31.216 | -1.905 | 0. |
| 9 | 0.69717 | SISMA WOOD SLV-1 | Min | -55.894 | 39.988 | 0. |
| 9 | 1.39435 | SISMA WOOD SLV-1 | Min | -80.571 | 81.881 | 0. |
| 9 | 0. | DEAD-1 | Max | -264.193 | -46.001 | 0. |
| 9 | 0.69717 | DEAD-1 | Max | -246.177 | -35.389 | 0. |
| 9 | 1.39435 | DEAD-1 | Max | -228.161 | -24.777 | 0. |
| 9 | 0. | DEAD-1 | Min | -264.193 | -46.001 | 0. |
| 9 | 0.69717 | DEAD-1 | Min | -246.177 | -35.389 | 0. |
| 9 | 1.39435 | DEAD-1 | Min | -228.161 | -24.777 | 0. |
| 9 | 0. | SLU_PROVA | | -1712.985 | -511.233 | 0. |
| 9 | 0.69717 | SLU_PROVA | | -1620.213 | -326.833 | 0. |
| 9 | 1.39435 | SLU_PROVA | | -1530.25 | -151.211 | 0. |
| 10 | 0. | DEAD | | -157.76 | -42.171 | 0. |
| 10 | 1.03974 | DEAD | | -137.224 | -26.247 | 0. |
| 10 | 2.07949 | DEAD | | -116.689 | -10.323 | 0. |
| 10 | 0. | SIMM_KA | | -44.201 | 27.43 | 0. |
| 10 | 1.03974 | SIMM_KA | | -62.556 | 51.1 | 0. |
| 10 | 2.07949 | SIMM_KA | | -79.264 | 72.646 | 0. |
| 10 | 0. | SIMM_K0 | | -65.817 | 39.54 | 0. |
| 10 | 1.03974 | SIMM_K0 | | -94.814 | 76.933 | 0. |
| 10 | 2.07949 | SIMM_K0 | | -121.172 | 110.925 | 0. |
| 10 | 0. | A--SIMM_KA | | -11.476 | 23.214 | 0. |
| 10 | 1.03974 | A--SIMM_KA | | -42.317 | 62.986 | 0. |
| 10 | 2.07949 | A--SIMM_KA | | -71.203 | 100.236 | 0. |
| 10 | 0. | A--SIMM_K0 | | -18.961 | 35.98 | 0. |
| 10 | 1.03974 | A--SIMM_K0 | | -65.234 | 95.652 | 0. |
| 10 | 2.07949 | A--SIMM_K0 | | -108.608 | 151.586 | 0. |
| 10 | 0. | A-- SIMM_SOVR_K A | | -3.726 | 0.595 | 0. |
| 10 | 1.03974 | A-- SIMM_SOVR_K A | | -7.976 | 6.076 | 0. |
| 10 | 2.07949 | A-- SIMM_SOVR_K A | | -12.226 | 11.556 | 0. |
| 10 | 0. | A-- SIMM_SOVR_K 0 | | -5.587 | 0.893 | 0. |
| 10 | 1.03974 | A-- SIMM_SOVR_K 0 | | -11.958 | 9.109 | 0. |
| 10 | 2.07949 | A-- SIMM_SOVR_K 0 | | -18.33 | 17.326 | 0. |
| 10 | 0. | SIMM_SOVR_K 0 | | -5.587 | 0.893 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|----------|----------|
| 10 | 1.03974 | SIMM_SOVR_K 0 | | -11.958 | 9.109 | 0. |
| 10 | 2.07949 | SIMM_SOVR_K 0 | | -18.33 | 17.326 | 0. |
| 10 | 0. | SIMM_SOVR_K A | | -3.726 | 0.595 | 0. |
| 10 | 1.03974 | SIMM_SOVR_K A | | -7.976 | 6.076 | 0. |
| 10 | 2.07949 | SIMM_SOVR_K A | | -12.226 | 11.556 | 0. |
| 10 | 0. | SOVR | | -140.451 | -43.25 | 0. |
| 10 | 1.03974 | SOVR | | -124.018 | -30.507 | 0. |
| 10 | 2.07949 | SOVR | | -107.585 | -17.764 | 0. |
| 10 | 0. | TERR_SIMM | | -477.136 | -164.241 | 0. |
| 10 | 1.03974 | TERR_SIMM | | -402.103 | -106.056 | 0. |
| 10 | 2.07949 | TERR_SIMM | | -333.38 | -52.765 | 0. |
| 10 | 0. | TERR_A--SIMM | | -699.245 | -264.03 | 0. |
| 10 | 1.03974 | TERR_A--SIMM | | -579.915 | -171.495 | 0. |
| 10 | 2.07949 | TERR_A--SIMM | | -468.107 | -84.793 | 0. |
| 10 | 0. | INERZIA H SLV | | 5.502 | -1.088 | 0. |
| 10 | 1.03974 | INERZIA H SLV | | 5.502 | -1.088 | 0. |
| 10 | 2.07949 | INERZIA H SLV | | 5.502 | -1.088 | 0. |
| 10 | 0. | INERZIA V + SLV | | -2.206 | -0.44 | 0. |
| 10 | 1.03974 | INERZIA V + SLV | | -2.206 | -0.44 | 0. |
| 10 | 2.07949 | INERZIA V + SLV | | -2.206 | -0.44 | 0. |
| 10 | 0. | INERZIA V - SLV | | 2.206 | 0.44 | 0. |
| 10 | 1.03974 | INERZIA V - SLV | | 2.206 | 0.44 | 0. |
| 10 | 2.07949 | INERZIA V - SLV | | 2.206 | 0.44 | 0. |
| 10 | 0. | SISMA WOOD SLV | | 222.328 | -63.787 | 0. |
| 10 | 1.03974 | SISMA WOOD SLV | | 177.894 | -6.486 | 0. |
| 10 | 2.07949 | SISMA WOOD SLV | | 133.459 | 50.816 | 0. |
| 10 | 0. | iDROSTATICA | | -282.911 | -65.466 | 0. |
| 10 | 1.03974 | iDROSTATICA | | -282.911 | -4.049 | 0. |
| 10 | 2.07949 | iDROSTATICA | | -282.911 | 49.696 | 0. |
| 10 | 0. | SISMA WOOD SLD | | 98.189 | -28.171 | 0. |
| 10 | 1.03974 | SISMA WOOD SLD | | 78.565 | -2.864 | 0. |
| 10 | 2.07949 | SISMA WOOD SLD | | 58.941 | 22.443 | 0. |
| 10 | 0. | INERZIA H SLD | | 2.43 | -0.481 | 0. |
| 10 | 1.03974 | INERZIA H SLD | | 2.43 | -0.481 | 0. |
| 10 | 2.07949 | INERZIA H SLD | | 2.43 | -0.481 | 0. |
| 10 | 0. | INERZIA V + SLD | | -0.974 | -0.194 | 0. |
| 10 | 1.03974 | INERZIA V + SLD | | -0.974 | -0.194 | 0. |
| 10 | 2.07949 | INERZIA V + SLD | | -0.974 | -0.194 | 0. |
| 10 | 0. | INERZIA V SLD | | 0.974 | 0.194 | 0. |
| 10 | 1.03974 | INERZIA V SLD | | 0.974 | 0.194 | 0. |
| 10 | 2.07949 | INERZIA V SLD | | 0.974 | 0.194 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------|----------|-----------|----------|----------|
| 10 | 0. | INERZIA V -1 | | 2.206 | 0.44 | 0. |
| 10 | 1.03974 | INERZIA V -1 | | 2.206 | 0.44 | 0. |
| 10 | 2.07949 | INERZIA V -1 | | 2.206 | 0.44 | 0. |
| 10 | 0. | SLU_1 | Max | -1703.71 | -410.641 | 0. |
| 10 | 1.03974 | SLU_1 | Max | -1602.075 | -154.406 | 0. |
| 10 | 2.07949 | SLU_1 | Max | -1505.214 | 81.07 | 0. |
| 10 | 0. | SLU_1 | Min | -1703.71 | -410.641 | 0. |
| 10 | 1.03974 | SLU_1 | Min | -1602.075 | -154.406 | 0. |
| 10 | 2.07949 | SLU_1 | Min | -1505.214 | 81.07 | 0. |
| 10 | 0. | SLU_2 | Max | -1684.215 | -435.574 | 0. |
| 10 | 1.03974 | SLU_2 | Max | -1565.563 | -201.285 | 0. |
| 10 | 2.07949 | SLU_2 | Max | -1452.973 | 13.908 | 0. |
| 10 | 0. | SLU_2 | Min | -1684.215 | -435.574 | 0. |
| 10 | 1.03974 | SLU_2 | Min | -1565.563 | -201.285 | 0. |
| 10 | 2.07949 | SLU_2 | Min | -1452.973 | 13.908 | 0. |
| 10 | 0. | SLU_3 | Max | -1959.692 | -578.812 | 0. |
| 10 | 1.03974 | SLU_3 | Max | -1822.929 | -248.959 | 0. |
| 10 | 2.07949 | SLU_3 | Max | -1692.177 | 58.476 | 0. |
| 10 | 0. | SLU_3 | Min | -1959.692 | -578.812 | 0. |
| 10 | 1.03974 | SLU_3 | Min | -1822.929 | -248.959 | 0. |
| 10 | 2.07949 | SLU_3 | Min | -1692.177 | 58.476 | 0. |
| 10 | 0. | SLU_4 | Max | -1963.713 | -599.236 | 0. |
| 10 | 1.03974 | SLU_4 | Max | -1803.706 | -299.358 | 0. |
| 10 | 2.07949 | SLU_4 | Max | -1650.936 | -20.317 | 0. |
| 10 | 0. | SLU_4 | Min | -1963.713 | -599.236 | 0. |
| 10 | 1.03974 | SLU_4 | Min | -1803.706 | -299.358 | 0. |
| 10 | 2.07949 | SLU_4 | Min | -1650.936 | -20.317 | 0. |
| 10 | 0. | SLE_F1 | Max | -1239.478 | -297.314 | 0. |
| 10 | 1.03974 | SLE_F1 | Max | -1165.36 | -108.675 | 0. |
| 10 | 2.07949 | SLE_F1 | Max | -1094.915 | 63.996 | 0. |
| 10 | 0. | SLE_F1 | Min | -1239.478 | -297.314 | 0. |
| 10 | 1.03974 | SLE_F1 | Min | -1165.36 | -108.675 | 0. |
| 10 | 2.07949 | SLE_F1 | Min | -1094.915 | 63.996 | 0. |
| 10 | 0. | SLE_F2 | Max | -1224.563 | -316.268 | 0. |
| 10 | 1.03974 | SLE_F2 | Max | -1138.212 | -143.405 | 0. |
| 10 | 2.07949 | SLE_F2 | Max | -1056.524 | 14.768 | 0. |
| 10 | 0. | SLE_F2 | Min | -1224.563 | -316.268 | 0. |
| 10 | 1.03974 | SLE_F2 | Min | -1138.212 | -143.405 | 0. |
| 10 | 2.07949 | SLE_F2 | Min | -1056.524 | 14.768 | 0. |
| 10 | 0. | SLE_F3 | Max | -1439.906 | -441.757 | 0. |
| 10 | 1.03974 | SLE_F3 | Max | -1321.744 | -218.441 | 0. |
| 10 | 2.07949 | SLE_F3 | Max | -1209.149 | -11.154 | 0. |
| 10 | 0. | SLE_F3 | Min | -1439.906 | -441.757 | 0. |
| 10 | 1.03974 | SLE_F3 | Min | -1321.744 | -218.441 | 0. |
| 10 | 2.07949 | SLE_F3 | Min | -1209.149 | -11.154 | 0. |
| 10 | 0. | SLE_F4 | Max | -1438.47 | -424.229 | 0. |
| 10 | 1.03974 | SLE_F4 | Max | -1337.331 | -178.96 | 0. |
| 10 | 2.07949 | SLE_F4 | Max | -1240.816 | 49.063 | 0. |
| 10 | 0. | SLE_F4 | Min | -1438.47 | -424.229 | 0. |
| 10 | 1.03974 | SLE_F4 | Min | -1337.331 | -178.96 | 0. |
| 10 | 2.07949 | SLE_F4 | Min | -1240.816 | 49.063 | 0. |
| 10 | 0. | SLE_QP1 | Max | -1106.896 | -263.218 | 0. |
| 10 | 1.03974 | SLE_QP1 | Max | -1040.324 | -90.298 | 0. |
| 10 | 2.07949 | SLE_QP1 | Max | -977.425 | 66.653 | 0. |
| 10 | 0. | SLE_QP1 | Min | -1106.896 | -263.218 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 10 | 1.03974 | SLE_QP1 | Min | -1040.324 | -90.298 | 0. |
| 10 | 2.07949 | SLE_QP1 | Min | -977.425 | 66.653 | 0. |
| 10 | 0. | SLE_QP2 | Max | -1092.73 | -281.374 | 0. |
| 10 | 1.03974 | SLE_QP2 | Max | -1015.516 | -122.178 | 0. |
| 10 | 2.07949 | SLE_QP2 | Max | -942.966 | 22.328 | 0. |
| 10 | 0. | SLE_QP2 | Min | -1092.73 | -281.374 | 0. |
| 10 | 1.03974 | SLE_QP2 | Min | -1015.516 | -122.178 | 0. |
| 10 | 2.07949 | SLE_QP2 | Min | -942.966 | 22.328 | 0. |
| 10 | 0. | SLE_QP3 | Max | -1308.714 | -406.112 | 0. |
| 10 | 1.03974 | SLE_QP3 | Max | -1199.69 | -196.463 | 0. |
| 10 | 2.07949 | SLE_QP3 | Max | -1096.231 | -2.843 | 0. |
| 10 | 0. | SLE_QP3 | Min | -1308.714 | -406.112 | 0. |
| 10 | 1.03974 | SLE_QP3 | Min | -1199.69 | -196.463 | 0. |
| 10 | 2.07949 | SLE_QP3 | Min | -1096.231 | -2.843 | 0. |
| 10 | 0. | SLE_QP4 | Max | -1310.882 | -384.812 | 0. |
| 10 | 1.03974 | SLE_QP4 | Max | -1217.289 | -155.263 | 0. |
| 10 | 2.07949 | SLE_QP4 | Max | -1128.32 | 57.041 | 0. |
| 10 | 0. | SLE_QP4 | Min | -1310.882 | -384.812 | 0. |
| 10 | 1.03974 | SLE_QP4 | Min | -1217.289 | -155.263 | 0. |
| 10 | 2.07949 | SLE_QP4 | Min | -1128.32 | 57.041 | 0. |
| 10 | 0. | SLV_1 | Max | -1001.389 | -236.47 | 0. |
| 10 | 1.03974 | SLV_1 | Max | -979.252 | -6.249 | 0. |
| 10 | 2.07949 | SLV_1 | Max | -960.788 | 208.005 | 0. |
| 10 | 0. | SLV_1 | Min | -1001.389 | -236.47 | 0. |
| 10 | 1.03974 | SLV_1 | Min | -979.252 | -6.249 | 0. |
| 10 | 2.07949 | SLV_1 | Min | -960.788 | 208.005 | 0. |
| 10 | 0. | SLV_2 | Max | -996.128 | -235.013 | 0. |
| 10 | 1.03974 | SLV_2 | Max | -973.991 | -4.792 | 0. |
| 10 | 2.07949 | SLV_2 | Max | -955.527 | 209.461 | 0. |
| 10 | 0. | SLV_2 | Min | -996.128 | -235.013 | 0. |
| 10 | 1.03974 | SLV_2 | Min | -973.991 | -4.792 | 0. |
| 10 | 2.07949 | SLV_2 | Min | -955.527 | 209.461 | 0. |
| 10 | 0. | SLV_3 | Max | -1249.407 | -329.848 | 0. |
| 10 | 1.03974 | SLV_3 | Max | -1200.249 | -42.998 | 0. |
| 10 | 2.07949 | SLV_3 | Max | -1155.715 | 226.608 | 0. |
| 10 | 0. | SLV_3 | Min | -1249.407 | -329.848 | 0. |
| 10 | 1.03974 | SLV_3 | Min | -1200.249 | -42.998 | 0. |
| 10 | 2.07949 | SLV_3 | Min | -1155.715 | 226.608 | 0. |
| 10 | 0. | SLV_4 | Max | -1243.925 | -328.252 | 0. |
| 10 | 1.03974 | SLV_4 | Max | -1194.768 | -41.401 | 0. |
| 10 | 2.07949 | SLV_4 | Max | -1150.233 | 228.205 | 0. |
| 10 | 0. | SLV_4 | Min | -1243.925 | -328.252 | 0. |
| 10 | 1.03974 | SLV_4 | Min | -1194.768 | -41.401 | 0. |
| 10 | 2.07949 | SLV_4 | Min | -1150.233 | 228.205 | 0. |
| 10 | 0. | SLD_1 | Max | -1029.475 | -268.195 | 0. |
| 10 | 1.03974 | SLD_1 | Max | -982.528 | -69.969 | 0. |
| 10 | 2.07949 | SLD_1 | Max | -939.253 | 112.289 | 0. |
| 10 | 0. | SLD_1 | Min | -1029.475 | -268.195 | 0. |
| 10 | 1.03974 | SLD_1 | Min | -982.528 | -69.969 | 0. |
| 10 | 2.07949 | SLD_1 | Min | -939.253 | 112.289 | 0. |
| 10 | 0. | SLD_2 | Max | -1026.69 | -267.682 | 0. |
| 10 | 1.03974 | SLD_2 | Max | -979.743 | -69.456 | 0. |
| 10 | 2.07949 | SLD_2 | Max | -936.468 | 112.802 | 0. |
| 10 | 0. | SLD_2 | Min | -1026.69 | -267.682 | 0. |
| 10 | 1.03974 | SLD_2 | Min | -979.743 | -69.456 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 10 | 2.07949 | SLD_2 | Min | -936.468 | 112.802 | 0. |
| 10 | 0. | SLD_3 | Max | -1274.251 | -359.286 | 0. |
| 10 | 1.03974 | SLD_3 | Max | -1200.283 | -104.43 | 0. |
| 10 | 2.07949 | SLD_3 | Max | -1130.938 | 133.181 | 0. |
| 10 | 0. | SLD_3 | Min | -1274.251 | -359.286 | 0. |
| 10 | 1.03974 | SLD_3 | Min | -1200.283 | -104.43 | 0. |
| 10 | 2.07949 | SLD_3 | Min | -1130.938 | 133.181 | 0. |
| 10 | 0. | SLD_4 | Max | -1271.71 | -358.609 | 0. |
| 10 | 1.03974 | SLD_4 | Max | -1197.742 | -103.753 | 0. |
| 10 | 2.07949 | SLD_4 | Max | -1128.397 | 133.858 | 0. |
| 10 | 0. | SLD_4 | Min | -1271.71 | -358.609 | 0. |
| 10 | 1.03974 | SLD_4 | Min | -1197.742 | -103.753 | 0. |
| 10 | 2.07949 | SLD_4 | Min | -1128.397 | 133.858 | 0. |
| 10 | 0. | SLU_IDR_1 | Max | -1222.647 | -385.858 | 0. |
| 10 | 1.03974 | SLU_IDR_1 | Max | -1124.525 | -184.89 | 0. |
| 10 | 2.07949 | SLU_IDR_1 | Max | -1031.413 | 0.116 | 0. |
| 10 | 0. | SLU_IDR_1 | Min | -1222.647 | -385.858 | 0. |
| 10 | 1.03974 | SLU_IDR_1 | Min | -1124.525 | -184.89 | 0. |
| 10 | 2.07949 | SLU_IDR_1 | Min | -1031.413 | 0.116 | 0. |
| 10 | 0. | SLU_IDR_2 | Max | -1026.828 | -275.238 | 0. |
| 10 | 1.03974 | SLU_IDR_2 | Max | -957.336 | -119.678 | 0. |
| 10 | 2.07949 | SLU_IDR_2 | Max | -892.041 | 21.126 | 0. |
| 10 | 0. | SLU_IDR_2 | Min | -1026.828 | -275.238 | 0. |
| 10 | 1.03974 | SLU_IDR_2 | Min | -957.336 | -119.678 | 0. |
| 10 | 2.07949 | SLU_IDR_2 | Min | -892.041 | 21.126 | 0. |
| 10 | 0. | SISMA WOOD SLV-1 | Max | -90.311 | 70.994 | 0. |
| 10 | 1.03974 | SISMA WOOD SLV-1 | Max | -134.746 | 128.295 | 0. |
| 10 | 2.07949 | SISMA WOOD SLV-1 | Max | -179.181 | 185.597 | 0. |
| 10 | 0. | SISMA WOOD SLV-1 | Min | -90.311 | 70.994 | 0. |
| 10 | 1.03974 | SISMA WOOD SLV-1 | Min | -134.746 | 128.295 | 0. |
| 10 | 2.07949 | SISMA WOOD SLV-1 | Min | -179.181 | 185.597 | 0. |
| 10 | 0. | DEAD-1 | Max | -223.172 | -53.533 | 0. |
| 10 | 1.03974 | DEAD-1 | Max | -202.637 | -37.608 | 0. |
| 10 | 2.07949 | DEAD-1 | Max | -182.102 | -21.684 | 0. |
| 10 | 0. | DEAD-1 | Min | -223.172 | -53.533 | 0. |
| 10 | 1.03974 | DEAD-1 | Min | -202.637 | -37.608 | 0. |
| 10 | 2.07949 | DEAD-1 | Min | -182.102 | -21.684 | 0. |
| 10 | 0. | SLU_PROVA | | -1497.766 | -365.576 | 0. |
| 10 | 1.03974 | SLU_PROVA | | -1396.13 | -109.342 | 0. |
| 10 | 2.07949 | SLU_PROVA | | -1299.269 | 126.134 | 0. |
| 11 | 0. | DEAD | | -109.246 | -50.926 | 0. |
| 11 | 1.05223 | DEAD | | -93.093 | -30.173 | 0. |
| 11 | 2.10446 | DEAD | | -76.94 | -9.421 | 0. |
| 11 | 0. | SIMM_KA | | -94.42 | 48.743 | 0. |
| 11 | 1.05223 | SIMM_KA | | -114.415 | 64.306 | 0. |
| 11 | 2.10446 | SIMM_KA | | -132.998 | 78.77 | 0. |
| 11 | 0. | SIMM_K0 | | -144.29 | 74.241 | 0. |
| 11 | 1.05223 | SIMM_K0 | | -176.527 | 99.332 | 0. |
| 11 | 2.10446 | SIMM_K0 | | -207.97 | 123.806 | 0. |
| 11 | 0. | A--SIMM_KA | | -91.732 | 65.401 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 11 | 1.05223 | A--SIMM_KA | | -126.001 | 92.074 | 0. |
| 11 | 2.10446 | A--SIMM_KA | | -156.068 | 115.476 | 0. |
| 11 | 0. | A--SIMM_K0 | | -139.688 | 99.132 | 0. |
| 11 | 1.05223 | A--SIMM_K0 | | -191.153 | 139.19 | 0. |
| 11 | 2.10446 | A--SIMM_K0 | | -236.274 | 174.309 | 0. |
| 11 | 0. | A-- SIMM_SOVR_K A | | -14.622 | 7.626 | 0. |
| 11 | 1.05223 | A-- SIMM_SOVR_K A | | -20.16 | 11.937 | 0. |
| 11 | 2.10446 | A-- SIMM_SOVR_K A | | -25.698 | 16.248 | 0. |
| 11 | 0. | A-- SIMM_SOVR_K 0 | | -21.921 | 11.433 | 0. |
| 11 | 1.05223 | A-- SIMM_SOVR_K 0 | | -30.225 | 17.896 | 0. |
| 11 | 2.10446 | A-- SIMM_SOVR_K 0 | | -38.528 | 24.359 | 0. |
| 11 | 0. | SIMM_SOVR_K 0 | | -21.921 | 11.433 | 0. |
| 11 | 1.05223 | SIMM_SOVR_K 0 | | -30.225 | 17.896 | 0. |
| 11 | 2.10446 | SIMM_SOVR_K 0 | | -38.528 | 24.359 | 0. |
| 11 | 0. | SIMM_SOVR_K A | | -14.622 | 7.626 | 0. |
| 11 | 1.05223 | SIMM_SOVR_K A | | -20.16 | 11.937 | 0. |
| 11 | 2.10446 | SIMM_SOVR_K A | | -25.698 | 16.248 | 0. |
| 11 | 0. | SOVR | | -99.446 | -48.059 | 0. |
| 11 | 1.05223 | SOVR | | -86.52 | -31.452 | 0. |
| 11 | 2.10446 | SOVR | | -73.594 | -14.845 | 0. |
| 11 | 0. | TERR_SIMM | | -308.182 | -151.638 | 0. |
| 11 | 1.05223 | TERR_SIMM | | -259.067 | -88.536 | 0. |
| 11 | 2.10446 | TERR_SIMM | | -214.87 | -31.752 | 0. |
| 11 | 0. | TERR_A--SIMM | | -429.719 | -226.687 | 0. |
| 11 | 1.05223 | TERR_A--SIMM | | -349.652 | -123.819 | 0. |
| 11 | 2.10446 | TERR_A--SIMM | | -279.428 | -33.597 | 0. |
| 11 | 0. | INERZIA H SLV | | 4.452 | 0.019 | 0. |
| 11 | 1.05223 | INERZIA H SLV | | 4.452 | 0.019 | 0. |
| 11 | 2.10446 | INERZIA H SLV | | 4.452 | 0.019 | 0. |
| 11 | 0. | INERZIA V + SLV | | -1.489 | -0.5 | 0. |
| 11 | 1.05223 | INERZIA V + SLV | | -1.489 | -0.5 | 0. |
| 11 | 2.10446 | INERZIA V + SLV | | -1.489 | -0.5 | 0. |
| 11 | 0. | INERZIA V - SLV | | 1.489 | 0.5 | 0. |
| 11 | 1.05223 | INERZIA V - SLV | | 1.489 | 0.5 | 0. |
| 11 | 2.10446 | INERZIA V - SLV | | 1.489 | 0.5 | 0. |
| 11 | 0. | SISMA WOOD SLV | | 124.428 | 27.632 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|-----------|----------|
| 11 | 1.05223 | SISMA WOOD SLV | | 66.52 | 72.705 | 0. |
| 11 | 2.10446 | SISMA WOOD SLV | | 8.611 | 117.778 | 0. |
| 11 | 0. | iDROSTATICA | | -287.064 | -15.762 | 0. |
| 11 | 1.05223 | iDROSTATICA | | -287.064 | 30.888 | 0. |
| 11 | 2.10446 | iDROSTATICA | | -287.064 | 69.826 | 0. |
| 11 | 0. | SISMA WOOD SLD | | 54.953 | 12.204 | 0. |
| 11 | 1.05223 | SISMA WOOD SLD | | 29.378 | 32.11 | 0. |
| 11 | 2.10446 | SISMA WOOD SLD | | 3.803 | 52.016 | 0. |
| 11 | 0. | INERZIA H SLD | | 1.966 | 8.221E-03 | 0. |
| 11 | 1.05223 | INERZIA H SLD | | 1.966 | 8.221E-03 | 0. |
| 11 | 2.10446 | INERZIA H SLD | | 1.966 | 8.221E-03 | 0. |
| 11 | 0. | INERZIA V + SLD | | -0.657 | -0.221 | 0. |
| 11 | 1.05223 | INERZIA V + SLD | | -0.657 | -0.221 | 0. |
| 11 | 2.10446 | INERZIA V + SLD | | -0.657 | -0.221 | 0. |
| 11 | 0. | INERZIA V SLD | | 0.657 | 0.221 | 0. |
| 11 | 1.05223 | INERZIA V SLD | | 0.657 | 0.221 | 0. |
| 11 | 2.10446 | INERZIA V SLD | | 0.657 | 0.221 | 0. |
| 11 | 0. | INERZIA V -1 | | 1.489 | 0.5 | 0. |
| 11 | 1.05223 | INERZIA V -1 | | 1.489 | 0.5 | 0. |
| 11 | 2.10446 | INERZIA V -1 | | 1.489 | 0.5 | 0. |
| 11 | 0. | SLU_1 | Max | -1478.534 | -293.563 | 0. |
| 11 | 1.05223 | SLU_1 | Max | -1428.659 | -56.682 | 0. |
| 11 | 2.10446 | SLU_1 | Max | -1384.146 | 161.154 | 0. |
| 11 | 0. | SLU_1 | Min | -1478.534 | -293.563 | 0. |
| 11 | 1.05223 | SLU_1 | Min | -1428.659 | -56.682 | 0. |
| 11 | 2.10446 | SLU_1 | Min | -1384.146 | 161.154 | 0. |
| 11 | 0. | SLU_2 | Max | -1411.311 | -345.726 | 0. |
| 11 | 1.05223 | SLU_2 | Max | -1341.374 | -124.46 | 0. |
| 11 | 2.10446 | SLU_2 | Max | -1275.996 | 77.136 | 0. |
| 11 | 0. | SLU_2 | Min | -1411.311 | -345.726 | 0. |
| 11 | 1.05223 | SLU_2 | Min | -1341.374 | -124.46 | 0. |
| 11 | 2.10446 | SLU_2 | Min | -1275.996 | 77.136 | 0. |
| 11 | 0. | SLU_3 | Max | -1654.106 | -361.688 | 0. |
| 11 | 1.05223 | SLU_3 | Max | -1588.992 | -53.656 | 0. |
| 11 | 2.10446 | SLU_3 | Max | -1528.426 | 221.491 | 0. |
| 11 | 0. | SLU_3 | Min | -1654.106 | -361.688 | 0. |
| 11 | 1.05223 | SLU_3 | Min | -1588.992 | -53.656 | 0. |
| 11 | 2.10446 | SLU_3 | Min | -1528.426 | 221.491 | 0. |
| 11 | 0. | SLU_4 | Max | -1594.667 | -427.837 | 0. |
| 11 | 1.05223 | SLU_4 | Max | -1503.049 | -140.434 | 0. |
| 11 | 2.10446 | SLU_4 | Max | -1418.766 | 116.252 | 0. |
| 11 | 0. | SLU_4 | Min | -1594.667 | -427.837 | 0. |
| 11 | 1.05223 | SLU_4 | Min | -1503.049 | -140.434 | 0. |
| 11 | 2.10446 | SLU_4 | Min | -1418.766 | 116.252 | 0. |
| 11 | 0. | SLE_F1 | Max | -1076.75 | -208.673 | 0. |
| 11 | 1.05223 | SLE_F1 | Max | -1040.251 | -35.774 | 0. |
| 11 | 2.10446 | SLE_F1 | Max | -1007.877 | 122.476 | 0. |
| 11 | 0. | SLE_F1 | Min | -1076.75 | -208.673 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 11 | 1.05223 | SLE_F1 | Min | -1040.251 | -35.774 | 0. |
| 11 | 2.10446 | SLE_F1 | Min | -1007.877 | 122.476 | 0. |
| 11 | 0. | SLE_F2 | Max | -1027.381 | -246.882 | 0. |
| 11 | 1.05223 | SLE_F2 | Max | -976.566 | -85.126 | 0. |
| 11 | 2.10446 | SLE_F2 | Max | -929.259 | 61.501 | 0. |
| 11 | 0. | SLE_F2 | Min | -1027.381 | -246.882 | 0. |
| 11 | 1.05223 | SLE_F2 | Min | -976.566 | -85.126 | 0. |
| 11 | 2.10446 | SLE_F2 | Min | -929.259 | 61.501 | 0. |
| 11 | 0. | SLE_F3 | Max | -1168.859 | -309.738 | 0. |
| 11 | 1.05223 | SLE_F3 | Max | -1101.367 | -97.106 | 0. |
| 11 | 2.10446 | SLE_F3 | Max | -1039.517 | 91.897 | 0. |
| 11 | 0. | SLE_F3 | Min | -1168.859 | -309.738 | 0. |
| 11 | 1.05223 | SLE_F3 | Min | -1101.367 | -97.106 | 0. |
| 11 | 2.10446 | SLE_F3 | Min | -1039.517 | 91.897 | 0. |
| 11 | 0. | SLE_F4 | Max | -1214.429 | -259.221 | 0. |
| 11 | 1.05223 | SLE_F4 | Max | -1166.208 | -31.59 | 0. |
| 11 | 2.10446 | SLE_F4 | Max | -1121.486 | 170.745 | 0. |
| 11 | 0. | SLE_F4 | Min | -1214.429 | -259.221 | 0. |
| 11 | 1.05223 | SLE_F4 | Min | -1166.208 | -31.59 | 0. |
| 11 | 2.10446 | SLE_F4 | Min | -1121.486 | 170.745 | 0. |
| 11 | 0. | SLE_QP1 | Max | -963.561 | -177.079 | 0. |
| 11 | 1.05223 | SLE_QP1 | Max | -930.529 | -21.482 | 0. |
| 11 | 2.10446 | SLE_QP1 | Max | -901.622 | 119.465 | 0. |
| 11 | 0. | SLE_QP1 | Min | -963.561 | -177.079 | 0. |
| 11 | 1.05223 | SLE_QP1 | Min | -930.529 | -21.482 | 0. |
| 11 | 2.10446 | SLE_QP1 | Min | -901.622 | 119.465 | 0. |
| 11 | 0. | SLE_QP2 | Max | -919.216 | -211.484 | 0. |
| 11 | 1.05223 | SLE_QP2 | Max | -873.943 | -65.415 | 0. |
| 11 | 2.10446 | SLE_QP2 | Max | -832.176 | 65.523 | 0. |
| 11 | 0. | SLE_QP2 | Min | -919.216 | -211.484 | 0. |
| 11 | 1.05223 | SLE_QP2 | Min | -873.943 | -65.415 | 0. |
| 11 | 2.10446 | SLE_QP2 | Min | -832.176 | 65.523 | 0. |
| 11 | 0. | SLE_QP3 | Max | -1061.501 | -273.77 | 0. |
| 11 | 1.05223 | SLE_QP3 | Max | -999.55 | -76.826 | 0. |
| 11 | 2.10446 | SLE_QP3 | Max | -943.24 | 96.488 | 0. |
| 11 | 0. | SLE_QP3 | Min | -1061.501 | -273.77 | 0. |
| 11 | 1.05223 | SLE_QP3 | Min | -999.55 | -76.826 | 0. |
| 11 | 2.10446 | SLE_QP3 | Min | -943.24 | 96.488 | 0. |
| 11 | 0. | SLE_QP4 | Max | -1107.397 | -223.68 | 0. |
| 11 | 1.05223 | SLE_QP4 | Max | -1062.643 | -13.351 | 0. |
| 11 | 2.10446 | SLE_QP4 | Max | -1021.388 | 171.681 | 0. |
| 11 | 0. | SLE_QP4 | Min | -1107.397 | -223.68 | 0. |
| 11 | 1.05223 | SLE_QP4 | Min | -1062.643 | -13.351 | 0. |
| 11 | 2.10446 | SLE_QP4 | Min | -1021.388 | 171.681 | 0. |
| 11 | 0. | SLV_1 | Max | -983.2 | -34.283 | 0. |
| 11 | 1.05223 | SLV_1 | Max | -1008.077 | 166.387 | 0. |
| 11 | 2.10446 | SLV_1 | Max | -1037.079 | 352.407 | 0. |
| 11 | 0. | SLV_1 | Min | -983.2 | -34.283 | 0. |
| 11 | 1.05223 | SLV_1 | Min | -1008.077 | 166.387 | 0. |
| 11 | 2.10446 | SLV_1 | Min | -1037.079 | 352.407 | 0. |
| 11 | 0. | SLV_2 | Max | -979.501 | -32.904 | 0. |
| 11 | 1.05223 | SLV_2 | Max | -1004.377 | 167.765 | 0. |
| 11 | 2.10446 | SLV_2 | Max | -1033.379 | 353.786 | 0. |
| 11 | 0. | SLV_2 | Min | -979.501 | -32.904 | 0. |
| 11 | 1.05223 | SLV_2 | Min | -1004.377 | 167.765 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 11 | 2.10446 | SLV_2 | Min | -1033.379 | 353.786 | 0. |
| 11 | 0. | SLV_3 | Max | -1176.675 | -64.449 | 0. |
| 11 | 1.05223 | SLV_3 | Max | -1189.829 | 190.952 | 0. |
| 11 | 2.10446 | SLV_3 | Max | -1206.483 | 421.057 | 0. |
| 11 | 0. | SLV_3 | Min | -1176.675 | -64.449 | 0. |
| 11 | 1.05223 | SLV_3 | Min | -1189.829 | 190.952 | 0. |
| 11 | 2.10446 | SLV_3 | Min | -1206.483 | 421.057 | 0. |
| 11 | 0. | SLV_4 | Max | -1172.797 | -62.881 | 0. |
| 11 | 1.05223 | SLV_4 | Max | -1185.951 | 192.521 | 0. |
| 11 | 2.10446 | SLV_4 | Max | -1202.604 | 422.625 | 0. |
| 11 | 0. | SLV_4 | Min | -1172.797 | -62.881 | 0. |
| 11 | 1.05223 | SLV_4 | Min | -1185.951 | 192.521 | 0. |
| 11 | 2.10446 | SLV_4 | Min | -1202.604 | 422.625 | 0. |
| 11 | 0. | SLD_1 | Max | -938.216 | -122.656 | 0. |
| 11 | 1.05223 | SLD_1 | Max | -930.759 | 52.847 | 0. |
| 11 | 2.10446 | SLD_1 | Max | -927.427 | 213.701 | 0. |
| 11 | 0. | SLD_1 | Min | -938.216 | -122.656 | 0. |
| 11 | 1.05223 | SLD_1 | Min | -930.759 | 52.847 | 0. |
| 11 | 2.10446 | SLD_1 | Min | -927.427 | 213.701 | 0. |
| 11 | 0. | SLD_2 | Max | -936.103 | -122.059 | 0. |
| 11 | 1.05223 | SLD_2 | Max | -928.646 | 53.444 | 0. |
| 11 | 2.10446 | SLD_2 | Max | -925.314 | 214.297 | 0. |
| 11 | 0. | SLD_2 | Min | -936.103 | -122.059 | 0. |
| 11 | 1.05223 | SLD_2 | Min | -928.646 | 53.444 | 0. |
| 11 | 2.10446 | SLD_2 | Min | -925.314 | 214.297 | 0. |
| 11 | 0. | SLD_3 | Max | -1129.115 | -149.811 | 0. |
| 11 | 1.05223 | SLD_3 | Max | -1109.935 | 80.424 | 0. |
| 11 | 2.10446 | SLD_3 | Max | -1094.255 | 285.362 | 0. |
| 11 | 0. | SLD_3 | Min | -1129.115 | -149.811 | 0. |
| 11 | 1.05223 | SLD_3 | Min | -1109.935 | 80.424 | 0. |
| 11 | 2.10446 | SLD_3 | Min | -1094.255 | 285.362 | 0. |
| 11 | 0. | SLD_4 | Max | -1127.279 | -149.115 | 0. |
| 11 | 1.05223 | SLD_4 | Max | -1108.099 | 81.12 | 0. |
| 11 | 2.10446 | SLD_4 | Max | -1092.419 | 286.057 | 0. |
| 11 | 0. | SLD_4 | Min | -1127.279 | -149.115 | 0. |
| 11 | 1.05223 | SLD_4 | Min | -1108.099 | 81.12 | 0. |
| 11 | 2.10446 | SLD_4 | Min | -1092.419 | 286.057 | 0. |
| 11 | 0. | SLU_IDR_1 | Max | -999.426 | -254.877 | 0. |
| 11 | 1.05223 | SLU_IDR_1 | Max | -943.67 | -68.297 | 0. |
| 11 | 2.10446 | SLU_IDR_1 | Max | -892.991 | 95.474 | 0. |
| 11 | 0. | SLU_IDR_1 | Min | -999.426 | -254.877 | 0. |
| 11 | 1.05223 | SLU_IDR_1 | Min | -943.67 | -68.297 | 0. |
| 11 | 2.10446 | SLU_IDR_1 | Min | -892.991 | 95.474 | 0. |
| 11 | 0. | SLU_IDR_2 | Max | -869.575 | -200.058 | 0. |
| 11 | 1.05223 | SLU_IDR_2 | Max | -828.829 | -59.266 | 0. |
| 11 | 2.10446 | SLU_IDR_2 | Max | -791.239 | 66.366 | 0. |
| 11 | 0. | SLU_IDR_2 | Min | -869.575 | -200.058 | 0. |
| 11 | 1.05223 | SLU_IDR_2 | Min | -828.829 | -59.266 | 0. |
| 11 | 2.10446 | SLU_IDR_2 | Min | -791.239 | 66.366 | 0. |
| 11 | 0. | SISMA WOOD SLV-1 | Max | -219.502 | 135.54 | 0. |
| 11 | 1.05223 | SISMA WOOD SLV-1 | Max | -277.411 | 180.613 | 0. |
| 11 | 2.10446 | SISMA WOOD SLV-1 | Max | -335.319 | 225.686 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 11 | 0. | SISMA WOOD SLV-1 | Min | -219.502 | 135.54 | 0. |
| 11 | 1.05223 | SISMA WOOD SLV-1 | Min | -277.411 | 180.613 | 0. |
| 11 | 2.10446 | SISMA WOOD SLV-1 | Min | -335.319 | 225.686 | 0. |
| 11 | 0. | DEAD-1 | Max | -171.088 | -66.031 | 0. |
| 11 | 1.05223 | DEAD-1 | Max | -154.936 | -45.278 | 0. |
| 11 | 2.10446 | DEAD-1 | Max | -138.783 | -24.526 | 0. |
| 11 | 0. | DEAD-1 | Min | -171.088 | -66.031 | 0. |
| 11 | 1.05223 | DEAD-1 | Min | -154.936 | -45.278 | 0. |
| 11 | 2.10446 | DEAD-1 | Min | -138.783 | -24.526 | 0. |
| 11 | 0. | SLU_PROVA | | -1285.468 | -242.249 | 0. |
| 11 | 1.05223 | SLU_PROVA | | -1235.593 | -5.369 | 0. |
| 11 | 2.10446 | SLU_PROVA | | -1191.08 | 212.468 | 0. |
| 12 | 0. | DEAD | | -69.569 | -47.311 | 0. |
| 12 | 1.04817 | DEAD | | -59.458 | -23.145 | 0. |
| 12 | 2.09633 | DEAD | | -49.348 | 1.022 | 0. |
| 12 | 0. | SIMM_KA | | -149.473 | 45.445 | 0. |
| 12 | 1.04817 | SIMM_KA | | -169.905 | 53.993 | 0. |
| 12 | 2.09633 | SIMM_KA | | -189.563 | 62.217 | 0. |
| 12 | 0. | SIMM_K0 | | -233.874 | 71.482 | 0. |
| 12 | 1.04817 | SIMM_K0 | | -268.796 | 86.092 | 0. |
| 12 | 2.09633 | SIMM_K0 | | -301.251 | 99.671 | 0. |
| 12 | 0. | A--SIMM_KA | | -180.05 | 67.023 | 0. |
| 12 | 1.04817 | A--SIMM_KA | | -211.323 | 80.107 | 0. |
| 12 | 2.09633 | A--SIMM_KA | | -240.01 | 92.109 | 0. |
| 12 | 0. | A--SIMM_K0 | | -272.508 | 101.354 | 0. |
| 12 | 1.04817 | A--SIMM_K0 | | -319.419 | 120.98 | 0. |
| 12 | 2.09633 | A--SIMM_K0 | | -362.453 | 138.985 | 0. |
| 12 | 0. | A-- SIMM_SOVR_K A | | -29.113 | 9.462 | 0. |
| 12 | 1.04817 | A-- SIMM_SOVR_K A | | -35.562 | 12.16 | 0. |
| 12 | 2.09633 | A-- SIMM_SOVR_K A | | -42.012 | 14.859 | 0. |
| 12 | 0. | A-- SIMM_SOVR_K 0 | | -43.647 | 14.186 | 0. |
| 12 | 1.04817 | A-- SIMM_SOVR_K 0 | | -53.316 | 18.231 | 0. |
| 12 | 2.09633 | A-- SIMM_SOVR_K 0 | | -62.986 | 22.277 | 0. |
| 12 | 0. | SIMM_SOVR_K 0 | | -43.647 | 14.186 | 0. |
| 12 | 1.04817 | SIMM_SOVR_K 0 | | -53.316 | 18.231 | 0. |
| 12 | 2.09633 | SIMM_SOVR_K 0 | | -62.986 | 22.277 | 0. |
| 12 | 0. | SIMM_SOVR_K A | | -29.113 | 9.462 | 0. |
| 12 | 1.04817 | SIMM_SOVR_K A | | -35.562 | 12.16 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 12 | 2.09633 | SIMM_SOVR_K A | | -42.012 | 14.859 | 0. |
| 12 | 0. | SOVR | | -66.06 | -42.458 | 0. |
| 12 | 1.04817 | SOVR | | -57.969 | -23.119 | 0. |
| 12 | 2.09633 | SOVR | | -49.878 | -3.78 | 0. |
| 12 | 0. | TERR_SIMM | | -194.985 | -120.256 | 0. |
| 12 | 1.04817 | TERR_SIMM | | -169.374 | -59.041 | 0. |
| 12 | 2.09633 | TERR_SIMM | | -144.793 | -0.287 | 0. |
| 12 | 0. | TERR_A--SIMM | | -254.983 | -154.216 | 0. |
| 12 | 1.04817 | TERR_A--SIMM | | -215.729 | -60.393 | 0. |
| 12 | 2.09633 | TERR_A--SIMM | | -179.72 | 25.675 | 0. |
| 12 | 0. | INERZIA H SLV | | 2.89 | 0.817 | 0. |
| 12 | 1.04817 | INERZIA H SLV | | 2.89 | 0.817 | 0. |
| 12 | 2.09633 | INERZIA H SLV | | 2.89 | 0.817 | 0. |
| 12 | 0. | INERZIA V + SLV | | -0.942 | -0.382 | 0. |
| 12 | 1.04817 | INERZIA V + SLV | | -0.942 | -0.382 | 0. |
| 12 | 2.09633 | INERZIA V + SLV | | -0.942 | -0.382 | 0. |
| 12 | 0. | INERZIA V - SLV | | 0.942 | 0.382 | 0. |
| 12 | 1.04817 | INERZIA V - SLV | | 0.942 | 0.382 | 0. |
| 12 | 2.09633 | INERZIA V - SLV | | 0.942 | 0.382 | 0. |
| 12 | 0. | SISMA WOOD SLV | | -16.503 | 79.532 | 0. |
| 12 | 1.04817 | SISMA WOOD SLV | | -83.938 | 107.745 | 0. |
| 12 | 2.09633 | SISMA WOOD SLV | | -151.373 | 135.959 | 0. |
| 12 | 0. | iDROSTATICA | | -296.312 | 0.112 | 0. |
| 12 | 1.04817 | iDROSTATICA | | -296.312 | 32.487 | 0. |
| 12 | 2.09633 | iDROSTATICA | | -296.312 | 59.721 | 0. |
| 12 | 0. | SISMA WOOD SLD | | -7.288 | 35.125 | 0. |
| 12 | 1.04817 | SISMA WOOD SLD | | -37.07 | 47.585 | 0. |
| 12 | 2.09633 | SISMA WOOD SLD | | -66.853 | 60.045 | 0. |
| 12 | 0. | INERZIA H SLD | | 1.277 | 0.361 | 0. |
| 12 | 1.04817 | INERZIA H SLD | | 1.277 | 0.361 | 0. |
| 12 | 2.09633 | INERZIA H SLD | | 1.277 | 0.361 | 0. |
| 12 | 0. | INERZIA V + SLD | | -0.416 | -0.169 | 0. |
| 12 | 1.04817 | INERZIA V + SLD | | -0.416 | -0.169 | 0. |
| 12 | 2.09633 | INERZIA V + SLD | | -0.416 | -0.169 | 0. |
| 12 | 0. | INERZIA V SLD | | 0.416 | 0.169 | 0. |
| 12 | 1.04817 | INERZIA V SLD | | 0.416 | 0.169 | 0. |
| 12 | 2.09633 | INERZIA V SLD | | 0.416 | 0.169 | 0. |
| 12 | 0. | INERZIA V -1 | | 0.942 | 0.382 | 0. |
| 12 | 1.04817 | INERZIA V -1 | | 0.942 | 0.382 | 0. |
| 12 | 2.09633 | INERZIA V -1 | | 0.942 | 0.382 | 0. |
| 12 | 0. | SLU_1 | Max | -1378.005 | -207.206 | 0. |
| 12 | 1.04817 | SLU_1 | Max | -1379.332 | -0.052 | 0. |
| 12 | 2.09633 | SLU_1 | Max | -1378.792 | 195.879 | 0. |
| 12 | 0. | SLU_1 | Min | -1378.005 | -207.206 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 12 | 1.04817 | SLU_1 | Min | -1379.332 | -0.052 | 0. |
| 12 | 2.09633 | SLU_1 | Min | -1378.792 | 195.879 | 0. |
| 12 | 0. | SLU_2 | Max | -1251.617 | -259.948 | 0. |
| 12 | 1.04817 | SLU_2 | Max | -1229.277 | -62.695 | 0. |
| 12 | 2.09633 | SLU_2 | Max | -1207.271 | 124.254 | 0. |
| 12 | 0. | SLU_2 | Min | -1251.617 | -259.948 | 0. |
| 12 | 1.04817 | SLU_2 | Min | -1229.277 | -62.695 | 0. |
| 12 | 2.09633 | SLU_2 | Min | -1207.271 | 124.254 | 0. |
| 12 | 0. | SLU_3 | Max | -1533.053 | -186.798 | 0. |
| 12 | 1.04817 | SLU_3 | Max | -1532.232 | 69.268 | 0. |
| 12 | 2.09633 | SLU_3 | Max | -1530.588 | 306.46 | 0. |
| 12 | 0. | SLU_3 | Min | -1533.053 | -186.798 | 0. |
| 12 | 1.04817 | SLU_3 | Min | -1532.232 | 69.268 | 0. |
| 12 | 2.09633 | SLU_3 | Min | -1530.588 | 306.46 | 0. |
| 12 | 0. | SLU_4 | Max | -1399.647 | -259.621 | 0. |
| 12 | 1.04817 | SLU_4 | Max | -1373.667 | -14.081 | 0. |
| 12 | 2.09633 | SLU_4 | Max | -1348.542 | 213.287 | 0. |
| 12 | 0. | SLU_4 | Min | -1399.647 | -259.621 | 0. |
| 12 | 1.04817 | SLU_4 | Min | -1373.667 | -14.081 | 0. |
| 12 | 2.09633 | SLU_4 | Min | -1348.542 | 213.287 | 0. |
| 12 | 0. | SLE_F1 | Max | -1004.75 | -145.928 | 0. |
| 12 | 1.04817 | SLE_F1 | Max | -1005.133 | 3.978 | 0. |
| 12 | 2.09633 | SLE_F1 | Max | -1004.08 | 145.25 | 0. |
| 12 | 0. | SLE_F1 | Min | -1004.75 | -145.928 | 0. |
| 12 | 1.04817 | SLE_F1 | Min | -1005.133 | 3.978 | 0. |
| 12 | 2.09633 | SLE_F1 | Min | -1004.08 | 145.25 | 0. |
| 12 | 0. | SLE_F2 | Max | -912.9 | -184.17 | 0. |
| 12 | 1.04817 | SLE_F2 | Max | -896.379 | -41.337 | 0. |
| 12 | 2.09633 | SLE_F2 | Max | -880.114 | 93.57 | 0. |
| 12 | 0. | SLE_F2 | Min | -912.9 | -184.17 | 0. |
| 12 | 1.04817 | SLE_F2 | Min | -896.379 | -41.337 | 0. |
| 12 | 2.09633 | SLE_F2 | Min | -880.114 | 93.57 | 0. |
| 12 | 0. | SLE_F3 | Max | -1027.269 | -183.737 | 0. |
| 12 | 1.04817 | SLE_F3 | Max | -1007.948 | -3.76 | 0. |
| 12 | 2.09633 | SLE_F3 | Max | -989.284 | 162.239 | 0. |
| 12 | 0. | SLE_F3 | Min | -1027.269 | -183.737 | 0. |
| 12 | 1.04817 | SLE_F3 | Min | -1007.948 | -3.76 | 0. |
| 12 | 2.09633 | SLE_F3 | Min | -989.284 | 162.239 | 0. |
| 12 | 0. | SLE_F4 | Max | -1127.036 | -129.126 | 0. |
| 12 | 1.04817 | SLE_F4 | Max | -1125.767 | 58.404 | 0. |
| 12 | 2.09633 | SLE_F4 | Max | -1123.865 | 231.416 | 0. |
| 12 | 0. | SLE_F4 | Min | -1127.036 | -129.126 | 0. |
| 12 | 1.04817 | SLE_F4 | Min | -1125.767 | 58.404 | 0. |
| 12 | 2.09633 | SLE_F4 | Min | -1123.865 | 231.416 | 0. |
| 12 | 0. | SLE_QP1 | Max | -901.415 | -121.02 | 0. |
| 12 | 1.04817 | SLE_QP1 | Max | -900.615 | 11.348 | 0. |
| 12 | 2.09633 | SLE_QP1 | Max | -898.378 | 135.081 | 0. |
| 12 | 0. | SLE_QP1 | Min | -901.415 | -121.02 | 0. |
| 12 | 1.04817 | SLE_QP1 | Min | -900.615 | 11.348 | 0. |
| 12 | 2.09633 | SLE_QP1 | Min | -898.378 | 135.081 | 0. |
| 12 | 0. | SLE_QP2 | Max | -820.264 | -154.847 | 0. |
| 12 | 1.04817 | SLE_QP2 | Max | -804.974 | -28.542 | 0. |
| 12 | 2.09633 | SLE_QP2 | Max | -789.94 | 89.838 | 0. |
| 12 | 0. | SLE_QP2 | Min | -820.264 | -154.847 | 0. |
| 12 | 1.04817 | SLE_QP2 | Min | -804.974 | -28.542 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 12 | 2.09633 | SLE_QP2 | Min | -789.94 | 89.838 | 0. |
| 12 | 0. | SLE_QP3 | Max | -935.561 | -154.075 | 0. |
| 12 | 1.04817 | SLE_QP3 | Max | -917.47 | 9.374 | 0. |
| 12 | 2.09633 | SLE_QP3 | Max | -900.037 | 158.845 | 0. |
| 12 | 0. | SLE_QP3 | Min | -935.561 | -154.075 | 0. |
| 12 | 1.04817 | SLE_QP3 | Min | -917.47 | 9.374 | 0. |
| 12 | 2.09633 | SLE_QP3 | Min | -900.037 | 158.845 | 0. |
| 12 | 0. | SLE_QP4 | Max | -1030.681 | -101.991 | 0. |
| 12 | 1.04817 | SLE_QP4 | Max | -1028.228 | 68.001 | 0. |
| 12 | 2.09633 | SLE_QP4 | Max | -1025.143 | 223.474 | 0. |
| 12 | 0. | SLE_QP4 | Min | -1030.681 | -101.991 | 0. |
| 12 | 1.04817 | SLE_QP4 | Min | -1028.228 | 68.001 | 0. |
| 12 | 2.09633 | SLE_QP4 | Min | -1025.143 | 223.474 | 0. |
| 12 | 0. | SLV_1 | Max | -1094.423 | 69.752 | 0. |
| 12 | 1.04817 | SLV_1 | Max | -1161.057 | 230.332 | 0. |
| 12 | 2.09633 | SLV_1 | Max | -1226.256 | 382.279 | 0. |
| 12 | 0. | SLV_1 | Min | -1094.423 | 69.752 | 0. |
| 12 | 1.04817 | SLV_1 | Min | -1161.057 | 230.332 | 0. |
| 12 | 2.09633 | SLV_1 | Min | -1226.256 | 382.279 | 0. |
| 12 | 0. | SLV_2 | Max | -1091.869 | 70.486 | 0. |
| 12 | 1.04817 | SLV_2 | Max | -1158.503 | 231.067 | 0. |
| 12 | 2.09633 | SLV_2 | Max | -1223.702 | 383.014 | 0. |
| 12 | 0. | SLV_2 | Min | -1091.869 | 70.486 | 0. |
| 12 | 1.04817 | SLV_2 | Min | -1158.503 | 231.067 | 0. |
| 12 | 2.09633 | SLV_2 | Min | -1223.702 | 383.014 | 0. |
| 12 | 0. | SLV_3 | Max | -1275.896 | 91.607 | 0. |
| 12 | 1.04817 | SLV_3 | Max | -1340.878 | 289.812 | 0. |
| 12 | 2.09633 | SLV_3 | Max | -1405.228 | 473.499 | 0. |
| 12 | 0. | SLV_3 | Min | -1275.896 | 91.607 | 0. |
| 12 | 1.04817 | SLV_3 | Min | -1340.878 | 289.812 | 0. |
| 12 | 2.09633 | SLV_3 | Min | -1405.228 | 473.499 | 0. |
| 12 | 0. | SLV_4 | Max | -1273.219 | 92.572 | 0. |
| 12 | 1.04817 | SLV_4 | Max | -1338.201 | 290.777 | 0. |
| 12 | 2.09633 | SLV_4 | Max | -1402.551 | 474.463 | 0. |
| 12 | 0. | SLV_4 | Min | -1273.219 | 92.572 | 0. |
| 12 | 1.04817 | SLV_4 | Min | -1338.201 | 290.777 | 0. |
| 12 | 2.09633 | SLV_4 | Min | -1402.551 | 474.463 | 0. |
| 12 | 0. | SLD_1 | Max | -951.563 | -36.181 | 0. |
| 12 | 1.04817 | SLD_1 | Max | -980.544 | 108.646 | 0. |
| 12 | 2.09633 | SLD_1 | Max | -1008.09 | 244.84 | 0. |
| 12 | 0. | SLD_1 | Min | -951.563 | -36.181 | 0. |
| 12 | 1.04817 | SLD_1 | Min | -980.544 | 108.646 | 0. |
| 12 | 2.09633 | SLD_1 | Min | -1008.09 | 244.84 | 0. |
| 12 | 0. | SLD_2 | Max | -949.969 | -35.743 | 0. |
| 12 | 1.04817 | SLD_2 | Max | -978.95 | 109.085 | 0. |
| 12 | 2.09633 | SLD_2 | Max | -1006.496 | 245.278 | 0. |
| 12 | 0. | SLD_2 | Min | -949.969 | -35.743 | 0. |
| 12 | 1.04817 | SLD_2 | Min | -978.95 | 109.085 | 0. |
| 12 | 2.09633 | SLD_2 | Min | -1006.496 | 245.278 | 0. |
| 12 | 0. | SLD_3 | Max | -1131.338 | -10.75 | 0. |
| 12 | 1.04817 | SLD_3 | Max | -1158.668 | 171.702 | 0. |
| 12 | 2.09633 | SLD_3 | Max | -1185.364 | 339.636 | 0. |
| 12 | 0. | SLD_3 | Min | -1131.338 | -10.75 | 0. |
| 12 | 1.04817 | SLD_3 | Min | -1158.668 | 171.702 | 0. |
| 12 | 2.09633 | SLD_3 | Min | -1185.364 | 339.636 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 12 | 0. | SLD_4 | Max | -1130.037 | -10.289 | 0. |
| 12 | 1.04817 | SLD_4 | Max | -1157.367 | 172.163 | 0. |
| 12 | 2.09633 | SLD_4 | Max | -1184.063 | 340.097 | 0. |
| 12 | 0. | SLD_4 | Min | -1130.037 | -10.289 | 0. |
| 12 | 1.04817 | SLD_4 | Min | -1157.367 | 172.163 | 0. |
| 12 | 2.09633 | SLD_4 | Min | -1184.063 | 340.097 | 0. |
| 12 | 0. | SLU_IDR_1 | Max | -886.802 | -141.885 | 0. |
| 12 | 1.04817 | SLU_IDR_1 | Max | -870.52 | 11.695 | 0. |
| 12 | 2.09633 | SLU_IDR_1 | Max | -854.831 | 151.665 | 0. |
| 12 | 0. | SLU_IDR_1 | Min | -886.802 | -141.885 | 0. |
| 12 | 1.04817 | SLU_IDR_1 | Min | -870.52 | 11.695 | 0. |
| 12 | 2.09633 | SLU_IDR_1 | Min | -854.831 | 151.665 | 0. |
| 12 | 0. | SLU_IDR_2 | Max | -780.978 | -143.305 | 0. |
| 12 | 1.04817 | SLU_IDR_2 | Max | -767.217 | -23.155 | 0. |
| 12 | 2.09633 | SLU_IDR_2 | Max | -753.687 | 88.833 | 0. |
| 12 | 0. | SLU_IDR_2 | Min | -780.978 | -143.305 | 0. |
| 12 | 1.04817 | SLU_IDR_2 | Min | -767.217 | -23.155 | 0. |
| 12 | 2.09633 | SLU_IDR_2 | Min | -753.687 | 88.833 | 0. |
| 12 | 0. | SISMA WOOD SLV-1 | Max | -382.743 | 131.112 | 0. |
| 12 | 1.04817 | SISMA WOOD SLV-1 | Max | -450.178 | 159.325 | 0. |
| 12 | 2.09633 | SISMA WOOD SLV-1 | Max | -517.613 | 187.538 | 0. |
| 12 | 0. | SISMA WOOD SLV-1 | Min | -382.743 | 131.112 | 0. |
| 12 | 1.04817 | SISMA WOOD SLV-1 | Min | -450.178 | 159.325 | 0. |
| 12 | 2.09633 | SISMA WOOD SLV-1 | Min | -517.613 | 187.538 | 0. |
| 12 | 0. | DEAD-1 | Max | -127.505 | -60.04 | 0. |
| 12 | 1.04817 | DEAD-1 | Max | -117.395 | -35.873 | 0. |
| 12 | 2.09633 | DEAD-1 | Max | -107.284 | -11.707 | 0. |
| 12 | 0. | DEAD-1 | Min | -127.505 | -60.04 | 0. |
| 12 | 1.04817 | DEAD-1 | Min | -117.395 | -35.873 | 0. |
| 12 | 2.09633 | DEAD-1 | Min | -107.284 | -11.707 | 0. |
| 12 | 0. | SLU_PROVA | | -1197.724 | -167.174 | 0. |
| 12 | 1.04817 | SLU_PROVA | | -1199.051 | 39.98 | 0. |
| 12 | 2.09633 | SLU_PROVA | | -1198.511 | 235.911 | 0. |
| 13 | 0. | DEAD | | -44.899 | -34.63 | 0. |
| 13 | 1.04614 | DEAD | | -41.585 | -8.695 | 0. |
| 13 | 2.09228 | DEAD | | -38.271 | 17.24 | 0. |
| 13 | 0. | SIMM_KA | | -200.56 | 19.405 | 0. |
| 13 | 1.04614 | SIMM_KA | | -221.242 | 22.048 | 0. |
| 13 | 2.09228 | SIMM_KA | | -241.923 | 24.691 | 0. |
| 13 | 0. | SIMM_K0 | | -318.878 | 31.137 | 0. |
| 13 | 1.04614 | SIMM_K0 | | -351.724 | 35.334 | 0. |
| 13 | 2.09228 | SIMM_K0 | | -383.247 | 39.363 | 0. |
| 13 | 0. | A--SIMM_KA | | -256.555 | 32.663 | 0. |
| 13 | 1.04614 | A--SIMM_KA | | -284.957 | 36.293 | 0. |
| 13 | 2.09228 | A--SIMM_KA | | -311.366 | 39.667 | 0. |
| 13 | 0. | A--SIMM_K0 | | -387.454 | 49.489 | 0. |
| 13 | 1.04614 | A--SIMM_K0 | | -430.059 | 54.933 | 0. |
| 13 | 2.09228 | A--SIMM_K0 | | -469.671 | 59.995 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 13 | 0. | A-- SIMM_SOVR_K A | | -44.65 | 4.697 | 0. |
| 13 | 1.04614 | A-- SIMM_SOVR_K A | | -51.572 | 5.581 | 0. |
| 13 | 2.09228 | A-- SIMM_SOVR_K A | | -58.493 | 6.466 | 0. |
| 13 | 0. | A-- SIMM_SOVR_K 0 | | -66.942 | 7.042 | 0. |
| 13 | 1.04614 | A-- SIMM_SOVR_K 0 | | -77.319 | 8.368 | 0. |
| 13 | 2.09228 | A-- SIMM_SOVR_K 0 | | -87.696 | 9.694 | 0. |
| 13 | 0. | SIMM_SOVR_K 0 | | -66.942 | 7.042 | 0. |
| 13 | 1.04614 | SIMM_SOVR_K 0 | | -77.319 | 8.368 | 0. |
| 13 | 2.09228 | SIMM_SOVR_K 0 | | -87.696 | 9.694 | 0. |
| 13 | 0. | SIMM_SOVR_K A | | -44.65 | 4.697 | 0. |
| 13 | 1.04614 | SIMM_SOVR_K A | | -51.572 | 5.581 | 0. |
| 13 | 2.09228 | SIMM_SOVR_K A | | -58.493 | 6.466 | 0. |
| 13 | 0. | SOVR | | -45.455 | -29.319 | 0. |
| 13 | 1.04614 | SOVR | | -42.803 | -8.565 | 0. |
| 13 | 2.09228 | SOVR | | -40.151 | 12.189 | 0. |
| 13 | 0. | TERR_SIMM | | -133.672 | -83.385 | 0. |
| 13 | 1.04614 | TERR_SIMM | | -125.784 | -21.652 | 0. |
| 13 | 2.09228 | TERR_SIMM | | -117.896 | 40.081 | 0. |
| 13 | 0. | TERR_A--SIMM | | -172.158 | -84.122 | 0. |
| 13 | 1.04614 | TERR_A--SIMM | | -161.269 | 1.091 | 0. |
| 13 | 2.09228 | TERR_A--SIMM | | -151.145 | 80.322 | 0. |
| 13 | 0. | INERZIA H SLV | | 0.998 | 1.223 | 0. |
| 13 | 1.04614 | INERZIA H SLV | | 0.998 | 1.223 | 0. |
| 13 | 2.09228 | INERZIA H SLV | | 0.998 | 1.223 | 0. |
| 13 | 0. | INERZIA V + SLV | | -0.652 | -0.143 | 0. |
| 13 | 1.04614 | INERZIA V + SLV | | -0.652 | -0.143 | 0. |
| 13 | 2.09228 | INERZIA V + SLV | | -0.652 | -0.143 | 0. |
| 13 | 0. | INERZIA V - SLV | | 0.652 | 0.143 | 0. |
| 13 | 1.04614 | INERZIA V - SLV | | 0.652 | 0.143 | 0. |
| 13 | 2.09228 | INERZIA V - SLV | | 0.652 | 0.143 | 0. |
| 13 | 0. | SISMA WOOD SLV | | -179.23 | 79.69 | 0. |
| 13 | 1.04614 | SISMA WOOD SLV | | -251.599 | 88.937 | 0. |
| 13 | 2.09228 | SISMA WOOD SLV | | -323.968 | 98.185 | 0. |
| 13 | 0. | iDROSTATICA | | -302.842 | -11.263 | 0. |
| 13 | 1.04614 | iDROSTATICA | | -302.842 | 12.071 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 13 | 2.09228 | iDROSTATICA | | -302.842 | 32.842 | 0. |
| 13 | 0. | SISMA WOOD SLD | | -79.155 | 35.194 | 0. |
| 13 | 1.04614 | SISMA WOOD SLD | | -111.116 | 39.278 | 0. |
| 13 | 2.09228 | SISMA WOOD SLD | | -143.077 | 43.362 | 0. |
| 13 | 0. | INERZIA H SLD | | 0.441 | 0.54 | 0. |
| 13 | 1.04614 | INERZIA H SLD | | 0.441 | 0.54 | 0. |
| 13 | 2.09228 | INERZIA H SLD | | 0.441 | 0.54 | 0. |
| 13 | 0. | INERZIA V + SLD | | -0.288 | -0.063 | 0. |
| 13 | 1.04614 | INERZIA V + SLD | | -0.288 | -0.063 | 0. |
| 13 | 2.09228 | INERZIA V + SLD | | -0.288 | -0.063 | 0. |
| 13 | 0. | INERZIA V SLD | | 0.288 | 0.063 | 0. |
| 13 | 1.04614 | INERZIA V SLD | | 0.288 | 0.063 | 0. |
| 13 | 2.09228 | INERZIA V SLD | | 0.288 | 0.063 | 0. |
| 13 | 0. | INERZIA V -1 | | 0.652 | 0.143 | 0. |
| 13 | 1.04614 | INERZIA V -1 | | 0.652 | 0.143 | 0. |
| 13 | 2.09228 | INERZIA V -1 | | 0.652 | 0.143 | 0. |
| 13 | 0. | SLU_1 | Max | -1381.236 | -177.829 | 0. |
| 13 | 1.04614 | SLU_1 | Max | -1420.96 | 5.049 | 0. |
| 13 | 2.09228 | SLU_1 | Max | -1458.964 | 184.376 | 0. |
| 13 | 0. | SLU_1 | Min | -1381.236 | -177.829 | 0. |
| 13 | 1.04614 | SLU_1 | Min | -1420.96 | 5.049 | 0. |
| 13 | 2.09228 | SLU_1 | Min | -1458.964 | 184.376 | 0. |
| 13 | 0. | SLU_2 | Max | -1196.844 | -201.266 | 0. |
| 13 | 1.04614 | SLU_2 | Max | -1215.571 | -21.07 | 0. |
| 13 | 2.09228 | SLU_2 | Max | -1234.298 | 155.793 | 0. |
| 13 | 0. | SLU_2 | Min | -1196.844 | -201.266 | 0. |
| 13 | 1.04614 | SLU_2 | Min | -1215.571 | -21.07 | 0. |
| 13 | 2.09228 | SLU_2 | Min | -1234.298 | 155.793 | 0. |
| 13 | 0. | SLU_3 | Max | -1556.971 | -111.602 | 0. |
| 13 | 1.04614 | SLU_3 | Max | -1605.482 | 103.423 | 0. |
| 13 | 2.09228 | SLU_3 | Max | -1651.095 | 306.841 | 0. |
| 13 | 0. | SLU_3 | Min | -1556.971 | -111.602 | 0. |
| 13 | 1.04614 | SLU_3 | Min | -1605.482 | 103.423 | 0. |
| 13 | 2.09228 | SLU_3 | Min | -1651.095 | 306.841 | 0. |
| 13 | 0. | SLU_4 | Max | -1356.703 | -153.011 | 0. |
| 13 | 1.04614 | SLU_4 | Max | -1381.566 | 58.991 | 0. |
| 13 | 2.09228 | SLU_4 | Max | -1404.832 | 259.554 | 0. |
| 13 | 0. | SLU_4 | Min | -1356.703 | -153.011 | 0. |
| 13 | 1.04614 | SLU_4 | Min | -1381.566 | 58.991 | 0. |
| 13 | 2.09228 | SLU_4 | Min | -1404.832 | 259.554 | 0. |
| 13 | 0. | SLE_F1 | Max | -1006.553 | -126.99 | 0. |
| 13 | 1.04614 | SLE_F1 | Max | -1033.99 | 4.769 | 0. |
| 13 | 2.09228 | SLE_F1 | Max | -1060.104 | 133.796 | 0. |
| 13 | 0. | SLE_F1 | Min | -1006.553 | -126.99 | 0. |
| 13 | 1.04614 | SLE_F1 | Min | -1033.99 | 4.769 | 0. |
| 13 | 2.09228 | SLE_F1 | Min | -1060.104 | 133.796 | 0. |
| 13 | 0. | SLE_F2 | Max | -873.307 | -143.845 | 0. |
| 13 | 1.04614 | SLE_F2 | Max | -885.988 | -13.972 | 0. |
| 13 | 2.09228 | SLE_F2 | Max | -898.669 | 113.339 | 0. |
| 13 | 0. | SLE_F2 | Min | -873.307 | -143.845 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 13 | 1.04614 | SLE_F2 | Min | -885.988 | -13.972 | 0. |
| 13 | 2.09228 | SLE_F2 | Min | -898.669 | 113.339 | 0. |
| 13 | 0. | SLE_F3 | Max | -996.806 | -106.683 | 0. |
| 13 | 1.04614 | SLE_F3 | Max | -1014.207 | 47.657 | 0. |
| 13 | 2.09228 | SLE_F3 | Max | -1030.38 | 193.198 | 0. |
| 13 | 0. | SLE_F3 | Min | -996.806 | -106.683 | 0. |
| 13 | 1.04614 | SLE_F3 | Min | -1014.207 | 47.657 | 0. |
| 13 | 2.09228 | SLE_F3 | Min | -1030.38 | 193.198 | 0. |
| 13 | 0. | SLE_F4 | Max | -1144.937 | -75.784 | 0. |
| 13 | 1.04614 | SLE_F4 | Max | -1179.133 | 80.702 | 0. |
| 13 | 2.09228 | SLE_F4 | Max | -1211.1 | 228.261 | 0. |
| 13 | 0. | SLE_F4 | Min | -1144.937 | -75.784 | 0. |
| 13 | 1.04614 | SLE_F4 | Min | -1179.133 | 80.702 | 0. |
| 13 | 2.09228 | SLE_F4 | Min | -1211.1 | 228.261 | 0. |
| 13 | 0. | SLE_QP1 | Max | -901.948 | -108.717 | 0. |
| 13 | 1.04614 | SLE_QP1 | Max | -923.592 | 6.481 | 0. |
| 13 | 2.09228 | SLE_QP1 | Max | -943.912 | 118.948 | 0. |
| 13 | 0. | SLE_QP1 | Min | -901.948 | -108.717 | 0. |
| 13 | 1.04614 | SLE_QP1 | Min | -923.592 | 6.481 | 0. |
| 13 | 2.09228 | SLE_QP1 | Min | -943.912 | 118.948 | 0. |
| 13 | 0. | SLE_QP2 | Max | -785.387 | -123.463 | 0. |
| 13 | 1.04614 | SLE_QP2 | Max | -794.866 | -9.818 | 0. |
| 13 | 2.09228 | SLE_QP2 | Max | -804.345 | 101.263 | 0. |
| 13 | 0. | SLE_QP2 | Min | -785.387 | -123.463 | 0. |
| 13 | 1.04614 | SLE_QP2 | Min | -794.866 | -9.818 | 0. |
| 13 | 2.09228 | SLE_QP2 | Min | -804.345 | 101.263 | 0. |
| 13 | 0. | SLE_QP3 | Max | -909.87 | -86.222 | 0. |
| 13 | 1.04614 | SLE_QP3 | Max | -924.069 | 51.89 | 0. |
| 13 | 2.09228 | SLE_QP3 | Max | -937.04 | 181.201 | 0. |
| 13 | 0. | SLE_QP3 | Min | -909.87 | -86.222 | 0. |
| 13 | 1.04614 | SLE_QP3 | Min | -924.069 | 51.89 | 0. |
| 13 | 2.09228 | SLE_QP3 | Min | -937.04 | 181.201 | 0. |
| 13 | 0. | SLE_QP4 | Max | -1047.657 | -57.187 | 0. |
| 13 | 1.04614 | SLE_QP4 | Max | -1076.06 | 82.74 | 0. |
| 13 | 2.09228 | SLE_QP4 | Max | -1102.233 | 213.738 | 0. |
| 13 | 0. | SLE_QP4 | Min | -1047.657 | -57.187 | 0. |
| 13 | 1.04614 | SLE_QP4 | Min | -1076.06 | 82.74 | 0. |
| 13 | 2.09228 | SLE_QP4 | Min | -1102.233 | 213.738 | 0. |
| 13 | 0. | SLV_1 | Max | -1285.331 | 43.487 | 0. |
| 13 | 1.04614 | SLV_1 | Max | -1379.343 | 167.933 | 0. |
| 13 | 2.09228 | SLV_1 | Max | -1472.033 | 289.648 | 0. |
| 13 | 0. | SLV_1 | Min | -1285.331 | 43.487 | 0. |
| 13 | 1.04614 | SLV_1 | Min | -1379.343 | 167.933 | 0. |
| 13 | 2.09228 | SLV_1 | Min | -1472.033 | 289.648 | 0. |
| 13 | 0. | SLV_2 | Max | -1283.279 | 43.196 | 0. |
| 13 | 1.04614 | SLV_2 | Max | -1377.291 | 167.642 | 0. |
| 13 | 2.09228 | SLV_2 | Max | -1469.981 | 289.357 | 0. |
| 13 | 0. | SLV_2 | Min | -1283.279 | 43.196 | 0. |
| 13 | 1.04614 | SLV_2 | Min | -1377.291 | 167.642 | 0. |
| 13 | 2.09228 | SLV_2 | Min | -1469.981 | 289.357 | 0. |
| 13 | 0. | SLV_3 | Max | -1482.116 | 83.83 | 0. |
| 13 | 1.04614 | SLV_3 | Max | -1582.887 | 233.004 | 0. |
| 13 | 2.09228 | SLV_3 | Max | -1681.43 | 373.25 | 0. |
| 13 | 0. | SLV_3 | Min | -1482.116 | 83.83 | 0. |
| 13 | 1.04614 | SLV_3 | Min | -1582.887 | 233.004 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 13 | 2.09228 | SLV_3 | Min | -1681.43 | 373.25 | 0. |
| 13 | 0. | SLV_4 | Max | -1480.006 | 83.793 | 0. |
| 13 | 1.04614 | SLV_4 | Max | -1580.777 | 232.967 | 0. |
| 13 | 2.09228 | SLV_4 | Max | -1679.32 | 373.213 | 0. |
| 13 | 0. | SLV_4 | Min | -1480.006 | 83.793 | 0. |
| 13 | 1.04614 | SLV_4 | Min | -1580.777 | 232.967 | 0. |
| 13 | 2.09228 | SLV_4 | Min | -1679.32 | 373.213 | 0. |
| 13 | 0. | SLD_1 | Max | -1037.594 | -31.587 | 0. |
| 13 | 1.04614 | SLD_1 | Max | -1091.198 | 87.696 | 0. |
| 13 | 2.09228 | SLD_1 | Max | -1143.48 | 204.247 | 0. |
| 13 | 0. | SLD_1 | Min | -1037.594 | -31.587 | 0. |
| 13 | 1.04614 | SLD_1 | Min | -1091.198 | 87.696 | 0. |
| 13 | 2.09228 | SLD_1 | Min | -1143.48 | 204.247 | 0. |
| 13 | 0. | SLD_2 | Max | -1036.269 | -31.482 | 0. |
| 13 | 1.04614 | SLD_2 | Max | -1089.873 | 87.801 | 0. |
| 13 | 2.09228 | SLD_2 | Max | -1142.155 | 204.352 | 0. |
| 13 | 0. | SLD_2 | Min | -1036.269 | -31.482 | 0. |
| 13 | 1.04614 | SLD_2 | Min | -1089.873 | 87.801 | 0. |
| 13 | 2.09228 | SLD_2 | Min | -1142.155 | 204.352 | 0. |
| 13 | 0. | SLD_3 | Max | -1233.692 | 12.652 | 0. |
| 13 | 1.04614 | SLD_3 | Max | -1294.056 | 156.662 | 0. |
| 13 | 2.09228 | SLD_3 | Max | -1352.191 | 291.745 | 0. |
| 13 | 0. | SLD_3 | Min | -1233.692 | 12.652 | 0. |
| 13 | 1.04614 | SLD_3 | Min | -1294.056 | 156.662 | 0. |
| 13 | 2.09228 | SLD_3 | Min | -1352.191 | 291.745 | 0. |
| 13 | 0. | SLD_4 | Max | -1232.656 | 12.701 | 0. |
| 13 | 1.04614 | SLD_4 | Max | -1293.02 | 156.711 | 0. |
| 13 | 2.09228 | SLD_4 | Max | -1351.154 | 291.794 | 0. |
| 13 | 0. | SLD_4 | Min | -1232.656 | 12.701 | 0. |
| 13 | 1.04614 | SLD_4 | Min | -1293.02 | 156.711 | 0. |
| 13 | 2.09228 | SLD_4 | Min | -1351.154 | 291.794 | 0. |
| 13 | 0. | SLU_IDR_1 | Max | -864.382 | -81.12 | 0. |
| 13 | 1.04614 | SLU_IDR_1 | Max | -877.161 | 47.847 | 0. |
| 13 | 2.09228 | SLU_IDR_1 | Max | -888.835 | 168.381 | 0. |
| 13 | 0. | SLU_IDR_1 | Min | -864.382 | -81.12 | 0. |
| 13 | 1.04614 | SLU_IDR_1 | Min | -877.161 | 47.847 | 0. |
| 13 | 2.09228 | SLU_IDR_1 | Min | -888.835 | 168.381 | 0. |
| 13 | 0. | SLU_IDR_2 | Max | -750.172 | -114.79 | 0. |
| 13 | 1.04614 | SLU_IDR_2 | Max | -758.703 | -7.843 | 0. |
| 13 | 2.09228 | SLU_IDR_2 | Max | -767.234 | 96.285 | 0. |
| 13 | 0. | SLU_IDR_2 | Min | -750.172 | -114.79 | 0. |
| 13 | 1.04614 | SLU_IDR_2 | Min | -758.703 | -7.843 | 0. |
| 13 | 2.09228 | SLU_IDR_2 | Min | -767.234 | 96.285 | 0. |
| 13 | 0. | SISMA WOOD SLV-1 | Max | -549.307 | 72.681 | 0. |
| 13 | 1.04614 | SISMA WOOD SLV-1 | Max | -621.676 | 81.929 | 0. |
| 13 | 2.09228 | SISMA WOOD SLV-1 | Max | -694.045 | 91.176 | 0. |
| 13 | 0. | SISMA WOOD SLV-1 | Min | -549.307 | 72.681 | 0. |
| 13 | 1.04614 | SISMA WOOD SLV-1 | Min | -621.676 | 81.929 | 0. |
| 13 | 2.09228 | SISMA WOOD SLV-1 | Min | -694.045 | 91.176 | 0. |
| 13 | 0. | DEAD-1 | Max | -100.308 | -39.818 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 13 | 1.04614 | DEAD-1 | Max | -96.994 | -13.883 | 0. |
| 13 | 2.09228 | DEAD-1 | Max | -93.68 | 12.052 | 0. |
| 13 | 0. | DEAD-1 | Min | -100.308 | -39.818 | 0. |
| 13 | 1.04614 | DEAD-1 | Min | -96.994 | -13.883 | 0. |
| 13 | 2.09228 | DEAD-1 | Min | -93.68 | 12.052 | 0. |
| 13 | 0. | SLU_PROVA | | -1208.974 | -160.998 | 0. |
| 13 | 1.04614 | SLU_PROVA | | -1248.698 | 21.88 | 0. |
| 13 | 2.09228 | SLU_PROVA | | -1286.702 | 201.207 | 0. |
| 14 | 0. | DEAD | | 29.143 | -8.94 | 0. |
| 14 | 0.94151 | DEAD | | 35.891 | 18.479 | 0. |
| 14 | 1.88301 | DEAD | | 42.639 | 45.897 | 0. |
| 14 | 0. | SIMM_KA | | -147.852 | 0.091 | 0. |
| 14 | 0.94151 | SIMM_KA | | -147.852 | 0.091 | 0. |
| 14 | 1.88301 | SIMM_KA | | -147.852 | 0.091 | 0. |
| 14 | 0. | SIMM_K0 | | -223.174 | -0.438 | 0. |
| 14 | 0.94151 | SIMM_K0 | | -223.174 | -0.438 | 0. |
| 14 | 1.88301 | SIMM_K0 | | -223.174 | -0.438 | 0. |
| 14 | 0. | A--SIMM_KA | | -185.446 | -11.884 | 0. |
| 14 | 0.94151 | A--SIMM_KA | | -185.446 | -11.884 | 0. |
| 14 | 1.88301 | A--SIMM_KA | | -185.446 | -11.884 | 0. |
| 14 | 0. | A--SIMM_K0 | | -285.607 | -17.665 | 0. |
| 14 | 0.94151 | A--SIMM_K0 | | -285.607 | -17.665 | 0. |
| 14 | 1.88301 | A--SIMM_K0 | | -285.607 | -17.665 | 0. |
| 14 | 0. | A-- SIMM_SOVR_K A | | -9.058 | -1.878 | 0. |
| 14 | 0.94151 | A-- SIMM_SOVR_K A | | -9.058 | -1.878 | 0. |
| 14 | 1.88301 | A-- SIMM_SOVR_K A | | -9.058 | -1.878 | 0. |
| 14 | 0. | A-- SIMM_SOVR_K 0 | | -13.581 | -2.816 | 0. |
| 14 | 0.94151 | A-- SIMM_SOVR_K 0 | | -13.581 | -2.816 | 0. |
| 14 | 1.88301 | A-- SIMM_SOVR_K 0 | | -13.581 | -2.816 | 0. |
| 14 | 0. | SIMM_SOVR_K 0 | | -13.581 | -2.816 | 0. |
| 14 | 0.94151 | SIMM_SOVR_K 0 | | -13.581 | -2.816 | 0. |
| 14 | 1.88301 | SIMM_SOVR_K 0 | | -13.581 | -2.816 | 0. |
| 14 | 0. | SIMM_SOVR_K A | | -9.058 | -1.878 | 0. |
| 14 | 0.94151 | SIMM_SOVR_K A | | -9.058 | -1.878 | 0. |
| 14 | 1.88301 | SIMM_SOVR_K A | | -9.058 | -1.878 | 0. |
| 14 | 0. | SOVR | | 6.52 | -20.229 | 0. |
| 14 | 0.94151 | SOVR | | 6.52 | -20.229 | 0. |
| 14 | 1.88301 | SOVR | | 6.52 | -20.229 | 0. |
| 14 | 0. | TERR_SIMM | | 1.774 | -85.235 | 0. |
| 14 | 0.94151 | TERR_SIMM | | 1.774 | -85.235 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 14 | 1.88301 | TERR_SIMM | | 1.774 | -85.235 | 0. |
| 14 | 0. | TERR_A--SIMM | | 4.173 | -124.605 | 0. |
| 14 | 0.94151 | TERR_A--SIMM | | 4.173 | -124.605 | 0. |
| 14 | 1.88301 | TERR_A--SIMM | | 4.173 | -124.605 | 0. |
| 14 | 0. | INERZIA H SLV | | 5.361 | -0.415 | 0. |
| 14 | 0.94151 | INERZIA H SLV | | 5.361 | -0.415 | 0. |
| 14 | 1.88301 | INERZIA H SLV | | 5.361 | -0.415 | 0. |
| 14 | 0. | INERZIA V + SLV | | 0.56 | 0.304 | 0. |
| 14 | 0.94151 | INERZIA V + SLV | | 0.56 | 0.304 | 0. |
| 14 | 1.88301 | INERZIA V + SLV | | 0.56 | 0.304 | 0. |
| 14 | 0. | INERZIA V - SLV | | -0.56 | -0.304 | 0. |
| 14 | 0.94151 | INERZIA V - SLV | | -0.56 | -0.304 | 0. |
| 14 | 1.88301 | INERZIA V - SLV | | -0.56 | -0.304 | 0. |
| 14 | 0. | SISMA WOOD SLV | | -76.055 | -3.839 | 0. |
| 14 | 0.94151 | SISMA WOOD SLV | | -12.297 | -19.531 | 0. |
| 14 | 1.88301 | SISMA WOOD SLV | | 51.461 | -35.222 | 0. |
| 14 | 0. | iDROSTATICA | | -607.828 | -143.841 | 0. |
| 14 | 0.94151 | iDROSTATICA | | -607.828 | -259.712 | 0. |
| 14 | 1.88301 | iDROSTATICA | | -607.828 | -375.583 | 0. |
| 14 | 0. | SISMA WOOD SLD | | -33.589 | -1.696 | 0. |
| 14 | 0.94151 | SISMA WOOD SLD | | -5.431 | -8.626 | 0. |
| 14 | 1.88301 | SISMA WOOD SLD | | 22.727 | -15.556 | 0. |
| 14 | 0. | INERZIA H SLD | | 2.368 | -0.183 | 0. |
| 14 | 0.94151 | INERZIA H SLD | | 2.368 | -0.183 | 0. |
| 14 | 1.88301 | INERZIA H SLD | | 2.368 | -0.183 | 0. |
| 14 | 0. | INERZIA V + SLD | | 0.247 | 0.134 | 0. |
| 14 | 0.94151 | INERZIA V + SLD | | 0.247 | 0.134 | 0. |
| 14 | 1.88301 | INERZIA V + SLD | | 0.247 | 0.134 | 0. |
| 14 | 0. | INERZIA V SLD | | -0.247 | -0.134 | 0. |
| 14 | 0.94151 | INERZIA V SLD | | -0.247 | -0.134 | 0. |
| 14 | 1.88301 | INERZIA V SLD | | -0.247 | -0.134 | 0. |
| 14 | 0. | INERZIA V -1 | | -0.56 | -0.304 | 0. |
| 14 | 0.94151 | INERZIA V -1 | | -0.56 | -0.304 | 0. |
| 14 | 1.88301 | INERZIA V -1 | | -0.56 | -0.304 | 0. |
| 14 | 0. | SLU_1 | Max | -1061.5 | -387.325 | 0. |
| 14 | 0.94151 | SLU_1 | Max | -1052.727 | -502.313 | 0. |
| 14 | 1.88301 | SLU_1 | Max | -1043.955 | -617.301 | 0. |
| 14 | 0. | SLU_1 | Min | -1061.5 | -387.325 | 0. |
| 14 | 0.94151 | SLU_1 | Min | -1052.727 | -502.313 | 0. |
| 14 | 1.88301 | SLU_1 | Min | -1043.955 | -617.301 | 0. |
| 14 | 0. | SLU_2 | Max | -965.462 | -400.016 | 0. |
| 14 | 0.94151 | SLU_2 | Max | -956.69 | -515.004 | 0. |
| 14 | 1.88301 | SLU_2 | Max | -947.917 | -629.992 | 0. |
| 14 | 0. | SLU_2 | Min | -965.462 | -400.016 | 0. |
| 14 | 0.94151 | SLU_2 | Min | -956.69 | -515.004 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 14 | 1.88301 | SLU_2 | Min | -947.917 | -629.992 | 0. |
| 14 | 0. | SLU_3 | Max | -1139.901 | -479.77 | 0. |
| 14 | 0.94151 | SLU_3 | Max | -1131.129 | -594.758 | 0. |
| 14 | 1.88301 | SLU_3 | Max | -1122.356 | -709.746 | 0. |
| 14 | 0. | SLU_3 | Min | -1139.901 | -479.77 | 0. |
| 14 | 0.94151 | SLU_3 | Min | -1131.129 | -594.758 | 0. |
| 14 | 1.88301 | SLU_3 | Min | -1122.356 | -709.746 | 0. |
| 14 | 0. | SLU_4 | Max | -1002.166 | -474.986 | 0. |
| 14 | 0.94151 | SLU_4 | Max | -993.394 | -589.974 | 0. |
| 14 | 1.88301 | SLU_4 | Max | -984.621 | -704.962 | 0. |
| 14 | 0. | SLU_4 | Min | -1002.166 | -474.986 | 0. |
| 14 | 0.94151 | SLU_4 | Min | -993.394 | -589.974 | 0. |
| 14 | 1.88301 | SLU_4 | Min | -984.621 | -704.962 | 0. |
| 14 | 0. | SLE_F1 | Max | -817.962 | -291.339 | 0. |
| 14 | 0.94151 | SLE_F1 | Max | -811.214 | -379.791 | 0. |
| 14 | 1.88301 | SLE_F1 | Max | -804.466 | -468.243 | 0. |
| 14 | 0. | SLE_F1 | Min | -817.962 | -291.339 | 0. |
| 14 | 0.94151 | SLE_F1 | Min | -811.214 | -379.791 | 0. |
| 14 | 1.88301 | SLE_F1 | Min | -804.466 | -468.243 | 0. |
| 14 | 0. | SLE_F2 | Max | -746.764 | -301.509 | 0. |
| 14 | 0.94151 | SLE_F2 | Max | -740.016 | -389.961 | 0. |
| 14 | 1.88301 | SLE_F2 | Max | -733.268 | -478.414 | 0. |
| 14 | 0. | SLE_F2 | Min | -746.764 | -301.509 | 0. |
| 14 | 0.94151 | SLE_F2 | Min | -740.016 | -389.961 | 0. |
| 14 | 1.88301 | SLE_F2 | Min | -733.268 | -478.414 | 0. |
| 14 | 0. | SLE_F3 | Max | -774.088 | -357.28 | 0. |
| 14 | 0.94151 | SLE_F3 | Max | -767.34 | -445.732 | 0. |
| 14 | 1.88301 | SLE_F3 | Max | -760.592 | -534.184 | 0. |
| 14 | 0. | SLE_F3 | Min | -774.088 | -357.28 | 0. |
| 14 | 0.94151 | SLE_F3 | Min | -767.34 | -445.732 | 0. |
| 14 | 1.88301 | SLE_F3 | Min | -760.592 | -534.184 | 0. |
| 14 | 0. | SLE_F4 | Max | -884.21 | -359.421 | 0. |
| 14 | 0.94151 | SLE_F4 | Max | -877.462 | -447.874 | 0. |
| 14 | 1.88301 | SLE_F4 | Max | -870.714 | -536.326 | 0. |
| 14 | 0. | SLE_F4 | Min | -884.21 | -359.421 | 0. |
| 14 | 0.94151 | SLE_F4 | Min | -877.462 | -447.874 | 0. |
| 14 | 1.88301 | SLE_F4 | Min | -870.714 | -536.326 | 0. |
| 14 | 0. | SLE_QP1 | Max | -822.586 | -279.935 | 0. |
| 14 | 0.94151 | SLE_QP1 | Max | -815.838 | -368.387 | 0. |
| 14 | 1.88301 | SLE_QP1 | Max | -809.09 | -456.839 | 0. |
| 14 | 0. | SLE_QP1 | Min | -822.586 | -279.935 | 0. |
| 14 | 0.94151 | SLE_QP1 | Min | -815.838 | -368.387 | 0. |
| 14 | 1.88301 | SLE_QP1 | Min | -809.09 | -456.839 | 0. |
| 14 | 0. | SLE_QP2 | Max | -754.382 | -290.002 | 0. |
| 14 | 0.94151 | SLE_QP2 | Max | -747.634 | -378.454 | 0. |
| 14 | 1.88301 | SLE_QP2 | Max | -740.886 | -466.906 | 0. |
| 14 | 0. | SLE_QP2 | Min | -754.382 | -290.002 | 0. |
| 14 | 0.94151 | SLE_QP2 | Min | -747.634 | -378.454 | 0. |
| 14 | 1.88301 | SLE_QP2 | Min | -740.886 | -466.906 | 0. |
| 14 | 0. | SLE_QP3 | Max | -780.015 | -342.247 | 0. |
| 14 | 0.94151 | SLE_QP3 | Max | -773.267 | -430.7 | 0. |
| 14 | 1.88301 | SLE_QP3 | Max | -766.519 | -519.152 | 0. |
| 14 | 0. | SLE_QP3 | Min | -780.015 | -342.247 | 0. |
| 14 | 0.94151 | SLE_QP3 | Min | -773.267 | -430.7 | 0. |
| 14 | 1.88301 | SLE_QP3 | Min | -766.519 | -519.152 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 14 | 0. | SLE_QP4 | Max | -899.093 | -341.25 | 0. |
| 14 | 0.94151 | SLE_QP4 | Max | -892.345 | -429.702 | 0. |
| 14 | 1.88301 | SLE_QP4 | Max | -885.597 | -518.154 | 0. |
| 14 | 0. | SLE_QP4 | Min | -899.093 | -341.25 | 0. |
| 14 | 0.94151 | SLE_QP4 | Min | -892.345 | -429.702 | 0. |
| 14 | 1.88301 | SLE_QP4 | Min | -885.597 | -518.154 | 0. |
| 14 | 0. | SLV_1 | Max | -1369.979 | -241.65 | 0. |
| 14 | 0.94151 | SLV_1 | Max | -1299.473 | -345.794 | 0. |
| 14 | 1.88301 | SLV_1 | Max | -1228.967 | -449.938 | 0. |
| 14 | 0. | SLV_1 | Min | -1369.979 | -241.65 | 0. |
| 14 | 0.94151 | SLV_1 | Min | -1299.473 | -345.794 | 0. |
| 14 | 1.88301 | SLV_1 | Min | -1228.967 | -449.938 | 0. |
| 14 | 0. | SLV_2 | Max | -1372.043 | -242.339 | 0. |
| 14 | 0.94151 | SLV_2 | Max | -1301.537 | -346.483 | 0. |
| 14 | 1.88301 | SLV_2 | Max | -1231.031 | -450.627 | 0. |
| 14 | 0. | SLV_2 | Min | -1372.043 | -242.339 | 0. |
| 14 | 0.94151 | SLV_2 | Min | -1301.537 | -346.483 | 0. |
| 14 | 1.88301 | SLV_2 | Min | -1231.031 | -450.627 | 0. |
| 14 | 0. | SLV_3 | Max | -1556.227 | -304.745 | 0. |
| 14 | 0.94151 | SLV_3 | Max | -1485.721 | -408.889 | 0. |
| 14 | 1.88301 | SLV_3 | Max | -1415.215 | -513.032 | 0. |
| 14 | 0. | SLV_3 | Min | -1556.227 | -304.745 | 0. |
| 14 | 0.94151 | SLV_3 | Min | -1485.721 | -408.889 | 0. |
| 14 | 1.88301 | SLV_3 | Min | -1415.215 | -513.032 | 0. |
| 14 | 0. | SLV_4 | Max | -1558.153 | -304.706 | 0. |
| 14 | 0.94151 | SLV_4 | Max | -1487.646 | -408.85 | 0. |
| 14 | 1.88301 | SLV_4 | Max | -1417.14 | -512.994 | 0. |
| 14 | 0. | SLV_4 | Min | -1558.153 | -304.706 | 0. |
| 14 | 0.94151 | SLV_4 | Min | -1487.646 | -408.85 | 0. |
| 14 | 1.88301 | SLV_4 | Min | -1417.14 | -512.994 | 0. |
| 14 | 0. | SLD_1 | Max | -1001.755 | -268.099 | 0. |
| 14 | 0.94151 | SLD_1 | Max | -966.848 | -363.481 | 0. |
| 14 | 1.88301 | SLD_1 | Max | -931.942 | -458.864 | 0. |
| 14 | 0. | SLD_1 | Min | -1001.755 | -268.099 | 0. |
| 14 | 0.94151 | SLD_1 | Min | -966.848 | -363.481 | 0. |
| 14 | 1.88301 | SLD_1 | Min | -931.942 | -458.864 | 0. |
| 14 | 0. | SLD_2 | Max | -1002.927 | -268.824 | 0. |
| 14 | 0.94151 | SLD_2 | Max | -968.021 | -364.206 | 0. |
| 14 | 1.88301 | SLD_2 | Max | -933.115 | -459.589 | 0. |
| 14 | 0. | SLD_2 | Min | -1002.927 | -268.824 | 0. |
| 14 | 0.94151 | SLD_2 | Min | -968.021 | -364.206 | 0. |
| 14 | 1.88301 | SLD_2 | Min | -933.115 | -459.589 | 0. |
| 14 | 0. | SLD_3 | Max | -1188.732 | -322.361 | 0. |
| 14 | 0.94151 | SLD_3 | Max | -1153.826 | -417.744 | 0. |
| 14 | 1.88301 | SLD_3 | Max | -1118.919 | -513.126 | 0. |
| 14 | 0. | SLD_3 | Min | -1188.732 | -322.361 | 0. |
| 14 | 0.94151 | SLD_3 | Min | -1153.826 | -417.744 | 0. |
| 14 | 1.88301 | SLD_3 | Min | -1118.919 | -513.126 | 0. |
| 14 | 0. | SLD_4 | Max | -1189.509 | -322.515 | 0. |
| 14 | 0.94151 | SLD_4 | Max | -1154.603 | -417.898 | 0. |
| 14 | 1.88301 | SLD_4 | Max | -1119.697 | -513.28 | 0. |
| 14 | 0. | SLD_4 | Min | -1189.509 | -322.515 | 0. |
| 14 | 0.94151 | SLD_4 | Min | -1154.603 | -417.898 | 0. |
| 14 | 1.88301 | SLD_4 | Min | -1119.697 | -513.28 | 0. |
| 14 | 0. | SLU_IDR_1 | Max | -858.938 | -368.495 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 14 | 0.94151 | SLU_IDR_1 | Max | -852.864 | -471.276 | 0. |
| 14 | 1.88301 | SLU_IDR_1 | Max | -846.791 | -574.058 | 0. |
| 14 | 0. | SLU_IDR_1 | Min | -858.938 | -368.495 | 0. |
| 14 | 0.94151 | SLU_IDR_1 | Min | -852.864 | -471.276 | 0. |
| 14 | 1.88301 | SLU_IDR_1 | Min | -846.791 | -574.058 | 0. |
| 14 | 0. | SLU_IDR_2 | Max | -842.172 | -335.243 | 0. |
| 14 | 0.94151 | SLU_IDR_2 | Max | -836.099 | -438.025 | 0. |
| 14 | 1.88301 | SLU_IDR_2 | Max | -830.026 | -540.806 | 0. |
| 14 | 0. | SLU_IDR_2 | Min | -842.172 | -335.243 | 0. |
| 14 | 0.94151 | SLU_IDR_2 | Min | -836.099 | -438.025 | 0. |
| 14 | 1.88301 | SLU_IDR_2 | Min | -830.026 | -540.806 | 0. |
| 14 | 0. | SISMA WOOD SLV-1 | Max | -557.669 | 108.553 | 0. |
| 14 | 0.94151 | SISMA WOOD SLV-1 | Max | -493.911 | 92.862 | 0. |
| 14 | 1.88301 | SISMA WOOD SLV-1 | Max | -430.153 | 77.17 | 0. |
| 14 | 0. | SISMA WOOD SLV-1 | Min | -557.669 | 108.553 | 0. |
| 14 | 0.94151 | SISMA WOOD SLV-1 | Min | -493.911 | 92.862 | 0. |
| 14 | 1.88301 | SISMA WOOD SLV-1 | Min | -430.153 | 77.17 | 0. |
| 14 | 0. | DEAD-1 | Max | 33.506 | -15.171 | 0. |
| 14 | 0.94151 | DEAD-1 | Max | 40.254 | 12.248 | 0. |
| 14 | 1.88301 | DEAD-1 | Max | 47.002 | 39.667 | 0. |
| 14 | 0. | DEAD-1 | Min | 33.506 | -15.171 | 0. |
| 14 | 0.94151 | DEAD-1 | Min | 40.254 | 12.248 | 0. |
| 14 | 1.88301 | DEAD-1 | Min | 47.002 | 39.667 | 0. |
| 14 | 0. | SLU_PROVA | | -1050.704 | -344.557 | 0. |
| 14 | 0.94151 | SLU_PROVA | | -1041.932 | -459.545 | 0. |
| 14 | 1.88301 | SLU_PROVA | | -1033.159 | -574.533 | 0. |
| 16 | 0. | DEAD | | 11.976 | -10.553 | 0. |
| 16 | 0.39245 | DEAD | | 11.976 | 1.217 | 0. |
| 16 | 0.7849 | DEAD | | 11.976 | 12.987 | 0. |
| 16 | 0. | SIMM_KA | | -147.662 | -3.242 | 0. |
| 16 | 0.39245 | SIMM_KA | | -147.662 | -3.242 | 0. |
| 16 | 0.7849 | SIMM_KA | | -147.662 | -3.242 | 0. |
| 16 | 0. | SIMM_K0 | | -222.816 | -4.951 | 0. |
| 16 | 0.39245 | SIMM_K0 | | -222.816 | -4.951 | 0. |
| 16 | 0.7849 | SIMM_K0 | | -222.816 | -4.951 | 0. |
| 16 | 0. | A--SIMM_KA | | -181.564 | -20.042 | 0. |
| 16 | 0.39245 | A--SIMM_KA | | -181.564 | -20.042 | 0. |
| 16 | 0.7849 | A--SIMM_KA | | -181.564 | -20.042 | 0. |
| 16 | 0. | A--SIMM_K0 | | -279.843 | -29.96 | 0. |
| 16 | 0.39245 | A--SIMM_K0 | | -279.843 | -29.96 | 0. |
| 16 | 0.7849 | A--SIMM_K0 | | -279.843 | -29.96 | 0. |
| 16 | 0. | A-- SIMM_SOVR_K A | | -8.817 | -0.35 | 0. |
| 16 | 0.39245 | A-- SIMM_SOVR_K A | | -8.817 | -0.35 | 0. |
| 16 | 0.7849 | A-- SIMM_SOVR_K A | | -8.817 | -0.35 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 16 | 0. | A-- SIMM_SOVR_K 0 | | -13.22 | -0.524 | 0. |
| 16 | 0.39245 | A-- SIMM_SOVR_K 0 | | -13.22 | -0.524 | 0. |
| 16 | 0.7849 | A-- SIMM_SOVR_K 0 | | -13.22 | -0.524 | 0. |
| 16 | 0. | SIMM_SOVR_K 0 | | -13.22 | -0.524 | 0. |
| 16 | 0.39245 | SIMM_SOVR_K 0 | | -13.22 | -0.524 | 0. |
| 16 | 0.7849 | SIMM_SOVR_K 0 | | -13.22 | -0.524 | 0. |
| 16 | 0. | SIMM_SOVR_K A | | -8.817 | -0.35 | 0. |
| 16 | 0.39245 | SIMM_SOVR_K A | | -8.817 | -0.35 | 0. |
| 16 | 0.7849 | SIMM_SOVR_K A | | -8.817 | -0.35 | 0. |
| 16 | 0. | SOVR | | 8.446 | -0.724 | 0. |
| 16 | 0.39245 | SOVR | | 8.446 | -0.724 | 0. |
| 16 | 0.7849 | SOVR | | 8.446 | -0.724 | 0. |
| 16 | 0. | TERR_SIMM | | 10.053 | -3.808 | 0. |
| 16 | 0.39245 | TERR_SIMM | | 10.053 | -3.808 | 0. |
| 16 | 0.7849 | TERR_SIMM | | 10.053 | -3.808 | 0. |
| 16 | 0. | TERR_A--SIMM | | 14.914 | 2.188 | 0. |
| 16 | 0.39245 | TERR_A--SIMM | | 14.914 | 2.188 | 0. |
| 16 | 0.7849 | TERR_A--SIMM | | 14.914 | 2.188 | 0. |
| 16 | 0. | INERZIA H SLV | | 0.376 | -0.603 | 0. |
| 16 | 0.39245 | INERZIA H SLV | | 0.376 | -0.603 | 0. |
| 16 | 0.7849 | INERZIA H SLV | | 0.376 | -0.603 | 0. |
| 16 | 0. | INERZIA V + SLV | | 0.173 | 0.019 | 0. |
| 16 | 0.39245 | INERZIA V + SLV | | 0.173 | 0.019 | 0. |
| 16 | 0.7849 | INERZIA V + SLV | | 0.173 | 0.019 | 0. |
| 16 | 0. | INERZIA V - SLV | | -0.173 | -0.019 | 0. |
| 16 | 0.39245 | INERZIA V - SLV | | -0.173 | -0.019 | 0. |
| 16 | 0.7849 | INERZIA V - SLV | | -0.173 | -0.019 | 0. |
| 16 | 0. | SISMA WOOD SLV | | -403.24 | -34.653 | 0. |
| 16 | 0.39245 | SISMA WOOD SLV | | -375.871 | -34.653 | 0. |
| 16 | 0.7849 | SISMA WOOD SLV | | -348.501 | -34.653 | 0. |
| 16 | 0. | iDROSTATICA | | -580.943 | 25.792 | 0. |
| 16 | 0.39245 | iDROSTATICA | | -580.943 | -25.776 | 0. |
| 16 | 0.7849 | iDROSTATICA | | -580.943 | -77.344 | 0. |
| 16 | 0. | SISMA WOOD SLD | | -178.087 | -15.304 | 0. |
| 16 | 0.39245 | SISMA WOOD SLD | | -166. | -15.304 | 0. |
| 16 | 0.7849 | SISMA WOOD SLD | | -153.912 | -15.304 | 0. |
| 16 | 0. | INERZIA H SLD | | 0.166 | -0.266 | 0. |
| 16 | 0.39245 | INERZIA H SLD | | 0.166 | -0.266 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|------------|----------|
| 16 | 0.7849 | INERZIA H SLD | | 0.166 | -0.266 | 0. |
| 16 | 0. | INERZIA V + SLD | | 0.076 | 8.600E-03 | 0. |
| 16 | 0.39245 | INERZIA V + SLD | | 0.076 | 8.600E-03 | 0. |
| 16 | 0.7849 | INERZIA V + SLD | | 0.076 | 8.600E-03 | 0. |
| 16 | 0. | INERZIA V SLD | | -0.076 | -8.600E-03 | 0. |
| 16 | 0.39245 | INERZIA V SLD | | -0.076 | -8.600E-03 | 0. |
| 16 | 0.7849 | INERZIA V SLD | | -0.076 | -8.600E-03 | 0. |
| 16 | 0. | INERZIA V -1 | | -0.173 | -0.019 | 0. |
| 16 | 0.39245 | INERZIA V -1 | | -0.173 | -0.019 | 0. |
| 16 | 0.7849 | INERZIA V -1 | | -0.173 | -0.019 | 0. |
| 16 | 0. | SLU_1 | Max | -1027.042 | -0.619 | 0. |
| 16 | 0.39245 | SLU_1 | Max | -1027.042 | -52.356 | 0. |
| 16 | 0.7849 | SLU_1 | Max | -1027.042 | -104.093 | 0. |
| 16 | 0. | SLU_1 | Min | -1027.042 | -0.619 | 0. |
| 16 | 0.39245 | SLU_1 | Min | -1027.042 | -52.356 | 0. |
| 16 | 0.7849 | SLU_1 | Min | -1027.042 | -104.093 | 0. |
| 16 | 0. | SLU_2 | Max | -928.803 | 0.397 | 0. |
| 16 | 0.39245 | SLU_2 | Max | -928.803 | -51.341 | 0. |
| 16 | 0.7849 | SLU_2 | Max | -928.803 | -103.078 | 0. |
| 16 | 0. | SLU_2 | Min | -928.803 | 0.397 | 0. |
| 16 | 0.39245 | SLU_2 | Min | -928.803 | -51.341 | 0. |
| 16 | 0.7849 | SLU_2 | Min | -928.803 | -103.078 | 0. |
| 16 | 0. | SLU_3 | Max | -1091.704 | -46.464 | 0. |
| 16 | 0.39245 | SLU_3 | Max | -1091.704 | -98.201 | 0. |
| 16 | 0.7849 | SLU_3 | Max | -1091.704 | -149.938 | 0. |
| 16 | 0. | SLU_3 | Min | -1091.704 | -46.464 | 0. |
| 16 | 0.39245 | SLU_3 | Min | -1091.704 | -98.201 | 0. |
| 16 | 0.7849 | SLU_3 | Min | -1091.704 | -149.938 | 0. |
| 16 | 0. | SLU_4 | Max | -955.452 | -31.878 | 0. |
| 16 | 0.39245 | SLU_4 | Max | -955.452 | -83.615 | 0. |
| 16 | 0.7849 | SLU_4 | Max | -955.452 | -135.352 | 0. |
| 16 | 0. | SLU_4 | Min | -955.452 | -31.878 | 0. |
| 16 | 0.39245 | SLU_4 | Min | -955.452 | -83.615 | 0. |
| 16 | 0.7849 | SLU_4 | Min | -955.452 | -135.352 | 0. |
| 16 | 0. | SLE_F1 | Max | -791.921 | 0.331 | 0. |
| 16 | 0.39245 | SLE_F1 | Max | -791.921 | -39.467 | 0. |
| 16 | 0.7849 | SLE_F1 | Max | -791.921 | -79.265 | 0. |
| 16 | 0. | SLE_F1 | Min | -791.921 | 0.331 | 0. |
| 16 | 0.39245 | SLE_F1 | Min | -791.921 | -39.467 | 0. |
| 16 | 0.7849 | SLE_F1 | Min | -791.921 | -79.265 | 0. |
| 16 | 0. | SLE_F2 | Max | -718.886 | 0.226 | 0. |
| 16 | 0.39245 | SLE_F2 | Max | -718.886 | -39.572 | 0. |
| 16 | 0.7849 | SLE_F2 | Max | -718.886 | -79.37 | 0. |
| 16 | 0. | SLE_F2 | Min | -718.886 | 0.226 | 0. |
| 16 | 0.39245 | SLE_F2 | Min | -718.886 | -39.572 | 0. |
| 16 | 0.7849 | SLE_F2 | Min | -718.886 | -79.37 | 0. |
| 16 | 0. | SLE_F3 | Max | -738.631 | -25.323 | 0. |
| 16 | 0.39245 | SLE_F3 | Max | -738.631 | -65.121 | 0. |
| 16 | 0.7849 | SLE_F3 | Max | -738.631 | -104.919 | 0. |
| 16 | 0. | SLE_F3 | Min | -738.631 | -25.323 | 0. |
| 16 | 0.39245 | SLE_F3 | Min | -738.631 | -65.121 | 0. |
| 16 | 0.7849 | SLE_F3 | Min | -738.631 | -104.919 | 0. |
| 16 | 0. | SLE_F4 | Max | -847.866 | -35.909 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 16 | 0.39245 | SLE_F4 | Max | -847.866 | -75.707 | 0. |
| 16 | 0.7849 | SLE_F4 | Max | -847.866 | -115.505 | 0. |
| 16 | 0. | SLE_F4 | Min | -847.866 | -35.909 | 0. |
| 16 | 0.39245 | SLE_F4 | Min | -847.866 | -75.707 | 0. |
| 16 | 0.7849 | SLE_F4 | Min | -847.866 | -115.505 | 0. |
| 16 | 0. | SLE_QP1 | Max | -797.084 | 0.192 | 0. |
| 16 | 0.39245 | SLE_QP1 | Max | -797.084 | -39.606 | 0. |
| 16 | 0.7849 | SLE_QP1 | Max | -797.084 | -79.404 | 0. |
| 16 | 0. | SLE_QP1 | Min | -797.084 | 0.192 | 0. |
| 16 | 0.39245 | SLE_QP1 | Min | -797.084 | -39.606 | 0. |
| 16 | 0.7849 | SLE_QP1 | Min | -797.084 | -79.404 | 0. |
| 16 | 0. | SLE_QP2 | Max | -727.101 | 0.078 | 0. |
| 16 | 0.39245 | SLE_QP2 | Max | -727.101 | -39.72 | 0. |
| 16 | 0.7849 | SLE_QP2 | Max | -727.101 | -79.518 | 0. |
| 16 | 0. | SLE_QP2 | Min | -727.101 | 0.078 | 0. |
| 16 | 0.39245 | SLE_QP2 | Min | -727.101 | -39.72 | 0. |
| 16 | 0.7849 | SLE_QP2 | Min | -727.101 | -79.518 | 0. |
| 16 | 0. | SLE_QP3 | Max | -745.443 | -26.81 | 0. |
| 16 | 0.39245 | SLE_QP3 | Max | -745.443 | -66.608 | 0. |
| 16 | 0.7849 | SLE_QP3 | Max | -745.443 | -106.406 | 0. |
| 16 | 0. | SLE_QP3 | Min | -745.443 | -26.81 | 0. |
| 16 | 0.39245 | SLE_QP3 | Min | -745.443 | -66.608 | 0. |
| 16 | 0.7849 | SLE_QP3 | Min | -745.443 | -106.406 | 0. |
| 16 | 0. | SLE_QP4 | Max | -864.141 | -36.204 | 0. |
| 16 | 0.39245 | SLE_QP4 | Max | -864.141 | -76.002 | 0. |
| 16 | 0.7849 | SLE_QP4 | Max | -864.141 | -115.8 | 0. |
| 16 | 0. | SLE_QP4 | Min | -864.141 | -36.204 | 0. |
| 16 | 0.39245 | SLE_QP4 | Min | -864.141 | -76.002 | 0. |
| 16 | 0.7849 | SLE_QP4 | Min | -864.141 | -115.8 | 0. |
| 16 | 0. | SLV_1 | Max | -1676.894 | -82.619 | 0. |
| 16 | 0.39245 | SLV_1 | Max | -1649.525 | -122.417 | 0. |
| 16 | 0.7849 | SLV_1 | Max | -1622.155 | -162.215 | 0. |
| 16 | 0. | SLV_1 | Min | -1676.894 | -82.619 | 0. |
| 16 | 0.39245 | SLV_1 | Min | -1649.525 | -122.417 | 0. |
| 16 | 0.7849 | SLV_1 | Min | -1622.155 | -162.215 | 0. |
| 16 | 0. | SLV_2 | Max | -1678.35 | -81.982 | 0. |
| 16 | 0.39245 | SLV_2 | Max | -1650.98 | -121.78 | 0. |
| 16 | 0.7849 | SLV_2 | Max | -1623.611 | -161.577 | 0. |
| 16 | 0. | SLV_2 | Min | -1678.35 | -81.982 | 0. |
| 16 | 0.39245 | SLV_2 | Min | -1650.98 | -121.78 | 0. |
| 16 | 0.7849 | SLV_2 | Min | -1623.611 | -161.577 | 0. |
| 16 | 0. | SLV_3 | Max | -1852.068 | -120.1 | 0. |
| 16 | 0.39245 | SLV_3 | Max | -1824.698 | -159.898 | 0. |
| 16 | 0.7849 | SLV_3 | Max | -1797.329 | -199.696 | 0. |
| 16 | 0. | SLV_3 | Min | -1852.068 | -120.1 | 0. |
| 16 | 0.39245 | SLV_3 | Min | -1824.698 | -159.898 | 0. |
| 16 | 0.7849 | SLV_3 | Min | -1797.329 | -199.696 | 0. |
| 16 | 0. | SLV_4 | Max | -1853.299 | -120.009 | 0. |
| 16 | 0.39245 | SLV_4 | Max | -1825.929 | -159.807 | 0. |
| 16 | 0.7849 | SLV_4 | Max | -1798.56 | -199.605 | 0. |
| 16 | 0. | SLV_4 | Min | -1853.299 | -120.009 | 0. |
| 16 | 0.39245 | SLV_4 | Min | -1825.929 | -159.807 | 0. |
| 16 | 0.7849 | SLV_4 | Min | -1798.56 | -199.605 | 0. |
| 16 | 0. | SLD_1 | Max | -1123.778 | -30.165 | 0. |
| 16 | 0.39245 | SLD_1 | Max | -1111.69 | -69.963 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 16 | 0.7849 | SLD_1 | Max | -1099.603 | -109.761 | 0. |
| 16 | 0. | SLD_1 | Min | -1123.778 | -30.165 | 0. |
| 16 | 0.39245 | SLD_1 | Min | -1111.69 | -69.963 | 0. |
| 16 | 0.7849 | SLD_1 | Min | -1099.603 | -109.761 | 0. |
| 16 | 0. | SLD_2 | Max | -1124.545 | -30.002 | 0. |
| 16 | 0.39245 | SLD_2 | Max | -1112.458 | -69.8 | 0. |
| 16 | 0.7849 | SLD_2 | Max | -1100.37 | -109.597 | 0. |
| 16 | 0. | SLD_2 | Min | -1124.545 | -30.002 | 0. |
| 16 | 0.39245 | SLD_2 | Min | -1112.458 | -69.8 | 0. |
| 16 | 0.7849 | SLD_2 | Min | -1100.37 | -109.597 | 0. |
| 16 | 0. | SLD_3 | Max | -1301.142 | -69.686 | 0. |
| 16 | 0.39245 | SLD_3 | Max | -1289.054 | -109.484 | 0. |
| 16 | 0.7849 | SLD_3 | Max | -1276.967 | -149.282 | 0. |
| 16 | 0. | SLD_3 | Min | -1301.142 | -69.686 | 0. |
| 16 | 0.39245 | SLD_3 | Min | -1289.054 | -109.484 | 0. |
| 16 | 0.7849 | SLD_3 | Min | -1276.967 | -149.282 | 0. |
| 16 | 0. | SLD_4 | Max | -1301.606 | -69.55 | 0. |
| 16 | 0.39245 | SLD_4 | Max | -1289.518 | -109.348 | 0. |
| 16 | 0.7849 | SLD_4 | Max | -1277.431 | -149.146 | 0. |
| 16 | 0. | SLD_4 | Min | -1301.606 | -69.55 | 0. |
| 16 | 0.39245 | SLD_4 | Min | -1289.518 | -109.348 | 0. |
| 16 | 0.7849 | SLD_4 | Min | -1277.431 | -149.146 | 0. |
| 16 | 0. | SLU_IDR_1 | Max | -816.414 | -25.194 | 0. |
| 16 | 0.39245 | SLU_IDR_1 | Max | -816.414 | -71.325 | 0. |
| 16 | 0.7849 | SLU_IDR_1 | Max | -816.414 | -117.457 | 0. |
| 16 | 0. | SLU_IDR_1 | Min | -816.414 | -25.194 | 0. |
| 16 | 0.39245 | SLU_IDR_1 | Min | -816.414 | -71.325 | 0. |
| 16 | 0.7849 | SLU_IDR_1 | Min | -816.414 | -117.457 | 0. |
| 16 | 0. | SLU_IDR_2 | Max | -806.024 | 0.834 | 0. |
| 16 | 0.39245 | SLU_IDR_2 | Max | -806.024 | -45.297 | 0. |
| 16 | 0.7849 | SLU_IDR_2 | Max | -806.024 | -91.429 | 0. |
| 16 | 0. | SLU_IDR_2 | Min | -806.024 | 0.834 | 0. |
| 16 | 0.39245 | SLU_IDR_2 | Min | -806.024 | -45.297 | 0. |
| 16 | 0.7849 | SLU_IDR_2 | Min | -806.024 | -91.429 | 0. |
| 16 | 0. | SISMA WOOD SLV-1 | Max | -901.453 | -27.863 | 0. |
| 16 | 0.39245 | SISMA WOOD SLV-1 | Max | -874.084 | -27.863 | 0. |
| 16 | 0.7849 | SISMA WOOD SLV-1 | Max | -846.714 | -27.863 | 0. |
| 16 | 0. | SISMA WOOD SLV-1 | Min | -901.453 | -27.863 | 0. |
| 16 | 0.39245 | SISMA WOOD SLV-1 | Min | -874.084 | -27.863 | 0. |
| 16 | 0.7849 | SISMA WOOD SLV-1 | Min | -846.714 | -27.863 | 0. |
| 16 | 0. | DEAD-1 | Max | 16.915 | -10.698 | 0. |
| 16 | 0.39245 | DEAD-1 | Max | 16.915 | 1.072 | 0. |
| 16 | 0.7849 | DEAD-1 | Max | 16.915 | 12.842 | 0. |
| 16 | 0. | DEAD-1 | Min | 16.915 | -10.698 | 0. |
| 16 | 0.39245 | DEAD-1 | Min | 16.915 | 1.072 | 0. |
| 16 | 0.7849 | DEAD-1 | Min | 16.915 | 12.842 | 0. |
| 16 | 0. | SLU_PROVA | | -1023.41 | 6.552 | 0. |
| 16 | 0.39245 | SLU_PROVA | | -1023.41 | -45.186 | 0. |
| 16 | 0.7849 | SLU_PROVA | | -1023.41 | -96.923 | 0. |
| 17 | 0. | DEAD | | 12.232 | -14.699 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 17 | 0.6275 | DEAD | | 14.481 | 3.986 | 0. |
| 17 | 1.255 | DEAD | | 16.731 | 22.67 | 0. |
| 17 | 0. | SIMM_KA | | -147.35 | 6.692 | 0. |
| 17 | 0.6275 | SIMM_KA | | -147.35 | 6.692 | 0. |
| 17 | 1.255 | SIMM_KA | | -147.35 | 6.692 | 0. |
| 17 | 0. | SIMM_K0 | | -222.357 | 9.927 | 0. |
| 17 | 0.6275 | SIMM_K0 | | -222.357 | 9.927 | 0. |
| 17 | 1.255 | SIMM_K0 | | -222.357 | 9.927 | 0. |
| 17 | 0. | A--SIMM_KA | | -183.12 | -7.377 | 0. |
| 17 | 0.6275 | A--SIMM_KA | | -183.12 | -7.377 | 0. |
| 17 | 1.255 | A--SIMM_KA | | -183.12 | -7.377 | 0. |
| 17 | 0. | A--SIMM_K0 | | -282.124 | -10.433 | 0. |
| 17 | 0.6275 | A--SIMM_K0 | | -282.124 | -10.433 | 0. |
| 17 | 1.255 | A--SIMM_K0 | | -282.124 | -10.433 | 0. |
| 17 | 0. | A-- SIMM_SOVR_K A | | -8.835 | -0.132 | 0. |
| 17 | 0.6275 | A-- SIMM_SOVR_K A | | -8.835 | -0.132 | 0. |
| 17 | 1.255 | A-- SIMM_SOVR_K A | | -8.835 | -0.132 | 0. |
| 17 | 0. | A-- SIMM_SOVR_K 0 | | -13.246 | -0.197 | 0. |
| 17 | 0.6275 | A-- SIMM_SOVR_K 0 | | -13.246 | -0.197 | 0. |
| 17 | 1.255 | A-- SIMM_SOVR_K 0 | | -13.246 | -0.197 | 0. |
| 17 | 0. | SIMM_SOVR_K 0 | | -13.246 | -0.197 | 0. |
| 17 | 0.6275 | SIMM_SOVR_K 0 | | -13.246 | -0.197 | 0. |
| 17 | 1.255 | SIMM_SOVR_K 0 | | -13.246 | -0.197 | 0. |
| 17 | 0. | SIMM_SOVR_K A | | -8.835 | -0.132 | 0. |
| 17 | 0.6275 | SIMM_SOVR_K A | | -8.835 | -0.132 | 0. |
| 17 | 1.255 | SIMM_SOVR_K A | | -8.835 | -0.132 | 0. |
| 17 | 0. | SOVR | | 8.223 | -3.373 | 0. |
| 17 | 0.6275 | SOVR | | 8.223 | -3.373 | 0. |
| 17 | 1.255 | SOVR | | 8.223 | -3.373 | 0. |
| 17 | 0. | TERR_SIMM | | 9.124 | -13.718 | 0. |
| 17 | 0.6275 | TERR_SIMM | | 9.124 | -13.718 | 0. |
| 17 | 1.255 | TERR_SIMM | | 9.124 | -13.718 | 0. |
| 17 | 0. | TERR_A--SIMM | | 14.509 | -11.448 | 0. |
| 17 | 0.6275 | TERR_A--SIMM | | 14.509 | -11.448 | 0. |
| 17 | 1.255 | TERR_A--SIMM | | 14.509 | -11.448 | 0. |
| 17 | 0. | INERZIA H SLV | | 1.282 | -0.615 | 0. |
| 17 | 0.6275 | INERZIA H SLV | | 1.282 | -0.615 | 0. |
| 17 | 1.255 | INERZIA H SLV | | 1.282 | -0.615 | 0. |
| 17 | 0. | INERZIA V + SLV | | 0.214 | 0.066 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 17 | 0.6275 | INERZIA V + SLV | | 0.214 | 0.066 | 0. |
| 17 | 1.255 | INERZIA V + SLV | | 0.214 | 0.066 | 0. |
| 17 | 0. | INERZIA V - SLV | | -0.214 | -0.066 | 0. |
| 17 | 0.6275 | INERZIA V - SLV | | -0.214 | -0.066 | 0. |
| 17 | 1.255 | INERZIA V - SLV | | -0.214 | -0.066 | 0. |
| 17 | 0. | SISMA WOOD SLV | | -350.609 | 2.542 | 0. |
| 17 | 0.6275 | SISMA WOOD SLV | | -307.161 | -2.689 | 0. |
| 17 | 1.255 | SISMA WOOD SLV | | -263.713 | -7.919 | 0. |
| 17 | 0. | iDROSTATICA | | -582.937 | 59.307 | 0. |
| 17 | 0.6275 | iDROSTATICA | | -582.937 | -19.226 | 0. |
| 17 | 1.255 | iDROSTATICA | | -582.937 | -100.372 | 0. |
| 17 | 0. | SISMA WOOD SLD | | -154.843 | 1.122 | 0. |
| 17 | 0.6275 | SISMA WOOD SLD | | -135.655 | -1.188 | 0. |
| 17 | 1.255 | SISMA WOOD SLD | | -116.466 | -3.498 | 0. |
| 17 | 0. | INERZIA H SLD | | 0.566 | -0.272 | 0. |
| 17 | 0.6275 | INERZIA H SLD | | 0.566 | -0.272 | 0. |
| 17 | 1.255 | INERZIA H SLD | | 0.566 | -0.272 | 0. |
| 17 | 0. | INERZIA V + SLD | | 0.094 | 0.029 | 0. |
| 17 | 0.6275 | INERZIA V + SLD | | 0.094 | 0.029 | 0. |
| 17 | 1.255 | INERZIA V + SLD | | 0.094 | 0.029 | 0. |
| 17 | 0. | INERZIA V SLD | | -0.094 | -0.029 | 0. |
| 17 | 0.6275 | INERZIA V SLD | | -0.094 | -0.029 | 0. |
| 17 | 1.255 | INERZIA V SLD | | -0.094 | -0.029 | 0. |
| 17 | 0. | INERZIA V -1 | | -0.214 | -0.066 | 0. |
| 17 | 0.6275 | INERZIA V -1 | | -0.214 | -0.066 | 0. |
| 17 | 1.255 | INERZIA V -1 | | -0.214 | -0.066 | 0. |
| 17 | 0. | SLU_1 | Max | -1032.121 | 19.412 | 0. |
| 17 | 0.6275 | SLU_1 | Max | -1029.196 | -58.391 | 0. |
| 17 | 1.255 | SLU_1 | Max | -1026.272 | -139.591 | 0. |
| 17 | 0. | SLU_1 | Min | -1032.121 | 19.412 | 0. |
| 17 | 0.6275 | SLU_1 | Min | -1029.196 | -58.391 | 0. |
| 17 | 1.255 | SLU_1 | Min | -1026.272 | -139.591 | 0. |
| 17 | 0. | SLU_2 | Max | -934.465 | 8.681 | 0. |
| 17 | 0.6275 | SLU_2 | Max | -931.541 | -69.122 | 0. |
| 17 | 1.255 | SLU_2 | Max | -928.616 | -150.322 | 0. |
| 17 | 0. | SLU_2 | Min | -934.465 | 8.681 | 0. |
| 17 | 0.6275 | SLU_2 | Min | -931.541 | -69.122 | 0. |
| 17 | 1.255 | SLU_2 | Min | -928.616 | -150.322 | 0. |
| 17 | 0. | SLU_3 | Max | -1101.799 | -18.379 | 0. |
| 17 | 0.6275 | SLU_3 | Max | -1098.875 | -96.182 | 0. |
| 17 | 1.255 | SLU_3 | Max | -1095.951 | -177.382 | 0. |
| 17 | 0. | SLU_3 | Min | -1101.799 | -18.379 | 0. |
| 17 | 0.6275 | SLU_3 | Min | -1098.875 | -96.182 | 0. |
| 17 | 1.255 | SLU_3 | Min | -1095.951 | -177.382 | 0. |
| 17 | 0. | SLU_4 | Max | -964.78 | -20.179 | 0. |
| 17 | 0.6275 | SLU_4 | Max | -961.856 | -97.982 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 17 | 1.255 | SLU_4 | Max | -958.932 | -179.183 | 0. |
| 17 | 0. | SLU_4 | Min | -964.78 | -20.179 | 0. |
| 17 | 0.6275 | SLU_4 | Min | -961.856 | -97.982 | 0. |
| 17 | 1.255 | SLU_4 | Min | -958.932 | -179.183 | 0. |
| 17 | 0. | SLE_F1 | Max | -795.718 | 15.96 | 0. |
| 17 | 0.6275 | SLE_F1 | Max | -793.468 | -43.888 | 0. |
| 17 | 1.255 | SLE_F1 | Max | -791.219 | -106.35 | 0. |
| 17 | 0. | SLE_F1 | Min | -795.718 | 15.96 | 0. |
| 17 | 0.6275 | SLE_F1 | Min | -793.468 | -43.888 | 0. |
| 17 | 1.255 | SLE_F1 | Min | -791.219 | -106.35 | 0. |
| 17 | 0. | SLE_F2 | Max | -723.218 | 7.128 | 0. |
| 17 | 0.6275 | SLE_F2 | Max | -720.969 | -52.72 | 0. |
| 17 | 1.255 | SLE_F2 | Max | -718.72 | -115.182 | 0. |
| 17 | 0. | SLE_F2 | Min | -723.218 | 7.128 | 0. |
| 17 | 0.6275 | SLE_F2 | Min | -720.969 | -52.72 | 0. |
| 17 | 1.255 | SLE_F2 | Min | -718.72 | -115.182 | 0. |
| 17 | 0. | SLE_F3 | Max | -745.876 | -15.879 | 0. |
| 17 | 0.6275 | SLE_F3 | Max | -743.627 | -75.728 | 0. |
| 17 | 1.255 | SLE_F3 | Max | -741.378 | -138.19 | 0. |
| 17 | 0. | SLE_F3 | Min | -745.876 | -15.879 | 0. |
| 17 | 0.6275 | SLE_F3 | Min | -743.627 | -75.728 | 0. |
| 17 | 1.255 | SLE_F3 | Min | -741.378 | -138.19 | 0. |
| 17 | 0. | SLE_F4 | Max | -855.594 | -13.336 | 0. |
| 17 | 0.6275 | SLE_F4 | Max | -853.344 | -73.184 | 0. |
| 17 | 1.255 | SLE_F4 | Max | -851.095 | -135.646 | 0. |
| 17 | 0. | SLE_F4 | Min | -855.594 | -13.336 | 0. |
| 17 | 0.6275 | SLE_F4 | Min | -853.344 | -73.184 | 0. |
| 17 | 1.255 | SLE_F4 | Min | -851.095 | -135.646 | 0. |
| 17 | 0. | SLE_QP1 | Max | -800.859 | 16.455 | 0. |
| 17 | 0.6275 | SLE_QP1 | Max | -798.61 | -43.394 | 0. |
| 17 | 1.255 | SLE_QP1 | Max | -796.361 | -105.856 | 0. |
| 17 | 0. | SLE_QP1 | Min | -800.859 | 16.455 | 0. |
| 17 | 0.6275 | SLE_QP1 | Min | -798.61 | -43.394 | 0. |
| 17 | 1.255 | SLE_QP1 | Min | -796.361 | -105.856 | 0. |
| 17 | 0. | SLE_QP2 | Max | -731.392 | 7.964 | 0. |
| 17 | 0.6275 | SLE_QP2 | Max | -729.143 | -51.884 | 0. |
| 17 | 1.255 | SLE_QP2 | Max | -726.894 | -114.346 | 0. |
| 17 | 0. | SLE_QP2 | Min | -731.392 | 7.964 | 0. |
| 17 | 0.6275 | SLE_QP2 | Min | -729.143 | -51.884 | 0. |
| 17 | 1.255 | SLE_QP2 | Min | -726.894 | -114.346 | 0. |
| 17 | 0. | SLE_QP3 | Max | -752.817 | -16.541 | 0. |
| 17 | 0.6275 | SLE_QP3 | Max | -750.568 | -76.39 | 0. |
| 17 | 1.255 | SLE_QP3 | Max | -748.319 | -138.852 | 0. |
| 17 | 0. | SLE_QP3 | Min | -752.817 | -16.541 | 0. |
| 17 | 0.6275 | SLE_QP3 | Min | -750.568 | -76.39 | 0. |
| 17 | 1.255 | SLE_QP3 | Min | -748.319 | -138.852 | 0. |
| 17 | 0. | SLE_QP4 | Max | -871.787 | -11.683 | 0. |
| 17 | 0.6275 | SLE_QP4 | Max | -869.538 | -71.531 | 0. |
| 17 | 1.255 | SLE_QP4 | Max | -867.289 | -133.993 | 0. |
| 17 | 0. | SLE_QP4 | Min | -871.787 | -11.683 | 0. |
| 17 | 0.6275 | SLE_QP4 | Min | -869.538 | -71.531 | 0. |
| 17 | 1.255 | SLE_QP4 | Min | -867.289 | -133.993 | 0. |
| 17 | 0. | SLV_1 | Max | -1629.533 | 27.728 | 0. |
| 17 | 0.6275 | SLV_1 | Max | -1583.836 | -37.351 | 0. |
| 17 | 1.255 | SLV_1 | Max | -1538.139 | -105.044 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 17 | 0. | SLV_1 | Min | -1629.533 | 27.728 | 0. |
| 17 | 0.6275 | SLV_1 | Min | -1583.836 | -37.351 | 0. |
| 17 | 1.255 | SLV_1 | Min | -1538.139 | -105.044 | 0. |
| 17 | 0. | SLV_2 | Max | -1630.976 | 27.921 | 0. |
| 17 | 0.6275 | SLV_2 | Max | -1585.279 | -37.158 | 0. |
| 17 | 1.255 | SLV_2 | Max | -1539.582 | -104.851 | 0. |
| 17 | 0. | SLV_2 | Min | -1630.976 | 27.921 | 0. |
| 17 | 0.6275 | SLV_2 | Min | -1585.279 | -37.158 | 0. |
| 17 | 1.255 | SLV_2 | Min | -1539.582 | -104.851 | 0. |
| 17 | 0. | SLV_3 | Max | -1808.57 | 4.023 | 0. |
| 17 | 0.6275 | SLV_3 | Max | -1762.872 | -61.055 | 0. |
| 17 | 1.255 | SLV_3 | Max | -1717.175 | -128.748 | 0. |
| 17 | 0. | SLV_3 | Min | -1808.57 | 4.023 | 0. |
| 17 | 0.6275 | SLV_3 | Min | -1762.872 | -61.055 | 0. |
| 17 | 1.255 | SLV_3 | Min | -1717.175 | -128.748 | 0. |
| 17 | 0. | SLV_4 | Max | -1809.86 | 4.135 | 0. |
| 17 | 0.6275 | SLV_4 | Max | -1764.163 | -60.944 | 0. |
| 17 | 1.255 | SLV_4 | Max | -1718.465 | -128.636 | 0. |
| 17 | 0. | SLV_4 | Min | -1809.86 | 4.135 | 0. |
| 17 | 0.6275 | SLV_4 | Min | -1764.163 | -60.944 | 0. |
| 17 | 1.255 | SLV_4 | Min | -1718.465 | -128.636 | 0. |
| 17 | 0. | SLD_1 | Max | -1104.38 | 22.62 | 0. |
| 17 | 0.6275 | SLD_1 | Max | -1082.942 | -39.539 | 0. |
| 17 | 1.255 | SLD_1 | Max | -1061.504 | -104.311 | 0. |
| 17 | 0. | SLD_1 | Min | -1104.38 | 22.62 | 0. |
| 17 | 0.6275 | SLD_1 | Min | -1082.942 | -39.539 | 0. |
| 17 | 1.255 | SLD_1 | Min | -1061.504 | -104.311 | 0. |
| 17 | 0. | SLD_2 | Max | -1105.174 | 22.44 | 0. |
| 17 | 0.6275 | SLD_2 | Max | -1083.736 | -39.718 | 0. |
| 17 | 1.255 | SLD_2 | Max | -1062.298 | -104.49 | 0. |
| 17 | 0. | SLD_2 | Min | -1105.174 | 22.44 | 0. |
| 17 | 0.6275 | SLD_2 | Min | -1083.736 | -39.718 | 0. |
| 17 | 1.255 | SLD_2 | Min | -1062.298 | -104.49 | 0. |
| 17 | 0. | SLD_3 | Max | -1285.519 | 1.895 | 0. |
| 17 | 0.6275 | SLD_3 | Max | -1264.081 | -60.263 | 0. |
| 17 | 1.255 | SLD_3 | Max | -1242.643 | -125.035 | 0. |
| 17 | 0. | SLD_3 | Min | -1285.519 | 1.895 | 0. |
| 17 | 0.6275 | SLD_3 | Min | -1264.081 | -60.263 | 0. |
| 17 | 1.255 | SLD_3 | Min | -1242.643 | -125.035 | 0. |
| 17 | 0. | SLD_4 | Max | -1285.997 | 1.8 | 0. |
| 17 | 0.6275 | SLD_4 | Max | -1264.56 | -60.358 | 0. |
| 17 | 1.255 | SLD_4 | Max | -1243.122 | -125.13 | 0. |
| 17 | 0. | SLD_4 | Min | -1285.997 | 1.8 | 0. |
| 17 | 0.6275 | SLD_4 | Min | -1264.56 | -60.358 | 0. |
| 17 | 1.255 | SLD_4 | Min | -1243.122 | -125.13 | 0. |
| 17 | 0. | SLU_IDR_1 | Max | -824.599 | -19.025 | 0. |
| 17 | 0.6275 | SLU_IDR_1 | Max | -822.575 | -88.595 | 0. |
| 17 | 1.255 | SLU_IDR_1 | Max | -820.551 | -161.04 | 0. |
| 17 | 0. | SLU_IDR_1 | Min | -824.599 | -19.025 | 0. |
| 17 | 0.6275 | SLU_IDR_1 | Min | -822.575 | -88.595 | 0. |
| 17 | 1.255 | SLU_IDR_1 | Min | -820.551 | -161.04 | 0. |
| 17 | 0. | SLU_IDR_2 | Max | -811.173 | 5.577 | 0. |
| 17 | 0.6275 | SLU_IDR_2 | Max | -809.149 | -63.993 | 0. |
| 17 | 1.255 | SLU_IDR_2 | Max | -807.124 | -136.438 | 0. |
| 17 | 0. | SLU_IDR_2 | Min | -811.173 | 5.577 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 17 | 0.6275 | SLU_IDR_2 | Min | -809.149 | -63.993 | 0. |
| 17 | 1.255 | SLU_IDR_2 | Min | -807.124 | -136.438 | 0. |
| 17 | 0. | SISMA WOOD SLV-1 | Max | -843.975 | 73.538 | 0. |
| 17 | 0.6275 | SISMA WOOD SLV-1 | Max | -800.527 | 68.307 | 0. |
| 17 | 1.255 | SISMA WOOD SLV-1 | Max | -757.079 | 63.077 | 0. |
| 17 | 0. | SISMA WOOD SLV-1 | Min | -843.975 | 73.538 | 0. |
| 17 | 0.6275 | SISMA WOOD SLV-1 | Min | -800.527 | 68.307 | 0. |
| 17 | 1.255 | SISMA WOOD SLV-1 | Min | -757.079 | 63.077 | 0. |
| 17 | 0. | DEAD-1 | Max | 17.103 | -15.77 | 0. |
| 17 | 0.6275 | DEAD-1 | Max | 19.353 | 2.915 | 0. |
| 17 | 1.255 | DEAD-1 | Max | 21.602 | 21.599 | 0. |
| 17 | 0. | DEAD-1 | Min | 17.103 | -15.77 | 0. |
| 17 | 0.6275 | DEAD-1 | Min | 19.353 | 2.915 | 0. |
| 17 | 1.255 | DEAD-1 | Min | 21.602 | 21.599 | 0. |
| 17 | 0. | SLU_PROVA | | -1026.654 | 47.708 | 0. |
| 17 | 0.6275 | SLU_PROVA | | -1023.729 | -30.095 | 0. |
| 17 | 1.255 | SLU_PROVA | | -1020.805 | -111.295 | 0. |
| 19 | 0. | DEAD | | -302.795 | 61.609 | 0. |
| 19 | 0.5 | DEAD | | -284.05 | 61.609 | 0. |
| 19 | 1. | DEAD | | -265.306 | 61.609 | 0. |
| 19 | 0. | SIMM_KA | | -12.176 | -86.956 | 0. |
| 19 | 0.5 | SIMM_KA | | -12.176 | -63.449 | 0. |
| 19 | 1. | SIMM_KA | | -12.176 | -41.641 | 0. |
| 19 | 0. | SIMM_K0 | | -18.659 | -132.355 | 0. |
| 19 | 0.5 | SIMM_K0 | | -18.659 | -97.095 | 0. |
| 19 | 1. | SIMM_K0 | | -18.659 | -64.385 | 0. |
| 19 | 0. | A--SIMM_KA | | -53.237 | -64.136 | 0. |
| 19 | 0.5 | A--SIMM_KA | | -53.237 | -46.354 | 0. |
| 19 | 1. | A--SIMM_KA | | -53.237 | -29.586 | 0. |
| 19 | 0. | A--SIMM_K0 | | -79.793 | -102.202 | 0. |
| 19 | 0.5 | A--SIMM_K0 | | -79.793 | -70.192 | 0. |
| 19 | 1. | A--SIMM_K0 | | -79.793 | -41.232 | 0. |
| 19 | 0. | A-- SIMM_SOVR_K A | | -1.62 | -11.645 | 0. |
| 19 | 0.5 | A-- SIMM_SOVR_K A | | -1.62 | -11.645 | 0. |
| 19 | 1. | A-- SIMM_SOVR_K A | | -1.62 | -11.645 | 0. |
| 19 | 0. | A-- SIMM_SOVR_K 0 | | -2.429 | -17.458 | 0. |
| 19 | 0.5 | A-- SIMM_SOVR_K 0 | | -2.429 | -17.458 | 0. |
| 19 | 1. | A-- SIMM_SOVR_K 0 | | -2.429 | -17.458 | 0. |
| 19 | 0. | SIMM_SOVR_K 0 | | -2.429 | -17.458 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|----------|----------|
| 19 | 0.5 | SIMM_SOVR_K 0 | | -2.429 | -17.458 | 0. |
| 19 | 1. | SIMM_SOVR_K 0 | | -2.429 | -17.458 | 0. |
| 19 | 0. | SIMM_SOVR_K A | | -1.62 | -11.645 | 0. |
| 19 | 0.5 | SIMM_SOVR_K A | | -1.62 | -11.645 | 0. |
| 19 | 1. | SIMM_SOVR_K A | | -1.62 | -11.645 | 0. |
| 19 | 0. | SOVR | | -195.45 | 36.857 | 0. |
| 19 | 0.5 | SOVR | | -195.45 | 36.857 | 0. |
| 19 | 1. | SOVR | | -195.45 | 36.857 | 0. |
| 19 | 0. | TERR_SIMM | | -782.714 | 115.777 | 0. |
| 19 | 0.5 | TERR_SIMM | | -782.714 | 115.777 | 0. |
| 19 | 1. | TERR_SIMM | | -782.714 | 115.777 | 0. |
| 19 | 0. | TERR_A--SIMM | | -764.488 | 140.16 | 0. |
| 19 | 0.5 | TERR_A--SIMM | | -764.488 | 140.16 | 0. |
| 19 | 1. | TERR_A--SIMM | | -764.488 | 140.16 | 0. |
| 19 | 0. | INERZIA H SLV | | -4.979 | 1.145 | 0. |
| 19 | 0.5 | INERZIA H SLV | | -4.979 | 1.145 | 0. |
| 19 | 1. | INERZIA H SLV | | -4.979 | 1.145 | 0. |
| 19 | 0. | INERZIA V + SLV | | -4.591 | 0.975 | 0. |
| 19 | 0.5 | INERZIA V + SLV | | -4.591 | 0.975 | 0. |
| 19 | 1. | INERZIA V + SLV | | -4.591 | 0.975 | 0. |
| 19 | 0. | INERZIA V - SLV | | 4.591 | -0.975 | 0. |
| 19 | 0.5 | INERZIA V - SLV | | 4.591 | -0.975 | 0. |
| 19 | 1. | INERZIA V - SLV | | 4.591 | -0.975 | 0. |
| 19 | 0. | SISMA WOOD SLV | | -218.64 | -8.38 | 0. |
| 19 | 0.5 | SISMA WOOD SLV | | -218.64 | -8.38 | 0. |
| 19 | 1. | SISMA WOOD SLV | | -218.64 | -8.38 | 0. |
| 19 | 0. | iDROSTATICA | | -364.069 | -234.407 | 0. |
| 19 | 0.5 | iDROSTATICA | | -364.069 | -183.557 | 0. |
| 19 | 1. | iDROSTATICA | | -364.069 | -137.807 | 0. |
| 19 | 0. | SISMA WOOD SLD | | -96.56 | -3.701 | 0. |
| 19 | 0.5 | SISMA WOOD SLD | | -96.56 | -3.701 | 0. |
| 19 | 1. | SISMA WOOD SLD | | -96.56 | -3.701 | 0. |
| 19 | 0. | INERZIA H SLD | | -2.199 | 0.505 | 0. |
| 19 | 0.5 | INERZIA H SLD | | -2.199 | 0.505 | 0. |
| 19 | 1. | INERZIA H SLD | | -2.199 | 0.505 | 0. |
| 19 | 0. | INERZIA V + SLD | | -2.028 | 0.431 | 0. |
| 19 | 0.5 | INERZIA V + SLD | | -2.028 | 0.431 | 0. |
| 19 | 1. | INERZIA V + SLD | | -2.028 | 0.431 | 0. |
| 19 | 0. | INERZIA V SLD | | 2.028 | -0.431 | 0. |
| 19 | 0.5 | INERZIA V SLD | | 2.028 | -0.431 | 0. |
| 19 | 1. | INERZIA V SLD | | 2.028 | -0.431 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------|----------|-----------|----------|----------|
| 19 | 0. | INERZIA V -1 | | 4.591 | -0.975 | 0. |
| 19 | 0.5 | INERZIA V -1 | | 4.591 | -0.975 | 0. |
| 19 | 1. | INERZIA V -1 | | 4.591 | -0.975 | 0. |
| 19 | 0. | SLU_1 | Max | -2415.919 | -182.185 | 0. |
| 19 | 0.5 | SLU_1 | Max | -2391.552 | -70.242 | 0. |
| 19 | 1. | SLU_1 | Max | -2367.184 | 31.756 | 0. |
| 19 | 0. | SLU_1 | Min | -2415.919 | -182.185 | 0. |
| 19 | 0.5 | SLU_1 | Min | -2391.552 | -70.242 | 0. |
| 19 | 1. | SLU_1 | Min | -2367.184 | 31.756 | 0. |
| 19 | 0. | SLU_2 | Max | -2416.041 | -112.082 | 0. |
| 19 | 0.5 | SLU_2 | Max | -2391.673 | -15.419 | 0. |
| 19 | 1. | SLU_2 | Max | -2367.305 | 72.407 | 0. |
| 19 | 0. | SLU_2 | Min | -2416.041 | -112.082 | 0. |
| 19 | 0.5 | SLU_2 | Min | -2391.673 | -15.419 | 0. |
| 19 | 1. | SLU_2 | Min | -2367.305 | 72.407 | 0. |
| 19 | 0. | SLU_3 | Max | -2486.22 | -68.147 | 0. |
| 19 | 0.5 | SLU_3 | Max | -2461.852 | 39.571 | 0. |
| 19 | 1. | SLU_3 | Max | -2437.484 | 136.694 | 0. |
| 19 | 0. | SLU_3 | Min | -2486.22 | -68.147 | 0. |
| 19 | 0.5 | SLU_3 | Min | -2461.852 | 39.571 | 0. |
| 19 | 1. | SLU_3 | Min | -2437.484 | 136.694 | 0. |
| 19 | 0. | SLU_4 | Max | -2467.818 | -13.314 | 0. |
| 19 | 0.5 | SLU_4 | Max | -2443.45 | 75.909 | 0. |
| 19 | 1. | SLU_4 | Max | -2419.082 | 157.181 | 0. |
| 19 | 0. | SLU_4 | Min | -2467.818 | -13.314 | 0. |
| 19 | 0.5 | SLU_4 | Min | -2443.45 | 75.909 | 0. |
| 19 | 1. | SLU_4 | Min | -2419.082 | 157.181 | 0. |
| 19 | 0. | SLE_F1 | Max | -1767.213 | -152.617 | 0. |
| 19 | 0.5 | SLE_F1 | Max | -1748.469 | -66.507 | 0. |
| 19 | 1. | SLE_F1 | Max | -1729.724 | 11.953 | 0. |
| 19 | 0. | SLE_F1 | Min | -1767.213 | -152.617 | 0. |
| 19 | 0.5 | SLE_F1 | Min | -1748.469 | -66.507 | 0. |
| 19 | 1. | SLE_F1 | Min | -1729.724 | 11.953 | 0. |
| 19 | 0. | SLE_F2 | Max | -1767.381 | -101.667 | 0. |
| 19 | 0.5 | SLE_F2 | Max | -1748.636 | -27.311 | 0. |
| 19 | 1. | SLE_F2 | Max | -1729.892 | 40.248 | 0. |
| 19 | 0. | SLE_F2 | Min | -1767.381 | -101.667 | 0. |
| 19 | 0.5 | SLE_F2 | Min | -1748.636 | -27.311 | 0. |
| 19 | 1. | SLE_F2 | Min | -1729.892 | 40.248 | 0. |
| 19 | 0. | SLE_F3 | Max | -1807.688 | -25.528 | 0. |
| 19 | 0.5 | SLE_F3 | Max | -1788.943 | 43.105 | 0. |
| 19 | 1. | SLE_F3 | Max | -1770.199 | 105.622 | 0. |
| 19 | 0. | SLE_F3 | Min | -1807.688 | -25.528 | 0. |
| 19 | 0.5 | SLE_F3 | Min | -1788.943 | 43.105 | 0. |
| 19 | 1. | SLE_F3 | Min | -1770.199 | 105.622 | 0. |
| 19 | 0. | SLE_F4 | Max | -1822.691 | -66.006 | 0. |
| 19 | 0.5 | SLE_F4 | Max | -1803.947 | 16.854 | 0. |
| 19 | 1. | SLE_F4 | Max | -1785.202 | 91.564 | 0. |
| 19 | 0. | SLE_F4 | Min | -1822.691 | -66.006 | 0. |
| 19 | 0.5 | SLE_F4 | Min | -1803.947 | 16.854 | 0. |
| 19 | 1. | SLE_F4 | Min | -1785.202 | 91.564 | 0. |
| 19 | 0. | SLE_QP1 | Max | -1597.896 | -176.726 | 0. |
| 19 | 0.5 | SLE_QP1 | Max | -1579.151 | -90.616 | 0. |
| 19 | 1. | SLE_QP1 | Max | -1560.407 | -12.156 | 0. |
| 19 | 0. | SLE_QP1 | Min | -1597.896 | -176.726 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 19 | 0.5 | SLE_QP1 | Min | -1579.151 | -90.616 | 0. |
| 19 | 1. | SLE_QP1 | Min | -1560.407 | -12.156 | 0. |
| 19 | 0. | SLE_QP2 | Max | -1598.178 | -130.368 | 0. |
| 19 | 0.5 | SLE_QP2 | Max | -1579.434 | -56.011 | 0. |
| 19 | 1. | SLE_QP2 | Max | -1560.689 | 11.547 | 0. |
| 19 | 0. | SLE_QP2 | Min | -1598.178 | -130.368 | 0. |
| 19 | 0.5 | SLE_QP2 | Min | -1579.434 | -56.011 | 0. |
| 19 | 1. | SLE_QP2 | Min | -1560.689 | 11.547 | 0. |
| 19 | 0. | SLE_QP3 | Max | -1639.369 | -53.917 | 0. |
| 19 | 0.5 | SLE_QP3 | Max | -1620.624 | 14.716 | 0. |
| 19 | 1. | SLE_QP3 | Max | -1601.88 | 77.233 | 0. |
| 19 | 0. | SLE_QP3 | Min | -1639.369 | -53.917 | 0. |
| 19 | 0.5 | SLE_QP3 | Min | -1620.624 | 14.716 | 0. |
| 19 | 1. | SLE_QP3 | Min | -1601.88 | 77.233 | 0. |
| 19 | 0. | SLE_QP4 | Max | -1656.321 | -91.596 | 0. |
| 19 | 0.5 | SLE_QP4 | Max | -1637.576 | -8.736 | 0. |
| 19 | 1. | SLE_QP4 | Max | -1618.832 | 65.974 | 0. |
| 19 | 0. | SLE_QP4 | Min | -1656.321 | -91.596 | 0. |
| 19 | 0.5 | SLE_QP4 | Min | -1637.576 | -8.736 | 0. |
| 19 | 1. | SLE_QP4 | Min | -1618.832 | 65.974 | 0. |
| 19 | 0. | SLV_1 | Max | -1890.913 | -233.24 | 0. |
| 19 | 0.5 | SLV_1 | Max | -1872.168 | -147.13 | 0. |
| 19 | 1. | SLV_1 | Max | -1853.424 | -68.67 | 0. |
| 19 | 0. | SLV_1 | Min | -1890.913 | -233.24 | 0. |
| 19 | 0.5 | SLV_1 | Min | -1872.168 | -147.13 | 0. |
| 19 | 1. | SLV_1 | Min | -1853.424 | -68.67 | 0. |
| 19 | 0. | SLV_2 | Max | -1880.875 | -235.967 | 0. |
| 19 | 0.5 | SLV_2 | Max | -1862.131 | -149.857 | 0. |
| 19 | 1. | SLV_2 | Max | -1843.386 | -71.397 | 0. |
| 19 | 0. | SLV_2 | Min | -1880.875 | -235.967 | 0. |
| 19 | 0.5 | SLV_2 | Min | -1862.131 | -149.857 | 0. |
| 19 | 1. | SLV_2 | Min | -1843.386 | -71.397 | 0. |
| 19 | 0. | SLV_3 | Max | -1993.637 | -182.29 | 0. |
| 19 | 0.5 | SLV_3 | Max | -1974.893 | -99.43 | 0. |
| 19 | 1. | SLV_3 | Max | -1956.148 | -24.72 | 0. |
| 19 | 0. | SLV_3 | Min | -1993.637 | -182.29 | 0. |
| 19 | 0.5 | SLV_3 | Min | -1974.893 | -99.43 | 0. |
| 19 | 1. | SLV_3 | Min | -1956.148 | -24.72 | 0. |
| 19 | 0. | SLV_4 | Max | -1983.457 | -184.92 | 0. |
| 19 | 0.5 | SLV_4 | Max | -1964.713 | -102.06 | 0. |
| 19 | 1. | SLV_4 | Max | -1945.968 | -27.35 | 0. |
| 19 | 0. | SLV_4 | Min | -1983.457 | -184.92 | 0. |
| 19 | 0.5 | SLV_4 | Min | -1964.713 | -102.06 | 0. |
| 19 | 1. | SLV_4 | Min | -1945.968 | -27.35 | 0. |
| 19 | 0. | SLD_1 | Max | -1696.251 | -182.225 | 0. |
| 19 | 0.5 | SLD_1 | Max | -1677.506 | -96.115 | 0. |
| 19 | 1. | SLD_1 | Max | -1658.762 | -17.655 | 0. |
| 19 | 0. | SLD_1 | Min | -1696.251 | -182.225 | 0. |
| 19 | 0.5 | SLD_1 | Min | -1677.506 | -96.115 | 0. |
| 19 | 1. | SLD_1 | Min | -1658.762 | -17.655 | 0. |
| 19 | 0. | SLD_2 | Max | -1691.477 | -183.67 | 0. |
| 19 | 0.5 | SLD_2 | Max | -1672.732 | -97.56 | 0. |
| 19 | 1. | SLD_2 | Max | -1653.988 | -19.1 | 0. |
| 19 | 0. | SLD_2 | Min | -1691.477 | -183.67 | 0. |
| 19 | 0.5 | SLD_2 | Min | -1672.732 | -97.56 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 19 | 1. | SLD_2 | Min | -1653.988 | -19.1 | 0. |
| 19 | 0. | SLD_3 | Max | -1793.277 | -130.205 | 0. |
| 19 | 0.5 | SLD_3 | Max | -1774.532 | -47.345 | 0. |
| 19 | 1. | SLD_3 | Max | -1755.788 | 27.365 | 0. |
| 19 | 0. | SLD_3 | Min | -1793.277 | -130.205 | 0. |
| 19 | 0.5 | SLD_3 | Min | -1774.532 | -47.345 | 0. |
| 19 | 1. | SLD_3 | Min | -1755.788 | 27.365 | 0. |
| 19 | 0. | SLD_4 | Max | -1788.669 | -131.39 | 0. |
| 19 | 0.5 | SLD_4 | Max | -1769.924 | -48.53 | 0. |
| 19 | 1. | SLD_4 | Max | -1751.18 | 26.18 | 0. |
| 19 | 0. | SLD_4 | Min | -1788.669 | -131.39 | 0. |
| 19 | 0.5 | SLD_4 | Min | -1769.924 | -48.53 | 0. |
| 19 | 1. | SLD_4 | Min | -1751.18 | 26.18 | 0. |
| 19 | 0. | SLU_IDR_1 | Max | -1544.448 | -115.538 | 0. |
| 19 | 0.5 | SLU_IDR_1 | Max | -1527.578 | -43.599 | 0. |
| 19 | 1. | SLU_IDR_1 | Max | -1510.708 | 21.817 | 0. |
| 19 | 0. | SLU_IDR_1 | Min | -1544.448 | -115.538 | 0. |
| 19 | 0.5 | SLU_IDR_1 | Min | -1527.578 | -43.599 | 0. |
| 19 | 1. | SLU_IDR_1 | Min | -1510.708 | 21.817 | 0. |
| 19 | 0. | SLU_IDR_2 | Max | -1505.841 | -186.041 | 0. |
| 19 | 0.5 | SLU_IDR_2 | Max | -1488.971 | -108.95 | 0. |
| 19 | 1. | SLU_IDR_2 | Max | -1472.101 | -38.997 | 0. |
| 19 | 0. | SLU_IDR_2 | Min | -1505.841 | -186.041 | 0. |
| 19 | 0.5 | SLU_IDR_2 | Min | -1488.971 | -108.95 | 0. |
| 19 | 1. | SLU_IDR_2 | Min | -1472.101 | -38.997 | 0. |
| 19 | 0. | SISMA WOOD SLV-1 | Max | -448.569 | -66.217 | 0. |
| 19 | 0.5 | SISMA WOOD SLV-1 | Max | -448.569 | -66.217 | 0. |
| 19 | 1. | SISMA WOOD SLV-1 | Max | -448.569 | -66.217 | 0. |
| 19 | 0. | SISMA WOOD SLV-1 | Min | -448.569 | -66.217 | 0. |
| 19 | 0.5 | SISMA WOOD SLV-1 | Min | -448.569 | -66.217 | 0. |
| 19 | 1. | SISMA WOOD SLV-1 | Min | -448.569 | -66.217 | 0. |
| 19 | 0. | DEAD-1 | Max | -367.707 | 76.664 | 0. |
| 19 | 0.5 | DEAD-1 | Max | -348.962 | 76.664 | 0. |
| 19 | 1. | DEAD-1 | Max | -330.218 | 76.664 | 0. |
| 19 | 0. | DEAD-1 | Min | -367.707 | 76.664 | 0. |
| 19 | 0.5 | DEAD-1 | Min | -348.962 | 76.664 | 0. |
| 19 | 1. | DEAD-1 | Min | -330.218 | 76.664 | 0. |
| 19 | 0. | SLU_PROVA | | -2205.526 | -217.09 | 0. |
| 19 | 0.5 | SLU_PROVA | | -2181.158 | -105.147 | 0. |
| 19 | 1. | SLU_PROVA | | -2156.791 | -3.149 | 0. |
| 20 | 0. | DEAD | | -265.306 | 70.012 | 0. |
| 20 | 0.28595 | DEAD | | -254.586 | 70.012 | 0. |
| 20 | 0.5719 | DEAD | | -243.866 | 70.012 | 0. |
| 20 | 0. | SIMM_KA | | -12.176 | -59.078 | 0. |
| 20 | 0.28595 | SIMM_KA | | -12.176 | -47.334 | 0. |
| 20 | 0.5719 | SIMM_KA | | -12.176 | -36.076 | 0. |
| 20 | 0. | SIMM_K0 | | -18.659 | -91.078 | 0. |
| 20 | 0.28595 | SIMM_K0 | | -18.659 | -73.464 | 0. |
| 20 | 0.5719 | SIMM_K0 | | -18.659 | -56.578 | 0. |
| 20 | 0. | A--SIMM_KA | | -53.237 | -19.716 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 20 | 0.28595 | A--SIMM_KA | | -53.237 | -10.707 | 0. |
| 20 | 0.5719 | A--SIMM_KA | | -53.237 | -2.281 | 0. |
| 20 | 0. | A--SIMM_K0 | | -79.793 | -28.513 | 0. |
| 20 | 0.28595 | A--SIMM_K0 | | -79.793 | -13.259 | 0. |
| 20 | 0.5719 | A--SIMM_K0 | | -79.793 | 1.125 | 0. |
| 20 | 0. | A-- SIMM_SOVR_K A | | -1.62 | -14.014 | 0. |
| 20 | 0.28595 | A-- SIMM_SOVR_K A | | -1.62 | -14.014 | 0. |
| 20 | 0.5719 | A-- SIMM_SOVR_K A | | -1.62 | -14.014 | 0. |
| 20 | 0. | A-- SIMM_SOVR_K 0 | | -2.429 | -21.01 | 0. |
| 20 | 0.28595 | A-- SIMM_SOVR_K 0 | | -2.429 | -21.01 | 0. |
| 20 | 0.5719 | A-- SIMM_SOVR_K 0 | | -2.429 | -21.01 | 0. |
| 20 | 0. | SIMM_SOVR_K 0 | | -2.429 | -21.01 | 0. |
| 20 | 0.28595 | SIMM_SOVR_K 0 | | -2.429 | -21.01 | 0. |
| 20 | 0.5719 | SIMM_SOVR_K 0 | | -2.429 | -21.01 | 0. |
| 20 | 0. | SIMM_SOVR_K A | | -1.62 | -14.014 | 0. |
| 20 | 0.28595 | SIMM_SOVR_K A | | -1.62 | -14.014 | 0. |
| 20 | 0.5719 | SIMM_SOVR_K A | | -1.62 | -14.014 | 0. |
| 20 | 0. | SOVR | | -195.45 | 47.747 | 0. |
| 20 | 0.28595 | SOVR | | -195.45 | 47.747 | 0. |
| 20 | 0.5719 | SOVR | | -195.45 | 47.747 | 0. |
| 20 | 0. | TERR_SIMM | | -782.714 | 152.955 | 0. |
| 20 | 0.28595 | TERR_SIMM | | -782.714 | 152.955 | 0. |
| 20 | 0.5719 | TERR_SIMM | | -782.714 | 152.955 | 0. |
| 20 | 0. | TERR_A--SIMM | | -764.488 | 186.081 | 0. |
| 20 | 0.28595 | TERR_A--SIMM | | -764.488 | 186.081 | 0. |
| 20 | 0.5719 | TERR_A--SIMM | | -764.488 | 186.081 | 0. |
| 20 | 0. | INERZIA H SLV | | -4.979 | 4.664 | 0. |
| 20 | 0.28595 | INERZIA H SLV | | -4.979 | 4.664 | 0. |
| 20 | 0.5719 | INERZIA H SLV | | -4.979 | 4.664 | 0. |
| 20 | 0. | INERZIA V + SLV | | -4.115 | 1.111 | 0. |
| 20 | 0.28595 | INERZIA V + SLV | | -4.115 | 1.111 | 0. |
| 20 | 0.5719 | INERZIA V + SLV | | -4.115 | 1.111 | 0. |
| 20 | 0. | INERZIA V - SLV | | 4.115 | -1.111 | 0. |
| 20 | 0.28595 | INERZIA V - SLV | | 4.115 | -1.111 | 0. |
| 20 | 0.5719 | INERZIA V - SLV | | 4.115 | -1.111 | 0. |
| 20 | 0. | SISMA WOOD SLV | | -218.64 | 134.668 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 20 | 0.28595 | SISMA WOOD SLV | | -218.64 | 134.668 | 0. |
| 20 | 0.5719 | SISMA WOOD SLV | | -218.64 | 134.668 | 0. |
| 20 | 0. | iDROSTATICA | | -364.069 | -127.596 | 0. |
| 20 | 0.28595 | iDROSTATICA | | -364.069 | -103.879 | 0. |
| 20 | 0.5719 | iDROSTATICA | | -364.069 | -82.141 | 0. |
| 20 | 0. | SISMA WOOD SLD | | -96.56 | 59.475 | 0. |
| 20 | 0.28595 | SISMA WOOD SLD | | -96.56 | 59.475 | 0. |
| 20 | 0.5719 | SISMA WOOD SLD | | -96.56 | 59.475 | 0. |
| 20 | 0. | INERZIA H SLD | | -2.199 | 2.06 | 0. |
| 20 | 0.28595 | INERZIA H SLD | | -2.199 | 2.06 | 0. |
| 20 | 0.5719 | INERZIA H SLD | | -2.199 | 2.06 | 0. |
| 20 | 0. | INERZIA V + SLD | | -1.817 | 0.491 | 0. |
| 20 | 0.28595 | INERZIA V + SLD | | -1.817 | 0.491 | 0. |
| 20 | 0.5719 | INERZIA V + SLD | | -1.817 | 0.491 | 0. |
| 20 | 0. | INERZIA V SLD | | 1.817 | -0.491 | 0. |
| 20 | 0.28595 | INERZIA V SLD | | 1.817 | -0.491 | 0. |
| 20 | 0.5719 | INERZIA V SLD | | 1.817 | -0.491 | 0. |
| 20 | 0. | INERZIA V -1 | | 4.115 | -1.111 | 0. |
| 20 | 0.28595 | INERZIA V -1 | | 4.115 | -1.111 | 0. |
| 20 | 0.5719 | INERZIA V -1 | | 4.115 | -1.111 | 0. |
| 20 | 0. | SLU_1 | Max | -2367.184 | 96.6 | 0. |
| 20 | 0.28595 | SLU_1 | Max | -2353.248 | 150.33 | 0. |
| 20 | 0.5719 | SLU_1 | Max | -2339.312 | 200.541 | 0. |
| 20 | 0. | SLU_1 | Min | -2367.184 | 96.6 | 0. |
| 20 | 0.28595 | SLU_1 | Min | -2353.248 | 150.33 | 0. |
| 20 | 0.5719 | SLU_1 | Min | -2339.312 | 200.541 | 0. |
| 20 | 0. | SLU_2 | Max | -2367.305 | 155.241 | 0. |
| 20 | 0.28595 | SLU_2 | Max | -2353.369 | 201.34 | 0. |
| 20 | 0.5719 | SLU_2 | Max | -2339.433 | 244.234 | 0. |
| 20 | 0. | SLU_2 | Min | -2367.305 | 155.241 | 0. |
| 20 | 0.28595 | SLU_2 | Min | -2353.369 | 201.34 | 0. |
| 20 | 0.5719 | SLU_2 | Min | -2339.433 | 244.234 | 0. |
| 20 | 0. | SLU_3 | Max | -2437.484 | 287.994 | 0. |
| 20 | 0.28595 | SLU_3 | Max | -2423.548 | 338.657 | 0. |
| 20 | 0.5719 | SLU_3 | Max | -2409.612 | 385.615 | 0. |
| 20 | 0. | SLU_3 | Min | -2437.484 | 287.994 | 0. |
| 20 | 0.28595 | SLU_3 | Min | -2423.548 | 338.657 | 0. |
| 20 | 0.5719 | SLU_3 | Min | -2409.612 | 385.615 | 0. |
| 20 | 0. | SLU_4 | Max | -2419.082 | 303.709 | 0. |
| 20 | 0.28595 | SLU_4 | Max | -2405.146 | 346.251 | 0. |
| 20 | 0.5719 | SLU_4 | Max | -2391.21 | 385.465 | 0. |
| 20 | 0. | SLU_4 | Min | -2419.082 | 303.709 | 0. |
| 20 | 0.28595 | SLU_4 | Min | -2405.146 | 346.251 | 0. |
| 20 | 0.5719 | SLU_4 | Min | -2391.21 | 385.465 | 0. |
| 20 | 0. | SLE_F1 | Max | -1729.724 | 58.479 | 0. |
| 20 | 0.28595 | SLE_F1 | Max | -1719.004 | 99.81 | 0. |
| 20 | 0.5719 | SLE_F1 | Max | -1708.284 | 138.434 | 0. |
| 20 | 0. | SLE_F1 | Min | -1729.724 | 58.479 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 20 | 0.28595 | SLE_F1 | Min | -1719.004 | 99.81 | 0. |
| 20 | 0.5719 | SLE_F1 | Min | -1708.284 | 138.434 | 0. |
| 20 | 0. | SLE_F2 | Max | -1729.892 | 100.115 | 0. |
| 20 | 0.28595 | SLE_F2 | Max | -1719.172 | 135.576 | 0. |
| 20 | 0.5719 | SLE_F2 | Max | -1708.452 | 168.571 | 0. |
| 20 | 0. | SLE_F2 | Min | -1729.892 | 100.115 | 0. |
| 20 | 0.28595 | SLE_F2 | Min | -1719.172 | 135.576 | 0. |
| 20 | 0.5719 | SLE_F2 | Min | -1708.452 | 168.571 | 0. |
| 20 | 0. | SLE_F3 | Max | -1770.199 | 214.208 | 0. |
| 20 | 0.28595 | SLE_F3 | Max | -1759.479 | 246.933 | 0. |
| 20 | 0.5719 | SLE_F3 | Max | -1748.759 | 277.097 | 0. |
| 20 | 0. | SLE_F3 | Min | -1770.199 | 214.208 | 0. |
| 20 | 0.28595 | SLE_F3 | Min | -1759.479 | 246.933 | 0. |
| 20 | 0.5719 | SLE_F3 | Min | -1748.759 | 277.097 | 0. |
| 20 | 0. | SLE_F4 | Max | -1785.202 | 206.029 | 0. |
| 20 | 0.28595 | SLE_F4 | Max | -1774.483 | 245. | 0. |
| 20 | 0.5719 | SLE_F4 | Max | -1763.763 | 281.122 | 0. |
| 20 | 0. | SLE_F4 | Min | -1785.202 | 206.029 | 0. |
| 20 | 0.28595 | SLE_F4 | Min | -1774.483 | 245. | 0. |
| 20 | 0.5719 | SLE_F4 | Min | -1763.763 | 281.122 | 0. |
| 20 | 0. | SLE_QP1 | Max | -1560.407 | 28.355 | 0. |
| 20 | 0.28595 | SLE_QP1 | Max | -1549.687 | 69.685 | 0. |
| 20 | 0.5719 | SLE_QP1 | Max | -1538.967 | 108.309 | 0. |
| 20 | 0. | SLE_QP1 | Min | -1560.407 | 28.355 | 0. |
| 20 | 0.28595 | SLE_QP1 | Min | -1549.687 | 69.685 | 0. |
| 20 | 0.5719 | SLE_QP1 | Min | -1538.967 | 108.309 | 0. |
| 20 | 0. | SLE_QP2 | Max | -1560.689 | 64.26 | 0. |
| 20 | 0.28595 | SLE_QP2 | Max | -1549.969 | 99.721 | 0. |
| 20 | 0.5719 | SLE_QP2 | Max | -1539.249 | 132.717 | 0. |
| 20 | 0. | SLE_QP2 | Min | -1560.689 | 64.26 | 0. |
| 20 | 0.28595 | SLE_QP2 | Min | -1549.969 | 99.721 | 0. |
| 20 | 0.5719 | SLE_QP2 | Min | -1539.249 | 132.717 | 0. |
| 20 | 0. | SLE_QP3 | Max | -1601.88 | 178.152 | 0. |
| 20 | 0.28595 | SLE_QP3 | Max | -1591.16 | 210.876 | 0. |
| 20 | 0.5719 | SLE_QP3 | Max | -1580.44 | 241.041 | 0. |
| 20 | 0. | SLE_QP3 | Min | -1601.88 | 178.152 | 0. |
| 20 | 0.28595 | SLE_QP3 | Min | -1591.16 | 210.876 | 0. |
| 20 | 0.5719 | SLE_QP3 | Min | -1580.44 | 241.041 | 0. |
| 20 | 0. | SLE_QP4 | Max | -1618.832 | 177.077 | 0. |
| 20 | 0.28595 | SLE_QP4 | Max | -1608.112 | 216.049 | 0. |
| 20 | 0.5719 | SLE_QP4 | Max | -1597.392 | 252.171 | 0. |
| 20 | 0. | SLE_QP4 | Min | -1618.832 | 177.077 | 0. |
| 20 | 0.28595 | SLE_QP4 | Min | -1608.112 | 216.049 | 0. |
| 20 | 0.5719 | SLE_QP4 | Min | -1597.392 | 252.171 | 0. |
| 20 | 0. | SLV_1 | Max | -1852.948 | 260.246 | 0. |
| 20 | 0.28595 | SLV_1 | Max | -1842.228 | 301.577 | 0. |
| 20 | 0.5719 | SLV_1 | Max | -1831.508 | 340.201 | 0. |
| 20 | 0. | SLV_1 | Min | -1852.948 | 260.246 | 0. |
| 20 | 0.28595 | SLV_1 | Min | -1842.228 | 301.577 | 0. |
| 20 | 0.5719 | SLV_1 | Min | -1831.508 | 340.201 | 0. |
| 20 | 0. | SLV_2 | Max | -1843.862 | 257.251 | 0. |
| 20 | 0.28595 | SLV_2 | Max | -1833.142 | 298.581 | 0. |
| 20 | 0.5719 | SLV_2 | Max | -1822.422 | 337.205 | 0. |
| 20 | 0. | SLV_2 | Min | -1843.862 | 257.251 | 0. |
| 20 | 0.28595 | SLV_2 | Min | -1833.142 | 298.581 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 20 | 0.5719 | SLV_2 | Min | -1822.422 | 337.205 | 0. |
| 20 | 0. | SLV_3 | Max | -1955.672 | 393.708 | 0. |
| 20 | 0.28595 | SLV_3 | Max | -1944.952 | 432.68 | 0. |
| 20 | 0.5719 | SLV_3 | Max | -1934.232 | 468.802 | 0. |
| 20 | 0. | SLV_3 | Min | -1955.672 | 393.708 | 0. |
| 20 | 0.28595 | SLV_3 | Min | -1944.952 | 432.68 | 0. |
| 20 | 0.5719 | SLV_3 | Min | -1934.232 | 468.802 | 0. |
| 20 | 0. | SLV_4 | Max | -1946.445 | 390.756 | 0. |
| 20 | 0.28595 | SLV_4 | Max | -1935.725 | 429.728 | 0. |
| 20 | 0.5719 | SLV_4 | Max | -1925.005 | 465.85 | 0. |
| 20 | 0. | SLV_4 | Min | -1946.445 | 390.756 | 0. |
| 20 | 0.28595 | SLV_4 | Min | -1935.725 | 429.728 | 0. |
| 20 | 0.5719 | SLV_4 | Min | -1925.005 | 465.85 | 0. |
| 20 | 0. | SLD_1 | Max | -1658.552 | 139.992 | 0. |
| 20 | 0.28595 | SLD_1 | Max | -1647.832 | 181.322 | 0. |
| 20 | 0.5719 | SLD_1 | Max | -1637.112 | 219.946 | 0. |
| 20 | 0. | SLD_1 | Min | -1658.552 | 139.992 | 0. |
| 20 | 0.28595 | SLD_1 | Min | -1647.832 | 181.322 | 0. |
| 20 | 0.5719 | SLD_1 | Min | -1637.112 | 219.946 | 0. |
| 20 | 0. | SLD_2 | Max | -1654.198 | 138.416 | 0. |
| 20 | 0.28595 | SLD_2 | Max | -1643.478 | 179.746 | 0. |
| 20 | 0.5719 | SLD_2 | Max | -1632.758 | 218.37 | 0. |
| 20 | 0. | SLD_2 | Min | -1654.198 | 138.416 | 0. |
| 20 | 0.28595 | SLD_2 | Min | -1643.478 | 179.746 | 0. |
| 20 | 0.5719 | SLD_2 | Min | -1632.758 | 218.37 | 0. |
| 20 | 0. | SLD_3 | Max | -1755.578 | 275.258 | 0. |
| 20 | 0.28595 | SLD_3 | Max | -1744.858 | 314.23 | 0. |
| 20 | 0.5719 | SLD_3 | Max | -1734.138 | 350.352 | 0. |
| 20 | 0. | SLD_3 | Min | -1755.578 | 275.258 | 0. |
| 20 | 0.28595 | SLD_3 | Min | -1744.858 | 314.23 | 0. |
| 20 | 0.5719 | SLD_3 | Min | -1734.138 | 350.352 | 0. |
| 20 | 0. | SLD_4 | Max | -1751.39 | 273.902 | 0. |
| 20 | 0.28595 | SLD_4 | Max | -1740.67 | 312.874 | 0. |
| 20 | 0.5719 | SLD_4 | Max | -1729.95 | 348.995 | 0. |
| 20 | 0. | SLD_4 | Min | -1751.39 | 273.902 | 0. |
| 20 | 0.28595 | SLD_4 | Min | -1740.67 | 312.874 | 0. |
| 20 | 0.5719 | SLD_4 | Min | -1729.95 | 348.995 | 0. |
| 20 | 0. | SLU_IDR_1 | Max | -1510.708 | 117.891 | 0. |
| 20 | 0.28595 | SLU_IDR_1 | Max | -1501.06 | 152.087 | 0. |
| 20 | 0.5719 | SLU_IDR_1 | Max | -1491.412 | 183.582 | 0. |
| 20 | 0. | SLU_IDR_1 | Min | -1510.708 | 117.891 | 0. |
| 20 | 0.28595 | SLU_IDR_1 | Min | -1501.06 | 152.087 | 0. |
| 20 | 0.5719 | SLU_IDR_1 | Min | -1491.412 | 183.582 | 0. |
| 20 | 0. | SLU_IDR_2 | Max | -1472.101 | 15.246 | 0. |
| 20 | 0.28595 | SLU_IDR_2 | Max | -1462.453 | 51.904 | 0. |
| 20 | 0.5719 | SLU_IDR_2 | Max | -1452.805 | 85.947 | 0. |
| 20 | 0. | SLU_IDR_2 | Min | -1472.101 | 15.246 | 0. |
| 20 | 0.28595 | SLU_IDR_2 | Min | -1462.453 | 51.904 | 0. |
| 20 | 0.5719 | SLU_IDR_2 | Min | -1452.805 | 85.947 | 0. |
| 20 | 0. | SISMA WOOD SLV-1 | Max | -448.569 | 242.98 | 0. |
| 20 | 0.28595 | SISMA WOOD SLV-1 | Max | -448.569 | 242.98 | 0. |
| 20 | 0.5719 | SISMA WOOD SLV-1 | Max | -448.569 | 242.98 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 20 | 0. | SISMA WOOD SLV-1 | Min | -448.569 | 242.98 | 0. |
| 20 | 0.28595 | SISMA WOOD SLV-1 | Min | -448.569 | 242.98 | 0. |
| 20 | 0.5719 | SISMA WOOD SLV-1 | Min | -448.569 | 242.98 | 0. |
| 20 | 0. | DEAD-1 | Max | -330.218 | 89.277 | 0. |
| 20 | 0.28595 | DEAD-1 | Max | -319.498 | 89.277 | 0. |
| 20 | 0.5719 | DEAD-1 | Max | -308.778 | 89.277 | 0. |
| 20 | 0. | DEAD-1 | Min | -330.218 | 89.277 | 0. |
| 20 | 0.28595 | DEAD-1 | Min | -319.498 | 89.277 | 0. |
| 20 | 0.5719 | DEAD-1 | Min | -308.778 | 89.277 | 0. |
| 20 | 0. | SLU_PROVA | | -2156.791 | 45.686 | 0. |
| 20 | 0.28595 | SLU_PROVA | | -2142.855 | 99.416 | 0. |
| 20 | 0.5719 | SLU_PROVA | | -2128.919 | 149.627 | 0. |
| 21 | 0. | DEAD | | -252.321 | -36.769 | 0. |
| 21 | 0.81908 | DEAD | | -224.404 | -23.98 | 0. |
| 21 | 1.63815 | DEAD | | -196.488 | -11.191 | 0. |
| 21 | 0. | SIMM_KA | | 6.904 | -46.362 | 0. |
| 21 | 0.81908 | SIMM_KA | | -5.947 | -18.311 | 0. |
| 21 | 1.63815 | SIMM_KA | | -18.218 | 8.475 | 0. |
| 21 | 0. | SIMM_K0 | | 11.12 | -72.226 | 0. |
| 21 | 0.81908 | SIMM_K0 | | -8.157 | -30.15 | 0. |
| 21 | 1.63815 | SIMM_K0 | | -26.564 | 10.028 | 0. |
| 21 | 0. | A--SIMM_KA | | -48.921 | -19.948 | 0. |
| 21 | 0.81908 | A--SIMM_KA | | -59.668 | 3.51 | 0. |
| 21 | 1.63815 | A--SIMM_KA | | -69.721 | 25.453 | 0. |
| 21 | 0. | A--SIMM_K0 | | -74.901 | -26.696 | 0. |
| 21 | 0.81908 | A--SIMM_K0 | | -91.022 | 8.492 | 0. |
| 21 | 1.63815 | A--SIMM_K0 | | -106.103 | 41.409 | 0. |
| 21 | 0. | A-- SIMM_SOVR_K A | | 4.782 | -14.625 | 0. |
| 21 | 0.81908 | A-- SIMM_SOVR_K A | | 2.506 | -9.659 | 0. |
| 21 | 1.63815 | A-- SIMM_SOVR_K A | | 0.231 | -4.692 | 0. |
| 21 | 0. | A-- SIMM_SOVR_K 0 | | 7.169 | -21.927 | 0. |
| 21 | 0.81908 | A-- SIMM_SOVR_K 0 | | 3.757 | -14.481 | 0. |
| 21 | 1.63815 | A-- SIMM_SOVR_K 0 | | 0.346 | -7.034 | 0. |
| 21 | 0. | SIMM_SOVR_K 0 | | 7.169 | -21.927 | 0. |
| 21 | 0.81908 | SIMM_SOVR_K 0 | | 3.757 | -14.481 | 0. |
| 21 | 1.63815 | SIMM_SOVR_K 0 | | 0.346 | -7.034 | 0. |
| 21 | 0. | SIMM_SOVR_K A | | 4.782 | -14.625 | 0. |
| 21 | 0.81908 | SIMM_SOVR_K A | | 2.506 | -9.659 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 21 | 1.63815 | SIMM_SOVR_K A | | 0.231 | -4.692 | 0. |
| 21 | 0. | SOVR | | -199.375 | -33.91 | 0. |
| 21 | 0.81908 | SOVR | | -184.482 | -27.087 | 0. |
| 21 | 1.63815 | SOVR | | -169.589 | -20.264 | 0. |
| 21 | 0. | TERR_SIMM | | -781.368 | -173.831 | 0. |
| 21 | 0.81908 | TERR_SIMM | | -697.221 | -135.28 | 0. |
| 21 | 1.63815 | TERR_SIMM | | -616.868 | -98.468 | 0. |
| 21 | 0. | TERR_A--SIMM | | -779.983 | -131.859 | 0. |
| 21 | 0.81908 | TERR_A--SIMM | | -709.611 | -99.62 | 0. |
| 21 | 1.63815 | TERR_A--SIMM | | -643.779 | -69.46 | 0. |
| 21 | 0. | INERZIA H SLV | | -6.609 | 2.994 | 0. |
| 21 | 0.81908 | INERZIA H SLV | | -6.609 | 2.994 | 0. |
| 21 | 1.63815 | INERZIA H SLV | | -6.609 | 2.994 | 0. |
| 21 | 0. | INERZIA V + SLV | | -3.619 | -0.406 | 0. |
| 21 | 0.81908 | INERZIA V + SLV | | -3.619 | -0.406 | 0. |
| 21 | 1.63815 | INERZIA V + SLV | | -3.619 | -0.406 | 0. |
| 21 | 0. | INERZIA V - SLV | | 3.619 | 0.406 | 0. |
| 21 | 0.81908 | INERZIA V - SLV | | 3.619 | 0.406 | 0. |
| 21 | 1.63815 | INERZIA V - SLV | | 3.619 | 0.406 | 0. |
| 21 | 0. | SISMA WOOD SLV | | -277.232 | 96.761 | 0. |
| 21 | 0.81908 | SISMA WOOD SLV | | -277.232 | 96.761 | 0. |
| 21 | 1.63815 | SISMA WOOD SLV | | -277.232 | 96.761 | 0. |
| 21 | 0. | iDROSTATICA | | -297.992 | -220.618 | 0. |
| 21 | 0.81908 | iDROSTATICA | | -297.992 | -161.186 | 0. |
| 21 | 1.63815 | iDROSTATICA | | -297.992 | -101.754 | 0. |
| 21 | 0. | SISMA WOOD SLD | | -122.437 | 42.734 | 0. |
| 21 | 0.81908 | SISMA WOOD SLD | | -122.437 | 42.734 | 0. |
| 21 | 1.63815 | SISMA WOOD SLD | | -122.437 | 42.734 | 0. |
| 21 | 0. | INERZIA H SLD | | -2.919 | 1.322 | 0. |
| 21 | 0.81908 | INERZIA H SLD | | -2.919 | 1.322 | 0. |
| 21 | 1.63815 | INERZIA H SLD | | -2.919 | 1.322 | 0. |
| 21 | 0. | INERZIA V + SLD | | -1.598 | -0.179 | 0. |
| 21 | 0.81908 | INERZIA V + SLD | | -1.598 | -0.179 | 0. |
| 21 | 1.63815 | INERZIA V + SLD | | -1.598 | -0.179 | 0. |
| 21 | 0. | INERZIA V SLD | | 1.598 | 0.179 | 0. |
| 21 | 0.81908 | INERZIA V SLD | | 1.598 | 0.179 | 0. |
| 21 | 1.63815 | INERZIA V SLD | | 1.598 | 0.179 | 0. |
| 21 | 0. | INERZIA V -1 | | 3.619 | 0.406 | 0. |
| 21 | 0.81908 | INERZIA V -1 | | 3.619 | 0.406 | 0. |
| 21 | 1.63815 | INERZIA V -1 | | 3.619 | 0.406 | 0. |
| 21 | 0. | SLU_1 | Max | -2220.123 | -770.517 | 0. |
| 21 | 0.81908 | SLU_1 | Max | -2082.278 | -550.409 | 0. |
| 21 | 1.63815 | SLU_1 | Max | -1948.234 | -335.029 | 0. |
| 21 | 0. | SLU_1 | Min | -2220.123 | -770.517 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 21 | 0.81908 | SLU_1 | Min | -2082.278 | -550.409 | 0. |
| 21 | 1.63815 | SLU_1 | Min | -1948.234 | -335.029 | 0. |
| 21 | 0. | SLU_2 | Max | -2241.466 | -724.22 | 0. |
| 21 | 0.81908 | SLU_2 | Max | -2093.564 | -526.065 | 0. |
| 21 | 1.63815 | SLU_2 | Max | -1949.84 | -331.816 | 0. |
| 21 | 0. | SLU_2 | Min | -2241.466 | -724.22 | 0. |
| 21 | 0.81908 | SLU_2 | Min | -2093.564 | -526.065 | 0. |
| 21 | 1.63815 | SLU_2 | Min | -1949.84 | -331.816 | 0. |
| 21 | 0. | SLU_3 | Max | -2375.459 | -592.379 | 0. |
| 21 | 0.81908 | SLU_3 | Max | -2251.421 | -389.43 | 0. |
| 21 | 1.63815 | SLU_3 | Max | -2131.93 | -192.137 | 0. |
| 21 | 0. | SLU_3 | Min | -2375.459 | -592.379 | 0. |
| 21 | 0.81908 | SLU_3 | Min | -2251.421 | -389.43 | 0. |
| 21 | 1.63815 | SLU_3 | Min | -2131.93 | -192.137 | 0. |
| 21 | 0. | SLU_4 | Max | -2357.923 | -587.051 | 0. |
| 21 | 0.81908 | SLU_4 | Max | -2225.194 | -403.071 | 0. |
| 21 | 1.63815 | SLU_4 | Max | -2097.463 | -223.764 | 0. |
| 21 | 0. | SLU_4 | Min | -2357.923 | -587.051 | 0. |
| 21 | 0.81908 | SLU_4 | Min | -2225.194 | -403.071 | 0. |
| 21 | 1.63815 | SLU_4 | Min | -2097.463 | -223.764 | 0. |
| 21 | 0. | SLE_F1 | Max | -1617.746 | -570.31 | 0. |
| 21 | 0.81908 | SLE_F1 | Max | -1516.349 | -406.759 | 0. |
| 21 | 1.63815 | SLE_F1 | Max | -1417.875 | -246.845 | 0. |
| 21 | 0. | SLE_F1 | Min | -1617.746 | -570.31 | 0. |
| 21 | 0.81908 | SLE_F1 | Min | -1516.349 | -406.759 | 0. |
| 21 | 1.63815 | SLE_F1 | Min | -1417.875 | -246.845 | 0. |
| 21 | 0. | SLE_F2 | Max | -1632.699 | -538.075 | 0. |
| 21 | 0.81908 | SLE_F2 | Max | -1524.023 | -390.409 | 0. |
| 21 | 1.63815 | SLE_F2 | Max | -1418.562 | -245.748 | 0. |
| 21 | 0. | SLE_F2 | Min | -1632.699 | -538.075 | 0. |
| 21 | 0.81908 | SLE_F2 | Min | -1524.023 | -390.409 | 0. |
| 21 | 1.63815 | SLE_F2 | Min | -1418.562 | -245.748 | 0. |
| 21 | 0. | SLE_F3 | Max | -1722.625 | -432.897 | 0. |
| 21 | 0.81908 | SLE_F3 | Max | -1625.622 | -296.135 | 0. |
| 21 | 1.63815 | SLE_F3 | Max | -1532.462 | -162.968 | 0. |
| 21 | 0. | SLE_F3 | Min | -1722.625 | -432.897 | 0. |
| 21 | 0.81908 | SLE_F3 | Min | -1625.622 | -296.135 | 0. |
| 21 | 1.63815 | SLE_F3 | Min | -1532.462 | -162.968 | 0. |
| 21 | 0. | SLE_F4 | Max | -1738.852 | -432.801 | 0. |
| 21 | 0.81908 | SLE_F4 | Max | -1648.075 | -282.449 | 0. |
| 21 | 1.63815 | SLE_F4 | Max | -1560.796 | -136.448 | 0. |
| 21 | 0. | SLE_F4 | Min | -1738.852 | -432.801 | 0. |
| 21 | 0.81908 | SLE_F4 | Min | -1648.075 | -282.449 | 0. |
| 21 | 1.63815 | SLE_F4 | Min | -1560.796 | -136.448 | 0. |
| 21 | 0. | SLE_QP1 | Max | -1450.287 | -529.317 | 0. |
| 21 | 0.81908 | SLE_QP1 | Max | -1357.5 | -376.468 | 0. |
| 21 | 1.63815 | SLE_QP1 | Max | -1267.638 | -227.257 | 0. |
| 21 | 0. | SLE_QP1 | Min | -1450.287 | -529.317 | 0. |
| 21 | 0.81908 | SLE_QP1 | Min | -1357.5 | -376.468 | 0. |
| 21 | 1.63815 | SLE_QP1 | Min | -1267.638 | -227.257 | 0. |
| 21 | 0. | SLE_QP2 | Max | -1462.76 | -502.755 | 0. |
| 21 | 0.81908 | SLE_QP2 | Max | -1363.547 | -363.932 | 0. |
| 21 | 1.63815 | SLE_QP2 | Max | -1267.549 | -228.112 | 0. |
| 21 | 0. | SLE_QP2 | Min | -1462.76 | -502.755 | 0. |
| 21 | 0.81908 | SLE_QP2 | Min | -1363.547 | -363.932 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 21 | 1.63815 | SLE_QP2 | Min | -1267.549 | -228.112 | 0. |
| 21 | 0. | SLE_QP3 | Max | -1553.325 | -398.206 | 0. |
| 21 | 0.81908 | SLE_QP3 | Max | -1465.785 | -270.286 | 0. |
| 21 | 1.63815 | SLE_QP3 | Max | -1382.089 | -145.962 | 0. |
| 21 | 0. | SLE_QP3 | Min | -1553.325 | -398.206 | 0. |
| 21 | 0.81908 | SLE_QP3 | Min | -1465.785 | -270.286 | 0. |
| 21 | 1.63815 | SLE_QP3 | Min | -1382.089 | -145.962 | 0. |
| 21 | 0. | SLE_QP4 | Max | -1574.938 | -390.537 | 0. |
| 21 | 0.81908 | SLE_QP4 | Max | -1492.771 | -250.887 | 0. |
| 21 | 1.63815 | SLE_QP4 | Max | -1414.103 | -115.588 | 0. |
| 21 | 0. | SLE_QP4 | Min | -1574.938 | -390.537 | 0. |
| 21 | 0.81908 | SLE_QP4 | Min | -1492.771 | -250.887 | 0. |
| 21 | 1.63815 | SLE_QP4 | Min | -1414.103 | -115.588 | 0. |
| 21 | 0. | SLV_1 | Max | -1856.329 | -311.051 | 0. |
| 21 | 0.81908 | SLV_1 | Max | -1763.542 | -158.202 | 0. |
| 21 | 1.63815 | SLV_1 | Max | -1673.679 | -8.99 | 0. |
| 21 | 0. | SLV_1 | Min | -1856.329 | -311.051 | 0. |
| 21 | 0.81908 | SLV_1 | Min | -1763.542 | -158.202 | 0. |
| 21 | 1.63815 | SLV_1 | Min | -1673.679 | -8.99 | 0. |
| 21 | 0. | SLV_2 | Max | -1847.985 | -310.594 | 0. |
| 21 | 0.81908 | SLV_2 | Max | -1755.198 | -157.745 | 0. |
| 21 | 1.63815 | SLV_2 | Max | -1665.336 | -8.534 | 0. |
| 21 | 0. | SLV_2 | Min | -1847.985 | -310.594 | 0. |
| 21 | 0.81908 | SLV_2 | Min | -1755.198 | -157.745 | 0. |
| 21 | 1.63815 | SLV_2 | Min | -1665.336 | -8.534 | 0. |
| 21 | 0. | SLV_3 | Max | -2017.467 | -195.366 | 0. |
| 21 | 0.81908 | SLV_3 | Max | -1935.301 | -55.716 | 0. |
| 21 | 1.63815 | SLV_3 | Max | -1856.632 | 79.583 | 0. |
| 21 | 0. | SLV_3 | Min | -2017.467 | -195.366 | 0. |
| 21 | 0.81908 | SLV_3 | Min | -1935.301 | -55.716 | 0. |
| 21 | 1.63815 | SLV_3 | Min | -1856.632 | 79.583 | 0. |
| 21 | 0. | SLV_4 | Max | -2009.005 | -194.833 | 0. |
| 21 | 0.81908 | SLV_4 | Max | -1926.839 | -55.184 | 0. |
| 21 | 1.63815 | SLV_4 | Max | -1848.17 | 80.115 | 0. |
| 21 | 0. | SLV_4 | Min | -2009.005 | -194.833 | 0. |
| 21 | 0.81908 | SLV_4 | Min | -1926.839 | -55.184 | 0. |
| 21 | 1.63815 | SLV_4 | Min | -1848.17 | 80.115 | 0. |
| 21 | 0. | SLD_1 | Max | -1603.858 | -416.534 | 0. |
| 21 | 0.81908 | SLD_1 | Max | -1511.071 | -263.685 | 0. |
| 21 | 1.63815 | SLD_1 | Max | -1421.208 | -114.473 | 0. |
| 21 | 0. | SLD_1 | Min | -1603.858 | -416.534 | 0. |
| 21 | 0.81908 | SLD_1 | Min | -1511.071 | -263.685 | 0. |
| 21 | 1.63815 | SLD_1 | Min | -1421.208 | -114.473 | 0. |
| 21 | 0. | SLD_2 | Max | -1599.756 | -416.421 | 0. |
| 21 | 0.81908 | SLD_2 | Max | -1506.969 | -263.572 | 0. |
| 21 | 1.63815 | SLD_2 | Max | -1417.106 | -114.36 | 0. |
| 21 | 0. | SLD_2 | Min | -1599.756 | -416.421 | 0. |
| 21 | 0.81908 | SLD_2 | Min | -1506.969 | -263.572 | 0. |
| 21 | 1.63815 | SLD_2 | Min | -1417.106 | -114.36 | 0. |
| 21 | 0. | SLD_3 | Max | -1760.689 | -296.466 | 0. |
| 21 | 0.81908 | SLD_3 | Max | -1678.523 | -156.816 | 0. |
| 21 | 1.63815 | SLD_3 | Max | -1599.855 | -21.517 | 0. |
| 21 | 0. | SLD_3 | Min | -1760.689 | -296.466 | 0. |
| 21 | 0.81908 | SLD_3 | Min | -1678.523 | -156.816 | 0. |
| 21 | 1.63815 | SLD_3 | Min | -1599.855 | -21.517 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 21 | 0. | SLD_4 | Max | -1756.824 | -296.243 | 0. |
| 21 | 0.81908 | SLD_4 | Max | -1674.658 | -156.594 | 0. |
| 21 | 1.63815 | SLD_4 | Max | -1595.989 | -21.295 | 0. |
| 21 | 0. | SLD_4 | Min | -1756.824 | -296.243 | 0. |
| 21 | 0.81908 | SLD_4 | Min | -1674.658 | -156.594 | 0. |
| 21 | 1.63815 | SLD_4 | Min | -1595.989 | -21.295 | 0. |
| 21 | 0. | SLU_IDR_1 | Max | -1447.559 | -414.628 | 0. |
| 21 | 0.81908 | SLU_IDR_1 | Max | -1368.773 | -287.614 | 0. |
| 21 | 1.63815 | SLU_IDR_1 | Max | -1293.446 | -163.836 | 0. |
| 21 | 0. | SLU_IDR_1 | Min | -1447.559 | -414.628 | 0. |
| 21 | 0.81908 | SLU_IDR_1 | Min | -1368.773 | -287.614 | 0. |
| 21 | 1.63815 | SLU_IDR_1 | Min | -1293.446 | -163.836 | 0. |
| 21 | 0. | SLU_IDR_2 | Max | -1364.837 | -507.446 | 0. |
| 21 | 0.81908 | SLU_IDR_2 | Max | -1275.546 | -370.618 | 0. |
| 21 | 1.63815 | SLU_IDR_2 | Max | -1189.147 | -236.495 | 0. |
| 21 | 0. | SLU_IDR_2 | Min | -1364.837 | -507.446 | 0. |
| 21 | 0.81908 | SLU_IDR_2 | Min | -1275.546 | -370.618 | 0. |
| 21 | 1.63815 | SLU_IDR_2 | Min | -1189.147 | -236.495 | 0. |
| 21 | 0. | SISMA WOOD SLV-1 | Max | -557.568 | 175.847 | 0. |
| 21 | 0.81908 | SISMA WOOD SLV-1 | Max | -557.568 | 175.847 | 0. |
| 21 | 1.63815 | SISMA WOOD SLV-1 | Max | -557.568 | 175.847 | 0. |
| 21 | 0. | SISMA WOOD SLV-1 | Min | -557.568 | 175.847 | 0. |
| 21 | 0.81908 | SISMA WOOD SLV-1 | Min | -557.568 | 175.847 | 0. |
| 21 | 1.63815 | SISMA WOOD SLV-1 | Min | -557.568 | 175.847 | 0. |
| 21 | 0. | DEAD-1 | Max | -320.061 | -42.736 | 0. |
| 21 | 0.81908 | DEAD-1 | Max | -292.145 | -29.946 | 0. |
| 21 | 1.63815 | DEAD-1 | Max | -264.229 | -17.157 | 0. |
| 21 | 0. | DEAD-1 | Min | -320.061 | -42.736 | 0. |
| 21 | 0.81908 | DEAD-1 | Min | -292.145 | -29.946 | 0. |
| 21 | 1.63815 | DEAD-1 | Min | -264.229 | -17.157 | 0. |
| 21 | 0. | SLU_PROVA | | -2005.039 | -738.234 | 0. |
| 21 | 0.81908 | SLU_PROVA | | -1867.194 | -518.127 | 0. |
| 21 | 1.63815 | SLU_PROVA | | -1733.151 | -302.747 | 0. |
| 22 | 0. | DEAD | | -194.439 | -33.05 | 0. |
| 22 | 0.63397 | DEAD | | -177.962 | -23.562 | 0. |
| 22 | 1.26794 | DEAD | | -161.484 | -14.074 | 0. |
| 22 | 0. | SIMM_KA | | -18.687 | 2.323 | 0. |
| 22 | 0.63397 | SIMM_KA | | -29.4 | 20.929 | 0. |
| 22 | 1.26794 | SIMM_KA | | -39.319 | 38.155 | 0. |
| 22 | 0. | SIMM_K0 | | -27.012 | 0.704 | 0. |
| 22 | 0.63397 | SIMM_K0 | | -43.274 | 28.946 | 0. |
| 22 | 1.26794 | SIMM_K0 | | -58.73 | 55.787 | 0. |
| 22 | 0. | A--SIMM_KA | | -71.901 | 21.127 | 0. |
| 22 | 0.63397 | A--SIMM_KA | | -80.588 | 36.214 | 0. |
| 22 | 1.26794 | A--SIMM_KA | | -88.648 | 50.212 | 0. |
| 22 | 0. | A--SIMM_K0 | | -109.644 | 34.365 | 0. |
| 22 | 0.63397 | A--SIMM_K0 | | -122.675 | 56.996 | 0. |
| 22 | 1.26794 | A--SIMM_K0 | | -134.765 | 77.993 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 22 | 0. | A-- SIMM_SOVR_K A | | 0.703 | -5.371 | 0. |
| 22 | 0.63397 | A-- SIMM_SOVR_K A | | -1.407 | -1.706 | 0. |
| 22 | 1.26794 | A-- SIMM_SOVR_K A | | -3.517 | 1.958 | 0. |
| 22 | 0. | A-- SIMM_SOVR_K 0 | | 1.054 | -8.052 | 0. |
| 22 | 0.63397 | A-- SIMM_SOVR_K 0 | | -2.109 | -2.558 | 0. |
| 22 | 1.26794 | A-- SIMM_SOVR_K 0 | | -5.273 | 2.936 | 0. |
| 22 | 0. | SIMM_SOVR_K 0 | | 1.054 | -8.052 | 0. |
| 22 | 0.63397 | SIMM_SOVR_K 0 | | -2.109 | -2.558 | 0. |
| 22 | 1.26794 | SIMM_SOVR_K 0 | | -5.273 | 2.936 | 0. |
| 22 | 0. | SIMM_SOVR_K A | | 0.703 | -5.371 | 0. |
| 22 | 0.63397 | SIMM_SOVR_K A | | -1.407 | -1.706 | 0. |
| 22 | 1.26794 | SIMM_SOVR_K A | | -3.517 | 1.958 | 0. |
| 22 | 0. | SOVR | | -167.008 | -35.599 | 0. |
| 22 | 0.63397 | SOVR | | -156.02 | -29.272 | 0. |
| 22 | 1.26794 | SOVR | | -145.032 | -22.945 | 0. |
| 22 | 0. | TERR_SIMM | | -605.095 | -155.91 | 0. |
| 22 | 0.63397 | TERR_SIMM | | -548.611 | -123.386 | 0. |
| 22 | 1.26794 | TERR_SIMM | | -494.929 | -92.475 | 0. |
| 22 | 0. | TERR_A--SIMM | | -634.704 | -127.16 | 0. |
| 22 | 0.63397 | TERR_A--SIMM | | -589.44 | -101.097 | 0. |
| 22 | 1.26794 | TERR_A--SIMM | | -547.443 | -76.914 | 0. |
| 22 | 0. | INERZIA H SLV | | -6.11 | 1.969 | 0. |
| 22 | 0.63397 | INERZIA H SLV | | -6.11 | 1.969 | 0. |
| 22 | 1.26794 | INERZIA H SLV | | -6.11 | 1.969 | 0. |
| 22 | 0. | INERZIA V + SLV | | -2.866 | -0.398 | 0. |
| 22 | 0.63397 | INERZIA V + SLV | | -2.866 | -0.398 | 0. |
| 22 | 1.26794 | INERZIA V + SLV | | -2.866 | -0.398 | 0. |
| 22 | 0. | INERZIA V - SLV | | 2.866 | 0.398 | 0. |
| 22 | 0.63397 | INERZIA V - SLV | | 2.866 | 0.398 | 0. |
| 22 | 1.26794 | INERZIA V - SLV | | 2.866 | 0.398 | 0. |
| 22 | 0. | SISMA WOOD SLV | | -286.736 | 102.865 | 0. |
| 22 | 0.63397 | SISMA WOOD SLV | | -286.736 | 102.865 | 0. |
| 22 | 1.26794 | SISMA WOOD SLV | | -286.736 | 102.865 | 0. |
| 22 | 0. | iDROSTATICA | | -287.461 | -125.103 | 0. |
| 22 | 0.63397 | iDROSTATICA | | -287.461 | -74.438 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 22 | 1.26794 | iDROSTATICA | | -287.461 | -26.882 | 0. |
| 22 | 0. | SISMA WOOD SLD | | -126.634 | 45.43 | 0. |
| 22 | 0.63397 | SISMA WOOD SLD | | -126.634 | 45.43 | 0. |
| 22 | 1.26794 | SISMA WOOD SLD | | -126.634 | 45.43 | 0. |
| 22 | 0. | INERZIA H SLD | | -2.698 | 0.869 | 0. |
| 22 | 0.63397 | INERZIA H SLD | | -2.698 | 0.869 | 0. |
| 22 | 1.26794 | INERZIA H SLD | | -2.698 | 0.869 | 0. |
| 22 | 0. | INERZIA V + SLD | | -1.266 | -0.176 | 0. |
| 22 | 0.63397 | INERZIA V + SLD | | -1.266 | -0.176 | 0. |
| 22 | 1.26794 | INERZIA V + SLD | | -1.266 | -0.176 | 0. |
| 22 | 0. | INERZIA V SLD | | 1.266 | 0.176 | 0. |
| 22 | 0.63397 | INERZIA V SLD | | 1.266 | 0.176 | 0. |
| 22 | 1.26794 | INERZIA V SLD | | 1.266 | 0.176 | 0. |
| 22 | 0. | INERZIA V -1 | | 2.866 | 0.398 | 0. |
| 22 | 0.63397 | INERZIA V -1 | | 2.866 | 0.398 | 0. |
| 22 | 1.26794 | INERZIA V -1 | | 2.866 | 0.398 | 0. |
| 22 | 0. | SLU_1 | Max | -1908.782 | -514.209 | 0. |
| 22 | 0.63397 | SLU_1 | Max | -1823.336 | -339.283 | 0. |
| 22 | 1.26794 | SLU_1 | Max | -1740.485 | -172.318 | 0. |
| 22 | 0. | SLU_1 | Min | -1908.782 | -514.209 | 0. |
| 22 | 0.63397 | SLU_1 | Min | -1823.336 | -339.283 | 0. |
| 22 | 1.26794 | SLU_1 | Min | -1740.485 | -172.318 | 0. |
| 22 | 0. | SLU_2 | Max | -1910.679 | -511.157 | 0. |
| 22 | 0.63397 | SLU_2 | Max | -1816.44 | -351.503 | 0. |
| 22 | 1.26794 | SLU_2 | Max | -1724.811 | -199.781 | 0. |
| 22 | 0. | SLU_2 | Min | -1910.679 | -511.157 | 0. |
| 22 | 0.63397 | SLU_2 | Min | -1816.44 | -351.503 | 0. |
| 22 | 1.26794 | SLU_2 | Min | -1724.811 | -199.781 | 0. |
| 22 | 0. | SLU_3 | Max | -2105.802 | -374.787 | 0. |
| 22 | 0.63397 | SLU_3 | Max | -2030.743 | -215.554 | 0. |
| 22 | 1.26794 | SLU_3 | Max | -1958.706 | -64.933 | 0. |
| 22 | 0. | SLU_3 | Min | -2105.802 | -374.787 | 0. |
| 22 | 0.63397 | SLU_3 | Min | -2030.743 | -215.554 | 0. |
| 22 | 1.26794 | SLU_3 | Min | -1958.706 | -64.933 | 0. |
| 22 | 0. | SLU_4 | Max | -2068.467 | -404.682 | 0. |
| 22 | 0.63397 | SLU_4 | Max | -1986.18 | -258.001 | 0. |
| 22 | 1.26794 | SLU_4 | Max | -1907.324 | -119.222 | 0. |
| 22 | 0. | SLU_4 | Min | -2068.467 | -404.682 | 0. |
| 22 | 0.63397 | SLU_4 | Min | -1986.18 | -258.001 | 0. |
| 22 | 1.26794 | SLU_4 | Min | -1907.324 | -119.222 | 0. |
| 22 | 0. | SLE_F1 | Max | -1388.883 | -377.234 | 0. |
| 22 | 0.63397 | SLE_F1 | Max | -1326.315 | -247.45 | 0. |
| 22 | 1.26794 | SLE_F1 | Max | -1265.743 | -123.789 | 0. |
| 22 | 0. | SLE_F1 | Min | -1388.883 | -377.234 | 0. |
| 22 | 0.63397 | SLE_F1 | Min | -1326.315 | -247.45 | 0. |
| 22 | 1.26794 | SLE_F1 | Min | -1265.743 | -123.789 | 0. |
| 22 | 0. | SLE_F2 | Max | -1389.668 | -376.205 | 0. |
| 22 | 0.63397 | SLE_F2 | Max | -1320.762 | -257.429 | 0. |
| 22 | 1.26794 | SLE_F2 | Max | -1253.864 | -144.755 | 0. |
| 22 | 0. | SLE_F2 | Min | -1389.668 | -376.205 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 22 | 0.63397 | SLE_F2 | Min | -1320.762 | -257.429 | 0. |
| 22 | 1.26794 | SLE_F2 | Min | -1253.864 | -144.755 | 0. |
| 22 | 0. | SLE_F3 | Max | -1511.357 | -294.52 | 0. |
| 22 | 0.63397 | SLE_F3 | Max | -1451.645 | -185.723 | 0. |
| 22 | 1.26794 | SLE_F3 | Max | -1394.572 | -83.005 | 0. |
| 22 | 0. | SLE_F3 | Min | -1511.357 | -294.52 | 0. |
| 22 | 0.63397 | SLE_F3 | Min | -1451.645 | -185.723 | 0. |
| 22 | 1.26794 | SLE_F3 | Min | -1394.572 | -83.005 | 0. |
| 22 | 0. | SLE_F4 | Max | -1542.117 | -269.048 | 0. |
| 22 | 0.63397 | SLE_F4 | Max | -1487.539 | -151.335 | 0. |
| 22 | 1.26794 | SLE_F4 | Max | -1435.286 | -40.247 | 0. |
| 22 | 0. | SLE_F4 | Min | -1542.117 | -269.048 | 0. |
| 22 | 0.63397 | SLE_F4 | Min | -1487.539 | -151.335 | 0. |
| 22 | 1.26794 | SLE_F4 | Min | -1435.286 | -40.247 | 0. |
| 22 | 0. | SLE_QP1 | Max | -1241.108 | -343.81 | 0. |
| 22 | 0.63397 | SLE_QP1 | Max | -1184.409 | -222.891 | 0. |
| 22 | 1.26794 | SLE_QP1 | Max | -1129.706 | -108.096 | 0. |
| 22 | 0. | SLE_QP1 | Min | -1241.108 | -343.81 | 0. |
| 22 | 0.63397 | SLE_QP1 | Min | -1184.409 | -222.891 | 0. |
| 22 | 1.26794 | SLE_QP1 | Min | -1129.706 | -108.096 | 0. |
| 22 | 0. | SLE_QP2 | Max | -1240.941 | -344.645 | 0. |
| 22 | 0.63397 | SLE_QP2 | Max | -1178.693 | -233.363 | 0. |
| 22 | 1.26794 | SLE_QP2 | Max | -1118.453 | -128.182 | 0. |
| 22 | 0. | SLE_QP2 | Min | -1240.941 | -344.645 | 0. |
| 22 | 0.63397 | SLE_QP2 | Min | -1178.693 | -233.363 | 0. |
| 22 | 1.26794 | SLE_QP2 | Min | -1118.453 | -128.182 | 0. |
| 22 | 0. | SLE_QP3 | Max | -1363.212 | -263.369 | 0. |
| 22 | 0.63397 | SLE_QP3 | Max | -1310.158 | -162.066 | 0. |
| 22 | 1.26794 | SLE_QP3 | Max | -1259.744 | -66.841 | 0. |
| 22 | 0. | SLE_QP3 | Min | -1363.212 | -263.369 | 0. |
| 22 | 0.63397 | SLE_QP3 | Min | -1310.158 | -162.066 | 0. |
| 22 | 1.26794 | SLE_QP3 | Min | -1259.744 | -66.841 | 0. |
| 22 | 0. | SLE_QP4 | Max | -1398.041 | -233.521 | 0. |
| 22 | 0.63397 | SLE_QP4 | Max | -1349.332 | -124.674 | 0. |
| 22 | 1.26794 | SLE_QP4 | Max | -1302.947 | -22.451 | 0. |
| 22 | 0. | SLE_QP4 | Min | -1398.041 | -233.521 | 0. |
| 22 | 0.63397 | SLE_QP4 | Min | -1349.332 | -124.674 | 0. |
| 22 | 1.26794 | SLE_QP4 | Min | -1302.947 | -22.451 | 0. |
| 22 | 0. | SLV_1 | Max | -1667.334 | -106.584 | 0. |
| 22 | 0.63397 | SLV_1 | Max | -1610.635 | 14.334 | 0. |
| 22 | 1.26794 | SLV_1 | Max | -1555.932 | 129.129 | 0. |
| 22 | 0. | SLV_1 | Min | -1667.334 | -106.584 | 0. |
| 22 | 0.63397 | SLV_1 | Min | -1610.635 | 14.334 | 0. |
| 22 | 1.26794 | SLV_1 | Min | -1555.932 | 129.129 | 0. |
| 22 | 0. | SLV_2 | Max | -1660.466 | -106.057 | 0. |
| 22 | 0.63397 | SLV_2 | Max | -1603.767 | 14.862 | 0. |
| 22 | 1.26794 | SLV_2 | Max | -1549.063 | 129.657 | 0. |
| 22 | 0. | SLV_2 | Min | -1660.466 | -106.057 | 0. |
| 22 | 0.63397 | SLV_2 | Min | -1603.767 | 14.862 | 0. |
| 22 | 1.26794 | SLV_2 | Min | -1549.063 | 129.657 | 0. |
| 22 | 0. | SLV_3 | Max | -1858.846 | -14.165 | 0. |
| 22 | 0.63397 | SLV_3 | Max | -1810.136 | 94.682 | 0. |
| 22 | 1.26794 | SLV_3 | Max | -1763.752 | 196.905 | 0. |
| 22 | 0. | SLV_3 | Min | -1858.846 | -14.165 | 0. |
| 22 | 0.63397 | SLV_3 | Min | -1810.136 | 94.682 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 22 | 1.26794 | SLV_3 | Min | -1763.752 | 196.905 | 0. |
| 22 | 0. | SLV_4 | Max | -1851.866 | -13.56 | 0. |
| 22 | 0.63397 | SLV_4 | Max | -1803.157 | 95.288 | 0. |
| 22 | 1.26794 | SLV_4 | Max | -1756.772 | 197.511 | 0. |
| 22 | 0. | SLV_4 | Min | -1851.866 | -13.56 | 0. |
| 22 | 0.63397 | SLV_4 | Min | -1803.157 | 95.288 | 0. |
| 22 | 1.26794 | SLV_4 | Min | -1756.772 | 197.511 | 0. |
| 22 | 0. | SLD_1 | Max | -1405.019 | -224.848 | 0. |
| 22 | 0.63397 | SLD_1 | Max | -1348.32 | -103.929 | 0. |
| 22 | 1.26794 | SLD_1 | Max | -1293.616 | 10.866 | 0. |
| 22 | 0. | SLD_1 | Min | -1405.019 | -224.848 | 0. |
| 22 | 0.63397 | SLD_1 | Min | -1348.32 | -103.929 | 0. |
| 22 | 1.26794 | SLD_1 | Min | -1293.616 | 10.866 | 0. |
| 22 | 0. | SLD_2 | Max | -1401.562 | -224.659 | 0. |
| 22 | 0.63397 | SLD_2 | Max | -1344.863 | -103.74 | 0. |
| 22 | 1.26794 | SLD_2 | Max | -1290.159 | 11.055 | 0. |
| 22 | 0. | SLD_2 | Min | -1401.562 | -224.659 | 0. |
| 22 | 0.63397 | SLD_2 | Min | -1344.863 | -103.74 | 0. |
| 22 | 1.26794 | SLD_2 | Min | -1290.159 | 11.055 | 0. |
| 22 | 0. | SLD_3 | Max | -1592.663 | -127.391 | 0. |
| 22 | 0.63397 | SLD_3 | Max | -1543.953 | -18.544 | 0. |
| 22 | 1.26794 | SLD_3 | Max | -1497.569 | 83.679 | 0. |
| 22 | 0. | SLD_3 | Min | -1592.663 | -127.391 | 0. |
| 22 | 0.63397 | SLD_3 | Min | -1543.953 | -18.544 | 0. |
| 22 | 1.26794 | SLD_3 | Min | -1497.569 | 83.679 | 0. |
| 22 | 0. | SLD_4 | Max | -1589.451 | -127.128 | 0. |
| 22 | 0.63397 | SLD_4 | Max | -1540.742 | -18.281 | 0. |
| 22 | 1.26794 | SLD_4 | Max | -1494.357 | 83.942 | 0. |
| 22 | 0. | SLD_4 | Min | -1589.451 | -127.128 | 0. |
| 22 | 0.63397 | SLD_4 | Min | -1540.742 | -18.281 | 0. |
| 22 | 1.26794 | SLD_4 | Min | -1494.357 | 83.942 | 0. |
| 22 | 0. | SLU_IDR_1 | Max | -1273.324 | -272.132 | 0. |
| 22 | 0.63397 | SLU_IDR_1 | Max | -1225.575 | -170.826 | 0. |
| 22 | 1.26794 | SLU_IDR_1 | Max | -1180.203 | -75.613 | 0. |
| 22 | 0. | SLU_IDR_1 | Min | -1273.324 | -272.132 | 0. |
| 22 | 0.63397 | SLU_IDR_1 | Min | -1225.575 | -170.826 | 0. |
| 22 | 1.26794 | SLU_IDR_1 | Min | -1180.203 | -75.613 | 0. |
| 22 | 0. | SLU_IDR_2 | Max | -1162.136 | -345.335 | 0. |
| 22 | 0.63397 | SLU_IDR_2 | Max | -1106.113 | -235.048 | 0. |
| 22 | 1.26794 | SLU_IDR_2 | Max | -1051.897 | -130.874 | 0. |
| 22 | 0. | SLU_IDR_2 | Min | -1162.136 | -345.335 | 0. |
| 22 | 0.63397 | SLU_IDR_2 | Min | -1106.113 | -235.048 | 0. |
| 22 | 1.26794 | SLU_IDR_2 | Min | -1051.897 | -130.874 | 0. |
| 22 | 0. | SISMA WOOD SLV-1 | Max | -575.26 | 194.072 | 0. |
| 22 | 0.63397 | SISMA WOOD SLV-1 | Max | -575.26 | 194.072 | 0. |
| 22 | 1.26794 | SISMA WOOD SLV-1 | Max | -575.26 | 194.072 | 0. |
| 22 | 0. | SISMA WOOD SLV-1 | Min | -575.26 | 194.072 | 0. |
| 22 | 0.63397 | SISMA WOOD SLV-1 | Min | -575.26 | 194.072 | 0. |
| 22 | 1.26794 | SISMA WOOD SLV-1 | Min | -575.26 | 194.072 | 0. |
| 22 | 0. | DEAD-1 | Max | -261.5 | -41.58 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 22 | 0.63397 | DEAD-1 | Max | -245.023 | -32.092 | 0. |
| 22 | 1.26794 | DEAD-1 | Max | -228.546 | -22.605 | 0. |
| 22 | 0. | DEAD-1 | Min | -261.5 | -41.58 | 0. |
| 22 | 0.63397 | DEAD-1 | Min | -245.023 | -32.092 | 0. |
| 22 | 1.26794 | DEAD-1 | Min | -228.546 | -22.605 | 0. |
| 22 | 0. | SLU_PROVA | | -1697.14 | -472.843 | 0. |
| 22 | 0.63397 | SLU_PROVA | | -1611.695 | -297.917 | 0. |
| 22 | 1.26794 | SLU_PROVA | | -1528.843 | -130.952 | 0. |
| 23 | 0. | DEAD | | -157.973 | -41.484 | 0. |
| 23 | 1.0466 | DEAD | | -137.221 | -25.561 | 0. |
| 23 | 2.09321 | DEAD | | -116.468 | -9.639 | 0. |
| 23 | 0. | SIMM_KA | | -43.75 | 27.96 | 0. |
| 23 | 1.0466 | SIMM_KA | | -62.103 | 51.88 | 0. |
| 23 | 2.09321 | SIMM_KA | | -78.81 | 73.654 | 0. |
| 23 | 0. | SIMM_K0 | | -65.175 | 40.311 | 0. |
| 23 | 1.0466 | SIMM_K0 | | -94.17 | 78.1 | 0. |
| 23 | 2.09321 | SIMM_K0 | | -120.527 | 112.452 | 0. |
| 23 | 0. | A--SIMM_KA | | -94.668 | 41.587 | 0. |
| 23 | 1.0466 | A--SIMM_KA | | -110.27 | 61.923 | 0. |
| 23 | 2.09321 | A--SIMM_KA | | -125.873 | 82.258 | 0. |
| 23 | 0. | A--SIMM_K0 | | -144.11 | 64.411 | 0. |
| 23 | 1.0466 | A--SIMM_K0 | | -167.511 | 94.91 | 0. |
| 23 | 2.09321 | A--SIMM_K0 | | -190.912 | 125.409 | 0. |
| 23 | 0. | A-- SIMM_SOVR_K A | | -3.7 | 0.635 | 0. |
| 23 | 1.0466 | A-- SIMM_SOVR_K A | | -7.949 | 6.173 | 0. |
| 23 | 2.09321 | A-- SIMM_SOVR_K A | | -12.199 | 11.711 | 0. |
| 23 | 0. | A-- SIMM_SOVR_K 0 | | -5.547 | 0.951 | 0. |
| 23 | 1.0466 | A-- SIMM_SOVR_K 0 | | -11.918 | 9.255 | 0. |
| 23 | 2.09321 | A-- SIMM_SOVR_K 0 | | -18.289 | 17.558 | 0. |
| 23 | 0. | SIMM_SOVR_K 0 | | -5.547 | 0.951 | 0. |
| 23 | 1.0466 | SIMM_SOVR_K 0 | | -11.918 | 9.255 | 0. |
| 23 | 2.09321 | SIMM_SOVR_K 0 | | -18.289 | 17.558 | 0. |
| 23 | 0. | SIMM_SOVR_K A | | -3.7 | 0.635 | 0. |
| 23 | 1.0466 | SIMM_SOVR_K A | | -7.949 | 6.173 | 0. |
| 23 | 2.09321 | SIMM_SOVR_K A | | -12.199 | 11.711 | 0. |
| 23 | 0. | SOVR | | -140.739 | -42.631 | 0. |
| 23 | 1.0466 | SOVR | | -124.132 | -29.889 | 0. |
| 23 | 2.09321 | SOVR | | -107.525 | -17.147 | 0. |
| 23 | 0. | TERR_SIMM | | -478.291 | -162.151 | 0. |
| 23 | 1.0466 | TERR_SIMM | | -402.464 | -103.971 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 23 | 2.09321 | TERR_SIMM | | -333.013 | -50.684 | 0. |
| 23 | 0. | TERR_A--SIMM | | -532.525 | -151.103 | 0. |
| 23 | 1.0466 | TERR_A--SIMM | | -471.519 | -104.296 | 0. |
| 23 | 2.09321 | TERR_A--SIMM | | -410.514 | -57.488 | 0. |
| 23 | 0. | INERZIA H SLV | | -5.486 | 1.124 | 0. |
| 23 | 1.0466 | INERZIA H SLV | | -5.486 | 1.124 | 0. |
| 23 | 2.09321 | INERZIA H SLV | | -5.486 | 1.124 | 0. |
| 23 | 0. | INERZIA V + SLV | | -2.206 | -0.429 | 0. |
| 23 | 1.0466 | INERZIA V + SLV | | -2.206 | -0.429 | 0. |
| 23 | 2.09321 | INERZIA V + SLV | | -2.206 | -0.429 | 0. |
| 23 | 0. | INERZIA V - SLV | | 2.206 | 0.429 | 0. |
| 23 | 1.0466 | INERZIA V - SLV | | 2.206 | 0.429 | 0. |
| 23 | 2.09321 | INERZIA V - SLV | | 2.206 | 0.429 | 0. |
| 23 | 0. | SISMA WOOD SLV | | -299.784 | 102.271 | 0. |
| 23 | 1.0466 | SISMA WOOD SLV | | -299.784 | 102.271 | 0. |
| 23 | 2.09321 | SISMA WOOD SLV | | -299.784 | 102.271 | 0. |
| 23 | 0. | iDROSTATICA | | -281.583 | -60.602 | 0. |
| 23 | 1.0466 | iDROSTATICA | | -281.583 | 1.22 | 0. |
| 23 | 2.09321 | iDROSTATICA | | -281.583 | 55.319 | 0. |
| 23 | 0. | SISMA WOOD SLD | | -132.397 | 45.167 | 0. |
| 23 | 1.0466 | SISMA WOOD SLD | | -132.397 | 45.167 | 0. |
| 23 | 2.09321 | SISMA WOOD SLD | | -132.397 | 45.167 | 0. |
| 23 | 0. | INERZIA H SLD | | -2.423 | 0.496 | 0. |
| 23 | 1.0466 | INERZIA H SLD | | -2.423 | 0.496 | 0. |
| 23 | 2.09321 | INERZIA H SLD | | -2.423 | 0.496 | 0. |
| 23 | 0. | INERZIA V + SLD | | -0.974 | -0.189 | 0. |
| 23 | 1.0466 | INERZIA V + SLD | | -0.974 | -0.189 | 0. |
| 23 | 2.09321 | INERZIA V + SLD | | -0.974 | -0.189 | 0. |
| 23 | 0. | INERZIA V SLD | | 0.974 | 0.189 | 0. |
| 23 | 1.0466 | INERZIA V SLD | | 0.974 | 0.189 | 0. |
| 23 | 2.09321 | INERZIA V SLD | | 0.974 | 0.189 | 0. |
| 23 | 0. | INERZIA V -1 | | 2.206 | 0.429 | 0. |
| 23 | 1.0466 | INERZIA V -1 | | 2.206 | 0.429 | 0. |
| 23 | 2.09321 | INERZIA V -1 | | 2.206 | 0.429 | 0. |
| 23 | 0. | SLU_1 | Max | -1702.657 | -399.927 | 0. |
| 23 | 1.0466 | SLU_1 | Max | -1599.441 | -142.529 | 0. |
| 23 | 2.09321 | SLU_1 | Max | -1501.087 | 93.997 | 0. |
| 23 | 0. | SLU_1 | Min | -1702.657 | -399.927 | 0. |
| 23 | 1.0466 | SLU_1 | Min | -1599.441 | -142.529 | 0. |
| 23 | 2.09321 | SLU_1 | Min | -1501.087 | 93.997 | 0. |
| 23 | 0. | SLU_2 | Max | -1683.504 | -425.087 | 0. |
| 23 | 1.0466 | SLU_2 | Max | -1563.273 | -189.867 | 0. |
| 23 | 2.09321 | SLU_2 | Max | -1449.191 | 26.161 | 0. |
| 23 | 0. | SLU_2 | Min | -1683.504 | -425.087 | 0. |
| 23 | 1.0466 | SLU_2 | Min | -1563.273 | -189.867 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 23 | 2.09321 | SLU_2 | Min | -1449.191 | 26.161 | 0. |
| 23 | 0. | SLU_3 | Max | -1933.76 | -315.012 | 0. |
| 23 | 1.0466 | SLU_3 | Max | -1842.54 | -81.876 | 0. |
| 23 | 2.09321 | SLU_3 | Max | -1751.321 | 141.219 | 0. |
| 23 | 0. | SLU_3 | Min | -1933.76 | -315.012 | 0. |
| 23 | 1.0466 | SLU_3 | Min | -1842.54 | -81.876 | 0. |
| 23 | 2.09321 | SLU_3 | Min | -1751.321 | 141.219 | 0. |
| 23 | 0. | SLU_4 | Max | -1875.523 | -365.121 | 0. |
| 23 | 1.0466 | SLU_4 | Max | -1770.984 | -149.345 | 0. |
| 23 | 2.09321 | SLU_4 | Max | -1666.445 | 56.39 | 0. |
| 23 | 0. | SLU_4 | Min | -1875.523 | -365.121 | 0. |
| 23 | 1.0466 | SLU_4 | Min | -1770.984 | -149.345 | 0. |
| 23 | 2.09321 | SLU_4 | Min | -1666.445 | 56.39 | 0. |
| 23 | 0. | SLE_F1 | Max | -1238.434 | -289.328 | 0. |
| 23 | 1.0466 | SLE_F1 | Max | -1163.171 | -99.829 | 0. |
| 23 | 2.09321 | SLE_F1 | Max | -1091.648 | 73.616 | 0. |
| 23 | 0. | SLE_F1 | Min | -1238.434 | -289.328 | 0. |
| 23 | 1.0466 | SLE_F1 | Min | -1163.171 | -99.829 | 0. |
| 23 | 2.09321 | SLE_F1 | Min | -1091.648 | 73.616 | 0. |
| 23 | 0. | SLE_F2 | Max | -1223.898 | -308.547 | 0. |
| 23 | 1.0466 | SLE_F2 | Max | -1136.403 | -134.991 | 0. |
| 23 | 2.09321 | SLE_F2 | Max | -1053.639 | 23.802 | 0. |
| 23 | 0. | SLE_F2 | Min | -1223.898 | -308.547 | 0. |
| 23 | 1.0466 | SLE_F2 | Min | -1136.403 | -134.991 | 0. |
| 23 | 2.09321 | SLE_F2 | Min | -1053.639 | 23.802 | 0. |
| 23 | 0. | SLE_F3 | Max | -1371.909 | -261.982 | 0. |
| 23 | 1.0466 | SLE_F3 | Max | -1296.485 | -103.383 | 0. |
| 23 | 2.09321 | SLE_F3 | Max | -1221.061 | 47.492 | 0. |
| 23 | 0. | SLE_F3 | Min | -1371.909 | -261.982 | 0. |
| 23 | 1.0466 | SLE_F3 | Min | -1296.485 | -103.383 | 0. |
| 23 | 2.09321 | SLE_F3 | Min | -1221.061 | 47.492 | 0. |
| 23 | 0. | SLE_F4 | Max | -1418.044 | -222.097 | 0. |
| 23 | 1.0466 | SLE_F4 | Max | -1352.009 | -51.261 | 0. |
| 23 | 2.09321 | SLE_F4 | Max | -1285.974 | 111.852 | 0. |
| 23 | 0. | SLE_F4 | Min | -1418.044 | -222.097 | 0. |
| 23 | 1.0466 | SLE_F4 | Min | -1352.009 | -51.261 | 0. |
| 23 | 2.09321 | SLE_F4 | Min | -1285.974 | 111.852 | 0. |
| 23 | 0. | SLE_QP1 | Max | -1105.646 | -255.879 | 0. |
| 23 | 1.0466 | SLE_QP1 | Max | -1038.06 | -82.164 | 0. |
| 23 | 2.09321 | SLE_QP1 | Max | -974.213 | 75.496 | 0. |
| 23 | 0. | SLE_QP1 | Min | -1105.646 | -255.879 | 0. |
| 23 | 1.0466 | SLE_QP1 | Min | -1038.06 | -82.164 | 0. |
| 23 | 2.09321 | SLE_QP1 | Min | -974.213 | 75.496 | 0. |
| 23 | 0. | SLE_QP2 | Max | -1091.848 | -274.294 | 0. |
| 23 | 1.0466 | SLE_QP2 | Max | -1013.621 | -114.448 | 0. |
| 23 | 2.09321 | SLE_QP2 | Max | -940.124 | 30.635 | 0. |
| 23 | 0. | SLE_QP2 | Min | -1091.848 | -274.294 | 0. |
| 23 | 1.0466 | SLE_QP2 | Min | -1013.621 | -114.448 | 0. |
| 23 | 2.09321 | SLE_QP2 | Min | -940.124 | 30.635 | 0. |
| 23 | 0. | SLE_QP3 | Max | -1240.422 | -226.918 | 0. |
| 23 | 1.0466 | SLE_QP3 | Max | -1174.266 | -82.03 | 0. |
| 23 | 2.09321 | SLE_QP3 | Max | -1108.11 | 55.135 | 0. |
| 23 | 0. | SLE_QP3 | Min | -1240.422 | -226.918 | 0. |
| 23 | 1.0466 | SLE_QP3 | Min | -1174.266 | -82.03 | 0. |
| 23 | 2.09321 | SLE_QP3 | Min | -1108.11 | 55.135 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 23 | 0. | SLE_QP4 | Max | -1289.29 | -184.792 | 0. |
| 23 | 1.0466 | SLE_QP4 | Max | -1230.932 | -29.74 | 0. |
| 23 | 2.09321 | SLE_QP4 | Max | -1172.574 | 117.588 | 0. |
| 23 | 0. | SLE_QP4 | Min | -1289.29 | -184.792 | 0. |
| 23 | 1.0466 | SLE_QP4 | Min | -1230.932 | -29.74 | 0. |
| 23 | 2.09321 | SLE_QP4 | Min | -1172.574 | 117.588 | 0. |
| 23 | 0. | SLV_1 | Max | -1561.299 | -16.166 | 0. |
| 23 | 1.0466 | SLV_1 | Max | -1493.714 | 157.548 | 0. |
| 23 | 2.09321 | SLV_1 | Max | -1429.867 | 315.209 | 0. |
| 23 | 0. | SLV_1 | Min | -1561.299 | -16.166 | 0. |
| 23 | 1.0466 | SLV_1 | Min | -1493.714 | 157.548 | 0. |
| 23 | 2.09321 | SLV_1 | Min | -1429.867 | 315.209 | 0. |
| 23 | 0. | SLV_2 | Max | -1555.725 | -15.462 | 0. |
| 23 | 1.0466 | SLV_2 | Max | -1488.139 | 158.253 | 0. |
| 23 | 2.09321 | SLV_2 | Max | -1424.293 | 315.913 | 0. |
| 23 | 0. | SLV_2 | Min | -1555.725 | -15.462 | 0. |
| 23 | 1.0466 | SLV_2 | Min | -1488.139 | 158.253 | 0. |
| 23 | 2.09321 | SLV_2 | Min | -1424.293 | 315.913 | 0. |
| 23 | 0. | SLV_3 | Max | -1777.549 | 48.749 | 0. |
| 23 | 1.0466 | SLV_3 | Max | -1719.192 | 203.801 | 0. |
| 23 | 2.09321 | SLV_3 | Max | -1660.834 | 351.129 | 0. |
| 23 | 0. | SLV_3 | Min | -1777.549 | 48.749 | 0. |
| 23 | 1.0466 | SLV_3 | Min | -1719.192 | 203.801 | 0. |
| 23 | 2.09321 | SLV_3 | Min | -1660.834 | 351.129 | 0. |
| 23 | 0. | SLV_4 | Max | -1771.875 | 49.542 | 0. |
| 23 | 1.0466 | SLV_4 | Max | -1713.517 | 204.594 | 0. |
| 23 | 2.09321 | SLV_4 | Max | -1655.159 | 351.922 | 0. |
| 23 | 0. | SLV_4 | Min | -1771.875 | 49.542 | 0. |
| 23 | 1.0466 | SLV_4 | Min | -1713.517 | 204.594 | 0. |
| 23 | 2.09321 | SLV_4 | Min | -1655.159 | 351.922 | 0. |
| 23 | 0. | SLD_1 | Max | -1284.273 | -141.315 | 0. |
| 23 | 1.0466 | SLD_1 | Max | -1216.688 | 32.399 | 0. |
| 23 | 2.09321 | SLD_1 | Max | -1152.841 | 190.06 | 0. |
| 23 | 0. | SLD_1 | Min | -1284.273 | -141.315 | 0. |
| 23 | 1.0466 | SLD_1 | Min | -1216.688 | 32.399 | 0. |
| 23 | 2.09321 | SLD_1 | Min | -1152.841 | 190.06 | 0. |
| 23 | 0. | SLD_2 | Max | -1281.386 | -140.982 | 0. |
| 23 | 1.0466 | SLD_2 | Max | -1213.801 | 32.733 | 0. |
| 23 | 2.09321 | SLD_2 | Max | -1149.954 | 190.393 | 0. |
| 23 | 0. | SLD_2 | Min | -1281.386 | -140.982 | 0. |
| 23 | 1.0466 | SLD_2 | Min | -1213.801 | 32.733 | 0. |
| 23 | 2.09321 | SLD_2 | Min | -1149.954 | 190.393 | 0. |
| 23 | 0. | SLD_3 | Max | -1497.376 | -70.443 | 0. |
| 23 | 1.0466 | SLD_3 | Max | -1439.018 | 84.609 | 0. |
| 23 | 2.09321 | SLD_3 | Max | -1380.66 | 231.937 | 0. |
| 23 | 0. | SLD_3 | Min | -1497.376 | -70.443 | 0. |
| 23 | 1.0466 | SLD_3 | Min | -1439.018 | 84.609 | 0. |
| 23 | 2.09321 | SLD_3 | Min | -1380.66 | 231.937 | 0. |
| 23 | 0. | SLD_4 | Max | -1494.741 | -70.084 | 0. |
| 23 | 1.0466 | SLD_4 | Max | -1436.383 | 84.969 | 0. |
| 23 | 2.09321 | SLD_4 | Max | -1378.025 | 232.297 | 0. |
| 23 | 0. | SLD_4 | Min | -1494.741 | -70.084 | 0. |
| 23 | 1.0466 | SLD_4 | Min | -1436.383 | 84.969 | 0. |
| 23 | 2.09321 | SLD_4 | Min | -1378.025 | 232.297 | 0. |
| 23 | 0. | SLU_IDR_1 | Max | -1160.46 | -223.759 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 23 | 1.0466 | SLU_IDR_1 | Max | -1100.919 | -80.995 | 0. |
| 23 | 2.09321 | SLU_IDR_1 | Max | -1041.379 | 53.273 | 0. |
| 23 | 0. | SLU_IDR_1 | Min | -1160.46 | -223.759 | 0. |
| 23 | 1.0466 | SLU_IDR_1 | Min | -1100.919 | -80.995 | 0. |
| 23 | 2.09321 | SLU_IDR_1 | Min | -1041.379 | 53.273 | 0. |
| 23 | 0. | SLU_IDR_2 | Max | -1025.517 | -268.2 | 0. |
| 23 | 1.0466 | SLU_IDR_2 | Max | -955.112 | -111.974 | 0. |
| 23 | 2.09321 | SLU_IDR_2 | Max | -888.965 | 29.42 | 0. |
| 23 | 0. | SLU_IDR_2 | Min | -1025.517 | -268.2 | 0. |
| 23 | 1.0466 | SLU_IDR_2 | Min | -955.112 | -111.974 | 0. |
| 23 | 2.09321 | SLU_IDR_2 | Min | -888.965 | 29.42 | 0. |
| 23 | 0. | SISMA WOOD SLV-1 | Max | -600.257 | 201.361 | 0. |
| 23 | 1.0466 | SISMA WOOD SLV-1 | Max | -600.257 | 201.361 | 0. |
| 23 | 2.09321 | SISMA WOOD SLV-1 | Max | -600.257 | 201.361 | 0. |
| 23 | 0. | SISMA WOOD SLV-1 | Min | -600.257 | 201.361 | 0. |
| 23 | 1.0466 | SISMA WOOD SLV-1 | Min | -600.257 | 201.361 | 0. |
| 23 | 2.09321 | SISMA WOOD SLV-1 | Min | -600.257 | 201.361 | 0. |
| 23 | 0. | DEAD-1 | Max | -223.582 | -52.493 | 0. |
| 23 | 1.0466 | DEAD-1 | Max | -202.829 | -36.57 | 0. |
| 23 | 2.09321 | DEAD-1 | Max | -182.077 | -20.647 | 0. |
| 23 | 0. | DEAD-1 | Min | -223.582 | -52.493 | 0. |
| 23 | 1.0466 | DEAD-1 | Min | -202.829 | -36.57 | 0. |
| 23 | 2.09321 | DEAD-1 | Min | -182.077 | -20.647 | 0. |
| 23 | 0. | SLU_PROVA | | -1497.359 | -353.624 | 0. |
| 23 | 1.0466 | SLU_PROVA | | -1394.144 | -96.226 | 0. |
| 23 | 2.09321 | SLU_PROVA | | -1295.789 | 140.3 | 0. |
| 24 | 0. | DEAD | | -108.692 | -51.534 | 0. |
| 24 | 1.0467 | DEAD | | -92.767 | -30.78 | 0. |
| 24 | 2.09341 | DEAD | | -76.842 | -10.026 | 0. |
| 24 | 0. | SIMM_KA | | -94.812 | 48.615 | 0. |
| 24 | 1.0467 | SIMM_KA | | -114.808 | 63.959 | 0. |
| 24 | 2.09341 | SIMM_KA | | -133.392 | 78.22 | 0. |
| 24 | 0. | SIMM_K0 | | -144.933 | 74.037 | 0. |
| 24 | 1.0467 | SIMM_K0 | | -177.171 | 98.775 | 0. |
| 24 | 2.09341 | SIMM_K0 | | -208.617 | 122.904 | 0. |
| 24 | 0. | A--SIMM_KA | | -144.074 | 55.473 | 0. |
| 24 | 1.0467 | A--SIMM_KA | | -164.41 | 71.078 | 0. |
| 24 | 2.09341 | A--SIMM_KA | | -184.747 | 86.683 | 0. |
| 24 | 0. | A--SIMM_K0 | | -218.621 | 84.345 | 0. |
| 24 | 1.0467 | A--SIMM_K0 | | -249.121 | 107.75 | 0. |
| 24 | 2.09341 | A--SIMM_K0 | | -279.622 | 131.154 | 0. |
| 24 | 0. | A-- SIMM_SOVR_K A | | -14.728 | 7.604 | 0. |
| 24 | 1.0467 | A-- SIMM_SOVR_K A | | -20.266 | 11.855 | 0. |
| 24 | 2.09341 | A-- SIMM_SOVR_K A | | -25.805 | 16.105 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 24 | 0. | A-- SIMM_SOVR_K 0 | | -22.08 | 11.401 | 0. |
| 24 | 1.0467 | A-- SIMM_SOVR_K 0 | | -30.384 | 17.773 | 0. |
| 24 | 2.09341 | A-- SIMM_SOVR_K 0 | | -38.688 | 24.145 | 0. |
| 24 | 0. | SIMM_SOVR_K 0 | | -22.08 | 11.401 | 0. |
| 24 | 1.0467 | SIMM_SOVR_K 0 | | -30.384 | 17.773 | 0. |
| 24 | 2.09341 | SIMM_SOVR_K 0 | | -38.688 | 24.145 | 0. |
| 24 | 0. | SIMM_SOVR_K A | | -14.728 | 7.604 | 0. |
| 24 | 1.0467 | SIMM_SOVR_K A | | -20.266 | 11.855 | 0. |
| 24 | 2.09341 | SIMM_SOVR_K A | | -25.805 | 16.105 | 0. |
| 24 | 0. | SOVR | | -99.002 | -48.648 | 0. |
| 24 | 1.0467 | SOVR | | -86.258 | -32.04 | 0. |
| 24 | 2.09341 | SOVR | | -73.514 | -15.432 | 0. |
| 24 | 0. | TERR_SIMM | | -306.675 | -153.313 | 0. |
| 24 | 1.0467 | TERR_SIMM | | -258.251 | -90.207 | 0. |
| 24 | 2.09341 | TERR_SIMM | | -214.676 | -33.42 | 0. |
| 24 | 0. | TERR_A--SIMM | | -379.919 | -179. | 0. |
| 24 | 1.0467 | TERR_A--SIMM | | -333.104 | -117.99 | 0. |
| 24 | 2.09341 | TERR_A--SIMM | | -286.289 | -56.981 | 0. |
| 24 | 0. | INERZIA H SLV | | -4.445 | -0.043 | 0. |
| 24 | 1.0467 | INERZIA H SLV | | -4.445 | -0.043 | 0. |
| 24 | 2.09341 | INERZIA H SLV | | -4.445 | -0.043 | 0. |
| 24 | 0. | INERZIA V + SLV | | -1.483 | -0.51 | 0. |
| 24 | 1.0467 | INERZIA V + SLV | | -1.483 | -0.51 | 0. |
| 24 | 2.09341 | INERZIA V + SLV | | -1.483 | -0.51 | 0. |
| 24 | 0. | INERZIA V - SLV | | 1.483 | 0.51 | 0. |
| 24 | 1.0467 | INERZIA V - SLV | | 1.483 | 0.51 | 0. |
| 24 | 2.09341 | INERZIA V - SLV | | 1.483 | 0.51 | 0. |
| 24 | 0. | SISMA WOOD SLV | | -323.257 | 70.416 | 0. |
| 24 | 1.0467 | SISMA WOOD SLV | | -323.257 | 70.416 | 0. |
| 24 | 2.09341 | SISMA WOOD SLV | | -323.257 | 70.416 | 0. |
| 24 | 0. | iDROSTATICA | | -286.768 | -14.849 | 0. |
| 24 | 1.0467 | iDROSTATICA | | -286.768 | 31.557 | 0. |
| 24 | 2.09341 | iDROSTATICA | | -286.768 | 70.29 | 0. |
| 24 | 0. | SISMA WOOD SLD | | -142.763 | 31.098 | 0. |
| 24 | 1.0467 | SISMA WOOD SLD | | -142.763 | 31.098 | 0. |
| 24 | 2.09341 | SISMA WOOD SLD | | -142.763 | 31.098 | 0. |
| 24 | 0. | INERZIA H SLD | | -1.963 | -0.019 | 0. |
| 24 | 1.0467 | INERZIA H SLD | | -1.963 | -0.019 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 24 | 2.09341 | INERZIA H SLD | | -1.963 | -0.019 | 0. |
| 24 | 0. | INERZIA V + SLD | | -0.655 | -0.225 | 0. |
| 24 | 1.0467 | INERZIA V + SLD | | -0.655 | -0.225 | 0. |
| 24 | 2.09341 | INERZIA V + SLD | | -0.655 | -0.225 | 0. |
| 24 | 0. | INERZIA V SLD | | 0.655 | 0.225 | 0. |
| 24 | 1.0467 | INERZIA V SLD | | 0.655 | 0.225 | 0. |
| 24 | 2.09341 | INERZIA V SLD | | 0.655 | 0.225 | 0. |
| 24 | 0. | INERZIA V -1 | | 1.483 | 0.51 | 0. |
| 24 | 1.0467 | INERZIA V -1 | | 1.483 | 0.51 | 0. |
| 24 | 2.09341 | INERZIA V -1 | | 1.483 | 0.51 | 0. |
| 24 | 0. | SLU_1 | Max | -1474.258 | -297.762 | 0. |
| 24 | 1.0467 | SLU_1 | Max | -1425.854 | -61.788 | 0. |
| 24 | 2.09341 | SLU_1 | Max | -1382.722 | 155.206 | 0. |
| 24 | 0. | SLU_1 | Min | -1474.258 | -297.762 | 0. |
| 24 | 1.0467 | SLU_1 | Min | -1425.854 | -61.788 | 0. |
| 24 | 2.09341 | SLU_1 | Min | -1382.722 | 155.206 | 0. |
| 24 | 0. | SLU_2 | Max | -1406.571 | -349.853 | 0. |
| 24 | 1.0467 | SLU_2 | Max | -1338.104 | -129.273 | 0. |
| 24 | 2.09341 | SLU_2 | Max | -1274.106 | 71.709 | 0. |
| 24 | 0. | SLU_2 | Min | -1406.571 | -349.853 | 0. |
| 24 | 1.0467 | SLU_2 | Min | -1338.104 | -129.273 | 0. |
| 24 | 2.09341 | SLU_2 | Min | -1274.106 | 71.709 | 0. |
| 24 | 0. | SLU_3 | Max | -1728.189 | -316.912 | 0. |
| 24 | 1.0467 | SLU_3 | Max | -1679.617 | -85.397 | 0. |
| 24 | 2.09341 | SLU_3 | Max | -1631.045 | 136.145 | 0. |
| 24 | 0. | SLU_3 | Min | -1728.189 | -316.912 | 0. |
| 24 | 1.0467 | SLU_3 | Min | -1679.617 | -85.397 | 0. |
| 24 | 2.09341 | SLU_3 | Min | -1631.045 | 136.145 | 0. |
| 24 | 0. | SLU_4 | Max | -1624.247 | -376.883 | 0. |
| 24 | 1.0467 | SLU_4 | Max | -1558.314 | -158.689 | 0. |
| 24 | 2.09341 | SLU_4 | Max | -1492.381 | 49.53 | 0. |
| 24 | 0. | SLU_4 | Min | -1624.247 | -376.883 | 0. |
| 24 | 1.0467 | SLU_4 | Min | -1558.314 | -158.689 | 0. |
| 24 | 2.09341 | SLU_4 | Min | -1492.381 | 49.53 | 0. |
| 24 | 0. | SLE_F1 | Max | -1073.498 | -211.466 | 0. |
| 24 | 1.0467 | SLE_F1 | Max | -1038.057 | -39.228 | 0. |
| 24 | 2.09341 | SLE_F1 | Max | -1006.672 | 118.411 | 0. |
| 24 | 0. | SLE_F1 | Min | -1073.498 | -211.466 | 0. |
| 24 | 1.0467 | SLE_F1 | Min | -1038.057 | -39.228 | 0. |
| 24 | 2.09341 | SLE_F1 | Min | -1006.672 | 118.411 | 0. |
| 24 | 0. | SLE_F2 | Max | -1023.89 | -249.743 | 0. |
| 24 | 1.0467 | SLE_F2 | Max | -974.132 | -88.49 | 0. |
| 24 | 2.09341 | SLE_F2 | Max | -927.813 | 57.689 | 0. |
| 24 | 0. | SLE_F2 | Min | -1023.89 | -249.743 | 0. |
| 24 | 1.0467 | SLE_F2 | Min | -974.132 | -88.49 | 0. |
| 24 | 2.09341 | SLE_F2 | Min | -927.813 | 57.689 | 0. |
| 24 | 0. | SLE_F3 | Max | -1191.739 | -270.192 | 0. |
| 24 | 1.0467 | SLE_F3 | Max | -1143.931 | -110.774 | 0. |
| 24 | 2.09341 | SLE_F3 | Max | -1096.123 | 40.971 | 0. |
| 24 | 0. | SLE_F3 | Min | -1191.739 | -270.192 | 0. |
| 24 | 1.0467 | SLE_F3 | Min | -1143.931 | -110.774 | 0. |
| 24 | 2.09341 | SLE_F3 | Min | -1096.123 | 40.971 | 0. |
| 24 | 0. | SLE_F4 | Max | -1271.287 | -224.126 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 24 | 1.0467 | SLE_F4 | Max | -1235.717 | -55.317 | 0. |
| 24 | 2.09341 | SLE_F4 | Max | -1200.148 | 105.819 | 0. |
| 24 | 0. | SLE_F4 | Min | -1271.287 | -224.126 | 0. |
| 24 | 1.0467 | SLE_F4 | Min | -1235.717 | -55.317 | 0. |
| 24 | 2.09341 | SLE_F4 | Min | -1200.148 | 105.819 | 0. |
| 24 | 0. | SLE_QP1 | Max | -960.549 | -179.278 | 0. |
| 24 | 1.0467 | SLE_QP1 | Max | -928.438 | -24.274 | 0. |
| 24 | 2.09341 | SLE_QP1 | Max | -900.383 | 116.129 | 0. |
| 24 | 0. | SLE_QP1 | Min | -960.549 | -179.278 | 0. |
| 24 | 1.0467 | SLE_QP1 | Min | -928.438 | -24.274 | 0. |
| 24 | 2.09341 | SLE_QP1 | Min | -900.383 | 116.129 | 0. |
| 24 | 0. | SLE_QP2 | Max | -916.013 | -213.76 | 0. |
| 24 | 1.0467 | SLE_QP2 | Max | -871.659 | -68.15 | 0. |
| 24 | 2.09341 | SLE_QP2 | Max | -830.744 | 62.384 | 0. |
| 24 | 0. | SLE_QP2 | Min | -916.013 | -213.76 | 0. |
| 24 | 1.0467 | SLE_QP2 | Min | -871.659 | -68.15 | 0. |
| 24 | 2.09341 | SLE_QP2 | Min | -830.744 | 62.384 | 0. |
| 24 | 0. | SLE_QP3 | Max | -1084.616 | -233.572 | 0. |
| 24 | 1.0467 | SLE_QP3 | Max | -1042.212 | -89.798 | 0. |
| 24 | 2.09341 | SLE_QP3 | Max | -999.808 | 46.304 | 0. |
| 24 | 0. | SLE_QP3 | Min | -1084.616 | -233.572 | 0. |
| 24 | 1.0467 | SLE_QP3 | Min | -1042.212 | -89.798 | 0. |
| 24 | 2.09341 | SLE_QP3 | Min | -999.808 | 46.304 | 0. |
| 24 | 0. | SLE_QP4 | Max | -1163.807 | -187.103 | 0. |
| 24 | 1.0467 | SLE_QP4 | Max | -1131.567 | -35.529 | 0. |
| 24 | 2.09341 | SLE_QP4 | Max | -1099.328 | 108.372 | 0. |
| 24 | 0. | SLE_QP4 | Min | -1163.807 | -187.103 | 0. |
| 24 | 1.0467 | SLE_QP4 | Min | -1131.567 | -35.529 | 0. |
| 24 | 2.09341 | SLE_QP4 | Min | -1099.328 | 108.372 | 0. |
| 24 | 0. | SLV_1 | Max | -1471.744 | 1.723 | 0. |
| 24 | 1.0467 | SLV_1 | Max | -1439.633 | 156.726 | 0. |
| 24 | 2.09341 | SLV_1 | Max | -1411.578 | 297.129 | 0. |
| 24 | 0. | SLV_1 | Min | -1471.744 | 1.723 | 0. |
| 24 | 1.0467 | SLV_1 | Min | -1439.633 | 156.726 | 0. |
| 24 | 2.09341 | SLV_1 | Min | -1411.578 | 297.129 | 0. |
| 24 | 0. | SLV_2 | Max | -1467.605 | 2.84 | 0. |
| 24 | 1.0467 | SLV_2 | Max | -1435.494 | 157.843 | 0. |
| 24 | 2.09341 | SLV_2 | Max | -1407.439 | 298.246 | 0. |
| 24 | 0. | SLV_2 | Min | -1467.605 | 2.84 | 0. |
| 24 | 1.0467 | SLV_2 | Min | -1435.494 | 157.843 | 0. |
| 24 | 2.09341 | SLV_2 | Min | -1407.439 | 298.246 | 0. |
| 24 | 0. | SLV_3 | Max | -1708.561 | 6.741 | 0. |
| 24 | 1.0467 | SLV_3 | Max | -1676.321 | 158.314 | 0. |
| 24 | 2.09341 | SLV_3 | Max | -1644.082 | 302.215 | 0. |
| 24 | 0. | SLV_3 | Min | -1708.561 | 6.741 | 0. |
| 24 | 1.0467 | SLV_3 | Min | -1676.321 | 158.314 | 0. |
| 24 | 2.09341 | SLV_3 | Min | -1644.082 | 302.215 | 0. |
| 24 | 0. | SLV_4 | Max | -1704.349 | 7.976 | 0. |
| 24 | 1.0467 | SLV_4 | Max | -1672.109 | 159.55 | 0. |
| 24 | 2.09341 | SLV_4 | Max | -1639.87 | 303.451 | 0. |
| 24 | 0. | SLV_4 | Min | -1704.349 | 7.976 | 0. |
| 24 | 1.0467 | SLV_4 | Min | -1672.109 | 159.55 | 0. |
| 24 | 2.09341 | SLV_4 | Min | -1639.87 | 303.451 | 0. |
| 24 | 0. | SLD_1 | Max | -1164.792 | -102.188 | 0. |
| 24 | 1.0467 | SLD_1 | Max | -1132.68 | 52.815 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 24 | 2.09341 | SLD_1 | Max | -1104.625 | 193.218 | 0. |
| 24 | 0. | SLD_1 | Min | -1164.792 | -102.188 | 0. |
| 24 | 1.0467 | SLD_1 | Min | -1132.68 | 52.815 | 0. |
| 24 | 2.09341 | SLD_1 | Min | -1104.625 | 193.218 | 0. |
| 24 | 0. | SLD_2 | Max | -1162.561 | -101.544 | 0. |
| 24 | 1.0467 | SLD_2 | Max | -1130.45 | 53.459 | 0. |
| 24 | 2.09341 | SLD_2 | Max | -1102.395 | 193.862 | 0. |
| 24 | 0. | SLD_2 | Min | -1162.561 | -101.544 | 0. |
| 24 | 1.0467 | SLD_2 | Min | -1130.45 | 53.459 | 0. |
| 24 | 2.09341 | SLD_2 | Min | -1102.395 | 193.862 | 0. |
| 24 | 0. | SLD_3 | Max | -1400.247 | -89.615 | 0. |
| 24 | 1.0467 | SLD_3 | Max | -1368.007 | 61.958 | 0. |
| 24 | 2.09341 | SLD_3 | Max | -1335.767 | 205.859 | 0. |
| 24 | 0. | SLD_3 | Min | -1400.247 | -89.615 | 0. |
| 24 | 1.0467 | SLD_3 | Min | -1368.007 | 61.958 | 0. |
| 24 | 2.09341 | SLD_3 | Min | -1335.767 | 205.859 | 0. |
| 24 | 0. | SLD_4 | Max | -1398.264 | -89.028 | 0. |
| 24 | 1.0467 | SLD_4 | Max | -1366.024 | 62.545 | 0. |
| 24 | 2.09341 | SLD_4 | Max | -1333.784 | 206.446 | 0. |
| 24 | 0. | SLD_4 | Min | -1398.264 | -89.028 | 0. |
| 24 | 1.0467 | SLD_4 | Min | -1366.024 | 62.545 | 0. |
| 24 | 2.09341 | SLD_4 | Min | -1333.784 | 206.446 | 0. |
| 24 | 0. | SLU_IDR_1 | Max | -1019.677 | -218.097 | 0. |
| 24 | 1.0467 | SLU_IDR_1 | Max | -981.514 | -79.419 | 0. |
| 24 | 2.09341 | SLU_IDR_1 | Max | -943.35 | 50.819 | 0. |
| 24 | 0. | SLU_IDR_1 | Min | -1019.677 | -218.097 | 0. |
| 24 | 1.0467 | SLU_IDR_1 | Min | -981.514 | -79.419 | 0. |
| 24 | 2.09341 | SLU_IDR_1 | Min | -943.35 | 50.819 | 0. |
| 24 | 0. | SLU_IDR_2 | Max | -866.283 | -201.69 | 0. |
| 24 | 1.0467 | SLU_IDR_2 | Max | -826.365 | -61.361 | 0. |
| 24 | 2.09341 | SLU_IDR_2 | Max | -789.541 | 63.867 | 0. |
| 24 | 0. | SLU_IDR_2 | Min | -866.283 | -201.69 | 0. |
| 24 | 1.0467 | SLU_IDR_2 | Min | -826.365 | -61.361 | 0. |
| 24 | 2.09341 | SLU_IDR_2 | Min | -789.541 | 63.867 | 0. |
| 24 | 0. | SISMA WOOD SLV-1 | Max | -648.653 | 153.766 | 0. |
| 24 | 1.0467 | SISMA WOOD SLV-1 | Max | -648.653 | 153.766 | 0. |
| 24 | 2.09341 | SISMA WOOD SLV-1 | Max | -648.653 | 153.766 | 0. |
| 24 | 0. | SISMA WOOD SLV-1 | Min | -648.653 | 153.766 | 0. |
| 24 | 1.0467 | SISMA WOOD SLV-1 | Min | -648.653 | 153.766 | 0. |
| 24 | 2.09341 | SISMA WOOD SLV-1 | Min | -648.653 | 153.766 | 0. |
| 24 | 0. | DEAD-1 | Max | -170.527 | -67.074 | 0. |
| 24 | 1.0467 | DEAD-1 | Max | -154.601 | -46.321 | 0. |
| 24 | 2.09341 | DEAD-1 | Max | -138.676 | -25.567 | 0. |
| 24 | 0. | DEAD-1 | Min | -170.527 | -67.074 | 0. |
| 24 | 1.0467 | DEAD-1 | Min | -154.601 | -46.321 | 0. |
| 24 | 2.09341 | DEAD-1 | Min | -138.676 | -25.567 | 0. |
| 24 | 0. | SLU_PROVA | | -1282.812 | -245.226 | 0. |
| 24 | 1.0467 | SLU_PROVA | | -1234.408 | -9.252 | 0. |
| 24 | 2.09341 | SLU_PROVA | | -1191.276 | 207.742 | 0. |
| 25 | 0. | DEAD | | -69.459 | -47.635 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 25 | 1.04666 | DEAD | | -59.449 | -23.467 | 0. |
| 25 | 2.09331 | DEAD | | -49.44 | 0.701 | 0. |
| 25 | 0. | SIMM_KA | | -149.555 | 45.207 | 0. |
| 25 | 1.04666 | SIMM_KA | | -169.988 | 53.669 | 0. |
| 25 | 2.09331 | SIMM_KA | | -189.647 | 61.811 | 0. |
| 25 | 0. | SIMM_K0 | | -234.021 | 71.08 | 0. |
| 25 | 1.04666 | SIMM_K0 | | -268.944 | 85.544 | 0. |
| 25 | 2.09331 | SIMM_K0 | | -301.402 | 98.986 | 0. |
| 25 | 0. | A--SIMM_KA | | -202.837 | 49.777 | 0. |
| 25 | 1.04666 | A--SIMM_KA | | -226.518 | 59.586 | 0. |
| 25 | 2.09331 | A--SIMM_KA | | -250.2 | 69.394 | 0. |
| 25 | 0. | A--SIMM_K0 | | -306.952 | 75.086 | 0. |
| 25 | 1.04666 | A--SIMM_K0 | | -342.469 | 89.797 | 0. |
| 25 | 2.09331 | A--SIMM_K0 | | -377.987 | 104.507 | 0. |
| 25 | 0. | A-- SIMM_SOVR_K A | | -29.147 | 9.385 | 0. |
| 25 | 1.04666 | A-- SIMM_SOVR_K A | | -35.597 | 12.056 | 0. |
| 25 | 2.09331 | A-- SIMM_SOVR_K A | | -42.047 | 14.728 | 0. |
| 25 | 0. | A-- SIMM_SOVR_K 0 | | -43.699 | 14.071 | 0. |
| 25 | 1.04666 | A-- SIMM_SOVR_K 0 | | -53.369 | 18.076 | 0. |
| 25 | 2.09331 | A-- SIMM_SOVR_K 0 | | -63.039 | 22.081 | 0. |
| 25 | 0. | SIMM_SOVR_K 0 | | -43.699 | 14.071 | 0. |
| 25 | 1.04666 | SIMM_SOVR_K 0 | | -53.369 | 18.076 | 0. |
| 25 | 2.09331 | SIMM_SOVR_K 0 | | -63.039 | 22.081 | 0. |
| 25 | 0. | SIMM_SOVR_K A | | -29.147 | 9.385 | 0. |
| 25 | 1.04666 | SIMM_SOVR_K A | | -35.597 | 12.056 | 0. |
| 25 | 2.09331 | SIMM_SOVR_K A | | -42.047 | 14.728 | 0. |
| 25 | 0. | SOVR | | -65.962 | -42.775 | 0. |
| 25 | 1.04666 | SOVR | | -57.952 | -23.435 | 0. |
| 25 | 2.09331 | SOVR | | -49.942 | -4.095 | 0. |
| 25 | 0. | TERR_SIMM | | -194.724 | -121.18 | 0. |
| 25 | 1.04666 | TERR_SIMM | | -169.369 | -59.962 | 0. |
| 25 | 2.09331 | TERR_SIMM | | -145.034 | -1.204 | 0. |
| 25 | 0. | TERR_A--SIMM | | -257.328 | -166.172 | 0. |
| 25 | 1.04666 | TERR_A--SIMM | | -227.903 | -95.126 | 0. |
| 25 | 2.09331 | TERR_A--SIMM | | -198.478 | -24.081 | 0. |
| 25 | 0. | INERZIA H SLV | | -2.88 | -0.83 | 0. |
| 25 | 1.04666 | INERZIA H SLV | | -2.88 | -0.83 | 0. |
| 25 | 2.09331 | INERZIA H SLV | | -2.88 | -0.83 | 0. |
| 25 | 0. | INERZIA V + SLV | | -0.942 | -0.387 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 25 | 1.04666 | INERZIA V + SLV | | -0.942 | -0.387 | 0. |
| 25 | 2.09331 | INERZIA V + SLV | | -0.942 | -0.387 | 0. |
| 25 | 0. | INERZIA V - SLV | | 0.942 | 0.387 | 0. |
| 25 | 1.04666 | INERZIA V - SLV | | 0.942 | 0.387 | 0. |
| 25 | 2.09331 | INERZIA V - SLV | | 0.942 | 0.387 | 0. |
| 25 | 0. | SISMA WOOD SLV | | -337.328 | 29.159 | 0. |
| 25 | 1.04666 | SISMA WOOD SLV | | -337.328 | 29.159 | 0. |
| 25 | 2.09331 | SISMA WOOD SLV | | -337.328 | 29.159 | 0. |
| 25 | 0. | iDROSTATICA | | -295.978 | 0.519 | 0. |
| 25 | 1.04666 | iDROSTATICA | | -295.978 | 32.848 | 0. |
| 25 | 2.09331 | iDROSTATICA | | -295.978 | 60.043 | 0. |
| 25 | 0. | SISMA WOOD SLD | | -148.978 | 12.878 | 0. |
| 25 | 1.04666 | SISMA WOOD SLD | | -148.978 | 12.878 | 0. |
| 25 | 2.09331 | SISMA WOOD SLD | | -148.978 | 12.878 | 0. |
| 25 | 0. | INERZIA H SLD | | -1.272 | -0.366 | 0. |
| 25 | 1.04666 | INERZIA H SLD | | -1.272 | -0.366 | 0. |
| 25 | 2.09331 | INERZIA H SLD | | -1.272 | -0.366 | 0. |
| 25 | 0. | INERZIA V + SLD | | -0.416 | -0.171 | 0. |
| 25 | 1.04666 | INERZIA V + SLD | | -0.416 | -0.171 | 0. |
| 25 | 2.09331 | INERZIA V + SLD | | -0.416 | -0.171 | 0. |
| 25 | 0. | INERZIA V SLD | | 0.416 | 0.171 | 0. |
| 25 | 1.04666 | INERZIA V SLD | | 0.416 | 0.171 | 0. |
| 25 | 2.09331 | INERZIA V SLD | | 0.416 | 0.171 | 0. |
| 25 | 0. | INERZIA V -1 | | 0.942 | 0.387 | 0. |
| 25 | 1.04666 | INERZIA V -1 | | 0.942 | 0.387 | 0. |
| 25 | 2.09331 | INERZIA V -1 | | 0.942 | 0.387 | 0. |
| 25 | 0. | SLU_1 | Max | -1375.766 | -208.032 | 0. |
| 25 | 1.04666 | SLU_1 | Max | -1377.683 | -1.182 | 0. |
| 25 | 2.09331 | SLU_1 | Max | -1377.719 | 194.467 | 0. |
| 25 | 0. | SLU_1 | Min | -1375.766 | -208.032 | 0. |
| 25 | 1.04666 | SLU_1 | Min | -1377.683 | -1.182 | 0. |
| 25 | 2.09331 | SLU_1 | Min | -1377.719 | 194.467 | 0. |
| 25 | 0. | SLU_2 | Max | -1249.238 | -260.567 | 0. |
| 25 | 1.04666 | SLU_2 | Max | -1227.486 | -63.519 | 0. |
| 25 | 2.09331 | SLU_2 | Max | -1206.055 | 123.238 | 0. |
| 25 | 0. | SLU_2 | Min | -1249.238 | -260.567 | 0. |
| 25 | 1.04666 | SLU_2 | Min | -1227.486 | -63.519 | 0. |
| 25 | 2.09331 | SLU_2 | Min | -1206.055 | 123.238 | 0. |
| 25 | 0. | SLU_3 | Max | -1610.692 | -290.719 | 0. |
| 25 | 1.04666 | SLU_3 | Max | -1608.09 | -70.773 | 0. |
| 25 | 2.09331 | SLU_3 | Max | -1605.489 | 142.498 | 0. |
| 25 | 0. | SLU_3 | Min | -1610.692 | -290.719 | 0. |
| 25 | 1.04666 | SLU_3 | Min | -1608.09 | -70.773 | 0. |
| 25 | 2.09331 | SLU_3 | Min | -1605.489 | 142.498 | 0. |
| 25 | 0. | SLU_4 | Max | -1454.332 | -338.488 | 0. |
| 25 | 1.04666 | SLU_4 | Max | -1431.514 | -126.916 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 25 | 2.09331 | SLU_4 | Max | -1408.695 | 77.982 | 0. |
| 25 | 0. | SLU_4 | Min | -1454.332 | -338.488 | 0. |
| 25 | 1.04666 | SLU_4 | Min | -1431.514 | -126.916 | 0. |
| 25 | 2.09331 | SLU_4 | Min | -1408.695 | 77.982 | 0. |
| 25 | 0. | SLE_F1 | Max | -1003.009 | -146.225 | 0. |
| 25 | 1.04666 | SLE_F1 | Max | -1003.813 | 3.463 | 0. |
| 25 | 2.09331 | SLE_F1 | Max | -1003.171 | 144.535 | 0. |
| 25 | 0. | SLE_F1 | Min | -1003.009 | -146.225 | 0. |
| 25 | 1.04666 | SLE_F1 | Min | -1003.813 | 3.463 | 0. |
| 25 | 2.09331 | SLE_F1 | Min | -1003.171 | 144.535 | 0. |
| 25 | 0. | SLE_F2 | Max | -911.119 | -184.463 | 0. |
| 25 | 1.04666 | SLE_F2 | Max | -895.018 | -41.778 | 0. |
| 25 | 2.09331 | SLE_F2 | Max | -879.162 | 92.993 | 0. |
| 25 | 0. | SLE_F2 | Min | -911.119 | -184.463 | 0. |
| 25 | 1.04666 | SLE_F2 | Min | -895.018 | -41.778 | 0. |
| 25 | 2.09331 | SLE_F2 | Min | -879.162 | 92.993 | 0. |
| 25 | 0. | SLE_F3 | Max | -1069.366 | -244.177 | 0. |
| 25 | 1.04666 | SLE_F3 | Max | -1052.443 | -90.318 | 0. |
| 25 | 2.09331 | SLE_F3 | Max | -1035.521 | 58.407 | 0. |
| 25 | 0. | SLE_F3 | Min | -1069.366 | -244.177 | 0. |
| 25 | 1.04666 | SLE_F3 | Min | -1052.443 | -90.318 | 0. |
| 25 | 2.09331 | SLE_F3 | Min | -1035.521 | 58.407 | 0. |
| 25 | 0. | SLE_F4 | Max | -1186.632 | -208.465 | 0. |
| 25 | 1.04666 | SLE_F4 | Max | -1183.96 | -48.704 | 0. |
| 25 | 2.09331 | SLE_F4 | Max | -1181.289 | 105.923 | 0. |
| 25 | 0. | SLE_F4 | Min | -1186.632 | -208.465 | 0. |
| 25 | 1.04666 | SLE_F4 | Min | -1183.96 | -48.704 | 0. |
| 25 | 2.09331 | SLE_F4 | Min | -1181.289 | 105.923 | 0. |
| 25 | 0. | SLE_QP1 | Max | -899.749 | -120.946 | 0. |
| 25 | 1.04666 | SLE_QP1 | Max | -899.308 | 11.233 | 0. |
| 25 | 2.09331 | SLE_QP1 | Max | -897.421 | 134.796 | 0. |
| 25 | 0. | SLE_QP1 | Min | -899.749 | -120.946 | 0. |
| 25 | 1.04666 | SLE_QP1 | Min | -899.308 | 11.233 | 0. |
| 25 | 2.09331 | SLE_QP1 | Min | -897.421 | 134.796 | 0. |
| 25 | 0. | SLE_QP2 | Max | -818.575 | -154.799 | 0. |
| 25 | 1.04666 | SLE_QP2 | Max | -803.643 | -28.621 | 0. |
| 25 | 2.09331 | SLE_QP2 | Max | -788.958 | 89.641 | 0. |
| 25 | 0. | SLE_QP2 | Min | -818.575 | -154.799 | 0. |
| 25 | 1.04666 | SLE_QP2 | Min | -803.643 | -28.621 | 0. |
| 25 | 2.09331 | SLE_QP2 | Min | -788.958 | 89.641 | 0. |
| 25 | 0. | SLE_QP3 | Max | -977.715 | -214.092 | 0. |
| 25 | 1.04666 | SLE_QP3 | Max | -961.962 | -76.742 | 0. |
| 25 | 2.09331 | SLE_QP3 | Max | -946.21 | 55.474 | 0. |
| 25 | 0. | SLE_QP3 | Min | -977.715 | -214.092 | 0. |
| 25 | 1.04666 | SLE_QP3 | Min | -961.962 | -76.742 | 0. |
| 25 | 2.09331 | SLE_QP3 | Min | -946.21 | 55.474 | 0. |
| 25 | 0. | SLE_QP4 | Max | -1089.909 | -179.9 | 0. |
| 25 | 1.04666 | SLE_QP4 | Max | -1085.993 | -37.647 | 0. |
| 25 | 2.09331 | SLE_QP4 | Max | -1082.076 | 99.471 | 0. |
| 25 | 0. | SLE_QP4 | Min | -1089.909 | -179.9 | 0. |
| 25 | 1.04666 | SLE_QP4 | Min | -1085.993 | -37.647 | 0. |
| 25 | 2.09331 | SLE_QP4 | Min | -1082.076 | 99.471 | 0. |
| 25 | 0. | SLV_1 | Max | -1447.205 | -29.197 | 0. |
| 25 | 1.04666 | SLV_1 | Max | -1446.764 | 102.982 | 0. |
| 25 | 2.09331 | SLV_1 | Max | -1444.876 | 226.545 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 25 | 0. | SLV_1 | Min | -1447.205 | -29.197 | 0. |
| 25 | 1.04666 | SLV_1 | Min | -1446.764 | 102.982 | 0. |
| 25 | 2.09331 | SLV_1 | Min | -1444.876 | 226.545 | 0. |
| 25 | 0. | SLV_2 | Max | -1444.209 | -28.047 | 0. |
| 25 | 1.04666 | SLV_2 | Max | -1443.768 | 104.132 | 0. |
| 25 | 2.09331 | SLV_2 | Max | -1441.88 | 227.695 | 0. |
| 25 | 0. | SLV_2 | Min | -1444.209 | -28.047 | 0. |
| 25 | 1.04666 | SLV_2 | Min | -1443.768 | 104.132 | 0. |
| 25 | 2.09331 | SLV_2 | Min | -1441.88 | 227.695 | 0. |
| 25 | 0. | SLV_3 | Max | -1676.627 | -62.14 | 0. |
| 25 | 1.04666 | SLV_3 | Max | -1672.711 | 80.112 | 0. |
| 25 | 2.09331 | SLV_3 | Max | -1668.795 | 217.231 | 0. |
| 25 | 0. | SLV_3 | Min | -1676.627 | -62.14 | 0. |
| 25 | 1.04666 | SLV_3 | Min | -1672.711 | 80.112 | 0. |
| 25 | 2.09331 | SLV_3 | Min | -1668.795 | 217.231 | 0. |
| 25 | 0. | SLV_4 | Max | -1673.594 | -60.834 | 0. |
| 25 | 1.04666 | SLV_4 | Max | -1669.678 | 81.418 | 0. |
| 25 | 2.09331 | SLV_4 | Max | -1665.762 | 218.537 | 0. |
| 25 | 0. | SLV_4 | Min | -1673.594 | -60.834 | 0. |
| 25 | 1.04666 | SLV_4 | Min | -1669.678 | 81.418 | 0. |
| 25 | 2.09331 | SLV_4 | Min | -1665.762 | 218.537 | 0. |
| 25 | 0. | SLD_1 | Max | -1117.014 | -96.06 | 0. |
| 25 | 1.04666 | SLD_1 | Max | -1116.573 | 36.119 | 0. |
| 25 | 2.09331 | SLD_1 | Max | -1114.685 | 159.682 | 0. |
| 25 | 0. | SLD_1 | Min | -1117.014 | -96.06 | 0. |
| 25 | 1.04666 | SLD_1 | Min | -1116.573 | 36.119 | 0. |
| 25 | 2.09331 | SLD_1 | Min | -1114.685 | 159.682 | 0. |
| 25 | 0. | SLD_2 | Max | -1115.344 | -95.429 | 0. |
| 25 | 1.04666 | SLD_2 | Max | -1114.903 | 36.75 | 0. |
| 25 | 2.09331 | SLD_2 | Max | -1113.016 | 160.312 | 0. |
| 25 | 0. | SLD_2 | Min | -1115.344 | -95.429 | 0. |
| 25 | 1.04666 | SLD_2 | Min | -1114.903 | 36.75 | 0. |
| 25 | 2.09331 | SLD_2 | Min | -1113.016 | 160.312 | 0. |
| 25 | 0. | SLD_3 | Max | -1347.269 | -125.923 | 0. |
| 25 | 1.04666 | SLD_3 | Max | -1343.353 | 16.329 | 0. |
| 25 | 2.09331 | SLD_3 | Max | -1339.437 | 153.447 | 0. |
| 25 | 0. | SLD_3 | Min | -1347.269 | -125.923 | 0. |
| 25 | 1.04666 | SLD_3 | Min | -1343.353 | 16.329 | 0. |
| 25 | 2.09331 | SLD_3 | Min | -1339.437 | 153.447 | 0. |
| 25 | 0. | SLD_4 | Max | -1345.823 | -125.273 | 0. |
| 25 | 1.04666 | SLD_4 | Max | -1341.906 | 16.979 | 0. |
| 25 | 2.09331 | SLD_4 | Max | -1337.99 | 154.098 | 0. |
| 25 | 0. | SLD_4 | Min | -1345.823 | -125.273 | 0. |
| 25 | 1.04666 | SLD_4 | Min | -1341.906 | 16.979 | 0. |
| 25 | 2.09331 | SLD_4 | Min | -1337.99 | 154.098 | 0. |
| 25 | 0. | SLU_IDR_1 | Max | -924.35 | -195.115 | 0. |
| 25 | 1.04666 | SLU_IDR_1 | Max | -910.173 | -65.034 | 0. |
| 25 | 2.09331 | SLU_IDR_1 | Max | -895.996 | 59.399 | 0. |
| 25 | 0. | SLU_IDR_1 | Min | -924.35 | -195.115 | 0. |
| 25 | 1.04666 | SLU_IDR_1 | Min | -910.173 | -65.034 | 0. |
| 25 | 2.09331 | SLU_IDR_1 | Min | -895.996 | 59.399 | 0. |
| 25 | 0. | SLU_IDR_2 | Max | -779.16 | -142.7 | 0. |
| 25 | 1.04666 | SLU_IDR_2 | Max | -765.722 | -22.674 | 0. |
| 25 | 2.09331 | SLU_IDR_2 | Max | -752.505 | 89.201 | 0. |
| 25 | 0. | SLU_IDR_2 | Min | -779.16 | -142.7 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 25 | 1.04666 | SLU_IDR_2 | Min | -765.722 | -22.674 | 0. |
| 25 | 2.09331 | SLU_IDR_2 | Min | -752.505 | 89.201 | 0. |
| 25 | 0. | SISMA WOOD SLV-1 | Max | -683.57 | 94.834 | 0. |
| 25 | 1.04666 | SISMA WOOD SLV-1 | Max | -683.57 | 94.834 | 0. |
| 25 | 2.09331 | SISMA WOOD SLV-1 | Max | -683.57 | 94.834 | 0. |
| 25 | 0. | SISMA WOOD SLV-1 | Min | -683.57 | 94.834 | 0. |
| 25 | 1.04666 | SISMA WOOD SLV-1 | Min | -683.57 | 94.834 | 0. |
| 25 | 2.09331 | SISMA WOOD SLV-1 | Min | -683.57 | 94.834 | 0. |
| 25 | 0. | DEAD-1 | Max | -127.33 | -60.596 | 0. |
| 25 | 1.04666 | DEAD-1 | Max | -117.321 | -36.429 | 0. |
| 25 | 2.09331 | DEAD-1 | Max | -107.311 | -12.261 | 0. |
| 25 | 0. | DEAD-1 | Min | -127.33 | -60.596 | 0. |
| 25 | 1.04666 | DEAD-1 | Min | -117.321 | -36.429 | 0. |
| 25 | 2.09331 | DEAD-1 | Min | -107.311 | -12.261 | 0. |
| 25 | 0. | SLU_PROVA | | -1196.927 | -169.437 | 0. |
| 25 | 1.04666 | SLU_PROVA | | -1198.844 | 37.413 | 0. |
| 25 | 2.09331 | SLU_PROVA | | -1198.88 | 233.062 | 0. |
| 26 | 0. | DEAD | | -45.091 | -34.623 | 0. |
| 26 | 1.04666 | DEAD | | -41.676 | -8.688 | 0. |
| 26 | 2.09332 | DEAD | | -38.261 | 17.247 | 0. |
| 26 | 0. | SIMM_KA | | -200.412 | 20.399 | 0. |
| 26 | 1.04666 | SIMM_KA | | -221.093 | 23.123 | 0. |
| 26 | 2.09332 | SIMM_KA | | -241.774 | 25.846 | 0. |
| 26 | 0. | SIMM_K0 | | -318.647 | 32.686 | 0. |
| 26 | 1.04666 | SIMM_K0 | | -351.493 | 37.012 | 0. |
| 26 | 2.09332 | SIMM_K0 | | -383.015 | 41.163 | 0. |
| 26 | 0. | A--SIMM_KA | | -262.058 | 19.213 | 0. |
| 26 | 1.04666 | A--SIMM_KA | | -287.471 | 22.56 | 0. |
| 26 | 2.09332 | A--SIMM_KA | | -312.885 | 25.906 | 0. |
| 26 | 0. | A--SIMM_K0 | | -395.806 | 28.708 | 0. |
| 26 | 1.04666 | A--SIMM_K0 | | -433.92 | 33.727 | 0. |
| 26 | 2.09332 | A--SIMM_K0 | | -472.035 | 38.746 | 0. |
| 26 | 0. | A-- SIMM_SOVR_K A | | -44.619 | 4.883 | 0. |
| 26 | 1.04666 | A-- SIMM_SOVR_K A | | -51.541 | 5.795 | 0. |
| 26 | 2.09332 | A-- SIMM_SOVR_K A | | -58.462 | 6.706 | 0. |
| 26 | 0. | A-- SIMM_SOVR_K 0 | | -66.895 | 7.321 | 0. |
| 26 | 1.04666 | A-- SIMM_SOVR_K 0 | | -77.272 | 8.687 | 0. |
| 26 | 2.09332 | A-- SIMM_SOVR_K 0 | | -87.649 | 10.054 | 0. |
| 26 | 0. | SIMM_SOVR_K 0 | | -66.895 | 7.321 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|----------|----------|
| 26 | 1.04666 | SIMM_SOVR_K 0 | | -77.272 | 8.687 | 0. |
| 26 | 2.09332 | SIMM_SOVR_K 0 | | -87.649 | 10.054 | 0. |
| 26 | 0. | SIMM_SOVR_K A | | -44.619 | 4.883 | 0. |
| 26 | 1.04666 | SIMM_SOVR_K A | | -51.541 | 5.795 | 0. |
| 26 | 2.09332 | SIMM_SOVR_K A | | -58.462 | 6.706 | 0. |
| 26 | 0. | SOVR | | -45.611 | -29.291 | 0. |
| 26 | 1.04666 | SOVR | | -42.878 | -8.537 | 0. |
| 26 | 2.09332 | SOVR | | -40.145 | 12.217 | 0. |
| 26 | 0. | TERR_SIMM | | -134.135 | -83.329 | 0. |
| 26 | 1.04666 | TERR_SIMM | | -126.006 | -21.596 | 0. |
| 26 | 2.09332 | TERR_SIMM | | -117.877 | 40.136 | 0. |
| 26 | 0. | TERR_A--SIMM | | -178.598 | -128.596 | 0. |
| 26 | 1.04666 | TERR_A--SIMM | | -168.559 | -52.356 | 0. |
| 26 | 2.09332 | TERR_A--SIMM | | -158.519 | 23.884 | 0. |
| 26 | 0. | INERZIA H SLV | | -0.993 | -1.222 | 0. |
| 26 | 1.04666 | INERZIA H SLV | | -0.993 | -1.222 | 0. |
| 26 | 2.09332 | INERZIA H SLV | | -0.993 | -1.222 | 0. |
| 26 | 0. | INERZIA V + SLV | | -0.654 | -0.143 | 0. |
| 26 | 1.04666 | INERZIA V + SLV | | -0.654 | -0.143 | 0. |
| 26 | 2.09332 | INERZIA V + SLV | | -0.654 | -0.143 | 0. |
| 26 | 0. | INERZIA V - SLV | | 0.654 | 0.143 | 0. |
| 26 | 1.04666 | INERZIA V - SLV | | 0.654 | 0.143 | 0. |
| 26 | 2.09332 | INERZIA V - SLV | | 0.654 | 0.143 | 0. |
| 26 | 0. | SISMA WOOD SLV | | -338.872 | -26.12 | 0. |
| 26 | 1.04666 | SISMA WOOD SLV | | -338.872 | -26.12 | 0. |
| 26 | 2.09332 | SISMA WOOD SLV | | -338.872 | -26.12 | 0. |
| 26 | 0. | iDROSTATICA | | -302.595 | -9.221 | 0. |
| 26 | 1.04666 | iDROSTATICA | | -302.595 | 14.124 | 0. |
| 26 | 2.09332 | iDROSTATICA | | -302.595 | 34.906 | 0. |
| 26 | 0. | SISMA WOOD SLD | | -149.66 | -11.536 | 0. |
| 26 | 1.04666 | SISMA WOOD SLD | | -149.66 | -11.536 | 0. |
| 26 | 2.09332 | SISMA WOOD SLD | | -149.66 | -11.536 | 0. |
| 26 | 0. | INERZIA H SLD | | -0.439 | -0.54 | 0. |
| 26 | 1.04666 | INERZIA H SLD | | -0.439 | -0.54 | 0. |
| 26 | 2.09332 | INERZIA H SLD | | -0.439 | -0.54 | 0. |
| 26 | 0. | INERZIA V + SLD | | -0.289 | -0.063 | 0. |
| 26 | 1.04666 | INERZIA V + SLD | | -0.289 | -0.063 | 0. |
| 26 | 2.09332 | INERZIA V + SLD | | -0.289 | -0.063 | 0. |
| 26 | 0. | INERZIA V SLD | | 0.289 | 0.063 | 0. |
| 26 | 1.04666 | INERZIA V SLD | | 0.289 | 0.063 | 0. |
| 26 | 2.09332 | INERZIA V SLD | | 0.289 | 0.063 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------|----------|-----------|----------|----------|
| 26 | 0. | INERZIA V -1 | | 0.654 | 0.143 | 0. |
| 26 | 1.04666 | INERZIA V -1 | | 0.654 | 0.143 | 0. |
| 26 | 2.09332 | INERZIA V -1 | | 0.654 | 0.143 | 0. |
| 26 | 0. | SLU_1 | Max | -1381.117 | -168.653 | 0. |
| 26 | 1.04666 | SLU_1 | Max | -1420.274 | 14.468 | 0. |
| 26 | 2.09332 | SLU_1 | Max | -1457.712 | 194.029 | 0. |
| 26 | 0. | SLU_1 | Min | -1381.117 | -168.653 | 0. |
| 26 | 1.04666 | SLU_1 | Min | -1420.274 | 14.468 | 0. |
| 26 | 2.09332 | SLU_1 | Min | -1457.712 | 194.029 | 0. |
| 26 | 0. | SLU_2 | Max | -1196.868 | -193.039 | 0. |
| 26 | 1.04666 | SLU_2 | Max | -1215.028 | -12.683 | 0. |
| 26 | 2.09332 | SLU_2 | Max | -1233.189 | 164.339 | 0. |
| 26 | 0. | SLU_2 | Min | -1196.868 | -193.039 | 0. |
| 26 | 1.04666 | SLU_2 | Min | -1215.028 | -12.683 | 0. |
| 26 | 2.09332 | SLU_2 | Min | -1233.189 | 164.339 | 0. |
| 26 | 0. | SLU_3 | Max | -1587.684 | -277.784 | 0. |
| 26 | 1.04666 | SLU_3 | Max | -1631.207 | -74.902 | 0. |
| 26 | 2.09332 | SLU_3 | Max | -1674.731 | 124.647 | 0. |
| 26 | 0. | SLU_3 | Min | -1587.684 | -277.784 | 0. |
| 26 | 1.04666 | SLU_3 | Min | -1631.207 | -74.902 | 0. |
| 26 | 2.09332 | SLU_3 | Min | -1674.731 | 124.647 | 0. |
| 26 | 0. | SLU_4 | Max | -1380.898 | -289.186 | 0. |
| 26 | 1.04666 | SLU_4 | Max | -1402.726 | -89.161 | 0. |
| 26 | 2.09332 | SLU_4 | Max | -1424.555 | 107.531 | 0. |
| 26 | 0. | SLU_4 | Min | -1380.898 | -289.186 | 0. |
| 26 | 1.04666 | SLU_4 | Min | -1402.726 | -89.161 | 0. |
| 26 | 2.09332 | SLU_4 | Min | -1424.555 | 107.531 | 0. |
| 26 | 0. | SLE_F1 | Max | -1006.404 | -119.967 | 0. |
| 26 | 1.04666 | SLE_F1 | Max | -1033.439 | 11.962 | 0. |
| 26 | 2.09332 | SLE_F1 | Max | -1059.15 | 141.153 | 0. |
| 26 | 0. | SLE_F1 | Min | -1006.404 | -119.967 | 0. |
| 26 | 1.04666 | SLE_F1 | Min | -1033.439 | 11.962 | 0. |
| 26 | 2.09332 | SLE_F1 | Min | -1059.15 | 141.153 | 0. |
| 26 | 0. | SLE_F2 | Max | -873.282 | -137.667 | 0. |
| 26 | 1.04666 | SLE_F2 | Max | -885.56 | -7.681 | 0. |
| 26 | 2.09332 | SLE_F2 | Max | -897.838 | 119.74 | 0. |
| 26 | 0. | SLE_F2 | Min | -873.282 | -137.667 | 0. |
| 26 | 1.04666 | SLE_F2 | Min | -885.56 | -7.681 | 0. |
| 26 | 2.09332 | SLE_F2 | Min | -897.838 | 119.74 | 0. |
| 26 | 0. | SLE_F3 | Max | -1015.367 | -211.532 | 0. |
| 26 | 1.04666 | SLE_F3 | Max | -1030.467 | -66.416 | 0. |
| 26 | 2.09332 | SLE_F3 | Max | -1045.567 | 76.136 | 0. |
| 26 | 0. | SLE_F3 | Min | -1015.367 | -211.532 | 0. |
| 26 | 1.04666 | SLE_F3 | Min | -1030.467 | -66.416 | 0. |
| 26 | 2.09332 | SLE_F3 | Min | -1045.567 | 76.136 | 0. |
| 26 | 0. | SLE_F4 | Max | -1168.466 | -203.349 | 0. |
| 26 | 1.04666 | SLE_F4 | Max | -1198.859 | -56.219 | 0. |
| 26 | 2.09332 | SLE_F4 | Max | -1229.252 | 88.346 | 0. |
| 26 | 0. | SLE_F4 | Min | -1168.466 | -203.349 | 0. |
| 26 | 1.04666 | SLE_F4 | Min | -1198.859 | -56.219 | 0. |
| 26 | 2.09332 | SLE_F4 | Min | -1229.252 | 88.346 | 0. |
| 26 | 0. | SLE_QP1 | Max | -901.731 | -102.045 | 0. |
| 26 | 1.04666 | SLE_QP1 | Max | -923.033 | 13.293 | 0. |
| 26 | 2.09332 | SLE_QP1 | Max | -943.011 | 125.894 | 0. |
| 26 | 0. | SLE_QP1 | Min | -901.731 | -102.045 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 26 | 1.04666 | SLE_QP1 | Min | -923.033 | 13.293 | 0. |
| 26 | 2.09332 | SLE_QP1 | Min | -943.011 | 125.894 | 0. |
| 26 | 0. | SLE_QP2 | Max | -785.283 | -117.563 | 0. |
| 26 | 1.04666 | SLE_QP2 | Max | -794.419 | -3.827 | 0. |
| 26 | 2.09332 | SLE_QP2 | Max | -803.556 | 107.346 | 0. |
| 26 | 0. | SLE_QP2 | Min | -785.283 | -117.563 | 0. |
| 26 | 1.04666 | SLE_QP2 | Min | -794.419 | -3.827 | 0. |
| 26 | 2.09332 | SLE_QP2 | Min | -803.556 | 107.346 | 0. |
| 26 | 0. | SLE_QP3 | Max | -928.339 | -191.254 | 0. |
| 26 | 1.04666 | SLE_QP3 | Max | -940.297 | -62.387 | 0. |
| 26 | 2.09332 | SLE_QP3 | Max | -952.256 | 63.916 | 0. |
| 26 | 0. | SLE_QP3 | Min | -928.339 | -191.254 | 0. |
| 26 | 1.04666 | SLE_QP3 | Min | -940.297 | -62.387 | 0. |
| 26 | 2.09332 | SLE_QP3 | Min | -952.256 | 63.916 | 0. |
| 26 | 0. | SLE_QP4 | Max | -1070.963 | -183.908 | 0. |
| 26 | 1.04666 | SLE_QP4 | Max | -1095.623 | -53.369 | 0. |
| 26 | 2.09332 | SLE_QP4 | Max | -1120.283 | 74.607 | 0. |
| 26 | 0. | SLE_QP4 | Min | -1070.963 | -183.908 | 0. |
| 26 | 1.04666 | SLE_QP4 | Min | -1095.623 | -53.369 | 0. |
| 26 | 2.09332 | SLE_QP4 | Min | -1120.283 | 74.607 | 0. |
| 26 | 0. | SLV_1 | Max | -1457.72 | -133.254 | 0. |
| 26 | 1.04666 | SLV_1 | Max | -1479.021 | -17.915 | 0. |
| 26 | 2.09332 | SLV_1 | Max | -1498.999 | 94.685 | 0. |
| 26 | 0. | SLV_1 | Min | -1457.72 | -133.254 | 0. |
| 26 | 1.04666 | SLV_1 | Min | -1479.021 | -17.915 | 0. |
| 26 | 2.09332 | SLV_1 | Min | -1498.999 | 94.685 | 0. |
| 26 | 0. | SLV_2 | Max | -1455.44 | -132.273 | 0. |
| 26 | 1.04666 | SLV_2 | Max | -1476.742 | -16.935 | 0. |
| 26 | 2.09332 | SLV_2 | Max | -1496.72 | 95.666 | 0. |
| 26 | 0. | SLV_2 | Min | -1455.44 | -132.273 | 0. |
| 26 | 1.04666 | SLV_2 | Min | -1476.742 | -16.935 | 0. |
| 26 | 2.09332 | SLV_2 | Min | -1496.72 | 95.666 | 0. |
| 26 | 0. | SLV_3 | Max | -1673.478 | -190.977 | 0. |
| 26 | 1.04666 | SLV_3 | Max | -1698.137 | -60.437 | 0. |
| 26 | 2.09332 | SLV_3 | Max | -1722.797 | 67.538 | 0. |
| 26 | 0. | SLV_3 | Min | -1673.478 | -190.977 | 0. |
| 26 | 1.04666 | SLV_3 | Min | -1698.137 | -60.437 | 0. |
| 26 | 2.09332 | SLV_3 | Min | -1722.797 | 67.538 | 0. |
| 26 | 0. | SLV_4 | Max | -1671.207 | -189.803 | 0. |
| 26 | 1.04666 | SLV_4 | Max | -1695.867 | -59.264 | 0. |
| 26 | 2.09332 | SLV_4 | Max | -1720.527 | 68.711 | 0. |
| 26 | 0. | SLV_4 | Min | -1671.207 | -189.803 | 0. |
| 26 | 1.04666 | SLV_4 | Min | -1695.867 | -59.264 | 0. |
| 26 | 2.09332 | SLV_4 | Min | -1720.527 | 68.711 | 0. |
| 26 | 0. | SLD_1 | Max | -1117.253 | -133.908 | 0. |
| 26 | 1.04666 | SLD_1 | Max | -1138.554 | -18.569 | 0. |
| 26 | 2.09332 | SLD_1 | Max | -1158.532 | 94.031 | 0. |
| 26 | 0. | SLD_1 | Min | -1117.253 | -133.908 | 0. |
| 26 | 1.04666 | SLD_1 | Min | -1138.554 | -18.569 | 0. |
| 26 | 2.09332 | SLD_1 | Min | -1158.532 | 94.031 | 0. |
| 26 | 0. | SLD_2 | Max | -1115.901 | -133.607 | 0. |
| 26 | 1.04666 | SLD_2 | Max | -1137.202 | -18.268 | 0. |
| 26 | 2.09332 | SLD_2 | Max | -1157.18 | 94.332 | 0. |
| 26 | 0. | SLD_2 | Min | -1115.901 | -133.607 | 0. |
| 26 | 1.04666 | SLD_2 | Min | -1137.202 | -18.268 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 26 | 2.09332 | SLD_2 | Min | -1157.18 | 94.332 | 0. |
| 26 | 0. | SLD_3 | Max | -1333.341 | -195.828 | 0. |
| 26 | 1.04666 | SLD_3 | Max | -1358.001 | -65.288 | 0. |
| 26 | 2.09332 | SLD_3 | Max | -1382.66 | 62.687 | 0. |
| 26 | 0. | SLD_3 | Min | -1333.341 | -195.828 | 0. |
| 26 | 1.04666 | SLD_3 | Min | -1358.001 | -65.288 | 0. |
| 26 | 2.09332 | SLD_3 | Min | -1382.66 | 62.687 | 0. |
| 26 | 0. | SLD_4 | Max | -1332.254 | -195.4 | 0. |
| 26 | 1.04666 | SLD_4 | Max | -1356.913 | -64.86 | 0. |
| 26 | 2.09332 | SLD_4 | Max | -1381.573 | 63.115 | 0. |
| 26 | 0. | SLD_4 | Min | -1332.254 | -195.4 | 0. |
| 26 | 1.04666 | SLD_4 | Min | -1356.913 | -64.86 | 0. |
| 26 | 2.09332 | SLD_4 | Min | -1381.573 | 63.115 | 0. |
| 26 | 0. | SLU_IDR_1 | Max | -880.851 | -174.469 | 0. |
| 26 | 1.04666 | SLU_IDR_1 | Max | -891.613 | -53.819 | 0. |
| 26 | 2.09332 | SLU_IDR_1 | Max | -902.376 | 64.009 | 0. |
| 26 | 0. | SLU_IDR_1 | Min | -880.851 | -174.469 | 0. |
| 26 | 1.04666 | SLU_IDR_1 | Min | -891.613 | -53.819 | 0. |
| 26 | 2.09332 | SLU_IDR_1 | Min | -902.376 | 64.009 | 0. |
| 26 | 0. | SLU_IDR_2 | Max | -749.957 | -108.555 | 0. |
| 26 | 1.04666 | SLU_IDR_2 | Max | -758.181 | -1.523 | 0. |
| 26 | 2.09332 | SLU_IDR_2 | Max | -766.404 | 102.688 | 0. |
| 26 | 0. | SLU_IDR_2 | Min | -749.957 | -108.555 | 0. |
| 26 | 1.04666 | SLU_IDR_2 | Min | -758.181 | -1.523 | 0. |
| 26 | 2.09332 | SLU_IDR_2 | Min | -766.404 | 102.688 | 0. |
| 26 | 0. | SISMA WOOD SLV-1 | Max | -700.815 | 15.755 | 0. |
| 26 | 1.04666 | SISMA WOOD SLV-1 | Max | -700.815 | 15.755 | 0. |
| 26 | 2.09332 | SISMA WOOD SLV-1 | Max | -700.815 | 15.755 | 0. |
| 26 | 0. | SISMA WOOD SLV-1 | Min | -700.815 | 15.755 | 0. |
| 26 | 1.04666 | SISMA WOOD SLV-1 | Min | -700.815 | 15.755 | 0. |
| 26 | 2.09332 | SISMA WOOD SLV-1 | Min | -700.815 | 15.755 | 0. |
| 26 | 0. | DEAD-1 | Max | -100.484 | -39.614 | 0. |
| 26 | 1.04666 | DEAD-1 | Max | -97.069 | -13.679 | 0. |
| 26 | 2.09332 | DEAD-1 | Max | -93.653 | 12.256 | 0. |
| 26 | 0. | DEAD-1 | Min | -100.484 | -39.614 | 0. |
| 26 | 1.04666 | DEAD-1 | Min | -97.069 | -13.679 | 0. |
| 26 | 2.09332 | DEAD-1 | Min | -93.653 | 12.256 | 0. |
| 26 | 0. | SLU_PROVA | | -1209.368 | -155.788 | 0. |
| 26 | 1.04666 | SLU_PROVA | | -1248.525 | 27.333 | 0. |
| 26 | 2.09332 | SLU_PROVA | | -1285.963 | 206.894 | 0. |
| 27 | 0. | DEAD | | 11.976 | -11.216 | 0. |
| 27 | 0.44885 | DEAD | | 11.976 | 2.246 | 0. |
| 27 | 0.8977 | DEAD | | 11.976 | 15.708 | 0. |
| 27 | 0. | SIMM_KA | | -147.662 | -3.268 | 0. |
| 27 | 0.44885 | SIMM_KA | | -147.662 | -3.268 | 0. |
| 27 | 0.8977 | SIMM_KA | | -147.662 | -3.268 | 0. |
| 27 | 0. | SIMM_K0 | | -222.816 | -4.966 | 0. |
| 27 | 0.44885 | SIMM_K0 | | -222.816 | -4.966 | 0. |
| 27 | 0.8977 | SIMM_K0 | | -222.816 | -4.966 | 0. |
| 27 | 0. | A--SIMM_KA | | -181.564 | 11.913 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 27 | 0.44885 | A--SIMM_KA | | -181.564 | 11.913 | 0. |
| 27 | 0.8977 | A--SIMM_KA | | -181.564 | 11.913 | 0. |
| 27 | 0. | A--SIMM_K0 | | -279.843 | 17.504 | 0. |
| 27 | 0.44885 | A--SIMM_K0 | | -279.843 | 17.504 | 0. |
| 27 | 0.8977 | A--SIMM_K0 | | -279.843 | 17.504 | 0. |
| 27 | 0. | A-- SIMM_SOVR_K A | | -8.817 | -0.353 | 0. |
| 27 | 0.44885 | A-- SIMM_SOVR_K A | | -8.817 | -0.353 | 0. |
| 27 | 0.8977 | A-- SIMM_SOVR_K A | | -8.817 | -0.353 | 0. |
| 27 | 0. | A-- SIMM_SOVR_K 0 | | -13.22 | -0.529 | 0. |
| 27 | 0.44885 | A-- SIMM_SOVR_K 0 | | -13.22 | -0.529 | 0. |
| 27 | 0.8977 | A-- SIMM_SOVR_K 0 | | -13.22 | -0.529 | 0. |
| 27 | 0. | A-- SIMM_SOVR_K 0 | | -13.22 | -0.529 | 0. |
| 27 | 0.44885 | A-- SIMM_SOVR_K 0 | | -13.22 | -0.529 | 0. |
| 27 | 0.8977 | A-- SIMM_SOVR_K 0 | | -13.22 | -0.529 | 0. |
| 27 | 0. | A-- SIMM_SOVR_K A | | -8.817 | -0.353 | 0. |
| 27 | 0.44885 | A-- SIMM_SOVR_K A | | -8.817 | -0.353 | 0. |
| 27 | 0.8977 | A-- SIMM_SOVR_K A | | -8.817 | -0.353 | 0. |
| 27 | 0. | SOVR | | 8.446 | -0.565 | 0. |
| 27 | 0.44885 | SOVR | | 8.446 | -0.565 | 0. |
| 27 | 0.8977 | SOVR | | 8.446 | -0.565 | 0. |
| 27 | 0. | TERR_SIMM | | 10.053 | -3.162 | 0. |
| 27 | 0.44885 | TERR_SIMM | | 10.053 | -3.162 | 0. |
| 27 | 0.8977 | TERR_SIMM | | 10.053 | -3.162 | 0. |
| 27 | 0. | TERR_A--SIMM | | 14.914 | -10.849 | 0. |
| 27 | 0.44885 | TERR_A--SIMM | | 14.914 | -10.849 | 0. |
| 27 | 0.8977 | TERR_A--SIMM | | 14.914 | -10.849 | 0. |
| 27 | 0. | INERZIA H SLV | | -0.44 | 0.599 | 0. |
| 27 | 0.44885 | INERZIA H SLV | | -0.44 | 0.599 | 0. |
| 27 | 0.8977 | INERZIA H SLV | | -0.44 | 0.599 | 0. |
| 27 | 0. | INERZIA V + SLV | | 0.173 | 0.036 | 0. |
| 27 | 0.44885 | INERZIA V + SLV | | 0.173 | 0.036 | 0. |
| 27 | 0.8977 | INERZIA V + SLV | | 0.173 | 0.036 | 0. |
| 27 | 0. | INERZIA V - SLV | | -0.173 | -0.036 | 0. |
| 27 | 0.44885 | INERZIA V - SLV | | -0.173 | -0.036 | 0. |
| 27 | 0.8977 | INERZIA V - SLV | | -0.173 | -0.036 | 0. |
| 27 | 0. | SISMA WOOD SLV | | -403.24 | 26.373 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 27 | 0.44885 | SISMA WOOD SLV | | -403.24 | 26.373 | 0. |
| 27 | 0.8977 | SISMA WOOD SLV | | -403.24 | 26.373 | 0. |
| 27 | 0. | iDROSTATICA | | -580.943 | 30.167 | 0. |
| 27 | 0.44885 | iDROSTATICA | | -580.943 | -28.812 | 0. |
| 27 | 0.8977 | iDROSTATICA | | -580.943 | -87.791 | 0. |
| 27 | 0. | SISMA WOOD SLD | | -178.087 | 11.648 | 0. |
| 27 | 0.44885 | SISMA WOOD SLD | | -178.087 | 11.648 | 0. |
| 27 | 0.8977 | SISMA WOOD SLD | | -178.087 | 11.648 | 0. |
| 27 | 0. | INERZIA H SLD | | -0.194 | 0.265 | 0. |
| 27 | 0.44885 | INERZIA H SLD | | -0.194 | 0.265 | 0. |
| 27 | 0.8977 | INERZIA H SLD | | -0.194 | 0.265 | 0. |
| 27 | 0. | INERZIA V + SLD | | 0.076 | 0.016 | 0. |
| 27 | 0.44885 | INERZIA V + SLD | | 0.076 | 0.016 | 0. |
| 27 | 0.8977 | INERZIA V + SLD | | 0.076 | 0.016 | 0. |
| 27 | 0. | INERZIA V SLD | | -0.076 | -0.016 | 0. |
| 27 | 0.44885 | INERZIA V SLD | | -0.076 | -0.016 | 0. |
| 27 | 0.8977 | INERZIA V SLD | | -0.076 | -0.016 | 0. |
| 27 | 0. | INERZIA V -1 | | -0.173 | -0.036 | 0. |
| 27 | 0.44885 | INERZIA V -1 | | -0.173 | -0.036 | 0. |
| 27 | 0.8977 | INERZIA V -1 | | -0.173 | -0.036 | 0. |
| 27 | 0. | SLU_1 | Max | -1027.042 | 0.623 | 0. |
| 27 | 0.44885 | SLU_1 | Max | -1027.042 | -58.549 | 0. |
| 27 | 0.8977 | SLU_1 | Max | -1027.042 | -117.722 | 0. |
| 27 | 0. | SLU_1 | Min | -1027.042 | 0.623 | 0. |
| 27 | 0.44885 | SLU_1 | Min | -1027.042 | -58.549 | 0. |
| 27 | 0.8977 | SLU_1 | Min | -1027.042 | -117.722 | 0. |
| 27 | 0. | SLU_2 | Max | -928.803 | -0.39 | 0. |
| 27 | 0.44885 | SLU_2 | Max | -928.803 | -59.562 | 0. |
| 27 | 0.8977 | SLU_2 | Max | -928.803 | -118.735 | 0. |
| 27 | 0. | SLU_2 | Min | -928.803 | -0.39 | 0. |
| 27 | 0.44885 | SLU_2 | Min | -928.803 | -59.562 | 0. |
| 27 | 0.8977 | SLU_2 | Min | -928.803 | -118.735 | 0. |
| 27 | 0. | SLU_3 | Max | -1091.704 | 46.466 | 0. |
| 27 | 0.44885 | SLU_3 | Max | -1091.704 | -12.707 | 0. |
| 27 | 0.8977 | SLU_3 | Max | -1091.704 | -71.879 | 0. |
| 27 | 0. | SLU_3 | Min | -1091.704 | 46.466 | 0. |
| 27 | 0.44885 | SLU_3 | Min | -1091.704 | -12.707 | 0. |
| 27 | 0.8977 | SLU_3 | Min | -1091.704 | -71.879 | 0. |
| 27 | 0. | SLU_4 | Max | -955.452 | 31.883 | 0. |
| 27 | 0.44885 | SLU_4 | Max | -955.452 | -27.29 | 0. |
| 27 | 0.8977 | SLU_4 | Max | -955.452 | -86.463 | 0. |
| 27 | 0. | SLU_4 | Min | -955.452 | 31.883 | 0. |
| 27 | 0.44885 | SLU_4 | Min | -955.452 | -27.29 | 0. |
| 27 | 0.8977 | SLU_4 | Min | -955.452 | -86.463 | 0. |
| 27 | 0. | SLE_F1 | Max | -791.921 | -0.327 | 0. |
| 27 | 0.44885 | SLE_F1 | Max | -791.921 | -45.845 | 0. |
| 27 | 0.8977 | SLE_F1 | Max | -791.921 | -91.362 | 0. |
| 27 | 0. | SLE_F1 | Min | -791.921 | -0.327 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 27 | 0.44885 | SLE_F1 | Min | -791.921 | -45.845 | 0. |
| 27 | 0.8977 | SLE_F1 | Min | -791.921 | -91.362 | 0. |
| 27 | 0. | SLE_F2 | Max | -718.886 | -0.22 | 0. |
| 27 | 0.44885 | SLE_F2 | Max | -718.886 | -45.737 | 0. |
| 27 | 0.8977 | SLE_F2 | Max | -718.886 | -91.255 | 0. |
| 27 | 0. | SLE_F2 | Min | -718.886 | -0.22 | 0. |
| 27 | 0.44885 | SLE_F2 | Min | -718.886 | -45.737 | 0. |
| 27 | 0.8977 | SLE_F2 | Min | -718.886 | -91.255 | 0. |
| 27 | 0. | SLE_F3 | Max | -738.631 | 25.327 | 0. |
| 27 | 0.44885 | SLE_F3 | Max | -738.631 | -20.191 | 0. |
| 27 | 0.8977 | SLE_F3 | Max | -738.631 | -65.708 | 0. |
| 27 | 0. | SLE_F3 | Min | -738.631 | 25.327 | 0. |
| 27 | 0.44885 | SLE_F3 | Min | -738.631 | -20.191 | 0. |
| 27 | 0.8977 | SLE_F3 | Min | -738.631 | -65.708 | 0. |
| 27 | 0. | SLE_F4 | Max | -847.866 | 35.911 | 0. |
| 27 | 0.44885 | SLE_F4 | Max | -847.866 | -9.607 | 0. |
| 27 | 0.8977 | SLE_F4 | Max | -847.866 | -55.124 | 0. |
| 27 | 0. | SLE_F4 | Min | -847.866 | 35.911 | 0. |
| 27 | 0.44885 | SLE_F4 | Min | -847.866 | -9.607 | 0. |
| 27 | 0.8977 | SLE_F4 | Min | -847.866 | -55.124 | 0. |
| 27 | 0. | SLE_QP1 | Max | -797.084 | -0.175 | 0. |
| 27 | 0.44885 | SLE_QP1 | Max | -797.084 | -45.692 | 0. |
| 27 | 0.8977 | SLE_QP1 | Max | -797.084 | -91.209 | 0. |
| 27 | 0. | SLE_QP1 | Min | -797.084 | -0.175 | 0. |
| 27 | 0.44885 | SLE_QP1 | Min | -797.084 | -45.692 | 0. |
| 27 | 0.8977 | SLE_QP1 | Min | -797.084 | -91.209 | 0. |
| 27 | 0. | SLE_QP2 | Max | -727.101 | -0.071 | 0. |
| 27 | 0.44885 | SLE_QP2 | Max | -727.101 | -45.588 | 0. |
| 27 | 0.8977 | SLE_QP2 | Max | -727.101 | -91.106 | 0. |
| 27 | 0. | SLE_QP2 | Min | -727.101 | -0.071 | 0. |
| 27 | 0.44885 | SLE_QP2 | Min | -727.101 | -45.588 | 0. |
| 27 | 0.8977 | SLE_QP2 | Min | -727.101 | -91.106 | 0. |
| 27 | 0. | SLE_QP3 | Max | -745.443 | 26.815 | 0. |
| 27 | 0.44885 | SLE_QP3 | Max | -745.443 | -18.702 | 0. |
| 27 | 0.8977 | SLE_QP3 | Max | -745.443 | -64.22 | 0. |
| 27 | 0. | SLE_QP3 | Min | -745.443 | 26.815 | 0. |
| 27 | 0.44885 | SLE_QP3 | Min | -745.443 | -18.702 | 0. |
| 27 | 0.8977 | SLE_QP3 | Min | -745.443 | -64.22 | 0. |
| 27 | 0. | SLE_QP4 | Max | -864.141 | 36.207 | 0. |
| 27 | 0.44885 | SLE_QP4 | Max | -864.141 | -9.311 | 0. |
| 27 | 0.8977 | SLE_QP4 | Max | -864.141 | -54.828 | 0. |
| 27 | 0. | SLE_QP4 | Min | -864.141 | 36.207 | 0. |
| 27 | 0.44885 | SLE_QP4 | Min | -864.141 | -9.311 | 0. |
| 27 | 0.8977 | SLE_QP4 | Min | -864.141 | -54.828 | 0. |
| 27 | 0. | SLV_1 | Max | -1677.71 | 73.136 | 0. |
| 27 | 0.44885 | SLV_1 | Max | -1677.71 | 27.619 | 0. |
| 27 | 0.8977 | SLV_1 | Max | -1677.71 | -17.898 | 0. |
| 27 | 0. | SLV_1 | Min | -1677.71 | 73.136 | 0. |
| 27 | 0.44885 | SLV_1 | Min | -1677.71 | 27.619 | 0. |
| 27 | 0.8977 | SLV_1 | Min | -1677.71 | -17.898 | 0. |
| 27 | 0. | SLV_2 | Max | -1679.165 | 72.466 | 0. |
| 27 | 0.44885 | SLV_2 | Max | -1679.165 | 26.948 | 0. |
| 27 | 0.8977 | SLV_2 | Max | -1679.165 | -18.569 | 0. |
| 27 | 0. | SLV_2 | Min | -1679.165 | 72.466 | 0. |
| 27 | 0.44885 | SLV_2 | Min | -1679.165 | 26.948 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 27 | 0.8977 | SLV_2 | Min | -1679.165 | -18.569 | 0. |
| 27 | 0. | SLV_3 | Max | -1852.883 | 101.054 | 0. |
| 27 | 0.44885 | SLV_3 | Max | -1852.883 | 55.537 | 0. |
| 27 | 0.8977 | SLV_3 | Max | -1852.883 | 10.02 | 0. |
| 27 | 0. | SLV_3 | Min | -1852.883 | 101.054 | 0. |
| 27 | 0.44885 | SLV_3 | Min | -1852.883 | 55.537 | 0. |
| 27 | 0.8977 | SLV_3 | Min | -1852.883 | 10.02 | 0. |
| 27 | 0. | SLV_4 | Max | -1854.114 | 100.847 | 0. |
| 27 | 0.44885 | SLV_4 | Max | -1854.114 | 55.329 | 0. |
| 27 | 0.8977 | SLV_4 | Max | -1854.114 | 9.812 | 0. |
| 27 | 0. | SLV_4 | Min | -1854.114 | 100.847 | 0. |
| 27 | 0.44885 | SLV_4 | Min | -1854.114 | 55.329 | 0. |
| 27 | 0.8977 | SLV_4 | Min | -1854.114 | 9.812 | 0. |
| 27 | 0. | SLD_1 | Max | -1124.138 | 30.346 | 0. |
| 27 | 0.44885 | SLD_1 | Max | -1124.138 | -15.171 | 0. |
| 27 | 0.8977 | SLD_1 | Max | -1124.138 | -60.688 | 0. |
| 27 | 0. | SLD_1 | Min | -1124.138 | 30.346 | 0. |
| 27 | 0.44885 | SLD_1 | Min | -1124.138 | -15.171 | 0. |
| 27 | 0.8977 | SLD_1 | Min | -1124.138 | -60.688 | 0. |
| 27 | 0. | SLD_2 | Max | -1124.905 | 29.823 | 0. |
| 27 | 0.44885 | SLD_2 | Max | -1124.905 | -15.694 | 0. |
| 27 | 0.8977 | SLD_2 | Max | -1124.905 | -61.212 | 0. |
| 27 | 0. | SLD_2 | Min | -1124.905 | 29.823 | 0. |
| 27 | 0.44885 | SLD_2 | Min | -1124.905 | -15.694 | 0. |
| 27 | 0.8977 | SLD_2 | Min | -1124.905 | -61.212 | 0. |
| 27 | 0. | SLD_3 | Max | -1301.502 | 67.337 | 0. |
| 27 | 0.44885 | SLD_3 | Max | -1301.502 | 21.819 | 0. |
| 27 | 0.8977 | SLD_3 | Max | -1301.502 | -23.698 | 0. |
| 27 | 0. | SLD_3 | Min | -1301.502 | 67.337 | 0. |
| 27 | 0.44885 | SLD_3 | Min | -1301.502 | 21.819 | 0. |
| 27 | 0.8977 | SLD_3 | Min | -1301.502 | -23.698 | 0. |
| 27 | 0. | SLD_4 | Max | -1301.966 | 67.16 | 0. |
| 27 | 0.44885 | SLD_4 | Max | -1301.966 | 21.642 | 0. |
| 27 | 0.8977 | SLD_4 | Max | -1301.966 | -23.875 | 0. |
| 27 | 0. | SLD_4 | Min | -1301.966 | 67.16 | 0. |
| 27 | 0.44885 | SLD_4 | Min | -1301.966 | 21.642 | 0. |
| 27 | 0.8977 | SLD_4 | Min | -1301.966 | -23.875 | 0. |
| 27 | 0. | SLU_IDR_1 | Max | -816.414 | 25.203 | 0. |
| 27 | 0.44885 | SLU_IDR_1 | Max | -816.414 | -27.559 | 0. |
| 27 | 0.8977 | SLU_IDR_1 | Max | -816.414 | -80.32 | 0. |
| 27 | 0. | SLU_IDR_1 | Min | -816.414 | 25.203 | 0. |
| 27 | 0.44885 | SLU_IDR_1 | Min | -816.414 | -27.559 | 0. |
| 27 | 0.8977 | SLU_IDR_1 | Min | -816.414 | -80.32 | 0. |
| 27 | 0. | SLU_IDR_2 | Max | -806.024 | -0.823 | 0. |
| 27 | 0.44885 | SLU_IDR_2 | Max | -806.024 | -53.585 | 0. |
| 27 | 0.8977 | SLU_IDR_2 | Max | -806.024 | -106.346 | 0. |
| 27 | 0. | SLU_IDR_2 | Min | -806.024 | -0.823 | 0. |
| 27 | 0.44885 | SLU_IDR_2 | Min | -806.024 | -53.585 | 0. |
| 27 | 0.8977 | SLU_IDR_2 | Min | -806.024 | -106.346 | 0. |
| 27 | 0. | SISMA WOOD SLV-1 | Max | -901.453 | 27.873 | 0. |
| 27 | 0.44885 | SISMA WOOD SLV-1 | Max | -901.453 | 27.873 | 0. |
| 27 | 0.8977 | SISMA WOOD SLV-1 | Max | -901.453 | 27.873 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 27 | 0. | SISMA WOOD SLV-1 | Min | -901.453 | 27.873 | 0. |
| 27 | 0.44885 | SISMA WOOD SLV-1 | Min | -901.453 | 27.873 | 0. |
| 27 | 0.8977 | SISMA WOOD SLV-1 | Min | -901.453 | 27.873 | 0. |
| 27 | 0. | DEAD-1 | Max | 16.915 | -11.322 | 0. |
| 27 | 0.44885 | DEAD-1 | Max | 16.915 | 2.14 | 0. |
| 27 | 0.8977 | DEAD-1 | Max | 16.915 | 15.601 | 0. |
| 27 | 0. | DEAD-1 | Min | 16.915 | -11.322 | 0. |
| 27 | 0.44885 | DEAD-1 | Min | 16.915 | 2.14 | 0. |
| 27 | 0.8977 | DEAD-1 | Min | 16.915 | 15.601 | 0. |
| 27 | 0. | SLU_PROVA | | -1023.41 | 12.429 | 0. |
| 27 | 0.44885 | SLU_PROVA | | -1023.41 | -46.743 | 0. |
| 27 | 0.8977 | SLU_PROVA | | -1023.41 | -105.916 | 0. |
| 28 | 0. | DEAD | | 12.374 | -13.557 | 0. |
| 28 | 0.6275 | DEAD | | 14.624 | 5.128 | 0. |
| 28 | 1.255 | DEAD | | 16.873 | 23.812 | 0. |
| 28 | 0. | SIMM_KA | | -147.403 | 6.252 | 0. |
| 28 | 0.6275 | SIMM_KA | | -147.403 | 6.252 | 0. |
| 28 | 1.255 | SIMM_KA | | -147.403 | 6.252 | 0. |
| 28 | 0. | SIMM_K0 | | -222.436 | 9.281 | 0. |
| 28 | 0.6275 | SIMM_K0 | | -222.436 | 9.281 | 0. |
| 28 | 1.255 | SIMM_K0 | | -222.436 | 9.281 | 0. |
| 28 | 0. | A--SIMM_KA | | -179.333 | 22.923 | 0. |
| 28 | 0.6275 | A--SIMM_KA | | -179.333 | 22.923 | 0. |
| 28 | 1.255 | A--SIMM_KA | | -179.333 | 22.923 | 0. |
| 28 | 0. | A--SIMM_K0 | | -276.502 | 34.64 | 0. |
| 28 | 0.6275 | A--SIMM_K0 | | -276.502 | 34.64 | 0. |
| 28 | 1.255 | A--SIMM_K0 | | -276.502 | 34.64 | 0. |
| 28 | 0. | A-- SIMM_SOVR_K A | | -8.841 | -0.18 | 0. |
| 28 | 0.6275 | A-- SIMM_SOVR_K A | | -8.841 | -0.18 | 0. |
| 28 | 1.255 | A-- SIMM_SOVR_K A | | -8.841 | -0.18 | 0. |
| 28 | 0. | A-- SIMM_SOVR_K 0 | | -13.255 | -0.269 | 0. |
| 28 | 0.6275 | A-- SIMM_SOVR_K 0 | | -13.255 | -0.269 | 0. |
| 28 | 1.255 | A-- SIMM_SOVR_K 0 | | -13.255 | -0.269 | 0. |
| 28 | 0. | SIMM_SOVR_K 0 | | -13.255 | -0.269 | 0. |
| 28 | 0.6275 | SIMM_SOVR_K 0 | | -13.255 | -0.269 | 0. |
| 28 | 1.255 | SIMM_SOVR_K 0 | | -13.255 | -0.269 | 0. |
| 28 | 0. | SIMM_SOVR_K A | | -8.841 | -0.18 | 0. |
| 28 | 0.6275 | SIMM_SOVR_K A | | -8.841 | -0.18 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 28 | 1.255 | SIMM_SOVR_K A | | -8.841 | -0.18 | 0. |
| 28 | 0. | SOVR | | 8.227 | -3.381 | 0. |
| 28 | 0.6275 | SOVR | | 8.227 | -3.381 | 0. |
| 28 | 1.255 | SOVR | | 8.227 | -3.381 | 0. |
| 28 | 0. | TERR_SIMM | | 9.123 | -13.861 | 0. |
| 28 | 0.6275 | TERR_SIMM | | 9.123 | -13.861 | 0. |
| 28 | 1.255 | TERR_SIMM | | 9.123 | -13.861 | 0. |
| 28 | 0. | TERR_A--SIMM | | 12.989 | -23.177 | 0. |
| 28 | 0.6275 | TERR_A--SIMM | | 12.989 | -23.177 | 0. |
| 28 | 1.255 | TERR_A--SIMM | | 12.989 | -23.177 | 0. |
| 28 | 0. | INERZIA H SLV | | -1.401 | 0.616 | 0. |
| 28 | 0.6275 | INERZIA H SLV | | -1.401 | 0.616 | 0. |
| 28 | 1.255 | INERZIA H SLV | | -1.401 | 0.616 | 0. |
| 28 | 0. | INERZIA V + SLV | | 0.216 | 0.085 | 0. |
| 28 | 0.6275 | INERZIA V + SLV | | 0.216 | 0.085 | 0. |
| 28 | 1.255 | INERZIA V + SLV | | 0.216 | 0.085 | 0. |
| 28 | 0. | INERZIA V - SLV | | -0.216 | -0.085 | 0. |
| 28 | 0.6275 | INERZIA V - SLV | | -0.216 | -0.085 | 0. |
| 28 | 1.255 | INERZIA V - SLV | | -0.216 | -0.085 | 0. |
| 28 | 0. | SISMA WOOD SLV | | -397.702 | 59.022 | 0. |
| 28 | 0.6275 | SISMA WOOD SLV | | -397.702 | 59.022 | 0. |
| 28 | 1.255 | SISMA WOOD SLV | | -397.702 | 59.022 | 0. |
| 28 | 0. | iDROSTATICA | | -583.753 | 52.374 | 0. |
| 28 | 0.6275 | iDROSTATICA | | -583.753 | -28.772 | 0. |
| 28 | 1.255 | iDROSTATICA | | -583.753 | -107.305 | 0. |
| 28 | 0. | SISMA WOOD SLD | | -175.641 | 26.067 | 0. |
| 28 | 0.6275 | SISMA WOOD SLD | | -175.641 | 26.067 | 0. |
| 28 | 1.255 | SISMA WOOD SLD | | -175.641 | 26.067 | 0. |
| 28 | 0. | INERZIA H SLD | | -0.619 | 0.272 | 0. |
| 28 | 0.6275 | INERZIA H SLD | | -0.619 | 0.272 | 0. |
| 28 | 1.255 | INERZIA H SLD | | -0.619 | 0.272 | 0. |
| 28 | 0. | INERZIA V + SLD | | 0.095 | 0.037 | 0. |
| 28 | 0.6275 | INERZIA V + SLD | | 0.095 | 0.037 | 0. |
| 28 | 1.255 | INERZIA V + SLD | | 0.095 | 0.037 | 0. |
| 28 | 0. | INERZIA V SLD | | -0.095 | -0.037 | 0. |
| 28 | 0.6275 | INERZIA V SLD | | -0.095 | -0.037 | 0. |
| 28 | 1.255 | INERZIA V SLD | | -0.095 | -0.037 | 0. |
| 28 | 0. | INERZIA V -1 | | -0.216 | -0.085 | 0. |
| 28 | 0.6275 | INERZIA V -1 | | -0.216 | -0.085 | 0. |
| 28 | 1.255 | INERZIA V -1 | | -0.216 | -0.085 | 0. |
| 28 | 0. | SLU_1 | Max | -1033.749 | 5.882 | 0. |
| 28 | 0.6275 | SLU_1 | Max | -1030.825 | -75.319 | 0. |
| 28 | 1.255 | SLU_1 | Max | -1027.901 | -153.122 | 0. |
| 28 | 0. | SLU_1 | Min | -1033.749 | 5.882 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 28 | 0.6275 | SLU_1 | Min | -1030.825 | -75.319 | 0. |
| 28 | 1.255 | SLU_1 | Min | -1027.901 | -153.122 | 0. |
| 28 | 0. | SLU_2 | Max | -936.336 | -6.863 | 0. |
| 28 | 0.6275 | SLU_2 | Max | -933.412 | -88.064 | 0. |
| 28 | 1.255 | SLU_2 | Max | -930.488 | -165.867 | 0. |
| 28 | 0. | SLU_2 | Min | -936.336 | -6.863 | 0. |
| 28 | 0.6275 | SLU_2 | Min | -933.412 | -88.064 | 0. |
| 28 | 1.255 | SLU_2 | Min | -930.488 | -165.867 | 0. |
| 28 | 0. | SLU_3 | Max | -1092.469 | 59.122 | 0. |
| 28 | 0.6275 | SLU_3 | Max | -1089.545 | -22.079 | 0. |
| 28 | 1.255 | SLU_3 | Max | -1086.621 | -99.882 | 0. |
| 28 | 0. | SLU_3 | Min | -1092.469 | 59.122 | 0. |
| 28 | 0.6275 | SLU_3 | Min | -1089.545 | -22.079 | 0. |
| 28 | 1.255 | SLU_3 | Min | -1086.621 | -99.882 | 0. |
| 28 | 0. | SLU_4 | Max | -958.937 | 28.361 | 0. |
| 28 | 0.6275 | SLU_4 | Max | -956.013 | -52.84 | 0. |
| 28 | 1.255 | SLU_4 | Max | -953.089 | -130.643 | 0. |
| 28 | 0. | SLU_4 | Min | -958.937 | 28.361 | 0. |
| 28 | 0.6275 | SLU_4 | Min | -956.013 | -52.84 | 0. |
| 28 | 1.255 | SLU_4 | Min | -953.089 | -130.643 | 0. |
| 28 | 0. | SLE_F1 | Max | -797.164 | 3.95 | 0. |
| 28 | 0.6275 | SLE_F1 | Max | -794.914 | -58.512 | 0. |
| 28 | 1.255 | SLE_F1 | Max | -792.665 | -118.361 | 0. |
| 28 | 0. | SLE_F1 | Min | -797.164 | 3.95 | 0. |
| 28 | 0.6275 | SLE_F1 | Min | -794.914 | -58.512 | 0. |
| 28 | 1.255 | SLE_F1 | Min | -792.665 | -118.361 | 0. |
| 28 | 0. | SLE_F2 | Max | -724.639 | -4.671 | 0. |
| 28 | 0.6275 | SLE_F2 | Max | -722.389 | -67.133 | 0. |
| 28 | 1.255 | SLE_F2 | Max | -720.14 | -126.981 | 0. |
| 28 | 0. | SLE_F2 | Min | -724.639 | -4.671 | 0. |
| 28 | 0.6275 | SLE_F2 | Min | -722.389 | -67.133 | 0. |
| 28 | 1.255 | SLE_F2 | Min | -720.14 | -126.981 | 0. |
| 28 | 0. | SLE_F3 | Max | -741.19 | 23.051 | 0. |
| 28 | 0.6275 | SLE_F3 | Max | -738.94 | -39.411 | 0. |
| 28 | 1.255 | SLE_F3 | Max | -736.691 | -99.26 | 0. |
| 28 | 0. | SLE_F3 | Min | -741.19 | 23.051 | 0. |
| 28 | 0.6275 | SLE_F3 | Min | -738.94 | -39.411 | 0. |
| 28 | 1.255 | SLE_F3 | Min | -736.691 | -99.26 | 0. |
| 28 | 0. | SLE_F4 | Max | -848.377 | 46.613 | 0. |
| 28 | 0.6275 | SLE_F4 | Max | -846.128 | -15.849 | 0. |
| 28 | 1.255 | SLE_F4 | Max | -843.878 | -75.698 | 0. |
| 28 | 0. | SLE_F4 | Min | -848.377 | 46.613 | 0. |
| 28 | 0.6275 | SLE_F4 | Min | -846.128 | -15.849 | 0. |
| 28 | 1.255 | SLE_F4 | Min | -843.878 | -75.698 | 0. |
| 28 | 0. | SLE_QP1 | Max | -802.27 | 4.734 | 0. |
| 28 | 0.6275 | SLE_QP1 | Max | -800.021 | -57.728 | 0. |
| 28 | 1.255 | SLE_QP1 | Max | -797.772 | -117.576 | 0. |
| 28 | 0. | SLE_QP1 | Min | -802.27 | 4.734 | 0. |
| 28 | 0.6275 | SLE_QP1 | Min | -800.021 | -57.728 | 0. |
| 28 | 1.255 | SLE_QP1 | Min | -797.772 | -117.576 | 0. |
| 28 | 0. | SLE_QP2 | Max | -732.777 | -3.54 | 0. |
| 28 | 0.6275 | SLE_QP2 | Max | -730.528 | -66.002 | 0. |
| 28 | 1.255 | SLE_QP2 | Max | -728.279 | -125.85 | 0. |
| 28 | 0. | SLE_QP2 | Min | -732.777 | -3.54 | 0. |
| 28 | 0.6275 | SLE_QP2 | Min | -730.528 | -66.002 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 28 | 1.255 | SLE_QP2 | Min | -728.279 | -125.85 | 0. |
| 28 | 0. | SLE_QP3 | Max | -747.775 | 25.344 | 0. |
| 28 | 0.6275 | SLE_QP3 | Max | -745.526 | -37.118 | 0. |
| 28 | 1.255 | SLE_QP3 | Max | -743.276 | -96.967 | 0. |
| 28 | 0. | SLE_QP3 | Min | -747.775 | 25.344 | 0. |
| 28 | 0.6275 | SLE_QP3 | Min | -745.526 | -37.118 | 0. |
| 28 | 1.255 | SLE_QP3 | Min | -743.276 | -96.967 | 0. |
| 28 | 0. | SLE_QP4 | Max | -864.5 | 48.852 | 0. |
| 28 | 0.6275 | SLE_QP4 | Max | -862.251 | -13.61 | 0. |
| 28 | 1.255 | SLE_QP4 | Max | -860.001 | -73.458 | 0. |
| 28 | 0. | SLE_QP4 | Min | -864.5 | 48.852 | 0. |
| 28 | 0.6275 | SLE_QP4 | Min | -862.251 | -13.61 | 0. |
| 28 | 1.255 | SLE_QP4 | Min | -860.001 | -73.458 | 0. |
| 28 | 0. | SLV_1 | Max | -1669.376 | 159.927 | 0. |
| 28 | 0.6275 | SLV_1 | Max | -1667.126 | 97.465 | 0. |
| 28 | 1.255 | SLV_1 | Max | -1664.877 | 37.616 | 0. |
| 28 | 0. | SLV_1 | Min | -1669.376 | 159.927 | 0. |
| 28 | 0.6275 | SLV_1 | Min | -1667.126 | 97.465 | 0. |
| 28 | 1.255 | SLV_1 | Min | -1664.877 | 37.616 | 0. |
| 28 | 0. | SLV_2 | Max | -1670.977 | 159.364 | 0. |
| 28 | 0.6275 | SLV_2 | Max | -1668.727 | 96.902 | 0. |
| 28 | 1.255 | SLV_2 | Max | -1666.478 | 37.054 | 0. |
| 28 | 0. | SLV_2 | Min | -1670.977 | 159.364 | 0. |
| 28 | 0.6275 | SLV_2 | Min | -1668.727 | 96.902 | 0. |
| 28 | 1.255 | SLV_2 | Min | -1666.478 | 37.054 | 0. |
| 28 | 0. | SLV_3 | Max | -1840.434 | 196. | 0. |
| 28 | 0.6275 | SLV_3 | Max | -1838.185 | 133.538 | 0. |
| 28 | 1.255 | SLV_3 | Max | -1835.935 | 73.69 | 0. |
| 28 | 0. | SLV_3 | Min | -1840.434 | 196. | 0. |
| 28 | 0.6275 | SLV_3 | Min | -1838.185 | 133.538 | 0. |
| 28 | 1.255 | SLV_3 | Min | -1835.935 | 73.69 | 0. |
| 28 | 0. | SLV_4 | Max | -1841.762 | 195.778 | 0. |
| 28 | 0.6275 | SLV_4 | Max | -1839.512 | 133.316 | 0. |
| 28 | 1.255 | SLV_4 | Max | -1837.263 | 73.467 | 0. |
| 28 | 0. | SLV_4 | Min | -1841.762 | 195.778 | 0. |
| 28 | 0.6275 | SLV_4 | Min | -1839.512 | 133.316 | 0. |
| 28 | 1.255 | SLV_4 | Min | -1837.263 | 73.467 | 0. |
| 28 | 0. | SLD_1 | Max | -1123.763 | 74.391 | 0. |
| 28 | 0.6275 | SLD_1 | Max | -1121.514 | 11.929 | 0. |
| 28 | 1.255 | SLD_1 | Max | -1119.265 | -47.92 | 0. |
| 28 | 0. | SLD_1 | Min | -1123.763 | 74.391 | 0. |
| 28 | 0.6275 | SLD_1 | Min | -1121.514 | 11.929 | 0. |
| 28 | 1.255 | SLD_1 | Min | -1119.265 | -47.92 | 0. |
| 28 | 0. | SLD_2 | Max | -1124.643 | 73.505 | 0. |
| 28 | 0.6275 | SLD_2 | Max | -1122.393 | 11.043 | 0. |
| 28 | 1.255 | SLD_2 | Max | -1120.144 | -48.805 | 0. |
| 28 | 0. | SLD_2 | Min | -1124.643 | 73.505 | 0. |
| 28 | 0.6275 | SLD_2 | Min | -1122.393 | 11.043 | 0. |
| 28 | 1.255 | SLD_2 | Min | -1120.144 | -48.805 | 0. |
| 28 | 0. | SLD_3 | Max | -1295.485 | 123.605 | 0. |
| 28 | 0.6275 | SLD_3 | Max | -1293.235 | 61.143 | 0. |
| 28 | 1.255 | SLD_3 | Max | -1290.986 | 1.294 | 0. |
| 28 | 0. | SLD_3 | Min | -1295.485 | 123.605 | 0. |
| 28 | 0.6275 | SLD_3 | Min | -1293.235 | 61.143 | 0. |
| 28 | 1.255 | SLD_3 | Min | -1290.986 | 1.294 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 28 | 0. | SLD_4 | Max | -1296.001 | 123.428 | 0. |
| 28 | 0.6275 | SLD_4 | Max | -1293.752 | 60.966 | 0. |
| 28 | 1.255 | SLD_4 | Max | -1291.502 | 1.118 | 0. |
| 28 | 0. | SLD_4 | Min | -1296.001 | 123.428 | 0. |
| 28 | 0.6275 | SLD_4 | Min | -1293.752 | 60.966 | 0. |
| 28 | 1.255 | SLD_4 | Min | -1291.502 | 1.118 | 0. |
| 28 | 0. | SLU_IDR_1 | Max | -820.161 | 17.847 | 0. |
| 28 | 0.6275 | SLU_IDR_1 | Max | -818.136 | -54.598 | 0. |
| 28 | 1.255 | SLU_IDR_1 | Max | -816.112 | -124.168 | 0. |
| 28 | 0. | SLU_IDR_1 | Min | -820.161 | 17.847 | 0. |
| 28 | 0.6275 | SLU_IDR_1 | Min | -818.136 | -54.598 | 0. |
| 28 | 1.255 | SLU_IDR_1 | Min | -816.112 | -124.168 | 0. |
| 28 | 0. | SLU_IDR_2 | Max | -812.956 | -9.232 | 0. |
| 28 | 0.6275 | SLU_IDR_2 | Max | -810.932 | -81.677 | 0. |
| 28 | 1.255 | SLU_IDR_2 | Max | -808.907 | -151.248 | 0. |
| 28 | 0. | SLU_IDR_2 | Min | -812.956 | -9.232 | 0. |
| 28 | 0.6275 | SLU_IDR_2 | Min | -810.932 | -81.677 | 0. |
| 28 | 1.255 | SLU_IDR_2 | Min | -808.907 | -151.248 | 0. |
| 28 | 0. | SISMA WOOD SLV-1 | Max | -891.66 | 128.556 | 0. |
| 28 | 0.6275 | SISMA WOOD SLV-1 | Max | -891.66 | 128.556 | 0. |
| 28 | 1.255 | SISMA WOOD SLV-1 | Max | -891.66 | 128.556 | 0. |
| 28 | 0. | SISMA WOOD SLV-1 | Min | -891.66 | 128.556 | 0. |
| 28 | 0.6275 | SISMA WOOD SLV-1 | Min | -891.66 | 128.556 | 0. |
| 28 | 1.255 | SISMA WOOD SLV-1 | Min | -891.66 | 128.556 | 0. |
| 28 | 0. | DEAD-1 | Max | 17.246 | -14.632 | 0. |
| 28 | 0.6275 | DEAD-1 | Max | 19.496 | 4.053 | 0. |
| 28 | 1.255 | DEAD-1 | Max | 21.745 | 22.737 | 0. |
| 28 | 0. | DEAD-1 | Min | 17.246 | -14.632 | 0. |
| 28 | 0.6275 | DEAD-1 | Min | 19.496 | 4.053 | 0. |
| 28 | 1.255 | DEAD-1 | Min | 21.745 | 22.737 | 0. |
| 28 | 0. | SLU_PROVA | | -1027.641 | 39.033 | 0. |
| 28 | 0.6275 | SLU_PROVA | | -1024.717 | -42.168 | 0. |
| 28 | 1.255 | SLU_PROVA | | -1021.793 | -119.971 | 0. |
| 29 | 0. | DEAD | | 16.794 | -10.069 | 0. |
| 29 | 0.68666 | DEAD | | 19.043 | 10.401 | 0. |
| 29 | 1.37332 | DEAD | | 21.293 | 30.872 | 0. |
| 29 | 0. | SIMM_KA | | -147.415 | -4.5 | 0. |
| 29 | 0.68666 | SIMM_KA | | -147.415 | -4.5 | 0. |
| 29 | 1.37332 | SIMM_KA | | -147.415 | -4.5 | 0. |
| 29 | 0. | SIMM_K0 | | -222.451 | -7.084 | 0. |
| 29 | 0.68666 | SIMM_K0 | | -222.451 | -7.084 | 0. |
| 29 | 1.37332 | SIMM_K0 | | -222.451 | -7.084 | 0. |
| 29 | 0. | A--SIMM_KA | | -179.5 | 8.885 | 0. |
| 29 | 0.68666 | A--SIMM_KA | | -179.5 | 8.885 | 0. |
| 29 | 1.37332 | A--SIMM_KA | | -179.5 | 8.885 | 0. |
| 29 | 0. | A--SIMM_K0 | | -276.754 | 13.236 | 0. |
| 29 | 0.68666 | A--SIMM_K0 | | -276.754 | 13.236 | 0. |
| 29 | 1.37332 | A--SIMM_K0 | | -276.754 | 13.236 | 0. |

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 29 | 0. | A-- SIMM_SOVR_K A | | -8.833 | -1.29 | 0. |
| 29 | 0.68666 | A-- SIMM_SOVR_K A | | -8.833 | -1.29 | 0. |
| 29 | 1.37332 | A-- SIMM_SOVR_K A | | -8.833 | -1.29 | 0. |
| 29 | 0. | A-- SIMM_SOVR_K 0 | | -13.243 | -1.935 | 0. |
| 29 | 0.68666 | A-- SIMM_SOVR_K 0 | | -13.243 | -1.935 | 0. |
| 29 | 1.37332 | A-- SIMM_SOVR_K 0 | | -13.243 | -1.935 | 0. |
| 29 | 0. | SIMM_SOVR_K 0 | | -13.243 | -1.935 | 0. |
| 29 | 0.68666 | SIMM_SOVR_K 0 | | -13.243 | -1.935 | 0. |
| 29 | 1.37332 | SIMM_SOVR_K 0 | | -13.243 | -1.935 | 0. |
| 29 | 0. | SIMM_SOVR_K A | | -8.833 | -1.29 | 0. |
| 29 | 0.68666 | SIMM_SOVR_K A | | -8.833 | -1.29 | 0. |
| 29 | 1.37332 | SIMM_SOVR_K A | | -8.833 | -1.29 | 0. |
| 29 | 0. | SOVR | | 8.277 | -6.43 | 0. |
| 29 | 0.68666 | SOVR | | 8.277 | -6.43 | 0. |
| 29 | 1.37332 | SOVR | | 8.277 | -6.43 | 0. |
| 29 | 0. | TERR_SIMM | | 9.341 | -28.921 | 0. |
| 29 | 0.68666 | TERR_SIMM | | 9.341 | -28.921 | 0. |
| 29 | 1.37332 | TERR_SIMM | | 9.341 | -28.921 | 0. |
| 29 | 0. | TERR_A--SIMM | | 13.303 | -38.073 | 0. |
| 29 | 0.68666 | TERR_A--SIMM | | 13.303 | -38.073 | 0. |
| 29 | 1.37332 | TERR_A--SIMM | | 13.303 | -38.073 | 0. |
| 29 | 0. | INERZIA H SLV | | -2.672 | 0.431 | 0. |
| 29 | 0.68666 | INERZIA H SLV | | -2.672 | 0.431 | 0. |
| 29 | 1.37332 | INERZIA H SLV | | -2.672 | 0.431 | 0. |
| 29 | 0. | INERZIA V + SLV | | 0.287 | 0.17 | 0. |
| 29 | 0.68666 | INERZIA V + SLV | | 0.287 | 0.17 | 0. |
| 29 | 1.37332 | INERZIA V + SLV | | 0.287 | 0.17 | 0. |
| 29 | 0. | INERZIA V - SLV | | -0.287 | -0.17 | 0. |
| 29 | 0.68666 | INERZIA V - SLV | | -0.287 | -0.17 | 0. |
| 29 | 1.37332 | INERZIA V - SLV | | -0.287 | -0.17 | 0. |
| 29 | 0. | SISMA WOOD SLV | | -398.184 | 33.461 | 0. |
| 29 | 0.68666 | SISMA WOOD SLV | | -398.184 | 33.461 | 0. |
| 29 | 1.37332 | SISMA WOOD SLV | | -398.184 | 33.461 | 0. |
| 29 | 0. | iDROSTATICA | | -583.006 | -33.208 | 0. |
| 29 | 0.68666 | iDROSTATICA | | -583.006 | -117.715 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 29 | 1.37332 | iDROSTATICA | | -583.006 | -202.222 | 0. |
| 29 | 0. | SISMA WOOD SLD | | -175.854 | 14.778 | 0. |
| 29 | 0.68666 | SISMA WOOD SLD | | -175.854 | 14.778 | 0. |
| 29 | 1.37332 | SISMA WOOD SLD | | -175.854 | 14.778 | 0. |
| 29 | 0. | INERZIA H SLD | | -1.18 | 0.19 | 0. |
| 29 | 0.68666 | INERZIA H SLD | | -1.18 | 0.19 | 0. |
| 29 | 1.37332 | INERZIA H SLD | | -1.18 | 0.19 | 0. |
| 29 | 0. | INERZIA V + SLD | | 0.127 | 0.075 | 0. |
| 29 | 0.68666 | INERZIA V + SLD | | 0.127 | 0.075 | 0. |
| 29 | 1.37332 | INERZIA V + SLD | | 0.127 | 0.075 | 0. |
| 29 | 0. | INERZIA V SLD | | -0.127 | -0.075 | 0. |
| 29 | 0.68666 | INERZIA V SLD | | -0.127 | -0.075 | 0. |
| 29 | 1.37332 | INERZIA V SLD | | -0.127 | -0.075 | 0. |
| 29 | 0. | INERZIA V -1 | | -0.287 | -0.17 | 0. |
| 29 | 0.68666 | INERZIA V -1 | | -0.287 | -0.17 | 0. |
| 29 | 1.37332 | INERZIA V -1 | | -0.287 | -0.17 | 0. |
| 29 | 0. | SLU_1 | Max | -1026.259 | -163.764 | 0. |
| 29 | 0.68666 | SLU_1 | Max | -1023.335 | -247.011 | 0. |
| 29 | 1.37332 | SLU_1 | Max | -1020.411 | -330.259 | 0. |
| 29 | 0. | SLU_1 | Min | -1026.259 | -163.764 | 0. |
| 29 | 0.68666 | SLU_1 | Min | -1023.335 | -247.011 | 0. |
| 29 | 1.37332 | SLU_1 | Min | -1020.411 | -330.259 | 0. |
| 29 | 0. | SLU_2 | Max | -928.719 | -175.495 | 0. |
| 29 | 0.68666 | SLU_2 | Max | -925.794 | -258.743 | 0. |
| 29 | 1.37332 | SLU_2 | Max | -922.87 | -341.99 | 0. |
| 29 | 0. | SLU_2 | Min | -928.719 | -175.495 | 0. |
| 29 | 0.68666 | SLU_2 | Min | -925.794 | -258.743 | 0. |
| 29 | 1.37332 | SLU_2 | Min | -922.87 | -341.99 | 0. |
| 29 | 0. | SLU_3 | Max | -1085.527 | -111.137 | 0. |
| 29 | 0.68666 | SLU_3 | Max | -1082.603 | -194.385 | 0. |
| 29 | 1.37332 | SLU_3 | Max | -1079.679 | -277.633 | 0. |
| 29 | 0. | SLU_3 | Min | -1085.527 | -111.137 | 0. |
| 29 | 0.68666 | SLU_3 | Min | -1082.603 | -194.385 | 0. |
| 29 | 1.37332 | SLU_3 | Min | -1079.679 | -277.633 | 0. |
| 29 | 0. | SLU_4 | Max | -951.683 | -140.509 | 0. |
| 29 | 0.68666 | SLU_4 | Max | -948.759 | -223.757 | 0. |
| 29 | 1.37332 | SLU_4 | Max | -945.835 | -307.004 | 0. |
| 29 | 0. | SLU_4 | Min | -951.683 | -140.509 | 0. |
| 29 | 0.68666 | SLU_4 | Min | -948.759 | -223.757 | 0. |
| 29 | 1.37332 | SLU_4 | Min | -945.835 | -307.004 | 0. |
| 29 | 0. | SLE_F1 | Max | -791.396 | -126.567 | 0. |
| 29 | 0.68666 | SLE_F1 | Max | -789.146 | -190.603 | 0. |
| 29 | 1.37332 | SLE_F1 | Max | -786.897 | -254.64 | 0. |
| 29 | 0. | SLE_F1 | Min | -791.396 | -126.567 | 0. |
| 29 | 0.68666 | SLE_F1 | Min | -789.146 | -190.603 | 0. |
| 29 | 1.37332 | SLE_F1 | Min | -786.897 | -254.64 | 0. |
| 29 | 0. | SLE_F2 | Max | -718.785 | -134.432 | 0. |
| 29 | 0.68666 | SLE_F2 | Max | -716.536 | -198.469 | 0. |
| 29 | 1.37332 | SLE_F2 | Max | -714.287 | -262.506 | 0. |
| 29 | 0. | SLE_F2 | Min | -718.785 | -134.432 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 29 | 0.68666 | SLE_F2 | Min | -716.536 | -198.469 | 0. |
| 29 | 1.37332 | SLE_F2 | Min | -714.287 | -262.506 | 0. |
| 29 | 0. | SLE_F3 | Max | -735.623 | -106.885 | 0. |
| 29 | 0.68666 | SLE_F3 | Max | -733.373 | -170.922 | 0. |
| 29 | 1.37332 | SLE_F3 | Max | -731.124 | -234.959 | 0. |
| 29 | 0. | SLE_F3 | Min | -735.623 | -106.885 | 0. |
| 29 | 0.68666 | SLE_F3 | Min | -733.373 | -170.922 | 0. |
| 29 | 1.37332 | SLE_F3 | Min | -731.124 | -234.959 | 0. |
| 29 | 0. | SLE_F4 | Max | -843.048 | -84.438 | 0. |
| 29 | 0.68666 | SLE_F4 | Max | -840.799 | -148.475 | 0. |
| 29 | 1.37332 | SLE_F4 | Max | -838.55 | -212.512 | 0. |
| 29 | 0. | SLE_F4 | Min | -843.048 | -84.438 | 0. |
| 29 | 0.68666 | SLE_F4 | Min | -840.799 | -148.475 | 0. |
| 29 | 1.37332 | SLE_F4 | Min | -838.55 | -212.512 | 0. |
| 29 | 0. | SLE_QP1 | Max | -796.51 | -125.822 | 0. |
| 29 | 0.68666 | SLE_QP1 | Max | -794.261 | -189.859 | 0. |
| 29 | 1.37332 | SLE_QP1 | Max | -792.011 | -253.896 | 0. |
| 29 | 0. | SLE_QP1 | Min | -796.51 | -125.822 | 0. |
| 29 | 0.68666 | SLE_QP1 | Min | -794.261 | -189.859 | 0. |
| 29 | 1.37332 | SLE_QP1 | Min | -792.011 | -253.896 | 0. |
| 29 | 0. | SLE_QP2 | Max | -726.935 | -133.384 | 0. |
| 29 | 0.68666 | SLE_QP2 | Max | -724.686 | -197.421 | 0. |
| 29 | 1.37332 | SLE_QP2 | Max | -722.436 | -261.458 | 0. |
| 29 | 0. | SLE_QP2 | Min | -726.935 | -133.384 | 0. |
| 29 | 0.68666 | SLE_QP2 | Min | -724.686 | -197.421 | 0. |
| 29 | 1.37332 | SLE_QP2 | Min | -722.436 | -261.458 | 0. |
| 29 | 0. | SLE_QP3 | Max | -742.231 | -104.66 | 0. |
| 29 | 0.68666 | SLE_QP3 | Max | -739.982 | -168.696 | 0. |
| 29 | 1.37332 | SLE_QP3 | Max | -737.733 | -232.733 | 0. |
| 29 | 0. | SLE_QP3 | Min | -742.231 | -104.66 | 0. |
| 29 | 0.68666 | SLE_QP3 | Min | -739.982 | -168.696 | 0. |
| 29 | 1.37332 | SLE_QP3 | Min | -737.733 | -232.733 | 0. |
| 29 | 0. | SLE_QP4 | Max | -859.194 | -82.365 | 0. |
| 29 | 0.68666 | SLE_QP4 | Max | -856.944 | -146.402 | 0. |
| 29 | 1.37332 | SLE_QP4 | Max | -854.695 | -210.438 | 0. |
| 29 | 0. | SLE_QP4 | Min | -859.194 | -82.365 | 0. |
| 29 | 0.68666 | SLE_QP4 | Min | -856.944 | -146.402 | 0. |
| 29 | 1.37332 | SLE_QP4 | Min | -854.695 | -210.438 | 0. |
| 29 | 0. | SLV_1 | Max | -1666.17 | -18.999 | 0. |
| 29 | 0.68666 | SLV_1 | Max | -1663.921 | -83.036 | 0. |
| 29 | 1.37332 | SLV_1 | Max | -1661.671 | -147.072 | 0. |
| 29 | 0. | SLV_1 | Min | -1666.17 | -18.999 | 0. |
| 29 | 0.68666 | SLV_1 | Min | -1663.921 | -83.036 | 0. |
| 29 | 1.37332 | SLV_1 | Min | -1661.671 | -147.072 | 0. |
| 29 | 0. | SLV_2 | Max | -1667.91 | -19.698 | 0. |
| 29 | 0.68666 | SLV_2 | Max | -1665.661 | -83.735 | 0. |
| 29 | 1.37332 | SLV_2 | Max | -1663.412 | -147.771 | 0. |
| 29 | 0. | SLV_2 | Min | -1667.91 | -19.698 | 0. |
| 29 | 0.68666 | SLV_2 | Min | -1665.661 | -83.735 | 0. |
| 29 | 1.37332 | SLV_2 | Min | -1663.412 | -147.771 | 0. |
| 29 | 0. | SLV_3 | Max | -1837.524 | 1.627 | 0. |
| 29 | 0.68666 | SLV_3 | Max | -1835.275 | -62.409 | 0. |
| 29 | 1.37332 | SLV_3 | Max | -1833.025 | -126.446 | 0. |
| 29 | 0. | SLV_3 | Min | -1837.524 | 1.627 | 0. |
| 29 | 0.68666 | SLV_3 | Min | -1835.275 | -62.409 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 29 | 1.37332 | SLV_3 | Min | -1833.025 | -126.446 | 0. |
| 29 | 0. | SLV_4 | Max | -1838.994 | 1.184 | 0. |
| 29 | 0.68666 | SLV_4 | Max | -1836.745 | -62.852 | 0. |
| 29 | 1.37332 | SLV_4 | Max | -1834.495 | -126.889 | 0. |
| 29 | 0. | SLV_4 | Min | -1838.994 | 1.184 | 0. |
| 29 | 0.68666 | SLV_4 | Min | -1836.745 | -62.852 | 0. |
| 29 | 1.37332 | SLV_4 | Min | -1834.495 | -126.889 | 0. |
| 29 | 0. | SLD_1 | Max | -1119.225 | -60.983 | 0. |
| 29 | 0.68666 | SLD_1 | Max | -1116.976 | -125.02 | 0. |
| 29 | 1.37332 | SLD_1 | Max | -1114.727 | -189.056 | 0. |
| 29 | 0. | SLD_1 | Min | -1119.225 | -60.983 | 0. |
| 29 | 0.68666 | SLD_1 | Min | -1116.976 | -125.02 | 0. |
| 29 | 1.37332 | SLD_1 | Min | -1114.727 | -189.056 | 0. |
| 29 | 0. | SLD_2 | Max | -1120.16 | -61.781 | 0. |
| 29 | 0.68666 | SLD_2 | Max | -1117.911 | -125.817 | 0. |
| 29 | 1.37332 | SLD_2 | Max | -1115.661 | -189.854 | 0. |
| 29 | 0. | SLD_2 | Min | -1120.16 | -61.781 | 0. |
| 29 | 0.68666 | SLD_2 | Min | -1117.911 | -125.817 | 0. |
| 29 | 1.37332 | SLD_2 | Min | -1115.661 | -189.854 | 0. |
| 29 | 0. | SLD_3 | Max | -1291.364 | -30.132 | 0. |
| 29 | 0.68666 | SLD_3 | Max | -1289.115 | -94.169 | 0. |
| 29 | 1.37332 | SLD_3 | Max | -1286.865 | -158.205 | 0. |
| 29 | 0. | SLD_3 | Min | -1291.364 | -30.132 | 0. |
| 29 | 0.68666 | SLD_3 | Min | -1289.115 | -94.169 | 0. |
| 29 | 1.37332 | SLD_3 | Min | -1286.865 | -158.205 | 0. |
| 29 | 0. | SLD_4 | Max | -1291.943 | -30.385 | 0. |
| 29 | 0.68666 | SLD_4 | Max | -1289.693 | -94.421 | 0. |
| 29 | 1.37332 | SLD_4 | Max | -1287.444 | -158.458 | 0. |
| 29 | 0. | SLD_4 | Min | -1291.943 | -30.385 | 0. |
| 29 | 0.68666 | SLD_4 | Min | -1289.693 | -94.421 | 0. |
| 29 | 1.37332 | SLD_4 | Min | -1287.444 | -158.458 | 0. |
| 29 | 0. | SLU_IDR_1 | Max | -814.781 | -132.608 | 0. |
| 29 | 0.68666 | SLU_IDR_1 | Max | -812.757 | -207.143 | 0. |
| 29 | 1.37332 | SLU_IDR_1 | Max | -810.732 | -281.677 | 0. |
| 29 | 0. | SLU_IDR_1 | Min | -814.781 | -132.608 | 0. |
| 29 | 0.68666 | SLU_IDR_1 | Min | -812.757 | -207.143 | 0. |
| 29 | 1.37332 | SLU_IDR_1 | Min | -810.732 | -281.677 | 0. |
| 29 | 0. | SLU_IDR_2 | Max | -807.296 | -159.61 | 0. |
| 29 | 0.68666 | SLU_IDR_2 | Max | -805.272 | -234.144 | 0. |
| 29 | 1.37332 | SLU_IDR_2 | Max | -803.247 | -308.678 | 0. |
| 29 | 0. | SLU_IDR_2 | Min | -807.296 | -159.61 | 0. |
| 29 | 0.68666 | SLU_IDR_2 | Min | -805.272 | -234.144 | 0. |
| 29 | 1.37332 | SLU_IDR_2 | Min | -803.247 | -308.678 | 0. |
| 29 | 0. | SISMA WOOD SLV-1 | Max | -892.828 | 96.825 | 0. |
| 29 | 0.68666 | SISMA WOOD SLV-1 | Max | -892.828 | 96.825 | 0. |
| 29 | 1.37332 | SISMA WOOD SLV-1 | Max | -892.828 | 96.825 | 0. |
| 29 | 0. | SISMA WOOD SLV-1 | Min | -892.828 | 96.825 | 0. |
| 29 | 0.68666 | SISMA WOOD SLV-1 | Min | -892.828 | 96.825 | 0. |
| 29 | 1.37332 | SISMA WOOD SLV-1 | Min | -892.828 | 96.825 | 0. |
| 29 | 0. | DEAD-1 | Max | 21.681 | -11.881 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 29 | 0.68666 | DEAD-1 | Max | 23.93 | 8.59 | 0. |
| 29 | 1.37332 | DEAD-1 | Max | 26.179 | 29.06 | 0. |
| 29 | 0. | DEAD-1 | Min | 21.681 | -11.881 | 0. |
| 29 | 0.68666 | DEAD-1 | Min | 23.93 | 8.59 | 0. |
| 29 | 1.37332 | DEAD-1 | Min | 26.179 | 29.06 | 0. |
| 29 | 0. | SLU_PROVA | | -1020.569 | -115.614 | 0. |
| 29 | 0.68666 | SLU_PROVA | | -1017.644 | -198.862 | 0. |
| 29 | 1.37332 | SLU_PROVA | | -1014.72 | -282.109 | 0. |
| 30 | 0. | DEAD | | 21.748 | -5.828 | 0. |
| 30 | 0.68801 | DEAD | | 24.747 | 14.587 | 0. |
| 30 | 1.37601 | DEAD | | 27.746 | 35.002 | 0. |
| 30 | 0. | SIMM_KA | | -147.629 | -7.263 | 0. |
| 30 | 0.68801 | SIMM_KA | | -147.629 | -7.263 | 0. |
| 30 | 1.37601 | SIMM_KA | | -147.629 | -7.263 | 0. |
| 30 | 0. | SIMM_K0 | | -222.788 | -11.387 | 0. |
| 30 | 0.68801 | SIMM_K0 | | -222.788 | -11.387 | 0. |
| 30 | 1.37601 | SIMM_K0 | | -222.788 | -11.387 | 0. |
| 30 | 0. | A--SIMM_KA | | -179.251 | 4.534 | 0. |
| 30 | 0.68801 | A--SIMM_KA | | -179.251 | 4.534 | 0. |
| 30 | 1.37601 | A--SIMM_KA | | -179.251 | 4.534 | 0. |
| 30 | 0. | A--SIMM_K0 | | -276.384 | 6.773 | 0. |
| 30 | 0.68801 | A--SIMM_K0 | | -276.384 | 6.773 | 0. |
| 30 | 1.37601 | A--SIMM_K0 | | -276.384 | 6.773 | 0. |
| 30 | 0. | A-- SIMM_SOVR_K A | | -8.892 | -1.901 | 0. |
| 30 | 0.68801 | A-- SIMM_SOVR_K A | | -8.892 | -1.901 | 0. |
| 30 | 1.37601 | A-- SIMM_SOVR_K A | | -8.892 | -1.901 | 0. |
| 30 | 0. | A-- SIMM_SOVR_K 0 | | -13.331 | -2.851 | 0. |
| 30 | 0.68801 | A-- SIMM_SOVR_K 0 | | -13.331 | -2.851 | 0. |
| 30 | 1.37601 | A-- SIMM_SOVR_K 0 | | -13.331 | -2.851 | 0. |
| 30 | 0. | SIMM_SOVR_K 0 | | -13.331 | -2.851 | 0. |
| 30 | 0.68801 | SIMM_SOVR_K 0 | | -13.331 | -2.851 | 0. |
| 30 | 1.37601 | SIMM_SOVR_K 0 | | -13.331 | -2.851 | 0. |
| 30 | 0. | SIMM_SOVR_K A | | -8.892 | -1.901 | 0. |
| 30 | 0.68801 | SIMM_SOVR_K A | | -8.892 | -1.901 | 0. |
| 30 | 1.37601 | SIMM_SOVR_K A | | -8.892 | -1.901 | 0. |
| 30 | 0. | SOVR | | 7.943 | -11.876 | 0. |
| 30 | 0.68801 | SOVR | | 7.943 | -11.876 | 0. |
| 30 | 1.37601 | SOVR | | 7.943 | -11.876 | 0. |
| 30 | 0. | TERR_SIMM | | 7.864 | -52.195 | 0. |
| 30 | 0.68801 | TERR_SIMM | | 7.864 | -52.195 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 30 | 1.37601 | TERR_SIMM | | 7.864 | -52.195 | 0. |
| 30 | 0. | TERR_A--SIMM | | 11.515 | -60.202 | 0. |
| 30 | 0.68801 | TERR_A--SIMM | | 11.515 | -60.202 | 0. |
| 30 | 1.37601 | TERR_A--SIMM | | 11.515 | -60.202 | 0. |
| 30 | 0. | INERZIA H SLV | | -3.979 | 0.35 | 0. |
| 30 | 0.68801 | INERZIA H SLV | | -3.979 | 0.35 | 0. |
| 30 | 1.37601 | INERZIA H SLV | | -3.979 | 0.35 | 0. |
| 30 | 0. | INERZIA V + SLV | | 0.38 | 0.238 | 0. |
| 30 | 0.68801 | INERZIA V + SLV | | 0.38 | 0.238 | 0. |
| 30 | 1.37601 | INERZIA V + SLV | | 0.38 | 0.238 | 0. |
| 30 | 0. | INERZIA V - SLV | | -0.38 | -0.238 | 0. |
| 30 | 0.68801 | INERZIA V - SLV | | -0.38 | -0.238 | 0. |
| 30 | 1.37601 | INERZIA V - SLV | | -0.38 | -0.238 | 0. |
| 30 | 0. | SISMA WOOD SLV | | -397.069 | 26.049 | 0. |
| 30 | 0.68801 | SISMA WOOD SLV | | -397.069 | 26.049 | 0. |
| 30 | 1.37601 | SISMA WOOD SLV | | -397.069 | 26.049 | 0. |
| 30 | 0. | iDROSTATICA | | -588.663 | -108.502 | 0. |
| 30 | 0.68801 | iDROSTATICA | | -588.663 | -193.175 | 0. |
| 30 | 1.37601 | iDROSTATICA | | -588.663 | -277.848 | 0. |
| 30 | 0. | SISMA WOOD SLD | | -175.362 | 11.504 | 0. |
| 30 | 0.68801 | SISMA WOOD SLD | | -175.362 | 11.504 | 0. |
| 30 | 1.37601 | SISMA WOOD SLD | | -175.362 | 11.504 | 0. |
| 30 | 0. | INERZIA H SLD | | -1.757 | 0.155 | 0. |
| 30 | 0.68801 | INERZIA H SLD | | -1.757 | 0.155 | 0. |
| 30 | 1.37601 | INERZIA H SLD | | -1.757 | 0.155 | 0. |
| 30 | 0. | INERZIA V + SLD | | 0.168 | 0.105 | 0. |
| 30 | 0.68801 | INERZIA V + SLD | | 0.168 | 0.105 | 0. |
| 30 | 1.37601 | INERZIA V + SLD | | 0.168 | 0.105 | 0. |
| 30 | 0. | INERZIA V SLD | | -0.168 | -0.105 | 0. |
| 30 | 0.68801 | INERZIA V SLD | | -0.168 | -0.105 | 0. |
| 30 | 1.37601 | INERZIA V SLD | | -0.168 | -0.105 | 0. |
| 30 | 0. | INERZIA V -1 | | -0.38 | -0.238 | 0. |
| 30 | 0.68801 | INERZIA V -1 | | -0.38 | -0.238 | 0. |
| 30 | 1.37601 | INERZIA V -1 | | -0.38 | -0.238 | 0. |
| 30 | 0. | SLU_1 | Max | -1031.844 | -297.511 | 0. |
| 30 | 0.68801 | SLU_1 | Max | -1027.945 | -381.046 | 0. |
| 30 | 1.37601 | SLU_1 | Max | -1024.046 | -464.581 | 0. |
| 30 | 0. | SLU_1 | Min | -1031.844 | -297.511 | 0. |
| 30 | 0.68801 | SLU_1 | Min | -1027.945 | -381.046 | 0. |
| 30 | 1.37601 | SLU_1 | Min | -1024.046 | -464.581 | 0. |
| 30 | 0. | SLU_2 | Max | -934.711 | -308.157 | 0. |
| 30 | 0.68801 | SLU_2 | Max | -930.812 | -391.692 | 0. |
| 30 | 1.37601 | SLU_2 | Max | -926.913 | -475.228 | 0. |
| 30 | 0. | SLU_2 | Min | -934.711 | -308.157 | 0. |
| 30 | 0.68801 | SLU_2 | Min | -930.812 | -391.692 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 30 | 1.37601 | SLU_2 | Min | -926.913 | -475.228 | 0. |
| 30 | 0. | SLU_3 | Max | -1089.258 | -248.998 | 0. |
| 30 | 0.68801 | SLU_3 | Max | -1085.359 | -332.534 | 0. |
| 30 | 1.37601 | SLU_3 | Max | -1081.46 | -416.069 | 0. |
| 30 | 0. | SLU_3 | Min | -1089.258 | -248.998 | 0. |
| 30 | 0.68801 | SLU_3 | Min | -1085.359 | -332.534 | 0. |
| 30 | 1.37601 | SLU_3 | Min | -1081.46 | -416.069 | 0. |
| 30 | 0. | SLU_4 | Max | -956.387 | -272.358 | 0. |
| 30 | 0.68801 | SLU_4 | Max | -952.488 | -355.894 | 0. |
| 30 | 1.37601 | SLU_4 | Max | -948.589 | -439.429 | 0. |
| 30 | 0. | SLU_4 | Min | -956.387 | -272.358 | 0. |
| 30 | 0.68801 | SLU_4 | Min | -952.488 | -355.894 | 0. |
| 30 | 1.37601 | SLU_4 | Min | -948.589 | -439.429 | 0. |
| 30 | 0. | SLE_F1 | Max | -795.647 | -225.817 | 0. |
| 30 | 0.68801 | SLE_F1 | Max | -792.648 | -290.075 | 0. |
| 30 | 1.37601 | SLE_F1 | Max | -789.649 | -354.333 | 0. |
| 30 | 0. | SLE_F1 | Min | -795.647 | -225.817 | 0. |
| 30 | 0.68801 | SLE_F1 | Min | -792.648 | -290.075 | 0. |
| 30 | 1.37601 | SLE_F1 | Min | -789.649 | -354.333 | 0. |
| 30 | 0. | SLE_F2 | Max | -723.371 | -236.318 | 0. |
| 30 | 0.68801 | SLE_F2 | Max | -720.372 | -300.576 | 0. |
| 30 | 1.37601 | SLE_F2 | Max | -717.373 | -364.834 | 0. |
| 30 | 0. | SLE_F2 | Min | -723.371 | -236.318 | 0. |
| 30 | 0.68801 | SLE_F2 | Min | -720.372 | -300.576 | 0. |
| 30 | 1.37601 | SLE_F2 | Min | -717.373 | -364.834 | 0. |
| 30 | 0. | SLE_F3 | Max | -739.195 | -208.178 | 0. |
| 30 | 0.68801 | SLE_F3 | Max | -736.196 | -272.436 | 0. |
| 30 | 1.37601 | SLE_F3 | Max | -733.196 | -336.694 | 0. |
| 30 | 0. | SLE_F3 | Min | -739.195 | -208.178 | 0. |
| 30 | 0.68801 | SLE_F3 | Min | -736.196 | -272.436 | 0. |
| 30 | 1.37601 | SLE_F3 | Min | -733.196 | -336.694 | 0. |
| 30 | 0. | SLE_F4 | Max | -845.821 | -187.281 | 0. |
| 30 | 0.68801 | SLE_F4 | Max | -842.821 | -251.539 | 0. |
| 30 | 1.37601 | SLE_F4 | Max | -839.822 | -315.797 | 0. |
| 30 | 0. | SLE_F4 | Min | -845.821 | -187.281 | 0. |
| 30 | 0.68801 | SLE_F4 | Min | -842.821 | -251.539 | 0. |
| 30 | 1.37601 | SLE_F4 | Min | -839.822 | -315.797 | 0. |
| 30 | 0. | SLE_QP1 | Max | -800.731 | -224.886 | 0. |
| 30 | 0.68801 | SLE_QP1 | Max | -797.732 | -289.144 | 0. |
| 30 | 1.37601 | SLE_QP1 | Max | -794.733 | -353.402 | 0. |
| 30 | 0. | SLE_QP1 | Min | -800.731 | -224.886 | 0. |
| 30 | 0.68801 | SLE_QP1 | Min | -797.732 | -289.144 | 0. |
| 30 | 1.37601 | SLE_QP1 | Min | -794.733 | -353.402 | 0. |
| 30 | 0. | SLE_QP2 | Max | -731.478 | -234.973 | 0. |
| 30 | 0.68801 | SLE_QP2 | Max | -728.478 | -299.231 | 0. |
| 30 | 1.37601 | SLE_QP2 | Max | -725.479 | -363.489 | 0. |
| 30 | 0. | SLE_QP2 | Min | -731.478 | -234.973 | 0. |
| 30 | 0.68801 | SLE_QP2 | Min | -728.478 | -299.231 | 0. |
| 30 | 1.37601 | SLE_QP2 | Min | -725.479 | -363.489 | 0. |
| 30 | 0. | SLE_QP3 | Max | -745.718 | -205.711 | 0. |
| 30 | 0.68801 | SLE_QP3 | Max | -742.719 | -269.969 | 0. |
| 30 | 1.37601 | SLE_QP3 | Max | -739.72 | -334.227 | 0. |
| 30 | 0. | SLE_QP3 | Min | -745.718 | -205.711 | 0. |
| 30 | 0.68801 | SLE_QP3 | Min | -742.719 | -269.969 | 0. |
| 30 | 1.37601 | SLE_QP3 | Min | -739.72 | -334.227 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 30 | 0. | SLE_QP4 | Max | -861.791 | -179.559 | 0. |
| 30 | 0.68801 | SLE_QP4 | Max | -858.792 | -243.817 | 0. |
| 30 | 1.37601 | SLE_QP4 | Max | -855.793 | -308.075 | 0. |
| 30 | 0. | SLE_QP4 | Min | -861.791 | -179.559 | 0. |
| 30 | 0.68801 | SLE_QP4 | Min | -858.792 | -243.817 | 0. |
| 30 | 1.37601 | SLE_QP4 | Min | -855.793 | -308.075 | 0. |
| 30 | 0. | SLV_1 | Max | -1668.062 | -139.806 | 0. |
| 30 | 0.68801 | SLV_1 | Max | -1665.063 | -204.064 | 0. |
| 30 | 1.37601 | SLV_1 | Max | -1662.064 | -268.322 | 0. |
| 30 | 0. | SLV_1 | Min | -1668.062 | -139.806 | 0. |
| 30 | 0.68801 | SLV_1 | Min | -1665.063 | -204.064 | 0. |
| 30 | 1.37601 | SLV_1 | Min | -1662.064 | -268.322 | 0. |
| 30 | 0. | SLV_2 | Max | -1669.999 | -140.578 | 0. |
| 30 | 0.68801 | SLV_2 | Max | -1667. | -204.836 | 0. |
| 30 | 1.37601 | SLV_2 | Max | -1664.001 | -269.094 | 0. |
| 30 | 0. | SLV_2 | Min | -1669.999 | -140.578 | 0. |
| 30 | 0.68801 | SLV_2 | Min | -1667. | -204.836 | 0. |
| 30 | 1.37601 | SLV_2 | Min | -1664.001 | -269.094 | 0. |
| 30 | 0. | SLV_3 | Max | -1838.742 | -124.386 | 0. |
| 30 | 0.68801 | SLV_3 | Max | -1835.743 | -188.644 | 0. |
| 30 | 1.37601 | SLV_3 | Max | -1832.744 | -252.901 | 0. |
| 30 | 0. | SLV_3 | Min | -1838.742 | -124.386 | 0. |
| 30 | 0.68801 | SLV_3 | Min | -1835.743 | -188.644 | 0. |
| 30 | 1.37601 | SLV_3 | Min | -1832.744 | -252.901 | 0. |
| 30 | 0. | SLV_4 | Max | -1840.4 | -124.971 | 0. |
| 30 | 0.68801 | SLV_4 | Max | -1837.401 | -189.229 | 0. |
| 30 | 1.37601 | SLV_4 | Max | -1834.402 | -253.487 | 0. |
| 30 | 0. | SLV_4 | Min | -1840.4 | -124.971 | 0. |
| 30 | 0.68801 | SLV_4 | Min | -1837.401 | -189.229 | 0. |
| 30 | 1.37601 | SLV_4 | Min | -1834.402 | -253.487 | 0. |
| 30 | 0. | SLD_1 | Max | -1121.711 | -165.981 | 0. |
| 30 | 0.68801 | SLD_1 | Max | -1118.712 | -230.239 | 0. |
| 30 | 1.37601 | SLD_1 | Max | -1115.713 | -294.497 | 0. |
| 30 | 0. | SLD_1 | Min | -1121.711 | -165.981 | 0. |
| 30 | 0.68801 | SLD_1 | Min | -1118.712 | -230.239 | 0. |
| 30 | 1.37601 | SLD_1 | Min | -1115.713 | -294.497 | 0. |
| 30 | 0. | SLD_2 | Max | -1122.748 | -166.675 | 0. |
| 30 | 0.68801 | SLD_2 | Max | -1119.749 | -230.933 | 0. |
| 30 | 1.37601 | SLD_2 | Max | -1116.75 | -295.191 | 0. |
| 30 | 0. | SLD_2 | Min | -1122.748 | -166.675 | 0. |
| 30 | 0.68801 | SLD_2 | Min | -1119.749 | -230.933 | 0. |
| 30 | 1.37601 | SLD_2 | Min | -1116.75 | -295.191 | 0. |
| 30 | 0. | SLD_3 | Max | -1292.843 | -142.553 | 0. |
| 30 | 0.68801 | SLD_3 | Max | -1289.844 | -206.81 | 0. |
| 30 | 1.37601 | SLD_3 | Max | -1286.845 | -271.068 | 0. |
| 30 | 0. | SLD_3 | Min | -1292.843 | -142.553 | 0. |
| 30 | 0.68801 | SLD_3 | Min | -1289.844 | -206.81 | 0. |
| 30 | 1.37601 | SLD_3 | Min | -1286.845 | -271.068 | 0. |
| 30 | 0. | SLD_4 | Max | -1293.507 | -142.85 | 0. |
| 30 | 0.68801 | SLD_4 | Max | -1290.508 | -207.108 | 0. |
| 30 | 1.37601 | SLD_4 | Max | -1287.508 | -271.366 | 0. |
| 30 | 0. | SLD_4 | Min | -1293.507 | -142.85 | 0. |
| 30 | 0.68801 | SLD_4 | Min | -1290.508 | -207.108 | 0. |
| 30 | 1.37601 | SLD_4 | Min | -1287.508 | -271.366 | 0. |
| 30 | 0. | SLU_IDR_1 | Max | -820.451 | -251.959 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 30 | 0.68801 | SLU_IDR_1 | Max | -817.752 | -326.726 | 0. |
| 30 | 1.37601 | SLU_IDR_1 | Max | -815.053 | -401.492 | 0. |
| 30 | 0. | SLU_IDR_1 | Min | -820.451 | -251.959 | 0. |
| 30 | 0.68801 | SLU_IDR_1 | Min | -817.752 | -326.726 | 0. |
| 30 | 1.37601 | SLU_IDR_1 | Min | -815.053 | -401.492 | 0. |
| 30 | 0. | SLU_IDR_2 | Max | -813.954 | -279.214 | 0. |
| 30 | 0.68801 | SLU_IDR_2 | Max | -811.255 | -353.98 | 0. |
| 30 | 1.37601 | SLU_IDR_2 | Max | -808.556 | -428.747 | 0. |
| 30 | 0. | SLU_IDR_2 | Min | -813.954 | -279.214 | 0. |
| 30 | 0.68801 | SLU_IDR_2 | Min | -811.255 | -353.98 | 0. |
| 30 | 1.37601 | SLU_IDR_2 | Min | -808.556 | -428.747 | 0. |
| 30 | 0. | SISMA WOOD SLV-1 | Max | -889.243 | 96.365 | 0. |
| 30 | 0.68801 | SISMA WOOD SLV-1 | Max | -889.243 | 96.365 | 0. |
| 30 | 1.37601 | SISMA WOOD SLV-1 | Max | -889.243 | 96.365 | 0. |
| 30 | 0. | SISMA WOOD SLV-1 | Min | -889.243 | 96.365 | 0. |
| 30 | 0.68801 | SISMA WOOD SLV-1 | Min | -889.243 | 96.365 | 0. |
| 30 | 1.37601 | SISMA WOOD SLV-1 | Min | -889.243 | 96.365 | 0. |
| 30 | 0. | DEAD-1 | Max | 26.538 | -9.298 | 0. |
| 30 | 0.68801 | DEAD-1 | Max | 29.537 | 11.117 | 0. |
| 30 | 1.37601 | DEAD-1 | Max | 32.536 | 31.532 | 0. |
| 30 | 0. | DEAD-1 | Min | 26.538 | -9.298 | 0. |
| 30 | 0.68801 | DEAD-1 | Min | 29.537 | 11.117 | 0. |
| 30 | 1.37601 | DEAD-1 | Min | 32.536 | 31.532 | 0. |
| 30 | 0. | SLU_PROVA | | -1024.473 | -253.375 | 0. |
| 30 | 0.68801 | SLU_PROVA | | -1020.574 | -336.911 | 0. |
| 30 | 1.37601 | SLU_PROVA | | -1016.676 | -420.446 | 0. |
| 31 | 0. | DEAD | | 29.216 | -10.457 | 0. |
| 31 | 0.94153 | DEAD | | 35.964 | 16.963 | 0. |
| 31 | 1.88306 | DEAD | | 42.712 | 44.382 | 0. |
| 31 | 0. | SIMM_KA | | -147.929 | 0.045 | 0. |
| 31 | 0.94153 | SIMM_KA | | -147.929 | 0.045 | 0. |
| 31 | 1.88306 | SIMM_KA | | -147.929 | 0.045 | 0. |
| 31 | 0. | SIMM_K0 | | -223.286 | -0.484 | 0. |
| 31 | 0.94153 | SIMM_K0 | | -223.286 | -0.484 | 0. |
| 31 | 1.88306 | SIMM_K0 | | -223.286 | -0.484 | 0. |
| 31 | 0. | A--SIMM_KA | | -178.421 | 10.488 | 0. |
| 31 | 0.94153 | A--SIMM_KA | | -178.421 | 10.488 | 0. |
| 31 | 1.88306 | A--SIMM_KA | | -178.421 | 10.488 | 0. |
| 31 | 0. | A--SIMM_K0 | | -275.112 | 16.384 | 0. |
| 31 | 0.94153 | A--SIMM_K0 | | -275.112 | 16.384 | 0. |
| 31 | 1.88306 | A--SIMM_K0 | | -275.112 | 16.384 | 0. |
| 31 | 0. | A-- SIMM_SOVR_K A | | -9.066 | -1.878 | 0. |
| 31 | 0.94153 | A-- SIMM_SOVR_K A | | -9.066 | -1.878 | 0. |
| 31 | 1.88306 | A-- SIMM_SOVR_K A | | -9.066 | -1.878 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 31 | 0. | A-- SIMM_SOVR_K 0 | | -13.593 | -2.816 | 0. |
| 31 | 0.94153 | A-- SIMM_SOVR_K 0 | | -13.593 | -2.816 | 0. |
| 31 | 1.88306 | A-- SIMM_SOVR_K 0 | | -13.593 | -2.816 | 0. |
| 31 | 0. | SIMM_SOVR_K 0 | | -13.593 | -2.816 | 0. |
| 31 | 0.94153 | SIMM_SOVR_K 0 | | -13.593 | -2.816 | 0. |
| 31 | 1.88306 | SIMM_SOVR_K 0 | | -13.593 | -2.816 | 0. |
| 31 | 0. | SIMM_SOVR_K A | | -9.066 | -1.878 | 0. |
| 31 | 0.94153 | SIMM_SOVR_K A | | -9.066 | -1.878 | 0. |
| 31 | 1.88306 | SIMM_SOVR_K A | | -9.066 | -1.878 | 0. |
| 31 | 0. | SOVR | | 6.404 | -21.715 | 0. |
| 31 | 0.94153 | SOVR | | 6.404 | -21.715 | 0. |
| 31 | 1.88306 | SOVR | | 6.404 | -21.715 | 0. |
| 31 | 0. | TERR_SIMM | | 1.287 | -91.274 | 0. |
| 31 | 0.94153 | TERR_SIMM | | 1.287 | -91.274 | 0. |
| 31 | 1.88306 | TERR_SIMM | | 1.287 | -91.274 | 0. |
| 31 | 0. | TERR_A--SIMM | | 4.244 | -97.808 | 0. |
| 31 | 0.94153 | TERR_A--SIMM | | 4.244 | -97.808 | 0. |
| 31 | 1.88306 | TERR_A--SIMM | | 4.244 | -97.808 | 0. |
| 31 | 0. | INERZIA H SLV | | -5.484 | 0.384 | 0. |
| 31 | 0.94153 | INERZIA H SLV | | -5.484 | 0.384 | 0. |
| 31 | 1.88306 | INERZIA H SLV | | -5.484 | 0.384 | 0. |
| 31 | 0. | INERZIA V + SLV | | 0.561 | 0.279 | 0. |
| 31 | 0.94153 | INERZIA V + SLV | | 0.561 | 0.279 | 0. |
| 31 | 1.88306 | INERZIA V + SLV | | 0.561 | 0.279 | 0. |
| 31 | 0. | INERZIA V - SLV | | -0.561 | -0.279 | 0. |
| 31 | 0.94153 | INERZIA V - SLV | | -0.561 | -0.279 | 0. |
| 31 | 1.88306 | INERZIA V - SLV | | -0.561 | -0.279 | 0. |
| 31 | 0. | SISMA WOOD SLV | | -393.838 | 31.495 | 0. |
| 31 | 0.94153 | SISMA WOOD SLV | | -393.838 | 31.495 | 0. |
| 31 | 1.88306 | SISMA WOOD SLV | | -393.838 | 31.495 | 0. |
| 31 | 0. | iDROSTATICA | | -609.725 | -153.438 | 0. |
| 31 | 0.94153 | iDROSTATICA | | -609.725 | -269.312 | 0. |
| 31 | 1.88306 | iDROSTATICA | | -609.725 | -385.186 | 0. |
| 31 | 0. | SISMA WOOD SLD | | -173.935 | 13.91 | 0. |
| 31 | 0.94153 | SISMA WOOD SLD | | -173.935 | 13.91 | 0. |
| 31 | 1.88306 | SISMA WOOD SLD | | -173.935 | 13.91 | 0. |
| 31 | 0. | INERZIA H SLD | | -2.422 | 0.169 | 0. |
| 31 | 0.94153 | INERZIA H SLD | | -2.422 | 0.169 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 31 | 1.88306 | INERZIA H SLD | | -2.422 | 0.169 | 0. |
| 31 | 0. | INERZIA V + SLD | | 0.248 | 0.123 | 0. |
| 31 | 0.94153 | INERZIA V + SLD | | 0.248 | 0.123 | 0. |
| 31 | 1.88306 | INERZIA V + SLD | | 0.248 | 0.123 | 0. |
| 31 | 0. | INERZIA V SLD | | -0.248 | -0.123 | 0. |
| 31 | 0.94153 | INERZIA V SLD | | -0.248 | -0.123 | 0. |
| 31 | 1.88306 | INERZIA V SLD | | -0.248 | -0.123 | 0. |
| 31 | 0. | INERZIA V -1 | | -0.561 | -0.279 | 0. |
| 31 | 0.94153 | INERZIA V -1 | | -0.561 | -0.279 | 0. |
| 31 | 1.88306 | INERZIA V -1 | | -0.561 | -0.279 | 0. |
| 31 | 0. | SLU_1 | Max | -1065.67 | -414.523 | 0. |
| 31 | 0.94153 | SLU_1 | Max | -1056.898 | -529.514 | 0. |
| 31 | 1.88306 | SLU_1 | Max | -1048.126 | -644.506 | 0. |
| 31 | 0. | SLU_1 | Min | -1065.67 | -414.523 | 0. |
| 31 | 0.94153 | SLU_1 | Min | -1056.898 | -529.514 | 0. |
| 31 | 1.88306 | SLU_1 | Min | -1048.126 | -644.506 | 0. |
| 31 | 0. | SLU_2 | Max | -969.616 | -425.19 | 0. |
| 31 | 0.94153 | SLU_2 | Max | -960.844 | -540.181 | 0. |
| 31 | 1.88306 | SLU_2 | Max | -952.071 | -655.173 | 0. |
| 31 | 0. | SLU_2 | Min | -969.616 | -425.19 | 0. |
| 31 | 0.94153 | SLU_2 | Min | -960.844 | -540.181 | 0. |
| 31 | 1.88306 | SLU_2 | Min | -952.071 | -655.173 | 0. |
| 31 | 0. | SLU_3 | Max | -1118.423 | -368.716 | 0. |
| 31 | 0.94153 | SLU_3 | Max | -1109.65 | -483.707 | 0. |
| 31 | 1.88306 | SLU_3 | Max | -1100.878 | -598.698 | 0. |
| 31 | 0. | SLU_3 | Min | -1118.423 | -368.716 | 0. |
| 31 | 0.94153 | SLU_3 | Min | -1109.65 | -483.707 | 0. |
| 31 | 1.88306 | SLU_3 | Min | -1100.878 | -598.698 | 0. |
| 31 | 0. | SLU_4 | Max | -987.953 | -393.504 | 0. |
| 31 | 0.94153 | SLU_4 | Max | -979.181 | -508.495 | 0. |
| 31 | 1.88306 | SLU_4 | Max | -970.408 | -623.486 | 0. |
| 31 | 0. | SLU_4 | Min | -987.953 | -393.504 | 0. |
| 31 | 0.94153 | SLU_4 | Min | -979.181 | -508.495 | 0. |
| 31 | 1.88306 | SLU_4 | Min | -970.408 | -623.486 | 0. |
| 31 | 0. | SLE_F1 | Max | -821.148 | -310.232 | 0. |
| 31 | 0.94153 | SLE_F1 | Max | -814.4 | -398.687 | 0. |
| 31 | 1.88306 | SLE_F1 | Max | -807.652 | -487.142 | 0. |
| 31 | 0. | SLE_F1 | Min | -821.148 | -310.232 | 0. |
| 31 | 0.94153 | SLE_F1 | Min | -814.4 | -398.687 | 0. |
| 31 | 1.88306 | SLE_F1 | Min | -807.652 | -487.142 | 0. |
| 31 | 0. | SLE_F2 | Max | -749.905 | -320.345 | 0. |
| 31 | 0.94153 | SLE_F2 | Max | -743.157 | -408.8 | 0. |
| 31 | 1.88306 | SLE_F2 | Max | -736.409 | -497.254 | 0. |
| 31 | 0. | SLE_F2 | Min | -749.905 | -320.345 | 0. |
| 31 | 0.94153 | SLE_F2 | Min | -743.157 | -408.8 | 0. |
| 31 | 1.88306 | SLE_F2 | Min | -736.409 | -497.254 | 0. |
| 31 | 0. | SLE_F3 | Max | -763.115 | -295.653 | 0. |
| 31 | 0.94153 | SLE_F3 | Max | -756.367 | -384.108 | 0. |
| 31 | 1.88306 | SLE_F3 | Max | -749.619 | -472.563 | 0. |
| 31 | 0. | SLE_F3 | Min | -763.115 | -295.653 | 0. |
| 31 | 0.94153 | SLE_F3 | Min | -756.367 | -384.108 | 0. |
| 31 | 1.88306 | SLE_F3 | Min | -749.619 | -472.563 | 0. |
| 31 | 0. | SLE_F4 | Max | -867.626 | -274.132 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 31 | 0.94153 | SLE_F4 | Max | -860.878 | -362.587 | 0. |
| 31 | 1.88306 | SLE_F4 | Max | -854.13 | -451.042 | 0. |
| 31 | 0. | SLE_F4 | Min | -867.626 | -274.132 | 0. |
| 31 | 0.94153 | SLE_F4 | Min | -860.878 | -362.587 | 0. |
| 31 | 1.88306 | SLE_F4 | Min | -854.13 | -451.042 | 0. |
| 31 | 0. | SLE_QP1 | Max | -825.675 | -297.871 | 0. |
| 31 | 0.94153 | SLE_QP1 | Max | -818.927 | -386.325 | 0. |
| 31 | 1.88306 | SLE_QP1 | Max | -812.179 | -474.78 | 0. |
| 31 | 0. | SLE_QP1 | Min | -825.675 | -297.871 | 0. |
| 31 | 0.94153 | SLE_QP1 | Min | -818.927 | -386.325 | 0. |
| 31 | 1.88306 | SLE_QP1 | Min | -812.179 | -474.78 | 0. |
| 31 | 0. | SLE_QP2 | Max | -757.424 | -307.858 | 0. |
| 31 | 0.94153 | SLE_QP2 | Max | -750.676 | -396.313 | 0. |
| 31 | 1.88306 | SLE_QP2 | Max | -743.928 | -484.768 | 0. |
| 31 | 0. | SLE_QP2 | Min | -757.424 | -307.858 | 0. |
| 31 | 0.94153 | SLE_QP2 | Min | -750.676 | -396.313 | 0. |
| 31 | 1.88306 | SLE_QP2 | Min | -743.928 | -484.768 | 0. |
| 31 | 0. | SLE_QP3 | Max | -768.967 | -282.575 | 0. |
| 31 | 0.94153 | SLE_QP3 | Max | -762.219 | -371.03 | 0. |
| 31 | 1.88306 | SLE_QP3 | Max | -755.471 | -459.485 | 0. |
| 31 | 0. | SLE_QP3 | Min | -768.967 | -282.575 | 0. |
| 31 | 0.94153 | SLE_QP3 | Min | -762.219 | -371.03 | 0. |
| 31 | 1.88306 | SLE_QP3 | Min | -755.471 | -459.485 | 0. |
| 31 | 0. | SLE_QP4 | Max | -882.444 | -256.685 | 0. |
| 31 | 0.94153 | SLE_QP4 | Max | -875.696 | -345.14 | 0. |
| 31 | 1.88306 | SLE_QP4 | Max | -868.948 | -433.595 | 0. |
| 31 | 0. | SLE_QP4 | Min | -882.444 | -256.685 | 0. |
| 31 | 0.94153 | SLE_QP4 | Min | -875.696 | -345.14 | 0. |
| 31 | 1.88306 | SLE_QP4 | Min | -868.948 | -433.595 | 0. |
| 31 | 0. | SLV_1 | Max | -1684.919 | -207.876 | 0. |
| 31 | 0.94153 | SLV_1 | Max | -1678.171 | -296.331 | 0. |
| 31 | 1.88306 | SLV_1 | Max | -1671.423 | -384.785 | 0. |
| 31 | 0. | SLV_1 | Min | -1684.919 | -207.876 | 0. |
| 31 | 0.94153 | SLV_1 | Min | -1678.171 | -296.331 | 0. |
| 31 | 1.88306 | SLV_1 | Min | -1671.423 | -384.785 | 0. |
| 31 | 0. | SLV_2 | Max | -1687.241 | -208.612 | 0. |
| 31 | 0.94153 | SLV_2 | Max | -1680.493 | -297.067 | 0. |
| 31 | 1.88306 | SLV_2 | Max | -1673.745 | -385.521 | 0. |
| 31 | 0. | SLV_2 | Min | -1687.241 | -208.612 | 0. |
| 31 | 0.94153 | SLV_2 | Min | -1680.493 | -297.067 | 0. |
| 31 | 1.88306 | SLV_2 | Min | -1673.745 | -385.521 | 0. |
| 31 | 0. | SLV_3 | Max | -1853.842 | -191.884 | 0. |
| 31 | 0.94153 | SLV_3 | Max | -1847.094 | -280.339 | 0. |
| 31 | 1.88306 | SLV_3 | Max | -1840.346 | -368.793 | 0. |
| 31 | 0. | SLV_3 | Min | -1853.842 | -191.884 | 0. |
| 31 | 0.94153 | SLV_3 | Min | -1847.094 | -280.339 | 0. |
| 31 | 1.88306 | SLV_3 | Min | -1840.346 | -368.793 | 0. |
| 31 | 0. | SLV_4 | Max | -1855.871 | -192.497 | 0. |
| 31 | 0.94153 | SLV_4 | Max | -1849.123 | -280.951 | 0. |
| 31 | 1.88306 | SLV_4 | Max | -1842.375 | -369.406 | 0. |
| 31 | 0. | SLV_4 | Min | -1855.871 | -192.497 | 0. |
| 31 | 0.94153 | SLV_4 | Min | -1849.123 | -280.951 | 0. |
| 31 | 1.88306 | SLV_4 | Min | -1842.375 | -369.406 | 0. |
| 31 | 0. | SLD_1 | Max | -1141.239 | -239.731 | 0. |
| 31 | 0.94153 | SLD_1 | Max | -1134.491 | -328.186 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 31 | 1.88306 | SLD_1 | Max | -1127.743 | -416.641 | 0. |
| 31 | 0. | SLD_1 | Min | -1141.239 | -239.731 | 0. |
| 31 | 0.94153 | SLD_1 | Min | -1134.491 | -328.186 | 0. |
| 31 | 1.88306 | SLD_1 | Min | -1127.743 | -416.641 | 0. |
| 31 | 0. | SLD_2 | Max | -1142.474 | -240.272 | 0. |
| 31 | 0.94153 | SLD_2 | Max | -1135.726 | -328.726 | 0. |
| 31 | 1.88306 | SLD_2 | Max | -1128.978 | -417.181 | 0. |
| 31 | 0. | SLD_2 | Min | -1142.474 | -240.272 | 0. |
| 31 | 0.94153 | SLD_2 | Min | -1135.726 | -328.726 | 0. |
| 31 | 1.88306 | SLD_2 | Min | -1128.978 | -417.181 | 0. |
| 31 | 0. | SLD_3 | Max | -1309.917 | -217.463 | 0. |
| 31 | 0.94153 | SLD_3 | Max | -1303.169 | -305.918 | 0. |
| 31 | 1.88306 | SLD_3 | Max | -1296.421 | -394.372 | 0. |
| 31 | 0. | SLD_3 | Min | -1309.917 | -217.463 | 0. |
| 31 | 0.94153 | SLD_3 | Min | -1303.169 | -305.918 | 0. |
| 31 | 1.88306 | SLD_3 | Min | -1296.421 | -394.372 | 0. |
| 31 | 0. | SLD_4 | Max | -1310.748 | -217.756 | 0. |
| 31 | 0.94153 | SLD_4 | Max | -1304. | -306.211 | 0. |
| 31 | 1.88306 | SLD_4 | Max | -1297.252 | -394.665 | 0. |
| 31 | 0. | SLD_4 | Min | -1310.748 | -217.756 | 0. |
| 31 | 0.94153 | SLD_4 | Min | -1304. | -306.211 | 0. |
| 31 | 1.88306 | SLD_4 | Min | -1297.252 | -394.665 | 0. |
| 31 | 0. | SLU_IDR_1 | Max | -849.605 | -321.988 | 0. |
| 31 | 0.94153 | SLU_IDR_1 | Max | -843.531 | -424.772 | 0. |
| 31 | 1.88306 | SLU_IDR_1 | Max | -837.458 | -527.556 | 0. |
| 31 | 0. | SLU_IDR_1 | Min | -849.605 | -321.988 | 0. |
| 31 | 0.94153 | SLU_IDR_1 | Min | -843.531 | -424.772 | 0. |
| 31 | 1.88306 | SLU_IDR_1 | Min | -837.458 | -527.556 | 0. |
| 31 | 0. | SLU_IDR_2 | Max | -845.735 | -349.74 | 0. |
| 31 | 0.94153 | SLU_IDR_2 | Max | -839.662 | -452.524 | 0. |
| 31 | 1.88306 | SLU_IDR_2 | Max | -833.589 | -555.308 | 0. |
| 31 | 0. | SLU_IDR_2 | Min | -845.735 | -349.74 | 0. |
| 31 | 0.94153 | SLU_IDR_2 | Min | -839.662 | -452.524 | 0. |
| 31 | 1.88306 | SLU_IDR_2 | Min | -833.589 | -555.308 | 0. |
| 31 | 0. | SISMA WOOD SLV-1 | Max | -877.963 | 119.638 | 0. |
| 31 | 0.94153 | SISMA WOOD SLV-1 | Max | -877.963 | 119.638 | 0. |
| 31 | 1.88306 | SISMA WOOD SLV-1 | Max | -877.963 | 119.638 | 0. |
| 31 | 0. | SISMA WOOD SLV-1 | Min | -877.963 | 119.638 | 0. |
| 31 | 0.94153 | SISMA WOOD SLV-1 | Min | -877.963 | 119.638 | 0. |
| 31 | 1.88306 | SISMA WOOD SLV-1 | Min | -877.963 | 119.638 | 0. |
| 31 | 0. | DEAD-1 | Max | 33.539 | -17.206 | 0. |
| 31 | 0.94153 | DEAD-1 | Max | 40.287 | 10.214 | 0. |
| 31 | 1.88306 | DEAD-1 | Max | 47.035 | 37.633 | 0. |
| 31 | 0. | DEAD-1 | Min | 33.539 | -17.206 | 0. |
| 31 | 0.94153 | DEAD-1 | Min | 40.287 | 10.214 | 0. |
| 31 | 1.88306 | DEAD-1 | Min | 47.035 | 37.633 | 0. |
| 31 | 0. | SLU_PROVA | | -1054.043 | -369.145 | 0. |
| 31 | 0.94153 | SLU_PROVA | | -1045.27 | -484.136 | 0. |
| 31 | 1.88306 | SLU_PROVA | | -1036.498 | -599.127 | 0. |
| 34 | 0. | DEAD | | 45.507 | 2.896 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 34 | 0.28669 | DEAD | | 49.121 | 10.697 | 0. |
| 34 | 0.57337 | DEAD | | 52.736 | 18.499 | 0. |
| 34 | 0. | SIMM_KA | | -145.339 | 27.439 | 0. |
| 34 | 0.28669 | SIMM_KA | | -145.339 | 27.439 | 0. |
| 34 | 0.57337 | SIMM_KA | | -145.339 | 27.439 | 0. |
| 34 | 0. | SIMM_K0 | | -219.487 | 40.838 | 0. |
| 34 | 0.28669 | SIMM_K0 | | -219.487 | 40.838 | 0. |
| 34 | 0.57337 | SIMM_K0 | | -219.487 | 40.838 | 0. |
| 34 | 0. | A--SIMM_KA | | -173.933 | 38.544 | 0. |
| 34 | 0.28669 | A--SIMM_KA | | -173.933 | 38.544 | 0. |
| 34 | 0.57337 | A--SIMM_KA | | -173.933 | 38.544 | 0. |
| 34 | 0. | A--SIMM_K0 | | -268.09 | 60.111 | 0. |
| 34 | 0.28669 | A--SIMM_K0 | | -268.09 | 60.111 | 0. |
| 34 | 0.57337 | A--SIMM_K0 | | -268.09 | 60.111 | 0. |
| 34 | 0. | A-- SIMM_SOVR_K A | | -9.286 | -0.281 | 0. |
| 34 | 0.28669 | A-- SIMM_SOVR_K A | | -9.286 | -0.281 | 0. |
| 34 | 0.57337 | A-- SIMM_SOVR_K A | | -9.286 | -0.281 | 0. |
| 34 | 0. | A-- SIMM_SOVR_K 0 | | -13.922 | -0.421 | 0. |
| 34 | 0.28669 | A-- SIMM_SOVR_K 0 | | -13.922 | -0.421 | 0. |
| 34 | 0.57337 | A-- SIMM_SOVR_K 0 | | -13.922 | -0.421 | 0. |
| 34 | 0. | SIMM_SOVR_K 0 | | -13.922 | -0.421 | 0. |
| 34 | 0.28669 | SIMM_SOVR_K 0 | | -13.922 | -0.421 | 0. |
| 34 | 0.57337 | SIMM_SOVR_K 0 | | -13.922 | -0.421 | 0. |
| 34 | 0. | SIMM_SOVR_K A | | -9.286 | -0.281 | 0. |
| 34 | 0.28669 | SIMM_SOVR_K A | | -9.286 | -0.281 | 0. |
| 34 | 0.57337 | SIMM_SOVR_K A | | -9.286 | -0.281 | 0. |
| 34 | 0. | SOVR | | 0.537 | -33.135 | 0. |
| 34 | 0.28669 | SOVR | | 0.537 | -33.135 | 0. |
| 34 | 0.57337 | SOVR | | 0.537 | -33.135 | 0. |
| 34 | 0. | TERR_SIMM | | -22.622 | -132.484 | 0. |
| 34 | 0.28669 | TERR_SIMM | | -22.622 | -132.484 | 0. |
| 34 | 0.57337 | TERR_SIMM | | -22.622 | -132.484 | 0. |
| 34 | 0. | TERR_A--SIMM | | -20.792 | -138.484 | 0. |
| 34 | 0.28669 | TERR_A--SIMM | | -20.792 | -138.484 | 0. |
| 34 | 0.57337 | TERR_A--SIMM | | -20.792 | -138.484 | 0. |
| 34 | 0. | INERZIA H SLV | | -6.495 | 1.106 | 0. |
| 34 | 0.28669 | INERZIA H SLV | | -6.495 | 1.106 | 0. |
| 34 | 0.57337 | INERZIA H SLV | | -6.495 | 1.106 | 0. |
| 34 | 0. | INERZIA V + SLV | | 0.775 | 0.182 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 34 | 0.28669 | INERZIA V + SLV | | 0.775 | 0.182 | 0. |
| 34 | 0.57337 | INERZIA V + SLV | | 0.775 | 0.182 | 0. |
| 34 | 0. | INERZIA V - SLV | | -0.775 | -0.182 | 0. |
| 34 | 0.28669 | INERZIA V - SLV | | -0.775 | -0.182 | 0. |
| 34 | 0.57337 | INERZIA V - SLV | | -0.775 | -0.182 | 0. |
| 34 | 0. | SISMA WOOD SLV | | -384.512 | 76.046 | 0. |
| 34 | 0.28669 | SISMA WOOD SLV | | -384.512 | 76.046 | 0. |
| 34 | 0.57337 | SISMA WOOD SLV | | -384.512 | 76.046 | 0. |
| 34 | 0. | iDROSTATICA | | -667.489 | -230.54 | 0. |
| 34 | 0.28669 | iDROSTATICA | | -667.489 | -265.822 | 0. |
| 34 | 0.57337 | iDROSTATICA | | -667.489 | -301.105 | 0. |
| 34 | 0. | SISMA WOOD SLD | | -169.816 | 33.585 | 0. |
| 34 | 0.28669 | SISMA WOOD SLD | | -169.816 | 33.585 | 0. |
| 34 | 0.57337 | SISMA WOOD SLD | | -169.816 | 33.585 | 0. |
| 34 | 0. | INERZIA H SLD | | -2.869 | 0.489 | 0. |
| 34 | 0.28669 | INERZIA H SLD | | -2.869 | 0.489 | 0. |
| 34 | 0.57337 | INERZIA H SLD | | -2.869 | 0.489 | 0. |
| 34 | 0. | INERZIA V + SLD | | 0.342 | 0.081 | 0. |
| 34 | 0.28669 | INERZIA V + SLD | | 0.342 | 0.081 | 0. |
| 34 | 0.57337 | INERZIA V + SLD | | 0.342 | 0.081 | 0. |
| 34 | 0. | INERZIA V SLD | | -0.342 | -0.081 | 0. |
| 34 | 0.28669 | INERZIA V SLD | | -0.342 | -0.081 | 0. |
| 34 | 0.57337 | INERZIA V SLD | | -0.342 | -0.081 | 0. |
| 34 | 0. | INERZIA V -1 | | -0.775 | -0.182 | 0. |
| 34 | 0.28669 | INERZIA V -1 | | -0.775 | -0.182 | 0. |
| 34 | 0.57337 | INERZIA V -1 | | -0.775 | -0.182 | 0. |
| 34 | 0. | SLU_1 | Max | -1164.789 | -516.407 | 0. |
| 34 | 0.28669 | SLU_1 | Max | -1160.09 | -552.133 | 0. |
| 34 | 0.57337 | SLU_1 | Max | -1155.39 | -587.858 | 0. |
| 34 | 0. | SLU_1 | Min | -1164.789 | -516.407 | 0. |
| 34 | 0.28669 | SLU_1 | Min | -1160.09 | -552.133 | 0. |
| 34 | 0.57337 | SLU_1 | Min | -1155.39 | -587.858 | 0. |
| 34 | 0. | SLU_2 | Max | -1072.268 | -543.493 | 0. |
| 34 | 0.28669 | SLU_2 | Max | -1067.569 | -579.218 | 0. |
| 34 | 0.57337 | SLU_2 | Max | -1062.869 | -614.944 | 0. |
| 34 | 0. | SLU_2 | Min | -1072.268 | -543.493 | 0. |
| 34 | 0.28669 | SLU_2 | Min | -1067.569 | -579.218 | 0. |
| 34 | 0.57337 | SLU_2 | Min | -1062.869 | -614.944 | 0. |
| 34 | 0. | SLU_3 | Max | -1209.173 | -472.012 | 0. |
| 34 | 0.28669 | SLU_3 | Max | -1204.473 | -507.738 | 0. |
| 34 | 0.57337 | SLU_3 | Max | -1199.774 | -543.463 | 0. |
| 34 | 0. | SLU_3 | Min | -1209.173 | -472.012 | 0. |
| 34 | 0.28669 | SLU_3 | Min | -1204.473 | -507.738 | 0. |
| 34 | 0.57337 | SLU_3 | Min | -1199.774 | -543.463 | 0. |
| 34 | 0. | SLU_4 | Max | -1085.221 | -516.77 | 0. |
| 34 | 0.28669 | SLU_4 | Max | -1080.522 | -552.496 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 34 | 0.57337 | SLU_4 | Max | -1075.822 | -588.222 | 0. |
| 34 | 0. | SLU_4 | Min | -1085.221 | -516.77 | 0. |
| 34 | 0.28669 | SLU_4 | Min | -1080.522 | -552.496 | 0. |
| 34 | 0.57337 | SLU_4 | Min | -1075.822 | -588.222 | 0. |
| 34 | 0. | SLE_F1 | Max | -894.923 | -383.236 | 0. |
| 34 | 0.28669 | SLE_F1 | Max | -891.308 | -410.717 | 0. |
| 34 | 0.57337 | SLE_F1 | Max | -887.693 | -438.199 | 0. |
| 34 | 0. | SLE_F1 | Min | -894.923 | -383.236 | 0. |
| 34 | 0.28669 | SLE_F1 | Min | -891.308 | -410.717 | 0. |
| 34 | 0.57337 | SLE_F1 | Min | -887.693 | -438.199 | 0. |
| 34 | 0. | SLE_F2 | Max | -826.692 | -405.29 | 0. |
| 34 | 0.28669 | SLE_F2 | Max | -823.077 | -432.771 | 0. |
| 34 | 0.57337 | SLE_F2 | Max | -819.462 | -460.252 | 0. |
| 34 | 0. | SLE_F2 | Min | -826.692 | -405.29 | 0. |
| 34 | 0.28669 | SLE_F2 | Min | -823.077 | -432.771 | 0. |
| 34 | 0.57337 | SLE_F2 | Min | -819.462 | -460.252 | 0. |
| 34 | 0. | SLE_F3 | Max | -835.727 | -384.662 | 0. |
| 34 | 0.28669 | SLE_F3 | Max | -832.112 | -412.143 | 0. |
| 34 | 0.57337 | SLE_F3 | Max | -828.497 | -439.624 | 0. |
| 34 | 0. | SLE_F3 | Min | -835.727 | -384.662 | 0. |
| 34 | 0.28669 | SLE_F3 | Min | -832.112 | -412.143 | 0. |
| 34 | 0.57337 | SLE_F3 | Min | -828.497 | -439.624 | 0. |
| 34 | 0. | SLE_F4 | Max | -934.758 | -347.625 | 0. |
| 34 | 0.28669 | SLE_F4 | Max | -931.143 | -375.106 | 0. |
| 34 | 0.57337 | SLE_F4 | Max | -927.528 | -402.587 | 0. |
| 34 | 0. | SLE_F4 | Min | -934.758 | -347.625 | 0. |
| 34 | 0.28669 | SLE_F4 | Min | -931.143 | -375.106 | 0. |
| 34 | 0.57337 | SLE_F4 | Min | -927.528 | -402.587 | 0. |
| 34 | 0. | SLE_QP1 | Max | -895.465 | -360.054 | 0. |
| 34 | 0.28669 | SLE_QP1 | Max | -891.85 | -387.536 | 0. |
| 34 | 0.57337 | SLE_QP1 | Max | -888.235 | -415.017 | 0. |
| 34 | 0. | SLE_QP1 | Min | -895.465 | -360.054 | 0. |
| 34 | 0.28669 | SLE_QP1 | Min | -891.85 | -387.536 | 0. |
| 34 | 0.57337 | SLE_QP1 | Min | -888.235 | -415.017 | 0. |
| 34 | 0. | SLE_QP2 | Max | -830.169 | -381.554 | 0. |
| 34 | 0.28669 | SLE_QP2 | Max | -826.554 | -409.035 | 0. |
| 34 | 0.57337 | SLE_QP2 | Max | -822.939 | -436.516 | 0. |
| 34 | 0. | SLE_QP2 | Min | -830.169 | -381.554 | 0. |
| 34 | 0.28669 | SLE_QP2 | Min | -826.554 | -409.035 | 0. |
| 34 | 0.57337 | SLE_QP2 | Min | -822.939 | -436.516 | 0. |
| 34 | 0. | SLE_QP3 | Max | -837.476 | -360.79 | 0. |
| 34 | 0.28669 | SLE_QP3 | Max | -833.861 | -388.272 | 0. |
| 34 | 0.57337 | SLE_QP3 | Max | -830.246 | -415.753 | 0. |
| 34 | 0. | SLE_QP3 | Min | -837.476 | -360.79 | 0. |
| 34 | 0.28669 | SLE_QP3 | Min | -833.861 | -388.272 | 0. |
| 34 | 0.57337 | SLE_QP3 | Min | -830.246 | -415.753 | 0. |
| 34 | 0. | SLE_QP4 | Max | -944.627 | -318.929 | 0. |
| 34 | 0.28669 | SLE_QP4 | Max | -941.013 | -346.41 | 0. |
| 34 | 0.57337 | SLE_QP4 | Max | -937.398 | -373.892 | 0. |
| 34 | 0. | SLE_QP4 | Min | -944.627 | -318.929 | 0. |
| 34 | 0.28669 | SLE_QP4 | Min | -941.013 | -346.41 | 0. |
| 34 | 0.57337 | SLE_QP4 | Min | -937.398 | -373.892 | 0. |
| 34 | 0. | SLV_1 | Max | -1730.445 | -167.895 | 0. |
| 34 | 0.28669 | SLV_1 | Max | -1726.83 | -195.376 | 0. |
| 34 | 0.57337 | SLV_1 | Max | -1723.215 | -222.857 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 34 | 0. | SLV_1 | Min | -1730.445 | -167.895 | 0. |
| 34 | 0.28669 | SLV_1 | Min | -1726.83 | -195.376 | 0. |
| 34 | 0.57337 | SLV_1 | Min | -1723.215 | -222.857 | 0. |
| 34 | 0. | SLV_2 | Max | -1733.203 | -168.185 | 0. |
| 34 | 0.28669 | SLV_2 | Max | -1729.588 | -195.666 | 0. |
| 34 | 0.57337 | SLV_2 | Max | -1725.973 | -223.148 | 0. |
| 34 | 0. | SLV_2 | Min | -1733.203 | -168.185 | 0. |
| 34 | 0.28669 | SLV_2 | Min | -1729.588 | -195.666 | 0. |
| 34 | 0.57337 | SLV_2 | Min | -1725.973 | -223.148 | 0. |
| 34 | 0. | SLV_3 | Max | -1895.176 | -135.271 | 0. |
| 34 | 0.28669 | SLV_3 | Max | -1891.561 | -162.752 | 0. |
| 34 | 0.57337 | SLV_3 | Max | -1887.946 | -190.233 | 0. |
| 34 | 0. | SLV_3 | Min | -1895.176 | -135.271 | 0. |
| 34 | 0.28669 | SLV_3 | Min | -1891.561 | -162.752 | 0. |
| 34 | 0.57337 | SLV_3 | Min | -1887.946 | -190.233 | 0. |
| 34 | 0. | SLV_4 | Max | -1897.622 | -135.498 | 0. |
| 34 | 0.28669 | SLV_4 | Max | -1894.008 | -162.979 | 0. |
| 34 | 0.57337 | SLV_4 | Max | -1890.393 | -190.46 | 0. |
| 34 | 0. | SLV_4 | Min | -1897.622 | -135.498 | 0. |
| 34 | 0.28669 | SLV_4 | Min | -1894.008 | -162.979 | 0. |
| 34 | 0.57337 | SLV_4 | Min | -1890.393 | -190.46 | 0. |
| 34 | 0. | SLD_1 | Max | -1197.591 | -266.366 | 0. |
| 34 | 0.28669 | SLD_1 | Max | -1193.976 | -293.848 | 0. |
| 34 | 0.57337 | SLD_1 | Max | -1190.361 | -321.329 | 0. |
| 34 | 0. | SLD_1 | Min | -1197.591 | -266.366 | 0. |
| 34 | 0.28669 | SLD_1 | Min | -1193.976 | -293.848 | 0. |
| 34 | 0.57337 | SLD_1 | Min | -1190.361 | -321.329 | 0. |
| 34 | 0. | SLD_2 | Max | -1199.047 | -266.606 | 0. |
| 34 | 0.28669 | SLD_2 | Max | -1195.432 | -294.087 | 0. |
| 34 | 0.57337 | SLD_2 | Max | -1191.817 | -321.569 | 0. |
| 34 | 0. | SLD_2 | Min | -1199.047 | -266.606 | 0. |
| 34 | 0.28669 | SLD_2 | Min | -1195.432 | -294.087 | 0. |
| 34 | 0.57337 | SLD_2 | Min | -1191.817 | -321.569 | 0. |
| 34 | 0. | SLD_3 | Max | -1360.952 | -228.144 | 0. |
| 34 | 0.28669 | SLD_3 | Max | -1357.337 | -255.625 | 0. |
| 34 | 0.57337 | SLD_3 | Max | -1353.722 | -283.106 | 0. |
| 34 | 0. | SLD_3 | Min | -1360.952 | -228.144 | 0. |
| 34 | 0.28669 | SLD_3 | Min | -1357.337 | -255.625 | 0. |
| 34 | 0.57337 | SLD_3 | Min | -1353.722 | -283.106 | 0. |
| 34 | 0. | SLD_4 | Max | -1361.97 | -228.263 | 0. |
| 34 | 0.28669 | SLD_4 | Max | -1358.356 | -255.745 | 0. |
| 34 | 0.57337 | SLD_4 | Max | -1354.741 | -283.226 | 0. |
| 34 | 0. | SLD_4 | Min | -1361.97 | -228.263 | 0. |
| 34 | 0.28669 | SLD_4 | Min | -1358.356 | -255.745 | 0. |
| 34 | 0.57337 | SLD_4 | Min | -1354.741 | -283.226 | 0. |
| 34 | 0. | SLU_IDR_1 | Max | -928.562 | -395.894 | 0. |
| 34 | 0.28669 | SLU_IDR_1 | Max | -925.309 | -427.683 | 0. |
| 34 | 0.57337 | SLU_IDR_1 | Max | -922.055 | -459.473 | 0. |
| 34 | 0. | SLU_IDR_1 | Min | -928.562 | -395.894 | 0. |
| 34 | 0.28669 | SLU_IDR_1 | Min | -925.309 | -427.683 | 0. |
| 34 | 0.57337 | SLU_IDR_1 | Min | -922.055 | -459.473 | 0. |
| 34 | 0. | SLU_IDR_2 | Max | -929.249 | -417.663 | 0. |
| 34 | 0.28669 | SLU_IDR_2 | Max | -925.996 | -449.453 | 0. |
| 34 | 0.57337 | SLU_IDR_2 | Max | -922.743 | -481.242 | 0. |
| 34 | 0. | SLU_IDR_2 | Min | -929.249 | -417.663 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 34 | 0.28669 | SLU_IDR_2 | Min | -925.996 | -449.453 | 0. |
| 34 | 0.57337 | SLU_IDR_2 | Min | -922.743 | -481.242 | 0. |
| 34 | 0. | SISMA WOOD SLV-1 | Max | -847.246 | 221.579 | 0. |
| 34 | 0.28669 | SISMA WOOD SLV-1 | Max | -847.246 | 221.579 | 0. |
| 34 | 0.57337 | SISMA WOOD SLV-1 | Max | -847.246 | 221.579 | 0. |
| 34 | 0. | SISMA WOOD SLV-1 | Min | -847.246 | 221.579 | 0. |
| 34 | 0.28669 | SISMA WOOD SLV-1 | Min | -847.246 | 221.579 | 0. |
| 34 | 0.57337 | SISMA WOOD SLV-1 | Min | -847.246 | 221.579 | 0. |
| 34 | 0. | DEAD-1 | Max | 47.933 | -8.047 | 0. |
| 34 | 0.28669 | DEAD-1 | Max | 51.548 | -0.246 | 0. |
| 34 | 0.57337 | DEAD-1 | Max | 55.163 | 7.555 | 0. |
| 34 | 0. | DEAD-1 | Min | 47.933 | -8.047 | 0. |
| 34 | 0.28669 | DEAD-1 | Min | 51.548 | -0.246 | 0. |
| 34 | 0.57337 | DEAD-1 | Min | 55.163 | 7.555 | 0. |
| 34 | 0. | SLU_PROVA | | -1143.396 | -465.41 | 0. |
| 34 | 0.28669 | SLU_PROVA | | -1138.696 | -501.136 | 0. |
| 34 | 0.57337 | SLU_PROVA | | -1133.997 | -536.861 | 0. |
| 35 | 0. | DEAD | | 53.324 | 0.217 | 0. |
| 35 | 0.29586 | DEAD | | 57.551 | 8.018 | 0. |
| 35 | 0.59172 | DEAD | | 61.779 | 15.819 | 0. |
| 35 | 0. | SIMM_KA | | -143.32 | 36.983 | 0. |
| 35 | 0.29586 | SIMM_KA | | -143.32 | 36.983 | 0. |
| 35 | 0.59172 | SIMM_KA | | -143.32 | 36.983 | 0. |
| 35 | 0. | SIMM_K0 | | -216.476 | 55.249 | 0. |
| 35 | 0.29586 | SIMM_K0 | | -216.476 | 55.249 | 0. |
| 35 | 0.59172 | SIMM_K0 | | -216.476 | 55.249 | 0. |
| 35 | 0. | A--SIMM_KA | | -171.268 | 46.275 | 0. |
| 35 | 0.29586 | A--SIMM_KA | | -171.268 | 46.275 | 0. |
| 35 | 0.59172 | A--SIMM_KA | | -171.268 | 46.275 | 0. |
| 35 | 0. | A--SIMM_K0 | | -263.927 | 72.378 | 0. |
| 35 | 0.29586 | A--SIMM_K0 | | -263.927 | 72.378 | 0. |
| 35 | 0.59172 | A--SIMM_K0 | | -263.927 | 72.378 | 0. |
| 35 | 0. | A-- SIMM_SOVR_K A | | -9.284 | 0.326 | 0. |
| 35 | 0.29586 | A-- SIMM_SOVR_K A | | -9.284 | 0.326 | 0. |
| 35 | 0.59172 | A-- SIMM_SOVR_K A | | -9.284 | 0.326 | 0. |
| 35 | 0. | A-- SIMM_SOVR_K 0 | | -13.92 | 0.489 | 0. |
| 35 | 0.29586 | A-- SIMM_SOVR_K 0 | | -13.92 | 0.489 | 0. |
| 35 | 0.59172 | A-- SIMM_SOVR_K 0 | | -13.92 | 0.489 | 0. |
| 35 | 0. | SIMM_SOVR_K 0 | | -13.92 | 0.489 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|----------|----------|
| 35 | 0.29586 | SIMM_SOVR_K 0 | | -13.92 | 0.489 | 0. |
| 35 | 0.59172 | SIMM_SOVR_K 0 | | -13.92 | 0.489 | 0. |
| 35 | 0. | SIMM_SOVR_K A | | -9.284 | 0.326 | 0. |
| 35 | 0.29586 | SIMM_SOVR_K A | | -9.284 | 0.326 | 0. |
| 35 | 0.59172 | SIMM_SOVR_K A | | -9.284 | 0.326 | 0. |
| 35 | 0. | SOVR | | -1.712 | -38.599 | 0. |
| 35 | 0.29586 | SOVR | | -1.712 | -38.599 | 0. |
| 35 | 0.59172 | SOVR | | -1.712 | -38.599 | 0. |
| 35 | 0. | TERR_SIMM | | -31.56 | -152.629 | 0. |
| 35 | 0.29586 | TERR_SIMM | | -31.56 | -152.629 | 0. |
| 35 | 0.59172 | TERR_SIMM | | -31.56 | -152.629 | 0. |
| 35 | 0. | TERR_A--SIMM | | -30.107 | -158.728 | 0. |
| 35 | 0.29586 | TERR_A--SIMM | | -30.107 | -158.728 | 0. |
| 35 | 0.59172 | TERR_A--SIMM | | -30.107 | -158.728 | 0. |
| 35 | 0. | INERZIA H SLV | | -6.928 | 1.17 | 0. |
| 35 | 0.29586 | INERZIA H SLV | | -6.928 | 1.17 | 0. |
| 35 | 0.59172 | INERZIA H SLV | | -6.928 | 1.17 | 0. |
| 35 | 0. | INERZIA V + SLV | | 0.912 | 0.14 | 0. |
| 35 | 0.29586 | INERZIA V + SLV | | 0.912 | 0.14 | 0. |
| 35 | 0.59172 | INERZIA V + SLV | | 0.912 | 0.14 | 0. |
| 35 | 0. | INERZIA V - SLV | | -0.912 | -0.14 | 0. |
| 35 | 0.29586 | INERZIA V - SLV | | -0.912 | -0.14 | 0. |
| 35 | 0.59172 | INERZIA V - SLV | | -0.912 | -0.14 | 0. |
| 35 | 0. | SISMA WOOD SLV | | -379.61 | 78.857 | 0. |
| 35 | 0.29586 | SISMA WOOD SLV | | -379.61 | 78.857 | 0. |
| 35 | 0.59172 | SISMA WOOD SLV | | -379.61 | 78.857 | 0. |
| 35 | 0. | iDROSTATICA | | -684.686 | -247.342 | 0. |
| 35 | 0.29586 | iDROSTATICA | | -684.686 | -283.754 | 0. |
| 35 | 0.59172 | iDROSTATICA | | -684.686 | -320.165 | 0. |
| 35 | 0. | SISMA WOOD SLD | | -167.651 | 34.826 | 0. |
| 35 | 0.29586 | SISMA WOOD SLD | | -167.651 | 34.826 | 0. |
| 35 | 0.59172 | SISMA WOOD SLD | | -167.651 | 34.826 | 0. |
| 35 | 0. | INERZIA H SLD | | -3.059 | 0.517 | 0. |
| 35 | 0.29586 | INERZIA H SLD | | -3.059 | 0.517 | 0. |
| 35 | 0.59172 | INERZIA H SLD | | -3.059 | 0.517 | 0. |
| 35 | 0. | INERZIA V + SLD | | 0.403 | 0.062 | 0. |
| 35 | 0.29586 | INERZIA V + SLD | | 0.403 | 0.062 | 0. |
| 35 | 0.59172 | INERZIA V + SLD | | 0.403 | 0.062 | 0. |
| 35 | 0. | INERZIA V SLD | | -0.403 | -0.062 | 0. |
| 35 | 0.29586 | INERZIA V SLD | | -0.403 | -0.062 | 0. |
| 35 | 0.59172 | INERZIA V SLD | | -0.403 | -0.062 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------|----------|-----------|----------|----------|
| 35 | 0. | INERZIA V -1 | | -0.912 | -0.14 | 0. |
| 35 | 0.29586 | INERZIA V -1 | | -0.912 | -0.14 | 0. |
| 35 | 0.59172 | INERZIA V -1 | | -0.912 | -0.14 | 0. |
| 35 | 0. | SLU_1 | Max | -1191.37 | -559.694 | 0. |
| 35 | 0.29586 | SLU_1 | Max | -1185.874 | -596.887 | 0. |
| 35 | 0.59172 | SLU_1 | Max | -1180.378 | -634.08 | 0. |
| 35 | 0. | SLU_1 | Min | -1191.37 | -559.694 | 0. |
| 35 | 0.29586 | SLU_1 | Min | -1185.874 | -596.887 | 0. |
| 35 | 0.59172 | SLU_1 | Min | -1180.378 | -634.08 | 0. |
| 35 | 0. | SLU_2 | Max | -1100.734 | -592.739 | 0. |
| 35 | 0.29586 | SLU_2 | Max | -1095.238 | -629.932 | 0. |
| 35 | 0.59172 | SLU_2 | Max | -1089.741 | -667.126 | 0. |
| 35 | 0. | SLU_2 | Min | -1100.734 | -592.739 | 0. |
| 35 | 0.29586 | SLU_2 | Min | -1095.238 | -629.932 | 0. |
| 35 | 0.59172 | SLU_2 | Min | -1089.741 | -667.126 | 0. |
| 35 | 0. | SLU_3 | Max | -1233.139 | -521.302 | 0. |
| 35 | 0.29586 | SLU_3 | Max | -1227.643 | -558.495 | 0. |
| 35 | 0.59172 | SLU_3 | Max | -1222.147 | -595.689 | 0. |
| 35 | 0. | SLU_3 | Min | -1233.139 | -521.302 | 0. |
| 35 | 0.29586 | SLU_3 | Min | -1227.643 | -558.495 | 0. |
| 35 | 0.59172 | SLU_3 | Min | -1222.147 | -595.689 | 0. |
| 35 | 0. | SLU_4 | Max | -1112.174 | -571.67 | 0. |
| 35 | 0.29586 | SLU_4 | Max | -1106.678 | -608.863 | 0. |
| 35 | 0.59172 | SLU_4 | Max | -1101.182 | -646.057 | 0. |
| 35 | 0. | SLU_4 | Min | -1112.174 | -571.67 | 0. |
| 35 | 0.29586 | SLU_4 | Min | -1106.678 | -608.863 | 0. |
| 35 | 0.59172 | SLU_4 | Min | -1101.182 | -646.057 | 0. |
| 35 | 0. | SLE_F1 | Max | -914.413 | -414.024 | 0. |
| 35 | 0.29586 | SLE_F1 | Max | -910.186 | -442.635 | 0. |
| 35 | 0.59172 | SLE_F1 | Max | -905.958 | -471.245 | 0. |
| 35 | 0. | SLE_F1 | Min | -914.413 | -414.024 | 0. |
| 35 | 0.29586 | SLE_F1 | Min | -910.186 | -442.635 | 0. |
| 35 | 0.59172 | SLE_F1 | Min | -905.958 | -471.245 | 0. |
| 35 | 0. | SLE_F2 | Max | -847.7 | -440.393 | 0. |
| 35 | 0.29586 | SLE_F2 | Max | -843.472 | -469.003 | 0. |
| 35 | 0.59172 | SLE_F2 | Max | -839.244 | -497.613 | 0. |
| 35 | 0. | SLE_F2 | Min | -847.7 | -440.393 | 0. |
| 35 | 0.29586 | SLE_F2 | Min | -843.472 | -469.003 | 0. |
| 35 | 0.59172 | SLE_F2 | Min | -839.244 | -497.613 | 0. |
| 35 | 0. | SLE_F3 | Max | -855.57 | -424.184 | 0. |
| 35 | 0.29586 | SLE_F3 | Max | -851.342 | -452.794 | 0. |
| 35 | 0.59172 | SLE_F3 | Max | -847.114 | -481.404 | 0. |
| 35 | 0. | SLE_F3 | Min | -855.57 | -424.184 | 0. |
| 35 | 0.29586 | SLE_F3 | Min | -851.342 | -452.794 | 0. |
| 35 | 0.59172 | SLE_F3 | Min | -847.114 | -481.404 | 0. |
| 35 | 0. | SLE_F4 | Max | -952.143 | -382.982 | 0. |
| 35 | 0.29586 | SLE_F4 | Max | -947.915 | -411.592 | 0. |
| 35 | 0.59172 | SLE_F4 | Max | -943.688 | -440.202 | 0. |
| 35 | 0. | SLE_F4 | Min | -952.143 | -382.982 | 0. |
| 35 | 0.29586 | SLE_F4 | Min | -947.915 | -411.592 | 0. |
| 35 | 0.59172 | SLE_F4 | Min | -943.688 | -440.202 | 0. |
| 35 | 0. | SLE_QP1 | Max | -913.345 | -385.859 | 0. |
| 35 | 0.29586 | SLE_QP1 | Max | -909.117 | -414.469 | 0. |
| 35 | 0.59172 | SLE_QP1 | Max | -904.89 | -443.079 | 0. |
| 35 | 0. | SLE_QP1 | Min | -913.345 | -385.859 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 35 | 0.29586 | SLE_QP1 | Min | -909.117 | -414.469 | 0. |
| 35 | 0.59172 | SLE_QP1 | Min | -904.89 | -443.079 | 0. |
| 35 | 0. | SLE_QP2 | Max | -849.527 | -411.497 | 0. |
| 35 | 0.29586 | SLE_QP2 | Max | -845.299 | -440.107 | 0. |
| 35 | 0.59172 | SLE_QP2 | Max | -841.071 | -468.717 | 0. |
| 35 | 0. | SLE_QP2 | Min | -849.527 | -411.497 | 0. |
| 35 | 0.29586 | SLE_QP2 | Min | -845.299 | -440.107 | 0. |
| 35 | 0.59172 | SLE_QP2 | Min | -841.071 | -468.717 | 0. |
| 35 | 0. | SLE_QP3 | Max | -855.664 | -395.282 | 0. |
| 35 | 0.29586 | SLE_QP3 | Max | -851.436 | -423.892 | 0. |
| 35 | 0.59172 | SLE_QP3 | Max | -847.209 | -452.502 | 0. |
| 35 | 0. | SLE_QP3 | Min | -855.664 | -395.282 | 0. |
| 35 | 0.29586 | SLE_QP3 | Min | -851.436 | -423.892 | 0. |
| 35 | 0.59172 | SLE_QP3 | Min | -847.209 | -452.502 | 0. |
| 35 | 0. | SLE_QP4 | Max | -960.062 | -349.502 | 0. |
| 35 | 0.29586 | SLE_QP4 | Max | -955.834 | -378.113 | 0. |
| 35 | 0.59172 | SLE_QP4 | Max | -951.607 | -406.723 | 0. |
| 35 | 0. | SLE_QP4 | Min | -960.062 | -349.502 | 0. |
| 35 | 0.29586 | SLE_QP4 | Min | -955.834 | -378.113 | 0. |
| 35 | 0.59172 | SLE_QP4 | Min | -951.607 | -406.723 | 0. |
| 35 | 0. | SLV_1 | Max | -1736.251 | -184.047 | 0. |
| 35 | 0.29586 | SLV_1 | Max | -1732.023 | -212.657 | 0. |
| 35 | 0.59172 | SLV_1 | Max | -1727.795 | -241.267 | 0. |
| 35 | 0. | SLV_1 | Min | -1736.251 | -184.047 | 0. |
| 35 | 0.29586 | SLV_1 | Min | -1732.023 | -212.657 | 0. |
| 35 | 0.59172 | SLV_1 | Min | -1727.795 | -241.267 | 0. |
| 35 | 0. | SLV_2 | Max | -1739.275 | -184.174 | 0. |
| 35 | 0.29586 | SLV_2 | Max | -1735.048 | -212.785 | 0. |
| 35 | 0.59172 | SLV_2 | Max | -1730.82 | -241.395 | 0. |
| 35 | 0. | SLV_2 | Min | -1739.275 | -184.174 | 0. |
| 35 | 0.29586 | SLV_2 | Min | -1735.048 | -212.785 | 0. |
| 35 | 0.59172 | SLV_2 | Min | -1730.82 | -241.395 | 0. |
| 35 | 0. | SLV_3 | Max | -1898.948 | -152.626 | 0. |
| 35 | 0.29586 | SLV_3 | Max | -1894.72 | -181.236 | 0. |
| 35 | 0.59172 | SLV_3 | Max | -1890.492 | -209.846 | 0. |
| 35 | 0. | SLV_3 | Min | -1898.948 | -152.626 | 0. |
| 35 | 0.29586 | SLV_3 | Min | -1894.72 | -181.236 | 0. |
| 35 | 0.59172 | SLV_3 | Min | -1890.492 | -209.846 | 0. |
| 35 | 0. | SLV_4 | Max | -1901.657 | -152.705 | 0. |
| 35 | 0.29586 | SLV_4 | Max | -1897.43 | -181.315 | 0. |
| 35 | 0.59172 | SLV_4 | Max | -1893.202 | -209.925 | 0. |
| 35 | 0. | SLV_4 | Min | -1901.657 | -152.705 | 0. |
| 35 | 0.29586 | SLV_4 | Min | -1897.43 | -181.315 | 0. |
| 35 | 0.59172 | SLV_4 | Min | -1893.202 | -209.925 | 0. |
| 35 | 0. | SLD_1 | Max | -1209.656 | -289.988 | 0. |
| 35 | 0.29586 | SLD_1 | Max | -1205.428 | -318.598 | 0. |
| 35 | 0.59172 | SLD_1 | Max | -1201.2 | -347.208 | 0. |
| 35 | 0. | SLD_1 | Min | -1209.656 | -289.988 | 0. |
| 35 | 0.29586 | SLD_1 | Min | -1205.428 | -318.598 | 0. |
| 35 | 0.59172 | SLD_1 | Min | -1201.2 | -347.208 | 0. |
| 35 | 0. | SLD_2 | Max | -1211.235 | -290.115 | 0. |
| 35 | 0.29586 | SLD_2 | Max | -1207.008 | -318.725 | 0. |
| 35 | 0.59172 | SLD_2 | Max | -1202.78 | -347.335 | 0. |
| 35 | 0. | SLD_2 | Min | -1211.235 | -290.115 | 0. |
| 35 | 0.29586 | SLD_2 | Min | -1207.008 | -318.725 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 35 | 0.59172 | SLD_2 | Min | -1202.78 | -347.335 | 0. |
| 35 | 0. | SLD_3 | Max | -1370.641 | -253.274 | 0. |
| 35 | 0.29586 | SLD_3 | Max | -1366.413 | -281.884 | 0. |
| 35 | 0.59172 | SLD_3 | Max | -1362.186 | -310.494 | 0. |
| 35 | 0. | SLD_3 | Min | -1370.641 | -253.274 | 0. |
| 35 | 0.29586 | SLD_3 | Min | -1366.413 | -281.884 | 0. |
| 35 | 0.59172 | SLD_3 | Min | -1362.186 | -310.494 | 0. |
| 35 | 0. | SLD_4 | Max | -1371.777 | -253.323 | 0. |
| 35 | 0.29586 | SLD_4 | Max | -1367.549 | -281.933 | 0. |
| 35 | 0.59172 | SLD_4 | Max | -1363.321 | -310.544 | 0. |
| 35 | 0. | SLD_4 | Min | -1371.777 | -253.323 | 0. |
| 35 | 0.29586 | SLD_4 | Min | -1367.549 | -281.933 | 0. |
| 35 | 0.59172 | SLD_4 | Min | -1363.321 | -310.544 | 0. |
| 35 | 0. | SLU_IDR_1 | Max | -949.812 | -426.104 | 0. |
| 35 | 0.29586 | SLU_IDR_1 | Max | -946.007 | -459.136 | 0. |
| 35 | 0.59172 | SLU_IDR_1 | Max | -942.202 | -492.167 | 0. |
| 35 | 0. | SLU_IDR_1 | Min | -949.812 | -426.104 | 0. |
| 35 | 0.29586 | SLU_IDR_1 | Min | -946.007 | -459.136 | 0. |
| 35 | 0.59172 | SLU_IDR_1 | Min | -942.202 | -492.167 | 0. |
| 35 | 0. | SLU_IDR_2 | Max | -951.725 | -443.173 | 0. |
| 35 | 0.29586 | SLU_IDR_2 | Max | -947.92 | -476.204 | 0. |
| 35 | 0.59172 | SLU_IDR_2 | Max | -944.116 | -509.235 | 0. |
| 35 | 0. | SLU_IDR_2 | Min | -951.725 | -443.173 | 0. |
| 35 | 0.29586 | SLU_IDR_2 | Min | -947.92 | -476.204 | 0. |
| 35 | 0.59172 | SLU_IDR_2 | Min | -944.116 | -509.235 | 0. |
| 35 | 0. | SISMA WOOD SLV-1 | Max | -833.018 | 229.104 | 0. |
| 35 | 0.29586 | SISMA WOOD SLV-1 | Max | -833.018 | 229.104 | 0. |
| 35 | 0.59172 | SISMA WOOD SLV-1 | Max | -833.018 | 229.104 | 0. |
| 35 | 0. | SISMA WOOD SLV-1 | Min | -833.018 | 229.104 | 0. |
| 35 | 0.29586 | SISMA WOOD SLV-1 | Min | -833.018 | 229.104 | 0. |
| 35 | 0.59172 | SISMA WOOD SLV-1 | Min | -833.018 | 229.104 | 0. |
| 35 | 0. | DEAD-1 | Max | 55.002 | -12.696 | 0. |
| 35 | 0.29586 | DEAD-1 | Max | 59.23 | -4.895 | 0. |
| 35 | 0.59172 | DEAD-1 | Max | 63.458 | 2.907 | 0. |
| 35 | 0. | DEAD-1 | Min | 55.002 | -12.696 | 0. |
| 35 | 0.29586 | DEAD-1 | Min | 59.23 | -4.895 | 0. |
| 35 | 0.59172 | DEAD-1 | Min | 63.458 | 2.907 | 0. |
| 35 | 0. | SLU_PROVA | | -1166.665 | -505.023 | 0. |
| 35 | 0.29586 | SLU_PROVA | | -1161.169 | -542.216 | 0. |
| 35 | 0.59172 | SLU_PROVA | | -1155.673 | -579.409 | 0. |
| 38 | 0. | DEAD | | -341.473 | -52.421 | 0. |
| 38 | 0.2636 | DEAD | | -331.591 | -52.421 | 0. |
| 38 | 0.5272 | DEAD | | -321.709 | -52.421 | 0. |
| 38 | 0. | SIMM_KA | | -12.661 | 121.687 | 0. |
| 38 | 0.2636 | SIMM_KA | | -12.661 | 107.178 | 0. |
| 38 | 0.5272 | SIMM_KA | | -12.661 | 93.184 | 0. |
| 38 | 0. | SIMM_K0 | | -19.338 | 183.934 | 0. |
| 38 | 0.2636 | SIMM_K0 | | -19.338 | 162.171 | 0. |
| 38 | 0.5272 | SIMM_K0 | | -19.338 | 141.181 | 0. |
| 38 | 0. | A--SIMM_KA | | 22.454 | 168.091 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 38 | 0.2636 | A--SIMM_KA | | 22.454 | 145.54 | 0. |
| 38 | 0.5272 | A--SIMM_KA | | 22.454 | 123.501 | 0. |
| 38 | 0. | A--SIMM_K0 | | 32.768 | 257.974 | 0. |
| 38 | 0.2636 | A--SIMM_K0 | | 32.768 | 224.166 | 0. |
| 38 | 0.5272 | A--SIMM_K0 | | 32.768 | 191.162 | 0. |
| 38 | 0. | A-- SIMM_SOVR_K A | | -1.65 | 9.148 | 0. |
| 38 | 0.2636 | A-- SIMM_SOVR_K A | | -1.65 | 9.148 | 0. |
| 38 | 0.5272 | A-- SIMM_SOVR_K A | | -1.65 | 9.148 | 0. |
| 38 | 0. | A-- SIMM_SOVR_K 0 | | -2.474 | 13.715 | 0. |
| 38 | 0.2636 | A-- SIMM_SOVR_K 0 | | -2.474 | 13.715 | 0. |
| 38 | 0.5272 | A-- SIMM_SOVR_K 0 | | -2.474 | 13.715 | 0. |
| 38 | 0. | A-- SIMM_SOVR_K 0 | | -2.474 | 13.715 | 0. |
| 38 | 0.2636 | A-- SIMM_SOVR_K 0 | | -2.474 | 13.715 | 0. |
| 38 | 0.5272 | A-- SIMM_SOVR_K 0 | | -2.474 | 13.715 | 0. |
| 38 | 0. | A-- SIMM_SOVR_K A | | -1.65 | 9.148 | 0. |
| 38 | 0.2636 | A-- SIMM_SOVR_K A | | -1.65 | 9.148 | 0. |
| 38 | 0.5272 | A-- SIMM_SOVR_K A | | -1.65 | 9.148 | 0. |
| 38 | 0. | SOVR | | -195.416 | -23.224 | 0. |
| 38 | 0.2636 | SOVR | | -195.416 | -23.224 | 0. |
| 38 | 0.5272 | SOVR | | -195.416 | -23.224 | 0. |
| 38 | 0. | TERR_SIMM | | -781.351 | -67.962 | 0. |
| 38 | 0.2636 | TERR_SIMM | | -781.351 | -67.962 | 0. |
| 38 | 0.5272 | TERR_SIMM | | -781.351 | -67.962 | 0. |
| 38 | 0. | TERR_A--SIMM | | -1243.062 | -98.62 | 0. |
| 38 | 0.2636 | TERR_A--SIMM | | -1243.062 | -98.62 | 0. |
| 38 | 0.5272 | TERR_A--SIMM | | -1243.062 | -98.62 | 0. |
| 38 | 0. | INERZIA H SLV | | 4.991 | -4.282 | 0. |
| 38 | 0.2636 | INERZIA H SLV | | 4.991 | -4.282 | 0. |
| 38 | 0.5272 | INERZIA H SLV | | 4.991 | -4.282 | 0. |
| 38 | 0. | INERZIA V + SLV | | -5.359 | -0.827 | 0. |
| 38 | 0.2636 | INERZIA V + SLV | | -5.359 | -0.827 | 0. |
| 38 | 0.5272 | INERZIA V + SLV | | -5.359 | -0.827 | 0. |
| 38 | 0. | INERZIA V - SLV | | 5.359 | 0.827 | 0. |
| 38 | 0.2636 | INERZIA V - SLV | | 5.359 | 0.827 | 0. |
| 38 | 0.5272 | INERZIA V - SLV | | 5.359 | 0.827 | 0. |
| 38 | 0. | SISMA WOOD SLV | | 191.868 | -44.1 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 38 | 0.2636 | SISMA WOOD SLV | | 191.868 | -62.484 | 0. |
| 38 | 0.5272 | SISMA WOOD SLV | | 191.868 | -80.867 | 0. |
| 38 | 0. | iDROSTATICA | | -362.043 | 374.269 | 0. |
| 38 | 0.2636 | iDROSTATICA | | -362.043 | 343.615 | 0. |
| 38 | 0.5272 | iDROSTATICA | | -362.043 | 313.675 | 0. |
| 38 | 0. | SISMA WOOD SLD | | 84.737 | -19.476 | 0. |
| 38 | 0.2636 | SISMA WOOD SLD | | 84.737 | -27.595 | 0. |
| 38 | 0.5272 | SISMA WOOD SLD | | 84.737 | -35.714 | 0. |
| 38 | 0. | INERZIA H SLD | | 2.204 | -1.891 | 0. |
| 38 | 0.2636 | INERZIA H SLD | | 2.204 | -1.891 | 0. |
| 38 | 0.5272 | INERZIA H SLD | | 2.204 | -1.891 | 0. |
| 38 | 0. | INERZIA V + SLD | | -2.367 | -0.365 | 0. |
| 38 | 0.2636 | INERZIA V + SLD | | -2.367 | -0.365 | 0. |
| 38 | 0.5272 | INERZIA V + SLD | | -2.367 | -0.365 | 0. |
| 38 | 0. | INERZIA V SLD | | 2.367 | 0.365 | 0. |
| 38 | 0.2636 | INERZIA V SLD | | 2.367 | 0.365 | 0. |
| 38 | 0.5272 | INERZIA V SLD | | 2.367 | 0.365 | 0. |
| 38 | 0. | INERZIA V -1 | | 5.359 | 0.827 | 0. |
| 38 | 0.2636 | INERZIA V -1 | | 5.359 | 0.827 | 0. |
| 38 | 0.5272 | INERZIA V -1 | | 5.359 | 0.827 | 0. |
| 38 | 0. | SLU_1 | Max | -2459.848 | 539.559 | 0. |
| 38 | 0.2636 | SLU_1 | Max | -2447.002 | 471.416 | 0. |
| 38 | 0.5272 | SLU_1 | Max | -2434.155 | 405.208 | 0. |
| 38 | 0. | SLU_1 | Min | -2459.848 | 539.559 | 0. |
| 38 | 0.2636 | SLU_1 | Min | -2447.002 | 471.416 | 0. |
| 38 | 0.5272 | SLU_1 | Min | -2434.155 | 405.208 | 0. |
| 38 | 0. | SLU_2 | Max | -2460.396 | 455.135 | 0. |
| 38 | 0.2636 | SLU_2 | Max | -2447.549 | 396.422 | 0. |
| 38 | 0.5272 | SLU_2 | Max | -2434.702 | 339.309 | 0. |
| 38 | 0. | SLU_2 | Min | -2460.396 | 455.135 | 0. |
| 38 | 0.2636 | SLU_2 | Min | -2447.549 | 396.422 | 0. |
| 38 | 0.5272 | SLU_2 | Min | -2434.702 | 339.309 | 0. |
| 38 | 0. | SLU_3 | Max | -3063.327 | 597.906 | 0. |
| 38 | 0.2636 | SLU_3 | Max | -3050.481 | 514.105 | 0. |
| 38 | 0.5272 | SLU_3 | Max | -3037.634 | 432.279 | 0. |
| 38 | 0. | SLU_3 | Min | -3063.327 | 597.906 | 0. |
| 38 | 0.2636 | SLU_3 | Min | -3050.481 | 514.105 | 0. |
| 38 | 0.5272 | SLU_3 | Min | -3037.634 | 432.279 | 0. |
| 38 | 0. | SLU_4 | Max | -3079.024 | 469.927 | 0. |
| 38 | 0.2636 | SLU_4 | Max | -3066.177 | 400.76 | 0. |
| 38 | 0.5272 | SLU_4 | Max | -3053.331 | 333.187 | 0. |
| 38 | 0. | SLU_4 | Min | -3079.024 | 469.927 | 0. |
| 38 | 0.2636 | SLU_4 | Min | -3066.177 | 400.76 | 0. |
| 38 | 0.5272 | SLU_4 | Min | -3053.331 | 333.187 | 0. |
| 38 | 0. | SLE_F1 | Max | -1801.171 | 423.116 | 0. |
| 38 | 0.2636 | SLE_F1 | Max | -1791.289 | 370.698 | 0. |
| 38 | 0.5272 | SLE_F1 | Max | -1781.406 | 319.769 | 0. |
| 38 | 0. | SLE_F1 | Min | -1801.171 | 423.116 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 38 | 0.2636 | SLE_F1 | Min | -1791.289 | 370.698 | 0. |
| 38 | 0.5272 | SLE_F1 | Min | -1781.406 | 319.769 | 0. |
| 38 | 0. | SLE_F2 | Max | -1801.541 | 360.76 | 0. |
| 38 | 0.2636 | SLE_F2 | Max | -1791.658 | 315.596 | 0. |
| 38 | 0.5272 | SLE_F2 | Max | -1781.776 | 271.663 | 0. |
| 38 | 0. | SLE_F2 | Min | -1801.541 | 360.76 | 0. |
| 38 | 0.2636 | SLE_F2 | Min | -1791.658 | 315.596 | 0. |
| 38 | 0.5272 | SLE_F2 | Min | -1781.776 | 271.663 | 0. |
| 38 | 0. | SLE_F3 | Max | -2277.41 | 371.554 | 0. |
| 38 | 0.2636 | SLE_F3 | Max | -2267.528 | 318.349 | 0. |
| 38 | 0.5272 | SLE_F3 | Max | -2257.646 | 266.37 | 0. |
| 38 | 0. | SLE_F3 | Min | -2277.41 | 371.554 | 0. |
| 38 | 0.2636 | SLE_F3 | Min | -2267.528 | 318.349 | 0. |
| 38 | 0.5272 | SLE_F3 | Min | -2257.646 | 266.37 | 0. |
| 38 | 0. | SLE_F4 | Max | -2265.532 | 472.818 | 0. |
| 38 | 0.2636 | SLE_F4 | Max | -2255.65 | 408.356 | 0. |
| 38 | 0.5272 | SLE_F4 | Max | -2245.768 | 345.412 | 0. |
| 38 | 0. | SLE_F4 | Min | -2265.532 | 472.818 | 0. |
| 38 | 0.2636 | SLE_F4 | Min | -2255.65 | 408.356 | 0. |
| 38 | 0.5272 | SLE_F4 | Min | -2245.768 | 345.412 | 0. |
| 38 | 0. | SLE_QP1 | Max | -1631.881 | 439.552 | 0. |
| 38 | 0.2636 | SLE_QP1 | Max | -1621.999 | 387.134 | 0. |
| 38 | 0.5272 | SLE_QP1 | Max | -1612.117 | 336.205 | 0. |
| 38 | 0. | SLE_QP1 | Min | -1631.881 | 439.552 | 0. |
| 38 | 0.2636 | SLE_QP1 | Min | -1621.999 | 387.134 | 0. |
| 38 | 0.5272 | SLE_QP1 | Min | -1612.117 | 336.205 | 0. |
| 38 | 0. | SLE_QP2 | Max | -1632.408 | 380.552 | 0. |
| 38 | 0.2636 | SLE_QP2 | Max | -1622.526 | 335.388 | 0. |
| 38 | 0.5272 | SLE_QP2 | Max | -1612.644 | 291.455 | 0. |
| 38 | 0. | SLE_QP2 | Min | -1632.408 | 380.552 | 0. |
| 38 | 0.2636 | SLE_QP2 | Min | -1622.526 | 335.388 | 0. |
| 38 | 0.5272 | SLE_QP2 | Min | -1612.644 | 291.455 | 0. |
| 38 | 0. | SLE_QP3 | Max | -2108.281 | 390.258 | 0. |
| 38 | 0.2636 | SLE_QP3 | Max | -2098.399 | 337.053 | 0. |
| 38 | 0.5272 | SLE_QP3 | Max | -2088.517 | 285.074 | 0. |
| 38 | 0. | SLE_QP3 | Min | -2108.281 | 390.258 | 0. |
| 38 | 0.2636 | SLE_QP3 | Min | -2098.399 | 337.053 | 0. |
| 38 | 0.5272 | SLE_QP3 | Min | -2088.517 | 285.074 | 0. |
| 38 | 0. | SLE_QP4 | Max | -2096.94 | 498.042 | 0. |
| 38 | 0.2636 | SLE_QP4 | Max | -2087.058 | 433.58 | 0. |
| 38 | 0.5272 | SLE_QP4 | Max | -2077.175 | 370.636 | 0. |
| 38 | 0. | SLE_QP4 | Min | -2096.94 | 498.042 | 0. |
| 38 | 0.2636 | SLE_QP4 | Min | -2087.058 | 433.58 | 0. |
| 38 | 0.5272 | SLE_QP4 | Min | -2077.175 | 370.636 | 0. |
| 38 | 0. | SLV_1 | Max | -1535.554 | 746.641 | 0. |
| 38 | 0.2636 | SLV_1 | Max | -1525.672 | 675.84 | 0. |
| 38 | 0.5272 | SLV_1 | Max | -1515.79 | 606.528 | 0. |
| 38 | 0. | SLV_1 | Min | -1535.554 | 746.641 | 0. |
| 38 | 0.2636 | SLV_1 | Min | -1525.672 | 675.84 | 0. |
| 38 | 0.5272 | SLV_1 | Min | -1515.79 | 606.528 | 0. |
| 38 | 0. | SLV_2 | Max | -1523.615 | 748.714 | 0. |
| 38 | 0.2636 | SLV_2 | Max | -1513.733 | 677.913 | 0. |
| 38 | 0.5272 | SLV_2 | Max | -1503.851 | 608.6 | 0. |
| 38 | 0. | SLV_2 | Min | -1523.615 | 748.714 | 0. |
| 38 | 0.2636 | SLV_2 | Min | -1513.733 | 677.913 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 38 | 0.5272 | SLV_2 | Min | -1503.851 | 608.6 | 0. |
| 38 | 0. | SLV_3 | Max | -2018.108 | 884.887 | 0. |
| 38 | 0.2636 | SLV_3 | Max | -2008.226 | 802.041 | 0. |
| 38 | 0.5272 | SLV_3 | Max | -1998.344 | 720.714 | 0. |
| 38 | 0. | SLV_3 | Min | -2018.108 | 884.887 | 0. |
| 38 | 0.2636 | SLV_3 | Min | -2008.226 | 802.041 | 0. |
| 38 | 0.5272 | SLV_3 | Min | -1998.344 | 720.714 | 0. |
| 38 | 0. | SLV_4 | Max | -2005.91 | 886.984 | 0. |
| 38 | 0.2636 | SLV_4 | Max | -1996.028 | 804.138 | 0. |
| 38 | 0.5272 | SLV_4 | Max | -1986.146 | 722.811 | 0. |
| 38 | 0. | SLV_4 | Min | -2005.91 | 886.984 | 0. |
| 38 | 0.2636 | SLV_4 | Min | -1996.028 | 804.138 | 0. |
| 38 | 0.5272 | SLV_4 | Min | -1986.146 | 722.811 | 0. |
| 38 | 0. | SLD_1 | Max | -1575.271 | 535.249 | 0. |
| 38 | 0.2636 | SLD_1 | Max | -1565.389 | 474.712 | 0. |
| 38 | 0.5272 | SLD_1 | Max | -1555.507 | 415.664 | 0. |
| 38 | 0. | SLD_1 | Min | -1575.271 | 535.249 | 0. |
| 38 | 0.2636 | SLD_1 | Min | -1565.389 | 474.712 | 0. |
| 38 | 0.5272 | SLD_1 | Min | -1555.507 | 415.664 | 0. |
| 38 | 0. | SLD_2 | Max | -1569.713 | 536.55 | 0. |
| 38 | 0.2636 | SLD_2 | Max | -1559.831 | 476.013 | 0. |
| 38 | 0.5272 | SLD_2 | Max | -1549.949 | 416.965 | 0. |
| 38 | 0. | SLD_2 | Min | -1569.713 | 536.55 | 0. |
| 38 | 0.2636 | SLD_2 | Min | -1559.831 | 476.013 | 0. |
| 38 | 0.5272 | SLD_2 | Min | -1549.949 | 416.965 | 0. |
| 38 | 0. | SLD_3 | Max | -2053.857 | 673.628 | 0. |
| 38 | 0.2636 | SLD_3 | Max | -2043.974 | 601.046 | 0. |
| 38 | 0.5272 | SLD_3 | Max | -2034.092 | 529.984 | 0. |
| 38 | 0. | SLD_3 | Min | -2053.857 | 673.628 | 0. |
| 38 | 0.2636 | SLD_3 | Min | -2043.974 | 601.046 | 0. |
| 38 | 0.5272 | SLD_3 | Min | -2034.092 | 529.984 | 0. |
| 38 | 0. | SLD_4 | Max | -2048.391 | 674.65 | 0. |
| 38 | 0.2636 | SLD_4 | Max | -2038.509 | 602.069 | 0. |
| 38 | 0.5272 | SLD_4 | Max | -2028.627 | 531.006 | 0. |
| 38 | 0. | SLD_4 | Min | -2048.391 | 674.65 | 0. |
| 38 | 0.2636 | SLD_4 | Min | -2038.509 | 602.069 | 0. |
| 38 | 0.5272 | SLD_4 | Min | -2028.627 | 531.006 | 0. |
| 38 | 0. | SLU_IDR_1 | Max | -1963.725 | 450.886 | 0. |
| 38 | 0.2636 | SLU_IDR_1 | Max | -1954.831 | 396.871 | 0. |
| 38 | 0.5272 | SLU_IDR_1 | Max | -1945.937 | 344.102 | 0. |
| 38 | 0. | SLU_IDR_1 | Min | -1963.725 | 450.886 | 0. |
| 38 | 0.2636 | SLU_IDR_1 | Min | -1954.831 | 396.871 | 0. |
| 38 | 0.5272 | SLU_IDR_1 | Min | -1945.937 | 344.102 | 0. |
| 38 | 0. | SLU_IDR_2 | Max | -1536.444 | 446.139 | 0. |
| 38 | 0.2636 | SLU_IDR_2 | Max | -1527.55 | 399.361 | 0. |
| 38 | 0.5272 | SLU_IDR_2 | Max | -1518.656 | 353.833 | 0. |
| 38 | 0. | SLU_IDR_2 | Min | -1536.444 | 446.139 | 0. |
| 38 | 0.2636 | SLU_IDR_2 | Min | -1527.55 | 399.361 | 0. |
| 38 | 0.5272 | SLU_IDR_2 | Min | -1518.656 | 353.833 | 0. |
| 38 | 0. | SISMA WOOD SLV-1 | Max | -27.863 | 274.48 | 0. |
| 38 | 0.2636 | SISMA WOOD SLV-1 | Max | -27.863 | 256.097 | 0. |
| 38 | 0.5272 | SISMA WOOD SLV-1 | Max | -27.863 | 237.714 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 38 | 0. | SISMA WOOD SLV-1 | Min | -27.863 | 274.48 | 0. |
| 38 | 0.2636 | SISMA WOOD SLV-1 | Min | -27.863 | 256.097 | 0. |
| 38 | 0.5272 | SISMA WOOD SLV-1 | Min | -27.863 | 237.714 | 0. |
| 38 | 0. | DEAD-1 | Max | -406.165 | -62.409 | 0. |
| 38 | 0.2636 | DEAD-1 | Max | -396.283 | -62.409 | 0. |
| 38 | 0.5272 | DEAD-1 | Max | -386.401 | -62.409 | 0. |
| 38 | 0. | DEAD-1 | Min | -406.165 | -62.409 | 0. |
| 38 | 0.2636 | DEAD-1 | Min | -396.283 | -62.409 | 0. |
| 38 | 0.5272 | DEAD-1 | Min | -386.401 | -62.409 | 0. |
| 38 | 0. | SLU_PROVA | | -2252.301 | 554.903 | 0. |
| 38 | 0.2636 | SLU_PROVA | | -2239.455 | 486.76 | 0. |
| 38 | 0.5272 | SLU_PROVA | | -2226.608 | 420.552 | 0. |
| 39 | 0. | DEAD | | -321.709 | -55.697 | 0. |
| 39 | 0.2636 | DEAD | | -311.827 | -55.697 | 0. |
| 39 | 0.5272 | DEAD | | -301.945 | -55.697 | 0. |
| 39 | 0. | SIMM_KA | | -12.661 | 100.455 | 0. |
| 39 | 0.2636 | SIMM_KA | | -12.661 | 86.943 | 0. |
| 39 | 0.5272 | SIMM_KA | | -12.661 | 73.879 | 0. |
| 39 | 0. | SIMM_K0 | | -19.338 | 152.293 | 0. |
| 39 | 0.2636 | SIMM_K0 | | -19.338 | 132.025 | 0. |
| 39 | 0.5272 | SIMM_K0 | | -19.338 | 112.429 | 0. |
| 39 | 0. | A--SIMM_KA | | 22.454 | 149.673 | 0. |
| 39 | 0.2636 | A--SIMM_KA | | 22.454 | 128.437 | 0. |
| 39 | 0.5272 | A--SIMM_KA | | 22.454 | 108.296 | 0. |
| 39 | 0. | A--SIMM_K0 | | 32.768 | 229.678 | 0. |
| 39 | 0.2636 | A--SIMM_K0 | | 32.768 | 197.477 | 0. |
| 39 | 0.5272 | A--SIMM_K0 | | 32.768 | 166.079 | 0. |
| 39 | 0. | A-- SIMM_SOVR_K A | | -1.65 | 10.02 | 0. |
| 39 | 0.2636 | A-- SIMM_SOVR_K A | | -1.65 | 10.02 | 0. |
| 39 | 0.5272 | A-- SIMM_SOVR_K A | | -1.65 | 10.02 | 0. |
| 39 | 0. | A-- SIMM_SOVR_K 0 | | -2.474 | 15.023 | 0. |
| 39 | 0.2636 | A-- SIMM_SOVR_K 0 | | -2.474 | 15.023 | 0. |
| 39 | 0.5272 | A-- SIMM_SOVR_K 0 | | -2.474 | 15.023 | 0. |
| 39 | 0. | SIMM_SOVR_K 0 | | -2.474 | 15.023 | 0. |
| 39 | 0.2636 | SIMM_SOVR_K 0 | | -2.474 | 15.023 | 0. |
| 39 | 0.5272 | SIMM_SOVR_K 0 | | -2.474 | 15.023 | 0. |
| 39 | 0. | SIMM_SOVR_K A | | -1.65 | 10.02 | 0. |
| 39 | 0.2636 | SIMM_SOVR_K A | | -1.65 | 10.02 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 39 | 0.5272 | SIMM_SOVR_K A | | -1.65 | 10.02 | 0. |
| 39 | 0. | SOVR | | -195.416 | -28.22 | 0. |
| 39 | 0.2636 | SOVR | | -195.416 | -28.22 | 0. |
| 39 | 0.5272 | SOVR | | -195.416 | -28.22 | 0. |
| 39 | 0. | TERR_SIMM | | -781.351 | -85.569 | 0. |
| 39 | 0.2636 | TERR_SIMM | | -781.351 | -85.569 | 0. |
| 39 | 0.5272 | TERR_SIMM | | -781.351 | -85.569 | 0. |
| 39 | 0. | TERR_A--SIMM | | -1243.062 | -121.27 | 0. |
| 39 | 0.2636 | TERR_A--SIMM | | -1243.062 | -121.27 | 0. |
| 39 | 0.5272 | TERR_A--SIMM | | -1243.062 | -121.27 | 0. |
| 39 | 0. | INERZIA H SLV | | 4.991 | -2.113 | 0. |
| 39 | 0.2636 | INERZIA H SLV | | 4.991 | -2.113 | 0. |
| 39 | 0.5272 | INERZIA H SLV | | 4.991 | -2.113 | 0. |
| 39 | 0. | INERZIA V + SLV | | -5.04 | -0.88 | 0. |
| 39 | 0.2636 | INERZIA V + SLV | | -5.04 | -0.88 | 0. |
| 39 | 0.5272 | INERZIA V + SLV | | -5.04 | -0.88 | 0. |
| 39 | 0. | INERZIA V - SLV | | 5.04 | 0.88 | 0. |
| 39 | 0.2636 | INERZIA V - SLV | | 5.04 | 0.88 | 0. |
| 39 | 0.5272 | INERZIA V - SLV | | 5.04 | 0.88 | 0. |
| 39 | 0. | SISMA WOOD SLV | | 191.868 | 26.346 | 0. |
| 39 | 0.2636 | SISMA WOOD SLV | | 191.868 | 7.963 | 0. |
| 39 | 0.5272 | SISMA WOOD SLV | | 191.868 | -10.421 | 0. |
| 39 | 0. | iDROSTATICA | | -362.043 | 303.44 | 0. |
| 39 | 0.2636 | iDROSTATICA | | -362.043 | 274.216 | 0. |
| 39 | 0.5272 | iDROSTATICA | | -362.043 | 245.706 | 0. |
| 39 | 0. | SISMA WOOD SLD | | 84.737 | 11.635 | 0. |
| 39 | 0.2636 | SISMA WOOD SLD | | 84.737 | 3.517 | 0. |
| 39 | 0.5272 | SISMA WOOD SLD | | 84.737 | -4.602 | 0. |
| 39 | 0. | INERZIA H SLD | | 2.204 | -0.933 | 0. |
| 39 | 0.2636 | INERZIA H SLD | | 2.204 | -0.933 | 0. |
| 39 | 0.5272 | INERZIA H SLD | | 2.204 | -0.933 | 0. |
| 39 | 0. | INERZIA V + SLD | | -2.226 | -0.388 | 0. |
| 39 | 0.2636 | INERZIA V + SLD | | -2.226 | -0.388 | 0. |
| 39 | 0.5272 | INERZIA V + SLD | | -2.226 | -0.388 | 0. |
| 39 | 0. | INERZIA V SLD | | 2.226 | 0.388 | 0. |
| 39 | 0.2636 | INERZIA V SLD | | 2.226 | 0.388 | 0. |
| 39 | 0.5272 | INERZIA V SLD | | 2.226 | 0.388 | 0. |
| 39 | 0. | INERZIA V -1 | | 5.04 | 0.88 | 0. |
| 39 | 0.2636 | INERZIA V -1 | | 5.04 | 0.88 | 0. |
| 39 | 0.5272 | INERZIA V -1 | | 5.04 | 0.88 | 0. |
| 39 | 0. | SLU_1 | Max | -2434.155 | 365.043 | 0. |
| 39 | 0.2636 | SLU_1 | Max | -2421.308 | 300.703 | 0. |
| 39 | 0.5272 | SLU_1 | Max | -2408.462 | 238.165 | 0. |
| 39 | 0. | SLU_1 | Min | -2434.155 | 365.043 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 39 | 0.2636 | SLU_1 | Min | -2421.308 | 300.703 | 0. |
| 39 | 0.5272 | SLU_1 | Min | -2408.462 | 238.165 | 0. |
| 39 | 0. | SLU_2 | Max | -2434.702 | 291.737 | 0. |
| 39 | 0.2636 | SLU_2 | Max | -2421.856 | 236.179 | 0. |
| 39 | 0.5272 | SLU_2 | Max | -2409.009 | 182.133 | 0. |
| 39 | 0. | SLU_2 | Min | -2434.702 | 291.737 | 0. |
| 39 | 0.2636 | SLU_2 | Min | -2421.856 | 236.179 | 0. |
| 39 | 0.5272 | SLU_2 | Min | -2409.009 | 182.133 | 0. |
| 39 | 0. | SLU_3 | Max | -3037.634 | 431.897 | 0. |
| 39 | 0.2636 | SLU_3 | Max | -3024.787 | 352.044 | 0. |
| 39 | 0.5272 | SLU_3 | Max | -3011.94 | 274.163 | 0. |
| 39 | 0. | SLU_3 | Min | -3037.634 | 431.897 | 0. |
| 39 | 0.2636 | SLU_3 | Min | -3024.787 | 352.044 | 0. |
| 39 | 0.5272 | SLU_3 | Min | -3011.94 | 274.163 | 0. |
| 39 | 0. | SLU_4 | Max | -3053.331 | 310.323 | 0. |
| 39 | 0.2636 | SLU_4 | Max | -3040.484 | 244.724 | 0. |
| 39 | 0.5272 | SLU_4 | Max | -3027.637 | 181.478 | 0. |
| 39 | 0. | SLU_4 | Min | -3053.331 | 310.323 | 0. |
| 39 | 0.2636 | SLU_4 | Min | -3040.484 | 244.724 | 0. |
| 39 | 0.5272 | SLU_4 | Min | -3027.637 | 181.478 | 0. |
| 39 | 0. | SLE_F1 | Max | -1781.406 | 290.51 | 0. |
| 39 | 0.2636 | SLE_F1 | Max | -1771.524 | 241.017 | 0. |
| 39 | 0.5272 | SLE_F1 | Max | -1761.642 | 192.911 | 0. |
| 39 | 0. | SLE_F1 | Min | -1781.406 | 290.51 | 0. |
| 39 | 0.2636 | SLE_F1 | Min | -1771.524 | 241.017 | 0. |
| 39 | 0.5272 | SLE_F1 | Min | -1761.642 | 192.911 | 0. |
| 39 | 0. | SLE_F2 | Max | -1781.776 | 236.847 | 0. |
| 39 | 0.2636 | SLE_F2 | Max | -1771.894 | 194.11 | 0. |
| 39 | 0.5272 | SLE_F2 | Max | -1762.012 | 152.536 | 0. |
| 39 | 0. | SLE_F2 | Min | -1781.776 | 236.847 | 0. |
| 39 | 0.2636 | SLE_F2 | Min | -1771.894 | 194.11 | 0. |
| 39 | 0.5272 | SLE_F2 | Min | -1762.012 | 152.536 | 0. |
| 39 | 0. | SLE_F3 | Max | -2257.646 | 250.549 | 0. |
| 39 | 0.2636 | SLE_F3 | Max | -2247.764 | 200.088 | 0. |
| 39 | 0.5272 | SLE_F3 | Max | -2237.882 | 151.437 | 0. |
| 39 | 0. | SLE_F3 | Min | -2257.646 | 250.549 | 0. |
| 39 | 0.2636 | SLE_F3 | Min | -2247.764 | 200.088 | 0. |
| 39 | 0.5272 | SLE_F3 | Min | -2237.882 | 151.437 | 0. |
| 39 | 0. | SLE_F4 | Max | -2245.768 | 345.412 | 0. |
| 39 | 0.2636 | SLE_F4 | Max | -2235.886 | 283.987 | 0. |
| 39 | 0.5272 | SLE_F4 | Max | -2226.004 | 224.079 | 0. |
| 39 | 0. | SLE_F4 | Min | -2245.768 | 345.412 | 0. |
| 39 | 0.2636 | SLE_F4 | Min | -2235.886 | 283.987 | 0. |
| 39 | 0.5272 | SLE_F4 | Min | -2226.004 | 224.079 | 0. |
| 39 | 0. | SLE_QP1 | Max | -1612.117 | 309.789 | 0. |
| 39 | 0.2636 | SLE_QP1 | Max | -1602.235 | 260.297 | 0. |
| 39 | 0.5272 | SLE_QP1 | Max | -1592.352 | 212.19 | 0. |
| 39 | 0. | SLE_QP1 | Min | -1612.117 | 309.789 | 0. |
| 39 | 0.2636 | SLE_QP1 | Min | -1602.235 | 260.297 | 0. |
| 39 | 0.5272 | SLE_QP1 | Min | -1592.352 | 212.19 | 0. |
| 39 | 0. | SLE_QP2 | Max | -1612.644 | 259.94 | 0. |
| 39 | 0.2636 | SLE_QP2 | Max | -1602.762 | 217.203 | 0. |
| 39 | 0.5272 | SLE_QP2 | Max | -1592.88 | 175.629 | 0. |
| 39 | 0. | SLE_QP2 | Min | -1612.644 | 259.94 | 0. |
| 39 | 0.2636 | SLE_QP2 | Min | -1602.762 | 217.203 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 39 | 0.5272 | SLE_QP2 | Min | -1592.88 | 175.629 | 0. |
| 39 | 0. | SLE_QP3 | Max | -2088.517 | 272.536 | 0. |
| 39 | 0.2636 | SLE_QP3 | Max | -2078.635 | 222.075 | 0. |
| 39 | 0.5272 | SLE_QP3 | Max | -2068.753 | 173.424 | 0. |
| 39 | 0. | SLE_QP3 | Min | -2088.517 | 272.536 | 0. |
| 39 | 0.2636 | SLE_QP3 | Min | -2078.635 | 222.075 | 0. |
| 39 | 0.5272 | SLE_QP3 | Min | -2068.753 | 173.424 | 0. |
| 39 | 0. | SLE_QP4 | Max | -2077.175 | 370.638 | 0. |
| 39 | 0.2636 | SLE_QP4 | Max | -2067.293 | 309.213 | 0. |
| 39 | 0.5272 | SLE_QP4 | Max | -2057.411 | 249.305 | 0. |
| 39 | 0. | SLE_QP4 | Min | -2077.175 | 370.638 | 0. |
| 39 | 0.2636 | SLE_QP4 | Min | -2067.293 | 309.213 | 0. |
| 39 | 0.5272 | SLE_QP4 | Min | -2057.411 | 249.305 | 0. |
| 39 | 0. | SLV_1 | Max | -1515.471 | 605.921 | 0. |
| 39 | 0.2636 | SLV_1 | Max | -1505.588 | 538.045 | 0. |
| 39 | 0.5272 | SLV_1 | Max | -1495.706 | 471.555 | 0. |
| 39 | 0. | SLV_1 | Min | -1515.471 | 605.921 | 0. |
| 39 | 0.2636 | SLV_1 | Min | -1505.588 | 538.045 | 0. |
| 39 | 0.5272 | SLV_1 | Min | -1495.706 | 471.555 | 0. |
| 39 | 0. | SLV_2 | Max | -1504.171 | 607.994 | 0. |
| 39 | 0.2636 | SLV_2 | Max | -1494.289 | 540.118 | 0. |
| 39 | 0.5272 | SLV_2 | Max | -1484.406 | 473.628 | 0. |
| 39 | 0. | SLV_2 | Min | -1504.171 | 607.994 | 0. |
| 39 | 0.2636 | SLV_2 | Min | -1494.289 | 540.118 | 0. |
| 39 | 0.5272 | SLV_2 | Min | -1484.406 | 473.628 | 0. |
| 39 | 0. | SLV_3 | Max | -1998.025 | 720.116 | 0. |
| 39 | 0.2636 | SLV_3 | Max | -1988.143 | 640.307 | 0. |
| 39 | 0.5272 | SLV_3 | Max | -1978.261 | 562.016 | 0. |
| 39 | 0. | SLV_3 | Min | -1998.025 | 720.116 | 0. |
| 39 | 0.2636 | SLV_3 | Min | -1988.143 | 640.307 | 0. |
| 39 | 0.5272 | SLV_3 | Min | -1978.261 | 562.016 | 0. |
| 39 | 0. | SLV_4 | Max | -1986.465 | 722.213 | 0. |
| 39 | 0.2636 | SLV_4 | Max | -1976.583 | 642.404 | 0. |
| 39 | 0.5272 | SLV_4 | Max | -1966.701 | 564.113 | 0. |
| 39 | 0. | SLV_4 | Min | -1986.465 | 722.213 | 0. |
| 39 | 0.2636 | SLV_4 | Min | -1976.583 | 642.404 | 0. |
| 39 | 0.5272 | SLV_4 | Min | -1966.701 | 564.113 | 0. |
| 39 | 0. | SLD_1 | Max | -1555.366 | 415.399 | 0. |
| 39 | 0.2636 | SLD_1 | Max | -1545.483 | 357.788 | 0. |
| 39 | 0.5272 | SLD_1 | Max | -1535.601 | 301.562 | 0. |
| 39 | 0. | SLD_1 | Min | -1555.366 | 415.399 | 0. |
| 39 | 0.2636 | SLD_1 | Min | -1545.483 | 357.788 | 0. |
| 39 | 0.5272 | SLD_1 | Min | -1535.601 | 301.562 | 0. |
| 39 | 0. | SLD_2 | Max | -1550.09 | 416.7 | 0. |
| 39 | 0.2636 | SLD_2 | Max | -1540.208 | 359.089 | 0. |
| 39 | 0.5272 | SLD_2 | Max | -1530.326 | 302.863 | 0. |
| 39 | 0. | SLD_2 | Min | -1550.09 | 416.7 | 0. |
| 39 | 0.2636 | SLD_2 | Min | -1540.208 | 359.089 | 0. |
| 39 | 0.5272 | SLD_2 | Min | -1530.326 | 302.863 | 0. |
| 39 | 0. | SLD_3 | Max | -2033.951 | 529.734 | 0. |
| 39 | 0.2636 | SLD_3 | Max | -2024.069 | 460.19 | 0. |
| 39 | 0.5272 | SLD_3 | Max | -2014.187 | 392.163 | 0. |
| 39 | 0. | SLD_3 | Min | -2033.951 | 529.734 | 0. |
| 39 | 0.2636 | SLD_3 | Min | -2024.069 | 460.19 | 0. |
| 39 | 0.5272 | SLD_3 | Min | -2014.187 | 392.163 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 39 | 0. | SLD_4 | Max | -2028.768 | 530.756 | 0. |
| 39 | 0.2636 | SLD_4 | Max | -2018.886 | 461.212 | 0. |
| 39 | 0.5272 | SLD_4 | Max | -2009.004 | 393.185 | 0. |
| 39 | 0. | SLD_4 | Min | -2028.768 | 530.756 | 0. |
| 39 | 0.2636 | SLD_4 | Min | -2018.886 | 461.212 | 0. |
| 39 | 0.5272 | SLD_4 | Min | -2009.004 | 393.185 | 0. |
| 39 | 0. | SLU_IDR_1 | Max | -1945.937 | 327.843 | 0. |
| 39 | 0.2636 | SLU_IDR_1 | Max | -1937.043 | 276.583 | 0. |
| 39 | 0.5272 | SLU_IDR_1 | Max | -1928.149 | 227.096 | 0. |
| 39 | 0. | SLU_IDR_1 | Min | -1945.937 | 327.843 | 0. |
| 39 | 0.2636 | SLU_IDR_1 | Min | -1937.043 | 276.583 | 0. |
| 39 | 0.5272 | SLU_IDR_1 | Min | -1928.149 | 227.096 | 0. |
| 39 | 0. | SLU_IDR_2 | Max | -1518.656 | 320.693 | 0. |
| 39 | 0.2636 | SLU_IDR_2 | Max | -1509.763 | 276.385 | 0. |
| 39 | 0.5272 | SLU_IDR_2 | Max | -1500.869 | 233.267 | 0. |
| 39 | 0. | SLU_IDR_2 | Min | -1518.656 | 320.693 | 0. |
| 39 | 0.2636 | SLU_IDR_2 | Min | -1509.763 | 276.385 | 0. |
| 39 | 0.5272 | SLU_IDR_2 | Min | -1500.869 | 233.267 | 0. |
| 39 | 0. | SISMA WOOD SLV-1 | Max | -27.863 | 237.714 | 0. |
| 39 | 0.2636 | SISMA WOOD SLV-1 | Max | -27.863 | 219.33 | 0. |
| 39 | 0.5272 | SISMA WOOD SLV-1 | Max | -27.863 | 200.947 | 0. |
| 39 | 0. | SISMA WOOD SLV-1 | Min | -27.863 | 237.714 | 0. |
| 39 | 0.2636 | SISMA WOOD SLV-1 | Min | -27.863 | 219.33 | 0. |
| 39 | 0.5272 | SISMA WOOD SLV-1 | Min | -27.863 | 200.947 | 0. |
| 39 | 0. | DEAD-1 | Max | -386.401 | -67.599 | 0. |
| 39 | 0.2636 | DEAD-1 | Max | -376.519 | -67.599 | 0. |
| 39 | 0.5272 | DEAD-1 | Max | -366.636 | -67.599 | 0. |
| 39 | 0. | DEAD-1 | Min | -386.401 | -67.599 | 0. |
| 39 | 0.2636 | DEAD-1 | Min | -376.519 | -67.599 | 0. |
| 39 | 0.5272 | DEAD-1 | Min | -366.636 | -67.599 | 0. |
| 39 | 0. | SLU_PROVA | | -2226.608 | 389.012 | 0. |
| 39 | 0.2636 | SLU_PROVA | | -2213.761 | 324.672 | 0. |
| 39 | 0.5272 | SLU_PROVA | | -2200.914 | 262.133 | 0. |
| 41 | 0. | DEAD | | -342.323 | 52.89 | 0. |
| 41 | 0.2636 | DEAD | | -332.441 | 52.89 | 0. |
| 41 | 0.5272 | DEAD | | -322.559 | 52.89 | 0. |
| 41 | 0. | SIMM_KA | | -12.176 | -121.863 | 0. |
| 41 | 0.2636 | SIMM_KA | | -12.176 | -107.354 | 0. |
| 41 | 0.5272 | SIMM_KA | | -12.176 | -93.36 | 0. |
| 41 | 0. | SIMM_K0 | | -18.659 | -184.175 | 0. |
| 41 | 0.2636 | SIMM_K0 | | -18.659 | -162.412 | 0. |
| 41 | 0.5272 | SIMM_K0 | | -18.659 | -141.422 | 0. |
| 41 | 0. | A--SIMM_KA | | -53.237 | -130.149 | 0. |
| 41 | 0.2636 | A--SIMM_KA | | -53.237 | -116.756 | 0. |
| 41 | 0.5272 | A--SIMM_KA | | -53.237 | -104.435 | 0. |
| 41 | 0. | A--SIMM_K0 | | -79.793 | -204.712 | 0. |
| 41 | 0.2636 | A--SIMM_K0 | | -79.793 | -184.181 | 0. |
| 41 | 0.5272 | A--SIMM_K0 | | -79.793 | -164.376 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 41 | 0. | A-- SIMM_SOVR_K A | | -1.62 | -9.163 | 0. |
| 41 | 0.2636 | A-- SIMM_SOVR_K A | | -1.62 | -9.163 | 0. |
| 41 | 0.5272 | A-- SIMM_SOVR_K A | | -1.62 | -9.163 | 0. |
| 41 | 0. | A-- SIMM_SOVR_K 0 | | -2.429 | -13.738 | 0. |
| 41 | 0.2636 | A-- SIMM_SOVR_K 0 | | -2.429 | -13.738 | 0. |
| 41 | 0.5272 | A-- SIMM_SOVR_K 0 | | -2.429 | -13.738 | 0. |
| 41 | 0. | SIMM_SOVR_K 0 | | -2.429 | -13.738 | 0. |
| 41 | 0.2636 | SIMM_SOVR_K 0 | | -2.429 | -13.738 | 0. |
| 41 | 0.5272 | SIMM_SOVR_K 0 | | -2.429 | -13.738 | 0. |
| 41 | 0. | SIMM_SOVR_K A | | -1.62 | -9.163 | 0. |
| 41 | 0.2636 | SIMM_SOVR_K A | | -1.62 | -9.163 | 0. |
| 41 | 0.5272 | SIMM_SOVR_K A | | -1.62 | -9.163 | 0. |
| 41 | 0. | SOVR | | -195.45 | 23.572 | 0. |
| 41 | 0.2636 | SOVR | | -195.45 | 23.572 | 0. |
| 41 | 0.5272 | SOVR | | -195.45 | 23.572 | 0. |
| 41 | 0. | TERR_SIMM | | -782.714 | 69.378 | 0. |
| 41 | 0.2636 | TERR_SIMM | | -782.714 | 69.378 | 0. |
| 41 | 0.5272 | TERR_SIMM | | -782.714 | 69.378 | 0. |
| 41 | 0. | TERR_A--SIMM | | -764.488 | 80.846 | 0. |
| 41 | 0.2636 | TERR_A--SIMM | | -764.488 | 80.846 | 0. |
| 41 | 0.5272 | TERR_A--SIMM | | -764.488 | 80.846 | 0. |
| 41 | 0. | INERZIA H SLV | | -4.979 | -4.249 | 0. |
| 41 | 0.2636 | INERZIA H SLV | | -4.979 | -4.249 | 0. |
| 41 | 0.5272 | INERZIA H SLV | | -4.979 | -4.249 | 0. |
| 41 | 0. | INERZIA V + SLV | | -5.373 | 0.834 | 0. |
| 41 | 0.2636 | INERZIA V + SLV | | -5.373 | 0.834 | 0. |
| 41 | 0.5272 | INERZIA V + SLV | | -5.373 | 0.834 | 0. |
| 41 | 0. | INERZIA V - SLV | | 5.373 | -0.834 | 0. |
| 41 | 0.2636 | INERZIA V - SLV | | 5.373 | -0.834 | 0. |
| 41 | 0.5272 | INERZIA V - SLV | | 5.373 | -0.834 | 0. |
| 41 | 0. | SISMA WOOD SLV | | -218.64 | -232.043 | 0. |
| 41 | 0.2636 | SISMA WOOD SLV | | -218.64 | -232.043 | 0. |
| 41 | 0.5272 | SISMA WOOD SLV | | -218.64 | -232.043 | 0. |
| 41 | 0. | iDROSTATICA | | -364.069 | -374.604 | 0. |
| 41 | 0.2636 | iDROSTATICA | | -364.069 | -343.949 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 41 | 0.5272 | iDROSTATICA | | -364.069 | -314.01 | 0. |
| 41 | 0. | SISMA WOOD SLD | | -96.56 | -102.479 | 0. |
| 41 | 0.2636 | SISMA WOOD SLD | | -96.56 | -102.479 | 0. |
| 41 | 0.5272 | SISMA WOOD SLD | | -96.56 | -102.479 | 0. |
| 41 | 0. | INERZIA H SLD | | -2.199 | -1.876 | 0. |
| 41 | 0.2636 | INERZIA H SLD | | -2.199 | -1.876 | 0. |
| 41 | 0.5272 | INERZIA H SLD | | -2.199 | -1.876 | 0. |
| 41 | 0. | INERZIA V + SLD | | -2.373 | 0.368 | 0. |
| 41 | 0.2636 | INERZIA V + SLD | | -2.373 | 0.368 | 0. |
| 41 | 0.5272 | INERZIA V + SLD | | -2.373 | 0.368 | 0. |
| 41 | 0. | INERZIA V SLD | | 2.373 | -0.368 | 0. |
| 41 | 0.2636 | INERZIA V SLD | | 2.373 | -0.368 | 0. |
| 41 | 0.5272 | INERZIA V SLD | | 2.373 | -0.368 | 0. |
| 41 | 0. | INERZIA V -1 | | 5.373 | -0.834 | 0. |
| 41 | 0.2636 | INERZIA V -1 | | 5.373 | -0.834 | 0. |
| 41 | 0.5272 | INERZIA V -1 | | 5.373 | -0.834 | 0. |
| 41 | 0. | SLU_1 | Max | -2467.306 | -538.283 | 0. |
| 41 | 0.2636 | SLU_1 | Max | -2454.459 | -470.14 | 0. |
| 41 | 0.5272 | SLU_1 | Max | -2441.613 | -403.932 | 0. |
| 41 | 0. | SLU_1 | Min | -2467.306 | -538.283 | 0. |
| 41 | 0.2636 | SLU_1 | Min | -2454.459 | -470.14 | 0. |
| 41 | 0.5272 | SLU_1 | Min | -2441.613 | -403.932 | 0. |
| 41 | 0. | SLU_2 | Max | -2467.428 | -453.578 | 0. |
| 41 | 0.2636 | SLU_2 | Max | -2454.581 | -394.865 | 0. |
| 41 | 0.5272 | SLU_2 | Max | -2441.734 | -337.752 | 0. |
| 41 | 0. | SLU_2 | Min | -2467.428 | -453.578 | 0. |
| 41 | 0.2636 | SLU_2 | Min | -2454.581 | -394.865 | 0. |
| 41 | 0.5272 | SLU_2 | Min | -2441.734 | -337.752 | 0. |
| 41 | 0. | SLU_3 | Max | -2537.607 | -533.852 | 0. |
| 41 | 0.2636 | SLU_3 | Max | -2524.76 | -467.312 | 0. |
| 41 | 0.5272 | SLU_3 | Max | -2511.913 | -402.643 | 0. |
| 41 | 0. | SLU_3 | Min | -2537.607 | -533.852 | 0. |
| 41 | 0.2636 | SLU_3 | Min | -2524.76 | -467.312 | 0. |
| 41 | 0.5272 | SLU_3 | Min | -2511.913 | -402.643 | 0. |
| 41 | 0. | SLU_4 | Max | -2519.205 | -429.981 | 0. |
| 41 | 0.2636 | SLU_4 | Max | -2506.358 | -372.72 | 0. |
| 41 | 0.5272 | SLU_4 | Max | -2493.511 | -317.781 | 0. |
| 41 | 0. | SLU_4 | Min | -2519.205 | -429.981 | 0. |
| 41 | 0.2636 | SLU_4 | Min | -2506.358 | -372.72 | 0. |
| 41 | 0.5272 | SLU_4 | Min | -2493.511 | -317.781 | 0. |
| 41 | 0. | SLE_F1 | Max | -1806.742 | -422.409 | 0. |
| 41 | 0.2636 | SLE_F1 | Max | -1796.859 | -369.991 | 0. |
| 41 | 0.5272 | SLE_F1 | Max | -1786.977 | -319.062 | 0. |
| 41 | 0. | SLE_F1 | Min | -1806.742 | -422.409 | 0. |
| 41 | 0.2636 | SLE_F1 | Min | -1796.859 | -369.991 | 0. |
| 41 | 0.5272 | SLE_F1 | Min | -1786.977 | -319.062 | 0. |
| 41 | 0. | SLE_F2 | Max | -1806.909 | -359.677 | 0. |
| 41 | 0.2636 | SLE_F2 | Max | -1797.027 | -314.513 | 0. |
| 41 | 0.5272 | SLE_F2 | Max | -1787.145 | -270.58 | 0. |
| 41 | 0. | SLE_F2 | Min | -1806.909 | -359.677 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|-----------|----------|
| 41 | 0.2636 | SLE_F2 | Min | -1797.027 | -314.513 | 0. |
| 41 | 0.5272 | SLE_F2 | Min | -1787.145 | -270.58 | 0. |
| 41 | 0. | SLE_F3 | Max | -1847.216 | -340.943 | 0. |
| 41 | 0.2636 | SLE_F3 | Max | -1837.334 | -296.896 | 0. |
| 41 | 0.5272 | SLE_F3 | Max | -1827.452 | -254.635 | 0. |
| 41 | 0. | SLE_F3 | Min | -1847.216 | -340.943 | 0. |
| 41 | 0.2636 | SLE_F3 | Min | -1837.334 | -296.896 | 0. |
| 41 | 0.5272 | SLE_F3 | Min | -1827.452 | -254.635 | 0. |
| 41 | 0. | SLE_F4 | Max | -1862.22 | -422.76 | 0. |
| 41 | 0.2636 | SLE_F4 | Max | -1852.338 | -371.576 | 0. |
| 41 | 0.5272 | SLE_F4 | Max | -1842.456 | -321.83 | 0. |
| 41 | 0. | SLE_F4 | Min | -1862.22 | -422.76 | 0. |
| 41 | 0.2636 | SLE_F4 | Min | -1852.338 | -371.576 | 0. |
| 41 | 0.5272 | SLE_F4 | Min | -1842.456 | -321.83 | 0. |
| 41 | 0. | SLE_QP1 | Max | -1637.424 | -439.071 | 0. |
| 41 | 0.2636 | SLE_QP1 | Max | -1627.542 | -386.653 | 0. |
| 41 | 0.5272 | SLE_QP1 | Max | -1617.66 | -335.724 | 0. |
| 41 | 0. | SLE_QP1 | Min | -1637.424 | -439.071 | 0. |
| 41 | 0.2636 | SLE_QP1 | Min | -1627.542 | -386.653 | 0. |
| 41 | 0.5272 | SLE_QP1 | Min | -1617.66 | -335.724 | 0. |
| 41 | 0. | SLE_QP2 | Max | -1637.707 | -379.685 | 0. |
| 41 | 0.2636 | SLE_QP2 | Max | -1627.825 | -334.522 | 0. |
| 41 | 0.5272 | SLE_QP2 | Max | -1617.942 | -290.588 | 0. |
| 41 | 0. | SLE_QP2 | Min | -1637.707 | -379.685 | 0. |
| 41 | 0.2636 | SLE_QP2 | Min | -1627.825 | -334.522 | 0. |
| 41 | 0.5272 | SLE_QP2 | Min | -1617.942 | -290.588 | 0. |
| 41 | 0. | SLE_QP3 | Max | -1678.897 | -359.865 | 0. |
| 41 | 0.2636 | SLE_QP3 | Max | -1669.015 | -315.817 | 0. |
| 41 | 0.5272 | SLE_QP3 | Max | -1659.133 | -273.557 | 0. |
| 41 | 0. | SLE_QP3 | Min | -1678.897 | -359.865 | 0. |
| 41 | 0.2636 | SLE_QP3 | Min | -1669.015 | -315.817 | 0. |
| 41 | 0.5272 | SLE_QP3 | Min | -1659.133 | -273.557 | 0. |
| 41 | 0. | SLE_QP4 | Max | -1695.849 | -446.041 | 0. |
| 41 | 0.2636 | SLE_QP4 | Max | -1685.967 | -394.856 | 0. |
| 41 | 0.5272 | SLE_QP4 | Max | -1676.085 | -345.111 | 0. |
| 41 | 0. | SLE_QP4 | Min | -1695.849 | -446.041 | 0. |
| 41 | 0.2636 | SLE_QP4 | Min | -1685.967 | -394.856 | 0. |
| 41 | 0.5272 | SLE_QP4 | Min | -1676.085 | -345.111 | 0. |
| 41 | 0. | SLV_1 | Max | -1931.223 | -961.467 | 0. |
| 41 | 0.2636 | SLV_1 | Max | -1921.341 | -909.049 | 0. |
| 41 | 0.5272 | SLV_1 | Max | -1911.459 | -858.12 | 0. |
| 41 | 0. | SLV_1 | Min | -1931.223 | -961.467 | 0. |
| 41 | 0.2636 | SLV_1 | Min | -1921.341 | -909.049 | 0. |
| 41 | 0.5272 | SLV_1 | Min | -1911.459 | -858.12 | 0. |
| 41 | 0. | SLV_2 | Max | -1919.621 | -964.081 | 0. |
| 41 | 0.2636 | SLV_2 | Max | -1909.739 | -911.664 | 0. |
| 41 | 0.5272 | SLV_2 | Max | -1899.857 | -860.734 | 0. |
| 41 | 0. | SLV_2 | Min | -1919.621 | -964.081 | 0. |
| 41 | 0.2636 | SLV_2 | Min | -1909.739 | -911.664 | 0. |
| 41 | 0.5272 | SLV_2 | Min | -1899.857 | -860.734 | 0. |
| 41 | 0. | SLV_3 | Max | -2033.947 | -1040.562 | 0. |
| 41 | 0.2636 | SLV_3 | Max | -2024.065 | -989.378 | 0. |
| 41 | 0.5272 | SLV_3 | Max | -2014.183 | -939.632 | 0. |
| 41 | 0. | SLV_3 | Min | -2033.947 | -1040.562 | 0. |
| 41 | 0.2636 | SLV_3 | Min | -2024.065 | -989.378 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|-----------|----------|
| 41 | 0.5272 | SLV_3 | Min | -2014.183 | -939.632 | 0. |
| 41 | 0. | SLV_4 | Max | -2022.204 | -1042.984 | 0. |
| 41 | 0.2636 | SLV_4 | Max | -2012.322 | -991.799 | 0. |
| 41 | 0.5272 | SLV_4 | Max | -2002.439 | -942.054 | 0. |
| 41 | 0. | SLV_4 | Min | -2022.204 | -1042.984 | 0. |
| 41 | 0.2636 | SLV_4 | Min | -2012.322 | -991.799 | 0. |
| 41 | 0.5272 | SLV_4 | Min | -2002.439 | -942.054 | 0. |
| 41 | 0. | SLD_1 | Max | -1736.125 | -629.329 | 0. |
| 41 | 0.2636 | SLD_1 | Max | -1726.243 | -576.911 | 0. |
| 41 | 0.5272 | SLD_1 | Max | -1716.36 | -525.982 | 0. |
| 41 | 0. | SLD_1 | Min | -1736.125 | -629.329 | 0. |
| 41 | 0.2636 | SLD_1 | Min | -1726.243 | -576.911 | 0. |
| 41 | 0.5272 | SLD_1 | Min | -1716.36 | -525.982 | 0. |
| 41 | 0. | SLD_2 | Max | -1730.66 | -630.694 | 0. |
| 41 | 0.2636 | SLD_2 | Max | -1720.777 | -578.276 | 0. |
| 41 | 0.5272 | SLD_2 | Max | -1710.895 | -527.347 | 0. |
| 41 | 0. | SLD_2 | Min | -1730.66 | -630.694 | 0. |
| 41 | 0.2636 | SLD_2 | Min | -1720.777 | -578.276 | 0. |
| 41 | 0.5272 | SLD_2 | Min | -1710.895 | -527.347 | 0. |
| 41 | 0. | SLD_3 | Max | -1833.151 | -708.541 | 0. |
| 41 | 0.2636 | SLD_3 | Max | -1823.269 | -657.357 | 0. |
| 41 | 0.5272 | SLD_3 | Max | -1813.386 | -607.612 | 0. |
| 41 | 0. | SLD_3 | Min | -1833.151 | -708.541 | 0. |
| 41 | 0.2636 | SLD_3 | Min | -1823.269 | -657.357 | 0. |
| 41 | 0.5272 | SLD_3 | Min | -1813.386 | -607.612 | 0. |
| 41 | 0. | SLD_4 | Max | -1827.852 | -709.585 | 0. |
| 41 | 0.2636 | SLD_4 | Max | -1817.97 | -658.4 | 0. |
| 41 | 0.5272 | SLD_4 | Max | -1808.088 | -608.655 | 0. |
| 41 | 0. | SLD_4 | Min | -1827.852 | -709.585 | 0. |
| 41 | 0.2636 | SLD_4 | Min | -1817.97 | -658.4 | 0. |
| 41 | 0.5272 | SLD_4 | Min | -1808.088 | -608.655 | 0. |
| 41 | 0. | SLU_IDR_1 | Max | -1580.023 | -424.062 | 0. |
| 41 | 0.2636 | SLU_IDR_1 | Max | -1571.129 | -378.289 | 0. |
| 41 | 0.5272 | SLU_IDR_1 | Max | -1562.235 | -334.266 | 0. |
| 41 | 0. | SLU_IDR_1 | Min | -1580.023 | -424.062 | 0. |
| 41 | 0.2636 | SLU_IDR_1 | Min | -1571.129 | -378.289 | 0. |
| 41 | 0.5272 | SLU_IDR_1 | Min | -1562.235 | -334.266 | 0. |
| 41 | 0. | SLU_IDR_2 | Max | -1541.416 | -445.958 | 0. |
| 41 | 0.2636 | SLU_IDR_2 | Max | -1532.522 | -399.18 | 0. |
| 41 | 0.5272 | SLU_IDR_2 | Max | -1523.629 | -353.652 | 0. |
| 41 | 0. | SLU_IDR_2 | Min | -1541.416 | -445.958 | 0. |
| 41 | 0.2636 | SLU_IDR_2 | Min | -1532.522 | -399.18 | 0. |
| 41 | 0.5272 | SLU_IDR_2 | Min | -1523.629 | -353.652 | 0. |
| 41 | 0. | SISMA WOOD SLV-1 | Max | -448.569 | -545.332 | 0. |
| 41 | 0.2636 | SISMA WOOD SLV-1 | Max | -448.569 | -545.332 | 0. |
| 41 | 0.5272 | SISMA WOOD SLV-1 | Max | -448.569 | -545.332 | 0. |
| 41 | 0. | SISMA WOOD SLV-1 | Min | -448.569 | -545.332 | 0. |
| 41 | 0.2636 | SISMA WOOD SLV-1 | Min | -448.569 | -545.332 | 0. |
| 41 | 0.5272 | SISMA WOOD SLV-1 | Min | -448.569 | -545.332 | 0. |
| 41 | 0. | DEAD-1 | Max | -407.235 | 62.93 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 41 | 0.2636 | DEAD-1 | Max | -397.353 | 62.93 | 0. |
| 41 | 0.5272 | DEAD-1 | Max | -387.471 | 62.93 | 0. |
| 41 | 0. | DEAD-1 | Min | -407.235 | 62.93 | 0. |
| 41 | 0.2636 | DEAD-1 | Min | -397.353 | 62.93 | 0. |
| 41 | 0.5272 | DEAD-1 | Min | -387.471 | 62.93 | 0. |
| 41 | 0. | SLU_PROVA | | -2256.913 | -552.713 | 0. |
| 41 | 0.2636 | SLU_PROVA | | -2244.066 | -484.57 | 0. |
| 41 | 0.5272 | SLU_PROVA | | -2231.22 | -418.362 | 0. |
| 42 | 0. | DEAD | | -322.559 | 55.872 | 0. |
| 42 | 0.2636 | DEAD | | -312.677 | 55.872 | 0. |
| 42 | 0.5272 | DEAD | | -302.795 | 55.872 | 0. |
| 42 | 0. | SIMM_KA | | -12.176 | -100.628 | 0. |
| 42 | 0.2636 | SIMM_KA | | -12.176 | -87.116 | 0. |
| 42 | 0.5272 | SIMM_KA | | -12.176 | -74.052 | 0. |
| 42 | 0. | SIMM_K0 | | -18.659 | -152.51 | 0. |
| 42 | 0.2636 | SIMM_K0 | | -18.659 | -132.242 | 0. |
| 42 | 0.5272 | SIMM_K0 | | -18.659 | -112.646 | 0. |
| 42 | 0. | A--SIMM_KA | | -53.237 | -96.312 | 0. |
| 42 | 0.2636 | A--SIMM_KA | | -53.237 | -85.062 | 0. |
| 42 | 0.5272 | A--SIMM_KA | | -53.237 | -74.884 | 0. |
| 42 | 0. | A--SIMM_K0 | | -79.793 | -153.493 | 0. |
| 42 | 0.2636 | A--SIMM_K0 | | -79.793 | -134.49 | 0. |
| 42 | 0.5272 | A--SIMM_K0 | | -79.793 | -116.37 | 0. |
| 42 | 0. | A-- SIMM_SOVR_K A | | -1.62 | -10.029 | 0. |
| 42 | 0.2636 | A-- SIMM_SOVR_K A | | -1.62 | -10.029 | 0. |
| 42 | 0.5272 | A-- SIMM_SOVR_K A | | -1.62 | -10.029 | 0. |
| 42 | 0. | A-- SIMM_SOVR_K 0 | | -2.429 | -15.036 | 0. |
| 42 | 0.2636 | A-- SIMM_SOVR_K 0 | | -2.429 | -15.036 | 0. |
| 42 | 0.5272 | A-- SIMM_SOVR_K 0 | | -2.429 | -15.036 | 0. |
| 42 | 0. | SIMM_SOVR_K 0 | | -2.429 | -15.036 | 0. |
| 42 | 0.2636 | SIMM_SOVR_K 0 | | -2.429 | -15.036 | 0. |
| 42 | 0.5272 | SIMM_SOVR_K 0 | | -2.429 | -15.036 | 0. |
| 42 | 0. | SIMM_SOVR_K A | | -1.62 | -10.029 | 0. |
| 42 | 0.2636 | SIMM_SOVR_K A | | -1.62 | -10.029 | 0. |
| 42 | 0.5272 | SIMM_SOVR_K A | | -1.62 | -10.029 | 0. |
| 42 | 0. | SOVR | | -195.45 | 28.442 | 0. |
| 42 | 0.2636 | SOVR | | -195.45 | 28.442 | 0. |
| 42 | 0.5272 | SOVR | | -195.45 | 28.442 | 0. |
| 42 | 0. | TERR_SIMM | | -782.714 | 86.501 | 0. |
| 42 | 0.2636 | TERR_SIMM | | -782.714 | 86.501 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 42 | 0.5272 | TERR_SIMM | | -782.714 | 86.501 | 0. |
| 42 | 0. | TERR_A--SIMM | | -764.488 | 103.098 | 0. |
| 42 | 0.2636 | TERR_A--SIMM | | -764.488 | 103.098 | 0. |
| 42 | 0.5272 | TERR_A--SIMM | | -764.488 | 103.098 | 0. |
| 42 | 0. | INERZIA H SLV | | -4.979 | -2.08 | 0. |
| 42 | 0.2636 | INERZIA H SLV | | -4.979 | -2.08 | 0. |
| 42 | 0.5272 | INERZIA H SLV | | -4.979 | -2.08 | 0. |
| 42 | 0. | INERZIA V + SLV | | -5.054 | 0.882 | 0. |
| 42 | 0.2636 | INERZIA V + SLV | | -5.054 | 0.882 | 0. |
| 42 | 0.5272 | INERZIA V + SLV | | -5.054 | 0.882 | 0. |
| 42 | 0. | INERZIA V - SLV | | 5.054 | -0.882 | 0. |
| 42 | 0.2636 | INERZIA V - SLV | | 5.054 | -0.882 | 0. |
| 42 | 0.5272 | INERZIA V - SLV | | 5.054 | -0.882 | 0. |
| 42 | 0. | SISMA WOOD SLV | | -218.64 | -141.546 | 0. |
| 42 | 0.2636 | SISMA WOOD SLV | | -218.64 | -141.546 | 0. |
| 42 | 0.5272 | SISMA WOOD SLV | | -218.64 | -141.546 | 0. |
| 42 | 0. | IDROSTATICA | | -364.069 | -304.78 | 0. |
| 42 | 0.2636 | IDROSTATICA | | -364.069 | -275.555 | 0. |
| 42 | 0.5272 | IDROSTATICA | | -364.069 | -247.045 | 0. |
| 42 | 0. | SISMA WOOD SLD | | -96.56 | -62.512 | 0. |
| 42 | 0.2636 | SISMA WOOD SLD | | -96.56 | -62.512 | 0. |
| 42 | 0.5272 | SISMA WOOD SLD | | -96.56 | -62.512 | 0. |
| 42 | 0. | INERZIA H SLD | | -2.199 | -0.919 | 0. |
| 42 | 0.2636 | INERZIA H SLD | | -2.199 | -0.919 | 0. |
| 42 | 0.5272 | INERZIA H SLD | | -2.199 | -0.919 | 0. |
| 42 | 0. | INERZIA V + SLD | | -2.232 | 0.39 | 0. |
| 42 | 0.2636 | INERZIA V + SLD | | -2.232 | 0.39 | 0. |
| 42 | 0.5272 | INERZIA V + SLD | | -2.232 | 0.39 | 0. |
| 42 | 0. | INERZIA V SLD | | 2.232 | -0.39 | 0. |
| 42 | 0.2636 | INERZIA V SLD | | 2.232 | -0.39 | 0. |
| 42 | 0.5272 | INERZIA V SLD | | 2.232 | -0.39 | 0. |
| 42 | 0. | INERZIA V -1 | | 5.054 | -0.882 | 0. |
| 42 | 0.2636 | INERZIA V -1 | | 5.054 | -0.882 | 0. |
| 42 | 0.5272 | INERZIA V -1 | | 5.054 | -0.882 | 0. |
| 42 | 0. | SLU_1 | Max | -2441.613 | -367.214 | 0. |
| 42 | 0.2636 | SLU_1 | Max | -2428.766 | -302.874 | 0. |
| 42 | 0.5272 | SLU_1 | Max | -2415.919 | -240.335 | 0. |
| 42 | 0. | SLU_1 | Min | -2441.613 | -367.214 | 0. |
| 42 | 0.2636 | SLU_1 | Min | -2428.766 | -302.874 | 0. |
| 42 | 0.5272 | SLU_1 | Min | -2415.919 | -240.335 | 0. |
| 42 | 0. | SLU_2 | Max | -2441.734 | -293.323 | 0. |
| 42 | 0.2636 | SLU_2 | Max | -2428.887 | -237.765 | 0. |
| 42 | 0.5272 | SLU_2 | Max | -2416.041 | -183.719 | 0. |
| 42 | 0. | SLU_2 | Min | -2441.734 | -293.323 | 0. |
| 42 | 0.2636 | SLU_2 | Min | -2428.887 | -237.765 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 42 | 0.5272 | SLU_2 | Min | -2416.041 | -183.719 | 0. |
| 42 | 0. | SLU_3 | Max | -2511.913 | -320.873 | 0. |
| 42 | 0.2636 | SLU_3 | Max | -2499.067 | -258.178 | 0. |
| 42 | 0.5272 | SLU_3 | Max | -2486.22 | -197.558 | 0. |
| 42 | 0. | SLU_3 | Min | -2511.913 | -320.873 | 0. |
| 42 | 0.2636 | SLU_3 | Min | -2499.067 | -258.178 | 0. |
| 42 | 0.5272 | SLU_3 | Min | -2486.22 | -197.558 | 0. |
| 42 | 0. | SLU_4 | Max | -2493.511 | -240.281 | 0. |
| 42 | 0.2636 | SLU_4 | Max | -2480.665 | -187.664 | 0. |
| 42 | 0.5272 | SLU_4 | Max | -2467.818 | -137.37 | 0. |
| 42 | 0. | SLU_4 | Min | -2493.511 | -240.281 | 0. |
| 42 | 0.2636 | SLU_4 | Min | -2480.665 | -187.664 | 0. |
| 42 | 0.5272 | SLU_4 | Min | -2467.818 | -137.37 | 0. |
| 42 | 0. | SLE_F1 | Max | -1786.977 | -292.328 | 0. |
| 42 | 0.2636 | SLE_F1 | Max | -1777.095 | -242.836 | 0. |
| 42 | 0.5272 | SLE_F1 | Max | -1767.213 | -194.729 | 0. |
| 42 | 0. | SLE_F1 | Min | -1786.977 | -292.328 | 0. |
| 42 | 0.2636 | SLE_F1 | Min | -1777.095 | -242.836 | 0. |
| 42 | 0.5272 | SLE_F1 | Min | -1767.213 | -194.729 | 0. |
| 42 | 0. | SLE_F2 | Max | -1787.145 | -238.113 | 0. |
| 42 | 0.2636 | SLE_F2 | Max | -1777.263 | -195.376 | 0. |
| 42 | 0.5272 | SLE_F2 | Max | -1767.381 | -153.802 | 0. |
| 42 | 0. | SLE_F2 | Min | -1787.145 | -238.113 | 0. |
| 42 | 0.2636 | SLE_F2 | Min | -1777.263 | -195.376 | 0. |
| 42 | 0.5272 | SLE_F2 | Min | -1767.381 | -153.802 | 0. |
| 42 | 0. | SLE_F3 | Max | -1827.452 | -196.896 | 0. |
| 42 | 0.2636 | SLE_F3 | Max | -1817.57 | -156.421 | 0. |
| 42 | 0.5272 | SLE_F3 | Max | -1807.688 | -117.733 | 0. |
| 42 | 0. | SLE_F3 | Min | -1827.452 | -196.896 | 0. |
| 42 | 0.2636 | SLE_F3 | Min | -1817.57 | -156.421 | 0. |
| 42 | 0.5272 | SLE_F3 | Min | -1807.688 | -117.733 | 0. |
| 42 | 0. | SLE_F4 | Max | -1842.456 | -259.324 | 0. |
| 42 | 0.2636 | SLE_F4 | Max | -1832.573 | -211.097 | 0. |
| 42 | 0.5272 | SLE_F4 | Max | -1822.691 | -164.466 | 0. |
| 42 | 0. | SLE_F4 | Min | -1842.456 | -259.324 | 0. |
| 42 | 0.2636 | SLE_F4 | Min | -1832.573 | -211.097 | 0. |
| 42 | 0.5272 | SLE_F4 | Min | -1822.691 | -164.466 | 0. |
| 42 | 0. | SLE_QP1 | Max | -1617.66 | -311.723 | 0. |
| 42 | 0.2636 | SLE_QP1 | Max | -1607.778 | -262.231 | 0. |
| 42 | 0.5272 | SLE_QP1 | Max | -1597.896 | -214.124 | 0. |
| 42 | 0. | SLE_QP1 | Min | -1617.66 | -311.723 | 0. |
| 42 | 0.2636 | SLE_QP1 | Min | -1607.778 | -262.231 | 0. |
| 42 | 0.5272 | SLE_QP1 | Min | -1597.896 | -214.124 | 0. |
| 42 | 0. | SLE_QP2 | Max | -1617.942 | -261.296 | 0. |
| 42 | 0.2636 | SLE_QP2 | Max | -1608.06 | -218.559 | 0. |
| 42 | 0.5272 | SLE_QP2 | Max | -1598.178 | -176.985 | 0. |
| 42 | 0. | SLE_QP2 | Min | -1617.942 | -261.296 | 0. |
| 42 | 0.2636 | SLE_QP2 | Min | -1608.06 | -218.559 | 0. |
| 42 | 0.5272 | SLE_QP2 | Min | -1598.178 | -176.985 | 0. |
| 42 | 0. | SLE_QP3 | Max | -1659.133 | -219.301 | 0. |
| 42 | 0.2636 | SLE_QP3 | Max | -1649.251 | -178.826 | 0. |
| 42 | 0.5272 | SLE_QP3 | Max | -1639.369 | -140.138 | 0. |
| 42 | 0. | SLE_QP3 | Min | -1659.133 | -219.301 | 0. |
| 42 | 0.2636 | SLE_QP3 | Min | -1649.251 | -178.826 | 0. |
| 42 | 0.5272 | SLE_QP3 | Min | -1639.369 | -140.138 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 42 | 0. | SLE_QP4 | Max | -1676.085 | -283.144 | 0. |
| 42 | 0.2636 | SLE_QP4 | Max | -1666.203 | -234.917 | 0. |
| 42 | 0.5272 | SLE_QP4 | Max | -1656.321 | -188.287 | 0. |
| 42 | 0. | SLE_QP4 | Min | -1676.085 | -283.144 | 0. |
| 42 | 0.2636 | SLE_QP4 | Min | -1666.203 | -234.917 | 0. |
| 42 | 0.5272 | SLE_QP4 | Min | -1656.321 | -188.287 | 0. |
| 42 | 0. | SLV_1 | Max | -1911.14 | -643.885 | 0. |
| 42 | 0.2636 | SLV_1 | Max | -1901.258 | -594.393 | 0. |
| 42 | 0.5272 | SLV_1 | Max | -1891.376 | -546.286 | 0. |
| 42 | 0. | SLV_1 | Min | -1911.14 | -643.885 | 0. |
| 42 | 0.2636 | SLV_1 | Min | -1901.258 | -594.393 | 0. |
| 42 | 0.5272 | SLV_1 | Min | -1891.376 | -546.286 | 0. |
| 42 | 0. | SLV_2 | Max | -1900.177 | -646.509 | 0. |
| 42 | 0.2636 | SLV_2 | Max | -1890.294 | -597.017 | 0. |
| 42 | 0.5272 | SLV_2 | Max | -1880.412 | -548.911 | 0. |
| 42 | 0. | SLV_2 | Min | -1900.177 | -646.509 | 0. |
| 42 | 0.2636 | SLV_2 | Min | -1890.294 | -597.017 | 0. |
| 42 | 0.5272 | SLV_2 | Min | -1880.412 | -548.911 | 0. |
| 42 | 0. | SLV_3 | Max | -2013.864 | -671.22 | 0. |
| 42 | 0.2636 | SLV_3 | Max | -2003.982 | -622.993 | 0. |
| 42 | 0.5272 | SLV_3 | Max | -1994.1 | -576.363 | 0. |
| 42 | 0. | SLV_3 | Min | -2013.864 | -671.22 | 0. |
| 42 | 0.2636 | SLV_3 | Min | -2003.982 | -622.993 | 0. |
| 42 | 0.5272 | SLV_3 | Min | -1994.1 | -576.363 | 0. |
| 42 | 0. | SLV_4 | Max | -2002.759 | -673.691 | 0. |
| 42 | 0.2636 | SLV_4 | Max | -1992.877 | -625.465 | 0. |
| 42 | 0.5272 | SLV_4 | Max | -1982.995 | -578.834 | 0. |
| 42 | 0. | SLV_4 | Min | -2002.759 | -673.691 | 0. |
| 42 | 0.2636 | SLV_4 | Min | -1992.877 | -625.465 | 0. |
| 42 | 0.5272 | SLV_4 | Min | -1982.995 | -578.834 | 0. |
| 42 | 0. | SLD_1 | Max | -1716.219 | -426.965 | 0. |
| 42 | 0.2636 | SLD_1 | Max | -1706.337 | -377.473 | 0. |
| 42 | 0.5272 | SLD_1 | Max | -1696.455 | -329.366 | 0. |
| 42 | 0. | SLD_1 | Min | -1716.219 | -426.965 | 0. |
| 42 | 0.2636 | SLD_1 | Min | -1706.337 | -377.473 | 0. |
| 42 | 0.5272 | SLD_1 | Min | -1696.455 | -329.366 | 0. |
| 42 | 0. | SLD_2 | Max | -1711.036 | -428.348 | 0. |
| 42 | 0.2636 | SLD_2 | Max | -1701.154 | -378.856 | 0. |
| 42 | 0.5272 | SLD_2 | Max | -1691.272 | -330.749 | 0. |
| 42 | 0. | SLD_2 | Min | -1711.036 | -428.348 | 0. |
| 42 | 0.2636 | SLD_2 | Min | -1701.154 | -378.856 | 0. |
| 42 | 0.5272 | SLD_2 | Min | -1691.272 | -330.749 | 0. |
| 42 | 0. | SLD_3 | Max | -1813.245 | -453.917 | 0. |
| 42 | 0.2636 | SLD_3 | Max | -1803.363 | -405.69 | 0. |
| 42 | 0.5272 | SLD_3 | Max | -1793.481 | -359.06 | 0. |
| 42 | 0. | SLD_3 | Min | -1813.245 | -453.917 | 0. |
| 42 | 0.2636 | SLD_3 | Min | -1803.363 | -405.69 | 0. |
| 42 | 0.5272 | SLD_3 | Min | -1793.481 | -359.06 | 0. |
| 42 | 0. | SLD_4 | Max | -1808.229 | -455.003 | 0. |
| 42 | 0.2636 | SLD_4 | Max | -1798.346 | -406.776 | 0. |
| 42 | 0.5272 | SLD_4 | Max | -1788.464 | -360.146 | 0. |
| 42 | 0. | SLD_4 | Min | -1808.229 | -455.003 | 0. |
| 42 | 0.2636 | SLD_4 | Min | -1798.346 | -406.776 | 0. |
| 42 | 0.5272 | SLD_4 | Min | -1788.464 | -360.146 | 0. |
| 42 | 0. | SLU_IDR_1 | Max | -1562.235 | -281.55 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 42 | 0.2636 | SLU_IDR_1 | Max | -1553.341 | -239.278 | 0. |
| 42 | 0.5272 | SLU_IDR_1 | Max | -1544.448 | -198.756 | 0. |
| 42 | 0. | SLU_IDR_1 | Min | -1562.235 | -281.55 | 0. |
| 42 | 0.2636 | SLU_IDR_1 | Min | -1553.341 | -239.278 | 0. |
| 42 | 0.5272 | SLU_IDR_1 | Min | -1544.448 | -198.756 | 0. |
| 42 | 0. | SLU_IDR_2 | Max | -1523.629 | -322.46 | 0. |
| 42 | 0.2636 | SLU_IDR_2 | Max | -1514.735 | -278.152 | 0. |
| 42 | 0.5272 | SLU_IDR_2 | Max | -1505.841 | -235.034 | 0. |
| 42 | 0. | SLU_IDR_2 | Min | -1523.629 | -322.46 | 0. |
| 42 | 0.2636 | SLU_IDR_2 | Min | -1514.735 | -278.152 | 0. |
| 42 | 0.5272 | SLU_IDR_2 | Min | -1505.841 | -235.034 | 0. |
| 42 | 0. | SISMA WOOD SLV-1 | Max | -448.569 | -351.929 | 0. |
| 42 | 0.2636 | SISMA WOOD SLV-1 | Max | -448.569 | -351.929 | 0. |
| 42 | 0.5272 | SISMA WOOD SLV-1 | Max | -448.569 | -351.929 | 0. |
| 42 | 0. | SISMA WOOD SLV-1 | Min | -448.569 | -351.929 | 0. |
| 42 | 0.2636 | SISMA WOOD SLV-1 | Min | -448.569 | -351.929 | 0. |
| 42 | 0.5272 | SISMA WOOD SLV-1 | Min | -448.569 | -351.929 | 0. |
| 42 | 0. | DEAD-1 | Max | -387.471 | 67.737 | 0. |
| 42 | 0.2636 | DEAD-1 | Max | -377.589 | 67.737 | 0. |
| 42 | 0.5272 | DEAD-1 | Max | -367.707 | 67.737 | 0. |
| 42 | 0. | DEAD-1 | Min | -387.471 | 67.737 | 0. |
| 42 | 0.2636 | DEAD-1 | Min | -377.589 | 67.737 | 0. |
| 42 | 0.5272 | DEAD-1 | Min | -367.707 | 67.737 | 0. |
| 42 | 0. | SLU_PROVA | | -2231.22 | -389.281 | 0. |
| 42 | 0.2636 | SLU_PROVA | | -2218.373 | -324.941 | 0. |
| 42 | 0.5272 | SLU_PROVA | | -2205.526 | -262.403 | 0. |
| 43 | 0. | DEAD | | 49.256 | -63.907 | 0. |
| 43 | 0.13945 | DEAD | | 49.256 | -58.679 | 0. |
| 43 | 0.27891 | DEAD | | 49.256 | -53.451 | 0. |
| 43 | 0. | SIMM_KA | | -143.72 | -32.204 | 0. |
| 43 | 0.13945 | SIMM_KA | | -143.72 | -32.204 | 0. |
| 43 | 0.27891 | SIMM_KA | | -143.72 | -32.204 | 0. |
| 43 | 0. | SIMM_K0 | | -216.792 | -49.164 | 0. |
| 43 | 0.13945 | SIMM_K0 | | -216.792 | -49.164 | 0. |
| 43 | 0.27891 | SIMM_K0 | | -216.792 | -49.164 | 0. |
| 43 | 0. | A--SIMM_KA | | -181.252 | -34.12 | 0. |
| 43 | 0.13945 | A--SIMM_KA | | -181.252 | -34.12 | 0. |
| 43 | 0.27891 | A--SIMM_KA | | -181.252 | -34.12 | 0. |
| 43 | 0. | A--SIMM_K0 | | -278.947 | -53.077 | 0. |
| 43 | 0.13945 | A--SIMM_K0 | | -278.947 | -53.077 | 0. |
| 43 | 0.27891 | A--SIMM_K0 | | -278.947 | -53.077 | 0. |
| 43 | 0. | A-- SIMM_SOVR_K A | | -8.323 | -3.835 | 0. |
| 43 | 0.13945 | A-- SIMM_SOVR_K A | | -8.323 | -3.835 | 0. |
| 43 | 0.27891 | A-- SIMM_SOVR_K A | | -8.323 | -3.835 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 43 | 0. | A-- SIMM_SOVR_K 0 | | -12.479 | -5.749 | 0. |
| 43 | 0.13945 | A-- SIMM_SOVR_K 0 | | -12.479 | -5.749 | 0. |
| 43 | 0.27891 | A-- SIMM_SOVR_K 0 | | -12.479 | -5.749 | 0. |
| 43 | 0. | SIMM_SOVR_K 0 | | -12.479 | -5.749 | 0. |
| 43 | 0.13945 | SIMM_SOVR_K 0 | | -12.479 | -5.749 | 0. |
| 43 | 0.27891 | SIMM_SOVR_K 0 | | -12.479 | -5.749 | 0. |
| 43 | 0. | SIMM_SOVR_K A | | -8.323 | -3.835 | 0. |
| 43 | 0.13945 | SIMM_SOVR_K A | | -8.323 | -3.835 | 0. |
| 43 | 0.27891 | SIMM_SOVR_K A | | -8.323 | -3.835 | 0. |
| 43 | 0. | SOVR | | 17.732 | -73.705 | 0. |
| 43 | 0.13945 | SOVR | | 17.732 | -73.705 | 0. |
| 43 | 0.27891 | SOVR | | 17.732 | -73.705 | 0. |
| 43 | 0. | TERR_SIMM | | 48.264 | -303.089 | 0. |
| 43 | 0.13945 | TERR_SIMM | | 48.264 | -303.089 | 0. |
| 43 | 0.27891 | TERR_SIMM | | 48.264 | -303.089 | 0. |
| 43 | 0. | TERR_A--SIMM | | 75.048 | -473.497 | 0. |
| 43 | 0.13945 | TERR_A--SIMM | | 75.048 | -473.497 | 0. |
| 43 | 0.27891 | TERR_A--SIMM | | 75.048 | -473.497 | 0. |
| 43 | 0. | INERZIA H SLV | | 6.932 | 3.053 | 0. |
| 43 | 0.13945 | INERZIA H SLV | | 6.932 | 3.053 | 0. |
| 43 | 0.27891 | INERZIA H SLV | | 6.932 | 3.053 | 0. |
| 43 | 0. | INERZIA V + SLV | | 0.775 | -0.948 | 0. |
| 43 | 0.13945 | INERZIA V + SLV | | 0.775 | -0.948 | 0. |
| 43 | 0.27891 | INERZIA V + SLV | | 0.775 | -0.948 | 0. |
| 43 | 0. | INERZIA V - SLV | | -0.775 | 0.948 | 0. |
| 43 | 0.13945 | INERZIA V - SLV | | -0.775 | 0.948 | 0. |
| 43 | 0.27891 | INERZIA V - SLV | | -0.775 | 0.948 | 0. |
| 43 | 0. | SISMA WOOD SLV | | 120.439 | 69.64 | 0. |
| 43 | 0.13945 | SISMA WOOD SLV | | 130.165 | 69.64 | 0. |
| 43 | 0.27891 | SISMA WOOD SLV | | 139.89 | 69.64 | 0. |
| 43 | 0. | iDROSTATICA | | -452.205 | -520.337 | 0. |
| 43 | 0.13945 | iDROSTATICA | | -452.205 | -537.5 | 0. |
| 43 | 0.27891 | iDROSTATICA | | -452.205 | -554.663 | 0. |
| 43 | 0. | SISMA WOOD SLD | | 53.191 | 30.756 | 0. |
| 43 | 0.13945 | SISMA WOOD SLD | | 57.486 | 30.756 | 0. |
| 43 | 0.27891 | SISMA WOOD SLD | | 61.781 | 30.756 | 0. |
| 43 | 0. | INERZIA H SLD | | 3.061 | 1.348 | 0. |
| 43 | 0.13945 | INERZIA H SLD | | 3.061 | 1.348 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|-----------|----------|
| 43 | 0.27891 | INERZIA H SLD | | 3.061 | 1.348 | 0. |
| 43 | 0. | INERZIA V + SLD | | 0.342 | -0.418 | 0. |
| 43 | 0.13945 | INERZIA V + SLD | | 0.342 | -0.418 | 0. |
| 43 | 0.27891 | INERZIA V + SLD | | 0.342 | -0.418 | 0. |
| 43 | 0. | INERZIA V SLD | | -0.342 | 0.418 | 0. |
| 43 | 0.13945 | INERZIA V SLD | | -0.342 | 0.418 | 0. |
| 43 | 0.27891 | INERZIA V SLD | | -0.342 | 0.418 | 0. |
| 43 | 0. | INERZIA V -1 | | -0.775 | 0.948 | 0. |
| 43 | 0.13945 | INERZIA V -1 | | -0.775 | 0.948 | 0. |
| 43 | 0.27891 | INERZIA V -1 | | -0.775 | 0.948 | 0. |
| 43 | 0. | SLU_1 | Max | -729.569 | -1429.861 | 0. |
| 43 | 0.13945 | SLU_1 | Max | -729.569 | -1445.376 | 0. |
| 43 | 0.27891 | SLU_1 | Max | -729.569 | -1460.891 | 0. |
| 43 | 0. | SLU_1 | Min | -729.569 | -1429.861 | 0. |
| 43 | 0.13945 | SLU_1 | Min | -729.569 | -1445.376 | 0. |
| 43 | 0.27891 | SLU_1 | Min | -729.569 | -1460.891 | 0. |
| 43 | 0. | SLU_2 | Max | -633.697 | -1418.136 | 0. |
| 43 | 0.13945 | SLU_2 | Max | -633.697 | -1433.651 | 0. |
| 43 | 0.27891 | SLU_2 | Max | -633.697 | -1449.166 | 0. |
| 43 | 0. | SLU_2 | Min | -633.697 | -1418.136 | 0. |
| 43 | 0.13945 | SLU_2 | Min | -633.697 | -1433.651 | 0. |
| 43 | 0.27891 | SLU_2 | Min | -633.697 | -1449.166 | 0. |
| 43 | 0. | SLU_3 | Max | -769.406 | -1694.882 | 0. |
| 43 | 0.13945 | SLU_3 | Max | -769.406 | -1710.397 | 0. |
| 43 | 0.27891 | SLU_3 | Max | -769.406 | -1725.912 | 0. |
| 43 | 0. | SLU_3 | Min | -769.406 | -1694.882 | 0. |
| 43 | 0.13945 | SLU_3 | Min | -769.406 | -1710.397 | 0. |
| 43 | 0.27891 | SLU_3 | Min | -769.406 | -1725.912 | 0. |
| 43 | 0. | SLU_4 | Max | -634.457 | -1669.559 | 0. |
| 43 | 0.13945 | SLU_4 | Max | -634.457 | -1685.074 | 0. |
| 43 | 0.27891 | SLU_4 | Max | -634.457 | -1700.589 | 0. |
| 43 | 0. | SLU_4 | Min | -634.457 | -1669.559 | 0. |
| 43 | 0.13945 | SLU_4 | Min | -634.457 | -1685.074 | 0. |
| 43 | 0.27891 | SLU_4 | Min | -634.457 | -1700.589 | 0. |
| 43 | 0. | SLE_F1 | Max | -567.425 | -1066.602 | 0. |
| 43 | 0.13945 | SLE_F1 | Max | -567.425 | -1078.537 | 0. |
| 43 | 0.27891 | SLE_F1 | Max | -567.425 | -1090.472 | 0. |
| 43 | 0. | SLE_F1 | Min | -567.425 | -1066.602 | 0. |
| 43 | 0.13945 | SLE_F1 | Min | -567.425 | -1078.537 | 0. |
| 43 | 0.27891 | SLE_F1 | Min | -567.425 | -1090.472 | 0. |
| 43 | 0. | SLE_F2 | Max | -496.179 | -1058.443 | 0. |
| 43 | 0.13945 | SLE_F2 | Max | -496.179 | -1070.377 | 0. |
| 43 | 0.27891 | SLE_F2 | Max | -496.179 | -1082.312 | 0. |
| 43 | 0. | SLE_F2 | Min | -496.179 | -1058.443 | 0. |
| 43 | 0.13945 | SLE_F2 | Min | -496.179 | -1070.377 | 0. |
| 43 | 0.27891 | SLE_F2 | Min | -496.179 | -1082.312 | 0. |
| 43 | 0. | SLE_F3 | Max | -496.219 | -1250.574 | 0. |
| 43 | 0.13945 | SLE_F3 | Max | -496.219 | -1262.509 | 0. |
| 43 | 0.27891 | SLE_F3 | Max | -496.219 | -1274.443 | 0. |
| 43 | 0. | SLE_F3 | Min | -496.219 | -1250.574 | 0. |
| 43 | 0.13945 | SLE_F3 | Min | -496.219 | -1262.509 | 0. |
| 43 | 0.27891 | SLE_F3 | Min | -496.219 | -1274.443 | 0. |
| 43 | 0. | SLE_F4 | Max | -604.74 | -1269.208 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|-----------|----------|
| 43 | 0.13945 | SLE_F4 | Max | -604.74 | -1281.142 | 0. |
| 43 | 0.27891 | SLE_F4 | Max | -604.74 | -1293.077 | 0. |
| 43 | 0. | SLE_F4 | Min | -604.74 | -1269.208 | 0. |
| 43 | 0.13945 | SLE_F4 | Min | -604.74 | -1281.142 | 0. |
| 43 | 0.27891 | SLE_F4 | Min | -604.74 | -1293.077 | 0. |
| 43 | 0. | SLE_QP1 | Max | -580.727 | -1005.603 | 0. |
| 43 | 0.13945 | SLE_QP1 | Max | -580.727 | -1017.537 | 0. |
| 43 | 0.27891 | SLE_QP1 | Max | -580.727 | -1029.472 | 0. |
| 43 | 0. | SLE_QP1 | Min | -580.727 | -1005.603 | 0. |
| 43 | 0.13945 | SLE_QP1 | Min | -580.727 | -1017.537 | 0. |
| 43 | 0.27891 | SLE_QP1 | Min | -580.727 | -1029.472 | 0. |
| 43 | 0. | SLE_QP2 | Max | -512.375 | -998.215 | 0. |
| 43 | 0.13945 | SLE_QP2 | Max | -512.375 | -1010.149 | 0. |
| 43 | 0.27891 | SLE_QP2 | Max | -512.375 | -1022.084 | 0. |
| 43 | 0. | SLE_QP2 | Min | -512.375 | -998.215 | 0. |
| 43 | 0.13945 | SLE_QP2 | Min | -512.375 | -1010.149 | 0. |
| 43 | 0.27891 | SLE_QP2 | Min | -512.375 | -1022.084 | 0. |
| 43 | 0. | SLE_QP3 | Max | -511.4 | -1187.983 | 0. |
| 43 | 0.13945 | SLE_QP3 | Max | -511.4 | -1199.918 | 0. |
| 43 | 0.27891 | SLE_QP3 | Max | -511.4 | -1211.853 | 0. |
| 43 | 0. | SLE_QP3 | Min | -511.4 | -1187.983 | 0. |
| 43 | 0.13945 | SLE_QP3 | Min | -511.4 | -1199.918 | 0. |
| 43 | 0.27891 | SLE_QP3 | Min | -511.4 | -1211.853 | 0. |
| 43 | 0. | SLE_QP4 | Max | -629.962 | -1205.024 | 0. |
| 43 | 0.13945 | SLE_QP4 | Max | -629.962 | -1216.959 | 0. |
| 43 | 0.27891 | SLE_QP4 | Max | -629.962 | -1228.893 | 0. |
| 43 | 0. | SLE_QP4 | Min | -629.962 | -1205.024 | 0. |
| 43 | 0.13945 | SLE_QP4 | Min | -629.962 | -1216.959 | 0. |
| 43 | 0.27891 | SLE_QP4 | Min | -629.962 | -1228.893 | 0. |
| 43 | 0. | SLV_1 | Max | -931.538 | -1009.424 | 0. |
| 43 | 0.13945 | SLV_1 | Max | -921.813 | -1021.359 | 0. |
| 43 | 0.27891 | SLV_1 | Max | -912.087 | -1033.294 | 0. |
| 43 | 0. | SLV_1 | Min | -931.538 | -1009.424 | 0. |
| 43 | 0.13945 | SLV_1 | Min | -921.813 | -1021.359 | 0. |
| 43 | 0.27891 | SLV_1 | Min | -912.087 | -1033.294 | 0. |
| 43 | 0. | SLV_2 | Max | -933.611 | -1007.971 | 0. |
| 43 | 0.13945 | SLV_2 | Max | -923.885 | -1019.905 | 0. |
| 43 | 0.27891 | SLV_2 | Max | -914.16 | -1031.84 | 0. |
| 43 | 0. | SLV_2 | Min | -933.611 | -1007.971 | 0. |
| 43 | 0.13945 | SLV_2 | Min | -923.885 | -1019.905 | 0. |
| 43 | 0.27891 | SLV_2 | Min | -914.16 | -1031.84 | 0. |
| 43 | 0. | SLV_3 | Max | -1093.9 | -1221.611 | 0. |
| 43 | 0.13945 | SLV_3 | Max | -1084.175 | -1233.545 | 0. |
| 43 | 0.27891 | SLV_3 | Max | -1074.449 | -1245.48 | 0. |
| 43 | 0. | SLV_3 | Min | -1093.9 | -1221.611 | 0. |
| 43 | 0.13945 | SLV_3 | Min | -1084.175 | -1233.545 | 0. |
| 43 | 0.27891 | SLV_3 | Min | -1074.449 | -1245.48 | 0. |
| 43 | 0. | SLV_4 | Max | -1095.997 | -1219.599 | 0. |
| 43 | 0.13945 | SLV_4 | Max | -1086.272 | -1231.534 | 0. |
| 43 | 0.27891 | SLV_4 | Max | -1076.546 | -1243.468 | 0. |
| 43 | 0. | SLV_4 | Min | -1095.997 | -1219.599 | 0. |
| 43 | 0.13945 | SLV_4 | Min | -1086.272 | -1231.534 | 0. |
| 43 | 0.27891 | SLV_4 | Min | -1076.546 | -1243.468 | 0. |
| 43 | 0. | SLD_1 | Max | -677.091 | -992.025 | 0. |
| 43 | 0.13945 | SLD_1 | Max | -672.796 | -1003.959 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|----------|-----------|----------|
| 43 | 0.27891 | SLD_1 | Max | -668.5 | -1015.894 | 0. |
| 43 | 0. | SLD_1 | Min | -677.091 | -992.025 | 0. |
| 43 | 0.13945 | SLD_1 | Min | -672.796 | -1003.959 | 0. |
| 43 | 0.27891 | SLD_1 | Min | -668.5 | -1015.894 | 0. |
| 43 | 0. | SLD_2 | Max | -678.392 | -991.289 | 0. |
| 43 | 0.13945 | SLD_2 | Max | -674.097 | -1003.223 | 0. |
| 43 | 0.27891 | SLD_2 | Max | -669.802 | -1015.158 | 0. |
| 43 | 0. | SLD_2 | Min | -678.392 | -991.289 | 0. |
| 43 | 0.13945 | SLD_2 | Min | -674.097 | -1003.223 | 0. |
| 43 | 0.27891 | SLD_2 | Min | -669.802 | -1015.158 | 0. |
| 43 | 0. | SLD_3 | Max | -839.577 | -1201.787 | 0. |
| 43 | 0.13945 | SLD_3 | Max | -835.282 | -1213.721 | 0. |
| 43 | 0.27891 | SLD_3 | Max | -830.987 | -1225.656 | 0. |
| 43 | 0. | SLD_3 | Min | -839.577 | -1201.787 | 0. |
| 43 | 0.13945 | SLD_3 | Min | -835.282 | -1213.721 | 0. |
| 43 | 0.27891 | SLD_3 | Min | -830.987 | -1225.656 | 0. |
| 43 | 0. | SLD_4 | Max | -840.599 | -1200.666 | 0. |
| 43 | 0.13945 | SLD_4 | Max | -836.304 | -1212.601 | 0. |
| 43 | 0.27891 | SLD_4 | Max | -832.009 | -1224.535 | 0. |
| 43 | 0. | SLD_4 | Min | -840.599 | -1200.666 | 0. |
| 43 | 0.13945 | SLD_4 | Min | -836.304 | -1212.601 | 0. |
| 43 | 0.27891 | SLD_4 | Min | -832.009 | -1224.535 | 0. |
| 43 | 0. | SLU_IDR_1 | Max | -579.405 | -1196.223 | 0. |
| 43 | 0.13945 | SLU_IDR_1 | Max | -579.405 | -1210.397 | 0. |
| 43 | 0.27891 | SLU_IDR_1 | Max | -579.405 | -1224.571 | 0. |
| 43 | 0. | SLU_IDR_1 | Min | -579.405 | -1196.223 | 0. |
| 43 | 0.13945 | SLU_IDR_1 | Min | -579.405 | -1210.397 | 0. |
| 43 | 0.27891 | SLU_IDR_1 | Min | -579.405 | -1224.571 | 0. |
| 43 | 0. | SLU_IDR_2 | Max | -583.867 | -1035.114 | 0. |
| 43 | 0.13945 | SLU_IDR_2 | Max | -583.867 | -1049.288 | 0. |
| 43 | 0.27891 | SLU_IDR_2 | Max | -583.867 | -1063.461 | 0. |
| 43 | 0. | SLU_IDR_2 | Min | -583.867 | -1035.114 | 0. |
| 43 | 0.13945 | SLU_IDR_2 | Min | -583.867 | -1049.288 | 0. |
| 43 | 0.27891 | SLU_IDR_2 | Min | -583.867 | -1063.461 | 0. |
| 43 | 0. | SISMA WOOD SLV-1 | Max | -350.163 | -27.863 | 0. |
| 43 | 0.13945 | SISMA WOOD SLV-1 | Max | -340.438 | -27.863 | 0. |
| 43 | 0.27891 | SISMA WOOD SLV-1 | Max | -330.712 | -27.863 | 0. |
| 43 | 0. | SISMA WOOD SLV-1 | Min | -350.163 | -27.863 | 0. |
| 43 | 0.13945 | SISMA WOOD SLV-1 | Min | -340.438 | -27.863 | 0. |
| 43 | 0.27891 | SISMA WOOD SLV-1 | Min | -330.712 | -27.863 | 0. |
| 43 | 0. | DEAD-1 | Max | 57.168 | -87.491 | 0. |
| 43 | 0.13945 | DEAD-1 | Max | 57.168 | -82.263 | 0. |
| 43 | 0.27891 | DEAD-1 | Max | 57.168 | -77.035 | 0. |
| 43 | 0. | DEAD-1 | Min | 57.168 | -87.491 | 0. |
| 43 | 0.13945 | DEAD-1 | Min | 57.168 | -82.263 | 0. |
| 43 | 0.27891 | DEAD-1 | Min | 57.168 | -77.035 | 0. |
| 43 | 0. | SLU_PROVA | | -735.042 | -1336.628 | 0. |
| 43 | 0.13945 | SLU_PROVA | | -735.042 | -1352.143 | 0. |
| 43 | 0.27891 | SLU_PROVA | | -735.042 | -1367.658 | 0. |
| 44 | 0. | DEAD | | 49.256 | -264.532 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 44 | 0.13945 | DEAD | | 49.256 | -259.304 | 0. |
| 44 | 0.27891 | DEAD | | 49.256 | -254.076 | 0. |
| 44 | 0. | SIMM_KA | | -143.72 | -20.806 | 0. |
| 44 | 0.13945 | SIMM_KA | | -143.72 | -20.806 | 0. |
| 44 | 0.27891 | SIMM_KA | | -143.72 | -20.806 | 0. |
| 44 | 0. | SIMM_K0 | | -216.792 | -31.78 | 0. |
| 44 | 0.13945 | SIMM_K0 | | -216.792 | -31.78 | 0. |
| 44 | 0.27891 | SIMM_K0 | | -216.792 | -31.78 | 0. |
| 44 | 0. | A--SIMM_KA | | -181.252 | 0.337 | 0. |
| 44 | 0.13945 | A--SIMM_KA | | -181.252 | 0.337 | 0. |
| 44 | 0.27891 | A--SIMM_KA | | -181.252 | 0.337 | 0. |
| 44 | 0. | A--SIMM_K0 | | -278.947 | -0.791 | 0. |
| 44 | 0.13945 | A--SIMM_K0 | | -278.947 | -0.791 | 0. |
| 44 | 0.27891 | A--SIMM_K0 | | -278.947 | -0.791 | 0. |
| 44 | 0. | A-- SIMM_SOVR_K A | | -8.323 | -2.603 | 0. |
| 44 | 0.13945 | A-- SIMM_SOVR_K A | | -8.323 | -2.603 | 0. |
| 44 | 0.27891 | A-- SIMM_SOVR_K A | | -8.323 | -2.603 | 0. |
| 44 | 0. | A-- SIMM_SOVR_K 0 | | -12.479 | -3.902 | 0. |
| 44 | 0.13945 | A-- SIMM_SOVR_K 0 | | -12.479 | -3.902 | 0. |
| 44 | 0.27891 | A-- SIMM_SOVR_K 0 | | -12.479 | -3.902 | 0. |
| 44 | 0. | SIMM_SOVR_K 0 | | -12.479 | -3.902 | 0. |
| 44 | 0.13945 | SIMM_SOVR_K 0 | | -12.479 | -3.902 | 0. |
| 44 | 0.27891 | SIMM_SOVR_K 0 | | -12.479 | -3.902 | 0. |
| 44 | 0. | SIMM_SOVR_K A | | -8.323 | -2.603 | 0. |
| 44 | 0.13945 | SIMM_SOVR_K A | | -8.323 | -2.603 | 0. |
| 44 | 0.27891 | SIMM_SOVR_K A | | -8.323 | -2.603 | 0. |
| 44 | 0. | SOVR | | 17.732 | -153.574 | 0. |
| 44 | 0.13945 | SOVR | | 17.732 | -153.574 | 0. |
| 44 | 0.27891 | SOVR | | 17.732 | -153.574 | 0. |
| 44 | 0. | TERR_SIMM | | 48.264 | -617.454 | 0. |
| 44 | 0.13945 | TERR_SIMM | | 48.264 | -617.454 | 0. |
| 44 | 0.27891 | TERR_SIMM | | 48.264 | -617.454 | 0. |
| 44 | 0. | TERR_A--SIMM | | 75.048 | -979.552 | 0. |
| 44 | 0.13945 | TERR_A--SIMM | | 75.048 | -979.552 | 0. |
| 44 | 0.27891 | TERR_A--SIMM | | 75.048 | -979.552 | 0. |
| 44 | 0. | INERZIA H SLV | | 7.27 | 4.292 | 0. |
| 44 | 0.13945 | INERZIA H SLV | | 7.27 | 4.292 | 0. |
| 44 | 0.27891 | INERZIA H SLV | | 7.27 | 4.292 | 0. |
| 44 | 0. | INERZIA V + SLV | | 0.775 | -4.191 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|-----------|----------|
| 44 | 0.13945 | INERZIA V + SLV | | 0.775 | -4.191 | 0. |
| 44 | 0.27891 | INERZIA V + SLV | | 0.775 | -4.191 | 0. |
| 44 | 0. | INERZIA V - SLV | | -0.775 | 4.191 | 0. |
| 44 | 0.13945 | INERZIA V - SLV | | -0.775 | 4.191 | 0. |
| 44 | 0.27891 | INERZIA V - SLV | | -0.775 | 4.191 | 0. |
| 44 | 0. | SISMA WOOD SLV | | 139.89 | 146.664 | 0. |
| 44 | 0.13945 | SISMA WOOD SLV | | 149.616 | 146.664 | 0. |
| 44 | 0.27891 | SISMA WOOD SLV | | 159.341 | 146.664 | 0. |
| 44 | 0. | iDROSTATICA | | -452.205 | -401.074 | 0. |
| 44 | 0.13945 | iDROSTATICA | | -452.205 | -418.237 | 0. |
| 44 | 0.27891 | iDROSTATICA | | -452.205 | -435.4 | 0. |
| 44 | 0. | SISMA WOOD SLD | | 61.781 | 64.773 | 0. |
| 44 | 0.13945 | SISMA WOOD SLD | | 66.076 | 64.773 | 0. |
| 44 | 0.27891 | SISMA WOOD SLD | | 70.372 | 64.773 | 0. |
| 44 | 0. | INERZIA H SLD | | 3.211 | 1.895 | 0. |
| 44 | 0.13945 | INERZIA H SLD | | 3.211 | 1.895 | 0. |
| 44 | 0.27891 | INERZIA H SLD | | 3.211 | 1.895 | 0. |
| 44 | 0. | INERZIA V + SLD | | 0.342 | -1.851 | 0. |
| 44 | 0.13945 | INERZIA V + SLD | | 0.342 | -1.851 | 0. |
| 44 | 0.27891 | INERZIA V + SLD | | 0.342 | -1.851 | 0. |
| 44 | 0. | INERZIA V SLD | | -0.342 | 1.851 | 0. |
| 44 | 0.13945 | INERZIA V SLD | | -0.342 | 1.851 | 0. |
| 44 | 0.27891 | INERZIA V SLD | | -0.342 | 1.851 | 0. |
| 44 | 0. | INERZIA V -1 | | -0.775 | 4.191 | 0. |
| 44 | 0.13945 | INERZIA V -1 | | -0.775 | 4.191 | 0. |
| 44 | 0.27891 | INERZIA V -1 | | -0.775 | 4.191 | 0. |
| 44 | 0. | SLU_1 | Max | -729.569 | -2113.014 | 0. |
| 44 | 0.13945 | SLU_1 | Max | -729.569 | -2128.53 | 0. |
| 44 | 0.27891 | SLU_1 | Max | -729.569 | -2144.045 | 0. |
| 44 | 0. | SLU_1 | Min | -729.569 | -2113.014 | 0. |
| 44 | 0.13945 | SLU_1 | Min | -729.569 | -2128.53 | 0. |
| 44 | 0.27891 | SLU_1 | Min | -729.569 | -2144.045 | 0. |
| 44 | 0. | SLU_2 | Max | -633.697 | -2107.778 | 0. |
| 44 | 0.13945 | SLU_2 | Max | -633.697 | -2123.293 | 0. |
| 44 | 0.27891 | SLU_2 | Max | -633.697 | -2138.808 | 0. |
| 44 | 0. | SLU_2 | Min | -633.697 | -2107.778 | 0. |
| 44 | 0.13945 | SLU_2 | Min | -633.697 | -2123.293 | 0. |
| 44 | 0.27891 | SLU_2 | Min | -633.697 | -2138.808 | 0. |
| 44 | 0. | SLU_3 | Max | -769.406 | -2605.126 | 0. |
| 44 | 0.13945 | SLU_3 | Max | -769.406 | -2620.641 | 0. |
| 44 | 0.27891 | SLU_3 | Max | -769.406 | -2636.156 | 0. |
| 44 | 0. | SLU_3 | Min | -769.406 | -2605.126 | 0. |
| 44 | 0.13945 | SLU_3 | Min | -769.406 | -2620.641 | 0. |
| 44 | 0.27891 | SLU_3 | Min | -769.406 | -2636.156 | 0. |
| 44 | 0. | SLU_4 | Max | -634.457 | -2603.954 | 0. |
| 44 | 0.13945 | SLU_4 | Max | -634.457 | -2619.469 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|----------|-----------|----------|
| 44 | 0.27891 | SLU_4 | Max | -634.457 | -2634.984 | 0. |
| 44 | 0. | SLU_4 | Min | -634.457 | -2603.954 | 0. |
| 44 | 0.13945 | SLU_4 | Min | -634.457 | -2619.469 | 0. |
| 44 | 0.27891 | SLU_4 | Min | -634.457 | -2634.984 | 0. |
| 44 | 0. | SLE_F1 | Max | -567.425 | -1554.038 | 0. |
| 44 | 0.13945 | SLE_F1 | Max | -567.425 | -1565.973 | 0. |
| 44 | 0.27891 | SLE_F1 | Max | -567.425 | -1577.907 | 0. |
| 44 | 0. | SLE_F1 | Min | -567.425 | -1554.038 | 0. |
| 44 | 0.13945 | SLE_F1 | Min | -567.425 | -1565.973 | 0. |
| 44 | 0.27891 | SLE_F1 | Min | -567.425 | -1577.907 | 0. |
| 44 | 0. | SLE_F2 | Max | -496.179 | -1550.32 | 0. |
| 44 | 0.13945 | SLE_F2 | Max | -496.179 | -1562.255 | 0. |
| 44 | 0.27891 | SLE_F2 | Max | -496.179 | -1574.189 | 0. |
| 44 | 0. | SLE_F2 | Min | -496.179 | -1550.32 | 0. |
| 44 | 0.13945 | SLE_F2 | Min | -496.179 | -1562.255 | 0. |
| 44 | 0.27891 | SLE_F2 | Min | -496.179 | -1574.189 | 0. |
| 44 | 0. | SLE_F3 | Max | -496.219 | -1931.59 | 0. |
| 44 | 0.13945 | SLE_F3 | Max | -496.219 | -1943.524 | 0. |
| 44 | 0.27891 | SLE_F3 | Max | -496.219 | -1955.459 | 0. |
| 44 | 0. | SLE_F3 | Min | -496.219 | -1931.59 | 0. |
| 44 | 0.13945 | SLE_F3 | Min | -496.219 | -1943.524 | 0. |
| 44 | 0.27891 | SLE_F3 | Min | -496.219 | -1955.459 | 0. |
| 44 | 0. | SLE_F4 | Max | -604.74 | -1932.345 | 0. |
| 44 | 0.13945 | SLE_F4 | Max | -604.74 | -1944.28 | 0. |
| 44 | 0.27891 | SLE_F4 | Max | -604.74 | -1956.215 | 0. |
| 44 | 0. | SLE_F4 | Min | -604.74 | -1932.345 | 0. |
| 44 | 0.13945 | SLE_F4 | Min | -604.74 | -1944.28 | 0. |
| 44 | 0.27891 | SLE_F4 | Min | -604.74 | -1956.215 | 0. |
| 44 | 0. | SLE_QP1 | Max | -580.727 | -1421.621 | 0. |
| 44 | 0.13945 | SLE_QP1 | Max | -580.727 | -1433.556 | 0. |
| 44 | 0.27891 | SLE_QP1 | Max | -580.727 | -1445.49 | 0. |
| 44 | 0. | SLE_QP1 | Min | -580.727 | -1421.621 | 0. |
| 44 | 0.13945 | SLE_QP1 | Min | -580.727 | -1433.556 | 0. |
| 44 | 0.27891 | SLE_QP1 | Min | -580.727 | -1445.49 | 0. |
| 44 | 0. | SLE_QP2 | Max | -512.375 | -1418.375 | 0. |
| 44 | 0.13945 | SLE_QP2 | Max | -512.375 | -1430.31 | 0. |
| 44 | 0.27891 | SLE_QP2 | Max | -512.375 | -1442.244 | 0. |
| 44 | 0. | SLE_QP2 | Min | -512.375 | -1418.375 | 0. |
| 44 | 0.13945 | SLE_QP2 | Min | -512.375 | -1430.31 | 0. |
| 44 | 0.27891 | SLE_QP2 | Min | -512.375 | -1442.244 | 0. |
| 44 | 0. | SLE_QP3 | Max | -511.4 | -1798.894 | 0. |
| 44 | 0.13945 | SLE_QP3 | Max | -511.4 | -1810.828 | 0. |
| 44 | 0.27891 | SLE_QP3 | Max | -511.4 | -1822.763 | 0. |
| 44 | 0. | SLE_QP3 | Min | -511.4 | -1798.894 | 0. |
| 44 | 0.13945 | SLE_QP3 | Min | -511.4 | -1810.828 | 0. |
| 44 | 0.27891 | SLE_QP3 | Min | -511.4 | -1822.763 | 0. |
| 44 | 0. | SLE_QP4 | Max | -629.962 | -1799.487 | 0. |
| 44 | 0.13945 | SLE_QP4 | Max | -629.962 | -1811.422 | 0. |
| 44 | 0.27891 | SLE_QP4 | Max | -629.962 | -1823.357 | 0. |
| 44 | 0. | SLE_QP4 | Min | -629.962 | -1799.487 | 0. |
| 44 | 0.13945 | SLE_QP4 | Min | -629.962 | -1811.422 | 0. |
| 44 | 0.27891 | SLE_QP4 | Min | -629.962 | -1823.357 | 0. |
| 44 | 0. | SLV_1 | Max | -911.749 | -1369.275 | 0. |
| 44 | 0.13945 | SLV_1 | Max | -902.024 | -1381.21 | 0. |
| 44 | 0.27891 | SLV_1 | Max | -892.298 | -1393.144 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|-----------|----------|
| 44 | 0. | SLV_1 | Min | -911.749 | -1369.275 | 0. |
| 44 | 0.13945 | SLV_1 | Min | -902.024 | -1381.21 | 0. |
| 44 | 0.27891 | SLV_1 | Min | -892.298 | -1393.144 | 0. |
| 44 | 0. | SLV_2 | Max | -913.822 | -1360.216 | 0. |
| 44 | 0.13945 | SLV_2 | Max | -904.096 | -1372.15 | 0. |
| 44 | 0.27891 | SLV_2 | Max | -894.371 | -1384.085 | 0. |
| 44 | 0. | SLV_2 | Min | -913.822 | -1360.216 | 0. |
| 44 | 0.13945 | SLV_2 | Min | -904.096 | -1372.15 | 0. |
| 44 | 0.27891 | SLV_2 | Min | -894.371 | -1384.085 | 0. |
| 44 | 0. | SLV_3 | Max | -1074.111 | -1762.935 | 0. |
| 44 | 0.13945 | SLV_3 | Max | -1064.385 | -1774.869 | 0. |
| 44 | 0.27891 | SLV_3 | Max | -1054.66 | -1786.804 | 0. |
| 44 | 0. | SLV_3 | Min | -1074.111 | -1762.935 | 0. |
| 44 | 0.13945 | SLV_3 | Min | -1064.385 | -1774.869 | 0. |
| 44 | 0.27891 | SLV_3 | Min | -1054.66 | -1786.804 | 0. |
| 44 | 0. | SLV_4 | Max | -1076.208 | -1753.529 | 0. |
| 44 | 0.13945 | SLV_4 | Max | -1066.483 | -1765.464 | 0. |
| 44 | 0.27891 | SLV_4 | Max | -1056.757 | -1777.399 | 0. |
| 44 | 0. | SLV_4 | Min | -1076.208 | -1753.529 | 0. |
| 44 | 0.13945 | SLV_4 | Min | -1066.483 | -1765.464 | 0. |
| 44 | 0.27891 | SLV_4 | Min | -1056.757 | -1777.399 | 0. |
| 44 | 0. | SLD_1 | Max | -668.351 | -1384.238 | 0. |
| 44 | 0.13945 | SLD_1 | Max | -664.056 | -1396.172 | 0. |
| 44 | 0.27891 | SLD_1 | Max | -659.761 | -1408.107 | 0. |
| 44 | 0. | SLD_1 | Min | -668.351 | -1384.238 | 0. |
| 44 | 0.13945 | SLD_1 | Min | -664.056 | -1396.172 | 0. |
| 44 | 0.27891 | SLD_1 | Min | -659.761 | -1408.107 | 0. |
| 44 | 0. | SLD_2 | Max | -669.652 | -1380.017 | 0. |
| 44 | 0.13945 | SLD_2 | Max | -665.357 | -1391.951 | 0. |
| 44 | 0.27891 | SLD_2 | Max | -661.062 | -1403.886 | 0. |
| 44 | 0. | SLD_2 | Min | -669.652 | -1380.017 | 0. |
| 44 | 0.13945 | SLD_2 | Min | -665.357 | -1391.951 | 0. |
| 44 | 0.27891 | SLD_2 | Min | -661.062 | -1403.886 | 0. |
| 44 | 0. | SLD_3 | Max | -830.838 | -1774.699 | 0. |
| 44 | 0.13945 | SLD_3 | Max | -826.542 | -1786.634 | 0. |
| 44 | 0.27891 | SLD_3 | Max | -822.247 | -1798.569 | 0. |
| 44 | 0. | SLD_3 | Min | -830.838 | -1774.699 | 0. |
| 44 | 0.13945 | SLD_3 | Min | -826.542 | -1786.634 | 0. |
| 44 | 0.27891 | SLD_3 | Min | -822.247 | -1798.569 | 0. |
| 44 | 0. | SLD_4 | Max | -831.86 | -1770.417 | 0. |
| 44 | 0.13945 | SLD_4 | Max | -827.564 | -1782.352 | 0. |
| 44 | 0.27891 | SLD_4 | Max | -823.269 | -1794.286 | 0. |
| 44 | 0. | SLD_4 | Min | -831.86 | -1770.417 | 0. |
| 44 | 0.13945 | SLD_4 | Min | -827.564 | -1782.352 | 0. |
| 44 | 0.27891 | SLD_4 | Min | -823.269 | -1794.286 | 0. |
| 44 | 0. | SLU_IDR_1 | Max | -579.405 | -1702.384 | 0. |
| 44 | 0.13945 | SLU_IDR_1 | Max | -579.405 | -1716.557 | 0. |
| 44 | 0.27891 | SLU_IDR_1 | Max | -579.405 | -1730.731 | 0. |
| 44 | 0. | SLU_IDR_1 | Min | -579.405 | -1702.384 | 0. |
| 44 | 0.13945 | SLU_IDR_1 | Min | -579.405 | -1716.557 | 0. |
| 44 | 0.27891 | SLU_IDR_1 | Min | -579.405 | -1730.731 | 0. |
| 44 | 0. | SLU_IDR_2 | Max | -583.867 | -1363.722 | 0. |
| 44 | 0.13945 | SLU_IDR_2 | Max | -583.867 | -1377.896 | 0. |
| 44 | 0.27891 | SLU_IDR_2 | Max | -583.867 | -1392.07 | 0. |
| 44 | 0. | SLU_IDR_2 | Min | -583.867 | -1363.722 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|-----------|----------|
| 44 | 0.13945 | SLU_IDR_2 | Min | -583.867 | -1377.896 | 0. |
| 44 | 0.27891 | SLU_IDR_2 | Min | -583.867 | -1392.07 | 0. |
| 44 | 0. | SISMA WOOD SLV-1 | Max | -330.712 | -27.863 | 0. |
| 44 | 0.13945 | SISMA WOOD SLV-1 | Max | -320.987 | -27.863 | 0. |
| 44 | 0.27891 | SISMA WOOD SLV-1 | Max | -311.261 | -27.863 | 0. |
| 44 | 0. | SISMA WOOD SLV-1 | Min | -330.712 | -27.863 | 0. |
| 44 | 0.13945 | SISMA WOOD SLV-1 | Min | -320.987 | -27.863 | 0. |
| 44 | 0.27891 | SISMA WOOD SLV-1 | Min | -311.261 | -27.863 | 0. |
| 44 | 0. | DEAD-1 | Max | 57.168 | -315.039 | 0. |
| 44 | 0.13945 | DEAD-1 | Max | 57.168 | -309.811 | 0. |
| 44 | 0.27891 | DEAD-1 | Max | 57.168 | -304.583 | 0. |
| 44 | 0. | DEAD-1 | Min | 57.168 | -315.039 | 0. |
| 44 | 0.13945 | DEAD-1 | Min | 57.168 | -309.811 | 0. |
| 44 | 0.27891 | DEAD-1 | Min | 57.168 | -304.583 | 0. |
| 44 | 0. | SLU_PROVA | | -735.042 | -1945.507 | 0. |
| 44 | 0.13945 | SLU_PROVA | | -735.042 | -1961.022 | 0. |
| 44 | 0.27891 | SLU_PROVA | | -735.042 | -1976.537 | 0. |
| 45 | 0. | DEAD | | -361.245 | -49.637 | 0. |
| 45 | 0.1319 | DEAD | | -356.3 | -49.637 | 0. |
| 45 | 0.2638 | DEAD | | -351.355 | -49.637 | 0. |
| 45 | 0. | SIMM_KA | | -12.661 | 144.685 | 0. |
| 45 | 0.1319 | SIMM_KA | | -12.661 | 137.296 | 0. |
| 45 | 0.2638 | SIMM_KA | | -12.661 | 129.907 | 0. |
| 45 | 0. | SIMM_K0 | | -19.338 | 218.263 | 0. |
| 45 | 0.1319 | SIMM_K0 | | -19.338 | 207.18 | 0. |
| 45 | 0.2638 | SIMM_K0 | | -19.338 | 196.096 | 0. |
| 45 | 0. | A--SIMM_KA | | 22.454 | 186.105 | 0. |
| 45 | 0.1319 | A--SIMM_KA | | 22.454 | 174.693 | 0. |
| 45 | 0.2638 | A--SIMM_KA | | 22.454 | 163.281 | 0. |
| 45 | 0. | A--SIMM_K0 | | 32.768 | 286.011 | 0. |
| 45 | 0.1319 | A--SIMM_K0 | | 32.768 | 268.893 | 0. |
| 45 | 0.2638 | A--SIMM_K0 | | 32.768 | 251.775 | 0. |
| 45 | 0. | A-- SIMM_SOVR_K A | | -1.65 | 8.422 | 0. |
| 45 | 0.1319 | A-- SIMM_SOVR_K A | | -1.65 | 8.422 | 0. |
| 45 | 0.2638 | A-- SIMM_SOVR_K A | | -1.65 | 8.422 | 0. |
| 45 | 0. | A-- SIMM_SOVR_K 0 | | -2.474 | 12.626 | 0. |
| 45 | 0.1319 | A-- SIMM_SOVR_K 0 | | -2.474 | 12.626 | 0. |
| 45 | 0.2638 | A-- SIMM_SOVR_K 0 | | -2.474 | 12.626 | 0. |
| 45 | 0. | A-- SIMM_SOVR_K 0 | | -2.474 | 12.626 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 45 | 0.1319 | SIMM_SOVR_K 0 | | -2.474 | 12.626 | 0. |
| 45 | 0.2638 | SIMM_SOVR_K 0 | | -2.474 | 12.626 | 0. |
| 45 | 0. | SIMM_SOVR_K A | | -1.65 | 8.422 | 0. |
| 45 | 0.1319 | SIMM_SOVR_K A | | -1.65 | 8.422 | 0. |
| 45 | 0.2638 | SIMM_SOVR_K A | | -1.65 | 8.422 | 0. |
| 45 | 0. | SOVR | | -195.416 | -18.469 | 0. |
| 45 | 0.1319 | SOVR | | -195.416 | -18.469 | 0. |
| 45 | 0.2638 | SOVR | | -195.416 | -18.469 | 0. |
| 45 | 0. | TERR_SIMM | | -781.351 | -50.941 | 0. |
| 45 | 0.1319 | TERR_SIMM | | -781.351 | -50.941 | 0. |
| 45 | 0.2638 | TERR_SIMM | | -781.351 | -50.941 | 0. |
| 45 | 0. | TERR_A--SIMM | | -1243.062 | -78.034 | 0. |
| 45 | 0.1319 | TERR_A--SIMM | | -1243.062 | -78.034 | 0. |
| 45 | 0.2638 | TERR_A--SIMM | | -1243.062 | -78.034 | 0. |
| 45 | 0. | INERZIA H SLV | | 4.991 | -6.92 | 0. |
| 45 | 0.1319 | INERZIA H SLV | | 4.991 | -6.92 | 0. |
| 45 | 0.2638 | INERZIA H SLV | | 4.991 | -6.92 | 0. |
| 45 | 0. | INERZIA V + SLV | | -5.759 | -0.782 | 0. |
| 45 | 0.1319 | INERZIA V + SLV | | -5.759 | -0.782 | 0. |
| 45 | 0.2638 | INERZIA V + SLV | | -5.759 | -0.782 | 0. |
| 45 | 0. | INERZIA V - SLV | | 5.759 | 0.782 | 0. |
| 45 | 0.1319 | INERZIA V - SLV | | 5.759 | 0.782 | 0. |
| 45 | 0.2638 | INERZIA V - SLV | | 5.759 | 0.782 | 0. |
| 45 | 0. | SISMA WOOD SLV | | 191.868 | -134.692 | 0. |
| 45 | 0.1319 | SISMA WOOD SLV | | 191.868 | -143.891 | 0. |
| 45 | 0.2638 | SISMA WOOD SLV | | 191.868 | -153.09 | 0. |
| 45 | 0. | iDROSTATICA | | -362.043 | 449.956 | 0. |
| 45 | 0.1319 | iDROSTATICA | | -362.043 | 433.813 | 0. |
| 45 | 0.2638 | iDROSTATICA | | -362.043 | 417.848 | 0. |
| 45 | 0. | SISMA WOOD SLD | | 84.737 | -59.485 | 0. |
| 45 | 0.1319 | SISMA WOOD SLD | | 84.737 | -63.548 | 0. |
| 45 | 0.2638 | SISMA WOOD SLD | | 84.737 | -67.611 | 0. |
| 45 | 0. | INERZIA H SLD | | 2.204 | -3.056 | 0. |
| 45 | 0.1319 | INERZIA H SLD | | 2.204 | -3.056 | 0. |
| 45 | 0.2638 | INERZIA H SLD | | 2.204 | -3.056 | 0. |
| 45 | 0. | INERZIA V + SLD | | -2.543 | -0.345 | 0. |
| 45 | 0.1319 | INERZIA V + SLD | | -2.543 | -0.345 | 0. |
| 45 | 0.2638 | INERZIA V + SLD | | -2.543 | -0.345 | 0. |
| 45 | 0. | INERZIA V SLD | | 2.543 | 0.345 | 0. |
| 45 | 0.1319 | INERZIA V SLD | | 2.543 | 0.345 | 0. |
| 45 | 0.2638 | INERZIA V SLD | | 2.543 | 0.345 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------|----------|-----------|----------|----------|
| 45 | 0. | INERZIA V -1 | | 5.759 | 0.782 | 0. |
| 45 | 0.1319 | INERZIA V -1 | | 5.759 | 0.782 | 0. |
| 45 | 0.2638 | INERZIA V -1 | | 5.759 | 0.782 | 0. |
| 45 | 0. | SLU_1 | Max | -2485.552 | 722.325 | 0. |
| 45 | 0.1319 | SLU_1 | Max | -2479.123 | 686.93 | 0. |
| 45 | 0.2638 | SLU_1 | Max | -2472.695 | 651.767 | 0. |
| 45 | 0. | SLU_1 | Min | -2485.552 | 722.325 | 0. |
| 45 | 0.1319 | SLU_1 | Min | -2479.123 | 686.93 | 0. |
| 45 | 0.2638 | SLU_1 | Min | -2472.695 | 651.767 | 0. |
| 45 | 0. | SLU_2 | Max | -2486.099 | 625.445 | 0. |
| 45 | 0.1319 | SLU_2 | Max | -2479.671 | 594.853 | 0. |
| 45 | 0.2638 | SLU_2 | Max | -2473.243 | 564.493 | 0. |
| 45 | 0. | SLU_2 | Min | -2486.099 | 625.445 | 0. |
| 45 | 0.1319 | SLU_2 | Min | -2479.671 | 594.853 | 0. |
| 45 | 0.2638 | SLU_2 | Min | -2473.243 | 564.493 | 0. |
| 45 | 0. | SLU_3 | Max | -3089.03 | 769.406 | 0. |
| 45 | 0.1319 | SLU_3 | Max | -3082.602 | 726.167 | 0. |
| 45 | 0.2638 | SLU_3 | Max | -3076.174 | 683.159 | 0. |
| 45 | 0. | SLU_3 | Min | -3089.03 | 769.406 | 0. |
| 45 | 0.1319 | SLU_3 | Min | -3082.602 | 726.167 | 0. |
| 45 | 0.2638 | SLU_3 | Min | -3076.174 | 683.159 | 0. |
| 45 | 0. | SLU_4 | Max | -3104.727 | 631.92 | 0. |
| 45 | 0.1319 | SLU_4 | Max | -3098.299 | 596.098 | 0. |
| 45 | 0.2638 | SLU_4 | Max | -3091.871 | 560.508 | 0. |
| 45 | 0. | SLU_4 | Min | -3104.727 | 631.92 | 0. |
| 45 | 0.1319 | SLU_4 | Min | -3098.299 | 596.098 | 0. |
| 45 | 0.2638 | SLU_4 | Min | -3091.871 | 560.508 | 0. |
| 45 | 0. | SLE_F1 | Max | -1820.942 | 562.107 | 0. |
| 45 | 0.1319 | SLE_F1 | Max | -1815.997 | 534.879 | 0. |
| 45 | 0.2638 | SLE_F1 | Max | -1811.053 | 507.831 | 0. |
| 45 | 0. | SLE_F1 | Min | -1820.942 | 562.107 | 0. |
| 45 | 0.1319 | SLE_F1 | Min | -1815.997 | 534.879 | 0. |
| 45 | 0.2638 | SLE_F1 | Min | -1811.053 | 507.831 | 0. |
| 45 | 0. | SLE_F2 | Max | -1821.312 | 490.089 | 0. |
| 45 | 0.1319 | SLE_F2 | Max | -1816.367 | 466.556 | 0. |
| 45 | 0.2638 | SLE_F2 | Max | -1811.423 | 443.203 | 0. |
| 45 | 0. | SLE_F2 | Min | -1821.312 | 490.089 | 0. |
| 45 | 0.1319 | SLE_F2 | Min | -1816.367 | 466.556 | 0. |
| 45 | 0.2638 | SLE_F2 | Min | -1811.423 | 443.203 | 0. |
| 45 | 0. | SLE_F3 | Max | -2297.182 | 494.516 | 0. |
| 45 | 0.1319 | SLE_F3 | Max | -2292.237 | 466.96 | 0. |
| 45 | 0.2638 | SLE_F3 | Max | -2287.293 | 439.583 | 0. |
| 45 | 0. | SLE_F3 | Min | -2297.182 | 494.516 | 0. |
| 45 | 0.1319 | SLE_F3 | Min | -2292.237 | 466.96 | 0. |
| 45 | 0.2638 | SLE_F3 | Min | -2287.293 | 439.583 | 0. |
| 45 | 0. | SLE_F4 | Max | -2285.304 | 604.74 | 0. |
| 45 | 0.1319 | SLE_F4 | Max | -2280.359 | 571.479 | 0. |
| 45 | 0.2638 | SLE_F4 | Max | -2275.414 | 538.396 | 0. |
| 45 | 0. | SLE_F4 | Min | -2285.304 | 604.74 | 0. |
| 45 | 0.1319 | SLE_F4 | Min | -2280.359 | 571.479 | 0. |
| 45 | 0.2638 | SLE_F4 | Min | -2275.414 | 538.396 | 0. |
| 45 | 0. | SLE_QP1 | Max | -1651.652 | 575.828 | 0. |
| 45 | 0.1319 | SLE_QP1 | Max | -1646.708 | 548.601 | 0. |
| 45 | 0.2638 | SLE_QP1 | Max | -1641.763 | 521.553 | 0. |
| 45 | 0. | SLE_QP1 | Min | -1651.652 | 575.828 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 45 | 0.1319 | SLE_QP1 | Min | -1646.708 | 548.601 | 0. |
| 45 | 0.2638 | SLE_QP1 | Min | -1641.763 | 521.553 | 0. |
| 45 | 0. | SLE_QP2 | Max | -1652.18 | 506.764 | 0. |
| 45 | 0.1319 | SLE_QP2 | Max | -1647.235 | 483.231 | 0. |
| 45 | 0.2638 | SLE_QP2 | Max | -1642.29 | 459.877 | 0. |
| 45 | 0. | SLE_QP2 | Min | -1652.18 | 506.764 | 0. |
| 45 | 0.1319 | SLE_QP2 | Min | -1647.235 | 483.231 | 0. |
| 45 | 0.2638 | SLE_QP2 | Min | -1642.29 | 459.877 | 0. |
| 45 | 0. | SLE_QP3 | Max | -2128.053 | 510.158 | 0. |
| 45 | 0.1319 | SLE_QP3 | Max | -2123.108 | 482.603 | 0. |
| 45 | 0.2638 | SLE_QP3 | Max | -2118.163 | 455.226 | 0. |
| 45 | 0. | SLE_QP3 | Min | -2128.053 | 510.158 | 0. |
| 45 | 0.1319 | SLE_QP3 | Min | -2123.108 | 482.603 | 0. |
| 45 | 0.2638 | SLE_QP3 | Min | -2118.163 | 455.226 | 0. |
| 45 | 0. | SLE_QP4 | Max | -2116.711 | 629.963 | 0. |
| 45 | 0.1319 | SLE_QP4 | Max | -2111.766 | 596.701 | 0. |
| 45 | 0.2638 | SLE_QP4 | Max | -2106.822 | 563.618 | 0. |
| 45 | 0. | SLE_QP4 | Min | -2116.711 | 629.963 | 0. |
| 45 | 0.1319 | SLE_QP4 | Min | -2111.766 | 596.701 | 0. |
| 45 | 0.2638 | SLE_QP4 | Min | -2106.822 | 563.618 | 0. |
| 45 | 0. | SLV_1 | Max | -1555.725 | 891.977 | 0. |
| 45 | 0.1319 | SLV_1 | Max | -1550.78 | 855.551 | 0. |
| 45 | 0.2638 | SLV_1 | Max | -1545.836 | 819.304 | 0. |
| 45 | 0. | SLV_1 | Min | -1555.725 | 891.977 | 0. |
| 45 | 0.1319 | SLV_1 | Min | -1550.78 | 855.551 | 0. |
| 45 | 0.2638 | SLV_1 | Min | -1545.836 | 819.304 | 0. |
| 45 | 0. | SLV_2 | Max | -1542.988 | 894.05 | 0. |
| 45 | 0.1319 | SLV_2 | Max | -1538.043 | 857.624 | 0. |
| 45 | 0.2638 | SLV_2 | Max | -1533.098 | 821.377 | 0. |
| 45 | 0. | SLV_2 | Min | -1542.988 | 894.05 | 0. |
| 45 | 0.1319 | SLV_2 | Min | -1538.043 | 857.624 | 0. |
| 45 | 0.2638 | SLV_2 | Min | -1533.098 | 821.377 | 0. |
| 45 | 0. | SLV_3 | Max | -2038.279 | 1054.341 | 0. |
| 45 | 0.1319 | SLV_3 | Max | -2033.335 | 1011.88 | 0. |
| 45 | 0.2638 | SLV_3 | Max | -2028.39 | 969.599 | 0. |
| 45 | 0. | SLV_3 | Min | -2038.279 | 1054.341 | 0. |
| 45 | 0.1319 | SLV_3 | Min | -2033.335 | 1011.88 | 0. |
| 45 | 0.2638 | SLV_3 | Min | -2028.39 | 969.599 | 0. |
| 45 | 0. | SLV_4 | Max | -2025.282 | 1056.438 | 0. |
| 45 | 0.1319 | SLV_4 | Max | -2020.337 | 1013.978 | 0. |
| 45 | 0.2638 | SLV_4 | Max | -2015.393 | 971.696 | 0. |
| 45 | 0. | SLV_4 | Min | -2025.282 | 1056.438 | 0. |
| 45 | 0.1319 | SLV_4 | Min | -2020.337 | 1013.978 | 0. |
| 45 | 0.2638 | SLV_4 | Min | -2015.393 | 971.696 | 0. |
| 45 | 0. | SLD_1 | Max | -1595.219 | 659.619 | 0. |
| 45 | 0.1319 | SLD_1 | Max | -1590.274 | 628.33 | 0. |
| 45 | 0.2638 | SLD_1 | Max | -1585.329 | 597.219 | 0. |
| 45 | 0. | SLD_1 | Min | -1595.219 | 659.619 | 0. |
| 45 | 0.1319 | SLD_1 | Min | -1590.274 | 628.33 | 0. |
| 45 | 0.2638 | SLD_1 | Min | -1585.329 | 597.219 | 0. |
| 45 | 0. | SLD_2 | Max | -1589.309 | 660.921 | 0. |
| 45 | 0.1319 | SLD_2 | Max | -1584.364 | 629.631 | 0. |
| 45 | 0.2638 | SLD_2 | Max | -1579.419 | 598.52 | 0. |
| 45 | 0. | SLD_2 | Min | -1589.309 | 660.921 | 0. |
| 45 | 0.1319 | SLD_2 | Min | -1584.364 | 629.631 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 45 | 0.2638 | SLD_2 | Min | -1579.419 | 598.52 | 0. |
| 45 | 0. | SLD_3 | Max | -2073.805 | 822.109 | 0. |
| 45 | 0.1319 | SLD_3 | Max | -2068.86 | 784.785 | 0. |
| 45 | 0.2638 | SLD_3 | Max | -2063.915 | 747.64 | 0. |
| 45 | 0. | SLD_3 | Min | -2073.805 | 822.109 | 0. |
| 45 | 0.1319 | SLD_3 | Min | -2068.86 | 784.785 | 0. |
| 45 | 0.2638 | SLD_3 | Min | -2063.915 | 747.64 | 0. |
| 45 | 0. | SLD_4 | Max | -2067.987 | 823.131 | 0. |
| 45 | 0.1319 | SLD_4 | Max | -2063.042 | 785.807 | 0. |
| 45 | 0.2638 | SLD_4 | Max | -2058.097 | 748.662 | 0. |
| 45 | 0. | SLD_4 | Min | -2067.987 | 823.131 | 0. |
| 45 | 0.1319 | SLD_4 | Min | -2063.042 | 785.807 | 0. |
| 45 | 0.2638 | SLD_4 | Min | -2058.097 | 748.662 | 0. |
| 45 | 0. | SLU_IDR_1 | Max | -1981.519 | 577.238 | 0. |
| 45 | 0.1319 | SLU_IDR_1 | Max | -1977.069 | 549.21 | 0. |
| 45 | 0.2638 | SLU_IDR_1 | Max | -1972.619 | 521.378 | 0. |
| 45 | 0. | SLU_IDR_1 | Min | -1981.519 | 577.238 | 0. |
| 45 | 0.1319 | SLU_IDR_1 | Min | -1977.069 | 549.21 | 0. |
| 45 | 0.2638 | SLU_IDR_1 | Min | -1972.619 | 521.378 | 0. |
| 45 | 0. | SLU_IDR_2 | Max | -1554.239 | 577.846 | 0. |
| 45 | 0.1319 | SLU_IDR_2 | Max | -1549.788 | 553.438 | 0. |
| 45 | 0.2638 | SLU_IDR_2 | Max | -1545.338 | 529.226 | 0. |
| 45 | 0. | SLU_IDR_2 | Min | -1554.239 | 577.846 | 0. |
| 45 | 0.1319 | SLU_IDR_2 | Min | -1549.788 | 553.438 | 0. |
| 45 | 0.2638 | SLU_IDR_2 | Min | -1545.338 | 529.226 | 0. |
| 45 | 0. | SISMA WOOD SLV-1 | Max | -27.863 | 311.261 | 0. |
| 45 | 0.1319 | SISMA WOOD SLV-1 | Max | -27.863 | 302.063 | 0. |
| 45 | 0.2638 | SISMA WOOD SLV-1 | Max | -27.863 | 292.864 | 0. |
| 45 | 0. | SISMA WOOD SLV-1 | Min | -27.863 | 311.261 | 0. |
| 45 | 0.1319 | SISMA WOOD SLV-1 | Min | -27.863 | 302.063 | 0. |
| 45 | 0.2638 | SISMA WOOD SLV-1 | Min | -27.863 | 292.864 | 0. |
| 45 | 0. | DEAD-1 | Max | -425.936 | -57.825 | 0. |
| 45 | 0.1319 | DEAD-1 | Max | -420.992 | -57.825 | 0. |
| 45 | 0.2638 | DEAD-1 | Max | -416.047 | -57.825 | 0. |
| 45 | 0. | DEAD-1 | Min | -425.936 | -57.825 | 0. |
| 45 | 0.1319 | DEAD-1 | Min | -420.992 | -57.825 | 0. |
| 45 | 0.2638 | DEAD-1 | Min | -416.047 | -57.825 | 0. |
| 45 | 0. | SLU_PROVA | | -2278.004 | 729.17 | 0. |
| 45 | 0.1319 | SLU_PROVA | | -2271.576 | 693.775 | 0. |
| 45 | 0.2638 | SLU_PROVA | | -2265.148 | 658.612 | 0. |
| 46 | 0. | DEAD | | -351.355 | -50.618 | 0. |
| 46 | 0.1318 | DEAD | | -346.414 | -50.618 | 0. |
| 46 | 0.2636 | DEAD | | -341.473 | -50.618 | 0. |
| 46 | 0. | SIMM_KA | | -12.661 | 132.268 | 0. |
| 46 | 0.1318 | SIMM_KA | | -12.661 | 124.885 | 0. |
| 46 | 0.2636 | SIMM_KA | | -12.661 | 117.502 | 0. |
| 46 | 0. | SIMM_K0 | | -19.338 | 199.697 | 0. |
| 46 | 0.1318 | SIMM_K0 | | -19.338 | 188.622 | 0. |
| 46 | 0.2636 | SIMM_K0 | | -19.338 | 177.547 | 0. |
| 46 | 0. | A--SIMM_KA | | 22.454 | 173.823 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 46 | 0.1318 | A--SIMM_KA | | 22.454 | 162.419 | 0. |
| 46 | 0.2636 | A--SIMM_KA | | 22.454 | 151.016 | 0. |
| 46 | 0. | A--SIMM_K0 | | 32.768 | 267.172 | 0. |
| 46 | 0.1318 | A--SIMM_K0 | | 32.768 | 250.067 | 0. |
| 46 | 0.2636 | A--SIMM_K0 | | 32.768 | 232.962 | 0. |
| 46 | 0. | A-- SIMM_SOVR_K A | | -1.65 | 8.677 | 0. |
| 46 | 0.1318 | A-- SIMM_SOVR_K A | | -1.65 | 8.677 | 0. |
| 46 | 0.2636 | A-- SIMM_SOVR_K A | | -1.65 | 8.677 | 0. |
| 46 | 0. | A-- SIMM_SOVR_K 0 | | -2.474 | 13.009 | 0. |
| 46 | 0.1318 | A-- SIMM_SOVR_K 0 | | -2.474 | 13.009 | 0. |
| 46 | 0.2636 | A-- SIMM_SOVR_K 0 | | -2.474 | 13.009 | 0. |
| 46 | 0. | SIMM_SOVR_K 0 | | -2.474 | 13.009 | 0. |
| 46 | 0.1318 | SIMM_SOVR_K 0 | | -2.474 | 13.009 | 0. |
| 46 | 0.2636 | SIMM_SOVR_K 0 | | -2.474 | 13.009 | 0. |
| 46 | 0. | SIMM_SOVR_K A | | -1.65 | 8.677 | 0. |
| 46 | 0.1318 | SIMM_SOVR_K A | | -1.65 | 8.677 | 0. |
| 46 | 0.2636 | SIMM_SOVR_K A | | -1.65 | 8.677 | 0. |
| 46 | 0. | SOVR | | -195.416 | -20.215 | 0. |
| 46 | 0.1318 | SOVR | | -195.416 | -20.215 | 0. |
| 46 | 0.2636 | SOVR | | -195.416 | -20.215 | 0. |
| 46 | 0. | TERR_SIMM | | -781.351 | -57.22 | 0. |
| 46 | 0.1318 | TERR_SIMM | | -781.351 | -57.22 | 0. |
| 46 | 0.2636 | TERR_SIMM | | -781.351 | -57.22 | 0. |
| 46 | 0. | TERR_A--SIMM | | -1243.062 | -85.446 | 0. |
| 46 | 0.1318 | TERR_A--SIMM | | -1243.062 | -85.446 | 0. |
| 46 | 0.2636 | TERR_A--SIMM | | -1243.062 | -85.446 | 0. |
| 46 | 0. | INERZIA H SLV | | 4.991 | -5.872 | 0. |
| 46 | 0.1318 | INERZIA H SLV | | 4.991 | -5.872 | 0. |
| 46 | 0.2636 | INERZIA H SLV | | 4.991 | -5.872 | 0. |
| 46 | 0. | INERZIA V + SLV | | -5.599 | -0.797 | 0. |
| 46 | 0.1318 | INERZIA V + SLV | | -5.599 | -0.797 | 0. |
| 46 | 0.2636 | INERZIA V + SLV | | -5.599 | -0.797 | 0. |
| 46 | 0. | INERZIA V - SLV | | 5.599 | 0.797 | 0. |
| 46 | 0.1318 | INERZIA V - SLV | | 5.599 | 0.797 | 0. |
| 46 | 0.2636 | INERZIA V - SLV | | 5.599 | 0.797 | 0. |
| 46 | 0. | SISMA WOOD SLV | | 191.868 | -102.77 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 46 | 0.1318 | SISMA WOOD SLV | | 191.868 | -111.962 | 0. |
| 46 | 0.2636 | SISMA WOOD SLV | | 191.868 | -121.153 | 0. |
| 46 | 0. | iDROSTATICA | | -362.043 | 413.076 | 0. |
| 46 | 0.1318 | iDROSTATICA | | -362.043 | 397.302 | 0. |
| 46 | 0.2636 | iDROSTATICA | | -362.043 | 381.707 | 0. |
| 46 | 0. | SISMA WOOD SLD | | 84.737 | -45.387 | 0. |
| 46 | 0.1318 | SISMA WOOD SLD | | 84.737 | -49.447 | 0. |
| 46 | 0.2636 | SISMA WOOD SLD | | 84.737 | -53.506 | 0. |
| 46 | 0. | INERZIA H SLD | | 2.204 | -2.593 | 0. |
| 46 | 0.1318 | INERZIA H SLD | | 2.204 | -2.593 | 0. |
| 46 | 0.2636 | INERZIA H SLD | | 2.204 | -2.593 | 0. |
| 46 | 0. | INERZIA V + SLD | | -2.473 | -0.352 | 0. |
| 46 | 0.1318 | INERZIA V + SLD | | -2.473 | -0.352 | 0. |
| 46 | 0.2636 | INERZIA V + SLD | | -2.473 | -0.352 | 0. |
| 46 | 0. | INERZIA V SLD | | 2.473 | 0.352 | 0. |
| 46 | 0.1318 | INERZIA V SLD | | 2.473 | 0.352 | 0. |
| 46 | 0.2636 | INERZIA V SLD | | 2.473 | 0.352 | 0. |
| 46 | 0. | INERZIA V -1 | | 5.599 | 0.797 | 0. |
| 46 | 0.1318 | INERZIA V -1 | | 5.599 | 0.797 | 0. |
| 46 | 0.2636 | INERZIA V -1 | | 5.599 | 0.797 | 0. |
| 46 | 0. | SLU_1 | Max | -2472.695 | 635.601 | 0. |
| 46 | 0.1318 | SLU_1 | Max | -2466.272 | 600.698 | 0. |
| 46 | 0.2636 | SLU_1 | Max | -2459.848 | 566.026 | 0. |
| 46 | 0. | SLU_1 | Min | -2472.695 | 635.601 | 0. |
| 46 | 0.1318 | SLU_1 | Min | -2466.272 | 600.698 | 0. |
| 46 | 0.2636 | SLU_1 | Min | -2459.848 | 566.026 | 0. |
| 46 | 0. | SLU_2 | Max | -2473.243 | 545.883 | 0. |
| 46 | 0.1318 | SLU_2 | Max | -2466.819 | 515.778 | 0. |
| 46 | 0.2636 | SLU_2 | Max | -2460.396 | 485.906 | 0. |
| 46 | 0. | SLU_2 | Min | -2473.243 | 545.883 | 0. |
| 46 | 0.1318 | SLU_2 | Min | -2466.819 | 515.778 | 0. |
| 46 | 0.2636 | SLU_2 | Min | -2460.396 | 485.906 | 0. |
| 46 | 0. | SLU_3 | Max | -3076.174 | 683.159 | 0. |
| 46 | 0.1318 | SLU_3 | Max | -3069.751 | 640.417 | 0. |
| 46 | 0.2636 | SLU_3 | Max | -3063.327 | 597.906 | 0. |
| 46 | 0. | SLU_3 | Min | -3076.174 | 683.159 | 0. |
| 46 | 0.1318 | SLU_3 | Min | -3069.751 | 640.417 | 0. |
| 46 | 0.2636 | SLU_3 | Min | -3063.327 | 597.906 | 0. |
| 46 | 0. | SLU_4 | Max | -3091.871 | 553.469 | 0. |
| 46 | 0.1318 | SLU_4 | Max | -3085.447 | 518.139 | 0. |
| 46 | 0.2636 | SLU_4 | Max | -3079.024 | 483.041 | 0. |
| 46 | 0. | SLU_4 | Min | -3091.871 | 553.469 | 0. |
| 46 | 0.1318 | SLU_4 | Min | -3085.447 | 518.139 | 0. |
| 46 | 0.2636 | SLU_4 | Min | -3079.024 | 483.041 | 0. |
| 46 | 0. | SLE_F1 | Max | -1811.053 | 495.987 | 0. |
| 46 | 0.1318 | SLE_F1 | Max | -1806.112 | 469.138 | 0. |
| 46 | 0.2636 | SLE_F1 | Max | -1801.171 | 442.468 | 0. |
| 46 | 0. | SLE_F1 | Min | -1811.053 | 495.987 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 46 | 0.1318 | SLE_F1 | Min | -1806.112 | 469.138 | 0. |
| 46 | 0.2636 | SLE_F1 | Min | -1801.171 | 442.468 | 0. |
| 46 | 0. | SLE_F2 | Max | -1811.423 | 429.501 | 0. |
| 46 | 0.1318 | SLE_F2 | Max | -1806.482 | 406.344 | 0. |
| 46 | 0.2636 | SLE_F2 | Max | -1801.541 | 383.365 | 0. |
| 46 | 0. | SLE_F2 | Min | -1811.423 | 429.501 | 0. |
| 46 | 0.1318 | SLE_F2 | Min | -1806.482 | 406.344 | 0. |
| 46 | 0.2636 | SLE_F2 | Min | -1801.541 | 383.365 | 0. |
| 46 | 0. | SLE_F3 | Max | -2287.293 | 434.769 | 0. |
| 46 | 0.1318 | SLE_F3 | Max | -2282.352 | 407.592 | 0. |
| 46 | 0.2636 | SLE_F3 | Max | -2277.41 | 380.593 | 0. |
| 46 | 0. | SLE_F3 | Min | -2287.293 | 434.769 | 0. |
| 46 | 0.1318 | SLE_F3 | Min | -2282.352 | 407.592 | 0. |
| 46 | 0.2636 | SLE_F3 | Min | -2277.41 | 380.593 | 0. |
| 46 | 0. | SLE_F4 | Max | -2275.414 | 538.396 | 0. |
| 46 | 0.1318 | SLE_F4 | Max | -2270.473 | 505.518 | 0. |
| 46 | 0.2636 | SLE_F4 | Max | -2265.532 | 472.817 | 0. |
| 46 | 0. | SLE_F4 | Min | -2275.414 | 538.396 | 0. |
| 46 | 0.1318 | SLE_F4 | Min | -2270.473 | 505.518 | 0. |
| 46 | 0.2636 | SLE_F4 | Min | -2265.532 | 472.817 | 0. |
| 46 | 0. | SLE_QP1 | Max | -1641.763 | 510.705 | 0. |
| 46 | 0.1318 | SLE_QP1 | Max | -1636.822 | 483.856 | 0. |
| 46 | 0.2636 | SLE_QP1 | Max | -1631.881 | 457.186 | 0. |
| 46 | 0. | SLE_QP1 | Min | -1641.763 | 510.705 | 0. |
| 46 | 0.1318 | SLE_QP1 | Min | -1636.822 | 483.856 | 0. |
| 46 | 0.2636 | SLE_QP1 | Min | -1631.881 | 457.186 | 0. |
| 46 | 0. | SLE_QP2 | Max | -1642.29 | 447.317 | 0. |
| 46 | 0.1318 | SLE_QP2 | Max | -1637.349 | 424.159 | 0. |
| 46 | 0.2636 | SLE_QP2 | Max | -1632.408 | 401.181 | 0. |
| 46 | 0. | SLE_QP2 | Min | -1642.29 | 447.317 | 0. |
| 46 | 0.1318 | SLE_QP2 | Min | -1637.349 | 424.159 | 0. |
| 46 | 0.2636 | SLE_QP2 | Min | -1632.408 | 401.181 | 0. |
| 46 | 0. | SLE_QP3 | Max | -2118.163 | 451.527 | 0. |
| 46 | 0.1318 | SLE_QP3 | Max | -2113.222 | 424.349 | 0. |
| 46 | 0.2636 | SLE_QP3 | Max | -2108.281 | 397.351 | 0. |
| 46 | 0. | SLE_QP3 | Min | -2118.163 | 451.527 | 0. |
| 46 | 0.1318 | SLE_QP3 | Min | -2113.222 | 424.349 | 0. |
| 46 | 0.2636 | SLE_QP3 | Min | -2108.281 | 397.351 | 0. |
| 46 | 0. | SLE_QP4 | Max | -2106.822 | 563.619 | 0. |
| 46 | 0.1318 | SLE_QP4 | Max | -2101.881 | 530.741 | 0. |
| 46 | 0.2636 | SLE_QP4 | Max | -2096.94 | 498.04 | 0. |
| 46 | 0. | SLE_QP4 | Min | -2106.822 | 563.619 | 0. |
| 46 | 0.1318 | SLE_QP4 | Min | -2101.881 | 530.741 | 0. |
| 46 | 0.2636 | SLE_QP4 | Min | -2096.94 | 498.04 | 0. |
| 46 | 0. | SLV_1 | Max | -1545.676 | 819. | 0. |
| 46 | 0.1318 | SLV_1 | Max | -1540.735 | 782.959 | 0. |
| 46 | 0.2636 | SLV_1 | Max | -1535.794 | 747.097 | 0. |
| 46 | 0. | SLV_1 | Min | -1545.676 | 819. | 0. |
| 46 | 0.1318 | SLV_1 | Min | -1540.735 | 782.959 | 0. |
| 46 | 0.2636 | SLV_1 | Min | -1535.794 | 747.097 | 0. |
| 46 | 0. | SLV_2 | Max | -1533.258 | 821.073 | 0. |
| 46 | 0.1318 | SLV_2 | Max | -1528.317 | 785.032 | 0. |
| 46 | 0.2636 | SLV_2 | Max | -1523.376 | 749.17 | 0. |
| 46 | 0. | SLV_2 | Min | -1533.258 | 821.073 | 0. |
| 46 | 0.1318 | SLV_2 | Min | -1528.317 | 785.032 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 46 | 0.2636 | SLV_2 | Min | -1523.376 | 749.17 | 0. |
| 46 | 0. | SLV_3 | Max | -2028.23 | 969.299 | 0. |
| 46 | 0.1318 | SLV_3 | Max | -2023.289 | 927.228 | 0. |
| 46 | 0.2636 | SLV_3 | Max | -2018.348 | 885.336 | 0. |
| 46 | 0. | SLV_3 | Min | -2028.23 | 969.299 | 0. |
| 46 | 0.1318 | SLV_3 | Min | -2023.289 | 927.228 | 0. |
| 46 | 0.2636 | SLV_3 | Min | -2018.348 | 885.336 | 0. |
| 46 | 0. | SLV_4 | Max | -2015.552 | 971.396 | 0. |
| 46 | 0.1318 | SLV_4 | Max | -2010.611 | 929.325 | 0. |
| 46 | 0.2636 | SLV_4 | Max | -2005.67 | 887.433 | 0. |
| 46 | 0. | SLV_4 | Min | -2015.552 | 971.396 | 0. |
| 46 | 0.1318 | SLV_4 | Min | -2010.611 | 929.325 | 0. |
| 46 | 0.2636 | SLV_4 | Min | -2005.67 | 887.433 | 0. |
| 46 | 0. | SLD_1 | Max | -1585.259 | 597.086 | 0. |
| 46 | 0.1318 | SLD_1 | Max | -1580.318 | 566.178 | 0. |
| 46 | 0.2636 | SLD_1 | Max | -1575.377 | 535.448 | 0. |
| 46 | 0. | SLD_1 | Min | -1585.259 | 597.086 | 0. |
| 46 | 0.1318 | SLD_1 | Min | -1580.318 | 566.178 | 0. |
| 46 | 0.2636 | SLD_1 | Min | -1575.377 | 535.448 | 0. |
| 46 | 0. | SLD_2 | Max | -1579.49 | 598.387 | 0. |
| 46 | 0.1318 | SLD_2 | Max | -1574.549 | 567.479 | 0. |
| 46 | 0.2636 | SLD_2 | Max | -1569.608 | 536.749 | 0. |
| 46 | 0. | SLD_2 | Min | -1579.49 | 598.387 | 0. |
| 46 | 0.1318 | SLD_2 | Min | -1574.549 | 567.479 | 0. |
| 46 | 0.2636 | SLD_2 | Min | -1569.608 | 536.749 | 0. |
| 46 | 0. | SLD_3 | Max | -2063.844 | 747.514 | 0. |
| 46 | 0.1318 | SLD_3 | Max | -2058.903 | 710.576 | 0. |
| 46 | 0.2636 | SLD_3 | Max | -2053.962 | 673.816 | 0. |
| 46 | 0. | SLD_3 | Min | -2063.844 | 747.514 | 0. |
| 46 | 0.1318 | SLD_3 | Min | -2058.903 | 710.576 | 0. |
| 46 | 0.2636 | SLD_3 | Min | -2053.962 | 673.816 | 0. |
| 46 | 0. | SLD_4 | Max | -2058.168 | 748.536 | 0. |
| 46 | 0.1318 | SLD_4 | Max | -2053.226 | 711.598 | 0. |
| 46 | 0.2636 | SLD_4 | Max | -2048.285 | 674.838 | 0. |
| 46 | 0. | SLD_4 | Min | -2058.168 | 748.536 | 0. |
| 46 | 0.1318 | SLD_4 | Min | -2053.226 | 711.598 | 0. |
| 46 | 0.2636 | SLD_4 | Min | -2048.285 | 674.838 | 0. |
| 46 | 0. | SLU_IDR_1 | Max | -1972.619 | 515.813 | 0. |
| 46 | 0.1318 | SLU_IDR_1 | Max | -1968.172 | 488.199 | 0. |
| 46 | 0.2636 | SLU_IDR_1 | Max | -1963.725 | 460.781 | 0. |
| 46 | 0. | SLU_IDR_1 | Min | -1972.619 | 515.813 | 0. |
| 46 | 0.1318 | SLU_IDR_1 | Min | -1968.172 | 488.199 | 0. |
| 46 | 0.2636 | SLU_IDR_1 | Min | -1963.725 | 460.781 | 0. |
| 46 | 0. | SLU_IDR_2 | Max | -1545.338 | 515.827 | 0. |
| 46 | 0.1318 | SLU_IDR_2 | Max | -1540.891 | 491.831 | 0. |
| 46 | 0.2636 | SLU_IDR_2 | Max | -1536.444 | 468.031 | 0. |
| 46 | 0. | SLU_IDR_2 | Min | -1545.338 | 515.827 | 0. |
| 46 | 0.1318 | SLU_IDR_2 | Min | -1540.891 | 491.831 | 0. |
| 46 | 0.2636 | SLU_IDR_2 | Min | -1536.444 | 468.031 | 0. |
| 46 | 0. | SISMA WOOD SLV-1 | Max | -27.863 | 292.864 | 0. |
| 46 | 0.1318 | SISMA WOOD SLV-1 | Max | -27.863 | 283.672 | 0. |
| 46 | 0.2636 | SISMA WOOD SLV-1 | Max | -27.863 | 274.48 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 46 | 0. | SISMA WOOD SLV-1 | Min | -27.863 | 292.864 | 0. |
| 46 | 0.1318 | SISMA WOOD SLV-1 | Min | -27.863 | 283.672 | 0. |
| 46 | 0.2636 | SISMA WOOD SLV-1 | Min | -27.863 | 274.48 | 0. |
| 46 | 0. | DEAD-1 | Max | -416.047 | -59.465 | 0. |
| 46 | 0.1318 | DEAD-1 | Max | -411.106 | -59.465 | 0. |
| 46 | 0.2636 | DEAD-1 | Max | -406.165 | -59.465 | 0. |
| 46 | 0. | DEAD-1 | Min | -416.047 | -59.465 | 0. |
| 46 | 0.1318 | DEAD-1 | Min | -411.106 | -59.465 | 0. |
| 46 | 0.2636 | DEAD-1 | Min | -406.165 | -59.465 | 0. |
| 46 | 0. | SLU_PROVA | | -2265.148 | 645.606 | 0. |
| 46 | 0.1318 | SLU_PROVA | | -2258.725 | 610.702 | 0. |
| 46 | 0.2636 | SLU_PROVA | | -2252.301 | 576.031 | 0. |
| 47 | 0. | DEAD | | 50.447 | -66.549 | 0. |
| 47 | 0.13006 | DEAD | | 50.447 | -61.673 | 0. |
| 47 | 0.26012 | DEAD | | 50.447 | -56.797 | 0. |
| 47 | 0. | SIMM_KA | | -143.95 | -31.565 | 0. |
| 47 | 0.13006 | SIMM_KA | | -143.95 | -31.565 | 0. |
| 47 | 0.26012 | SIMM_KA | | -143.95 | -31.565 | 0. |
| 47 | 0. | SIMM_K0 | | -217.139 | -48.187 | 0. |
| 47 | 0.13006 | SIMM_K0 | | -217.139 | -48.187 | 0. |
| 47 | 0.26012 | SIMM_K0 | | -217.139 | -48.187 | 0. |
| 47 | 0. | A--SIMM_KA | | -171.968 | -46.042 | 0. |
| 47 | 0.13006 | A--SIMM_KA | | -171.968 | -46.042 | 0. |
| 47 | 0.26012 | A--SIMM_KA | | -171.968 | -46.042 | 0. |
| 47 | 0. | A--SIMM_K0 | | -265.606 | -69.589 | 0. |
| 47 | 0.13006 | A--SIMM_K0 | | -265.606 | -69.589 | 0. |
| 47 | 0.26012 | A--SIMM_K0 | | -265.606 | -69.589 | 0. |
| 47 | 0. | A-- SIMM_SOVR_K A | | -8.35 | -3.752 | 0. |
| 47 | 0.13006 | A-- SIMM_SOVR_K A | | -8.35 | -3.752 | 0. |
| 47 | 0.26012 | A-- SIMM_SOVR_K A | | -8.35 | -3.752 | 0. |
| 47 | 0. | A-- SIMM_SOVR_K 0 | | -12.518 | -5.625 | 0. |
| 47 | 0.13006 | A-- SIMM_SOVR_K 0 | | -12.518 | -5.625 | 0. |
| 47 | 0.26012 | A-- SIMM_SOVR_K 0 | | -12.518 | -5.625 | 0. |
| 47 | 0. | SIMM_SOVR_K 0 | | -12.518 | -5.625 | 0. |
| 47 | 0.13006 | SIMM_SOVR_K 0 | | -12.518 | -5.625 | 0. |
| 47 | 0.26012 | SIMM_SOVR_K 0 | | -12.518 | -5.625 | 0. |
| 47 | 0. | SIMM_SOVR_K A | | -8.35 | -3.752 | 0. |
| 47 | 0.13006 | SIMM_SOVR_K A | | -8.35 | -3.752 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|-----------|----------|
| 47 | 0.26012 | SIMM_SOVR_K A | | -8.35 | -3.752 | 0. |
| 47 | 0. | SOVR | | 18.356 | -75.286 | 0. |
| 47 | 0.13006 | SOVR | | 18.356 | -75.286 | 0. |
| 47 | 0.26012 | SOVR | | 18.356 | -75.286 | 0. |
| 47 | 0. | TERR_SIMM | | 50.748 | -309.67 | 0. |
| 47 | 0.13006 | TERR_SIMM | | 50.748 | -309.67 | 0. |
| 47 | 0.26012 | TERR_SIMM | | 50.748 | -309.67 | 0. |
| 47 | 0. | TERR_A--SIMM | | 54.966 | -308.431 | 0. |
| 47 | 0.13006 | TERR_A--SIMM | | 54.966 | -308.431 | 0. |
| 47 | 0.26012 | TERR_A--SIMM | | 54.966 | -308.431 | 0. |
| 47 | 0. | INERZIA H SLV | | -6.932 | -3.105 | 0. |
| 47 | 0.13006 | INERZIA H SLV | | -6.932 | -3.105 | 0. |
| 47 | 0.26012 | INERZIA H SLV | | -6.932 | -3.105 | 0. |
| 47 | 0. | INERZIA V + SLV | | 0.795 | -0.996 | 0. |
| 47 | 0.13006 | INERZIA V + SLV | | 0.795 | -0.996 | 0. |
| 47 | 0.26012 | INERZIA V + SLV | | 0.795 | -0.996 | 0. |
| 47 | 0. | INERZIA V - SLV | | -0.795 | 0.996 | 0. |
| 47 | 0.13006 | INERZIA V - SLV | | -0.795 | 0.996 | 0. |
| 47 | 0.26012 | INERZIA V - SLV | | -0.795 | 0.996 | 0. |
| 47 | 0. | SISMA WOOD SLV | | -365.885 | -144.539 | 0. |
| 47 | 0.13006 | SISMA WOOD SLV | | -365.885 | -144.539 | 0. |
| 47 | 0.26012 | SISMA WOOD SLV | | -365.885 | -144.539 | 0. |
| 47 | 0. | iDROSTATICA | | -451.731 | -524.615 | 0. |
| 47 | 0.13006 | iDROSTATICA | | -451.731 | -540.621 | 0. |
| 47 | 0.26012 | iDROSTATICA | | -451.731 | -556.627 | 0. |
| 47 | 0. | SISMA WOOD SLD | | -161.589 | -63.834 | 0. |
| 47 | 0.13006 | SISMA WOOD SLD | | -161.589 | -63.834 | 0. |
| 47 | 0.26012 | SISMA WOOD SLD | | -161.589 | -63.834 | 0. |
| 47 | 0. | INERZIA H SLD | | -3.062 | -1.371 | 0. |
| 47 | 0.13006 | INERZIA H SLD | | -3.062 | -1.371 | 0. |
| 47 | 0.26012 | INERZIA H SLD | | -3.062 | -1.371 | 0. |
| 47 | 0. | INERZIA V + SLD | | 0.351 | -0.44 | 0. |
| 47 | 0.13006 | INERZIA V + SLD | | 0.351 | -0.44 | 0. |
| 47 | 0.26012 | INERZIA V + SLD | | 0.351 | -0.44 | 0. |
| 47 | 0. | INERZIA V SLD | | -0.351 | 0.44 | 0. |
| 47 | 0.13006 | INERZIA V SLD | | -0.351 | 0.44 | 0. |
| 47 | 0.26012 | INERZIA V SLD | | -0.351 | 0.44 | 0. |
| 47 | 0. | INERZIA V -1 | | -0.795 | 0.996 | 0. |
| 47 | 0.13006 | INERZIA V -1 | | -0.795 | 0.996 | 0. |
| 47 | 0.26012 | INERZIA V -1 | | -0.795 | 0.996 | 0. |
| 47 | 0. | SLU_1 | Max | -723.432 | -1452.213 | 0. |
| 47 | 0.13006 | SLU_1 | Max | -723.432 | -1466.683 | 0. |
| 47 | 0.26012 | SLU_1 | Max | -723.432 | -1481.153 | 0. |
| 47 | 0. | SLU_1 | Min | -723.432 | -1452.213 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|----------|-----------|----------|
| 47 | 0.13006 | SLU_1 | Min | -723.432 | -1466.683 | 0. |
| 47 | 0.26012 | SLU_1 | Min | -723.432 | -1481.153 | 0. |
| 47 | 0. | SLU_2 | Max | -627.731 | -1439.814 | 0. |
| 47 | 0.13006 | SLU_2 | Max | -627.731 | -1454.284 | 0. |
| 47 | 0.26012 | SLU_2 | Max | -627.731 | -1468.753 | 0. |
| 47 | 0. | SLU_2 | Min | -627.731 | -1439.814 | 0. |
| 47 | 0.13006 | SLU_2 | Min | -627.731 | -1454.284 | 0. |
| 47 | 0.26012 | SLU_2 | Min | -627.731 | -1468.753 | 0. |
| 47 | 0. | SLU_3 | Max | -775.921 | -1458.716 | 0. |
| 47 | 0.13006 | SLU_3 | Max | -775.921 | -1473.186 | 0. |
| 47 | 0.26012 | SLU_3 | Max | -775.921 | -1487.655 | 0. |
| 47 | 0. | SLU_3 | Min | -775.921 | -1458.716 | 0. |
| 47 | 0.13006 | SLU_3 | Min | -775.921 | -1473.186 | 0. |
| 47 | 0.26012 | SLU_3 | Min | -775.921 | -1487.655 | 0. |
| 47 | 0. | SLU_4 | Max | -645.96 | -1442.381 | 0. |
| 47 | 0.13006 | SLU_4 | Max | -645.96 | -1456.851 | 0. |
| 47 | 0.26012 | SLU_4 | Max | -645.96 | -1471.32 | 0. |
| 47 | 0. | SLU_4 | Min | -645.96 | -1442.381 | 0. |
| 47 | 0.13006 | SLU_4 | Min | -645.96 | -1456.851 | 0. |
| 47 | 0.26012 | SLU_4 | Min | -645.96 | -1471.32 | 0. |
| 47 | 0. | SLE_F1 | Max | -563.246 | -1082.327 | 0. |
| 47 | 0.13006 | SLE_F1 | Max | -563.246 | -1093.457 | 0. |
| 47 | 0.26012 | SLE_F1 | Max | -563.246 | -1104.588 | 0. |
| 47 | 0. | SLE_F1 | Min | -563.246 | -1082.327 | 0. |
| 47 | 0.13006 | SLE_F1 | Min | -563.246 | -1093.457 | 0. |
| 47 | 0.26012 | SLE_F1 | Min | -563.246 | -1104.588 | 0. |
| 47 | 0. | SLE_F2 | Max | -491.846 | -1074.518 | 0. |
| 47 | 0.13006 | SLE_F2 | Max | -491.846 | -1085.649 | 0. |
| 47 | 0.26012 | SLE_F2 | Max | -491.846 | -1096.779 | 0. |
| 47 | 0. | SLE_F2 | Min | -491.846 | -1074.518 | 0. |
| 47 | 0.13006 | SLE_F2 | Min | -491.846 | -1085.649 | 0. |
| 47 | 0.26012 | SLE_F2 | Min | -491.846 | -1096.779 | 0. |
| 47 | 0. | SLE_F3 | Max | -505.05 | -1076.293 | 0. |
| 47 | 0.13006 | SLE_F3 | Max | -505.05 | -1087.424 | 0. |
| 47 | 0.26012 | SLE_F3 | Max | -505.05 | -1098.554 | 0. |
| 47 | 0. | SLE_F3 | Min | -505.05 | -1076.293 | 0. |
| 47 | 0.13006 | SLE_F3 | Min | -505.05 | -1087.424 | 0. |
| 47 | 0.26012 | SLE_F3 | Min | -505.05 | -1098.554 | 0. |
| 47 | 0. | SLE_F4 | Max | -609.197 | -1088.872 | 0. |
| 47 | 0.13006 | SLE_F4 | Max | -609.197 | -1100.003 | 0. |
| 47 | 0.26012 | SLE_F4 | Max | -609.197 | -1111.133 | 0. |
| 47 | 0. | SLE_F4 | Min | -609.197 | -1088.872 | 0. |
| 47 | 0.13006 | SLE_F4 | Min | -609.197 | -1100.003 | 0. |
| 47 | 0.26012 | SLE_F4 | Min | -609.197 | -1111.133 | 0. |
| 47 | 0. | SLE_QP1 | Max | -577.013 | -1020.28 | 0. |
| 47 | 0.13006 | SLE_QP1 | Max | -577.013 | -1031.411 | 0. |
| 47 | 0.26012 | SLE_QP1 | Max | -577.013 | -1042.541 | 0. |
| 47 | 0. | SLE_QP1 | Min | -577.013 | -1020.28 | 0. |
| 47 | 0.13006 | SLE_QP1 | Min | -577.013 | -1031.411 | 0. |
| 47 | 0.26012 | SLE_QP1 | Min | -577.013 | -1042.541 | 0. |
| 47 | 0. | SLE_QP2 | Max | -508.517 | -1013.179 | 0. |
| 47 | 0.13006 | SLE_QP2 | Max | -508.517 | -1024.309 | 0. |
| 47 | 0.26012 | SLE_QP2 | Max | -508.517 | -1035.44 | 0. |
| 47 | 0. | SLE_QP2 | Min | -508.517 | -1013.179 | 0. |
| 47 | 0.13006 | SLE_QP2 | Min | -508.517 | -1024.309 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|-----------|----------|
| 47 | 0.26012 | SLE_QP2 | Min | -508.517 | -1035.44 | 0. |
| 47 | 0. | SLE_QP3 | Max | -520.2 | -1014.58 | 0. |
| 47 | 0.13006 | SLE_QP3 | Max | -520.2 | -1025.711 | 0. |
| 47 | 0.26012 | SLE_QP3 | Max | -520.2 | -1036.841 | 0. |
| 47 | 0. | SLE_QP3 | Min | -520.2 | -1014.58 | 0. |
| 47 | 0.13006 | SLE_QP3 | Min | -520.2 | -1025.711 | 0. |
| 47 | 0.26012 | SLE_QP3 | Min | -520.2 | -1036.841 | 0. |
| 47 | 0. | SLE_QP4 | Max | -633.228 | -1027.761 | 0. |
| 47 | 0.13006 | SLE_QP4 | Max | -633.228 | -1038.892 | 0. |
| 47 | 0.26012 | SLE_QP4 | Max | -633.228 | -1050.022 | 0. |
| 47 | 0. | SLE_QP4 | Min | -633.228 | -1027.761 | 0. |
| 47 | 0.13006 | SLE_QP4 | Min | -633.228 | -1038.892 | 0. |
| 47 | 0.26012 | SLE_QP4 | Min | -633.228 | -1050.022 | 0. |
| 47 | 0. | SLV_1 | Max | -1386.425 | -1271.138 | 0. |
| 47 | 0.13006 | SLV_1 | Max | -1386.425 | -1282.268 | 0. |
| 47 | 0.26012 | SLV_1 | Max | -1386.425 | -1293.399 | 0. |
| 47 | 0. | SLV_1 | Min | -1386.425 | -1271.138 | 0. |
| 47 | 0.13006 | SLV_1 | Min | -1386.425 | -1282.268 | 0. |
| 47 | 0.26012 | SLV_1 | Min | -1386.425 | -1293.399 | 0. |
| 47 | 0. | SLV_2 | Max | -1389.145 | -1269.288 | 0. |
| 47 | 0.13006 | SLV_2 | Max | -1389.145 | -1280.419 | 0. |
| 47 | 0.26012 | SLV_2 | Max | -1389.145 | -1291.549 | 0. |
| 47 | 0. | SLV_2 | Min | -1389.145 | -1269.288 | 0. |
| 47 | 0.13006 | SLV_2 | Min | -1389.145 | -1280.419 | 0. |
| 47 | 0.26012 | SLV_2 | Min | -1389.145 | -1291.549 | 0. |
| 47 | 0. | SLV_3 | Max | -1541.399 | -1336.75 | 0. |
| 47 | 0.13006 | SLV_3 | Max | -1541.399 | -1347.881 | 0. |
| 47 | 0.26012 | SLV_3 | Max | -1541.399 | -1359.011 | 0. |
| 47 | 0. | SLV_3 | Min | -1541.399 | -1336.75 | 0. |
| 47 | 0.13006 | SLV_3 | Min | -1541.399 | -1347.881 | 0. |
| 47 | 0.26012 | SLV_3 | Min | -1541.399 | -1359.011 | 0. |
| 47 | 0. | SLV_4 | Max | -1543.867 | -1334.721 | 0. |
| 47 | 0.13006 | SLV_4 | Max | -1543.867 | -1345.851 | 0. |
| 47 | 0.26012 | SLV_4 | Max | -1543.867 | -1356.982 | 0. |
| 47 | 0. | SLV_4 | Min | -1543.867 | -1334.721 | 0. |
| 47 | 0.13006 | SLV_4 | Min | -1543.867 | -1345.851 | 0. |
| 47 | 0.26012 | SLV_4 | Min | -1543.867 | -1356.982 | 0. |
| 47 | 0. | SLD_1 | Max | -879.178 | -1093.542 | 0. |
| 47 | 0.13006 | SLD_1 | Max | -879.178 | -1104.673 | 0. |
| 47 | 0.26012 | SLD_1 | Max | -879.178 | -1115.803 | 0. |
| 47 | 0. | SLD_1 | Min | -879.178 | -1093.542 | 0. |
| 47 | 0.13006 | SLD_1 | Min | -879.178 | -1104.673 | 0. |
| 47 | 0.26012 | SLD_1 | Min | -879.178 | -1115.803 | 0. |
| 47 | 0. | SLD_2 | Max | -880.566 | -1092.761 | 0. |
| 47 | 0.13006 | SLD_2 | Max | -880.566 | -1103.892 | 0. |
| 47 | 0.26012 | SLD_2 | Max | -880.566 | -1115.022 | 0. |
| 47 | 0. | SLD_2 | Min | -880.566 | -1092.761 | 0. |
| 47 | 0.13006 | SLD_2 | Min | -880.566 | -1103.892 | 0. |
| 47 | 0.26012 | SLD_2 | Min | -880.566 | -1115.022 | 0. |
| 47 | 0. | SLD_3 | Max | -1035.135 | -1153.82 | 0. |
| 47 | 0.13006 | SLD_3 | Max | -1035.135 | -1164.951 | 0. |
| 47 | 0.26012 | SLD_3 | Max | -1035.135 | -1176.081 | 0. |
| 47 | 0. | SLD_3 | Min | -1035.135 | -1153.82 | 0. |
| 47 | 0.13006 | SLD_3 | Min | -1035.135 | -1164.951 | 0. |
| 47 | 0.26012 | SLD_3 | Min | -1035.135 | -1176.081 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|-----------|----------|
| 47 | 0. | SLD_4 | Max | -1036.166 | -1152.88 | 0. |
| 47 | 0.13006 | SLD_4 | Max | -1036.166 | -1164.011 | 0. |
| 47 | 0.26012 | SLD_4 | Max | -1036.166 | -1175.141 | 0. |
| 47 | 0. | SLD_4 | Min | -1036.166 | -1152.88 | 0. |
| 47 | 0.13006 | SLD_4 | Min | -1036.166 | -1164.011 | 0. |
| 47 | 0.26012 | SLD_4 | Min | -1036.166 | -1175.141 | 0. |
| 47 | 0. | SLU_IDR_1 | Max | -586.487 | -1045.209 | 0. |
| 47 | 0.13006 | SLU_IDR_1 | Max | -586.487 | -1058.427 | 0. |
| 47 | 0.26012 | SLU_IDR_1 | Max | -586.487 | -1071.646 | 0. |
| 47 | 0. | SLU_IDR_1 | Min | -586.487 | -1045.209 | 0. |
| 47 | 0.13006 | SLU_IDR_1 | Min | -586.487 | -1058.427 | 0. |
| 47 | 0.26012 | SLU_IDR_1 | Min | -586.487 | -1071.646 | 0. |
| 47 | 0. | SLU_IDR_2 | Max | -581.355 | -1047.733 | 0. |
| 47 | 0.13006 | SLU_IDR_2 | Max | -581.355 | -1060.952 | 0. |
| 47 | 0.26012 | SLU_IDR_2 | Max | -581.355 | -1074.171 | 0. |
| 47 | 0. | SLU_IDR_2 | Min | -581.355 | -1047.733 | 0. |
| 47 | 0.13006 | SLU_IDR_2 | Min | -581.355 | -1060.952 | 0. |
| 47 | 0.26012 | SLU_IDR_2 | Min | -581.355 | -1074.171 | 0. |
| 47 | 0. | SISMA WOOD SLV-1 | Max | -829.829 | -271.056 | 0. |
| 47 | 0.13006 | SISMA WOOD SLV-1 | Max | -829.829 | -271.056 | 0. |
| 47 | 0.26012 | SISMA WOOD SLV-1 | Max | -829.829 | -271.056 | 0. |
| 47 | 0. | SISMA WOOD SLV-1 | Min | -829.829 | -271.056 | 0. |
| 47 | 0.13006 | SISMA WOOD SLV-1 | Min | -829.829 | -271.056 | 0. |
| 47 | 0.26012 | SISMA WOOD SLV-1 | Min | -829.829 | -271.056 | 0. |
| 47 | 0. | DEAD-1 | Max | 58.574 | -90.748 | 0. |
| 47 | 0.13006 | DEAD-1 | Max | 58.574 | -85.872 | 0. |
| 47 | 0.26012 | DEAD-1 | Max | 58.574 | -80.996 | 0. |
| 47 | 0. | DEAD-1 | Min | 58.574 | -90.748 | 0. |
| 47 | 0.13006 | DEAD-1 | Min | 58.574 | -85.872 | 0. |
| 47 | 0.26012 | DEAD-1 | Min | 58.574 | -80.996 | 0. |
| 47 | 0. | SLU_PROVA | | -729.221 | -1355.094 | 0. |
| 47 | 0.13006 | SLU_PROVA | | -729.221 | -1369.564 | 0. |
| 47 | 0.26012 | SLU_PROVA | | -729.221 | -1384.034 | 0. |
| 48 | 0. | DEAD | | 50.447 | -265.755 | 0. |
| 48 | 0.13006 | DEAD | | 50.447 | -260.88 | 0. |
| 48 | 0.26012 | DEAD | | 50.447 | -256.004 | 0. |
| 48 | 0. | SIMM_KA | | -143.95 | -20.084 | 0. |
| 48 | 0.13006 | SIMM_KA | | -143.95 | -20.084 | 0. |
| 48 | 0.26012 | SIMM_KA | | -143.95 | -20.084 | 0. |
| 48 | 0. | SIMM_K0 | | -217.139 | -30.714 | 0. |
| 48 | 0.13006 | SIMM_K0 | | -217.139 | -30.714 | 0. |
| 48 | 0.26012 | SIMM_K0 | | -217.139 | -30.714 | 0. |
| 48 | 0. | A--SIMM_KA | | -171.968 | -51.581 | 0. |
| 48 | 0.13006 | A--SIMM_KA | | -171.968 | -51.581 | 0. |
| 48 | 0.26012 | A--SIMM_KA | | -171.968 | -51.581 | 0. |
| 48 | 0. | A--SIMM_K0 | | -265.606 | -77.556 | 0. |
| 48 | 0.13006 | A--SIMM_K0 | | -265.606 | -77.556 | 0. |
| 48 | 0.26012 | A--SIMM_K0 | | -265.606 | -77.556 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 48 | 0. | A-- SIMM_SOVR_K A | | -8.35 | -2.528 | 0. |
| 48 | 0.13006 | A-- SIMM_SOVR_K A | | -8.35 | -2.528 | 0. |
| 48 | 0.26012 | A-- SIMM_SOVR_K A | | -8.35 | -2.528 | 0. |
| 48 | 0. | A-- SIMM_SOVR_K 0 | | -12.518 | -3.789 | 0. |
| 48 | 0.13006 | A-- SIMM_SOVR_K 0 | | -12.518 | -3.789 | 0. |
| 48 | 0.26012 | A-- SIMM_SOVR_K 0 | | -12.518 | -3.789 | 0. |
| 48 | 0. | SIMM_SOVR_K 0 | | -12.518 | -3.789 | 0. |
| 48 | 0.13006 | SIMM_SOVR_K 0 | | -12.518 | -3.789 | 0. |
| 48 | 0.26012 | SIMM_SOVR_K 0 | | -12.518 | -3.789 | 0. |
| 48 | 0. | SIMM_SOVR_K A | | -8.35 | -2.528 | 0. |
| 48 | 0.13006 | SIMM_SOVR_K A | | -8.35 | -2.528 | 0. |
| 48 | 0.26012 | SIMM_SOVR_K A | | -8.35 | -2.528 | 0. |
| 48 | 0. | SOVR | | 18.356 | -154.25 | 0. |
| 48 | 0.13006 | SOVR | | 18.356 | -154.25 | 0. |
| 48 | 0.26012 | SOVR | | 18.356 | -154.25 | 0. |
| 48 | 0. | TERR_SIMM | | 50.748 | -620.984 | 0. |
| 48 | 0.13006 | TERR_SIMM | | 50.748 | -620.984 | 0. |
| 48 | 0.26012 | TERR_SIMM | | 50.748 | -620.984 | 0. |
| 48 | 0. | TERR_A--SIMM | | 54.966 | -608.265 | 0. |
| 48 | 0.13006 | TERR_A--SIMM | | 54.966 | -608.265 | 0. |
| 48 | 0.26012 | TERR_A--SIMM | | 54.966 | -608.265 | 0. |
| 48 | 0. | INERZIA H SLV | | -7.248 | -4.309 | 0. |
| 48 | 0.13006 | INERZIA H SLV | | -7.248 | -4.309 | 0. |
| 48 | 0.26012 | INERZIA H SLV | | -7.248 | -4.309 | 0. |
| 48 | 0. | INERZIA V + SLV | | 0.795 | -4.216 | 0. |
| 48 | 0.13006 | INERZIA V + SLV | | 0.795 | -4.216 | 0. |
| 48 | 0.26012 | INERZIA V + SLV | | 0.795 | -4.216 | 0. |
| 48 | 0. | INERZIA V - SLV | | -0.795 | 4.216 | 0. |
| 48 | 0.13006 | INERZIA V - SLV | | -0.795 | 4.216 | 0. |
| 48 | 0.26012 | INERZIA V - SLV | | -0.795 | 4.216 | 0. |
| 48 | 0. | SISMA WOOD SLV | | -365.885 | -192.996 | 0. |
| 48 | 0.13006 | SISMA WOOD SLV | | -365.885 | -192.996 | 0. |
| 48 | 0.26012 | SISMA WOOD SLV | | -365.885 | -192.996 | 0. |
| 48 | 0. | iDROSTATICA | | -451.731 | -405.238 | 0. |
| 48 | 0.13006 | iDROSTATICA | | -451.731 | -421.244 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|----------|-----------|----------|
| 48 | 0.26012 | iDROSTATICA | | -451.731 | -437.25 | 0. |
| 48 | 0. | SISMA WOOD SLD | | -161.589 | -85.235 | 0. |
| 48 | 0.13006 | SISMA WOOD SLD | | -161.589 | -85.235 | 0. |
| 48 | 0.26012 | SISMA WOOD SLD | | -161.589 | -85.235 | 0. |
| 48 | 0. | INERZIA H SLD | | -3.201 | -1.903 | 0. |
| 48 | 0.13006 | INERZIA H SLD | | -3.201 | -1.903 | 0. |
| 48 | 0.26012 | INERZIA H SLD | | -3.201 | -1.903 | 0. |
| 48 | 0. | INERZIA V + SLD | | 0.351 | -1.862 | 0. |
| 48 | 0.13006 | INERZIA V + SLD | | 0.351 | -1.862 | 0. |
| 48 | 0.26012 | INERZIA V + SLD | | 0.351 | -1.862 | 0. |
| 48 | 0. | INERZIA V SLD | | -0.351 | 1.862 | 0. |
| 48 | 0.13006 | INERZIA V SLD | | -0.351 | 1.862 | 0. |
| 48 | 0.26012 | INERZIA V SLD | | -0.351 | 1.862 | 0. |
| 48 | 0. | INERZIA V -1 | | -0.795 | 4.216 | 0. |
| 48 | 0.13006 | INERZIA V -1 | | -0.795 | 4.216 | 0. |
| 48 | 0.26012 | INERZIA V -1 | | -0.795 | 4.216 | 0. |
| 48 | 0. | SLU_1 | Max | -723.432 | -2127.603 | 0. |
| 48 | 0.13006 | SLU_1 | Max | -723.432 | -2142.073 | 0. |
| 48 | 0.26012 | SLU_1 | Max | -723.432 | -2156.543 | 0. |
| 48 | 0. | SLU_1 | Min | -723.432 | -2127.603 | 0. |
| 48 | 0.13006 | SLU_1 | Min | -723.432 | -2142.073 | 0. |
| 48 | 0.26012 | SLU_1 | Min | -723.432 | -2156.543 | 0. |
| 48 | 0. | SLU_2 | Max | -627.731 | -2122.078 | 0. |
| 48 | 0.13006 | SLU_2 | Max | -627.731 | -2136.547 | 0. |
| 48 | 0.26012 | SLU_2 | Max | -627.731 | -2151.017 | 0. |
| 48 | 0. | SLU_2 | Min | -627.731 | -2122.078 | 0. |
| 48 | 0.13006 | SLU_2 | Min | -627.731 | -2136.547 | 0. |
| 48 | 0.26012 | SLU_2 | Min | -627.731 | -2151.017 | 0. |
| 48 | 0. | SLU_3 | Max | -775.921 | -2173.72 | 0. |
| 48 | 0.13006 | SLU_3 | Max | -775.921 | -2188.189 | 0. |
| 48 | 0.26012 | SLU_3 | Max | -775.921 | -2202.659 | 0. |
| 48 | 0. | SLU_3 | Min | -775.921 | -2173.72 | 0. |
| 48 | 0.13006 | SLU_3 | Min | -775.921 | -2188.189 | 0. |
| 48 | 0.26012 | SLU_3 | Min | -775.921 | -2202.659 | 0. |
| 48 | 0. | SLU_4 | Max | -645.96 | -2155.246 | 0. |
| 48 | 0.13006 | SLU_4 | Max | -645.96 | -2169.716 | 0. |
| 48 | 0.26012 | SLU_4 | Max | -645.96 | -2184.186 | 0. |
| 48 | 0. | SLU_4 | Min | -645.96 | -2155.246 | 0. |
| 48 | 0.13006 | SLU_4 | Min | -645.96 | -2169.716 | 0. |
| 48 | 0.26012 | SLU_4 | Min | -645.96 | -2184.186 | 0. |
| 48 | 0. | SLE_F1 | Max | -563.246 | -1564.642 | 0. |
| 48 | 0.13006 | SLE_F1 | Max | -563.246 | -1575.772 | 0. |
| 48 | 0.26012 | SLE_F1 | Max | -563.246 | -1586.903 | 0. |
| 48 | 0. | SLE_F1 | Min | -563.246 | -1564.642 | 0. |
| 48 | 0.13006 | SLE_F1 | Min | -563.246 | -1575.772 | 0. |
| 48 | 0.26012 | SLE_F1 | Min | -563.246 | -1586.903 | 0. |
| 48 | 0. | SLE_F2 | Max | -491.846 | -1561.048 | 0. |
| 48 | 0.13006 | SLE_F2 | Max | -491.846 | -1572.178 | 0. |
| 48 | 0.26012 | SLE_F2 | Max | -491.846 | -1583.309 | 0. |
| 48 | 0. | SLE_F2 | Min | -491.846 | -1561.048 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|-----------|----------|
| 48 | 0.13006 | SLE_F2 | Min | -491.846 | -1572.178 | 0. |
| 48 | 0.26012 | SLE_F2 | Min | -491.846 | -1583.309 | 0. |
| 48 | 0. | SLE_F3 | Max | -505.05 | -1586.823 | 0. |
| 48 | 0.13006 | SLE_F3 | Max | -505.05 | -1597.953 | 0. |
| 48 | 0.26012 | SLE_F3 | Max | -505.05 | -1609.084 | 0. |
| 48 | 0. | SLE_F3 | Min | -505.05 | -1586.823 | 0. |
| 48 | 0.13006 | SLE_F3 | Min | -505.05 | -1597.953 | 0. |
| 48 | 0.26012 | SLE_F3 | Min | -505.05 | -1609.084 | 0. |
| 48 | 0. | SLE_F4 | Max | -609.197 | -1601.626 | 0. |
| 48 | 0.13006 | SLE_F4 | Max | -609.197 | -1612.756 | 0. |
| 48 | 0.26012 | SLE_F4 | Max | -609.197 | -1623.887 | 0. |
| 48 | 0. | SLE_F4 | Min | -609.197 | -1601.626 | 0. |
| 48 | 0.13006 | SLE_F4 | Min | -609.197 | -1612.756 | 0. |
| 48 | 0.26012 | SLE_F4 | Min | -609.197 | -1623.887 | 0. |
| 48 | 0. | SLE_QP1 | Max | -577.013 | -1431.788 | 0. |
| 48 | 0.13006 | SLE_QP1 | Max | -577.013 | -1442.918 | 0. |
| 48 | 0.26012 | SLE_QP1 | Max | -577.013 | -1454.049 | 0. |
| 48 | 0. | SLE_QP1 | Min | -577.013 | -1431.788 | 0. |
| 48 | 0.13006 | SLE_QP1 | Min | -577.013 | -1442.918 | 0. |
| 48 | 0.26012 | SLE_QP1 | Min | -577.013 | -1454.049 | 0. |
| 48 | 0. | SLE_QP2 | Max | -508.517 | -1428.602 | 0. |
| 48 | 0.13006 | SLE_QP2 | Max | -508.517 | -1439.732 | 0. |
| 48 | 0.26012 | SLE_QP2 | Max | -508.517 | -1450.863 | 0. |
| 48 | 0. | SLE_QP2 | Min | -508.517 | -1428.602 | 0. |
| 48 | 0.13006 | SLE_QP2 | Min | -508.517 | -1439.732 | 0. |
| 48 | 0.26012 | SLE_QP2 | Min | -508.517 | -1450.863 | 0. |
| 48 | 0. | SLE_QP3 | Max | -520.2 | -1454.857 | 0. |
| 48 | 0.13006 | SLE_QP3 | Max | -520.2 | -1465.988 | 0. |
| 48 | 0.26012 | SLE_QP3 | Max | -520.2 | -1477.118 | 0. |
| 48 | 0. | SLE_QP3 | Min | -520.2 | -1454.857 | 0. |
| 48 | 0.13006 | SLE_QP3 | Min | -520.2 | -1465.988 | 0. |
| 48 | 0.26012 | SLE_QP3 | Min | -520.2 | -1477.118 | 0. |
| 48 | 0. | SLE_QP4 | Max | -633.228 | -1471.216 | 0. |
| 48 | 0.13006 | SLE_QP4 | Max | -633.228 | -1482.347 | 0. |
| 48 | 0.26012 | SLE_QP4 | Max | -633.228 | -1493.477 | 0. |
| 48 | 0. | SLE_QP4 | Min | -633.228 | -1471.216 | 0. |
| 48 | 0.13006 | SLE_QP4 | Min | -633.228 | -1482.347 | 0. |
| 48 | 0.26012 | SLE_QP4 | Min | -633.228 | -1493.477 | 0. |
| 48 | 0. | SLV_1 | Max | -1386.74 | -1712.544 | 0. |
| 48 | 0.13006 | SLV_1 | Max | -1386.74 | -1723.674 | 0. |
| 48 | 0.26012 | SLV_1 | Max | -1386.74 | -1734.805 | 0. |
| 48 | 0. | SLV_1 | Min | -1386.74 | -1712.544 | 0. |
| 48 | 0.13006 | SLV_1 | Min | -1386.74 | -1723.674 | 0. |
| 48 | 0.26012 | SLV_1 | Min | -1386.74 | -1734.805 | 0. |
| 48 | 0. | SLV_2 | Max | -1389.46 | -1703.611 | 0. |
| 48 | 0.13006 | SLV_2 | Max | -1389.46 | -1714.741 | 0. |
| 48 | 0.26012 | SLV_2 | Max | -1389.46 | -1725.872 | 0. |
| 48 | 0. | SLV_2 | Min | -1389.46 | -1703.611 | 0. |
| 48 | 0.13006 | SLV_2 | Min | -1389.46 | -1714.741 | 0. |
| 48 | 0.26012 | SLV_2 | Min | -1389.46 | -1725.872 | 0. |
| 48 | 0. | SLV_3 | Max | -1541.714 | -1801.701 | 0. |
| 48 | 0.13006 | SLV_3 | Max | -1541.714 | -1812.832 | 0. |
| 48 | 0.26012 | SLV_3 | Max | -1541.714 | -1823.962 | 0. |
| 48 | 0. | SLV_3 | Min | -1541.714 | -1801.701 | 0. |
| 48 | 0.13006 | SLV_3 | Min | -1541.714 | -1812.832 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|-----------|----------|
| 48 | 0.26012 | SLV_3 | Min | -1541.714 | -1823.962 | 0. |
| 48 | 0. | SLV_4 | Max | -1544.182 | -1792.615 | 0. |
| 48 | 0.13006 | SLV_4 | Max | -1544.182 | -1803.746 | 0. |
| 48 | 0.26012 | SLV_4 | Max | -1544.182 | -1814.876 | 0. |
| 48 | 0. | SLV_4 | Min | -1544.182 | -1792.615 | 0. |
| 48 | 0.13006 | SLV_4 | Min | -1544.182 | -1803.746 | 0. |
| 48 | 0.26012 | SLV_4 | Min | -1544.182 | -1814.876 | 0. |
| 48 | 0. | SLD_1 | Max | -879.318 | -1522.11 | 0. |
| 48 | 0.13006 | SLD_1 | Max | -879.318 | -1533.241 | 0. |
| 48 | 0.26012 | SLD_1 | Max | -879.318 | -1544.371 | 0. |
| 48 | 0. | SLD_1 | Min | -879.318 | -1522.11 | 0. |
| 48 | 0.13006 | SLD_1 | Min | -879.318 | -1533.241 | 0. |
| 48 | 0.26012 | SLD_1 | Min | -879.318 | -1544.371 | 0. |
| 48 | 0. | SLD_2 | Max | -880.705 | -1517.947 | 0. |
| 48 | 0.13006 | SLD_2 | Max | -880.705 | -1529.077 | 0. |
| 48 | 0.26012 | SLD_2 | Max | -880.705 | -1540.208 | 0. |
| 48 | 0. | SLD_2 | Min | -880.705 | -1517.947 | 0. |
| 48 | 0.13006 | SLD_2 | Min | -880.705 | -1529.077 | 0. |
| 48 | 0.26012 | SLD_2 | Min | -880.705 | -1540.208 | 0. |
| 48 | 0. | SLD_3 | Max | -1035.274 | -1605.779 | 0. |
| 48 | 0.13006 | SLD_3 | Max | -1035.274 | -1616.91 | 0. |
| 48 | 0.26012 | SLD_3 | Max | -1035.274 | -1628.041 | 0. |
| 48 | 0. | SLD_3 | Min | -1035.274 | -1605.779 | 0. |
| 48 | 0.13006 | SLD_3 | Min | -1035.274 | -1616.91 | 0. |
| 48 | 0.26012 | SLD_3 | Min | -1035.274 | -1628.041 | 0. |
| 48 | 0. | SLD_4 | Max | -1036.305 | -1601.677 | 0. |
| 48 | 0.13006 | SLD_4 | Max | -1036.305 | -1612.807 | 0. |
| 48 | 0.26012 | SLD_4 | Max | -1036.305 | -1623.938 | 0. |
| 48 | 0. | SLD_4 | Min | -1036.305 | -1601.677 | 0. |
| 48 | 0.13006 | SLD_4 | Min | -1036.305 | -1612.807 | 0. |
| 48 | 0.26012 | SLD_4 | Min | -1036.305 | -1623.938 | 0. |
| 48 | 0. | SLU_IDR_1 | Max | -586.487 | -1396.634 | 0. |
| 48 | 0.13006 | SLU_IDR_1 | Max | -586.487 | -1409.852 | 0. |
| 48 | 0.26012 | SLU_IDR_1 | Max | -586.487 | -1423.071 | 0. |
| 48 | 0. | SLU_IDR_1 | Min | -586.487 | -1396.634 | 0. |
| 48 | 0.13006 | SLU_IDR_1 | Min | -586.487 | -1409.852 | 0. |
| 48 | 0.26012 | SLU_IDR_1 | Min | -586.487 | -1423.071 | 0. |
| 48 | 0. | SLU_IDR_2 | Max | -581.355 | -1373.187 | 0. |
| 48 | 0.13006 | SLU_IDR_2 | Max | -581.355 | -1386.406 | 0. |
| 48 | 0.26012 | SLU_IDR_2 | Max | -581.355 | -1399.625 | 0. |
| 48 | 0. | SLU_IDR_2 | Min | -581.355 | -1373.187 | 0. |
| 48 | 0.13006 | SLU_IDR_2 | Min | -581.355 | -1386.406 | 0. |
| 48 | 0.26012 | SLU_IDR_2 | Min | -581.355 | -1399.625 | 0. |
| 48 | 0. | SISMA WOOD SLV-1 | Max | -829.829 | -386.641 | 0. |
| 48 | 0.13006 | SISMA WOOD SLV-1 | Max | -829.829 | -386.641 | 0. |
| 48 | 0.26012 | SISMA WOOD SLV-1 | Max | -829.829 | -386.641 | 0. |
| 48 | 0. | SISMA WOOD SLV-1 | Min | -829.829 | -386.641 | 0. |
| 48 | 0.13006 | SISMA WOOD SLV-1 | Min | -829.829 | -386.641 | 0. |
| 48 | 0.26012 | SISMA WOOD SLV-1 | Min | -829.829 | -386.641 | 0. |
| 48 | 0. | DEAD-1 | Max | 58.574 | -316.664 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|-----------|----------|
| 48 | 0.13006 | DEAD-1 | Max | 58.574 | -311.788 | 0. |
| 48 | 0.26012 | DEAD-1 | Max | 58.574 | -306.912 | 0. |
| 48 | 0. | DEAD-1 | Min | 58.574 | -316.664 | 0. |
| 48 | 0.13006 | DEAD-1 | Min | 58.574 | -311.788 | 0. |
| 48 | 0.26012 | DEAD-1 | Min | 58.574 | -306.912 | 0. |
| 48 | 0. | SLU_PROVA | | -729.221 | -1956.558 | 0. |
| 48 | 0.13006 | SLU_PROVA | | -729.221 | -1971.027 | 0. |
| 48 | 0.26012 | SLU_PROVA | | -729.221 | -1985.497 | 0. |
| 49 | 0. | DEAD | | -362.095 | 50.683 | 0. |
| 49 | 0.1319 | DEAD | | -357.15 | 50.683 | 0. |
| 49 | 0.2638 | DEAD | | -352.205 | 50.683 | 0. |
| 49 | 0. | SIMM_KA | | -12.176 | -144.902 | 0. |
| 49 | 0.1319 | SIMM_KA | | -12.176 | -137.513 | 0. |
| 49 | 0.2638 | SIMM_KA | | -12.176 | -130.124 | 0. |
| 49 | 0. | SIMM_K0 | | -18.659 | -218.586 | 0. |
| 49 | 0.1319 | SIMM_K0 | | -18.659 | -207.502 | 0. |
| 49 | 0.2638 | SIMM_K0 | | -18.659 | -196.419 | 0. |
| 49 | 0. | A--SIMM_KA | | -53.237 | -169.479 | 0. |
| 49 | 0.1319 | A--SIMM_KA | | -53.237 | -162.51 | 0. |
| 49 | 0.2638 | A--SIMM_KA | | -53.237 | -155.54 | 0. |
| 49 | 0. | A--SIMM_K0 | | -79.793 | -262.169 | 0. |
| 49 | 0.1319 | A--SIMM_K0 | | -79.793 | -251.714 | 0. |
| 49 | 0.2638 | A--SIMM_K0 | | -79.793 | -241.26 | 0. |
| 49 | 0. | A-- SIMM_SOVR_K A | | -1.62 | -8.446 | 0. |
| 49 | 0.1319 | A-- SIMM_SOVR_K A | | -1.62 | -8.446 | 0. |
| 49 | 0.2638 | A-- SIMM_SOVR_K A | | -1.62 | -8.446 | 0. |
| 49 | 0. | A-- SIMM_SOVR_K 0 | | -2.429 | -12.663 | 0. |
| 49 | 0.1319 | A-- SIMM_SOVR_K 0 | | -2.429 | -12.663 | 0. |
| 49 | 0.2638 | A-- SIMM_SOVR_K 0 | | -2.429 | -12.663 | 0. |
| 49 | 0. | SIMM_SOVR_K 0 | | -2.429 | -12.663 | 0. |
| 49 | 0.1319 | SIMM_SOVR_K 0 | | -2.429 | -12.663 | 0. |
| 49 | 0.2638 | SIMM_SOVR_K 0 | | -2.429 | -12.663 | 0. |
| 49 | 0. | SIMM_SOVR_K A | | -1.62 | -8.446 | 0. |
| 49 | 0.1319 | SIMM_SOVR_K A | | -1.62 | -8.446 | 0. |
| 49 | 0.2638 | SIMM_SOVR_K A | | -1.62 | -8.446 | 0. |
| 49 | 0. | SOVR | | -195.45 | 19.041 | 0. |
| 49 | 0.1319 | SOVR | | -195.45 | 19.041 | 0. |
| 49 | 0.2638 | SOVR | | -195.45 | 19.041 | 0. |
| 49 | 0. | TERR_SIMM | | -782.714 | 53.218 | 0. |
| 49 | 0.1319 | TERR_SIMM | | -782.714 | 53.218 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 49 | 0.2638 | TERR_SIMM | | -782.714 | 53.218 | 0. |
| 49 | 0. | TERR_A--SIMM | | -764.488 | 58.612 | 0. |
| 49 | 0.1319 | TERR_A--SIMM | | -764.488 | 58.612 | 0. |
| 49 | 0.2638 | TERR_A--SIMM | | -764.488 | 58.612 | 0. |
| 49 | 0. | INERZIA H SLV | | -4.979 | -6.886 | 0. |
| 49 | 0.1319 | INERZIA H SLV | | -4.979 | -6.886 | 0. |
| 49 | 0.2638 | INERZIA H SLV | | -4.979 | -6.886 | 0. |
| 49 | 0. | INERZIA V + SLV | | -5.772 | 0.798 | 0. |
| 49 | 0.1319 | INERZIA V + SLV | | -5.772 | 0.798 | 0. |
| 49 | 0.2638 | INERZIA V + SLV | | -5.772 | 0.798 | 0. |
| 49 | 0. | INERZIA V - SLV | | 5.772 | -0.798 | 0. |
| 49 | 0.1319 | INERZIA V - SLV | | 5.772 | -0.798 | 0. |
| 49 | 0.2638 | INERZIA V - SLV | | 5.772 | -0.798 | 0. |
| 49 | 0. | SISMA WOOD SLV | | -218.64 | -343.686 | 0. |
| 49 | 0.1319 | SISMA WOOD SLV | | -218.64 | -343.686 | 0. |
| 49 | 0.2638 | SISMA WOOD SLV | | -218.64 | -343.686 | 0. |
| 49 | 0. | iDROSTATICA | | -364.069 | -449.559 | 0. |
| 49 | 0.1319 | iDROSTATICA | | -364.069 | -433.416 | 0. |
| 49 | 0.2638 | iDROSTATICA | | -364.069 | -417.451 | 0. |
| 49 | 0. | SISMA WOOD SLD | | -96.56 | -151.785 | 0. |
| 49 | 0.1319 | SISMA WOOD SLD | | -96.56 | -151.785 | 0. |
| 49 | 0.2638 | SISMA WOOD SLD | | -96.56 | -151.785 | 0. |
| 49 | 0. | INERZIA H SLD | | -2.199 | -3.041 | 0. |
| 49 | 0.1319 | INERZIA H SLD | | -2.199 | -3.041 | 0. |
| 49 | 0.2638 | INERZIA H SLD | | -2.199 | -3.041 | 0. |
| 49 | 0. | INERZIA V + SLD | | -2.549 | 0.353 | 0. |
| 49 | 0.1319 | INERZIA V + SLD | | -2.549 | 0.353 | 0. |
| 49 | 0.2638 | INERZIA V + SLD | | -2.549 | 0.353 | 0. |
| 49 | 0. | INERZIA V SLD | | 2.549 | -0.353 | 0. |
| 49 | 0.1319 | INERZIA V SLD | | 2.549 | -0.353 | 0. |
| 49 | 0.2638 | INERZIA V SLD | | 2.549 | -0.353 | 0. |
| 49 | 0. | INERZIA V -1 | | 5.772 | -0.798 | 0. |
| 49 | 0.1319 | INERZIA V -1 | | 5.772 | -0.798 | 0. |
| 49 | 0.2638 | INERZIA V -1 | | 5.772 | -0.798 | 0. |
| 49 | 0. | SLU_1 | Max | -2493.009 | -716.976 | 0. |
| 49 | 0.1319 | SLU_1 | Max | -2486.581 | -681.581 | 0. |
| 49 | 0.2638 | SLU_1 | Max | -2480.153 | -646.418 | 0. |
| 49 | 0. | SLU_1 | Min | -2493.009 | -716.976 | 0. |
| 49 | 0.1319 | SLU_1 | Min | -2486.581 | -681.581 | 0. |
| 49 | 0.2638 | SLU_1 | Min | -2480.153 | -646.418 | 0. |
| 49 | 0. | SLU_2 | Max | -2493.131 | -620.192 | 0. |
| 49 | 0.1319 | SLU_2 | Max | -2486.702 | -589.6 | 0. |
| 49 | 0.2638 | SLU_2 | Max | -2480.274 | -559.24 | 0. |
| 49 | 0. | SLU_2 | Min | -2493.131 | -620.192 | 0. |
| 49 | 0.1319 | SLU_2 | Min | -2486.702 | -589.6 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|----------|----------|
| 49 | 0.2638 | SLU_2 | Min | -2480.274 | -559.24 | 0. |
| 49 | 0. | SLU_3 | Max | -2563.31 | -759.994 | 0. |
| 49 | 0.1319 | SLU_3 | Max | -2556.882 | -725.417 | 0. |
| 49 | 0.2638 | SLU_3 | Max | -2550.453 | -691.072 | 0. |
| 49 | 0. | SLU_3 | Min | -2563.31 | -759.994 | 0. |
| 49 | 0.1319 | SLU_3 | Min | -2556.882 | -725.417 | 0. |
| 49 | 0.2638 | SLU_3 | Min | -2550.453 | -691.072 | 0. |
| 49 | 0. | SLU_4 | Max | -2544.908 | -631.514 | 0. |
| 49 | 0.1319 | SLU_4 | Max | -2538.48 | -601.467 | 0. |
| 49 | 0.2638 | SLU_4 | Max | -2532.052 | -571.652 | 0. |
| 49 | 0. | SLU_4 | Min | -2544.908 | -631.514 | 0. |
| 49 | 0.1319 | SLU_4 | Min | -2538.48 | -601.467 | 0. |
| 49 | 0.2638 | SLU_4 | Min | -2532.052 | -571.652 | 0. |
| 49 | 0. | SLE_F1 | Max | -1826.513 | -558.483 | 0. |
| 49 | 0.1319 | SLE_F1 | Max | -1821.568 | -531.256 | 0. |
| 49 | 0.2638 | SLE_F1 | Max | -1816.624 | -504.207 | 0. |
| 49 | 0. | SLE_F1 | Min | -1826.513 | -558.483 | 0. |
| 49 | 0.1319 | SLE_F1 | Min | -1821.568 | -531.256 | 0. |
| 49 | 0.2638 | SLE_F1 | Min | -1816.624 | -504.207 | 0. |
| 49 | 0. | SLE_F2 | Max | -1826.681 | -486.277 | 0. |
| 49 | 0.1319 | SLE_F2 | Max | -1821.736 | -462.745 | 0. |
| 49 | 0.2638 | SLE_F2 | Max | -1816.791 | -439.391 | 0. |
| 49 | 0. | SLE_F2 | Min | -1826.681 | -486.277 | 0. |
| 49 | 0.1319 | SLE_F2 | Min | -1821.736 | -462.745 | 0. |
| 49 | 0.2638 | SLE_F2 | Min | -1816.791 | -439.391 | 0. |
| 49 | 0. | SLE_F3 | Max | -1866.988 | -494.207 | 0. |
| 49 | 0.1319 | SLE_F3 | Max | -1862.043 | -471.093 | 0. |
| 49 | 0.2638 | SLE_F3 | Max | -1857.098 | -448.159 | 0. |
| 49 | 0. | SLE_F3 | Min | -1866.988 | -494.207 | 0. |
| 49 | 0.1319 | SLE_F3 | Min | -1862.043 | -471.093 | 0. |
| 49 | 0.2638 | SLE_F3 | Min | -1857.098 | -448.159 | 0. |
| 49 | 0. | SLE_F4 | Max | -1881.991 | -596.834 | 0. |
| 49 | 0.1319 | SLE_F4 | Max | -1877.047 | -570.236 | 0. |
| 49 | 0.2638 | SLE_F4 | Max | -1872.102 | -543.817 | 0. |
| 49 | 0. | SLE_F4 | Min | -1881.991 | -596.834 | 0. |
| 49 | 0.1319 | SLE_F4 | Min | -1877.047 | -570.236 | 0. |
| 49 | 0.2638 | SLE_F4 | Min | -1872.102 | -543.817 | 0. |
| 49 | 0. | SLE_QP1 | Max | -1657.196 | -572.624 | 0. |
| 49 | 0.1319 | SLE_QP1 | Max | -1652.251 | -545.396 | 0. |
| 49 | 0.2638 | SLE_QP1 | Max | -1647.306 | -518.348 | 0. |
| 49 | 0. | SLE_QP1 | Min | -1657.196 | -572.624 | 0. |
| 49 | 0.1319 | SLE_QP1 | Min | -1652.251 | -545.396 | 0. |
| 49 | 0.2638 | SLE_QP1 | Min | -1647.306 | -518.348 | 0. |
| 49 | 0. | SLE_QP2 | Max | -1657.478 | -503.379 | 0. |
| 49 | 0.1319 | SLE_QP2 | Max | -1652.533 | -479.846 | 0. |
| 49 | 0.2638 | SLE_QP2 | Max | -1647.589 | -456.492 | 0. |
| 49 | 0. | SLE_QP2 | Min | -1657.478 | -503.379 | 0. |
| 49 | 0.1319 | SLE_QP2 | Min | -1652.533 | -479.846 | 0. |
| 49 | 0.2638 | SLE_QP2 | Min | -1647.589 | -456.492 | 0. |
| 49 | 0. | SLE_QP3 | Max | -1698.669 | -509.856 | 0. |
| 49 | 0.1319 | SLE_QP3 | Max | -1693.724 | -486.742 | 0. |
| 49 | 0.2638 | SLE_QP3 | Max | -1688.779 | -463.808 | 0. |
| 49 | 0. | SLE_QP3 | Min | -1698.669 | -509.856 | 0. |
| 49 | 0.1319 | SLE_QP3 | Min | -1693.724 | -486.742 | 0. |
| 49 | 0.2638 | SLE_QP3 | Min | -1688.779 | -463.808 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|-----------|----------|
| 49 | 0. | SLE_QP4 | Max | -1715.621 | -620.599 | 0. |
| 49 | 0.1319 | SLE_QP4 | Max | -1710.676 | -594.001 | 0. |
| 49 | 0.2638 | SLE_QP4 | Max | -1705.731 | -567.582 | 0. |
| 49 | 0. | SLE_QP4 | Min | -1715.621 | -620.599 | 0. |
| 49 | 0.1319 | SLE_QP4 | Min | -1710.676 | -594.001 | 0. |
| 49 | 0.2638 | SLE_QP4 | Min | -1705.731 | -567.582 | 0. |
| 49 | 0. | SLV_1 | Max | -1951.394 | -1334.297 | 0. |
| 49 | 0.1319 | SLV_1 | Max | -1946.449 | -1307.069 | 0. |
| 49 | 0.2638 | SLV_1 | Max | -1941.505 | -1280.021 | 0. |
| 49 | 0. | SLV_1 | Min | -1951.394 | -1334.297 | 0. |
| 49 | 0.1319 | SLV_1 | Min | -1946.449 | -1307.069 | 0. |
| 49 | 0.2638 | SLV_1 | Min | -1941.505 | -1280.021 | 0. |
| 49 | 0. | SLV_2 | Max | -1938.994 | -1336.989 | 0. |
| 49 | 0.1319 | SLV_2 | Max | -1934.049 | -1309.762 | 0. |
| 49 | 0.2638 | SLV_2 | Max | -1929.104 | -1282.714 | 0. |
| 49 | 0. | SLV_2 | Min | -1938.994 | -1336.989 | 0. |
| 49 | 0.1319 | SLV_2 | Min | -1934.049 | -1309.762 | 0. |
| 49 | 0.2638 | SLV_2 | Min | -1929.104 | -1282.714 | 0. |
| 49 | 0. | SLV_3 | Max | -2054.118 | -1476.407 | 0. |
| 49 | 0.1319 | SLV_3 | Max | -2049.174 | -1449.809 | 0. |
| 49 | 0.2638 | SLV_3 | Max | -2044.229 | -1423.39 | 0. |
| 49 | 0. | SLV_3 | Min | -2054.118 | -1476.407 | 0. |
| 49 | 0.1319 | SLV_3 | Min | -2049.174 | -1449.809 | 0. |
| 49 | 0.2638 | SLV_3 | Min | -2044.229 | -1423.39 | 0. |
| 49 | 0. | SLV_4 | Max | -2041.576 | -1478.857 | 0. |
| 49 | 0.1319 | SLV_4 | Max | -2036.631 | -1452.259 | 0. |
| 49 | 0.2638 | SLV_4 | Max | -2031.686 | -1425.84 | 0. |
| 49 | 0. | SLV_4 | Min | -2041.576 | -1478.857 | 0. |
| 49 | 0.1319 | SLV_4 | Min | -2036.631 | -1452.259 | 0. |
| 49 | 0.2638 | SLV_4 | Min | -2031.686 | -1425.84 | 0. |
| 49 | 0. | SLD_1 | Max | -1756.073 | -856.287 | 0. |
| 49 | 0.1319 | SLD_1 | Max | -1751.128 | -829.06 | 0. |
| 49 | 0.2638 | SLD_1 | Max | -1746.183 | -802.012 | 0. |
| 49 | 0. | SLD_1 | Min | -1756.073 | -856.287 | 0. |
| 49 | 0.1319 | SLD_1 | Min | -1751.128 | -829.06 | 0. |
| 49 | 0.2638 | SLD_1 | Min | -1746.183 | -802.012 | 0. |
| 49 | 0. | SLD_2 | Max | -1750.255 | -857.667 | 0. |
| 49 | 0.1319 | SLD_2 | Max | -1745.31 | -830.44 | 0. |
| 49 | 0.2638 | SLD_2 | Max | -1740.365 | -803.391 | 0. |
| 49 | 0. | SLD_2 | Min | -1750.255 | -857.667 | 0. |
| 49 | 0.1319 | SLD_2 | Min | -1745.31 | -830.44 | 0. |
| 49 | 0.2638 | SLD_2 | Min | -1740.365 | -803.391 | 0. |
| 49 | 0. | SLD_3 | Max | -1853.099 | -999.223 | 0. |
| 49 | 0.1319 | SLD_3 | Max | -1848.154 | -972.625 | 0. |
| 49 | 0.2638 | SLD_3 | Max | -1843.209 | -946.206 | 0. |
| 49 | 0. | SLD_3 | Min | -1853.099 | -999.223 | 0. |
| 49 | 0.1319 | SLD_3 | Min | -1848.154 | -972.625 | 0. |
| 49 | 0.2638 | SLD_3 | Min | -1843.209 | -946.206 | 0. |
| 49 | 0. | SLD_4 | Max | -1847.447 | -1000.251 | 0. |
| 49 | 0.1319 | SLD_4 | Max | -1842.502 | -973.653 | 0. |
| 49 | 0.2638 | SLD_4 | Max | -1837.557 | -947.234 | 0. |
| 49 | 0. | SLD_4 | Min | -1847.447 | -1000.251 | 0. |
| 49 | 0.1319 | SLD_4 | Min | -1842.502 | -973.653 | 0. |
| 49 | 0.2638 | SLD_4 | Min | -1837.557 | -947.234 | 0. |
| 49 | 0. | SLU_IDR_1 | Max | -1597.818 | -576.335 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|-----------|----------|----------|
| 49 | 0.1319 | SLU_IDR_1 | Max | -1593.367 | -552.304 | 0. |
| 49 | 0.2638 | SLU_IDR_1 | Max | -1588.917 | -528.471 | 0. |
| 49 | 0. | SLU_IDR_1 | Min | -1597.818 | -576.335 | 0. |
| 49 | 0.1319 | SLU_IDR_1 | Min | -1593.367 | -552.304 | 0. |
| 49 | 0.2638 | SLU_IDR_1 | Min | -1588.917 | -528.471 | 0. |
| 49 | 0. | SLU_IDR_2 | Max | -1559.211 | -575.675 | 0. |
| 49 | 0.1319 | SLU_IDR_2 | Max | -1554.76 | -551.267 | 0. |
| 49 | 0.2638 | SLU_IDR_2 | Max | -1550.31 | -527.056 | 0. |
| 49 | 0. | SLU_IDR_2 | Min | -1559.211 | -575.675 | 0. |
| 49 | 0.1319 | SLU_IDR_2 | Min | -1554.76 | -551.267 | 0. |
| 49 | 0.2638 | SLU_IDR_2 | Min | -1550.31 | -527.056 | 0. |
| 49 | 0. | SISMA WOOD SLV-1 | Max | -448.569 | -782.775 | 0. |
| 49 | 0.1319 | SISMA WOOD SLV-1 | Max | -448.569 | -782.775 | 0. |
| 49 | 0.2638 | SISMA WOOD SLV-1 | Max | -448.569 | -782.775 | 0. |
| 49 | 0. | SISMA WOOD SLV-1 | Min | -448.569 | -782.775 | 0. |
| 49 | 0.1319 | SISMA WOOD SLV-1 | Min | -448.569 | -782.775 | 0. |
| 49 | 0.2638 | SISMA WOOD SLV-1 | Min | -448.569 | -782.775 | 0. |
| 49 | 0. | DEAD-1 | Max | -427.007 | 59.057 | 0. |
| 49 | 0.1319 | DEAD-1 | Max | -422.062 | 59.057 | 0. |
| 49 | 0.2638 | DEAD-1 | Max | -417.117 | 59.057 | 0. |
| 49 | 0. | DEAD-1 | Min | -427.007 | 59.057 | 0. |
| 49 | 0.1319 | DEAD-1 | Min | -422.062 | 59.057 | 0. |
| 49 | 0.2638 | DEAD-1 | Min | -417.117 | 59.057 | 0. |
| 49 | 0. | SLU_PROVA | | -2282.616 | -723.95 | 0. |
| 49 | 0.1319 | SLU_PROVA | | -2276.188 | -688.555 | 0. |
| 49 | 0.2638 | SLU_PROVA | | -2269.76 | -653.392 | 0. |
| 50 | 0. | DEAD | | -352.205 | 51.412 | 0. |
| 50 | 0.1318 | DEAD | | -347.264 | 51.412 | 0. |
| 50 | 0.2636 | DEAD | | -342.323 | 51.412 | 0. |
| 50 | 0. | SIMM_KA | | -12.176 | -132.465 | 0. |
| 50 | 0.1318 | SIMM_KA | | -12.176 | -125.082 | 0. |
| 50 | 0.2636 | SIMM_KA | | -12.176 | -117.698 | 0. |
| 50 | 0. | SIMM_K0 | | -18.659 | -199.981 | 0. |
| 50 | 0.1318 | SIMM_K0 | | -18.659 | -188.906 | 0. |
| 50 | 0.2636 | SIMM_K0 | | -18.659 | -177.831 | 0. |
| 50 | 0. | A--SIMM_KA | | -53.237 | -150.812 | 0. |
| 50 | 0.1318 | A--SIMM_KA | | -53.237 | -143.848 | 0. |
| 50 | 0.2636 | A--SIMM_KA | | -53.237 | -136.883 | 0. |
| 50 | 0. | A--SIMM_K0 | | -79.793 | -234.774 | 0. |
| 50 | 0.1318 | A--SIMM_K0 | | -79.793 | -224.328 | 0. |
| 50 | 0.2636 | A--SIMM_K0 | | -79.793 | -213.881 | 0. |
| 50 | 0. | A-- SIMM_SOVR_K A | | -1.62 | -8.697 | 0. |
| 50 | 0.1318 | A-- SIMM_SOVR_K A | | -1.62 | -8.697 | 0. |
| 50 | 0.2636 | A-- SIMM_SOVR_K A | | -1.62 | -8.697 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|-------------------------|----------|----------|----------|----------|
| 50 | 0. | A-- SIMM_SOVR_K 0 | | -2.429 | -13.039 | 0. |
| 50 | 0.1318 | A-- SIMM_SOVR_K 0 | | -2.429 | -13.039 | 0. |
| 50 | 0.2636 | A-- SIMM_SOVR_K 0 | | -2.429 | -13.039 | 0. |
| 50 | 0. | SIMM_SOVR_K 0 | | -2.429 | -13.039 | 0. |
| 50 | 0.1318 | SIMM_SOVR_K 0 | | -2.429 | -13.039 | 0. |
| 50 | 0.2636 | SIMM_SOVR_K 0 | | -2.429 | -13.039 | 0. |
| 50 | 0. | SIMM_SOVR_K A | | -1.62 | -8.697 | 0. |
| 50 | 0.1318 | SIMM_SOVR_K A | | -1.62 | -8.697 | 0. |
| 50 | 0.2636 | SIMM_SOVR_K A | | -1.62 | -8.697 | 0. |
| 50 | 0. | SOVR | | -195.45 | 20.691 | 0. |
| 50 | 0.1318 | SOVR | | -195.45 | 20.691 | 0. |
| 50 | 0.2636 | SOVR | | -195.45 | 20.691 | 0. |
| 50 | 0. | TERR_SIMM | | -782.714 | 59.127 | 0. |
| 50 | 0.1318 | TERR_SIMM | | -782.714 | 59.127 | 0. |
| 50 | 0.2636 | TERR_SIMM | | -782.714 | 59.127 | 0. |
| 50 | 0. | TERR_A--SIMM | | -764.488 | 66.919 | 0. |
| 50 | 0.1318 | TERR_A--SIMM | | -764.488 | 66.919 | 0. |
| 50 | 0.2636 | TERR_A--SIMM | | -764.488 | 66.919 | 0. |
| 50 | 0. | INERZIA H SLV | | -4.979 | -5.838 | 0. |
| 50 | 0.1318 | INERZIA H SLV | | -4.979 | -5.838 | 0. |
| 50 | 0.2636 | INERZIA H SLV | | -4.979 | -5.838 | 0. |
| 50 | 0. | INERZIA V + SLV | | -5.613 | 0.81 | 0. |
| 50 | 0.1318 | INERZIA V + SLV | | -5.613 | 0.81 | 0. |
| 50 | 0.2636 | INERZIA V + SLV | | -5.613 | 0.81 | 0. |
| 50 | 0. | INERZIA V - SLV | | 5.613 | -0.81 | 0. |
| 50 | 0.1318 | INERZIA V - SLV | | 5.613 | -0.81 | 0. |
| 50 | 0.2636 | INERZIA V - SLV | | 5.613 | -0.81 | 0. |
| 50 | 0. | SISMA WOOD SLV | | -218.64 | -299.137 | 0. |
| 50 | 0.1318 | SISMA WOOD SLV | | -218.64 | -299.137 | 0. |
| 50 | 0.2636 | SISMA WOOD SLV | | -218.64 | -299.137 | 0. |
| 50 | 0. | iDROSTATICA | | -364.069 | -412.92 | 0. |
| 50 | 0.1318 | iDROSTATICA | | -364.069 | -397.146 | 0. |
| 50 | 0.2636 | iDROSTATICA | | -364.069 | -381.551 | 0. |
| 50 | 0. | SISMA WOOD SLD | | -96.56 | -132.111 | 0. |
| 50 | 0.1318 | SISMA WOOD SLD | | -96.56 | -132.111 | 0. |
| 50 | 0.2636 | SISMA WOOD SLD | | -96.56 | -132.111 | 0. |
| 50 | 0. | INERZIA H SLD | | -2.199 | -2.578 | 0. |
| 50 | 0.1318 | INERZIA H SLD | | -2.199 | -2.578 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|--------------------|----------|-----------|----------|----------|
| 50 | 0.2636 | INERZIA H SLD | | -2.199 | -2.578 | 0. |
| 50 | 0. | INERZIA V + SLD | | -2.479 | 0.358 | 0. |
| 50 | 0.1318 | INERZIA V + SLD | | -2.479 | 0.358 | 0. |
| 50 | 0.2636 | INERZIA V + SLD | | -2.479 | 0.358 | 0. |
| 50 | 0. | INERZIA V SLD | | 2.479 | -0.358 | 0. |
| 50 | 0.1318 | INERZIA V SLD | | 2.479 | -0.358 | 0. |
| 50 | 0.2636 | INERZIA V SLD | | 2.479 | -0.358 | 0. |
| 50 | 0. | INERZIA V -1 | | 5.613 | -0.81 | 0. |
| 50 | 0.1318 | INERZIA V -1 | | 5.613 | -0.81 | 0. |
| 50 | 0.2636 | INERZIA V -1 | | 5.613 | -0.81 | 0. |
| 50 | 0. | SLU_1 | Max | -2480.153 | -631.86 | 0. |
| 50 | 0.1318 | SLU_1 | Max | -2473.73 | -596.956 | 0. |
| 50 | 0.2636 | SLU_1 | Max | -2467.306 | -562.285 | 0. |
| 50 | 0. | SLU_1 | Min | -2480.153 | -631.86 | 0. |
| 50 | 0.1318 | SLU_1 | Min | -2473.73 | -596.956 | 0. |
| 50 | 0.2636 | SLU_1 | Min | -2467.306 | -562.285 | 0. |
| 50 | 0. | SLU_2 | Max | -2480.274 | -542.087 | 0. |
| 50 | 0.1318 | SLU_2 | Max | -2473.851 | -511.983 | 0. |
| 50 | 0.2636 | SLU_2 | Max | -2467.428 | -482.11 | 0. |
| 50 | 0. | SLU_2 | Min | -2480.274 | -542.087 | 0. |
| 50 | 0.1318 | SLU_2 | Min | -2473.851 | -511.983 | 0. |
| 50 | 0.2636 | SLU_2 | Min | -2467.428 | -482.11 | 0. |
| 50 | 0. | SLU_3 | Max | -2550.453 | -656.748 | 0. |
| 50 | 0.1318 | SLU_3 | Max | -2544.03 | -622.661 | 0. |
| 50 | 0.2636 | SLU_3 | Max | -2537.607 | -588.807 | 0. |
| 50 | 0. | SLU_3 | Min | -2550.453 | -656.748 | 0. |
| 50 | 0.1318 | SLU_3 | Min | -2544.03 | -622.661 | 0. |
| 50 | 0.2636 | SLU_3 | Min | -2537.607 | -588.807 | 0. |
| 50 | 0. | SLU_4 | Max | -2532.052 | -540.056 | 0. |
| 50 | 0.1318 | SLU_4 | Max | -2525.628 | -510.497 | 0. |
| 50 | 0.2636 | SLU_4 | Max | -2519.205 | -481.169 | 0. |
| 50 | 0. | SLU_4 | Min | -2532.052 | -540.056 | 0. |
| 50 | 0.1318 | SLU_4 | Min | -2525.628 | -510.497 | 0. |
| 50 | 0.2636 | SLU_4 | Min | -2519.205 | -481.169 | 0. |
| 50 | 0. | SLE_F1 | Max | -1816.624 | -493.508 | 0. |
| 50 | 0.1318 | SLE_F1 | Max | -1811.683 | -466.659 | 0. |
| 50 | 0.2636 | SLE_F1 | Max | -1806.742 | -439.989 | 0. |
| 50 | 0. | SLE_F1 | Min | -1816.624 | -493.508 | 0. |
| 50 | 0.1318 | SLE_F1 | Min | -1811.683 | -466.659 | 0. |
| 50 | 0.2636 | SLE_F1 | Min | -1806.742 | -439.989 | 0. |
| 50 | 0. | SLE_F2 | Max | -1816.791 | -426.762 | 0. |
| 50 | 0.1318 | SLE_F2 | Max | -1811.85 | -403.605 | 0. |
| 50 | 0.2636 | SLE_F2 | Max | -1806.909 | -380.626 | 0. |
| 50 | 0. | SLE_F2 | Min | -1816.791 | -426.762 | 0. |
| 50 | 0.1318 | SLE_F2 | Min | -1811.85 | -403.605 | 0. |
| 50 | 0.2636 | SLE_F2 | Min | -1806.909 | -380.626 | 0. |
| 50 | 0. | SLE_F3 | Max | -1857.098 | -424.498 | 0. |
| 50 | 0.1318 | SLE_F3 | Max | -1852.157 | -401.76 | 0. |
| 50 | 0.2636 | SLE_F3 | Max | -1847.216 | -379.2 | 0. |
| 50 | 0. | SLE_F3 | Min | -1857.098 | -424.498 | 0. |
| 50 | 0.1318 | SLE_F3 | Min | -1852.157 | -401.76 | 0. |
| 50 | 0.2636 | SLE_F3 | Min | -1847.216 | -379.2 | 0. |
| 50 | 0. | SLE_F4 | Max | -1872.102 | -517.302 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|------------|----------|-----------|-----------|----------|
| 50 | 0.1318 | SLE_F4 | Max | -1867.161 | -491.081 | 0. |
| 50 | 0.2636 | SLE_F4 | Max | -1862.22 | -465.04 | 0. |
| 50 | 0. | SLE_F4 | Min | -1872.102 | -517.302 | 0. |
| 50 | 0.1318 | SLE_F4 | Min | -1867.161 | -491.081 | 0. |
| 50 | 0.2636 | SLE_F4 | Min | -1862.22 | -465.04 | 0. |
| 50 | 0. | SLE_QP1 | Max | -1647.306 | -508.563 | 0. |
| 50 | 0.1318 | SLE_QP1 | Max | -1642.365 | -481.714 | 0. |
| 50 | 0.2636 | SLE_QP1 | Max | -1637.424 | -455.043 | 0. |
| 50 | 0. | SLE_QP1 | Min | -1647.306 | -508.563 | 0. |
| 50 | 0.1318 | SLE_QP1 | Min | -1642.365 | -481.714 | 0. |
| 50 | 0.2636 | SLE_QP1 | Min | -1637.424 | -455.043 | 0. |
| 50 | 0. | SLE_QP2 | Max | -1647.589 | -444.915 | 0. |
| 50 | 0.1318 | SLE_QP2 | Max | -1642.648 | -421.758 | 0. |
| 50 | 0.2636 | SLE_QP2 | Max | -1637.707 | -398.779 | 0. |
| 50 | 0. | SLE_QP2 | Min | -1647.589 | -444.915 | 0. |
| 50 | 0.1318 | SLE_QP2 | Min | -1642.648 | -421.758 | 0. |
| 50 | 0.2636 | SLE_QP2 | Min | -1637.707 | -398.779 | 0. |
| 50 | 0. | SLE_QP3 | Max | -1688.779 | -441.342 | 0. |
| 50 | 0.1318 | SLE_QP3 | Max | -1683.838 | -418.604 | 0. |
| 50 | 0.2636 | SLE_QP3 | Max | -1678.897 | -396.045 | 0. |
| 50 | 0. | SLE_QP3 | Min | -1688.779 | -441.342 | 0. |
| 50 | 0.1318 | SLE_QP3 | Min | -1683.838 | -418.604 | 0. |
| 50 | 0.2636 | SLE_QP3 | Min | -1678.897 | -396.045 | 0. |
| 50 | 0. | SLE_QP4 | Max | -1705.731 | -540.75 | 0. |
| 50 | 0.1318 | SLE_QP4 | Max | -1700.79 | -514.53 | 0. |
| 50 | 0.2636 | SLE_QP4 | Max | -1695.849 | -488.488 | 0. |
| 50 | 0. | SLE_QP4 | Min | -1705.731 | -540.75 | 0. |
| 50 | 0.1318 | SLE_QP4 | Min | -1700.79 | -514.53 | 0. |
| 50 | 0.2636 | SLE_QP4 | Min | -1695.849 | -488.488 | 0. |
| 50 | 0. | SLV_1 | Max | -1941.345 | -1174.286 | 0. |
| 50 | 0.1318 | SLV_1 | Max | -1936.404 | -1147.437 | 0. |
| 50 | 0.2636 | SLV_1 | Max | -1931.463 | -1120.766 | 0. |
| 50 | 0. | SLV_1 | Min | -1941.345 | -1174.286 | 0. |
| 50 | 0.1318 | SLV_1 | Min | -1936.404 | -1147.437 | 0. |
| 50 | 0.2636 | SLV_1 | Min | -1931.463 | -1120.766 | 0. |
| 50 | 0. | SLV_2 | Max | -1929.264 | -1176.938 | 0. |
| 50 | 0.1318 | SLV_2 | Max | -1924.323 | -1150.089 | 0. |
| 50 | 0.2636 | SLV_2 | Max | -1919.382 | -1123.418 | 0. |
| 50 | 0. | SLV_2 | Min | -1929.264 | -1176.938 | 0. |
| 50 | 0.1318 | SLV_2 | Min | -1924.323 | -1150.089 | 0. |
| 50 | 0.2636 | SLV_2 | Min | -1919.382 | -1123.418 | 0. |
| 50 | 0. | SLV_3 | Max | -2044.069 | -1291.634 | 0. |
| 50 | 0.1318 | SLV_3 | Max | -2039.128 | -1265.413 | 0. |
| 50 | 0.2636 | SLV_3 | Max | -2034.187 | -1239.372 | 0. |
| 50 | 0. | SLV_3 | Min | -2044.069 | -1291.634 | 0. |
| 50 | 0.1318 | SLV_3 | Min | -2039.128 | -1265.413 | 0. |
| 50 | 0.2636 | SLV_3 | Min | -2034.187 | -1239.372 | 0. |
| 50 | 0. | SLV_4 | Max | -2031.846 | -1294.063 | 0. |
| 50 | 0.1318 | SLV_4 | Max | -2026.905 | -1267.843 | 0. |
| 50 | 0.2636 | SLV_4 | Max | -2021.964 | -1241.801 | 0. |
| 50 | 0. | SLV_4 | Min | -2031.846 | -1294.063 | 0. |
| 50 | 0.1318 | SLV_4 | Min | -2026.905 | -1267.843 | 0. |
| 50 | 0.2636 | SLV_4 | Min | -2021.964 | -1241.801 | 0. |
| 50 | 0. | SLD_1 | Max | -1746.113 | -754.857 | 0. |
| 50 | 0.1318 | SLD_1 | Max | -1741.171 | -728.007 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 1 of 2

| Frame | Station m | OutputCase | StepType | P KN | V2 KN | V3 KN |
|-------|--------------|---------------------|----------|-----------|----------|----------|
| 50 | 0.2636 | SLD_1 | Max | -1736.23 | -701.337 | 0. |
| 50 | 0. | SLD_1 | Min | -1746.113 | -754.857 | 0. |
| 50 | 0.1318 | SLD_1 | Min | -1741.171 | -728.007 | 0. |
| 50 | 0.2636 | SLD_1 | Min | -1736.23 | -701.337 | 0. |
| 50 | 0. | SLD_2 | Max | -1740.436 | -756.227 | 0. |
| 50 | 0.1318 | SLD_2 | Max | -1735.495 | -729.378 | 0. |
| 50 | 0.2636 | SLD_2 | Max | -1730.554 | -702.708 | 0. |
| 50 | 0. | SLD_2 | Min | -1740.436 | -756.227 | 0. |
| 50 | 0.1318 | SLD_2 | Min | -1735.495 | -729.378 | 0. |
| 50 | 0.2636 | SLD_2 | Min | -1730.554 | -702.708 | 0. |
| 50 | 0. | SLD_3 | Max | -1843.138 | -872.736 | 0. |
| 50 | 0.1318 | SLD_3 | Max | -1838.197 | -846.516 | 0. |
| 50 | 0.2636 | SLD_3 | Max | -1833.256 | -820.474 | 0. |
| 50 | 0. | SLD_3 | Min | -1843.138 | -872.736 | 0. |
| 50 | 0.1318 | SLD_3 | Min | -1838.197 | -846.516 | 0. |
| 50 | 0.2636 | SLD_3 | Min | -1833.256 | -820.474 | 0. |
| 50 | 0. | SLD_4 | Max | -1837.628 | -873.767 | 0. |
| 50 | 0.1318 | SLD_4 | Max | -1832.687 | -847.546 | 0. |
| 50 | 0.2636 | SLD_4 | Max | -1827.746 | -821.505 | 0. |
| 50 | 0. | SLD_4 | Min | -1837.628 | -873.767 | 0. |
| 50 | 0.1318 | SLD_4 | Min | -1832.687 | -847.546 | 0. |
| 50 | 0.2636 | SLD_4 | Min | -1827.746 | -821.505 | 0. |
| 50 | 0. | SLU_IDR_1 | Max | -1588.917 | -506.463 | 0. |
| 50 | 0.1318 | SLU_IDR_1 | Max | -1584.47 | -482.843 | 0. |
| 50 | 0.2636 | SLU_IDR_1 | Max | -1580.023 | -459.421 | 0. |
| 50 | 0. | SLU_IDR_1 | Min | -1588.917 | -506.463 | 0. |
| 50 | 0.1318 | SLU_IDR_1 | Min | -1584.47 | -482.843 | 0. |
| 50 | 0.2636 | SLU_IDR_1 | Min | -1580.023 | -459.421 | 0. |
| 50 | 0. | SLU_IDR_2 | Max | -1550.31 | -514.409 | 0. |
| 50 | 0.1318 | SLU_IDR_2 | Max | -1545.863 | -490.413 | 0. |
| 50 | 0.2636 | SLU_IDR_2 | Max | -1541.416 | -466.613 | 0. |
| 50 | 0. | SLU_IDR_2 | Min | -1550.31 | -514.409 | 0. |
| 50 | 0.1318 | SLU_IDR_2 | Min | -1545.863 | -490.413 | 0. |
| 50 | 0.2636 | SLU_IDR_2 | Min | -1541.416 | -466.613 | 0. |
| 50 | 0. | SISMA WOOD SLV-1 | Max | -448.569 | -688.147 | 0. |
| 50 | 0.1318 | SISMA WOOD SLV-1 | Max | -448.569 | -688.147 | 0. |
| 50 | 0.2636 | SISMA WOOD SLV-1 | Max | -448.569 | -688.147 | 0. |
| 50 | 0. | SISMA WOOD SLV-1 | Min | -448.569 | -688.147 | 0. |
| 50 | 0.1318 | SISMA WOOD SLV-1 | Min | -448.569 | -688.147 | 0. |
| 50 | 0.2636 | SISMA WOOD SLV-1 | Min | -448.569 | -688.147 | 0. |
| 50 | 0. | DEAD-1 | Max | -417.117 | 60.389 | 0. |
| 50 | 0.1318 | DEAD-1 | Max | -412.176 | 60.389 | 0. |
| 50 | 0.2636 | DEAD-1 | Max | -407.235 | 60.389 | 0. |
| 50 | 0. | DEAD-1 | Min | -417.117 | 60.389 | 0. |
| 50 | 0.1318 | DEAD-1 | Min | -412.176 | 60.389 | 0. |
| 50 | 0.2636 | DEAD-1 | Min | -407.235 | 60.389 | 0. |
| 50 | 0. | SLU_PROVA | | -2269.76 | -641.595 | 0. |
| 50 | 0.1318 | SLU_PROVA | | -2263.336 | -606.691 | 0. |
| 50 | 0.2636 | SLU_PROVA | | -2256.913 | -572.019 | 0. |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Table: Element Forces - Frames, Part 2 of 2 | | | | | | |
|---|--------------|-------------------------|----------|-----------|------------|------------|
| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
| 1 | 0. | DEAD | | 0. | 0. | -80.8647 |
| 1 | 0.30384 | DEAD | | 0. | 0. | -84.145 |
| 1 | 0.60768 | DEAD | | 0. | 0. | -89.9668 |
| 1 | 0. | SIMM_KA | | 0. | 0. | 74.6347 |
| 1 | 0.30384 | SIMM_KA | | 0. | 0. | 67.5304 |
| 1 | 0.60768 | SIMM_KA | | 0. | 0. | 60.4261 |
| 1 | 0. | SIMM_K0 | | 0. | 0. | 115.4029 |
| 1 | 0.30384 | SIMM_K0 | | 0. | 0. | 104.8631 |
| 1 | 0.60768 | SIMM_K0 | | 0. | 0. | 94.3233 |
| 1 | 0. | A--SIMM_KA | | 0. | 0. | 187.6236 |
| 1 | 0.30384 | A--SIMM_KA | | 0. | 0. | 180.9433 |
| 1 | 0.60768 | A--SIMM_KA | | 0. | 0. | 174.263 |
| 1 | 0. | A--SIMM_K0 | | 0. | 0. | 283.2606 |
| 1 | 0.30384 | A--SIMM_K0 | | 0. | 0. | 272.9018 |
| 1 | 0.60768 | A--SIMM_K0 | | 0. | 0. | 262.543 |
| 1 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 13.4743 |
| 1 | 0.30384 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.6443 |
| 1 | 0.60768 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.8144 |
| 1 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.2013 |
| 1 | 0.30384 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.4562 |
| 1 | 0.60768 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.7112 |
| 1 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 20.2013 |
| 1 | 0.30384 | SIMM_SOVR_K 0 | | 0. | 0. | 20.4562 |
| 1 | 0.60768 | SIMM_SOVR_K 0 | | 0. | 0. | 20.7112 |
| 1 | 0. | SIMM_SOVR_K A | | 0. | 0. | 13.4743 |
| 1 | 0.30384 | SIMM_SOVR_K A | | 0. | 0. | 13.6443 |
| 1 | 0.60768 | SIMM_SOVR_K A | | 0. | 0. | 13.8144 |
| 1 | 0. | SOVR | | 0. | 0. | -13.3201 |
| 1 | 0.30384 | SOVR | | 0. | 0. | -3.8805 |
| 1 | 0.60768 | SOVR | | 0. | 0. | 5.5591 |
| 1 | 0. | TERR_SIMM | | 0. | 0. | -18.2493 |
| 1 | 0.30384 | TERR_SIMM | | 0. | 0. | 19.6714 |
| 1 | 0.60768 | TERR_SIMM | | 0. | 0. | 57.5921 |
| 1 | 0. | TERR_A--SIMM | | 0. | 0. | -6.0307 |
| 1 | 0.30384 | TERR_A--SIMM | | 0. | 0. | 51.0311 |
| 1 | 0.60768 | TERR_A--SIMM | | 0. | 0. | 108.0928 |
| 1 | 0. | INERZIA H SLV | | 0. | 0. | 3.1626 |
| 1 | 0.30384 | INERZIA H SLV | | 0. | 0. | 3.4566 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 1 | 0.60768 | INERZIA H SLV | | 0. | 0. | 3.7506 |
| 1 | 0. | INERZIA V + SLV | | 0. | 0. | -1.248 |
| 1 | 0.30384 | INERZIA V + SLV | | 0. | 0. | -1.3243 |
| 1 | 0.60768 | INERZIA V + SLV | | 0. | 0. | -1.4005 |
| 1 | 0. | INERZIA V - SLV | | 0. | 0. | 1.248 |
| 1 | 0.30384 | INERZIA V - SLV | | 0. | 0. | 1.3243 |
| 1 | 0.60768 | INERZIA V - SLV | | 0. | 0. | 1.4005 |
| 1 | 0. | SISMA WOOD SLV | | 0. | 0. | 230.6806 |
| 1 | 0.30384 | SISMA WOOD SLV | | 0. | 0. | 236.4841 |
| 1 | 0.60768 | SISMA WOOD SLV | | 0. | 0. | 244.8416 |
| 1 | 0. | iDROSTATICA | | 0. | 0. | 431.7086 |
| 1 | 0.30384 | iDROSTATICA | | 0. | 0. | 509.7021 |
| 1 | 0.60768 | iDROSTATICA | | 0. | 0. | 599.0573 |
| 1 | 0. | SISMA WOOD SLD | | 0. | 0. | 101.8779 |
| 1 | 0.30384 | SISMA WOOD SLD | | 0. | 0. | 104.4409 |
| 1 | 0.60768 | SISMA WOOD SLD | | 0. | 0. | 108.1319 |
| 1 | 0. | INERZIA H SLD | | 0. | 0. | 1.3967 |
| 1 | 0.30384 | INERZIA H SLD | | 0. | 0. | 1.5266 |
| 1 | 0.60768 | INERZIA H SLD | | 0. | 0. | 1.6564 |
| 1 | 0. | INERZIA V + SLD | | 0. | 0. | -0.5512 |
| 1 | 0.30384 | INERZIA V + SLD | | 0. | 0. | -0.5849 |
| 1 | 0.60768 | INERZIA V + SLD | | 0. | 0. | -0.6185 |
| 1 | 0. | INERZIA V SLD | | 0. | 0. | 0.5512 |
| 1 | 0.30384 | INERZIA V SLD | | 0. | 0. | 0.5849 |
| 1 | 0.60768 | INERZIA V SLD | | 0. | 0. | 0.6185 |
| 1 | 0. | INERZIA V -1 | | 0. | 0. | 1.248 |
| 1 | 0.30384 | INERZIA V -1 | | 0. | 0. | 1.3243 |
| 1 | 0.60768 | INERZIA V -1 | | 0. | 0. | 1.4005 |
| 1 | 0. | SLU_1 | Max | 0. | 0. | 625.6041 |
| 1 | 0.30384 | SLU_1 | Max | 0. | 0. | 787.4948 |
| 1 | 0.60768 | SLU_1 | Max | 0. | 0. | 960.8515 |
| 1 | 0. | SLU_1 | Min | 0. | 0. | 625.6041 |
| 1 | 0.30384 | SLU_1 | Min | 0. | 0. | 787.4948 |
| 1 | 0.60768 | SLU_1 | Min | 0. | 0. | 960.8515 |
| 1 | 0. | SLU_2 | Max | 0. | 0. | 586.0634 |
| 1 | 0.30384 | SLU_2 | Max | 0. | 0. | 755.8971 |
| 1 | 0.60768 | SLU_2 | Max | 0. | 0. | 937.1969 |
| 1 | 0. | SLU_2 | Min | 0. | 0. | 586.0634 |
| 1 | 0.30384 | SLU_2 | Min | 0. | 0. | 755.8971 |
| 1 | 0.60768 | SLU_2 | Min | 0. | 0. | 937.1969 |
| 1 | 0. | SLU_3 | Max | 0. | 0. | 985.7048 |
| 1 | 0.30384 | SLU_3 | Max | 0. | 0. | 1179.8406 |
| 1 | 0.60768 | SLU_3 | Max | 0. | 0. | 1385.4425 |
| 1 | 0. | SLU_3 | Min | 0. | 0. | 985.7048 |
| 1 | 0.30384 | SLU_3 | Min | 0. | 0. | 1179.8406 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 1 | 0.60768 | SLU_3 | Min | 0. | 0. | 1385.4425 |
| 1 | 0. | SLU_4 | Max | 0. | 0. | 830.1426 |
| 1 | 0.30384 | SLU_4 | Max | 0. | 0. | 1029.9162 |
| 1 | 0.60768 | SLU_4 | Max | 0. | 0. | 1241.1558 |
| 1 | 0. | SLU_4 | Min | 0. | 0. | 830.1426 |
| 1 | 0.30384 | SLU_4 | Min | 0. | 0. | 1029.9162 |
| 1 | 0.60768 | SLU_4 | Min | 0. | 0. | 1241.1558 |
| 1 | 0. | SLE_F1 | Max | 0. | 0. | 486.9907 |
| 1 | 0.30384 | SLE_F1 | Max | 0. | 0. | 607.8976 |
| 1 | 0.60768 | SLE_F1 | Max | 0. | 0. | 737.6245 |
| 1 | 0. | SLE_F1 | Min | 0. | 0. | 486.9907 |
| 1 | 0.30384 | SLE_F1 | Min | 0. | 0. | 607.8976 |
| 1 | 0.60768 | SLE_F1 | Min | 0. | 0. | 737.6245 |
| 1 | 0. | SLE_F2 | Max | 0. | 0. | 461.1425 |
| 1 | 0.30384 | SLE_F2 | Max | 0. | 0. | 588.1571 |
| 1 | 0.60768 | SLE_F2 | Max | 0. | 0. | 723.9918 |
| 1 | 0. | SLE_F2 | Min | 0. | 0. | 461.1425 |
| 1 | 0.30384 | SLE_F2 | Min | 0. | 0. | 588.1571 |
| 1 | 0.60768 | SLE_F2 | Min | 0. | 0. | 723.9918 |
| 1 | 0. | SLE_F3 | Max | 0. | 0. | 646.8296 |
| 1 | 0.30384 | SLE_F3 | Max | 0. | 0. | 796.4173 |
| 1 | 0.60768 | SLE_F3 | Max | 0. | 0. | 954.8251 |
| 1 | 0. | SLE_F3 | Min | 0. | 0. | 646.8296 |
| 1 | 0.30384 | SLE_F3 | Min | 0. | 0. | 796.4173 |
| 1 | 0.60768 | SLE_F3 | Min | 0. | 0. | 954.8251 |
| 1 | 0. | SLE_F4 | Max | 0. | 0. | 762.9628 |
| 1 | 0.30384 | SLE_F4 | Max | 0. | 0. | 907.4489 |
| 1 | 0.60768 | SLE_F4 | Max | 0. | 0. | 1060.7551 |
| 1 | 0. | SLE_F4 | Min | 0. | 0. | 762.9628 |
| 1 | 0.30384 | SLE_F4 | Min | 0. | 0. | 907.4489 |
| 1 | 0.60768 | SLE_F4 | Min | 0. | 0. | 1060.7551 |
| 1 | 0. | SLE_QP1 | Max | 0. | 0. | 502.3026 |
| 1 | 0.30384 | SLE_QP1 | Max | 0. | 0. | 616.6075 |
| 1 | 0.60768 | SLE_QP1 | Max | 0. | 0. | 739.7324 |
| 1 | 0. | SLE_QP1 | Min | 0. | 0. | 502.3026 |
| 1 | 0.30384 | SLE_QP1 | Min | 0. | 0. | 616.6075 |
| 1 | 0.60768 | SLE_QP1 | Min | 0. | 0. | 739.7324 |
| 1 | 0. | SLE_QP2 | Max | 0. | 0. | 480.3143 |
| 1 | 0.30384 | SLE_QP2 | Max | 0. | 0. | 600.5933 |
| 1 | 0.60768 | SLE_QP2 | Max | 0. | 0. | 729.6924 |
| 1 | 0. | SLE_QP2 | Min | 0. | 0. | 480.3143 |
| 1 | 0.30384 | SLE_QP2 | Min | 0. | 0. | 600.5933 |
| 1 | 0.60768 | SLE_QP2 | Min | 0. | 0. | 729.6924 |
| 1 | 0. | SLE_QP3 | Max | 0. | 0. | 662.1644 |
| 1 | 0.30384 | SLE_QP3 | Max | 0. | 0. | 804.167 |
| 1 | 0.60768 | SLE_QP3 | Max | 0. | 0. | 954.9896 |
| 1 | 0. | SLE_QP3 | Min | 0. | 0. | 662.1644 |
| 1 | 0.30384 | SLE_QP3 | Min | 0. | 0. | 804.167 |
| 1 | 0.60768 | SLE_QP3 | Min | 0. | 0. | 954.9896 |
| 1 | 0. | SLE_QP4 | Max | 0. | 0. | 771.2607 |
| 1 | 0.30384 | SLE_QP4 | Max | 0. | 0. | 906.5824 |
| 1 | 0.60768 | SLE_QP4 | Max | 0. | 0. | 1050.7241 |
| 1 | 0. | SLE_QP4 | Min | 0. | 0. | 771.2607 |
| 1 | 0.30384 | SLE_QP4 | Min | 0. | 0. | 906.5824 |
| 1 | 0.60768 | SLE_QP4 | Min | 0. | 0. | 1050.7241 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 1 | 0. | SLV_1 | Max | 0. | 0. | 982.6366 |
| 1 | 0.30384 | SLV_1 | Max | 0. | 0. | 1063.3056 |
| 1 | 0.60768 | SLV_1 | Max | 0. | 0. | 1155.3488 |
| 1 | 0. | SLV_1 | Min | 0. | 0. | 982.6366 |
| 1 | 0.30384 | SLV_1 | Min | 0. | 0. | 1063.3056 |
| 1 | 0.60768 | SLV_1 | Min | 0. | 0. | 1155.3488 |
| 1 | 0. | SLV_2 | Max | 0. | 0. | 983.5921 |
| 1 | 0.30384 | SLV_2 | Max | 0. | 0. | 1064.4085 |
| 1 | 0.60768 | SLV_2 | Max | 0. | 0. | 1156.5991 |
| 1 | 0. | SLV_2 | Min | 0. | 0. | 983.5921 |
| 1 | 0.30384 | SLV_2 | Min | 0. | 0. | 1064.4085 |
| 1 | 0.60768 | SLV_2 | Min | 0. | 0. | 1156.5991 |
| 1 | 0. | SLV_3 | Max | 0. | 0. | 1266.5823 |
| 1 | 0.30384 | SLV_3 | Max | 0. | 0. | 1361.0508 |
| 1 | 0.60768 | SLV_3 | Max | 0. | 0. | 1466.8934 |
| 1 | 0. | SLV_3 | Min | 0. | 0. | 1266.5823 |
| 1 | 0.30384 | SLV_3 | Min | 0. | 0. | 1361.0508 |
| 1 | 0.60768 | SLV_3 | Min | 0. | 0. | 1466.8934 |
| 1 | 0. | SLV_4 | Max | 0. | 0. | 1267.5278 |
| 1 | 0.30384 | SLV_4 | Max | 0. | 0. | 1361.9488 |
| 1 | 0.60768 | SLV_4 | Max | 0. | 0. | 1467.7438 |
| 1 | 0. | SLV_4 | Min | 0. | 0. | 1267.5278 |
| 1 | 0.30384 | SLV_4 | Min | 0. | 0. | 1361.9488 |
| 1 | 0.60768 | SLV_4 | Min | 0. | 0. | 1467.7438 |
| 1 | 0. | SLD_1 | Max | 0. | 0. | 724.2605 |
| 1 | 0.30384 | SLD_1 | Max | 0. | 0. | 828.5986 |
| 1 | 0.60768 | SLD_1 | Max | 0. | 0. | 942.8847 |
| 1 | 0. | SLD_1 | Min | 0. | 0. | 724.2605 |
| 1 | 0.30384 | SLD_1 | Min | 0. | 0. | 828.5986 |
| 1 | 0.60768 | SLD_1 | Min | 0. | 0. | 942.8847 |
| 1 | 0. | SLD_2 | Max | 0. | 0. | 726.314 |
| 1 | 0.30384 | SLD_2 | Max | 0. | 0. | 830.7858 |
| 1 | 0.60768 | SLD_2 | Max | 0. | 0. | 945.2057 |
| 1 | 0. | SLD_2 | Min | 0. | 0. | 726.314 |
| 1 | 0.30384 | SLD_2 | Min | 0. | 0. | 830.7858 |
| 1 | 0.60768 | SLD_2 | Min | 0. | 0. | 945.2057 |
| 1 | 0. | SLD_3 | Max | 0. | 0. | 995.6987 |
| 1 | 0.30384 | SLD_3 | Max | 0. | 0. | 1111.8757 |
| 1 | 0.60768 | SLD_3 | Max | 0. | 0. | 1238.0006 |
| 1 | 0. | SLD_3 | Min | 0. | 0. | 995.6987 |
| 1 | 0.30384 | SLD_3 | Min | 0. | 0. | 1111.8757 |
| 1 | 0.60768 | SLD_3 | Min | 0. | 0. | 1238.0006 |
| 1 | 0. | SLD_4 | Max | 0. | 0. | 996.6167 |
| 1 | 0.30384 | SLD_4 | Max | 0. | 0. | 1112.7961 |
| 1 | 0.60768 | SLD_4 | Max | 0. | 0. | 1238.9235 |
| 1 | 0. | SLD_4 | Min | 0. | 0. | 996.6167 |
| 1 | 0.30384 | SLD_4 | Min | 0. | 0. | 1112.7961 |
| 1 | 0.60768 | SLD_4 | Min | 0. | 0. | 1238.9235 |
| 1 | 0. | SLU_IDR_1 | Max | 0. | 0. | 757.0863 |
| 1 | 0.30384 | SLU_IDR_1 | Max | 0. | 0. | 906.9683 |
| 1 | 0.60768 | SLU_IDR_1 | Max | 0. | 0. | 1067.0607 |
| 1 | 0. | SLU_IDR_1 | Min | 0. | 0. | 757.0863 |
| 1 | 0.30384 | SLU_IDR_1 | Min | 0. | 0. | 906.9683 |
| 1 | 0.60768 | SLU_IDR_1 | Min | 0. | 0. | 1067.0607 |
| 1 | 0. | SLU_IDR_2 | Max | 0. | 0. | 601.5818 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 1 | 0.30384 | SLU_IDR_2 | Max | 0. | 0. | 735.3058 |
| 1 | 0.60768 | SLU_IDR_2 | Max | 0. | 0. | 879.2402 |
| 1 | 0. | SLU_IDR_2 | Min | 0. | 0. | 601.5818 |
| 1 | 0.30384 | SLU_IDR_2 | Min | 0. | 0. | 735.3058 |
| 1 | 0.60768 | SLU_IDR_2 | Min | 0. | 0. | 879.2402 |
| 1 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 140.4708 |
| 1 | 0.30384 | SISMA WOOD SLV-1 | Max | 0. | 0. | 96.9508 |
| 1 | 0.60768 | SISMA WOOD SLV-1 | Max | 0. | 0. | 55.9848 |
| 1 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 140.4708 |
| 1 | 0.30384 | SISMA WOOD SLV-1 | Min | 0. | 0. | 96.9508 |
| 1 | 0.60768 | SISMA WOOD SLV-1 | Min | 0. | 0. | 55.9848 |
| 1 | 0. | DEAD-1 | Max | 0. | 0. | -88.8874 |
| 1 | 0.30384 | DEAD-1 | Max | 0. | 0. | -89.08 |
| 1 | 0.60768 | DEAD-1 | Max | 0. | 0. | -91.8141 |
| 1 | 0. | DEAD-1 | Min | 0. | 0. | -88.8874 |
| 1 | 0.30384 | DEAD-1 | Min | 0. | 0. | -89.08 |
| 1 | 0.60768 | DEAD-1 | Min | 0. | 0. | -91.8141 |
| 1 | 0. | SLU_PROVA | | 0. | 0. | 592.7186 |
| 1 | 0.30384 | SLU_PROVA | | 0. | 0. | 739.9828 |
| 1 | 0.60768 | SLU_PROVA | | 0. | 0. | 898.713 |
| 2 | 0. | DEAD | | 0. | 0. | -12.5618 |
| 2 | 0.68666 | DEAD | | 0. | 0. | -12.1784 |
| 2 | 1.37332 | DEAD | | 0. | 0. | -25.8513 |
| 2 | 0. | SIMM_KA | | 0. | 0. | 59.5301 |
| 2 | 0.68666 | SIMM_KA | | 0. | 0. | 62.3551 |
| 2 | 1.37332 | SIMM_KA | | 0. | 0. | 65.18 |
| 2 | 0. | SIMM_K0 | | 0. | 0. | 90.4816 |
| 2 | 0.68666 | SIMM_K0 | | 0. | 0. | 94.959 |
| 2 | 1.37332 | SIMM_K0 | | 0. | 0. | 99.4364 |
| 2 | 0. | A--SIMM_KA | | 0. | 0. | 105.6344 |
| 2 | 0.68666 | A--SIMM_KA | | 0. | 0. | 119.5009 |
| 2 | 1.37332 | A--SIMM_KA | | 0. | 0. | 133.3673 |
| 2 | 0. | A--SIMM_K0 | | 0. | 0. | 160.6068 |
| 2 | 0.68666 | A--SIMM_K0 | | 0. | 0. | 181.3457 |
| 2 | 1.37332 | A--SIMM_K0 | | 0. | 0. | 202.0846 |
| 2 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 5.6424 |
| 2 | 0.68666 | A-- SIMM_SOVR_K A | | 0. | 0. | 6.5002 |
| 2 | 1.37332 | A-- SIMM_SOVR_K A | | 0. | 0. | 7.3579 |
| 2 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.4594 |
| 2 | 0.68666 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 9.7454 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 2 | 1.37332 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 11.0314 |
| 2 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 8.4594 |
| 2 | 0.68666 | SIMM_SOVR_K 0 | | 0. | 0. | 9.7454 |
| 2 | 1.37332 | SIMM_SOVR_K 0 | | 0. | 0. | 11.0314 |
| 2 | 0. | SIMM_SOVR_K A | | 0. | 0. | 5.6424 |
| 2 | 0.68666 | SIMM_SOVR_K A | | 0. | 0. | 6.5002 |
| 2 | 1.37332 | SIMM_SOVR_K A | | 0. | 0. | 7.3579 |
| 2 | 0. | SOVR | | 0. | 0. | -75.2129 |
| 2 | 0.68666 | SOVR | | 0. | 0. | -70.9785 |
| 2 | 1.37332 | SOVR | | 0. | 0. | -66.744 |
| 2 | 0. | TERR_SIMM | | 0. | 0. | -284.4965 |
| 2 | 0.68666 | TERR_SIMM | | 0. | 0. | -265.4396 |
| 2 | 1.37332 | TERR_SIMM | | 0. | 0. | -246.3827 |
| 2 | 0. | TERR_A--SIMM | | 0. | 0. | -377.5251 |
| 2 | 0.68666 | TERR_A--SIMM | | 0. | 0. | -355.0676 |
| 2 | 1.37332 | TERR_A--SIMM | | 0. | 0. | -332.6102 |
| 2 | 0. | INERZIA H SLV | | 0. | 0. | 1.2552 |
| 2 | 0.68666 | INERZIA H SLV | | 0. | 0. | 1.5606 |
| 2 | 1.37332 | INERZIA H SLV | | 0. | 0. | 1.8661 |
| 2 | 0. | INERZIA V + SLV | | 0. | 0. | -0.1286 |
| 2 | 0.68666 | INERZIA V + SLV | | 0. | 0. | -0.237 |
| 2 | 1.37332 | INERZIA V + SLV | | 0. | 0. | -0.3454 |
| 2 | 0. | INERZIA V - SLV | | 0. | 0. | 0.1286 |
| 2 | 0.68666 | INERZIA V - SLV | | 0. | 0. | 0.237 |
| 2 | 1.37332 | INERZIA V - SLV | | 0. | 0. | 0.3454 |
| 2 | 0. | SISMA WOOD SLV | | 0. | 0. | 141.5941 |
| 2 | 0.68666 | SISMA WOOD SLV | | 0. | 0. | 151.6341 |
| 2 | 1.37332 | SISMA WOOD SLV | | 0. | 0. | 165.2657 |
| 2 | 0. | iDROSTATICA | | 0. | 0. | -462.4793 |
| 2 | 0.68666 | iDROSTATICA | | 0. | 0. | -415.9082 |
| 2 | 1.37332 | iDROSTATICA | | 0. | 0. | -311.3097 |
| 2 | 0. | SISMA WOOD SLD | | 0. | 0. | 62.5337 |
| 2 | 0.68666 | SISMA WOOD SLD | | 0. | 0. | 66.9677 |
| 2 | 1.37332 | SISMA WOOD SLD | | 0. | 0. | 72.988 |
| 2 | 0. | INERZIA H SLD | | 0. | 0. | 0.5544 |
| 2 | 0.68666 | INERZIA H SLD | | 0. | 0. | 0.6892 |
| 2 | 1.37332 | INERZIA H SLD | | 0. | 0. | 0.8241 |
| 2 | 0. | INERZIA V + SLD | | 0. | 0. | -0.0568 |
| 2 | 0.68666 | INERZIA V + SLD | | 0. | 0. | -0.1047 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-----------------|----------|-----------|------------|------------|
| 2 | 1.37332 | INERZIA V + SLD | | 0. | 0. | -0.1526 |
| 2 | 0. | INERZIA V SLD | | 0. | 0. | 0.0568 |
| 2 | 0.68666 | INERZIA V SLD | | 0. | 0. | 0.1047 |
| 2 | 1.37332 | INERZIA V SLD | | 0. | 0. | 0.1526 |
| 2 | 0. | INERZIA V -1 | | 0. | 0. | 0.1286 |
| 2 | 0.68666 | INERZIA V -1 | | 0. | 0. | 0.237 |
| 2 | 1.37332 | INERZIA V -1 | | 0. | 0. | 0.3454 |
| 2 | 0. | SLU_1 | Max | 0. | 0. | -1140.2771 |
| 2 | 0.68666 | SLU_1 | Max | 0. | 0. | -1008.5484 |
| 2 | 1.37332 | SLU_1 | Max | 0. | 0. | -819.6572 |
| 2 | 0. | SLU_1 | Min | 0. | 0. | -1140.2771 |
| 2 | 0.68666 | SLU_1 | Min | 0. | 0. | -1008.5484 |
| 2 | 1.37332 | SLU_1 | Min | 0. | 0. | -819.6572 |
| 2 | 0. | SLU_2 | Max | 0. | 0. | -1235.3099 |
| 2 | 0.68666 | SLU_2 | Max | 0. | 0. | -1096.9104 |
| 2 | 1.37332 | SLU_2 | Max | 0. | 0. | -901.3483 |
| 2 | 0. | SLU_2 | Min | 0. | 0. | -1235.3099 |
| 2 | 0.68666 | SLU_2 | Min | 0. | 0. | -1096.9104 |
| 2 | 1.37332 | SLU_2 | Min | 0. | 0. | -901.3483 |
| 2 | 0. | SLU_3 | Max | 0. | 0. | -1093.6285 |
| 2 | 0.68666 | SLU_3 | Max | 0. | 0. | -935.4525 |
| 2 | 1.37332 | SLU_3 | Max | 0. | 0. | -720.114 |
| 2 | 0. | SLU_3 | Min | 0. | 0. | -1093.6285 |
| 2 | 0.68666 | SLU_3 | Min | 0. | 0. | -935.4525 |
| 2 | 1.37332 | SLU_3 | Min | 0. | 0. | -720.114 |
| 2 | 0. | SLU_4 | Max | 0. | 0. | -1229.8925 |
| 2 | 0.68666 | SLU_4 | Max | 0. | 0. | -1071.4579 |
| 2 | 1.37332 | SLU_4 | Max | 0. | 0. | -855.8607 |
| 2 | 0. | SLU_4 | Min | 0. | 0. | -1229.8925 |
| 2 | 0.68666 | SLU_4 | Min | 0. | 0. | -1071.4579 |
| 2 | 1.37332 | SLU_4 | Min | 0. | 0. | -855.8607 |
| 2 | 0. | SLE_F1 | Max | 0. | 0. | -856.0777 |
| 2 | 0.68666 | SLE_F1 | Max | 0. | 0. | -755.4415 |
| 2 | 1.37332 | SLE_F1 | Max | 0. | 0. | -610.834 |
| 2 | 0. | SLE_F1 | Min | 0. | 0. | -856.0777 |
| 2 | 0.68666 | SLE_F1 | Min | 0. | 0. | -755.4415 |
| 2 | 1.37332 | SLE_F1 | Min | 0. | 0. | -610.834 |
| 2 | 0. | SLE_F2 | Max | 0. | 0. | -926.9118 |
| 2 | 0.68666 | SLE_F2 | Max | 0. | 0. | -820.7289 |
| 2 | 1.37332 | SLE_F2 | Max | 0. | 0. | -670.5747 |
| 2 | 0. | SLE_F2 | Min | 0. | 0. | -926.9118 |
| 2 | 0.68666 | SLE_F2 | Min | 0. | 0. | -820.7289 |
| 2 | 1.37332 | SLE_F2 | Min | 0. | 0. | -670.5747 |
| 2 | 0. | SLE_F3 | Max | 0. | 0. | -919.0074 |
| 2 | 0.68666 | SLE_F3 | Max | 0. | 0. | -796.8635 |
| 2 | 1.37332 | SLE_F3 | Max | 0. | 0. | -630.7484 |
| 2 | 0. | SLE_F3 | Min | 0. | 0. | -919.0074 |
| 2 | 0.68666 | SLE_F3 | Min | 0. | 0. | -796.8635 |
| 2 | 1.37332 | SLE_F3 | Min | 0. | 0. | -630.7484 |
| 2 | 0. | SLE_F4 | Max | 0. | 0. | -811.8173 |
| 2 | 0.68666 | SLE_F4 | Max | 0. | 0. | -690.6369 |
| 2 | 1.37332 | SLE_F4 | Max | 0. | 0. | -525.4854 |
| 2 | 0. | SLE_F4 | Min | 0. | 0. | -811.8173 |
| 2 | 0.68666 | SLE_F4 | Min | 0. | 0. | -690.6369 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 2 | 1.37332 | SLE_F4 | Min | 0. | 0. | -525.4854 |
| 2 | 0. | SLE_QP1 | Max | 0. | 0. | -817.78 |
| 2 | 0.68666 | SLE_QP1 | Max | 0. | 0. | -717.4563 |
| 2 | 1.37332 | SLE_QP1 | Max | 0. | 0. | -573.1613 |
| 2 | 0. | SLE_QP1 | Min | 0. | 0. | -817.78 |
| 2 | 0.68666 | SLE_QP1 | Min | 0. | 0. | -717.4563 |
| 2 | 1.37332 | SLE_QP1 | Min | 0. | 0. | -573.1613 |
| 2 | 0. | SLE_QP2 | Max | 0. | 0. | -883.5896 |
| 2 | 0.68666 | SLE_QP2 | Max | 0. | 0. | -777.9238 |
| 2 | 1.37332 | SLE_QP2 | Max | 0. | 0. | -628.2867 |
| 2 | 0. | SLE_QP2 | Min | 0. | 0. | -883.5896 |
| 2 | 0.68666 | SLE_QP2 | Min | 0. | 0. | -777.9238 |
| 2 | 1.37332 | SLE_QP2 | Min | 0. | 0. | -628.2867 |
| 2 | 0. | SLE_QP3 | Max | 0. | 0. | -868.7457 |
| 2 | 0.68666 | SLE_QP3 | Max | 0. | 0. | -746.0987 |
| 2 | 1.37332 | SLE_QP3 | Max | 0. | 0. | -579.4806 |
| 2 | 0. | SLE_QP3 | Min | 0. | 0. | -868.7457 |
| 2 | 0.68666 | SLE_QP3 | Min | 0. | 0. | -746.0987 |
| 2 | 1.37332 | SLE_QP3 | Min | 0. | 0. | -579.4806 |
| 2 | 0. | SLE_QP4 | Max | 0. | 0. | -756.6733 |
| 2 | 0.68666 | SLE_QP4 | Max | 0. | 0. | -636.5132 |
| 2 | 1.37332 | SLE_QP4 | Max | 0. | 0. | -472.3818 |
| 2 | 0. | SLE_QP4 | Min | 0. | 0. | -756.6733 |
| 2 | 0.68666 | SLE_QP4 | Min | 0. | 0. | -636.5132 |
| 2 | 1.37332 | SLE_QP4 | Min | 0. | 0. | -472.3818 |
| 2 | 0. | SLV_1 | Max | 0. | 0. | -330.8653 |
| 2 | 0.68666 | SLV_1 | Max | 0. | 0. | -223.146 |
| 2 | 1.37332 | SLV_1 | Max | 0. | 0. | -67.8638 |
| 2 | 0. | SLV_1 | Min | 0. | 0. | -330.8653 |
| 2 | 0.68666 | SLV_1 | Min | 0. | 0. | -223.146 |
| 2 | 1.37332 | SLV_1 | Min | 0. | 0. | -67.8638 |
| 2 | 0. | SLV_2 | Max | 0. | 0. | -331.4161 |
| 2 | 0.68666 | SLV_2 | Max | 0. | 0. | -223.6059 |
| 2 | 1.37332 | SLV_2 | Max | 0. | 0. | -68.2329 |
| 2 | 0. | SLV_2 | Min | 0. | 0. | -331.4161 |
| 2 | 0.68666 | SLV_2 | Min | 0. | 0. | -223.6059 |
| 2 | 1.37332 | SLV_2 | Min | 0. | 0. | -68.2329 |
| 2 | 0. | SLV_3 | Max | 0. | 0. | -301.1307 |
| 2 | 0.68666 | SLV_3 | Max | 0. | 0. | -164.6665 |
| 2 | 1.37332 | SLV_3 | Max | 0. | 0. | 19.3606 |
| 2 | 0. | SLV_3 | Min | 0. | 0. | -301.1307 |
| 2 | 0.68666 | SLV_3 | Min | 0. | 0. | -164.6665 |
| 2 | 1.37332 | SLV_3 | Min | 0. | 0. | 19.3606 |
| 2 | 0. | SLV_4 | Max | 0. | 0. | -300.2656 |
| 2 | 0.68666 | SLV_4 | Max | 0. | 0. | -163.7785 |
| 2 | 1.37332 | SLV_4 | Max | 0. | 0. | 20.2714 |
| 2 | 0. | SLV_4 | Min | 0. | 0. | -300.2656 |
| 2 | 0.68666 | SLV_4 | Min | 0. | 0. | -163.7785 |
| 2 | 1.37332 | SLV_4 | Min | 0. | 0. | 20.2714 |
| 2 | 0. | SLD_1 | Max | 0. | 0. | -592.9913 |
| 2 | 0.68666 | SLD_1 | Max | 0. | 0. | -491.1861 |
| 2 | 1.37332 | SLD_1 | Max | 0. | 0. | -343.8236 |
| 2 | 0. | SLD_1 | Min | 0. | 0. | -592.9913 |
| 2 | 0.68666 | SLD_1 | Min | 0. | 0. | -491.1861 |
| 2 | 1.37332 | SLD_1 | Min | 0. | 0. | -343.8236 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 2 | 0. | SLD_2 | Max | 0. | 0. | -594.6244 |
| 2 | 0.68666 | SLD_2 | Max | 0. | 0. | -492.3065 |
| 2 | 1.37332 | SLD_2 | Max | 0. | 0. | -344.4311 |
| 2 | 0. | SLD_2 | Min | 0. | 0. | -594.6244 |
| 2 | 0.68666 | SLD_2 | Min | 0. | 0. | -492.3065 |
| 2 | 1.37332 | SLD_2 | Min | 0. | 0. | -344.4311 |
| 2 | 0. | SLD_3 | Max | 0. | 0. | -525.0014 |
| 2 | 0.68666 | SLD_3 | Max | 0. | 0. | -403.6519 |
| 2 | 1.37332 | SLD_3 | Max | 0. | 0. | -236.7451 |
| 2 | 0. | SLD_3 | Min | 0. | 0. | -525.0014 |
| 2 | 0.68666 | SLD_3 | Min | 0. | 0. | -403.6519 |
| 2 | 1.37332 | SLD_3 | Min | 0. | 0. | -236.7451 |
| 2 | 0. | SLD_4 | Max | 0. | 0. | -524.8294 |
| 2 | 0.68666 | SLD_4 | Max | 0. | 0. | -403.375 |
| 2 | 1.37332 | SLD_4 | Max | 0. | 0. | -236.3632 |
| 2 | 0. | SLD_4 | Min | 0. | 0. | -524.8294 |
| 2 | 0.68666 | SLD_4 | Min | 0. | 0. | -403.375 |
| 2 | 1.37332 | SLD_4 | Min | 0. | 0. | -236.3632 |
| 2 | 0. | SLU_IDR_1 | Max | 0. | 0. | -965.6472 |
| 2 | 0.68666 | SLU_IDR_1 | Max | 0. | 0. | -823.6512 |
| 2 | 1.37332 | SLU_IDR_1 | Max | 0. | 0. | -630.4756 |
| 2 | 0. | SLU_IDR_1 | Min | 0. | 0. | -965.6472 |
| 2 | 0.68666 | SLU_IDR_1 | Min | 0. | 0. | -823.6512 |
| 2 | 1.37332 | SLU_IDR_1 | Min | 0. | 0. | -630.4756 |
| 2 | 0. | SLU_IDR_2 | Max | 0. | 0. | -991.1861 |
| 2 | 0.68666 | SLU_IDR_2 | Max | 0. | 0. | -866.1807 |
| 2 | 1.37332 | SLU_IDR_2 | Max | 0. | 0. | -689.9957 |
| 2 | 0. | SLU_IDR_2 | Min | 0. | 0. | -991.1861 |
| 2 | 0.68666 | SLU_IDR_2 | Min | 0. | 0. | -866.1807 |
| 2 | 1.37332 | SLU_IDR_2 | Min | 0. | 0. | -689.9957 |
| 2 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 469.1435 |
| 2 | 0.68666 | SISMA WOOD SLV-1 | Max | 0. | 0. | 433.0181 |
| 2 | 1.37332 | SISMA WOOD SLV-1 | Max | 0. | 0. | 400.4842 |
| 2 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 469.1435 |
| 2 | 0.68666 | SISMA WOOD SLV-1 | Min | 0. | 0. | 433.0181 |
| 2 | 1.37332 | SISMA WOOD SLV-1 | Min | 0. | 0. | 400.4842 |
| 2 | 0. | DEAD-1 | Max | 0. | 0. | -39.1004 |
| 2 | 0.68666 | DEAD-1 | Max | 0. | 0. | -37.5364 |
| 2 | 1.37332 | DEAD-1 | Max | 0. | 0. | -50.0285 |
| 2 | 0. | DEAD-1 | Min | 0. | 0. | -39.1004 |
| 2 | 0.68666 | DEAD-1 | Min | 0. | 0. | -37.5364 |
| 2 | 1.37332 | DEAD-1 | Min | 0. | 0. | -50.0285 |
| 2 | 0. | SLU_PROVA | | 0. | 0. | -969.903 |
| 2 | 0.68666 | SLU_PROVA | | 0. | 0. | -869.987 |
| 2 | 1.37332 | SLU_PROVA | | 0. | 0. | -712.9085 |
| 3 | 0. | DEAD | | 0. | 0. | -25.8513 |
| 3 | 0.68801 | DEAD | | 0. | 0. | -28.9376 |
| 3 | 1.37601 | DEAD | | 0. | 0. | -46.0695 |
| 3 | 0. | SIMM_KA | | 0. | 0. | 65.18 |
| 3 | 0.68801 | SIMM_KA | | 0. | 0. | 69.993 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 3 | 1.37601 | SIMM_KA | | 0. | 0. | 74.806 |
| 3 | 0. | SIMM_K0 | | 0. | 0. | 99.4364 |
| 3 | 0.68801 | SIMM_K0 | | 0. | 0. | 107.0075 |
| 3 | 1.37601 | SIMM_K0 | | 0. | 0. | 114.5786 |
| 3 | 0. | A--SIMM_KA | | 0. | 0. | 133.3673 |
| 3 | 0.68801 | A--SIMM_KA | | 0. | 0. | 149.3063 |
| 3 | 1.37601 | A--SIMM_KA | | 0. | 0. | 165.2452 |
| 3 | 0. | A--SIMM_K0 | | 0. | 0. | 202.0846 |
| 3 | 0.68801 | A--SIMM_K0 | | 0. | 0. | 226.0409 |
| 3 | 1.37601 | A--SIMM_K0 | | 0. | 0. | 249.9972 |
| 3 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 7.3579 |
| 3 | 0.68801 | A-- SIMM_SOVR_K A | | 0. | 0. | 8.6477 |
| 3 | 1.37601 | A-- SIMM_SOVR_K A | | 0. | 0. | 9.9375 |
| 3 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 11.0314 |
| 3 | 0.68801 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 12.9651 |
| 3 | 1.37601 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 14.8988 |
| 3 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 11.0314 |
| 3 | 0.68801 | SIMM_SOVR_K 0 | | 0. | 0. | 12.9651 |
| 3 | 1.37601 | SIMM_SOVR_K 0 | | 0. | 0. | 14.8988 |
| 3 | 0. | SIMM_SOVR_K A | | 0. | 0. | 7.3579 |
| 3 | 0.68801 | SIMM_SOVR_K A | | 0. | 0. | 8.6477 |
| 3 | 1.37601 | SIMM_SOVR_K A | | 0. | 0. | 9.9375 |
| 3 | 0. | SOVR | | 0. | 0. | -66.744 |
| 3 | 0.68801 | SOVR | | 0. | 0. | -59.0774 |
| 3 | 1.37601 | SOVR | | 0. | 0. | -51.4109 |
| 3 | 0. | TERR_SIMM | | 0. | 0. | -246.3827 |
| 3 | 0.68801 | TERR_SIMM | | 0. | 0. | -212.5649 |
| 3 | 1.37601 | TERR_SIMM | | 0. | 0. | -178.7471 |
| 3 | 0. | TERR_A--SIMM | | 0. | 0. | -332.6102 |
| 3 | 0.68801 | TERR_A--SIMM | | 0. | 0. | -286.637 |
| 3 | 1.37601 | TERR_A--SIMM | | 0. | 0. | -240.6637 |
| 3 | 0. | INERZIA H SLV | | 0. | 0. | 1.8661 |
| 3 | 0.68801 | INERZIA H SLV | | 0. | 0. | 2.1234 |
| 3 | 1.37601 | INERZIA H SLV | | 0. | 0. | 2.3808 |
| 3 | 0. | INERZIA V + SLV | | 0. | 0. | -0.3454 |
| 3 | 0.68801 | INERZIA V + SLV | | 0. | 0. | -0.5106 |
| 3 | 1.37601 | INERZIA V + SLV | | 0. | 0. | -0.6757 |
| 3 | 0. | INERZIA V - SLV | | 0. | 0. | 0.3454 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 3 | 0.68801 | INERZIA V - SLV | | 0. | 0. | 0.5106 |
| 3 | 1.37601 | INERZIA V - SLV | | 0. | 0. | 0.6757 |
| 3 | 0. | SISMA WOOD SLV | | 0. | 0. | 165.2657 |
| 3 | 0.68801 | SISMA WOOD SLV | | 0. | 0. | 177.1857 |
| 3 | 1.37601 | SISMA WOOD SLV | | 0. | 0. | 193.9039 |
| 3 | 0. | IDROSTATICA | | 0. | 0. | -311.3097 |
| 3 | 0.68801 | IDROSTATICA | | 0. | 0. | -213.4487 |
| 3 | 1.37601 | IDROSTATICA | | 0. | 0. | -57.3321 |
| 3 | 0. | SISMA WOOD SLD | | 0. | 0. | 72.988 |
| 3 | 0.68801 | SISMA WOOD SLD | | 0. | 0. | 78.2524 |
| 3 | 1.37601 | SISMA WOOD SLD | | 0. | 0. | 85.6358 |
| 3 | 0. | INERZIA H SLD | | 0. | 0. | 0.8241 |
| 3 | 0.68801 | INERZIA H SLD | | 0. | 0. | 0.9378 |
| 3 | 1.37601 | INERZIA H SLD | | 0. | 0. | 1.0515 |
| 3 | 0. | INERZIA V + SLD | | 0. | 0. | -0.1526 |
| 3 | 0.68801 | INERZIA V + SLD | | 0. | 0. | -0.2255 |
| 3 | 1.37601 | INERZIA V + SLD | | 0. | 0. | -0.2984 |
| 3 | 0. | INERZIA V SLD | | 0. | 0. | 0.1526 |
| 3 | 0.68801 | INERZIA V SLD | | 0. | 0. | 0.2255 |
| 3 | 1.37601 | INERZIA V SLD | | 0. | 0. | 0.2984 |
| 3 | 0. | INERZIA V -1 | | 0. | 0. | 0.3454 |
| 3 | 0.68801 | INERZIA V -1 | | 0. | 0. | 0.5106 |
| 3 | 1.37601 | INERZIA V -1 | | 0. | 0. | 0.6757 |
| 3 | 0. | SLU_1 | Max | 0. | 0. | -819.6572 |
| 3 | 0.68801 | SLU_1 | Max | 0. | 0. | -598.6933 |
| 3 | 1.37601 | SLU_1 | Max | 0. | 0. | -320.2566 |
| 3 | 0. | SLU_1 | Min | 0. | 0. | -819.6572 |
| 3 | 0.68801 | SLU_1 | Min | 0. | 0. | -598.6933 |
| 3 | 1.37601 | SLU_1 | Min | 0. | 0. | -320.2566 |
| 3 | 0. | SLU_2 | Max | 0. | 0. | -901.3483 |
| 3 | 0.68801 | SLU_2 | Max | 0. | 0. | -671.2581 |
| 3 | 1.37601 | SLU_2 | Max | 0. | 0. | -383.6952 |
| 3 | 0. | SLU_2 | Min | 0. | 0. | -901.3483 |
| 3 | 0.68801 | SLU_2 | Min | 0. | 0. | -671.2581 |
| 3 | 1.37601 | SLU_2 | Min | 0. | 0. | -383.6952 |
| 3 | 0. | SLU_3 | Max | 0. | 0. | -720.114 |
| 3 | 0.68801 | SLU_3 | Max | 0. | 0. | -455.9091 |
| 3 | 1.37601 | SLU_3 | Max | 0. | 0. | -134.2315 |
| 3 | 0. | SLU_3 | Min | 0. | 0. | -720.114 |
| 3 | 0.68801 | SLU_3 | Min | 0. | 0. | -455.9091 |
| 3 | 1.37601 | SLU_3 | Min | 0. | 0. | -134.2315 |
| 3 | 0. | SLU_4 | Max | 0. | 0. | -855.8607 |
| 3 | 0.68801 | SLU_4 | Max | 0. | 0. | -597.0593 |
| 3 | 1.37601 | SLU_4 | Max | 0. | 0. | -280.785 |
| 3 | 0. | SLU_4 | Min | 0. | 0. | -855.8607 |
| 3 | 0.68801 | SLU_4 | Min | 0. | 0. | -597.0593 |
| 3 | 1.37601 | SLU_4 | Min | 0. | 0. | -280.785 |
| 3 | 0. | SLE_F1 | Max | 0. | 0. | -610.834 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 3 | 0.68801 | SLE_F1 | Max | 0. | 0. | -441.6018 |
| 3 | 1.37601 | SLE_F1 | Max | 0. | 0. | -228.1598 |
| 3 | 0. | SLE_F1 | Min | 0. | 0. | -610.834 |
| 3 | 0.68801 | SLE_F1 | Min | 0. | 0. | -441.6018 |
| 3 | 1.37601 | SLE_F1 | Min | 0. | 0. | -228.1598 |
| 3 | 0. | SLE_F2 | Max | 0. | 0. | -670.5747 |
| 3 | 0.68801 | SLE_F2 | Max | 0. | 0. | -493.9717 |
| 3 | 1.37601 | SLE_F2 | Max | 0. | 0. | -273.1588 |
| 3 | 0. | SLE_F2 | Min | 0. | 0. | -670.5747 |
| 3 | 0.68801 | SLE_F2 | Min | 0. | 0. | -493.9717 |
| 3 | 1.37601 | SLE_F2 | Min | 0. | 0. | -273.1588 |
| 3 | 0. | SLE_F3 | Max | 0. | 0. | -630.7484 |
| 3 | 0.68801 | SLE_F3 | Max | 0. | 0. | -433.7235 |
| 3 | 1.37601 | SLE_F3 | Max | 0. | 0. | -192.4887 |
| 3 | 0. | SLE_F3 | Min | 0. | 0. | -630.7484 |
| 3 | 0.68801 | SLE_F3 | Min | 0. | 0. | -433.7235 |
| 3 | 1.37601 | SLE_F3 | Min | 0. | 0. | -192.4887 |
| 3 | 0. | SLE_F4 | Max | 0. | 0. | -525.4854 |
| 3 | 0.68801 | SLE_F4 | Max | 0. | 0. | -325.0416 |
| 3 | 1.37601 | SLE_F4 | Max | 0. | 0. | -80.388 |
| 3 | 0. | SLE_F4 | Min | 0. | 0. | -525.4854 |
| 3 | 0.68801 | SLE_F4 | Min | 0. | 0. | -325.0416 |
| 3 | 1.37601 | SLE_F4 | Min | 0. | 0. | -80.388 |
| 3 | 0. | SLE_QP1 | Max | 0. | 0. | -573.1613 |
| 3 | 0.68801 | SLE_QP1 | Max | 0. | 0. | -404.3726 |
| 3 | 1.37601 | SLE_QP1 | Max | 0. | 0. | -191.374 |
| 3 | 0. | SLE_QP1 | Min | 0. | 0. | -573.1613 |
| 3 | 0.68801 | SLE_QP1 | Min | 0. | 0. | -404.3726 |
| 3 | 1.37601 | SLE_QP1 | Min | 0. | 0. | -191.374 |
| 3 | 0. | SLE_QP2 | Max | 0. | 0. | -628.2867 |
| 3 | 0.68801 | SLE_QP2 | Max | 0. | 0. | -452.4076 |
| 3 | 1.37601 | SLE_QP2 | Max | 0. | 0. | -232.3185 |
| 3 | 0. | SLE_QP2 | Min | 0. | 0. | -628.2867 |
| 3 | 0.68801 | SLE_QP2 | Min | 0. | 0. | -452.4076 |
| 3 | 1.37601 | SLE_QP2 | Min | 0. | 0. | -232.3185 |
| 3 | 0. | SLE_QP3 | Max | 0. | 0. | -579.4806 |
| 3 | 0.68801 | SLE_QP3 | Max | 0. | 0. | -386.2691 |
| 3 | 1.37601 | SLE_QP3 | Max | 0. | 0. | -148.8477 |
| 3 | 0. | SLE_QP3 | Min | 0. | 0. | -579.4806 |
| 3 | 0.68801 | SLE_QP3 | Min | 0. | 0. | -386.2691 |
| 3 | 1.37601 | SLE_QP3 | Min | 0. | 0. | -148.8477 |
| 3 | 0. | SLE_QP4 | Max | 0. | 0. | -472.3818 |
| 3 | 0.68801 | SLE_QP4 | Max | 0. | 0. | -277.2322 |
| 3 | 1.37601 | SLE_QP4 | Max | 0. | 0. | -37.8727 |
| 3 | 0. | SLE_QP4 | Min | 0. | 0. | -472.3818 |
| 3 | 0.68801 | SLE_QP4 | Min | 0. | 0. | -277.2322 |
| 3 | 1.37601 | SLE_QP4 | Min | 0. | 0. | -37.8727 |
| 3 | 0. | SLV_1 | Max | 0. | 0. | -67.8638 |
| 3 | 0.68801 | SLV_1 | Max | 0. | 0. | 107.3151 |
| 3 | 1.37601 | SLV_1 | Max | 0. | 0. | 331.502 |
| 3 | 0. | SLV_1 | Min | 0. | 0. | -67.8638 |
| 3 | 0.68801 | SLV_1 | Min | 0. | 0. | 107.3151 |
| 3 | 1.37601 | SLV_1 | Min | 0. | 0. | 331.502 |
| 3 | 0. | SLV_2 | Max | 0. | 0. | -68.2329 |
| 3 | 0.68801 | SLV_2 | Max | 0. | 0. | 106.9597 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 3 | 1.37601 | SLV_2 | Max | 0. | 0. | 331.1602 |
| 3 | 0. | SLV_2 | Min | 0. | 0. | -68.2329 |
| 3 | 0.68801 | SLV_2 | Min | 0. | 0. | 106.9597 |
| 3 | 1.37601 | SLV_2 | Min | 0. | 0. | 331.1602 |
| 3 | 0. | SLV_3 | Max | 0. | 0. | 19.3606 |
| 3 | 0.68801 | SLV_3 | Max | 0. | 0. | 233.4967 |
| 3 | 1.37601 | SLV_3 | Max | 0. | 0. | 496.6408 |
| 3 | 0. | SLV_3 | Min | 0. | 0. | 19.3606 |
| 3 | 0.68801 | SLV_3 | Min | 0. | 0. | 233.4967 |
| 3 | 1.37601 | SLV_3 | Min | 0. | 0. | 496.6408 |
| 3 | 0. | SLV_4 | Max | 0. | 0. | 20.2714 |
| 3 | 0.68801 | SLV_4 | Max | 0. | 0. | 234.461 |
| 3 | 1.37601 | SLV_4 | Max | 0. | 0. | 497.6587 |
| 3 | 0. | SLV_4 | Min | 0. | 0. | 20.2714 |
| 3 | 0.68801 | SLV_4 | Min | 0. | 0. | 234.461 |
| 3 | 1.37601 | SLV_4 | Min | 0. | 0. | 497.6587 |
| 3 | 0. | SLD_1 | Max | 0. | 0. | -343.8236 |
| 3 | 0.68801 | SLD_1 | Max | 0. | 0. | -175.1654 |
| 3 | 1.37601 | SLD_1 | Max | 0. | 0. | 39.8216 |
| 3 | 0. | SLD_1 | Min | 0. | 0. | -343.8236 |
| 3 | 0.68801 | SLD_1 | Min | 0. | 0. | -175.1654 |
| 3 | 1.37601 | SLD_1 | Min | 0. | 0. | 39.8216 |
| 3 | 0. | SLD_2 | Max | 0. | 0. | -344.4311 |
| 3 | 0.68801 | SLD_2 | Max | 0. | 0. | -175.1252 |
| 3 | 1.37601 | SLD_2 | Max | 0. | 0. | 40.5097 |
| 3 | 0. | SLD_2 | Min | 0. | 0. | -344.4311 |
| 3 | 0.68801 | SLD_2 | Min | 0. | 0. | -175.1252 |
| 3 | 1.37601 | SLD_2 | Min | 0. | 0. | 40.5097 |
| 3 | 0. | SLD_3 | Max | 0. | 0. | -236.7451 |
| 3 | 0.68801 | SLD_3 | Max | 0. | 0. | -36.9957 |
| 3 | 1.37601 | SLD_3 | Max | 0. | 0. | 209.0827 |
| 3 | 0. | SLD_3 | Min | 0. | 0. | -236.7451 |
| 3 | 0.68801 | SLD_3 | Min | 0. | 0. | -36.9957 |
| 3 | 1.37601 | SLD_3 | Min | 0. | 0. | 209.0827 |
| 3 | 0. | SLD_4 | Max | 0. | 0. | -236.3632 |
| 3 | 0.68801 | SLD_4 | Max | 0. | 0. | -36.4905 |
| 3 | 1.37601 | SLD_4 | Max | 0. | 0. | 209.7112 |
| 3 | 0. | SLD_4 | Min | 0. | 0. | -236.3632 |
| 3 | 0.68801 | SLD_4 | Min | 0. | 0. | -36.4905 |
| 3 | 1.37601 | SLD_4 | Min | 0. | 0. | 209.7112 |
| 3 | 0. | SLU_IDR_1 | Max | 0. | 0. | -630.4756 |
| 3 | 0.68801 | SLU_IDR_1 | Max | 0. | 0. | -406.1238 |
| 3 | 1.37601 | SLU_IDR_1 | Max | 0. | 0. | -130.332 |
| 3 | 0. | SLU_IDR_1 | Min | 0. | 0. | -630.4756 |
| 3 | 0.68801 | SLU_IDR_1 | Min | 0. | 0. | -406.1238 |
| 3 | 1.37601 | SLU_IDR_1 | Min | 0. | 0. | -130.332 |
| 3 | 0. | SLU_IDR_2 | Max | 0. | 0. | -689.9957 |
| 3 | 0.68801 | SLU_IDR_2 | Max | 0. | 0. | -482.3294 |
| 3 | 1.37601 | SLU_IDR_2 | Max | 0. | 0. | -223.2232 |
| 3 | 0. | SLU_IDR_2 | Min | 0. | 0. | -689.9957 |
| 3 | 0.68801 | SLU_IDR_2 | Min | 0. | 0. | -482.3294 |
| 3 | 1.37601 | SLU_IDR_2 | Min | 0. | 0. | -223.2232 |
| 3 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 400.4842 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 3 | 0.68801 | SISMA WOOD SLV-1 | Max | 0. | 0. | 355.5083 |
| 3 | 1.37601 | SISMA WOOD SLV-1 | Max | 0. | 0. | 315.3305 |
| 3 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 400.4842 |
| 3 | 0.68801 | SISMA WOOD SLV-1 | Min | 0. | 0. | 355.5083 |
| 3 | 1.37601 | SISMA WOOD SLV-1 | Min | 0. | 0. | 315.3305 |
| 3 | 0. | DEAD-1 | Max | 0. | 0. | -50.0285 |
| 3 | 0.68801 | DEAD-1 | Max | 0. | 0. | -50.9035 |
| 3 | 1.37601 | DEAD-1 | Max | 0. | 0. | -65.8241 |
| 3 | 0. | DEAD-1 | Min | 0. | 0. | -50.0285 |
| 3 | 0.68801 | DEAD-1 | Min | 0. | 0. | -50.9035 |
| 3 | 1.37601 | DEAD-1 | Min | 0. | 0. | -65.8241 |
| 3 | 0. | SLU_PROVA | | 0. | 0. | -712.9085 |
| 3 | 0.68801 | SLU_PROVA | | 0. | 0. | -521.4952 |
| 3 | 1.37601 | SLU_PROVA | | 0. | 0. | -272.6091 |
| 4 | 0. | DEAD | | 0. | 0. | -89.9668 |
| 4 | 0.31251 | DEAD | | 0. | 0. | -92.7953 |
| 4 | 0.62502 | DEAD | | 0. | 0. | -98.2378 |
| 4 | 0. | SIMM_KA | | 0. | 0. | 60.4261 |
| 4 | 0.31251 | SIMM_KA | | 0. | 0. | 50.275 |
| 4 | 0.62502 | SIMM_KA | | 0. | 0. | 40.1239 |
| 4 | 0. | SIMM_K0 | | 0. | 0. | 94.3233 |
| 4 | 0.31251 | SIMM_K0 | | 0. | 0. | 79.1881 |
| 4 | 0.62502 | SIMM_K0 | | 0. | 0. | 64.0528 |
| 4 | 0. | A--SIMM_KA | | 0. | 0. | 174.263 |
| 4 | 0.31251 | A--SIMM_KA | | 0. | 0. | 162.6611 |
| 4 | 0.62502 | A--SIMM_KA | | 0. | 0. | 151.0592 |
| 4 | 0. | A--SIMM_K0 | | 0. | 0. | 262.543 |
| 4 | 0.31251 | A--SIMM_K0 | | 0. | 0. | 244.7094 |
| 4 | 0.62502 | A--SIMM_K0 | | 0. | 0. | 226.8757 |
| 4 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 13.8144 |
| 4 | 0.31251 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.8117 |
| 4 | 0.62502 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.809 |
| 4 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.7112 |
| 4 | 0.31251 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.7072 |
| 4 | 0.62502 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.7031 |
| 4 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 20.7112 |
| 4 | 0.31251 | SIMM_SOVR_K 0 | | 0. | 0. | 20.7072 |
| 4 | 0.62502 | SIMM_SOVR_K 0 | | 0. | 0. | 20.7031 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 4 | 0. | SIMM_SOVR_K A | | 0. | 0. | 13.8144 |
| 4 | 0.31251 | SIMM_SOVR_K A | | 0. | 0. | 13.8117 |
| 4 | 0.62502 | SIMM_SOVR_K A | | 0. | 0. | 13.809 |
| 4 | 0. | SOVR | | 0. | 0. | 5.5591 |
| 4 | 0.31251 | SOVR | | 0. | 0. | 17.0131 |
| 4 | 0.62502 | SOVR | | 0. | 0. | 28.4671 |
| 4 | 0. | TERR_SIMM | | 0. | 0. | 57.5921 |
| 4 | 0.31251 | TERR_SIMM | | 0. | 0. | 103.0612 |
| 4 | 0.62502 | TERR_SIMM | | 0. | 0. | 148.5302 |
| 4 | 0. | TERR_A--SIMM | | 0. | 0. | 108.0928 |
| 4 | 0.31251 | TERR_A--SIMM | | 0. | 0. | 176.9796 |
| 4 | 0.62502 | TERR_A--SIMM | | 0. | 0. | 245.8664 |
| 4 | 0. | INERZIA H SLV | | 0. | 0. | 3.7506 |
| 4 | 0.31251 | INERZIA H SLV | | 0. | 0. | 4.067 |
| 4 | 0.62502 | INERZIA H SLV | | 0. | 0. | 4.3834 |
| 4 | 0. | INERZIA V + SLV | | 0. | 0. | -1.4005 |
| 4 | 0.31251 | INERZIA V + SLV | | 0. | 0. | -1.4706 |
| 4 | 0.62502 | INERZIA V + SLV | | 0. | 0. | -1.5406 |
| 4 | 0. | INERZIA V - SLV | | 0. | 0. | 1.4005 |
| 4 | 0.31251 | INERZIA V - SLV | | 0. | 0. | 1.4706 |
| 4 | 0.62502 | INERZIA V - SLV | | 0. | 0. | 1.5406 |
| 4 | 0. | SISMA WOOD SLV | | 0. | 0. | 244.8416 |
| 4 | 0.31251 | SISMA WOOD SLV | | 0. | 0. | 250.8435 |
| 4 | 0.62502 | SISMA WOOD SLV | | 0. | 0. | 259.9177 |
| 4 | 0. | iDROSTATICA | | 0. | 0. | 599.0573 |
| 4 | 0.31251 | iDROSTATICA | | 0. | 0. | 686.5513 |
| 4 | 0.62502 | iDROSTATICA | | 0. | 0. | 786.0646 |
| 4 | 0. | SISMA WOOD SLD | | 0. | 0. | 108.1319 |
| 4 | 0.31251 | SISMA WOOD SLD | | 0. | 0. | 110.7826 |
| 4 | 0.62502 | SISMA WOOD SLD | | 0. | 0. | 114.7902 |
| 4 | 0. | INERZIA H SLD | | 0. | 0. | 1.6564 |
| 4 | 0.31251 | INERZIA H SLD | | 0. | 0. | 1.7962 |
| 4 | 0.62502 | INERZIA H SLD | | 0. | 0. | 1.9359 |
| 4 | 0. | INERZIA V + SLD | | 0. | 0. | -0.6185 |
| 4 | 0.31251 | INERZIA V + SLD | | 0. | 0. | -0.6495 |
| 4 | 0.62502 | INERZIA V + SLD | | 0. | 0. | -0.6804 |
| 4 | 0. | INERZIA V SLD | | 0. | 0. | 0.6185 |
| 4 | 0.31251 | INERZIA V SLD | | 0. | 0. | 0.6495 |
| 4 | 0.62502 | INERZIA V SLD | | 0. | 0. | 0.6804 |
| 4 | 0. | INERZIA V -1 | | 0. | 0. | 1.4005 |
| 4 | 0.31251 | INERZIA V -1 | | 0. | 0. | 1.4706 |
| 4 | 0.62502 | INERZIA V -1 | | 0. | 0. | 1.5406 |
| 4 | 0. | SLU_1 | Max | 0. | 0. | 960.8515 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 4 | 0.31251 | SLU_1 | Max | 0. | 0. | 1143.7723 |
| 4 | 0.62502 | SLU_1 | Max | 0. | 0. | 1338.9198 |
| 4 | 0. | SLU_1 | Min | 0. | 0. | 960.8515 |
| 4 | 0.31251 | SLU_1 | Min | 0. | 0. | 1143.7723 |
| 4 | 0.62502 | SLU_1 | Min | 0. | 0. | 1338.9198 |
| 4 | 0. | SLU_2 | Max | 0. | 0. | 937.1969 |
| 4 | 0.31251 | SLU_2 | Max | 0. | 0. | 1130.0089 |
| 4 | 0.62502 | SLU_2 | Max | 0. | 0. | 1335.0476 |
| 4 | 0. | SLU_2 | Min | 0. | 0. | 937.1969 |
| 4 | 0.31251 | SLU_2 | Min | 0. | 0. | 1130.0089 |
| 4 | 0.62502 | SLU_2 | Min | 0. | 0. | 1335.0476 |
| 4 | 0. | SLU_3 | Max | 0. | 0. | 1385.4425 |
| 4 | 0.31251 | SLU_3 | Max | 0. | 0. | 1602.9387 |
| 4 | 0.62502 | SLU_3 | Max | 0. | 0. | 1832.6616 |
| 4 | 0. | SLU_3 | Min | 0. | 0. | 1385.4425 |
| 4 | 0.31251 | SLU_3 | Min | 0. | 0. | 1602.9387 |
| 4 | 0.62502 | SLU_3 | Min | 0. | 0. | 1832.6616 |
| 4 | 0. | SLU_4 | Max | 0. | 0. | 1241.1558 |
| 4 | 0.31251 | SLU_4 | Max | 0. | 0. | 1467.8355 |
| 4 | 0.62502 | SLU_4 | Max | 0. | 0. | 1706.7419 |
| 4 | 0. | SLU_4 | Min | 0. | 0. | 1241.1558 |
| 4 | 0.31251 | SLU_4 | Min | 0. | 0. | 1467.8355 |
| 4 | 0.62502 | SLU_4 | Min | 0. | 0. | 1706.7419 |
| 4 | 0. | SLE_F1 | Max | 0. | 0. | 737.6245 |
| 4 | 0.31251 | SLE_F1 | Max | 0. | 0. | 873.7731 |
| 4 | 0.62502 | SLE_F1 | Max | 0. | 0. | 1019.3268 |
| 4 | 0. | SLE_F1 | Min | 0. | 0. | 737.6245 |
| 4 | 0.31251 | SLE_F1 | Min | 0. | 0. | 873.7731 |
| 4 | 0.62502 | SLE_F1 | Min | 0. | 0. | 1019.3268 |
| 4 | 0. | SLE_F2 | Max | 0. | 0. | 723.9918 |
| 4 | 0.31251 | SLE_F2 | Max | 0. | 0. | 867.6947 |
| 4 | 0.62502 | SLE_F2 | Max | 0. | 0. | 1020.8028 |
| 4 | 0. | SLE_F2 | Min | 0. | 0. | 723.9918 |
| 4 | 0.31251 | SLE_F2 | Min | 0. | 0. | 867.6947 |
| 4 | 0.62502 | SLE_F2 | Min | 0. | 0. | 1020.8028 |
| 4 | 0. | SLE_F3 | Max | 0. | 0. | 954.8251 |
| 4 | 0.31251 | SLE_F3 | Max | 0. | 0. | 1124.1606 |
| 4 | 0.62502 | SLE_F3 | Max | 0. | 0. | 1302.9011 |
| 4 | 0. | SLE_F3 | Min | 0. | 0. | 954.8251 |
| 4 | 0.31251 | SLE_F3 | Min | 0. | 0. | 1124.1606 |
| 4 | 0.62502 | SLE_F3 | Min | 0. | 0. | 1302.9011 |
| 4 | 0. | SLE_F4 | Max | 0. | 0. | 1060.7551 |
| 4 | 0.31251 | SLE_F4 | Max | 0. | 0. | 1222.0768 |
| 4 | 0.62502 | SLE_F4 | Max | 0. | 0. | 1392.8037 |
| 4 | 0. | SLE_F4 | Min | 0. | 0. | 1060.7551 |
| 4 | 0.31251 | SLE_F4 | Min | 0. | 0. | 1222.0768 |
| 4 | 0.62502 | SLE_F4 | Min | 0. | 0. | 1392.8037 |
| 4 | 0. | SLE_QP1 | Max | 0. | 0. | 739.7324 |
| 4 | 0.31251 | SLE_QP1 | Max | 0. | 0. | 867.5005 |
| 4 | 0.62502 | SLE_QP1 | Max | 0. | 0. | 1004.6737 |
| 4 | 0. | SLE_QP1 | Min | 0. | 0. | 739.7324 |
| 4 | 0.31251 | SLE_QP1 | Min | 0. | 0. | 867.5005 |
| 4 | 0.62502 | SLE_QP1 | Min | 0. | 0. | 1004.6737 |
| 4 | 0. | SLE_QP2 | Max | 0. | 0. | 729.6924 |
| 4 | 0.31251 | SLE_QP2 | Max | 0. | 0. | 864.8261 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 4 | 0.62502 | SLE_QP2 | Max | 0. | 0. | 1009.3649 |
| 4 | 0. | SLE_QP2 | Min | 0. | 0. | 729.6924 |
| 4 | 0.31251 | SLE_QP2 | Min | 0. | 0. | 864.8261 |
| 4 | 0.62502 | SLE_QP2 | Min | 0. | 0. | 1009.3649 |
| 4 | 0. | SLE_QP3 | Max | 0. | 0. | 954.9896 |
| 4 | 0.31251 | SLE_QP3 | Max | 0. | 0. | 1114.9769 |
| 4 | 0.62502 | SLE_QP3 | Max | 0. | 0. | 1284.3694 |
| 4 | 0. | SLE_QP3 | Min | 0. | 0. | 954.9896 |
| 4 | 0.31251 | SLE_QP3 | Min | 0. | 0. | 1114.9769 |
| 4 | 0.62502 | SLE_QP3 | Min | 0. | 0. | 1284.3694 |
| 4 | 0. | SLE_QP4 | Max | 0. | 0. | 1050.7241 |
| 4 | 0.31251 | SLE_QP4 | Max | 0. | 0. | 1200.7357 |
| 4 | 0.62502 | SLE_QP4 | Max | 0. | 0. | 1360.1525 |
| 4 | 0. | SLE_QP4 | Min | 0. | 0. | 1050.7241 |
| 4 | 0.31251 | SLE_QP4 | Min | 0. | 0. | 1200.7357 |
| 4 | 0.62502 | SLE_QP4 | Min | 0. | 0. | 1360.1525 |
| 4 | 0. | SLV_1 | Max | 0. | 0. | 1155.3488 |
| 4 | 0.31251 | SLV_1 | Max | 0. | 0. | 1238.6615 |
| 4 | 0.62502 | SLV_1 | Max | 0. | 0. | 1334.4515 |
| 4 | 0. | SLV_1 | Min | 0. | 0. | 1155.3488 |
| 4 | 0.31251 | SLV_1 | Min | 0. | 0. | 1238.6615 |
| 4 | 0.62502 | SLV_1 | Min | 0. | 0. | 1334.4515 |
| 4 | 0. | SLV_2 | Max | 0. | 0. | 1156.5991 |
| 4 | 0.31251 | SLV_2 | Max | 0. | 0. | 1240.1835 |
| 4 | 0.62502 | SLV_2 | Max | 0. | 0. | 1336.2452 |
| 4 | 0. | SLV_2 | Min | 0. | 0. | 1156.5991 |
| 4 | 0.31251 | SLV_2 | Min | 0. | 0. | 1240.1835 |
| 4 | 0.62502 | SLV_2 | Min | 0. | 0. | 1336.2452 |
| 4 | 0. | SLV_3 | Max | 0. | 0. | 1466.8934 |
| 4 | 0.31251 | SLV_3 | Max | 0. | 0. | 1560.6871 |
| 4 | 0.62502 | SLV_3 | Max | 0. | 0. | 1666.9583 |
| 4 | 0. | SLV_3 | Min | 0. | 0. | 1466.8934 |
| 4 | 0.31251 | SLV_3 | Min | 0. | 0. | 1560.6871 |
| 4 | 0.62502 | SLV_3 | Min | 0. | 0. | 1666.9583 |
| 4 | 0. | SLV_4 | Max | 0. | 0. | 1467.7438 |
| 4 | 0.31251 | SLV_4 | Max | 0. | 0. | 1561.6149 |
| 4 | 0.62502 | SLV_4 | Max | 0. | 0. | 1667.9634 |
| 4 | 0. | SLV_4 | Min | 0. | 0. | 1467.7438 |
| 4 | 0.31251 | SLV_4 | Min | 0. | 0. | 1561.6149 |
| 4 | 0.62502 | SLV_4 | Min | 0. | 0. | 1667.9634 |
| 4 | 0. | SLD_1 | Max | 0. | 0. | 942.8847 |
| 4 | 0.31251 | SLD_1 | Max | 0. | 0. | 1055.7852 |
| 4 | 0.62502 | SLD_1 | Max | 0. | 0. | 1179.4478 |
| 4 | 0. | SLD_1 | Min | 0. | 0. | 942.8847 |
| 4 | 0.31251 | SLD_1 | Min | 0. | 0. | 1055.7852 |
| 4 | 0.62502 | SLD_1 | Min | 0. | 0. | 1179.4478 |
| 4 | 0. | SLD_2 | Max | 0. | 0. | 945.2057 |
| 4 | 0.31251 | SLD_2 | Max | 0. | 0. | 1058.206 |
| 4 | 0.62502 | SLD_2 | Max | 0. | 0. | 1181.9683 |
| 4 | 0. | SLD_2 | Min | 0. | 0. | 945.2057 |
| 4 | 0.31251 | SLD_2 | Min | 0. | 0. | 1058.206 |
| 4 | 0.62502 | SLD_2 | Min | 0. | 0. | 1181.9683 |
| 4 | 0. | SLD_3 | Max | 0. | 0. | 1238.0006 |
| 4 | 0.31251 | SLD_3 | Max | 0. | 0. | 1360.4122 |
| 4 | 0.62502 | SLD_3 | Max | 0. | 0. | 1493.5859 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 4 | 0. | SLD_3 | Min | 0. | 0. | 1238.0006 |
| 4 | 0.31251 | SLD_3 | Min | 0. | 0. | 1360.4122 |
| 4 | 0.62502 | SLD_3 | Min | 0. | 0. | 1493.5859 |
| 4 | 0. | SLD_4 | Max | 0. | 0. | 1238.9235 |
| 4 | 0.31251 | SLD_4 | Max | 0. | 0. | 1361.3162 |
| 4 | 0.62502 | SLD_4 | Max | 0. | 0. | 1494.4708 |
| 4 | 0. | SLD_4 | Min | 0. | 0. | 1238.9235 |
| 4 | 0.31251 | SLD_4 | Min | 0. | 0. | 1361.3162 |
| 4 | 0.62502 | SLD_4 | Min | 0. | 0. | 1494.4708 |
| 4 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1067.0607 |
| 4 | 0.31251 | SLU_IDR_1 | Max | 0. | 0. | 1234.026 |
| 4 | 0.62502 | SLU_IDR_1 | Max | 0. | 0. | 1411.8598 |
| 4 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1067.0607 |
| 4 | 0.31251 | SLU_IDR_1 | Min | 0. | 0. | 1234.026 |
| 4 | 0.62502 | SLU_IDR_1 | Min | 0. | 0. | 1411.8598 |
| 4 | 0. | SLU_IDR_2 | Max | 0. | 0. | 879.2402 |
| 4 | 0.31251 | SLU_IDR_2 | Max | 0. | 0. | 1026.9794 |
| 4 | 0.62502 | SLU_IDR_2 | Max | 0. | 0. | 1185.5871 |
| 4 | 0. | SLU_IDR_2 | Min | 0. | 0. | 879.2402 |
| 4 | 0.31251 | SLU_IDR_2 | Min | 0. | 0. | 1026.9794 |
| 4 | 0.62502 | SLU_IDR_2 | Min | 0. | 0. | 1185.5871 |
| 4 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 55.9848 |
| 4 | 0.31251 | SISMA WOOD SLV-1 | Max | 0. | 0. | 9.7863 |
| 4 | 0.62502 | SISMA WOOD SLV-1 | Max | 0. | 0. | -33.3399 |
| 4 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 55.9848 |
| 4 | 0.31251 | SISMA WOOD SLV-1 | Min | 0. | 0. | 9.7863 |
| 4 | 0.62502 | SISMA WOOD SLV-1 | Min | 0. | 0. | -33.3399 |
| 4 | 0. | DEAD-1 | Max | 0. | 0. | -91.8141 |
| 4 | 0.31251 | DEAD-1 | Max | 0. | 0. | -90.8409 |
| 4 | 0.62502 | DEAD-1 | Max | 0. | 0. | -92.4818 |
| 4 | 0. | DEAD-1 | Min | 0. | 0. | -91.8141 |
| 4 | 0.31251 | DEAD-1 | Min | 0. | 0. | -90.8409 |
| 4 | 0.62502 | DEAD-1 | Min | 0. | 0. | -92.4818 |
| 4 | 0. | SLU_PROVA | | 0. | 0. | 898.713 |
| 4 | 0.31251 | SLU_PROVA | | 0. | 0. | 1065.3873 |
| 4 | 0.62502 | SLU_PROVA | | 0. | 0. | 1244.2882 |
| 6 | 0. | DEAD | | 0. | 0. | 73.8874 |
| 6 | 0.5 | DEAD | | 0. | 0. | 104.7161 |
| 6 | 1. | DEAD | | 0. | 0. | 135.5447 |
| 6 | 0. | SIMM_KA | | 0. | 0. | -116.6546 |
| 6 | 0.5 | SIMM_KA | | 0. | 0. | -154.0845 |
| 6 | 1. | SIMM_KA | | 0. | 0. | -180.1856 |
| 6 | 0. | SIMM_K0 | | 0. | 0. | -172.973 |
| 6 | 0.5 | SIMM_K0 | | 0. | 0. | -230.1155 |
| 6 | 1. | SIMM_K0 | | 0. | 0. | -270.2655 |
| 6 | 0. | A--SIMM_KA | | 0. | 0. | -72.9984 |
| 6 | 0.5 | A--SIMM_KA | | 0. | 0. | -139.3345 |
| 6 | 1. | A--SIMM_KA | | 0. | 0. | -187.5207 |
| 6 | 0. | A--SIMM_K0 | | 0. | 0. | -117.3833 |
| 6 | 0.5 | A--SIMM_K0 | | 0. | 0. | -217.5721 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 6 | 1. | A--SIMM_K0 | | 0. | 0. | -289.7859 |
| 6 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 0.9899 |
| 6 | 0.5 | A-- SIMM_SOVR_K A | | 0. | 0. | -4.8327 |
| 6 | 1. | A-- SIMM_SOVR_K A | | 0. | 0. | -10.6553 |
| 6 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 1.4841 |
| 6 | 0.5 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -7.2454 |
| 6 | 1. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -15.975 |
| 6 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 1.4841 |
| 6 | 0.5 | SIMM_SOVR_K 0 | | 0. | 0. | -7.2454 |
| 6 | 1. | SIMM_SOVR_K 0 | | 0. | 0. | -15.975 |
| 6 | 0. | SIMM_SOVR_K A | | 0. | 0. | 0.9899 |
| 6 | 0.5 | SIMM_SOVR_K A | | 0. | 0. | -4.8327 |
| 6 | 1. | SIMM_SOVR_K A | | 0. | 0. | -10.6553 |
| 6 | 0. | SOVR | | 0. | 0. | 129.1788 |
| 6 | 0.5 | SOVR | | 0. | 0. | 147.5574 |
| 6 | 1. | SOVR | | 0. | 0. | 165.9359 |
| 6 | 0. | TERR_SIMM | | 0. | 0. | 514.7408 |
| 6 | 0.5 | TERR_SIMM | | 0. | 0. | 572.3924 |
| 6 | 1. | TERR_SIMM | | 0. | 0. | 630.0439 |
| 6 | 0. | TERR_A--SIMM | | 0. | 0. | 810.1688 |
| 6 | 0.5 | TERR_A--SIMM | | 0. | 0. | 890.4701 |
| 6 | 1. | TERR_A--SIMM | | 0. | 0. | 970.7714 |
| 6 | 0. | INERZIA H SLV | | 0. | 0. | 9.0801 |
| 6 | 0.5 | INERZIA H SLV | | 0. | 0. | 8.5236 |
| 6 | 1. | INERZIA H SLV | | 0. | 0. | 7.9671 |
| 6 | 0. | INERZIA V + SLV | | 0. | 0. | 1.2084 |
| 6 | 0.5 | INERZIA V + SLV | | 0. | 0. | 1.6964 |
| 6 | 1. | INERZIA V + SLV | | 0. | 0. | 2.1845 |
| 6 | 0. | INERZIA V - SLV | | 0. | 0. | -1.2084 |
| 6 | 0.5 | INERZIA V - SLV | | 0. | 0. | -1.6964 |
| 6 | 1. | INERZIA V - SLV | | 0. | 0. | -2.1845 |
| 6 | 0. | SISMA WOOD SLV | | 0. | 0. | 295.8037 |
| 6 | 0.5 | SISMA WOOD SLV | | 0. | 0. | 228.6361 |
| 6 | 1. | SISMA WOOD SLV | | 0. | 0. | 178.9036 |
| 6 | 0. | iDROSTATICA | | 0. | 0. | 507.5975 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 6 | 0.5 | iDROSTATICA | | 0. | 0. | 404.9743 |
| 6 | 1. | iDROSTATICA | | 0. | 0. | 326.501 |
| 6 | 0. | SISMA WOOD SLD | | 0. | 0. | 130.6388 |
| 6 | 0.5 | SISMA WOOD SLD | | 0. | 0. | 100.9749 |
| 6 | 1. | SISMA WOOD SLD | | 0. | 0. | 79.011 |
| 6 | 0. | INERZIA H SLD | | 0. | 0. | 4.0101 |
| 6 | 0.5 | INERZIA H SLD | | 0. | 0. | 3.7644 |
| 6 | 1. | INERZIA H SLD | | 0. | 0. | 3.5186 |
| 6 | 0. | INERZIA V + SLD | | 0. | 0. | 0.5337 |
| 6 | 0.5 | INERZIA V + SLD | | 0. | 0. | 0.7492 |
| 6 | 1. | INERZIA V + SLD | | 0. | 0. | 0.9648 |
| 6 | 0. | INERZIA V SLD | | 0. | 0. | -0.5337 |
| 6 | 0.5 | INERZIA V SLD | | 0. | 0. | -0.7492 |
| 6 | 1. | INERZIA V SLD | | 0. | 0. | -0.9648 |
| 6 | 0. | INERZIA V -1 | | 0. | 0. | -1.2084 |
| 6 | 0.5 | INERZIA V -1 | | 0. | 0. | -1.6964 |
| 6 | 1. | INERZIA V -1 | | 0. | 0. | -2.1845 |
| 6 | 0. | SLU_1 | Max | 0. | 0. | 1588.7457 |
| 6 | 0.5 | SLU_1 | Max | 0. | 0. | 1529.7691 |
| 6 | 1. | SLU_1 | Max | 0. | 0. | 1524.2777 |
| 6 | 0. | SLU_1 | Min | 0. | 0. | 1588.7457 |
| 6 | 0.5 | SLU_1 | Min | 0. | 0. | 1529.7691 |
| 6 | 1. | SLU_1 | Min | 0. | 0. | 1524.2777 |
| 6 | 0. | SLU_2 | Max | 0. | 0. | 1700.4262 |
| 6 | 0.5 | SLU_2 | Max | 0. | 0. | 1672.1201 |
| 6 | 1. | SLU_2 | Max | 0. | 0. | 1689.9364 |
| 6 | 0. | SLU_2 | Min | 0. | 0. | 1700.4262 |
| 6 | 0.5 | SLU_2 | Min | 0. | 0. | 1672.1201 |
| 6 | 1. | SLU_2 | Min | 0. | 0. | 1689.9364 |
| 6 | 0. | SLU_3 | Max | 0. | 0. | 2223.2467 |
| 6 | 0.5 | SLU_3 | Max | 0. | 0. | 2122.2492 |
| 6 | 1. | SLU_3 | Max | 0. | 0. | 2089.0141 |
| 6 | 0. | SLU_3 | Min | 0. | 0. | 2223.2467 |
| 6 | 0.5 | SLU_3 | Min | 0. | 0. | 2122.2492 |
| 6 | 1. | SLU_3 | Min | 0. | 0. | 2089.0141 |
| 6 | 0. | SLU_4 | Max | 0. | 0. | 2272.8165 |
| 6 | 0.5 | SLU_4 | Max | 0. | 0. | 2230.0193 |
| 6 | 1. | SLU_4 | Max | 0. | 0. | 2242.2122 |
| 6 | 0. | SLU_4 | Min | 0. | 0. | 2272.8165 |
| 6 | 0.5 | SLU_4 | Min | 0. | 0. | 2230.0193 |
| 6 | 1. | SLU_4 | Min | 0. | 0. | 2242.2122 |
| 6 | 0. | SLE_F1 | Max | 0. | 0. | 1169.3721 |
| 6 | 0.5 | SLE_F1 | Max | 0. | 0. | 1117.7791 |
| 6 | 1. | SLE_F1 | Max | 0. | 0. | 1107.3287 |
| 6 | 0. | SLE_F1 | Min | 0. | 0. | 1169.3721 |
| 6 | 0.5 | SLE_F1 | Min | 0. | 0. | 1117.7791 |
| 6 | 1. | SLE_F1 | Min | 0. | 0. | 1107.3287 |
| 6 | 0. | SLE_F2 | Max | 0. | 0. | 1255.9327 |
| 6 | 0.5 | SLE_F2 | Max | 0. | 0. | 1226.4201 |
| 6 | 1. | SLE_F2 | Max | 0. | 0. | 1232.3862 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 6 | 0. | SLE_F2 | Min | 0. | 0. | 1255.9327 |
| 6 | 0.5 | SLE_F2 | Min | 0. | 0. | 1226.4201 |
| 6 | 1. | SLE_F2 | Min | 0. | 0. | 1232.3862 |
| 6 | 0. | SLE_F3 | Max | 0. | 0. | 1692.8626 |
| 6 | 0.5 | SLE_F3 | Max | 0. | 0. | 1652.5018 |
| 6 | 1. | SLE_F3 | Max | 0. | 0. | 1654.441 |
| 6 | 0. | SLE_F3 | Min | 0. | 0. | 1692.8626 |
| 6 | 0.5 | SLE_F3 | Min | 0. | 0. | 1652.5018 |
| 6 | 1. | SLE_F3 | Min | 0. | 0. | 1654.441 |
| 6 | 0. | SLE_F4 | Max | 0. | 0. | 1643.105 |
| 6 | 0.5 | SLE_F4 | Max | 0. | 0. | 1558.4504 |
| 6 | 1. | SLE_F4 | Max | 0. | 0. | 1525.9207 |
| 6 | 0. | SLE_F4 | Min | 0. | 0. | 1643.105 |
| 6 | 0.5 | SLE_F4 | Min | 0. | 0. | 1558.4504 |
| 6 | 1. | SLE_F4 | Min | 0. | 0. | 1525.9207 |
| 6 | 0. | SLE_QP1 | Max | 0. | 0. | 1074.4448 |
| 6 | 0.5 | SLE_QP1 | Max | 0. | 0. | 1010.7995 |
| 6 | 1. | SLE_QP1 | Max | 0. | 0. | 988.2968 |
| 6 | 0. | SLE_QP1 | Min | 0. | 0. | 1074.4448 |
| 6 | 0.5 | SLE_QP1 | Min | 0. | 0. | 1010.7995 |
| 6 | 1. | SLE_QP1 | Min | 0. | 0. | 988.2968 |
| 6 | 0. | SLE_QP2 | Max | 0. | 0. | 1159.1922 |
| 6 | 0.5 | SLE_QP2 | Max | 0. | 0. | 1115.3076 |
| 6 | 1. | SLE_QP2 | Max | 0. | 0. | 1106.9018 |
| 6 | 0. | SLE_QP2 | Min | 0. | 0. | 1159.1922 |
| 6 | 0.5 | SLE_QP2 | Min | 0. | 0. | 1115.3076 |
| 6 | 1. | SLE_QP2 | Min | 0. | 0. | 1106.9018 |
| 6 | 0. | SLE_QP3 | Max | 0. | 0. | 1589.8674 |
| 6 | 0.5 | SLE_QP3 | Max | 0. | 0. | 1535.6898 |
| 6 | 1. | SLE_QP3 | Max | 0. | 0. | 1523.8122 |
| 6 | 0. | SLE_QP3 | Min | 0. | 0. | 1589.8674 |
| 6 | 0.5 | SLE_QP3 | Min | 0. | 0. | 1535.6898 |
| 6 | 1. | SLE_QP3 | Min | 0. | 0. | 1523.8122 |
| 6 | 0. | SLE_QP4 | Max | 0. | 0. | 1515.5975 |
| 6 | 0.5 | SLE_QP4 | Max | 0. | 0. | 1418.3299 |
| 6 | 1. | SLE_QP4 | Max | 0. | 0. | 1373.1873 |
| 6 | 0. | SLE_QP4 | Min | 0. | 0. | 1515.5975 |
| 6 | 0.5 | SLE_QP4 | Min | 0. | 0. | 1418.3299 |
| 6 | 1. | SLE_QP4 | Min | 0. | 0. | 1373.1873 |
| 6 | 0. | SLV_1 | Max | 0. | 0. | 932.2367 |
| 6 | 0.5 | SLV_1 | Max | 0. | 0. | 727.4611 |
| 6 | 1. | SLV_1 | Max | 0. | 0. | 581.263 |
| 6 | 0. | SLV_1 | Min | 0. | 0. | 932.2367 |
| 6 | 0.5 | SLV_1 | Min | 0. | 0. | 727.4611 |
| 6 | 1. | SLV_1 | Min | 0. | 0. | 581.263 |
| 6 | 0. | SLV_2 | Max | 0. | 0. | 927.8198 |
| 6 | 0.5 | SLV_2 | Max | 0. | 0. | 722.0079 |
| 6 | 1. | SLV_2 | Max | 0. | 0. | 574.7734 |
| 6 | 0. | SLV_2 | Min | 0. | 0. | 927.8198 |
| 6 | 0.5 | SLV_2 | Min | 0. | 0. | 722.0079 |
| 6 | 1. | SLV_2 | Min | 0. | 0. | 574.7734 |
| 6 | 0. | SLV_3 | Max | 0. | 0. | 1233.9905 |
| 6 | 0.5 | SLV_3 | Max | 0. | 0. | 989.5188 |
| 6 | 1. | SLV_3 | Max | 0. | 0. | 814.6071 |
| 6 | 0. | SLV_3 | Min | 0. | 0. | 1233.9905 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 6 | 0.5 | SLV_3 | Min | 0. | 0. | 989.5188 |
| 6 | 1. | SLV_3 | Min | 0. | 0. | 814.6071 |
| 6 | 0. | SLV_4 | Max | 0. | 0. | 1228.4939 |
| 6 | 0.5 | SLV_4 | Max | 0. | 0. | 982.9735 |
| 6 | 1. | SLV_4 | Max | 0. | 0. | 807.0131 |
| 6 | 0. | SLV_4 | Min | 0. | 0. | 1228.4939 |
| 6 | 0.5 | SLV_4 | Min | 0. | 0. | 982.9735 |
| 6 | 1. | SLV_4 | Min | 0. | 0. | 807.0131 |
| 6 | 0. | SLD_1 | Max | 0. | 0. | 1094.7045 |
| 6 | 0.5 | SLD_1 | Max | 0. | 0. | 969.8111 |
| 6 | 1. | SLD_1 | Max | 0. | 0. | 893.7602 |
| 6 | 0. | SLD_1 | Min | 0. | 0. | 1094.7045 |
| 6 | 0.5 | SLD_1 | Min | 0. | 0. | 969.8111 |
| 6 | 1. | SLD_1 | Min | 0. | 0. | 893.7602 |
| 6 | 0. | SLD_2 | Max | 0. | 0. | 1093.7842 |
| 6 | 0.5 | SLD_2 | Max | 0. | 0. | 968.2402 |
| 6 | 1. | SLD_2 | Max | 0. | 0. | 891.5387 |
| 6 | 0. | SLD_2 | Min | 0. | 0. | 1093.7842 |
| 6 | 0.5 | SLD_2 | Min | 0. | 0. | 968.2402 |
| 6 | 1. | SLD_2 | Min | 0. | 0. | 891.5387 |
| 6 | 0. | SLD_3 | Max | 0. | 0. | 1376.3095 |
| 6 | 0.5 | SLD_3 | Max | 0. | 0. | 1211.6442 |
| 6 | 1. | SLD_3 | Max | 0. | 0. | 1106.8039 |
| 6 | 0. | SLD_3 | Min | 0. | 0. | 1376.3095 |
| 6 | 0.5 | SLD_3 | Min | 0. | 0. | 1211.6442 |
| 6 | 1. | SLD_3 | Min | 0. | 0. | 1106.8039 |
| 6 | 0. | SLD_4 | Max | 0. | 0. | 1374.0708 |
| 6 | 0.5 | SLD_4 | Max | 0. | 0. | 1208.8945 |
| 6 | 1. | SLD_4 | Max | 0. | 0. | 1103.5432 |
| 6 | 0. | SLD_4 | Min | 0. | 0. | 1374.0708 |
| 6 | 0.5 | SLD_4 | Min | 0. | 0. | 1208.8945 |
| 6 | 1. | SLD_4 | Min | 0. | 0. | 1103.5432 |
| 6 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1599.3136 |
| 6 | 0.5 | SLU_IDR_1 | Max | 0. | 0. | 1521.3345 |
| 6 | 1. | SLU_IDR_1 | Max | 0. | 0. | 1486.2554 |
| 6 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1599.3136 |
| 6 | 0.5 | SLU_IDR_1 | Min | 0. | 0. | 1521.3345 |
| 6 | 1. | SLU_IDR_1 | Min | 0. | 0. | 1486.2554 |
| 6 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1230.4207 |
| 6 | 0.5 | SLU_IDR_2 | Max | 0. | 0. | 1159.4919 |
| 6 | 1. | SLU_IDR_2 | Max | 0. | 0. | 1125.324 |
| 6 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1230.4207 |
| 6 | 0.5 | SLU_IDR_2 | Min | 0. | 0. | 1159.4919 |
| 6 | 1. | SLU_IDR_2 | Min | 0. | 0. | 1125.324 |
| 6 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -422.9025 |
| 6 | 0.5 | SISMA WOOD SLV-1 | Max | 0. | 0. | -514.6582 |
| 6 | 1. | SISMA WOOD SLV-1 | Max | 0. | 0. | -588.979 |
| 6 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -422.9025 |
| 6 | 0.5 | SISMA WOOD SLV-1 | Min | 0. | 0. | -514.6582 |
| 6 | 1. | SISMA WOOD SLV-1 | Min | 0. | 0. | -588.979 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 6 | 0. | DEAD-1 | Max | 0. | 0. | 116.34 |
| 6 | 0.5 | DEAD-1 | Max | 0. | 0. | 154.7691 |
| 6 | 1. | DEAD-1 | Max | 0. | 0. | 193.1982 |
| 6 | 0. | DEAD-1 | Min | 0. | 0. | 116.34 |
| 6 | 0.5 | DEAD-1 | Min | 0. | 0. | 154.7691 |
| 6 | 1. | DEAD-1 | Min | 0. | 0. | 193.1982 |
| 6 | 0. | SLU_PROVA | | 0. | 0. | 1396.223 |
| 6 | 0.5 | SLU_PROVA | | 0. | 0. | 1318.0253 |
| 6 | 1. | SLU_PROVA | | 0. | 0. | 1293.3128 |
| 7 | 0. | DEAD | | 0. | 0. | 135.5447 |
| 7 | 0.28595 | DEAD | | 0. | 0. | 155.5338 |
| 7 | 0.5719 | DEAD | | 0. | 0. | 175.5228 |
| 7 | 0. | SIMM_KA | | 0. | 0. | -180.1856 |
| 7 | 0.28595 | SIMM_KA | | 0. | 0. | -195.3073 |
| 7 | 0.5719 | SIMM_KA | | 0. | 0. | -207.1402 |
| 7 | 0. | SIMM_K0 | | 0. | 0. | -270.2655 |
| 7 | 0.28595 | SIMM_K0 | | 0. | 0. | -293.6847 |
| 7 | 0.5719 | SIMM_K0 | | 0. | 0. | -312.1713 |
| 7 | 0. | A--SIMM_KA | | 0. | 0. | -187.5207 |
| 7 | 0.28595 | A--SIMM_KA | | 0. | 0. | -222.3474 |
| 7 | 0.5719 | A--SIMM_KA | | 0. | 0. | -251.5702 |
| 7 | 0. | A--SIMM_K0 | | 0. | 0. | -289.7859 |
| 7 | 0.28595 | A--SIMM_K0 | | 0. | 0. | -341.6627 |
| 7 | 0.5719 | A--SIMM_K0 | | 0. | 0. | -385.1375 |
| 7 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -10.6553 |
| 7 | 0.28595 | A-- SIMM_SOVR_K A | | 0. | 0. | -14.6654 |
| 7 | 0.5719 | A-- SIMM_SOVR_K A | | 0. | 0. | -18.6755 |
| 7 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -15.975 |
| 7 | 0.28595 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -21.9871 |
| 7 | 0.5719 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -27.9993 |
| 7 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -15.975 |
| 7 | 0.28595 | SIMM_SOVR_K 0 | | 0. | 0. | -21.9871 |
| 7 | 0.5719 | SIMM_SOVR_K 0 | | 0. | 0. | -27.9993 |
| 7 | 0. | SIMM_SOVR_K A | | 0. | 0. | -10.6553 |
| 7 | 0.28595 | SIMM_SOVR_K A | | 0. | 0. | -14.6654 |
| 7 | 0.5719 | SIMM_SOVR_K A | | 0. | 0. | -18.6755 |
| 7 | 0. | SOVR | | 0. | 0. | 165.9359 |
| 7 | 0.28595 | SOVR | | 0. | 0. | 179.5639 |
| 7 | 0.5719 | SOVR | | 0. | 0. | 193.1919 |
| 7 | 0. | TERR_SIMM | | 0. | 0. | 630.0439 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 7 | 0.28595 | TERR_SIMM | | 0. | 0. | 673.6494 |
| 7 | 0.5719 | TERR_SIMM | | 0. | 0. | 717.2549 |
| 7 | 0. | TERR_A--SIMM | | 0. | 0. | 970.7714 |
| 7 | 0.28595 | TERR_A--SIMM | | 0. | 0. | 1031.1594 |
| 7 | 0.5719 | TERR_A--SIMM | | 0. | 0. | 1091.5473 |
| 7 | 0. | INERZIA H SLV | | 0. | 0. | 7.9671 |
| 7 | 0.28595 | INERZIA H SLV | | 0. | 0. | 6.6418 |
| 7 | 0.5719 | INERZIA H SLV | | 0. | 0. | 5.3166 |
| 7 | 0. | INERZIA V + SLV | | 0. | 0. | 2.1845 |
| 7 | 0.28595 | INERZIA V + SLV | | 0. | 0. | 2.5018 |
| 7 | 0.5719 | INERZIA V + SLV | | 0. | 0. | 2.8191 |
| 7 | 0. | INERZIA V - SLV | | 0. | 0. | -2.1845 |
| 7 | 0.28595 | INERZIA V - SLV | | 0. | 0. | -2.5018 |
| 7 | 0.5719 | INERZIA V - SLV | | 0. | 0. | -2.8191 |
| 7 | 0. | SISMA WOOD SLV | | 0. | 0. | 178.9036 |
| 7 | 0.28595 | SISMA WOOD SLV | | 0. | 0. | 106.3878 |
| 7 | 0.5719 | SISMA WOOD SLV | | 0. | 0. | 39.5745 |
| 7 | 0. | iDROSTATICA | | 0. | 0. | 326.501 |
| 7 | 0.28595 | iDROSTATICA | | 0. | 0. | 295.2741 |
| 7 | 0.5719 | iDROSTATICA | | 0. | 0. | 270.5461 |
| 7 | 0. | SISMA WOOD SLD | | 0. | 0. | 79.011 |
| 7 | 0.28595 | SISMA WOOD SLD | | 0. | 0. | 46.9852 |
| 7 | 0.5719 | SISMA WOOD SLD | | 0. | 0. | 17.4777 |
| 7 | 0. | INERZIA H SLD | | 0. | 0. | 3.5186 |
| 7 | 0.28595 | INERZIA H SLD | | 0. | 0. | 2.9333 |
| 7 | 0.5719 | INERZIA H SLD | | 0. | 0. | 2.348 |
| 7 | 0. | INERZIA V + SLD | | 0. | 0. | 0.9648 |
| 7 | 0.28595 | INERZIA V + SLD | | 0. | 0. | 1.1049 |
| 7 | 0.5719 | INERZIA V + SLD | | 0. | 0. | 1.245 |
| 7 | 0. | INERZIA V SLD | | 0. | 0. | -0.9648 |
| 7 | 0.28595 | INERZIA V SLD | | 0. | 0. | -1.1049 |
| 7 | 0.5719 | INERZIA V SLD | | 0. | 0. | -1.245 |
| 7 | 0. | INERZIA V -1 | | 0. | 0. | -2.1845 |
| 7 | 0.28595 | INERZIA V -1 | | 0. | 0. | -2.5018 |
| 7 | 0.5719 | INERZIA V -1 | | 0. | 0. | -2.8191 |
| 7 | 0. | SLU_1 | Max | 0. | 0. | 1524.2777 |
| 7 | 0.28595 | SLU_1 | Max | 0. | 0. | 1563.5164 |
| 7 | 0.5719 | SLU_1 | Max | 0. | 0. | 1617.6161 |
| 7 | 0. | SLU_1 | Min | 0. | 0. | 1524.2777 |
| 7 | 0.28595 | SLU_1 | Min | 0. | 0. | 1563.5164 |
| 7 | 0.5719 | SLU_1 | Min | 0. | 0. | 1617.6161 |
| 7 | 0. | SLU_2 | Max | 0. | 0. | 1689.9364 |
| 7 | 0.28595 | SLU_2 | Max | 0. | 0. | 1744.4163 |
| 7 | 0.5719 | SLU_2 | Max | 0. | 0. | 1811.6199 |
| 7 | 0. | SLU_2 | Min | 0. | 0. | 1689.9364 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 7 | 0.28595 | SLU_2 | Min | 0. | 0. | 1744.4163 |
| 7 | 0.5719 | SLU_2 | Min | 0. | 0. | 1811.6199 |
| 7 | 0. | SLU_3 | Max | 0. | 0. | 2089.0141 |
| 7 | 0.28595 | SLU_3 | Max | 0. | 0. | 2098.4513 |
| 7 | 0.5719 | SLU_3 | Max | 0. | 0. | 2127.2595 |
| 7 | 0. | SLU_3 | Min | 0. | 0. | 2089.0141 |
| 7 | 0.28595 | SLU_3 | Min | 0. | 0. | 2098.4513 |
| 7 | 0.5719 | SLU_3 | Min | 0. | 0. | 2127.2595 |
| 7 | 0. | SLU_4 | Max | 0. | 0. | 2242.2122 |
| 7 | 0.28595 | SLU_4 | Max | 0. | 0. | 2284.5631 |
| 7 | 0.5719 | SLU_4 | Max | 0. | 0. | 2342.6476 |
| 7 | 0. | SLU_4 | Min | 0. | 0. | 2242.2122 |
| 7 | 0.28595 | SLU_4 | Min | 0. | 0. | 2284.5631 |
| 7 | 0.5719 | SLU_4 | Min | 0. | 0. | 2342.6476 |
| 7 | 0. | SLE_F1 | Max | 0. | 0. | 1107.3287 |
| 7 | 0.28595 | SLE_F1 | Max | 0. | 0. | 1132.9842 |
| 7 | 0.5719 | SLE_F1 | Max | 0. | 0. | 1170.0712 |
| 7 | 0. | SLE_F1 | Min | 0. | 0. | 1107.3287 |
| 7 | 0.28595 | SLE_F1 | Min | 0. | 0. | 1132.9842 |
| 7 | 0.5719 | SLE_F1 | Min | 0. | 0. | 1170.0712 |
| 7 | 0. | SLE_F2 | Max | 0. | 0. | 1232.3862 |
| 7 | 0.28595 | SLE_F2 | Max | 0. | 0. | 1268.7598 |
| 7 | 0.5719 | SLE_F2 | Max | 0. | 0. | 1314.9209 |
| 7 | 0. | SLE_F2 | Min | 0. | 0. | 1232.3862 |
| 7 | 0.28595 | SLE_F2 | Min | 0. | 0. | 1268.7598 |
| 7 | 0.5719 | SLE_F2 | Min | 0. | 0. | 1314.9209 |
| 7 | 0. | SLE_F3 | Max | 0. | 0. | 1654.441 |
| 7 | 0.28595 | SLE_F3 | Max | 0. | 0. | 1681.6527 |
| 7 | 0.5719 | SLE_F3 | Max | 0. | 0. | 1720.9672 |
| 7 | 0. | SLE_F3 | Min | 0. | 0. | 1654.441 |
| 7 | 0.28595 | SLE_F3 | Min | 0. | 0. | 1681.6527 |
| 7 | 0.5719 | SLE_F3 | Min | 0. | 0. | 1720.9672 |
| 7 | 0. | SLE_F4 | Max | 0. | 0. | 1525.9207 |
| 7 | 0.28595 | SLE_F4 | Max | 0. | 0. | 1529.1974 |
| 7 | 0.5719 | SLE_F4 | Max | 0. | 0. | 1547.375 |
| 7 | 0. | SLE_F4 | Min | 0. | 0. | 1525.9207 |
| 7 | 0.28595 | SLE_F4 | Min | 0. | 0. | 1529.1974 |
| 7 | 0.5719 | SLE_F4 | Min | 0. | 0. | 1547.375 |
| 7 | 0. | SLE_QP1 | Max | 0. | 0. | 988.2968 |
| 7 | 0.28595 | SLE_QP1 | Max | 0. | 0. | 1005.3346 |
| 7 | 0.5719 | SLE_QP1 | Max | 0. | 0. | 1033.8039 |
| 7 | 0. | SLE_QP1 | Min | 0. | 0. | 988.2968 |
| 7 | 0.28595 | SLE_QP1 | Min | 0. | 0. | 1005.3346 |
| 7 | 0.5719 | SLE_QP1 | Min | 0. | 0. | 1033.8039 |
| 7 | 0. | SLE_QP2 | Max | 0. | 0. | 1106.9018 |
| 7 | 0.28595 | SLE_QP2 | Max | 0. | 0. | 1132.9983 |
| 7 | 0.5719 | SLE_QP2 | Max | 0. | 0. | 1168.8823 |
| 7 | 0. | SLE_QP2 | Min | 0. | 0. | 1106.9018 |
| 7 | 0.28595 | SLE_QP2 | Min | 0. | 0. | 1132.9983 |
| 7 | 0.5719 | SLE_QP2 | Min | 0. | 0. | 1168.8823 |
| 7 | 0. | SLE_QP3 | Max | 0. | 0. | 1523.8122 |
| 7 | 0.28595 | SLE_QP3 | Max | 0. | 0. | 1541.0589 |
| 7 | 0.5719 | SLE_QP3 | Max | 0. | 0. | 1570.4084 |
| 7 | 0. | SLE_QP3 | Min | 0. | 0. | 1523.8122 |
| 7 | 0.28595 | SLE_QP3 | Min | 0. | 0. | 1541.0589 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 7 | 0.5719 | SLE_QP3 | Min | 0. | 0. | 1570.4084 |
| 7 | 0. | SLE_QP4 | Max | 0. | 0. | 1373.1873 |
| 7 | 0.28595 | SLE_QP4 | Max | 0. | 0. | 1369.2498 |
| 7 | 0.5719 | SLE_QP4 | Max | 0. | 0. | 1380.2132 |
| 7 | 0. | SLE_QP4 | Min | 0. | 0. | 1373.1873 |
| 7 | 0.28595 | SLE_QP4 | Min | 0. | 0. | 1369.2498 |
| 7 | 0.5719 | SLE_QP4 | Min | 0. | 0. | 1380.2132 |
| 7 | 0. | SLV_1 | Max | 0. | 0. | 581.263 |
| 7 | 0.28595 | SLV_1 | Max | 0. | 0. | 522.7555 |
| 7 | 0.5719 | SLV_1 | Max | 0. | 0. | 481.382 |
| 7 | 0. | SLV_1 | Min | 0. | 0. | 581.263 |
| 7 | 0.28595 | SLV_1 | Min | 0. | 0. | 522.7555 |
| 7 | 0.5719 | SLV_1 | Min | 0. | 0. | 481.382 |
| 7 | 0. | SLV_2 | Max | 0. | 0. | 574.7734 |
| 7 | 0.28595 | SLV_2 | Max | 0. | 0. | 515.6733 |
| 7 | 0.5719 | SLV_2 | Max | 0. | 0. | 473.7071 |
| 7 | 0. | SLV_2 | Min | 0. | 0. | 574.7734 |
| 7 | 0.28595 | SLV_2 | Min | 0. | 0. | 515.6733 |
| 7 | 0.5719 | SLV_2 | Min | 0. | 0. | 473.7071 |
| 7 | 0. | SLV_3 | Max | 0. | 0. | 814.6071 |
| 7 | 0.28595 | SLV_3 | Max | 0. | 0. | 744.5462 |
| 7 | 0.5719 | SLV_3 | Max | 0. | 0. | 695.0886 |
| 7 | 0. | SLV_3 | Min | 0. | 0. | 814.6071 |
| 7 | 0.28595 | SLV_3 | Min | 0. | 0. | 744.5462 |
| 7 | 0.5719 | SLV_3 | Min | 0. | 0. | 695.0886 |
| 7 | 0. | SLV_4 | Max | 0. | 0. | 807.0131 |
| 7 | 0.28595 | SLV_4 | Max | 0. | 0. | 736.3524 |
| 7 | 0.5719 | SLV_4 | Max | 0. | 0. | 686.295 |
| 7 | 0. | SLV_4 | Min | 0. | 0. | 807.0131 |
| 7 | 0.28595 | SLV_4 | Min | 0. | 0. | 736.3524 |
| 7 | 0.5719 | SLV_4 | Min | 0. | 0. | 686.295 |
| 7 | 0. | SLD_1 | Max | 0. | 0. | 893.7602 |
| 7 | 0.28595 | SLD_1 | Max | 0. | 0. | 870.8491 |
| 7 | 0.5719 | SLD_1 | Max | 0. | 0. | 861.8878 |
| 7 | 0. | SLD_1 | Min | 0. | 0. | 893.7602 |
| 7 | 0.28595 | SLD_1 | Min | 0. | 0. | 870.8491 |
| 7 | 0.5719 | SLD_1 | Min | 0. | 0. | 861.8878 |
| 7 | 0. | SLD_2 | Max | 0. | 0. | 891.5387 |
| 7 | 0.28595 | SLD_2 | Max | 0. | 0. | 868.2555 |
| 7 | 0.5719 | SLD_2 | Max | 0. | 0. | 858.9221 |
| 7 | 0. | SLD_2 | Min | 0. | 0. | 891.5387 |
| 7 | 0.28595 | SLD_2 | Min | 0. | 0. | 868.2555 |
| 7 | 0.5719 | SLD_2 | Min | 0. | 0. | 858.9221 |
| 7 | 0. | SLD_3 | Max | 0. | 0. | 1106.8039 |
| 7 | 0.28595 | SLD_3 | Max | 0. | 0. | 1072.2922 |
| 7 | 0.5719 | SLD_3 | Max | 0. | 0. | 1055.1998 |
| 7 | 0. | SLD_3 | Min | 0. | 0. | 1106.8039 |
| 7 | 0.28595 | SLD_3 | Min | 0. | 0. | 1072.2922 |
| 7 | 0.5719 | SLD_3 | Min | 0. | 0. | 1055.1998 |
| 7 | 0. | SLD_4 | Max | 0. | 0. | 1103.5432 |
| 7 | 0.28595 | SLD_4 | Max | 0. | 0. | 1068.7392 |
| 7 | 0.5719 | SLD_4 | Max | 0. | 0. | 1051.3546 |
| 7 | 0. | SLD_4 | Min | 0. | 0. | 1103.5432 |
| 7 | 0.28595 | SLD_4 | Min | 0. | 0. | 1068.7392 |
| 7 | 0.5719 | SLD_4 | Min | 0. | 0. | 1051.3546 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 7 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1486.2554 |
| 7 | 0.28595 | SLU_IDR_1 | Max | 0. | 0. | 1491.9576 |
| 7 | 0.5719 | SLU_IDR_1 | Max | 0. | 0. | 1509.8521 |
| 7 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1486.2554 |
| 7 | 0.28595 | SLU_IDR_1 | Min | 0. | 0. | 1491.9576 |
| 7 | 0.5719 | SLU_IDR_1 | Min | 0. | 0. | 1509.8521 |
| 7 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1125.324 |
| 7 | 0.28595 | SLU_IDR_2 | Max | 0. | 0. | 1137.6641 |
| 7 | 0.5719 | SLU_IDR_2 | Max | 0. | 0. | 1160.1127 |
| 7 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1125.324 |
| 7 | 0.28595 | SLU_IDR_2 | Min | 0. | 0. | 1137.6641 |
| 7 | 0.5719 | SLU_IDR_2 | Min | 0. | 0. | 1160.1127 |
| 7 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -588.979 |
| 7 | 0.28595 | SISMA WOOD SLV-1 | Max | 0. | 0. | -623.6463 |
| 7 | 0.5719 | SISMA WOOD SLV-1 | Max | 0. | 0. | -652.6112 |
| 7 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -588.979 |
| 7 | 0.28595 | SISMA WOOD SLV-1 | Min | 0. | 0. | -623.6463 |
| 7 | 0.5719 | SISMA WOOD SLV-1 | Min | 0. | 0. | -652.6112 |
| 7 | 0. | DEAD-1 | Max | 0. | 0. | 193.1982 |
| 7 | 0.28595 | DEAD-1 | Max | 0. | 0. | 218.7598 |
| 7 | 0.5719 | DEAD-1 | Max | 0. | 0. | 244.3213 |
| 7 | 0. | DEAD-1 | Min | 0. | 0. | 193.1982 |
| 7 | 0.28595 | DEAD-1 | Min | 0. | 0. | 218.7598 |
| 7 | 0.5719 | DEAD-1 | Min | 0. | 0. | 244.3213 |
| 7 | 0. | SLU_PROVA | | 0. | 0. | 1293.3128 |
| 7 | 0.28595 | SLU_PROVA | | 0. | 0. | 1316.3695 |
| 7 | 0.5719 | SLU_PROVA | | 0. | 0. | 1354.2871 |
| 8 | 0. | DEAD | | 0. | 0. | -175.5228 |
| 8 | 0.75656 | DEAD | | 0. | 0. | -155.5658 |
| 8 | 1.51312 | DEAD | | 0. | 0. | -144.221 |
| 8 | 0. | SIMM_KA | | 0. | 0. | 207.1402 |
| 8 | 0.75656 | SIMM_KA | | 0. | 0. | 232.169 |
| 8 | 1.51312 | SIMM_KA | | 0. | 0. | 237.8946 |
| 8 | 0. | SIMM_K0 | | 0. | 0. | 312.1713 |
| 8 | 0.75656 | SIMM_K0 | | 0. | 0. | 351.8301 |
| 8 | 1.51312 | SIMM_K0 | | 0. | 0. | 362.5341 |
| 8 | 0. | A--SIMM_KA | | 0. | 0. | 251.5702 |
| 8 | 0.75656 | A--SIMM_KA | | 0. | 0. | 311.0305 |
| 8 | 1.51312 | A--SIMM_KA | | 0. | 0. | 337.9159 |
| 8 | 0. | A--SIMM_K0 | | 0. | 0. | 385.1375 |
| 8 | 0.75656 | A--SIMM_K0 | | 0. | 0. | 473.4375 |
| 8 | 1.51312 | A--SIMM_K0 | | 0. | 0. | 512.8766 |
| 8 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 18.6755 |
| 8 | 0.75656 | A-- SIMM_SOVR_K A | | 0. | 0. | 28.0554 |
| 8 | 1.51312 | A-- SIMM_SOVR_K A | | 0. | 0. | 33.9385 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 8 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 27.9993 |
| 8 | 0.75656 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 42.0621 |
| 8 | 1.51312 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 50.8824 |
| 8 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 27.9993 |
| 8 | 0.75656 | SIMM_SOVR_K 0 | | 0. | 0. | 42.0621 |
| 8 | 1.51312 | SIMM_SOVR_K 0 | | 0. | 0. | 50.8824 |
| 8 | 0. | SIMM_SOVR_K A | | 0. | 0. | 18.6755 |
| 8 | 0.75656 | SIMM_SOVR_K A | | 0. | 0. | 28.0554 |
| 8 | 1.51312 | SIMM_SOVR_K A | | 0. | 0. | 33.9385 |
| 8 | 0. | SOVR | | 0. | 0. | -193.1919 |
| 8 | 0.75656 | SOVR | | 0. | 0. | -172.3448 |
| 8 | 1.51312 | SOVR | | 0. | 0. | -156.0924 |
| 8 | 0. | TERR_SIMM | | 0. | 0. | -717.2549 |
| 8 | 0.75656 | TERR_SIMM | | 0. | 0. | -608.9942 |
| 8 | 1.51312 | TERR_SIMM | | 0. | 0. | -526.1083 |
| 8 | 0. | TERR_A--SIMM | | 0. | 0. | -1091.5473 |
| 8 | 0.75656 | TERR_A--SIMM | | 0. | 0. | -897.6713 |
| 8 | 1.51312 | TERR_A--SIMM | | 0. | 0. | -749.6274 |
| 8 | 0. | INERZIA H SLV | | 0. | 0. | -5.3166 |
| 8 | 0.75656 | INERZIA H SLV | | 0. | 0. | -2.966 |
| 8 | 1.51312 | INERZIA H SLV | | 0. | 0. | -0.6153 |
| 8 | 0. | INERZIA V + SLV | | 0. | 0. | -2.8191 |
| 8 | 0.75656 | INERZIA V + SLV | | 0. | 0. | -2.5523 |
| 8 | 1.51312 | INERZIA V + SLV | | 0. | 0. | -2.2855 |
| 8 | 0. | INERZIA V - SLV | | 0. | 0. | 2.8191 |
| 8 | 0.75656 | INERZIA V - SLV | | 0. | 0. | 2.5523 |
| 8 | 1.51312 | INERZIA V - SLV | | 0. | 0. | 2.2855 |
| 8 | 0. | SISMA WOOD SLV | | 0. | 0. | -39.5745 |
| 8 | 0.75656 | SISMA WOOD SLV | | 0. | 0. | 101.796 |
| 8 | 1.51312 | SISMA WOOD SLV | | 0. | 0. | 206.6049 |
| 8 | 0. | iDROSTATICA | | 0. | 0. | -270.5461 |
| 8 | 0.75656 | iDROSTATICA | | 0. | 0. | -134.1022 |
| 8 | 1.51312 | iDROSTATICA | | 0. | 0. | -39.1905 |
| 8 | 0. | SISMA WOOD SLD | | 0. | 0. | -17.4777 |
| 8 | 0.75656 | SISMA WOOD SLD | | 0. | 0. | 44.9572 |
| 8 | 1.51312 | SISMA WOOD SLD | | 0. | 0. | 91.245 |
| 8 | 0. | INERZIA H SLD | | 0. | 0. | -2.348 |
| 8 | 0.75656 | INERZIA H SLD | | 0. | 0. | -1.3099 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 8 | 1.51312 | INERZIA H SLD | | 0. | 0. | -0.2718 |
| 8 | 0. | INERZIA V + SLD | | 0. | 0. | -1.245 |
| 8 | 0.75656 | INERZIA V + SLD | | 0. | 0. | -1.1272 |
| 8 | 1.51312 | INERZIA V + SLD | | 0. | 0. | -1.0094 |
| 8 | 0. | INERZIA V SLD | | 0. | 0. | 1.245 |
| 8 | 0.75656 | INERZIA V SLD | | 0. | 0. | 1.1272 |
| 8 | 1.51312 | INERZIA V SLD | | 0. | 0. | 1.0094 |
| 8 | 0. | INERZIA V -1 | | 0. | 0. | 2.8191 |
| 8 | 0.75656 | INERZIA V -1 | | 0. | 0. | 2.5523 |
| 8 | 1.51312 | INERZIA V -1 | | 0. | 0. | 2.2855 |
| 8 | 0. | SLU_1 | Max | 0. | 0. | -1617.6161 |
| 8 | 0.75656 | SLU_1 | Max | 0. | 0. | -1152.2256 |
| 8 | 1.51312 | SLU_1 | Max | 0. | 0. | -837.4071 |
| 8 | 0. | SLU_1 | Min | 0. | 0. | -1617.6161 |
| 8 | 0.75656 | SLU_1 | Min | 0. | 0. | -1152.2256 |
| 8 | 1.51312 | SLU_1 | Min | 0. | 0. | -837.4071 |
| 8 | 0. | SLU_2 | Max | 0. | 0. | -1811.6199 |
| 8 | 0.75656 | SLU_2 | Max | 0. | 0. | -1373.3744 |
| 8 | 1.51312 | SLU_2 | Max | 0. | 0. | -1070.5351 |
| 8 | 0. | SLU_2 | Min | 0. | 0. | -1811.6199 |
| 8 | 0.75656 | SLU_2 | Min | 0. | 0. | -1373.3744 |
| 8 | 1.51312 | SLU_2 | Min | 0. | 0. | -1070.5351 |
| 8 | 0. | SLU_3 | Max | 0. | 0. | -2127.2595 |
| 8 | 0.75656 | SLU_3 | Max | 0. | 0. | -1432.5487 |
| 8 | 1.51312 | SLU_3 | Max | 0. | 0. | -940.8824 |
| 8 | 0. | SLU_3 | Min | 0. | 0. | -2127.2595 |
| 8 | 0.75656 | SLU_3 | Min | 0. | 0. | -1432.5487 |
| 8 | 1.51312 | SLU_3 | Min | 0. | 0. | -940.8824 |
| 8 | 0. | SLU_4 | Max | 0. | 0. | -2342.6476 |
| 8 | 0.75656 | SLU_4 | Max | 0. | 0. | -1707.6481 |
| 8 | 1.51312 | SLU_4 | Max | 0. | 0. | -1251.9025 |
| 8 | 0. | SLU_4 | Min | 0. | 0. | -2342.6476 |
| 8 | 0.75656 | SLU_4 | Min | 0. | 0. | -1707.6481 |
| 8 | 1.51312 | SLU_4 | Min | 0. | 0. | -1251.9025 |
| 8 | 0. | SLE_F1 | Max | 0. | 0. | -1170.0712 |
| 8 | 0.75656 | SLE_F1 | Max | 0. | 0. | -825.8539 |
| 8 | 1.51312 | SLE_F1 | Max | 0. | 0. | -593.4884 |
| 8 | 0. | SLE_F1 | Min | 0. | 0. | -1170.0712 |
| 8 | 0.75656 | SLE_F1 | Min | 0. | 0. | -825.8539 |
| 8 | 1.51312 | SLE_F1 | Min | 0. | 0. | -593.4884 |
| 8 | 0. | SLE_F2 | Max | 0. | 0. | -1314.9209 |
| 8 | 0.75656 | SLE_F2 | Max | 0. | 0. | -989.3955 |
| 8 | 1.51312 | SLE_F2 | Max | 0. | 0. | -764.761 |
| 8 | 0. | SLE_F2 | Min | 0. | 0. | -1314.9209 |
| 8 | 0.75656 | SLE_F2 | Min | 0. | 0. | -989.3955 |
| 8 | 1.51312 | SLE_F2 | Min | 0. | 0. | -764.761 |
| 8 | 0. | SLE_F3 | Max | 0. | 0. | -1720.9672 |
| 8 | 0.75656 | SLE_F3 | Max | 0. | 0. | -1244.4657 |
| 8 | 1.51312 | SLE_F3 | Max | 0. | 0. | -902.584 |
| 8 | 0. | SLE_F3 | Min | 0. | 0. | -1720.9672 |
| 8 | 0.75656 | SLE_F3 | Min | 0. | 0. | -1244.4657 |
| 8 | 1.51312 | SLE_F3 | Min | 0. | 0. | -902.584 |
| 8 | 0. | SLE_F4 | Max | 0. | 0. | -1547.375 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 8 | 0.75656 | SLE_F4 | Max | 0. | 0. | -1028.9379 |
| 8 | 1.51312 | SLE_F4 | Max | 0. | 0. | -662.7162 |
| 8 | 0. | SLE_F4 | Min | 0. | 0. | -1547.375 |
| 8 | 0.75656 | SLE_F4 | Min | 0. | 0. | -1028.9379 |
| 8 | 1.51312 | SLE_F4 | Min | 0. | 0. | -662.7162 |
| 8 | 0. | SLE_QP1 | Max | 0. | 0. | -1033.8039 |
| 8 | 0.75656 | SLE_QP1 | Max | 0. | 0. | -714.7973 |
| 8 | 1.51312 | SLE_QP1 | Max | 0. | 0. | -500.2646 |
| 8 | 0. | SLE_QP1 | Min | 0. | 0. | -1033.8039 |
| 8 | 0.75656 | SLE_QP1 | Min | 0. | 0. | -714.7973 |
| 8 | 1.51312 | SLE_QP1 | Min | 0. | 0. | -500.2646 |
| 8 | 0. | SLE_QP2 | Max | 0. | 0. | -1168.8823 |
| 8 | 0.75656 | SLE_QP2 | Max | 0. | 0. | -864.8757 |
| 8 | 1.51312 | SLE_QP2 | Max | 0. | 0. | -655.6914 |
| 8 | 0. | SLE_QP2 | Min | 0. | 0. | -1168.8823 |
| 8 | 0.75656 | SLE_QP2 | Min | 0. | 0. | -864.8757 |
| 8 | 1.51312 | SLE_QP2 | Min | 0. | 0. | -655.6914 |
| 8 | 0. | SLE_QP3 | Max | 0. | 0. | -1570.4084 |
| 8 | 0.75656 | SLE_QP3 | Max | 0. | 0. | -1116.1178 |
| 8 | 1.51312 | SLE_QP3 | Max | 0. | 0. | -790.3787 |
| 8 | 0. | SLE_QP3 | Min | 0. | 0. | -1570.4084 |
| 8 | 0.75656 | SLE_QP3 | Min | 0. | 0. | -1116.1178 |
| 8 | 1.51312 | SLE_QP3 | Min | 0. | 0. | -790.3787 |
| 8 | 0. | SLE_QP4 | Max | 0. | 0. | -1380.2132 |
| 8 | 0.75656 | SLE_QP4 | Max | 0. | 0. | -891.7971 |
| 8 | 1.51312 | SLE_QP4 | Max | 0. | 0. | -548.2184 |
| 8 | 0. | SLE_QP4 | Min | 0. | 0. | -1380.2132 |
| 8 | 0.75656 | SLE_QP4 | Min | 0. | 0. | -891.7971 |
| 8 | 1.51312 | SLE_QP4 | Min | 0. | 0. | -548.2184 |
| 8 | 0. | SLV_1 | Max | 0. | 0. | -481.382 |
| 8 | 0.75656 | SLV_1 | Max | 0. | 0. | -37.6662 |
| 8 | 1.51312 | SLV_1 | Max | 0. | 0. | 265.0139 |
| 8 | 0. | SLV_1 | Min | 0. | 0. | -481.382 |
| 8 | 0.75656 | SLV_1 | Min | 0. | 0. | -37.6662 |
| 8 | 1.51312 | SLV_1 | Min | 0. | 0. | 265.0139 |
| 8 | 0. | SLV_2 | Max | 0. | 0. | -473.7071 |
| 8 | 0.75656 | SLV_2 | Max | 0. | 0. | -31.0324 |
| 8 | 1.51312 | SLV_2 | Max | 0. | 0. | 270.6065 |
| 8 | 0. | SLV_2 | Min | 0. | 0. | -473.7071 |
| 8 | 0.75656 | SLV_2 | Min | 0. | 0. | -31.0324 |
| 8 | 1.51312 | SLV_2 | Min | 0. | 0. | 270.6065 |
| 8 | 0. | SLV_3 | Max | 0. | 0. | -695.0886 |
| 8 | 0.75656 | SLV_3 | Max | 0. | 0. | -110.809 |
| 8 | 1.51312 | SLV_3 | Max | 0. | 0. | 292.0713 |
| 8 | 0. | SLV_3 | Min | 0. | 0. | -695.0886 |
| 8 | 0.75656 | SLV_3 | Min | 0. | 0. | -110.809 |
| 8 | 1.51312 | SLV_3 | Min | 0. | 0. | 292.0713 |
| 8 | 0. | SLV_4 | Max | 0. | 0. | -686.295 |
| 8 | 0.75656 | SLV_4 | Max | 0. | 0. | -103.1182 |
| 8 | 1.51312 | SLV_4 | Max | 0. | 0. | 298.6593 |
| 8 | 0. | SLV_4 | Min | 0. | 0. | -686.295 |
| 8 | 0.75656 | SLV_4 | Min | 0. | 0. | -103.1182 |
| 8 | 1.51312 | SLV_4 | Min | 0. | 0. | 298.6593 |
| 8 | 0. | SLD_1 | Max | 0. | 0. | -861.8878 |
| 8 | 0.75656 | SLD_1 | Max | 0. | 0. | -469.7908 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 8 | 1.51312 | SLD_1 | Max | 0. | 0. | -198.3149 |
| 8 | 0. | SLD_1 | Min | 0. | 0. | -861.8878 |
| 8 | 0.75656 | SLD_1 | Min | 0. | 0. | -469.7908 |
| 8 | 1.51312 | SLD_1 | Min | 0. | 0. | -198.3149 |
| 8 | 0. | SLD_2 | Max | 0. | 0. | -858.9221 |
| 8 | 0.75656 | SLD_2 | Max | 0. | 0. | -467.104 |
| 8 | 1.51312 | SLD_2 | Max | 0. | 0. | -195.907 |
| 8 | 0. | SLD_2 | Min | 0. | 0. | -858.9221 |
| 8 | 0.75656 | SLD_2 | Min | 0. | 0. | -467.104 |
| 8 | 1.51312 | SLD_2 | Min | 0. | 0. | -195.907 |
| 8 | 0. | SLD_3 | Max | 0. | 0. | -1055.1998 |
| 8 | 0.75656 | SLD_3 | Max | 0. | 0. | -523.6253 |
| 8 | 1.51312 | SLD_3 | Max | 0. | 0. | -153.0355 |
| 8 | 0. | SLD_3 | Min | 0. | 0. | -1055.1998 |
| 8 | 0.75656 | SLD_3 | Min | 0. | 0. | -523.6253 |
| 8 | 1.51312 | SLD_3 | Min | 0. | 0. | -153.0355 |
| 8 | 0. | SLD_4 | Max | 0. | 0. | -1051.3546 |
| 8 | 0.75656 | SLD_4 | Max | 0. | 0. | -520.2245 |
| 8 | 1.51312 | SLD_4 | Max | 0. | 0. | -150.079 |
| 8 | 0. | SLD_4 | Min | 0. | 0. | -1051.3546 |
| 8 | 0.75656 | SLD_4 | Min | 0. | 0. | -520.2245 |
| 8 | 1.51312 | SLD_4 | Min | 0. | 0. | -150.079 |
| 8 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1509.8521 |
| 8 | 0.75656 | SLU_IDR_1 | Max | 0. | 0. | -1067.6954 |
| 8 | 1.51312 | SLU_IDR_1 | Max | 0. | 0. | -749.5413 |
| 8 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1509.8521 |
| 8 | 0.75656 | SLU_IDR_1 | Min | 0. | 0. | -1067.6954 |
| 8 | 1.51312 | SLU_IDR_1 | Min | 0. | 0. | -749.5413 |
| 8 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1160.1127 |
| 8 | 0.75656 | SLU_IDR_2 | Max | 0. | 0. | -850.7046 |
| 8 | 1.51312 | SLU_IDR_2 | Max | 0. | 0. | -634.943 |
| 8 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1160.1127 |
| 8 | 0.75656 | SLU_IDR_2 | Min | 0. | 0. | -850.7046 |
| 8 | 1.51312 | SLU_IDR_2 | Min | 0. | 0. | -634.943 |
| 8 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 652.6112 |
| 8 | 0.75656 | SISMA WOOD SLV-1 | Max | 0. | 0. | 706.0727 |
| 8 | 1.51312 | SISMA WOOD SLV-1 | Max | 0. | 0. | 722.9726 |
| 8 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 652.6112 |
| 8 | 0.75656 | SISMA WOOD SLV-1 | Min | 0. | 0. | 706.0727 |
| 8 | 1.51312 | SISMA WOOD SLV-1 | Min | 0. | 0. | 722.9726 |
| 8 | 0. | DEAD-1 | Max | 0. | 0. | -244.3213 |
| 8 | 0.75656 | DEAD-1 | Max | 0. | 0. | -220.6445 |
| 8 | 1.51312 | DEAD-1 | Max | 0. | 0. | -205.58 |
| 8 | 0. | DEAD-1 | Min | 0. | 0. | -244.3213 |
| 8 | 0.75656 | DEAD-1 | Min | 0. | 0. | -220.6445 |
| 8 | 1.51312 | DEAD-1 | Min | 0. | 0. | -205.58 |
| 8 | 0. | SLU_PROVA | | 0. | 0. | -1354.2871 |
| 8 | 0.75656 | SLU_PROVA | | 0. | 0. | -906.3058 |
| 8 | 1.51312 | SLU_PROVA | | 0. | 0. | -608.8964 |
| 9 | 0. | DEAD | | 0. | 0. | -144.221 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 9 | 0.69717 | DEAD | | 0. | 0. | -122.3919 |
| 9 | 1.39435 | DEAD | | 0. | 0. | -107.9613 |
| 9 | 0. | SIMM_KA | | 0. | 0. | 237.8946 |
| 9 | 0.69717 | SIMM_KA | | 0. | 0. | 231.8255 |
| 9 | 1.39435 | SIMM_KA | | 0. | 0. | 212.0996 |
| 9 | 0. | SIMM_K0 | | 0. | 0. | 362.5341 |
| 9 | 0.69717 | SIMM_K0 | | 0. | 0. | 355.3433 |
| 9 | 1.39435 | SIMM_K0 | | 0. | 0. | 327.1585 |
| 9 | 0. | A--SIMM_KA | | 0. | 0. | 337.9159 |
| 9 | 0.69717 | A--SIMM_KA | | 0. | 0. | 343.2185 |
| 9 | 1.39435 | A--SIMM_KA | | 0. | 0. | 325.9043 |
| 9 | 0. | A--SIMM_K0 | | 0. | 0. | 512.8766 |
| 9 | 0.69717 | A--SIMM_K0 | | 0. | 0. | 520.0149 |
| 9 | 1.39435 | A--SIMM_K0 | | 0. | 0. | 493.2311 |
| 9 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 33.9385 |
| 9 | 0.69717 | A-- SIMM_SOVR_K A | | 0. | 0. | 36.7812 |
| 9 | 1.39435 | A-- SIMM_SOVR_K A | | 0. | 0. | 36.8306 |
| 9 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 50.8824 |
| 9 | 0.69717 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 55.1443 |
| 9 | 1.39435 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 55.2183 |
| 9 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 50.8824 |
| 9 | 0.69717 | SIMM_SOVR_K 0 | | 0. | 0. | 55.1443 |
| 9 | 1.39435 | SIMM_SOVR_K 0 | | 0. | 0. | 55.2183 |
| 9 | 0. | SIMM_SOVR_K A | | 0. | 0. | 33.9385 |
| 9 | 0.69717 | SIMM_SOVR_K A | | 0. | 0. | 36.7812 |
| 9 | 1.39435 | SIMM_SOVR_K A | | 0. | 0. | 36.8306 |
| 9 | 0. | SOVR | | 0. | 0. | -156.0924 |
| 9 | 0.69717 | SOVR | | 0. | 0. | -131.7617 |
| 9 | 1.39435 | SOVR | | 0. | 0. | -112.3649 |
| 9 | 0. | TERR_SIMM | | 0. | 0. | -526.1083 |
| 9 | 0.69717 | TERR_SIMM | | 0. | 0. | -421.7989 |
| 9 | 1.39435 | TERR_SIMM | | 0. | 0. | -342.223 |
| 9 | 0. | TERR_A--SIMM | | 0. | 0. | -749.6274 |
| 9 | 0.69717 | TERR_A--SIMM | | 0. | 0. | -575.4622 |
| 9 | 1.39435 | TERR_A--SIMM | | 0. | 0. | -442.7675 |
| 9 | 0. | INERZIA H SLV | | 0. | 0. | -0.6153 |
| 9 | 0.69717 | INERZIA H SLV | | 0. | 0. | 0.7186 |
| 9 | 1.39435 | INERZIA H SLV | | 0. | 0. | 2.0526 |
| 9 | 0. | INERZIA V + SLV | | 0. | 0. | -2.2855 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 9 | 0.69717 | INERZIA V + SLV | | 0. | 0. | -1.9805 |
| 9 | 1.39435 | INERZIA V + SLV | | 0. | 0. | -1.6755 |
| 9 | 0. | INERZIA V - SLV | | 0. | 0. | 2.2855 |
| 9 | 0.69717 | INERZIA V - SLV | | 0. | 0. | 1.9805 |
| 9 | 1.39435 | INERZIA V - SLV | | 0. | 0. | 1.6755 |
| 9 | 0. | SISMA WOOD SLV | | 0. | 0. | 206.6049 |
| 9 | 0.69717 | SISMA WOOD SLV | | 0. | 0. | 279.3152 |
| 9 | 1.39435 | SISMA WOOD SLV | | 0. | 0. | 322.819 |
| 9 | 0. | iDROSTATICA | | 0. | 0. | -39.1905 |
| 9 | 0.69717 | iDROSTATICA | | 0. | 0. | 33.1997 |
| 9 | 1.39435 | iDROSTATICA | | 0. | 0. | 72.7038 |
| 9 | 0. | SISMA WOOD SLD | | 0. | 0. | 91.245 |
| 9 | 0.69717 | SISMA WOOD SLD | | 0. | 0. | 123.3569 |
| 9 | 1.39435 | SISMA WOOD SLD | | 0. | 0. | 142.5699 |
| 9 | 0. | INERZIA H SLD | | 0. | 0. | -0.2718 |
| 9 | 0.69717 | INERZIA H SLD | | 0. | 0. | 0.3174 |
| 9 | 1.39435 | INERZIA H SLD | | 0. | 0. | 0.9065 |
| 9 | 0. | INERZIA V + SLD | | 0. | 0. | -1.0094 |
| 9 | 0.69717 | INERZIA V + SLD | | 0. | 0. | -0.8747 |
| 9 | 1.39435 | INERZIA V + SLD | | 0. | 0. | -0.74 |
| 9 | 0. | INERZIA V SLD | | 0. | 0. | 1.0094 |
| 9 | 0.69717 | INERZIA V SLD | | 0. | 0. | 0.8747 |
| 9 | 1.39435 | INERZIA V SLD | | 0. | 0. | 0.74 |
| 9 | 0. | INERZIA V -1 | | 0. | 0. | 2.2855 |
| 9 | 0.69717 | INERZIA V -1 | | 0. | 0. | 1.9805 |
| 9 | 1.39435 | INERZIA V -1 | | 0. | 0. | 1.6755 |
| 9 | 0. | SLU_1 | Max | 0. | 0. | -837.4071 |
| 9 | 0.69717 | SLU_1 | Max | 0. | 0. | -517.9676 |
| 9 | 1.39435 | SLU_1 | Max | 0. | 0. | -324.0271 |
| 9 | 0. | SLU_1 | Min | 0. | 0. | -837.4071 |
| 9 | 0.69717 | SLU_1 | Min | 0. | 0. | -517.9676 |
| 9 | 1.39435 | SLU_1 | Min | 0. | 0. | -324.0271 |
| 9 | 0. | SLU_2 | Max | 0. | 0. | -1070.5351 |
| 9 | 0.69717 | SLU_2 | Max | 0. | 0. | -749.5658 |
| 9 | 1.39435 | SLU_2 | Max | 0. | 0. | -542.465 |
| 9 | 0. | SLU_2 | Min | 0. | 0. | -1070.5351 |
| 9 | 0.69717 | SLU_2 | Min | 0. | 0. | -749.5658 |
| 9 | 1.39435 | SLU_2 | Min | 0. | 0. | -542.465 |
| 9 | 0. | SLU_3 | Max | 0. | 0. | -940.8824 |
| 9 | 0.69717 | SLU_3 | Max | 0. | 0. | -472.0092 |
| 9 | 1.39435 | SLU_3 | Max | 0. | 0. | -167.1995 |
| 9 | 0. | SLU_3 | Min | 0. | 0. | -940.8824 |
| 9 | 0.69717 | SLU_3 | Min | 0. | 0. | -472.0092 |
| 9 | 1.39435 | SLU_3 | Min | 0. | 0. | -167.1995 |
| 9 | 0. | SLU_4 | Max | 0. | 0. | -1251.9025 |
| 9 | 0.69717 | SLU_4 | Max | 0. | 0. | -794.0724 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 9 | 1.39435 | SLU_4 | Max | 0. | 0. | -483.5171 |
| 9 | 0. | SLU_4 | Min | 0. | 0. | -1251.9025 |
| 9 | 0.69717 | SLU_4 | Min | 0. | 0. | -794.0724 |
| 9 | 1.39435 | SLU_4 | Min | 0. | 0. | -483.5171 |
| 9 | 0. | SLE_F1 | Max | 0. | 0. | -593.4884 |
| 9 | 0.69717 | SLE_F1 | Max | 0. | 0. | -359.8407 |
| 9 | 1.39435 | SLE_F1 | Max | 0. | 0. | -219.0468 |
| 9 | 0. | SLE_F1 | Min | 0. | 0. | -593.4884 |
| 9 | 0.69717 | SLE_F1 | Min | 0. | 0. | -359.8407 |
| 9 | 1.39435 | SLE_F1 | Min | 0. | 0. | -219.0468 |
| 9 | 0. | SLE_F2 | Max | 0. | 0. | -764.761 |
| 9 | 0.69717 | SLE_F2 | Max | 0. | 0. | -529.2546 |
| 9 | 1.39435 | SLE_F2 | Max | 0. | 0. | -378.2189 |
| 9 | 0. | SLE_F2 | Min | 0. | 0. | -764.761 |
| 9 | 0.69717 | SLE_F2 | Min | 0. | 0. | -529.2546 |
| 9 | 1.39435 | SLE_F2 | Min | 0. | 0. | -378.2189 |
| 9 | 0. | SLE_F3 | Max | 0. | 0. | -902.584 |
| 9 | 0.69717 | SLE_F3 | Max | 0. | 0. | -562.1107 |
| 9 | 1.39435 | SLE_F3 | Max | 0. | 0. | -331.8051 |
| 9 | 0. | SLE_F3 | Min | 0. | 0. | -902.584 |
| 9 | 0.69717 | SLE_F3 | Min | 0. | 0. | -562.1107 |
| 9 | 1.39435 | SLE_F3 | Min | 0. | 0. | -331.8051 |
| 9 | 0. | SLE_F4 | Max | 0. | 0. | -662.7162 |
| 9 | 0.69717 | SLE_F4 | Max | 0. | 0. | -315.9963 |
| 9 | 1.39435 | SLE_F4 | Max | 0. | 0. | -91.7952 |
| 9 | 0. | SLE_F4 | Min | 0. | 0. | -662.7162 |
| 9 | 0.69717 | SLE_F4 | Min | 0. | 0. | -315.9963 |
| 9 | 1.39435 | SLE_F4 | Min | 0. | 0. | -91.7952 |
| 9 | 0. | SLE_QP1 | Max | 0. | 0. | -500.2646 |
| 9 | 0.69717 | SLE_QP1 | Max | 0. | 0. | -288.737 |
| 9 | 1.39435 | SLE_QP1 | Max | 0. | 0. | -163.2219 |
| 9 | 0. | SLE_QP1 | Min | 0. | 0. | -500.2646 |
| 9 | 0.69717 | SLE_QP1 | Min | 0. | 0. | -288.737 |
| 9 | 1.39435 | SLE_QP1 | Min | 0. | 0. | -163.2219 |
| 9 | 0. | SLE_QP2 | Max | 0. | 0. | -655.6914 |
| 9 | 0.69717 | SLE_QP2 | Max | 0. | 0. | -441.3448 |
| 9 | 1.39435 | SLE_QP2 | Max | 0. | 0. | -305.6734 |
| 9 | 0. | SLE_QP2 | Min | 0. | 0. | -655.6914 |
| 9 | 0.69717 | SLE_QP2 | Min | 0. | 0. | -441.3448 |
| 9 | 1.39435 | SLE_QP2 | Min | 0. | 0. | -305.6734 |
| 9 | 0. | SLE_QP3 | Max | 0. | 0. | -790.3787 |
| 9 | 0.69717 | SLE_QP3 | Max | 0. | 0. | -471.6411 |
| 9 | 1.39435 | SLE_QP3 | Max | 0. | 0. | -257.2757 |
| 9 | 0. | SLE_QP3 | Min | 0. | 0. | -790.3787 |
| 9 | 0.69717 | SLE_QP3 | Min | 0. | 0. | -471.6411 |
| 9 | 1.39435 | SLE_QP3 | Min | 0. | 0. | -257.2757 |
| 9 | 0. | SLE_QP4 | Max | 0. | 0. | -548.2184 |
| 9 | 0.69717 | SLE_QP4 | Max | 0. | 0. | -227.7299 |
| 9 | 1.39435 | SLE_QP4 | Max | 0. | 0. | -22.919 |
| 9 | 0. | SLE_QP4 | Min | 0. | 0. | -548.2184 |
| 9 | 0.69717 | SLE_QP4 | Min | 0. | 0. | -227.7299 |
| 9 | 1.39435 | SLE_QP4 | Min | 0. | 0. | -22.919 |
| 9 | 0. | SLV_1 | Max | 0. | 0. | 265.0139 |
| 9 | 0.69717 | SLV_1 | Max | 0. | 0. | 512.3687 |
| 9 | 1.39435 | SLV_1 | Max | 0. | 0. | 644.5045 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 9 | 0. | SLV_1 | Min | 0. | 0. | 265.0139 |
| 9 | 0.69717 | SLV_1 | Min | 0. | 0. | 512.3687 |
| 9 | 1.39435 | SLV_1 | Min | 0. | 0. | 644.5045 |
| 9 | 0. | SLV_2 | Max | 0. | 0. | 270.6065 |
| 9 | 0.69717 | SLV_2 | Max | 0. | 0. | 516.8829 |
| 9 | 1.39435 | SLV_2 | Max | 0. | 0. | 647.9404 |
| 9 | 0. | SLV_2 | Min | 0. | 0. | 270.6065 |
| 9 | 0.69717 | SLV_2 | Min | 0. | 0. | 516.8829 |
| 9 | 1.39435 | SLV_2 | Min | 0. | 0. | 647.9404 |
| 9 | 0. | SLV_3 | Max | 0. | 0. | 292.0713 |
| 9 | 0.69717 | SLV_3 | Max | 0. | 0. | 624.9707 |
| 9 | 1.39435 | SLV_3 | Max | 0. | 0. | 812.986 |
| 9 | 0. | SLV_3 | Min | 0. | 0. | 292.0713 |
| 9 | 0.69717 | SLV_3 | Min | 0. | 0. | 624.9707 |
| 9 | 1.39435 | SLV_3 | Min | 0. | 0. | 812.986 |
| 9 | 0. | SLV_4 | Max | 0. | 0. | 298.6593 |
| 9 | 0.69717 | SLV_4 | Max | 0. | 0. | 630.4034 |
| 9 | 1.39435 | SLV_4 | Max | 0. | 0. | 817.2634 |
| 9 | 0. | SLV_4 | Min | 0. | 0. | 298.6593 |
| 9 | 0.69717 | SLV_4 | Min | 0. | 0. | 630.4034 |
| 9 | 1.39435 | SLV_4 | Min | 0. | 0. | 817.2634 |
| 9 | 0. | SLD_1 | Max | 0. | 0. | -198.3149 |
| 9 | 0.69717 | SLD_1 | Max | 0. | 0. | 43.3759 |
| 9 | 1.39435 | SLD_1 | Max | 0. | 0. | 186.1555 |
| 9 | 0. | SLD_1 | Min | 0. | 0. | -198.3149 |
| 9 | 0.69717 | SLD_1 | Min | 0. | 0. | 43.3759 |
| 9 | 1.39435 | SLD_1 | Min | 0. | 0. | 186.1555 |
| 9 | 0. | SLD_2 | Max | 0. | 0. | -195.907 |
| 9 | 0.69717 | SLD_2 | Max | 0. | 0. | 45.4387 |
| 9 | 1.39435 | SLD_2 | Max | 0. | 0. | 187.873 |
| 9 | 0. | SLD_2 | Min | 0. | 0. | -195.907 |
| 9 | 0.69717 | SLD_2 | Min | 0. | 0. | 45.4387 |
| 9 | 1.39435 | SLD_2 | Min | 0. | 0. | 187.873 |
| 9 | 0. | SLD_3 | Max | 0. | 0. | -153.0355 |
| 9 | 0.69717 | SLD_3 | Max | 0. | 0. | 172.9013 |
| 9 | 1.39435 | SLD_3 | Max | 0. | 0. | 370.2617 |
| 9 | 0. | SLD_3 | Min | 0. | 0. | -153.0355 |
| 9 | 0.69717 | SLD_3 | Min | 0. | 0. | 172.9013 |
| 9 | 1.39435 | SLD_3 | Min | 0. | 0. | 370.2617 |
| 9 | 0. | SLD_4 | Max | 0. | 0. | -150.079 |
| 9 | 0.69717 | SLD_4 | Max | 0. | 0. | 175.3775 |
| 9 | 1.39435 | SLD_4 | Max | 0. | 0. | 372.2576 |
| 9 | 0. | SLD_4 | Min | 0. | 0. | -150.079 |
| 9 | 0.69717 | SLD_4 | Min | 0. | 0. | 175.3775 |
| 9 | 1.39435 | SLD_4 | Min | 0. | 0. | 372.2576 |
| 9 | 0. | SLU_IDR_1 | Max | 0. | 0. | -749.5413 |
| 9 | 0.69717 | SLU_IDR_1 | Max | 0. | 0. | -442.8564 |
| 9 | 1.39435 | SLU_IDR_1 | Max | 0. | 0. | -236.6837 |
| 9 | 0. | SLU_IDR_1 | Min | 0. | 0. | -749.5413 |
| 9 | 0.69717 | SLU_IDR_1 | Min | 0. | 0. | -442.8564 |
| 9 | 1.39435 | SLU_IDR_1 | Min | 0. | 0. | -236.6837 |
| 9 | 0. | SLU_IDR_2 | Max | 0. | 0. | -634.943 |
| 9 | 0.69717 | SLU_IDR_2 | Max | 0. | 0. | -420.946 |
| 9 | 1.39435 | SLU_IDR_2 | Max | 0. | 0. | -284.3341 |
| 9 | 0. | SLU_IDR_2 | Min | 0. | 0. | -634.943 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 9 | 0.69717 | SLU_IDR_2 | Min | 0. | 0. | -420.946 |
| 9 | 1.39435 | SLU_IDR_2 | Min | 0. | 0. | -284.3341 |
| 9 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 722.9726 |
| 9 | 0.69717 | SISMA WOOD SLV-1 | Max | 0. | 0. | 709.6972 |
| 9 | 1.39435 | SISMA WOOD SLV-1 | Max | 0. | 0. | 667.2152 |
| 9 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 722.9726 |
| 9 | 0.69717 | SISMA WOOD SLV-1 | Min | 0. | 0. | 709.6972 |
| 9 | 1.39435 | SISMA WOOD SLV-1 | Min | 0. | 0. | 667.2152 |
| 9 | 0. | DEAD-1 | Max | 0. | 0. | -205.58 |
| 9 | 0.69717 | DEAD-1 | Max | 0. | 0. | -177.2084 |
| 9 | 1.39435 | DEAD-1 | Max | 0. | 0. | -156.2354 |
| 9 | 0. | DEAD-1 | Min | 0. | 0. | -205.58 |
| 9 | 0.69717 | DEAD-1 | Min | 0. | 0. | -177.2084 |
| 9 | 1.39435 | DEAD-1 | Min | 0. | 0. | -156.2354 |
| 9 | 0. | SLU_PROVA | | 0. | 0. | -608.8964 |
| 9 | 0.69717 | SLU_PROVA | | 0. | 0. | -317.2681 |
| 9 | 1.39435 | SLU_PROVA | | 0. | 0. | -151.1387 |
| 10 | 0. | DEAD | | 0. | 0. | -107.9613 |
| 10 | 1.03974 | DEAD | | 0. | 0. | -72.3925 |
| 10 | 2.07949 | DEAD | | 0. | 0. | -53.3806 |
| 10 | 0. | SIMM_KA | | 0. | 0. | 212.0996 |
| 10 | 1.03974 | SIMM_KA | | 0. | 0. | 171.0899 |
| 10 | 2.07949 | SIMM_KA | | 0. | 0. | 106.5739 |
| 10 | 0. | SIMM_K0 | | 0. | 0. | 327.1585 |
| 10 | 1.03974 | SIMM_K0 | | 0. | 0. | 266.3128 |
| 10 | 2.07949 | SIMM_K0 | | 0. | 0. | 168.356 |
| 10 | 0. | A--SIMM_KA | | 0. | 0. | 325.9043 |
| 10 | 1.03974 | A--SIMM_KA | | 0. | 0. | 280.8723 |
| 10 | 2.07949 | A--SIMM_KA | | 0. | 0. | 195.7991 |
| 10 | 0. | A--SIMM_K0 | | 0. | 0. | 493.2311 |
| 10 | 1.03974 | A--SIMM_K0 | | 0. | 0. | 424.4756 |
| 10 | 2.07949 | A--SIMM_K0 | | 0. | 0. | 295.6197 |
| 10 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 36.8306 |
| 10 | 1.03974 | A-- SIMM_SOVR_K A | | 0. | 0. | 33.3624 |
| 10 | 2.07949 | A-- SIMM_SOVR_K A | | 0. | 0. | 24.1959 |
| 10 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 55.2183 |
| 10 | 1.03974 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 50.0185 |
| 10 | 2.07949 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 36.2757 |
| 10 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 55.2183 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 10 | 1.03974 | SIMM_SOVR_K 0 | | 0. | 0. | 50.0185 |
| 10 | 2.07949 | SIMM_SOVR_K 0 | | 0. | 0. | 36.2757 |
| 10 | 0. | SIMM_SOVR_K A | | 0. | 0. | 36.8306 |
| 10 | 1.03974 | SIMM_SOVR_K A | | 0. | 0. | 33.3624 |
| 10 | 2.07949 | SIMM_SOVR_K A | | 0. | 0. | 24.1959 |
| 10 | 0. | SOVR | | 0. | 0. | -112.3649 |
| 10 | 1.03974 | SOVR | | 0. | 0. | -74.0205 |
| 10 | 2.07949 | SOVR | | 0. | 0. | -48.9255 |
| 10 | 0. | TERR_SIMM | | 0. | 0. | -342.223 |
| 10 | 1.03974 | TERR_SIMM | | 0. | 0. | -202.1273 |
| 10 | 2.07949 | TERR_SIMM | | 0. | 0. | -119.9848 |
| 10 | 0. | TERR_A--SIMM | | 0. | 0. | -442.7675 |
| 10 | 1.03974 | TERR_A--SIMM | | 0. | 0. | -216.856 |
| 10 | 2.07949 | TERR_A--SIMM | | 0. | 0. | -84.1246 |
| 10 | 0. | INERZIA H SLV | | 0. | 0. | 2.0526 |
| 10 | 1.03974 | INERZIA H SLV | | 0. | 0. | 3.1842 |
| 10 | 2.07949 | INERZIA H SLV | | 0. | 0. | 4.3159 |
| 10 | 0. | INERZIA V + SLV | | 0. | 0. | -1.6755 |
| 10 | 1.03974 | INERZIA V + SLV | | 0. | 0. | -1.218 |
| 10 | 2.07949 | INERZIA V + SLV | | 0. | 0. | -0.7606 |
| 10 | 0. | INERZIA V - SLV | | 0. | 0. | 1.6755 |
| 10 | 1.03974 | INERZIA V - SLV | | 0. | 0. | 1.218 |
| 10 | 2.07949 | INERZIA V - SLV | | 0. | 0. | 0.7606 |
| 10 | 0. | SISMA WOOD SLV | | 0. | 0. | 322.819 |
| 10 | 1.03974 | SISMA WOOD SLV | | 0. | 0. | 359.352 |
| 10 | 2.07949 | SISMA WOOD SLV | | 0. | 0. | 336.3056 |
| 10 | 0. | iDROSTATICA | | 0. | 0. | 72.7038 |
| 10 | 1.03974 | iDROSTATICA | | 0. | 0. | 108.178 |
| 10 | 2.07949 | iDROSTATICA | | 0. | 0. | 83.7825 |
| 10 | 0. | SISMA WOOD SLD | | 0. | 0. | 142.5699 |
| 10 | 1.03974 | SISMA WOOD SLD | | 0. | 0. | 158.7043 |
| 10 | 2.07949 | SISMA WOOD SLD | | 0. | 0. | 148.5261 |
| 10 | 0. | INERZIA H SLD | | 0. | 0. | 0.9065 |
| 10 | 1.03974 | INERZIA H SLD | | 0. | 0. | 1.4063 |
| 10 | 2.07949 | INERZIA H SLD | | 0. | 0. | 1.9061 |
| 10 | 0. | INERZIA V + SLD | | 0. | 0. | -0.74 |
| 10 | 1.03974 | INERZIA V + SLD | | 0. | 0. | -0.5379 |
| 10 | 2.07949 | INERZIA V + SLD | | 0. | 0. | -0.3359 |
| 10 | 0. | INERZIA V SLD | | 0. | 0. | 0.74 |
| 10 | 1.03974 | INERZIA V SLD | | 0. | 0. | 0.5379 |
| 10 | 2.07949 | INERZIA V SLD | | 0. | 0. | 0.3359 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------|----------|-----------|------------|------------|
| 10 | 0. | INERZIA V -1 | | 0. | 0. | 1.6755 |
| 10 | 1.03974 | INERZIA V -1 | | 0. | 0. | 1.218 |
| 10 | 2.07949 | INERZIA V -1 | | 0. | 0. | 0.7606 |
| 10 | 0. | SLU_1 | Max | 0. | 0. | -324.0271 |
| 10 | 1.03974 | SLU_1 | Max | 0. | 0. | -32.0738 |
| 10 | 2.07949 | SLU_1 | Max | 0. | 0. | 4.2527 |
| 10 | 0. | SLU_1 | Min | 0. | 0. | -324.0271 |
| 10 | 1.03974 | SLU_1 | Min | 0. | 0. | -32.0738 |
| 10 | 2.07949 | SLU_1 | Min | 0. | 0. | 4.2527 |
| 10 | 0. | SLU_2 | Max | 0. | 0. | -542.465 |
| 10 | 1.03974 | SLU_2 | Max | 0. | 0. | -213.0344 |
| 10 | 2.07949 | SLU_2 | Max | 0. | 0. | -117.2771 |
| 10 | 0. | SLU_2 | Min | 0. | 0. | -542.465 |
| 10 | 1.03974 | SLU_2 | Min | 0. | 0. | -213.0344 |
| 10 | 2.07949 | SLU_2 | Min | 0. | 0. | -117.2771 |
| 10 | 0. | SLU_3 | Max | 0. | 0. | -167.1995 |
| 10 | 1.03974 | SLU_3 | Max | 0. | 0. | 261.1929 |
| 10 | 2.07949 | SLU_3 | Max | 0. | 0. | 358.2772 |
| 10 | 0. | SLU_3 | Min | 0. | 0. | -167.1995 |
| 10 | 1.03974 | SLU_3 | Min | 0. | 0. | 261.1929 |
| 10 | 2.07949 | SLU_3 | Min | 0. | 0. | 358.2772 |
| 10 | 0. | SLU_4 | Max | 0. | 0. | -483.5171 |
| 10 | 1.03974 | SLU_4 | Max | 0. | 0. | -18.1682 |
| 10 | 2.07949 | SLU_4 | Max | 0. | 0. | 146.2168 |
| 10 | 0. | SLU_4 | Min | 0. | 0. | -483.5171 |
| 10 | 1.03974 | SLU_4 | Min | 0. | 0. | -18.1682 |
| 10 | 2.07949 | SLU_4 | Min | 0. | 0. | 146.2168 |
| 10 | 0. | SLE_F1 | Max | 0. | 0. | -219.0468 |
| 10 | 1.03974 | SLE_F1 | Max | 0. | 0. | -9.3682 |
| 10 | 2.07949 | SLE_F1 | Max | 0. | 0. | 12.4753 |
| 10 | 0. | SLE_F1 | Min | 0. | 0. | -219.0468 |
| 10 | 1.03974 | SLE_F1 | Min | 0. | 0. | -9.3682 |
| 10 | 2.07949 | SLE_F1 | Min | 0. | 0. | 12.4753 |
| 10 | 0. | SLE_F2 | Max | 0. | 0. | -378.2189 |
| 10 | 1.03974 | SLE_F2 | Max | 0. | 0. | -140.5204 |
| 10 | 2.07949 | SLE_F2 | Max | 0. | 0. | -74.9185 |
| 10 | 0. | SLE_F2 | Min | 0. | 0. | -378.2189 |
| 10 | 1.03974 | SLE_F2 | Min | 0. | 0. | -140.5204 |
| 10 | 2.07949 | SLE_F2 | Min | 0. | 0. | -74.9185 |
| 10 | 0. | SLE_F3 | Max | 0. | 0. | -331.8051 |
| 10 | 1.03974 | SLE_F3 | Max | 0. | 0. | 10.0251 |
| 10 | 2.07949 | SLE_F3 | Max | 0. | 0. | 127.9965 |
| 10 | 0. | SLE_F3 | Min | 0. | 0. | -331.8051 |
| 10 | 1.03974 | SLE_F3 | Min | 0. | 0. | 10.0251 |
| 10 | 2.07949 | SLE_F3 | Min | 0. | 0. | 127.9965 |
| 10 | 0. | SLE_F4 | Max | 0. | 0. | -91.7952 |
| 10 | 1.03974 | SLE_F4 | Max | 0. | 0. | 220.2919 |
| 10 | 2.07949 | SLE_F4 | Max | 0. | 0. | 286.3275 |
| 10 | 0. | SLE_F4 | Min | 0. | 0. | -91.7952 |
| 10 | 1.03974 | SLE_F4 | Min | 0. | 0. | 220.2919 |
| 10 | 2.07949 | SLE_F4 | Min | 0. | 0. | 286.3275 |
| 10 | 0. | SLE_QP1 | Max | 0. | 0. | -163.2219 |
| 10 | 1.03974 | SLE_QP1 | Max | 0. | 0. | 19.1776 |
| 10 | 2.07949 | SLE_QP1 | Max | 0. | 0. | 30.0864 |
| 10 | 0. | SLE_QP1 | Min | 0. | 0. | -163.2219 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 10 | 1.03974 | SLE_QP1 | Min | 0. | 0. | 19.1776 |
| 10 | 2.07949 | SLE_QP1 | Min | 0. | 0. | 30.0864 |
| 10 | 0. | SLE_QP2 | Max | 0. | 0. | -305.6734 |
| 10 | 1.03974 | SLE_QP2 | Max | 0. | 0. | -97.1512 |
| 10 | 2.07949 | SLE_QP2 | Max | 0. | 0. | -46.5149 |
| 10 | 0. | SLE_QP2 | Min | 0. | 0. | -305.6734 |
| 10 | 1.03974 | SLE_QP2 | Min | 0. | 0. | -97.1512 |
| 10 | 2.07949 | SLE_QP2 | Min | 0. | 0. | -46.5149 |
| 10 | 0. | SLE_QP3 | Max | 0. | 0. | -257.2757 |
| 10 | 1.03974 | SLE_QP3 | Max | 0. | 0. | 54.5974 |
| 10 | 2.07949 | SLE_QP3 | Max | 0. | 0. | 156.8225 |
| 10 | 0. | SLE_QP3 | Min | 0. | 0. | -257.2757 |
| 10 | 1.03974 | SLE_QP3 | Min | 0. | 0. | 54.5974 |
| 10 | 2.07949 | SLE_QP3 | Min | 0. | 0. | 156.8225 |
| 10 | 0. | SLE_QP4 | Max | 0. | 0. | -22.919 |
| 10 | 1.03974 | SLE_QP4 | Max | 0. | 0. | 256.3571 |
| 10 | 2.07949 | SLE_QP4 | Max | 0. | 0. | 305.926 |
| 10 | 0. | SLE_QP4 | Min | 0. | 0. | -22.919 |
| 10 | 1.03974 | SLE_QP4 | Min | 0. | 0. | 256.3571 |
| 10 | 2.07949 | SLE_QP4 | Min | 0. | 0. | 305.926 |
| 10 | 0. | SLV_1 | Max | 0. | 0. | 644.5045 |
| 10 | 1.03974 | SLV_1 | Max | 0. | 0. | 769.3037 |
| 10 | 2.07949 | SLV_1 | Max | 0. | 0. | 663.0328 |
| 10 | 0. | SLV_1 | Min | 0. | 0. | 644.5045 |
| 10 | 1.03974 | SLV_1 | Min | 0. | 0. | 769.3037 |
| 10 | 2.07949 | SLV_1 | Min | 0. | 0. | 663.0328 |
| 10 | 0. | SLV_2 | Max | 0. | 0. | 647.9404 |
| 10 | 1.03974 | SLV_2 | Max | 0. | 0. | 771.2248 |
| 10 | 2.07949 | SLV_2 | Max | 0. | 0. | 663.4391 |
| 10 | 0. | SLV_2 | Min | 0. | 0. | 647.9404 |
| 10 | 1.03974 | SLV_2 | Min | 0. | 0. | 771.2248 |
| 10 | 2.07949 | SLV_2 | Min | 0. | 0. | 663.4391 |
| 10 | 0. | SLV_3 | Max | 0. | 0. | 812.986 |
| 10 | 1.03974 | SLV_3 | Max | 0. | 0. | 1005.3241 |
| 10 | 2.07949 | SLV_3 | Max | 0. | 0. | 908.3757 |
| 10 | 0. | SLV_3 | Min | 0. | 0. | 812.986 |
| 10 | 1.03974 | SLV_3 | Min | 0. | 0. | 1005.3241 |
| 10 | 2.07949 | SLV_3 | Min | 0. | 0. | 908.3757 |
| 10 | 0. | SLV_4 | Max | 0. | 0. | 817.2634 |
| 10 | 1.03974 | SLV_4 | Max | 0. | 0. | 1007.9418 |
| 10 | 2.07949 | SLV_4 | Max | 0. | 0. | 909.3337 |
| 10 | 0. | SLV_4 | Min | 0. | 0. | 817.2634 |
| 10 | 1.03974 | SLV_4 | Min | 0. | 0. | 1007.9418 |
| 10 | 2.07949 | SLV_4 | Min | 0. | 0. | 909.3337 |
| 10 | 0. | SLD_1 | Max | 0. | 0. | 186.1555 |
| 10 | 1.03974 | SLD_1 | Max | 0. | 0. | 360.5739 |
| 10 | 2.07949 | SLD_1 | Max | 0. | 0. | 337.1889 |
| 10 | 0. | SLD_1 | Min | 0. | 0. | 186.1555 |
| 10 | 1.03974 | SLD_1 | Min | 0. | 0. | 360.5739 |
| 10 | 2.07949 | SLD_1 | Min | 0. | 0. | 337.1889 |
| 10 | 0. | SLD_2 | Max | 0. | 0. | 187.873 |
| 10 | 1.03974 | SLD_2 | Max | 0. | 0. | 361.758 |
| 10 | 2.07949 | SLD_2 | Max | 0. | 0. | 337.8397 |
| 10 | 0. | SLD_2 | Min | 0. | 0. | 187.873 |
| 10 | 1.03974 | SLD_2 | Min | 0. | 0. | 361.758 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 10 | 2.07949 | SLD_2 | Min | 0. | 0. | 337.8397 |
| 10 | 0. | SLD_3 | Max | 0. | 0. | 370.2617 |
| 10 | 1.03974 | SLD_3 | Max | 0. | 0. | 609.8405 |
| 10 | 2.07949 | SLD_3 | Max | 0. | 0. | 593.3996 |
| 10 | 0. | SLD_3 | Min | 0. | 0. | 370.2617 |
| 10 | 1.03974 | SLD_3 | Min | 0. | 0. | 609.8405 |
| 10 | 2.07949 | SLD_3 | Min | 0. | 0. | 593.3996 |
| 10 | 0. | SLD_4 | Max | 0. | 0. | 372.2576 |
| 10 | 1.03974 | SLD_4 | Max | 0. | 0. | 611.1323 |
| 10 | 2.07949 | SLD_4 | Max | 0. | 0. | 593.9872 |
| 10 | 0. | SLD_4 | Min | 0. | 0. | 372.2576 |
| 10 | 1.03974 | SLD_4 | Min | 0. | 0. | 611.1323 |
| 10 | 2.07949 | SLD_4 | Min | 0. | 0. | 593.9872 |
| 10 | 0. | SLU_IDR_1 | Max | 0. | 0. | -236.6837 |
| 10 | 1.03974 | SLU_IDR_1 | Max | 0. | 0. | 58.6494 |
| 10 | 2.07949 | SLU_IDR_1 | Max | 0. | 0. | 153.3255 |
| 10 | 0. | SLU_IDR_1 | Min | 0. | 0. | -236.6837 |
| 10 | 1.03974 | SLU_IDR_1 | Min | 0. | 0. | 58.6494 |
| 10 | 2.07949 | SLU_IDR_1 | Min | 0. | 0. | 153.3255 |
| 10 | 0. | SLU_IDR_2 | Max | 0. | 0. | -284.3341 |
| 10 | 1.03974 | SLU_IDR_2 | Max | 0. | 0. | -80.307 |
| 10 | 2.07949 | SLU_IDR_2 | Max | 0. | 0. | -30.3513 |
| 10 | 0. | SLU_IDR_2 | Min | 0. | 0. | -284.3341 |
| 10 | 1.03974 | SLU_IDR_2 | Min | 0. | 0. | -80.307 |
| 10 | 2.07949 | SLU_IDR_2 | Min | 0. | 0. | -30.3513 |
| 10 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 667.2152 |
| 10 | 1.03974 | SISMA WOOD SLV-1 | Max | 0. | 0. | 563.6104 |
| 10 | 2.07949 | SISMA WOOD SLV-1 | Max | 0. | 0. | 400.4262 |
| 10 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 667.2152 |
| 10 | 1.03974 | SISMA WOOD SLV-1 | Min | 0. | 0. | 563.6104 |
| 10 | 2.07949 | SISMA WOOD SLV-1 | Min | 0. | 0. | 400.4262 |
| 10 | 0. | DEAD-1 | Max | 0. | 0. | -156.2354 |
| 10 | 1.03974 | DEAD-1 | Max | 0. | 0. | -108.8537 |
| 10 | 2.07949 | DEAD-1 | Max | 0. | 0. | -78.029 |
| 10 | 0. | DEAD-1 | Min | 0. | 0. | -156.2354 |
| 10 | 1.03974 | DEAD-1 | Min | 0. | 0. | -108.8537 |
| 10 | 2.07949 | DEAD-1 | Min | 0. | 0. | -78.029 |
| 10 | 0. | SLU_PROVA | | 0. | 0. | -151.1387 |
| 10 | 1.03974 | SLU_PROVA | | 0. | 0. | 93.9592 |
| 10 | 2.07949 | SLU_PROVA | | 0. | 0. | 83.4304 |
| 11 | 0. | DEAD | | 0. | 0. | -53.3806 |
| 11 | 1.05223 | DEAD | | 0. | 0. | -10.713 |
| 11 | 2.10446 | DEAD | | 0. | 0. | 10.1181 |
| 11 | 0. | SIMM_KA | | 0. | 0. | 106.5739 |
| 11 | 1.05223 | SIMM_KA | | 0. | 0. | 47.0009 |
| 11 | 2.10446 | SIMM_KA | | 0. | 0. | -28.3699 |
| 11 | 0. | SIMM_K0 | | 0. | 0. | 168.356 |
| 11 | 1.05223 | SIMM_K0 | | 0. | 0. | 76.9825 |
| 11 | 2.10446 | SIMM_K0 | | 0. | 0. | -40.4678 |
| 11 | 0. | A--SIMM_KA | | 0. | 0. | 195.7991 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 11 | 1.05223 | A--SIMM_KA | | 0. | 0. | 112.6624 |
| 11 | 2.10446 | A--SIMM_KA | | 0. | 0. | 3.1804 |
| 11 | 0. | A--SIMM_K0 | | 0. | 0. | 295.6197 |
| 11 | 1.05223 | A--SIMM_K0 | | 0. | 0. | 169.8025 |
| 11 | 2.10446 | A--SIMM_K0 | | 0. | 0. | 4.4332 |
| 11 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 24.1959 |
| 11 | 1.05223 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.9037 |
| 11 | 2.10446 | A-- SIMM_SOVR_K A | | 0. | 0. | -0.9244 |
| 11 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 36.2757 |
| 11 | 1.05223 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.8452 |
| 11 | 2.10446 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -1.3859 |
| 11 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 36.2757 |
| 11 | 1.05223 | SIMM_SOVR_K 0 | | 0. | 0. | 20.8452 |
| 11 | 2.10446 | SIMM_SOVR_K 0 | | 0. | 0. | -1.3859 |
| 11 | 0. | SIMM_SOVR_K A | | 0. | 0. | 24.1959 |
| 11 | 1.05223 | SIMM_SOVR_K A | | 0. | 0. | 13.9037 |
| 11 | 2.10446 | SIMM_SOVR_K A | | 0. | 0. | -0.9244 |
| 11 | 0. | SOVR | | 0. | 0. | -48.9255 |
| 11 | 1.05223 | SOVR | | 0. | 0. | -7.0939 |
| 11 | 2.10446 | SOVR | | 0. | 0. | 17.2634 |
| 11 | 0. | TERR_SIMM | | 0. | 0. | -119.9848 |
| 11 | 1.05223 | TERR_SIMM | | 0. | 0. | 5.82 |
| 11 | 2.10446 | TERR_SIMM | | 0. | 0. | 68.5512 |
| 11 | 0. | TERR_A--SIMM | | 0. | 0. | -84.1246 |
| 11 | 1.05223 | TERR_A--SIMM | | 0. | 0. | 99.1723 |
| 11 | 2.10446 | TERR_A--SIMM | | 0. | 0. | 180.8821 |
| 11 | 0. | INERZIA H SLV | | 0. | 0. | 4.3159 |
| 11 | 1.05223 | INERZIA H SLV | | 0. | 0. | 4.2963 |
| 11 | 2.10446 | INERZIA H SLV | | 0. | 0. | 4.2767 |
| 11 | 0. | INERZIA V + SLV | | 0. | 0. | -0.7606 |
| 11 | 1.05223 | INERZIA V + SLV | | 0. | 0. | -0.2347 |
| 11 | 2.10446 | INERZIA V + SLV | | 0. | 0. | 0.2913 |
| 11 | 0. | INERZIA V - SLV | | 0. | 0. | 0.7606 |
| 11 | 1.05223 | INERZIA V - SLV | | 0. | 0. | 0.2347 |
| 11 | 2.10446 | INERZIA V - SLV | | 0. | 0. | -0.2913 |
| 11 | 0. | SISMA WOOD SLV | | 0. | 0. | 336.3056 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 11 | 1.05223 | SISMA WOOD SLV | | 0. | 0. | 283.5167 |
| 11 | 2.10446 | SISMA WOOD SLV | | 0. | 0. | 183.3007 |
| 11 | 0. | iDROSTATICA | | 0. | 0. | 83.7825 |
| 11 | 1.05223 | iDROSTATICA | | 0. | 0. | 75.1481 |
| 11 | 2.10446 | iDROSTATICA | | 0. | 0. | 21.4845 |
| 11 | 0. | SISMA WOOD SLD | | 0. | 0. | 148.5261 |
| 11 | 1.05223 | SISMA WOOD SLD | | 0. | 0. | 125.2124 |
| 11 | 2.10446 | SISMA WOOD SLD | | 0. | 0. | 80.953 |
| 11 | 0. | INERZIA H SLD | | 0. | 0. | 1.9061 |
| 11 | 1.05223 | INERZIA H SLD | | 0. | 0. | 1.8974 |
| 11 | 2.10446 | INERZIA H SLD | | 0. | 0. | 1.8888 |
| 11 | 0. | INERZIA V + SLD | | 0. | 0. | -0.3359 |
| 11 | 1.05223 | INERZIA V + SLD | | 0. | 0. | -0.1036 |
| 11 | 2.10446 | INERZIA V + SLD | | 0. | 0. | 0.1286 |
| 11 | 0. | INERZIA V SLD | | 0. | 0. | 0.3359 |
| 11 | 1.05223 | INERZIA V SLD | | 0. | 0. | 0.1036 |
| 11 | 2.10446 | INERZIA V SLD | | 0. | 0. | -0.1286 |
| 11 | 0. | INERZIA V -1 | | 0. | 0. | 0.7606 |
| 11 | 1.05223 | INERZIA V -1 | | 0. | 0. | 0.2347 |
| 11 | 2.10446 | INERZIA V -1 | | 0. | 0. | -0.2913 |
| 11 | 0. | SLU_1 | Max | 0. | 0. | 4.2527 |
| 11 | 1.05223 | SLU_1 | Max | 0. | 0. | 186.8519 |
| 11 | 2.10446 | SLU_1 | Max | 0. | 0. | 130.2179 |
| 11 | 0. | SLU_1 | Min | 0. | 0. | 4.2527 |
| 11 | 1.05223 | SLU_1 | Min | 0. | 0. | 186.8519 |
| 11 | 2.10446 | SLU_1 | Min | 0. | 0. | 130.2179 |
| 11 | 0. | SLU_2 | Max | 0. | 0. | -117.2771 |
| 11 | 1.05223 | SLU_2 | Max | 0. | 0. | 128.3696 |
| 11 | 2.10446 | SLU_2 | Max | 0. | 0. | 151.5426 |
| 11 | 0. | SLU_2 | Min | 0. | 0. | -117.2771 |
| 11 | 1.05223 | SLU_2 | Min | 0. | 0. | 128.3696 |
| 11 | 2.10446 | SLU_2 | Min | 0. | 0. | 151.5426 |
| 11 | 0. | SLU_3 | Max | 0. | 0. | 358.2772 |
| 11 | 1.05223 | SLU_3 | Max | 0. | 0. | 573.912 |
| 11 | 2.10446 | SLU_3 | Max | 0. | 0. | 482.7281 |
| 11 | 0. | SLU_3 | Min | 0. | 0. | 358.2772 |
| 11 | 1.05223 | SLU_3 | Min | 0. | 0. | 573.912 |
| 11 | 2.10446 | SLU_3 | Min | 0. | 0. | 482.7281 |
| 11 | 0. | SLU_4 | Max | 0. | 0. | 146.2168 |
| 11 | 1.05223 | SLU_4 | Max | 0. | 0. | 442.4986 |
| 11 | 2.10446 | SLU_4 | Max | 0. | 0. | 452.5272 |
| 11 | 0. | SLU_4 | Min | 0. | 0. | 146.2168 |
| 11 | 1.05223 | SLU_4 | Min | 0. | 0. | 442.4986 |
| 11 | 2.10446 | SLU_4 | Min | 0. | 0. | 452.5272 |
| 11 | 0. | SLE_F1 | Max | 0. | 0. | 12.4753 |
| 11 | 1.05223 | SLE_F1 | Max | 0. | 0. | 139.798 |
| 11 | 2.10446 | SLE_F1 | Max | 0. | 0. | 92.8985 |
| 11 | 0. | SLE_F1 | Min | 0. | 0. | 12.4753 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 11 | 1.05223 | SLE_F1 | Min | 0. | 0. | 139.798 |
| 11 | 2.10446 | SLE_F1 | Min | 0. | 0. | 92.8985 |
| 11 | 0. | SLE_F2 | Max | 0. | 0. | -74.9185 |
| 11 | 1.05223 | SLE_F2 | Max | 0. | 0. | 98.4289 |
| 11 | 2.10446 | SLE_F2 | Max | 0. | 0. | 109.5314 |
| 11 | 0. | SLE_F2 | Min | 0. | 0. | -74.9185 |
| 11 | 1.05223 | SLE_F2 | Min | 0. | 0. | 98.4289 |
| 11 | 2.10446 | SLE_F2 | Min | 0. | 0. | 109.5314 |
| 11 | 0. | SLE_F3 | Max | 0. | 0. | 127.9965 |
| 11 | 1.05223 | SLE_F3 | Max | 0. | 0. | 339.9711 |
| 11 | 2.10446 | SLE_F3 | Max | 0. | 0. | 340.6397 |
| 11 | 0. | SLE_F3 | Min | 0. | 0. | 127.9965 |
| 11 | 1.05223 | SLE_F3 | Min | 0. | 0. | 339.9711 |
| 11 | 2.10446 | SLE_F3 | Min | 0. | 0. | 340.6397 |
| 11 | 0. | SLE_F4 | Max | 0. | 0. | 286.3275 |
| 11 | 1.05223 | SLE_F4 | Max | 0. | 0. | 437.109 |
| 11 | 2.10446 | SLE_F4 | Max | 0. | 0. | 361.6795 |
| 11 | 0. | SLE_F4 | Min | 0. | 0. | 286.3275 |
| 11 | 1.05223 | SLE_F4 | Min | 0. | 0. | 437.109 |
| 11 | 2.10446 | SLE_F4 | Min | 0. | 0. | 361.6795 |
| 11 | 0. | SLE_QP1 | Max | 0. | 0. | 30.0864 |
| 11 | 1.05223 | SLE_QP1 | Max | 0. | 0. | 133.2677 |
| 11 | 2.10446 | SLE_QP1 | Max | 0. | 0. | 80.4329 |
| 11 | 0. | SLE_QP1 | Min | 0. | 0. | 30.0864 |
| 11 | 1.05223 | SLE_QP1 | Min | 0. | 0. | 133.2677 |
| 11 | 2.10446 | SLE_QP1 | Min | 0. | 0. | 80.4329 |
| 11 | 0. | SLE_QP2 | Max | 0. | 0. | -46.5149 |
| 11 | 1.05223 | SLE_QP2 | Max | 0. | 0. | 97.8386 |
| 11 | 2.10446 | SLE_QP2 | Max | 0. | 0. | 96.4551 |
| 11 | 0. | SLE_QP2 | Min | 0. | 0. | -46.5149 |
| 11 | 1.05223 | SLE_QP2 | Min | 0. | 0. | 97.8386 |
| 11 | 2.10446 | SLE_QP2 | Min | 0. | 0. | 96.4551 |
| 11 | 0. | SLE_QP3 | Max | 0. | 0. | 156.8225 |
| 11 | 1.05223 | SLE_QP3 | Max | 0. | 0. | 339.2043 |
| 11 | 2.10446 | SLE_QP3 | Max | 0. | 0. | 326.7878 |
| 11 | 0. | SLE_QP3 | Min | 0. | 0. | 156.8225 |
| 11 | 1.05223 | SLE_QP3 | Min | 0. | 0. | 339.2043 |
| 11 | 2.10446 | SLE_QP3 | Min | 0. | 0. | 326.7878 |
| 11 | 0. | SLE_QP4 | Max | 0. | 0. | 305.926 |
| 11 | 1.05223 | SLE_QP4 | Max | 0. | 0. | 428.4135 |
| 11 | 2.10446 | SLE_QP4 | Max | 0. | 0. | 342.8962 |
| 11 | 0. | SLE_QP4 | Min | 0. | 0. | 305.926 |
| 11 | 1.05223 | SLE_QP4 | Min | 0. | 0. | 428.4135 |
| 11 | 2.10446 | SLE_QP4 | Min | 0. | 0. | 342.8962 |
| 11 | 0. | SLV_1 | Max | 0. | 0. | 663.0328 |
| 11 | 1.05223 | SLV_1 | Max | 0. | 0. | 592.2464 |
| 11 | 2.10446 | SLV_1 | Max | 0. | 0. | 318.0169 |
| 11 | 0. | SLV_1 | Min | 0. | 0. | 663.0328 |
| 11 | 1.05223 | SLV_1 | Min | 0. | 0. | 592.2464 |
| 11 | 2.10446 | SLV_1 | Min | 0. | 0. | 318.0169 |
| 11 | 0. | SLV_2 | Max | 0. | 0. | 663.4391 |
| 11 | 1.05223 | SLV_2 | Max | 0. | 0. | 591.2021 |
| 11 | 2.10446 | SLV_2 | Max | 0. | 0. | 315.5219 |
| 11 | 0. | SLV_2 | Min | 0. | 0. | 663.4391 |
| 11 | 1.05223 | SLV_2 | Min | 0. | 0. | 591.2021 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 11 | 2.10446 | SLV_2 | Min | 0. | 0. | 315.5219 |
| 11 | 0. | SLV_3 | Max | 0. | 0. | 908.3757 |
| 11 | 1.05223 | SLV_3 | Max | 0. | 0. | 839.6025 |
| 11 | 2.10446 | SLV_3 | Max | 0. | 0. | 515.3973 |
| 11 | 0. | SLV_3 | Min | 0. | 0. | 908.3757 |
| 11 | 1.05223 | SLV_3 | Min | 0. | 0. | 839.6025 |
| 11 | 2.10446 | SLV_3 | Min | 0. | 0. | 515.3973 |
| 11 | 0. | SLV_4 | Max | 0. | 0. | 909.3337 |
| 11 | 1.05223 | SLV_4 | Max | 0. | 0. | 838.9104 |
| 11 | 2.10446 | SLV_4 | Max | 0. | 0. | 513.0552 |
| 11 | 0. | SLV_4 | Min | 0. | 0. | 909.3337 |
| 11 | 1.05223 | SLV_4 | Min | 0. | 0. | 838.9104 |
| 11 | 2.10446 | SLV_4 | Min | 0. | 0. | 513.0552 |
| 11 | 0. | SLD_1 | Max | 0. | 0. | 337.1889 |
| 11 | 1.05223 | SLD_1 | Max | 0. | 0. | 372.6316 |
| 11 | 2.10446 | SLD_1 | Max | 0. | 0. | 231.1125 |
| 11 | 0. | SLD_1 | Min | 0. | 0. | 337.1889 |
| 11 | 1.05223 | SLD_1 | Min | 0. | 0. | 372.6316 |
| 11 | 2.10446 | SLD_1 | Min | 0. | 0. | 231.1125 |
| 11 | 0. | SLD_2 | Max | 0. | 0. | 337.8397 |
| 11 | 1.05223 | SLD_2 | Max | 0. | 0. | 372.6547 |
| 11 | 2.10446 | SLD_2 | Max | 0. | 0. | 230.5079 |
| 11 | 0. | SLD_2 | Min | 0. | 0. | 337.8397 |
| 11 | 1.05223 | SLD_2 | Min | 0. | 0. | 372.6547 |
| 11 | 2.10446 | SLD_2 | Min | 0. | 0. | 230.5079 |
| 11 | 0. | SLD_3 | Max | 0. | 0. | 593.3996 |
| 11 | 1.05223 | SLD_3 | Max | 0. | 0. | 627.6867 |
| 11 | 2.10446 | SLD_3 | Max | 0. | 0. | 433.0232 |
| 11 | 0. | SLD_3 | Min | 0. | 0. | 593.3996 |
| 11 | 1.05223 | SLD_3 | Min | 0. | 0. | 627.6867 |
| 11 | 2.10446 | SLD_3 | Min | 0. | 0. | 433.0232 |
| 11 | 0. | SLD_4 | Max | 0. | 0. | 593.9872 |
| 11 | 1.05223 | SLD_4 | Max | 0. | 0. | 627.5426 |
| 11 | 2.10446 | SLD_4 | Max | 0. | 0. | 432.1474 |
| 11 | 0. | SLD_4 | Min | 0. | 0. | 593.9872 |
| 11 | 1.05223 | SLD_4 | Min | 0. | 0. | 627.5426 |
| 11 | 2.10446 | SLD_4 | Min | 0. | 0. | 432.1474 |
| 11 | 0. | SLU_IDR_1 | Max | 0. | 0. | 153.3255 |
| 11 | 1.05223 | SLU_IDR_1 | Max | 0. | 0. | 321.3516 |
| 11 | 2.10446 | SLU_IDR_1 | Max | 0. | 0. | 305.0534 |
| 11 | 0. | SLU_IDR_1 | Min | 0. | 0. | 153.3255 |
| 11 | 1.05223 | SLU_IDR_1 | Min | 0. | 0. | 321.3516 |
| 11 | 2.10446 | SLU_IDR_1 | Min | 0. | 0. | 305.0534 |
| 11 | 0. | SLU_IDR_2 | Max | 0. | 0. | -30.3513 |
| 11 | 1.05223 | SLU_IDR_2 | Max | 0. | 0. | 104.7531 |
| 11 | 2.10446 | SLU_IDR_2 | Max | 0. | 0. | 99.6884 |
| 11 | 0. | SLU_IDR_2 | Min | 0. | 0. | -30.3513 |
| 11 | 1.05223 | SLU_IDR_2 | Min | 0. | 0. | 104.7531 |
| 11 | 2.10446 | SLU_IDR_2 | Min | 0. | 0. | 99.6884 |
| 11 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 400.4262 |
| 11 | 1.05223 | SISMA WOOD SLV-1 | Max | 0. | 0. | 234.0938 |
| 11 | 2.10446 | SISMA WOOD SLV-1 | Max | 0. | 0. | 20.3343 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 11 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 400.4262 |
| 11 | 1.05223 | SISMA WOOD SLV-1 | Min | 0. | 0. | 234.0938 |
| 11 | 2.10446 | SISMA WOOD SLV-1 | Min | 0. | 0. | 20.3343 |
| 11 | 0. | DEAD-1 | Max | 0. | 0. | -78.029 |
| 11 | 1.05223 | DEAD-1 | Max | 0. | 0. | -19.4675 |
| 11 | 2.10446 | DEAD-1 | Max | 0. | 0. | 17.2575 |
| 11 | 0. | DEAD-1 | Min | 0. | 0. | -78.029 |
| 11 | 1.05223 | DEAD-1 | Min | 0. | 0. | -19.4675 |
| 11 | 2.10446 | DEAD-1 | Min | 0. | 0. | 17.2575 |
| 11 | 0. | SLU_PROVA | | 0. | 0. | 83.4304 |
| 11 | 1.05223 | SLU_PROVA | | 0. | 0. | 212.0359 |
| 11 | 2.10446 | SLU_PROVA | | 0. | 0. | 101.4081 |
| 12 | 0. | DEAD | | 0. | 0. | 10.1181 |
| 12 | 1.04817 | DEAD | | 0. | 0. | 47.043 |
| 12 | 2.09633 | DEAD | | 0. | 0. | 58.6373 |
| 12 | 0. | SIMM_KA | | 0. | 0. | -28.3699 |
| 12 | 1.04817 | SIMM_KA | | 0. | 0. | -80.5118 |
| 12 | 2.09633 | SIMM_KA | | 0. | 0. | -141.4439 |
| 12 | 0. | SIMM_K0 | | 0. | 0. | -40.4678 |
| 12 | 1.04817 | SIMM_K0 | | 0. | 0. | -123.1396 |
| 12 | 2.09633 | SIMM_K0 | | 0. | 0. | -220.5849 |
| 12 | 0. | A--SIMM_KA | | 0. | 0. | 3.1804 |
| 12 | 1.04817 | A--SIMM_KA | | 0. | 0. | -74.0221 |
| 12 | 2.09633 | A--SIMM_KA | | 0. | 0. | -164.3719 |
| 12 | 0. | A--SIMM_K0 | | 0. | 0. | 4.4332 |
| 12 | 1.04817 | A--SIMM_K0 | | 0. | 0. | -112.2301 |
| 12 | 2.09633 | A--SIMM_K0 | | 0. | 0. | -248.6152 |
| 12 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -0.9244 |
| 12 | 1.04817 | A-- SIMM_SOVR_K A | | 0. | 0. | -12.2561 |
| 12 | 2.09633 | A-- SIMM_SOVR_K A | | 0. | 0. | -26.4162 |
| 12 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -1.3859 |
| 12 | 1.04817 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -18.375 |
| 12 | 2.09633 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -39.6045 |
| 12 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -1.3859 |
| 12 | 1.04817 | SIMM_SOVR_K 0 | | 0. | 0. | -18.375 |
| 12 | 2.09633 | SIMM_SOVR_K 0 | | 0. | 0. | -39.6045 |
| 12 | 0. | SIMM_SOVR_K A | | 0. | 0. | -0.9244 |
| 12 | 1.04817 | SIMM_SOVR_K A | | 0. | 0. | -12.2561 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 12 | 2.09633 | SIMM_SOVR_K A | | 0. | 0. | -26.4162 |
| 12 | 0. | SOVR | | 0. | 0. | 17.2634 |
| 12 | 1.04817 | SOVR | | 0. | 0. | 51.6309 |
| 12 | 2.09633 | SOVR | | 0. | 0. | 65.7279 |
| 12 | 0. | TERR_SIMM | | 0. | 0. | 68.5512 |
| 12 | 1.04817 | TERR_SIMM | | 0. | 0. | 162.3027 |
| 12 | 2.09633 | TERR_SIMM | | 0. | 0. | 193.1802 |
| 12 | 0. | TERR_A--SIMM | | 0. | 0. | 180.8821 |
| 12 | 1.04817 | TERR_A--SIMM | | 0. | 0. | 292.6776 |
| 12 | 2.09633 | TERR_A--SIMM | | 0. | 0. | 310.1951 |
| 12 | 0. | INERZIA H SLV | | 0. | 0. | 4.2767 |
| 12 | 1.04817 | INERZIA H SLV | | 0. | 0. | 3.4207 |
| 12 | 2.09633 | INERZIA H SLV | | 0. | 0. | 2.5648 |
| 12 | 0. | INERZIA V + SLV | | 0. | 0. | 0.2913 |
| 12 | 1.04817 | INERZIA V + SLV | | 0. | 0. | 0.6913 |
| 12 | 2.09633 | INERZIA V + SLV | | 0. | 0. | 1.0914 |
| 12 | 0. | INERZIA V - SLV | | 0. | 0. | -0.2913 |
| 12 | 1.04817 | INERZIA V - SLV | | 0. | 0. | -0.6913 |
| 12 | 2.09633 | INERZIA V - SLV | | 0. | 0. | -1.0914 |
| 12 | 0. | SISMA WOOD SLV | | 0. | 0. | 183.3007 |
| 12 | 1.04817 | SISMA WOOD SLV | | 0. | 0. | 85.1518 |
| 12 | 2.09633 | SISMA WOOD SLV | | 0. | 0. | -42.5693 |
| 12 | 0. | iDROSTATICA | | 0. | 0. | 21.4845 |
| 12 | 1.04817 | iDROSTATICA | | 0. | 0. | 3.9509 |
| 12 | 2.09633 | iDROSTATICA | | 0. | 0. | -44.8229 |
| 12 | 0. | SISMA WOOD SLD | | 0. | 0. | 80.953 |
| 12 | 1.04817 | SISMA WOOD SLD | | 0. | 0. | 37.6065 |
| 12 | 2.09633 | SISMA WOOD SLD | | 0. | 0. | -18.8003 |
| 12 | 0. | INERZIA H SLD | | 0. | 0. | 1.8888 |
| 12 | 1.04817 | INERZIA H SLD | | 0. | 0. | 1.5107 |
| 12 | 2.09633 | INERZIA H SLD | | 0. | 0. | 1.1327 |
| 12 | 0. | INERZIA V + SLD | | 0. | 0. | 0.1286 |
| 12 | 1.04817 | INERZIA V + SLD | | 0. | 0. | 0.3053 |
| 12 | 2.09633 | INERZIA V + SLD | | 0. | 0. | 0.482 |
| 12 | 0. | INERZIA V SLD | | 0. | 0. | -0.1286 |
| 12 | 1.04817 | INERZIA V SLD | | 0. | 0. | -0.3053 |
| 12 | 2.09633 | INERZIA V SLD | | 0. | 0. | -0.482 |
| 12 | 0. | INERZIA V -1 | | 0. | 0. | -0.2913 |
| 12 | 1.04817 | INERZIA V -1 | | 0. | 0. | -0.6913 |
| 12 | 2.09633 | INERZIA V -1 | | 0. | 0. | -1.0914 |
| 12 | 0. | SLU_1 | Max | 0. | 0. | 130.2179 |
| 12 | 1.04817 | SLU_1 | Max | 0. | 0. | 237.8578 |
| 12 | 2.09633 | SLU_1 | Max | 0. | 0. | 134.2478 |
| 12 | 0. | SLU_1 | Min | 0. | 0. | 130.2179 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 12 | 1.04817 | SLU_1 | Min | 0. | 0. | 237.8578 |
| 12 | 2.09633 | SLU_1 | Min | 0. | 0. | 134.2478 |
| 12 | 0. | SLU_2 | Max | 0. | 0. | 151.5426 |
| 12 | 1.04817 | SLU_2 | Max | 0. | 0. | 319.7341 |
| 12 | 2.09633 | SLU_2 | Max | 0. | 0. | 286.5718 |
| 12 | 0. | SLU_2 | Min | 0. | 0. | 151.5426 |
| 12 | 1.04817 | SLU_2 | Min | 0. | 0. | 319.7341 |
| 12 | 2.09633 | SLU_2 | Min | 0. | 0. | 286.5718 |
| 12 | 0. | SLU_3 | Max | 0. | 0. | 482.7281 |
| 12 | 1.04817 | SLU_3 | Max | 0. | 0. | 542.6754 |
| 12 | 2.09633 | SLU_3 | Max | 0. | 0. | 344.1145 |
| 12 | 0. | SLU_3 | Min | 0. | 0. | 482.7281 |
| 12 | 1.04817 | SLU_3 | Min | 0. | 0. | 542.6754 |
| 12 | 2.09633 | SLU_3 | Min | 0. | 0. | 344.1145 |
| 12 | 0. | SLU_4 | Max | 0. | 0. | 452.5272 |
| 12 | 1.04817 | SLU_4 | Max | 0. | 0. | 594.3824 |
| 12 | 2.09633 | SLU_4 | Max | 0. | 0. | 488.3945 |
| 12 | 0. | SLU_4 | Min | 0. | 0. | 452.5272 |
| 12 | 1.04817 | SLU_4 | Min | 0. | 0. | 594.3824 |
| 12 | 2.09633 | SLU_4 | Min | 0. | 0. | 488.3945 |
| 12 | 0. | SLE_F1 | Max | 0. | 0. | 92.8985 |
| 12 | 1.04817 | SLE_F1 | Max | 0. | 0. | 166.538 |
| 12 | 2.09633 | SLE_F1 | Max | 0. | 0. | 87.576 |
| 12 | 0. | SLE_F1 | Min | 0. | 0. | 92.8985 |
| 12 | 1.04817 | SLE_F1 | Min | 0. | 0. | 166.538 |
| 12 | 2.09633 | SLE_F1 | Min | 0. | 0. | 87.576 |
| 12 | 0. | SLE_F2 | Max | 0. | 0. | 109.5314 |
| 12 | 1.04817 | SLE_F2 | Max | 0. | 0. | 227.0238 |
| 12 | 2.09633 | SLE_F2 | Max | 0. | 0. | 198.957 |
| 12 | 0. | SLE_F2 | Min | 0. | 0. | 109.5314 |
| 12 | 1.04817 | SLE_F2 | Min | 0. | 0. | 227.0238 |
| 12 | 2.09633 | SLE_F2 | Min | 0. | 0. | 198.957 |
| 12 | 0. | SLE_F3 | Max | 0. | 0. | 340.6397 |
| 12 | 1.04817 | SLE_F3 | Max | 0. | 0. | 437.6825 |
| 12 | 2.09633 | SLE_F3 | Max | 0. | 0. | 353.405 |
| 12 | 0. | SLE_F3 | Min | 0. | 0. | 340.6397 |
| 12 | 1.04817 | SLE_F3 | Min | 0. | 0. | 437.6825 |
| 12 | 2.09633 | SLE_F3 | Min | 0. | 0. | 353.405 |
| 12 | 0. | SLE_F4 | Max | 0. | 0. | 361.6795 |
| 12 | 1.04817 | SLE_F4 | Max | 0. | 0. | 397.4754 |
| 12 | 2.09633 | SLE_F4 | Max | 0. | 0. | 244.3174 |
| 12 | 0. | SLE_F4 | Min | 0. | 0. | 361.6795 |
| 12 | 1.04817 | SLE_F4 | Min | 0. | 0. | 397.4754 |
| 12 | 2.09633 | SLE_F4 | Min | 0. | 0. | 244.3174 |
| 12 | 0. | SLE_QP1 | Max | 0. | 0. | 80.4329 |
| 12 | 1.04817 | SLE_QP1 | Max | 0. | 0. | 137.1562 |
| 12 | 2.09633 | SLE_QP1 | Max | 0. | 0. | 59.6612 |
| 12 | 0. | SLE_QP1 | Min | 0. | 0. | 80.4329 |
| 12 | 1.04817 | SLE_QP1 | Min | 0. | 0. | 137.1562 |
| 12 | 2.09633 | SLE_QP1 | Min | 0. | 0. | 59.6612 |
| 12 | 0. | SLE_QP2 | Max | 0. | 0. | 96.4551 |
| 12 | 1.04817 | SLE_QP2 | Max | 0. | 0. | 191.8736 |
| 12 | 2.09633 | SLE_QP2 | Max | 0. | 0. | 159.057 |
| 12 | 0. | SLE_QP2 | Min | 0. | 0. | 96.4551 |
| 12 | 1.04817 | SLE_QP2 | Min | 0. | 0. | 191.8736 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 12 | 2.09633 | SLE_QP2 | Min | 0. | 0. | 159.057 |
| 12 | 0. | SLE_QP3 | Max | 0. | 0. | 326.7878 |
| 12 | 1.04817 | SLE_QP3 | Max | 0. | 0. | 401.4024 |
| 12 | 2.09633 | SLE_QP3 | Max | 0. | 0. | 312.0208 |
| 12 | 0. | SLE_QP3 | Min | 0. | 0. | 326.7878 |
| 12 | 1.04817 | SLE_QP3 | Min | 0. | 0. | 401.4024 |
| 12 | 2.09633 | SLE_QP3 | Min | 0. | 0. | 312.0208 |
| 12 | 0. | SLE_QP4 | Max | 0. | 0. | 342.8962 |
| 12 | 1.04817 | SLE_QP4 | Max | 0. | 0. | 359.4416 |
| 12 | 2.09633 | SLE_QP4 | Max | 0. | 0. | 205.4162 |
| 12 | 0. | SLE_QP4 | Min | 0. | 0. | 342.8962 |
| 12 | 1.04817 | SLE_QP4 | Min | 0. | 0. | 359.4416 |
| 12 | 2.09633 | SLE_QP4 | Min | 0. | 0. | 205.4162 |
| 12 | 0. | SLV_1 | Max | 0. | 0. | 318.0169 |
| 12 | 1.04817 | SLV_1 | Max | 0. | 0. | 159.9937 |
| 12 | 2.09633 | SLV_1 | Max | 0. | 0. | -161.8199 |
| 12 | 0. | SLV_1 | Min | 0. | 0. | 318.0169 |
| 12 | 1.04817 | SLV_1 | Min | 0. | 0. | 159.9937 |
| 12 | 2.09633 | SLV_1 | Min | 0. | 0. | -161.8199 |
| 12 | 0. | SLV_2 | Max | 0. | 0. | 315.5219 |
| 12 | 1.04817 | SLV_2 | Max | 0. | 0. | 156.7288 |
| 12 | 2.09633 | SLV_2 | Max | 0. | 0. | -165.8548 |
| 12 | 0. | SLV_2 | Min | 0. | 0. | 315.5219 |
| 12 | 1.04817 | SLV_2 | Min | 0. | 0. | 156.7288 |
| 12 | 2.09633 | SLV_2 | Min | 0. | 0. | -165.8548 |
| 12 | 0. | SLV_3 | Max | 0. | 0. | 515.3973 |
| 12 | 1.04817 | SLV_3 | Max | 0. | 0. | 314.2336 |
| 12 | 2.09633 | SLV_3 | Max | 0. | 0. | -87.0731 |
| 12 | 0. | SLV_3 | Min | 0. | 0. | 515.3973 |
| 12 | 1.04817 | SLV_3 | Min | 0. | 0. | 314.2336 |
| 12 | 2.09633 | SLV_3 | Min | 0. | 0. | -87.0731 |
| 12 | 0. | SLV_4 | Max | 0. | 0. | 513.0552 |
| 12 | 1.04817 | SLV_4 | Max | 0. | 0. | 310.8807 |
| 12 | 2.09633 | SLV_4 | Max | 0. | 0. | -91.4368 |
| 12 | 0. | SLV_4 | Min | 0. | 0. | 513.0552 |
| 12 | 1.04817 | SLV_4 | Min | 0. | 0. | 310.8807 |
| 12 | 2.09633 | SLV_4 | Min | 0. | 0. | -91.4368 |
| 12 | 0. | SLD_1 | Max | 0. | 0. | 231.1125 |
| 12 | 1.04817 | SLD_1 | Max | 0. | 0. | 192.3805 |
| 12 | 2.09633 | SLD_1 | Max | 0. | 0. | 6.37 |
| 12 | 0. | SLD_1 | Min | 0. | 0. | 231.1125 |
| 12 | 1.04817 | SLD_1 | Min | 0. | 0. | 192.3805 |
| 12 | 2.09633 | SLD_1 | Min | 0. | 0. | 6.37 |
| 12 | 0. | SLD_2 | Max | 0. | 0. | 230.5079 |
| 12 | 1.04817 | SLD_2 | Max | 0. | 0. | 191.3166 |
| 12 | 2.09633 | SLD_2 | Max | 0. | 0. | 4.8467 |
| 12 | 0. | SLD_2 | Min | 0. | 0. | 230.5079 |
| 12 | 1.04817 | SLD_2 | Min | 0. | 0. | 191.3166 |
| 12 | 2.09633 | SLD_2 | Min | 0. | 0. | 4.8467 |
| 12 | 0. | SLD_3 | Max | 0. | 0. | 433.0232 |
| 12 | 1.04817 | SLD_3 | Max | 0. | 0. | 347.4025 |
| 12 | 2.09633 | SLD_3 | Max | 0. | 0. | 78.1507 |
| 12 | 0. | SLD_3 | Min | 0. | 0. | 433.0232 |
| 12 | 1.04817 | SLD_3 | Min | 0. | 0. | 347.4025 |
| 12 | 2.09633 | SLD_3 | Min | 0. | 0. | 78.1507 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 12 | 0. | SLD_4 | Max | 0. | 0. | 432.1474 |
| 12 | 1.04817 | SLD_4 | Max | 0. | 0. | 346.0435 |
| 12 | 2.09633 | SLD_4 | Max | 0. | 0. | 76.3085 |
| 12 | 0. | SLD_4 | Min | 0. | 0. | 432.1474 |
| 12 | 1.04817 | SLD_4 | Min | 0. | 0. | 346.0435 |
| 12 | 2.09633 | SLD_4 | Min | 0. | 0. | 76.3085 |
| 12 | 0. | SLU_IDR_1 | Max | 0. | 0. | 305.0534 |
| 12 | 1.04817 | SLU_IDR_1 | Max | 0. | 0. | 372.0952 |
| 12 | 2.09633 | SLU_IDR_1 | Max | 0. | 0. | 285.2925 |
| 12 | 0. | SLU_IDR_1 | Min | 0. | 0. | 305.0534 |
| 12 | 1.04817 | SLU_IDR_1 | Min | 0. | 0. | 372.0952 |
| 12 | 2.09633 | SLU_IDR_1 | Min | 0. | 0. | 285.2925 |
| 12 | 0. | SLU_IDR_2 | Max | 0. | 0. | 99.6884 |
| 12 | 1.04817 | SLU_IDR_2 | Max | 0. | 0. | 186.2141 |
| 12 | 2.09633 | SLU_IDR_2 | Max | 0. | 0. | 151.0801 |
| 12 | 0. | SLU_IDR_2 | Min | 0. | 0. | 99.6884 |
| 12 | 1.04817 | SLU_IDR_2 | Min | 0. | 0. | 186.2141 |
| 12 | 2.09633 | SLU_IDR_2 | Min | 0. | 0. | 151.0801 |
| 12 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 20.3343 |
| 12 | 1.04817 | SISMA WOOD SLV-1 | Max | 0. | 0. | -131.8788 |
| 12 | 2.09633 | SISMA WOOD SLV-1 | Max | 0. | 0. | -313.6641 |
| 12 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 20.3343 |
| 12 | 1.04817 | SISMA WOOD SLV-1 | Min | 0. | 0. | -131.8788 |
| 12 | 2.09633 | SISMA WOOD SLV-1 | Min | 0. | 0. | -313.6641 |
| 12 | 0. | DEAD-1 | Max | 0. | 0. | 17.2575 |
| 12 | 1.04817 | DEAD-1 | Max | 0. | 0. | 67.5241 |
| 12 | 2.09633 | DEAD-1 | Max | 0. | 0. | 92.46 |
| 12 | 0. | DEAD-1 | Min | 0. | 0. | 17.2575 |
| 12 | 1.04817 | DEAD-1 | Min | 0. | 0. | 67.5241 |
| 12 | 2.09633 | DEAD-1 | Min | 0. | 0. | 92.46 |
| 12 | 0. | SLU_PROVA | | 0. | 0. | 101.4081 |
| 12 | 1.04817 | SLU_PROVA | | 0. | 0. | 167.0878 |
| 12 | 2.09633 | SLU_PROVA | | 0. | 0. | 21.5176 |
| 13 | 0. | DEAD | | 0. | 0. | 58.6373 |
| 13 | 1.04614 | DEAD | | 0. | 0. | 81.2993 |
| 13 | 2.09228 | DEAD | | 0. | 0. | 76.8299 |
| 13 | 0. | SIMM_KA | | 0. | 0. | -141.4439 |
| 13 | 1.04614 | SIMM_KA | | 0. | 0. | -163.1269 |
| 13 | 2.09228 | SIMM_KA | | 0. | 0. | -187.5746 |
| 13 | 0. | SIMM_K0 | | 0. | 0. | -220.5849 |
| 13 | 1.04614 | SIMM_K0 | | 0. | 0. | -255.369 |
| 13 | 2.09228 | SIMM_K0 | | 0. | 0. | -294.4554 |
| 13 | 0. | A--SIMM_KA | | 0. | 0. | -164.3719 |
| 13 | 1.04614 | A--SIMM_KA | | 0. | 0. | -200.4628 |
| 13 | 2.09228 | A--SIMM_KA | | 0. | 0. | -240.2173 |
| 13 | 0. | A--SIMM_K0 | | 0. | 0. | -248.6152 |
| 13 | 1.04614 | A--SIMM_K0 | | 0. | 0. | -303.2687 |
| 13 | 2.09228 | A--SIMM_K0 | | 0. | 0. | -363.4175 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 13 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -26.4162 |
| 13 | 1.04614 | A-- SIMM_SOVR_K A | | 0. | 0. | -31.7924 |
| 13 | 2.09228 | A-- SIMM_SOVR_K A | | 0. | 0. | -38.0939 |
| 13 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -39.6045 |
| 13 | 1.04614 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -47.6648 |
| 13 | 2.09228 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -57.1122 |
| 13 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -39.6045 |
| 13 | 1.04614 | SIMM_SOVR_K 0 | | 0. | 0. | -47.6648 |
| 13 | 2.09228 | SIMM_SOVR_K 0 | | 0. | 0. | -57.1122 |
| 13 | 0. | SIMM_SOVR_K A | | 0. | 0. | -26.4162 |
| 13 | 1.04614 | SIMM_SOVR_K A | | 0. | 0. | -31.7924 |
| 13 | 2.09228 | SIMM_SOVR_K A | | 0. | 0. | -38.0939 |
| 13 | 0. | SOVR | | 0. | 0. | 65.7279 |
| 13 | 1.04614 | SOVR | | 0. | 0. | 85.5433 |
| 13 | 2.09228 | SOVR | | 0. | 0. | 83.6473 |
| 13 | 0. | TERR_SIMM | | 0. | 0. | 193.1802 |
| 13 | 1.04614 | TERR_SIMM | | 0. | 0. | 248.1216 |
| 13 | 2.09228 | TERR_SIMM | | 0. | 0. | 238.482 |
| 13 | 0. | TERR_A--SIMM | | 0. | 0. | 310.1951 |
| 13 | 1.04614 | TERR_A--SIMM | | 0. | 0. | 353.1045 |
| 13 | 2.09228 | TERR_A--SIMM | | 0. | 0. | 309.9981 |
| 13 | 0. | INERZIA H SLV | | 0. | 0. | 2.5648 |
| 13 | 1.04614 | INERZIA H SLV | | 0. | 0. | 1.2856 |
| 13 | 2.09228 | INERZIA H SLV | | 0. | 0. | 0.0065 |
| 13 | 0. | INERZIA V + SLV | | 0. | 0. | 1.0914 |
| 13 | 1.04614 | INERZIA V + SLV | | 0. | 0. | 1.241 |
| 13 | 2.09228 | INERZIA V + SLV | | 0. | 0. | 1.3906 |
| 13 | 0. | INERZIA V - SLV | | 0. | 0. | -1.0914 |
| 13 | 1.04614 | INERZIA V - SLV | | 0. | 0. | -1.241 |
| 13 | 2.09228 | INERZIA V - SLV | | 0. | 0. | -1.3906 |
| 13 | 0. | SISMA WOOD SLV | | 0. | 0. | -42.5693 |
| 13 | 1.04614 | SISMA WOOD SLV | | 0. | 0. | -130.7727 |
| 13 | 2.09228 | SISMA WOOD SLV | | 0. | 0. | -228.6503 |
| 13 | 0. | iDROSTATICA | | 0. | 0. | -44.8229 |
| 13 | 1.04614 | iDROSTATICA | | 0. | 0. | -45.4686 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 13 | 2.09228 | iDROSTATICA | | 0. | 0. | -69.1844 |
| 13 | 0. | SISMA WOOD SLD | | 0. | 0. | -18.8003 |
| 13 | 1.04614 | SISMA WOOD SLD | | 0. | 0. | -57.7545 |
| 13 | 2.09228 | SISMA WOOD SLD | | 0. | 0. | -100.9812 |
| 13 | 0. | INERZIA H SLD | | 0. | 0. | 1.1327 |
| 13 | 1.04614 | INERZIA H SLD | | 0. | 0. | 0.5678 |
| 13 | 2.09228 | INERZIA H SLD | | 0. | 0. | 0.0029 |
| 13 | 0. | INERZIA V + SLD | | 0. | 0. | 0.482 |
| 13 | 1.04614 | INERZIA V + SLD | | 0. | 0. | 0.5481 |
| 13 | 2.09228 | INERZIA V + SLD | | 0. | 0. | 0.6141 |
| 13 | 0. | INERZIA V SLD | | 0. | 0. | -0.482 |
| 13 | 1.04614 | INERZIA V SLD | | 0. | 0. | -0.5481 |
| 13 | 2.09228 | INERZIA V SLD | | 0. | 0. | -0.6141 |
| 13 | 0. | INERZIA V -1 | | 0. | 0. | -1.0914 |
| 13 | 1.04614 | INERZIA V -1 | | 0. | 0. | -1.241 |
| 13 | 2.09228 | INERZIA V -1 | | 0. | 0. | -1.3906 |
| 13 | 0. | SLU_1 | Max | 0. | 0. | 134.2478 |
| 13 | 1.04614 | SLU_1 | Max | 0. | 0. | 224.3138 |
| 13 | 2.09228 | SLU_1 | Max | 0. | 0. | 124.9215 |
| 13 | 0. | SLU_1 | Min | 0. | 0. | 134.2478 |
| 13 | 1.04614 | SLU_1 | Min | 0. | 0. | 224.3138 |
| 13 | 2.09228 | SLU_1 | Min | 0. | 0. | 124.9215 |
| 13 | 0. | SLU_2 | Max | 0. | 0. | 286.5718 |
| 13 | 1.04614 | SLU_2 | Max | 0. | 0. | 402.5785 |
| 13 | 2.09228 | SLU_2 | Max | 0. | 0. | 331.8188 |
| 13 | 0. | SLU_2 | Min | 0. | 0. | 286.5718 |
| 13 | 1.04614 | SLU_2 | Min | 0. | 0. | 402.5785 |
| 13 | 2.09228 | SLU_2 | Min | 0. | 0. | 331.8188 |
| 13 | 0. | SLU_3 | Max | 0. | 0. | 344.1145 |
| 13 | 1.04614 | SLU_3 | Max | 0. | 0. | 347.3809 |
| 13 | 2.09228 | SLU_3 | Max | 0. | 0. | 131.773 |
| 13 | 0. | SLU_3 | Min | 0. | 0. | 344.1145 |
| 13 | 1.04614 | SLU_3 | Min | 0. | 0. | 347.3809 |
| 13 | 2.09228 | SLU_3 | Min | 0. | 0. | 131.773 |
| 13 | 0. | SLU_4 | Max | 0. | 0. | 488.3945 |
| 13 | 1.04614 | SLU_4 | Max | 0. | 0. | 536.576 |
| 13 | 2.09228 | SLU_4 | Max | 0. | 0. | 368.9574 |
| 13 | 0. | SLU_4 | Min | 0. | 0. | 488.3945 |
| 13 | 1.04614 | SLU_4 | Min | 0. | 0. | 536.576 |
| 13 | 2.09228 | SLU_4 | Min | 0. | 0. | 368.9574 |
| 13 | 0. | SLE_F1 | Max | 0. | 0. | 87.576 |
| 13 | 1.04614 | SLE_F1 | Max | 0. | 0. | 151.2674 |
| 13 | 2.09228 | SLE_F1 | Max | 0. | 0. | 78.5501 |
| 13 | 0. | SLE_F1 | Min | 0. | 0. | 87.576 |
| 13 | 1.04614 | SLE_F1 | Min | 0. | 0. | 151.2674 |
| 13 | 2.09228 | SLE_F1 | Min | 0. | 0. | 78.5501 |
| 13 | 0. | SLE_F2 | Max | 0. | 0. | 198.957 |
| 13 | 1.04614 | SLE_F2 | Max | 0. | 0. | 281.2825 |
| 13 | 2.09228 | SLE_F2 | Max | 0. | 0. | 229.0833 |
| 13 | 0. | SLE_F2 | Min | 0. | 0. | 198.957 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 13 | 1.04614 | SLE_F2 | Min | 0. | 0. | 281.2825 |
| 13 | 2.09228 | SLE_F2 | Min | 0. | 0. | 229.0833 |
| 13 | 0. | SLE_F3 | Max | 0. | 0. | 353.405 |
| 13 | 1.04614 | SLE_F3 | Max | 0. | 0. | 383.5125 |
| 13 | 2.09228 | SLE_F3 | Max | 0. | 0. | 256.7618 |
| 13 | 0. | SLE_F3 | Min | 0. | 0. | 353.405 |
| 13 | 1.04614 | SLE_F3 | Min | 0. | 0. | 383.5125 |
| 13 | 2.09228 | SLE_F3 | Min | 0. | 0. | 256.7618 |
| 13 | 0. | SLE_F4 | Max | 0. | 0. | 244.3174 |
| 13 | 1.04614 | SLE_F4 | Max | 0. | 0. | 240.9666 |
| 13 | 2.09228 | SLE_F4 | Max | 0. | 0. | 78.5793 |
| 13 | 0. | SLE_F4 | Min | 0. | 0. | 244.3174 |
| 13 | 1.04614 | SLE_F4 | Min | 0. | 0. | 240.9666 |
| 13 | 2.09228 | SLE_F4 | Min | 0. | 0. | 78.5793 |
| 13 | 0. | SLE_QP1 | Max | 0. | 0. | 59.6612 |
| 13 | 1.04614 | SLE_QP1 | Max | 0. | 0. | 112.8996 |
| 13 | 2.09228 | SLE_QP1 | Max | 0. | 0. | 47.0532 |
| 13 | 0. | SLE_QP1 | Min | 0. | 0. | 59.6612 |
| 13 | 1.04614 | SLE_QP1 | Min | 0. | 0. | 112.8996 |
| 13 | 2.09228 | SLE_QP1 | Min | 0. | 0. | 47.0532 |
| 13 | 0. | SLE_QP2 | Max | 0. | 0. | 159.057 |
| 13 | 1.04614 | SLE_QP2 | Max | 0. | 0. | 228.5489 |
| 13 | 2.09228 | SLE_QP2 | Max | 0. | 0. | 180.4938 |
| 13 | 0. | SLE_QP2 | Min | 0. | 0. | 159.057 |
| 13 | 1.04614 | SLE_QP2 | Min | 0. | 0. | 228.5489 |
| 13 | 2.09228 | SLE_QP2 | Min | 0. | 0. | 180.4938 |
| 13 | 0. | SLE_QP3 | Max | 0. | 0. | 312.0208 |
| 13 | 1.04614 | SLE_QP3 | Max | 0. | 0. | 329.2119 |
| 13 | 2.09228 | SLE_QP3 | Max | 0. | 0. | 206.5222 |
| 13 | 0. | SLE_QP3 | Min | 0. | 0. | 312.0208 |
| 13 | 1.04614 | SLE_QP3 | Min | 0. | 0. | 329.2119 |
| 13 | 2.09228 | SLE_QP3 | Min | 0. | 0. | 206.5222 |
| 13 | 0. | SLE_QP4 | Max | 0. | 0. | 205.4162 |
| 13 | 1.04614 | SLE_QP4 | Max | 0. | 0. | 191.2718 |
| 13 | 2.09228 | SLE_QP4 | Max | 0. | 0. | 35.4149 |
| 13 | 0. | SLE_QP4 | Min | 0. | 0. | 205.4162 |
| 13 | 1.04614 | SLE_QP4 | Min | 0. | 0. | 191.2718 |
| 13 | 2.09228 | SLE_QP4 | Min | 0. | 0. | 35.4149 |
| 13 | 0. | SLV_1 | Max | 0. | 0. | -161.8199 |
| 13 | 1.04614 | SLV_1 | Max | 0. | 0. | -272.6455 |
| 13 | 2.09228 | SLV_1 | Max | 0. | 0. | -512.23 |
| 13 | 0. | SLV_1 | Min | 0. | 0. | -161.8199 |
| 13 | 1.04614 | SLV_1 | Min | 0. | 0. | -272.6455 |
| 13 | 2.09228 | SLV_1 | Min | 0. | 0. | -512.23 |
| 13 | 0. | SLV_2 | Max | 0. | 0. | -165.8548 |
| 13 | 1.04614 | SLV_2 | Max | 0. | 0. | -276.3759 |
| 13 | 2.09228 | SLV_2 | Max | 0. | 0. | -515.656 |
| 13 | 0. | SLV_2 | Min | 0. | 0. | -165.8548 |
| 13 | 1.04614 | SLV_2 | Min | 0. | 0. | -276.3759 |
| 13 | 2.09228 | SLV_2 | Min | 0. | 0. | -515.656 |
| 13 | 0. | SLV_3 | Max | 0. | 0. | -87.0731 |
| 13 | 1.04614 | SLV_3 | Max | 0. | 0. | -253.5775 |
| 13 | 2.09228 | SLV_3 | Max | 0. | 0. | -571.4686 |
| 13 | 0. | SLV_3 | Min | 0. | 0. | -87.0731 |
| 13 | 1.04614 | SLV_3 | Min | 0. | 0. | -253.5775 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 13 | 2.09228 | SLV_3 | Min | 0. | 0. | -571.4686 |
| 13 | 0. | SLV_4 | Max | 0. | 0. | -91.4368 |
| 13 | 1.04614 | SLV_4 | Max | 0. | 0. | -257.9027 |
| 13 | 2.09228 | SLV_4 | Max | 0. | 0. | -575.7553 |
| 13 | 0. | SLV_4 | Min | 0. | 0. | -91.4368 |
| 13 | 1.04614 | SLV_4 | Min | 0. | 0. | -257.9027 |
| 13 | 2.09228 | SLV_4 | Min | 0. | 0. | -575.7553 |
| 13 | 0. | SLD_1 | Max | 0. | 0. | 6.37 |
| 13 | 1.04614 | SLD_1 | Max | 0. | 0. | -23.2174 |
| 13 | 2.09228 | SLD_1 | Max | 0. | 0. | -176.162 |
| 13 | 0. | SLD_1 | Min | 0. | 0. | 6.37 |
| 13 | 1.04614 | SLD_1 | Min | 0. | 0. | -23.2174 |
| 13 | 2.09228 | SLD_1 | Min | 0. | 0. | -176.162 |
| 13 | 0. | SLD_2 | Max | 0. | 0. | 4.8467 |
| 13 | 1.04614 | SLD_2 | Max | 0. | 0. | -24.8506 |
| 13 | 2.09228 | SLD_2 | Max | 0. | 0. | -177.9052 |
| 13 | 0. | SLD_2 | Min | 0. | 0. | 4.8467 |
| 13 | 1.04614 | SLD_2 | Min | 0. | 0. | -24.8506 |
| 13 | 2.09228 | SLD_2 | Min | 0. | 0. | -177.9052 |
| 13 | 0. | SLD_3 | Max | 0. | 0. | 78.1507 |
| 13 | 1.04614 | SLD_3 | Max | 0. | 0. | -11.1904 |
| 13 | 2.09228 | SLD_3 | Max | 0. | 0. | -246.5166 |
| 13 | 0. | SLD_3 | Min | 0. | 0. | 78.1507 |
| 13 | 1.04614 | SLD_3 | Min | 0. | 0. | -11.1904 |
| 13 | 2.09228 | SLD_3 | Min | 0. | 0. | -246.5166 |
| 13 | 0. | SLD_4 | Max | 0. | 0. | 76.3085 |
| 13 | 1.04614 | SLD_4 | Max | 0. | 0. | -13.0841 |
| 13 | 2.09228 | SLD_4 | Max | 0. | 0. | -248.4617 |
| 13 | 0. | SLD_4 | Min | 0. | 0. | 76.3085 |
| 13 | 1.04614 | SLD_4 | Min | 0. | 0. | -13.0841 |
| 13 | 2.09228 | SLD_4 | Min | 0. | 0. | -248.4617 |
| 13 | 0. | SLU_IDR_1 | Max | 0. | 0. | 285.2925 |
| 13 | 1.04614 | SLU_IDR_1 | Max | 0. | 0. | 301.9618 |
| 13 | 2.09228 | SLU_IDR_1 | Max | 0. | 0. | 188.1244 |
| 13 | 0. | SLU_IDR_1 | Min | 0. | 0. | 285.2925 |
| 13 | 1.04614 | SLU_IDR_1 | Min | 0. | 0. | 301.9618 |
| 13 | 2.09228 | SLU_IDR_1 | Min | 0. | 0. | 188.1244 |
| 13 | 0. | SLU_IDR_2 | Max | 0. | 0. | 151.0801 |
| 13 | 1.04614 | SLU_IDR_2 | Max | 0. | 0. | 214.9795 |
| 13 | 2.09228 | SLU_IDR_2 | Max | 0. | 0. | 168.4726 |
| 13 | 0. | SLU_IDR_2 | Min | 0. | 0. | 151.0801 |
| 13 | 1.04614 | SLU_IDR_2 | Min | 0. | 0. | 214.9795 |
| 13 | 2.09228 | SLU_IDR_2 | Min | 0. | 0. | 168.4726 |
| 13 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -313.6641 |
| 13 | 1.04614 | SISMA WOOD SLV-1 | Max | 0. | 0. | -394.5356 |
| 13 | 2.09228 | SISMA WOOD SLV-1 | Max | 0. | 0. | -485.0814 |
| 13 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -313.6641 |
| 13 | 1.04614 | SISMA WOOD SLV-1 | Min | 0. | 0. | -394.5356 |
| 13 | 2.09228 | SISMA WOOD SLV-1 | Min | 0. | 0. | -485.0814 |
| 13 | 0. | DEAD-1 | Max | 0. | 0. | 92.46 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 13 | 1.04614 | DEAD-1 | Max | 0. | 0. | 120.549 |
| 13 | 2.09228 | DEAD-1 | Max | 0. | 0. | 121.5067 |
| 13 | 0. | DEAD-1 | Min | 0. | 0. | 92.46 |
| 13 | 1.04614 | DEAD-1 | Min | 0. | 0. | 120.549 |
| 13 | 2.09228 | DEAD-1 | Min | 0. | 0. | 121.5067 |
| 13 | 0. | SLU_PROVA | | 0. | 0. | 21.5176 |
| 13 | 1.04614 | SLU_PROVA | | 0. | 0. | 93.976 |
| 13 | 2.09228 | SLU_PROVA | | 0. | 0. | -23.0238 |
| 14 | 0. | DEAD | | 0. | 0. | -46.0695 |
| 14 | 0.94151 | DEAD | | 0. | 0. | -50.5597 |
| 14 | 1.88301 | DEAD | | 0. | 0. | -80.8647 |
| 14 | 0. | SIMM_KA | | 0. | 0. | 74.806 |
| 14 | 0.94151 | SIMM_KA | | 0. | 0. | 74.7204 |
| 14 | 1.88301 | SIMM_KA | | 0. | 0. | 74.6347 |
| 14 | 0. | SIMM_K0 | | 0. | 0. | 114.5786 |
| 14 | 0.94151 | SIMM_K0 | | 0. | 0. | 114.9908 |
| 14 | 1.88301 | SIMM_K0 | | 0. | 0. | 115.4029 |
| 14 | 0. | A--SIMM_KA | | 0. | 0. | 165.2452 |
| 14 | 0.94151 | A--SIMM_KA | | 0. | 0. | 176.4344 |
| 14 | 1.88301 | A--SIMM_KA | | 0. | 0. | 187.6236 |
| 14 | 0. | A--SIMM_K0 | | 0. | 0. | 249.9972 |
| 14 | 0.94151 | A--SIMM_K0 | | 0. | 0. | 266.6289 |
| 14 | 1.88301 | A--SIMM_K0 | | 0. | 0. | 283.2606 |
| 14 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 9.9375 |
| 14 | 0.94151 | A-- SIMM_SOVR_K A | | 0. | 0. | 11.7059 |
| 14 | 1.88301 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.4743 |
| 14 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 14.8988 |
| 14 | 0.94151 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 17.5501 |
| 14 | 1.88301 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.2013 |
| 14 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 14.8988 |
| 14 | 0.94151 | SIMM_SOVR_K 0 | | 0. | 0. | 17.5501 |
| 14 | 1.88301 | SIMM_SOVR_K 0 | | 0. | 0. | 20.2013 |
| 14 | 0. | SIMM_SOVR_K A | | 0. | 0. | 9.9375 |
| 14 | 0.94151 | SIMM_SOVR_K A | | 0. | 0. | 11.7059 |
| 14 | 1.88301 | SIMM_SOVR_K A | | 0. | 0. | 13.4743 |
| 14 | 0. | SOVR | | 0. | 0. | -51.4109 |
| 14 | 0.94151 | SOVR | | 0. | 0. | -32.3655 |
| 14 | 1.88301 | SOVR | | 0. | 0. | -13.3201 |
| 14 | 0. | TERR_SIMM | | 0. | 0. | -178.7471 |
| 14 | 0.94151 | TERR_SIMM | | 0. | 0. | -98.4982 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 14 | 1.88301 | TERR_SIMM | | 0. | 0. | -18.2493 |
| 14 | 0. | TERR_A--SIMM | | 0. | 0. | -240.6637 |
| 14 | 0.94151 | TERR_A--SIMM | | 0. | 0. | -123.3472 |
| 14 | 1.88301 | TERR_A--SIMM | | 0. | 0. | -6.0307 |
| 14 | 0. | INERZIA H SLV | | 0. | 0. | 2.3808 |
| 14 | 0.94151 | INERZIA H SLV | | 0. | 0. | 2.7717 |
| 14 | 1.88301 | INERZIA H SLV | | 0. | 0. | 3.1626 |
| 14 | 0. | INERZIA V + SLV | | 0. | 0. | -0.6757 |
| 14 | 0.94151 | INERZIA V + SLV | | 0. | 0. | -0.9618 |
| 14 | 1.88301 | INERZIA V + SLV | | 0. | 0. | -1.248 |
| 14 | 0. | INERZIA V - SLV | | 0. | 0. | 0.6757 |
| 14 | 0.94151 | INERZIA V - SLV | | 0. | 0. | 0.9618 |
| 14 | 1.88301 | INERZIA V - SLV | | 0. | 0. | 1.248 |
| 14 | 0. | SISMA WOOD SLV | | 0. | 0. | 193.9039 |
| 14 | 0.94151 | SISMA WOOD SLV | | 0. | 0. | 204.9054 |
| 14 | 1.88301 | SISMA WOOD SLV | | 0. | 0. | 230.6806 |
| 14 | 0. | iDROSTATICA | | 0. | 0. | -57.3321 |
| 14 | 0.94151 | iDROSTATICA | | 0. | 0. | 132.6416 |
| 14 | 1.88301 | iDROSTATICA | | 0. | 0. | 431.7086 |
| 14 | 0. | SISMA WOOD SLD | | 0. | 0. | 85.6358 |
| 14 | 0.94151 | SISMA WOOD SLD | | 0. | 0. | 90.4945 |
| 14 | 1.88301 | SISMA WOOD SLD | | 0. | 0. | 101.8779 |
| 14 | 0. | INERZIA H SLD | | 0. | 0. | 1.0515 |
| 14 | 0.94151 | INERZIA H SLD | | 0. | 0. | 1.2241 |
| 14 | 1.88301 | INERZIA H SLD | | 0. | 0. | 1.3967 |
| 14 | 0. | INERZIA V + SLD | | 0. | 0. | -0.2984 |
| 14 | 0.94151 | INERZIA V + SLD | | 0. | 0. | -0.4248 |
| 14 | 1.88301 | INERZIA V + SLD | | 0. | 0. | -0.5512 |
| 14 | 0. | INERZIA V SLD | | 0. | 0. | 0.2984 |
| 14 | 0.94151 | INERZIA V SLD | | 0. | 0. | 0.4248 |
| 14 | 1.88301 | INERZIA V SLD | | 0. | 0. | 0.5512 |
| 14 | 0. | INERZIA V -1 | | 0. | 0. | 0.6757 |
| 14 | 0.94151 | INERZIA V -1 | | 0. | 0. | 0.9618 |
| 14 | 1.88301 | INERZIA V -1 | | 0. | 0. | 1.248 |
| 14 | 0. | SLU_1 | Max | 0. | 0. | -320.2566 |
| 14 | 0.94151 | SLU_1 | Max | 0. | 0. | 98.5428 |
| 14 | 1.88301 | SLU_1 | Max | 0. | 0. | 625.6041 |
| 14 | 0. | SLU_1 | Min | 0. | 0. | -320.2566 |
| 14 | 0.94151 | SLU_1 | Min | 0. | 0. | 98.5428 |
| 14 | 1.88301 | SLU_1 | Min | 0. | 0. | 625.6041 |
| 14 | 0. | SLU_2 | Max | 0. | 0. | -383.6952 |
| 14 | 0.94151 | SLU_2 | Max | 0. | 0. | 47.0531 |
| 14 | 1.88301 | SLU_2 | Max | 0. | 0. | 586.0634 |
| 14 | 0. | SLU_2 | Min | 0. | 0. | -383.6952 |
| 14 | 0.94151 | SLU_2 | Min | 0. | 0. | 47.0531 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 14 | 1.88301 | SLU_2 | Min | 0. | 0. | 586.0634 |
| 14 | 0. | SLU_3 | Max | 0. | 0. | -134.2315 |
| 14 | 0.94151 | SLU_3 | Max | 0. | 0. | 371.6057 |
| 14 | 1.88301 | SLU_3 | Max | 0. | 0. | 985.7048 |
| 14 | 0. | SLU_3 | Min | 0. | 0. | -134.2315 |
| 14 | 0.94151 | SLU_3 | Min | 0. | 0. | 371.6057 |
| 14 | 1.88301 | SLU_3 | Min | 0. | 0. | 985.7048 |
| 14 | 0. | SLU_4 | Max | 0. | 0. | -280.785 |
| 14 | 0.94151 | SLU_4 | Max | 0. | 0. | 220.5478 |
| 14 | 1.88301 | SLU_4 | Max | 0. | 0. | 830.1426 |
| 14 | 0. | SLU_4 | Min | 0. | 0. | -280.785 |
| 14 | 0.94151 | SLU_4 | Min | 0. | 0. | 220.5478 |
| 14 | 1.88301 | SLU_4 | Min | 0. | 0. | 830.1426 |
| 14 | 0. | SLE_F1 | Max | 0. | 0. | -228.1598 |
| 14 | 0.94151 | SLE_F1 | Max | 0. | 0. | 87.7762 |
| 14 | 1.88301 | SLE_F1 | Max | 0. | 0. | 486.9907 |
| 14 | 0. | SLE_F1 | Min | 0. | 0. | -228.1598 |
| 14 | 0.94151 | SLE_F1 | Min | 0. | 0. | 87.7762 |
| 14 | 1.88301 | SLE_F1 | Min | 0. | 0. | 486.9907 |
| 14 | 0. | SLE_F2 | Max | 0. | 0. | -273.1588 |
| 14 | 0.94151 | SLE_F2 | Max | 0. | 0. | 52.3526 |
| 14 | 1.88301 | SLE_F2 | Max | 0. | 0. | 461.1425 |
| 14 | 0. | SLE_F2 | Min | 0. | 0. | -273.1588 |
| 14 | 0.94151 | SLE_F2 | Min | 0. | 0. | 52.3526 |
| 14 | 1.88301 | SLE_F2 | Min | 0. | 0. | 461.1425 |
| 14 | 0. | SLE_F3 | Max | 0. | 0. | -192.4887 |
| 14 | 0.94151 | SLE_F3 | Max | 0. | 0. | 185.5312 |
| 14 | 1.88301 | SLE_F3 | Max | 0. | 0. | 646.8296 |
| 14 | 0. | SLE_F3 | Min | 0. | 0. | -192.4887 |
| 14 | 0.94151 | SLE_F3 | Min | 0. | 0. | 185.5312 |
| 14 | 1.88301 | SLE_F3 | Min | 0. | 0. | 646.8296 |
| 14 | 0. | SLE_F4 | Max | 0. | 0. | -80.388 |
| 14 | 0.94151 | SLE_F4 | Max | 0. | 0. | 299.6482 |
| 14 | 1.88301 | SLE_F4 | Max | 0. | 0. | 762.9628 |
| 14 | 0. | SLE_F4 | Min | 0. | 0. | -80.388 |
| 14 | 0.94151 | SLE_F4 | Min | 0. | 0. | 299.6482 |
| 14 | 1.88301 | SLE_F4 | Min | 0. | 0. | 762.9628 |
| 14 | 0. | SLE_QP1 | Max | 0. | 0. | -191.374 |
| 14 | 0.94151 | SLE_QP1 | Max | 0. | 0. | 113.8251 |
| 14 | 1.88301 | SLE_QP1 | Max | 0. | 0. | 502.3026 |
| 14 | 0. | SLE_QP1 | Min | 0. | 0. | -191.374 |
| 14 | 0.94151 | SLE_QP1 | Min | 0. | 0. | 113.8251 |
| 14 | 1.88301 | SLE_QP1 | Min | 0. | 0. | 502.3026 |
| 14 | 0. | SLE_QP2 | Max | 0. | 0. | -232.3185 |
| 14 | 0.94151 | SLE_QP2 | Max | 0. | 0. | 82.3587 |
| 14 | 1.88301 | SLE_QP2 | Max | 0. | 0. | 480.3143 |
| 14 | 0. | SLE_QP2 | Min | 0. | 0. | -232.3185 |
| 14 | 0.94151 | SLE_QP2 | Min | 0. | 0. | 82.3587 |
| 14 | 1.88301 | SLE_QP2 | Min | 0. | 0. | 480.3143 |
| 14 | 0. | SLE_QP3 | Max | 0. | 0. | -148.8477 |
| 14 | 0.94151 | SLE_QP3 | Max | 0. | 0. | 215.0191 |
| 14 | 1.88301 | SLE_QP3 | Max | 0. | 0. | 662.1644 |
| 14 | 0. | SLE_QP3 | Min | 0. | 0. | -148.8477 |
| 14 | 0.94151 | SLE_QP3 | Min | 0. | 0. | 215.0191 |
| 14 | 1.88301 | SLE_QP3 | Min | 0. | 0. | 662.1644 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 14 | 0. | SLE_QP4 | Max | 0. | 0. | -37.8727 |
| 14 | 0.94151 | SLE_QP4 | Max | 0. | 0. | 325.0548 |
| 14 | 1.88301 | SLE_QP4 | Max | 0. | 0. | 771.2607 |
| 14 | 0. | SLE_QP4 | Min | 0. | 0. | -37.8727 |
| 14 | 0.94151 | SLE_QP4 | Min | 0. | 0. | 325.0548 |
| 14 | 1.88301 | SLE_QP4 | Min | 0. | 0. | 771.2607 |
| 14 | 0. | SLV_1 | Max | 0. | 0. | 331.502 |
| 14 | 0.94151 | SLV_1 | Max | 0. | 0. | 608.0432 |
| 14 | 1.88301 | SLV_1 | Max | 0. | 0. | 982.6366 |
| 14 | 0. | SLV_1 | Min | 0. | 0. | 331.502 |
| 14 | 0.94151 | SLV_1 | Min | 0. | 0. | 608.0432 |
| 14 | 1.88301 | SLV_1 | Min | 0. | 0. | 982.6366 |
| 14 | 0. | SLV_2 | Max | 0. | 0. | 331.1602 |
| 14 | 0.94151 | SLV_2 | Max | 0. | 0. | 608.3501 |
| 14 | 1.88301 | SLV_2 | Max | 0. | 0. | 983.5921 |
| 14 | 0. | SLV_2 | Min | 0. | 0. | 331.1602 |
| 14 | 0.94151 | SLV_2 | Min | 0. | 0. | 608.3501 |
| 14 | 1.88301 | SLV_2 | Min | 0. | 0. | 983.5921 |
| 14 | 0. | SLV_3 | Max | 0. | 0. | 496.6408 |
| 14 | 0.94151 | SLV_3 | Max | 0. | 0. | 832.5856 |
| 14 | 1.88301 | SLV_3 | Max | 0. | 0. | 1266.5823 |
| 14 | 0. | SLV_3 | Min | 0. | 0. | 496.6408 |
| 14 | 0.94151 | SLV_3 | Min | 0. | 0. | 832.5856 |
| 14 | 1.88301 | SLV_3 | Min | 0. | 0. | 1266.5823 |
| 14 | 0. | SLV_4 | Max | 0. | 0. | 497.6587 |
| 14 | 0.94151 | SLV_4 | Max | 0. | 0. | 833.5672 |
| 14 | 1.88301 | SLV_4 | Max | 0. | 0. | 1267.5278 |
| 14 | 0. | SLV_4 | Min | 0. | 0. | 497.6587 |
| 14 | 0.94151 | SLV_4 | Min | 0. | 0. | 833.5672 |
| 14 | 1.88301 | SLV_4 | Min | 0. | 0. | 1267.5278 |
| 14 | 0. | SLD_1 | Max | 0. | 0. | 39.8216 |
| 14 | 0.94151 | SLD_1 | Max | 0. | 0. | 337.1395 |
| 14 | 1.88301 | SLD_1 | Max | 0. | 0. | 724.2605 |
| 14 | 0. | SLD_1 | Min | 0. | 0. | 39.8216 |
| 14 | 0.94151 | SLD_1 | Min | 0. | 0. | 337.1395 |
| 14 | 1.88301 | SLD_1 | Min | 0. | 0. | 724.2605 |
| 14 | 0. | SLD_2 | Max | 0. | 0. | 40.5097 |
| 14 | 0.94151 | SLD_2 | Max | 0. | 0. | 338.5103 |
| 14 | 1.88301 | SLD_2 | Max | 0. | 0. | 726.314 |
| 14 | 0. | SLD_2 | Min | 0. | 0. | 40.5097 |
| 14 | 0.94151 | SLD_2 | Min | 0. | 0. | 338.5103 |
| 14 | 1.88301 | SLD_2 | Min | 0. | 0. | 726.314 |
| 14 | 0. | SLD_3 | Max | 0. | 0. | 209.0827 |
| 14 | 0.94151 | SLD_3 | Max | 0. | 0. | 557.4892 |
| 14 | 1.88301 | SLD_3 | Max | 0. | 0. | 995.6987 |
| 14 | 0. | SLD_3 | Min | 0. | 0. | 209.0827 |
| 14 | 0.94151 | SLD_3 | Min | 0. | 0. | 557.4892 |
| 14 | 1.88301 | SLD_3 | Min | 0. | 0. | 995.6987 |
| 14 | 0. | SLD_4 | Max | 0. | 0. | 209.7112 |
| 14 | 0.94151 | SLD_4 | Max | 0. | 0. | 558.2624 |
| 14 | 1.88301 | SLD_4 | Max | 0. | 0. | 996.6167 |
| 14 | 0. | SLD_4 | Min | 0. | 0. | 209.7112 |
| 14 | 0.94151 | SLD_4 | Min | 0. | 0. | 558.2624 |
| 14 | 1.88301 | SLD_4 | Min | 0. | 0. | 996.6167 |
| 14 | 0. | SLU_IDR_1 | Max | 0. | 0. | -130.332 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 14 | 0.94151 | SLU_IDR_1 | Max | 0. | 0. | 264.9925 |
| 14 | 1.88301 | SLU_IDR_1 | Max | 0. | 0. | 757.0863 |
| 14 | 0. | SLU_IDR_1 | Min | 0. | 0. | -130.332 |
| 14 | 0.94151 | SLU_IDR_1 | Min | 0. | 0. | 264.9925 |
| 14 | 1.88301 | SLU_IDR_1 | Min | 0. | 0. | 757.0863 |
| 14 | 0. | SLU_IDR_2 | Max | 0. | 0. | -223.2232 |
| 14 | 0.94151 | SLU_IDR_2 | Max | 0. | 0. | 140.7947 |
| 14 | 1.88301 | SLU_IDR_2 | Max | 0. | 0. | 601.5818 |
| 14 | 0. | SLU_IDR_2 | Min | 0. | 0. | -223.2232 |
| 14 | 0.94151 | SLU_IDR_2 | Min | 0. | 0. | 140.7947 |
| 14 | 1.88301 | SLU_IDR_2 | Min | 0. | 0. | 601.5818 |
| 14 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 315.3305 |
| 14 | 0.94151 | SISMA WOOD SLV-1 | Max | 0. | 0. | 220.5138 |
| 14 | 1.88301 | SISMA WOOD SLV-1 | Max | 0. | 0. | 140.4708 |
| 14 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 315.3305 |
| 14 | 0.94151 | SISMA WOOD SLV-1 | Min | 0. | 0. | 220.5138 |
| 14 | 1.88301 | SISMA WOOD SLV-1 | Min | 0. | 0. | 140.4708 |
| 14 | 0. | DEAD-1 | Max | 0. | 0. | -65.8241 |
| 14 | 0.94151 | DEAD-1 | Max | 0. | 0. | -64.4483 |
| 14 | 1.88301 | DEAD-1 | Max | 0. | 0. | -88.8874 |
| 14 | 0. | DEAD-1 | Min | 0. | 0. | -65.8241 |
| 14 | 0.94151 | DEAD-1 | Min | 0. | 0. | -64.4483 |
| 14 | 1.88301 | DEAD-1 | Min | 0. | 0. | -88.8874 |
| 14 | 0. | SLU_PROVA | | 0. | 0. | -272.6091 |
| 14 | 0.94151 | SLU_PROVA | | 0. | 0. | 105.9238 |
| 14 | 1.88301 | SLU_PROVA | | 0. | 0. | 592.7186 |
| 16 | 0. | DEAD | | 0. | 0. | -6.6047 |
| 16 | 0.39245 | DEAD | | 0. | 0. | -4.7727 |
| 16 | 0.7849 | DEAD | | 0. | 0. | -7.5599 |
| 16 | 0. | SIMM_KA | | 0. | 0. | 65.384 |
| 16 | 0.39245 | SIMM_KA | | 0. | 0. | 66.6564 |
| 16 | 0.7849 | SIMM_KA | | 0. | 0. | 67.9288 |
| 16 | 0. | SIMM_K0 | | 0. | 0. | 99.0541 |
| 16 | 0.39245 | SIMM_K0 | | 0. | 0. | 100.9972 |
| 16 | 0.7849 | SIMM_K0 | | 0. | 0. | 102.9402 |
| 16 | 0. | A--SIMM_KA | | 0. | 0. | 80.645 |
| 16 | 0.39245 | A--SIMM_KA | | 0. | 0. | 88.5104 |
| 16 | 0.7849 | A--SIMM_KA | | 0. | 0. | 96.3758 |
| 16 | 0. | A--SIMM_K0 | | 0. | 0. | 123.9988 |
| 16 | 0.39245 | A--SIMM_K0 | | 0. | 0. | 135.7564 |
| 16 | 0.7849 | A--SIMM_K0 | | 0. | 0. | 147.514 |
| 16 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 5.2028 |
| 16 | 0.39245 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.3401 |
| 16 | 0.7849 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.4773 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 16 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 7.8004 |
| 16 | 0.39245 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.0061 |
| 16 | 0.7849 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.2118 |
| 16 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 7.8004 |
| 16 | 0.39245 | SIMM_SOVR_K 0 | | 0. | 0. | 8.0061 |
| 16 | 0.7849 | SIMM_SOVR_K 0 | | 0. | 0. | 8.2118 |
| 16 | 0. | SIMM_SOVR_K A | | 0. | 0. | 5.2028 |
| 16 | 0.39245 | SIMM_SOVR_K A | | 0. | 0. | 5.3401 |
| 16 | 0.7849 | SIMM_SOVR_K A | | 0. | 0. | 5.4773 |
| 16 | 0. | SOVR | | 0. | 0. | -80.0145 |
| 16 | 0.39245 | SOVR | | 0. | 0. | -79.7303 |
| 16 | 0.7849 | SOVR | | 0. | 0. | -79.446 |
| 16 | 0. | TERR_SIMM | | 0. | 0. | -304.7004 |
| 16 | 0.39245 | TERR_SIMM | | 0. | 0. | -303.2062 |
| 16 | 0.7849 | TERR_SIMM | | 0. | 0. | -301.7119 |
| 16 | 0. | TERR_A--SIMM | | 0. | 0. | -390.1751 |
| 16 | 0.39245 | TERR_A--SIMM | | 0. | 0. | -391.034 |
| 16 | 0.7849 | TERR_A--SIMM | | 0. | 0. | -391.8928 |
| 16 | 0. | INERZIA H SLV | | 0. | 0. | 0.0095 |
| 16 | 0.39245 | INERZIA H SLV | | 0. | 0. | 0.2463 |
| 16 | 0.7849 | INERZIA H SLV | | 0. | 0. | 0.483 |
| 16 | 0. | INERZIA V + SLV | | 0. | 0. | -0.0302 |
| 16 | 0.39245 | INERZIA V + SLV | | 0. | 0. | -0.0378 |
| 16 | 0.7849 | INERZIA V + SLV | | 0. | 0. | -0.0454 |
| 16 | 0. | INERZIA V - SLV | | 0. | 0. | 0.0302 |
| 16 | 0.39245 | INERZIA V - SLV | | 0. | 0. | 0.0378 |
| 16 | 0.7849 | INERZIA V - SLV | | 0. | 0. | 0.0454 |
| 16 | 0. | SISMA WOOD SLV | | 0. | 0. | 111.0204 |
| 16 | 0.39245 | SISMA WOOD SLV | | 0. | 0. | 124.6199 |
| 16 | 0.7849 | SISMA WOOD SLV | | 0. | 0. | 138.2195 |
| 16 | 0. | iDROSTATICA | | 0. | 0. | -507.3856 |
| 16 | 0.39245 | iDROSTATICA | | 0. | 0. | -507.3887 |
| 16 | 0.7849 | iDROSTATICA | | 0. | 0. | -487.154 |
| 16 | 0. | SISMA WOOD SLD | | 0. | 0. | 49.0311 |
| 16 | 0.39245 | SISMA WOOD SLD | | 0. | 0. | 55.0372 |
| 16 | 0.7849 | SISMA WOOD SLD | | 0. | 0. | 61.0433 |
| 16 | 0. | INERZIA H SLD | | 0. | 0. | 0.0042 |
| 16 | 0.39245 | INERZIA H SLD | | 0. | 0. | 0.1088 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 16 | 0.7849 | INERZIA H SLD | | 0. | 0. | 0.2133 |
| 16 | 0. | INERZIA V + SLD | | 0. | 0. | -0.0133 |
| 16 | 0.39245 | INERZIA V + SLD | | 0. | 0. | -0.0167 |
| 16 | 0.7849 | INERZIA V + SLD | | 0. | 0. | -0.0201 |
| 16 | 0. | INERZIA V SLD | | 0. | 0. | 0.0133 |
| 16 | 0.39245 | INERZIA V SLD | | 0. | 0. | 0.0167 |
| 16 | 0.7849 | INERZIA V SLD | | 0. | 0. | 0.0201 |
| 16 | 0. | INERZIA V -1 | | 0. | 0. | 0.0302 |
| 16 | 0.39245 | INERZIA V -1 | | 0. | 0. | 0.0378 |
| 16 | 0.7849 | INERZIA V -1 | | 0. | 0. | 0.0454 |
| 16 | 0. | SLU_1 | Max | 0. | 0. | -1255.3622 |
| 16 | 0.39245 | SLU_1 | Max | 0. | 0. | -1244.9672 |
| 16 | 0.7849 | SLU_1 | Max | 0. | 0. | -1214.2679 |
| 16 | 0. | SLU_1 | Min | 0. | 0. | -1255.3622 |
| 16 | 0.39245 | SLU_1 | Min | 0. | 0. | -1244.9672 |
| 16 | 0.7849 | SLU_1 | Min | 0. | 0. | -1214.2679 |
| 16 | 0. | SLU_2 | Max | 0. | 0. | -1363.0651 |
| 16 | 0.39245 | SLU_2 | Max | 0. | 0. | -1353.0686 |
| 16 | 0.7849 | SLU_2 | Max | 0. | 0. | -1322.7678 |
| 16 | 0. | SLU_2 | Min | 0. | 0. | -1363.0651 |
| 16 | 0.39245 | SLU_2 | Min | 0. | 0. | -1353.0686 |
| 16 | 0.7849 | SLU_2 | Min | 0. | 0. | -1322.7678 |
| 16 | 0. | SLU_3 | Max | 0. | 0. | -1292.1245 |
| 16 | 0.39245 | SLU_3 | Max | 0. | 0. | -1263.7377 |
| 16 | 0.7849 | SLU_3 | Max | 0. | 0. | -1215.0466 |
| 16 | 0. | SLU_3 | Min | 0. | 0. | -1292.1245 |
| 16 | 0.39245 | SLU_3 | Min | 0. | 0. | -1263.7377 |
| 16 | 0.7849 | SLU_3 | Min | 0. | 0. | -1215.0466 |
| 16 | 0. | SLU_4 | Max | 0. | 0. | -1419.2001 |
| 16 | 0.39245 | SLU_4 | Max | 0. | 0. | -1396.5375 |
| 16 | 0.7849 | SLU_4 | Max | 0. | 0. | -1353.5706 |
| 16 | 0. | SLU_4 | Min | 0. | 0. | -1419.2001 |
| 16 | 0.39245 | SLU_4 | Min | 0. | 0. | -1396.5375 |
| 16 | 0.7849 | SLU_4 | Min | 0. | 0. | -1353.5706 |
| 16 | 0. | SLE_F1 | Max | 0. | 0. | -942.6813 |
| 16 | 0.39245 | SLE_F1 | Max | 0. | 0. | -935.0019 |
| 16 | 0.7849 | SLE_F1 | Max | 0. | 0. | -911.7039 |
| 16 | 0. | SLE_F1 | Min | 0. | 0. | -942.6813 |
| 16 | 0.39245 | SLE_F1 | Min | 0. | 0. | -935.0019 |
| 16 | 0.7849 | SLE_F1 | Min | 0. | 0. | -911.7039 |
| 16 | 0. | SLE_F2 | Max | 0. | 0. | -1024.6828 |
| 16 | 0.39245 | SLE_F2 | Max | 0. | 0. | -1016.9619 |
| 16 | 0.7849 | SLE_F2 | Max | 0. | 0. | -993.6224 |
| 16 | 0. | SLE_F2 | Min | 0. | 0. | -1024.6828 |
| 16 | 0.39245 | SLE_F2 | Min | 0. | 0. | -1016.9619 |
| 16 | 0.7849 | SLE_F2 | Min | 0. | 0. | -993.6224 |
| 16 | 0. | SLE_F3 | Max | 0. | 0. | -1065.7052 |
| 16 | 0.39245 | SLE_F3 | Max | 0. | 0. | -1047.958 |
| 16 | 0.7849 | SLE_F3 | Max | 0. | 0. | -1014.592 |
| 16 | 0. | SLE_F3 | Min | 0. | 0. | -1065.7052 |
| 16 | 0.39245 | SLE_F3 | Min | 0. | 0. | -1047.958 |
| 16 | 0.7849 | SLE_F3 | Min | 0. | 0. | -1014.592 |
| 16 | 0. | SLE_F4 | Max | 0. | 0. | -963.632 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 16 | 0.39245 | SLE_F4 | Max | 0. | 0. | -941.7302 |
| 16 | 0.7849 | SLE_F4 | Max | 0. | 0. | -904.2098 |
| 16 | 0. | SLE_F4 | Min | 0. | 0. | -963.632 |
| 16 | 0.39245 | SLE_F4 | Min | 0. | 0. | -941.7302 |
| 16 | 0.7849 | SLE_F4 | Min | 0. | 0. | -904.2098 |
| 16 | 0. | SLE_QP1 | Max | 0. | 0. | -903.8727 |
| 16 | 0.39245 | SLE_QP1 | Max | 0. | 0. | -896.1387 |
| 16 | 0.7849 | SLE_QP1 | Max | 0. | 0. | -872.786 |
| 16 | 0. | SLE_QP1 | Min | 0. | 0. | -903.8727 |
| 16 | 0.39245 | SLE_QP1 | Min | 0. | 0. | -896.1387 |
| 16 | 0.7849 | SLE_QP1 | Min | 0. | 0. | -872.786 |
| 16 | 0. | SLE_QP2 | Max | 0. | 0. | -980.4269 |
| 16 | 0.39245 | SLE_QP2 | Max | 0. | 0. | -972.648 |
| 16 | 0.7849 | SLE_QP2 | Max | 0. | 0. | -949.2505 |
| 16 | 0. | SLE_QP2 | Min | 0. | 0. | -980.4269 |
| 16 | 0.39245 | SLE_QP2 | Min | 0. | 0. | -972.648 |
| 16 | 0.7849 | SLE_QP2 | Min | 0. | 0. | -949.2505 |
| 16 | 0. | SLE_QP3 | Max | 0. | 0. | -1017.4417 |
| 16 | 0.39245 | SLE_QP3 | Max | 0. | 0. | -999.1107 |
| 16 | 0.7849 | SLE_QP3 | Max | 0. | 0. | -965.1609 |
| 16 | 0. | SLE_QP3 | Min | 0. | 0. | -1017.4417 |
| 16 | 0.39245 | SLE_QP3 | Min | 0. | 0. | -999.1107 |
| 16 | 0.7849 | SLE_QP3 | Min | 0. | 0. | -965.1609 |
| 16 | 0. | SLE_QP4 | Max | 0. | 0. | -906.6456 |
| 16 | 0.39245 | SLE_QP4 | Max | 0. | 0. | -884.628 |
| 16 | 0.7849 | SLE_QP4 | Max | 0. | 0. | -846.9916 |
| 16 | 0. | SLE_QP4 | Min | 0. | 0. | -906.6456 |
| 16 | 0.39245 | SLE_QP4 | Min | 0. | 0. | -884.628 |
| 16 | 0.7849 | SLE_QP4 | Min | 0. | 0. | -846.9916 |
| 16 | 0. | SLV_1 | Max | 0. | 0. | -474.3728 |
| 16 | 0.39245 | SLV_1 | Max | 0. | 0. | -434.1397 |
| 16 | 0.7849 | SLV_1 | Max | 0. | 0. | -378.2879 |
| 16 | 0. | SLV_1 | Min | 0. | 0. | -474.3728 |
| 16 | 0.39245 | SLV_1 | Min | 0. | 0. | -434.1397 |
| 16 | 0.7849 | SLV_1 | Min | 0. | 0. | -378.2879 |
| 16 | 0. | SLV_2 | Max | 0. | 0. | -474.1809 |
| 16 | 0.39245 | SLV_2 | Max | 0. | 0. | -434.1978 |
| 16 | 0.7849 | SLV_2 | Max | 0. | 0. | -378.5961 |
| 16 | 0. | SLV_2 | Min | 0. | 0. | -474.1809 |
| 16 | 0.39245 | SLV_2 | Min | 0. | 0. | -434.1978 |
| 16 | 0.7849 | SLV_2 | Min | 0. | 0. | -378.5961 |
| 16 | 0. | SLV_3 | Max | 0. | 0. | -503.8054 |
| 16 | 0.39245 | SLV_3 | Max | 0. | 0. | -448.863 |
| 16 | 0.7849 | SLV_3 | Max | 0. | 0. | -378.3018 |
| 16 | 0. | SLV_3 | Min | 0. | 0. | -503.8054 |
| 16 | 0.39245 | SLV_3 | Min | 0. | 0. | -448.863 |
| 16 | 0.7849 | SLV_3 | Min | 0. | 0. | -378.3018 |
| 16 | 0. | SLV_4 | Max | 0. | 0. | -502.7289 |
| 16 | 0.39245 | SLV_4 | Max | 0. | 0. | -447.8219 |
| 16 | 0.7849 | SLV_4 | Max | 0. | 0. | -377.2962 |
| 16 | 0. | SLV_4 | Min | 0. | 0. | -502.7289 |
| 16 | 0.39245 | SLV_4 | Min | 0. | 0. | -447.8219 |
| 16 | 0.7849 | SLV_4 | Min | 0. | 0. | -377.2962 |
| 16 | 0. | SLD_1 | Max | 0. | 0. | -698.073 |
| 16 | 0.39245 | SLD_1 | Max | 0. | 0. | -678.4254 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 16 | 0.7849 | SLD_1 | Max | 0. | 0. | -643.1591 |
| 16 | 0. | SLD_1 | Min | 0. | 0. | -698.073 |
| 16 | 0.39245 | SLD_1 | Min | 0. | 0. | -678.4254 |
| 16 | 0.7849 | SLD_1 | Min | 0. | 0. | -643.1591 |
| 16 | 0. | SLD_2 | Max | 0. | 0. | -699.8033 |
| 16 | 0.39245 | SLD_2 | Max | 0. | 0. | -680.2198 |
| 16 | 0.7849 | SLD_2 | Max | 0. | 0. | -645.0176 |
| 16 | 0. | SLD_2 | Min | 0. | 0. | -699.8033 |
| 16 | 0.39245 | SLD_2 | Min | 0. | 0. | -680.2198 |
| 16 | 0.7849 | SLD_2 | Min | 0. | 0. | -645.0176 |
| 16 | 0. | SLD_3 | Max | 0. | 0. | -687.1123 |
| 16 | 0.39245 | SLD_3 | Max | 0. | 0. | -651.9547 |
| 16 | 0.7849 | SLD_3 | Max | 0. | 0. | -601.1785 |
| 16 | 0. | SLD_3 | Min | 0. | 0. | -687.1123 |
| 16 | 0.39245 | SLD_3 | Min | 0. | 0. | -651.9547 |
| 16 | 0.7849 | SLD_3 | Min | 0. | 0. | -601.1785 |
| 16 | 0. | SLD_4 | Max | 0. | 0. | -686.9528 |
| 16 | 0.39245 | SLD_4 | Max | 0. | 0. | -651.8485 |
| 16 | 0.7849 | SLD_4 | Max | 0. | 0. | -601.1255 |
| 16 | 0. | SLD_4 | Min | 0. | 0. | -686.9528 |
| 16 | 0.39245 | SLD_4 | Min | 0. | 0. | -651.8485 |
| 16 | 0.7849 | SLD_4 | Min | 0. | 0. | -601.1255 |
| 16 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1133.4181 |
| 16 | 0.39245 | SLU_IDR_1 | Max | 0. | 0. | -1114.4787 |
| 16 | 0.7849 | SLU_IDR_1 | Max | 0. | 0. | -1077.4349 |
| 16 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1133.4181 |
| 16 | 0.39245 | SLU_IDR_1 | Min | 0. | 0. | -1114.4787 |
| 16 | 0.7849 | SLU_IDR_1 | Min | 0. | 0. | -1077.4349 |
| 16 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1107.6521 |
| 16 | 0.39245 | SLU_IDR_2 | Max | 0. | 0. | -1098.9274 |
| 16 | 0.7849 | SLU_IDR_2 | Max | 0. | 0. | -1072.0983 |
| 16 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1107.6521 |
| 16 | 0.39245 | SLU_IDR_2 | Min | 0. | 0. | -1098.9274 |
| 16 | 0.7849 | SLU_IDR_2 | Min | 0. | 0. | -1072.0983 |
| 16 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 532.9987 |
| 16 | 0.39245 | SISMA WOOD SLV-1 | Max | 0. | 0. | 543.9337 |
| 16 | 0.7849 | SISMA WOOD SLV-1 | Max | 0. | 0. | 554.8687 |
| 16 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 532.9987 |
| 16 | 0.39245 | SISMA WOOD SLV-1 | Min | 0. | 0. | 543.9337 |
| 16 | 0.7849 | SISMA WOOD SLV-1 | Min | 0. | 0. | 554.8687 |
| 16 | 0. | DEAD-1 | Max | 0. | 0. | -34.6013 |
| 16 | 0.39245 | DEAD-1 | Max | 0. | 0. | -32.7122 |
| 16 | 0.7849 | DEAD-1 | Max | 0. | 0. | -35.4424 |
| 16 | 0. | DEAD-1 | Min | 0. | 0. | -34.6013 |
| 16 | 0.39245 | DEAD-1 | Min | 0. | 0. | -32.7122 |
| 16 | 0.7849 | DEAD-1 | Min | 0. | 0. | -35.4424 |
| 16 | 0. | SLU_PROVA | | 0. | 0. | -1043.8488 |
| 16 | 0.39245 | SLU_PROVA | | 0. | 0. | -1036.2678 |
| 16 | 0.7849 | SLU_PROVA | | 0. | 0. | -1008.3825 |
| 17 | 0. | DEAD | | 0. | 0. | -7.5599 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 17 | 0.6275 | DEAD | | 0. | 0. | -4.1986 |
| 17 | 1.255 | DEAD | | 0. | 0. | -12.5618 |
| 17 | 0. | SIMM_KA | | 0. | 0. | 67.9288 |
| 17 | 0.6275 | SIMM_KA | | 0. | 0. | 63.7295 |
| 17 | 1.255 | SIMM_KA | | 0. | 0. | 59.5301 |
| 17 | 0. | SIMM_K0 | | 0. | 0. | 102.9402 |
| 17 | 0.6275 | SIMM_K0 | | 0. | 0. | 96.7109 |
| 17 | 1.255 | SIMM_K0 | | 0. | 0. | 90.4816 |
| 17 | 0. | A--SIMM_KA | | 0. | 0. | 96.3758 |
| 17 | 0.6275 | A--SIMM_KA | | 0. | 0. | 101.0051 |
| 17 | 1.255 | A--SIMM_KA | | 0. | 0. | 105.6344 |
| 17 | 0. | A--SIMM_K0 | | 0. | 0. | 147.514 |
| 17 | 0.6275 | A--SIMM_K0 | | 0. | 0. | 154.0604 |
| 17 | 1.255 | A--SIMM_K0 | | 0. | 0. | 160.6068 |
| 17 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 5.4773 |
| 17 | 0.6275 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.5598 |
| 17 | 1.255 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.6424 |
| 17 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.2118 |
| 17 | 0.6275 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.3356 |
| 17 | 1.255 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.4594 |
| 17 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 8.2118 |
| 17 | 0.6275 | SIMM_SOVR_K 0 | | 0. | 0. | 8.3356 |
| 17 | 1.255 | SIMM_SOVR_K 0 | | 0. | 0. | 8.4594 |
| 17 | 0. | SIMM_SOVR_K A | | 0. | 0. | 5.4773 |
| 17 | 0.6275 | SIMM_SOVR_K A | | 0. | 0. | 5.5598 |
| 17 | 1.255 | SIMM_SOVR_K A | | 0. | 0. | 5.6424 |
| 17 | 0. | SOVR | | 0. | 0. | -79.446 |
| 17 | 0.6275 | SOVR | | 0. | 0. | -77.3295 |
| 17 | 1.255 | SOVR | | 0. | 0. | -75.2129 |
| 17 | 0. | TERR_SIMM | | 0. | 0. | -301.7119 |
| 17 | 0.6275 | TERR_SIMM | | 0. | 0. | -293.1042 |
| 17 | 1.255 | TERR_SIMM | | 0. | 0. | -284.4965 |
| 17 | 0. | TERR_A--SIMM | | 0. | 0. | -391.8928 |
| 17 | 0.6275 | TERR_A--SIMM | | 0. | 0. | -384.709 |
| 17 | 1.255 | TERR_A--SIMM | | 0. | 0. | -377.5251 |
| 17 | 0. | INERZIA H SLV | | 0. | 0. | 0.483 |
| 17 | 0.6275 | INERZIA H SLV | | 0. | 0. | 0.8691 |
| 17 | 1.255 | INERZIA H SLV | | 0. | 0. | 1.2552 |
| 17 | 0. | INERZIA V + SLV | | 0. | 0. | -0.0454 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 17 | 0.6275 | INERZIA V + SLV | | 0. | 0. | -0.087 |
| 17 | 1.255 | INERZIA V + SLV | | 0. | 0. | -0.1286 |
| 17 | 0. | INERZIA V - SLV | | 0. | 0. | 0.0454 |
| 17 | 0.6275 | INERZIA V - SLV | | 0. | 0. | 0.087 |
| 17 | 1.255 | INERZIA V - SLV | | 0. | 0. | 0.1286 |
| 17 | 0. | SISMA WOOD SLV | | 0. | 0. | 138.2195 |
| 17 | 0.6275 | SISMA WOOD SLV | | 0. | 0. | 138.2657 |
| 17 | 1.255 | SISMA WOOD SLV | | 0. | 0. | 141.5941 |
| 17 | 0. | iDROSTATICA | | 0. | 0. | -487.154 |
| 17 | 0.6275 | iDROSTATICA | | 0. | 0. | -499.8663 |
| 17 | 1.255 | iDROSTATICA | | 0. | 0. | -462.4793 |
| 17 | 0. | SISMA WOOD SLD | | 0. | 0. | 61.0433 |
| 17 | 0.6275 | SISMA WOOD SLD | | 0. | 0. | 61.0637 |
| 17 | 1.255 | SISMA WOOD SLD | | 0. | 0. | 62.5337 |
| 17 | 0. | INERZIA H SLD | | 0. | 0. | 0.2133 |
| 17 | 0.6275 | INERZIA H SLD | | 0. | 0. | 0.3838 |
| 17 | 1.255 | INERZIA H SLD | | 0. | 0. | 0.5544 |
| 17 | 0. | INERZIA V + SLD | | 0. | 0. | -0.0201 |
| 17 | 0.6275 | INERZIA V + SLD | | 0. | 0. | -0.0384 |
| 17 | 1.255 | INERZIA V + SLD | | 0. | 0. | -0.0568 |
| 17 | 0. | INERZIA V SLD | | 0. | 0. | 0.0201 |
| 17 | 0.6275 | INERZIA V SLD | | 0. | 0. | 0.0384 |
| 17 | 1.255 | INERZIA V SLD | | 0. | 0. | 0.0568 |
| 17 | 0. | INERZIA V -1 | | 0. | 0. | 0.0454 |
| 17 | 0.6275 | INERZIA V -1 | | 0. | 0. | 0.087 |
| 17 | 1.255 | INERZIA V -1 | | 0. | 0. | 0.1286 |
| 17 | 0. | SLU_1 | Max | 0. | 0. | -1214.2679 |
| 17 | 0.6275 | SLU_1 | Max | 0. | 0. | -1202.2161 |
| 17 | 1.255 | SLU_1 | Max | 0. | 0. | -1140.2771 |
| 17 | 0. | SLU_1 | Min | 0. | 0. | -1214.2679 |
| 17 | 0.6275 | SLU_1 | Min | 0. | 0. | -1202.2161 |
| 17 | 1.255 | SLU_1 | Min | 0. | 0. | -1140.2771 |
| 17 | 0. | SLU_2 | Max | 0. | 0. | -1322.7678 |
| 17 | 0.6275 | SLU_2 | Max | 0. | 0. | -1303.9825 |
| 17 | 1.255 | SLU_2 | Max | 0. | 0. | -1235.3099 |
| 17 | 0. | SLU_2 | Min | 0. | 0. | -1322.7678 |
| 17 | 0.6275 | SLU_2 | Min | 0. | 0. | -1303.9825 |
| 17 | 1.255 | SLU_2 | Min | 0. | 0. | -1235.3099 |
| 17 | 0. | SLU_3 | Max | 0. | 0. | -1215.0466 |
| 17 | 0.6275 | SLU_3 | Max | 0. | 0. | -1179.2812 |
| 17 | 1.255 | SLU_3 | Max | 0. | 0. | -1093.6285 |
| 17 | 0. | SLU_3 | Min | 0. | 0. | -1215.0466 |
| 17 | 0.6275 | SLU_3 | Min | 0. | 0. | -1179.2812 |
| 17 | 1.255 | SLU_3 | Min | 0. | 0. | -1093.6285 |
| 17 | 0. | SLU_4 | Max | 0. | 0. | -1353.5706 |
| 17 | 0.6275 | SLU_4 | Max | 0. | 0. | -1316.6751 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 17 | 1.255 | SLU_4 | Max | 0. | 0. | -1229.8925 |
| 17 | 0. | SLU_4 | Min | 0. | 0. | -1353.5706 |
| 17 | 0.6275 | SLU_4 | Min | 0. | 0. | -1316.6751 |
| 17 | 1.255 | SLU_4 | Min | 0. | 0. | -1229.8925 |
| 17 | 0. | SLE_F1 | Max | 0. | 0. | -911.7039 |
| 17 | 0.6275 | SLE_F1 | Max | 0. | 0. | -903.0782 |
| 17 | 1.255 | SLE_F1 | Max | 0. | 0. | -856.0777 |
| 17 | 0. | SLE_F1 | Min | 0. | 0. | -911.7039 |
| 17 | 0.6275 | SLE_F1 | Min | 0. | 0. | -903.0782 |
| 17 | 1.255 | SLE_F1 | Min | 0. | 0. | -856.0777 |
| 17 | 0. | SLE_F2 | Max | 0. | 0. | -993.6224 |
| 17 | 0.6275 | SLE_F2 | Max | 0. | 0. | -979.4545 |
| 17 | 1.255 | SLE_F2 | Max | 0. | 0. | -926.9118 |
| 17 | 0. | SLE_F2 | Min | 0. | 0. | -993.6224 |
| 17 | 0.6275 | SLE_F2 | Min | 0. | 0. | -979.4545 |
| 17 | 1.255 | SLE_F2 | Min | 0. | 0. | -926.9118 |
| 17 | 0. | SLE_F3 | Max | 0. | 0. | -1014.592 |
| 17 | 0.6275 | SLE_F3 | Max | 0. | 0. | -985.9871 |
| 17 | 1.255 | SLE_F3 | Max | 0. | 0. | -919.0074 |
| 17 | 0. | SLE_F3 | Min | 0. | 0. | -1014.592 |
| 17 | 0.6275 | SLE_F3 | Min | 0. | 0. | -985.9871 |
| 17 | 1.255 | SLE_F3 | Min | 0. | 0. | -919.0074 |
| 17 | 0. | SLE_F4 | Max | 0. | 0. | -904.2098 |
| 17 | 0.6275 | SLE_F4 | Max | 0. | 0. | -877.2009 |
| 17 | 1.255 | SLE_F4 | Max | 0. | 0. | -811.8173 |
| 17 | 0. | SLE_F4 | Min | 0. | 0. | -904.2098 |
| 17 | 0.6275 | SLE_F4 | Min | 0. | 0. | -877.2009 |
| 17 | 1.255 | SLE_F4 | Min | 0. | 0. | -811.8173 |
| 17 | 0. | SLE_QP1 | Max | 0. | 0. | -872.786 |
| 17 | 0.6275 | SLE_QP1 | Max | 0. | 0. | -864.4704 |
| 17 | 1.255 | SLE_QP1 | Max | 0. | 0. | -817.78 |
| 17 | 0. | SLE_QP1 | Min | 0. | 0. | -872.786 |
| 17 | 0.6275 | SLE_QP1 | Min | 0. | 0. | -864.4704 |
| 17 | 1.255 | SLE_QP1 | Min | 0. | 0. | -817.78 |
| 17 | 0. | SLE_QP2 | Max | 0. | 0. | -949.2505 |
| 17 | 0.6275 | SLE_QP2 | Max | 0. | 0. | -935.6074 |
| 17 | 1.255 | SLE_QP2 | Max | 0. | 0. | -883.5896 |
| 17 | 0. | SLE_QP2 | Min | 0. | 0. | -949.2505 |
| 17 | 0.6275 | SLE_QP2 | Min | 0. | 0. | -935.6074 |
| 17 | 1.255 | SLE_QP2 | Min | 0. | 0. | -883.5896 |
| 17 | 0. | SLE_QP3 | Max | 0. | 0. | -965.1609 |
| 17 | 0.6275 | SLE_QP3 | Max | 0. | 0. | -936.1407 |
| 17 | 1.255 | SLE_QP3 | Max | 0. | 0. | -868.7457 |
| 17 | 0. | SLE_QP3 | Min | 0. | 0. | -965.1609 |
| 17 | 0.6275 | SLE_QP3 | Min | 0. | 0. | -936.1407 |
| 17 | 1.255 | SLE_QP3 | Min | 0. | 0. | -868.7457 |
| 17 | 0. | SLE_QP4 | Max | 0. | 0. | -846.9916 |
| 17 | 0.6275 | SLE_QP4 | Max | 0. | 0. | -821.0199 |
| 17 | 1.255 | SLE_QP4 | Max | 0. | 0. | -756.6733 |
| 17 | 0. | SLE_QP4 | Min | 0. | 0. | -846.9916 |
| 17 | 0.6275 | SLE_QP4 | Min | 0. | 0. | -821.0199 |
| 17 | 1.255 | SLE_QP4 | Min | 0. | 0. | -756.6733 |
| 17 | 0. | SLV_1 | Max | 0. | 0. | -378.2879 |
| 17 | 0.6275 | SLV_1 | Max | 0. | 0. | -375.4051 |
| 17 | 1.255 | SLV_1 | Max | 0. | 0. | -330.8653 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 17 | 0. | SLV_1 | Min | 0. | 0. | -378.2879 |
| 17 | 0.6275 | SLV_1 | Min | 0. | 0. | -375.4051 |
| 17 | 1.255 | SLV_1 | Min | 0. | 0. | -330.8653 |
| 17 | 0. | SLV_2 | Max | 0. | 0. | -378.5961 |
| 17 | 0.6275 | SLV_2 | Max | 0. | 0. | -375.8346 |
| 17 | 1.255 | SLV_2 | Max | 0. | 0. | -331.4161 |
| 17 | 0. | SLV_2 | Min | 0. | 0. | -378.5961 |
| 17 | 0.6275 | SLV_2 | Min | 0. | 0. | -375.8346 |
| 17 | 1.255 | SLV_2 | Min | 0. | 0. | -331.4161 |
| 17 | 0. | SLV_3 | Max | 0. | 0. | -378.3018 |
| 17 | 0.6275 | SLV_3 | Max | 0. | 0. | -360.5447 |
| 17 | 1.255 | SLV_3 | Max | 0. | 0. | -301.1307 |
| 17 | 0. | SLV_3 | Min | 0. | 0. | -378.3018 |
| 17 | 0.6275 | SLV_3 | Min | 0. | 0. | -360.5447 |
| 17 | 1.255 | SLV_3 | Min | 0. | 0. | -301.1307 |
| 17 | 0. | SLV_4 | Max | 0. | 0. | -377.2962 |
| 17 | 0.6275 | SLV_4 | Max | 0. | 0. | -359.6094 |
| 17 | 1.255 | SLV_4 | Max | 0. | 0. | -300.2656 |
| 17 | 0. | SLV_4 | Min | 0. | 0. | -377.2962 |
| 17 | 0.6275 | SLV_4 | Min | 0. | 0. | -359.6094 |
| 17 | 1.255 | SLV_4 | Min | 0. | 0. | -300.2656 |
| 17 | 0. | SLD_1 | Max | 0. | 0. | -643.1591 |
| 17 | 0.6275 | SLD_1 | Max | 0. | 0. | -637.9874 |
| 17 | 1.255 | SLD_1 | Max | 0. | 0. | -592.9913 |
| 17 | 0. | SLD_1 | Min | 0. | 0. | -643.1591 |
| 17 | 0.6275 | SLD_1 | Min | 0. | 0. | -637.9874 |
| 17 | 1.255 | SLD_1 | Min | 0. | 0. | -592.9913 |
| 17 | 0. | SLD_2 | Max | 0. | 0. | -645.0176 |
| 17 | 0.6275 | SLD_2 | Max | 0. | 0. | -639.7332 |
| 17 | 1.255 | SLD_2 | Max | 0. | 0. | -594.6244 |
| 17 | 0. | SLD_2 | Min | 0. | 0. | -645.0176 |
| 17 | 0.6275 | SLD_2 | Min | 0. | 0. | -639.7332 |
| 17 | 1.255 | SLD_2 | Min | 0. | 0. | -594.6244 |
| 17 | 0. | SLD_3 | Max | 0. | 0. | -601.1785 |
| 17 | 0.6275 | SLD_3 | Max | 0. | 0. | -583.0021 |
| 17 | 1.255 | SLD_3 | Max | 0. | 0. | -525.0014 |
| 17 | 0. | SLD_3 | Min | 0. | 0. | -601.1785 |
| 17 | 0.6275 | SLD_3 | Min | 0. | 0. | -583.0021 |
| 17 | 1.255 | SLD_3 | Min | 0. | 0. | -525.0014 |
| 17 | 0. | SLD_4 | Max | 0. | 0. | -601.1255 |
| 17 | 0.6275 | SLD_4 | Max | 0. | 0. | -582.8896 |
| 17 | 1.255 | SLD_4 | Max | 0. | 0. | -524.8294 |
| 17 | 0. | SLD_4 | Min | 0. | 0. | -601.1255 |
| 17 | 0.6275 | SLD_4 | Min | 0. | 0. | -582.8896 |
| 17 | 1.255 | SLD_4 | Min | 0. | 0. | -524.8294 |
| 17 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1077.4349 |
| 17 | 0.6275 | SLU_IDR_1 | Max | 0. | 0. | -1043.8196 |
| 17 | 1.255 | SLU_IDR_1 | Max | 0. | 0. | -965.6472 |
| 17 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1077.4349 |
| 17 | 0.6275 | SLU_IDR_1 | Min | 0. | 0. | -1043.8196 |
| 17 | 1.255 | SLU_IDR_1 | Min | 0. | 0. | -965.6472 |
| 17 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1072.0983 |
| 17 | 0.6275 | SLU_IDR_2 | Max | 0. | 0. | -1053.9208 |
| 17 | 1.255 | SLU_IDR_2 | Max | 0. | 0. | -991.1861 |
| 17 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1072.0983 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 17 | 0.6275 | SLU_IDR_2 | Min | 0. | 0. | -1053.9208 |
| 17 | 1.255 | SLU_IDR_2 | Min | 0. | 0. | -991.1861 |
| 17 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 554.8687 |
| 17 | 0.6275 | SISMA WOOD SLV-1 | Max | 0. | 0. | 510.365 |
| 17 | 1.255 | SISMA WOOD SLV-1 | Max | 0. | 0. | 469.1435 |
| 17 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 554.8687 |
| 17 | 0.6275 | SISMA WOOD SLV-1 | Min | 0. | 0. | 510.365 |
| 17 | 1.255 | SISMA WOOD SLV-1 | Min | 0. | 0. | 469.1435 |
| 17 | 0. | DEAD-1 | Max | 0. | 0. | -35.4424 |
| 17 | 0.6275 | DEAD-1 | Max | 0. | 0. | -31.4092 |
| 17 | 1.255 | DEAD-1 | Max | 0. | 0. | -39.1004 |
| 17 | 0. | DEAD-1 | Min | 0. | 0. | -35.4424 |
| 17 | 0.6275 | DEAD-1 | Min | 0. | 0. | -31.4092 |
| 17 | 1.255 | DEAD-1 | Min | 0. | 0. | -39.1004 |
| 17 | 0. | SLU_PROVA | | 0. | 0. | -1008.3825 |
| 17 | 0.6275 | SLU_PROVA | | 0. | 0. | -1014.0864 |
| 17 | 1.255 | SLU_PROVA | | 0. | 0. | -969.903 |
| 19 | 0. | DEAD | | 0. | 0. | -75.9307 |
| 19 | 0.5 | DEAD | | 0. | 0. | -106.7354 |
| 19 | 1. | DEAD | | 0. | 0. | -137.54 |
| 19 | 0. | SIMM_KA | | 0. | 0. | 119.4794 |
| 19 | 0.5 | SIMM_KA | | 0. | 0. | 157.0099 |
| 19 | 1. | SIMM_KA | | 0. | 0. | 183.2116 |
| 19 | 0. | SIMM_K0 | | 0. | 0. | 177.4135 |
| 19 | 0.5 | SIMM_K0 | | 0. | 0. | 234.6696 |
| 19 | 1. | SIMM_K0 | | 0. | 0. | 274.9332 |
| 19 | 0. | A--SIMM_KA | | 0. | 0. | 208.4716 |
| 19 | 0.5 | A--SIMM_KA | | 0. | 0. | 236.0519 |
| 19 | 1. | A--SIMM_KA | | 0. | 0. | 254.9947 |
| 19 | 0. | A--SIMM_K0 | | 0. | 0. | 326.2346 |
| 19 | 0.5 | A--SIMM_K0 | | 0. | 0. | 369.2059 |
| 19 | 1. | A--SIMM_K0 | | 0. | 0. | 396.9346 |
| 19 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -0.6329 |
| 19 | 0.5 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.1894 |
| 19 | 1. | A-- SIMM_SOVR_K A | | 0. | 0. | 11.0117 |
| 19 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -0.9489 |
| 19 | 0.5 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 7.7802 |
| 19 | 1. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 16.5092 |
| 19 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -0.9489 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 19 | 0.5 | SIMM_SOVR_K 0 | | 0. | 0. | 7.7802 |
| 19 | 1. | SIMM_SOVR_K 0 | | 0. | 0. | 16.5092 |
| 19 | 0. | SIMM_SOVR_K A | | 0. | 0. | -0.6329 |
| 19 | 0.5 | SIMM_SOVR_K A | | 0. | 0. | 5.1894 |
| 19 | 1. | SIMM_SOVR_K A | | 0. | 0. | 11.0117 |
| 19 | 0. | SOVR | | 0. | 0. | -130.2429 |
| 19 | 0.5 | SOVR | | 0. | 0. | -148.6712 |
| 19 | 1. | SOVR | | 0. | 0. | -167.0996 |
| 19 | 0. | TERR_SIMM | | 0. | 0. | -519.1051 |
| 19 | 0.5 | TERR_SIMM | | 0. | 0. | -576.9936 |
| 19 | 1. | TERR_SIMM | | 0. | 0. | -634.8821 |
| 19 | 0. | TERR_A--SIMM | | 0. | 0. | -509.8045 |
| 19 | 0.5 | TERR_A--SIMM | | 0. | 0. | -579.8845 |
| 19 | 1. | TERR_A--SIMM | | 0. | 0. | -649.9646 |
| 19 | 0. | INERZIA H SLV | | 0. | 0. | 9.187 |
| 19 | 0.5 | INERZIA H SLV | | 0. | 0. | 8.6147 |
| 19 | 1. | INERZIA H SLV | | 0. | 0. | 8.0425 |
| 19 | 0. | INERZIA V + SLV | | 0. | 0. | -1.2416 |
| 19 | 0.5 | INERZIA V + SLV | | 0. | 0. | -1.7293 |
| 19 | 1. | INERZIA V + SLV | | 0. | 0. | -2.217 |
| 19 | 0. | INERZIA V - SLV | | 0. | 0. | 1.2416 |
| 19 | 0.5 | INERZIA V - SLV | | 0. | 0. | 1.7293 |
| 19 | 1. | INERZIA V - SLV | | 0. | 0. | 2.217 |
| 19 | 0. | SISMA WOOD SLV | | 0. | 0. | 496.768 |
| 19 | 0.5 | SISMA WOOD SLV | | 0. | 0. | 500.9582 |
| 19 | 1. | SISMA WOOD SLV | | 0. | 0. | 505.1484 |
| 19 | 0. | iDROSTATICA | | 0. | 0. | -513.3901 |
| 19 | 0.5 | iDROSTATICA | | 0. | 0. | -409.1115 |
| 19 | 1. | iDROSTATICA | | 0. | 0. | -328.983 |
| 19 | 0. | SISMA WOOD SLD | | 0. | 0. | 219.3928 |
| 19 | 0.5 | SISMA WOOD SLD | | 0. | 0. | 221.2433 |
| 19 | 1. | SISMA WOOD SLD | | 0. | 0. | 223.0939 |
| 19 | 0. | INERZIA H SLD | | 0. | 0. | 4.0573 |
| 19 | 0.5 | INERZIA H SLD | | 0. | 0. | 3.8046 |
| 19 | 1. | INERZIA H SLD | | 0. | 0. | 3.5519 |
| 19 | 0. | INERZIA V + SLD | | 0. | 0. | -0.5483 |
| 19 | 0.5 | INERZIA V + SLD | | 0. | 0. | -0.7637 |
| 19 | 1. | INERZIA V + SLD | | 0. | 0. | -0.9791 |
| 19 | 0. | INERZIA V SLD | | 0. | 0. | 0.5483 |
| 19 | 0.5 | INERZIA V SLD | | 0. | 0. | 0.7637 |
| 19 | 1. | INERZIA V SLD | | 0. | 0. | 0.9791 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------|----------|-----------|------------|------------|
| 19 | 0. | INERZIA V -1 | | 0. | 0. | 1.2416 |
| 19 | 0.5 | INERZIA V -1 | | 0. | 0. | 1.7293 |
| 19 | 1. | INERZIA V -1 | | 0. | 0. | 2.217 |
| 19 | 0. | SLU_1 | Max | 0. | 0. | -1615.0903 |
| 19 | 0.5 | SLU_1 | Max | 0. | 0. | -1552.3978 |
| 19 | 1. | SLU_1 | Max | 0. | 0. | -1543.1906 |
| 19 | 0. | SLU_1 | Min | 0. | 0. | -1615.0903 |
| 19 | 0.5 | SLU_1 | Min | 0. | 0. | -1552.3978 |
| 19 | 1. | SLU_1 | Min | 0. | 0. | -1543.1906 |
| 19 | 0. | SLU_2 | Max | 0. | 0. | -1726.2894 |
| 19 | 0.5 | SLU_2 | Max | 0. | 0. | -1694.7824 |
| 19 | 1. | SLU_2 | Max | 0. | 0. | -1709.3977 |
| 19 | 0. | SLU_2 | Min | 0. | 0. | -1726.2894 |
| 19 | 0.5 | SLU_2 | Min | 0. | 0. | -1694.7824 |
| 19 | 1. | SLU_2 | Min | 0. | 0. | -1709.3977 |
| 19 | 0. | SLU_3 | Max | 0. | 0. | -1217.2866 |
| 19 | 0.5 | SLU_3 | Max | 0. | 0. | -1210.5841 |
| 19 | 1. | SLU_3 | Max | 0. | 0. | -1255.0919 |
| 19 | 0. | SLU_3 | Min | 0. | 0. | -1217.2866 |
| 19 | 0.5 | SLU_3 | Min | 0. | 0. | -1210.5841 |
| 19 | 1. | SLU_3 | Min | 0. | 0. | -1255.0919 |
| 19 | 0. | SLU_4 | Max | 0. | 0. | -1456.7248 |
| 19 | 0.5 | SLU_4 | Max | 0. | 0. | -1472.7048 |
| 19 | 1. | SLU_4 | Max | 0. | 0. | -1531.3086 |
| 19 | 0. | SLU_4 | Min | 0. | 0. | -1456.7248 |
| 19 | 0.5 | SLU_4 | Min | 0. | 0. | -1472.7048 |
| 19 | 1. | SLU_4 | Min | 0. | 0. | -1531.3086 |
| 19 | 0. | SLE_F1 | Max | 0. | 0. | -1188.2285 |
| 19 | 0.5 | SLE_F1 | Max | 0. | 0. | -1133.7664 |
| 19 | 1. | SLE_F1 | Max | 0. | 0. | -1120.4467 |
| 19 | 0. | SLE_F1 | Min | 0. | 0. | -1188.2285 |
| 19 | 0.5 | SLE_F1 | Min | 0. | 0. | -1133.7664 |
| 19 | 1. | SLE_F1 | Min | 0. | 0. | -1120.4467 |
| 19 | 0. | SLE_F2 | Max | 0. | 0. | -1275.5313 |
| 19 | 0.5 | SLE_F2 | Max | 0. | 0. | -1243.5701 |
| 19 | 1. | SLE_F2 | Max | 0. | 0. | -1247.0877 |
| 19 | 0. | SLE_F2 | Min | 0. | 0. | -1275.5313 |
| 19 | 0.5 | SLE_F2 | Min | 0. | 0. | -1243.5701 |
| 19 | 1. | SLE_F2 | Min | 0. | 0. | -1247.0877 |
| 19 | 0. | SLE_F3 | Max | 0. | 0. | -1067.4901 |
| 19 | 0.5 | SLE_F3 | Max | 0. | 0. | -1072.1392 |
| 19 | 1. | SLE_F3 | Max | 0. | 0. | -1109.5759 |
| 19 | 0. | SLE_F3 | Min | 0. | 0. | -1067.4901 |
| 19 | 0.5 | SLE_F3 | Min | 0. | 0. | -1072.1392 |
| 19 | 1. | SLE_F3 | Min | 0. | 0. | -1109.5759 |
| 19 | 0. | SLE_F4 | Max | 0. | 0. | -874.0433 |
| 19 | 0.5 | SLE_F4 | Max | 0. | 0. | -862.095 |
| 19 | 1. | SLE_F4 | Max | 0. | 0. | -889.5393 |
| 19 | 0. | SLE_F4 | Min | 0. | 0. | -874.0433 |
| 19 | 0.5 | SLE_F4 | Min | 0. | 0. | -862.095 |
| 19 | 1. | SLE_F4 | Min | 0. | 0. | -889.5393 |
| 19 | 0. | SLE_QP1 | Max | 0. | 0. | -1092.9722 |
| 19 | 0.5 | SLE_QP1 | Max | 0. | 0. | -1026.4556 |
| 19 | 1. | SLE_QP1 | Max | 0. | 0. | -1001.0815 |
| 19 | 0. | SLE_QP1 | Min | 0. | 0. | -1092.9722 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 19 | 0.5 | SLE_QP1 | Min | 0. | 0. | -1026.4556 |
| 19 | 1. | SLE_QP1 | Min | 0. | 0. | -1001.0815 |
| 19 | 0. | SLE_QP2 | Max | 0. | 0. | -1178.2489 |
| 19 | 0.5 | SLE_QP2 | Max | 0. | 0. | -1131.9374 |
| 19 | 1. | SLE_QP2 | Max | 0. | 0. | -1121.1046 |
| 19 | 0. | SLE_QP2 | Min | 0. | 0. | -1178.2489 |
| 19 | 0.5 | SLE_QP2 | Min | 0. | 0. | -1131.9374 |
| 19 | 1. | SLE_QP2 | Min | 0. | 0. | -1121.1046 |
| 19 | 0. | SLE_QP3 | Max | 0. | 0. | -968.9374 |
| 19 | 0.5 | SLE_QP3 | Max | 0. | 0. | -959.3919 |
| 19 | 1. | SLE_QP3 | Max | 0. | 0. | -982.634 |
| 19 | 0. | SLE_QP3 | Min | 0. | 0. | -968.9374 |
| 19 | 0.5 | SLE_QP3 | Min | 0. | 0. | -959.3919 |
| 19 | 1. | SLE_QP3 | Min | 0. | 0. | -982.634 |
| 19 | 0. | SLE_QP4 | Max | 0. | 0. | -758.2634 |
| 19 | 0.5 | SLE_QP4 | Max | 0. | 0. | -733.52 |
| 19 | 1. | SLE_QP4 | Max | 0. | 0. | -748.1692 |
| 19 | 0. | SLE_QP4 | Min | 0. | 0. | -758.2634 |
| 19 | 0.5 | SLE_QP4 | Min | 0. | 0. | -733.52 |
| 19 | 1. | SLE_QP4 | Min | 0. | 0. | -748.1692 |
| 19 | 0. | SLV_1 | Max | 0. | 0. | 89.5946 |
| 19 | 0.5 | SLV_1 | Max | 0. | 0. | 184.3683 |
| 19 | 1. | SLV_1 | Max | 0. | 0. | 237.9996 |
| 19 | 0. | SLV_1 | Min | 0. | 0. | 89.5946 |
| 19 | 0.5 | SLV_1 | Min | 0. | 0. | 184.3683 |
| 19 | 1. | SLV_1 | Min | 0. | 0. | 237.9996 |
| 19 | 0. | SLV_2 | Max | 0. | 0. | 91.4194 |
| 19 | 0.5 | SLV_2 | Max | 0. | 0. | 187.5565 |
| 19 | 1. | SLV_2 | Max | 0. | 0. | 242.551 |
| 19 | 0. | SLV_2 | Min | 0. | 0. | 91.4194 |
| 19 | 0.5 | SLV_2 | Min | 0. | 0. | 187.5565 |
| 19 | 1. | SLV_2 | Min | 0. | 0. | 242.551 |
| 19 | 0. | SLV_3 | Max | 0. | 0. | 392.2542 |
| 19 | 0.5 | SLV_3 | Max | 0. | 0. | 462.3447 |
| 19 | 1. | SLV_3 | Max | 0. | 0. | 493.0427 |
| 19 | 0. | SLV_3 | Min | 0. | 0. | 392.2542 |
| 19 | 0.5 | SLV_3 | Min | 0. | 0. | 462.3447 |
| 19 | 1. | SLV_3 | Min | 0. | 0. | 493.0427 |
| 19 | 0. | SLV_4 | Max | 0. | 0. | 394.7265 |
| 19 | 0.5 | SLV_4 | Max | 0. | 0. | 466.1318 |
| 19 | 1. | SLV_4 | Max | 0. | 0. | 498.1447 |
| 19 | 0. | SLV_4 | Min | 0. | 0. | 394.7265 |
| 19 | 0.5 | SLV_4 | Min | 0. | 0. | 466.1318 |
| 19 | 1. | SLV_4 | Min | 0. | 0. | 498.1447 |
| 19 | 0. | SLD_1 | Max | 0. | 0. | -535.6674 |
| 19 | 0.5 | SLD_1 | Max | 0. | 0. | -466.4009 |
| 19 | 1. | SLD_1 | Max | 0. | 0. | -438.277 |
| 19 | 0. | SLD_1 | Min | 0. | 0. | -535.6674 |
| 19 | 0.5 | SLD_1 | Min | 0. | 0. | -466.4009 |
| 19 | 1. | SLD_1 | Min | 0. | 0. | -438.277 |
| 19 | 0. | SLD_2 | Max | 0. | 0. | -535.3377 |
| 19 | 0.5 | SLD_2 | Max | 0. | 0. | -465.3491 |
| 19 | 1. | SLD_2 | Max | 0. | 0. | -436.503 |
| 19 | 0. | SLD_2 | Min | 0. | 0. | -535.3377 |
| 19 | 0.5 | SLD_2 | Min | 0. | 0. | -465.3491 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 19 | 1. | SLD_2 | Min | 0. | 0. | -436.503 |
| 19 | 0. | SLD_3 | Max | 0. | 0. | -202.5092 |
| 19 | 0.5 | SLD_3 | Max | 0. | 0. | -158.4614 |
| 19 | 1. | SLD_3 | Max | 0. | 0. | -153.8062 |
| 19 | 0. | SLD_3 | Min | 0. | 0. | -202.5092 |
| 19 | 0.5 | SLD_3 | Min | 0. | 0. | -158.4614 |
| 19 | 1. | SLD_3 | Min | 0. | 0. | -153.8062 |
| 19 | 0. | SLD_4 | Max | 0. | 0. | -201.479 |
| 19 | 0.5 | SLD_4 | Max | 0. | 0. | -156.8387 |
| 19 | 1. | SLD_4 | Max | 0. | 0. | -151.5908 |
| 19 | 0. | SLD_4 | Min | 0. | 0. | -201.479 |
| 19 | 0.5 | SLD_4 | Min | 0. | 0. | -156.8387 |
| 19 | 1. | SLD_4 | Min | 0. | 0. | -151.5908 |
| 19 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1053.2223 |
| 19 | 0.5 | SLU_IDR_1 | Max | 0. | 0. | -1013.7097 |
| 19 | 1. | SLU_IDR_1 | Max | 0. | 0. | -1008.5359 |
| 19 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1053.2223 |
| 19 | 0.5 | SLU_IDR_1 | Min | 0. | 0. | -1013.7097 |
| 19 | 1. | SLU_IDR_1 | Min | 0. | 0. | -1008.5359 |
| 19 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1247.1809 |
| 19 | 0.5 | SLU_IDR_2 | Max | 0. | 0. | -1173.7307 |
| 19 | 1. | SLU_IDR_2 | Max | 0. | 0. | -1137.0413 |
| 19 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1247.1809 |
| 19 | 0.5 | SLU_IDR_2 | Min | 0. | 0. | -1173.7307 |
| 19 | 1. | SLU_IDR_2 | Min | 0. | 0. | -1137.0413 |
| 19 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 1096.6788 |
| 19 | 0.5 | SISMA WOOD SLV-1 | Max | 0. | 0. | 1129.7872 |
| 19 | 1. | SISMA WOOD SLV-1 | Max | 0. | 0. | 1162.8956 |
| 19 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 1096.6788 |
| 19 | 0.5 | SISMA WOOD SLV-1 | Min | 0. | 0. | 1129.7872 |
| 19 | 1. | SISMA WOOD SLV-1 | Min | 0. | 0. | 1162.8956 |
| 19 | 0. | DEAD-1 | Max | 0. | 0. | -118.9266 |
| 19 | 0.5 | DEAD-1 | Max | 0. | 0. | -157.2586 |
| 19 | 1. | DEAD-1 | Max | 0. | 0. | -195.5906 |
| 19 | 0. | DEAD-1 | Min | 0. | 0. | -118.9266 |
| 19 | 0.5 | DEAD-1 | Min | 0. | 0. | -157.2586 |
| 19 | 1. | DEAD-1 | Min | 0. | 0. | -195.5906 |
| 19 | 0. | SLU_PROVA | | 0. | 0. | -1407.1038 |
| 19 | 0.5 | SLU_PROVA | | 0. | 0. | -1326.9587 |
| 19 | 1. | SLU_PROVA | | 0. | 0. | -1300.2989 |
| 20 | 0. | DEAD | | 0. | 0. | -137.54 |
| 20 | 0.28595 | DEAD | | 0. | 0. | -157.5598 |
| 20 | 0.5719 | DEAD | | 0. | 0. | -177.5796 |
| 20 | 0. | SIMM_KA | | 0. | 0. | 183.2116 |
| 20 | 0.28595 | SIMM_KA | | 0. | 0. | 198.4143 |
| 20 | 0.5719 | SIMM_KA | | 0. | 0. | 210.3283 |
| 20 | 0. | SIMM_K0 | | 0. | 0. | 274.9332 |
| 20 | 0.28595 | SIMM_K0 | | 0. | 0. | 298.4412 |
| 20 | 0.5719 | SIMM_K0 | | 0. | 0. | 317.0165 |
| 20 | 0. | A--SIMM_KA | | 0. | 0. | 254.9947 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 20 | 0.28595 | A--SIMM_KA | | 0. | 0. | 259.3305 |
| 20 | 0.5719 | A--SIMM_KA | | 0. | 0. | 261.1737 |
| 20 | 0. | A--SIMM_K0 | | 0. | 0. | 396.9346 |
| 20 | 0.28595 | A--SIMM_K0 | | 0. | 0. | 402.8862 |
| 20 | 0.5719 | A--SIMM_K0 | | 0. | 0. | 404.6002 |
| 20 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 11.0117 |
| 20 | 0.28595 | A-- SIMM_SOVR_K A | | 0. | 0. | 15.0189 |
| 20 | 0.5719 | A-- SIMM_SOVR_K A | | 0. | 0. | 19.0261 |
| 20 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 16.5092 |
| 20 | 0.28595 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 22.5171 |
| 20 | 0.5719 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 28.5249 |
| 20 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 16.5092 |
| 20 | 0.28595 | SIMM_SOVR_K 0 | | 0. | 0. | 22.5171 |
| 20 | 0.5719 | SIMM_SOVR_K 0 | | 0. | 0. | 28.5249 |
| 20 | 0. | SIMM_SOVR_K A | | 0. | 0. | 11.0117 |
| 20 | 0.28595 | SIMM_SOVR_K A | | 0. | 0. | 15.0189 |
| 20 | 0.5719 | SIMM_SOVR_K A | | 0. | 0. | 19.0261 |
| 20 | 0. | SOVR | | 0. | 0. | -167.0996 |
| 20 | 0.28595 | SOVR | | 0. | 0. | -180.7528 |
| 20 | 0.5719 | SOVR | | 0. | 0. | -194.4061 |
| 20 | 0. | TERR_SIMM | | 0. | 0. | -634.8821 |
| 20 | 0.28595 | TERR_SIMM | | 0. | 0. | -678.6196 |
| 20 | 0.5719 | TERR_SIMM | | 0. | 0. | -722.3571 |
| 20 | 0. | TERR_A--SIMM | | 0. | 0. | -649.9646 |
| 20 | 0.28595 | TERR_A--SIMM | | 0. | 0. | -703.1744 |
| 20 | 0.5719 | TERR_A--SIMM | | 0. | 0. | -756.3843 |
| 20 | 0. | INERZIA H SLV | | 0. | 0. | 8.0425 |
| 20 | 0.28595 | INERZIA H SLV | | 0. | 0. | 6.7088 |
| 20 | 0.5719 | INERZIA H SLV | | 0. | 0. | 5.3752 |
| 20 | 0. | INERZIA V + SLV | | 0. | 0. | -2.217 |
| 20 | 0.28595 | INERZIA V + SLV | | 0. | 0. | -2.5348 |
| 20 | 0.5719 | INERZIA V + SLV | | 0. | 0. | -2.8526 |
| 20 | 0. | INERZIA V - SLV | | 0. | 0. | 2.217 |
| 20 | 0.28595 | INERZIA V - SLV | | 0. | 0. | 2.5348 |
| 20 | 0.5719 | INERZIA V - SLV | | 0. | 0. | 2.8526 |
| 20 | 0. | SISMA WOOD SLV | | 0. | 0. | 505.1484 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 20 | 0.28595 | SISMA WOOD SLV | | 0. | 0. | 466.64 |
| 20 | 0.5719 | SISMA WOOD SLV | | 0. | 0. | 428.1316 |
| 20 | 0. | iDROSTATICA | | 0. | 0. | -328.983 |
| 20 | 0.28595 | iDROSTATICA | | 0. | 0. | -295.9349 |
| 20 | 0.5719 | iDROSTATICA | | 0. | 0. | -269.3857 |
| 20 | 0. | SISMA WOOD SLD | | 0. | 0. | 223.0939 |
| 20 | 0.28595 | SISMA WOOD SLD | | 0. | 0. | 206.0871 |
| 20 | 0.5719 | SISMA WOOD SLD | | 0. | 0. | 189.0802 |
| 20 | 0. | INERZIA H SLD | | 0. | 0. | 3.5519 |
| 20 | 0.28595 | INERZIA H SLD | | 0. | 0. | 2.9629 |
| 20 | 0.5719 | INERZIA H SLD | | 0. | 0. | 2.3739 |
| 20 | 0. | INERZIA V + SLD | | 0. | 0. | -0.9791 |
| 20 | 0.28595 | INERZIA V + SLD | | 0. | 0. | -1.1195 |
| 20 | 0.5719 | INERZIA V + SLD | | 0. | 0. | -1.2598 |
| 20 | 0. | INERZIA V SLD | | 0. | 0. | 0.9791 |
| 20 | 0.28595 | INERZIA V SLD | | 0. | 0. | 1.1195 |
| 20 | 0.5719 | INERZIA V SLD | | 0. | 0. | 1.2598 |
| 20 | 0. | INERZIA V -1 | | 0. | 0. | 2.217 |
| 20 | 0.28595 | INERZIA V -1 | | 0. | 0. | 2.5348 |
| 20 | 0.5719 | INERZIA V -1 | | 0. | 0. | 2.8526 |
| 20 | 0. | SLU_1 | Max | 0. | 0. | -1543.1906 |
| 20 | 0.28595 | SLU_1 | Max | 0. | 0. | -1578.5793 |
| 20 | 0.5719 | SLU_1 | Max | 0. | 0. | -1628.8289 |
| 20 | 0. | SLU_1 | Min | 0. | 0. | -1543.1906 |
| 20 | 0.28595 | SLU_1 | Min | 0. | 0. | -1578.5793 |
| 20 | 0.5719 | SLU_1 | Min | 0. | 0. | -1628.8289 |
| 20 | 0. | SLU_2 | Max | 0. | 0. | -1709.3977 |
| 20 | 0.28595 | SLU_2 | Max | 0. | 0. | -1760.4562 |
| 20 | 0.5719 | SLU_2 | Max | 0. | 0. | -1824.2385 |
| 20 | 0. | SLU_2 | Min | 0. | 0. | -1709.3977 |
| 20 | 0.28595 | SLU_2 | Min | 0. | 0. | -1760.4562 |
| 20 | 0.5719 | SLU_2 | Min | 0. | 0. | -1824.2385 |
| 20 | 0. | SLU_3 | Max | 0. | 0. | -1255.0919 |
| 20 | 0.28595 | SLU_3 | Max | 0. | 0. | -1344.7756 |
| 20 | 0.5719 | SLU_3 | Max | 0. | 0. | -1448.4167 |
| 20 | 0. | SLU_3 | Min | 0. | 0. | -1255.0919 |
| 20 | 0.28595 | SLU_3 | Min | 0. | 0. | -1344.7756 |
| 20 | 0.5719 | SLU_3 | Min | 0. | 0. | -1448.4167 |
| 20 | 0. | SLU_4 | Max | 0. | 0. | -1531.3086 |
| 20 | 0.28595 | SLU_4 | Max | 0. | 0. | -1624.3161 |
| 20 | 0.5719 | SLU_4 | Max | 0. | 0. | -1729.0125 |
| 20 | 0. | SLU_4 | Min | 0. | 0. | -1531.3086 |
| 20 | 0.28595 | SLU_4 | Min | 0. | 0. | -1624.3161 |
| 20 | 0.5719 | SLU_4 | Min | 0. | 0. | -1729.0125 |
| 20 | 0. | SLE_F1 | Max | 0. | 0. | -1120.4467 |
| 20 | 0.28595 | SLE_F1 | Max | 0. | 0. | -1143.1427 |
| 20 | 0.5719 | SLE_F1 | Max | 0. | 0. | -1177.2701 |
| 20 | 0. | SLE_F1 | Min | 0. | 0. | -1120.4467 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 20 | 0.28595 | SLE_F1 | Min | 0. | 0. | -1143.1427 |
| 20 | 0.5719 | SLE_F1 | Min | 0. | 0. | -1177.2701 |
| 20 | 0. | SLE_F2 | Max | 0. | 0. | -1247.0877 |
| 20 | 0.28595 | SLE_F2 | Max | 0. | 0. | -1280.8442 |
| 20 | 0.5719 | SLE_F2 | Max | 0. | 0. | -1324.3884 |
| 20 | 0. | SLE_F2 | Min | 0. | 0. | -1247.0877 |
| 20 | 0.28595 | SLE_F2 | Min | 0. | 0. | -1280.8442 |
| 20 | 0.5719 | SLE_F2 | Min | 0. | 0. | -1324.3884 |
| 20 | 0. | SLE_F3 | Max | 0. | 0. | -1109.5759 |
| 20 | 0.28595 | SLE_F3 | Max | 0. | 0. | -1175.5685 |
| 20 | 0.5719 | SLE_F3 | Max | 0. | 0. | -1250.5526 |
| 20 | 0. | SLE_F3 | Min | 0. | 0. | -1109.5759 |
| 20 | 0.28595 | SLE_F3 | Min | 0. | 0. | -1175.5685 |
| 20 | 0.5719 | SLE_F3 | Min | 0. | 0. | -1250.5526 |
| 20 | 0. | SLE_F4 | Max | 0. | 0. | -889.5393 |
| 20 | 0.28595 | SLE_F4 | Max | 0. | 0. | -954.0932 |
| 20 | 0.5719 | SLE_F4 | Max | 0. | 0. | -1029.3835 |
| 20 | 0. | SLE_F4 | Min | 0. | 0. | -889.5393 |
| 20 | 0.28595 | SLE_F4 | Min | 0. | 0. | -954.0932 |
| 20 | 0.5719 | SLE_F4 | Min | 0. | 0. | -1029.3835 |
| 20 | 0. | SLE_QP1 | Max | 0. | 0. | -1001.0815 |
| 20 | 0.28595 | SLE_QP1 | Max | 0. | 0. | -1015.1632 |
| 20 | 0.5719 | SLE_QP1 | Max | 0. | 0. | -1040.6764 |
| 20 | 0. | SLE_QP1 | Min | 0. | 0. | -1001.0815 |
| 20 | 0.28595 | SLE_QP1 | Min | 0. | 0. | -1015.1632 |
| 20 | 0.5719 | SLE_QP1 | Min | 0. | 0. | -1040.6764 |
| 20 | 0. | SLE_QP2 | Max | 0. | 0. | -1121.1046 |
| 20 | 0.28595 | SLE_QP2 | Max | 0. | 0. | -1144.6085 |
| 20 | 0.5719 | SLE_QP2 | Max | 0. | 0. | -1177.9 |
| 20 | 0. | SLE_QP2 | Min | 0. | 0. | -1121.1046 |
| 20 | 0.28595 | SLE_QP2 | Min | 0. | 0. | -1144.6085 |
| 20 | 0.5719 | SLE_QP2 | Min | 0. | 0. | -1177.9 |
| 20 | 0. | SLE_QP3 | Max | 0. | 0. | -982.634 |
| 20 | 0.28595 | SLE_QP3 | Max | 0. | 0. | -1038.3163 |
| 20 | 0.5719 | SLE_QP3 | Max | 0. | 0. | -1102.9901 |
| 20 | 0. | SLE_QP3 | Min | 0. | 0. | -982.634 |
| 20 | 0.28595 | SLE_QP3 | Min | 0. | 0. | -1038.3163 |
| 20 | 0.5719 | SLE_QP3 | Min | 0. | 0. | -1102.9901 |
| 20 | 0. | SLE_QP4 | Max | 0. | 0. | -748.1692 |
| 20 | 0.28595 | SLE_QP4 | Max | 0. | 0. | -804.4443 |
| 20 | 0.5719 | SLE_QP4 | Max | 0. | 0. | -871.456 |
| 20 | 0. | SLE_QP4 | Min | 0. | 0. | -748.1692 |
| 20 | 0.28595 | SLE_QP4 | Min | 0. | 0. | -804.4443 |
| 20 | 0.5719 | SLE_QP4 | Min | 0. | 0. | -871.456 |
| 20 | 0. | SLV_1 | Max | 0. | 0. | 237.9996 |
| 20 | 0.28595 | SLV_1 | Max | 0. | 0. | 157.6084 |
| 20 | 0.5719 | SLV_1 | Max | 0. | 0. | 65.7858 |
| 20 | 0. | SLV_1 | Min | 0. | 0. | 237.9996 |
| 20 | 0.28595 | SLV_1 | Min | 0. | 0. | 157.6084 |
| 20 | 0.5719 | SLV_1 | Min | 0. | 0. | 65.7858 |
| 20 | 0. | SLV_2 | Max | 0. | 0. | 242.551 |
| 20 | 0.28595 | SLV_2 | Max | 0. | 0. | 163.0164 |
| 20 | 0.5719 | SLV_2 | Max | 0. | 0. | 72.0502 |
| 20 | 0. | SLV_2 | Min | 0. | 0. | 242.551 |
| 20 | 0.28595 | SLV_2 | Min | 0. | 0. | 163.0164 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 20 | 0.5719 | SLV_2 | Min | 0. | 0. | 72.0502 |
| 20 | 0. | SLV_3 | Max | 0. | 0. | 493.0427 |
| 20 | 0.28595 | SLV_3 | Max | 0. | 0. | 374.822 |
| 20 | 0.5719 | SLV_3 | Max | 0. | 0. | 245.8648 |
| 20 | 0. | SLV_3 | Min | 0. | 0. | 493.0427 |
| 20 | 0.28595 | SLV_3 | Min | 0. | 0. | 374.822 |
| 20 | 0.5719 | SLV_3 | Min | 0. | 0. | 245.8648 |
| 20 | 0. | SLV_4 | Max | 0. | 0. | 498.1447 |
| 20 | 0.28595 | SLV_4 | Max | 0. | 0. | 380.7681 |
| 20 | 0.5719 | SLV_4 | Max | 0. | 0. | 252.655 |
| 20 | 0. | SLV_4 | Min | 0. | 0. | 498.1447 |
| 20 | 0.28595 | SLV_4 | Min | 0. | 0. | 380.7681 |
| 20 | 0.5719 | SLV_4 | Min | 0. | 0. | 252.655 |
| 20 | 0. | SLD_1 | Max | 0. | 0. | -438.277 |
| 20 | 0.28595 | SLD_1 | Max | 0. | 0. | -484.2813 |
| 20 | 0.5719 | SLD_1 | Max | 0. | 0. | -541.7171 |
| 20 | 0. | SLD_1 | Min | 0. | 0. | -438.277 |
| 20 | 0.28595 | SLD_1 | Min | 0. | 0. | -484.2813 |
| 20 | 0.5719 | SLD_1 | Min | 0. | 0. | -541.7171 |
| 20 | 0. | SLD_2 | Max | 0. | 0. | -436.503 |
| 20 | 0.28595 | SLD_2 | Max | 0. | 0. | -482.0567 |
| 20 | 0.5719 | SLD_2 | Max | 0. | 0. | -539.042 |
| 20 | 0. | SLD_2 | Min | 0. | 0. | -436.503 |
| 20 | 0.28595 | SLD_2 | Min | 0. | 0. | -482.0567 |
| 20 | 0.5719 | SLD_2 | Min | 0. | 0. | -539.042 |
| 20 | 0. | SLD_3 | Max | 0. | 0. | -153.8062 |
| 20 | 0.28595 | SLD_3 | Max | 0. | 0. | -238.1561 |
| 20 | 0.5719 | SLD_3 | Max | 0. | 0. | -333.2425 |
| 20 | 0. | SLD_3 | Min | 0. | 0. | -153.8062 |
| 20 | 0.28595 | SLD_3 | Min | 0. | 0. | -238.1561 |
| 20 | 0.5719 | SLD_3 | Min | 0. | 0. | -333.2425 |
| 20 | 0. | SLD_4 | Max | 0. | 0. | -151.5908 |
| 20 | 0.28595 | SLD_4 | Max | 0. | 0. | -235.553 |
| 20 | 0.5719 | SLD_4 | Max | 0. | 0. | -330.2516 |
| 20 | 0. | SLD_4 | Min | 0. | 0. | -151.5908 |
| 20 | 0.28595 | SLD_4 | Min | 0. | 0. | -235.553 |
| 20 | 0.5719 | SLD_4 | Min | 0. | 0. | -330.2516 |
| 20 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1008.5359 |
| 20 | 0.28595 | SLU_IDR_1 | Max | 0. | 0. | -1047.2003 |
| 20 | 0.5719 | SLU_IDR_1 | Max | 0. | 0. | -1095.257 |
| 20 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1008.5359 |
| 20 | 0.28595 | SLU_IDR_1 | Min | 0. | 0. | -1047.2003 |
| 20 | 0.5719 | SLU_IDR_1 | Min | 0. | 0. | -1095.257 |
| 20 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1137.0413 |
| 20 | 0.28595 | SLU_IDR_2 | Max | 0. | 0. | -1146.7043 |
| 20 | 0.5719 | SLU_IDR_2 | Max | 0. | 0. | -1166.4758 |
| 20 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1137.0413 |
| 20 | 0.28595 | SLU_IDR_2 | Min | 0. | 0. | -1146.7043 |
| 20 | 0.5719 | SLU_IDR_2 | Min | 0. | 0. | -1166.4758 |
| 20 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 1162.8956 |
| 20 | 0.28595 | SISMA WOOD SLV-1 | Max | 0. | 0. | 1093.4155 |
| 20 | 0.5719 | SISMA WOOD SLV-1 | Max | 0. | 0. | 1023.9355 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 20 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 1162.8956 |
| 20 | 0.28595 | SISMA WOOD SLV-1 | Min | 0. | 0. | 1093.4155 |
| 20 | 0.5719 | SISMA WOOD SLV-1 | Min | 0. | 0. | 1023.9355 |
| 20 | 0. | DEAD-1 | Max | 0. | 0. | -195.5906 |
| 20 | 0.28595 | DEAD-1 | Max | 0. | 0. | -221.1193 |
| 20 | 0.5719 | DEAD-1 | Max | 0. | 0. | -246.648 |
| 20 | 0. | DEAD-1 | Min | 0. | 0. | -195.5906 |
| 20 | 0.28595 | DEAD-1 | Min | 0. | 0. | -221.1193 |
| 20 | 0.5719 | DEAD-1 | Min | 0. | 0. | -246.648 |
| 20 | 0. | SLU_PROVA | | 0. | 0. | -1300.2989 |
| 20 | 0.28595 | SLU_PROVA | | 0. | 0. | -1321.1287 |
| 20 | 0.5719 | SLU_PROVA | | 0. | 0. | -1356.8194 |
| 21 | 0. | DEAD | | 0. | 0. | -177.5796 |
| 21 | 0.81908 | DEAD | | 0. | 0. | -152.7005 |
| 21 | 1.63815 | DEAD | | 0. | 0. | -138.2968 |
| 21 | 0. | SIMM_KA | | 0. | 0. | 210.3283 |
| 21 | 0.81908 | SIMM_KA | | 0. | 0. | 236.7276 |
| 21 | 1.63815 | SIMM_KA | | 0. | 0. | 240.6695 |
| 21 | 0. | SIMM_K0 | | 0. | 0. | 317.0165 |
| 21 | 0.81908 | SIMM_K0 | | 0. | 0. | 358.8136 |
| 21 | 1.63815 | SIMM_K0 | | 0. | 0. | 366.9246 |
| 21 | 0. | A--SIMM_KA | | 0. | 0. | 261.1737 |
| 21 | 0.81908 | A--SIMM_KA | | 0. | 0. | 267.8023 |
| 21 | 1.63815 | A--SIMM_KA | | 0. | 0. | 255.8374 |
| 21 | 0. | A--SIMM_K0 | | 0. | 0. | 404.6002 |
| 21 | 0.81908 | A--SIMM_K0 | | 0. | 0. | 411.9006 |
| 21 | 1.63815 | A--SIMM_K0 | | 0. | 0. | 391.3091 |
| 21 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 19.0261 |
| 21 | 0.81908 | A-- SIMM_SOVR_K A | | 0. | 0. | 28.9713 |
| 21 | 1.63815 | A-- SIMM_SOVR_K A | | 0. | 0. | 34.8482 |
| 21 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 28.5249 |
| 21 | 0.81908 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 43.4352 |
| 21 | 1.63815 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 52.2462 |
| 21 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 28.5249 |
| 21 | 0.81908 | SIMM_SOVR_K 0 | | 0. | 0. | 43.4352 |
| 21 | 1.63815 | SIMM_SOVR_K 0 | | 0. | 0. | 52.2462 |
| 21 | 0. | SIMM_SOVR_K A | | 0. | 0. | 19.0261 |
| 21 | 0.81908 | SIMM_SOVR_K A | | 0. | 0. | 28.9713 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 21 | 1.63815 | SIMM_SOVR_K A | | 0. | 0. | 34.8482 |
| 21 | 0. | SOVR | | 0. | 0. | -194.4061 |
| 21 | 0.81908 | SOVR | | 0. | 0. | -169.4251 |
| 21 | 1.63815 | SOVR | | 0. | 0. | -150.0326 |
| 21 | 0. | TERR_SIMM | | 0. | 0. | -722.3571 |
| 21 | 0.81908 | TERR_SIMM | | 0. | 0. | -595.8827 |
| 21 | 1.63815 | TERR_SIMM | | 0. | 0. | -500.2725 |
| 21 | 0. | TERR_A--SIMM | | 0. | 0. | -756.3843 |
| 21 | 0.81908 | TERR_A--SIMM | | 0. | 0. | -661.7266 |
| 21 | 1.63815 | TERR_A--SIMM | | 0. | 0. | -592.6241 |
| 21 | 0. | INERZIA H SLV | | 0. | 0. | 5.3752 |
| 21 | 0.81908 | INERZIA H SLV | | 0. | 0. | 2.9233 |
| 21 | 1.63815 | INERZIA H SLV | | 0. | 0. | 0.4714 |
| 21 | 0. | INERZIA V + SLV | | 0. | 0. | -2.8526 |
| 21 | 0.81908 | INERZIA V + SLV | | 0. | 0. | -2.5203 |
| 21 | 1.63815 | INERZIA V + SLV | | 0. | 0. | -2.1879 |
| 21 | 0. | INERZIA V - SLV | | 0. | 0. | 2.8526 |
| 21 | 0.81908 | INERZIA V - SLV | | 0. | 0. | 2.5203 |
| 21 | 1.63815 | INERZIA V - SLV | | 0. | 0. | 2.1879 |
| 21 | 0. | SISMA WOOD SLV | | 0. | 0. | 428.1316 |
| 21 | 0.81908 | SISMA WOOD SLV | | 0. | 0. | 348.8768 |
| 21 | 1.63815 | SISMA WOOD SLV | | 0. | 0. | 269.622 |
| 21 | 0. | iDROSTATICA | | 0. | 0. | -269.3857 |
| 21 | 0.81908 | iDROSTATICA | | 0. | 0. | -113.0223 |
| 21 | 1.63815 | iDROSTATICA | | 0. | 0. | -5.3383 |
| 21 | 0. | SISMA WOOD SLD | | 0. | 0. | 189.0802 |
| 21 | 0.81908 | SISMA WOOD SLD | | 0. | 0. | 154.0781 |
| 21 | 1.63815 | SISMA WOOD SLD | | 0. | 0. | 119.0759 |
| 21 | 0. | INERZIA H SLD | | 0. | 0. | 2.3739 |
| 21 | 0.81908 | INERZIA H SLD | | 0. | 0. | 1.2911 |
| 21 | 1.63815 | INERZIA H SLD | | 0. | 0. | 0.2082 |
| 21 | 0. | INERZIA V + SLD | | 0. | 0. | -1.2598 |
| 21 | 0.81908 | INERZIA V + SLD | | 0. | 0. | -1.113 |
| 21 | 1.63815 | INERZIA V + SLD | | 0. | 0. | -0.9663 |
| 21 | 0. | INERZIA V SLD | | 0. | 0. | 1.2598 |
| 21 | 0.81908 | INERZIA V SLD | | 0. | 0. | 1.113 |
| 21 | 1.63815 | INERZIA V SLD | | 0. | 0. | 0.9663 |
| 21 | 0. | INERZIA V -1 | | 0. | 0. | 2.8526 |
| 21 | 0.81908 | INERZIA V -1 | | 0. | 0. | 2.5203 |
| 21 | 1.63815 | INERZIA V -1 | | 0. | 0. | 2.1879 |
| 21 | 0. | SLU_1 | Max | 0. | 0. | -1628.8289 |
| 21 | 0.81908 | SLU_1 | Max | 0. | 0. | -1088.1818 |
| 21 | 1.63815 | SLU_1 | Max | 0. | 0. | -725.8834 |
| 21 | 0. | SLU_1 | Min | 0. | 0. | -1628.8289 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 21 | 0.81908 | SLU_1 | Min | 0. | 0. | -1088.1818 |
| 21 | 1.63815 | SLU_1 | Min | 0. | 0. | -725.8834 |
| 21 | 0. | SLU_2 | Max | 0. | 0. | -1824.2385 |
| 21 | 0.81908 | SLU_2 | Max | 0. | 0. | -1312.465 |
| 21 | 1.63815 | SLU_2 | Max | 0. | 0. | -961.3963 |
| 21 | 0. | SLU_2 | Min | 0. | 0. | -1824.2385 |
| 21 | 0.81908 | SLU_2 | Min | 0. | 0. | -1312.465 |
| 21 | 1.63815 | SLU_2 | Min | 0. | 0. | -961.3963 |
| 21 | 0. | SLU_3 | Max | 0. | 0. | -1448.4167 |
| 21 | 0.81908 | SLU_3 | Max | 0. | 0. | -1046.7144 |
| 21 | 1.63815 | SLU_3 | Max | 0. | 0. | -808.9264 |
| 21 | 0. | SLU_3 | Min | 0. | 0. | -1448.4167 |
| 21 | 0.81908 | SLU_3 | Min | 0. | 0. | -1046.7144 |
| 21 | 1.63815 | SLU_3 | Min | 0. | 0. | -808.9264 |
| 21 | 0. | SLU_4 | Max | 0. | 0. | -1729.0125 |
| 21 | 0.81908 | SLU_4 | Max | 0. | 0. | -1323.8383 |
| 21 | 1.63815 | SLU_4 | Max | 0. | 0. | -1067.444 |
| 21 | 0. | SLU_4 | Min | 0. | 0. | -1729.0125 |
| 21 | 0.81908 | SLU_4 | Min | 0. | 0. | -1323.8383 |
| 21 | 1.63815 | SLU_4 | Min | 0. | 0. | -1067.444 |
| 21 | 0. | SLE_F1 | Max | 0. | 0. | -1177.2701 |
| 21 | 0.81908 | SLE_F1 | Max | 0. | 0. | -777.3711 |
| 21 | 1.63815 | SLE_F1 | Max | 0. | 0. | -509.9433 |
| 21 | 0. | SLE_F1 | Min | 0. | 0. | -1177.2701 |
| 21 | 0.81908 | SLE_F1 | Min | 0. | 0. | -777.3711 |
| 21 | 1.63815 | SLE_F1 | Min | 0. | 0. | -509.9433 |
| 21 | 0. | SLE_F2 | Max | 0. | 0. | -1324.3884 |
| 21 | 0.81908 | SLE_F2 | Max | 0. | 0. | -944.3434 |
| 21 | 1.63815 | SLE_F2 | Max | 0. | 0. | -684.0176 |
| 21 | 0. | SLE_F2 | Min | 0. | 0. | -1324.3884 |
| 21 | 0.81908 | SLE_F2 | Min | 0. | 0. | -944.3434 |
| 21 | 1.63815 | SLE_F2 | Min | 0. | 0. | -684.0176 |
| 21 | 0. | SLE_F3 | Max | 0. | 0. | -1250.5526 |
| 21 | 0.81908 | SLE_F3 | Max | 0. | 0. | -952.2311 |
| 21 | 1.63815 | SLE_F3 | Max | 0. | 0. | -764.4558 |
| 21 | 0. | SLE_F3 | Min | 0. | 0. | -1250.5526 |
| 21 | 0.81908 | SLE_F3 | Min | 0. | 0. | -952.2311 |
| 21 | 1.63815 | SLE_F3 | Min | 0. | 0. | -764.4558 |
| 21 | 0. | SLE_F4 | Max | 0. | 0. | -1029.3835 |
| 21 | 0.81908 | SLE_F4 | Max | 0. | 0. | -736.7578 |
| 21 | 1.63815 | SLE_F4 | Max | 0. | 0. | -565.5001 |
| 21 | 0. | SLE_F4 | Min | 0. | 0. | -1029.3835 |
| 21 | 0.81908 | SLE_F4 | Min | 0. | 0. | -736.7578 |
| 21 | 1.63815 | SLE_F4 | Min | 0. | 0. | -565.5001 |
| 21 | 0. | SLE_QP1 | Max | 0. | 0. | -1040.6764 |
| 21 | 0.81908 | SLE_QP1 | Max | 0. | 0. | -669.9706 |
| 21 | 1.63815 | SLE_QP1 | Max | 0. | 0. | -422.9703 |
| 21 | 0. | SLE_QP1 | Min | 0. | 0. | -1040.6764 |
| 21 | 0.81908 | SLE_QP1 | Min | 0. | 0. | -669.9706 |
| 21 | 1.63815 | SLE_QP1 | Min | 0. | 0. | -422.9703 |
| 21 | 0. | SLE_QP2 | Max | 0. | 0. | -1177.9 |
| 21 | 0.81908 | SLE_QP2 | Max | 0. | 0. | -823.1635 |
| 21 | 1.63815 | SLE_QP2 | Max | 0. | 0. | -580.9038 |
| 21 | 0. | SLE_QP2 | Min | 0. | 0. | -1177.9 |
| 21 | 0.81908 | SLE_QP2 | Min | 0. | 0. | -823.1635 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 21 | 1.63815 | SLE_QP2 | Min | 0. | 0. | -580.9038 |
| 21 | 0. | SLE_QP3 | Max | 0. | 0. | -1102.9901 |
| 21 | 0.81908 | SLE_QP3 | Max | 0. | 0. | -829.4623 |
| 21 | 1.63815 | SLE_QP3 | Max | 0. | 0. | -659.2382 |
| 21 | 0. | SLE_QP3 | Min | 0. | 0. | -1102.9901 |
| 21 | 0.81908 | SLE_QP3 | Min | 0. | 0. | -829.4623 |
| 21 | 1.63815 | SLE_QP3 | Min | 0. | 0. | -659.2382 |
| 21 | 0. | SLE_QP4 | Max | 0. | 0. | -871.456 |
| 21 | 0.81908 | SLE_QP4 | Max | 0. | 0. | -609.0651 |
| 21 | 1.63815 | SLE_QP4 | Max | 0. | 0. | -459.2763 |
| 21 | 0. | SLE_QP4 | Min | 0. | 0. | -871.456 |
| 21 | 0.81908 | SLE_QP4 | Min | 0. | 0. | -609.0651 |
| 21 | 1.63815 | SLE_QP4 | Min | 0. | 0. | -459.2763 |
| 21 | 0. | SLV_1 | Max | 0. | 0. | 65.7858 |
| 21 | 0.81908 | SLV_1 | Max | 0. | 0. | 257.7147 |
| 21 | 1.63815 | SLV_1 | Max | 0. | 0. | 325.9383 |
| 21 | 0. | SLV_1 | Min | 0. | 0. | 65.7858 |
| 21 | 0.81908 | SLV_1 | Min | 0. | 0. | 257.7147 |
| 21 | 1.63815 | SLV_1 | Min | 0. | 0. | 325.9383 |
| 21 | 0. | SLV_2 | Max | 0. | 0. | 72.0502 |
| 21 | 0.81908 | SLV_2 | Max | 0. | 0. | 263.6051 |
| 21 | 1.63815 | SLV_2 | Max | 0. | 0. | 331.4546 |
| 21 | 0. | SLV_2 | Min | 0. | 0. | 72.0502 |
| 21 | 0.81908 | SLV_2 | Min | 0. | 0. | 263.6051 |
| 21 | 1.63815 | SLV_2 | Min | 0. | 0. | 331.4546 |
| 21 | 0. | SLV_3 | Max | 0. | 0. | 245.8648 |
| 21 | 0.81908 | SLV_3 | Max | 0. | 0. | 348.3954 |
| 21 | 1.63815 | SLV_3 | Max | 0. | 0. | 338.324 |
| 21 | 0. | SLV_3 | Min | 0. | 0. | 245.8648 |
| 21 | 0.81908 | SLV_3 | Min | 0. | 0. | 348.3954 |
| 21 | 1.63815 | SLV_3 | Min | 0. | 0. | 338.324 |
| 21 | 0. | SLV_4 | Max | 0. | 0. | 252.655 |
| 21 | 0.81908 | SLV_4 | Max | 0. | 0. | 354.7497 |
| 21 | 1.63815 | SLV_4 | Max | 0. | 0. | 344.2424 |
| 21 | 0. | SLV_4 | Min | 0. | 0. | 252.655 |
| 21 | 0.81908 | SLV_4 | Min | 0. | 0. | 354.7497 |
| 21 | 1.63815 | SLV_4 | Min | 0. | 0. | 344.2424 |
| 21 | 0. | SLD_1 | Max | 0. | 0. | -541.7171 |
| 21 | 0.81908 | SLD_1 | Max | 0. | 0. | -263.3897 |
| 21 | 1.63815 | SLD_1 | Max | 0. | 0. | -108.7678 |
| 21 | 0. | SLD_1 | Min | 0. | 0. | -541.7171 |
| 21 | 0.81908 | SLD_1 | Min | 0. | 0. | -263.3897 |
| 21 | 1.63815 | SLD_1 | Min | 0. | 0. | -108.7678 |
| 21 | 0. | SLD_2 | Max | 0. | 0. | -539.042 |
| 21 | 0.81908 | SLD_2 | Max | 0. | 0. | -260.8068 |
| 21 | 1.63815 | SLD_2 | Max | 0. | 0. | -106.277 |
| 21 | 0. | SLD_2 | Min | 0. | 0. | -539.042 |
| 21 | 0.81908 | SLD_2 | Min | 0. | 0. | -260.8068 |
| 21 | 1.63815 | SLD_2 | Min | 0. | 0. | -106.277 |
| 21 | 0. | SLD_3 | Max | 0. | 0. | -333.2425 |
| 21 | 0.81908 | SLD_3 | Max | 0. | 0. | -147.903 |
| 21 | 1.63815 | SLD_3 | Max | 0. | 0. | -75.1656 |
| 21 | 0. | SLD_3 | Min | 0. | 0. | -333.2425 |
| 21 | 0.81908 | SLD_3 | Min | 0. | 0. | -147.903 |
| 21 | 1.63815 | SLD_3 | Min | 0. | 0. | -75.1656 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 21 | 0. | SLD_4 | Max | 0. | 0. | -330.2516 |
| 21 | 0.81908 | SLD_4 | Max | 0. | 0. | -145.0943 |
| 21 | 1.63815 | SLD_4 | Max | 0. | 0. | -72.539 |
| 21 | 0. | SLD_4 | Min | 0. | 0. | -330.2516 |
| 21 | 0.81908 | SLD_4 | Min | 0. | 0. | -145.0943 |
| 21 | 1.63815 | SLD_4 | Min | 0. | 0. | -72.539 |
| 21 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1095.257 |
| 21 | 0.81908 | SLU_IDR_1 | Max | 0. | 0. | -807.8824 |
| 21 | 1.63815 | SLU_IDR_1 | Max | 0. | 0. | -623.217 |
| 21 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1095.257 |
| 21 | 0.81908 | SLU_IDR_1 | Min | 0. | 0. | -807.8824 |
| 21 | 1.63815 | SLU_IDR_1 | Min | 0. | 0. | -623.217 |
| 21 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1166.4758 |
| 21 | 0.81908 | SLU_IDR_2 | Max | 0. | 0. | -807.0593 |
| 21 | 1.63815 | SLU_IDR_2 | Max | 0. | 0. | -558.6076 |
| 21 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1166.4758 |
| 21 | 0.81908 | SLU_IDR_2 | Min | 0. | 0. | -807.0593 |
| 21 | 1.63815 | SLU_IDR_2 | Min | 0. | 0. | -558.6076 |
| 21 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 1023.9355 |
| 21 | 0.81908 | SISMA WOOD SLV-1 | Max | 0. | 0. | 879.9036 |
| 21 | 1.63815 | SISMA WOOD SLV-1 | Max | 0. | 0. | 735.8716 |
| 21 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 1023.9355 |
| 21 | 0.81908 | SISMA WOOD SLV-1 | Min | 0. | 0. | 879.9036 |
| 21 | 1.63815 | SISMA WOOD SLV-1 | Min | 0. | 0. | 735.8716 |
| 21 | 0. | DEAD-1 | Max | 0. | 0. | -246.648 |
| 21 | 0.81908 | DEAD-1 | Max | 0. | 0. | -216.8819 |
| 21 | 1.63815 | DEAD-1 | Max | 0. | 0. | -197.5913 |
| 21 | 0. | DEAD-1 | Min | 0. | 0. | -246.648 |
| 21 | 0.81908 | DEAD-1 | Min | 0. | 0. | -216.8819 |
| 21 | 1.63815 | DEAD-1 | Min | 0. | 0. | -197.5913 |
| 21 | 0. | SLU_PROVA | | 0. | 0. | -1356.8194 |
| 21 | 0.81908 | SLU_PROVA | | 0. | 0. | -842.6141 |
| 21 | 1.63815 | SLU_PROVA | | 0. | 0. | -506.7575 |
| 22 | 0. | DEAD | | 0. | 0. | -138.2968 |
| 22 | 0.63397 | DEAD | | 0. | 0. | -120.3517 |
| 22 | 1.26794 | DEAD | | 0. | 0. | -108.4214 |
| 22 | 0. | SIMM_KA | | 0. | 0. | 240.6695 |
| 22 | 0.63397 | SIMM_KA | | 0. | 0. | 233.226 |
| 22 | 1.26794 | SIMM_KA | | 0. | 0. | 214.4243 |
| 22 | 0. | SIMM_K0 | | 0. | 0. | 366.9246 |
| 22 | 0.63397 | SIMM_K0 | | 0. | 0. | 357.452 |
| 22 | 1.26794 | SIMM_K0 | | 0. | 0. | 330.519 |
| 22 | 0. | A--SIMM_KA | | 0. | 0. | 255.8374 |
| 22 | 0.63397 | A--SIMM_KA | | 0. | 0. | 237.6038 |
| 22 | 1.26794 | A--SIMM_KA | | 0. | 0. | 210.1506 |
| 22 | 0. | A--SIMM_K0 | | 0. | 0. | 391.3091 |
| 22 | 0.63397 | A--SIMM_K0 | | 0. | 0. | 362.2624 |
| 22 | 1.26794 | A--SIMM_K0 | | 0. | 0. | 319.3864 |

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 22 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 34.8482 |
| 22 | 0.63397 | A-- SIMM_SOVR_K A | | 0. | 0. | 37.0915 |
| 22 | 1.26794 | A-- SIMM_SOVR_K A | | 0. | 0. | 37.0117 |
| 22 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 52.2462 |
| 22 | 0.63397 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 55.6095 |
| 22 | 1.26794 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 55.4897 |
| 22 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 52.2462 |
| 22 | 0.63397 | SIMM_SOVR_K 0 | | 0. | 0. | 55.6095 |
| 22 | 1.26794 | SIMM_SOVR_K 0 | | 0. | 0. | 55.4897 |
| 22 | 0. | SIMM_SOVR_K A | | 0. | 0. | 34.8482 |
| 22 | 0.63397 | SIMM_SOVR_K A | | 0. | 0. | 37.0915 |
| 22 | 1.26794 | SIMM_SOVR_K A | | 0. | 0. | 37.0117 |
| 22 | 0. | SOVR | | 0. | 0. | -150.0326 |
| 22 | 0.63397 | SOVR | | 0. | 0. | -129.4694 |
| 22 | 1.26794 | SOVR | | 0. | 0. | -112.9173 |
| 22 | 0. | TERR_SIMM | | 0. | 0. | -500.2725 |
| 22 | 0.63397 | TERR_SIMM | | 0. | 0. | -411.8254 |
| 22 | 1.26794 | TERR_SIMM | | 0. | 0. | -343.4861 |
| 22 | 0. | TERR_A--SIMM | | 0. | 0. | -592.6241 |
| 22 | 0.63397 | TERR_A--SIMM | | 0. | 0. | -520.3694 |
| 22 | 1.26794 | TERR_A--SIMM | | 0. | 0. | -464.0419 |
| 22 | 0. | INERZIA H SLV | | 0. | 0. | 0.4714 |
| 22 | 0.63397 | INERZIA H SLV | | 0. | 0. | -0.7767 |
| 22 | 1.26794 | INERZIA H SLV | | 0. | 0. | -2.0248 |
| 22 | 0. | INERZIA V + SLV | | 0. | 0. | -2.1879 |
| 22 | 0.63397 | INERZIA V + SLV | | 0. | 0. | -1.9355 |
| 22 | 1.26794 | INERZIA V + SLV | | 0. | 0. | -1.6831 |
| 22 | 0. | INERZIA V - SLV | | 0. | 0. | 2.1879 |
| 22 | 0.63397 | INERZIA V - SLV | | 0. | 0. | 1.9355 |
| 22 | 1.26794 | INERZIA V - SLV | | 0. | 0. | 1.6831 |
| 22 | 0. | SISMA WOOD SLV | | 0. | 0. | 269.622 |
| 22 | 0.63397 | SISMA WOOD SLV | | 0. | 0. | 204.4084 |
| 22 | 1.26794 | SISMA WOOD SLV | | 0. | 0. | 139.1949 |
| 22 | 0. | iDROSTATICA | | 0. | 0. | -5.3383 |
| 22 | 0.63397 | iDROSTATICA | | 0. | 0. | 57.749 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 22 | 1.26794 | iDROSTATICA | | 0. | 0. | 89.7018 |
| 22 | 0. | SISMA WOOD SLD | | 0. | 0. | 119.0759 |
| 22 | 0.63397 | SISMA WOOD SLD | | 0. | 0. | 90.275 |
| 22 | 1.26794 | SISMA WOOD SLD | | 0. | 0. | 61.4741 |
| 22 | 0. | INERZIA H SLD | | 0. | 0. | 0.2082 |
| 22 | 0.63397 | INERZIA H SLD | | 0. | 0. | -0.343 |
| 22 | 1.26794 | INERZIA H SLD | | 0. | 0. | -0.8943 |
| 22 | 0. | INERZIA V + SLD | | 0. | 0. | -0.9663 |
| 22 | 0.63397 | INERZIA V + SLD | | 0. | 0. | -0.8548 |
| 22 | 1.26794 | INERZIA V + SLD | | 0. | 0. | -0.7433 |
| 22 | 0. | INERZIA V SLD | | 0. | 0. | 0.9663 |
| 22 | 0.63397 | INERZIA V SLD | | 0. | 0. | 0.8548 |
| 22 | 1.26794 | INERZIA V SLD | | 0. | 0. | 0.7433 |
| 22 | 0. | INERZIA V -1 | | 0. | 0. | 2.1879 |
| 22 | 0.63397 | INERZIA V -1 | | 0. | 0. | 1.9355 |
| 22 | 1.26794 | INERZIA V -1 | | 0. | 0. | 1.6831 |
| 22 | 0. | SLU_1 | Max | 0. | 0. | -725.8834 |
| 22 | 0.63397 | SLU_1 | Max | 0. | 0. | -455.76 |
| 22 | 1.26794 | SLU_1 | Max | 0. | 0. | -294.0108 |
| 22 | 0. | SLU_1 | Min | 0. | 0. | -725.8834 |
| 22 | 0.63397 | SLU_1 | Min | 0. | 0. | -455.76 |
| 22 | 1.26794 | SLU_1 | Min | 0. | 0. | -294.0108 |
| 22 | 0. | SLU_2 | Max | 0. | 0. | -961.3963 |
| 22 | 0.63397 | SLU_2 | Max | 0. | 0. | -688.3652 |
| 22 | 1.26794 | SLU_2 | Max | 0. | 0. | -514.0356 |
| 22 | 0. | SLU_2 | Min | 0. | 0. | -961.3963 |
| 22 | 0.63397 | SLU_2 | Min | 0. | 0. | -688.3652 |
| 22 | 1.26794 | SLU_2 | Min | 0. | 0. | -514.0356 |
| 22 | 0. | SLU_3 | Max | 0. | 0. | -808.9264 |
| 22 | 0.63397 | SLU_3 | Max | 0. | 0. | -622.2523 |
| 22 | 1.26794 | SLU_3 | Max | 0. | 0. | -533.7972 |
| 22 | 0. | SLU_3 | Min | 0. | 0. | -808.9264 |
| 22 | 0.63397 | SLU_3 | Min | 0. | 0. | -622.2523 |
| 22 | 1.26794 | SLU_3 | Min | 0. | 0. | -533.7972 |
| 22 | 0. | SLU_4 | Max | 0. | 0. | -1067.444 |
| 22 | 0.63397 | SLU_4 | Max | 0. | 0. | -857.801 |
| 22 | 1.26794 | SLU_4 | Max | 0. | 0. | -738.6444 |
| 22 | 0. | SLU_4 | Min | 0. | 0. | -1067.444 |
| 22 | 0.63397 | SLU_4 | Min | 0. | 0. | -857.801 |
| 22 | 1.26794 | SLU_4 | Min | 0. | 0. | -738.6444 |
| 22 | 0. | SLE_F1 | Max | 0. | 0. | -509.9433 |
| 22 | 0.63397 | SLE_F1 | Max | 0. | 0. | -312.2515 |
| 22 | 1.26794 | SLE_F1 | Max | 0. | 0. | -194.8979 |
| 22 | 0. | SLE_F1 | Min | 0. | 0. | -509.9433 |
| 22 | 0.63397 | SLE_F1 | Min | 0. | 0. | -312.2515 |
| 22 | 1.26794 | SLE_F1 | Min | 0. | 0. | -194.8979 |
| 22 | 0. | SLE_F2 | Max | 0. | 0. | -684.0176 |
| 22 | 0.63397 | SLE_F2 | Max | 0. | 0. | -483.4876 |
| 22 | 1.26794 | SLE_F2 | Max | 0. | 0. | -356.3238 |
| 22 | 0. | SLE_F2 | Min | 0. | 0. | -684.0176 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 22 | 0.63397 | SLE_F2 | Min | 0. | 0. | -483.4876 |
| 22 | 1.26794 | SLE_F2 | Min | 0. | 0. | -356.3238 |
| 22 | 0. | SLE_F3 | Max | 0. | 0. | -764.4558 |
| 22 | 0.63397 | SLE_F3 | Max | 0. | 0. | -612.5472 |
| 22 | 1.26794 | SLE_F3 | Max | 0. | 0. | -527.6856 |
| 22 | 0. | SLE_F3 | Min | 0. | 0. | -764.4558 |
| 22 | 0.63397 | SLE_F3 | Min | 0. | 0. | -612.5472 |
| 22 | 1.26794 | SLE_F3 | Min | 0. | 0. | -527.6856 |
| 22 | 0. | SLE_F4 | Max | 0. | 0. | -565.5001 |
| 22 | 0.63397 | SLE_F4 | Max | 0. | 0. | -432.5949 |
| 22 | 1.26794 | SLE_F4 | Max | 0. | 0. | -372.2163 |
| 22 | 0. | SLE_F4 | Min | 0. | 0. | -565.5001 |
| 22 | 0.63397 | SLE_F4 | Min | 0. | 0. | -432.5949 |
| 22 | 1.26794 | SLE_F4 | Min | 0. | 0. | -372.2163 |
| 22 | 0. | SLE_QP1 | Max | 0. | 0. | -422.9703 |
| 22 | 0.63397 | SLE_QP1 | Max | 0. | 0. | -243.6584 |
| 22 | 1.26794 | SLE_QP1 | Max | 0. | 0. | -139.0642 |
| 22 | 0. | SLE_QP1 | Min | 0. | 0. | -422.9703 |
| 22 | 0.63397 | SLE_QP1 | Min | 0. | 0. | -243.6584 |
| 22 | 1.26794 | SLE_QP1 | Min | 0. | 0. | -139.0642 |
| 22 | 0. | SLE_QP2 | Max | 0. | 0. | -580.9038 |
| 22 | 0.63397 | SLE_QP2 | Max | 0. | 0. | -398.0065 |
| 22 | 1.26794 | SLE_QP2 | Max | 0. | 0. | -283.7246 |
| 22 | 0. | SLE_QP2 | Min | 0. | 0. | -580.9038 |
| 22 | 0.63397 | SLE_QP2 | Min | 0. | 0. | -398.0065 |
| 22 | 1.26794 | SLE_QP2 | Min | 0. | 0. | -283.7246 |
| 22 | 0. | SLE_QP3 | Max | 0. | 0. | -659.2382 |
| 22 | 0.63397 | SLE_QP3 | Max | 0. | 0. | -524.7029 |
| 22 | 1.26794 | SLE_QP3 | Max | 0. | 0. | -452.4638 |
| 22 | 0. | SLE_QP3 | Min | 0. | 0. | -659.2382 |
| 22 | 0.63397 | SLE_QP3 | Min | 0. | 0. | -524.7029 |
| 22 | 1.26794 | SLE_QP3 | Min | 0. | 0. | -452.4638 |
| 22 | 0. | SLE_QP4 | Max | 0. | 0. | -459.2763 |
| 22 | 0.63397 | SLE_QP4 | Max | 0. | 0. | -346.0837 |
| 22 | 1.26794 | SLE_QP4 | Max | 0. | 0. | -299.7972 |
| 22 | 0. | SLE_QP4 | Min | 0. | 0. | -459.2763 |
| 22 | 0.63397 | SLE_QP4 | Min | 0. | 0. | -346.0837 |
| 22 | 1.26794 | SLE_QP4 | Min | 0. | 0. | -299.7972 |
| 22 | 0. | SLV_1 | Max | 0. | 0. | 325.9383 |
| 22 | 0.63397 | SLV_1 | Max | 0. | 0. | 354.8566 |
| 22 | 1.26794 | SLV_1 | Max | 0. | 0. | 309.0573 |
| 22 | 0. | SLV_1 | Min | 0. | 0. | 325.9383 |
| 22 | 0.63397 | SLV_1 | Min | 0. | 0. | 354.8566 |
| 22 | 1.26794 | SLV_1 | Min | 0. | 0. | 309.0573 |
| 22 | 0. | SLV_2 | Max | 0. | 0. | 331.4546 |
| 22 | 0.63397 | SLV_2 | Max | 0. | 0. | 360.0385 |
| 22 | 1.26794 | SLV_2 | Max | 0. | 0. | 313.9047 |
| 22 | 0. | SLV_2 | Min | 0. | 0. | 331.4546 |
| 22 | 0.63397 | SLV_2 | Min | 0. | 0. | 360.0385 |
| 22 | 1.26794 | SLV_2 | Min | 0. | 0. | 313.9047 |
| 22 | 0. | SLV_3 | Max | 0. | 0. | 338.324 |
| 22 | 0.63397 | SLV_3 | Max | 0. | 0. | 312.4515 |
| 22 | 1.26794 | SLV_3 | Max | 0. | 0. | 219.673 |
| 22 | 0. | SLV_3 | Min | 0. | 0. | 338.324 |
| 22 | 0.63397 | SLV_3 | Min | 0. | 0. | 312.4515 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 22 | 1.26794 | SLV_3 | Min | 0. | 0. | 219.673 |
| 22 | 0. | SLV_4 | Max | 0. | 0. | 344.2424 |
| 22 | 0.63397 | SLV_4 | Max | 0. | 0. | 317.9858 |
| 22 | 1.26794 | SLV_4 | Max | 0. | 0. | 224.8231 |
| 22 | 0. | SLV_4 | Min | 0. | 0. | 344.2424 |
| 22 | 0.63397 | SLV_4 | Min | 0. | 0. | 317.9858 |
| 22 | 1.26794 | SLV_4 | Min | 0. | 0. | 224.8231 |
| 22 | 0. | SLD_1 | Max | 0. | 0. | -108.7678 |
| 22 | 0.63397 | SLD_1 | Max | 0. | 0. | -4.874 |
| 22 | 1.26794 | SLD_1 | Max | 0. | 0. | 24.3021 |
| 22 | 0. | SLD_1 | Min | 0. | 0. | -108.7678 |
| 22 | 0.63397 | SLD_1 | Min | 0. | 0. | -4.874 |
| 22 | 1.26794 | SLD_1 | Min | 0. | 0. | 24.3021 |
| 22 | 0. | SLD_2 | Max | 0. | 0. | -106.277 |
| 22 | 0.63397 | SLD_2 | Max | 0. | 0. | -2.5029 |
| 22 | 1.26794 | SLD_2 | Max | 0. | 0. | 26.5535 |
| 22 | 0. | SLD_2 | Min | 0. | 0. | -106.277 |
| 22 | 0.63397 | SLD_2 | Min | 0. | 0. | -2.5029 |
| 22 | 1.26794 | SLD_2 | Min | 0. | 0. | 26.5535 |
| 22 | 0. | SLD_3 | Max | 0. | 0. | -75.1656 |
| 22 | 0.63397 | SLD_3 | Max | 0. | 0. | -29.2564 |
| 22 | 1.26794 | SLD_3 | Max | 0. | 0. | -50.2531 |
| 22 | 0. | SLD_3 | Min | 0. | 0. | -75.1656 |
| 22 | 0.63397 | SLD_3 | Min | 0. | 0. | -29.2564 |
| 22 | 1.26794 | SLD_3 | Min | 0. | 0. | -50.2531 |
| 22 | 0. | SLD_4 | Max | 0. | 0. | -72.539 |
| 22 | 0.63397 | SLD_4 | Max | 0. | 0. | -26.7965 |
| 22 | 1.26794 | SLD_4 | Max | 0. | 0. | -47.96 |
| 22 | 0. | SLD_4 | Min | 0. | 0. | -72.539 |
| 22 | 0.63397 | SLD_4 | Min | 0. | 0. | -26.7965 |
| 22 | 1.26794 | SLD_4 | Min | 0. | 0. | -47.96 |
| 22 | 0. | SLU_IDR_1 | Max | 0. | 0. | -623.217 |
| 22 | 0.63397 | SLU_IDR_1 | Max | 0. | 0. | -483.1277 |
| 22 | 1.26794 | SLU_IDR_1 | Max | 0. | 0. | -405.332 |
| 22 | 0. | SLU_IDR_1 | Min | 0. | 0. | -623.217 |
| 22 | 0.63397 | SLU_IDR_1 | Min | 0. | 0. | -483.1277 |
| 22 | 1.26794 | SLU_IDR_1 | Min | 0. | 0. | -405.332 |
| 22 | 0. | SLU_IDR_2 | Max | 0. | 0. | -558.6076 |
| 22 | 0.63397 | SLU_IDR_2 | Max | 0. | 0. | -374.9582 |
| 22 | 1.26794 | SLU_IDR_2 | Max | 0. | 0. | -259.2895 |
| 22 | 0. | SLU_IDR_2 | Min | 0. | 0. | -558.6076 |
| 22 | 0.63397 | SLU_IDR_2 | Min | 0. | 0. | -374.9582 |
| 22 | 1.26794 | SLU_IDR_2 | Min | 0. | 0. | -259.2895 |
| 22 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 735.8716 |
| 22 | 0.63397 | SISMA WOOD SLV-1 | Max | 0. | 0. | 612.8361 |
| 22 | 1.26794 | SISMA WOOD SLV-1 | Max | 0. | 0. | 489.8005 |
| 22 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 735.8716 |
| 22 | 0.63397 | SISMA WOOD SLV-1 | Min | 0. | 0. | 612.8361 |
| 22 | 1.26794 | SISMA WOOD SLV-1 | Min | 0. | 0. | 489.8005 |
| 22 | 0. | DEAD-1 | Max | 0. | 0. | -197.5913 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 22 | 0.63397 | DEAD-1 | Max | 0. | 0. | -174.2383 |
| 22 | 1.26794 | DEAD-1 | Max | 0. | 0. | -156.9002 |
| 22 | 0. | DEAD-1 | Min | 0. | 0. | -197.5913 |
| 22 | 0.63397 | DEAD-1 | Min | 0. | 0. | -174.2383 |
| 22 | 1.26794 | DEAD-1 | Min | 0. | 0. | -156.9002 |
| 22 | 0. | SLU_PROVA | | 0. | 0. | -506.7575 |
| 22 | 0.63397 | SLU_PROVA | | 0. | 0. | -262.8587 |
| 22 | 1.26794 | SLU_PROVA | | 0. | 0. | -127.3341 |
| 23 | 0. | DEAD | | 0. | 0. | -108.4214 |
| 23 | 1.0466 | DEAD | | 0. | 0. | -73.3364 |
| 23 | 2.09321 | DEAD | | 0. | 0. | -54.9162 |
| 23 | 0. | SIMM_KA | | 0. | 0. | 214.4243 |
| 23 | 1.0466 | SIMM_KA | | 0. | 0. | 172.4567 |
| 23 | 2.09321 | SIMM_KA | | 0. | 0. | 106.5772 |
| 23 | 0. | SIMM_K0 | | 0. | 0. | 330.519 |
| 23 | 1.0466 | SIMM_K0 | | 0. | 0. | 268.2545 |
| 23 | 2.09321 | SIMM_K0 | | 0. | 0. | 168.2387 |
| 23 | 0. | A--SIMM_KA | | 0. | 0. | 210.1506 |
| 23 | 1.0466 | A--SIMM_KA | | 0. | 0. | 155.9836 |
| 23 | 2.09321 | A--SIMM_KA | | 0. | 0. | 80.5337 |
| 23 | 0. | A--SIMM_K0 | | 0. | 0. | 319.3864 |
| 23 | 1.0466 | A--SIMM_K0 | | 0. | 0. | 236.0134 |
| 23 | 2.09321 | A--SIMM_K0 | | 0. | 0. | 120.7204 |
| 23 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 37.0117 |
| 23 | 1.0466 | A-- SIMM_SOVR_K A | | 0. | 0. | 33.4493 |
| 23 | 2.09321 | A-- SIMM_SOVR_K A | | 0. | 0. | 24.0904 |
| 23 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 55.4897 |
| 23 | 1.0466 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 50.1489 |
| 23 | 2.09321 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 36.1176 |
| 23 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 55.4897 |
| 23 | 1.0466 | SIMM_SOVR_K 0 | | 0. | 0. | 50.1489 |
| 23 | 2.09321 | SIMM_SOVR_K 0 | | 0. | 0. | 36.1176 |
| 23 | 0. | SIMM_SOVR_K A | | 0. | 0. | 37.0117 |
| 23 | 1.0466 | SIMM_SOVR_K A | | 0. | 0. | 33.4493 |
| 23 | 2.09321 | SIMM_SOVR_K A | | 0. | 0. | 24.0904 |
| 23 | 0. | SOVR | | 0. | 0. | -112.9173 |
| 23 | 1.0466 | SOVR | | 0. | 0. | -74.9675 |
| 23 | 2.09321 | SOVR | | 0. | 0. | -50.3535 |
| 23 | 0. | TERR_SIMM | | 0. | 0. | -343.4861 |
| 23 | 1.0466 | TERR_SIMM | | 0. | 0. | -204.6512 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 23 | 2.09321 | TERR_SIMM | | 0. | 0. | -124.1473 |
| 23 | 0. | TERR_A--SIMM | | 0. | 0. | -464.0419 |
| 23 | 1.0466 | TERR_A--SIMM | | 0. | 0. | -330.3912 |
| 23 | 2.09321 | TERR_A--SIMM | | 0. | 0. | -245.7295 |
| 23 | 0. | INERZIA H SLV | | 0. | 0. | -2.0248 |
| 23 | 1.0466 | INERZIA H SLV | | 0. | 0. | -3.2014 |
| 23 | 2.09321 | INERZIA H SLV | | 0. | 0. | -4.3779 |
| 23 | 0. | INERZIA V + SLV | | 0. | 0. | -1.6831 |
| 23 | 1.0466 | INERZIA V + SLV | | 0. | 0. | -1.2342 |
| 23 | 2.09321 | INERZIA V + SLV | | 0. | 0. | -0.7853 |
| 23 | 0. | INERZIA V - SLV | | 0. | 0. | 1.6831 |
| 23 | 1.0466 | INERZIA V - SLV | | 0. | 0. | 1.2342 |
| 23 | 2.09321 | INERZIA V - SLV | | 0. | 0. | 0.7853 |
| 23 | 0. | SISMA WOOD SLV | | 0. | 0. | 139.1949 |
| 23 | 1.0466 | SISMA WOOD SLV | | 0. | 0. | 32.1577 |
| 23 | 2.09321 | SISMA WOOD SLV | | 0. | 0. | -74.8795 |
| 23 | 0. | iDROSTATICA | | 0. | 0. | 89.7018 |
| 23 | 1.0466 | iDROSTATICA | | 0. | 0. | 120.1029 |
| 23 | 2.09321 | iDROSTATICA | | 0. | 0. | 89.842 |
| 23 | 0. | SISMA WOOD SLD | | 0. | 0. | 61.4741 |
| 23 | 1.0466 | SISMA WOOD SLD | | 0. | 0. | 14.2021 |
| 23 | 2.09321 | SISMA WOOD SLD | | 0. | 0. | -33.0698 |
| 23 | 0. | INERZIA H SLD | | 0. | 0. | -0.8943 |
| 23 | 1.0466 | INERZIA H SLD | | 0. | 0. | -1.4139 |
| 23 | 2.09321 | INERZIA H SLD | | 0. | 0. | -1.9335 |
| 23 | 0. | INERZIA V + SLD | | 0. | 0. | -0.7433 |
| 23 | 1.0466 | INERZIA V + SLD | | 0. | 0. | -0.5451 |
| 23 | 2.09321 | INERZIA V + SLD | | 0. | 0. | -0.3468 |
| 23 | 0. | INERZIA V SLD | | 0. | 0. | 0.7433 |
| 23 | 1.0466 | INERZIA V SLD | | 0. | 0. | 0.5451 |
| 23 | 2.09321 | INERZIA V SLD | | 0. | 0. | 0.3468 |
| 23 | 0. | INERZIA V -1 | | 0. | 0. | 1.6831 |
| 23 | 1.0466 | INERZIA V -1 | | 0. | 0. | 1.2342 |
| 23 | 2.09321 | INERZIA V -1 | | 0. | 0. | 0.7853 |
| 23 | 0. | SLU_1 | Max | 0. | 0. | -294.0108 |
| 23 | 1.0466 | SLU_1 | Max | 0. | 0. | -11.9629 |
| 23 | 2.09321 | SLU_1 | Max | 0. | 0. | 11.6138 |
| 23 | 0. | SLU_1 | Min | 0. | 0. | -294.0108 |
| 23 | 1.0466 | SLU_1 | Min | 0. | 0. | -11.9629 |
| 23 | 2.09321 | SLU_1 | Min | 0. | 0. | 11.6138 |
| 23 | 0. | SLU_2 | Max | 0. | 0. | -514.0356 |
| 23 | 1.0466 | SLU_2 | Max | 0. | 0. | -193.9033 |
| 23 | 2.09321 | SLU_2 | Max | 0. | 0. | -109.9099 |
| 23 | 0. | SLU_2 | Min | 0. | 0. | -514.0356 |
| 23 | 1.0466 | SLU_2 | Min | 0. | 0. | -193.9033 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 23 | 2.09321 | SLU_2 | Min | 0. | 0. | -109.9099 |
| 23 | 0. | SLU_3 | Max | 0. | 0. | -533.7972 |
| 23 | 1.0466 | SLU_3 | Max | 0. | 0. | -326.9814 |
| 23 | 2.09321 | SLU_3 | Max | 0. | 0. | -358.9118 |
| 23 | 0. | SLU_3 | Min | 0. | 0. | -533.7972 |
| 23 | 1.0466 | SLU_3 | Min | 0. | 0. | -326.9814 |
| 23 | 2.09321 | SLU_3 | Min | 0. | 0. | -358.9118 |
| 23 | 0. | SLU_4 | Max | 0. | 0. | -738.6444 |
| 23 | 1.0466 | SLU_4 | Max | 0. | 0. | -470.2996 |
| 23 | 2.09321 | SLU_4 | Max | 0. | 0. | -422.5319 |
| 23 | 0. | SLU_4 | Min | 0. | 0. | -738.6444 |
| 23 | 1.0466 | SLU_4 | Min | 0. | 0. | -470.2996 |
| 23 | 2.09321 | SLU_4 | Min | 0. | 0. | -422.5319 |
| 23 | 0. | SLE_F1 | Max | 0. | 0. | -194.8979 |
| 23 | 1.0466 | SLE_F1 | Max | 0. | 0. | 7.348 |
| 23 | 2.09321 | SLE_F1 | Max | 0. | 0. | 19.6651 |
| 23 | 0. | SLE_F1 | Min | 0. | 0. | -194.8979 |
| 23 | 1.0466 | SLE_F1 | Min | 0. | 0. | 7.348 |
| 23 | 2.09321 | SLE_F1 | Min | 0. | 0. | 19.6651 |
| 23 | 0. | SLE_F2 | Max | 0. | 0. | -356.3238 |
| 23 | 1.0466 | SLE_F2 | Max | 0. | 0. | -125.5076 |
| 23 | 2.09321 | SLE_F2 | Max | 0. | 0. | -68.6102 |
| 23 | 0. | SLE_F2 | Min | 0. | 0. | -356.3238 |
| 23 | 1.0466 | SLE_F2 | Min | 0. | 0. | -125.5076 |
| 23 | 2.09321 | SLE_F2 | Min | 0. | 0. | -68.6102 |
| 23 | 0. | SLE_F3 | Max | 0. | 0. | -527.6856 |
| 23 | 1.0466 | SLE_F3 | Max | 0. | 0. | -337.1632 |
| 23 | 2.09321 | SLE_F3 | Max | 0. | 0. | -308.589 |
| 23 | 0. | SLE_F3 | Min | 0. | 0. | -527.6856 |
| 23 | 1.0466 | SLE_F3 | Min | 0. | 0. | -337.1632 |
| 23 | 2.09321 | SLE_F3 | Min | 0. | 0. | -308.589 |
| 23 | 0. | SLE_F4 | Max | 0. | 0. | -372.2163 |
| 23 | 1.0466 | SLE_F4 | Max | 0. | 0. | -229.8416 |
| 23 | 2.09321 | SLE_F4 | Max | 0. | 0. | -262.2227 |
| 23 | 0. | SLE_F4 | Min | 0. | 0. | -372.2163 |
| 23 | 1.0466 | SLE_F4 | Min | 0. | 0. | -229.8416 |
| 23 | 2.09321 | SLE_F4 | Min | 0. | 0. | -262.2227 |
| 23 | 0. | SLE_QP1 | Max | 0. | 0. | -139.0642 |
| 23 | 1.0466 | SLE_QP1 | Max | 0. | 0. | 36.4337 |
| 23 | 2.09321 | SLE_QP1 | Max | 0. | 0. | 38.5225 |
| 23 | 0. | SLE_QP1 | Min | 0. | 0. | -139.0642 |
| 23 | 1.0466 | SLE_QP1 | Min | 0. | 0. | 36.4337 |
| 23 | 2.09321 | SLE_QP1 | Min | 0. | 0. | 38.5225 |
| 23 | 0. | SLE_QP2 | Max | 0. | 0. | -283.7246 |
| 23 | 1.0466 | SLE_QP2 | Max | 0. | 0. | -81.5835 |
| 23 | 2.09321 | SLE_QP2 | Max | 0. | 0. | -39.0118 |
| 23 | 0. | SLE_QP2 | Min | 0. | 0. | -283.7246 |
| 23 | 1.0466 | SLE_QP2 | Min | 0. | 0. | -81.5835 |
| 23 | 2.09321 | SLE_QP2 | Min | 0. | 0. | -39.0118 |
| 23 | 0. | SLE_QP3 | Max | 0. | 0. | -452.4638 |
| 23 | 1.0466 | SLE_QP3 | Max | 0. | 0. | -291.4644 |
| 23 | 2.09321 | SLE_QP3 | Max | 0. | 0. | -278.064 |
| 23 | 0. | SLE_QP3 | Min | 0. | 0. | -452.4638 |
| 23 | 1.0466 | SLE_QP3 | Min | 0. | 0. | -291.4644 |
| 23 | 2.09321 | SLE_QP3 | Min | 0. | 0. | -278.064 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 23 | 0. | SLE_QP4 | Max | 0. | 0. | -299.7972 |
| 23 | 1.0466 | SLE_QP4 | Max | 0. | 0. | -188.2058 |
| 23 | 2.09321 | SLE_QP4 | Max | 0. | 0. | -234.8505 |
| 23 | 0. | SLE_QP4 | Min | 0. | 0. | -299.7972 |
| 23 | 1.0466 | SLE_QP4 | Min | 0. | 0. | -188.2058 |
| 23 | 2.09321 | SLE_QP4 | Min | 0. | 0. | -234.8505 |
| 23 | 0. | SLV_1 | Max | 0. | 0. | 309.0573 |
| 23 | 1.0466 | SLV_1 | Max | 0. | 0. | 233.6717 |
| 23 | 2.09321 | SLV_1 | Max | 0. | 0. | -15.123 |
| 23 | 0. | SLV_1 | Min | 0. | 0. | 309.0573 |
| 23 | 1.0466 | SLV_1 | Min | 0. | 0. | 233.6717 |
| 23 | 2.09321 | SLV_1 | Min | 0. | 0. | -15.123 |
| 23 | 0. | SLV_2 | Max | 0. | 0. | 313.9047 |
| 23 | 1.0466 | SLV_2 | Max | 0. | 0. | 237.7816 |
| 23 | 2.09321 | SLV_2 | Max | 0. | 0. | -11.7507 |
| 23 | 0. | SLV_2 | Min | 0. | 0. | 313.9047 |
| 23 | 1.0466 | SLV_2 | Min | 0. | 0. | 237.7816 |
| 23 | 2.09321 | SLV_2 | Min | 0. | 0. | -11.7507 |
| 23 | 0. | SLV_3 | Max | 0. | 0. | 219.673 |
| 23 | 1.0466 | SLV_3 | Max | 0. | 0. | 86.8396 |
| 23 | 2.09321 | SLV_3 | Max | 0. | 0. | -204.2299 |
| 23 | 0. | SLV_3 | Min | 0. | 0. | 219.673 |
| 23 | 1.0466 | SLV_3 | Min | 0. | 0. | 86.8396 |
| 23 | 2.09321 | SLV_3 | Min | 0. | 0. | -204.2299 |
| 23 | 0. | SLV_4 | Max | 0. | 0. | 224.8231 |
| 23 | 1.0466 | SLV_4 | Max | 0. | 0. | 91.1599 |
| 23 | 2.09321 | SLV_4 | Max | 0. | 0. | -200.7393 |
| 23 | 0. | SLV_4 | Min | 0. | 0. | 224.8231 |
| 23 | 1.0466 | SLV_4 | Min | 0. | 0. | 91.1599 |
| 23 | 2.09321 | SLV_4 | Min | 0. | 0. | -200.7393 |
| 23 | 0. | SLD_1 | Max | 0. | 0. | 24.3021 |
| 23 | 1.0466 | SLD_1 | Max | 0. | 0. | 79.8978 |
| 23 | 2.09321 | SLD_1 | Max | 0. | 0. | -37.9155 |
| 23 | 0. | SLD_1 | Min | 0. | 0. | 24.3021 |
| 23 | 1.0466 | SLD_1 | Min | 0. | 0. | 79.8978 |
| 23 | 2.09321 | SLD_1 | Min | 0. | 0. | -37.9155 |
| 23 | 0. | SLD_2 | Max | 0. | 0. | 26.5535 |
| 23 | 1.0466 | SLD_2 | Max | 0. | 0. | 81.8004 |
| 23 | 2.09321 | SLD_2 | Max | 0. | 0. | -36.3618 |
| 23 | 0. | SLD_2 | Min | 0. | 0. | 26.5535 |
| 23 | 1.0466 | SLD_2 | Min | 0. | 0. | 81.8004 |
| 23 | 2.09321 | SLD_2 | Min | 0. | 0. | -36.3618 |
| 23 | 0. | SLD_3 | Max | 0. | 0. | -50.2531 |
| 23 | 1.0466 | SLD_3 | Max | 0. | 0. | -58.34 |
| 23 | 2.09321 | SLD_3 | Max | 0. | 0. | -224.6628 |
| 23 | 0. | SLD_3 | Min | 0. | 0. | -50.2531 |
| 23 | 1.0466 | SLD_3 | Min | 0. | 0. | -58.34 |
| 23 | 2.09321 | SLD_3 | Min | 0. | 0. | -224.6628 |
| 23 | 0. | SLD_4 | Max | 0. | 0. | -47.96 |
| 23 | 1.0466 | SLD_4 | Max | 0. | 0. | -56.423 |
| 23 | 2.09321 | SLD_4 | Max | 0. | 0. | -223.122 |
| 23 | 0. | SLD_4 | Min | 0. | 0. | -47.96 |
| 23 | 1.0466 | SLD_4 | Min | 0. | 0. | -56.423 |
| 23 | 2.09321 | SLD_4 | Min | 0. | 0. | -223.122 |
| 23 | 0. | SLU_IDR_1 | Max | 0. | 0. | -405.332 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 23 | 1.0466 | SLU_IDR_1 | Max | 0. | 0. | -246.5948 |
| 23 | 2.09321 | SLU_IDR_1 | Max | 0. | 0. | -232.8291 |
| 23 | 0. | SLU_IDR_1 | Min | 0. | 0. | -405.332 |
| 23 | 1.0466 | SLU_IDR_1 | Min | 0. | 0. | -246.5948 |
| 23 | 2.09321 | SLU_IDR_1 | Min | 0. | 0. | -232.8291 |
| 23 | 0. | SLU_IDR_2 | Max | 0. | 0. | -259.2895 |
| 23 | 1.0466 | SLU_IDR_2 | Max | 0. | 0. | -61.6371 |
| 23 | 2.09321 | SLU_IDR_2 | Max | 0. | 0. | -19.7296 |
| 23 | 0. | SLU_IDR_2 | Min | 0. | 0. | -259.2895 |
| 23 | 1.0466 | SLU_IDR_2 | Min | 0. | 0. | -61.6371 |
| 23 | 2.09321 | SLU_IDR_2 | Min | 0. | 0. | -19.7296 |
| 23 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 489.8005 |
| 23 | 1.0466 | SISMA WOOD SLV-1 | Max | 0. | 0. | 279.0552 |
| 23 | 2.09321 | SISMA WOOD SLV-1 | Max | 0. | 0. | 68.3098 |
| 23 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 489.8005 |
| 23 | 1.0466 | SISMA WOOD SLV-1 | Min | 0. | 0. | 279.0552 |
| 23 | 2.09321 | SISMA WOOD SLV-1 | Min | 0. | 0. | 68.3098 |
| 23 | 0. | DEAD-1 | Max | 0. | 0. | -156.9002 |
| 23 | 1.0466 | DEAD-1 | Max | 0. | 0. | -110.2937 |
| 23 | 2.09321 | DEAD-1 | Max | 0. | 0. | -80.3521 |
| 23 | 0. | DEAD-1 | Min | 0. | 0. | -156.9002 |
| 23 | 1.0466 | DEAD-1 | Min | 0. | 0. | -110.2937 |
| 23 | 2.09321 | DEAD-1 | Min | 0. | 0. | -80.3521 |
| 23 | 0. | SLU_PROVA | | 0. | 0. | -127.3341 |
| 23 | 1.0466 | SLU_PROVA | | 0. | 0. | 106.2528 |
| 23 | 2.09321 | SLU_PROVA | | 0. | 0. | 81.3686 |
| 24 | 0. | DEAD | | 0. | 0. | -54.9162 |
| 24 | 1.0467 | DEAD | | 0. | 0. | -11.8368 |
| 24 | 2.09341 | DEAD | | 0. | 0. | 9.5194 |
| 24 | 0. | SIMM_KA | | 0. | 0. | 106.5772 |
| 24 | 1.0467 | SIMM_KA | | 0. | 0. | 47.5668 |
| 24 | 2.09341 | SIMM_KA | | 0. | 0. | -26.9371 |
| 24 | 0. | SIMM_K0 | | 0. | 0. | 168.2387 |
| 24 | 1.0467 | SIMM_K0 | | 0. | 0. | 77.7439 |
| 24 | 2.09341 | SIMM_K0 | | 0. | 0. | -38.3254 |
| 24 | 0. | A--SIMM_KA | | 0. | 0. | 80.5337 |
| 24 | 1.0467 | A--SIMM_KA | | 0. | 0. | 14.3032 |
| 24 | 2.09341 | A--SIMM_KA | | 0. | 0. | -68.261 |
| 24 | 0. | A--SIMM_K0 | | 0. | 0. | 120.7204 |
| 24 | 1.0467 | A--SIMM_K0 | | 0. | 0. | 20.1872 |
| 24 | 2.09341 | A--SIMM_K0 | | 0. | 0. | -104.8433 |
| 24 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 24.0904 |
| 24 | 1.0467 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.9065 |
| 24 | 2.09341 | A-- SIMM_SOVR_K A | | 0. | 0. | -0.7261 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 24 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 36.1176 |
| 24 | 1.0467 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.8493 |
| 24 | 2.09341 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -1.0885 |
| 24 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 36.1176 |
| 24 | 1.0467 | SIMM_SOVR_K 0 | | 0. | 0. | 20.8493 |
| 24 | 2.09341 | SIMM_SOVR_K 0 | | 0. | 0. | -1.0885 |
| 24 | 0. | SIMM_SOVR_K A | | 0. | 0. | 24.0904 |
| 24 | 1.0467 | SIMM_SOVR_K A | | 0. | 0. | 13.9065 |
| 24 | 2.09341 | SIMM_SOVR_K A | | 0. | 0. | -0.7261 |
| 24 | 0. | SOVR | | 0. | 0. | -50.3535 |
| 24 | 1.0467 | SOVR | | 0. | 0. | -8.1256 |
| 24 | 2.09341 | SOVR | | 0. | 0. | 16.7186 |
| 24 | 0. | TERR_SIMM | | 0. | 0. | -124.1473 |
| 24 | 1.0467 | TERR_SIMM | | 0. | 0. | 2.748 |
| 24 | 2.09341 | TERR_SIMM | | 0. | 0. | 66.897 |
| 24 | 0. | TERR_A--SIMM | | 0. | 0. | -245.7295 |
| 24 | 1.0467 | TERR_A--SIMM | | 0. | 0. | -90.2995 |
| 24 | 2.09341 | TERR_A--SIMM | | 0. | 0. | 1.2717 |
| 24 | 0. | INERZIA H SLV | | 0. | 0. | -4.3779 |
| 24 | 1.0467 | INERZIA H SLV | | 0. | 0. | -4.3331 |
| 24 | 2.09341 | INERZIA H SLV | | 0. | 0. | -4.2882 |
| 24 | 0. | INERZIA V + SLV | | 0. | 0. | -0.7853 |
| 24 | 1.0467 | INERZIA V + SLV | | 0. | 0. | -0.2519 |
| 24 | 2.09341 | INERZIA V + SLV | | 0. | 0. | 0.2814 |
| 24 | 0. | INERZIA V - SLV | | 0. | 0. | 0.7853 |
| 24 | 1.0467 | INERZIA V - SLV | | 0. | 0. | 0.2519 |
| 24 | 2.09341 | INERZIA V - SLV | | 0. | 0. | -0.2814 |
| 24 | 0. | SISMA WOOD SLV | | 0. | 0. | -74.8795 |
| 24 | 1.0467 | SISMA WOOD SLV | | 0. | 0. | -148.5839 |
| 24 | 2.09341 | SISMA WOOD SLV | | 0. | 0. | -222.2882 |
| 24 | 0. | iDROSTATICA | | 0. | 0. | 89.842 |
| 24 | 1.0467 | iDROSTATICA | | 0. | 0. | 80.4287 |
| 24 | 2.09341 | iDROSTATICA | | 0. | 0. | 26.4577 |
| 24 | 0. | SISMA WOOD SLD | | 0. | 0. | -33.0698 |
| 24 | 1.0467 | SISMA WOOD SLD | | 0. | 0. | -65.6206 |
| 24 | 2.09341 | SISMA WOOD SLD | | 0. | 0. | -98.1715 |
| 24 | 0. | INERZIA H SLD | | 0. | 0. | -1.9335 |
| 24 | 1.0467 | INERZIA H SLD | | 0. | 0. | -1.9137 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 24 | 2.09341 | INERZIA H SLD | | 0. | 0. | -1.8939 |
| 24 | 0. | INERZIA V + SLD | | 0. | 0. | -0.3468 |
| 24 | 1.0467 | INERZIA V + SLD | | 0. | 0. | -0.1113 |
| 24 | 2.09341 | INERZIA V + SLD | | 0. | 0. | 0.1243 |
| 24 | 0. | INERZIA V SLD | | 0. | 0. | 0.3468 |
| 24 | 1.0467 | INERZIA V SLD | | 0. | 0. | 0.1113 |
| 24 | 2.09341 | INERZIA V SLD | | 0. | 0. | -0.1243 |
| 24 | 0. | INERZIA V -1 | | 0. | 0. | 0.7853 |
| 24 | 1.0467 | INERZIA V -1 | | 0. | 0. | 0.2519 |
| 24 | 2.09341 | INERZIA V -1 | | 0. | 0. | -0.2814 |
| 24 | 0. | SLU_1 | Max | 0. | 0. | 11.6138 |
| 24 | 1.0467 | SLU_1 | Max | 0. | 0. | 198.1294 |
| 24 | 2.09341 | SLU_1 | Max | 0. | 0. | 147.5831 |
| 24 | 0. | SLU_1 | Min | 0. | 0. | 11.6138 |
| 24 | 1.0467 | SLU_1 | Min | 0. | 0. | 198.1294 |
| 24 | 2.09341 | SLU_1 | Min | 0. | 0. | 147.5831 |
| 24 | 0. | SLU_2 | Max | 0. | 0. | -109.9099 |
| 24 | 1.0467 | SLU_2 | Max | 0. | 0. | 139.1321 |
| 24 | 2.09341 | SLU_2 | Max | 0. | 0. | 167.5491 |
| 24 | 0. | SLU_2 | Min | 0. | 0. | -109.9099 |
| 24 | 1.0467 | SLU_2 | Min | 0. | 0. | 139.1321 |
| 24 | 2.09341 | SLU_2 | Min | 0. | 0. | 167.5491 |
| 24 | 0. | SLU_3 | Max | 0. | 0. | -358.9118 |
| 24 | 1.0467 | SLU_3 | Max | 0. | 0. | -149.2328 |
| 24 | 2.09341 | SLU_3 | Max | 0. | 0. | -176.6617 |
| 24 | 0. | SLU_3 | Min | 0. | 0. | -358.9118 |
| 24 | 1.0467 | SLU_3 | Min | 0. | 0. | -149.2328 |
| 24 | 2.09341 | SLU_3 | Min | 0. | 0. | -176.6617 |
| 24 | 0. | SLU_4 | Max | 0. | 0. | -422.5319 |
| 24 | 1.0467 | SLU_4 | Max | 0. | 0. | -143.1093 |
| 24 | 2.09341 | SLU_4 | Max | 0. | 0. | -86.8506 |
| 24 | 0. | SLU_4 | Min | 0. | 0. | -422.5319 |
| 24 | 1.0467 | SLU_4 | Min | 0. | 0. | -143.1093 |
| 24 | 2.09341 | SLU_4 | Min | 0. | 0. | -86.8506 |
| 24 | 0. | SLE_F1 | Max | 0. | 0. | 19.6651 |
| 24 | 1.0467 | SLE_F1 | Max | 0. | 0. | 149.5924 |
| 24 | 2.09341 | SLE_F1 | Max | 0. | 0. | 106.8782 |
| 24 | 0. | SLE_F1 | Min | 0. | 0. | 19.6651 |
| 24 | 1.0467 | SLE_F1 | Min | 0. | 0. | 149.5924 |
| 24 | 2.09341 | SLE_F1 | Min | 0. | 0. | 106.8782 |
| 24 | 0. | SLE_F2 | Max | 0. | 0. | -68.6102 |
| 24 | 1.0467 | SLE_F2 | Max | 0. | 0. | 107.0893 |
| 24 | 2.09341 | SLE_F2 | Max | 0. | 0. | 121.8942 |
| 24 | 0. | SLE_F2 | Min | 0. | 0. | -68.6102 |
| 24 | 1.0467 | SLE_F2 | Min | 0. | 0. | 107.0893 |
| 24 | 2.09341 | SLE_F2 | Min | 0. | 0. | 121.8942 |
| 24 | 0. | SLE_F3 | Max | 0. | 0. | -308.589 |
| 24 | 1.0467 | SLE_F3 | Max | 0. | 0. | -109.8791 |
| 24 | 2.09341 | SLE_F3 | Max | 0. | 0. | -74.0168 |
| 24 | 0. | SLE_F3 | Min | 0. | 0. | -308.589 |
| 24 | 1.0467 | SLE_F3 | Min | 0. | 0. | -109.8791 |
| 24 | 2.09341 | SLE_F3 | Min | 0. | 0. | -74.0168 |
| 24 | 0. | SLE_F4 | Max | 0. | 0. | -262.2227 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 24 | 1.0467 | SLE_F4 | Max | 0. | 0. | -116.645 |
| 24 | 2.09341 | SLE_F4 | Max | 0. | 0. | -143.7443 |
| 24 | 0. | SLE_F4 | Min | 0. | 0. | -262.2227 |
| 24 | 1.0467 | SLE_F4 | Min | 0. | 0. | -116.645 |
| 24 | 2.09341 | SLE_F4 | Min | 0. | 0. | -143.7443 |
| 24 | 0. | SLE_QP1 | Max | 0. | 0. | 38.5225 |
| 24 | 1.0467 | SLE_QP1 | Max | 0. | 0. | 143.7785 |
| 24 | 2.09341 | SLE_QP1 | Max | 0. | 0. | 94.4329 |
| 24 | 0. | SLE_QP1 | Min | 0. | 0. | 38.5225 |
| 24 | 1.0467 | SLE_QP1 | Min | 0. | 0. | 143.7785 |
| 24 | 2.09341 | SLE_QP1 | Min | 0. | 0. | 94.4329 |
| 24 | 0. | SLE_QP2 | Max | 0. | 0. | -39.0118 |
| 24 | 1.0467 | SLE_QP2 | Max | 0. | 0. | 107.2112 |
| 24 | 2.09341 | SLE_QP2 | Max | 0. | 0. | 108.9137 |
| 24 | 0. | SLE_QP2 | Min | 0. | 0. | -39.0118 |
| 24 | 1.0467 | SLE_QP2 | Min | 0. | 0. | 107.2112 |
| 24 | 2.09341 | SLE_QP2 | Min | 0. | 0. | 108.9137 |
| 24 | 0. | SLE_QP3 | Max | 0. | 0. | -278.064 |
| 24 | 1.0467 | SLE_QP3 | Max | 0. | 0. | -109.4971 |
| 24 | 2.09341 | SLE_QP3 | Max | 0. | 0. | -87.4037 |
| 24 | 0. | SLE_QP3 | Min | 0. | 0. | -278.064 |
| 24 | 1.0467 | SLE_QP3 | Min | 0. | 0. | -109.4971 |
| 24 | 2.09341 | SLE_QP3 | Min | 0. | 0. | -87.4037 |
| 24 | 0. | SLE_QP4 | Max | 0. | 0. | -234.8505 |
| 24 | 1.0467 | SLE_QP4 | Max | 0. | 0. | -119.0048 |
| 24 | 2.09341 | SLE_QP4 | Max | 0. | 0. | -157.796 |
| 24 | 0. | SLE_QP4 | Min | 0. | 0. | -234.8505 |
| 24 | 1.0467 | SLE_QP4 | Min | 0. | 0. | -119.0048 |
| 24 | 2.09341 | SLE_QP4 | Min | 0. | 0. | -157.796 |
| 24 | 0. | SLV_1 | Max | 0. | 0. | -15.123 |
| 24 | 1.0467 | SLV_1 | Max | 0. | 0. | -99.3208 |
| 24 | 2.09341 | SLV_1 | Max | 0. | 0. | -338.1202 |
| 24 | 0. | SLV_1 | Min | 0. | 0. | -15.123 |
| 24 | 1.0467 | SLV_1 | Min | 0. | 0. | -99.3208 |
| 24 | 2.09341 | SLV_1 | Min | 0. | 0. | -338.1202 |
| 24 | 0. | SLV_2 | Max | 0. | 0. | -11.7507 |
| 24 | 1.0467 | SLV_2 | Max | 0. | 0. | -97.1176 |
| 24 | 2.09341 | SLV_2 | Max | 0. | 0. | -337.0862 |
| 24 | 0. | SLV_2 | Min | 0. | 0. | -11.7507 |
| 24 | 1.0467 | SLV_2 | Min | 0. | 0. | -97.1176 |
| 24 | 2.09341 | SLV_2 | Min | 0. | 0. | -337.0862 |
| 24 | 0. | SLV_3 | Max | 0. | 0. | -204.2299 |
| 24 | 1.0467 | SLV_3 | Max | 0. | 0. | -291.2808 |
| 24 | 2.09341 | SLV_3 | Max | 0. | 0. | -532.9687 |
| 24 | 0. | SLV_3 | Min | 0. | 0. | -204.2299 |
| 24 | 1.0467 | SLV_3 | Min | 0. | 0. | -291.2808 |
| 24 | 2.09341 | SLV_3 | Min | 0. | 0. | -532.9687 |
| 24 | 0. | SLV_4 | Max | 0. | 0. | -200.7393 |
| 24 | 1.0467 | SLV_4 | Max | 0. | 0. | -289.0836 |
| 24 | 2.09341 | SLV_4 | Max | 0. | 0. | -532.0649 |
| 24 | 0. | SLV_4 | Min | 0. | 0. | -200.7393 |
| 24 | 1.0467 | SLV_4 | Min | 0. | 0. | -289.0836 |
| 24 | 2.09341 | SLV_4 | Min | 0. | 0. | -532.0649 |
| 24 | 0. | SLD_1 | Max | 0. | 0. | -37.9155 |
| 24 | 1.0467 | SLD_1 | Max | 0. | 0. | -13.3495 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 24 | 2.09341 | SLD_1 | Max | 0. | 0. | -143.3851 |
| 24 | 0. | SLD_1 | Min | 0. | 0. | -37.9155 |
| 24 | 1.0467 | SLD_1 | Min | 0. | 0. | -13.3495 |
| 24 | 2.09341 | SLD_1 | Min | 0. | 0. | -143.3851 |
| 24 | 0. | SLD_2 | Max | 0. | 0. | -36.3618 |
| 24 | 1.0467 | SLD_2 | Max | 0. | 0. | -12.47 |
| 24 | 2.09341 | SLD_2 | Max | 0. | 0. | -143.1797 |
| 24 | 0. | SLD_2 | Min | 0. | 0. | -36.3618 |
| 24 | 1.0467 | SLD_2 | Min | 0. | 0. | -12.47 |
| 24 | 2.09341 | SLD_2 | Min | 0. | 0. | -143.1797 |
| 24 | 0. | SLD_3 | Max | 0. | 0. | -224.6628 |
| 24 | 1.0467 | SLD_3 | Max | 0. | 0. | -210.858 |
| 24 | 2.09341 | SLD_3 | Max | 0. | 0. | -351.69 |
| 24 | 0. | SLD_3 | Min | 0. | 0. | -224.6628 |
| 24 | 1.0467 | SLD_3 | Min | 0. | 0. | -210.858 |
| 24 | 2.09341 | SLD_3 | Min | 0. | 0. | -351.69 |
| 24 | 0. | SLD_4 | Max | 0. | 0. | -223.122 |
| 24 | 1.0467 | SLD_4 | Max | 0. | 0. | -209.9315 |
| 24 | 2.09341 | SLD_4 | Max | 0. | 0. | -351.3779 |
| 24 | 0. | SLD_4 | Min | 0. | 0. | -223.122 |
| 24 | 1.0467 | SLD_4 | Min | 0. | 0. | -209.9315 |
| 24 | 2.09341 | SLD_4 | Min | 0. | 0. | -351.3779 |
| 24 | 0. | SLU_IDR_1 | Max | 0. | 0. | -232.8291 |
| 24 | 1.0467 | SLU_IDR_1 | Max | 0. | 0. | -77.8598 |
| 24 | 2.09341 | SLU_IDR_1 | Max | 0. | 0. | -63.6281 |
| 24 | 0. | SLU_IDR_1 | Min | 0. | 0. | -232.8291 |
| 24 | 1.0467 | SLU_IDR_1 | Min | 0. | 0. | -77.8598 |
| 24 | 2.09341 | SLU_IDR_1 | Min | 0. | 0. | -63.6281 |
| 24 | 0. | SLU_IDR_2 | Max | 0. | 0. | -19.7296 |
| 24 | 1.0467 | SLU_IDR_2 | Max | 0. | 0. | 116.6213 |
| 24 | 2.09341 | SLU_IDR_2 | Max | 0. | 0. | 113.9922 |
| 24 | 0. | SLU_IDR_2 | Min | 0. | 0. | -19.7296 |
| 24 | 1.0467 | SLU_IDR_2 | Min | 0. | 0. | 116.6213 |
| 24 | 2.09341 | SLU_IDR_2 | Min | 0. | 0. | 113.9922 |
| 24 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 68.3098 |
| 24 | 1.0467 | SISMA WOOD SLV-1 | Max | 0. | 0. | -92.6372 |
| 24 | 2.09341 | SISMA WOOD SLV-1 | Max | 0. | 0. | -253.5843 |
| 24 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 68.3098 |
| 24 | 1.0467 | SISMA WOOD SLV-1 | Min | 0. | 0. | -92.6372 |
| 24 | 2.09341 | SISMA WOOD SLV-1 | Min | 0. | 0. | -253.5843 |
| 24 | 0. | DEAD-1 | Max | 0. | 0. | -80.3521 |
| 24 | 1.0467 | DEAD-1 | Max | 0. | 0. | -21.0065 |
| 24 | 2.09341 | DEAD-1 | Max | 0. | 0. | 16.6158 |
| 24 | 0. | DEAD-1 | Min | 0. | 0. | -80.3521 |
| 24 | 1.0467 | DEAD-1 | Min | 0. | 0. | -21.0065 |
| 24 | 2.09341 | DEAD-1 | Min | 0. | 0. | 16.6158 |
| 24 | 0. | SLU_PROVA | | 0. | 0. | 81.3686 |
| 24 | 1.0467 | SLU_PROVA | | 0. | 0. | 212.8945 |
| 24 | 2.09341 | SLU_PROVA | | 0. | 0. | 107.3585 |
| 25 | 0. | DEAD | | 0. | 0. | 9.5194 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 25 | 1.04666 | DEAD | | 0. | 0. | 46.7288 |
| 25 | 2.09331 | DEAD | | 0. | 0. | 58.6429 |
| 25 | 0. | SIMM_KA | | 0. | 0. | -26.9371 |
| 25 | 1.04666 | SIMM_KA | | 0. | 0. | -78.7095 |
| 25 | 2.09331 | SIMM_KA | | 0. | 0. | -139.1717 |
| 25 | 0. | SIMM_K0 | | 0. | 0. | -38.3254 |
| 25 | 1.04666 | SIMM_K0 | | 0. | 0. | -120.3798 |
| 25 | 2.09331 | SIMM_K0 | | 0. | 0. | -217.0387 |
| 25 | 0. | A--SIMM_KA | | 0. | 0. | -68.261 |
| 25 | 1.04666 | A--SIMM_KA | | 0. | 0. | -125.4937 |
| 25 | 2.09331 | A--SIMM_KA | | 0. | 0. | -192.9922 |
| 25 | 0. | A--SIMM_K0 | | 0. | 0. | -104.8433 |
| 25 | 1.04666 | A--SIMM_K0 | | 0. | 0. | -191.1313 |
| 25 | 2.09331 | A--SIMM_K0 | | 0. | 0. | -292.816 |
| 25 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -0.7261 |
| 25 | 1.04666 | A-- SIMM_SOVR_K A | | 0. | 0. | -11.947 |
| 25 | 2.09331 | A-- SIMM_SOVR_K A | | 0. | 0. | -25.964 |
| 25 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -1.0885 |
| 25 | 1.04666 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -17.9116 |
| 25 | 2.09331 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -38.9265 |
| 25 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -1.0885 |
| 25 | 1.04666 | SIMM_SOVR_K 0 | | 0. | 0. | -17.9116 |
| 25 | 2.09331 | SIMM_SOVR_K 0 | | 0. | 0. | -38.9265 |
| 25 | 0. | SIMM_SOVR_K A | | 0. | 0. | -0.7261 |
| 25 | 1.04666 | SIMM_SOVR_K A | | 0. | 0. | -11.947 |
| 25 | 2.09331 | SIMM_SOVR_K A | | 0. | 0. | -25.964 |
| 25 | 0. | SOVR | | 0. | 0. | 16.7186 |
| 25 | 1.04666 | SOVR | | 0. | 0. | 51.3685 |
| 25 | 2.09331 | SOVR | | 0. | 0. | 65.7759 |
| 25 | 0. | TERR_SIMM | | 0. | 0. | 66.897 |
| 25 | 1.04666 | TERR_SIMM | | 0. | 0. | 161.4788 |
| 25 | 2.09331 | TERR_SIMM | | 0. | 0. | 193.274 |
| 25 | 0. | TERR_A--SIMM | | 0. | 0. | 1.2717 |
| 25 | 1.04666 | TERR_A--SIMM | | 0. | 0. | 138.016 |
| 25 | 2.09331 | TERR_A--SIMM | | 0. | 0. | 200.4002 |
| 25 | 0. | INERZIA H SLV | | 0. | 0. | -4.2882 |
| 25 | 1.04666 | INERZIA H SLV | | 0. | 0. | -3.4199 |
| 25 | 2.09331 | INERZIA H SLV | | 0. | 0. | -2.5515 |
| 25 | 0. | INERZIA V + SLV | | 0. | 0. | 0.2814 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 25 | 1.04666 | INERZIA V + SLV | | 0. | 0. | 0.6863 |
| 25 | 2.09331 | INERZIA V + SLV | | 0. | 0. | 1.0912 |
| 25 | 0. | INERZIA V - SLV | | 0. | 0. | -0.2814 |
| 25 | 1.04666 | INERZIA V - SLV | | 0. | 0. | -0.6863 |
| 25 | 2.09331 | INERZIA V - SLV | | 0. | 0. | -1.0912 |
| 25 | 0. | SISMA WOOD SLV | | 0. | 0. | -222.2882 |
| 25 | 1.04666 | SISMA WOOD SLV | | 0. | 0. | -252.808 |
| 25 | 2.09331 | SISMA WOOD SLV | | 0. | 0. | -283.3277 |
| 25 | 0. | iDROSTATICA | | 0. | 0. | 26.4577 |
| 25 | 1.04666 | iDROSTATICA | | 0. | 0. | 8.548 |
| 25 | 2.09331 | iDROSTATICA | | 0. | 0. | -40.512 |
| 25 | 0. | SISMA WOOD SLD | | 0. | 0. | -98.1715 |
| 25 | 1.04666 | SISMA WOOD SLD | | 0. | 0. | -111.6502 |
| 25 | 2.09331 | SISMA WOOD SLD | | 0. | 0. | -125.1289 |
| 25 | 0. | INERZIA H SLD | | 0. | 0. | -1.8939 |
| 25 | 1.04666 | INERZIA H SLD | | 0. | 0. | -1.5103 |
| 25 | 2.09331 | INERZIA H SLD | | 0. | 0. | -1.1268 |
| 25 | 0. | INERZIA V + SLD | | 0. | 0. | 0.1243 |
| 25 | 1.04666 | INERZIA V + SLD | | 0. | 0. | 0.3031 |
| 25 | 2.09331 | INERZIA V + SLD | | 0. | 0. | 0.4819 |
| 25 | 0. | INERZIA V SLD | | 0. | 0. | -0.1243 |
| 25 | 1.04666 | INERZIA V SLD | | 0. | 0. | -0.3031 |
| 25 | 2.09331 | INERZIA V SLD | | 0. | 0. | -0.4819 |
| 25 | 0. | INERZIA V -1 | | 0. | 0. | -0.2814 |
| 25 | 1.04666 | INERZIA V -1 | | 0. | 0. | -0.6863 |
| 25 | 2.09331 | INERZIA V -1 | | 0. | 0. | -1.0912 |
| 25 | 0. | SLU_1 | Max | 0. | 0. | 147.5831 |
| 25 | 1.04666 | SLU_1 | Max | 0. | 0. | 256.0938 |
| 25 | 2.09331 | SLU_1 | Max | 0. | 0. | 153.9654 |
| 25 | 0. | SLU_1 | Min | 0. | 0. | 147.5831 |
| 25 | 1.04666 | SLU_1 | Min | 0. | 0. | 256.0938 |
| 25 | 2.09331 | SLU_1 | Min | 0. | 0. | 153.9654 |
| 25 | 0. | SLU_2 | Max | 0. | 0. | 167.5491 |
| 25 | 1.04666 | SLU_2 | Max | 0. | 0. | 336.2553 |
| 25 | 2.09331 | SLU_2 | Max | 0. | 0. | 304.1052 |
| 25 | 0. | SLU_2 | Min | 0. | 0. | 167.5491 |
| 25 | 1.04666 | SLU_2 | Min | 0. | 0. | 336.2553 |
| 25 | 2.09331 | SLU_2 | Min | 0. | 0. | 304.1052 |
| 25 | 0. | SLU_3 | Max | 0. | 0. | -176.6617 |
| 25 | 1.04666 | SLU_3 | Max | 0. | 0. | 11.935 |
| 25 | 2.09331 | SLU_3 | Max | 0. | 0. | -26.183 |
| 25 | 0. | SLU_3 | Min | 0. | 0. | -176.6617 |
| 25 | 1.04666 | SLU_3 | Min | 0. | 0. | 11.935 |
| 25 | 2.09331 | SLU_3 | Min | 0. | 0. | -26.183 |
| 25 | 0. | SLU_4 | Max | 0. | 0. | -86.8506 |
| 25 | 1.04666 | SLU_4 | Max | 0. | 0. | 156.1266 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 25 | 2.09331 | SLU_4 | Max | 0. | 0. | 181.153 |
| 25 | 0. | SLU_4 | Min | 0. | 0. | -86.8506 |
| 25 | 1.04666 | SLU_4 | Min | 0. | 0. | 156.1266 |
| 25 | 2.09331 | SLU_4 | Min | 0. | 0. | 181.153 |
| 25 | 0. | SLE_F1 | Max | 0. | 0. | 106.8782 |
| 25 | 1.04666 | SLE_F1 | Max | 0. | 0. | 180.8378 |
| 25 | 2.09331 | SLE_F1 | Max | 0. | 0. | 102.6349 |
| 25 | 0. | SLE_F1 | Min | 0. | 0. | 106.8782 |
| 25 | 1.04666 | SLE_F1 | Min | 0. | 0. | 180.8378 |
| 25 | 2.09331 | SLE_F1 | Min | 0. | 0. | 102.6349 |
| 25 | 0. | SLE_F2 | Max | 0. | 0. | 121.8942 |
| 25 | 1.04666 | SLE_F2 | Max | 0. | 0. | 239.6021 |
| 25 | 2.09331 | SLE_F2 | Max | 0. | 0. | 212.1093 |
| 25 | 0. | SLE_F2 | Min | 0. | 0. | 121.8942 |
| 25 | 1.04666 | SLE_F2 | Min | 0. | 0. | 239.6021 |
| 25 | 2.09331 | SLE_F2 | Min | 0. | 0. | 212.1093 |
| 25 | 0. | SLE_F3 | Max | 0. | 0. | -74.0168 |
| 25 | 1.04666 | SLE_F3 | Max | 0. | 0. | 100.5858 |
| 25 | 2.09331 | SLE_F3 | Max | 0. | 0. | 116.8379 |
| 25 | 0. | SLE_F3 | Min | 0. | 0. | -74.0168 |
| 25 | 1.04666 | SLE_F3 | Min | 0. | 0. | 100.5858 |
| 25 | 2.09331 | SLE_F3 | Min | 0. | 0. | 116.8379 |
| 25 | 0. | SLE_F4 | Max | 0. | 0. | -143.7443 |
| 25 | 1.04666 | SLE_F4 | Max | 0. | 0. | -9.6079 |
| 25 | 2.09331 | SLE_F4 | Max | 0. | 0. | -39.9998 |
| 25 | 0. | SLE_F4 | Min | 0. | 0. | -143.7443 |
| 25 | 1.04666 | SLE_F4 | Min | 0. | 0. | -9.6079 |
| 25 | 2.09331 | SLE_F4 | Min | 0. | 0. | -39.9998 |
| 25 | 0. | SLE_QP1 | Max | 0. | 0. | 94.4329 |
| 25 | 1.04666 | SLE_QP1 | Max | 0. | 0. | 151.0975 |
| 25 | 2.09331 | SLE_QP1 | Max | 0. | 0. | 73.9252 |
| 25 | 0. | SLE_QP1 | Min | 0. | 0. | 94.4329 |
| 25 | 1.04666 | SLE_QP1 | Min | 0. | 0. | 151.0975 |
| 25 | 2.09331 | SLE_QP1 | Min | 0. | 0. | 73.9252 |
| 25 | 0. | SLE_QP2 | Max | 0. | 0. | 108.9137 |
| 25 | 1.04666 | SLE_QP2 | Max | 0. | 0. | 204.2122 |
| 25 | 2.09331 | SLE_QP2 | Max | 0. | 0. | 171.5887 |
| 25 | 0. | SLE_QP2 | Min | 0. | 0. | 108.9137 |
| 25 | 1.04666 | SLE_QP2 | Min | 0. | 0. | 204.2122 |
| 25 | 2.09331 | SLE_QP2 | Min | 0. | 0. | 171.5887 |
| 25 | 0. | SLE_QP3 | Max | 0. | 0. | -87.4037 |
| 25 | 1.04666 | SLE_QP3 | Max | 0. | 0. | 64.3501 |
| 25 | 2.09331 | SLE_QP3 | Max | 0. | 0. | 75.0322 |
| 25 | 0. | SLE_QP3 | Min | 0. | 0. | -87.4037 |
| 25 | 1.04666 | SLE_QP3 | Min | 0. | 0. | 64.3501 |
| 25 | 2.09331 | SLE_QP3 | Min | 0. | 0. | 75.0322 |
| 25 | 0. | SLE_QP4 | Max | 0. | 0. | -157.796 |
| 25 | 1.04666 | SLE_QP4 | Max | 0. | 0. | -44.3954 |
| 25 | 2.09331 | SLE_QP4 | Max | 0. | 0. | -77.1974 |
| 25 | 0. | SLE_QP4 | Min | 0. | 0. | -157.796 |
| 25 | 1.04666 | SLE_QP4 | Min | 0. | 0. | -44.3954 |
| 25 | 2.09331 | SLE_QP4 | Min | 0. | 0. | -77.1974 |
| 25 | 0. | SLV_1 | Max | 0. | 0. | -338.1202 |
| 25 | 1.04666 | SLV_1 | Max | 0. | 0. | -377.4857 |
| 25 | 2.09331 | SLV_1 | Max | 0. | 0. | -550.6879 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 25 | 0. | SLV_1 | Min | 0. | 0. | -338.1202 |
| 25 | 1.04666 | SLV_1 | Min | 0. | 0. | -377.4857 |
| 25 | 2.09331 | SLV_1 | Min | 0. | 0. | -550.6879 |
| 25 | 0. | SLV_2 | Max | 0. | 0. | -337.0862 |
| 25 | 1.04666 | SLV_2 | Max | 0. | 0. | -377.6551 |
| 25 | 2.09331 | SLV_2 | Max | 0. | 0. | -552.0608 |
| 25 | 0. | SLV_2 | Min | 0. | 0. | -337.0862 |
| 25 | 1.04666 | SLV_2 | Min | 0. | 0. | -377.6551 |
| 25 | 2.09331 | SLV_2 | Min | 0. | 0. | -552.0608 |
| 25 | 0. | SLV_3 | Max | 0. | 0. | -532.9687 |
| 25 | 1.04666 | SLV_3 | Max | 0. | 0. | -542.8219 |
| 25 | 2.09331 | SLV_3 | Max | 0. | 0. | -698.8776 |
| 25 | 0. | SLV_3 | Min | 0. | 0. | -532.9687 |
| 25 | 1.04666 | SLV_3 | Min | 0. | 0. | -542.8219 |
| 25 | 2.09331 | SLV_3 | Min | 0. | 0. | -698.8776 |
| 25 | 0. | SLV_4 | Max | 0. | 0. | -532.0649 |
| 25 | 1.04666 | SLV_4 | Max | 0. | 0. | -543.2852 |
| 25 | 2.09331 | SLV_4 | Max | 0. | 0. | -700.7081 |
| 25 | 0. | SLV_4 | Min | 0. | 0. | -532.0649 |
| 25 | 1.04666 | SLV_4 | Min | 0. | 0. | -543.2852 |
| 25 | 2.09331 | SLV_4 | Min | 0. | 0. | -700.7081 |
| 25 | 0. | SLD_1 | Max | 0. | 0. | -143.3851 |
| 25 | 1.04666 | SLD_1 | Max | 0. | 0. | -112.7682 |
| 25 | 2.09331 | SLD_1 | Max | 0. | 0. | -215.988 |
| 25 | 0. | SLD_1 | Min | 0. | 0. | -143.3851 |
| 25 | 1.04666 | SLD_1 | Min | 0. | 0. | -112.7682 |
| 25 | 2.09331 | SLD_1 | Min | 0. | 0. | -215.988 |
| 25 | 0. | SLD_2 | Max | 0. | 0. | -143.1797 |
| 25 | 1.04666 | SLD_2 | Max | 0. | 0. | -113.2226 |
| 25 | 2.09331 | SLD_2 | Max | 0. | 0. | -217.1022 |
| 25 | 0. | SLD_2 | Min | 0. | 0. | -143.1797 |
| 25 | 1.04666 | SLD_2 | Min | 0. | 0. | -113.2226 |
| 25 | 2.09331 | SLD_2 | Min | 0. | 0. | -217.1022 |
| 25 | 0. | SLD_3 | Max | 0. | 0. | -351.69 |
| 25 | 1.04666 | SLD_3 | Max | 0. | 0. | -294.7841 |
| 25 | 2.09331 | SLD_3 | Max | 0. | 0. | -384.0806 |
| 25 | 0. | SLD_3 | Min | 0. | 0. | -351.69 |
| 25 | 1.04666 | SLD_3 | Min | 0. | 0. | -294.7841 |
| 25 | 2.09331 | SLD_3 | Min | 0. | 0. | -384.0806 |
| 25 | 0. | SLD_4 | Max | 0. | 0. | -351.3779 |
| 25 | 1.04666 | SLD_4 | Max | 0. | 0. | -295.1523 |
| 25 | 2.09331 | SLD_4 | Max | 0. | 0. | -385.1293 |
| 25 | 0. | SLD_4 | Min | 0. | 0. | -351.3779 |
| 25 | 1.04666 | SLD_4 | Min | 0. | 0. | -295.1523 |
| 25 | 2.09331 | SLD_4 | Min | 0. | 0. | -385.1293 |
| 25 | 0. | SLU_IDR_1 | Max | 0. | 0. | -63.6281 |
| 25 | 1.04666 | SLU_IDR_1 | Max | 0. | 0. | 72.0229 |
| 25 | 2.09331 | SLU_IDR_1 | Max | 0. | 0. | 74.4794 |
| 25 | 0. | SLU_IDR_1 | Min | 0. | 0. | -63.6281 |
| 25 | 1.04666 | SLU_IDR_1 | Min | 0. | 0. | 72.0229 |
| 25 | 2.09331 | SLU_IDR_1 | Min | 0. | 0. | 74.4794 |
| 25 | 0. | SLU_IDR_2 | Max | 0. | 0. | 113.9922 |
| 25 | 1.04666 | SLU_IDR_2 | Max | 0. | 0. | 199.8261 |
| 25 | 2.09331 | SLU_IDR_2 | Max | 0. | 0. | 164.3001 |
| 25 | 0. | SLU_IDR_2 | Min | 0. | 0. | 113.9922 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 25 | 1.04666 | SLU_IDR_2 | Min | 0. | 0. | 199.8261 |
| 25 | 2.09331 | SLU_IDR_2 | Min | 0. | 0. | 164.3001 |
| 25 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -253.5843 |
| 25 | 1.04666 | SISMA WOOD SLV-1 | Max | 0. | 0. | -352.8429 |
| 25 | 2.09331 | SISMA WOOD SLV-1 | Max | 0. | 0. | -452.1016 |
| 25 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -253.5843 |
| 25 | 1.04666 | SISMA WOOD SLV-1 | Min | 0. | 0. | -352.8429 |
| 25 | 2.09331 | SISMA WOOD SLV-1 | Min | 0. | 0. | -452.1016 |
| 25 | 0. | DEAD-1 | Max | 0. | 0. | 16.6158 |
| 25 | 1.04666 | DEAD-1 | Max | 0. | 0. | 67.3917 |
| 25 | 2.09331 | DEAD-1 | Max | 0. | 0. | 92.8722 |
| 25 | 0. | DEAD-1 | Min | 0. | 0. | 16.6158 |
| 25 | 1.04666 | DEAD-1 | Min | 0. | 0. | 67.3917 |
| 25 | 2.09331 | DEAD-1 | Min | 0. | 0. | 92.8722 |
| 25 | 0. | SLU_PROVA | | 0. | 0. | 107.3585 |
| 25 | 1.04666 | SLU_PROVA | | 0. | 0. | 175.4738 |
| 25 | 2.09331 | SLU_PROVA | | 0. | 0. | 32.95 |
| 26 | 0. | DEAD | | 0. | 0. | 58.6429 |
| 26 | 1.04666 | DEAD | | 0. | 0. | 81.3088 |
| 26 | 2.09332 | DEAD | | 0. | 0. | 76.8299 |
| 26 | 0. | SIMM_KA | | 0. | 0. | -139.1717 |
| 26 | 1.04666 | SIMM_KA | | 0. | 0. | -161.9479 |
| 26 | 2.09332 | SIMM_KA | | 0. | 0. | -187.5746 |
| 26 | 0. | SIMM_K0 | | 0. | 0. | -217.0387 |
| 26 | 1.04666 | SIMM_K0 | | 0. | 0. | -253.5291 |
| 26 | 2.09332 | SIMM_K0 | | 0. | 0. | -294.4554 |
| 26 | 0. | A--SIMM_KA | | 0. | 0. | -192.9922 |
| 26 | 1.04666 | A--SIMM_KA | | 0. | 0. | -214.8534 |
| 26 | 2.09332 | A--SIMM_KA | | 0. | 0. | -240.2173 |
| 26 | 0. | A--SIMM_K0 | | 0. | 0. | -292.816 |
| 26 | 1.04666 | A--SIMM_K0 | | 0. | 0. | -325.49 |
| 26 | 2.09332 | A--SIMM_K0 | | 0. | 0. | -363.4175 |
| 26 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -25.964 |
| 26 | 1.04666 | A-- SIMM_SOVR_K A | | 0. | 0. | -31.5519 |
| 26 | 2.09332 | A-- SIMM_SOVR_K A | | 0. | 0. | -38.0939 |
| 26 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -38.9265 |
| 26 | 1.04666 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -47.3043 |
| 26 | 2.09332 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -57.1122 |
| 26 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -38.9265 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 26 | 1.04666 | SIMM_SOVR_K 0 | | 0. | 0. | -47.3043 |
| 26 | 2.09332 | SIMM_SOVR_K 0 | | 0. | 0. | -57.1122 |
| 26 | 0. | SIMM_SOVR_K A | | 0. | 0. | -25.964 |
| 26 | 1.04666 | SIMM_SOVR_K A | | 0. | 0. | -31.5519 |
| 26 | 2.09332 | SIMM_SOVR_K A | | 0. | 0. | -38.0939 |
| 26 | 0. | SOVR | | 0. | 0. | 65.7759 |
| 26 | 1.04666 | SOVR | | 0. | 0. | 85.5728 |
| 26 | 2.09332 | SOVR | | 0. | 0. | 83.6473 |
| 26 | 0. | TERR_SIMM | | 0. | 0. | 193.274 |
| 26 | 1.04666 | TERR_SIMM | | 0. | 0. | 248.1846 |
| 26 | 2.09332 | TERR_SIMM | | 0. | 0. | 238.482 |
| 26 | 0. | TERR_A--SIMM | | 0. | 0. | 200.4002 |
| 26 | 1.04666 | TERR_A--SIMM | | 0. | 0. | 295.0977 |
| 26 | 2.09332 | TERR_A--SIMM | | 0. | 0. | 309.9981 |
| 26 | 0. | INERZIA H SLV | | 0. | 0. | -2.5515 |
| 26 | 1.04666 | INERZIA H SLV | | 0. | 0. | -1.2725 |
| 26 | 2.09332 | INERZIA H SLV | | 0. | 0. | 0.0065 |
| 26 | 0. | INERZIA V + SLV | | 0. | 0. | 1.0912 |
| 26 | 1.04666 | INERZIA V + SLV | | 0. | 0. | 1.2409 |
| 26 | 2.09332 | INERZIA V + SLV | | 0. | 0. | 1.3906 |
| 26 | 0. | INERZIA V - SLV | | 0. | 0. | -1.0912 |
| 26 | 1.04666 | INERZIA V - SLV | | 0. | 0. | -1.2409 |
| 26 | 2.09332 | INERZIA V - SLV | | 0. | 0. | -1.3906 |
| 26 | 0. | SISMA WOOD SLV | | 0. | 0. | -283.3277 |
| 26 | 1.04666 | SISMA WOOD SLV | | 0. | 0. | -255.989 |
| 26 | 2.09332 | SISMA WOOD SLV | | 0. | 0. | -228.6503 |
| 26 | 0. | iDROSTATICA | | 0. | 0. | -40.512 |
| 26 | 1.04666 | iDROSTATICA | | 0. | 0. | -43.3017 |
| 26 | 2.09332 | iDROSTATICA | | 0. | 0. | -69.1844 |
| 26 | 0. | SISMA WOOD SLD | | 0. | 0. | -125.1289 |
| 26 | 1.04666 | SISMA WOOD SLD | | 0. | 0. | -113.0551 |
| 26 | 2.09332 | SISMA WOOD SLD | | 0. | 0. | -100.9812 |
| 26 | 0. | INERZIA H SLD | | 0. | 0. | -1.1268 |
| 26 | 1.04666 | INERZIA H SLD | | 0. | 0. | -0.562 |
| 26 | 2.09332 | INERZIA H SLD | | 0. | 0. | 0.0029 |
| 26 | 0. | INERZIA V + SLD | | 0. | 0. | 0.4819 |
| 26 | 1.04666 | INERZIA V + SLD | | 0. | 0. | 0.548 |
| 26 | 2.09332 | INERZIA V + SLD | | 0. | 0. | 0.6141 |
| 26 | 0. | INERZIA V SLD | | 0. | 0. | -0.4819 |
| 26 | 1.04666 | INERZIA V SLD | | 0. | 0. | -0.548 |
| 26 | 2.09332 | INERZIA V SLD | | 0. | 0. | -0.6141 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------|----------|-----------|------------|------------|
| 26 | 0. | INERZIA V -1 | | 0. | 0. | -1.0912 |
| 26 | 1.04666 | INERZIA V -1 | | 0. | 0. | -1.2409 |
| 26 | 2.09332 | INERZIA V -1 | | 0. | 0. | -1.3906 |
| 26 | 0. | SLU_1 | Max | 0. | 0. | 153.9654 |
| 26 | 1.04666 | SLU_1 | Max | 0. | 0. | 234.3445 |
| 26 | 2.09332 | SLU_1 | Max | 0. | 0. | 124.9215 |
| 26 | 0. | SLU_1 | Min | 0. | 0. | 153.9654 |
| 26 | 1.04666 | SLU_1 | Min | 0. | 0. | 234.3445 |
| 26 | 2.09332 | SLU_1 | Min | 0. | 0. | 124.9215 |
| 26 | 0. | SLU_2 | Max | 0. | 0. | 304.1052 |
| 26 | 1.04666 | SLU_2 | Max | 0. | 0. | 411.4753 |
| 26 | 2.09332 | SLU_2 | Max | 0. | 0. | 331.8188 |
| 26 | 0. | SLU_2 | Min | 0. | 0. | 304.1052 |
| 26 | 1.04666 | SLU_2 | Min | 0. | 0. | 411.4753 |
| 26 | 2.09332 | SLU_2 | Min | 0. | 0. | 331.8188 |
| 26 | 0. | SLU_3 | Max | 0. | 0. | -26.183 |
| 26 | 1.04666 | SLU_3 | Max | 0. | 0. | 158.0969 |
| 26 | 2.09332 | SLU_3 | Max | 0. | 0. | 131.773 |
| 26 | 0. | SLU_3 | Min | 0. | 0. | -26.183 |
| 26 | 1.04666 | SLU_3 | Min | 0. | 0. | 158.0969 |
| 26 | 2.09332 | SLU_3 | Min | 0. | 0. | 131.773 |
| 26 | 0. | SLU_4 | Max | 0. | 0. | 181.153 |
| 26 | 1.04666 | SLU_4 | Max | 0. | 0. | 378.862 |
| 26 | 2.09332 | SLU_4 | Max | 0. | 0. | 368.9574 |
| 26 | 0. | SLU_4 | Min | 0. | 0. | 181.153 |
| 26 | 1.04666 | SLU_4 | Min | 0. | 0. | 378.862 |
| 26 | 2.09332 | SLU_4 | Min | 0. | 0. | 368.9574 |
| 26 | 0. | SLE_F1 | Max | 0. | 0. | 102.6349 |
| 26 | 1.04666 | SLE_F1 | Max | 0. | 0. | 158.9182 |
| 26 | 2.09332 | SLE_F1 | Max | 0. | 0. | 78.5501 |
| 26 | 0. | SLE_F1 | Min | 0. | 0. | 102.6349 |
| 26 | 1.04666 | SLE_F1 | Min | 0. | 0. | 158.9182 |
| 26 | 2.09332 | SLE_F1 | Min | 0. | 0. | 78.5501 |
| 26 | 0. | SLE_F2 | Max | 0. | 0. | 212.1093 |
| 26 | 1.04666 | SLE_F2 | Max | 0. | 0. | 287.9507 |
| 26 | 2.09332 | SLE_F2 | Max | 0. | 0. | 229.0833 |
| 26 | 0. | SLE_F2 | Min | 0. | 0. | 212.1093 |
| 26 | 1.04666 | SLE_F2 | Min | 0. | 0. | 287.9507 |
| 26 | 2.09332 | SLE_F2 | Min | 0. | 0. | 229.0833 |
| 26 | 0. | SLE_F3 | Max | 0. | 0. | 116.8379 |
| 26 | 1.04666 | SLE_F3 | Max | 0. | 0. | 262.0723 |
| 26 | 2.09332 | SLE_F3 | Max | 0. | 0. | 256.7618 |
| 26 | 0. | SLE_F3 | Min | 0. | 0. | 116.8379 |
| 26 | 1.04666 | SLE_F3 | Min | 0. | 0. | 262.0723 |
| 26 | 2.09332 | SLE_F3 | Min | 0. | 0. | 256.7618 |
| 26 | 0. | SLE_F4 | Max | 0. | 0. | -39.9998 |
| 26 | 1.04666 | SLE_F4 | Max | 0. | 0. | 95.6162 |
| 26 | 2.09332 | SLE_F4 | Max | 0. | 0. | 78.5793 |
| 26 | 0. | SLE_F4 | Min | 0. | 0. | -39.9998 |
| 26 | 1.04666 | SLE_F4 | Min | 0. | 0. | 95.6162 |
| 26 | 2.09332 | SLE_F4 | Min | 0. | 0. | 78.5793 |
| 26 | 0. | SLE_QP1 | Max | 0. | 0. | 73.9252 |
| 26 | 1.04666 | SLE_QP1 | Max | 0. | 0. | 120.1327 |
| 26 | 2.09332 | SLE_QP1 | Max | 0. | 0. | 47.0532 |
| 26 | 0. | SLE_QP1 | Min | 0. | 0. | 73.9252 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 26 | 1.04666 | SLE_QP1 | Min | 0. | 0. | 120.1327 |
| 26 | 2.09332 | SLE_QP1 | Min | 0. | 0. | 47.0532 |
| 26 | 0. | SLE_QP2 | Max | 0. | 0. | 171.5887 |
| 26 | 1.04666 | SLE_QP2 | Max | 0. | 0. | 234.892 |
| 26 | 2.09332 | SLE_QP2 | Max | 0. | 0. | 180.4938 |
| 26 | 0. | SLE_QP2 | Min | 0. | 0. | 171.5887 |
| 26 | 1.04666 | SLE_QP2 | Min | 0. | 0. | 234.892 |
| 26 | 2.09332 | SLE_QP2 | Min | 0. | 0. | 180.4938 |
| 26 | 0. | SLE_QP3 | Max | 0. | 0. | 75.0322 |
| 26 | 1.04666 | SLE_QP3 | Max | 0. | 0. | 207.5461 |
| 26 | 2.09332 | SLE_QP3 | Max | 0. | 0. | 206.5222 |
| 26 | 0. | SLE_QP3 | Min | 0. | 0. | 75.0322 |
| 26 | 1.04666 | SLE_QP3 | Min | 0. | 0. | 207.5461 |
| 26 | 2.09332 | SLE_QP3 | Min | 0. | 0. | 206.5222 |
| 26 | 0. | SLE_QP4 | Max | 0. | 0. | -77.1974 |
| 26 | 1.04666 | SLE_QP4 | Max | 0. | 0. | 46.7529 |
| 26 | 2.09332 | SLE_QP4 | Max | 0. | 0. | 35.4149 |
| 26 | 0. | SLE_QP4 | Min | 0. | 0. | -77.1974 |
| 26 | 1.04666 | SLE_QP4 | Min | 0. | 0. | 46.7529 |
| 26 | 2.09332 | SLE_QP4 | Min | 0. | 0. | 35.4149 |
| 26 | 0. | SLV_1 | Max | 0. | 0. | -550.6879 |
| 26 | 1.04666 | SLV_1 | Max | 0. | 0. | -471.8154 |
| 26 | 2.09332 | SLV_1 | Max | 0. | 0. | -512.23 |
| 26 | 0. | SLV_1 | Min | 0. | 0. | -550.6879 |
| 26 | 1.04666 | SLV_1 | Min | 0. | 0. | -471.8154 |
| 26 | 2.09332 | SLV_1 | Min | 0. | 0. | -512.23 |
| 26 | 0. | SLV_2 | Max | 0. | 0. | -552.0608 |
| 26 | 1.04666 | SLV_2 | Max | 0. | 0. | -474.2149 |
| 26 | 2.09332 | SLV_2 | Max | 0. | 0. | -515.656 |
| 26 | 0. | SLV_2 | Min | 0. | 0. | -552.0608 |
| 26 | 1.04666 | SLV_2 | Min | 0. | 0. | -474.2149 |
| 26 | 2.09332 | SLV_2 | Min | 0. | 0. | -515.656 |
| 26 | 0. | SLV_3 | Max | 0. | 0. | -698.8776 |
| 26 | 1.04666 | SLV_3 | Max | 0. | 0. | -567.5289 |
| 26 | 2.09332 | SLV_3 | Max | 0. | 0. | -571.4686 |
| 26 | 0. | SLV_3 | Min | 0. | 0. | -698.8776 |
| 26 | 1.04666 | SLV_3 | Min | 0. | 0. | -567.5289 |
| 26 | 2.09332 | SLV_3 | Min | 0. | 0. | -571.4686 |
| 26 | 0. | SLV_4 | Max | 0. | 0. | -700.7081 |
| 26 | 1.04666 | SLV_4 | Max | 0. | 0. | -570.5875 |
| 26 | 2.09332 | SLV_4 | Max | 0. | 0. | -575.7553 |
| 26 | 0. | SLV_4 | Min | 0. | 0. | -700.7081 |
| 26 | 1.04666 | SLV_4 | Min | 0. | 0. | -570.5875 |
| 26 | 2.09332 | SLV_4 | Min | 0. | 0. | -575.7553 |
| 26 | 0. | SLD_1 | Max | 0. | 0. | -215.988 |
| 26 | 1.04666 | SLD_1 | Max | 0. | 0. | -136.4315 |
| 26 | 2.09332 | SLD_1 | Max | 0. | 0. | -176.162 |
| 26 | 0. | SLD_1 | Min | 0. | 0. | -215.988 |
| 26 | 1.04666 | SLD_1 | Min | 0. | 0. | -136.4315 |
| 26 | 2.09332 | SLD_1 | Min | 0. | 0. | -176.162 |
| 26 | 0. | SLD_2 | Max | 0. | 0. | -217.1022 |
| 26 | 1.04666 | SLD_2 | Max | 0. | 0. | -137.8602 |
| 26 | 2.09332 | SLD_2 | Max | 0. | 0. | -177.9052 |
| 26 | 0. | SLD_2 | Min | 0. | 0. | -217.1022 |
| 26 | 1.04666 | SLD_2 | Min | 0. | 0. | -137.8602 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 26 | 2.09332 | SLD_2 | Min | 0. | 0. | -177.9052 |
| 26 | 0. | SLD_3 | Max | 0. | 0. | -384.0806 |
| 26 | 1.04666 | SLD_3 | Max | 0. | 0. | -247.6544 |
| 26 | 2.09332 | SLD_3 | Max | 0. | 0. | -246.5166 |
| 26 | 0. | SLD_3 | Min | 0. | 0. | -384.0806 |
| 26 | 1.04666 | SLD_3 | Min | 0. | 0. | -247.6544 |
| 26 | 2.09332 | SLD_3 | Min | 0. | 0. | -246.5166 |
| 26 | 0. | SLD_4 | Max | 0. | 0. | -385.1293 |
| 26 | 1.04666 | SLD_4 | Max | 0. | 0. | -249.1513 |
| 26 | 2.09332 | SLD_4 | Max | 0. | 0. | -248.4617 |
| 26 | 0. | SLD_4 | Min | 0. | 0. | -385.1293 |
| 26 | 1.04666 | SLD_4 | Min | 0. | 0. | -249.1513 |
| 26 | 2.09332 | SLD_4 | Min | 0. | 0. | -248.4617 |
| 26 | 0. | SLU_IDR_1 | Max | 0. | 0. | 74.4794 |
| 26 | 1.04666 | SLU_IDR_1 | Max | 0. | 0. | 193.7032 |
| 26 | 2.09332 | SLU_IDR_1 | Max | 0. | 0. | 188.1244 |
| 26 | 0. | SLU_IDR_1 | Min | 0. | 0. | 74.4794 |
| 26 | 1.04666 | SLU_IDR_1 | Min | 0. | 0. | 193.7032 |
| 26 | 2.09332 | SLU_IDR_1 | Min | 0. | 0. | 188.1244 |
| 26 | 0. | SLU_IDR_2 | Max | 0. | 0. | 164.3001 |
| 26 | 1.04666 | SLU_IDR_2 | Max | 0. | 0. | 221.6614 |
| 26 | 2.09332 | SLU_IDR_2 | Max | 0. | 0. | 168.4726 |
| 26 | 0. | SLU_IDR_2 | Min | 0. | 0. | 164.3001 |
| 26 | 1.04666 | SLU_IDR_2 | Min | 0. | 0. | 221.6614 |
| 26 | 2.09332 | SLU_IDR_2 | Min | 0. | 0. | 168.4726 |
| 26 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -452.1016 |
| 26 | 1.04666 | SISMA WOOD SLV-1 | Max | 0. | 0. | -468.5915 |
| 26 | 2.09332 | SISMA WOOD SLV-1 | Max | 0. | 0. | -485.0814 |
| 26 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -452.1016 |
| 26 | 1.04666 | SISMA WOOD SLV-1 | Min | 0. | 0. | -468.5915 |
| 26 | 2.09332 | SISMA WOOD SLV-1 | Min | 0. | 0. | -485.0814 |
| 26 | 0. | DEAD-1 | Max | 0. | 0. | 92.8722 |
| 26 | 1.04666 | DEAD-1 | Max | 0. | 0. | 120.7619 |
| 26 | 2.09332 | DEAD-1 | Max | 0. | 0. | 121.5067 |
| 26 | 0. | DEAD-1 | Min | 0. | 0. | 92.8722 |
| 26 | 1.04666 | DEAD-1 | Min | 0. | 0. | 120.7619 |
| 26 | 2.09332 | DEAD-1 | Min | 0. | 0. | 121.5067 |
| 26 | 0. | SLU_PROVA | | 0. | 0. | 32.95 |
| 26 | 1.04666 | SLU_PROVA | | 0. | 0. | 99.8642 |
| 26 | 2.09332 | SLU_PROVA | | 0. | 0. | -23.0238 |
| 27 | 0. | DEAD | | 0. | 0. | -6.6047 |
| 27 | 0.44885 | DEAD | | 0. | 0. | -4.5917 |
| 27 | 0.8977 | DEAD | | 0. | 0. | -8.6209 |
| 27 | 0. | SIMM_KA | | 0. | 0. | 65.384 |
| 27 | 0.44885 | SIMM_KA | | 0. | 0. | 66.8508 |
| 27 | 0.8977 | SIMM_KA | | 0. | 0. | 68.3175 |
| 27 | 0. | SIMM_K0 | | 0. | 0. | 99.0541 |
| 27 | 0.44885 | SIMM_K0 | | 0. | 0. | 101.2832 |
| 27 | 0.8977 | SIMM_K0 | | 0. | 0. | 103.5122 |
| 27 | 0. | A--SIMM_KA | | 0. | 0. | 80.645 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 27 | 0.44885 | A--SIMM_KA | | 0. | 0. | 75.2978 |
| 27 | 0.8977 | A--SIMM_KA | | 0. | 0. | 69.9506 |
| 27 | 0. | A--SIMM_K0 | | 0. | 0. | 123.9988 |
| 27 | 0.44885 | A--SIMM_K0 | | 0. | 0. | 116.1422 |
| 27 | 0.8977 | A--SIMM_K0 | | 0. | 0. | 108.2857 |
| 27 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 5.2028 |
| 27 | 0.44885 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.3613 |
| 27 | 0.8977 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.5197 |
| 27 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 7.8004 |
| 27 | 0.44885 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.0379 |
| 27 | 0.8977 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.2754 |
| 27 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 7.8004 |
| 27 | 0.44885 | SIMM_SOVR_K 0 | | 0. | 0. | 8.0379 |
| 27 | 0.8977 | SIMM_SOVR_K 0 | | 0. | 0. | 8.2754 |
| 27 | 0. | SIMM_SOVR_K A | | 0. | 0. | 5.2028 |
| 27 | 0.44885 | SIMM_SOVR_K A | | 0. | 0. | 5.3613 |
| 27 | 0.8977 | SIMM_SOVR_K A | | 0. | 0. | 5.5197 |
| 27 | 0. | SOVR | | 0. | 0. | -80.0145 |
| 27 | 0.44885 | SOVR | | 0. | 0. | -79.7609 |
| 27 | 0.8977 | SOVR | | 0. | 0. | -79.5073 |
| 27 | 0. | TERR_SIMM | | 0. | 0. | -304.7004 |
| 27 | 0.44885 | TERR_SIMM | | 0. | 0. | -303.2812 |
| 27 | 0.8977 | TERR_SIMM | | 0. | 0. | -301.862 |
| 27 | 0. | TERR_A--SIMM | | 0. | 0. | -390.1751 |
| 27 | 0.44885 | TERR_A--SIMM | | 0. | 0. | -385.3054 |
| 27 | 0.8977 | TERR_A--SIMM | | 0. | 0. | -380.4356 |
| 27 | 0. | INERZIA H SLV | | 0. | 0. | 0.0095 |
| 27 | 0.44885 | INERZIA H SLV | | 0. | 0. | -0.2594 |
| 27 | 0.8977 | INERZIA H SLV | | 0. | 0. | -0.5283 |
| 27 | 0. | INERZIA V + SLV | | 0. | 0. | -0.0302 |
| 27 | 0.44885 | INERZIA V + SLV | | 0. | 0. | -0.0464 |
| 27 | 0.8977 | INERZIA V + SLV | | 0. | 0. | -0.0626 |
| 27 | 0. | INERZIA V - SLV | | 0. | 0. | 0.0302 |
| 27 | 0.44885 | INERZIA V - SLV | | 0. | 0. | 0.0464 |
| 27 | 0.8977 | INERZIA V - SLV | | 0. | 0. | 0.0626 |
| 27 | 0. | SISMA WOOD SLV | | 0. | 0. | 111.0204 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 27 | 0.44885 | SISMA WOOD SLV | | 0. | 0. | 99.1828 |
| 27 | 0.8977 | SISMA WOOD SLV | | 0. | 0. | 87.3451 |
| 27 | 0. | IDROSTATICA | | 0. | 0. | -507.3856 |
| 27 | 0.44885 | IDROSTATICA | | 0. | 0. | -507.6898 |
| 27 | 0.8977 | IDROSTATICA | | 0. | 0. | -481.5213 |
| 27 | 0. | SISMA WOOD SLD | | 0. | 0. | 49.0311 |
| 27 | 0.44885 | SISMA WOOD SLD | | 0. | 0. | 43.8031 |
| 27 | 0.8977 | SISMA WOOD SLD | | 0. | 0. | 38.5751 |
| 27 | 0. | INERZIA H SLD | | 0. | 0. | 0.0042 |
| 27 | 0.44885 | INERZIA H SLD | | 0. | 0. | -0.1146 |
| 27 | 0.8977 | INERZIA H SLD | | 0. | 0. | -0.2333 |
| 27 | 0. | INERZIA V + SLD | | 0. | 0. | -0.0133 |
| 27 | 0.44885 | INERZIA V + SLD | | 0. | 0. | -0.0205 |
| 27 | 0.8977 | INERZIA V + SLD | | 0. | 0. | -0.0276 |
| 27 | 0. | INERZIA V SLD | | 0. | 0. | 0.0133 |
| 27 | 0.44885 | INERZIA V SLD | | 0. | 0. | 0.0205 |
| 27 | 0.8977 | INERZIA V SLD | | 0. | 0. | 0.0276 |
| 27 | 0. | INERZIA V -1 | | 0. | 0. | 0.0302 |
| 27 | 0.44885 | INERZIA V -1 | | 0. | 0. | 0.0464 |
| 27 | 0.8977 | INERZIA V -1 | | 0. | 0. | 0.0626 |
| 27 | 0. | SLU_1 | Max | 0. | 0. | -1255.3622 |
| 27 | 0.44885 | SLU_1 | Max | 0. | 0. | -1242.3622 |
| 27 | 0.8977 | SLU_1 | Max | 0. | 0. | -1202.8026 |
| 27 | 0. | SLU_1 | Min | 0. | 0. | -1255.3622 |
| 27 | 0.44885 | SLU_1 | Min | 0. | 0. | -1242.3622 |
| 27 | 0.8977 | SLU_1 | Min | 0. | 0. | -1202.8026 |
| 27 | 0. | SLU_2 | Max | 0. | 0. | -1363.0651 |
| 27 | 0.44885 | SLU_2 | Max | 0. | 0. | -1349.6103 |
| 27 | 0.8977 | SLU_2 | Max | 0. | 0. | -1309.5959 |
| 27 | 0. | SLU_2 | Min | 0. | 0. | -1363.0651 |
| 27 | 0.44885 | SLU_2 | Min | 0. | 0. | -1349.6103 |
| 27 | 0.8977 | SLU_2 | Min | 0. | 0. | -1309.5959 |
| 27 | 0. | SLU_3 | Max | 0. | 0. | -1292.1245 |
| 27 | 0.44885 | SLU_3 | Max | 0. | 0. | -1299.7009 |
| 27 | 0.8977 | SLU_3 | Max | 0. | 0. | -1280.7176 |
| 27 | 0. | SLU_3 | Min | 0. | 0. | -1292.1245 |
| 27 | 0.44885 | SLU_3 | Min | 0. | 0. | -1299.7009 |
| 27 | 0.8977 | SLU_3 | Min | 0. | 0. | -1280.7176 |
| 27 | 0. | SLU_4 | Max | 0. | 0. | -1419.2001 |
| 27 | 0.44885 | SLU_4 | Max | 0. | 0. | -1420.2308 |
| 27 | 0.8977 | SLU_4 | Max | 0. | 0. | -1394.7018 |
| 27 | 0. | SLU_4 | Min | 0. | 0. | -1419.2001 |
| 27 | 0.44885 | SLU_4 | Min | 0. | 0. | -1420.2308 |
| 27 | 0.8977 | SLU_4 | Min | 0. | 0. | -1394.7018 |
| 27 | 0. | SLE_F1 | Max | 0. | 0. | -942.6813 |
| 27 | 0.44885 | SLE_F1 | Max | 0. | 0. | -932.3191 |
| 27 | 0.8977 | SLE_F1 | Max | 0. | 0. | -901.5265 |
| 27 | 0. | SLE_F1 | Min | 0. | 0. | -942.6813 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 27 | 0.44885 | SLE_F1 | Min | 0. | 0. | -932.3191 |
| 27 | 0.8977 | SLE_F1 | Min | 0. | 0. | -901.5265 |
| 27 | 0. | SLE_F2 | Max | 0. | 0. | -1024.6828 |
| 27 | 0.44885 | SLE_F2 | Max | 0. | 0. | -1014.3689 |
| 27 | 0.8977 | SLE_F2 | Max | 0. | 0. | -983.6245 |
| 27 | 0. | SLE_F2 | Min | 0. | 0. | -1024.6828 |
| 27 | 0.44885 | SLE_F2 | Min | 0. | 0. | -1014.3689 |
| 27 | 0.8977 | SLE_F2 | Min | 0. | 0. | -983.6245 |
| 27 | 0. | SLE_F3 | Max | 0. | 0. | -1065.7052 |
| 27 | 0.44885 | SLE_F3 | Max | 0. | 0. | -1066.8578 |
| 27 | 0.8977 | SLE_F3 | Max | 0. | 0. | -1047.58 |
| 27 | 0. | SLE_F3 | Min | 0. | 0. | -1065.7052 |
| 27 | 0.44885 | SLE_F3 | Min | 0. | 0. | -1066.8578 |
| 27 | 0.8977 | SLE_F3 | Min | 0. | 0. | -1047.58 |
| 27 | 0. | SLE_F4 | Max | 0. | 0. | -963.632 |
| 27 | 0.44885 | SLE_F4 | Max | 0. | 0. | -969.5353 |
| 27 | 0.8977 | SLE_F4 | Max | 0. | 0. | -955.0081 |
| 27 | 0. | SLE_F4 | Min | 0. | 0. | -963.632 |
| 27 | 0.44885 | SLE_F4 | Min | 0. | 0. | -969.5353 |
| 27 | 0.8977 | SLE_F4 | Min | 0. | 0. | -955.0081 |
| 27 | 0. | SLE_QP1 | Max | 0. | 0. | -903.8727 |
| 27 | 0.44885 | SLE_QP1 | Max | 0. | 0. | -893.5791 |
| 27 | 0.8977 | SLE_QP1 | Max | 0. | 0. | -862.855 |
| 27 | 0. | SLE_QP1 | Min | 0. | 0. | -903.8727 |
| 27 | 0.44885 | SLE_QP1 | Min | 0. | 0. | -893.5791 |
| 27 | 0.8977 | SLE_QP1 | Min | 0. | 0. | -862.855 |
| 27 | 0. | SLE_QP2 | Max | 0. | 0. | -980.4269 |
| 27 | 0.44885 | SLE_QP2 | Max | 0. | 0. | -970.1797 |
| 27 | 0.8977 | SLE_QP2 | Max | 0. | 0. | -939.5021 |
| 27 | 0. | SLE_QP2 | Min | 0. | 0. | -980.4269 |
| 27 | 0.44885 | SLE_QP2 | Min | 0. | 0. | -970.1797 |
| 27 | 0.8977 | SLE_QP2 | Min | 0. | 0. | -939.5021 |
| 27 | 0. | SLE_QP3 | Max | 0. | 0. | -1017.4417 |
| 27 | 0.44885 | SLE_QP3 | Max | 0. | 0. | -1019.2624 |
| 27 | 0.8977 | SLE_QP3 | Max | 0. | 0. | -1000.6527 |
| 27 | 0. | SLE_QP3 | Min | 0. | 0. | -1017.4417 |
| 27 | 0.44885 | SLE_QP3 | Min | 0. | 0. | -1019.2624 |
| 27 | 0.8977 | SLE_QP3 | Min | 0. | 0. | -1000.6527 |
| 27 | 0. | SLE_QP4 | Max | 0. | 0. | -906.6456 |
| 27 | 0.44885 | SLE_QP4 | Max | 0. | 0. | -912.6818 |
| 27 | 0.8977 | SLE_QP4 | Max | 0. | 0. | -898.2874 |
| 27 | 0. | SLE_QP4 | Min | 0. | 0. | -906.6456 |
| 27 | 0.44885 | SLE_QP4 | Min | 0. | 0. | -912.6818 |
| 27 | 0.8977 | SLE_QP4 | Min | 0. | 0. | -898.2874 |
| 27 | 0. | SLV_1 | Max | 0. | 0. | -474.3728 |
| 27 | 0.44885 | SLV_1 | Max | 0. | 0. | -496.9848 |
| 27 | 0.8977 | SLV_1 | Max | 0. | 0. | -499.1664 |
| 27 | 0. | SLV_1 | Min | 0. | 0. | -474.3728 |
| 27 | 0.44885 | SLV_1 | Min | 0. | 0. | -496.9848 |
| 27 | 0.8977 | SLV_1 | Min | 0. | 0. | -499.1664 |
| 27 | 0. | SLV_2 | Max | 0. | 0. | -474.1809 |
| 27 | 0.44885 | SLV_2 | Max | 0. | 0. | -496.4919 |
| 27 | 0.8977 | SLV_2 | Max | 0. | 0. | -498.3724 |
| 27 | 0. | SLV_2 | Min | 0. | 0. | -474.1809 |
| 27 | 0.44885 | SLV_2 | Min | 0. | 0. | -496.4919 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 27 | 0.8977 | SLV_2 | Min | 0. | 0. | -498.3724 |
| 27 | 0. | SLV_3 | Max | 0. | 0. | -503.8054 |
| 27 | 0.44885 | SLV_3 | Max | 0. | 0. | -538.9484 |
| 27 | 0.8977 | SLV_3 | Max | 0. | 0. | -553.6609 |
| 27 | 0. | SLV_3 | Min | 0. | 0. | -503.8054 |
| 27 | 0.44885 | SLV_3 | Min | 0. | 0. | -538.9484 |
| 27 | 0.8977 | SLV_3 | Min | 0. | 0. | -553.6609 |
| 27 | 0. | SLV_4 | Max | 0. | 0. | -502.7289 |
| 27 | 0.44885 | SLV_4 | Max | 0. | 0. | -537.7786 |
| 27 | 0.8977 | SLV_4 | Max | 0. | 0. | -552.3979 |
| 27 | 0. | SLV_4 | Min | 0. | 0. | -502.7289 |
| 27 | 0.44885 | SLV_4 | Min | 0. | 0. | -537.7786 |
| 27 | 0.8977 | SLV_4 | Min | 0. | 0. | -552.3979 |
| 27 | 0. | SLD_1 | Max | 0. | 0. | -698.073 |
| 27 | 0.44885 | SLD_1 | Max | 0. | 0. | -701.4787 |
| 27 | 0.8977 | SLD_1 | Max | 0. | 0. | -684.4539 |
| 27 | 0. | SLD_1 | Min | 0. | 0. | -698.073 |
| 27 | 0.44885 | SLD_1 | Min | 0. | 0. | -701.4787 |
| 27 | 0.8977 | SLD_1 | Min | 0. | 0. | -684.4539 |
| 27 | 0. | SLD_2 | Max | 0. | 0. | -699.8033 |
| 27 | 0.44885 | SLD_2 | Max | 0. | 0. | -702.9741 |
| 27 | 0.8977 | SLD_2 | Max | 0. | 0. | -685.7144 |
| 27 | 0. | SLD_2 | Min | 0. | 0. | -699.8033 |
| 27 | 0.44885 | SLD_2 | Min | 0. | 0. | -702.9741 |
| 27 | 0.8977 | SLD_2 | Min | 0. | 0. | -685.7144 |
| 27 | 0. | SLD_3 | Max | 0. | 0. | -687.1123 |
| 27 | 0.44885 | SLD_3 | Max | 0. | 0. | -707.1212 |
| 27 | 0.8977 | SLD_3 | Max | 0. | 0. | -706.6996 |
| 27 | 0. | SLD_3 | Min | 0. | 0. | -687.1123 |
| 27 | 0.44885 | SLD_3 | Min | 0. | 0. | -707.1212 |
| 27 | 0.8977 | SLD_3 | Min | 0. | 0. | -706.6996 |
| 27 | 0. | SLD_4 | Max | 0. | 0. | -686.9528 |
| 27 | 0.44885 | SLD_4 | Max | 0. | 0. | -706.8821 |
| 27 | 0.8977 | SLD_4 | Max | 0. | 0. | -706.381 |
| 27 | 0. | SLD_4 | Min | 0. | 0. | -686.9528 |
| 27 | 0.44885 | SLD_4 | Min | 0. | 0. | -706.8821 |
| 27 | 0.8977 | SLD_4 | Min | 0. | 0. | -706.381 |
| 27 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1133.4181 |
| 27 | 0.44885 | SLU_IDR_1 | Max | 0. | 0. | -1132.8894 |
| 27 | 0.8977 | SLU_IDR_1 | Max | 0. | 0. | -1108.6787 |
| 27 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1133.4181 |
| 27 | 0.44885 | SLU_IDR_1 | Min | 0. | 0. | -1132.8894 |
| 27 | 0.8977 | SLU_IDR_1 | Min | 0. | 0. | -1108.6787 |
| 27 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1107.6521 |
| 27 | 0.44885 | SLU_IDR_2 | Max | 0. | 0. | -1095.4416 |
| 27 | 0.8977 | SLU_IDR_2 | Max | 0. | 0. | -1059.5492 |
| 27 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1107.6521 |
| 27 | 0.44885 | SLU_IDR_2 | Min | 0. | 0. | -1095.4416 |
| 27 | 0.8977 | SLU_IDR_2 | Min | 0. | 0. | -1059.5492 |
| 27 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 532.9987 |
| 27 | 0.44885 | SISMA WOOD SLV-1 | Max | 0. | 0. | 520.4881 |
| 27 | 0.8977 | SISMA WOOD SLV-1 | Max | 0. | 0. | 507.9776 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 27 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 532.9987 |
| 27 | 0.44885 | SISMA WOOD SLV-1 | Min | 0. | 0. | 520.4881 |
| 27 | 0.8977 | SISMA WOOD SLV-1 | Min | 0. | 0. | 507.9776 |
| 27 | 0. | DEAD-1 | Max | 0. | 0. | -34.6013 |
| 27 | 0.44885 | DEAD-1 | Max | 0. | 0. | -32.5406 |
| 27 | 0.8977 | DEAD-1 | Max | 0. | 0. | -36.5222 |
| 27 | 0. | DEAD-1 | Min | 0. | 0. | -34.6013 |
| 27 | 0.44885 | DEAD-1 | Min | 0. | 0. | -32.5406 |
| 27 | 0.8977 | DEAD-1 | Min | 0. | 0. | -36.5222 |
| 27 | 0. | SLU_PROVA | | 0. | 0. | -1043.8488 |
| 27 | 0.44885 | SLU_PROVA | | 0. | 0. | -1036.1479 |
| 27 | 0.8977 | SLU_PROVA | | 0. | 0. | -1001.8875 |
| 28 | 0. | DEAD | | 0. | 0. | -8.6209 |
| 28 | 0.6275 | DEAD | | 0. | 0. | -5.9764 |
| 28 | 1.255 | DEAD | | 0. | 0. | -15.0563 |
| 28 | 0. | SIMM_KA | | 0. | 0. | 68.3175 |
| 28 | 0.6275 | SIMM_KA | | 0. | 0. | 64.3942 |
| 28 | 1.255 | SIMM_KA | | 0. | 0. | 60.4708 |
| 28 | 0. | SIMM_K0 | | 0. | 0. | 103.5122 |
| 28 | 0.6275 | SIMM_K0 | | 0. | 0. | 97.6885 |
| 28 | 1.255 | SIMM_K0 | | 0. | 0. | 91.8648 |
| 28 | 0. | A--SIMM_KA | | 0. | 0. | 69.9506 |
| 28 | 0.6275 | A--SIMM_KA | | 0. | 0. | 55.5667 |
| 28 | 1.255 | A--SIMM_KA | | 0. | 0. | 41.1827 |
| 28 | 0. | A--SIMM_K0 | | 0. | 0. | 108.2857 |
| 28 | 0.6275 | A--SIMM_K0 | | 0. | 0. | 86.5494 |
| 28 | 1.255 | A--SIMM_K0 | | 0. | 0. | 64.8131 |
| 28 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 5.5197 |
| 28 | 0.6275 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.6323 |
| 28 | 1.255 | A-- SIMM_SOVR_K A | | 0. | 0. | 5.745 |
| 28 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.2754 |
| 28 | 0.6275 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.4443 |
| 28 | 1.255 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.6132 |
| 28 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 8.2754 |
| 28 | 0.6275 | SIMM_SOVR_K 0 | | 0. | 0. | 8.4443 |
| 28 | 1.255 | SIMM_SOVR_K 0 | | 0. | 0. | 8.6132 |
| 28 | 0. | SIMM_SOVR_K A | | 0. | 0. | 5.5197 |
| 28 | 0.6275 | SIMM_SOVR_K A | | 0. | 0. | 5.6323 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 28 | 1.255 | SIMM_SOVR_K A | | 0. | 0. | 5.745 |
| 28 | 0. | SOVR | | 0. | 0. | -79.5073 |
| 28 | 0.6275 | SOVR | | 0. | 0. | -77.3858 |
| 28 | 1.255 | SOVR | | 0. | 0. | -75.2643 |
| 28 | 0. | TERR_SIMM | | 0. | 0. | -301.862 |
| 28 | 0.6275 | TERR_SIMM | | 0. | 0. | -293.164 |
| 28 | 1.255 | TERR_SIMM | | 0. | 0. | -284.466 |
| 28 | 0. | TERR_A--SIMM | | 0. | 0. | -380.4356 |
| 28 | 0.6275 | TERR_A--SIMM | | 0. | 0. | -365.892 |
| 28 | 1.255 | TERR_A--SIMM | | 0. | 0. | -351.3484 |
| 28 | 0. | INERZIA H SLV | | 0. | 0. | -0.5283 |
| 28 | 0.6275 | INERZIA H SLV | | 0. | 0. | -0.9146 |
| 28 | 1.255 | INERZIA H SLV | | 0. | 0. | -1.3008 |
| 28 | 0. | INERZIA V + SLV | | 0. | 0. | -0.0626 |
| 28 | 0.6275 | INERZIA V + SLV | | 0. | 0. | -0.1157 |
| 28 | 1.255 | INERZIA V + SLV | | 0. | 0. | -0.1689 |
| 28 | 0. | INERZIA V - SLV | | 0. | 0. | 0.0626 |
| 28 | 0.6275 | INERZIA V - SLV | | 0. | 0. | 0.1157 |
| 28 | 1.255 | INERZIA V - SLV | | 0. | 0. | 0.1689 |
| 28 | 0. | SISMA WOOD SLV | | 0. | 0. | 87.3451 |
| 28 | 0.6275 | SISMA WOOD SLV | | 0. | 0. | 50.3089 |
| 28 | 1.255 | SISMA WOOD SLV | | 0. | 0. | 13.2726 |
| 28 | 0. | iDROSTATICA | | 0. | 0. | -481.5213 |
| 28 | 0.6275 | iDROSTATICA | | 0. | 0. | -488.7897 |
| 28 | 1.255 | iDROSTATICA | | 0. | 0. | -445.9589 |
| 28 | 0. | SISMA WOOD SLD | | 0. | 0. | 38.5751 |
| 28 | 0.6275 | SISMA WOOD SLD | | 0. | 0. | 22.2184 |
| 28 | 1.255 | SISMA WOOD SLD | | 0. | 0. | 5.8617 |
| 28 | 0. | INERZIA H SLD | | 0. | 0. | -0.2333 |
| 28 | 0.6275 | INERZIA H SLD | | 0. | 0. | -0.4039 |
| 28 | 1.255 | INERZIA H SLD | | 0. | 0. | -0.5745 |
| 28 | 0. | INERZIA V + SLD | | 0. | 0. | -0.0276 |
| 28 | 0.6275 | INERZIA V + SLD | | 0. | 0. | -0.0511 |
| 28 | 1.255 | INERZIA V + SLD | | 0. | 0. | -0.0746 |
| 28 | 0. | INERZIA V SLD | | 0. | 0. | 0.0276 |
| 28 | 0.6275 | INERZIA V SLD | | 0. | 0. | 0.0511 |
| 28 | 1.255 | INERZIA V SLD | | 0. | 0. | 0.0746 |
| 28 | 0. | INERZIA V -1 | | 0. | 0. | 0.0626 |
| 28 | 0.6275 | INERZIA V -1 | | 0. | 0. | 0.1157 |
| 28 | 1.255 | INERZIA V -1 | | 0. | 0. | 0.1689 |
| 28 | 0. | SLU_1 | Max | 0. | 0. | -1202.8026 |
| 28 | 0.6275 | SLU_1 | Max | 0. | 0. | -1180.8391 |
| 28 | 1.255 | SLU_1 | Max | 0. | 0. | -1108.9884 |
| 28 | 0. | SLU_1 | Min | 0. | 0. | -1202.8026 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 28 | 0.6275 | SLU_1 | Min | 0. | 0. | -1180.8391 |
| 28 | 1.255 | SLU_1 | Min | 0. | 0. | -1108.9884 |
| 28 | 0. | SLU_2 | Max | 0. | 0. | -1309.5959 |
| 28 | 0.6275 | SLU_2 | Max | 0. | 0. | -1279.6349 |
| 28 | 1.255 | SLU_2 | Max | 0. | 0. | -1199.7867 |
| 28 | 0. | SLU_2 | Min | 0. | 0. | -1309.5959 |
| 28 | 0.6275 | SLU_2 | Min | 0. | 0. | -1279.6349 |
| 28 | 1.255 | SLU_2 | Min | 0. | 0. | -1199.7867 |
| 28 | 0. | SLU_3 | Max | 0. | 0. | -1280.7176 |
| 28 | 0.6275 | SLU_3 | Max | 0. | 0. | -1292.162 |
| 28 | 1.255 | SLU_3 | Max | 0. | 0. | -1253.7191 |
| 28 | 0. | SLU_3 | Min | 0. | 0. | -1280.7176 |
| 28 | 0.6275 | SLU_3 | Min | 0. | 0. | -1292.162 |
| 28 | 1.255 | SLU_3 | Min | 0. | 0. | -1253.7191 |
| 28 | 0. | SLU_4 | Max | 0. | 0. | -1394.7018 |
| 28 | 0.6275 | SLU_4 | Max | 0. | 0. | -1386.844 |
| 28 | 1.255 | SLU_4 | Max | 0. | 0. | -1329.0989 |
| 28 | 0. | SLU_4 | Min | 0. | 0. | -1394.7018 |
| 28 | 0.6275 | SLU_4 | Min | 0. | 0. | -1386.844 |
| 28 | 1.255 | SLU_4 | Min | 0. | 0. | -1329.0989 |
| 28 | 0. | SLE_F1 | Max | 0. | 0. | -901.5265 |
| 28 | 0.6275 | SLE_F1 | Max | 0. | 0. | -884.2708 |
| 28 | 1.255 | SLE_F1 | Max | 0. | 0. | -828.6404 |
| 28 | 0. | SLE_F1 | Min | 0. | 0. | -901.5265 |
| 28 | 0.6275 | SLE_F1 | Min | 0. | 0. | -884.2708 |
| 28 | 1.255 | SLE_F1 | Min | 0. | 0. | -828.6404 |
| 28 | 0. | SLE_F2 | Max | 0. | 0. | -983.6245 |
| 28 | 0.6275 | SLE_F2 | Max | 0. | 0. | -960.9595 |
| 28 | 1.255 | SLE_F2 | Max | 0. | 0. | -899.9197 |
| 28 | 0. | SLE_F2 | Min | 0. | 0. | -983.6245 |
| 28 | 0.6275 | SLE_F2 | Min | 0. | 0. | -960.9595 |
| 28 | 1.255 | SLE_F2 | Min | 0. | 0. | -899.9197 |
| 28 | 0. | SLE_F3 | Max | 0. | 0. | -1047.58 |
| 28 | 0.6275 | SLE_F3 | Max | 0. | 0. | -1042.3103 |
| 28 | 1.255 | SLE_F3 | Max | 0. | 0. | -998.6658 |
| 28 | 0. | SLE_F3 | Min | 0. | 0. | -1047.58 |
| 28 | 0.6275 | SLE_F3 | Min | 0. | 0. | -1042.3103 |
| 28 | 1.255 | SLE_F3 | Min | 0. | 0. | -998.6658 |
| 28 | 0. | SLE_F4 | Max | 0. | 0. | -955.0081 |
| 28 | 0.6275 | SLE_F4 | Max | 0. | 0. | -964.5233 |
| 28 | 1.255 | SLE_F4 | Max | 0. | 0. | -935.6638 |
| 28 | 0. | SLE_F4 | Min | 0. | 0. | -955.0081 |
| 28 | 0.6275 | SLE_F4 | Min | 0. | 0. | -964.5233 |
| 28 | 1.255 | SLE_F4 | Min | 0. | 0. | -935.6638 |
| 28 | 0. | SLE_QP1 | Max | 0. | 0. | -862.855 |
| 28 | 0.6275 | SLE_QP1 | Max | 0. | 0. | -846.0916 |
| 28 | 1.255 | SLE_QP1 | Max | 0. | 0. | -790.9534 |
| 28 | 0. | SLE_QP1 | Min | 0. | 0. | -862.855 |
| 28 | 0.6275 | SLE_QP1 | Min | 0. | 0. | -846.0916 |
| 28 | 1.255 | SLE_QP1 | Min | 0. | 0. | -790.9534 |
| 28 | 0. | SLE_QP2 | Max | 0. | 0. | -939.5021 |
| 28 | 0.6275 | SLE_QP2 | Max | 0. | 0. | -917.5467 |
| 28 | 1.255 | SLE_QP2 | Max | 0. | 0. | -857.2166 |
| 28 | 0. | SLE_QP2 | Min | 0. | 0. | -939.5021 |
| 28 | 0.6275 | SLE_QP2 | Min | 0. | 0. | -917.5467 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 28 | 1.255 | SLE_QP2 | Min | 0. | 0. | -857.2166 |
| 28 | 0. | SLE_QP3 | Max | 0. | 0. | -1000.6527 |
| 28 | 0.6275 | SLE_QP3 | Max | 0. | 0. | -996.8218 |
| 28 | 1.255 | SLE_QP3 | Max | 0. | 0. | -954.6161 |
| 28 | 0. | SLE_QP3 | Min | 0. | 0. | -1000.6527 |
| 28 | 0.6275 | SLE_QP3 | Min | 0. | 0. | -996.8218 |
| 28 | 1.255 | SLE_QP3 | Min | 0. | 0. | -954.6161 |
| 28 | 0. | SLE_QP4 | Max | 0. | 0. | -898.2874 |
| 28 | 0.6275 | SLE_QP4 | Max | 0. | 0. | -909.2081 |
| 28 | 1.255 | SLE_QP4 | Max | 0. | 0. | -881.754 |
| 28 | 0. | SLE_QP4 | Min | 0. | 0. | -898.2874 |
| 28 | 0.6275 | SLE_QP4 | Min | 0. | 0. | -909.2081 |
| 28 | 1.255 | SLE_QP4 | Min | 0. | 0. | -881.754 |
| 28 | 0. | SLV_1 | Max | 0. | 0. | -499.1664 |
| 28 | 0.6275 | SLV_1 | Max | 0. | 0. | -579.7862 |
| 28 | 1.255 | SLV_1 | Max | 0. | 0. | -622.0313 |
| 28 | 0. | SLV_1 | Min | 0. | 0. | -499.1664 |
| 28 | 0.6275 | SLV_1 | Min | 0. | 0. | -579.7862 |
| 28 | 1.255 | SLV_1 | Min | 0. | 0. | -622.0313 |
| 28 | 0. | SLV_2 | Max | 0. | 0. | -498.3724 |
| 28 | 0.6275 | SLV_2 | Max | 0. | 0. | -578.6391 |
| 28 | 1.255 | SLV_2 | Max | 0. | 0. | -620.531 |
| 28 | 0. | SLV_2 | Min | 0. | 0. | -498.3724 |
| 28 | 0.6275 | SLV_2 | Min | 0. | 0. | -578.6391 |
| 28 | 1.255 | SLV_2 | Min | 0. | 0. | -620.531 |
| 28 | 0. | SLV_3 | Max | 0. | 0. | -553.6609 |
| 28 | 0.6275 | SLV_3 | Max | 0. | 0. | -656.9167 |
| 28 | 1.255 | SLV_3 | Max | 0. | 0. | -721.7977 |
| 28 | 0. | SLV_3 | Min | 0. | 0. | -553.6609 |
| 28 | 0.6275 | SLV_3 | Min | 0. | 0. | -656.9167 |
| 28 | 1.255 | SLV_3 | Min | 0. | 0. | -721.7977 |
| 28 | 0. | SLV_4 | Max | 0. | 0. | -552.3979 |
| 28 | 0.6275 | SLV_4 | Max | 0. | 0. | -655.5142 |
| 28 | 1.255 | SLV_4 | Max | 0. | 0. | -720.2557 |
| 28 | 0. | SLV_4 | Min | 0. | 0. | -552.3979 |
| 28 | 0.6275 | SLV_4 | Min | 0. | 0. | -655.5142 |
| 28 | 1.255 | SLV_4 | Min | 0. | 0. | -720.2557 |
| 28 | 0. | SLD_1 | Max | 0. | 0. | -684.4539 |
| 28 | 0.6275 | SLD_1 | Max | 0. | 0. | -711.3999 |
| 28 | 1.255 | SLD_1 | Max | 0. | 0. | -699.9711 |
| 28 | 0. | SLD_1 | Min | 0. | 0. | -684.4539 |
| 28 | 0.6275 | SLD_1 | Min | 0. | 0. | -711.3999 |
| 28 | 1.255 | SLD_1 | Min | 0. | 0. | -699.9711 |
| 28 | 0. | SLD_2 | Max | 0. | 0. | -685.7144 |
| 28 | 0.6275 | SLD_2 | Max | 0. | 0. | -712.1048 |
| 28 | 1.255 | SLD_2 | Max | 0. | 0. | -700.1205 |
| 28 | 0. | SLD_2 | Min | 0. | 0. | -685.7144 |
| 28 | 0.6275 | SLD_2 | Min | 0. | 0. | -712.1048 |
| 28 | 1.255 | SLD_2 | Min | 0. | 0. | -700.1205 |
| 28 | 0. | SLD_3 | Max | 0. | 0. | -706.6996 |
| 28 | 0.6275 | SLD_3 | Max | 0. | 0. | -764.5274 |
| 28 | 1.255 | SLD_3 | Max | 0. | 0. | -783.9804 |
| 28 | 0. | SLD_3 | Min | 0. | 0. | -706.6996 |
| 28 | 0.6275 | SLD_3 | Min | 0. | 0. | -764.5274 |
| 28 | 1.255 | SLD_3 | Min | 0. | 0. | -783.9804 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 28 | 0. | SLD_4 | Max | 0. | 0. | -706.381 |
| 28 | 0.6275 | SLD_4 | Max | 0. | 0. | -764.0981 |
| 28 | 1.255 | SLD_4 | Max | 0. | 0. | -783.4403 |
| 28 | 0. | SLD_4 | Min | 0. | 0. | -706.381 |
| 28 | 0.6275 | SLD_4 | Min | 0. | 0. | -764.0981 |
| 28 | 1.255 | SLD_4 | Min | 0. | 0. | -783.4403 |
| 28 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1108.6787 |
| 28 | 0.6275 | SLU_IDR_1 | Max | 0. | 0. | -1096.9978 |
| 28 | 1.255 | SLU_IDR_1 | Max | 0. | 0. | -1040.7596 |
| 28 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1108.6787 |
| 28 | 0.6275 | SLU_IDR_1 | Min | 0. | 0. | -1096.9978 |
| 28 | 1.255 | SLU_IDR_1 | Min | 0. | 0. | -1040.7596 |
| 28 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1059.5492 |
| 28 | 0.6275 | SLU_IDR_2 | Max | 0. | 0. | -1030.8761 |
| 28 | 1.255 | SLU_IDR_2 | Max | 0. | 0. | -957.6458 |
| 28 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1059.5492 |
| 28 | 0.6275 | SLU_IDR_2 | Min | 0. | 0. | -1030.8761 |
| 28 | 1.255 | SLU_IDR_2 | Min | 0. | 0. | -957.6458 |
| 28 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 507.9776 |
| 28 | 0.6275 | SISMA WOOD SLV-1 | Max | 0. | 0. | 427.3086 |
| 28 | 1.255 | SISMA WOOD SLV-1 | Max | 0. | 0. | 346.6397 |
| 28 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 507.9776 |
| 28 | 0.6275 | SISMA WOOD SLV-1 | Min | 0. | 0. | 427.3086 |
| 28 | 1.255 | SISMA WOOD SLV-1 | Min | 0. | 0. | 346.6397 |
| 28 | 0. | DEAD-1 | Max | 0. | 0. | -36.5222 |
| 28 | 0.6275 | DEAD-1 | Max | 0. | 0. | -33.203 |
| 28 | 1.255 | DEAD-1 | Max | 0. | 0. | -41.6083 |
| 28 | 0. | DEAD-1 | Min | 0. | 0. | -36.5222 |
| 28 | 0.6275 | DEAD-1 | Min | 0. | 0. | -33.203 |
| 28 | 1.255 | DEAD-1 | Min | 0. | 0. | -41.6083 |
| 28 | 0. | SLU_PROVA | | 0. | 0. | -1001.8875 |
| 28 | 0.6275 | SLU_PROVA | | 0. | 0. | -1000.7264 |
| 28 | 1.255 | SLU_PROVA | | 0. | 0. | -949.678 |
| 29 | 0. | DEAD | | 0. | 0. | -15.0563 |
| 29 | 0.68666 | DEAD | | 0. | 0. | -15.1702 |
| 29 | 1.37332 | DEAD | | 0. | 0. | -29.3404 |
| 29 | 0. | SIMM_KA | | 0. | 0. | 60.4708 |
| 29 | 0.68666 | SIMM_KA | | 0. | 0. | 63.5605 |
| 29 | 1.37332 | SIMM_KA | | 0. | 0. | 66.6502 |
| 29 | 0. | SIMM_K0 | | 0. | 0. | 91.8648 |
| 29 | 0.68666 | SIMM_K0 | | 0. | 0. | 96.7289 |
| 29 | 1.37332 | SIMM_K0 | | 0. | 0. | 101.593 |
| 29 | 0. | A--SIMM_KA | | 0. | 0. | 41.1827 |
| 29 | 0.68666 | A--SIMM_KA | | 0. | 0. | 35.0816 |
| 29 | 1.37332 | A--SIMM_KA | | 0. | 0. | 28.9805 |
| 29 | 0. | A--SIMM_K0 | | 0. | 0. | 64.8131 |
| 29 | 0.68666 | A--SIMM_K0 | | 0. | 0. | 55.7247 |
| 29 | 1.37332 | A--SIMM_K0 | | 0. | 0. | 46.6364 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 29 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 5.745 |
| 29 | 0.68666 | A-- SIMM_SOVR_K A | | 0. | 0. | 6.631 |
| 29 | 1.37332 | A-- SIMM_SOVR_K A | | 0. | 0. | 7.517 |
| 29 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 8.6132 |
| 29 | 0.68666 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 9.9415 |
| 29 | 1.37332 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 11.2699 |
| 29 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 8.6132 |
| 29 | 0.68666 | SIMM_SOVR_K 0 | | 0. | 0. | 9.9415 |
| 29 | 1.37332 | SIMM_SOVR_K 0 | | 0. | 0. | 11.2699 |
| 29 | 0. | SIMM_SOVR_K A | | 0. | 0. | 5.745 |
| 29 | 0.68666 | SIMM_SOVR_K A | | 0. | 0. | 6.631 |
| 29 | 1.37332 | SIMM_SOVR_K A | | 0. | 0. | 7.517 |
| 29 | 0. | SOVR | | 0. | 0. | -75.2643 |
| 29 | 0.68666 | SOVR | | 0. | 0. | -70.8488 |
| 29 | 1.37332 | SOVR | | 0. | 0. | -66.4332 |
| 29 | 0. | TERR_SIMM | | 0. | 0. | -284.466 |
| 29 | 0.68666 | TERR_SIMM | | 0. | 0. | -264.607 |
| 29 | 1.37332 | TERR_SIMM | | 0. | 0. | -244.748 |
| 29 | 0. | TERR_A--SIMM | | 0. | 0. | -351.3484 |
| 29 | 0.68666 | TERR_A--SIMM | | 0. | 0. | -325.2053 |
| 29 | 1.37332 | TERR_A--SIMM | | 0. | 0. | -299.0621 |
| 29 | 0. | INERZIA H SLV | | 0. | 0. | -1.3008 |
| 29 | 0.68666 | INERZIA H SLV | | 0. | 0. | -1.5967 |
| 29 | 1.37332 | INERZIA H SLV | | 0. | 0. | -1.8925 |
| 29 | 0. | INERZIA V + SLV | | 0. | 0. | -0.1689 |
| 29 | 0.68666 | INERZIA V + SLV | | 0. | 0. | -0.2854 |
| 29 | 1.37332 | INERZIA V + SLV | | 0. | 0. | -0.4018 |
| 29 | 0. | INERZIA V - SLV | | 0. | 0. | 0.1689 |
| 29 | 0.68666 | INERZIA V - SLV | | 0. | 0. | 0.2854 |
| 29 | 1.37332 | INERZIA V - SLV | | 0. | 0. | 0.4018 |
| 29 | 0. | SISMA WOOD SLV | | 0. | 0. | 13.2726 |
| 29 | 0.68666 | SISMA WOOD SLV | | 0. | 0. | -9.7035 |
| 29 | 1.37332 | SISMA WOOD SLV | | 0. | 0. | -32.6795 |
| 29 | 0. | iDROSTATICA | | 0. | 0. | -445.9589 |
| 29 | 0.68666 | iDROSTATICA | | 0. | 0. | -394.1427 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 29 | 1.37332 | iDROSTATICA | | 0. | 0. | -284.2991 |
| 29 | 0. | SISMA WOOD SLD | | 0. | 0. | 5.8617 |
| 29 | 0.68666 | SISMA WOOD SLD | | 0. | 0. | -4.2854 |
| 29 | 1.37332 | SISMA WOOD SLD | | 0. | 0. | -14.4326 |
| 29 | 0. | INERZIA H SLD | | 0. | 0. | -0.5745 |
| 29 | 0.68666 | INERZIA H SLD | | 0. | 0. | -0.7052 |
| 29 | 1.37332 | INERZIA H SLD | | 0. | 0. | -0.8358 |
| 29 | 0. | INERZIA V + SLD | | 0. | 0. | -0.0746 |
| 29 | 0.68666 | INERZIA V + SLD | | 0. | 0. | -0.126 |
| 29 | 1.37332 | INERZIA V + SLD | | 0. | 0. | -0.1775 |
| 29 | 0. | INERZIA V SLD | | 0. | 0. | 0.0746 |
| 29 | 0.68666 | INERZIA V SLD | | 0. | 0. | 0.126 |
| 29 | 1.37332 | INERZIA V SLD | | 0. | 0. | 0.1775 |
| 29 | 0. | INERZIA V -1 | | 0. | 0. | 0.1689 |
| 29 | 0.68666 | INERZIA V -1 | | 0. | 0. | 0.2854 |
| 29 | 1.37332 | INERZIA V -1 | | 0. | 0. | 0.4018 |
| 29 | 0. | SLU_1 | Max | 0. | 0. | -1108.9884 |
| 29 | 0.68666 | SLU_1 | Max | 0. | 0. | -967.9575 |
| 29 | 1.37332 | SLU_1 | Max | 0. | 0. | -769.764 |
| 29 | 0. | SLU_1 | Min | 0. | 0. | -1108.9884 |
| 29 | 0.68666 | SLU_1 | Min | 0. | 0. | -967.9575 |
| 29 | 1.37332 | SLU_1 | Min | 0. | 0. | -769.764 |
| 29 | 0. | SLU_2 | Max | 0. | 0. | -1199.7867 |
| 29 | 0.68666 | SLU_2 | Max | 0. | 0. | -1050.7002 |
| 29 | 1.37332 | SLU_2 | Max | 0. | 0. | -844.451 |
| 29 | 0. | SLU_2 | Min | 0. | 0. | -1199.7867 |
| 29 | 0.68666 | SLU_2 | Min | 0. | 0. | -1050.7002 |
| 29 | 1.37332 | SLU_2 | Min | 0. | 0. | -844.451 |
| 29 | 0. | SLU_3 | Max | 0. | 0. | -1253.7191 |
| 29 | 0.68666 | SLU_3 | Max | 0. | 0. | -1148.8243 |
| 29 | 1.37332 | SLU_3 | Max | 0. | 0. | -986.7669 |
| 29 | 0. | SLU_3 | Min | 0. | 0. | -1253.7191 |
| 29 | 0.68666 | SLU_3 | Min | 0. | 0. | -1148.8243 |
| 29 | 1.37332 | SLU_3 | Min | 0. | 0. | -986.7669 |
| 29 | 0. | SLU_4 | Max | 0. | 0. | -1329.0989 |
| 29 | 0.68666 | SLU_4 | Max | 0. | 0. | -1204.0358 |
| 29 | 1.37332 | SLU_4 | Max | 0. | 0. | -1021.8102 |
| 29 | 0. | SLU_4 | Min | 0. | 0. | -1329.0989 |
| 29 | 0.68666 | SLU_4 | Min | 0. | 0. | -1204.0358 |
| 29 | 1.37332 | SLU_4 | Min | 0. | 0. | -1021.8102 |
| 29 | 0. | SLE_F1 | Max | 0. | 0. | -828.6404 |
| 29 | 0.68666 | SLE_F1 | Max | 0. | 0. | -719.7468 |
| 29 | 1.37332 | SLE_F1 | Max | 0. | 0. | -566.882 |
| 29 | 0. | SLE_F1 | Min | 0. | 0. | -828.6404 |
| 29 | 0.68666 | SLE_F1 | Min | 0. | 0. | -719.7468 |
| 29 | 1.37332 | SLE_F1 | Min | 0. | 0. | -566.882 |
| 29 | 0. | SLE_F2 | Max | 0. | 0. | -899.9197 |
| 29 | 0.68666 | SLE_F2 | Max | 0. | 0. | -785.6249 |
| 29 | 1.37332 | SLE_F2 | Max | 0. | 0. | -627.3589 |
| 29 | 0. | SLE_F2 | Min | 0. | 0. | -899.9197 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 29 | 0.68666 | SLE_F2 | Min | 0. | 0. | -785.6249 |
| 29 | 1.37332 | SLE_F2 | Min | 0. | 0. | -627.3589 |
| 29 | 0. | SLE_F3 | Max | 0. | 0. | -998.6658 |
| 29 | 0.68666 | SLE_F3 | Max | 0. | 0. | -903.2864 |
| 29 | 1.37332 | SLE_F3 | Max | 0. | 0. | -763.9357 |
| 29 | 0. | SLE_F3 | Min | 0. | 0. | -998.6658 |
| 29 | 0.68666 | SLE_F3 | Min | 0. | 0. | -903.2864 |
| 29 | 1.37332 | SLE_F3 | Min | 0. | 0. | -763.9357 |
| 29 | 0. | SLE_F4 | Max | 0. | 0. | -935.6638 |
| 29 | 0.68666 | SLE_F4 | Max | 0. | 0. | -855.6978 |
| 29 | 1.37332 | SLE_F4 | Max | 0. | 0. | -731.7606 |
| 29 | 0. | SLE_F4 | Min | 0. | 0. | -935.6638 |
| 29 | 0.68666 | SLE_F4 | Min | 0. | 0. | -855.6978 |
| 29 | 1.37332 | SLE_F4 | Min | 0. | 0. | -731.7606 |
| 29 | 0. | SLE_QP1 | Max | 0. | 0. | -790.9534 |
| 29 | 0.68666 | SLE_QP1 | Max | 0. | 0. | -682.5707 |
| 29 | 1.37332 | SLE_QP1 | Max | 0. | 0. | -530.2168 |
| 29 | 0. | SLE_QP1 | Min | 0. | 0. | -790.9534 |
| 29 | 0.68666 | SLE_QP1 | Min | 0. | 0. | -682.5707 |
| 29 | 1.37332 | SLE_QP1 | Min | 0. | 0. | -530.2168 |
| 29 | 0. | SLE_QP2 | Max | 0. | 0. | -857.2166 |
| 29 | 0.68666 | SLE_QP2 | Max | 0. | 0. | -743.6414 |
| 29 | 1.37332 | SLE_QP2 | Max | 0. | 0. | -586.095 |
| 29 | 0. | SLE_QP2 | Min | 0. | 0. | -857.2166 |
| 29 | 0.68666 | SLE_QP2 | Min | 0. | 0. | -743.6414 |
| 29 | 1.37332 | SLE_QP2 | Min | 0. | 0. | -586.095 |
| 29 | 0. | SLE_QP3 | Max | 0. | 0. | -954.6161 |
| 29 | 0.68666 | SLE_QP3 | Max | 0. | 0. | -860.7651 |
| 29 | 1.37332 | SLE_QP3 | Max | 0. | 0. | -722.9429 |
| 29 | 0. | SLE_QP3 | Min | 0. | 0. | -954.6161 |
| 29 | 0.68666 | SLE_QP3 | Min | 0. | 0. | -860.7651 |
| 29 | 1.37332 | SLE_QP3 | Min | 0. | 0. | -722.9429 |
| 29 | 0. | SLE_QP4 | Max | 0. | 0. | -881.754 |
| 29 | 0.68666 | SLE_QP4 | Max | 0. | 0. | -803.2117 |
| 29 | 1.37332 | SLE_QP4 | Max | 0. | 0. | -680.6981 |
| 29 | 0. | SLE_QP4 | Min | 0. | 0. | -881.754 |
| 29 | 0.68666 | SLE_QP4 | Min | 0. | 0. | -803.2117 |
| 29 | 1.37332 | SLE_QP4 | Min | 0. | 0. | -680.6981 |
| 29 | 0. | SLV_1 | Max | 0. | 0. | -622.0313 |
| 29 | 0.68666 | SLV_1 | Max | 0. | 0. | -586.9999 |
| 29 | 1.37332 | SLV_1 | Max | 0. | 0. | -507.9972 |
| 29 | 0. | SLV_1 | Min | 0. | 0. | -622.0313 |
| 29 | 0.68666 | SLV_1 | Min | 0. | 0. | -586.9999 |
| 29 | 1.37332 | SLV_1 | Min | 0. | 0. | -507.9972 |
| 29 | 0. | SLV_2 | Max | 0. | 0. | -620.531 |
| 29 | 0.68666 | SLV_2 | Max | 0. | 0. | -585.0194 |
| 29 | 1.37332 | SLV_2 | Max | 0. | 0. | -505.5365 |
| 29 | 0. | SLV_2 | Min | 0. | 0. | -620.531 |
| 29 | 0.68666 | SLV_2 | Min | 0. | 0. | -585.0194 |
| 29 | 1.37332 | SLV_2 | Min | 0. | 0. | -505.5365 |
| 29 | 0. | SLV_3 | Max | 0. | 0. | -721.7977 |
| 29 | 0.68666 | SLV_3 | Max | 0. | 0. | -700.9293 |
| 29 | 1.37332 | SLV_3 | Max | 0. | 0. | -636.0897 |
| 29 | 0. | SLV_3 | Min | 0. | 0. | -721.7977 |
| 29 | 0.68666 | SLV_3 | Min | 0. | 0. | -700.9293 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 29 | 1.37332 | SLV_3 | Min | 0. | 0. | -636.0897 |
| 29 | 0. | SLV_4 | Max | 0. | 0. | -720.2557 |
| 29 | 0.68666 | SLV_4 | Max | 0. | 0. | -699.0834 |
| 29 | 1.37332 | SLV_4 | Max | 0. | 0. | -633.9399 |
| 29 | 0. | SLV_4 | Min | 0. | 0. | -720.2557 |
| 29 | 0.68666 | SLV_4 | Min | 0. | 0. | -699.0834 |
| 29 | 1.37332 | SLV_4 | Min | 0. | 0. | -633.9399 |
| 29 | 0. | SLD_1 | Max | 0. | 0. | -699.9711 |
| 29 | 0.68666 | SLD_1 | Max | 0. | 0. | -636.1109 |
| 29 | 1.37332 | SLD_1 | Max | 0. | 0. | -528.2794 |
| 29 | 0. | SLD_1 | Min | 0. | 0. | -699.9711 |
| 29 | 0.68666 | SLD_1 | Min | 0. | 0. | -636.1109 |
| 29 | 1.37332 | SLD_1 | Min | 0. | 0. | -528.2794 |
| 29 | 0. | SLD_2 | Max | 0. | 0. | -700.1205 |
| 29 | 0.68666 | SLD_2 | Max | 0. | 0. | -635.7126 |
| 29 | 1.37332 | SLD_2 | Max | 0. | 0. | -527.3335 |
| 29 | 0. | SLD_2 | Min | 0. | 0. | -700.1205 |
| 29 | 0.68666 | SLD_2 | Min | 0. | 0. | -635.7126 |
| 29 | 1.37332 | SLD_2 | Min | 0. | 0. | -527.3335 |
| 29 | 0. | SLD_3 | Max | 0. | 0. | -783.9804 |
| 29 | 0.68666 | SLD_3 | Max | 0. | 0. | -741.3042 |
| 29 | 1.37332 | SLD_3 | Max | 0. | 0. | -654.6567 |
| 29 | 0. | SLD_3 | Min | 0. | 0. | -783.9804 |
| 29 | 0.68666 | SLD_3 | Min | 0. | 0. | -741.3042 |
| 29 | 1.37332 | SLD_3 | Min | 0. | 0. | -654.6567 |
| 29 | 0. | SLD_4 | Max | 0. | 0. | -783.4403 |
| 29 | 0.68666 | SLD_4 | Max | 0. | 0. | -740.5907 |
| 29 | 1.37332 | SLD_4 | Max | 0. | 0. | -653.7698 |
| 29 | 0. | SLD_4 | Min | 0. | 0. | -783.4403 |
| 29 | 0.68666 | SLD_4 | Min | 0. | 0. | -740.5907 |
| 29 | 1.37332 | SLD_4 | Min | 0. | 0. | -653.7698 |
| 29 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1040.7596 |
| 29 | 0.68666 | SLU_IDR_1 | Max | 0. | 0. | -924.1133 |
| 29 | 1.37332 | SLU_IDR_1 | Max | 0. | 0. | -756.2873 |
| 29 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1040.7596 |
| 29 | 0.68666 | SLU_IDR_1 | Min | 0. | 0. | -924.1133 |
| 29 | 1.37332 | SLU_IDR_1 | Min | 0. | 0. | -756.2873 |
| 29 | 0. | SLU_IDR_2 | Max | 0. | 0. | -957.6458 |
| 29 | 0.68666 | SLU_IDR_2 | Max | 0. | 0. | -822.4588 |
| 29 | 1.37332 | SLU_IDR_2 | Max | 0. | 0. | -636.0922 |
| 29 | 0. | SLU_IDR_2 | Min | 0. | 0. | -957.6458 |
| 29 | 0.68666 | SLU_IDR_2 | Min | 0. | 0. | -822.4588 |
| 29 | 1.37332 | SLU_IDR_2 | Min | 0. | 0. | -636.0922 |
| 29 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 346.6397 |
| 29 | 0.68666 | SISMA WOOD SLV-1 | Max | 0. | 0. | 280.1539 |
| 29 | 1.37332 | SISMA WOOD SLV-1 | Max | 0. | 0. | 213.6682 |
| 29 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 346.6397 |
| 29 | 0.68666 | SISMA WOOD SLV-1 | Min | 0. | 0. | 280.1539 |
| 29 | 1.37332 | SISMA WOOD SLV-1 | Min | 0. | 0. | 213.6682 |
| 29 | 0. | DEAD-1 | Max | 0. | 0. | -41.6083 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 29 | 0.68666 | DEAD-1 | Max | 0. | 0. | -40.4782 |
| 29 | 1.37332 | DEAD-1 | Max | 0. | 0. | -53.4044 |
| 29 | 0. | DEAD-1 | Min | 0. | 0. | -41.6083 |
| 29 | 0.68666 | DEAD-1 | Min | 0. | 0. | -40.4782 |
| 29 | 1.37332 | DEAD-1 | Min | 0. | 0. | -53.4044 |
| 29 | 0. | SLU_PROVA | | 0. | 0. | -949.678 |
| 29 | 0.68666 | SLU_PROVA | | 0. | 0. | -841.7092 |
| 29 | 1.37332 | SLU_PROVA | | 0. | 0. | -676.5779 |
| 30 | 0. | DEAD | | 0. | 0. | -29.3404 |
| 30 | 0.68801 | DEAD | | 0. | 0. | -32.3537 |
| 30 | 1.37601 | DEAD | | 0. | 0. | -49.4127 |
| 30 | 0. | SIMM_KA | | 0. | 0. | 66.6502 |
| 30 | 0.68801 | SIMM_KA | | 0. | 0. | 71.6471 |
| 30 | 1.37601 | SIMM_KA | | 0. | 0. | 76.644 |
| 30 | 0. | SIMM_K0 | | 0. | 0. | 101.593 |
| 30 | 0.68801 | SIMM_K0 | | 0. | 0. | 109.4273 |
| 30 | 1.37601 | SIMM_K0 | | 0. | 0. | 117.2616 |
| 30 | 0. | A--SIMM_KA | | 0. | 0. | 28.9805 |
| 30 | 0.68801 | A--SIMM_KA | | 0. | 0. | 25.8609 |
| 30 | 1.37601 | A--SIMM_KA | | 0. | 0. | 22.7414 |
| 30 | 0. | A--SIMM_K0 | | 0. | 0. | 46.6364 |
| 30 | 0.68801 | A--SIMM_K0 | | 0. | 0. | 41.9763 |
| 30 | 1.37601 | A--SIMM_K0 | | 0. | 0. | 37.3162 |
| 30 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 7.517 |
| 30 | 0.68801 | A-- SIMM_SOVR_K A | | 0. | 0. | 8.8252 |
| 30 | 1.37601 | A-- SIMM_SOVR_K A | | 0. | 0. | 10.1334 |
| 30 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 11.2699 |
| 30 | 0.68801 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 13.2312 |
| 30 | 1.37601 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 15.1925 |
| 30 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 11.2699 |
| 30 | 0.68801 | SIMM_SOVR_K 0 | | 0. | 0. | 13.2312 |
| 30 | 1.37601 | SIMM_SOVR_K 0 | | 0. | 0. | 15.1925 |
| 30 | 0. | SIMM_SOVR_K A | | 0. | 0. | 7.517 |
| 30 | 0.68801 | SIMM_SOVR_K A | | 0. | 0. | 8.8252 |
| 30 | 1.37601 | SIMM_SOVR_K A | | 0. | 0. | 10.1334 |
| 30 | 0. | SOVR | | 0. | 0. | -66.4332 |
| 30 | 0.68801 | SOVR | | 0. | 0. | -58.2622 |
| 30 | 1.37601 | SOVR | | 0. | 0. | -50.0913 |
| 30 | 0. | TERR_SIMM | | 0. | 0. | -244.748 |
| 30 | 0.68801 | TERR_SIMM | | 0. | 0. | -208.8376 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 30 | 1.37601 | TERR_SIMM | | 0. | 0. | -172.9273 |
| 30 | 0. | TERR_A--SIMM | | 0. | 0. | -299.0621 |
| 30 | 0.68801 | TERR_A--SIMM | | 0. | 0. | -257.6427 |
| 30 | 1.37601 | TERR_A--SIMM | | 0. | 0. | -216.2233 |
| 30 | 0. | INERZIA H SLV | | 0. | 0. | -1.8925 |
| 30 | 0.68801 | INERZIA H SLV | | 0. | 0. | -2.1332 |
| 30 | 1.37601 | INERZIA H SLV | | 0. | 0. | -2.3739 |
| 30 | 0. | INERZIA V + SLV | | 0. | 0. | -0.4018 |
| 30 | 0.68801 | INERZIA V + SLV | | 0. | 0. | -0.5657 |
| 30 | 1.37601 | INERZIA V + SLV | | 0. | 0. | -0.7297 |
| 30 | 0. | INERZIA V - SLV | | 0. | 0. | 0.4018 |
| 30 | 0.68801 | INERZIA V - SLV | | 0. | 0. | 0.5657 |
| 30 | 1.37601 | INERZIA V - SLV | | 0. | 0. | 0.7297 |
| 30 | 0. | SISMA WOOD SLV | | 0. | 0. | -32.6795 |
| 30 | 0.68801 | SISMA WOOD SLV | | 0. | 0. | -50.6011 |
| 30 | 1.37601 | SISMA WOOD SLV | | 0. | 0. | -68.5226 |
| 30 | 0. | IDROSTATICA | | 0. | 0. | -284.2991 |
| 30 | 0.68801 | IDROSTATICA | | 0. | 0. | -180.5214 |
| 30 | 1.37601 | IDROSTATICA | | 0. | 0. | -18.4882 |
| 30 | 0. | SISMA WOOD SLD | | 0. | 0. | -14.4326 |
| 30 | 0.68801 | SISMA WOOD SLD | | 0. | 0. | -22.3475 |
| 30 | 1.37601 | SISMA WOOD SLD | | 0. | 0. | -30.2624 |
| 30 | 0. | INERZIA H SLD | | 0. | 0. | -0.8358 |
| 30 | 0.68801 | INERZIA H SLD | | 0. | 0. | -0.9421 |
| 30 | 1.37601 | INERZIA H SLD | | 0. | 0. | -1.0484 |
| 30 | 0. | INERZIA V + SLD | | 0. | 0. | -0.1775 |
| 30 | 0.68801 | INERZIA V + SLD | | 0. | 0. | -0.2499 |
| 30 | 1.37601 | INERZIA V + SLD | | 0. | 0. | -0.3223 |
| 30 | 0. | INERZIA V SLD | | 0. | 0. | 0.1775 |
| 30 | 0.68801 | INERZIA V SLD | | 0. | 0. | 0.2499 |
| 30 | 1.37601 | INERZIA V SLD | | 0. | 0. | 0.3223 |
| 30 | 0. | INERZIA V -1 | | 0. | 0. | 0.4018 |
| 30 | 0.68801 | INERZIA V -1 | | 0. | 0. | 0.5657 |
| 30 | 1.37601 | INERZIA V -1 | | 0. | 0. | 0.7297 |
| 30 | 0. | SLU_1 | Max | 0. | 0. | -769.764 |
| 30 | 0.68801 | SLU_1 | Max | 0. | 0. | -536.3384 |
| 30 | 1.37601 | SLU_1 | Max | 0. | 0. | -245.4399 |
| 30 | 0. | SLU_1 | Min | 0. | 0. | -769.764 |
| 30 | 0.68801 | SLU_1 | Min | 0. | 0. | -536.3384 |
| 30 | 1.37601 | SLU_1 | Min | 0. | 0. | -245.4399 |
| 30 | 0. | SLU_2 | Max | 0. | 0. | -844.451 |
| 30 | 0.68801 | SLU_2 | Max | 0. | 0. | -603.7006 |
| 30 | 1.37601 | SLU_2 | Max | 0. | 0. | -305.4773 |
| 30 | 0. | SLU_2 | Min | 0. | 0. | -844.451 |
| 30 | 0.68801 | SLU_2 | Min | 0. | 0. | -603.7006 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 30 | 1.37601 | SLU_2 | Min | 0. | 0. | -305.4773 |
| 30 | 0. | SLU_3 | Max | 0. | 0. | -986.7669 |
| 30 | 0.68801 | SLU_3 | Max | 0. | 0. | -786.7181 |
| 30 | 1.37601 | SLU_3 | Max | 0. | 0. | -529.1965 |
| 30 | 0. | SLU_3 | Min | 0. | 0. | -986.7669 |
| 30 | 0.68801 | SLU_3 | Min | 0. | 0. | -786.7181 |
| 30 | 1.37601 | SLU_3 | Min | 0. | 0. | -529.1965 |
| 30 | 0. | SLU_4 | Max | 0. | 0. | -1021.8102 |
| 30 | 0.68801 | SLU_4 | Max | 0. | 0. | -805.6896 |
| 30 | 1.37601 | SLU_4 | Max | 0. | 0. | -532.0962 |
| 30 | 0. | SLU_4 | Min | 0. | 0. | -1021.8102 |
| 30 | 0.68801 | SLU_4 | Min | 0. | 0. | -805.6896 |
| 30 | 1.37601 | SLU_4 | Min | 0. | 0. | -532.0962 |
| 30 | 0. | SLE_F1 | Max | 0. | 0. | -566.882 |
| 30 | 0.68801 | SLE_F1 | Max | 0. | 0. | -389.4134 |
| 30 | 1.37601 | SLE_F1 | Max | 0. | 0. | -167.735 |
| 30 | 0. | SLE_F1 | Min | 0. | 0. | -566.882 |
| 30 | 0.68801 | SLE_F1 | Min | 0. | 0. | -389.4134 |
| 30 | 1.37601 | SLE_F1 | Min | 0. | 0. | -167.735 |
| 30 | 0. | SLE_F2 | Max | 0. | 0. | -627.3589 |
| 30 | 0.68801 | SLE_F2 | Max | 0. | 0. | -442.6654 |
| 30 | 1.37601 | SLE_F2 | Max | 0. | 0. | -213.7621 |
| 30 | 0. | SLE_F2 | Min | 0. | 0. | -627.3589 |
| 30 | 0.68801 | SLE_F2 | Min | 0. | 0. | -442.6654 |
| 30 | 1.37601 | SLE_F2 | Min | 0. | 0. | -213.7621 |
| 30 | 0. | SLE_F3 | Max | 0. | 0. | -763.9357 |
| 30 | 0.68801 | SLE_F3 | Max | 0. | 0. | -598.603 |
| 30 | 1.37601 | SLE_F3 | Max | 0. | 0. | -389.0603 |
| 30 | 0. | SLE_F3 | Min | 0. | 0. | -763.9357 |
| 30 | 0.68801 | SLE_F3 | Min | 0. | 0. | -598.603 |
| 30 | 1.37601 | SLE_F3 | Min | 0. | 0. | -389.0603 |
| 30 | 0. | SLE_F4 | Max | 0. | 0. | -731.7606 |
| 30 | 0.68801 | SLE_F4 | Max | 0. | 0. | -580.8054 |
| 30 | 1.37601 | SLE_F4 | Max | 0. | 0. | -385.6404 |
| 30 | 0. | SLE_F4 | Min | 0. | 0. | -731.7606 |
| 30 | 0.68801 | SLE_F4 | Min | 0. | 0. | -580.8054 |
| 30 | 1.37601 | SLE_F4 | Min | 0. | 0. | -385.6404 |
| 30 | 0. | SLE_QP1 | Max | 0. | 0. | -530.2168 |
| 30 | 0.68801 | SLE_QP1 | Max | 0. | 0. | -353.3886 |
| 30 | 1.37601 | SLE_QP1 | Max | 0. | 0. | -132.3505 |
| 30 | 0. | SLE_QP1 | Min | 0. | 0. | -530.2168 |
| 30 | 0.68801 | SLE_QP1 | Min | 0. | 0. | -353.3886 |
| 30 | 1.37601 | SLE_QP1 | Min | 0. | 0. | -132.3505 |
| 30 | 0. | SLE_QP2 | Max | 0. | 0. | -586.095 |
| 30 | 0.68801 | SLE_QP2 | Max | 0. | 0. | -402.3274 |
| 30 | 1.37601 | SLE_QP2 | Max | 0. | 0. | -174.3499 |
| 30 | 0. | SLE_QP2 | Min | 0. | 0. | -586.095 |
| 30 | 0.68801 | SLE_QP2 | Min | 0. | 0. | -402.3274 |
| 30 | 1.37601 | SLE_QP2 | Min | 0. | 0. | -174.3499 |
| 30 | 0. | SLE_QP3 | Max | 0. | 0. | -722.9429 |
| 30 | 0.68801 | SLE_QP3 | Max | 0. | 0. | -559.3076 |
| 30 | 1.37601 | SLE_QP3 | Max | 0. | 0. | -351.4623 |
| 30 | 0. | SLE_QP3 | Min | 0. | 0. | -722.9429 |
| 30 | 0.68801 | SLE_QP3 | Min | 0. | 0. | -559.3076 |
| 30 | 1.37601 | SLE_QP3 | Min | 0. | 0. | -351.4623 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 30 | 0. | SLE_QP4 | Max | 0. | 0. | -680.6981 |
| 30 | 0.68801 | SLE_QP4 | Max | 0. | 0. | -535.0554 |
| 30 | 1.37601 | SLE_QP4 | Max | 0. | 0. | -345.2028 |
| 30 | 0. | SLE_QP4 | Min | 0. | 0. | -680.6981 |
| 30 | 0.68801 | SLE_QP4 | Min | 0. | 0. | -535.0554 |
| 30 | 1.37601 | SLE_QP4 | Min | 0. | 0. | -345.2028 |
| 30 | 0. | SLV_1 | Max | 0. | 0. | -507.9972 |
| 30 | 0.68801 | SLV_1 | Max | 0. | 0. | -389.7048 |
| 30 | 1.37601 | SLV_1 | Max | 0. | 0. | -227.2024 |
| 30 | 0. | SLV_1 | Min | 0. | 0. | -507.9972 |
| 30 | 0.68801 | SLV_1 | Min | 0. | 0. | -389.7048 |
| 30 | 1.37601 | SLV_1 | Min | 0. | 0. | -227.2024 |
| 30 | 0. | SLV_2 | Max | 0. | 0. | -505.5365 |
| 30 | 0.68801 | SLV_2 | Max | 0. | 0. | -386.7128 |
| 30 | 1.37601 | SLV_2 | Max | 0. | 0. | -223.6793 |
| 30 | 0. | SLV_2 | Min | 0. | 0. | -505.5365 |
| 30 | 0.68801 | SLV_2 | Min | 0. | 0. | -386.7128 |
| 30 | 1.37601 | SLV_2 | Min | 0. | 0. | -223.6793 |
| 30 | 0. | SLV_3 | Max | 0. | 0. | -636.0897 |
| 30 | 0.68801 | SLV_3 | Max | 0. | 0. | -528.4067 |
| 30 | 1.37601 | SLV_3 | Max | 0. | 0. | -376.5139 |
| 30 | 0. | SLV_3 | Min | 0. | 0. | -636.0897 |
| 30 | 0.68801 | SLV_3 | Min | 0. | 0. | -528.4067 |
| 30 | 1.37601 | SLV_3 | Min | 0. | 0. | -376.5139 |
| 30 | 0. | SLV_4 | Max | 0. | 0. | -633.9399 |
| 30 | 0.68801 | SLV_4 | Max | 0. | 0. | -525.8542 |
| 30 | 1.37601 | SLV_4 | Max | 0. | 0. | -373.5587 |
| 30 | 0. | SLV_4 | Min | 0. | 0. | -633.9399 |
| 30 | 0.68801 | SLV_4 | Min | 0. | 0. | -525.8542 |
| 30 | 1.37601 | SLV_4 | Min | 0. | 0. | -373.5587 |
| 30 | 0. | SLD_1 | Max | 0. | 0. | -528.2794 |
| 30 | 0.68801 | SLD_1 | Max | 0. | 0. | -391.9785 |
| 30 | 1.37601 | SLD_1 | Max | 0. | 0. | -211.4677 |
| 30 | 0. | SLD_1 | Min | 0. | 0. | -528.2794 |
| 30 | 0.68801 | SLD_1 | Min | 0. | 0. | -391.9785 |
| 30 | 1.37601 | SLD_1 | Min | 0. | 0. | -211.4677 |
| 30 | 0. | SLD_2 | Max | 0. | 0. | -527.3335 |
| 30 | 0.68801 | SLD_2 | Max | 0. | 0. | -390.5549 |
| 30 | 1.37601 | SLD_2 | Max | 0. | 0. | -209.5665 |
| 30 | 0. | SLD_2 | Min | 0. | 0. | -527.3335 |
| 30 | 0.68801 | SLD_2 | Min | 0. | 0. | -390.5549 |
| 30 | 1.37601 | SLD_2 | Min | 0. | 0. | -209.5665 |
| 30 | 0. | SLD_3 | Max | 0. | 0. | -654.6567 |
| 30 | 0.68801 | SLD_3 | Max | 0. | 0. | -534.4748 |
| 30 | 1.37601 | SLD_3 | Max | 0. | 0. | -370.083 |
| 30 | 0. | SLD_3 | Min | 0. | 0. | -654.6567 |
| 30 | 0.68801 | SLD_3 | Min | 0. | 0. | -534.4748 |
| 30 | 1.37601 | SLD_3 | Min | 0. | 0. | -370.083 |
| 30 | 0. | SLD_4 | Max | 0. | 0. | -653.7698 |
| 30 | 0.68801 | SLD_4 | Max | 0. | 0. | -533.383 |
| 30 | 1.37601 | SLD_4 | Max | 0. | 0. | -368.7863 |
| 30 | 0. | SLD_4 | Min | 0. | 0. | -653.7698 |
| 30 | 0.68801 | SLD_4 | Min | 0. | 0. | -533.383 |
| 30 | 1.37601 | SLD_4 | Min | 0. | 0. | -368.7863 |
| 30 | 0. | SLU_IDR_1 | Max | 0. | 0. | -756.2873 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 30 | 0.68801 | SLU_IDR_1 | Max | 0. | 0. | -557.218 |
| 30 | 1.37601 | SLU_IDR_1 | Max | 0. | 0. | -306.7088 |
| 30 | 0. | SLU_IDR_1 | Min | 0. | 0. | -756.2873 |
| 30 | 0.68801 | SLU_IDR_1 | Min | 0. | 0. | -557.218 |
| 30 | 1.37601 | SLU_IDR_1 | Min | 0. | 0. | -306.7088 |
| 30 | 0. | SLU_IDR_2 | Max | 0. | 0. | -636.0922 |
| 30 | 0.68801 | SLU_IDR_2 | Max | 0. | 0. | -418.2715 |
| 30 | 1.37601 | SLU_IDR_2 | Max | 0. | 0. | -149.0108 |
| 30 | 0. | SLU_IDR_2 | Min | 0. | 0. | -636.0922 |
| 30 | 0.68801 | SLU_IDR_2 | Min | 0. | 0. | -418.2715 |
| 30 | 1.37601 | SLU_IDR_2 | Min | 0. | 0. | -149.0108 |
| 30 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 213.6682 |
| 30 | 0.68801 | SISMA WOOD SLV-1 | Max | 0. | 0. | 147.3682 |
| 30 | 1.37601 | SISMA WOOD SLV-1 | Max | 0. | 0. | 81.0683 |
| 30 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 213.6682 |
| 30 | 0.68801 | SISMA WOOD SLV-1 | Min | 0. | 0. | 147.3682 |
| 30 | 1.37601 | SISMA WOOD SLV-1 | Min | 0. | 0. | 81.0683 |
| 30 | 0. | DEAD-1 | Max | 0. | 0. | -53.4044 |
| 30 | 0.68801 | DEAD-1 | Max | 0. | 0. | -54.0301 |
| 30 | 1.37601 | DEAD-1 | Max | 0. | 0. | -68.7014 |
| 30 | 0. | DEAD-1 | Min | 0. | 0. | -53.4044 |
| 30 | 0.68801 | DEAD-1 | Min | 0. | 0. | -54.0301 |
| 30 | 1.37601 | DEAD-1 | Min | 0. | 0. | -68.7014 |
| 30 | 0. | SLU_PROVA | | 0. | 0. | -676.5779 |
| 30 | 0.68801 | SLU_PROVA | | 0. | 0. | -473.5176 |
| 30 | 1.37601 | SLU_PROVA | | 0. | 0. | -212.9846 |
| 31 | 0. | DEAD | | 0. | 0. | -49.4127 |
| 31 | 0.94153 | DEAD | | 0. | 0. | -52.4754 |
| 31 | 1.88306 | DEAD | | 0. | 0. | -81.3543 |
| 31 | 0. | SIMM_KA | | 0. | 0. | 76.644 |
| 31 | 0.94153 | SIMM_KA | | 0. | 0. | 76.6016 |
| 31 | 1.88306 | SIMM_KA | | 0. | 0. | 76.5591 |
| 31 | 0. | SIMM_K0 | | 0. | 0. | 117.2616 |
| 31 | 0.94153 | SIMM_K0 | | 0. | 0. | 117.7173 |
| 31 | 1.88306 | SIMM_K0 | | 0. | 0. | 118.1731 |
| 31 | 0. | A--SIMM_KA | | 0. | 0. | 22.7414 |
| 31 | 0.94153 | A--SIMM_KA | | 0. | 0. | 12.8665 |
| 31 | 1.88306 | A--SIMM_KA | | 0. | 0. | 2.9916 |
| 31 | 0. | A--SIMM_K0 | | 0. | 0. | 37.3162 |
| 31 | 0.94153 | A--SIMM_K0 | | 0. | 0. | 21.8899 |
| 31 | 1.88306 | A--SIMM_K0 | | 0. | 0. | 6.4637 |
| 31 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 10.1334 |
| 31 | 0.94153 | A-- SIMM_SOVR_K A | | 0. | 0. | 11.9018 |
| 31 | 1.88306 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.6702 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 31 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 15.1925 |
| 31 | 0.94153 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 17.8438 |
| 31 | 1.88306 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.4951 |
| 31 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 15.1925 |
| 31 | 0.94153 | SIMM_SOVR_K 0 | | 0. | 0. | 17.8438 |
| 31 | 1.88306 | SIMM_SOVR_K 0 | | 0. | 0. | 20.4951 |
| 31 | 0. | SIMM_SOVR_K A | | 0. | 0. | 10.1334 |
| 31 | 0.94153 | SIMM_SOVR_K A | | 0. | 0. | 11.9018 |
| 31 | 1.88306 | SIMM_SOVR_K A | | 0. | 0. | 13.6702 |
| 31 | 0. | SOVR | | 0. | 0. | -50.0913 |
| 31 | 0.94153 | SOVR | | 0. | 0. | -29.646 |
| 31 | 1.88306 | SOVR | | 0. | 0. | -9.2007 |
| 31 | 0. | TERR_SIMM | | 0. | 0. | -172.9273 |
| 31 | 0.94153 | TERR_SIMM | | 0. | 0. | -86.9902 |
| 31 | 1.88306 | TERR_SIMM | | 0. | 0. | -1.0531 |
| 31 | 0. | TERR_A--SIMM | | 0. | 0. | -216.2233 |
| 31 | 0.94153 | TERR_A--SIMM | | 0. | 0. | -124.1345 |
| 31 | 1.88306 | TERR_A--SIMM | | 0. | 0. | -32.0457 |
| 31 | 0. | INERZIA H SLV | | 0. | 0. | -2.3739 |
| 31 | 0.94153 | INERZIA H SLV | | 0. | 0. | -2.7353 |
| 31 | 1.88306 | INERZIA H SLV | | 0. | 0. | -3.0966 |
| 31 | 0. | INERZIA V + SLV | | 0. | 0. | -0.7297 |
| 31 | 0.94153 | INERZIA V + SLV | | 0. | 0. | -0.9928 |
| 31 | 1.88306 | INERZIA V + SLV | | 0. | 0. | -1.2559 |
| 31 | 0. | INERZIA V - SLV | | 0. | 0. | 0.7297 |
| 31 | 0.94153 | INERZIA V - SLV | | 0. | 0. | 0.9928 |
| 31 | 1.88306 | INERZIA V - SLV | | 0. | 0. | 1.2559 |
| 31 | 0. | SISMA WOOD SLV | | 0. | 0. | -68.5226 |
| 31 | 0.94153 | SISMA WOOD SLV | | 0. | 0. | -98.1763 |
| 31 | 1.88306 | SISMA WOOD SLV | | 0. | 0. | -127.8301 |
| 31 | 0. | iDROSTATICA | | 0. | 0. | -18.4882 |
| 31 | 0.94153 | iDROSTATICA | | 0. | 0. | 180.5278 |
| 31 | 1.88306 | iDROSTATICA | | 0. | 0. | 488.6426 |
| 31 | 0. | SISMA WOOD SLD | | 0. | 0. | -30.2624 |
| 31 | 0.94153 | SISMA WOOD SLD | | 0. | 0. | -43.3586 |
| 31 | 1.88306 | SISMA WOOD SLD | | 0. | 0. | -56.4549 |
| 31 | 0. | INERZIA H SLD | | 0. | 0. | -1.0484 |
| 31 | 0.94153 | INERZIA H SLD | | 0. | 0. | -1.208 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 31 | 1.88306 | INERZIA H SLD | | 0. | 0. | -1.3676 |
| 31 | 0. | INERZIA V + SLD | | 0. | 0. | -0.3223 |
| 31 | 0.94153 | INERZIA V + SLD | | 0. | 0. | -0.4384 |
| 31 | 1.88306 | INERZIA V + SLD | | 0. | 0. | -0.5546 |
| 31 | 0. | INERZIA V SLD | | 0. | 0. | 0.3223 |
| 31 | 0.94153 | INERZIA V SLD | | 0. | 0. | 0.4384 |
| 31 | 1.88306 | INERZIA V SLD | | 0. | 0. | 0.5546 |
| 31 | 0. | INERZIA V -1 | | 0. | 0. | 0.7297 |
| 31 | 0.94153 | INERZIA V -1 | | 0. | 0. | 0.9928 |
| 31 | 1.88306 | INERZIA V -1 | | 0. | 0. | 1.2559 |
| 31 | 0. | SLU_1 | Max | 0. | 0. | -245.4399 |
| 31 | 0.94153 | SLU_1 | Max | 0. | 0. | 198.9799 |
| 31 | 1.88306 | SLU_1 | Max | 0. | 0. | 751.6673 |
| 31 | 0. | SLU_1 | Min | 0. | 0. | -245.4399 |
| 31 | 0.94153 | SLU_1 | Min | 0. | 0. | 198.9799 |
| 31 | 1.88306 | SLU_1 | Min | 0. | 0. | 751.6673 |
| 31 | 0. | SLU_2 | Max | 0. | 0. | -305.4773 |
| 31 | 0.94153 | SLU_2 | Max | 0. | 0. | 148.9858 |
| 31 | 1.88306 | SLU_2 | Max | 0. | 0. | 711.7164 |
| 31 | 0. | SLU_2 | Min | 0. | 0. | -305.4773 |
| 31 | 0.94153 | SLU_2 | Min | 0. | 0. | 148.9858 |
| 31 | 1.88306 | SLU_2 | Min | 0. | 0. | 711.7164 |
| 31 | 0. | SLU_3 | Max | 0. | 0. | -529.1965 |
| 31 | 0.94153 | SLU_3 | Max | 0. | 0. | -127.9061 |
| 31 | 1.88306 | SLU_3 | Max | 0. | 0. | 381.6518 |
| 31 | 0. | SLU_3 | Min | 0. | 0. | -529.1965 |
| 31 | 0.94153 | SLU_3 | Min | 0. | 0. | -127.9061 |
| 31 | 1.88306 | SLU_3 | Min | 0. | 0. | 381.6518 |
| 31 | 0. | SLU_4 | Max | 0. | 0. | -532.0962 |
| 31 | 0.94153 | SLU_4 | Max | 0. | 0. | -107.4666 |
| 31 | 1.88306 | SLU_4 | Max | 0. | 0. | 425.4304 |
| 31 | 0. | SLU_4 | Min | 0. | 0. | -532.0962 |
| 31 | 0.94153 | SLU_4 | Min | 0. | 0. | -107.4666 |
| 31 | 1.88306 | SLU_4 | Min | 0. | 0. | 425.4304 |
| 31 | 0. | SLE_F1 | Max | 0. | 0. | -167.735 |
| 31 | 0.94153 | SLE_F1 | Max | 0. | 0. | 165.9992 |
| 31 | 1.88306 | SLE_F1 | Max | 0. | 0. | 583.0161 |
| 31 | 0. | SLE_F1 | Min | 0. | 0. | -167.735 |
| 31 | 0.94153 | SLE_F1 | Min | 0. | 0. | 165.9992 |
| 31 | 1.88306 | SLE_F1 | Min | 0. | 0. | 583.0161 |
| 31 | 0. | SLE_F2 | Max | 0. | 0. | -213.7621 |
| 31 | 0.94153 | SLE_F2 | Max | 0. | 0. | 129.4936 |
| 31 | 1.88306 | SLE_F2 | Max | 0. | 0. | 556.032 |
| 31 | 0. | SLE_F2 | Min | 0. | 0. | -213.7621 |
| 31 | 0.94153 | SLE_F2 | Min | 0. | 0. | 129.4936 |
| 31 | 1.88306 | SLE_F2 | Min | 0. | 0. | 556.032 |
| 31 | 0. | SLE_F3 | Max | 0. | 0. | -389.0603 |
| 31 | 0.94153 | SLE_F3 | Max | 0. | 0. | -69.0525 |
| 31 | 1.88306 | SLE_F3 | Max | 0. | 0. | 334.2381 |
| 31 | 0. | SLE_F3 | Min | 0. | 0. | -389.0603 |
| 31 | 0.94153 | SLE_F3 | Min | 0. | 0. | -69.0525 |
| 31 | 1.88306 | SLE_F3 | Min | 0. | 0. | 334.2381 |
| 31 | 0. | SLE_F4 | Max | 0. | 0. | -385.6404 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 31 | 0.94153 | SLE_F4 | Max | 0. | 0. | -85.8953 |
| 31 | 1.88306 | SLE_F4 | Max | 0. | 0. | 297.1324 |
| 31 | 0. | SLE_F4 | Min | 0. | 0. | -385.6404 |
| 31 | 0.94153 | SLE_F4 | Min | 0. | 0. | -85.8953 |
| 31 | 1.88306 | SLE_F4 | Min | 0. | 0. | 297.1324 |
| 31 | 0. | SLE_QP1 | Max | 0. | 0. | -132.3505 |
| 31 | 0.94153 | SLE_QP1 | Max | 0. | 0. | 189.7448 |
| 31 | 1.88306 | SLE_QP1 | Max | 0. | 0. | 595.1228 |
| 31 | 0. | SLE_QP1 | Min | 0. | 0. | -132.3505 |
| 31 | 0.94153 | SLE_QP1 | Min | 0. | 0. | 189.7448 |
| 31 | 1.88306 | SLE_QP1 | Min | 0. | 0. | 595.1228 |
| 31 | 0. | SLE_QP2 | Max | 0. | 0. | -174.3499 |
| 31 | 0.94153 | SLE_QP2 | Max | 0. | 0. | 157.1493 |
| 31 | 1.88306 | SLE_QP2 | Max | 0. | 0. | 571.9312 |
| 31 | 0. | SLE_QP2 | Min | 0. | 0. | -174.3499 |
| 31 | 0.94153 | SLE_QP2 | Min | 0. | 0. | 157.1493 |
| 31 | 1.88306 | SLE_QP2 | Min | 0. | 0. | 571.9312 |
| 31 | 0. | SLE_QP3 | Max | 0. | 0. | -351.4623 |
| 31 | 0.94153 | SLE_QP3 | Max | 0. | 0. | -43.768 |
| 31 | 1.88306 | SLE_QP3 | Max | 0. | 0. | 347.209 |
| 31 | 0. | SLE_QP3 | Min | 0. | 0. | -351.4623 |
| 31 | 0.94153 | SLE_QP3 | Min | 0. | 0. | -43.768 |
| 31 | 1.88306 | SLE_QP3 | Min | 0. | 0. | 347.209 |
| 31 | 0. | SLE_QP4 | Max | 0. | 0. | -345.2028 |
| 31 | 0.94153 | SLE_QP4 | Max | 0. | 0. | -61.8846 |
| 31 | 1.88306 | SLE_QP4 | Max | 0. | 0. | 304.7163 |
| 31 | 0. | SLE_QP4 | Min | 0. | 0. | -345.2028 |
| 31 | 0.94153 | SLE_QP4 | Min | 0. | 0. | -61.8846 |
| 31 | 1.88306 | SLE_QP4 | Min | 0. | 0. | 304.7163 |
| 31 | 0. | SLV_1 | Max | 0. | 0. | -227.2024 |
| 31 | 0.94153 | SLV_1 | Max | 0. | 0. | 10.1603 |
| 31 | 1.88306 | SLV_1 | Max | 0. | 0. | 330.8057 |
| 31 | 0. | SLV_1 | Min | 0. | 0. | -227.2024 |
| 31 | 0.94153 | SLV_1 | Min | 0. | 0. | 10.1603 |
| 31 | 1.88306 | SLV_1 | Min | 0. | 0. | 330.8057 |
| 31 | 0. | SLV_2 | Max | 0. | 0. | -223.6793 |
| 31 | 0.94153 | SLV_2 | Max | 0. | 0. | 14.3764 |
| 31 | 1.88306 | SLV_2 | Max | 0. | 0. | 335.7147 |
| 31 | 0. | SLV_2 | Min | 0. | 0. | -223.6793 |
| 31 | 0.94153 | SLV_2 | Min | 0. | 0. | 14.3764 |
| 31 | 1.88306 | SLV_2 | Min | 0. | 0. | 335.7147 |
| 31 | 0. | SLV_3 | Max | 0. | 0. | -376.5139 |
| 31 | 0.94153 | SLV_3 | Max | 0. | 0. | -154.208 |
| 31 | 1.88306 | SLV_3 | Max | 0. | 0. | 151.3806 |
| 31 | 0. | SLV_3 | Min | 0. | 0. | -376.5139 |
| 31 | 0.94153 | SLV_3 | Min | 0. | 0. | -154.208 |
| 31 | 1.88306 | SLV_3 | Min | 0. | 0. | 151.3806 |
| 31 | 0. | SLV_4 | Max | 0. | 0. | -373.5587 |
| 31 | 0.94153 | SLV_4 | Max | 0. | 0. | -150.6761 |
| 31 | 1.88306 | SLV_4 | Max | 0. | 0. | 155.4892 |
| 31 | 0. | SLV_4 | Min | 0. | 0. | -373.5587 |
| 31 | 0.94153 | SLV_4 | Min | 0. | 0. | -150.6761 |
| 31 | 1.88306 | SLV_4 | Min | 0. | 0. | 155.4892 |
| 31 | 0. | SLD_1 | Max | 0. | 0. | -211.4677 |
| 31 | 0.94153 | SLD_1 | Max | 0. | 0. | 55.8879 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 31 | 1.88306 | SLD_1 | Max | 0. | 0. | 406.5261 |
| 31 | 0. | SLD_1 | Min | 0. | 0. | -211.4677 |
| 31 | 0.94153 | SLD_1 | Min | 0. | 0. | 55.8879 |
| 31 | 1.88306 | SLD_1 | Min | 0. | 0. | 406.5261 |
| 31 | 0. | SLD_2 | Max | 0. | 0. | -209.5665 |
| 31 | 0.94153 | SLD_2 | Max | 0. | 0. | 58.2977 |
| 31 | 1.88306 | SLD_2 | Max | 0. | 0. | 409.4445 |
| 31 | 0. | SLD_2 | Min | 0. | 0. | -209.5665 |
| 31 | 0.94153 | SLD_2 | Min | 0. | 0. | 58.2977 |
| 31 | 1.88306 | SLD_2 | Min | 0. | 0. | 409.4445 |
| 31 | 0. | SLD_3 | Max | 0. | 0. | -370.083 |
| 31 | 0.94153 | SLD_3 | Max | 0. | 0. | -123.6939 |
| 31 | 1.88306 | SLD_3 | Max | 0. | 0. | 205.9778 |
| 31 | 0. | SLD_3 | Min | 0. | 0. | -370.083 |
| 31 | 0.94153 | SLD_3 | Min | 0. | 0. | -123.6939 |
| 31 | 1.88306 | SLD_3 | Min | 0. | 0. | 205.9778 |
| 31 | 0. | SLD_4 | Max | 0. | 0. | -368.7863 |
| 31 | 0.94153 | SLD_4 | Max | 0. | 0. | -122.1211 |
| 31 | 1.88306 | SLD_4 | Max | 0. | 0. | 207.8268 |
| 31 | 0. | SLD_4 | Min | 0. | 0. | -368.7863 |
| 31 | 0.94153 | SLD_4 | Min | 0. | 0. | -122.1211 |
| 31 | 1.88306 | SLD_4 | Min | 0. | 0. | 207.8268 |
| 31 | 0. | SLU_IDR_1 | Max | 0. | 0. | -306.7088 |
| 31 | 0.94153 | SLU_IDR_1 | Max | 0. | 0. | 44.8398 |
| 31 | 1.88306 | SLU_IDR_1 | Max | 0. | 0. | 493.1626 |
| 31 | 0. | SLU_IDR_1 | Min | 0. | 0. | -306.7088 |
| 31 | 0.94153 | SLU_IDR_1 | Min | 0. | 0. | 44.8398 |
| 31 | 1.88306 | SLU_IDR_1 | Min | 0. | 0. | 493.1626 |
| 31 | 0. | SLU_IDR_2 | Max | 0. | 0. | -149.0108 |
| 31 | 0.94153 | SLU_IDR_2 | Max | 0. | 0. | 228.6668 |
| 31 | 1.88306 | SLU_IDR_2 | Max | 0. | 0. | 703.1186 |
| 31 | 0. | SLU_IDR_2 | Min | 0. | 0. | -149.0108 |
| 31 | 0.94153 | SLU_IDR_2 | Min | 0. | 0. | 228.6668 |
| 31 | 1.88306 | SLU_IDR_2 | Min | 0. | 0. | 703.1186 |
| 31 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 81.0683 |
| 31 | 0.94153 | SISMA WOOD SLV-1 | Max | 0. | 0. | -31.5745 |
| 31 | 1.88306 | SISMA WOOD SLV-1 | Max | 0. | 0. | -144.2173 |
| 31 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 81.0683 |
| 31 | 0.94153 | SISMA WOOD SLV-1 | Min | 0. | 0. | -31.5745 |
| 31 | 1.88306 | SISMA WOOD SLV-1 | Min | 0. | 0. | -144.2173 |
| 31 | 0. | DEAD-1 | Max | 0. | 0. | -68.7014 |
| 31 | 0.94153 | DEAD-1 | Max | 0. | 0. | -65.4099 |
| 31 | 1.88306 | DEAD-1 | Max | 0. | 0. | -87.9346 |
| 31 | 0. | DEAD-1 | Min | 0. | 0. | -68.7014 |
| 31 | 0.94153 | DEAD-1 | Min | 0. | 0. | -65.4099 |
| 31 | 1.88306 | DEAD-1 | Min | 0. | 0. | -87.9346 |
| 31 | 0. | SLU_PROVA | | 0. | 0. | -212.9846 |
| 31 | 0.94153 | SLU_PROVA | | 0. | 0. | 188.7101 |
| 31 | 1.88306 | SLU_PROVA | | 0. | 0. | 698.6724 |
| 34 | 0. | DEAD | | 0. | 0. | -81.3543 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 34 | 0.28669 | DEAD | | 0. | 0. | -83.3029 |
| 34 | 0.57337 | DEAD | | 0. | 0. | -87.4879 |
| 34 | 0. | SIMM_KA | | 0. | 0. | 76.5591 |
| 34 | 0.28669 | SIMM_KA | | 0. | 0. | 68.6927 |
| 34 | 0.57337 | SIMM_KA | | 0. | 0. | 60.8264 |
| 34 | 0. | SIMM_K0 | | 0. | 0. | 118.1731 |
| 34 | 0.28669 | SIMM_K0 | | 0. | 0. | 106.4654 |
| 34 | 0.57337 | SIMM_K0 | | 0. | 0. | 94.7578 |
| 34 | 0. | A--SIMM_KA | | 0. | 0. | 2.9916 |
| 34 | 0.28669 | A--SIMM_KA | | 0. | 0. | -8.0583 |
| 34 | 0.57337 | A--SIMM_KA | | 0. | 0. | -19.1082 |
| 34 | 0. | A--SIMM_K0 | | 0. | 0. | 6.4637 |
| 34 | 0.28669 | A--SIMM_K0 | | 0. | 0. | -10.7694 |
| 34 | 0.57337 | A--SIMM_K0 | | 0. | 0. | -28.0026 |
| 34 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 13.6702 |
| 34 | 0.28669 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.7507 |
| 34 | 0.57337 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.8312 |
| 34 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.4951 |
| 34 | 0.28669 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.6158 |
| 34 | 0.57337 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.7364 |
| 34 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 20.4951 |
| 34 | 0.28669 | SIMM_SOVR_K 0 | | 0. | 0. | 20.6158 |
| 34 | 0.57337 | SIMM_SOVR_K 0 | | 0. | 0. | 20.7364 |
| 34 | 0. | SIMM_SOVR_K A | | 0. | 0. | 13.6702 |
| 34 | 0.28669 | SIMM_SOVR_K A | | 0. | 0. | 13.7507 |
| 34 | 0.57337 | SIMM_SOVR_K A | | 0. | 0. | 13.8312 |
| 34 | 0. | SOVR | | 0. | 0. | -9.2007 |
| 34 | 0.28669 | SOVR | | 0. | 0. | 0.2986 |
| 34 | 0.57337 | SOVR | | 0. | 0. | 9.7979 |
| 34 | 0. | TERR_SIMM | | 0. | 0. | -1.0531 |
| 34 | 0.28669 | TERR_SIMM | | 0. | 0. | 36.9282 |
| 34 | 0.57337 | TERR_SIMM | | 0. | 0. | 74.9094 |
| 34 | 0. | TERR_A--SIMM | | 0. | 0. | -32.0457 |
| 34 | 0.28669 | TERR_A--SIMM | | 0. | 0. | 7.6558 |
| 34 | 0.57337 | TERR_A--SIMM | | 0. | 0. | 47.3574 |
| 34 | 0. | INERZIA H SLV | | 0. | 0. | -3.0966 |
| 34 | 0.28669 | INERZIA H SLV | | 0. | 0. | -3.4138 |
| 34 | 0.57337 | INERZIA H SLV | | 0. | 0. | -3.731 |
| 34 | 0. | INERZIA V + SLV | | 0. | 0. | -1.2559 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 34 | 0.28669 | INERZIA V + SLV | | 0. | 0. | -1.3081 |
| 34 | 0.57337 | INERZIA V + SLV | | 0. | 0. | -1.3604 |
| 34 | 0. | INERZIA V - SLV | | 0. | 0. | 1.2559 |
| 34 | 0.28669 | INERZIA V - SLV | | 0. | 0. | 1.3081 |
| 34 | 0.57337 | INERZIA V - SLV | | 0. | 0. | 1.3604 |
| 34 | 0. | SISMA WOOD SLV | | 0. | 0. | -127.8301 |
| 34 | 0.28669 | SISMA WOOD SLV | | 0. | 0. | -149.6314 |
| 34 | 0.57337 | SISMA WOOD SLV | | 0. | 0. | -171.4327 |
| 34 | 0. | iDROSTATICA | | 0. | 0. | 488.6426 |
| 34 | 0.28669 | iDROSTATICA | | 0. | 0. | 559.7927 |
| 34 | 0.57337 | iDROSTATICA | | 0. | 0. | 641.0578 |
| 34 | 0. | SISMA WOOD SLD | | 0. | 0. | -56.4549 |
| 34 | 0.28669 | SISMA WOOD SLD | | 0. | 0. | -66.0833 |
| 34 | 0.57337 | SISMA WOOD SLD | | 0. | 0. | -75.7116 |
| 34 | 0. | INERZIA H SLD | | 0. | 0. | -1.3676 |
| 34 | 0.28669 | INERZIA H SLD | | 0. | 0. | -1.5077 |
| 34 | 0.57337 | INERZIA H SLD | | 0. | 0. | -1.6477 |
| 34 | 0. | INERZIA V + SLD | | 0. | 0. | -0.5546 |
| 34 | 0.28669 | INERZIA V + SLD | | 0. | 0. | -0.5777 |
| 34 | 0.57337 | INERZIA V + SLD | | 0. | 0. | -0.6008 |
| 34 | 0. | INERZIA V SLD | | 0. | 0. | 0.5546 |
| 34 | 0.28669 | INERZIA V SLD | | 0. | 0. | 0.5777 |
| 34 | 0.57337 | INERZIA V SLD | | 0. | 0. | 0.6008 |
| 34 | 0. | INERZIA V -1 | | 0. | 0. | 1.2559 |
| 34 | 0.28669 | INERZIA V -1 | | 0. | 0. | 1.3081 |
| 34 | 0.57337 | INERZIA V -1 | | 0. | 0. | 1.3604 |
| 34 | 0. | SLU_1 | Max | 0. | 0. | 751.6673 |
| 34 | 0.28669 | SLU_1 | Max | 0. | 0. | 904.835 |
| 34 | 0.57337 | SLU_1 | Max | 0. | 0. | 1068.2448 |
| 34 | 0. | SLU_1 | Min | 0. | 0. | 751.6673 |
| 34 | 0.28669 | SLU_1 | Min | 0. | 0. | 904.835 |
| 34 | 0.57337 | SLU_1 | Min | 0. | 0. | 1068.2448 |
| 34 | 0. | SLU_2 | Max | 0. | 0. | 711.7164 |
| 34 | 0.28669 | SLU_2 | Max | 0. | 0. | 872.6493 |
| 34 | 0.57337 | SLU_2 | Max | 0. | 0. | 1043.8241 |
| 34 | 0. | SLU_2 | Min | 0. | 0. | 711.7164 |
| 34 | 0.28669 | SLU_2 | Min | 0. | 0. | 872.6493 |
| 34 | 0.57337 | SLU_2 | Min | 0. | 0. | 1043.8241 |
| 34 | 0. | SLU_3 | Max | 0. | 0. | 381.6518 |
| 34 | 0.28669 | SLU_3 | Max | 0. | 0. | 522.0922 |
| 34 | 0.57337 | SLU_3 | Max | 0. | 0. | 672.7746 |
| 34 | 0. | SLU_3 | Min | 0. | 0. | 381.6518 |
| 34 | 0.28669 | SLU_3 | Min | 0. | 0. | 522.0922 |
| 34 | 0.57337 | SLU_3 | Min | 0. | 0. | 672.7746 |
| 34 | 0. | SLU_4 | Max | 0. | 0. | 425.4304 |
| 34 | 0.28669 | SLU_4 | Max | 0. | 0. | 578.7023 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 34 | 0.57337 | SLU_4 | Max | 0. | 0. | 742.2163 |
| 34 | 0. | SLU_4 | Min | 0. | 0. | 425.4304 |
| 34 | 0.28669 | SLU_4 | Min | 0. | 0. | 578.7023 |
| 34 | 0.57337 | SLU_4 | Min | 0. | 0. | 742.2163 |
| 34 | 0. | SLE_F1 | Max | 0. | 0. | 583.0161 |
| 34 | 0.28669 | SLE_F1 | Max | 0. | 0. | 696.8239 |
| 34 | 0.57337 | SLE_F1 | Max | 0. | 0. | 818.5101 |
| 34 | 0. | SLE_F1 | Min | 0. | 0. | 583.0161 |
| 34 | 0.28669 | SLE_F1 | Min | 0. | 0. | 696.8239 |
| 34 | 0.57337 | SLE_F1 | Min | 0. | 0. | 818.5101 |
| 34 | 0. | SLE_F2 | Max | 0. | 0. | 556.032 |
| 34 | 0.28669 | SLE_F2 | Max | 0. | 0. | 676.1622 |
| 34 | 0.57337 | SLE_F2 | Max | 0. | 0. | 804.1709 |
| 34 | 0. | SLE_F2 | Min | 0. | 0. | 556.032 |
| 34 | 0.28669 | SLE_F2 | Min | 0. | 0. | 676.1622 |
| 34 | 0.57337 | SLE_F2 | Min | 0. | 0. | 804.1709 |
| 34 | 0. | SLE_F3 | Max | 0. | 0. | 334.2381 |
| 34 | 0.28669 | SLE_F3 | Max | 0. | 0. | 448.4546 |
| 34 | 0.57337 | SLE_F3 | Max | 0. | 0. | 570.5495 |
| 34 | 0. | SLE_F3 | Min | 0. | 0. | 334.2381 |
| 34 | 0.28669 | SLE_F3 | Min | 0. | 0. | 448.4546 |
| 34 | 0.57337 | SLE_F3 | Min | 0. | 0. | 570.5495 |
| 34 | 0. | SLE_F4 | Max | 0. | 0. | 297.1324 |
| 34 | 0.28669 | SLE_F4 | Max | 0. | 0. | 400.7309 |
| 34 | 0.57337 | SLE_F4 | Max | 0. | 0. | 512.2079 |
| 34 | 0. | SLE_F4 | Min | 0. | 0. | 297.1324 |
| 34 | 0.28669 | SLE_F4 | Min | 0. | 0. | 400.7309 |
| 34 | 0.57337 | SLE_F4 | Min | 0. | 0. | 512.2079 |
| 34 | 0. | SLE_QP1 | Max | 0. | 0. | 595.1228 |
| 34 | 0.28669 | SLE_QP1 | Max | 0. | 0. | 702.2847 |
| 34 | 0.57337 | SLE_QP1 | Max | 0. | 0. | 817.3251 |
| 34 | 0. | SLE_QP1 | Min | 0. | 0. | 595.1228 |
| 34 | 0.28669 | SLE_QP1 | Min | 0. | 0. | 702.2847 |
| 34 | 0.57337 | SLE_QP1 | Min | 0. | 0. | 817.3251 |
| 34 | 0. | SLE_QP2 | Max | 0. | 0. | 571.9312 |
| 34 | 0.28669 | SLE_QP2 | Max | 0. | 0. | 685.2566 |
| 34 | 0.57337 | SLE_QP2 | Max | 0. | 0. | 806.4606 |
| 34 | 0. | SLE_QP2 | Min | 0. | 0. | 571.9312 |
| 34 | 0.28669 | SLE_QP2 | Min | 0. | 0. | 685.2566 |
| 34 | 0.57337 | SLE_QP2 | Min | 0. | 0. | 806.4606 |
| 34 | 0. | SLE_QP3 | Max | 0. | 0. | 347.209 |
| 34 | 0.28669 | SLE_QP3 | Max | 0. | 0. | 454.5819 |
| 34 | 0.57337 | SLE_QP3 | Max | 0. | 0. | 569.8333 |
| 34 | 0. | SLE_QP3 | Min | 0. | 0. | 347.209 |
| 34 | 0.28669 | SLE_QP3 | Min | 0. | 0. | 454.5819 |
| 34 | 0.57337 | SLE_QP3 | Min | 0. | 0. | 569.8333 |
| 34 | 0. | SLE_QP4 | Max | 0. | 0. | 304.7163 |
| 34 | 0.28669 | SLE_QP4 | Max | 0. | 0. | 400.0881 |
| 34 | 0.57337 | SLE_QP4 | Max | 0. | 0. | 503.3384 |
| 34 | 0. | SLE_QP4 | Min | 0. | 0. | 304.7163 |
| 34 | 0.28669 | SLE_QP4 | Min | 0. | 0. | 400.0881 |
| 34 | 0.57337 | SLE_QP4 | Min | 0. | 0. | 503.3384 |
| 34 | 0. | SLV_1 | Max | 0. | 0. | 330.8057 |
| 34 | 0.28669 | SLV_1 | Max | 0. | 0. | 382.878 |
| 34 | 0.57337 | SLV_1 | Max | 0. | 0. | 442.8289 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 34 | 0. | SLV_1 | Min | 0. | 0. | 330.8057 |
| 34 | 0.28669 | SLV_1 | Min | 0. | 0. | 382.878 |
| 34 | 0.57337 | SLV_1 | Min | 0. | 0. | 442.8289 |
| 34 | 0. | SLV_2 | Max | 0. | 0. | 335.7147 |
| 34 | 0.28669 | SLV_2 | Max | 0. | 0. | 387.8703 |
| 34 | 0.57337 | SLV_2 | Max | 0. | 0. | 447.9044 |
| 34 | 0. | SLV_2 | Min | 0. | 0. | 335.7147 |
| 34 | 0.28669 | SLV_2 | Min | 0. | 0. | 387.8703 |
| 34 | 0.57337 | SLV_2 | Min | 0. | 0. | 447.9044 |
| 34 | 0. | SLV_3 | Max | 0. | 0. | 151.3806 |
| 34 | 0.28669 | SLV_3 | Max | 0. | 0. | 194.1002 |
| 34 | 0.57337 | SLV_3 | Max | 0. | 0. | 244.6983 |
| 34 | 0. | SLV_3 | Min | 0. | 0. | 151.3806 |
| 34 | 0.28669 | SLV_3 | Min | 0. | 0. | 194.1002 |
| 34 | 0.57337 | SLV_3 | Min | 0. | 0. | 244.6983 |
| 34 | 0. | SLV_4 | Max | 0. | 0. | 155.4892 |
| 34 | 0.28669 | SLV_4 | Max | 0. | 0. | 198.2738 |
| 34 | 0.57337 | SLV_4 | Max | 0. | 0. | 248.9368 |
| 34 | 0. | SLV_4 | Min | 0. | 0. | 155.4892 |
| 34 | 0.28669 | SLV_4 | Min | 0. | 0. | 198.2738 |
| 34 | 0.57337 | SLV_4 | Min | 0. | 0. | 248.9368 |
| 34 | 0. | SLD_1 | Max | 0. | 0. | 406.5261 |
| 34 | 0.28669 | SLD_1 | Max | 0. | 0. | 486.8289 |
| 34 | 0.57337 | SLD_1 | Max | 0. | 0. | 575.0102 |
| 34 | 0. | SLD_1 | Min | 0. | 0. | 406.5261 |
| 34 | 0.28669 | SLD_1 | Min | 0. | 0. | 486.8289 |
| 34 | 0.57337 | SLD_1 | Min | 0. | 0. | 575.0102 |
| 34 | 0. | SLD_2 | Max | 0. | 0. | 409.4445 |
| 34 | 0.28669 | SLD_2 | Max | 0. | 0. | 489.8161 |
| 34 | 0.57337 | SLD_2 | Max | 0. | 0. | 578.0661 |
| 34 | 0. | SLD_2 | Min | 0. | 0. | 409.4445 |
| 34 | 0.28669 | SLD_2 | Min | 0. | 0. | 489.8161 |
| 34 | 0.57337 | SLD_2 | Min | 0. | 0. | 578.0661 |
| 34 | 0. | SLD_3 | Max | 0. | 0. | 205.9778 |
| 34 | 0.28669 | SLD_3 | Max | 0. | 0. | 275.3228 |
| 34 | 0.57337 | SLD_3 | Max | 0. | 0. | 352.5462 |
| 34 | 0. | SLD_3 | Min | 0. | 0. | 205.9778 |
| 34 | 0.28669 | SLD_3 | Min | 0. | 0. | 275.3228 |
| 34 | 0.57337 | SLD_3 | Min | 0. | 0. | 352.5462 |
| 34 | 0. | SLD_4 | Max | 0. | 0. | 207.8268 |
| 34 | 0.28669 | SLD_4 | Max | 0. | 0. | 277.2061 |
| 34 | 0.57337 | SLD_4 | Max | 0. | 0. | 354.4638 |
| 34 | 0. | SLD_4 | Min | 0. | 0. | 207.8268 |
| 34 | 0.28669 | SLD_4 | Min | 0. | 0. | 277.2061 |
| 34 | 0.57337 | SLD_4 | Min | 0. | 0. | 354.4638 |
| 34 | 0. | SLU_IDR_1 | Max | 0. | 0. | 493.1626 |
| 34 | 0.28669 | SLU_IDR_1 | Max | 0. | 0. | 611.2167 |
| 34 | 0.57337 | SLU_IDR_1 | Max | 0. | 0. | 738.3845 |
| 34 | 0. | SLU_IDR_1 | Min | 0. | 0. | 493.1626 |
| 34 | 0.28669 | SLU_IDR_1 | Min | 0. | 0. | 611.2167 |
| 34 | 0.57337 | SLU_IDR_1 | Min | 0. | 0. | 738.3845 |
| 34 | 0. | SLU_IDR_2 | Max | 0. | 0. | 703.1186 |
| 34 | 0.28669 | SLU_IDR_2 | Max | 0. | 0. | 827.4137 |
| 34 | 0.57337 | SLU_IDR_2 | Max | 0. | 0. | 960.8224 |
| 34 | 0. | SLU_IDR_2 | Min | 0. | 0. | 703.1186 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 34 | 0.28669 | SLU_IDR_2 | Min | 0. | 0. | 827.4137 |
| 34 | 0.57337 | SLU_IDR_2 | Min | 0. | 0. | 960.8224 |
| 34 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -144.2173 |
| 34 | 0.28669 | SISMA WOOD SLV-1 | Max | 0. | 0. | -207.741 |
| 34 | 0.57337 | SISMA WOOD SLV-1 | Max | 0. | 0. | -271.2647 |
| 34 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -144.2173 |
| 34 | 0.28669 | SISMA WOOD SLV-1 | Min | 0. | 0. | -207.741 |
| 34 | 0.57337 | SISMA WOOD SLV-1 | Min | 0. | 0. | -271.2647 |
| 34 | 0. | DEAD-1 | Max | 0. | 0. | -87.9346 |
| 34 | 0.28669 | DEAD-1 | Max | 0. | 0. | -86.7458 |
| 34 | 0.57337 | DEAD-1 | Max | 0. | 0. | -87.7935 |
| 34 | 0. | DEAD-1 | Min | 0. | 0. | -87.9346 |
| 34 | 0.28669 | DEAD-1 | Min | 0. | 0. | -86.7458 |
| 34 | 0.57337 | DEAD-1 | Min | 0. | 0. | -87.7935 |
| 34 | 0. | SLU_PROVA | | 0. | 0. | 698.6724 |
| 34 | 0.28669 | SLU_PROVA | | 0. | 0. | 837.22 |
| 34 | 0.57337 | SLU_PROVA | | 0. | 0. | 986.0096 |
| 35 | 0. | DEAD | | 0. | 0. | -87.4879 |
| 35 | 0.29586 | DEAD | | 0. | 0. | -88.7061 |
| 35 | 0.59172 | DEAD | | 0. | 0. | -92.2324 |
| 35 | 0. | SIMM_KA | | 0. | 0. | 60.8264 |
| 35 | 0.29586 | SIMM_KA | | 0. | 0. | 49.8846 |
| 35 | 0.59172 | SIMM_KA | | 0. | 0. | 38.9428 |
| 35 | 0. | SIMM_K0 | | 0. | 0. | 94.7578 |
| 35 | 0.29586 | SIMM_K0 | | 0. | 0. | 78.4119 |
| 35 | 0.59172 | SIMM_K0 | | 0. | 0. | 62.0661 |
| 35 | 0. | A--SIMM_KA | | 0. | 0. | -19.1082 |
| 35 | 0.29586 | A--SIMM_KA | | 0. | 0. | -32.799 |
| 35 | 0.59172 | A--SIMM_KA | | 0. | 0. | -46.4898 |
| 35 | 0. | A--SIMM_K0 | | 0. | 0. | -28.0026 |
| 35 | 0.29586 | A--SIMM_K0 | | 0. | 0. | -49.4161 |
| 35 | 0.59172 | A--SIMM_K0 | | 0. | 0. | -70.8296 |
| 35 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 13.8312 |
| 35 | 0.29586 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.7346 |
| 35 | 0.59172 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.6381 |
| 35 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.7364 |
| 35 | 0.29586 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.5917 |
| 35 | 0.59172 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.4469 |
| 35 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 20.7364 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 35 | 0.29586 | SIMM_SOVR_K 0 | | 0. | 0. | 20.5917 |
| 35 | 0.59172 | SIMM_SOVR_K 0 | | 0. | 0. | 20.4469 |
| 35 | 0. | SIMM_SOVR_K A | | 0. | 0. | 13.8312 |
| 35 | 0.29586 | SIMM_SOVR_K A | | 0. | 0. | 13.7346 |
| 35 | 0.59172 | SIMM_SOVR_K A | | 0. | 0. | 13.6381 |
| 35 | 0. | SOVR | | 0. | 0. | 9.7979 |
| 35 | 0.29586 | SOVR | | 0. | 0. | 21.2178 |
| 35 | 0.59172 | SOVR | | 0. | 0. | 32.6378 |
| 35 | 0. | TERR_SIMM | | 0. | 0. | 74.9094 |
| 35 | 0.29586 | TERR_SIMM | | 0. | 0. | 120.0661 |
| 35 | 0.59172 | TERR_SIMM | | 0. | 0. | 165.2228 |
| 35 | 0. | TERR_A--SIMM | | 0. | 0. | 47.3574 |
| 35 | 0.29586 | TERR_A--SIMM | | 0. | 0. | 94.3185 |
| 35 | 0.59172 | TERR_A--SIMM | | 0. | 0. | 141.2796 |
| 35 | 0. | INERZIA H SLV | | 0. | 0. | -3.731 |
| 35 | 0.29586 | INERZIA H SLV | | 0. | 0. | -4.0773 |
| 35 | 0.59172 | INERZIA H SLV | | 0. | 0. | -4.4236 |
| 35 | 0. | INERZIA V + SLV | | 0. | 0. | -1.3604 |
| 35 | 0.29586 | INERZIA V + SLV | | 0. | 0. | -1.4018 |
| 35 | 0.59172 | INERZIA V + SLV | | 0. | 0. | -1.4433 |
| 35 | 0. | INERZIA V - SLV | | 0. | 0. | 1.3604 |
| 35 | 0.29586 | INERZIA V - SLV | | 0. | 0. | 1.4018 |
| 35 | 0.59172 | INERZIA V - SLV | | 0. | 0. | 1.4433 |
| 35 | 0. | SISMA WOOD SLV | | 0. | 0. | -171.4327 |
| 35 | 0.29586 | SISMA WOOD SLV | | 0. | 0. | -194.7632 |
| 35 | 0.59172 | SISMA WOOD SLV | | 0. | 0. | -218.0938 |
| 35 | 0. | iDROSTATICA | | 0. | 0. | 641.0578 |
| 35 | 0.29586 | iDROSTATICA | | 0. | 0. | 719.6224 |
| 35 | 0.59172 | iDROSTATICA | | 0. | 0. | 808.9597 |
| 35 | 0. | SISMA WOOD SLD | | 0. | 0. | -75.7116 |
| 35 | 0.29586 | SISMA WOOD SLD | | 0. | 0. | -86.0153 |
| 35 | 0.59172 | SISMA WOOD SLD | | 0. | 0. | -96.319 |
| 35 | 0. | INERZIA H SLD | | 0. | 0. | -1.6477 |
| 35 | 0.29586 | INERZIA H SLD | | 0. | 0. | -1.8007 |
| 35 | 0.59172 | INERZIA H SLD | | 0. | 0. | -1.9536 |
| 35 | 0. | INERZIA V + SLD | | 0. | 0. | -0.6008 |
| 35 | 0.29586 | INERZIA V + SLD | | 0. | 0. | -0.6191 |
| 35 | 0.59172 | INERZIA V + SLD | | 0. | 0. | -0.6374 |
| 35 | 0. | INERZIA V SLD | | 0. | 0. | 0.6008 |
| 35 | 0.29586 | INERZIA V SLD | | 0. | 0. | 0.6191 |
| 35 | 0.59172 | INERZIA V SLD | | 0. | 0. | 0.6374 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------|----------|-----------|------------|------------|
| 35 | 0. | INERZIA V -1 | | 0. | 0. | 1.3604 |
| 35 | 0.29586 | INERZIA V -1 | | 0. | 0. | 1.4018 |
| 35 | 0.59172 | INERZIA V -1 | | 0. | 0. | 1.4433 |
| 35 | 0. | SLU_1 | Max | 0. | 0. | 1068.2448 |
| 35 | 0.29586 | SLU_1 | Max | 0. | 0. | 1239.3369 |
| 35 | 0.59172 | SLU_1 | Max | 0. | 0. | 1421.4329 |
| 35 | 0. | SLU_1 | Min | 0. | 0. | 1068.2448 |
| 35 | 0.29586 | SLU_1 | Min | 0. | 0. | 1239.3369 |
| 35 | 0.59172 | SLU_1 | Min | 0. | 0. | 1421.4329 |
| 35 | 0. | SLU_2 | Max | 0. | 0. | 1043.8241 |
| 35 | 0.29586 | SLU_2 | Max | 0. | 0. | 1224.6931 |
| 35 | 0.59172 | SLU_2 | Max | 0. | 0. | 1416.5659 |
| 35 | 0. | SLU_2 | Min | 0. | 0. | 1043.8241 |
| 35 | 0.29586 | SLU_2 | Min | 0. | 0. | 1224.6931 |
| 35 | 0.59172 | SLU_2 | Min | 0. | 0. | 1416.5659 |
| 35 | 0. | SLU_3 | Max | 0. | 0. | 672.7746 |
| 35 | 0.29586 | SLU_3 | Max | 0. | 0. | 832.5083 |
| 35 | 0.59172 | SLU_3 | Max | 0. | 0. | 1003.2459 |
| 35 | 0. | SLU_3 | Min | 0. | 0. | 672.7746 |
| 35 | 0.29586 | SLU_3 | Min | 0. | 0. | 832.5083 |
| 35 | 0.59172 | SLU_3 | Min | 0. | 0. | 1003.2459 |
| 35 | 0. | SLU_4 | Max | 0. | 0. | 742.2163 |
| 35 | 0.29586 | SLU_4 | Max | 0. | 0. | 916.8518 |
| 35 | 0.59172 | SLU_4 | Max | 0. | 0. | 1102.4912 |
| 35 | 0. | SLU_4 | Min | 0. | 0. | 742.2163 |
| 35 | 0.29586 | SLU_4 | Min | 0. | 0. | 916.8518 |
| 35 | 0.59172 | SLU_4 | Min | 0. | 0. | 1102.4912 |
| 35 | 0. | SLE_F1 | Max | 0. | 0. | 818.5101 |
| 35 | 0.29586 | SLE_F1 | Max | 0. | 0. | 945.2351 |
| 35 | 0.59172 | SLE_F1 | Max | 0. | 0. | 1080.4246 |
| 35 | 0. | SLE_F1 | Min | 0. | 0. | 818.5101 |
| 35 | 0.29586 | SLE_F1 | Min | 0. | 0. | 945.2351 |
| 35 | 0.59172 | SLE_F1 | Min | 0. | 0. | 1080.4246 |
| 35 | 0. | SLE_F2 | Max | 0. | 0. | 804.1709 |
| 35 | 0.29586 | SLE_F2 | Max | 0. | 0. | 938.6973 |
| 35 | 0.59172 | SLE_F2 | Max | 0. | 0. | 1081.6882 |
| 35 | 0. | SLE_F2 | Min | 0. | 0. | 804.1709 |
| 35 | 0.29586 | SLE_F2 | Min | 0. | 0. | 938.6973 |
| 35 | 0.59172 | SLE_F2 | Min | 0. | 0. | 1081.6882 |
| 35 | 0. | SLE_F3 | Max | 0. | 0. | 570.5495 |
| 35 | 0.29586 | SLE_F3 | Max | 0. | 0. | 700.2802 |
| 35 | 0.59172 | SLE_F3 | Max | 0. | 0. | 838.4755 |
| 35 | 0. | SLE_F3 | Min | 0. | 0. | 570.5495 |
| 35 | 0.29586 | SLE_F3 | Min | 0. | 0. | 700.2802 |
| 35 | 0.59172 | SLE_F3 | Min | 0. | 0. | 838.4755 |
| 35 | 0. | SLE_F4 | Max | 0. | 0. | 512.2079 |
| 35 | 0.29586 | SLE_F4 | Max | 0. | 0. | 629.7487 |
| 35 | 0.59172 | SLE_F4 | Max | 0. | 0. | 755.754 |
| 35 | 0. | SLE_F4 | Min | 0. | 0. | 512.2079 |
| 35 | 0.29586 | SLE_F4 | Min | 0. | 0. | 629.7487 |
| 35 | 0.59172 | SLE_F4 | Min | 0. | 0. | 755.754 |
| 35 | 0. | SLE_QP1 | Max | 0. | 0. | 817.3251 |
| 35 | 0.29586 | SLE_QP1 | Max | 0. | 0. | 935.717 |
| 35 | 0.59172 | SLE_QP1 | Max | 0. | 0. | 1062.5734 |
| 35 | 0. | SLE_QP1 | Min | 0. | 0. | 817.3251 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 35 | 0.29586 | SLE_QP1 | Min | 0. | 0. | 935.717 |
| 35 | 0.59172 | SLE_QP1 | Min | 0. | 0. | 1062.5734 |
| 35 | 0. | SLE_QP2 | Max | 0. | 0. | 806.4606 |
| 35 | 0.29586 | SLE_QP2 | Max | 0. | 0. | 932.4376 |
| 35 | 0.59172 | SLE_QP2 | Max | 0. | 0. | 1066.8792 |
| 35 | 0. | SLE_QP2 | Min | 0. | 0. | 806.4606 |
| 35 | 0.29586 | SLE_QP2 | Min | 0. | 0. | 932.4376 |
| 35 | 0.59172 | SLE_QP2 | Min | 0. | 0. | 1066.8792 |
| 35 | 0. | SLE_QP3 | Max | 0. | 0. | 569.8333 |
| 35 | 0.29586 | SLE_QP3 | Max | 0. | 0. | 691.0132 |
| 35 | 0.59172 | SLE_QP3 | Max | 0. | 0. | 820.6576 |
| 35 | 0. | SLE_QP3 | Min | 0. | 0. | 569.8333 |
| 35 | 0.29586 | SLE_QP3 | Min | 0. | 0. | 691.0132 |
| 35 | 0.59172 | SLE_QP3 | Min | 0. | 0. | 820.6576 |
| 35 | 0. | SLE_QP4 | Max | 0. | 0. | 503.3384 |
| 35 | 0.29586 | SLE_QP4 | Max | 0. | 0. | 610.974 |
| 35 | 0.59172 | SLE_QP4 | Max | 0. | 0. | 727.0741 |
| 35 | 0. | SLE_QP4 | Min | 0. | 0. | 503.3384 |
| 35 | 0.29586 | SLE_QP4 | Min | 0. | 0. | 610.974 |
| 35 | 0.59172 | SLE_QP4 | Min | 0. | 0. | 727.0741 |
| 35 | 0. | SLV_1 | Max | 0. | 0. | 442.8289 |
| 35 | 0.29586 | SLV_1 | Max | 0. | 0. | 501.513 |
| 35 | 0.59172 | SLV_1 | Max | 0. | 0. | 568.6617 |
| 35 | 0. | SLV_1 | Min | 0. | 0. | 442.8289 |
| 35 | 0.29586 | SLV_1 | Min | 0. | 0. | 501.513 |
| 35 | 0.59172 | SLV_1 | Min | 0. | 0. | 568.6617 |
| 35 | 0. | SLV_2 | Max | 0. | 0. | 447.9044 |
| 35 | 0.29586 | SLV_2 | Max | 0. | 0. | 506.6263 |
| 35 | 0.59172 | SLV_2 | Max | 0. | 0. | 573.8127 |
| 35 | 0. | SLV_2 | Min | 0. | 0. | 447.9044 |
| 35 | 0.29586 | SLV_2 | Min | 0. | 0. | 506.6263 |
| 35 | 0.59172 | SLV_2 | Min | 0. | 0. | 573.8127 |
| 35 | 0. | SLV_3 | Max | 0. | 0. | 244.6983 |
| 35 | 0.29586 | SLV_3 | Max | 0. | 0. | 294.0862 |
| 35 | 0.59172 | SLV_3 | Max | 0. | 0. | 351.9388 |
| 35 | 0. | SLV_3 | Min | 0. | 0. | 244.6983 |
| 35 | 0.29586 | SLV_3 | Min | 0. | 0. | 294.0862 |
| 35 | 0.59172 | SLV_3 | Min | 0. | 0. | 351.9388 |
| 35 | 0. | SLV_4 | Max | 0. | 0. | 248.9368 |
| 35 | 0.29586 | SLV_4 | Max | 0. | 0. | 298.3482 |
| 35 | 0.59172 | SLV_4 | Max | 0. | 0. | 356.2241 |
| 35 | 0. | SLV_4 | Min | 0. | 0. | 248.9368 |
| 35 | 0.29586 | SLV_4 | Min | 0. | 0. | 298.3482 |
| 35 | 0.59172 | SLV_4 | Min | 0. | 0. | 356.2241 |
| 35 | 0. | SLD_1 | Max | 0. | 0. | 575.0102 |
| 35 | 0.29586 | SLD_1 | Max | 0. | 0. | 665.038 |
| 35 | 0.59172 | SLD_1 | Max | 0. | 0. | 763.5303 |
| 35 | 0. | SLD_1 | Min | 0. | 0. | 575.0102 |
| 35 | 0.29586 | SLD_1 | Min | 0. | 0. | 665.038 |
| 35 | 0.59172 | SLD_1 | Min | 0. | 0. | 763.5303 |
| 35 | 0. | SLD_2 | Max | 0. | 0. | 578.0661 |
| 35 | 0.29586 | SLD_2 | Max | 0. | 0. | 668.1314 |
| 35 | 0.59172 | SLD_2 | Max | 0. | 0. | 766.6612 |
| 35 | 0. | SLD_2 | Min | 0. | 0. | 578.0661 |
| 35 | 0.29586 | SLD_2 | Min | 0. | 0. | 668.1314 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 35 | 0.59172 | SLD_2 | Min | 0. | 0. | 766.6612 |
| 35 | 0. | SLD_3 | Max | 0. | 0. | 352.5462 |
| 35 | 0.29586 | SLD_3 | Max | 0. | 0. | 431.7117 |
| 35 | 0.59172 | SLD_3 | Max | 0. | 0. | 519.3416 |
| 35 | 0. | SLD_3 | Min | 0. | 0. | 352.5462 |
| 35 | 0.29586 | SLD_3 | Min | 0. | 0. | 431.7117 |
| 35 | 0.59172 | SLD_3 | Min | 0. | 0. | 519.3416 |
| 35 | 0. | SLD_4 | Max | 0. | 0. | 354.4638 |
| 35 | 0.29586 | SLD_4 | Max | 0. | 0. | 433.644 |
| 35 | 0.59172 | SLD_4 | Max | 0. | 0. | 521.2887 |
| 35 | 0. | SLD_4 | Min | 0. | 0. | 354.4638 |
| 35 | 0.29586 | SLD_4 | Min | 0. | 0. | 433.644 |
| 35 | 0.59172 | SLD_4 | Min | 0. | 0. | 521.2887 |
| 35 | 0. | SLU_IDR_1 | Max | 0. | 0. | 738.3845 |
| 35 | 0.29586 | SLU_IDR_1 | Max | 0. | 0. | 869.3375 |
| 35 | 0.59172 | SLU_IDR_1 | Max | 0. | 0. | 1010.063 |
| 35 | 0. | SLU_IDR_1 | Min | 0. | 0. | 738.3845 |
| 35 | 0.29586 | SLU_IDR_1 | Min | 0. | 0. | 869.3375 |
| 35 | 0.59172 | SLU_IDR_1 | Min | 0. | 0. | 1010.063 |
| 35 | 0. | SLU_IDR_2 | Max | 0. | 0. | 960.8224 |
| 35 | 0.29586 | SLU_IDR_2 | Max | 0. | 0. | 1096.8251 |
| 35 | 0.59172 | SLU_IDR_2 | Max | 0. | 0. | 1242.6004 |
| 35 | 0. | SLU_IDR_2 | Min | 0. | 0. | 960.8224 |
| 35 | 0.29586 | SLU_IDR_2 | Min | 0. | 0. | 1096.8251 |
| 35 | 0.59172 | SLU_IDR_2 | Min | 0. | 0. | 1242.6004 |
| 35 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -271.2647 |
| 35 | 0.29586 | SISMA WOOD SLV-1 | Max | 0. | 0. | -339.047 |
| 35 | 0.59172 | SISMA WOOD SLV-1 | Max | 0. | 0. | -406.8293 |
| 35 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -271.2647 |
| 35 | 0.29586 | SISMA WOOD SLV-1 | Min | 0. | 0. | -339.047 |
| 35 | 0.59172 | SISMA WOOD SLV-1 | Min | 0. | 0. | -406.8293 |
| 35 | 0. | DEAD-1 | Max | 0. | 0. | -87.7935 |
| 35 | 0.29586 | DEAD-1 | Max | 0. | 0. | -85.1914 |
| 35 | 0.59172 | DEAD-1 | Max | 0. | 0. | -84.8973 |
| 35 | 0. | DEAD-1 | Min | 0. | 0. | -87.7935 |
| 35 | 0.29586 | DEAD-1 | Min | 0. | 0. | -85.1914 |
| 35 | 0.59172 | DEAD-1 | Min | 0. | 0. | -84.8973 |
| 35 | 0. | SLU_PROVA | | 0. | 0. | 986.0096 |
| 35 | 0.29586 | SLU_PROVA | | 0. | 0. | 1140.9269 |
| 35 | 0.59172 | SLU_PROVA | | 0. | 0. | 1306.848 |
| 38 | 0. | DEAD | | 0. | 0. | 16.8875 |
| 38 | 0.2636 | DEAD | | 0. | 0. | 30.7057 |
| 38 | 0.5272 | DEAD | | 0. | 0. | 44.5239 |
| 38 | 0. | SIMM_KA | | 0. | 0. | -14.2296 |
| 38 | 0.2636 | SIMM_KA | | 0. | 0. | -44.3826 |
| 38 | 0.5272 | SIMM_KA | | 0. | 0. | -70.7789 |
| 38 | 0. | SIMM_K0 | | 0. | 0. | -17.7458 |
| 38 | 0.2636 | SIMM_K0 | | 0. | 0. | -63.3455 |
| 38 | 0.5272 | SIMM_K0 | | 0. | 0. | -103.3103 |
| 38 | 0. | A--SIMM_KA | | 0. | 0. | 71.5837 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 38 | 0.2636 | A--SIMM_KA | | 0. | 0. | 30.2582 |
| 38 | 0.5272 | A--SIMM_KA | | 0. | 0. | -5.1902 |
| 38 | 0. | A--SIMM_K0 | | 0. | 0. | 105.0483 |
| 38 | 0.2636 | A--SIMM_K0 | | 0. | 0. | 41.5199 |
| 38 | 0.5272 | A--SIMM_K0 | | 0. | 0. | -13.2028 |
| 38 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 11.0955 |
| 38 | 0.2636 | A-- SIMM_SOVR_K A | | 0. | 0. | 8.6841 |
| 38 | 0.5272 | A-- SIMM_SOVR_K A | | 0. | 0. | 6.2726 |
| 38 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 16.6349 |
| 38 | 0.2636 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 13.0196 |
| 38 | 0.5272 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 9.4042 |
| 38 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 16.6349 |
| 38 | 0.2636 | SIMM_SOVR_K 0 | | 0. | 0. | 13.0196 |
| 38 | 0.5272 | SIMM_SOVR_K 0 | | 0. | 0. | 9.4042 |
| 38 | 0. | SIMM_SOVR_K A | | 0. | 0. | 11.0955 |
| 38 | 0.2636 | SIMM_SOVR_K A | | 0. | 0. | 8.6841 |
| 38 | 0.5272 | SIMM_SOVR_K A | | 0. | 0. | 6.2726 |
| 38 | 0. | SOVR | | 0. | 0. | 102.0577 |
| 38 | 0.2636 | SOVR | | 0. | 0. | 108.1794 |
| 38 | 0.5272 | SOVR | | 0. | 0. | 114.3012 |
| 38 | 0. | TERR_SIMM | | 0. | 0. | 433.7991 |
| 38 | 0.2636 | TERR_SIMM | | 0. | 0. | 451.714 |
| 38 | 0.5272 | TERR_SIMM | | 0. | 0. | 469.6289 |
| 38 | 0. | TERR_A--SIMM | | 0. | 0. | 694.2428 |
| 38 | 0.2636 | TERR_A--SIMM | | 0. | 0. | 720.2391 |
| 38 | 0.5272 | TERR_A--SIMM | | 0. | 0. | 746.2353 |
| 38 | 0. | INERZIA H SLV | | 0. | 0. | 5.7082 |
| 38 | 0.2636 | INERZIA H SLV | | 0. | 0. | 6.8371 |
| 38 | 0.5272 | INERZIA H SLV | | 0. | 0. | 7.9659 |
| 38 | 0. | INERZIA V + SLV | | 0. | 0. | 0.3088 |
| 38 | 0.2636 | INERZIA V + SLV | | 0. | 0. | 0.5267 |
| 38 | 0.5272 | INERZIA V + SLV | | 0. | 0. | 0.7446 |
| 38 | 0. | INERZIA V - SLV | | 0. | 0. | -0.3088 |
| 38 | 0.2636 | INERZIA V - SLV | | 0. | 0. | -0.5267 |
| 38 | 0.5272 | INERZIA V - SLV | | 0. | 0. | -0.7446 |
| 38 | 0. | SISMA WOOD SLV | | 0. | 0. | 267.0601 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 38 | 0.2636 | SISMA WOOD SLV | | 0. | 0. | 281.1079 |
| 38 | 0.5272 | SISMA WOOD SLV | | 0. | 0. | 300.0015 |
| 38 | 0. | IDROSTATICA | | 0. | 0. | 833.4433 |
| 38 | 0.2636 | IDROSTATICA | | 0. | 0. | 738.8419 |
| 38 | 0.5272 | IDROSTATICA | | 0. | 0. | 652.2268 |
| 38 | 0. | SISMA WOOD SLD | | 0. | 0. | 117.9445 |
| 38 | 0.2636 | SISMA WOOD SLD | | 0. | 0. | 124.1486 |
| 38 | 0.5272 | SISMA WOOD SLD | | 0. | 0. | 132.4928 |
| 38 | 0. | INERZIA H SLD | | 0. | 0. | 2.521 |
| 38 | 0.2636 | INERZIA H SLD | | 0. | 0. | 3.0195 |
| 38 | 0.5272 | INERZIA H SLD | | 0. | 0. | 3.5181 |
| 38 | 0. | INERZIA V + SLD | | 0. | 0. | 0.1364 |
| 38 | 0.2636 | INERZIA V + SLD | | 0. | 0. | 0.2326 |
| 38 | 0.5272 | INERZIA V + SLD | | 0. | 0. | 0.3289 |
| 38 | 0. | INERZIA V SLD | | 0. | 0. | -0.1364 |
| 38 | 0.2636 | INERZIA V SLD | | 0. | 0. | -0.2326 |
| 38 | 0.5272 | INERZIA V SLD | | 0. | 0. | -0.3289 |
| 38 | 0. | INERZIA V -1 | | 0. | 0. | -0.3088 |
| 38 | 0.2636 | INERZIA V -1 | | 0. | 0. | -0.5267 |
| 38 | 0.5272 | INERZIA V -1 | | 0. | 0. | -0.7446 |
| 38 | 0. | SLU_1 | Max | 0. | 0. | 1996.1353 |
| 38 | 0.2636 | SLU_1 | Max | 0. | 0. | 1862.9312 |
| 38 | 0.5272 | SLU_1 | Max | 0. | 0. | 1747.4346 |
| 38 | 0. | SLU_1 | Min | 0. | 0. | 1996.1353 |
| 38 | 0.2636 | SLU_1 | Min | 0. | 0. | 1862.9312 |
| 38 | 0.5272 | SLU_1 | Min | 0. | 0. | 1747.4346 |
| 38 | 0. | SLU_2 | Max | 0. | 0. | 2034.2071 |
| 38 | 0.2636 | SLU_2 | Max | 0. | 0. | 1922.007 |
| 38 | 0.5272 | SLU_2 | Max | 0. | 0. | 1825.0727 |
| 38 | 0. | SLU_2 | Min | 0. | 0. | 2034.2071 |
| 38 | 0.2636 | SLU_2 | Min | 0. | 0. | 1922.007 |
| 38 | 0.5272 | SLU_2 | Min | 0. | 0. | 1825.0727 |
| 38 | 0. | SLU_3 | Max | 0. | 0. | 2680.2273 |
| 38 | 0.2636 | SLU_3 | Max | 0. | 0. | 2533.7075 |
| 38 | 0.5272 | SLU_3 | Max | 0. | 0. | 2409.0174 |
| 38 | 0. | SLU_3 | Min | 0. | 0. | 2680.2273 |
| 38 | 0.2636 | SLU_3 | Min | 0. | 0. | 2533.7075 |
| 38 | 0.5272 | SLU_3 | Min | 0. | 0. | 2409.0174 |
| 38 | 0. | SLU_4 | Max | 0. | 0. | 2613.4623 |
| 38 | 0.2636 | SLU_4 | Max | 0. | 0. | 2498.7408 |
| 38 | 0.5272 | SLU_4 | Max | 0. | 0. | 2402.0416 |
| 38 | 0. | SLU_4 | Min | 0. | 0. | 2613.4623 |
| 38 | 0.2636 | SLU_4 | Min | 0. | 0. | 2498.7408 |
| 38 | 0.5272 | SLU_4 | Min | 0. | 0. | 2402.0416 |
| 38 | 0. | SLE_F1 | Max | 0. | 0. | 1492.1208 |
| 38 | 0.2636 | SLE_F1 | Max | 0. | 0. | 1387.5289 |
| 38 | 0.5272 | SLE_F1 | Max | 0. | 0. | 1296.5581 |
| 38 | 0. | SLE_F1 | Min | 0. | 0. | 1492.1208 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 38 | 0.2636 | SLE_F1 | Min | 0. | 0. | 1387.5289 |
| 38 | 0.5272 | SLE_F1 | Min | 0. | 0. | 1296.5581 |
| 38 | 0. | SLE_F2 | Max | 0. | 0. | 1524.8603 |
| 38 | 0.2636 | SLE_F2 | Max | 0. | 0. | 1435.7435 |
| 38 | 0.5272 | SLE_F2 | Max | 0. | 0. | 1358.3698 |
| 38 | 0. | SLE_F2 | Min | 0. | 0. | 1524.8603 |
| 38 | 0.2636 | SLE_F2 | Min | 0. | 0. | 1435.7435 |
| 38 | 0.5272 | SLE_F2 | Min | 0. | 0. | 1358.3698 |
| 38 | 0. | SLE_F3 | Max | 0. | 0. | 1966.4494 |
| 38 | 0.2636 | SLE_F3 | Max | 0. | 0. | 1875.5472 |
| 38 | 0.5272 | SLE_F3 | Max | 0. | 0. | 1798.5082 |
| 38 | 0. | SLE_F3 | Min | 0. | 0. | 1966.4494 |
| 38 | 0.2636 | SLE_F3 | Min | 0. | 0. | 1875.5472 |
| 38 | 0.5272 | SLE_F3 | Min | 0. | 0. | 1798.5082 |
| 38 | 0. | SLE_F4 | Max | 0. | 0. | 2008.3746 |
| 38 | 0.2636 | SLE_F4 | Max | 0. | 0. | 1892.2694 |
| 38 | 0.5272 | SLE_F4 | Max | 0. | 0. | 1792.9562 |
| 38 | 0. | SLE_F4 | Min | 0. | 0. | 2008.3746 |
| 38 | 0.2636 | SLE_F4 | Min | 0. | 0. | 1892.2694 |
| 38 | 0.5272 | SLE_F4 | Min | 0. | 0. | 1792.9562 |
| 38 | 0. | SLE_QP1 | Max | 0. | 0. | 1416.0228 |
| 38 | 0.2636 | SLE_QP1 | Max | 0. | 0. | 1307.0984 |
| 38 | 0.5272 | SLE_QP1 | Max | 0. | 0. | 1211.7951 |
| 38 | 0. | SLE_QP1 | Min | 0. | 0. | 1416.0228 |
| 38 | 0.2636 | SLE_QP1 | Min | 0. | 0. | 1307.0984 |
| 38 | 0.5272 | SLE_QP1 | Min | 0. | 0. | 1211.7951 |
| 38 | 0. | SLE_QP2 | Max | 0. | 0. | 1450.7286 |
| 38 | 0.2636 | SLE_QP2 | Max | 0. | 0. | 1356.3947 |
| 38 | 0.5272 | SLE_QP2 | Max | 0. | 0. | 1273.8038 |
| 38 | 0. | SLE_QP2 | Min | 0. | 0. | 1450.7286 |
| 38 | 0.2636 | SLE_QP2 | Min | 0. | 0. | 1356.3947 |
| 38 | 0.5272 | SLE_QP2 | Min | 0. | 0. | 1273.8038 |
| 38 | 0. | SLE_QP3 | Max | 0. | 0. | 1884.9067 |
| 38 | 0.2636 | SLE_QP3 | Max | 0. | 0. | 1789.074 |
| 38 | 0.5272 | SLE_QP3 | Max | 0. | 0. | 1707.1045 |
| 38 | 0. | SLE_QP3 | Min | 0. | 0. | 1884.9067 |
| 38 | 0.2636 | SLE_QP3 | Min | 0. | 0. | 1789.074 |
| 38 | 0.5272 | SLE_QP3 | Min | 0. | 0. | 1707.1045 |
| 38 | 0. | SLE_QP4 | Max | 0. | 0. | 1907.4645 |
| 38 | 0.2636 | SLE_QP4 | Max | 0. | 0. | 1784.7101 |
| 38 | 0.5272 | SLE_QP4 | Max | 0. | 0. | 1678.7479 |
| 38 | 0. | SLE_QP4 | Min | 0. | 0. | 1907.4645 |
| 38 | 0.2636 | SLE_QP4 | Min | 0. | 0. | 1784.7101 |
| 38 | 0.5272 | SLE_QP4 | Min | 0. | 0. | 1678.7479 |
| 38 | 0. | SLV_1 | Max | 0. | 0. | 1572.4498 |
| 38 | 0.2636 | SLV_1 | Max | 0. | 0. | 1384.9994 |
| 38 | 0.5272 | SLV_1 | Max | 0. | 0. | 1216.016 |
| 38 | 0. | SLV_1 | Min | 0. | 0. | 1572.4498 |
| 38 | 0.2636 | SLV_1 | Min | 0. | 0. | 1384.9994 |
| 38 | 0.5272 | SLV_1 | Min | 0. | 0. | 1216.016 |
| 38 | 0. | SLV_2 | Max | 0. | 0. | 1570.2182 |
| 38 | 0.2636 | SLV_2 | Max | 0. | 0. | 1382.2215 |
| 38 | 0.5272 | SLV_2 | Max | 0. | 0. | 1212.6918 |
| 38 | 0. | SLV_2 | Min | 0. | 0. | 1570.2182 |
| 38 | 0.2636 | SLV_2 | Min | 0. | 0. | 1382.2215 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 38 | 0.5272 | SLV_2 | Min | 0. | 0. | 1212.6918 |
| 38 | 0. | SLV_3 | Max | 0. | 0. | 1994.6631 |
| 38 | 0.2636 | SLV_3 | Max | 0. | 0. | 1772.3595 |
| 38 | 0.5272 | SLV_3 | Max | 0. | 0. | 1571.6938 |
| 38 | 0. | SLV_3 | Min | 0. | 0. | 1994.6631 |
| 38 | 0.2636 | SLV_3 | Min | 0. | 0. | 1772.3595 |
| 38 | 0.5272 | SLV_3 | Min | 0. | 0. | 1571.6938 |
| 38 | 0. | SLV_4 | Max | 0. | 0. | 1991.3779 |
| 38 | 0.2636 | SLV_4 | Max | 0. | 0. | 1768.5214 |
| 38 | 0.5272 | SLV_4 | Max | 0. | 0. | 1567.3029 |
| 38 | 0. | SLV_4 | Min | 0. | 0. | 1991.3779 |
| 38 | 0.2636 | SLV_4 | Min | 0. | 0. | 1768.5214 |
| 38 | 0.5272 | SLV_4 | Min | 0. | 0. | 1567.3029 |
| 38 | 0. | SLD_1 | Max | 0. | 0. | 1533.8509 |
| 38 | 0.2636 | SLD_1 | Max | 0. | 0. | 1400.7708 |
| 38 | 0.5272 | SLD_1 | Max | 0. | 0. | 1283.4519 |
| 38 | 0. | SLD_1 | Min | 0. | 0. | 1533.8509 |
| 38 | 0.2636 | SLD_1 | Min | 0. | 0. | 1400.7708 |
| 38 | 0.5272 | SLD_1 | Min | 0. | 0. | 1283.4519 |
| 38 | 0. | SLD_2 | Max | 0. | 0. | 1534.3026 |
| 38 | 0.2636 | SLD_2 | Max | 0. | 0. | 1400.8795 |
| 38 | 0.5272 | SLD_2 | Max | 0. | 0. | 1283.2177 |
| 38 | 0. | SLD_2 | Min | 0. | 0. | 1534.3026 |
| 38 | 0.2636 | SLD_2 | Min | 0. | 0. | 1400.8795 |
| 38 | 0.5272 | SLD_2 | Min | 0. | 0. | 1283.2177 |
| 38 | 0. | SLD_3 | Max | 0. | 0. | 1936.0602 |
| 38 | 0.2636 | SLD_3 | Max | 0. | 0. | 1768.0915 |
| 38 | 0.5272 | SLD_3 | Max | 0. | 0. | 1619.055 |
| 38 | 0. | SLD_3 | Min | 0. | 0. | 1936.0602 |
| 38 | 0.2636 | SLD_3 | Min | 0. | 0. | 1768.0915 |
| 38 | 0.5272 | SLD_3 | Min | 0. | 0. | 1619.055 |
| 38 | 0. | SLD_4 | Max | 0. | 0. | 1934.8992 |
| 38 | 0.2636 | SLD_4 | Max | 0. | 0. | 1766.6611 |
| 38 | 0.5272 | SLD_4 | Max | 0. | 0. | 1617.3552 |
| 38 | 0. | SLD_4 | Min | 0. | 0. | 1934.8992 |
| 38 | 0.2636 | SLD_4 | Min | 0. | 0. | 1766.6611 |
| 38 | 0.5272 | SLD_4 | Min | 0. | 0. | 1617.3552 |
| 38 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1954.6238 |
| 38 | 0.2636 | SLU_IDR_1 | Max | 0. | 0. | 1842.9168 |
| 38 | 0.5272 | SLU_IDR_1 | Max | 0. | 0. | 1745.284 |
| 38 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1954.6238 |
| 38 | 0.2636 | SLU_IDR_1 | Min | 0. | 0. | 1842.9168 |
| 38 | 0.5272 | SLU_IDR_1 | Min | 0. | 0. | 1745.284 |
| 38 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1586.8881 |
| 38 | 0.2636 | SLU_IDR_2 | Max | 0. | 0. | 1475.4788 |
| 38 | 0.5272 | SLU_IDR_2 | Max | 0. | 0. | 1376.2354 |
| 38 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1586.8881 |
| 38 | 0.2636 | SLU_IDR_2 | Min | 0. | 0. | 1475.4788 |
| 38 | 0.5272 | SLU_IDR_2 | Min | 0. | 0. | 1376.2354 |
| 38 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -172.2573 |
| 38 | 0.2636 | SISMA WOOD SLV-1 | Max | 0. | 0. | -242.1874 |
| 38 | 0.5272 | SISMA WOOD SLV-1 | Max | 0. | 0. | -307.2717 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 38 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -172.2573 |
| 38 | 0.2636 | SISMA WOOD SLV-1 | Min | 0. | 0. | -242.1874 |
| 38 | 0.5272 | SISMA WOOD SLV-1 | Min | 0. | 0. | -307.2717 |
| 38 | 0. | DEAD-1 | Max | 0. | 0. | 47.7999 |
| 38 | 0.2636 | DEAD-1 | Max | 0. | 0. | 64.251 |
| 38 | 0.5272 | DEAD-1 | Max | 0. | 0. | 80.702 |
| 38 | 0. | DEAD-1 | Min | 0. | 0. | 47.7999 |
| 38 | 0.2636 | DEAD-1 | Min | 0. | 0. | 64.251 |
| 38 | 0.5272 | DEAD-1 | Min | 0. | 0. | 80.702 |
| 38 | 0. | SLU_PROVA | | 0. | 0. | 1824.3383 |
| 38 | 0.2636 | SLU_PROVA | | 0. | 0. | 1687.0895 |
| 38 | 0.5272 | SLU_PROVA | | 0. | 0. | 1567.5482 |
| 39 | 0. | DEAD | | 0. | 0. | 44.5239 |
| 39 | 0.2636 | DEAD | | 0. | 0. | 59.2057 |
| 39 | 0.5272 | DEAD | | 0. | 0. | 73.8874 |
| 39 | 0. | SIMM_KA | | 0. | 0. | -70.7789 |
| 39 | 0.2636 | SIMM_KA | | 0. | 0. | -95.4682 |
| 39 | 0.5272 | SIMM_KA | | 0. | 0. | -116.6546 |
| 39 | 0. | SIMM_K0 | | 0. | 0. | -103.3103 |
| 39 | 0.2636 | SIMM_K0 | | 0. | 0. | -140.7687 |
| 39 | 0.5272 | SIMM_K0 | | 0. | 0. | -172.973 |
| 39 | 0. | A--SIMM_KA | | 0. | 0. | -5.1902 |
| 39 | 0.2636 | A--SIMM_KA | | 0. | 0. | -41.821 |
| 39 | 0.5272 | A--SIMM_KA | | 0. | 0. | -72.9984 |
| 39 | 0. | A--SIMM_K0 | | 0. | 0. | -13.2028 |
| 39 | 0.2636 | A--SIMM_K0 | | 0. | 0. | -69.4842 |
| 39 | 0.5272 | A--SIMM_K0 | | 0. | 0. | -117.3833 |
| 39 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 6.2726 |
| 39 | 0.2636 | A-- SIMM_SOVR_K A | | 0. | 0. | 3.6313 |
| 39 | 0.5272 | A-- SIMM_SOVR_K A | | 0. | 0. | 0.9899 |
| 39 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 9.4042 |
| 39 | 0.2636 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 5.4442 |
| 39 | 0.5272 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 1.4841 |
| 39 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 9.4042 |
| 39 | 0.2636 | SIMM_SOVR_K 0 | | 0. | 0. | 5.4442 |
| 39 | 0.5272 | SIMM_SOVR_K 0 | | 0. | 0. | 1.4841 |
| 39 | 0. | SIMM_SOVR_K A | | 0. | 0. | 6.2726 |
| 39 | 0.2636 | SIMM_SOVR_K A | | 0. | 0. | 3.6313 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 39 | 0.5272 | SIMM_SOVR_K A | | 0. | 0. | 0.9899 |
| 39 | 0. | SOVR | | 0. | 0. | 114.3012 |
| 39 | 0.2636 | SOVR | | 0. | 0. | 121.74 |
| 39 | 0.5272 | SOVR | | 0. | 0. | 129.1788 |
| 39 | 0. | TERR_SIMM | | 0. | 0. | 469.6289 |
| 39 | 0.2636 | TERR_SIMM | | 0. | 0. | 492.1849 |
| 39 | 0.5272 | TERR_SIMM | | 0. | 0. | 514.7408 |
| 39 | 0. | TERR_A--SIMM | | 0. | 0. | 746.2353 |
| 39 | 0.2636 | TERR_A--SIMM | | 0. | 0. | 778.2021 |
| 39 | 0.5272 | TERR_A--SIMM | | 0. | 0. | 810.1688 |
| 39 | 0. | INERZIA H SLV | | 0. | 0. | 7.9659 |
| 39 | 0.2636 | INERZIA H SLV | | 0. | 0. | 8.523 |
| 39 | 0.5272 | INERZIA H SLV | | 0. | 0. | 9.0801 |
| 39 | 0. | INERZIA V + SLV | | 0. | 0. | 0.7446 |
| 39 | 0.2636 | INERZIA V + SLV | | 0. | 0. | 0.9765 |
| 39 | 0.5272 | INERZIA V + SLV | | 0. | 0. | 1.2084 |
| 39 | 0. | INERZIA V - SLV | | 0. | 0. | -0.7446 |
| 39 | 0.2636 | INERZIA V - SLV | | 0. | 0. | -0.9765 |
| 39 | 0.5272 | INERZIA V - SLV | | 0. | 0. | -1.2084 |
| 39 | 0. | SISMA WOOD SLV | | 0. | 0. | 300.0015 |
| 39 | 0.2636 | SISMA WOOD SLV | | 0. | 0. | 295.4796 |
| 39 | 0.5272 | SISMA WOOD SLV | | 0. | 0. | 295.8037 |
| 39 | 0. | iDROSTATICA | | 0. | 0. | 652.2268 |
| 39 | 0.2636 | iDROSTATICA | | 0. | 0. | 576.1075 |
| 39 | 0.5272 | iDROSTATICA | | 0. | 0. | 507.5975 |
| 39 | 0. | SISMA WOOD SLD | | 0. | 0. | 132.4928 |
| 39 | 0.2636 | SISMA WOOD SLD | | 0. | 0. | 130.4957 |
| 39 | 0.5272 | SISMA WOOD SLD | | 0. | 0. | 130.6388 |
| 39 | 0. | INERZIA H SLD | | 0. | 0. | 3.5181 |
| 39 | 0.2636 | INERZIA H SLD | | 0. | 0. | 3.7641 |
| 39 | 0.5272 | INERZIA H SLD | | 0. | 0. | 4.0101 |
| 39 | 0. | INERZIA V + SLD | | 0. | 0. | 0.3289 |
| 39 | 0.2636 | INERZIA V + SLD | | 0. | 0. | 0.4313 |
| 39 | 0.5272 | INERZIA V + SLD | | 0. | 0. | 0.5337 |
| 39 | 0. | INERZIA V SLD | | 0. | 0. | -0.3289 |
| 39 | 0.2636 | INERZIA V SLD | | 0. | 0. | -0.4313 |
| 39 | 0.5272 | INERZIA V SLD | | 0. | 0. | -0.5337 |
| 39 | 0. | INERZIA V -1 | | 0. | 0. | -0.7446 |
| 39 | 0.2636 | INERZIA V -1 | | 0. | 0. | -0.9765 |
| 39 | 0.5272 | INERZIA V -1 | | 0. | 0. | -1.2084 |
| 39 | 0. | SLU_1 | Max | 0. | 0. | 1747.4346 |
| 39 | 0.2636 | SLU_1 | Max | 0. | 0. | 1659.7289 |
| 39 | 0.5272 | SLU_1 | Max | 0. | 0. | 1588.7457 |
| 39 | 0. | SLU_1 | Min | 0. | 0. | 1747.4346 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 39 | 0.2636 | SLU_1 | Min | 0. | 0. | 1659.7289 |
| 39 | 0.5272 | SLU_1 | Min | 0. | 0. | 1588.7457 |
| 39 | 0. | SLU_2 | Max | 0. | 0. | 1825.0727 |
| 39 | 0.2636 | SLU_2 | Max | 0. | 0. | 1755.5266 |
| 39 | 0.5272 | SLU_2 | Max | 0. | 0. | 1700.4262 |
| 39 | 0. | SLU_2 | Min | 0. | 0. | 1825.0727 |
| 39 | 0.2636 | SLU_2 | Min | 0. | 0. | 1755.5266 |
| 39 | 0.5272 | SLU_2 | Min | 0. | 0. | 1700.4262 |
| 39 | 0. | SLU_3 | Max | 0. | 0. | 2409.0174 |
| 39 | 0.2636 | SLU_3 | Max | 0. | 0. | 2305.7374 |
| 39 | 0.5272 | SLU_3 | Max | 0. | 0. | 2223.2467 |
| 39 | 0. | SLU_3 | Min | 0. | 0. | 2409.0174 |
| 39 | 0.2636 | SLU_3 | Min | 0. | 0. | 2305.7374 |
| 39 | 0.5272 | SLU_3 | Min | 0. | 0. | 2223.2467 |
| 39 | 0. | SLU_4 | Max | 0. | 0. | 2402.0416 |
| 39 | 0.2636 | SLU_4 | Max | 0. | 0. | 2328.9381 |
| 39 | 0.5272 | SLU_4 | Max | 0. | 0. | 2272.8165 |
| 39 | 0. | SLU_4 | Min | 0. | 0. | 2402.0416 |
| 39 | 0.2636 | SLU_4 | Min | 0. | 0. | 2328.9381 |
| 39 | 0.5272 | SLU_4 | Min | 0. | 0. | 2272.8165 |
| 39 | 0. | SLE_F1 | Max | 0. | 0. | 1296.5581 |
| 39 | 0.2636 | SLE_F1 | Max | 0. | 0. | 1226.5333 |
| 39 | 0.5272 | SLE_F1 | Max | 0. | 0. | 1169.3721 |
| 39 | 0. | SLE_F1 | Min | 0. | 0. | 1296.5581 |
| 39 | 0.2636 | SLE_F1 | Min | 0. | 0. | 1226.5333 |
| 39 | 0.5272 | SLE_F1 | Min | 0. | 0. | 1169.3721 |
| 39 | 0. | SLE_F2 | Max | 0. | 0. | 1358.3698 |
| 39 | 0.2636 | SLE_F2 | Max | 0. | 0. | 1301.5952 |
| 39 | 0.5272 | SLE_F2 | Max | 0. | 0. | 1255.9327 |
| 39 | 0. | SLE_F2 | Min | 0. | 0. | 1358.3698 |
| 39 | 0.2636 | SLE_F2 | Min | 0. | 0. | 1301.5952 |
| 39 | 0.5272 | SLE_F2 | Min | 0. | 0. | 1255.9327 |
| 39 | 0. | SLE_F3 | Max | 0. | 0. | 1798.5082 |
| 39 | 0.2636 | SLE_F3 | Max | 0. | 0. | 1739.1539 |
| 39 | 0.5272 | SLE_F3 | Max | 0. | 0. | 1692.8626 |
| 39 | 0. | SLE_F3 | Min | 0. | 0. | 1798.5082 |
| 39 | 0.2636 | SLE_F3 | Min | 0. | 0. | 1739.1539 |
| 39 | 0.5272 | SLE_F3 | Min | 0. | 0. | 1692.8626 |
| 39 | 0. | SLE_F4 | Max | 0. | 0. | 1792.9562 |
| 39 | 0.2636 | SLE_F4 | Max | 0. | 0. | 1710.0347 |
| 39 | 0.5272 | SLE_F4 | Max | 0. | 0. | 1643.105 |
| 39 | 0. | SLE_F4 | Min | 0. | 0. | 1792.9562 |
| 39 | 0.2636 | SLE_F4 | Min | 0. | 0. | 1710.0347 |
| 39 | 0.5272 | SLE_F4 | Min | 0. | 0. | 1643.105 |
| 39 | 0. | SLE_QP1 | Max | 0. | 0. | 1211.7951 |
| 39 | 0.2636 | SLE_QP1 | Max | 0. | 0. | 1136.6882 |
| 39 | 0.5272 | SLE_QP1 | Max | 0. | 0. | 1074.4448 |
| 39 | 0. | SLE_QP1 | Min | 0. | 0. | 1211.7951 |
| 39 | 0.2636 | SLE_QP1 | Min | 0. | 0. | 1136.6882 |
| 39 | 0.5272 | SLE_QP1 | Min | 0. | 0. | 1074.4448 |
| 39 | 0. | SLE_QP2 | Max | 0. | 0. | 1273.8038 |
| 39 | 0.2636 | SLE_QP2 | Max | 0. | 0. | 1210.942 |
| 39 | 0.5272 | SLE_QP2 | Max | 0. | 0. | 1159.1922 |
| 39 | 0. | SLE_QP2 | Min | 0. | 0. | 1273.8038 |
| 39 | 0.2636 | SLE_QP2 | Min | 0. | 0. | 1210.942 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 39 | 0.5272 | SLE_QP2 | Min | 0. | 0. | 1159.1922 |
| 39 | 0. | SLE_QP3 | Max | 0. | 0. | 1707.1045 |
| 39 | 0.2636 | SLE_QP3 | Max | 0. | 0. | 1641.9545 |
| 39 | 0.5272 | SLE_QP3 | Max | 0. | 0. | 1589.8674 |
| 39 | 0. | SLE_QP3 | Min | 0. | 0. | 1707.1045 |
| 39 | 0.2636 | SLE_QP3 | Min | 0. | 0. | 1641.9545 |
| 39 | 0.5272 | SLE_QP3 | Min | 0. | 0. | 1589.8674 |
| 39 | 0. | SLE_QP4 | Max | 0. | 0. | 1678.7479 |
| 39 | 0.2636 | SLE_QP4 | Max | 0. | 0. | 1589.1768 |
| 39 | 0.5272 | SLE_QP4 | Max | 0. | 0. | 1515.5975 |
| 39 | 0. | SLE_QP4 | Min | 0. | 0. | 1678.7479 |
| 39 | 0.2636 | SLE_QP4 | Min | 0. | 0. | 1589.1768 |
| 39 | 0.5272 | SLE_QP4 | Min | 0. | 0. | 1515.5975 |
| 39 | 0. | SLV_1 | Max | 0. | 0. | 1216.016 |
| 39 | 0.2636 | SLV_1 | Max | 0. | 0. | 1065.2717 |
| 39 | 0.5272 | SLV_1 | Max | 0. | 0. | 932.2367 |
| 39 | 0. | SLV_1 | Min | 0. | 0. | 1216.016 |
| 39 | 0.2636 | SLV_1 | Min | 0. | 0. | 1065.2717 |
| 39 | 0.5272 | SLV_1 | Min | 0. | 0. | 932.2367 |
| 39 | 0. | SLV_2 | Max | 0. | 0. | 1212.6918 |
| 39 | 0.2636 | SLV_2 | Max | 0. | 0. | 1061.4011 |
| 39 | 0.5272 | SLV_2 | Max | 0. | 0. | 927.8198 |
| 39 | 0. | SLV_2 | Min | 0. | 0. | 1212.6918 |
| 39 | 0.2636 | SLV_2 | Min | 0. | 0. | 1061.4011 |
| 39 | 0.5272 | SLV_2 | Min | 0. | 0. | 927.8198 |
| 39 | 0. | SLV_3 | Max | 0. | 0. | 1571.6938 |
| 39 | 0.2636 | SLV_3 | Max | 0. | 0. | 1392.4233 |
| 39 | 0.5272 | SLV_3 | Max | 0. | 0. | 1233.9905 |
| 39 | 0. | SLV_3 | Min | 0. | 0. | 1571.6938 |
| 39 | 0.2636 | SLV_3 | Min | 0. | 0. | 1392.4233 |
| 39 | 0.5272 | SLV_3 | Min | 0. | 0. | 1233.9905 |
| 39 | 0. | SLV_4 | Max | 0. | 0. | 1567.3029 |
| 39 | 0.2636 | SLV_4 | Max | 0. | 0. | 1387.4796 |
| 39 | 0.5272 | SLV_4 | Max | 0. | 0. | 1228.4939 |
| 39 | 0. | SLV_4 | Min | 0. | 0. | 1567.3029 |
| 39 | 0.2636 | SLV_4 | Min | 0. | 0. | 1387.4796 |
| 39 | 0.5272 | SLV_4 | Min | 0. | 0. | 1228.4939 |
| 39 | 0. | SLD_1 | Max | 0. | 0. | 1283.4519 |
| 39 | 0.2636 | SLD_1 | Max | 0. | 0. | 1181.5764 |
| 39 | 0.5272 | SLD_1 | Max | 0. | 0. | 1094.7045 |
| 39 | 0. | SLD_1 | Min | 0. | 0. | 1283.4519 |
| 39 | 0.2636 | SLD_1 | Min | 0. | 0. | 1181.5764 |
| 39 | 0.5272 | SLD_1 | Min | 0. | 0. | 1094.7045 |
| 39 | 0. | SLD_2 | Max | 0. | 0. | 1283.2177 |
| 39 | 0.2636 | SLD_2 | Max | 0. | 0. | 1180.9991 |
| 39 | 0.5272 | SLD_2 | Max | 0. | 0. | 1093.7842 |
| 39 | 0. | SLD_2 | Min | 0. | 0. | 1283.2177 |
| 39 | 0.2636 | SLD_2 | Min | 0. | 0. | 1180.9991 |
| 39 | 0.5272 | SLD_2 | Min | 0. | 0. | 1093.7842 |
| 39 | 0. | SLD_3 | Max | 0. | 0. | 1619.055 |
| 39 | 0.2636 | SLD_3 | Max | 0. | 0. | 1488.6163 |
| 39 | 0.5272 | SLD_3 | Max | 0. | 0. | 1376.3095 |
| 39 | 0. | SLD_3 | Min | 0. | 0. | 1619.055 |
| 39 | 0.2636 | SLD_3 | Min | 0. | 0. | 1488.6163 |
| 39 | 0.5272 | SLD_3 | Min | 0. | 0. | 1376.3095 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 39 | 0. | SLD_4 | Max | 0. | 0. | 1617.3552 |
| 39 | 0.2636 | SLD_4 | Max | 0. | 0. | 1486.6471 |
| 39 | 0.5272 | SLD_4 | Max | 0. | 0. | 1374.0708 |
| 39 | 0. | SLD_4 | Min | 0. | 0. | 1617.3552 |
| 39 | 0.2636 | SLD_4 | Min | 0. | 0. | 1486.6471 |
| 39 | 0.5272 | SLD_4 | Min | 0. | 0. | 1374.0708 |
| 39 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1745.284 |
| 39 | 0.2636 | SLU_IDR_1 | Max | 0. | 0. | 1665.6595 |
| 39 | 0.5272 | SLU_IDR_1 | Max | 0. | 0. | 1599.3136 |
| 39 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1745.284 |
| 39 | 0.2636 | SLU_IDR_1 | Min | 0. | 0. | 1665.6595 |
| 39 | 0.5272 | SLU_IDR_1 | Min | 0. | 0. | 1599.3136 |
| 39 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1376.2354 |
| 39 | 0.2636 | SLU_IDR_2 | Max | 0. | 0. | 1297.5666 |
| 39 | 0.5272 | SLU_IDR_2 | Max | 0. | 0. | 1230.4207 |
| 39 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1376.2354 |
| 39 | 0.2636 | SLU_IDR_2 | Min | 0. | 0. | 1297.5666 |
| 39 | 0.5272 | SLU_IDR_2 | Min | 0. | 0. | 1230.4207 |
| 39 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -307.2717 |
| 39 | 0.2636 | SISMA WOOD SLV-1 | Max | 0. | 0. | -367.51 |
| 39 | 0.5272 | SISMA WOOD SLV-1 | Max | 0. | 0. | -422.9025 |
| 39 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -307.2717 |
| 39 | 0.2636 | SISMA WOOD SLV-1 | Min | 0. | 0. | -367.51 |
| 39 | 0.5272 | SISMA WOOD SLV-1 | Min | 0. | 0. | -422.9025 |
| 39 | 0. | DEAD-1 | Max | 0. | 0. | 80.702 |
| 39 | 0.2636 | DEAD-1 | Max | 0. | 0. | 98.521 |
| 39 | 0.5272 | DEAD-1 | Max | 0. | 0. | 116.34 |
| 39 | 0. | DEAD-1 | Min | 0. | 0. | 80.702 |
| 39 | 0.2636 | DEAD-1 | Min | 0. | 0. | 98.521 |
| 39 | 0.5272 | DEAD-1 | Min | 0. | 0. | 116.34 |
| 39 | 0. | SLU_PROVA | | 0. | 0. | 1567.5482 |
| 39 | 0.2636 | SLU_PROVA | | 0. | 0. | 1473.5244 |
| 39 | 0.5272 | SLU_PROVA | | 0. | 0. | 1396.223 |
| 41 | 0. | DEAD | | 0. | 0. | -18.5914 |
| 41 | 0.2636 | DEAD | | 0. | 0. | -32.5331 |
| 41 | 0.5272 | DEAD | | 0. | 0. | -46.4748 |
| 41 | 0. | SIMM_KA | | 0. | 0. | 16.87 |
| 41 | 0.2636 | SIMM_KA | | 0. | 0. | 47.0695 |
| 41 | 0.5272 | SIMM_KA | | 0. | 0. | 73.5123 |
| 41 | 0. | SIMM_K0 | | 0. | 0. | 21.9451 |
| 41 | 0.2636 | SIMM_K0 | | 0. | 0. | 67.6082 |
| 41 | 0.5272 | SIMM_K0 | | 0. | 0. | 107.6364 |
| 41 | 0. | A--SIMM_KA | | 0. | 0. | 101.8847 |
| 41 | 0.2636 | A--SIMM_KA | | 0. | 0. | 134.4032 |
| 41 | 0.5272 | A--SIMM_KA | | 0. | 0. | 163.5326 |
| 41 | 0. | A--SIMM_K0 | | 0. | 0. | 158.0898 |
| 41 | 0.2636 | A--SIMM_K0 | | 0. | 0. | 209.33 |
| 41 | 0.5272 | A--SIMM_K0 | | 0. | 0. | 255.2538 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 41 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -10.7509 |
| 41 | 0.2636 | A-- SIMM_SOVR_K A | | 0. | 0. | -8.3355 |
| 41 | 0.5272 | A-- SIMM_SOVR_K A | | 0. | 0. | -5.9201 |
| 41 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -16.1182 |
| 41 | 0.2636 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -12.497 |
| 41 | 0.5272 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -8.8757 |
| 41 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -16.1182 |
| 41 | 0.2636 | SIMM_SOVR_K 0 | | 0. | 0. | -12.497 |
| 41 | 0.5272 | SIMM_SOVR_K 0 | | 0. | 0. | -8.8757 |
| 41 | 0. | SIMM_SOVR_K A | | 0. | 0. | -10.7509 |
| 41 | 0.2636 | SIMM_SOVR_K A | | 0. | 0. | -8.3355 |
| 41 | 0.5272 | SIMM_SOVR_K A | | 0. | 0. | -5.9201 |
| 41 | 0. | SOVR | | 0. | 0. | -102.8208 |
| 41 | 0.2636 | SOVR | | 0. | 0. | -109.0345 |
| 41 | 0.5272 | SOVR | | 0. | 0. | -115.2481 |
| 41 | 0. | TERR_SIMM | | 0. | 0. | -436.9261 |
| 41 | 0.2636 | TERR_SIMM | | 0. | 0. | -455.2141 |
| 41 | 0.5272 | TERR_SIMM | | 0. | 0. | -473.502 |
| 41 | 0. | TERR_A--SIMM | | 0. | 0. | -412.829 |
| 41 | 0.2636 | TERR_A--SIMM | | 0. | 0. | -434.14 |
| 41 | 0.5272 | TERR_A--SIMM | | 0. | 0. | -455.4511 |
| 41 | 0. | INERZIA H SLV | | 0. | 0. | 5.8504 |
| 41 | 0.2636 | INERZIA H SLV | | 0. | 0. | 6.9703 |
| 41 | 0.5272 | INERZIA H SLV | | 0. | 0. | 8.0903 |
| 41 | 0. | INERZIA V + SLV | | 0. | 0. | -0.3366 |
| 41 | 0.2636 | INERZIA V + SLV | | 0. | 0. | -0.5565 |
| 41 | 0.5272 | INERZIA V + SLV | | 0. | 0. | -0.7764 |
| 41 | 0. | INERZIA V - SLV | | 0. | 0. | 0.3366 |
| 41 | 0.2636 | INERZIA V - SLV | | 0. | 0. | 0.5565 |
| 41 | 0.5272 | INERZIA V - SLV | | 0. | 0. | 0.7764 |
| 41 | 0. | SISMA WOOD SLV | | 0. | 0. | 299.8121 |
| 41 | 0.2636 | SISMA WOOD SLV | | 0. | 0. | 360.9786 |
| 41 | 0.5272 | SISMA WOOD SLV | | 0. | 0. | 422.1451 |
| 41 | 0. | iDROSTATICA | | 0. | 0. | -840.1183 |
| 41 | 0.2636 | iDROSTATICA | | 0. | 0. | -745.4288 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 41 | 0.5272 | iDROSTATICA | | 0. | 0. | -658.7254 |
| 41 | 0. | SISMA WOOD SLD | | 0. | 0. | 132.4091 |
| 41 | 0.2636 | SISMA WOOD SLD | | 0. | 0. | 159.4227 |
| 41 | 0.5272 | SISMA WOOD SLD | | 0. | 0. | 186.4363 |
| 41 | 0. | INERZIA H SLD | | 0. | 0. | 2.5838 |
| 41 | 0.2636 | INERZIA H SLD | | 0. | 0. | 3.0784 |
| 41 | 0.5272 | INERZIA H SLD | | 0. | 0. | 3.573 |
| 41 | 0. | INERZIA V + SLD | | 0. | 0. | -0.1487 |
| 41 | 0.2636 | INERZIA V + SLD | | 0. | 0. | -0.2458 |
| 41 | 0.5272 | INERZIA V + SLD | | 0. | 0. | -0.3429 |
| 41 | 0. | INERZIA V SLD | | 0. | 0. | 0.1487 |
| 41 | 0.2636 | INERZIA V SLD | | 0. | 0. | 0.2458 |
| 41 | 0.5272 | INERZIA V SLD | | 0. | 0. | 0.3429 |
| 41 | 0. | INERZIA V -1 | | 0. | 0. | 0.3366 |
| 41 | 0.2636 | INERZIA V -1 | | 0. | 0. | 0.5565 |
| 41 | 0.5272 | INERZIA V -1 | | 0. | 0. | 0.7764 |
| 41 | 0. | SLU_1 | Max | 0. | 0. | -2022.9514 |
| 41 | 0.2636 | SLU_1 | Max | 0. | 0. | -1890.0838 |
| 41 | 0.5272 | SLU_1 | Max | 0. | 0. | -1774.9236 |
| 41 | 0. | SLU_1 | Min | 0. | 0. | -2022.9514 |
| 41 | 0.2636 | SLU_1 | Min | 0. | 0. | -1890.0838 |
| 41 | 0.5272 | SLU_1 | Min | 0. | 0. | -1774.9236 |
| 41 | 0. | SLU_2 | Max | 0. | 0. | -2060.0854 |
| 41 | 0.2636 | SLU_2 | Max | 0. | 0. | -1948.2957 |
| 41 | 0.5272 | SLU_2 | Max | 0. | 0. | -1851.7719 |
| 41 | 0. | SLU_2 | Min | 0. | 0. | -2060.0854 |
| 41 | 0.2636 | SLU_2 | Min | 0. | 0. | -1948.2957 |
| 41 | 0.5272 | SLU_2 | Min | 0. | 0. | -1851.7719 |
| 41 | 0. | SLU_3 | Max | 0. | 0. | -1600.1116 |
| 41 | 0.2636 | SLU_3 | Max | 0. | 0. | -1468.1994 |
| 41 | 0.5272 | SLU_3 | Max | 0. | 0. | -1353.5804 |
| 41 | 0. | SLU_3 | Min | 0. | 0. | -1600.1116 |
| 41 | 0.2636 | SLU_3 | Min | 0. | 0. | -1468.1994 |
| 41 | 0.5272 | SLU_3 | Min | 0. | 0. | -1353.5804 |
| 41 | 0. | SLU_4 | Max | 0. | 0. | -1752.5673 |
| 41 | 0.2636 | SLU_4 | Max | 0. | 0. | -1646.8223 |
| 41 | 0.5272 | SLU_4 | Max | 0. | 0. | -1555.8653 |
| 41 | 0. | SLU_4 | Min | 0. | 0. | -1752.5673 |
| 41 | 0.2636 | SLU_4 | Min | 0. | 0. | -1646.8223 |
| 41 | 0.5272 | SLU_4 | Min | 0. | 0. | -1555.8653 |
| 41 | 0. | SLE_F1 | Max | 0. | 0. | -1511.5634 |
| 41 | 0.2636 | SLE_F1 | Max | 0. | 0. | -1407.1578 |
| 41 | 0.5272 | SLE_F1 | Max | 0. | 0. | -1316.3734 |
| 41 | 0. | SLE_F1 | Min | 0. | 0. | -1511.5634 |
| 41 | 0.2636 | SLE_F1 | Min | 0. | 0. | -1407.1578 |
| 41 | 0.5272 | SLE_F1 | Min | 0. | 0. | -1316.3734 |
| 41 | 0. | SLE_F2 | Max | 0. | 0. | -1544.5553 |
| 41 | 0.2636 | SLE_F2 | Max | 0. | 0. | -1455.724 |
| 41 | 0.5272 | SLE_F2 | Max | 0. | 0. | -1378.6357 |
| 41 | 0. | SLE_F2 | Min | 0. | 0. | -1544.5553 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 41 | 0.2636 | SLE_F2 | Min | 0. | 0. | -1455.724 |
| 41 | 0.5272 | SLE_F2 | Min | 0. | 0. | -1378.6357 |
| 41 | 0. | SLE_F3 | Max | 0. | 0. | -1306.7929 |
| 41 | 0.2636 | SLE_F3 | Max | 0. | 0. | -1222.7649 |
| 41 | 0.5272 | SLE_F3 | Max | 0. | 0. | -1150.1123 |
| 41 | 0. | SLE_F3 | Min | 0. | 0. | -1306.7929 |
| 41 | 0.2636 | SLE_F3 | Min | 0. | 0. | -1222.7649 |
| 41 | 0.5272 | SLE_F3 | Min | 0. | 0. | -1150.1123 |
| 41 | 0. | SLE_F4 | Max | 0. | 0. | -1181.4948 |
| 41 | 0.2636 | SLE_F4 | Max | 0. | 0. | -1076.833 |
| 41 | 0.5272 | SLE_F4 | Max | 0. | 0. | -985.4737 |
| 41 | 0. | SLE_F4 | Min | 0. | 0. | -1181.4948 |
| 41 | 0.2636 | SLE_F4 | Min | 0. | 0. | -1076.833 |
| 41 | 0.5272 | SLE_F4 | Min | 0. | 0. | -985.4737 |
| 41 | 0. | SLE_QP1 | Max | 0. | 0. | -1435.3165 |
| 41 | 0.2636 | SLE_QP1 | Max | 0. | 0. | -1326.5187 |
| 41 | 0.5272 | SLE_QP1 | Max | 0. | 0. | -1231.342 |
| 41 | 0. | SLE_QP1 | Min | 0. | 0. | -1435.3165 |
| 41 | 0.2636 | SLE_QP1 | Min | 0. | 0. | -1326.5187 |
| 41 | 0.5272 | SLE_QP1 | Min | 0. | 0. | -1231.342 |
| 41 | 0. | SLE_QP2 | Max | 0. | 0. | -1470.0431 |
| 41 | 0.2636 | SLE_QP2 | Max | 0. | 0. | -1375.9377 |
| 41 | 0.5272 | SLE_QP2 | Max | 0. | 0. | -1293.5753 |
| 41 | 0. | SLE_QP2 | Min | 0. | 0. | -1470.0431 |
| 41 | 0.2636 | SLE_QP2 | Min | 0. | 0. | -1375.9377 |
| 41 | 0.5272 | SLE_QP2 | Min | 0. | 0. | -1293.5753 |
| 41 | 0. | SLE_QP3 | Max | 0. | 0. | -1230.0275 |
| 41 | 0.2636 | SLE_QP3 | Max | 0. | 0. | -1141.0119 |
| 41 | 0.5272 | SLE_QP3 | Max | 0. | 0. | -1063.3716 |
| 41 | 0. | SLE_QP3 | Min | 0. | 0. | -1230.0275 |
| 41 | 0.2636 | SLE_QP3 | Min | 0. | 0. | -1141.0119 |
| 41 | 0.5272 | SLE_QP3 | Min | 0. | 0. | -1063.3716 |
| 41 | 0. | SLE_QP4 | Max | 0. | 0. | -1090.5469 |
| 41 | 0.2636 | SLE_QP4 | Max | 0. | 0. | -979.7483 |
| 41 | 0.5272 | SLE_QP4 | Max | 0. | 0. | -882.2521 |
| 41 | 0. | SLE_QP4 | Min | 0. | 0. | -1090.5469 |
| 41 | 0.2636 | SLE_QP4 | Min | 0. | 0. | -979.7483 |
| 41 | 0.5272 | SLE_QP4 | Min | 0. | 0. | -882.2521 |
| 41 | 0. | SLV_1 | Max | 0. | 0. | -703.2725 |
| 41 | 0.2636 | SLV_1 | Max | 0. | 0. | -456.7711 |
| 41 | 0.5272 | SLV_1 | Max | 0. | 0. | -223.8909 |
| 41 | 0. | SLV_1 | Min | 0. | 0. | -703.2725 |
| 41 | 0.2636 | SLV_1 | Min | 0. | 0. | -456.7711 |
| 41 | 0.5272 | SLV_1 | Min | 0. | 0. | -223.8909 |
| 41 | 0. | SLV_2 | Max | 0. | 0. | -704.2096 |
| 41 | 0.2636 | SLV_2 | Max | 0. | 0. | -457.0191 |
| 41 | 0.5272 | SLV_2 | Max | 0. | 0. | -223.4497 |
| 41 | 0. | SLV_2 | Min | 0. | 0. | -704.2096 |
| 41 | 0.2636 | SLV_2 | Min | 0. | 0. | -457.0191 |
| 41 | 0.5272 | SLV_2 | Min | 0. | 0. | -223.4497 |
| 41 | 0. | SLV_3 | Max | 0. | 0. | -458.0544 |
| 41 | 0.2636 | SLV_3 | Max | 0. | 0. | -190.54 |
| 41 | 0.5272 | SLV_3 | Max | 0. | 0. | 63.6719 |
| 41 | 0. | SLV_3 | Min | 0. | 0. | -458.0544 |
| 41 | 0.2636 | SLV_3 | Min | 0. | 0. | -190.54 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 41 | 0.5272 | SLV_3 | Min | 0. | 0. | 63.6719 |
| 41 | 0. | SLV_4 | Max | 0. | 0. | -458.1617 |
| 41 | 0.2636 | SLV_4 | Max | 0. | 0. | -190.0089 |
| 41 | 0.5272 | SLV_4 | Max | 0. | 0. | 64.8413 |
| 41 | 0. | SLV_4 | Min | 0. | 0. | -458.1617 |
| 41 | 0.2636 | SLV_4 | Min | 0. | 0. | -190.0089 |
| 41 | 0.5272 | SLV_4 | Min | 0. | 0. | 64.8413 |
| 41 | 0. | SLD_1 | Max | 0. | 0. | -1039.0712 |
| 41 | 0.2636 | SLD_1 | Max | 0. | 0. | -880.1215 |
| 41 | 0.5272 | SLD_1 | Max | 0. | 0. | -734.7929 |
| 41 | 0. | SLD_1 | Min | 0. | 0. | -1039.0712 |
| 41 | 0.2636 | SLD_1 | Min | 0. | 0. | -880.1215 |
| 41 | 0.5272 | SLD_1 | Min | 0. | 0. | -734.7929 |
| 41 | 0. | SLD_2 | Max | 0. | 0. | -1040.1905 |
| 41 | 0.2636 | SLD_2 | Max | 0. | 0. | -880.8809 |
| 41 | 0.5272 | SLD_2 | Max | 0. | 0. | -735.1924 |
| 41 | 0. | SLD_2 | Min | 0. | 0. | -1040.1905 |
| 41 | 0.2636 | SLD_2 | Min | 0. | 0. | -880.8809 |
| 41 | 0.5272 | SLD_2 | Min | 0. | 0. | -735.1924 |
| 41 | 0. | SLD_3 | Max | 0. | 0. | -763.2144 |
| 41 | 0.2636 | SLD_3 | Max | 0. | 0. | -583.2206 |
| 41 | 0.5272 | SLD_3 | Max | 0. | 0. | -416.5294 |
| 41 | 0. | SLD_3 | Min | 0. | 0. | -763.2144 |
| 41 | 0.2636 | SLD_3 | Min | 0. | 0. | -583.2206 |
| 41 | 0.5272 | SLD_3 | Min | 0. | 0. | -416.5294 |
| 41 | 0. | SLD_4 | Max | 0. | 0. | -763.3066 |
| 41 | 0.2636 | SLD_4 | Max | 0. | 0. | -583.0379 |
| 41 | 0.5272 | SLD_4 | Max | 0. | 0. | -416.0717 |
| 41 | 0. | SLD_4 | Min | 0. | 0. | -763.3066 |
| 41 | 0.2636 | SLD_4 | Min | 0. | 0. | -583.0379 |
| 41 | 0.5272 | SLD_4 | Min | 0. | 0. | -416.0717 |
| 41 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1379.111 |
| 41 | 0.2636 | SLU_IDR_1 | Max | 0. | 0. | -1273.3996 |
| 41 | 0.5272 | SLU_IDR_1 | Max | 0. | 0. | -1179.5233 |
| 41 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1379.111 |
| 41 | 0.2636 | SLU_IDR_1 | Min | 0. | 0. | -1273.3996 |
| 41 | 0.5272 | SLU_IDR_1 | Min | 0. | 0. | -1179.5233 |
| 41 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1604.4846 |
| 41 | 0.2636 | SLU_IDR_2 | Max | 0. | 0. | -1493.1229 |
| 41 | 0.5272 | SLU_IDR_2 | Max | 0. | 0. | -1393.9272 |
| 41 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1604.4846 |
| 41 | 0.2636 | SLU_IDR_2 | Min | 0. | 0. | -1493.1229 |
| 41 | 0.5272 | SLU_IDR_2 | Min | 0. | 0. | -1393.9272 |
| 41 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 623.6429 |
| 41 | 0.2636 | SISMA WOOD SLV-1 | Max | 0. | 0. | 767.3925 |
| 41 | 0.5272 | SISMA WOOD SLV-1 | Max | 0. | 0. | 911.142 |
| 41 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 623.6429 |
| 41 | 0.2636 | SISMA WOOD SLV-1 | Min | 0. | 0. | 767.3925 |
| 41 | 0.5272 | SISMA WOOD SLV-1 | Min | 0. | 0. | 911.142 |
| 41 | 0. | DEAD-1 | Max | 0. | 0. | -50.0385 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 41 | 0.2636 | DEAD-1 | Max | 0. | 0. | -66.627 |
| 41 | 0.5272 | DEAD-1 | Max | 0. | 0. | -83.2154 |
| 41 | 0. | DEAD-1 | Min | 0. | 0. | -50.0385 |
| 41 | 0.2636 | DEAD-1 | Min | 0. | 0. | -66.627 |
| 41 | 0.5272 | DEAD-1 | Min | 0. | 0. | -83.2154 |
| 41 | 0. | SLU_PROVA | | 0. | 0. | -1834.2065 |
| 41 | 0.2636 | SLU_PROVA | | 0. | 0. | -1697.5352 |
| 41 | 0.5272 | SLU_PROVA | | 0. | 0. | -1578.5712 |
| 42 | 0. | DEAD | | 0. | 0. | -46.4748 |
| 42 | 0.2636 | DEAD | | 0. | 0. | -61.2028 |
| 42 | 0.5272 | DEAD | | 0. | 0. | -75.9307 |
| 42 | 0. | SIMM_KA | | 0. | 0. | 73.5123 |
| 42 | 0.2636 | SIMM_KA | | 0. | 0. | 98.2472 |
| 42 | 0.5272 | SIMM_KA | | 0. | 0. | 119.4794 |
| 42 | 0. | SIMM_K0 | | 0. | 0. | 107.6364 |
| 42 | 0.2636 | SIMM_K0 | | 0. | 0. | 145.152 |
| 42 | 0.5272 | SIMM_K0 | | 0. | 0. | 177.4135 |
| 42 | 0. | A--SIMM_KA | | 0. | 0. | 163.5326 |
| 42 | 0.2636 | A--SIMM_KA | | 0. | 0. | 187.4142 |
| 42 | 0.5272 | A--SIMM_KA | | 0. | 0. | 208.4716 |
| 42 | 0. | A--SIMM_K0 | | 0. | 0. | 255.2538 |
| 42 | 0.2636 | A--SIMM_K0 | | 0. | 0. | 293.1906 |
| 42 | 0.5272 | A--SIMM_K0 | | 0. | 0. | 326.2346 |
| 42 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -5.9201 |
| 42 | 0.2636 | A-- SIMM_SOVR_K A | | 0. | 0. | -3.2765 |
| 42 | 0.5272 | A-- SIMM_SOVR_K A | | 0. | 0. | -0.6329 |
| 42 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -8.8757 |
| 42 | 0.2636 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -4.9123 |
| 42 | 0.5272 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -0.9489 |
| 42 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -8.8757 |
| 42 | 0.2636 | SIMM_SOVR_K 0 | | 0. | 0. | -4.9123 |
| 42 | 0.5272 | SIMM_SOVR_K 0 | | 0. | 0. | -0.9489 |
| 42 | 0. | SIMM_SOVR_K A | | 0. | 0. | -5.9201 |
| 42 | 0.2636 | SIMM_SOVR_K A | | 0. | 0. | -3.2765 |
| 42 | 0.5272 | SIMM_SOVR_K A | | 0. | 0. | -0.6329 |
| 42 | 0. | SOVR | | 0. | 0. | -115.2481 |
| 42 | 0.2636 | SOVR | | 0. | 0. | -122.7455 |
| 42 | 0.5272 | SOVR | | 0. | 0. | -130.2429 |
| 42 | 0. | TERR_SIMM | | 0. | 0. | -473.502 |
| 42 | 0.2636 | TERR_SIMM | | 0. | 0. | -496.3036 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 42 | 0.5272 | TERR_SIMM | | 0. | 0. | -519.1051 |
| 42 | 0. | TERR_A--SIMM | | 0. | 0. | -455.4511 |
| 42 | 0.2636 | TERR_A--SIMM | | 0. | 0. | -482.6278 |
| 42 | 0.5272 | TERR_A--SIMM | | 0. | 0. | -509.8045 |
| 42 | 0. | INERZIA H SLV | | 0. | 0. | 8.0903 |
| 42 | 0.2636 | INERZIA H SLV | | 0. | 0. | 8.6386 |
| 42 | 0.5272 | INERZIA H SLV | | 0. | 0. | 9.187 |
| 42 | 0. | INERZIA V + SLV | | 0. | 0. | -0.7764 |
| 42 | 0.2636 | INERZIA V + SLV | | 0. | 0. | -1.009 |
| 42 | 0.5272 | INERZIA V + SLV | | 0. | 0. | -1.2416 |
| 42 | 0. | INERZIA V - SLV | | 0. | 0. | 0.7764 |
| 42 | 0.2636 | INERZIA V - SLV | | 0. | 0. | 1.009 |
| 42 | 0.5272 | INERZIA V - SLV | | 0. | 0. | 1.2416 |
| 42 | 0. | SISMA WOOD SLV | | 0. | 0. | 422.1451 |
| 42 | 0.2636 | SISMA WOOD SLV | | 0. | 0. | 459.4565 |
| 42 | 0.5272 | SISMA WOOD SLV | | 0. | 0. | 496.768 |
| 42 | 0. | IDROSTATICA | | 0. | 0. | -658.7254 |
| 42 | 0.2636 | IDROSTATICA | | 0. | 0. | -582.2531 |
| 42 | 0.5272 | IDROSTATICA | | 0. | 0. | -513.3901 |
| 42 | 0. | SISMA WOOD SLD | | 0. | 0. | 186.4363 |
| 42 | 0.2636 | SISMA WOOD SLD | | 0. | 0. | 202.9145 |
| 42 | 0.5272 | SISMA WOOD SLD | | 0. | 0. | 219.3928 |
| 42 | 0. | INERZIA H SLD | | 0. | 0. | 3.573 |
| 42 | 0.2636 | INERZIA H SLD | | 0. | 0. | 3.8152 |
| 42 | 0.5272 | INERZIA H SLD | | 0. | 0. | 4.0573 |
| 42 | 0. | INERZIA V + SLD | | 0. | 0. | -0.3429 |
| 42 | 0.2636 | INERZIA V + SLD | | 0. | 0. | -0.4456 |
| 42 | 0.5272 | INERZIA V + SLD | | 0. | 0. | -0.5483 |
| 42 | 0. | INERZIA V SLD | | 0. | 0. | 0.3429 |
| 42 | 0.2636 | INERZIA V SLD | | 0. | 0. | 0.4456 |
| 42 | 0.5272 | INERZIA V SLD | | 0. | 0. | 0.5483 |
| 42 | 0. | INERZIA V -1 | | 0. | 0. | 0.7764 |
| 42 | 0.2636 | INERZIA V -1 | | 0. | 0. | 1.009 |
| 42 | 0.5272 | INERZIA V -1 | | 0. | 0. | 1.2416 |
| 42 | 0. | SLU_1 | Max | 0. | 0. | -1774.9236 |
| 42 | 0.2636 | SLU_1 | Max | 0. | 0. | -1686.6457 |
| 42 | 0.5272 | SLU_1 | Max | 0. | 0. | -1615.0903 |
| 42 | 0. | SLU_1 | Min | 0. | 0. | -1774.9236 |
| 42 | 0.2636 | SLU_1 | Min | 0. | 0. | -1686.6457 |
| 42 | 0.5272 | SLU_1 | Min | 0. | 0. | -1615.0903 |
| 42 | 0. | SLU_2 | Max | 0. | 0. | -1851.7719 |
| 42 | 0.2636 | SLU_2 | Max | 0. | 0. | -1781.8078 |
| 42 | 0.5272 | SLU_2 | Max | 0. | 0. | -1726.2894 |
| 42 | 0. | SLU_2 | Min | 0. | 0. | -1851.7719 |
| 42 | 0.2636 | SLU_2 | Min | 0. | 0. | -1781.8078 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 42 | 0.5272 | SLU_2 | Min | 0. | 0. | -1726.2894 |
| 42 | 0. | SLU_3 | Max | 0. | 0. | -1353.5804 |
| 42 | 0.2636 | SLU_3 | Max | 0. | 0. | -1277.3071 |
| 42 | 0.5272 | SLU_3 | Max | 0. | 0. | -1217.2866 |
| 42 | 0. | SLU_3 | Min | 0. | 0. | -1353.5804 |
| 42 | 0.2636 | SLU_3 | Min | 0. | 0. | -1277.3071 |
| 42 | 0.5272 | SLU_3 | Min | 0. | 0. | -1217.2866 |
| 42 | 0. | SLU_4 | Max | 0. | 0. | -1555.8653 |
| 42 | 0.2636 | SLU_4 | Max | 0. | 0. | -1499.5132 |
| 42 | 0.5272 | SLU_4 | Max | 0. | 0. | -1456.7248 |
| 42 | 0. | SLU_4 | Min | 0. | 0. | -1555.8653 |
| 42 | 0.2636 | SLU_4 | Min | 0. | 0. | -1499.5132 |
| 42 | 0.5272 | SLU_4 | Min | 0. | 0. | -1456.7248 |
| 42 | 0. | SLE_F1 | Max | 0. | 0. | -1316.3734 |
| 42 | 0.2636 | SLE_F1 | Max | 0. | 0. | -1245.8692 |
| 42 | 0.5272 | SLE_F1 | Max | 0. | 0. | -1188.2285 |
| 42 | 0. | SLE_F1 | Min | 0. | 0. | -1316.3734 |
| 42 | 0.2636 | SLE_F1 | Min | 0. | 0. | -1245.8692 |
| 42 | 0.5272 | SLE_F1 | Min | 0. | 0. | -1188.2285 |
| 42 | 0. | SLE_F2 | Max | 0. | 0. | -1378.6357 |
| 42 | 0.2636 | SLE_F2 | Max | 0. | 0. | -1321.5274 |
| 42 | 0.5272 | SLE_F2 | Max | 0. | 0. | -1275.5313 |
| 42 | 0. | SLE_F2 | Min | 0. | 0. | -1378.6357 |
| 42 | 0.2636 | SLE_F2 | Min | 0. | 0. | -1321.5274 |
| 42 | 0.5272 | SLE_F2 | Min | 0. | 0. | -1275.5313 |
| 42 | 0. | SLE_F3 | Max | 0. | 0. | -1150.1123 |
| 42 | 0.2636 | SLE_F3 | Max | 0. | 0. | -1103.5844 |
| 42 | 0.5272 | SLE_F3 | Max | 0. | 0. | -1067.4901 |
| 42 | 0. | SLE_F3 | Min | 0. | 0. | -1150.1123 |
| 42 | 0.2636 | SLE_F3 | Min | 0. | 0. | -1103.5844 |
| 42 | 0.5272 | SLE_F3 | Min | 0. | 0. | -1067.4901 |
| 42 | 0. | SLE_F4 | Max | 0. | 0. | -985.4737 |
| 42 | 0.2636 | SLE_F4 | Max | 0. | 0. | -923.5074 |
| 42 | 0.5272 | SLE_F4 | Max | 0. | 0. | -874.0433 |
| 42 | 0. | SLE_F4 | Min | 0. | 0. | -985.4737 |
| 42 | 0.2636 | SLE_F4 | Min | 0. | 0. | -923.5074 |
| 42 | 0.5272 | SLE_F4 | Min | 0. | 0. | -874.0433 |
| 42 | 0. | SLE_QP1 | Max | 0. | 0. | -1231.342 |
| 42 | 0.2636 | SLE_QP1 | Max | 0. | 0. | -1155.7253 |
| 42 | 0.5272 | SLE_QP1 | Max | 0. | 0. | -1092.9722 |
| 42 | 0. | SLE_QP1 | Min | 0. | 0. | -1231.342 |
| 42 | 0.2636 | SLE_QP1 | Min | 0. | 0. | -1155.7253 |
| 42 | 0.5272 | SLE_QP1 | Min | 0. | 0. | -1092.9722 |
| 42 | 0. | SLE_QP2 | Max | 0. | 0. | -1293.5753 |
| 42 | 0.2636 | SLE_QP2 | Max | 0. | 0. | -1230.356 |
| 42 | 0.5272 | SLE_QP2 | Max | 0. | 0. | -1178.2489 |
| 42 | 0. | SLE_QP2 | Min | 0. | 0. | -1293.5753 |
| 42 | 0.2636 | SLE_QP2 | Min | 0. | 0. | -1230.356 |
| 42 | 0.5272 | SLE_QP2 | Min | 0. | 0. | -1178.2489 |
| 42 | 0. | SLE_QP3 | Max | 0. | 0. | -1063.3716 |
| 42 | 0.2636 | SLE_QP3 | Max | 0. | 0. | -1010.9377 |
| 42 | 0.5272 | SLE_QP3 | Max | 0. | 0. | -968.9374 |
| 42 | 0. | SLE_QP3 | Min | 0. | 0. | -1063.3716 |
| 42 | 0.2636 | SLE_QP3 | Min | 0. | 0. | -1010.9377 |
| 42 | 0.5272 | SLE_QP3 | Min | 0. | 0. | -968.9374 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 42 | 0. | SLE_QP4 | Max | 0. | 0. | -882.2521 |
| 42 | 0.2636 | SLE_QP4 | Max | 0. | 0. | -814.0066 |
| 42 | 0.5272 | SLE_QP4 | Max | 0. | 0. | -758.2634 |
| 42 | 0. | SLE_QP4 | Min | 0. | 0. | -882.2521 |
| 42 | 0.2636 | SLE_QP4 | Min | 0. | 0. | -814.0066 |
| 42 | 0.5272 | SLE_QP4 | Min | 0. | 0. | -758.2634 |
| 42 | 0. | SLV_1 | Max | 0. | 0. | -223.8909 |
| 42 | 0.2636 | SLV_1 | Max | 0. | 0. | -60.7164 |
| 42 | 0.5272 | SLV_1 | Max | 0. | 0. | 89.5946 |
| 42 | 0. | SLV_1 | Min | 0. | 0. | -223.8909 |
| 42 | 0.2636 | SLV_1 | Min | 0. | 0. | -60.7164 |
| 42 | 0.5272 | SLV_1 | Min | 0. | 0. | 89.5946 |
| 42 | 0. | SLV_2 | Max | 0. | 0. | -223.4497 |
| 42 | 0.2636 | SLV_2 | Max | 0. | 0. | -59.5834 |
| 42 | 0.5272 | SLV_2 | Max | 0. | 0. | 91.4194 |
| 42 | 0. | SLV_2 | Min | 0. | 0. | -223.4497 |
| 42 | 0.2636 | SLV_2 | Min | 0. | 0. | -59.5834 |
| 42 | 0.5272 | SLV_2 | Min | 0. | 0. | 91.4194 |
| 42 | 0. | SLV_3 | Max | 0. | 0. | 63.6719 |
| 42 | 0.2636 | SLV_3 | Max | 0. | 0. | 234.2141 |
| 42 | 0.5272 | SLV_3 | Max | 0. | 0. | 392.2542 |
| 42 | 0. | SLV_3 | Min | 0. | 0. | 63.6719 |
| 42 | 0.2636 | SLV_3 | Min | 0. | 0. | 234.2141 |
| 42 | 0.5272 | SLV_3 | Min | 0. | 0. | 392.2542 |
| 42 | 0. | SLV_4 | Max | 0. | 0. | 64.8413 |
| 42 | 0.2636 | SLV_4 | Max | 0. | 0. | 236.035 |
| 42 | 0.5272 | SLV_4 | Max | 0. | 0. | 394.7265 |
| 42 | 0. | SLV_4 | Min | 0. | 0. | 64.8413 |
| 42 | 0.2636 | SLV_4 | Min | 0. | 0. | 236.035 |
| 42 | 0.5272 | SLV_4 | Min | 0. | 0. | 394.7265 |
| 42 | 0. | SLD_1 | Max | 0. | 0. | -734.7929 |
| 42 | 0.2636 | SLD_1 | Max | 0. | 0. | -628.7984 |
| 42 | 0.5272 | SLD_1 | Max | 0. | 0. | -535.6674 |
| 42 | 0. | SLD_1 | Min | 0. | 0. | -734.7929 |
| 42 | 0.2636 | SLD_1 | Min | 0. | 0. | -628.7984 |
| 42 | 0.5272 | SLD_1 | Min | 0. | 0. | -535.6674 |
| 42 | 0. | SLD_2 | Max | 0. | 0. | -735.1924 |
| 42 | 0.2636 | SLD_2 | Max | 0. | 0. | -628.8333 |
| 42 | 0.5272 | SLD_2 | Max | 0. | 0. | -535.3377 |
| 42 | 0. | SLD_2 | Min | 0. | 0. | -735.1924 |
| 42 | 0.2636 | SLD_2 | Min | 0. | 0. | -628.8333 |
| 42 | 0.5272 | SLD_2 | Min | 0. | 0. | -535.3377 |
| 42 | 0. | SLD_3 | Max | 0. | 0. | -416.5294 |
| 42 | 0.2636 | SLD_3 | Max | 0. | 0. | -303.2682 |
| 42 | 0.5272 | SLD_3 | Max | 0. | 0. | -202.5092 |
| 42 | 0. | SLD_3 | Min | 0. | 0. | -416.5294 |
| 42 | 0.2636 | SLD_3 | Min | 0. | 0. | -303.2682 |
| 42 | 0.5272 | SLD_3 | Min | 0. | 0. | -202.5092 |
| 42 | 0. | SLD_4 | Max | 0. | 0. | -416.0717 |
| 42 | 0.2636 | SLD_4 | Max | 0. | 0. | -302.5243 |
| 42 | 0.5272 | SLD_4 | Max | 0. | 0. | -201.479 |
| 42 | 0. | SLD_4 | Min | 0. | 0. | -416.0717 |
| 42 | 0.2636 | SLD_4 | Min | 0. | 0. | -302.5243 |
| 42 | 0.5272 | SLD_4 | Min | 0. | 0. | -201.479 |
| 42 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1179.5233 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 42 | 0.2636 | SLU_IDR_1 | Max | 0. | 0. | -1110.9167 |
| 42 | 0.5272 | SLU_IDR_1 | Max | 0. | 0. | -1053.2223 |
| 42 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1179.5233 |
| 42 | 0.2636 | SLU_IDR_1 | Min | 0. | 0. | -1110.9167 |
| 42 | 0.5272 | SLU_IDR_1 | Min | 0. | 0. | -1053.2223 |
| 42 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1393.9272 |
| 42 | 0.2636 | SLU_IDR_2 | Max | 0. | 0. | -1314.7926 |
| 42 | 0.5272 | SLU_IDR_2 | Max | 0. | 0. | -1247.1809 |
| 42 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1393.9272 |
| 42 | 0.2636 | SLU_IDR_2 | Min | 0. | 0. | -1314.7926 |
| 42 | 0.5272 | SLU_IDR_2 | Min | 0. | 0. | -1247.1809 |
| 42 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 911.142 |
| 42 | 0.2636 | SISMA WOOD SLV-1 | Max | 0. | 0. | 1003.9104 |
| 42 | 0.5272 | SISMA WOOD SLV-1 | Max | 0. | 0. | 1096.6788 |
| 42 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 911.142 |
| 42 | 0.2636 | SISMA WOOD SLV-1 | Min | 0. | 0. | 1003.9104 |
| 42 | 0.5272 | SISMA WOOD SLV-1 | Min | 0. | 0. | 1096.6788 |
| 42 | 0. | DEAD-1 | Max | 0. | 0. | -83.2154 |
| 42 | 0.2636 | DEAD-1 | Max | 0. | 0. | -101.071 |
| 42 | 0.5272 | DEAD-1 | Max | 0. | 0. | -118.9266 |
| 42 | 0. | DEAD-1 | Min | 0. | 0. | -83.2154 |
| 42 | 0.2636 | DEAD-1 | Min | 0. | 0. | -101.071 |
| 42 | 0.5272 | DEAD-1 | Min | 0. | 0. | -118.9266 |
| 42 | 0. | SLU_PROVA | | 0. | 0. | -1578.5712 |
| 42 | 0.2636 | SLU_PROVA | | 0. | 0. | -1484.4762 |
| 42 | 0.5272 | SLU_PROVA | | 0. | 0. | -1407.1038 |
| 43 | 0. | DEAD | | 0. | 0. | -98.2378 |
| 43 | 0.13945 | DEAD | | 0. | 0. | -89.6902 |
| 43 | 0.27891 | DEAD | | 0. | 0. | -81.8716 |
| 43 | 0. | SIMM_KA | | 0. | 0. | 40.1239 |
| 43 | 0.13945 | SIMM_KA | | 0. | 0. | 44.6149 |
| 43 | 0.27891 | SIMM_KA | | 0. | 0. | 49.1059 |
| 43 | 0. | SIMM_K0 | | 0. | 0. | 64.0528 |
| 43 | 0.13945 | SIMM_K0 | | 0. | 0. | 70.909 |
| 43 | 0.27891 | SIMM_K0 | | 0. | 0. | 77.7651 |
| 43 | 0. | A--SIMM_KA | | 0. | 0. | 151.0592 |
| 43 | 0.13945 | A--SIMM_KA | | 0. | 0. | 155.8173 |
| 43 | 0.27891 | A--SIMM_KA | | 0. | 0. | 160.5755 |
| 43 | 0. | A--SIMM_K0 | | 0. | 0. | 226.8757 |
| 43 | 0.13945 | A--SIMM_K0 | | 0. | 0. | 234.2775 |
| 43 | 0.27891 | A--SIMM_K0 | | 0. | 0. | 241.6794 |
| 43 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 13.809 |
| 43 | 0.13945 | A-- SIMM_SOVR_K A | | 0. | 0. | 14.3437 |
| 43 | 0.27891 | A-- SIMM_SOVR_K A | | 0. | 0. | 14.8785 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 43 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.7031 |
| 43 | 0.13945 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 21.5048 |
| 43 | 0.27891 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 22.3066 |
| 43 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 20.7031 |
| 43 | 0.13945 | SIMM_SOVR_K 0 | | 0. | 0. | 21.5048 |
| 43 | 0.27891 | SIMM_SOVR_K 0 | | 0. | 0. | 22.3066 |
| 43 | 0. | SIMM_SOVR_K A | | 0. | 0. | 13.809 |
| 43 | 0.13945 | SIMM_SOVR_K A | | 0. | 0. | 14.3437 |
| 43 | 0.27891 | SIMM_SOVR_K A | | 0. | 0. | 14.8785 |
| 43 | 0. | SOVR | | 0. | 0. | 28.4671 |
| 43 | 0.13945 | SOVR | | 0. | 0. | 38.7455 |
| 43 | 0.27891 | SOVR | | 0. | 0. | 49.0239 |
| 43 | 0. | TERR_SIMM | | 0. | 0. | 148.5302 |
| 43 | 0.13945 | TERR_SIMM | | 0. | 0. | 190.7973 |
| 43 | 0.27891 | TERR_SIMM | | 0. | 0. | 233.0644 |
| 43 | 0. | TERR_A--SIMM | | 0. | 0. | 245.8664 |
| 43 | 0.13945 | TERR_A--SIMM | | 0. | 0. | 311.8975 |
| 43 | 0.27891 | TERR_A--SIMM | | 0. | 0. | 377.9286 |
| 43 | 0. | INERZIA H SLV | | 0. | 0. | 4.3834 |
| 43 | 0.13945 | INERZIA H SLV | | 0. | 0. | 3.9577 |
| 43 | 0.27891 | INERZIA H SLV | | 0. | 0. | 3.532 |
| 43 | 0. | INERZIA V + SLV | | 0. | 0. | -1.5406 |
| 43 | 0.13945 | INERZIA V + SLV | | 0. | 0. | -1.4084 |
| 43 | 0.27891 | INERZIA V + SLV | | 0. | 0. | -1.2763 |
| 43 | 0. | INERZIA V - SLV | | 0. | 0. | 1.5406 |
| 43 | 0.13945 | INERZIA V - SLV | | 0. | 0. | 1.4084 |
| 43 | 0.27891 | INERZIA V - SLV | | 0. | 0. | 1.2763 |
| 43 | 0. | SISMA WOOD SLV | | 0. | 0. | 259.9177 |
| 43 | 0.13945 | SISMA WOOD SLV | | 0. | 0. | 250.2061 |
| 43 | 0.27891 | SISMA WOOD SLV | | 0. | 0. | 240.4946 |
| 43 | 0. | iDROSTATICA | | 0. | 0. | 786.0646 |
| 43 | 0.13945 | iDROSTATICA | | 0. | 0. | 859.8245 |
| 43 | 0.27891 | iDROSTATICA | | 0. | 0. | 935.9778 |
| 43 | 0. | SISMA WOOD SLD | | 0. | 0. | 114.7902 |
| 43 | 0.13945 | SISMA WOOD SLD | | 0. | 0. | 110.5011 |
| 43 | 0.27891 | SISMA WOOD SLD | | 0. | 0. | 106.2121 |
| 43 | 0. | INERZIA H SLD | | 0. | 0. | 1.9359 |
| 43 | 0.13945 | INERZIA H SLD | | 0. | 0. | 1.7479 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 43 | 0.27891 | INERZIA H SLD | | 0. | 0. | 1.5599 |
| 43 | 0. | INERZIA V + SLD | | 0. | 0. | -0.6804 |
| 43 | 0.13945 | INERZIA V + SLD | | 0. | 0. | -0.622 |
| 43 | 0.27891 | INERZIA V + SLD | | 0. | 0. | -0.5637 |
| 43 | 0. | INERZIA V SLD | | 0. | 0. | 0.6804 |
| 43 | 0.13945 | INERZIA V SLD | | 0. | 0. | 0.622 |
| 43 | 0.27891 | INERZIA V SLD | | 0. | 0. | 0.5637 |
| 43 | 0. | INERZIA V -1 | | 0. | 0. | 1.5406 |
| 43 | 0.13945 | INERZIA V -1 | | 0. | 0. | 1.4084 |
| 43 | 0.27891 | INERZIA V -1 | | 0. | 0. | 1.2763 |
| 43 | 0. | SLU_1 | Max | 0. | 0. | 1338.9198 |
| 43 | 0.13945 | SLU_1 | Max | 0. | 0. | 1539.4017 |
| 43 | 0.27891 | SLU_1 | Max | 0. | 0. | 1742.0472 |
| 43 | 0. | SLU_1 | Min | 0. | 0. | 1338.9198 |
| 43 | 0.13945 | SLU_1 | Min | 0. | 0. | 1539.4017 |
| 43 | 0.27891 | SLU_1 | Min | 0. | 0. | 1742.0472 |
| 43 | 0. | SLU_2 | Max | 0. | 0. | 1335.0476 |
| 43 | 0.13945 | SLU_2 | Max | 0. | 0. | 1533.8944 |
| 43 | 0.27891 | SLU_2 | Max | 0. | 0. | 1734.9048 |
| 43 | 0. | SLU_2 | Min | 0. | 0. | 1335.0476 |
| 43 | 0.13945 | SLU_2 | Min | 0. | 0. | 1533.8944 |
| 43 | 0.27891 | SLU_2 | Min | 0. | 0. | 1734.9048 |
| 43 | 0. | SLU_3 | Max | 0. | 0. | 1832.6616 |
| 43 | 0.13945 | SLU_3 | Max | 0. | 0. | 2070.1018 |
| 43 | 0.27891 | SLU_3 | Max | 0. | 0. | 2309.7057 |
| 43 | 0. | SLU_3 | Min | 0. | 0. | 1832.6616 |
| 43 | 0.13945 | SLU_3 | Min | 0. | 0. | 2070.1018 |
| 43 | 0.27891 | SLU_3 | Min | 0. | 0. | 2309.7057 |
| 43 | 0. | SLU_4 | Max | 0. | 0. | 1706.7419 |
| 43 | 0.13945 | SLU_4 | Max | 0. | 0. | 1940.6507 |
| 43 | 0.27891 | SLU_4 | Max | 0. | 0. | 2176.7232 |
| 43 | 0. | SLU_4 | Min | 0. | 0. | 1706.7419 |
| 43 | 0.13945 | SLU_4 | Min | 0. | 0. | 1940.6507 |
| 43 | 0.27891 | SLU_4 | Min | 0. | 0. | 2176.7232 |
| 43 | 0. | SLE_F1 | Max | 0. | 0. | 1019.3268 |
| 43 | 0.13945 | SLE_F1 | Max | 0. | 0. | 1168.9011 |
| 43 | 0.27891 | SLE_F1 | Max | 0. | 0. | 1320.1398 |
| 43 | 0. | SLE_F1 | Min | 0. | 0. | 1019.3268 |
| 43 | 0.13945 | SLE_F1 | Min | 0. | 0. | 1168.9011 |
| 43 | 0.27891 | SLE_F1 | Min | 0. | 0. | 1320.1398 |
| 43 | 0. | SLE_F2 | Max | 0. | 0. | 1020.8028 |
| 43 | 0.13945 | SLE_F2 | Max | 0. | 0. | 1169.2392 |
| 43 | 0.27891 | SLE_F2 | Max | 0. | 0. | 1319.34 |
| 43 | 0. | SLE_F2 | Min | 0. | 0. | 1020.8028 |
| 43 | 0.13945 | SLE_F2 | Min | 0. | 0. | 1169.2392 |
| 43 | 0.27891 | SLE_F2 | Min | 0. | 0. | 1319.34 |
| 43 | 0. | SLE_F3 | Max | 0. | 0. | 1302.9011 |
| 43 | 0.13945 | SLE_F3 | Max | 0. | 0. | 1478.131 |
| 43 | 0.27891 | SLE_F3 | Max | 0. | 0. | 1655.0253 |
| 43 | 0. | SLE_F3 | Min | 0. | 0. | 1302.9011 |
| 43 | 0.13945 | SLE_F3 | Min | 0. | 0. | 1478.131 |
| 43 | 0.27891 | SLE_F3 | Min | 0. | 0. | 1655.0253 |
| 43 | 0. | SLE_F4 | Max | 0. | 0. | 1392.8037 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 43 | 0.13945 | SLE_F4 | Max | 0. | 0. | 1570.6322 |
| 43 | 0.27891 | SLE_F4 | Max | 0. | 0. | 1750.125 |
| 43 | 0. | SLE_F4 | Min | 0. | 0. | 1392.8037 |
| 43 | 0.13945 | SLE_F4 | Min | 0. | 0. | 1570.6322 |
| 43 | 0.27891 | SLE_F4 | Min | 0. | 0. | 1750.125 |
| 43 | 0. | SLE_QP1 | Max | 0. | 0. | 1004.6737 |
| 43 | 0.13945 | SLE_QP1 | Max | 0. | 0. | 1145.7414 |
| 43 | 0.27891 | SLE_QP1 | Max | 0. | 0. | 1288.4734 |
| 43 | 0. | SLE_QP1 | Min | 0. | 0. | 1004.6737 |
| 43 | 0.13945 | SLE_QP1 | Min | 0. | 0. | 1145.7414 |
| 43 | 0.27891 | SLE_QP1 | Min | 0. | 0. | 1288.4734 |
| 43 | 0. | SLE_QP2 | Max | 0. | 0. | 1009.3649 |
| 43 | 0.13945 | SLE_QP2 | Max | 0. | 0. | 1149.4022 |
| 43 | 0.27891 | SLE_QP2 | Max | 0. | 0. | 1291.1039 |
| 43 | 0. | SLE_QP2 | Min | 0. | 0. | 1009.3649 |
| 43 | 0.13945 | SLE_QP2 | Min | 0. | 0. | 1149.4022 |
| 43 | 0.27891 | SLE_QP2 | Min | 0. | 0. | 1291.1039 |
| 43 | 0. | SLE_QP3 | Max | 0. | 0. | 1284.3694 |
| 43 | 0.13945 | SLE_QP3 | Max | 0. | 0. | 1450.8708 |
| 43 | 0.27891 | SLE_QP3 | Max | 0. | 0. | 1619.0365 |
| 43 | 0. | SLE_QP3 | Min | 0. | 0. | 1284.3694 |
| 43 | 0.13945 | SLE_QP3 | Min | 0. | 0. | 1450.8708 |
| 43 | 0.27891 | SLE_QP3 | Min | 0. | 0. | 1619.0365 |
| 43 | 0. | SLE_QP4 | Max | 0. | 0. | 1360.1525 |
| 43 | 0.13945 | SLE_QP4 | Max | 0. | 0. | 1529.0303 |
| 43 | 0.27891 | SLE_QP4 | Max | 0. | 0. | 1699.5724 |
| 43 | 0. | SLE_QP4 | Min | 0. | 0. | 1360.1525 |
| 43 | 0.13945 | SLE_QP4 | Min | 0. | 0. | 1529.0303 |
| 43 | 0.27891 | SLE_QP4 | Min | 0. | 0. | 1699.5724 |
| 43 | 0. | SLV_1 | Max | 0. | 0. | 1334.4515 |
| 43 | 0.13945 | SLV_1 | Max | 0. | 0. | 1476.0521 |
| 43 | 0.27891 | SLV_1 | Max | 0. | 0. | 1619.3171 |
| 43 | 0. | SLV_1 | Min | 0. | 0. | 1334.4515 |
| 43 | 0.13945 | SLV_1 | Min | 0. | 0. | 1476.0521 |
| 43 | 0.27891 | SLV_1 | Min | 0. | 0. | 1619.3171 |
| 43 | 0. | SLV_2 | Max | 0. | 0. | 1336.2452 |
| 43 | 0.13945 | SLV_2 | Max | 0. | 0. | 1477.6431 |
| 43 | 0.27891 | SLV_2 | Max | 0. | 0. | 1620.7053 |
| 43 | 0. | SLV_2 | Min | 0. | 0. | 1336.2452 |
| 43 | 0.13945 | SLV_2 | Min | 0. | 0. | 1477.6431 |
| 43 | 0.27891 | SLV_2 | Min | 0. | 0. | 1620.7053 |
| 43 | 0. | SLV_3 | Max | 0. | 0. | 1666.9583 |
| 43 | 0.13945 | SLV_3 | Max | 0. | 0. | 1838.1491 |
| 43 | 0.27891 | SLV_3 | Max | 0. | 0. | 2011.0044 |
| 43 | 0. | SLV_3 | Min | 0. | 0. | 1666.9583 |
| 43 | 0.13945 | SLV_3 | Min | 0. | 0. | 1838.1491 |
| 43 | 0.27891 | SLV_3 | Min | 0. | 0. | 2011.0044 |
| 43 | 0. | SLV_4 | Max | 0. | 0. | 1667.9634 |
| 43 | 0.13945 | SLV_4 | Max | 0. | 0. | 1838.8738 |
| 43 | 0.27891 | SLV_4 | Max | 0. | 0. | 2011.4485 |
| 43 | 0. | SLV_4 | Min | 0. | 0. | 1667.9634 |
| 43 | 0.13945 | SLV_4 | Min | 0. | 0. | 1838.8738 |
| 43 | 0.27891 | SLV_4 | Min | 0. | 0. | 2011.4485 |
| 43 | 0. | SLD_1 | Max | 0. | 0. | 1179.4478 |
| 43 | 0.13945 | SLD_1 | Max | 0. | 0. | 1318.6219 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 43 | 0.27891 | SLD_1 | Max | 0. | 0. | 1459.4603 |
| 43 | 0. | SLD_1 | Min | 0. | 0. | 1179.4478 |
| 43 | 0.13945 | SLD_1 | Min | 0. | 0. | 1318.6219 |
| 43 | 0.27891 | SLD_1 | Min | 0. | 0. | 1459.4603 |
| 43 | 0. | SLD_2 | Max | 0. | 0. | 1181.9683 |
| 43 | 0.13945 | SLD_2 | Max | 0. | 0. | 1321.0398 |
| 43 | 0.27891 | SLD_2 | Max | 0. | 0. | 1461.7756 |
| 43 | 0. | SLD_2 | Min | 0. | 0. | 1181.9683 |
| 43 | 0.13945 | SLD_2 | Min | 0. | 0. | 1321.0398 |
| 43 | 0.27891 | SLD_2 | Min | 0. | 0. | 1461.7756 |
| 43 | 0. | SLD_3 | Max | 0. | 0. | 1493.5859 |
| 43 | 0.13945 | SLD_3 | Max | 0. | 0. | 1662.0122 |
| 43 | 0.27891 | SLD_3 | Max | 0. | 0. | 1832.1029 |
| 43 | 0. | SLD_3 | Min | 0. | 0. | 1493.5859 |
| 43 | 0.13945 | SLD_3 | Min | 0. | 0. | 1662.0122 |
| 43 | 0.27891 | SLD_3 | Min | 0. | 0. | 1832.1029 |
| 43 | 0. | SLD_4 | Max | 0. | 0. | 1494.4708 |
| 43 | 0.13945 | SLD_4 | Max | 0. | 0. | 1662.7409 |
| 43 | 0.27891 | SLD_4 | Max | 0. | 0. | 1832.6753 |
| 43 | 0. | SLD_4 | Min | 0. | 0. | 1494.4708 |
| 43 | 0.13945 | SLD_4 | Min | 0. | 0. | 1662.7409 |
| 43 | 0.27891 | SLD_4 | Min | 0. | 0. | 1832.6753 |
| 43 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1411.8598 |
| 43 | 0.13945 | SLU_IDR_1 | Max | 0. | 0. | 1579.6664 |
| 43 | 0.27891 | SLU_IDR_1 | Max | 0. | 0. | 1749.4496 |
| 43 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1411.8598 |
| 43 | 0.13945 | SLU_IDR_1 | Min | 0. | 0. | 1579.6664 |
| 43 | 0.27891 | SLU_IDR_1 | Min | 0. | 0. | 1749.4496 |
| 43 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1185.5871 |
| 43 | 0.13945 | SLU_IDR_2 | Max | 0. | 0. | 1330.9263 |
| 43 | 0.27891 | SLU_IDR_2 | Max | 0. | 0. | 1478.2421 |
| 43 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1185.5871 |
| 43 | 0.13945 | SLU_IDR_2 | Min | 0. | 0. | 1330.9263 |
| 43 | 0.27891 | SLU_IDR_2 | Min | 0. | 0. | 1478.2421 |
| 43 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -33.3399 |
| 43 | 0.13945 | SISMA WOOD SLV-1 | Max | 0. | 0. | -29.4542 |
| 43 | 0.27891 | SISMA WOOD SLV-1 | Max | 0. | 0. | -25.5686 |
| 43 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -33.3399 |
| 43 | 0.13945 | SISMA WOOD SLV-1 | Min | 0. | 0. | -29.4542 |
| 43 | 0.27891 | SISMA WOOD SLV-1 | Min | 0. | 0. | -25.5686 |
| 43 | 0. | DEAD-1 | Max | 0. | 0. | -92.4818 |
| 43 | 0.13945 | DEAD-1 | Max | 0. | 0. | -80.6454 |
| 43 | 0.27891 | DEAD-1 | Max | 0. | 0. | -69.538 |
| 43 | 0. | DEAD-1 | Min | 0. | 0. | -92.4818 |
| 43 | 0.13945 | DEAD-1 | Min | 0. | 0. | -80.6454 |
| 43 | 0.27891 | DEAD-1 | Min | 0. | 0. | -69.538 |
| 43 | 0. | SLU_PROVA | | 0. | 0. | 1244.2882 |
| 43 | 0.13945 | SLU_PROVA | | 0. | 0. | 1431.7684 |
| 43 | 0.27891 | SLU_PROVA | | 0. | 0. | 1621.4122 |
| 44 | 0. | DEAD | | 0. | 0. | -81.8716 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 44 | 0.13945 | DEAD | | 0. | 0. | -45.346 |
| 44 | 0.27891 | DEAD | | 0. | 0. | -9.5495 |
| 44 | 0. | SIMM_KA | | 0. | 0. | 49.1059 |
| 44 | 0.13945 | SIMM_KA | | 0. | 0. | 52.0073 |
| 44 | 0.27891 | SIMM_KA | | 0. | 0. | 54.9088 |
| 44 | 0. | SIMM_K0 | | 0. | 0. | 77.7651 |
| 44 | 0.13945 | SIMM_K0 | | 0. | 0. | 82.197 |
| 44 | 0.27891 | SIMM_K0 | | 0. | 0. | 86.6289 |
| 44 | 0. | A--SIMM_KA | | 0. | 0. | 160.5755 |
| 44 | 0.13945 | A--SIMM_KA | | 0. | 0. | 160.5285 |
| 44 | 0.27891 | A--SIMM_KA | | 0. | 0. | 160.4816 |
| 44 | 0. | A--SIMM_K0 | | 0. | 0. | 241.6794 |
| 44 | 0.13945 | A--SIMM_K0 | | 0. | 0. | 241.7897 |
| 44 | 0.27891 | A--SIMM_K0 | | 0. | 0. | 241.9 |
| 44 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 14.8785 |
| 44 | 0.13945 | A-- SIMM_SOVR_K A | | 0. | 0. | 15.2414 |
| 44 | 0.27891 | A-- SIMM_SOVR_K A | | 0. | 0. | 15.6044 |
| 44 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 22.3066 |
| 44 | 0.13945 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 22.8507 |
| 44 | 0.27891 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 23.3948 |
| 44 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 22.3066 |
| 44 | 0.13945 | SIMM_SOVR_K 0 | | 0. | 0. | 22.8507 |
| 44 | 0.27891 | SIMM_SOVR_K 0 | | 0. | 0. | 23.3948 |
| 44 | 0. | SIMM_SOVR_K A | | 0. | 0. | 14.8785 |
| 44 | 0.13945 | SIMM_SOVR_K A | | 0. | 0. | 15.2414 |
| 44 | 0.27891 | SIMM_SOVR_K A | | 0. | 0. | 15.6044 |
| 44 | 0. | SOVR | | 0. | 0. | 49.0239 |
| 44 | 0.13945 | SOVR | | 0. | 0. | 70.4404 |
| 44 | 0.27891 | SOVR | | 0. | 0. | 91.8569 |
| 44 | 0. | TERR_SIMM | | 0. | 0. | 233.0644 |
| 44 | 0.13945 | TERR_SIMM | | 0. | 0. | 319.171 |
| 44 | 0.27891 | TERR_SIMM | | 0. | 0. | 405.2775 |
| 44 | 0. | TERR_A--SIMM | | 0. | 0. | 377.9286 |
| 44 | 0.13945 | TERR_A--SIMM | | 0. | 0. | 514.5312 |
| 44 | 0.27891 | TERR_A--SIMM | | 0. | 0. | 651.1337 |
| 44 | 0. | INERZIA H SLV | | 0. | 0. | 3.532 |
| 44 | 0.13945 | INERZIA H SLV | | 0. | 0. | 2.9335 |
| 44 | 0.27891 | INERZIA H SLV | | 0. | 0. | 2.335 |
| 44 | 0. | INERZIA V + SLV | | 0. | 0. | -1.2763 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 44 | 0.13945 | INERZIA V + SLV | | 0. | 0. | -0.6919 |
| 44 | 0.27891 | INERZIA V + SLV | | 0. | 0. | -0.1075 |
| 44 | 0. | INERZIA V - SLV | | 0. | 0. | 1.2763 |
| 44 | 0.13945 | INERZIA V - SLV | | 0. | 0. | 0.6919 |
| 44 | 0.27891 | INERZIA V - SLV | | 0. | 0. | 0.1075 |
| 44 | 0. | SISMA WOOD SLV | | 0. | 0. | 240.4946 |
| 44 | 0.13945 | SISMA WOOD SLV | | 0. | 0. | 220.0416 |
| 44 | 0.27891 | SISMA WOOD SLV | | 0. | 0. | 199.5886 |
| 44 | 0. | iDROSTATICA | | 0. | 0. | 935.9778 |
| 44 | 0.13945 | iDROSTATICA | | 0. | 0. | 993.106 |
| 44 | 0.27891 | iDROSTATICA | | 0. | 0. | 1052.6276 |
| 44 | 0. | SISMA WOOD SLD | | 0. | 0. | 106.2121 |
| 44 | 0.13945 | SISMA WOOD SLD | | 0. | 0. | 97.1793 |
| 44 | 0.27891 | SISMA WOOD SLD | | 0. | 0. | 88.1464 |
| 44 | 0. | INERZIA H SLD | | 0. | 0. | 1.5599 |
| 44 | 0.13945 | INERZIA H SLD | | 0. | 0. | 1.2955 |
| 44 | 0.27891 | INERZIA H SLD | | 0. | 0. | 1.0312 |
| 44 | 0. | INERZIA V + SLD | | 0. | 0. | -0.5637 |
| 44 | 0.13945 | INERZIA V + SLD | | 0. | 0. | -0.3056 |
| 44 | 0.27891 | INERZIA V + SLD | | 0. | 0. | -0.0475 |
| 44 | 0. | INERZIA V SLD | | 0. | 0. | 0.5637 |
| 44 | 0.13945 | INERZIA V SLD | | 0. | 0. | 0.3056 |
| 44 | 0.27891 | INERZIA V SLD | | 0. | 0. | 0.0475 |
| 44 | 0. | INERZIA V -1 | | 0. | 0. | 1.2763 |
| 44 | 0.13945 | INERZIA V -1 | | 0. | 0. | 0.6919 |
| 44 | 0.27891 | INERZIA V -1 | | 0. | 0. | 0.1075 |
| 44 | 0. | SLU_1 | Max | 0. | 0. | 1742.0472 |
| 44 | 0.13945 | SLU_1 | Max | 0. | 0. | 2037.7977 |
| 44 | 0.27891 | SLU_1 | Max | 0. | 0. | 2335.7118 |
| 44 | 0. | SLU_1 | Min | 0. | 0. | 1742.0472 |
| 44 | 0.13945 | SLU_1 | Min | 0. | 0. | 2037.7977 |
| 44 | 0.27891 | SLU_1 | Min | 0. | 0. | 2335.7118 |
| 44 | 0. | SLU_2 | Max | 0. | 0. | 1734.9048 |
| 44 | 0.13945 | SLU_2 | Max | 0. | 0. | 2029.925 |
| 44 | 0.27891 | SLU_2 | Max | 0. | 0. | 2327.1088 |
| 44 | 0. | SLU_2 | Min | 0. | 0. | 1734.9048 |
| 44 | 0.13945 | SLU_2 | Min | 0. | 0. | 2029.925 |
| 44 | 0.27891 | SLU_2 | Min | 0. | 0. | 2327.1088 |
| 44 | 0. | SLU_3 | Max | 0. | 0. | 2309.7057 |
| 44 | 0.13945 | SLU_3 | Max | 0. | 0. | 2674.0832 |
| 44 | 0.27891 | SLU_3 | Max | 0. | 0. | 3040.6243 |
| 44 | 0. | SLU_3 | Min | 0. | 0. | 2309.7057 |
| 44 | 0.13945 | SLU_3 | Min | 0. | 0. | 2674.0832 |
| 44 | 0.27891 | SLU_3 | Min | 0. | 0. | 3040.6243 |
| 44 | 0. | SLU_4 | Max | 0. | 0. | 2176.7232 |
| 44 | 0.13945 | SLU_4 | Max | 0. | 0. | 2540.9372 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 44 | 0.27891 | SLU_4 | Max | 0. | 0. | 2907.3148 |
| 44 | 0. | SLU_4 | Min | 0. | 0. | 2176.7232 |
| 44 | 0.13945 | SLU_4 | Min | 0. | 0. | 2540.9372 |
| 44 | 0.27891 | SLU_4 | Min | 0. | 0. | 2907.3148 |
| 44 | 0. | SLE_F1 | Max | 0. | 0. | 1320.1398 |
| 44 | 0.13945 | SLE_F1 | Max | 0. | 0. | 1537.689 |
| 44 | 0.27891 | SLE_F1 | Max | 0. | 0. | 1756.9026 |
| 44 | 0. | SLE_F1 | Min | 0. | 0. | 1320.1398 |
| 44 | 0.13945 | SLE_F1 | Min | 0. | 0. | 1537.689 |
| 44 | 0.27891 | SLE_F1 | Min | 0. | 0. | 1756.9026 |
| 44 | 0. | SLE_F2 | Max | 0. | 0. | 1319.34 |
| 44 | 0.13945 | SLE_F2 | Max | 0. | 0. | 1536.3707 |
| 44 | 0.27891 | SLE_F2 | Max | 0. | 0. | 1755.0658 |
| 44 | 0. | SLE_F2 | Min | 0. | 0. | 1319.34 |
| 44 | 0.13945 | SLE_F2 | Min | 0. | 0. | 1536.3707 |
| 44 | 0.27891 | SLE_F2 | Min | 0. | 0. | 1755.0658 |
| 44 | 0. | SLE_F3 | Max | 0. | 0. | 1655.0253 |
| 44 | 0.13945 | SLE_F3 | Max | 0. | 0. | 1925.2257 |
| 44 | 0.27891 | SLE_F3 | Max | 0. | 0. | 2197.0904 |
| 44 | 0. | SLE_F3 | Min | 0. | 0. | 1655.0253 |
| 44 | 0.13945 | SLE_F3 | Min | 0. | 0. | 1925.2257 |
| 44 | 0.27891 | SLE_F3 | Min | 0. | 0. | 2197.0904 |
| 44 | 0. | SLE_F4 | Max | 0. | 0. | 1750.125 |
| 44 | 0.13945 | SLE_F4 | Max | 0. | 0. | 2020.4308 |
| 44 | 0.27891 | SLE_F4 | Max | 0. | 0. | 2292.4009 |
| 44 | 0. | SLE_F4 | Min | 0. | 0. | 1750.125 |
| 44 | 0.13945 | SLE_F4 | Min | 0. | 0. | 2020.4308 |
| 44 | 0.27891 | SLE_F4 | Min | 0. | 0. | 2292.4009 |
| 44 | 0. | SLE_QP1 | Max | 0. | 0. | 1288.4734 |
| 44 | 0.13945 | SLE_QP1 | Max | 0. | 0. | 1487.5566 |
| 44 | 0.27891 | SLE_QP1 | Max | 0. | 0. | 1688.304 |
| 44 | 0. | SLE_QP1 | Min | 0. | 0. | 1288.4734 |
| 44 | 0.13945 | SLE_QP1 | Min | 0. | 0. | 1487.5566 |
| 44 | 0.27891 | SLE_QP1 | Min | 0. | 0. | 1688.304 |
| 44 | 0. | SLE_QP2 | Max | 0. | 0. | 1291.1039 |
| 44 | 0.13945 | SLE_QP2 | Max | 0. | 0. | 1489.7343 |
| 44 | 0.27891 | SLE_QP2 | Max | 0. | 0. | 1690.0291 |
| 44 | 0. | SLE_QP2 | Min | 0. | 0. | 1291.1039 |
| 44 | 0.13945 | SLE_QP2 | Min | 0. | 0. | 1489.7343 |
| 44 | 0.27891 | SLE_QP2 | Min | 0. | 0. | 1690.0291 |
| 44 | 0. | SLE_QP3 | Max | 0. | 0. | 1619.0365 |
| 44 | 0.13945 | SLE_QP3 | Max | 0. | 0. | 1870.7319 |
| 44 | 0.27891 | SLE_QP3 | Max | 0. | 0. | 2124.0916 |
| 44 | 0. | SLE_QP3 | Min | 0. | 0. | 1619.0365 |
| 44 | 0.13945 | SLE_QP3 | Min | 0. | 0. | 1870.7319 |
| 44 | 0.27891 | SLE_QP3 | Min | 0. | 0. | 2124.0916 |
| 44 | 0. | SLE_QP4 | Max | 0. | 0. | 1699.5724 |
| 44 | 0.13945 | SLE_QP4 | Max | 0. | 0. | 1951.3506 |
| 44 | 0.27891 | SLE_QP4 | Max | 0. | 0. | 2204.7931 |
| 44 | 0. | SLE_QP4 | Min | 0. | 0. | 1699.5724 |
| 44 | 0.13945 | SLE_QP4 | Min | 0. | 0. | 1951.3506 |
| 44 | 0.27891 | SLE_QP4 | Min | 0. | 0. | 2204.7931 |
| 44 | 0. | SLV_1 | Max | 0. | 0. | 1619.3171 |
| 44 | 0.13945 | SLV_1 | Max | 0. | 0. | 1811.1004 |
| 44 | 0.27891 | SLV_1 | Max | 0. | 0. | 2004.548 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 44 | 0. | SLV_1 | Min | 0. | 0. | 1619.3171 |
| 44 | 0.13945 | SLV_1 | Min | 0. | 0. | 1811.1004 |
| 44 | 0.27891 | SLV_1 | Min | 0. | 0. | 2004.548 |
| 44 | 0. | SLV_2 | Max | 0. | 0. | 1620.7053 |
| 44 | 0.13945 | SLV_2 | Max | 0. | 0. | 1811.2252 |
| 44 | 0.27891 | SLV_2 | Max | 0. | 0. | 2003.4095 |
| 44 | 0. | SLV_2 | Min | 0. | 0. | 1620.7053 |
| 44 | 0.13945 | SLV_2 | Min | 0. | 0. | 1811.2252 |
| 44 | 0.27891 | SLV_2 | Min | 0. | 0. | 2003.4095 |
| 44 | 0. | SLV_3 | Max | 0. | 0. | 2011.0044 |
| 44 | 0.13945 | SLV_3 | Max | 0. | 0. | 2257.6851 |
| 44 | 0.27891 | SLV_3 | Max | 0. | 0. | 2506.0302 |
| 44 | 0. | SLV_3 | Min | 0. | 0. | 2011.0044 |
| 44 | 0.13945 | SLV_3 | Min | 0. | 0. | 2257.6851 |
| 44 | 0.27891 | SLV_3 | Min | 0. | 0. | 2506.0302 |
| 44 | 0. | SLV_4 | Max | 0. | 0. | 2011.4485 |
| 44 | 0.13945 | SLV_4 | Max | 0. | 0. | 2256.8176 |
| 44 | 0.27891 | SLV_4 | Max | 0. | 0. | 2503.8511 |
| 44 | 0. | SLV_4 | Min | 0. | 0. | 2011.4485 |
| 44 | 0.13945 | SLV_4 | Min | 0. | 0. | 2256.8176 |
| 44 | 0.27891 | SLV_4 | Min | 0. | 0. | 2503.8511 |
| 44 | 0. | SLD_1 | Max | 0. | 0. | 1459.4603 |
| 44 | 0.13945 | SLD_1 | Max | 0. | 0. | 1653.3302 |
| 44 | 0.27891 | SLD_1 | Max | 0. | 0. | 1848.8644 |
| 44 | 0. | SLD_1 | Min | 0. | 0. | 1459.4603 |
| 44 | 0.13945 | SLD_1 | Min | 0. | 0. | 1653.3302 |
| 44 | 0.27891 | SLD_1 | Min | 0. | 0. | 1848.8644 |
| 44 | 0. | SLD_2 | Max | 0. | 0. | 1461.7756 |
| 44 | 0.13945 | SLD_2 | Max | 0. | 0. | 1655.0568 |
| 44 | 0.27891 | SLD_2 | Max | 0. | 0. | 1850.0024 |
| 44 | 0. | SLD_2 | Min | 0. | 0. | 1461.7756 |
| 44 | 0.13945 | SLD_2 | Min | 0. | 0. | 1655.0568 |
| 44 | 0.27891 | SLD_2 | Min | 0. | 0. | 1850.0024 |
| 44 | 0. | SLD_3 | Max | 0. | 0. | 1832.1029 |
| 44 | 0.13945 | SLD_3 | Max | 0. | 0. | 2080.4243 |
| 44 | 0.27891 | SLD_3 | Max | 0. | 0. | 2330.41 |
| 44 | 0. | SLD_3 | Min | 0. | 0. | 1832.1029 |
| 44 | 0.13945 | SLD_3 | Min | 0. | 0. | 2080.4243 |
| 44 | 0.27891 | SLD_3 | Min | 0. | 0. | 2330.41 |
| 44 | 0. | SLD_4 | Max | 0. | 0. | 1832.6753 |
| 44 | 0.13945 | SLD_4 | Max | 0. | 0. | 2080.3995 |
| 44 | 0.27891 | SLD_4 | Max | 0. | 0. | 2329.788 |
| 44 | 0. | SLD_4 | Min | 0. | 0. | 1832.6753 |
| 44 | 0.13945 | SLD_4 | Min | 0. | 0. | 2080.3995 |
| 44 | 0.27891 | SLD_4 | Min | 0. | 0. | 2329.788 |
| 44 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1749.4496 |
| 44 | 0.13945 | SLU_IDR_1 | Max | 0. | 0. | 1987.8424 |
| 44 | 0.27891 | SLU_IDR_1 | Max | 0. | 0. | 2228.2118 |
| 44 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1749.4496 |
| 44 | 0.13945 | SLU_IDR_1 | Min | 0. | 0. | 1987.8424 |
| 44 | 0.27891 | SLU_IDR_1 | Min | 0. | 0. | 2228.2118 |
| 44 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1478.2421 |
| 44 | 0.13945 | SLU_IDR_2 | Max | 0. | 0. | 1669.4072 |
| 44 | 0.27891 | SLU_IDR_2 | Max | 0. | 0. | 1862.5488 |
| 44 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1478.2421 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 44 | 0.13945 | SLU_IDR_2 | Min | 0. | 0. | 1669.4072 |
| 44 | 0.27891 | SLU_IDR_2 | Min | 0. | 0. | 1862.5488 |
| 44 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -25.5686 |
| 44 | 0.13945 | SISMA WOOD SLV-1 | Max | 0. | 0. | -21.6829 |
| 44 | 0.27891 | SISMA WOOD SLV-1 | Max | 0. | 0. | -17.7972 |
| 44 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -25.5686 |
| 44 | 0.13945 | SISMA WOOD SLV-1 | Min | 0. | 0. | -21.6829 |
| 44 | 0.27891 | SISMA WOOD SLV-1 | Min | 0. | 0. | -17.7972 |
| 44 | 0. | DEAD-1 | Max | 0. | 0. | -69.538 |
| 44 | 0.13945 | DEAD-1 | Max | 0. | 0. | -25.9691 |
| 44 | 0.27891 | DEAD-1 | Max | 0. | 0. | 16.8707 |
| 44 | 0. | DEAD-1 | Min | 0. | 0. | -69.538 |
| 44 | 0.13945 | DEAD-1 | Min | 0. | 0. | -25.9691 |
| 44 | 0.27891 | DEAD-1 | Min | 0. | 0. | 16.8707 |
| 44 | 0. | SLU_PROVA | | 0. | 0. | 1621.4122 |
| 44 | 0.13945 | SLU_PROVA | | 0. | 0. | 1893.803 |
| 44 | 0.27891 | SLU_PROVA | | 0. | 0. | 2168.3575 |
| 45 | 0. | DEAD | | 0. | 0. | -9.5495 |
| 45 | 0.1319 | DEAD | | 0. | 0. | -3.0024 |
| 45 | 0.2638 | DEAD | | 0. | 0. | 3.5446 |
| 45 | 0. | SIMM_KA | | 0. | 0. | 54.9088 |
| 45 | 0.1319 | SIMM_KA | | 0. | 0. | 36.3122 |
| 45 | 0.2638 | SIMM_KA | | 0. | 0. | 18.6901 |
| 45 | 0. | SIMM_K0 | | 0. | 0. | 86.6289 |
| 45 | 0.1319 | SIMM_K0 | | 0. | 0. | 58.5709 |
| 45 | 0.2638 | SIMM_K0 | | 0. | 0. | 31.9749 |
| 45 | 0. | A--SIMM_KA | | 0. | 0. | 160.4816 |
| 45 | 0.1319 | A--SIMM_KA | | 0. | 0. | 136.6869 |
| 45 | 0.2638 | A--SIMM_KA | | 0. | 0. | 114.3974 |
| 45 | 0. | A--SIMM_K0 | | 0. | 0. | 241.9 |
| 45 | 0.1319 | A--SIMM_K0 | | 0. | 0. | 205.3041 |
| 45 | 0.2638 | A--SIMM_K0 | | 0. | 0. | 170.966 |
| 45 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 15.6044 |
| 45 | 0.1319 | A-- SIMM_SOVR_K A | | 0. | 0. | 14.4935 |
| 45 | 0.2638 | A-- SIMM_SOVR_K A | | 0. | 0. | 13.3827 |
| 45 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 23.3948 |
| 45 | 0.1319 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 21.7294 |
| 45 | 0.2638 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.064 |
| 45 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 23.3948 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 45 | 0.1319 | SIMM_SOVR_K 0 | | 0. | 0. | 21.7294 |
| 45 | 0.2638 | SIMM_SOVR_K 0 | | 0. | 0. | 20.064 |
| 45 | 0. | SIMM_SOVR_K A | | 0. | 0. | 15.6044 |
| 45 | 0.1319 | SIMM_SOVR_K A | | 0. | 0. | 14.4935 |
| 45 | 0.2638 | SIMM_SOVR_K A | | 0. | 0. | 13.3827 |
| 45 | 0. | SOVR | | 0. | 0. | 91.8569 |
| 45 | 0.1319 | SOVR | | 0. | 0. | 94.293 |
| 45 | 0.2638 | SOVR | | 0. | 0. | 96.7291 |
| 45 | 0. | TERR_SIMM | | 0. | 0. | 405.2775 |
| 45 | 0.1319 | TERR_SIMM | | 0. | 0. | 411.9967 |
| 45 | 0.2638 | TERR_SIMM | | 0. | 0. | 418.7158 |
| 45 | 0. | TERR_A--SIMM | | 0. | 0. | 651.1337 |
| 45 | 0.1319 | TERR_A--SIMM | | 0. | 0. | 661.4264 |
| 45 | 0.2638 | TERR_A--SIMM | | 0. | 0. | 671.7192 |
| 45 | 0. | INERZIA H SLV | | 0. | 0. | 2.335 |
| 45 | 0.1319 | INERZIA H SLV | | 0. | 0. | 3.2477 |
| 45 | 0.2638 | INERZIA H SLV | | 0. | 0. | 4.1605 |
| 45 | 0. | INERZIA V + SLV | | 0. | 0. | -0.1075 |
| 45 | 0.1319 | INERZIA V + SLV | | 0. | 0. | -0.0044 |
| 45 | 0.2638 | INERZIA V + SLV | | 0. | 0. | 0.0986 |
| 45 | 0. | INERZIA V - SLV | | 0. | 0. | 0.1075 |
| 45 | 0.1319 | INERZIA V - SLV | | 0. | 0. | 0.0044 |
| 45 | 0.2638 | INERZIA V - SLV | | 0. | 0. | -0.0986 |
| 45 | 0. | SISMA WOOD SLV | | 0. | 0. | 199.5886 |
| 45 | 0.1319 | SISMA WOOD SLV | | 0. | 0. | 217.9612 |
| 45 | 0.2638 | SISMA WOOD SLV | | 0. | 0. | 237.547 |
| 45 | 0. | iDROSTATICA | | 0. | 0. | 1052.6276 |
| 45 | 0.1319 | iDROSTATICA | | 0. | 0. | 994.345 |
| 45 | 0.2638 | iDROSTATICA | | 0. | 0. | 938.18 |
| 45 | 0. | SISMA WOOD SLD | | 0. | 0. | 88.1464 |
| 45 | 0.1319 | SISMA WOOD SLD | | 0. | 0. | 96.2605 |
| 45 | 0.2638 | SISMA WOOD SLD | | 0. | 0. | 104.9104 |
| 45 | 0. | INERZIA H SLD | | 0. | 0. | 1.0312 |
| 45 | 0.1319 | INERZIA H SLD | | 0. | 0. | 1.4343 |
| 45 | 0.2638 | INERZIA H SLD | | 0. | 0. | 1.8374 |
| 45 | 0. | INERZIA V + SLD | | 0. | 0. | -0.0475 |
| 45 | 0.1319 | INERZIA V + SLD | | 0. | 0. | -0.002 |
| 45 | 0.2638 | INERZIA V + SLD | | 0. | 0. | 0.0436 |
| 45 | 0. | INERZIA V SLD | | 0. | 0. | 0.0475 |
| 45 | 0.1319 | INERZIA V SLD | | 0. | 0. | 0.002 |
| 45 | 0.2638 | INERZIA V SLD | | 0. | 0. | -0.0436 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------|----------|-----------|------------|------------|
| 45 | 0. | INERZIA V -1 | | 0. | 0. | 0.1075 |
| 45 | 0.1319 | INERZIA V -1 | | 0. | 0. | 0.0044 |
| 45 | 0.2638 | INERZIA V -1 | | 0. | 0. | -0.0986 |
| 45 | 0. | SLU_1 | Max | 0. | 0. | 2335.7118 |
| 45 | 0.1319 | SLU_1 | Max | 0. | 0. | 2242.774 |
| 45 | 0.2638 | SLU_1 | Max | 0. | 0. | 2154.4894 |
| 45 | 0. | SLU_1 | Min | 0. | 0. | 2335.7118 |
| 45 | 0.1319 | SLU_1 | Min | 0. | 0. | 2242.774 |
| 45 | 0.2638 | SLU_1 | Min | 0. | 0. | 2154.4894 |
| 45 | 0. | SLU_2 | Max | 0. | 0. | 2327.1088 |
| 45 | 0.1319 | SLU_2 | Max | 0. | 0. | 2246.6327 |
| 45 | 0.2638 | SLU_2 | Max | 0. | 0. | 2170.1764 |
| 45 | 0. | SLU_2 | Min | 0. | 0. | 2327.1088 |
| 45 | 0.1319 | SLU_2 | Min | 0. | 0. | 2246.6327 |
| 45 | 0.2638 | SLU_2 | Min | 0. | 0. | 2170.1764 |
| 45 | 0. | SLU_3 | Max | 0. | 0. | 3040.6243 |
| 45 | 0.1319 | SLU_3 | Max | 0. | 0. | 2941.9938 |
| 45 | 0.2638 | SLU_3 | Max | 0. | 0. | 2849.0513 |
| 45 | 0. | SLU_3 | Min | 0. | 0. | 3040.6243 |
| 45 | 0.1319 | SLU_3 | Min | 0. | 0. | 2941.9938 |
| 45 | 0.2638 | SLU_3 | Min | 0. | 0. | 2849.0513 |
| 45 | 0. | SLU_4 | Max | 0. | 0. | 2907.3148 |
| 45 | 0.1319 | SLU_4 | Max | 0. | 0. | 2826.3296 |
| 45 | 0.2638 | SLU_4 | Max | 0. | 0. | 2750.0539 |
| 45 | 0. | SLU_4 | Min | 0. | 0. | 2907.3148 |
| 45 | 0.1319 | SLU_4 | Min | 0. | 0. | 2826.3296 |
| 45 | 0.2638 | SLU_4 | Min | 0. | 0. | 2750.0539 |
| 45 | 0. | SLE_F1 | Max | 0. | 0. | 1756.9026 |
| 45 | 0.1319 | SLE_F1 | Max | 0. | 0. | 1684.5583 |
| 45 | 0.2638 | SLE_F1 | Max | 0. | 0. | 1615.7935 |
| 45 | 0. | SLE_F1 | Min | 0. | 0. | 1756.9026 |
| 45 | 0.1319 | SLE_F1 | Min | 0. | 0. | 1684.5583 |
| 45 | 0.2638 | SLE_F1 | Min | 0. | 0. | 1615.7935 |
| 45 | 0. | SLE_F2 | Max | 0. | 0. | 1755.0658 |
| 45 | 0.1319 | SLE_F2 | Max | 0. | 0. | 1691.977 |
| 45 | 0.2638 | SLE_F2 | Max | 0. | 0. | 1631.9804 |
| 45 | 0. | SLE_F2 | Min | 0. | 0. | 1755.0658 |
| 45 | 0.1319 | SLE_F2 | Min | 0. | 0. | 1691.977 |
| 45 | 0.2638 | SLE_F2 | Min | 0. | 0. | 1631.9804 |
| 45 | 0. | SLE_F3 | Max | 0. | 0. | 2197.0904 |
| 45 | 0.1319 | SLE_F3 | Max | 0. | 0. | 2133.683 |
| 45 | 0.2638 | SLE_F3 | Max | 0. | 0. | 2073.8984 |
| 45 | 0. | SLE_F3 | Min | 0. | 0. | 2197.0904 |
| 45 | 0.1319 | SLE_F3 | Min | 0. | 0. | 2133.683 |
| 45 | 0.2638 | SLE_F3 | Min | 0. | 0. | 2073.8984 |
| 45 | 0. | SLE_F4 | Max | 0. | 0. | 2292.4009 |
| 45 | 0.1319 | SLE_F4 | Max | 0. | 0. | 2214.8312 |
| 45 | 0.2638 | SLE_F4 | Max | 0. | 0. | 2141.6369 |
| 45 | 0. | SLE_F4 | Min | 0. | 0. | 2292.4009 |
| 45 | 0.1319 | SLE_F4 | Min | 0. | 0. | 2214.8312 |
| 45 | 0.2638 | SLE_F4 | Min | 0. | 0. | 2141.6369 |
| 45 | 0. | SLE_QP1 | Max | 0. | 0. | 1688.304 |
| 45 | 0.1319 | SLE_QP1 | Max | 0. | 0. | 1614.1499 |
| 45 | 0.2638 | SLE_QP1 | Max | 0. | 0. | 1543.5752 |
| 45 | 0. | SLE_QP1 | Min | 0. | 0. | 1688.304 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 45 | 0.1319 | SLE_QP1 | Min | 0. | 0. | 1614.1499 |
| 45 | 0.2638 | SLE_QP1 | Min | 0. | 0. | 1543.5752 |
| 45 | 0. | SLE_QP2 | Max | 0. | 0. | 1690.0291 |
| 45 | 0.1319 | SLE_QP2 | Max | 0. | 0. | 1624.7409 |
| 45 | 0.2638 | SLE_QP2 | Max | 0. | 0. | 1562.5449 |
| 45 | 0. | SLE_QP2 | Min | 0. | 0. | 1690.0291 |
| 45 | 0.1319 | SLE_QP2 | Min | 0. | 0. | 1624.7409 |
| 45 | 0.2638 | SLE_QP2 | Min | 0. | 0. | 1562.5449 |
| 45 | 0. | SLE_QP3 | Max | 0. | 0. | 2124.0916 |
| 45 | 0.1319 | SLE_QP3 | Max | 0. | 0. | 2058.6209 |
| 45 | 0.2638 | SLE_QP3 | Max | 0. | 0. | 1996.7731 |
| 45 | 0. | SLE_QP3 | Min | 0. | 0. | 2124.0916 |
| 45 | 0.1319 | SLE_QP3 | Min | 0. | 0. | 2058.6209 |
| 45 | 0.2638 | SLE_QP3 | Min | 0. | 0. | 1996.7731 |
| 45 | 0. | SLE_QP4 | Max | 0. | 0. | 2204.7931 |
| 45 | 0.1319 | SLE_QP4 | Max | 0. | 0. | 2123.8966 |
| 45 | 0.2638 | SLE_QP4 | Max | 0. | 0. | 2047.3755 |
| 45 | 0. | SLE_QP4 | Min | 0. | 0. | 2204.7931 |
| 45 | 0.1319 | SLE_QP4 | Min | 0. | 0. | 2123.8966 |
| 45 | 0.2638 | SLE_QP4 | Min | 0. | 0. | 2047.3755 |
| 45 | 0. | SLV_1 | Max | 0. | 0. | 2004.548 |
| 45 | 0.1319 | SLV_1 | Max | 0. | 0. | 1889.3005 |
| 45 | 0.2638 | SLV_1 | Max | 0. | 0. | 1778.8457 |
| 45 | 0. | SLV_1 | Min | 0. | 0. | 2004.548 |
| 45 | 0.1319 | SLV_1 | Min | 0. | 0. | 1889.3005 |
| 45 | 0.2638 | SLV_1 | Min | 0. | 0. | 1778.8457 |
| 45 | 0. | SLV_2 | Max | 0. | 0. | 2003.4095 |
| 45 | 0.1319 | SLV_2 | Max | 0. | 0. | 1887.8886 |
| 45 | 0.2638 | SLV_2 | Max | 0. | 0. | 1777.1605 |
| 45 | 0. | SLV_2 | Min | 0. | 0. | 2003.4095 |
| 45 | 0.1319 | SLV_2 | Min | 0. | 0. | 1887.8886 |
| 45 | 0.2638 | SLV_2 | Min | 0. | 0. | 1777.1605 |
| 45 | 0. | SLV_3 | Max | 0. | 0. | 2506.0302 |
| 45 | 0.1319 | SLV_3 | Max | 0. | 0. | 2369.7649 |
| 45 | 0.2638 | SLV_3 | Max | 0. | 0. | 2239.0883 |
| 45 | 0. | SLV_3 | Min | 0. | 0. | 2506.0302 |
| 45 | 0.1319 | SLV_3 | Min | 0. | 0. | 2369.7649 |
| 45 | 0.2638 | SLV_3 | Min | 0. | 0. | 2239.0883 |
| 45 | 0. | SLV_4 | Max | 0. | 0. | 2503.8511 |
| 45 | 0.1319 | SLV_4 | Max | 0. | 0. | 2367.3091 |
| 45 | 0.2638 | SLV_4 | Max | 0. | 0. | 2236.3559 |
| 45 | 0. | SLV_4 | Min | 0. | 0. | 2503.8511 |
| 45 | 0.1319 | SLV_4 | Min | 0. | 0. | 2367.3091 |
| 45 | 0.2638 | SLV_4 | Min | 0. | 0. | 2236.3559 |
| 45 | 0. | SLD_1 | Max | 0. | 0. | 1848.8644 |
| 45 | 0.1319 | SLD_1 | Max | 0. | 0. | 1763.9261 |
| 45 | 0.2638 | SLD_1 | Max | 0. | 0. | 1683.1031 |
| 45 | 0. | SLD_1 | Min | 0. | 0. | 1848.8644 |
| 45 | 0.1319 | SLD_1 | Min | 0. | 0. | 1763.9261 |
| 45 | 0.2638 | SLD_1 | Min | 0. | 0. | 1683.1031 |
| 45 | 0. | SLD_2 | Max | 0. | 0. | 1850.0024 |
| 45 | 0.1319 | SLD_2 | Max | 0. | 0. | 1764.8925 |
| 45 | 0.2638 | SLD_2 | Max | 0. | 0. | 1683.8979 |
| 45 | 0. | SLD_2 | Min | 0. | 0. | 1850.0024 |
| 45 | 0.1319 | SLD_2 | Min | 0. | 0. | 1764.8925 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 45 | 0.2638 | SLD_2 | Min | 0. | 0. | 1683.8979 |
| 45 | 0. | SLD_3 | Max | 0. | 0. | 2330.41 |
| 45 | 0.1319 | SLD_3 | Max | 0. | 0. | 2224.4373 |
| 45 | 0.2638 | SLD_3 | Max | 0. | 0. | 2123.3758 |
| 45 | 0. | SLD_3 | Min | 0. | 0. | 2330.41 |
| 45 | 0.1319 | SLD_3 | Min | 0. | 0. | 2224.4373 |
| 45 | 0.2638 | SLD_3 | Min | 0. | 0. | 2123.3758 |
| 45 | 0. | SLD_4 | Max | 0. | 0. | 2329.788 |
| 45 | 0.1319 | SLD_4 | Max | 0. | 0. | 2223.6805 |
| 45 | 0.2638 | SLD_4 | Max | 0. | 0. | 2122.4842 |
| 45 | 0. | SLD_4 | Min | 0. | 0. | 2329.788 |
| 45 | 0.1319 | SLD_4 | Min | 0. | 0. | 2223.6805 |
| 45 | 0.2638 | SLD_4 | Min | 0. | 0. | 2122.4842 |
| 45 | 0. | SLU_IDR_1 | Max | 0. | 0. | 2228.2118 |
| 45 | 0.1319 | SLU_IDR_1 | Max | 0. | 0. | 2153.9248 |
| 45 | 0.2638 | SLU_IDR_1 | Max | 0. | 0. | 2083.3217 |
| 45 | 0. | SLU_IDR_1 | Min | 0. | 0. | 2228.2118 |
| 45 | 0.1319 | SLU_IDR_1 | Min | 0. | 0. | 2153.9248 |
| 45 | 0.2638 | SLU_IDR_1 | Min | 0. | 0. | 2083.3217 |
| 45 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1862.5488 |
| 45 | 0.1319 | SLU_IDR_2 | Max | 0. | 0. | 1787.9428 |
| 45 | 0.2638 | SLU_IDR_2 | Max | 0. | 0. | 1716.5433 |
| 45 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1862.5488 |
| 45 | 0.1319 | SLU_IDR_2 | Min | 0. | 0. | 1787.9428 |
| 45 | 0.2638 | SLU_IDR_2 | Min | 0. | 0. | 1716.5433 |
| 45 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -17.7972 |
| 45 | 0.1319 | SISMA WOOD SLV-1 | Max | 0. | 0. | -58.2459 |
| 45 | 0.2638 | SISMA WOOD SLV-1 | Max | 0. | 0. | -97.4813 |
| 45 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -17.7972 |
| 45 | 0.1319 | SISMA WOOD SLV-1 | Min | 0. | 0. | -58.2459 |
| 45 | 0.2638 | SISMA WOOD SLV-1 | Min | 0. | 0. | -97.4813 |
| 45 | 0. | DEAD-1 | Max | 0. | 0. | 16.8707 |
| 45 | 0.1319 | DEAD-1 | Max | 0. | 0. | 24.4979 |
| 45 | 0.2638 | DEAD-1 | Max | 0. | 0. | 32.125 |
| 45 | 0. | DEAD-1 | Min | 0. | 0. | 16.8707 |
| 45 | 0.1319 | DEAD-1 | Min | 0. | 0. | 24.4979 |
| 45 | 0.2638 | DEAD-1 | Min | 0. | 0. | 32.125 |
| 45 | 0. | SLU_PROVA | | 0. | 0. | 2168.3575 |
| 45 | 0.1319 | SLU_PROVA | | 0. | 0. | 2074.5169 |
| 45 | 0.2638 | SLU_PROVA | | 0. | 0. | 1985.3295 |
| 46 | 0. | DEAD | | 0. | 0. | 3.5446 |
| 46 | 0.1318 | DEAD | | 0. | 0. | 10.2161 |
| 46 | 0.2636 | DEAD | | 0. | 0. | 16.8875 |
| 46 | 0. | SIMM_KA | | 0. | 0. | 18.6901 |
| 46 | 0.1318 | SIMM_KA | | 0. | 0. | 1.7437 |
| 46 | 0.2636 | SIMM_KA | | 0. | 0. | -14.2296 |
| 46 | 0. | SIMM_K0 | | 0. | 0. | 31.9749 |
| 46 | 0.1318 | SIMM_K0 | | 0. | 0. | 6.3847 |
| 46 | 0.2636 | SIMM_K0 | | 0. | 0. | -17.7458 |
| 46 | 0. | A--SIMM_KA | | 0. | 0. | 114.3974 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 46 | 0.1318 | A--SIMM_KA | | 0. | 0. | 92.2391 |
| 46 | 0.2636 | A--SIMM_KA | | 0. | 0. | 71.5837 |
| 46 | 0. | A--SIMM_K0 | | 0. | 0. | 170.966 |
| 46 | 0.1318 | A--SIMM_K0 | | 0. | 0. | 136.8799 |
| 46 | 0.2636 | A--SIMM_K0 | | 0. | 0. | 105.0483 |
| 46 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 13.3827 |
| 46 | 0.1318 | A-- SIMM_SOVR_K A | | 0. | 0. | 12.2391 |
| 46 | 0.2636 | A-- SIMM_SOVR_K A | | 0. | 0. | 11.0955 |
| 46 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.064 |
| 46 | 0.1318 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 18.3495 |
| 46 | 0.2636 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 16.6349 |
| 46 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 20.064 |
| 46 | 0.1318 | SIMM_SOVR_K 0 | | 0. | 0. | 18.3495 |
| 46 | 0.2636 | SIMM_SOVR_K 0 | | 0. | 0. | 16.6349 |
| 46 | 0. | SIMM_SOVR_K A | | 0. | 0. | 13.3827 |
| 46 | 0.1318 | SIMM_SOVR_K A | | 0. | 0. | 12.2391 |
| 46 | 0.2636 | SIMM_SOVR_K A | | 0. | 0. | 11.0955 |
| 46 | 0. | SOVR | | 0. | 0. | 96.7291 |
| 46 | 0.1318 | SOVR | | 0. | 0. | 99.3934 |
| 46 | 0.2636 | SOVR | | 0. | 0. | 102.0577 |
| 46 | 0. | TERR_SIMM | | 0. | 0. | 418.7158 |
| 46 | 0.1318 | TERR_SIMM | | 0. | 0. | 426.2575 |
| 46 | 0.2636 | TERR_SIMM | | 0. | 0. | 433.7991 |
| 46 | 0. | TERR_A--SIMM | | 0. | 0. | 671.7192 |
| 46 | 0.1318 | TERR_A--SIMM | | 0. | 0. | 682.981 |
| 46 | 0.2636 | TERR_A--SIMM | | 0. | 0. | 694.2428 |
| 46 | 0. | INERZIA H SLV | | 0. | 0. | 4.1605 |
| 46 | 0.1318 | INERZIA H SLV | | 0. | 0. | 4.9343 |
| 46 | 0.2636 | INERZIA H SLV | | 0. | 0. | 5.7082 |
| 46 | 0. | INERZIA V + SLV | | 0. | 0. | 0.0986 |
| 46 | 0.1318 | INERZIA V + SLV | | 0. | 0. | 0.2037 |
| 46 | 0.2636 | INERZIA V + SLV | | 0. | 0. | 0.3088 |
| 46 | 0. | INERZIA V - SLV | | 0. | 0. | -0.0986 |
| 46 | 0.1318 | INERZIA V - SLV | | 0. | 0. | -0.2037 |
| 46 | 0.2636 | INERZIA V - SLV | | 0. | 0. | -0.3088 |
| 46 | 0. | SISMA WOOD SLV | | 0. | 0. | 237.547 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 46 | 0.1318 | SISMA WOOD SLV | | 0. | 0. | 251.6979 |
| 46 | 0.2636 | SISMA WOOD SLV | | 0. | 0. | 267.0601 |
| 46 | 0. | IDROSTATICA | | 0. | 0. | 938.18 |
| 46 | 0.1318 | IDROSTATICA | | 0. | 0. | 884.778 |
| 46 | 0.2636 | IDROSTATICA | | 0. | 0. | 833.4433 |
| 46 | 0. | SISMA WOOD SLD | | 0. | 0. | 104.9104 |
| 46 | 0.1318 | SISMA WOOD SLD | | 0. | 0. | 111.1599 |
| 46 | 0.2636 | SISMA WOOD SLD | | 0. | 0. | 117.9445 |
| 46 | 0. | INERZIA H SLD | | 0. | 0. | 1.8374 |
| 46 | 0.1318 | INERZIA H SLD | | 0. | 0. | 2.1792 |
| 46 | 0.2636 | INERZIA H SLD | | 0. | 0. | 2.521 |
| 46 | 0. | INERZIA V + SLD | | 0. | 0. | 0.0436 |
| 46 | 0.1318 | INERZIA V + SLD | | 0. | 0. | 0.09 |
| 46 | 0.2636 | INERZIA V + SLD | | 0. | 0. | 0.1364 |
| 46 | 0. | INERZIA V SLD | | 0. | 0. | -0.0436 |
| 46 | 0.1318 | INERZIA V SLD | | 0. | 0. | -0.09 |
| 46 | 0.2636 | INERZIA V SLD | | 0. | 0. | -0.1364 |
| 46 | 0. | INERZIA V -1 | | 0. | 0. | -0.0986 |
| 46 | 0.1318 | INERZIA V -1 | | 0. | 0. | -0.2037 |
| 46 | 0.2636 | INERZIA V -1 | | 0. | 0. | -0.3088 |
| 46 | 0. | SLU_1 | Max | 0. | 0. | 2154.4894 |
| 46 | 0.1318 | SLU_1 | Max | 0. | 0. | 2073.0199 |
| 46 | 0.2636 | SLU_1 | Max | 0. | 0. | 1996.1353 |
| 46 | 0. | SLU_1 | Min | 0. | 0. | 2154.4894 |
| 46 | 0.1318 | SLU_1 | Min | 0. | 0. | 2073.0199 |
| 46 | 0.2636 | SLU_1 | Min | 0. | 0. | 1996.1353 |
| 46 | 0. | SLU_2 | Max | 0. | 0. | 2170.1764 |
| 46 | 0.1318 | SLU_2 | Max | 0. | 0. | 2100.2155 |
| 46 | 0.2636 | SLU_2 | Max | 0. | 0. | 2034.2071 |
| 46 | 0. | SLU_2 | Min | 0. | 0. | 2170.1764 |
| 46 | 0.1318 | SLU_2 | Min | 0. | 0. | 2100.2155 |
| 46 | 0.2636 | SLU_2 | Min | 0. | 0. | 2034.2071 |
| 46 | 0. | SLU_3 | Max | 0. | 0. | 2849.0513 |
| 46 | 0.1318 | SLU_3 | Max | 0. | 0. | 2761.8302 |
| 46 | 0.2636 | SLU_3 | Max | 0. | 0. | 2680.2273 |
| 46 | 0. | SLU_3 | Min | 0. | 0. | 2849.0513 |
| 46 | 0.1318 | SLU_3 | Min | 0. | 0. | 2761.8302 |
| 46 | 0.2636 | SLU_3 | Min | 0. | 0. | 2680.2273 |
| 46 | 0. | SLU_4 | Max | 0. | 0. | 2750.0539 |
| 46 | 0.1318 | SLU_4 | Max | 0. | 0. | 2679.4375 |
| 46 | 0.2636 | SLU_4 | Max | 0. | 0. | 2613.4623 |
| 46 | 0. | SLU_4 | Min | 0. | 0. | 2750.0539 |
| 46 | 0.1318 | SLU_4 | Min | 0. | 0. | 2679.4375 |
| 46 | 0.2636 | SLU_4 | Min | 0. | 0. | 2613.4623 |
| 46 | 0. | SLE_F1 | Max | 0. | 0. | 1615.7935 |
| 46 | 0.1318 | SLE_F1 | Max | 0. | 0. | 1552.1937 |
| 46 | 0.2636 | SLE_F1 | Max | 0. | 0. | 1492.1208 |
| 46 | 0. | SLE_F1 | Min | 0. | 0. | 1615.7935 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 46 | 0.1318 | SLE_F1 | Min | 0. | 0. | 1552.1937 |
| 46 | 0.2636 | SLE_F1 | Min | 0. | 0. | 1492.1208 |
| 46 | 0. | SLE_F2 | Max | 0. | 0. | 1631.9804 |
| 46 | 0.1318 | SLE_F2 | Max | 0. | 0. | 1576.9001 |
| 46 | 0.2636 | SLE_F2 | Max | 0. | 0. | 1524.8603 |
| 46 | 0. | SLE_F2 | Min | 0. | 0. | 1631.9804 |
| 46 | 0.1318 | SLE_F2 | Min | 0. | 0. | 1576.9001 |
| 46 | 0.2636 | SLE_F2 | Min | 0. | 0. | 1524.8603 |
| 46 | 0. | SLE_F3 | Max | 0. | 0. | 2073.8984 |
| 46 | 0.1318 | SLE_F3 | Max | 0. | 0. | 2018.3888 |
| 46 | 0.2636 | SLE_F3 | Max | 0. | 0. | 1966.4494 |
| 46 | 0. | SLE_F3 | Min | 0. | 0. | 2073.8984 |
| 46 | 0.1318 | SLE_F3 | Min | 0. | 0. | 2018.3888 |
| 46 | 0.2636 | SLE_F3 | Min | 0. | 0. | 1966.4494 |
| 46 | 0. | SLE_F4 | Max | 0. | 0. | 2141.6369 |
| 46 | 0.1318 | SLE_F4 | Max | 0. | 0. | 2072.845 |
| 46 | 0.2636 | SLE_F4 | Max | 0. | 0. | 2008.3746 |
| 46 | 0. | SLE_F4 | Min | 0. | 0. | 2141.6369 |
| 46 | 0.1318 | SLE_F4 | Min | 0. | 0. | 2072.845 |
| 46 | 0.2636 | SLE_F4 | Min | 0. | 0. | 2008.3746 |
| 46 | 0. | SLE_QP1 | Max | 0. | 0. | 1543.5752 |
| 46 | 0.1318 | SLE_QP1 | Max | 0. | 0. | 1478.0355 |
| 46 | 0.2636 | SLE_QP1 | Max | 0. | 0. | 1416.0228 |
| 46 | 0. | SLE_QP1 | Min | 0. | 0. | 1543.5752 |
| 46 | 0.1318 | SLE_QP1 | Min | 0. | 0. | 1478.0355 |
| 46 | 0.2636 | SLE_QP1 | Min | 0. | 0. | 1416.0228 |
| 46 | 0. | SLE_QP2 | Max | 0. | 0. | 1562.5449 |
| 46 | 0.1318 | SLE_QP2 | Max | 0. | 0. | 1505.1166 |
| 46 | 0.2636 | SLE_QP2 | Max | 0. | 0. | 1450.7286 |
| 46 | 0. | SLE_QP2 | Min | 0. | 0. | 1562.5449 |
| 46 | 0.1318 | SLE_QP2 | Min | 0. | 0. | 1505.1166 |
| 46 | 0.2636 | SLE_QP2 | Min | 0. | 0. | 1450.7286 |
| 46 | 0. | SLE_QP3 | Max | 0. | 0. | 1996.7731 |
| 46 | 0.1318 | SLE_QP3 | Max | 0. | 0. | 1939.0548 |
| 46 | 0.2636 | SLE_QP3 | Max | 0. | 0. | 1884.9067 |
| 46 | 0. | SLE_QP3 | Min | 0. | 0. | 1996.7731 |
| 46 | 0.1318 | SLE_QP3 | Min | 0. | 0. | 1939.0548 |
| 46 | 0.2636 | SLE_QP3 | Min | 0. | 0. | 1884.9067 |
| 46 | 0. | SLE_QP4 | Max | 0. | 0. | 2047.3755 |
| 46 | 0.1318 | SLE_QP4 | Max | 0. | 0. | 1975.2592 |
| 46 | 0.2636 | SLE_QP4 | Max | 0. | 0. | 1907.4645 |
| 46 | 0. | SLE_QP4 | Min | 0. | 0. | 2047.3755 |
| 46 | 0.1318 | SLE_QP4 | Min | 0. | 0. | 1975.2592 |
| 46 | 0.2636 | SLE_QP4 | Min | 0. | 0. | 1907.4645 |
| 46 | 0. | SLV_1 | Max | 0. | 0. | 1778.8457 |
| 46 | 0.1318 | SLV_1 | Max | 0. | 0. | 1673.2786 |
| 46 | 0.2636 | SLV_1 | Max | 0. | 0. | 1572.4498 |
| 46 | 0. | SLV_1 | Min | 0. | 0. | 1778.8457 |
| 46 | 0.1318 | SLV_1 | Min | 0. | 0. | 1673.2786 |
| 46 | 0.2636 | SLV_1 | Min | 0. | 0. | 1572.4498 |
| 46 | 0. | SLV_2 | Max | 0. | 0. | 1777.1605 |
| 46 | 0.1318 | SLV_2 | Max | 0. | 0. | 1671.3202 |
| 46 | 0.2636 | SLV_2 | Max | 0. | 0. | 1570.2182 |
| 46 | 0. | SLV_2 | Min | 0. | 0. | 1777.1605 |
| 46 | 0.1318 | SLV_2 | Min | 0. | 0. | 1671.3202 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 46 | 0.2636 | SLV_2 | Min | 0. | 0. | 1570.2182 |
| 46 | 0. | SLV_3 | Max | 0. | 0. | 2239.0883 |
| 46 | 0.1318 | SLV_3 | Max | 0. | 0. | 2114.1092 |
| 46 | 0.2636 | SLV_3 | Max | 0. | 0. | 1994.6631 |
| 46 | 0. | SLV_3 | Min | 0. | 0. | 2239.0883 |
| 46 | 0.1318 | SLV_3 | Min | 0. | 0. | 2114.1092 |
| 46 | 0.2636 | SLV_3 | Min | 0. | 0. | 1994.6631 |
| 46 | 0. | SLV_4 | Max | 0. | 0. | 2236.3559 |
| 46 | 0.1318 | SLV_4 | Max | 0. | 0. | 2111.1003 |
| 46 | 0.2636 | SLV_4 | Max | 0. | 0. | 1991.3779 |
| 46 | 0. | SLV_4 | Min | 0. | 0. | 2236.3559 |
| 46 | 0.1318 | SLV_4 | Min | 0. | 0. | 2111.1003 |
| 46 | 0.2636 | SLV_4 | Min | 0. | 0. | 1991.3779 |
| 46 | 0. | SLD_1 | Max | 0. | 0. | 1683.1031 |
| 46 | 0.1318 | SLD_1 | Max | 0. | 0. | 1606.446 |
| 46 | 0.2636 | SLD_1 | Max | 0. | 0. | 1533.8509 |
| 46 | 0. | SLD_1 | Min | 0. | 0. | 1683.1031 |
| 46 | 0.1318 | SLD_1 | Min | 0. | 0. | 1606.446 |
| 46 | 0.2636 | SLD_1 | Min | 0. | 0. | 1533.8509 |
| 46 | 0. | SLD_2 | Max | 0. | 0. | 1683.8979 |
| 46 | 0.1318 | SLD_2 | Max | 0. | 0. | 1607.0693 |
| 46 | 0.2636 | SLD_2 | Max | 0. | 0. | 1534.3026 |
| 46 | 0. | SLD_2 | Min | 0. | 0. | 1683.8979 |
| 46 | 0.1318 | SLD_2 | Min | 0. | 0. | 1607.0693 |
| 46 | 0.2636 | SLD_2 | Min | 0. | 0. | 1534.3026 |
| 46 | 0. | SLD_3 | Max | 0. | 0. | 2123.3758 |
| 46 | 0.1318 | SLD_3 | Max | 0. | 0. | 2027.2896 |
| 46 | 0.2636 | SLD_3 | Max | 0. | 0. | 1936.0602 |
| 46 | 0. | SLD_3 | Min | 0. | 0. | 2123.3758 |
| 46 | 0.1318 | SLD_3 | Min | 0. | 0. | 2027.2896 |
| 46 | 0.2636 | SLD_3 | Min | 0. | 0. | 1936.0602 |
| 46 | 0. | SLD_4 | Max | 0. | 0. | 2122.4842 |
| 46 | 0.1318 | SLD_4 | Max | 0. | 0. | 2026.2633 |
| 46 | 0.2636 | SLD_4 | Max | 0. | 0. | 1934.8992 |
| 46 | 0. | SLD_4 | Min | 0. | 0. | 2122.4842 |
| 46 | 0.1318 | SLD_4 | Min | 0. | 0. | 2026.2633 |
| 46 | 0.2636 | SLD_4 | Min | 0. | 0. | 1934.8992 |
| 46 | 0. | SLU_IDR_1 | Max | 0. | 0. | 2083.3217 |
| 46 | 0.1318 | SLU_IDR_1 | Max | 0. | 0. | 2017.1595 |
| 46 | 0.2636 | SLU_IDR_1 | Max | 0. | 0. | 1954.6238 |
| 46 | 0. | SLU_IDR_1 | Min | 0. | 0. | 2083.3217 |
| 46 | 0.1318 | SLU_IDR_1 | Min | 0. | 0. | 2017.1595 |
| 46 | 0.2636 | SLU_IDR_1 | Min | 0. | 0. | 1954.6238 |
| 46 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1716.5433 |
| 46 | 0.1318 | SLU_IDR_2 | Max | 0. | 0. | 1650.1408 |
| 46 | 0.2636 | SLU_IDR_2 | Max | 0. | 0. | 1586.8881 |
| 46 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1716.5433 |
| 46 | 0.1318 | SLU_IDR_2 | Min | 0. | 0. | 1650.1408 |
| 46 | 0.2636 | SLU_IDR_2 | Min | 0. | 0. | 1586.8881 |
| 46 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -97.4813 |
| 46 | 0.1318 | SISMA WOOD SLV-1 | Max | 0. | 0. | -135.4751 |
| 46 | 0.2636 | SISMA WOOD SLV-1 | Max | 0. | 0. | -172.2573 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 46 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -97.4813 |
| 46 | 0.1318 | SISMA WOOD SLV-1 | Min | 0. | 0. | -135.4751 |
| 46 | 0.2636 | SISMA WOOD SLV-1 | Min | 0. | 0. | -172.2573 |
| 46 | 0. | DEAD-1 | Max | 0. | 0. | 32.125 |
| 46 | 0.1318 | DEAD-1 | Max | 0. | 0. | 39.9625 |
| 46 | 0.2636 | DEAD-1 | Max | 0. | 0. | 47.7999 |
| 46 | 0. | DEAD-1 | Min | 0. | 0. | 32.125 |
| 46 | 0.1318 | DEAD-1 | Min | 0. | 0. | 39.9625 |
| 46 | 0.2636 | DEAD-1 | Min | 0. | 0. | 47.7999 |
| 46 | 0. | SLU_PROVA | | 0. | 0. | 1985.3295 |
| 46 | 0.1318 | SLU_PROVA | | 0. | 0. | 1902.5414 |
| 46 | 0.2636 | SLU_PROVA | | 0. | 0. | 1824.3383 |
| 47 | 0. | DEAD | | 0. | 0. | -92.2324 |
| 47 | 0.13006 | DEAD | | 0. | 0. | -83.8943 |
| 47 | 0.26012 | DEAD | | 0. | 0. | -76.1902 |
| 47 | 0. | SIMM_KA | | 0. | 0. | 38.9428 |
| 47 | 0.13006 | SIMM_KA | | 0. | 0. | 43.048 |
| 47 | 0.26012 | SIMM_KA | | 0. | 0. | 47.1533 |
| 47 | 0. | SIMM_K0 | | 0. | 0. | 62.0661 |
| 47 | 0.13006 | SIMM_K0 | | 0. | 0. | 68.3332 |
| 47 | 0.26012 | SIMM_K0 | | 0. | 0. | 74.6003 |
| 47 | 0. | A--SIMM_KA | | 0. | 0. | -46.4898 |
| 47 | 0.13006 | A--SIMM_KA | | 0. | 0. | -40.5017 |
| 47 | 0.26012 | A--SIMM_KA | | 0. | 0. | -34.5136 |
| 47 | 0. | A--SIMM_K0 | | 0. | 0. | -70.8296 |
| 47 | 0.13006 | A--SIMM_K0 | | 0. | 0. | -61.779 |
| 47 | 0.26012 | A--SIMM_K0 | | 0. | 0. | -52.7284 |
| 47 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 13.6381 |
| 47 | 0.13006 | A-- SIMM_SOVR_K A | | 0. | 0. | 14.1261 |
| 47 | 0.26012 | A-- SIMM_SOVR_K A | | 0. | 0. | 14.6141 |
| 47 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 20.4469 |
| 47 | 0.13006 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 21.1786 |
| 47 | 0.26012 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 21.9102 |
| 47 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 20.4469 |
| 47 | 0.13006 | SIMM_SOVR_K 0 | | 0. | 0. | 21.1786 |
| 47 | 0.26012 | SIMM_SOVR_K 0 | | 0. | 0. | 21.9102 |
| 47 | 0. | SIMM_SOVR_K A | | 0. | 0. | 13.6381 |
| 47 | 0.13006 | SIMM_SOVR_K A | | 0. | 0. | 14.1261 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 47 | 0.26012 | SIMM_SOVR_K A | | 0. | 0. | 14.6141 |
| 47 | 0. | SOVR | | 0. | 0. | 32.6378 |
| 47 | 0.13006 | SOVR | | 0. | 0. | 42.4293 |
| 47 | 0.26012 | SOVR | | 0. | 0. | 52.2209 |
| 47 | 0. | TERR_SIMM | | 0. | 0. | 165.2228 |
| 47 | 0.13006 | TERR_SIMM | | 0. | 0. | 205.498 |
| 47 | 0.26012 | TERR_SIMM | | 0. | 0. | 245.7732 |
| 47 | 0. | TERR_A--SIMM | | 0. | 0. | 141.2796 |
| 47 | 0.13006 | TERR_A--SIMM | | 0. | 0. | 181.3936 |
| 47 | 0.26012 | TERR_A--SIMM | | 0. | 0. | 221.5076 |
| 47 | 0. | INERZIA H SLV | | 0. | 0. | -4.4236 |
| 47 | 0.13006 | INERZIA H SLV | | 0. | 0. | -4.0197 |
| 47 | 0.26012 | INERZIA H SLV | | 0. | 0. | -3.6159 |
| 47 | 0. | INERZIA V + SLV | | 0. | 0. | -1.4433 |
| 47 | 0.13006 | INERZIA V + SLV | | 0. | 0. | -1.3138 |
| 47 | 0.26012 | INERZIA V + SLV | | 0. | 0. | -1.1843 |
| 47 | 0. | INERZIA V - SLV | | 0. | 0. | 1.4433 |
| 47 | 0.13006 | INERZIA V - SLV | | 0. | 0. | 1.3138 |
| 47 | 0.26012 | INERZIA V - SLV | | 0. | 0. | 1.1843 |
| 47 | 0. | SISMA WOOD SLV | | 0. | 0. | -218.0938 |
| 47 | 0.13006 | SISMA WOOD SLV | | 0. | 0. | -199.2953 |
| 47 | 0.26012 | SISMA WOOD SLV | | 0. | 0. | -180.4968 |
| 47 | 0. | iDROSTATICA | | 0. | 0. | 808.9597 |
| 47 | 0.13006 | iDROSTATICA | | 0. | 0. | 878.2311 |
| 47 | 0.26012 | iDROSTATICA | | 0. | 0. | 949.5842 |
| 47 | 0. | SISMA WOOD SLD | | 0. | 0. | -96.319 |
| 47 | 0.13006 | SISMA WOOD SLD | | 0. | 0. | -88.0169 |
| 47 | 0.26012 | SISMA WOOD SLD | | 0. | 0. | -79.7147 |
| 47 | 0. | INERZIA H SLD | | 0. | 0. | -1.9536 |
| 47 | 0.13006 | INERZIA H SLD | | 0. | 0. | -1.7753 |
| 47 | 0.26012 | INERZIA H SLD | | 0. | 0. | -1.5969 |
| 47 | 0. | INERZIA V + SLD | | 0. | 0. | -0.6374 |
| 47 | 0.13006 | INERZIA V + SLD | | 0. | 0. | -0.5802 |
| 47 | 0.26012 | INERZIA V + SLD | | 0. | 0. | -0.523 |
| 47 | 0. | INERZIA V SLD | | 0. | 0. | 0.6374 |
| 47 | 0.13006 | INERZIA V SLD | | 0. | 0. | 0.5802 |
| 47 | 0.26012 | INERZIA V SLD | | 0. | 0. | 0.523 |
| 47 | 0. | INERZIA V -1 | | 0. | 0. | 1.4433 |
| 47 | 0.13006 | INERZIA V -1 | | 0. | 0. | 1.3138 |
| 47 | 0.26012 | INERZIA V -1 | | 0. | 0. | 1.1843 |
| 47 | 0. | SLU_1 | Max | 0. | 0. | 1421.4329 |
| 47 | 0.13006 | SLU_1 | Max | 0. | 0. | 1611.2463 |
| 47 | 0.26012 | SLU_1 | Max | 0. | 0. | 1802.9416 |
| 47 | 0. | SLU_1 | Min | 0. | 0. | 1421.4329 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 47 | 0.13006 | SLU_1 | Min | 0. | 0. | 1611.2463 |
| 47 | 0.26012 | SLU_1 | Min | 0. | 0. | 1802.9416 |
| 47 | 0. | SLU_2 | Max | 0. | 0. | 1416.5659 |
| 47 | 0.13006 | SLU_2 | Max | 0. | 0. | 1604.7667 |
| 47 | 0.26012 | SLU_2 | Max | 0. | 0. | 1794.8493 |
| 47 | 0. | SLU_2 | Min | 0. | 0. | 1416.5659 |
| 47 | 0.13006 | SLU_2 | Min | 0. | 0. | 1604.7667 |
| 47 | 0.26012 | SLU_2 | Min | 0. | 0. | 1794.8493 |
| 47 | 0. | SLU_3 | Max | 0. | 0. | 1003.2459 |
| 47 | 0.13006 | SLU_3 | Max | 0. | 0. | 1193.905 |
| 47 | 0.26012 | SLU_3 | Max | 0. | 0. | 1386.446 |
| 47 | 0. | SLU_3 | Min | 0. | 0. | 1003.2459 |
| 47 | 0.13006 | SLU_3 | Min | 0. | 0. | 1193.905 |
| 47 | 0.26012 | SLU_3 | Min | 0. | 0. | 1386.446 |
| 47 | 0. | SLU_4 | Max | 0. | 0. | 1102.4912 |
| 47 | 0.13006 | SLU_4 | Max | 0. | 0. | 1291.0258 |
| 47 | 0.26012 | SLU_4 | Max | 0. | 0. | 1481.4423 |
| 47 | 0. | SLU_4 | Min | 0. | 0. | 1102.4912 |
| 47 | 0.13006 | SLU_4 | Min | 0. | 0. | 1291.0258 |
| 47 | 0.26012 | SLU_4 | Min | 0. | 0. | 1481.4423 |
| 47 | 0. | SLE_F1 | Max | 0. | 0. | 1080.4246 |
| 47 | 0.13006 | SLE_F1 | Max | 0. | 0. | 1221.914 |
| 47 | 0.26012 | SLE_F1 | Max | 0. | 0. | 1364.851 |
| 47 | 0. | SLE_F1 | Min | 0. | 0. | 1080.4246 |
| 47 | 0.13006 | SLE_F1 | Min | 0. | 0. | 1221.914 |
| 47 | 0.26012 | SLE_F1 | Min | 0. | 0. | 1364.851 |
| 47 | 0. | SLE_F2 | Max | 0. | 0. | 1081.6882 |
| 47 | 0.13006 | SLE_F2 | Max | 0. | 0. | 1222.1621 |
| 47 | 0.26012 | SLE_F2 | Max | 0. | 0. | 1364.0836 |
| 47 | 0. | SLE_F2 | Min | 0. | 0. | 1081.6882 |
| 47 | 0.13006 | SLE_F2 | Min | 0. | 0. | 1222.1621 |
| 47 | 0.26012 | SLE_F2 | Min | 0. | 0. | 1364.0836 |
| 47 | 0. | SLE_F3 | Max | 0. | 0. | 838.4755 |
| 47 | 0.13006 | SLE_F3 | Max | 0. | 0. | 979.1802 |
| 47 | 0.26012 | SLE_F3 | Max | 0. | 0. | 1121.3326 |
| 47 | 0. | SLE_F3 | Min | 0. | 0. | 838.4755 |
| 47 | 0.13006 | SLE_F3 | Min | 0. | 0. | 979.1802 |
| 47 | 0.26012 | SLE_F3 | Min | 0. | 0. | 1121.3326 |
| 47 | 0. | SLE_F4 | Max | 0. | 0. | 755.754 |
| 47 | 0.13006 | SLE_F4 | Max | 0. | 0. | 898.0947 |
| 47 | 0.26012 | SLE_F4 | Max | 0. | 0. | 1041.883 |
| 47 | 0. | SLE_F4 | Min | 0. | 0. | 755.754 |
| 47 | 0.13006 | SLE_F4 | Min | 0. | 0. | 898.0947 |
| 47 | 0.26012 | SLE_F4 | Min | 0. | 0. | 1041.883 |
| 47 | 0. | SLE_QP1 | Max | 0. | 0. | 1062.5734 |
| 47 | 0.13006 | SLE_QP1 | Max | 0. | 0. | 1195.9931 |
| 47 | 0.26012 | SLE_QP1 | Max | 0. | 0. | 1330.8605 |
| 47 | 0. | SLE_QP1 | Min | 0. | 0. | 1062.5734 |
| 47 | 0.13006 | SLE_QP1 | Min | 0. | 0. | 1195.9931 |
| 47 | 0.26012 | SLE_QP1 | Min | 0. | 0. | 1330.8605 |
| 47 | 0. | SLE_QP2 | Max | 0. | 0. | 1066.8792 |
| 47 | 0.13006 | SLE_QP2 | Max | 0. | 0. | 1199.3754 |
| 47 | 0.26012 | SLE_QP2 | Max | 0. | 0. | 1333.3192 |
| 47 | 0. | SLE_QP2 | Min | 0. | 0. | 1066.8792 |
| 47 | 0.13006 | SLE_QP2 | Min | 0. | 0. | 1199.3754 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 47 | 0.26012 | SLE_QP2 | Min | 0. | 0. | 1333.3192 |
| 47 | 0. | SLE_QP3 | Max | 0. | 0. | 820.6576 |
| 47 | 0.13006 | SLE_QP3 | Max | 0. | 0. | 953.336 |
| 47 | 0.26012 | SLE_QP3 | Max | 0. | 0. | 1087.462 |
| 47 | 0. | SLE_QP3 | Min | 0. | 0. | 820.6576 |
| 47 | 0.13006 | SLE_QP3 | Min | 0. | 0. | 953.336 |
| 47 | 0.26012 | SLE_QP3 | Min | 0. | 0. | 1087.462 |
| 47 | 0. | SLE_QP4 | Max | 0. | 0. | 727.0741 |
| 47 | 0.13006 | SLE_QP4 | Max | 0. | 0. | 861.4669 |
| 47 | 0.26012 | SLE_QP4 | Max | 0. | 0. | 997.3072 |
| 47 | 0. | SLE_QP4 | Min | 0. | 0. | 727.0741 |
| 47 | 0.13006 | SLE_QP4 | Min | 0. | 0. | 861.4669 |
| 47 | 0.26012 | SLE_QP4 | Min | 0. | 0. | 997.3072 |
| 47 | 0. | SLV_1 | Max | 0. | 0. | 568.6617 |
| 47 | 0.13006 | SLV_1 | Max | 0. | 0. | 734.7076 |
| 47 | 0.26012 | SLV_1 | Max | 0. | 0. | 902.2011 |
| 47 | 0. | SLV_1 | Min | 0. | 0. | 568.6617 |
| 47 | 0.13006 | SLV_1 | Min | 0. | 0. | 734.7076 |
| 47 | 0.26012 | SLV_1 | Min | 0. | 0. | 902.2011 |
| 47 | 0. | SLV_2 | Max | 0. | 0. | 573.8127 |
| 47 | 0.13006 | SLV_2 | Max | 0. | 0. | 739.618 |
| 47 | 0.26012 | SLV_2 | Max | 0. | 0. | 906.871 |
| 47 | 0. | SLV_2 | Min | 0. | 0. | 573.8127 |
| 47 | 0.13006 | SLV_2 | Min | 0. | 0. | 739.618 |
| 47 | 0.26012 | SLV_2 | Min | 0. | 0. | 906.871 |
| 47 | 0. | SLV_3 | Max | 0. | 0. | 351.9388 |
| 47 | 0.13006 | SLV_3 | Max | 0. | 0. | 526.5181 |
| 47 | 0.26012 | SLV_3 | Max | 0. | 0. | 702.545 |
| 47 | 0. | SLV_3 | Min | 0. | 0. | 351.9388 |
| 47 | 0.13006 | SLV_3 | Min | 0. | 0. | 526.5181 |
| 47 | 0.26012 | SLV_3 | Min | 0. | 0. | 702.545 |
| 47 | 0. | SLV_4 | Max | 0. | 0. | 356.2241 |
| 47 | 0.13006 | SLV_4 | Max | 0. | 0. | 530.5394 |
| 47 | 0.26012 | SLV_4 | Max | 0. | 0. | 706.3024 |
| 47 | 0. | SLV_4 | Min | 0. | 0. | 356.2241 |
| 47 | 0.13006 | SLV_4 | Min | 0. | 0. | 530.5394 |
| 47 | 0.26012 | SLV_4 | Min | 0. | 0. | 706.3024 |
| 47 | 0. | SLD_1 | Max | 0. | 0. | 763.5303 |
| 47 | 0.13006 | SLD_1 | Max | 0. | 0. | 906.4784 |
| 47 | 0.26012 | SLD_1 | Max | 0. | 0. | 1050.8741 |
| 47 | 0. | SLD_1 | Min | 0. | 0. | 763.5303 |
| 47 | 0.13006 | SLD_1 | Min | 0. | 0. | 906.4784 |
| 47 | 0.26012 | SLD_1 | Min | 0. | 0. | 1050.8741 |
| 47 | 0. | SLD_2 | Max | 0. | 0. | 766.6612 |
| 47 | 0.13006 | SLD_2 | Max | 0. | 0. | 909.5077 |
| 47 | 0.26012 | SLD_2 | Max | 0. | 0. | 1053.8018 |
| 47 | 0. | SLD_2 | Min | 0. | 0. | 766.6612 |
| 47 | 0.13006 | SLD_2 | Min | 0. | 0. | 909.5077 |
| 47 | 0.26012 | SLD_2 | Min | 0. | 0. | 1053.8018 |
| 47 | 0. | SLD_3 | Max | 0. | 0. | 519.3416 |
| 47 | 0.13006 | SLD_3 | Max | 0. | 0. | 670.1294 |
| 47 | 0.26012 | SLD_3 | Max | 0. | 0. | 822.3648 |
| 47 | 0. | SLD_3 | Min | 0. | 0. | 519.3416 |
| 47 | 0.13006 | SLD_3 | Min | 0. | 0. | 670.1294 |
| 47 | 0.26012 | SLD_3 | Min | 0. | 0. | 822.3648 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 47 | 0. | SLD_4 | Max | 0. | 0. | 521.2887 |
| 47 | 0.13006 | SLD_4 | Max | 0. | 0. | 671.9542 |
| 47 | 0.26012 | SLD_4 | Max | 0. | 0. | 824.0673 |
| 47 | 0. | SLD_4 | Min | 0. | 0. | 521.2887 |
| 47 | 0.13006 | SLD_4 | Min | 0. | 0. | 671.9542 |
| 47 | 0.26012 | SLD_4 | Min | 0. | 0. | 824.0673 |
| 47 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1010.063 |
| 47 | 0.13006 | SLU_IDR_1 | Max | 0. | 0. | 1146.8607 |
| 47 | 0.26012 | SLU_IDR_1 | Max | 0. | 0. | 1285.3776 |
| 47 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1010.063 |
| 47 | 0.13006 | SLU_IDR_1 | Min | 0. | 0. | 1146.8607 |
| 47 | 0.26012 | SLU_IDR_1 | Min | 0. | 0. | 1285.3776 |
| 47 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1242.6004 |
| 47 | 0.13006 | SLU_IDR_2 | Max | 0. | 0. | 1379.7264 |
| 47 | 0.26012 | SLU_IDR_2 | Max | 0. | 0. | 1518.5717 |
| 47 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1242.6004 |
| 47 | 0.13006 | SLU_IDR_2 | Min | 0. | 0. | 1379.7264 |
| 47 | 0.26012 | SLU_IDR_2 | Min | 0. | 0. | 1518.5717 |
| 47 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -406.8293 |
| 47 | 0.13006 | SISMA WOOD SLV-1 | Max | 0. | 0. | -371.5763 |
| 47 | 0.26012 | SISMA WOOD SLV-1 | Max | 0. | 0. | -336.3232 |
| 47 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -406.8293 |
| 47 | 0.13006 | SISMA WOOD SLV-1 | Min | 0. | 0. | -371.5763 |
| 47 | 0.26012 | SISMA WOOD SLV-1 | Min | 0. | 0. | -336.3232 |
| 47 | 0. | DEAD-1 | Max | 0. | 0. | -84.8973 |
| 47 | 0.13006 | DEAD-1 | Max | 0. | 0. | -73.4118 |
| 47 | 0.26012 | DEAD-1 | Max | 0. | 0. | -62.5605 |
| 47 | 0. | DEAD-1 | Min | 0. | 0. | -84.8973 |
| 47 | 0.13006 | DEAD-1 | Min | 0. | 0. | -73.4118 |
| 47 | 0.26012 | DEAD-1 | Min | 0. | 0. | -62.5605 |
| 47 | 0. | SLU_PROVA | | 0. | 0. | 1306.848 |
| 47 | 0.13006 | SLU_PROVA | | 0. | 0. | 1484.0303 |
| 47 | 0.26012 | SLU_PROVA | | 0. | 0. | 1663.0945 |
| 48 | 0. | DEAD | | 0. | 0. | -76.1902 |
| 48 | 0.13006 | DEAD | | 0. | 0. | -41.9436 |
| 48 | 0.26012 | DEAD | | 0. | 0. | -8.3311 |
| 48 | 0. | SIMM_KA | | 0. | 0. | 47.1533 |
| 48 | 0.13006 | SIMM_KA | | 0. | 0. | 49.7653 |
| 48 | 0.26012 | SIMM_KA | | 0. | 0. | 52.3774 |
| 48 | 0. | SIMM_K0 | | 0. | 0. | 74.6003 |
| 48 | 0.13006 | SIMM_K0 | | 0. | 0. | 78.595 |
| 48 | 0.26012 | SIMM_K0 | | 0. | 0. | 82.5896 |
| 48 | 0. | A--SIMM_KA | | 0. | 0. | -34.5136 |
| 48 | 0.13006 | A--SIMM_KA | | 0. | 0. | -27.805 |
| 48 | 0.26012 | A--SIMM_KA | | 0. | 0. | -21.0964 |
| 48 | 0. | A--SIMM_K0 | | 0. | 0. | -52.7284 |
| 48 | 0.13006 | A--SIMM_K0 | | 0. | 0. | -42.6416 |
| 48 | 0.26012 | A--SIMM_K0 | | 0. | 0. | -32.5548 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 48 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | 14.6141 |
| 48 | 0.13006 | A-- SIMM_SOVR_K A | | 0. | 0. | 14.9428 |
| 48 | 0.26012 | A-- SIMM_SOVR_K A | | 0. | 0. | 15.2716 |
| 48 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | 21.9102 |
| 48 | 0.13006 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 22.4031 |
| 48 | 0.26012 | A-- SIMM_SOVR_K 0 | | 0. | 0. | 22.8959 |
| 48 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | 21.9102 |
| 48 | 0.13006 | SIMM_SOVR_K 0 | | 0. | 0. | 22.4031 |
| 48 | 0.26012 | SIMM_SOVR_K 0 | | 0. | 0. | 22.8959 |
| 48 | 0. | SIMM_SOVR_K A | | 0. | 0. | 14.6141 |
| 48 | 0.13006 | SIMM_SOVR_K A | | 0. | 0. | 14.9428 |
| 48 | 0.26012 | SIMM_SOVR_K A | | 0. | 0. | 15.2716 |
| 48 | 0. | SOVR | | 0. | 0. | 52.2209 |
| 48 | 0.13006 | SOVR | | 0. | 0. | 72.2824 |
| 48 | 0.26012 | SOVR | | 0. | 0. | 92.3439 |
| 48 | 0. | TERR_SIMM | | 0. | 0. | 245.7732 |
| 48 | 0.13006 | TERR_SIMM | | 0. | 0. | 326.5373 |
| 48 | 0.26012 | TERR_SIMM | | 0. | 0. | 407.3014 |
| 48 | 0. | TERR_A--SIMM | | 0. | 0. | 221.5076 |
| 48 | 0.13006 | TERR_A--SIMM | | 0. | 0. | 300.6175 |
| 48 | 0.26012 | TERR_A--SIMM | | 0. | 0. | 379.7274 |
| 48 | 0. | INERZIA H SLV | | 0. | 0. | -3.6159 |
| 48 | 0.13006 | INERZIA H SLV | | 0. | 0. | -3.0555 |
| 48 | 0.26012 | INERZIA H SLV | | 0. | 0. | -2.4951 |
| 48 | 0. | INERZIA V + SLV | | 0. | 0. | -1.1843 |
| 48 | 0.13006 | INERZIA V + SLV | | 0. | 0. | -0.6359 |
| 48 | 0.26012 | INERZIA V + SLV | | 0. | 0. | -0.0876 |
| 48 | 0. | INERZIA V - SLV | | 0. | 0. | 1.1843 |
| 48 | 0.13006 | INERZIA V - SLV | | 0. | 0. | 0.6359 |
| 48 | 0.26012 | INERZIA V - SLV | | 0. | 0. | 0.0876 |
| 48 | 0. | SISMA WOOD SLV | | 0. | 0. | -180.4968 |
| 48 | 0.13006 | SISMA WOOD SLV | | 0. | 0. | -155.396 |
| 48 | 0.26012 | SISMA WOOD SLV | | 0. | 0. | -130.2952 |
| 48 | 0. | iDROSTATICA | | 0. | 0. | 949.5842 |
| 48 | 0.13006 | iDROSTATICA | | 0. | 0. | 1003.3296 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 48 | 0.26012 | iDROSTATICA | | 0. | 0. | 1059.1568 |
| 48 | 0. | SISMA WOOD SLD | | 0. | 0. | -79.7147 |
| 48 | 0.13006 | SISMA WOOD SLD | | 0. | 0. | -68.6292 |
| 48 | 0.26012 | SISMA WOOD SLD | | 0. | 0. | -57.5436 |
| 48 | 0. | INERZIA H SLD | | 0. | 0. | -1.5969 |
| 48 | 0.13006 | INERZIA H SLD | | 0. | 0. | -1.3494 |
| 48 | 0.26012 | INERZIA H SLD | | 0. | 0. | -1.1019 |
| 48 | 0. | INERZIA V + SLD | | 0. | 0. | -0.523 |
| 48 | 0.13006 | INERZIA V + SLD | | 0. | 0. | -0.2809 |
| 48 | 0.26012 | INERZIA V + SLD | | 0. | 0. | -0.0387 |
| 48 | 0. | INERZIA V SLD | | 0. | 0. | 0.523 |
| 48 | 0.13006 | INERZIA V SLD | | 0. | 0. | 0.2809 |
| 48 | 0.26012 | INERZIA V SLD | | 0. | 0. | 0.0387 |
| 48 | 0. | INERZIA V -1 | | 0. | 0. | 1.1843 |
| 48 | 0.13006 | INERZIA V -1 | | 0. | 0. | 0.6359 |
| 48 | 0.26012 | INERZIA V -1 | | 0. | 0. | 0.0876 |
| 48 | 0. | SLU_1 | Max | 0. | 0. | 1802.9416 |
| 48 | 0.13006 | SLU_1 | Max | 0. | 0. | 2080.5951 |
| 48 | 0.26012 | SLU_1 | Max | 0. | 0. | 2360.1305 |
| 48 | 0. | SLU_1 | Min | 0. | 0. | 1802.9416 |
| 48 | 0.13006 | SLU_1 | Min | 0. | 0. | 2080.5951 |
| 48 | 0.26012 | SLU_1 | Min | 0. | 0. | 2360.1305 |
| 48 | 0. | SLU_2 | Max | 0. | 0. | 1794.8493 |
| 48 | 0.13006 | SLU_2 | Max | 0. | 0. | 2071.7841 |
| 48 | 0.26012 | SLU_2 | Max | 0. | 0. | 2350.6009 |
| 48 | 0. | SLU_2 | Min | 0. | 0. | 1794.8493 |
| 48 | 0.13006 | SLU_2 | Min | 0. | 0. | 2071.7841 |
| 48 | 0.26012 | SLU_2 | Min | 0. | 0. | 2350.6009 |
| 48 | 0. | SLU_3 | Max | 0. | 0. | 1386.446 |
| 48 | 0.13006 | SLU_3 | Max | 0. | 0. | 1670.0974 |
| 48 | 0.26012 | SLU_3 | Max | 0. | 0. | 1955.6306 |
| 48 | 0. | SLU_3 | Min | 0. | 0. | 1386.446 |
| 48 | 0.13006 | SLU_3 | Min | 0. | 0. | 1670.0974 |
| 48 | 0.26012 | SLU_3 | Min | 0. | 0. | 1955.6306 |
| 48 | 0. | SLU_4 | Max | 0. | 0. | 1481.4423 |
| 48 | 0.13006 | SLU_4 | Max | 0. | 0. | 1762.691 |
| 48 | 0.26012 | SLU_4 | Max | 0. | 0. | 2045.8216 |
| 48 | 0. | SLU_4 | Min | 0. | 0. | 1481.4423 |
| 48 | 0.13006 | SLU_4 | Min | 0. | 0. | 1762.691 |
| 48 | 0.26012 | SLU_4 | Min | 0. | 0. | 2045.8216 |
| 48 | 0. | SLE_F1 | Max | 0. | 0. | 1364.851 |
| 48 | 0.13006 | SLE_F1 | Max | 0. | 0. | 1569.0695 |
| 48 | 0.26012 | SLE_F1 | Max | 0. | 0. | 1774.7356 |
| 48 | 0. | SLE_F1 | Min | 0. | 0. | 1364.851 |
| 48 | 0.13006 | SLE_F1 | Min | 0. | 0. | 1569.0695 |
| 48 | 0.26012 | SLE_F1 | Min | 0. | 0. | 1774.7356 |
| 48 | 0. | SLE_F2 | Max | 0. | 0. | 1364.0836 |
| 48 | 0.13006 | SLE_F2 | Max | 0. | 0. | 1567.8347 |
| 48 | 0.26012 | SLE_F2 | Max | 0. | 0. | 1773.0333 |
| 48 | 0. | SLE_F2 | Min | 0. | 0. | 1364.0836 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 48 | 0.13006 | SLE_F2 | Min | 0. | 0. | 1567.8347 |
| 48 | 0.26012 | SLE_F2 | Min | 0. | 0. | 1773.0333 |
| 48 | 0. | SLE_F3 | Max | 0. | 0. | 1121.3326 |
| 48 | 0.13006 | SLE_F3 | Max | 0. | 0. | 1328.4359 |
| 48 | 0.26012 | SLE_F3 | Max | 0. | 0. | 1536.9869 |
| 48 | 0. | SLE_F3 | Min | 0. | 0. | 1121.3326 |
| 48 | 0.13006 | SLE_F3 | Min | 0. | 0. | 1328.4359 |
| 48 | 0.26012 | SLE_F3 | Min | 0. | 0. | 1536.9869 |
| 48 | 0. | SLE_F4 | Max | 0. | 0. | 1041.883 |
| 48 | 0.13006 | SLE_F4 | Max | 0. | 0. | 1250.9116 |
| 48 | 0.26012 | SLE_F4 | Max | 0. | 0. | 1461.3878 |
| 48 | 0. | SLE_F4 | Min | 0. | 0. | 1041.883 |
| 48 | 0.13006 | SLE_F4 | Min | 0. | 0. | 1250.9116 |
| 48 | 0.26012 | SLE_F4 | Min | 0. | 0. | 1461.3878 |
| 48 | 0. | SLE_QP1 | Max | 0. | 0. | 1330.8605 |
| 48 | 0.13006 | SLE_QP1 | Max | 0. | 0. | 1517.8002 |
| 48 | 0.26012 | SLE_QP1 | Max | 0. | 0. | 1706.1876 |
| 48 | 0. | SLE_QP1 | Min | 0. | 0. | 1330.8605 |
| 48 | 0.13006 | SLE_QP1 | Min | 0. | 0. | 1517.8002 |
| 48 | 0.26012 | SLE_QP1 | Min | 0. | 0. | 1706.1876 |
| 48 | 0. | SLE_QP2 | Max | 0. | 0. | 1333.3192 |
| 48 | 0.13006 | SLE_QP2 | Max | 0. | 0. | 1519.8445 |
| 48 | 0.26012 | SLE_QP2 | Max | 0. | 0. | 1707.8175 |
| 48 | 0. | SLE_QP2 | Min | 0. | 0. | 1333.3192 |
| 48 | 0.13006 | SLE_QP2 | Min | 0. | 0. | 1519.8445 |
| 48 | 0.26012 | SLE_QP2 | Min | 0. | 0. | 1707.8175 |
| 48 | 0. | SLE_QP3 | Max | 0. | 0. | 1087.462 |
| 48 | 0.13006 | SLE_QP3 | Max | 0. | 0. | 1277.4022 |
| 48 | 0.26012 | SLE_QP3 | Max | 0. | 0. | 1468.7899 |
| 48 | 0. | SLE_QP3 | Min | 0. | 0. | 1087.462 |
| 48 | 0.13006 | SLE_QP3 | Min | 0. | 0. | 1277.4022 |
| 48 | 0.26012 | SLE_QP3 | Min | 0. | 0. | 1468.7899 |
| 48 | 0. | SLE_QP4 | Max | 0. | 0. | 997.3072 |
| 48 | 0.13006 | SLE_QP4 | Max | 0. | 0. | 1189.375 |
| 48 | 0.26012 | SLE_QP4 | Max | 0. | 0. | 1382.8903 |
| 48 | 0. | SLE_QP4 | Min | 0. | 0. | 997.3072 |
| 48 | 0.13006 | SLE_QP4 | Min | 0. | 0. | 1189.375 |
| 48 | 0.26012 | SLE_QP4 | Min | 0. | 0. | 1382.8903 |
| 48 | 0. | SLV_1 | Max | 0. | 0. | 902.2011 |
| 48 | 0.13006 | SLV_1 | Max | 0. | 0. | 1125.6555 |
| 48 | 0.26012 | SLV_1 | Max | 0. | 0. | 1350.5575 |
| 48 | 0. | SLV_1 | Min | 0. | 0. | 902.2011 |
| 48 | 0.13006 | SLV_1 | Min | 0. | 0. | 1125.6555 |
| 48 | 0.26012 | SLV_1 | Min | 0. | 0. | 1350.5575 |
| 48 | 0. | SLV_2 | Max | 0. | 0. | 906.871 |
| 48 | 0.13006 | SLV_2 | Max | 0. | 0. | 1129.1636 |
| 48 | 0.26012 | SLV_2 | Max | 0. | 0. | 1352.9038 |
| 48 | 0. | SLV_2 | Min | 0. | 0. | 906.871 |
| 48 | 0.13006 | SLV_2 | Min | 0. | 0. | 1129.1636 |
| 48 | 0.26012 | SLV_2 | Min | 0. | 0. | 1352.9038 |
| 48 | 0. | SLV_3 | Max | 0. | 0. | 702.545 |
| 48 | 0.13006 | SLV_3 | Max | 0. | 0. | 937.595 |
| 48 | 0.26012 | SLV_3 | Max | 0. | 0. | 1174.0927 |
| 48 | 0. | SLV_3 | Min | 0. | 0. | 702.545 |
| 48 | 0.13006 | SLV_3 | Min | 0. | 0. | 937.595 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 48 | 0.26012 | SLV_3 | Min | 0. | 0. | 1174.0927 |
| 48 | 0. | SLV_4 | Max | 0. | 0. | 706.3024 |
| 48 | 0.13006 | SLV_4 | Max | 0. | 0. | 940.1707 |
| 48 | 0.26012 | SLV_4 | Max | 0. | 0. | 1175.4867 |
| 48 | 0. | SLV_4 | Min | 0. | 0. | 706.3024 |
| 48 | 0.13006 | SLV_4 | Min | 0. | 0. | 940.1707 |
| 48 | 0.26012 | SLV_4 | Min | 0. | 0. | 1175.4867 |
| 48 | 0. | SLD_1 | Max | 0. | 0. | 1050.8741 |
| 48 | 0.13006 | SLD_1 | Max | 0. | 0. | 1249.5611 |
| 48 | 0.26012 | SLD_1 | Max | 0. | 0. | 1449.6957 |
| 48 | 0. | SLD_1 | Min | 0. | 0. | 1050.8741 |
| 48 | 0.13006 | SLD_1 | Min | 0. | 0. | 1249.5611 |
| 48 | 0.26012 | SLD_1 | Min | 0. | 0. | 1449.6957 |
| 48 | 0. | SLD_2 | Max | 0. | 0. | 1053.8018 |
| 48 | 0.13006 | SLD_2 | Max | 0. | 0. | 1251.9472 |
| 48 | 0.26012 | SLD_2 | Max | 0. | 0. | 1451.5403 |
| 48 | 0. | SLD_2 | Min | 0. | 0. | 1053.8018 |
| 48 | 0.13006 | SLD_2 | Min | 0. | 0. | 1251.9472 |
| 48 | 0.26012 | SLD_2 | Min | 0. | 0. | 1451.5403 |
| 48 | 0. | SLD_3 | Max | 0. | 0. | 822.3648 |
| 48 | 0.13006 | SLD_3 | Max | 0. | 0. | 1031.9336 |
| 48 | 0.26012 | SLD_3 | Max | 0. | 0. | 1242.95 |
| 48 | 0. | SLD_3 | Min | 0. | 0. | 822.3648 |
| 48 | 0.13006 | SLD_3 | Min | 0. | 0. | 1031.9336 |
| 48 | 0.26012 | SLD_3 | Min | 0. | 0. | 1242.95 |
| 48 | 0. | SLD_4 | Max | 0. | 0. | 824.0673 |
| 48 | 0.13006 | SLD_4 | Max | 0. | 0. | 1033.1025 |
| 48 | 0.26012 | SLD_4 | Max | 0. | 0. | 1243.5853 |
| 48 | 0. | SLD_4 | Min | 0. | 0. | 824.0673 |
| 48 | 0.13006 | SLD_4 | Min | 0. | 0. | 1033.1025 |
| 48 | 0.26012 | SLD_4 | Min | 0. | 0. | 1243.5853 |
| 48 | 0. | SLU_IDR_1 | Max | 0. | 0. | 1285.3776 |
| 48 | 0.13006 | SLU_IDR_1 | Max | 0. | 0. | 1467.8811 |
| 48 | 0.26012 | SLU_IDR_1 | Max | 0. | 0. | 1652.1037 |
| 48 | 0. | SLU_IDR_1 | Min | 0. | 0. | 1285.3776 |
| 48 | 0.13006 | SLU_IDR_1 | Min | 0. | 0. | 1467.8811 |
| 48 | 0.26012 | SLU_IDR_1 | Min | 0. | 0. | 1652.1037 |
| 48 | 0. | SLU_IDR_2 | Max | 0. | 0. | 1518.5717 |
| 48 | 0.13006 | SLU_IDR_2 | Max | 0. | 0. | 1698.0257 |
| 48 | 0.26012 | SLU_IDR_2 | Max | 0. | 0. | 1879.199 |
| 48 | 0. | SLU_IDR_2 | Min | 0. | 0. | 1518.5717 |
| 48 | 0.13006 | SLU_IDR_2 | Min | 0. | 0. | 1698.0257 |
| 48 | 0.26012 | SLU_IDR_2 | Min | 0. | 0. | 1879.199 |
| 48 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | -336.3232 |
| 48 | 0.13006 | SISMA WOOD SLV-1 | Max | 0. | 0. | -286.0373 |
| 48 | 0.26012 | SISMA WOOD SLV-1 | Max | 0. | 0. | -235.7515 |
| 48 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | -336.3232 |
| 48 | 0.13006 | SISMA WOOD SLV-1 | Min | 0. | 0. | -286.0373 |
| 48 | 0.26012 | SISMA WOOD SLV-1 | Min | 0. | 0. | -235.7515 |
| 48 | 0. | DEAD-1 | Max | 0. | 0. | -62.5605 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 48 | 0.13006 | DEAD-1 | Max | 0. | 0. | -21.6928 |
| 48 | 0.26012 | DEAD-1 | Max | 0. | 0. | 18.5407 |
| 48 | 0. | DEAD-1 | Min | 0. | 0. | -62.5605 |
| 48 | 0.13006 | DEAD-1 | Min | 0. | 0. | -21.6928 |
| 48 | 0.26012 | DEAD-1 | Min | 0. | 0. | 18.5407 |
| 48 | 0. | SLU_PROVA | | 0. | 0. | 1663.0945 |
| 48 | 0.13006 | SLU_PROVA | | 0. | 0. | 1918.502 |
| 48 | 0.26012 | SLU_PROVA | | 0. | 0. | 2175.7915 |
| 49 | 0. | DEAD | | 0. | 0. | 8.3311 |
| 49 | 0.1319 | DEAD | | 0. | 0. | 1.646 |
| 49 | 0.2638 | DEAD | | 0. | 0. | -5.0391 |
| 49 | 0. | SIMM_KA | | 0. | 0. | -52.3774 |
| 49 | 0.1319 | SIMM_KA | | 0. | 0. | -33.7521 |
| 49 | 0.2638 | SIMM_KA | | 0. | 0. | -16.1015 |
| 49 | 0. | SIMM_K0 | | 0. | 0. | -82.5896 |
| 49 | 0.1319 | SIMM_K0 | | 0. | 0. | -54.4891 |
| 49 | 0.2638 | SIMM_K0 | | 0. | 0. | -27.8506 |
| 49 | 0. | A--SIMM_KA | | 0. | 0. | 21.0964 |
| 49 | 0.1319 | A--SIMM_KA | | 0. | 0. | 42.9911 |
| 49 | 0.2638 | A--SIMM_KA | | 0. | 0. | 63.9665 |
| 49 | 0. | A--SIMM_K0 | | 0. | 0. | 32.5548 |
| 49 | 0.1319 | A--SIMM_K0 | | 0. | 0. | 66.4454 |
| 49 | 0.2638 | A--SIMM_K0 | | 0. | 0. | 98.957 |
| 49 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -15.2716 |
| 49 | 0.1319 | A-- SIMM_SOVR_K A | | 0. | 0. | -14.1575 |
| 49 | 0.2638 | A-- SIMM_SOVR_K A | | 0. | 0. | -13.0435 |
| 49 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -22.8959 |
| 49 | 0.1319 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -21.2257 |
| 49 | 0.2638 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -19.5554 |
| 49 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -22.8959 |
| 49 | 0.1319 | SIMM_SOVR_K 0 | | 0. | 0. | -21.2257 |
| 49 | 0.2638 | SIMM_SOVR_K 0 | | 0. | 0. | -19.5554 |
| 49 | 0. | SIMM_SOVR_K A | | 0. | 0. | -15.2716 |
| 49 | 0.1319 | SIMM_SOVR_K A | | 0. | 0. | -14.1575 |
| 49 | 0.2638 | SIMM_SOVR_K A | | 0. | 0. | -13.0435 |
| 49 | 0. | SOVR | | 0. | 0. | -92.3439 |
| 49 | 0.1319 | SOVR | | 0. | 0. | -94.8553 |
| 49 | 0.2638 | SOVR | | 0. | 0. | -97.3668 |
| 49 | 0. | TERR_SIMM | | 0. | 0. | -407.3014 |
| 49 | 0.1319 | TERR_SIMM | | 0. | 0. | -414.3209 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 49 | 0.2638 | TERR_SIMM | | 0. | 0. | -421.3404 |
| 49 | 0. | TERR_A--SIMM | | 0. | 0. | -379.7274 |
| 49 | 0.1319 | TERR_A--SIMM | | 0. | 0. | -387.4582 |
| 49 | 0.2638 | TERR_A--SIMM | | 0. | 0. | -395.1891 |
| 49 | 0. | INERZIA H SLV | | 0. | 0. | 2.4951 |
| 49 | 0.1319 | INERZIA H SLV | | 0. | 0. | 3.4034 |
| 49 | 0.2638 | INERZIA H SLV | | 0. | 0. | 4.3116 |
| 49 | 0. | INERZIA V + SLV | | 0. | 0. | 0.0876 |
| 49 | 0.1319 | INERZIA V + SLV | | 0. | 0. | -0.0177 |
| 49 | 0.2638 | INERZIA V + SLV | | 0. | 0. | -0.123 |
| 49 | 0. | INERZIA V - SLV | | 0. | 0. | -0.0876 |
| 49 | 0.1319 | INERZIA V - SLV | | 0. | 0. | 0.0177 |
| 49 | 0.2638 | INERZIA V - SLV | | 0. | 0. | 0.123 |
| 49 | 0. | SISMA WOOD SLV | | 0. | 0. | 130.2952 |
| 49 | 0.1319 | SISMA WOOD SLV | | 0. | 0. | 175.6274 |
| 49 | 0.2638 | SISMA WOOD SLV | | 0. | 0. | 220.9595 |
| 49 | 0. | iDROSTATICA | | 0. | 0. | -1059.1568 |
| 49 | 0.1319 | iDROSTATICA | | 0. | 0. | -1000.9266 |
| 49 | 0.2638 | iDROSTATICA | | 0. | 0. | -944.8139 |
| 49 | 0. | SISMA WOOD SLD | | 0. | 0. | 57.5436 |
| 49 | 0.1319 | SISMA WOOD SLD | | 0. | 0. | 77.5641 |
| 49 | 0.2638 | SISMA WOOD SLD | | 0. | 0. | 97.5846 |
| 49 | 0. | INERZIA H SLD | | 0. | 0. | 1.1019 |
| 49 | 0.1319 | INERZIA H SLD | | 0. | 0. | 1.5031 |
| 49 | 0.2638 | INERZIA H SLD | | 0. | 0. | 1.9042 |
| 49 | 0. | INERZIA V + SLD | | 0. | 0. | 0.0387 |
| 49 | 0.1319 | INERZIA V + SLD | | 0. | 0. | -0.0078 |
| 49 | 0.2638 | INERZIA V + SLD | | 0. | 0. | -0.0543 |
| 49 | 0. | INERZIA V SLD | | 0. | 0. | -0.0387 |
| 49 | 0.1319 | INERZIA V SLD | | 0. | 0. | 0.0078 |
| 49 | 0.2638 | INERZIA V SLD | | 0. | 0. | 0.0543 |
| 49 | 0. | INERZIA V -1 | | 0. | 0. | -0.0876 |
| 49 | 0.1319 | INERZIA V -1 | | 0. | 0. | 0.0177 |
| 49 | 0.2638 | INERZIA V -1 | | 0. | 0. | 0.123 |
| 49 | 0. | SLU_1 | Max | 0. | 0. | -2360.1305 |
| 49 | 0.1319 | SLU_1 | Max | 0. | 0. | -2267.8983 |
| 49 | 0.2638 | SLU_1 | Max | 0. | 0. | -2180.3193 |
| 49 | 0. | SLU_1 | Min | 0. | 0. | -2360.1305 |
| 49 | 0.1319 | SLU_1 | Min | 0. | 0. | -2267.8983 |
| 49 | 0.2638 | SLU_1 | Min | 0. | 0. | -2180.3193 |
| 49 | 0. | SLU_2 | Max | 0. | 0. | -2350.6009 |
| 49 | 0.1319 | SLU_2 | Max | 0. | 0. | -2270.8176 |
| 49 | 0.2638 | SLU_2 | Max | 0. | 0. | -2195.0542 |
| 49 | 0. | SLU_2 | Min | 0. | 0. | -2350.6009 |
| 49 | 0.1319 | SLU_2 | Min | 0. | 0. | -2270.8176 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 49 | 0.2638 | SLU_2 | Min | 0. | 0. | -2195.0542 |
| 49 | 0. | SLU_3 | Max | 0. | 0. | -1955.6306 |
| 49 | 0.1319 | SLU_3 | Max | 0. | 0. | -1857.6703 |
| 49 | 0.2638 | SLU_3 | Max | 0. | 0. | -1764.2553 |
| 49 | 0. | SLU_3 | Min | 0. | 0. | -1955.6306 |
| 49 | 0.1319 | SLU_3 | Min | 0. | 0. | -1857.6703 |
| 49 | 0.2638 | SLU_3 | Min | 0. | 0. | -1764.2553 |
| 49 | 0. | SLU_4 | Max | 0. | 0. | -2045.8216 |
| 49 | 0.1319 | SLU_4 | Max | 0. | 0. | -1964.509 |
| 49 | 0.2638 | SLU_4 | Max | 0. | 0. | -1887.1444 |
| 49 | 0. | SLU_4 | Min | 0. | 0. | -2045.8216 |
| 49 | 0.1319 | SLU_4 | Min | 0. | 0. | -1964.509 |
| 49 | 0.2638 | SLU_4 | Min | 0. | 0. | -1887.1444 |
| 49 | 0. | SLE_F1 | Max | 0. | 0. | -1774.7356 |
| 49 | 0.1319 | SLE_F1 | Max | 0. | 0. | -1702.8693 |
| 49 | 0.2638 | SLE_F1 | Max | 0. | 0. | -1634.5825 |
| 49 | 0. | SLE_F1 | Min | 0. | 0. | -1774.7356 |
| 49 | 0.1319 | SLE_F1 | Min | 0. | 0. | -1702.8693 |
| 49 | 0.2638 | SLE_F1 | Min | 0. | 0. | -1634.5825 |
| 49 | 0. | SLE_F2 | Max | 0. | 0. | -1773.0333 |
| 49 | 0.1319 | SLE_F2 | Max | 0. | 0. | -1710.4473 |
| 49 | 0.2638 | SLE_F2 | Max | 0. | 0. | -1650.9534 |
| 49 | 0. | SLE_F2 | Min | 0. | 0. | -1773.0333 |
| 49 | 0.1319 | SLE_F2 | Min | 0. | 0. | -1710.4473 |
| 49 | 0.2638 | SLE_F2 | Min | 0. | 0. | -1650.9534 |
| 49 | 0. | SLE_F3 | Max | 0. | 0. | -1536.9869 |
| 49 | 0.1319 | SLE_F3 | Max | 0. | 0. | -1473.3273 |
| 49 | 0.2638 | SLE_F3 | Max | 0. | 0. | -1412.7046 |
| 49 | 0. | SLE_F3 | Min | 0. | 0. | -1536.9869 |
| 49 | 0.1319 | SLE_F3 | Min | 0. | 0. | -1473.3273 |
| 49 | 0.2638 | SLE_F3 | Min | 0. | 0. | -1412.7046 |
| 49 | 0. | SLE_F4 | Max | 0. | 0. | -1461.3878 |
| 49 | 0.1319 | SLE_F4 | Max | 0. | 0. | -1384.4215 |
| 49 | 0.2638 | SLE_F4 | Max | 0. | 0. | -1310.9517 |
| 49 | 0. | SLE_F4 | Min | 0. | 0. | -1461.3878 |
| 49 | 0.1319 | SLE_F4 | Min | 0. | 0. | -1384.4215 |
| 49 | 0.2638 | SLE_F4 | Min | 0. | 0. | -1310.9517 |
| 49 | 0. | SLE_QP1 | Max | 0. | 0. | -1706.1876 |
| 49 | 0.1319 | SLE_QP1 | Max | 0. | 0. | -1632.4561 |
| 49 | 0.2638 | SLE_QP1 | Max | 0. | 0. | -1562.3041 |
| 49 | 0. | SLE_QP1 | Min | 0. | 0. | -1706.1876 |
| 49 | 0.1319 | SLE_QP1 | Min | 0. | 0. | -1632.4561 |
| 49 | 0.2638 | SLE_QP1 | Min | 0. | 0. | -1562.3041 |
| 49 | 0. | SLE_QP2 | Max | 0. | 0. | -1707.8175 |
| 49 | 0.1319 | SLE_QP2 | Max | 0. | 0. | -1642.9758 |
| 49 | 0.2638 | SLE_QP2 | Max | 0. | 0. | -1581.2263 |
| 49 | 0. | SLE_QP2 | Min | 0. | 0. | -1707.8175 |
| 49 | 0.1319 | SLE_QP2 | Min | 0. | 0. | -1642.9758 |
| 49 | 0.2638 | SLE_QP2 | Min | 0. | 0. | -1581.2263 |
| 49 | 0. | SLE_QP3 | Max | 0. | 0. | -1468.7899 |
| 49 | 0.1319 | SLE_QP3 | Max | 0. | 0. | -1403.0662 |
| 49 | 0.2638 | SLE_QP3 | Max | 0. | 0. | -1340.3794 |
| 49 | 0. | SLE_QP3 | Min | 0. | 0. | -1468.7899 |
| 49 | 0.1319 | SLE_QP3 | Min | 0. | 0. | -1403.0662 |
| 49 | 0.2638 | SLE_QP3 | Min | 0. | 0. | -1340.3794 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 49 | 0. | SLE_QP4 | Max | 0. | 0. | -1382.8903 |
| 49 | 0.1319 | SLE_QP4 | Max | 0. | 0. | -1302.7894 |
| 49 | 0.2638 | SLE_QP4 | Max | 0. | 0. | -1226.1849 |
| 49 | 0. | SLE_QP4 | Min | 0. | 0. | -1382.8903 |
| 49 | 0.1319 | SLE_QP4 | Min | 0. | 0. | -1302.7894 |
| 49 | 0.2638 | SLE_QP4 | Min | 0. | 0. | -1226.1849 |
| 49 | 0. | SLV_1 | Max | 0. | 0. | -1350.5575 |
| 49 | 0.1319 | SLV_1 | Max | 0. | 0. | -1176.3613 |
| 49 | 0.2638 | SLV_1 | Max | 0. | 0. | -1005.7447 |
| 49 | 0. | SLV_1 | Min | 0. | 0. | -1350.5575 |
| 49 | 0.1319 | SLV_1 | Min | 0. | 0. | -1176.3613 |
| 49 | 0.2638 | SLV_1 | Min | 0. | 0. | -1005.7447 |
| 49 | 0. | SLV_2 | Max | 0. | 0. | -1352.9038 |
| 49 | 0.1319 | SLV_2 | Max | 0. | 0. | -1178.3526 |
| 49 | 0.2638 | SLV_2 | Max | 0. | 0. | -1007.3808 |
| 49 | 0. | SLV_2 | Min | 0. | 0. | -1352.9038 |
| 49 | 0.1319 | SLV_2 | Min | 0. | 0. | -1178.3526 |
| 49 | 0.2638 | SLV_2 | Min | 0. | 0. | -1007.3808 |
| 49 | 0. | SLV_3 | Max | 0. | 0. | -1174.0927 |
| 49 | 0.1319 | SLV_3 | Max | 0. | 0. | -981.1108 |
| 49 | 0.2638 | SLV_3 | Max | 0. | 0. | -791.6252 |
| 49 | 0. | SLV_3 | Min | 0. | 0. | -1174.0927 |
| 49 | 0.1319 | SLV_3 | Min | 0. | 0. | -981.1108 |
| 49 | 0.2638 | SLV_3 | Min | 0. | 0. | -791.6252 |
| 49 | 0. | SLV_4 | Max | 0. | 0. | -1175.4867 |
| 49 | 0.1319 | SLV_4 | Max | 0. | 0. | -982.1815 |
| 49 | 0.2638 | SLV_4 | Max | 0. | 0. | -792.3729 |
| 49 | 0. | SLV_4 | Min | 0. | 0. | -1175.4867 |
| 49 | 0.1319 | SLV_4 | Min | 0. | 0. | -982.1815 |
| 49 | 0.2638 | SLV_4 | Min | 0. | 0. | -792.3729 |
| 49 | 0. | SLD_1 | Max | 0. | 0. | -1449.6957 |
| 49 | 0.1319 | SLD_1 | Max | 0. | 0. | -1338.549 |
| 49 | 0.2638 | SLD_1 | Max | 0. | 0. | -1230.9818 |
| 49 | 0. | SLD_1 | Min | 0. | 0. | -1449.6957 |
| 49 | 0.1319 | SLD_1 | Min | 0. | 0. | -1338.549 |
| 49 | 0.2638 | SLD_1 | Min | 0. | 0. | -1230.9818 |
| 49 | 0. | SLD_2 | Max | 0. | 0. | -1451.5403 |
| 49 | 0.1319 | SLD_2 | Max | 0. | 0. | -1340.2116 |
| 49 | 0.2638 | SLD_2 | Max | 0. | 0. | -1232.4624 |
| 49 | 0. | SLD_2 | Min | 0. | 0. | -1451.5403 |
| 49 | 0.1319 | SLD_2 | Min | 0. | 0. | -1340.2116 |
| 49 | 0.2638 | SLD_2 | Min | 0. | 0. | -1232.4624 |
| 49 | 0. | SLD_3 | Max | 0. | 0. | -1242.95 |
| 49 | 0.1319 | SLD_3 | Max | 0. | 0. | -1112.9087 |
| 49 | 0.2638 | SLD_3 | Max | 0. | 0. | -986.3638 |
| 49 | 0. | SLD_3 | Min | 0. | 0. | -1242.95 |
| 49 | 0.1319 | SLD_3 | Min | 0. | 0. | -1112.9087 |
| 49 | 0.2638 | SLD_3 | Min | 0. | 0. | -986.3638 |
| 49 | 0. | SLD_4 | Max | 0. | 0. | -1243.5853 |
| 49 | 0.1319 | SLD_4 | Max | 0. | 0. | -1113.4083 |
| 49 | 0.2638 | SLD_4 | Max | 0. | 0. | -986.7277 |
| 49 | 0. | SLD_4 | Min | 0. | 0. | -1243.5853 |
| 49 | 0.1319 | SLD_4 | Min | 0. | 0. | -1113.4083 |
| 49 | 0.2638 | SLD_4 | Min | 0. | 0. | -986.7277 |
| 49 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1652.1037 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 49 | 0.1319 | SLU_IDR_1 | Max | 0. | 0. | -1577.6721 |
| 49 | 0.2638 | SLU_IDR_1 | Max | 0. | 0. | -1506.3972 |
| 49 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1652.1037 |
| 49 | 0.1319 | SLU_IDR_1 | Min | 0. | 0. | -1577.6721 |
| 49 | 0.2638 | SLU_IDR_1 | Min | 0. | 0. | -1506.3972 |
| 49 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1879.199 |
| 49 | 0.1319 | SLU_IDR_2 | Max | 0. | 0. | -1804.8793 |
| 49 | 0.2638 | SLU_IDR_2 | Max | 0. | 0. | -1733.7661 |
| 49 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1879.199 |
| 49 | 0.1319 | SLU_IDR_2 | Min | 0. | 0. | -1804.8793 |
| 49 | 0.2638 | SLU_IDR_2 | Min | 0. | 0. | -1733.7661 |
| 49 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 235.7515 |
| 49 | 0.1319 | SISMA WOOD SLV-1 | Max | 0. | 0. | 338.9995 |
| 49 | 0.2638 | SISMA WOOD SLV-1 | Max | 0. | 0. | 442.2475 |
| 49 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 235.7515 |
| 49 | 0.1319 | SISMA WOOD SLV-1 | Min | 0. | 0. | 338.9995 |
| 49 | 0.2638 | SISMA WOOD SLV-1 | Min | 0. | 0. | 442.2475 |
| 49 | 0. | DEAD-1 | Max | 0. | 0. | -18.5407 |
| 49 | 0.1319 | DEAD-1 | Max | 0. | 0. | -26.3303 |
| 49 | 0.2638 | DEAD-1 | Max | 0. | 0. | -34.1199 |
| 49 | 0. | DEAD-1 | Min | 0. | 0. | -18.5407 |
| 49 | 0.1319 | DEAD-1 | Min | 0. | 0. | -26.3303 |
| 49 | 0.2638 | DEAD-1 | Min | 0. | 0. | -34.1199 |
| 49 | 0. | SLU_PROVA | | 0. | 0. | -2175.7915 |
| 49 | 0.1319 | SLU_PROVA | | 0. | 0. | -2082.6393 |
| 49 | 0.2638 | SLU_PROVA | | 0. | 0. | -1994.1405 |
| 50 | 0. | DEAD | | 0. | 0. | -5.0391 |
| 50 | 0.1318 | DEAD | | 0. | 0. | -11.8153 |
| 50 | 0.2636 | DEAD | | 0. | 0. | -18.5914 |
| 50 | 0. | SIMM_KA | | 0. | 0. | -16.1015 |
| 50 | 0.1318 | SIMM_KA | | 0. | 0. | 0.8709 |
| 50 | 0.2636 | SIMM_KA | | 0. | 0. | 16.87 |
| 50 | 0. | SIMM_K0 | | 0. | 0. | -27.8506 |
| 50 | 0.1318 | SIMM_K0 | | 0. | 0. | -2.2229 |
| 50 | 0.2636 | SIMM_K0 | | 0. | 0. | 21.9451 |
| 50 | 0. | A--SIMM_KA | | 0. | 0. | 63.9665 |
| 50 | 0.1318 | A--SIMM_KA | | 0. | 0. | 83.3845 |
| 50 | 0.2636 | A--SIMM_KA | | 0. | 0. | 101.8847 |
| 50 | 0. | A--SIMM_K0 | | 0. | 0. | 98.957 |
| 50 | 0.1318 | A--SIMM_K0 | | 0. | 0. | 129.2119 |
| 50 | 0.2636 | A--SIMM_K0 | | 0. | 0. | 158.0898 |
| 50 | 0. | A-- SIMM_SOVR_K A | | 0. | 0. | -13.0435 |
| 50 | 0.1318 | A-- SIMM_SOVR_K A | | 0. | 0. | -11.8972 |
| 50 | 0.2636 | A-- SIMM_SOVR_K A | | 0. | 0. | -10.7509 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|-------------------------|----------|-----------|------------|------------|
| 50 | 0. | A-- SIMM_SOVR_K 0 | | 0. | 0. | -19.5554 |
| 50 | 0.1318 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -17.8368 |
| 50 | 0.2636 | A-- SIMM_SOVR_K 0 | | 0. | 0. | -16.1182 |
| 50 | 0. | SIMM_SOVR_K 0 | | 0. | 0. | -19.5554 |
| 50 | 0.1318 | SIMM_SOVR_K 0 | | 0. | 0. | -17.8368 |
| 50 | 0.2636 | SIMM_SOVR_K 0 | | 0. | 0. | -16.1182 |
| 50 | 0. | SIMM_SOVR_K A | | 0. | 0. | -13.0435 |
| 50 | 0.1318 | SIMM_SOVR_K A | | 0. | 0. | -11.8972 |
| 50 | 0.2636 | SIMM_SOVR_K A | | 0. | 0. | -10.7509 |
| 50 | 0. | SOVR | | 0. | 0. | -97.3668 |
| 50 | 0.1318 | SOVR | | 0. | 0. | -100.0938 |
| 50 | 0.2636 | SOVR | | 0. | 0. | -102.8208 |
| 50 | 0. | TERR_SIMM | | 0. | 0. | -421.3404 |
| 50 | 0.1318 | TERR_SIMM | | 0. | 0. | -429.1333 |
| 50 | 0.2636 | TERR_SIMM | | 0. | 0. | -436.9261 |
| 50 | 0. | TERR_A--SIMM | | 0. | 0. | -395.1891 |
| 50 | 0.1318 | TERR_A--SIMM | | 0. | 0. | -404.009 |
| 50 | 0.2636 | TERR_A--SIMM | | 0. | 0. | -412.829 |
| 50 | 0. | INERZIA H SLV | | 0. | 0. | 4.3116 |
| 50 | 0.1318 | INERZIA H SLV | | 0. | 0. | 5.081 |
| 50 | 0.2636 | INERZIA H SLV | | 0. | 0. | 5.8504 |
| 50 | 0. | INERZIA V + SLV | | 0. | 0. | -0.123 |
| 50 | 0.1318 | INERZIA V + SLV | | 0. | 0. | -0.2298 |
| 50 | 0.2636 | INERZIA V + SLV | | 0. | 0. | -0.3366 |
| 50 | 0. | INERZIA V - SLV | | 0. | 0. | 0.123 |
| 50 | 0.1318 | INERZIA V - SLV | | 0. | 0. | 0.2298 |
| 50 | 0.2636 | INERZIA V - SLV | | 0. | 0. | 0.3366 |
| 50 | 0. | SISMA WOOD SLV | | 0. | 0. | 220.9595 |
| 50 | 0.1318 | SISMA WOOD SLV | | 0. | 0. | 260.3858 |
| 50 | 0.2636 | SISMA WOOD SLV | | 0. | 0. | 299.8121 |
| 50 | 0. | iDROSTATICA | | 0. | 0. | -944.8139 |
| 50 | 0.1318 | iDROSTATICA | | 0. | 0. | -891.4325 |
| 50 | 0.2636 | iDROSTATICA | | 0. | 0. | -840.1183 |
| 50 | 0. | SISMA WOOD SLD | | 0. | 0. | 97.5846 |
| 50 | 0.1318 | SISMA WOOD SLD | | 0. | 0. | 114.9969 |
| 50 | 0.2636 | SISMA WOOD SLD | | 0. | 0. | 132.4091 |
| 50 | 0. | INERZIA H SLD | | 0. | 0. | 1.9042 |
| 50 | 0.1318 | INERZIA H SLD | | 0. | 0. | 2.244 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|--------------------|----------|-----------|------------|------------|
| 50 | 0.2636 | INERZIA H SLD | | 0. | 0. | 2.5838 |
| 50 | 0. | INERZIA V + SLD | | 0. | 0. | -0.0543 |
| 50 | 0.1318 | INERZIA V + SLD | | 0. | 0. | -0.1015 |
| 50 | 0.2636 | INERZIA V + SLD | | 0. | 0. | -0.1487 |
| 50 | 0. | INERZIA V SLD | | 0. | 0. | 0.0543 |
| 50 | 0.1318 | INERZIA V SLD | | 0. | 0. | 0.1015 |
| 50 | 0.2636 | INERZIA V SLD | | 0. | 0. | 0.1487 |
| 50 | 0. | INERZIA V -1 | | 0. | 0. | 0.123 |
| 50 | 0.1318 | INERZIA V -1 | | 0. | 0. | 0.2298 |
| 50 | 0.2636 | INERZIA V -1 | | 0. | 0. | 0.3366 |
| 50 | 0. | SLU_1 | Max | 0. | 0. | -2180.3193 |
| 50 | 0.1318 | SLU_1 | Max | 0. | 0. | -2099.3428 |
| 50 | 0.2636 | SLU_1 | Max | 0. | 0. | -2022.9514 |
| 50 | 0. | SLU_1 | Min | 0. | 0. | -2180.3193 |
| 50 | 0.1318 | SLU_1 | Min | 0. | 0. | -2099.3428 |
| 50 | 0.2636 | SLU_1 | Min | 0. | 0. | -2022.9514 |
| 50 | 0. | SLU_2 | Max | 0. | 0. | -2195.0542 |
| 50 | 0.1318 | SLU_2 | Max | 0. | 0. | -2125.5935 |
| 50 | 0.2636 | SLU_2 | Max | 0. | 0. | -2060.0854 |
| 50 | 0. | SLU_2 | Min | 0. | 0. | -2195.0542 |
| 50 | 0.1318 | SLU_2 | Min | 0. | 0. | -2125.5935 |
| 50 | 0.2636 | SLU_2 | Min | 0. | 0. | -2060.0854 |
| 50 | 0. | SLU_3 | Max | 0. | 0. | -1764.2553 |
| 50 | 0.1318 | SLU_3 | Max | 0. | 0. | -1679.9448 |
| 50 | 0.2636 | SLU_3 | Max | 0. | 0. | -1600.1116 |
| 50 | 0. | SLU_3 | Min | 0. | 0. | -1764.2553 |
| 50 | 0.1318 | SLU_3 | Min | 0. | 0. | -1679.9448 |
| 50 | 0.2636 | SLU_3 | Min | 0. | 0. | -1600.1116 |
| 50 | 0. | SLU_4 | Max | 0. | 0. | -1887.1444 |
| 50 | 0.1318 | SLU_4 | Max | 0. | 0. | -1817.9155 |
| 50 | 0.2636 | SLU_4 | Max | 0. | 0. | -1752.5673 |
| 50 | 0. | SLU_4 | Min | 0. | 0. | -1887.1444 |
| 50 | 0.1318 | SLU_4 | Min | 0. | 0. | -1817.9155 |
| 50 | 0.2636 | SLU_4 | Min | 0. | 0. | -1752.5673 |
| 50 | 0. | SLE_F1 | Max | 0. | 0. | -1634.5825 |
| 50 | 0.1318 | SLE_F1 | Max | 0. | 0. | -1571.3095 |
| 50 | 0.2636 | SLE_F1 | Max | 0. | 0. | -1511.5634 |
| 50 | 0. | SLE_F1 | Min | 0. | 0. | -1634.5825 |
| 50 | 0.1318 | SLE_F1 | Min | 0. | 0. | -1571.3095 |
| 50 | 0.2636 | SLE_F1 | Min | 0. | 0. | -1511.5634 |
| 50 | 0. | SLE_F2 | Max | 0. | 0. | -1650.9534 |
| 50 | 0.1318 | SLE_F2 | Max | 0. | 0. | -1596.2341 |
| 50 | 0.2636 | SLE_F2 | Max | 0. | 0. | -1544.5553 |
| 50 | 0. | SLE_F2 | Min | 0. | 0. | -1650.9534 |
| 50 | 0.1318 | SLE_F2 | Min | 0. | 0. | -1596.2341 |
| 50 | 0.2636 | SLE_F2 | Min | 0. | 0. | -1544.5553 |
| 50 | 0. | SLE_F3 | Max | 0. | 0. | -1412.7046 |
| 50 | 0.1318 | SLE_F3 | Max | 0. | 0. | -1358.2562 |
| 50 | 0.2636 | SLE_F3 | Max | 0. | 0. | -1306.7929 |
| 50 | 0. | SLE_F3 | Min | 0. | 0. | -1412.7046 |
| 50 | 0.1318 | SLE_F3 | Min | 0. | 0. | -1358.2562 |
| 50 | 0.2636 | SLE_F3 | Min | 0. | 0. | -1306.7929 |
| 50 | 0. | SLE_F4 | Max | 0. | 0. | -1310.9517 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|------------|----------|-----------|------------|------------|
| 50 | 0.1318 | SLE_F4 | Max | 0. | 0. | -1244.5012 |
| 50 | 0.2636 | SLE_F4 | Max | 0. | 0. | -1181.4948 |
| 50 | 0. | SLE_F4 | Min | 0. | 0. | -1310.9517 |
| 50 | 0.1318 | SLE_F4 | Min | 0. | 0. | -1244.5012 |
| 50 | 0.2636 | SLE_F4 | Min | 0. | 0. | -1181.4948 |
| 50 | 0. | SLE_QP1 | Max | 0. | 0. | -1562.3041 |
| 50 | 0.1318 | SLE_QP1 | Max | 0. | 0. | -1497.0469 |
| 50 | 0.2636 | SLE_QP1 | Max | 0. | 0. | -1435.3165 |
| 50 | 0. | SLE_QP1 | Min | 0. | 0. | -1562.3041 |
| 50 | 0.1318 | SLE_QP1 | Min | 0. | 0. | -1497.0469 |
| 50 | 0.2636 | SLE_QP1 | Min | 0. | 0. | -1435.3165 |
| 50 | 0. | SLE_QP2 | Max | 0. | 0. | -1581.2263 |
| 50 | 0.1318 | SLE_QP2 | Max | 0. | 0. | -1524.1145 |
| 50 | 0.2636 | SLE_QP2 | Max | 0. | 0. | -1470.0431 |
| 50 | 0. | SLE_QP2 | Min | 0. | 0. | -1581.2263 |
| 50 | 0.1318 | SLE_QP2 | Min | 0. | 0. | -1524.1145 |
| 50 | 0.2636 | SLE_QP2 | Min | 0. | 0. | -1470.0431 |
| 50 | 0. | SLE_QP3 | Max | 0. | 0. | -1340.3794 |
| 50 | 0.1318 | SLE_QP3 | Max | 0. | 0. | -1283.7109 |
| 50 | 0.2636 | SLE_QP3 | Max | 0. | 0. | -1230.0275 |
| 50 | 0. | SLE_QP3 | Min | 0. | 0. | -1340.3794 |
| 50 | 0.1318 | SLE_QP3 | Min | 0. | 0. | -1283.7109 |
| 50 | 0.2636 | SLE_QP3 | Min | 0. | 0. | -1230.0275 |
| 50 | 0. | SLE_QP4 | Max | 0. | 0. | -1226.1849 |
| 50 | 0.1318 | SLE_QP4 | Max | 0. | 0. | -1156.6439 |
| 50 | 0.2636 | SLE_QP4 | Max | 0. | 0. | -1090.5469 |
| 50 | 0. | SLE_QP4 | Min | 0. | 0. | -1226.1849 |
| 50 | 0.1318 | SLE_QP4 | Min | 0. | 0. | -1156.6439 |
| 50 | 0.2636 | SLE_QP4 | Min | 0. | 0. | -1090.5469 |
| 50 | 0. | SLV_1 | Max | 0. | 0. | -1005.7447 |
| 50 | 0.1318 | SLV_1 | Max | 0. | 0. | -852.7451 |
| 50 | 0.2636 | SLV_1 | Max | 0. | 0. | -703.2725 |
| 50 | 0. | SLV_1 | Min | 0. | 0. | -1005.7447 |
| 50 | 0.1318 | SLV_1 | Min | 0. | 0. | -852.7451 |
| 50 | 0.2636 | SLV_1 | Min | 0. | 0. | -703.2725 |
| 50 | 0. | SLV_2 | Max | 0. | 0. | -1007.3808 |
| 50 | 0.1318 | SLV_2 | Max | 0. | 0. | -854.0317 |
| 50 | 0.2636 | SLV_2 | Max | 0. | 0. | -704.2096 |
| 50 | 0. | SLV_2 | Min | 0. | 0. | -1007.3808 |
| 50 | 0.1318 | SLV_2 | Min | 0. | 0. | -854.0317 |
| 50 | 0.2636 | SLV_2 | Min | 0. | 0. | -704.2096 |
| 50 | 0. | SLV_3 | Max | 0. | 0. | -791.6252 |
| 50 | 0.1318 | SLV_3 | Max | 0. | 0. | -623.1178 |
| 50 | 0.2636 | SLV_3 | Max | 0. | 0. | -458.0544 |
| 50 | 0. | SLV_3 | Min | 0. | 0. | -791.6252 |
| 50 | 0.1318 | SLV_3 | Min | 0. | 0. | -623.1178 |
| 50 | 0.2636 | SLV_3 | Min | 0. | 0. | -458.0544 |
| 50 | 0. | SLV_4 | Max | 0. | 0. | -792.3729 |
| 50 | 0.1318 | SLV_4 | Max | 0. | 0. | -623.5452 |
| 50 | 0.2636 | SLV_4 | Max | 0. | 0. | -458.1617 |
| 50 | 0. | SLV_4 | Min | 0. | 0. | -792.3729 |
| 50 | 0.1318 | SLV_4 | Min | 0. | 0. | -623.5452 |
| 50 | 0.2636 | SLV_4 | Min | 0. | 0. | -458.1617 |
| 50 | 0. | SLD_1 | Max | 0. | 0. | -1230.9818 |
| 50 | 0.1318 | SLD_1 | Max | 0. | 0. | -1133.263 |

PROGETTAZIONE ATI:

Table: Element Forces - Frames, Part 2 of 2

| Frame | Station m | OutputCase | StepType | T KN-m | M2 KN-m | M3 KN-m |
|-------|--------------|---------------------|----------|-----------|------------|------------|
| 50 | 0.2636 | SLD_1 | Max | 0. | 0. | -1039.0712 |
| 50 | 0. | SLD_1 | Min | 0. | 0. | -1230.9818 |
| 50 | 0.1318 | SLD_1 | Min | 0. | 0. | -1133.263 |
| 50 | 0.2636 | SLD_1 | Min | 0. | 0. | -1039.0712 |
| 50 | 0. | SLD_2 | Max | 0. | 0. | -1232.4624 |
| 50 | 0.1318 | SLD_2 | Max | 0. | 0. | -1134.563 |
| 50 | 0.2636 | SLD_2 | Max | 0. | 0. | -1040.1905 |
| 50 | 0. | SLD_2 | Min | 0. | 0. | -1232.4624 |
| 50 | 0.1318 | SLD_2 | Min | 0. | 0. | -1134.563 |
| 50 | 0.2636 | SLD_2 | Min | 0. | 0. | -1040.1905 |
| 50 | 0. | SLD_3 | Max | 0. | 0. | -986.3638 |
| 50 | 0.1318 | SLD_3 | Max | 0. | 0. | -873.0671 |
| 50 | 0.2636 | SLD_3 | Max | 0. | 0. | -763.2144 |
| 50 | 0. | SLD_3 | Min | 0. | 0. | -986.3638 |
| 50 | 0.1318 | SLD_3 | Min | 0. | 0. | -873.0671 |
| 50 | 0.2636 | SLD_3 | Min | 0. | 0. | -763.2144 |
| 50 | 0. | SLD_4 | Max | 0. | 0. | -986.7277 |
| 50 | 0.1318 | SLD_4 | Max | 0. | 0. | -873.2951 |
| 50 | 0.2636 | SLD_4 | Max | 0. | 0. | -763.3066 |
| 50 | 0. | SLD_4 | Min | 0. | 0. | -986.7277 |
| 50 | 0.1318 | SLD_4 | Min | 0. | 0. | -873.2951 |
| 50 | 0.2636 | SLD_4 | Min | 0. | 0. | -763.3066 |
| 50 | 0. | SLU_IDR_1 | Max | 0. | 0. | -1506.3972 |
| 50 | 0.1318 | SLU_IDR_1 | Max | 0. | 0. | -1441.2041 |
| 50 | 0.2636 | SLU_IDR_1 | Max | 0. | 0. | -1379.111 |
| 50 | 0. | SLU_IDR_1 | Min | 0. | 0. | -1506.3972 |
| 50 | 0.1318 | SLU_IDR_1 | Min | 0. | 0. | -1441.2041 |
| 50 | 0.2636 | SLU_IDR_1 | Min | 0. | 0. | -1379.111 |
| 50 | 0. | SLU_IDR_2 | Max | 0. | 0. | -1733.7661 |
| 50 | 0.1318 | SLU_IDR_2 | Max | 0. | 0. | -1667.5505 |
| 50 | 0.2636 | SLU_IDR_2 | Max | 0. | 0. | -1604.4846 |
| 50 | 0. | SLU_IDR_2 | Min | 0. | 0. | -1733.7661 |
| 50 | 0.1318 | SLU_IDR_2 | Min | 0. | 0. | -1667.5505 |
| 50 | 0.2636 | SLU_IDR_2 | Min | 0. | 0. | -1604.4846 |
| 50 | 0. | SISMA WOOD SLV-1 | Max | 0. | 0. | 442.2475 |
| 50 | 0.1318 | SISMA WOOD SLV-1 | Max | 0. | 0. | 532.9452 |
| 50 | 0.2636 | SISMA WOOD SLV-1 | Max | 0. | 0. | 623.6429 |
| 50 | 0. | SISMA WOOD SLV-1 | Min | 0. | 0. | 442.2475 |
| 50 | 0.1318 | SISMA WOOD SLV-1 | Min | 0. | 0. | 532.9452 |
| 50 | 0.2636 | SISMA WOOD SLV-1 | Min | 0. | 0. | 623.6429 |
| 50 | 0. | DEAD-1 | Max | 0. | 0. | -34.1199 |
| 50 | 0.1318 | DEAD-1 | Max | 0. | 0. | -42.0792 |
| 50 | 0.2636 | DEAD-1 | Max | 0. | 0. | -50.0385 |
| 50 | 0. | DEAD-1 | Min | 0. | 0. | -34.1199 |
| 50 | 0.1318 | DEAD-1 | Min | 0. | 0. | -42.0792 |
| 50 | 0.2636 | DEAD-1 | Min | 0. | 0. | -50.0385 |
| 50 | 0. | SLU_PROVA | | 0. | 0. | -1994.1405 |
| 50 | 0.1318 | SLU_PROVA | | 0. | 0. | -1911.881 |
| 50 | 0.2636 | SLU_PROVA | | 0. | 0. | -1834.2065 |

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