IL CONCEDENTE

Regione Emilia-Romagna

IL CONCESSIONARIO

AUTOSTRADA REGIONALE CISPADANA

AUTOSTRADA REGIONALE CISPADANA
DAL CASELLO DI REGGIOLO-ROLO SULLA A22 AL CASELLO DI FERRARA SUD SULLA A13

CODICE C.U.P. E81B08000060009

PROGETTO DEFINITIVO

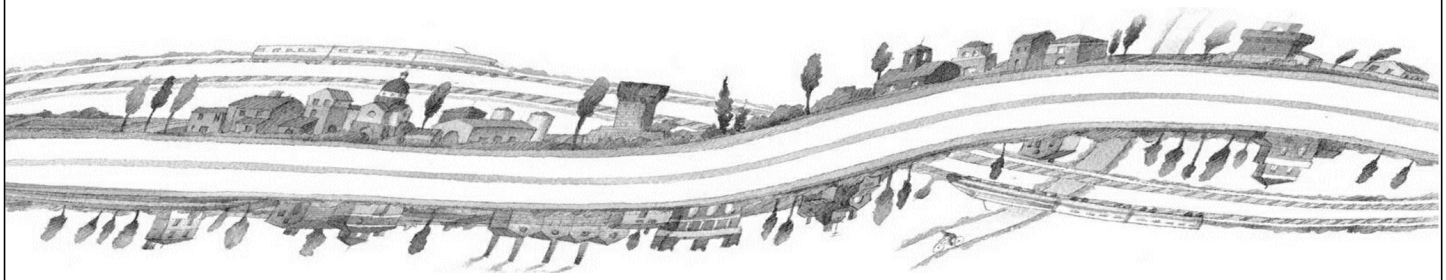
ASSE AUTOSTRADALE (COMPRENSIVO DEGLI INTERVENTI LOCALI DI COLLEGAMENTO VIARIO AL SISTEMA AUTOSTRADALE)

OPERE STRUTTURALI

OPERE D'ARTE MAGGIORI - SOTTOVIA SVINCOLO E INTERCONNESSIONE

IST05 - INTERCONNESSIONE CON A13 - ADEGUAMENTO SOTTOVIA PODERALE RAMPA NORD-OVEST

RELAZIONE DI CALCOLO



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IL CONCESSIONARIO

Autostrada Regionale Cispadana S.p.A.
IL PRESIDENTE
Graziano Pattuzzi

REV.	DATA	DESCRIZIONE	REDAZIONE	CONTROLLO	APPROVAZIONE
G					
F					
E					
D					
C					
B					
A	17.04.2012	EMISSIONE	Castorri	Mezzaluna	Salsi

IDENTIFICAZIONE ELABORATO

NUM. PROGR.	FASE	LOTTO	GRUPPO	CODICE OPERA WBS	TRATTO OPERA	AMBITO	TIPO ELABORATO	PROGRESSIVO	REV.
XXXX	PD	0	I02	IST05	0	OM	RC	01	A

DATA: MAGGIO 2012

SCALA:

I N D I C E

1. DESCRIZIONE DELL'OPERA

L'opera IST05 – Adeguamento Sottovia Poderale Rampa Nord-Ovest, si colloca nell'ambito dei lavori inerenti l'autostrada regionale Cispadana collegamento autostradale di connessione tra il casello di Reggiolo Rolo sull'A22 al Casello di Ferrara Sud sull'A13, alla progressiva chilometrica 62+187 dell'autostrada regionale Cispadana e alla progressiva chilometrica 0+255.13 dello svincolo rampa Nord-Ovest sull'asse autostradale PD-VR.

La zona interessata dall'opera, planimetricamente, si colloca nel territorio del comune di Ferrara.

Il tracciato stradale del sottovia ha un andamento planimetrico quasi perpendicolare all'asse autostradale (angolo fra asse sottovia e asse autostradale = 85°).

L'intervento in esame inteso come opera coordinata, ha quindi lo scopo di garantire la continuità alla strada poderale, anche dopo la costruzione dello svincolo rampa Nord-Ovest sull'asse autostradale PD-VR.

Lo scatolare in c.a. presenta una lunghezza complessiva di 15.00 m, le dimensioni interne nette sono pari a 4.50x6.00m, con uno spessore della soletta superiore pari a 0.40 m, della soletta inferiore pari a 0.60 m e dei piedritti laterali pari a 0.50m.

Il manufatto prevede una preparazione del sottofondo per mezzo della realizzazione di un getto di calcestruzzo magro avente uno spessore pari a circa 15 cm che sarà realizzata a partire dal piano di scavo. Allo scopo di preservare il manufatto dalle infiltrazioni e dall'umidità si prevede di rivestire esternamente l'intero manufatto con guaine impermeabilizzanti bitumate armate con TNT in poliestere (s=4mm) e geotessile in polipropilene da 500 g/mq nonché in corrispondenza di tutti i giunti strutturali è previsto il posizionamento di water stop e cordoni bentonitici. Lateralmente allo scatolare in c.a. verranno realizzate due solette di transizione dello spessore di 40cm; ciò comporta la parziale demolizione dei muri d'ala del sottovia esistente.

La strada poderale ha una larghezza di 4.5m all'interno del sottopassaggio (muri ad "U" + scatolare) con un pacchetto di pavimentazione dello spessore di 50cm. La pendenza trasversale è costante con due falde con pendenza 2,5% verso l'esterno in tutto il tratto.

Il franco altimetrico minimo è di 5.35m (in mezzeria dello scatolare); il ricoprimento, ovvero la distanza tra la quota del piano stradale autostradale e l'estradosso della soletta superiore, è variabile da un massimo di 0.75 m ad un minimo di 0.25 m.

Il pacchetto stradale scelto ha quindi uno spessore minimo di 14cm; si è infatti deciso di abbassare tale valore rispetto a quelli forniti dai tipologici sui pacchetti di pavimentazione per sottovia al fine di ottenere l'altezza libera interna massima possibile ovvero 5.35m.La pendenza trasversale è costante con un'unica falda con pendenza 2.5% verso l'interno curva.

Fa parte dell'intervento in oggetto anche il tratto con muri ad "U" collegati allo stesso manufatto, che presentano nel lato ovest uno sviluppo in asse pari a 7.00m.

Per quanto riguarda lo smaltimento delle acque meteoriche sono previste n° 2 caditoie con griglia continua (dim. 30x30 cm) poste ai lati del sottopasso. Le caditoie raccolgono il deflusso delle acque e lo convogliano all'interno di fossi laterali in progetto.

Per quanto riguarda le opere provvisionali a presidio degli scavi, si rimanda agli elaborati geotecnici tipologici:

- **PD_0_000_00000_0_GT_FC_04: TIPOLOGIE DI OPERE PROVVISIONALI A PRESIDIO DEGLI SCAVI 1/2.**
- **PD_0_000_00000_0_GT_FC_05: TIPOLOGIE DI OPERE PROVVISIONALI A PRESIDIO DEGLI SCAVI 2/2.**
- **PD_0_000_00000_0_GT_RC_01: RELAZIONE DI CALCOLO OPERE PROVVISIONALI A PRESIDIO DEGLI SCAVI.**

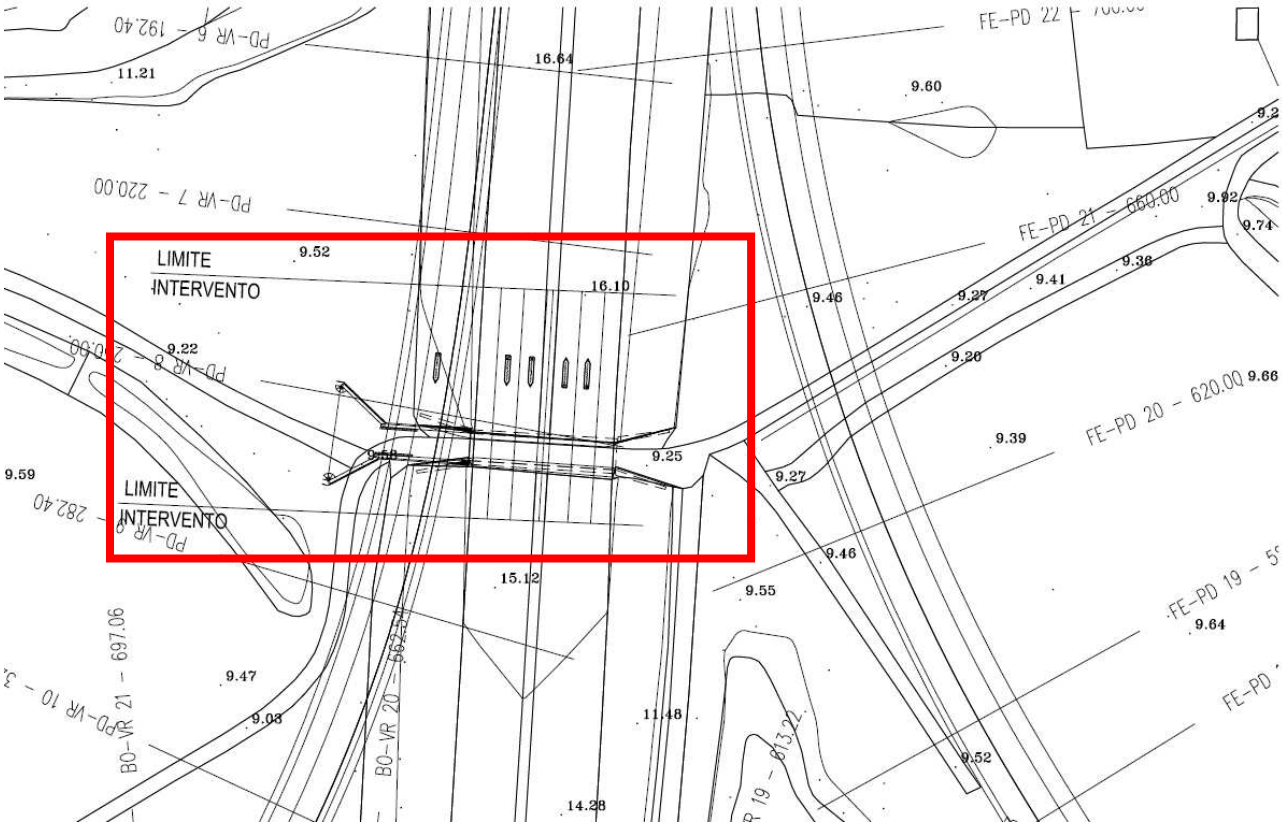


FIG. 1-1: PLANIMETRIA SOTTOPASSO

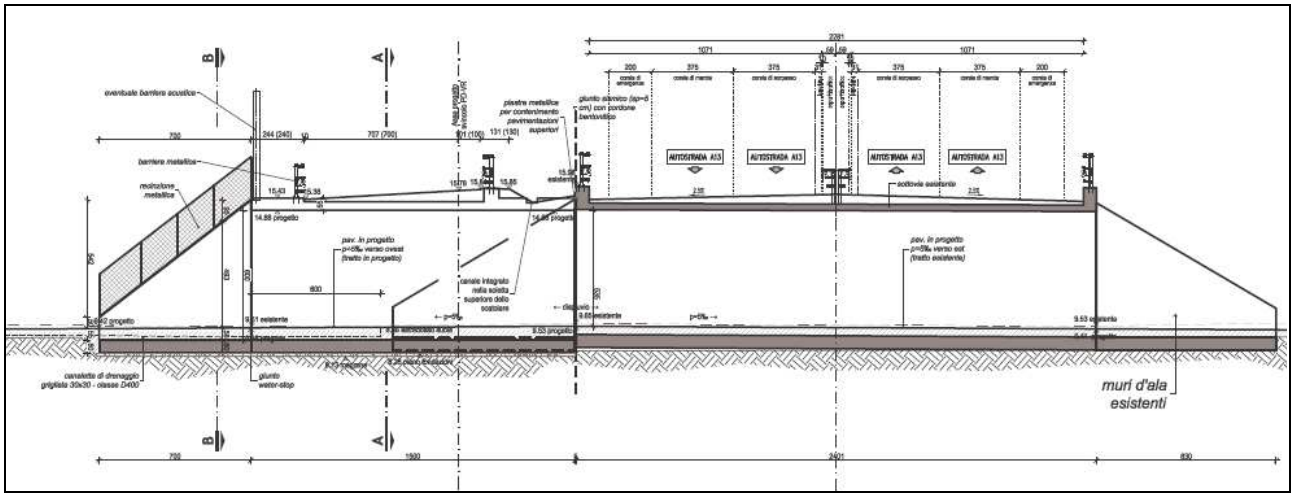


FIG. 1-2: PROFILO LONGITUDINALE SOTTOPASSO

2. NORMATIVA DI RIFERIMENTO

Vedi elaborato "PD-0-0000-0000-0-GE-KT-01:Elenco delle Normative di riferimento".

3. CARATTERISTICHE DEI MATERIALI

Vedi elaborato "PD-0-0000-0000-0-GE-TB-01:Tabella Materiali e Classi di esposizione del calcestruzzo".

4. INCIDENZE

Si anticipano qui di seguito le incidenze d'armatura relative ai singoli elementi costituenti l'Opera.

NA : NON APPLICABILE.

WBS	Parte d'opera	Incidenza kg/mc				
		Pali	Fondazione	Elevazione	Soletta	Traverso Precompresso
IST 05	SCATOLARE	NA	120	150	220	NA
IST 05	MURO AD U	NA	120	90	NA	NA

5. CRITERI DI CALCOLO

In ottemperanza con la normativa vigente, i calcoli sono condotti con il metodo semiprobabilistico agli stati limite.

5.1. CALCOLO DELLE SPINTE SUI PARAMENTI VERTICALI

In generale occorre considerare, di volta in volta, le spinte più appropriate a seconda della deformabilità della parete.

Nel caso di muri per i quali si possano accettare significative deformazioni, è possibile assumere, sia in condizioni statiche sia in condizioni sismiche, un regime di spinte attive. Altrimenti è in genere necessario assumere condizioni di spinta a riposo.

In presenza di sisma, è consentito l'approccio pseudo-statico, secondo il quale il complesso muro + terreno mobilitato è pensato soggetto ad un'accelerazione sismica uniforme avente le seguenti componenti

Orizzontale = k_h g Verticale = k_v g = $\pm$ 0.5 k_h g

Come nel caso statico, anche in condizioni sismiche è necessario distinguere tra:

- muri indeformabili;
- muri deformabili;
- muri molto deformabili;

Nella prima classe di muri (**muri indeformabili**) possono essere inclusi i manufatti aventi pareti adeguatamente contrastate, quali, ad esempio, gli scatolari. In questo caso è opportuno adottare spinte sismiche secondo la teoria di Wood (1973), come meglio indicato nel 5.2.3, assumendo

(SLV) $k_h = a_{max}/g$

Nella categoria dei **muri deformabili** si possono includere le pareti sufficientemente deformabili grazie alla loro snellezza ma tuttavia sostanzialmente vincolate, in qualche modo, ad altre strutture, come ad esempio le pareti di manufatti a U. In questo caso potranno essere considerate spinte comprese tra valori a riposo e attive, in ragione della deformabilità. Queste ultime (sismiche attive) saranno valutate assumendo

(SLV) $k_h = \beta_m \cdot a_{max}/g$, con β_m=1

Nella categoria dei **muri molto deformabili** per i quali possono essere ipotizzati significativi spostamenti relativi tra muro e terreno, si possono includere, ad esempio, i muri di sostegno fondati su fondazioni dirette. In questo caso si assumeranno certamente spinte attive, da valutarsi, introducendo nel caso sismico un coefficiente β_m in accordo con la Tabella 7.11.II di NTC2008.

(SLV) $k_h = \beta_m \cdot a_{max}/g$ (β_m da Tab 7.11.II)

in questo caso β_m= 0.31,

Seguono ora criteri generali di valutazione delle spinte, applicabili a geometrie ordinarie.

5.2. SPINTE ATTIVE IN CONDIZIONI STATICHE

Ad una generica profondità z, nel caso di terreno puramente granulare, lo sforzo orizzontale totale $\sigma_A(z)$ sulla parete è dato da:

$$\sigma_A(z) = K_A \cdot [\sigma_v(z) - u(z)] + u(z) \qquad (5\text{-}1)$$

In cui

$\sigma_v(z)$ = sforzo verticale totale alla generica profondità, ossia il peso della colonna di terreno e di acqua soprastante la quota z.

$u(z)$ = pressione dell'acqua alla generica profondità

Il coefficiente di spinta attiva KA può, in genere, essere assunto pari a

$$K_A = \tan^2\left(\frac{\pi}{4} - \frac{\phi}{2}\right) \qquad (5\text{-}2)$$

È possibile, tuttavia, mettere in conto l'angolo d'attrito δ tra terra e muro, assumendo quindi che la spinta sia inclinata, rispetto alla normale alla superficie di contatto tra muro e terreno, di un angolo δ.

In questo caso il coefficiente di spinta attiva può essere valutato con le note formule derivate dalla teoria di Coulomb e sviluppate da Muller-Breslau.

CONDIZIONI DI SPINTA ATTIVA – Teoria di Coulomb

$$K_A = \frac{sen^2(\psi + \phi)}{\text{sen}^2\psi \, \text{sen}(\psi - \delta)\left[1 + \sqrt{\frac{sen(\phi + \delta)sen(\phi - \beta)}{sen(\psi - \delta)sen(\psi + \beta)}}\right]^2} \qquad \text{(5-3)}$$

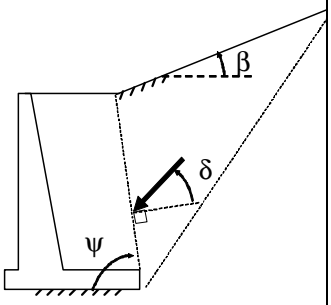


TABELLA 5.2-1-CONDIZIONI DI SPINTA ATTIVA – TEORIA DI COULOMB

Operando nell'ambito del metodo agli stati limite, nelle formule precedenti, va introdotto l'angolo d'attrito di calcolo, cioè $\tan(\phi_d)=\tan(\phi_k) / \gamma_\phi$ se si opera nell'ambito di una combinazione GEO (ad esempio A2+M2+R2).

5.2.1. Spinte a riposo

Ad una generica profondità z, nel caso di terreno puramente granulare, lo sforzo orizzontale totale $\sigma_0(z)$ sulla parete è dato da:

$$\sigma_0(z) = K_0 \cdot [\sigma_v(z) - u(z)] + u(z) \qquad \text{(5-4)}$$

In cui, nel caso di piano campagna orizzontale, il coefficiente di spinta a riposo K_0 se non diversamente definito, può essere assunto pari a

$$K_0 = (1 - \sin(\phi)) \cdot \sqrt{OCR} \qquad \text{(5-5)}$$

Con OCR = GSC = grado di sovraconsolidazione.

5.2.2. Spinte attive in condizioni sismiche

Nell'ambito dell'approccio pseudo-statico, il complesso muro + terreno mobilitato è pensato soggetto ad un'accelerazione sismica uniforme avente le seguenti componenti

Orizzontale = $k_h \cdot g$ Verticale = $k_v \cdot g$

La spinta totale attiva su un paramento di altezza pari ad H è data da:

$$E_d = \tfrac{1}{2}\gamma^*(1 \pm k_v)K_{A,E}H^2 + E_{ws} + E_{wd} \qquad (5\text{-}6)$$

Il primo termine è la spinta attiva dovuta allo scheletro solido, il secondo termine E_{ws} è la risultante delle pressioni idrostatiche ed il terzo E_{wd} è la risultante delle sovrappressioni interstiziali.

I coefficienti di spinta attiva sono dati dalle seguenti espressioni (Mononobe & Okabe, nel seguito M-O):

CONDIZIONI DI SPINTA ATTIVA – Teoria di M-O

$$\beta \le \phi - \theta: \quad K_{A,E} = \frac{sen^2(\psi + \phi - \theta)}{\cos\theta\, sen^2\psi\, sen(\psi - \theta - \delta)\left[1 + \sqrt{\frac{sen(\phi + \delta)sen(\phi - \beta - \theta)}{sen(\psi - \theta - \delta)sen(\psi + \beta)}}\right]^2}$$

$$\beta > \phi - \theta: \quad K_{A,E} = \frac{sen^2(\psi + \phi - \theta)}{\cos\theta\, sen^2\psi\, sen(\psi - \theta - \delta)}$$

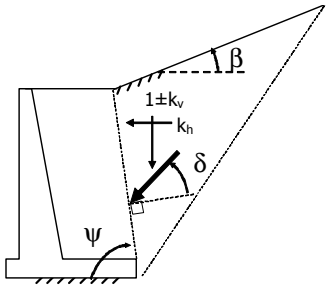


TABELLA 5.2-2- CONDIZIONI DI SPINTA ATTIVA – TEORIA DI M-O

Operando nell'ambito del metodo agli stati limite, nelle formule precedenti, va introdotto l'angolo d'attrito di calcolo, cioè $\tan(\phi_d)=\tan(\phi_k) / \gamma_\phi$ se si opera nell'ambito di una combinazione GEO (ad esempio A2+M2+R2).

A seconda della definizione del peso specifico γ^* del cuneo e dell'angolo θ definito come l'angolo, rispetto alla verticale, fra le azioni esterne orizzontali e quelle verticali agenti sul cuneo di spinta di volume V, l'espressione generale può essere utilizzata per tre diverse condizioni nelle quali può trovarsi il rilevato.

5.2.2.1 Rilevato asciutto

Non c'è alcuna azione dovuta all'acqua: corrisponde alla configurazione originale ipotizzata da M-O. Come peso specifico γ^* si deve assumere il peso secco γ_d ; la forza orizzontale F_h è pari alla massa del terreno

moltiplicata per l'accelerazione orizzontale mentre la forza verticale F_V è il peso del cuneo incrementato o decrementato dall'accelerazione sismica verticale; quindi:

□□=□□d

$$\tan\theta = \frac{k_h}{1 \pm k_v}$$

$E_{ws} = E_{wd}=0$

5.2.2.2 Rilevato saturo a grana fine (dinamicamente impervio: k<5·10^{-4} m/s)

In sostanza si assume che l'acqua, imprigionata negli interstizi, si muova insieme con il terreno: l'accelerazione sismica agirà quindi sulla massa complessiva (terreno+acqua) del cuneo, pari a $V\cdot \gamma_{sat}$. Si ammette che le pressioni interstiziali non subiscano variazioni ai fini del calcolo delle azioni sulla parete. In questo caso l'equilibrio limite del cuneo è fatto al netto della risultante delle azioni idrostatiche e quindi, nelle formule generali, si assumerà:

$\gamma^* = \gamma'$

$$\tan\theta = \frac{\gamma_{sat}}{\gamma'}\frac{k_h}{1 \pm k_v}$$

Alla spinta efficace dovrà essere aggiunta la spinta idrostatica dell'acqua, mentre, per ipotesi, la componente idrodinamica non può svilupparsi. Quindi:

$E_{ws} = \frac{1}{2}\gamma_w H^2$

$E_{wd}=0$

5.2.2.3 Rilevato saturo a grana grossa (dinamicamente permeabile: k≥5·10^{-4} m/s)

Si ammette che l'acqua negli interstizi possa muoversi liberamente, indipendentemente dalle deformazioni subite dal terreno: l'accelerazione sismica agirà quindi sulla massa della sola parte solida del cuneo, pari a $V\cdot \gamma_d$. L'equilibrio limite del cuneo è fatto al netto della risultante delle pressioni interstiziali e quindi, nelle formule generali, si assumerà:

$\gamma^* = \gamma'$

$$\tan\theta = \frac{\gamma_d}{\gamma'}\frac{k_h}{1 \pm k_v}$$

In questo caso dovranno essere aggiunte sia la spinta idrostatica sia la sovraspinta idrodinamica della stessa acqua di falda.

$E_{ws} = \frac{1}{2}\gamma_w H^2$

$E_{wd} = \frac{7}{12} k_h \gamma_w H'^2$ con H' = altezza della freatica dal piede del muro.

5.2.2.4 Rilevato parzialmente immerso

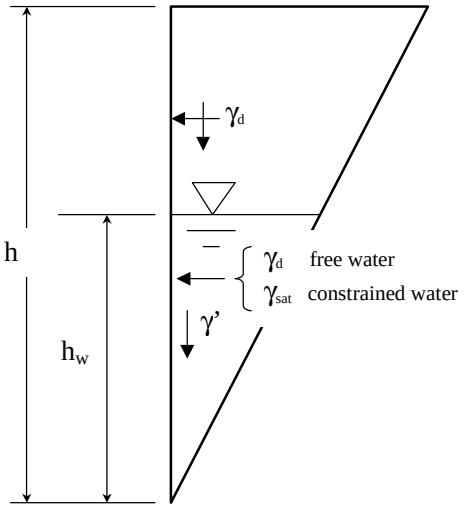


FIGURA 5.2-1 - TERRAPIENO PARZIALMENTE IMMERSO.

Ebeling e Morrison (1992) indicano il modo per utilizzare, anche in questo caso, le equazioni di M-O: sostanzialmente questo caso può essere assimilato a quello di un terrapieno completamente immerso omogeneo, avente un peso specifico equivalente. Per calcolare la risultante delle spinte, si potrà operare come segue. Si definiscono i pesi specifici medi da associare rispettivamente alla componente efficace verticale ed alla componente laterale

$$\gamma_V^* = \left(\frac{h_w}{h}\right)^2 \cdot \gamma' + \left[1 - \left(\frac{h_w}{h}\right)^2\right] \cdot \gamma_d$$

$$\gamma_H^* = \begin{cases} \gamma_d & \text{se terreno din. permeabile} \\ \left(\frac{h_w}{h}\right)^2 \cdot \gamma_{sat} + \left[1 - \left(\frac{h_w}{h}\right)^2\right] \cdot \gamma_d & \text{se terreno din. impervio} \end{cases}$$

Definendo:

$$\tan\theta = \frac{\gamma_H^*}{\gamma_V^*} \frac{k_h}{1 - k_v}$$

si applicherà poi la (5-6) calcolando i coefficienti di spinta tramite le **Errore. L'origine riferimento non è stata trovata.** e ponendo $\gamma^* = \gamma_V^*$.

5.2.2.5 Punto di applicazione delle spinte attive sismiche

Considerato che la spinta attiva complessiva è in generale composta da tre termini, occorre calcolare il punto di applicazione di ognuno di essi

1. **Componente associata allo scheletro solido**: è possibile operare come segue

a) si calcola la spinta attiva in condizioni statiche ($S_{A,S}$)

b) si calcola la quota parte efficace di spinta sismica E_d dovuta alla terra:

$S_{A,E} = \frac{1}{2}\gamma^*(1 \pm k_v)K_{A,E}H^2$

Nel caso di terreno eterogeneo, la spinta attiva è calcolata considerando la variabilità di $K_{A,sismico}$. Nel caso di terreno omogeneo ma parzialmente in falda, si suggerisce di adottare l'approccio sopra indicato, piuttosto che introdurre diversi valori dei coefficienti di spinta.

c) si calcola l'incremento di spinta dovuto alla terra in caso di sisma (componente efficace):

$\Delta S_A = S_{A,E} - S_{A,S}$

d) Nel caso di muri che possano ruotare alla base, si può considerare che tale incremento abbia una risultante nello stesso punto della risultante delle spinte statiche

e) Negli altri casi si può assumere che tale azione si distribuisca uniformemente sulla parete, il che equivale ad applicare un carico uniformemente distribuito pari a:

$q = \Delta S_A / H$

2. **Componente idrostatica**: è applicata come nel caso statico

3. **Componente idrodinamica (E_{wd})**: se esiste, è applicata considerando la seguente distribuzione di pressioni:

$q_{wd}(z) = \pm \frac{7}{8} k_h \gamma_w \sqrt{H' \cdot z}$ con z quota del generico punto rispetto la base della parete.

5.2.3. Sovraspinte sismiche sui muri non in grado di spostarsi

In questo caso l'utilizzo delle equazioni di M-O non è raccomandato. Le spinte delle terre, sono calcolate in regime di spinta a riposo che comporta il calcolo delle spinte sismiche in tali condizioni; l'incremento dinamico di spinta del terreno può essere quindi calcolato attraverso la nota formulazione di Wood (1973) come:

$\Delta P_d = S \cdot a_g / g \cdot \gamma \cdot h_{tot}^2 = a_{max} / g \cdot \gamma \cdot h_{tot}^2$

Con h_{tot} = altezza del muro.

Questa spinta è applicata come una distribuzione uniforme lungo l'altezza h_{tot}.

Nel caso di scatolare, si assumerà γ = 19.5 kN/m^3 = peso di volume del materiale compattato del rilevato.

Il punto di applicazione della spinta che interessa lo scatolare è posto $h_{scat}/2$, con "h_{tot}" altezza dalla fondazione dello scatolare al piano stradale e h_{scat} l'altezza dello scatolare.

Essendo "ΔP_d" la risultante globale, ed il diagramma di spinta di tipo rettangolare, è immediato ricavare la quota parte della spinta che agisce sul piedritto dello scatolare.

L'azione sismica è rappresentata da un insieme di forze statiche orizzontali e verticali, date dal prodotto delle forze di gravità per i coefficienti sismici in precedenza definiti, di cui la componente verticale è considerata agente verso l'alto o verso il basso, in modo da produrre gli effetti più sfavorevoli.

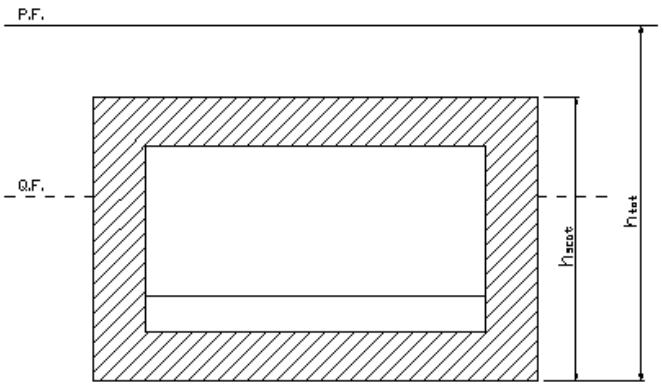


Figura 5-2 Altezze di riferimento per il calcolo dell'azione sismica

5.3. CRITERI E DEFINIZIONE DELL'AZIONE SISMICA

L'effetto dell'azione sismica di progetto sull'opera nel suo complesso, includendo il volume significativo di terreno, la struttura di fondazione, gli elementi strutturali e non strutturali, nonché gli impianti, deve rispettare gli stati limite ultimi e di esercizio definiti al § 3.2.1, i cui requisiti di sicurezza sono indicati nel § 7.1 della norma.

Il rispetto degli stati limite si considera conseguito quando:

nei confronti degli stati limite di esercizio siano rispettate le verifiche relative al solo Stato Limite di Danno;

nei confronti degli stati limite ultimi siano rispettate le indicazioni progettuali e costruttive riportate nel § 7 e siano soddisfatte le verifiche relative al solo Stato Limite di salvaguardia della Vita.

Per Stato Limite di Danno (SLD) s'intende che l'opera, nel suo complesso, a seguito del terremoto, includendo gli elementi strutturali, quelli non strutturali, le apparecchiature rilevanti alla sua funzione, subisce danni tali da non provocare rischi agli utenti e non compromette significativamente la capacità di resistenza e di rigidezza nei confronti delle azioni verticali e orizzontali. Lo stato limite di esercizio comporta la verifica delle tensioni di lavoro, in conformità al § 4.1.2.2.5 (NT).

Per Stato Limite di salvaguardia della Vita (SLV) si intende che l'opera a seguito del terremoto subisce rotture e crolli dei componenti non strutturali e impiantistici e significativi danni di componenti strutturali, cui si associa una perdita significativa di rigidezza nei confronti delle azioni orizzontali (creazione di cerniere plastiche secondo il criterio della gerarchia delle resistenze), mantenendo ancora un margine di sicurezza (resistenza e rigidezza) nei confronti delle azioni verticali.

Gli stati limite, sia di esercizio sia ultimi, sono individuati riferendosi alle prestazioni che l'opera a realizzarsi deve assolvere durante un evento sismico; per la funzione che l'opera deve espletare nella sua vita utile, è significativo calcolare lo Stato Limite di Danno (SLD) per l'esercizio e lo Stato Limite di Salvaguardia della Vita (SLV) per lo stato limite ultimo.

In merito alle opere scatolari di cui trattasi, nel rispetto del punto § 7.9.2., assimilando l'opera scatolare alla categoria delle spalle da ponte, rientrando tra le opere che si muovono con il terreno (§ 7.9.2.1), si può ritenere che la struttura debba mantenere sotto l'azione sismica un comportamento elastico; queste categorie di opere che si muovono con il terreno non subiscono le amplificazioni dell'accelerazione del suolo.

I dati sismici sono riassunti nell'elaborato "PD-0-0000-0000-0-GE-KT-02:Vita Utile e Classe d'Uso delle opere".

Le azioni sismiche sono valutate in relazione al periodo di riferimento della struttura, che si ricava moltiplicandone la vita nominale V_N per il coefficiente d'uso C_U

$V_R = V_N \cdot C_u$

Il valore del coefficiente d'uso C_U è definito, al variare della classe d'uso, come mostrato nella tabella seguente:

CLASSE D'USO	I	II	III	IV
COEFFICIENTE C_U	0,7	1,0	1,5	2,0

TABELLA 5.3 VALORI DEL COEFFICIENTE D'USO CU

Il valore di probabilità di superamento del periodo di riferimento P_{VR}, cui riferirsi per individuare l'azione sismica agente, è:

$P_{VR}(SLV) = 10\%$

Il **periodo di ritorno** dell'azione sismica T_R espresso in anni vale:

$$T_R(SLV) = -\frac{Vr}{\ln(1-Pvr)}$$

ASSE AUTOSTRADALE					
OPERA	***Vita Nominale [anni]***	***Classe d'uso***	***Coefficiente d'uso***	***Periodo di Riferimento [anni]***	***Periodo di ritorno SLV [anni]***
Rilevati	*100*	*IV*	*2*	*200*	1898
Viadotti	100	*IV*	*2*	*200*	1898
Sovrappassi di svincolo	100	*IV*	*2*	*200*	1898
Ponti	100	*IV*	*2*	*200*	1898
Gallerie e trincee confinate	100	*IV*	*2*	*200*	1898
Sovrappassi	100	*IV*	*2*	*200*	1898
Sottovia					
Manufatto scatolare per sottovia la cui proiezione cade sull'asse autostradale	100	*IV*	*2*	*200*	1898
Muri ad U per sottovia statali	50	*IV*	*2*	*100*	949
Muri ad U per sottovia ex statali e provinciali	50	III	*1.5*	*75*	712
Muri ad U per sottovia comunali e poderali	50	II	*1*	*50*	475
Edifici di stazione e caserma di	50	IV	*2*	*100*	949

polizia					
Caselli autostradali	50	IV	*2*	*100*	949
Opere minori: attraversamenti idraulici	100	IV	*2*	*200*	1898
Opere minori: muri di sostegno per rilevato autostradale (sottoscarpa)	100	IV	*2*	*200*	1898
Opere minori: muri di sostegno per trincea autostradale (controripa)	100	IV	*2*	*200*	1898
Opere provvisionali (1)	10	II	*1*	*10*	95
VIABILITA' DI ADDUZIONE E DI COLLEGAMENTO (tipologia C1 e C2)					
OPERA	*Vita Nominale [anni]*	*Classe d'uso*	*Coefficiente d'uso*	*Periodo di Riferimento [anni]*	*Periodo di ritorno SLV [anni]*
Opere provvisionali (1)	*10*	*II*	*1*	*10*	
Riqualificazione della S.P. 72 "Parma-Mezzani (1PR) - Tipologia F2					
Rilevati	*50*	*III*	*1.5*	*75*	712
Opere minori: attraversamenti idraulici	*50*	*III*	*1.5*	*75*	712
Variante alla S.P. n 41 in corrispondenza del tracciato Cispadano – tratto tra S.P. n 60 e Brescello (1RE) – tipologia C1					
Rilevati	*50*	*III*	*1.5*	*75*	712
Ponti	*50*	*III*	*1.5*	*75*	712
Viadotti	*50*	*III*	*1.5*	*75*	712
Sottovia	*50*	*III*	*1.5*	*75*	712
Opere minori: attraversamenti idraulici	*50*	*III*	*1.5*	*75*	712
Cispadana tra la S.P. n 2 "Reggiolo-Gonzaga" e la ex S.S. n 62 "della Cisa" (2RE) – tipologia C1					
Rilevati	*50*	*III*	*1.5*	*75*	712

Ponti	*50*	*III*	*1.5*	*75*	712
Opere minori: attraversamenti idraulici	*50*	*III*	*1.5*	*75*	712
Raccordo Bondeno-Cento-Autostrada Cispadana (1FE)					
Rilevati tipologia C2	*50*	*III*	*1.5*	*75*	712
Rilevati tipologia F2	*50*	*III*	*1.5*	*75*	712
Ponti	*50*	*III*	*1.5*	*75*	712
Opere minori: attraversamenti idraulici	*50*	*III*	*1.5*	*75*	712

(1) Le verifiche sismiche di opere provvisorie o strutture in fase costruttiva possono omettersi quando le relative durate previste in progetto siano inferiori a 2 anni. (Rif. NTC 2008 par. 2.4.1)

Tabella 5.4 Periodo di ritorno per l'azione sismica

Dato il valore del periodo di ritorno suddetto, tramite le tabelle riportate nell'Allegato B della norma o tramite la mappatura messa a disposizione in rete dall'Istituto Nazionale di Geofisica e Vulcanologia (INGV), è possibile definire i valori di a_g, F_0, T^*_c.

$a_g \rightarrow$ accelerazione massima al sito;

$F_0 \rightarrow$ valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

$T^*_c \rightarrow$ periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

S → coefficiente che comprende l'effetto dell'amplificazione stratigrafica (Ss) e dell'amplificazione topografica (St).

L'opera in oggetto ricade nelle vicinanze del comune di Ferrara di cui si riportano le caratteristiche sismiche in funzione del periodo di ritorno del sisma definito nella tabella precedente :

	Periodo di ritorno SLV [anni]	ag/g	F0	Tc* (s)	Categoria sottosuolo	Ss	amax/g
Sottovia Poderale	1898	0.258	2.468	0.287	D	1.444	0.373
Muri ad U per Sottovia Poderali	475	0.148	2.590	0.271	D	1.800	0.266

Il calcolo viene eseguito con il metodo pseudostatico (§ 7.11.6 NT). In queste condizioni l'azione sismica è rappresentata da una forza statica equivalente pari al prodotto delle forze di gravità per un opportuno coefficiente sismico.

Le verifiche sismiche delle opere provvisionali saranno omesse in quanto la loro durata prevista è inferiori a

2 anni.

5.4. COMBINAZIONI DI CARICO

Le combinazioni di carico, utilizzate per condurre le verifiche agli stati limite ultimi e agli stati limite di esercizio, sono state originate in ottemperanza con quanto prescritto dalla vigente normativa.

5.4.1. Combinazioni per le verifiche agli SLU

Gli stati limite ultimi delle opere interrate si riferiscono allo sviluppo di meccanismi di collasso, determinati dalla mobilitazione della resistenza del terreno, e al raggiungimento della resistenza degli elementi strutturali che compongono l'opera.

Le verifiche agli stati limite ultimi sono eseguiti in riferimento ai seguenti stati limite:

-SLU di tipo geotecnico (GEO) e di equilibrio di corpo rigido (EQU)

collasso per carico limite dell'insieme fondazione-terreno;

-SLU di tipo strutturale (STR)

raggiungimento della resistenza negli elementi strutturali.

Trattandosi di opere interrate, le verifiche saranno condotte secondo l'approccio progettuale "Approccio 1", utilizzando i coefficienti parziali riportati nelle Tabelle 6.2.I e 5.1.V per i parametri geotecnici e le azioni.

combinazione 1 → (A1+M1+R1) ⇒ STR (verifiche degli elementi strutturali)

combinazione 2 → (A2+M2+R2) ⇒ GEO (carico limite)

PARAMETRO	GRANDEZZA ALLA QUALE APPLICARE IL COEFF. PARZIALE	COEFFICIENTE PARZIALE γ_M	M_1	M_2
Tangente dell'angolo di resistenza al taglio	$\tan \varphi'_k$	$\gamma_{\varphi'}$	1	1,25
Coesione efficace	c'_k	$\gamma_{c'}$	1	1,25
Resistenza non drenata	c'_{uk}	γ_{cu}	1	1,4
Peso dell'unità di	γ	γ_γ	1	1

volume				

TABELLA 5.5 - COEFFICIENTI PARZIALI PER I PARAMETRI DEL TERRENO (TABELLA 6.2.II NTC 2008)

VERIFICA	COEFF. PARZIALE (R1)	COEFF. PARZIALE (R2)
Capacità portante della fondazione	$\gamma_{R=1}$	$\gamma_{R=1}$
Scorrimento	$\gamma_{R=1}$	$\gamma_{R=1}$
Resistenza del terreno a valle	$\gamma_{R=1}$	$\gamma_{R=1}$

TABELLA 5.6- COEFFICIENTI PARZIALI γ_R PER LA RESISTENZA DEL SISTEMA

Ai fini delle verifiche degli stati limite ultimi si definiscono le seguenti combinazioni:

STR) $\Rightarrow$ $\gamma_{G1}\cdot G_1+ \gamma_{G2}\cdot G_2 + \gamma_{Q1}\cdot Q_{k1}+ \gamma_{0i}\sum_i \psi_{0i}\cdot Q_{ki}$ $\Rightarrow (\Phi_d'= \Phi_k')$

GEO) $\Rightarrow$ $\gamma_{G1}\cdot G_1+ \gamma_{G2}\cdot G_2 + \gamma_{Q1}\cdot Q_{k1}+ \gamma_{0i}\sum_i \psi_{0i}\cdot Q_{ki}$ $\Rightarrow(\Phi_d'=\tan^{-1}(\tan\Phi_k'/ \gamma_\Phi))$

I valori dei coefficienti parziali delle azioni sono dedotti dalla tabella 5.1.V del D.M. 14 Gennaio 2008

Tabella 5.1.V – *Coefficienti parziali di sicurezza per le combinazioni di carico agli SLU*

		Coefficiente	EQU[1]	A1 STR	A2 GEO
Carichi permanenti	favorevoli sfavorevoli	γ_{G1}	0,90 1,10	1,00 1,35	1,00 1,00
Carichi permanenti non strutturali[2]	favorevoli sfavorevoli	γ_{G2}	0,00 1,50	0,00 1,50	0,00 1,30
Carichi variabili da traffico	favorevoli sfavorevoli	γ_Q	0,00 1,35	0,00 1,35	0,00 1,15
Carichi variabili	favorevoli sfavorevoli	γ_{Qi}	0,00 1,50	0,00 1,50	0,00 1,30
Distorsioni e presollecitazioni di progetto	favorevoli sfavorevoli	$\gamma_{\varepsilon 1}$	0,90 1,00[3]	1,00 1,00[4]	1,00 1,00
Ritiro e viscosità, Variazioni termiche, Cedimenti vincolari	favorevoli sfavorevoli	$\gamma_{\varepsilon 2}$, $\gamma_{\varepsilon 3}$, $\gamma_{\varepsilon 4}$	0,00 1,20	0,00 1,20	0,00 1,00

(1) Equilibrio che non coinvolga i parametri di deformabilità e resistenza del terreno; altrimenti si applicano i valori di GEO.
(2) Nel caso in cui i carichi permanenti non strutturali (ad es. carichi permanenti portati) siano compiutamente definiti si potranno adottare gli stessi coefficienti validi per le azioni permanenti.
(3) 1,30 per instabilità in strutture con precompressione esterna
(4) 1,20 per effetti locali

5.4.2. Combinazioni per la verifica allo SLE

Ai fini delle verifiche degli stati limite di esercizio (fessurazione/ stato tensionale) si definiscono le seguenti combinazioni:

Frequente) $\Rightarrow$ $G_1+ G_2 + \psi_{11}\cdot Q_{k1}+\sum_i\psi_{2i}\cdot Q_{ki}$ $\Rightarrow (\Phi_d'= \Phi_k')$

Quasi permanente) $\Rightarrow$ $G_1+ G_2 + \psi_{21}\cdot Q_{k1}+\sum_i\psi_{2i}\cdot Q_{ki}$ $\Rightarrow (\Phi_d'= \Phi_k')$

Rara) $\Rightarrow$ $G_1+ G_2 + Q_{k1}+\sum_i\psi_{0i}\cdot Q_{ki}$ $\Rightarrow (\Phi_d'= \Phi_k')$

I valori dei coefficienti di combinazione sono dedotti dalla tabella 5.1.Vi del D.M. 14 Gennaio 2008.

Tabella 5.1.VI - *Coefficienti ψ per le azioni variabili per ponti stradali e pedonali*

Azioni	*Gruppo di azioni (Tabella 5.1.IV)*	*Coefficiente ψ_0 di combinazione*	*Coefficiente ψ_1 (valori frequenti)*	*Coefficiente ψ_2 (valori quasi permanenti)*
Azioni da traffico (Tabella 5.1.IV)	Schema 1 (Carichi tandem)	0,75	0,75	0,0
	Schemi 1, 5 e 6 (Carichi distribuiti	0,40	0,40	0,0
	Schemi 3 e 4 (carichi concentrati)	0,40	0,40	0,0
	Schema 2	0,0	0,75	0,0
	2	0,0	0,0	0,0
	3	0,0	0,0	0,0
	4 (folla)	----	0,75	0,0
	5	0,0	0,0	0,0
Vento q_5	Vento a ponte scarico			
	SLU e SLE	0,6	0,2	0,0
	Esecuzione	0,8	----	0,0
	Vento a ponte carico	0,6		
Neve q_5	SLU e SLE	0,0	0,0	0,0
	esecuzione	0,8	0,6	0,5
Temperatura	T_k	0,6	0,6	0,5

5.4.3. Combinazioni per la condizione sismica

Per la condizione sismica, le combinazioni per gli stati limite ultimi da prendere in considerazione sono le seguenti (approccio 1):

STR) $\Rightarrow$ $E+G_1+G_2+\sum_i\psi_{2i}\cdot Q_{ki}$ $\Rightarrow (\Phi_d'= \Phi_k')$

GEO) $\Rightarrow$ $E+G_1+G_2+\sum_i\psi_{2i}\cdot Q_{ki}$ $\Rightarrow$ (spinte $\Phi_d'=\tan^{-1}(\tan\Phi_k'/ \gamma_\Phi)$)

Gli effetti dell'azione sismica saranno valutati tenendo conto delle masse associate ai seguenti carichi gravitazionali:

$G_1+G_2+\sum_i\psi_{2i}\cdot Q_{ki}$

6. PARAMETRI GEOTECNICI

Ai fini del calcolo della spinta esercitata dalle terre sui piedritti e del carico da ricoprimento sulla soletta superiore del **manufatto scatolare** si utilizzano i parametri seguenti, in accordo con quanto riportato nella Relazione Geotecnica:

- angolo di attrito interno del terreno Φ = 38.0 °
- coefficiente di spinta a riposo k_0 = 0.384 (stato limite STR)
- coefficiente di spinta attiva k_a = 0.238 (stato limite STR)
- peso specifico del terreno asciutto γ_{dry} = 19.50 [kN/m3]
- peso specifico del terreno saturo d'acqua γ_{sat} = 19.50 [kN/m3]
- coefficiente di sottofondazione ks = 3500 [kN/m3]

Si assume inoltre, ai fini del calcolo dei carichi permanenti, un peso specifico per la piattaforma stradale pari a γ_{pav} = 22.00 kN/m^3.

7. SOTTOPASSO SCATOLARE

Si riportano di seguito le dimensioni geometriche della struttura:

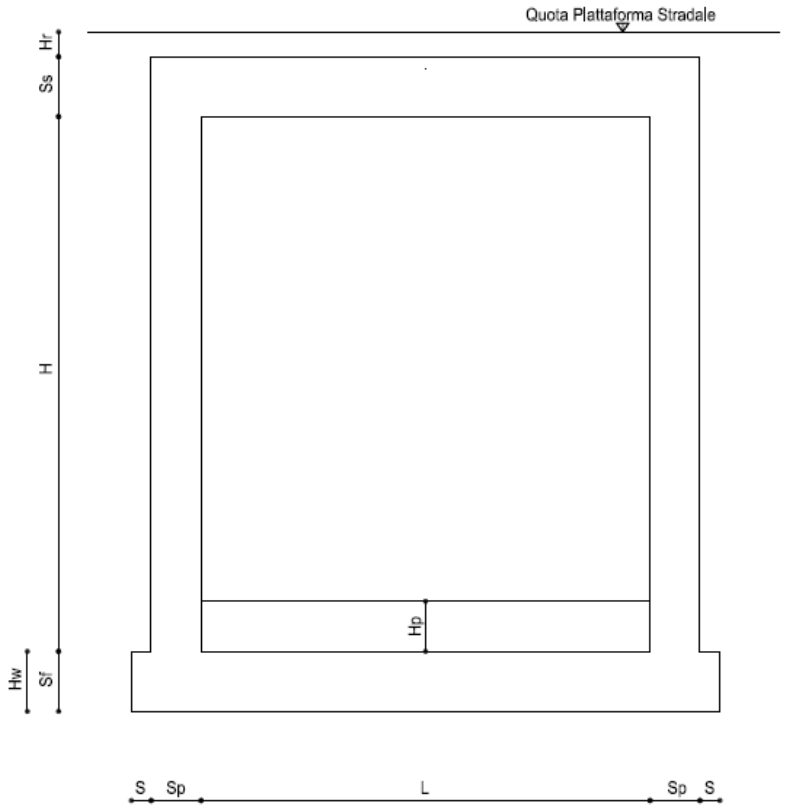


FIGURA 7-1– SEZIONE TIPOLOGICA

L	=	4.50	m
H	=	6.00	m
Hr	=	0.25	m
Sp	=	0.50	m
Ss	=	0.40	m
S	=	0.20	m
Sf	=	0.60	m
Hi	=	0.50	m
Falda		si	
Hw	=	0.60	m
rispetto ad intradosso soletta inferiore			

TABELLA 7-1- DIMENSIONI GEOMETRICHE (SEZIONE IN RETTO)

7.1. PROGRAMMI DI CALCOLO UTILIZZATI

L'analisi della struttura scatolare è stata condotta con un programma agli elementi finiti (PRO_SAP prodotto dalla 2S.I. Software e Servizi per l'Ingegneria S.r.l. P.tta Schiatti 8/b 44100 Ferrara)) schematizzando i vari setti con elementi "beam".

7.1.1. Modellazione adottata

La struttura viene schematizzata attraverso un modello analitico agli elementi finiti. Si è assunto lo schema statico di telaio chiuso. La mesh è composta da 26 beam elements e da 26 nodi (figure 2a e 2b); l'output di calcolo viene raccolto nell'allegato.

L'analisi strutturale e' condotta con il metodo degli spostamenti per la valutazione dello stato tenso-deformativo indotto da carichi statici.

Il suolo viene modellato facendo ricorso all'usuale artificio delle molle elastiche alla Winkler.

Nel caso in esame il valore della costante di sottofondo si assume pari a: Ks = 3500 kN/m3

Agli effetti delle caratteristiche geometriche delle varie aste si è quindi assunto:

- una sezione rettangolare b x h = 100 x Ss cm per la soletta superiore
- una sezione rettangolare b x h = 100 x Sf cm per la soletta di fondazione
- una sezione rettangolare b x h = 100 x Sp cm per i piedritti

Per le aste del reticolo si è assunto:

Ec = 31447 / 32588 N/mm² ; modulo elastico del calcestruzzo rispettivamente per classe di resistenza C25/30 e C28/35.

Lo schema statico della struttura e la relativa numerazione dei nodi e delle aste sono riportati nelle figure seguenti:

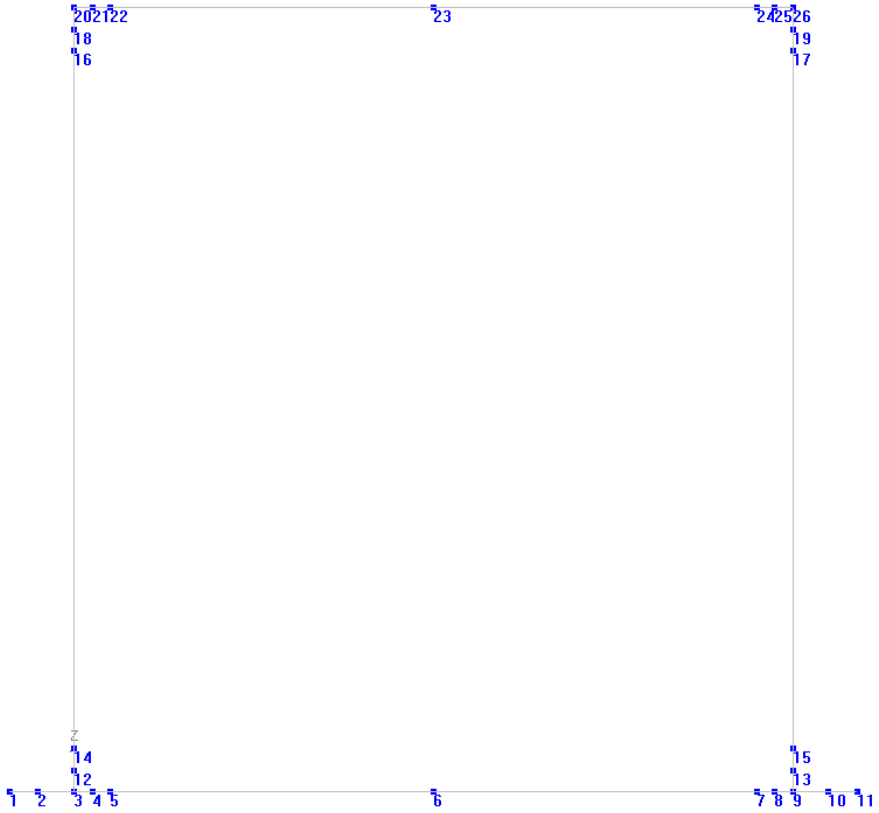


FIG. 2A - NUMERAZIONE DEI NODI

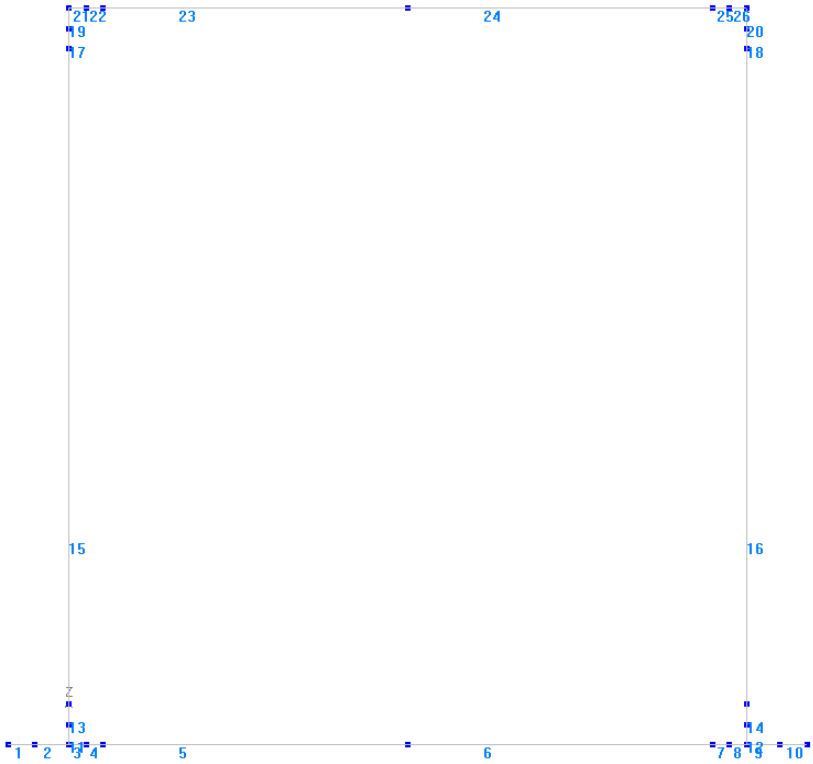


FIG. 2B - NUMERAZIONE DELLE ASTE

7.2. ANALISI DEI CARICHI

Nel seguente paragrafo si descrivono i carichi elementari da assumere per le verifiche di resistenza in esercizio ed in presenza dell'evento sismico.

Vengono prese in considerazione n°19 Condizioni Elementari di carico (CDC1÷ CDC 19), di seguito determinate.

Si considerano nel calcolo delle sollecitazioni agenti nello scatolare i seguenti carichi. I dettagli relativi a ciascuna condizione di carico sono riportati nel paragrafo di analisi dei carichi.

CDC	Tipo	Sigla Id
1	Ggk	CDC=Ggk (peso proprio della struttura)
2	Gk	CDC=Gk (permanenti portati)
3	Gk	CDC=Gk (spinta a riposo piedritto sx)
4	Gk	CDC=Gk (spinta a riposo piedritto dx)
5	Gk	CDC=Gk (spinta attiva piedritto sx)
6	Gk	CDC=Gk (spinta attiva piedritto dx)
7	Qk	CDC=Qk (Q1k centrato)
8	Qk	CDC=Qk (Q1k filo piedritto dx)

CDC	Tipo	Sigla Id
9	Qk	CDC=Qk (Q1k filo piedritto sx)
10	Qk	CDC=Qk (Accidentale su piedritto sx)
11	Qk	CDC=Qk (Accidentale su piedritto dx)
12	Qk	CDC=Qk (Accidentale 20kPa su piedritto sx)
13	Qk	CDC=Qk (Accidentale 20kPa su piedritto dx)
14	Qk	CDC=Qk (frenatura)
15	Qk	CDC=Qk (Sisma orizzontale)
16	Qk	CDC=Qk (Sisma verticale)
17	Qk	CDC=Qk (Variazione termica uniforme)
18	Qk	CDC=Qk (Variazione termica lineare su soletta e piedritti)
19	Qk	CDC=Qk (Ritiro differenziale soletta)

Tali Combinazioni Elementari saranno opportunamente combinate secondo quanto previsto dalla normativa vigente.

Per i materiali si assumono i seguenti pesi specifici:

- calcestruzzo armato: 25 kN/m³
- rilevato 20 kN/m³
- pavimentazione (spessore 0.50m) 22 kN/m³

7.2.1. Carichi elementari applicati:

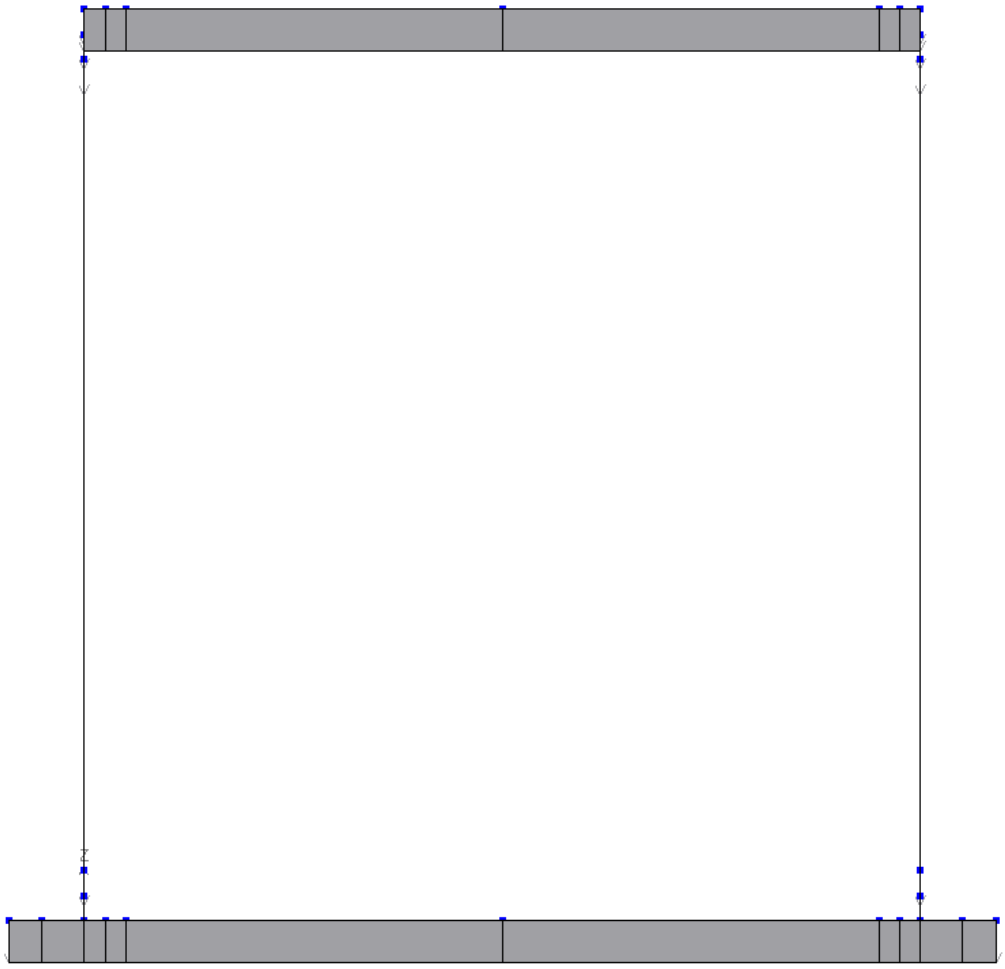


FIGURA 7.2-1 - PESO PROPRIO DELLA STRUTTURA (CARICO AUTOMATICO, CDC 1)

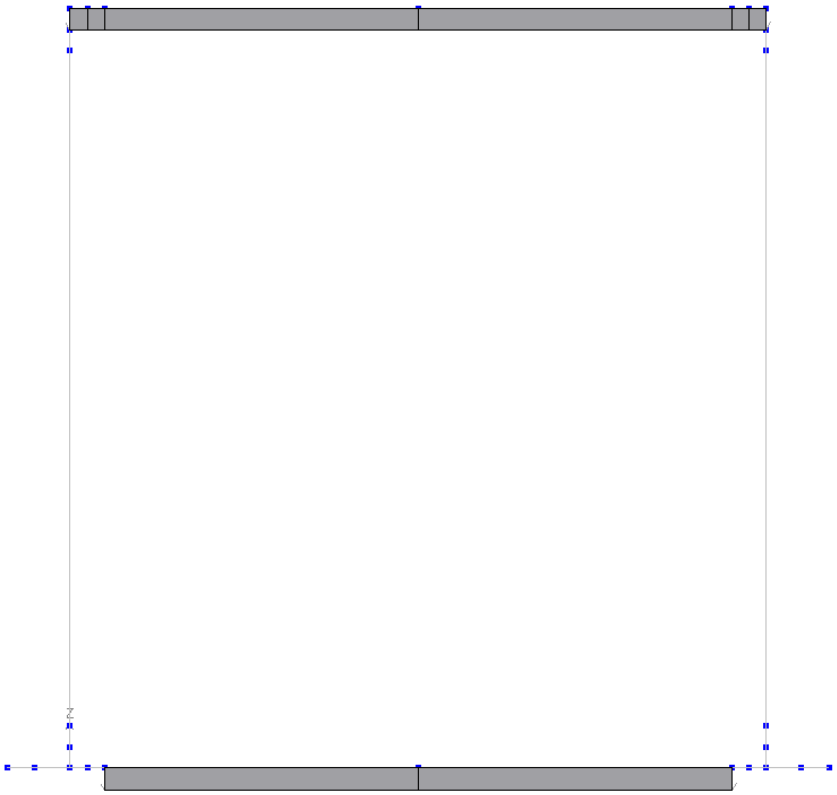


FIGURA 7.2-2 - CARICHI PERMANENTI (CDC 2)

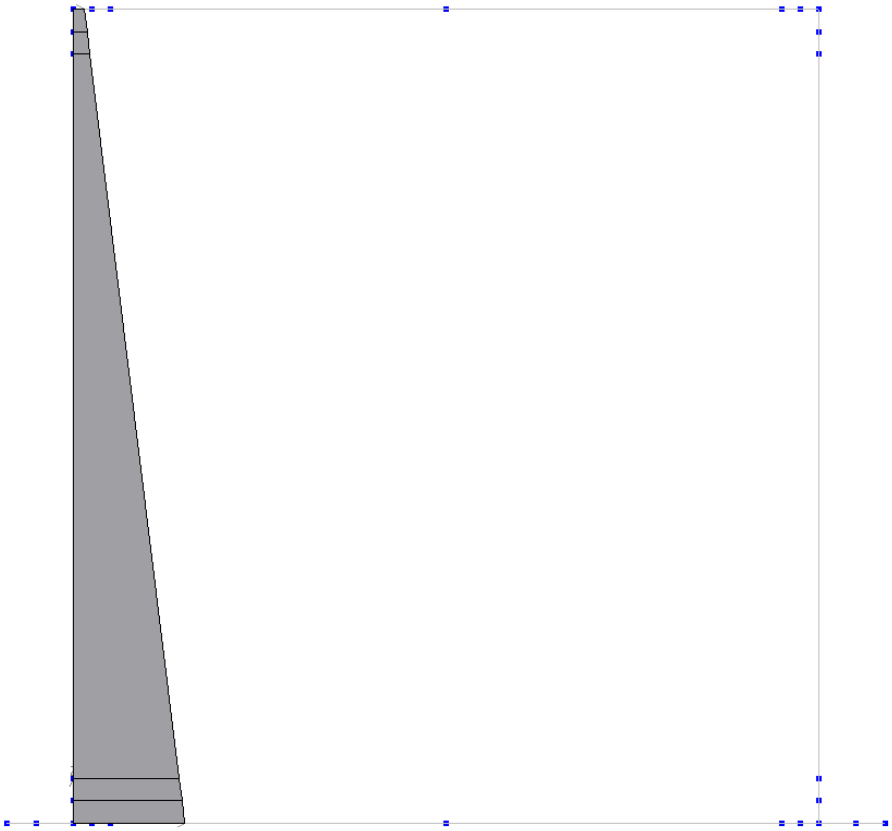


FIGURA 7.2-3 - SPINTA A RIPOSO DELLE TERRE SUL PIEDRITTO SINISTRO (CDC 3)

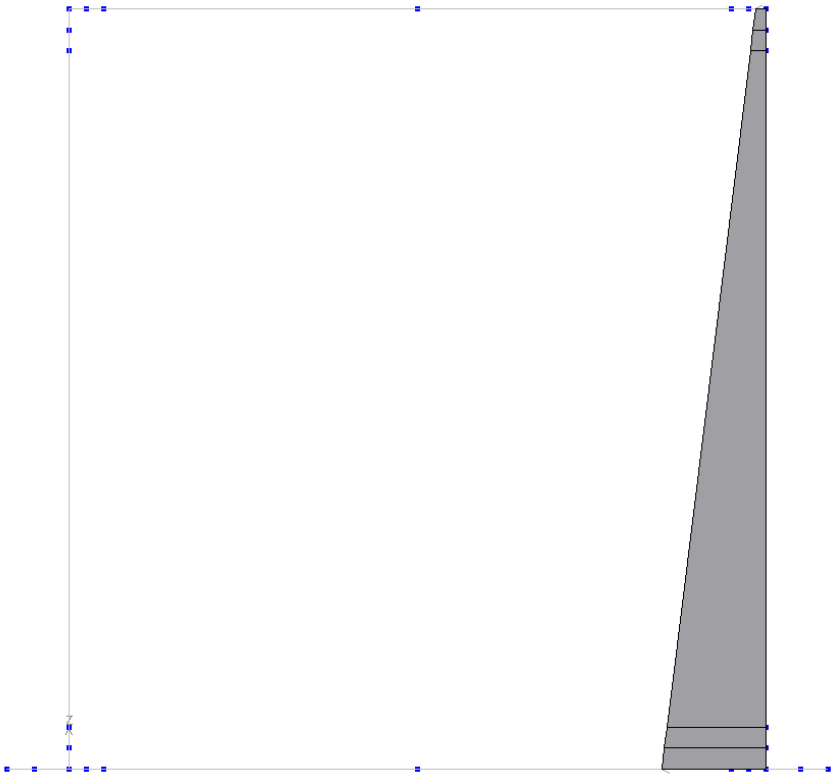


FIGURA 7.2-4 - SPINTA A RIPOSO DELLE TERRE SUL PIEDRITTO DESTRO (CDC 4)

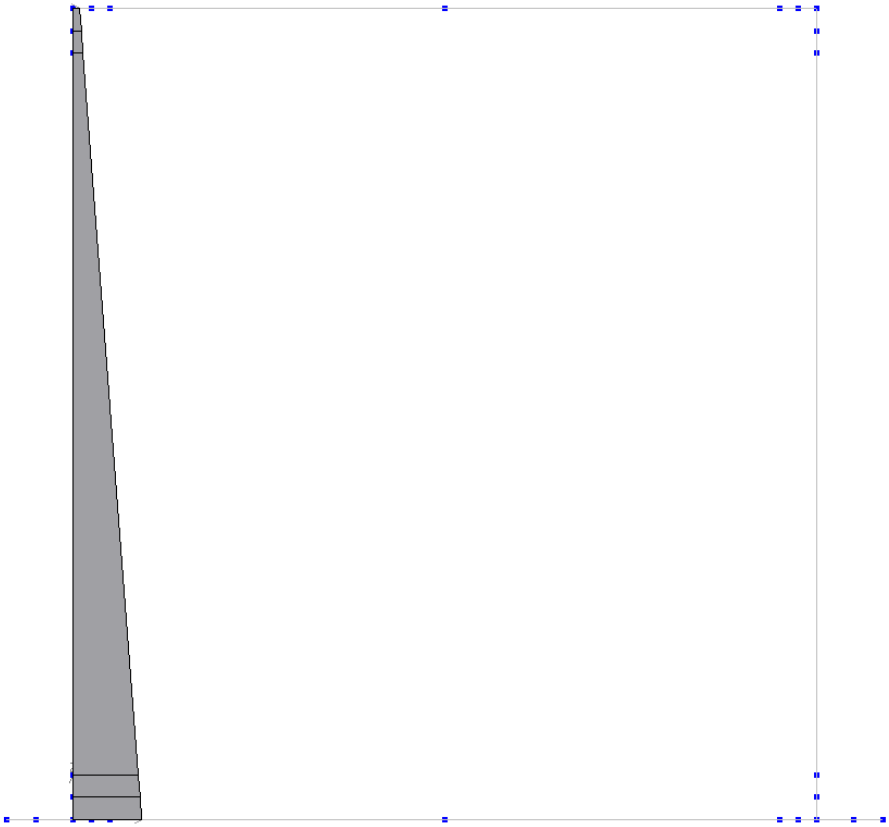


FIGURA 7.2-5 - SPINTA ATTIVA DELLE TERRE SUL PIEDRITTO SINISTRO (CDC 5)

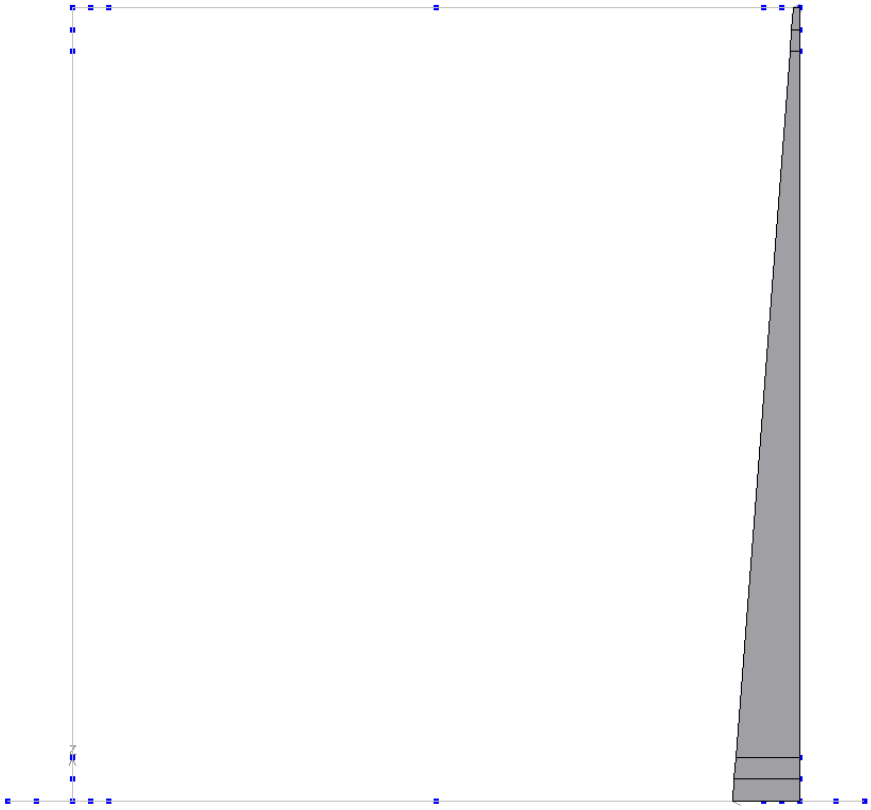


FIGURA 7.2-6 - SPINTA ATTIVA DELLE TERRE SUL PIEDRITTO DESTRO (CDC 6)

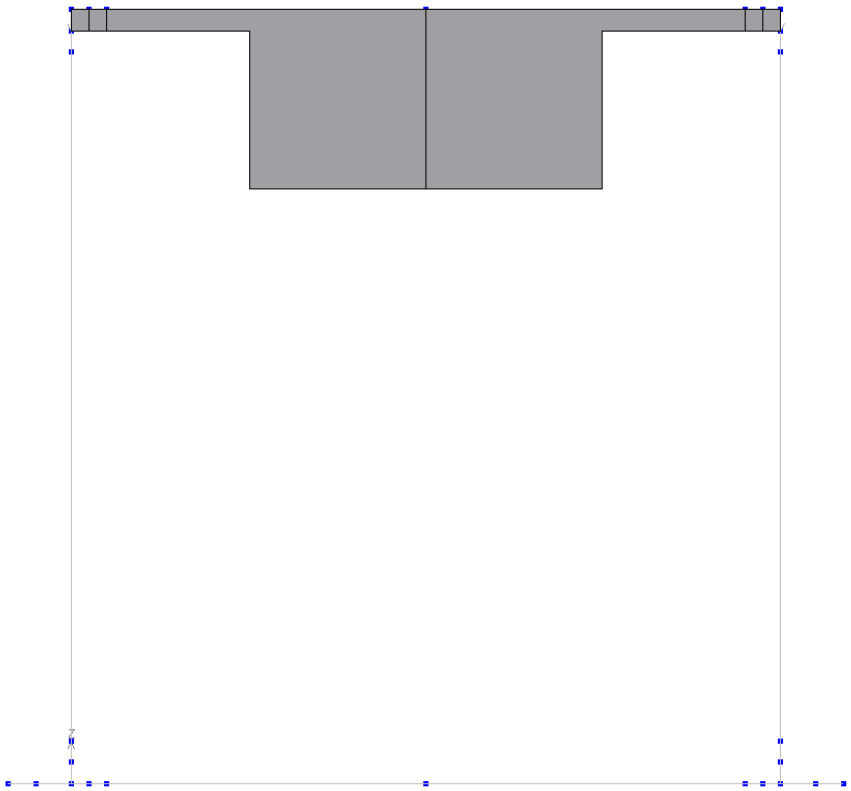


FIGURA 7.2-7 - CARICO DA TRAFFICO SU SOLETTA SUPERIORE, CENTRATO (CDC 7)

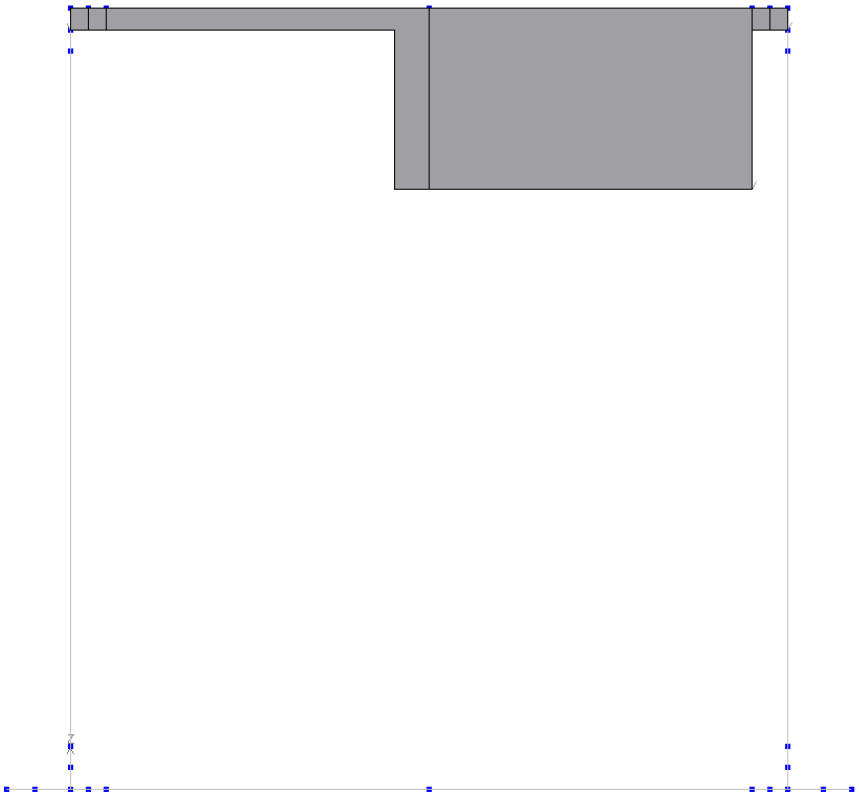


FIGURA 7.2-8 - CARICO DA TRAFFICO SU SOLETTA SUPERIORE, DESTRA (CDC 8)

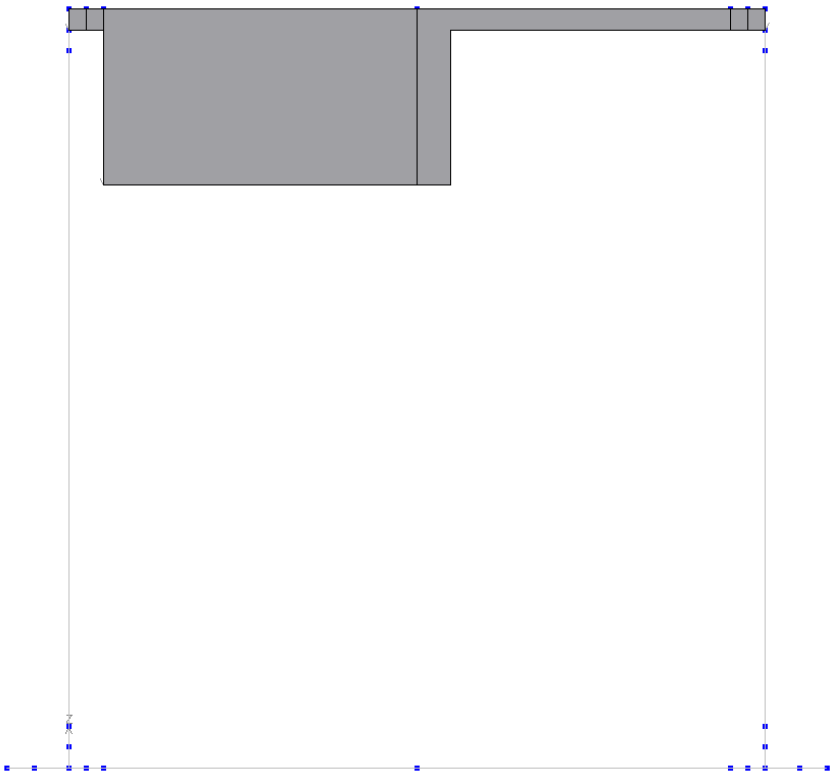


FIGURA 7.2-9 - CARICO DA TRAFFICO SU SOLETTA SUPERIORE, SINISTRA (CDC 9)

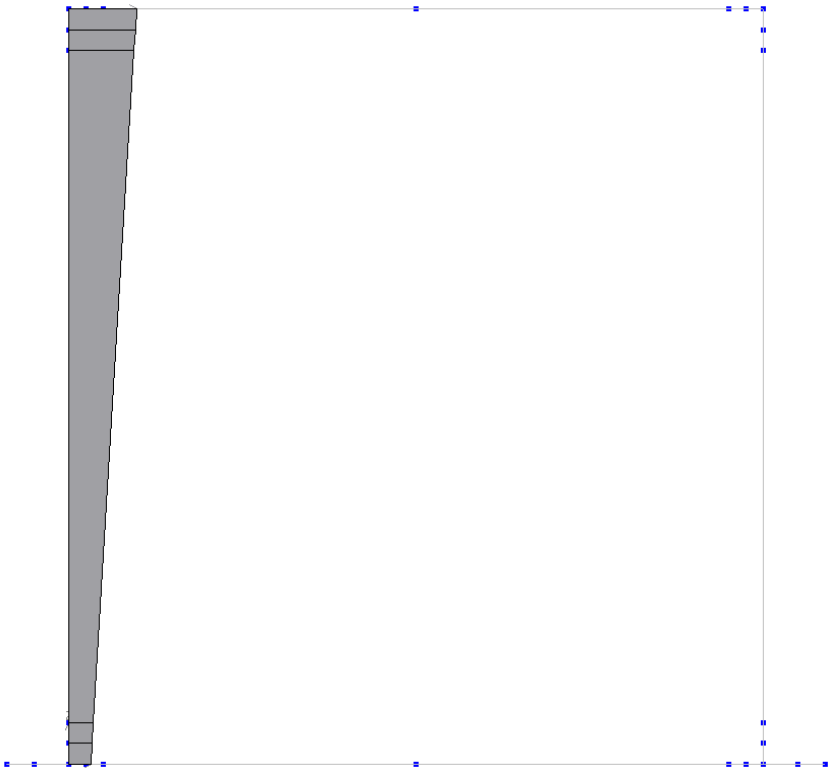


FIGURA 7.2-10 - SPINTA DEL SOVRACCARICO DA TRAFFICO SUL PIEDRITTO SINISTRO (CDC 10)

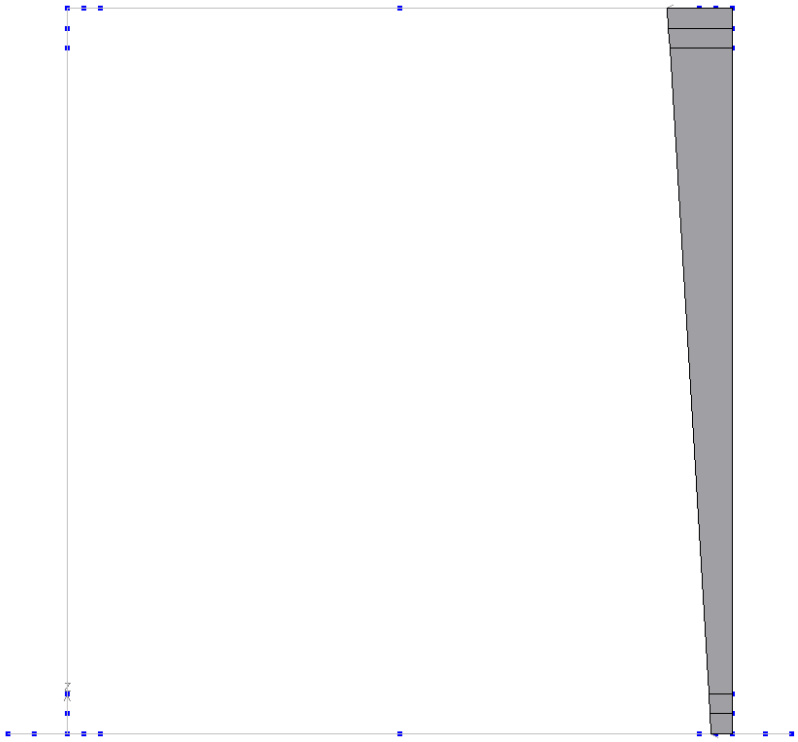


FIGURA 7.2-11 - SPINTA DEL SOVRACCARICO DA TRAFFICO SUL PIEDRITTO DESTRO (CDC 11)

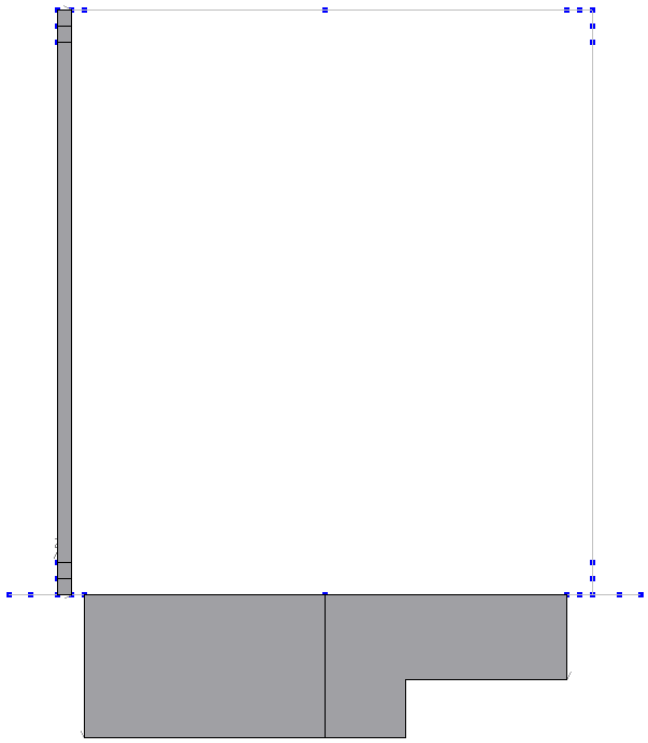


FIGURA 7.2-12 - SPINTA DEL SOVRACCARICO 20 KN/M2 SUL PIEDRITTO SINISTRO E SOVRACCARICO ACCIDENTALE SULLA SOLETTA DI FONDAZIONE (CDC 12)

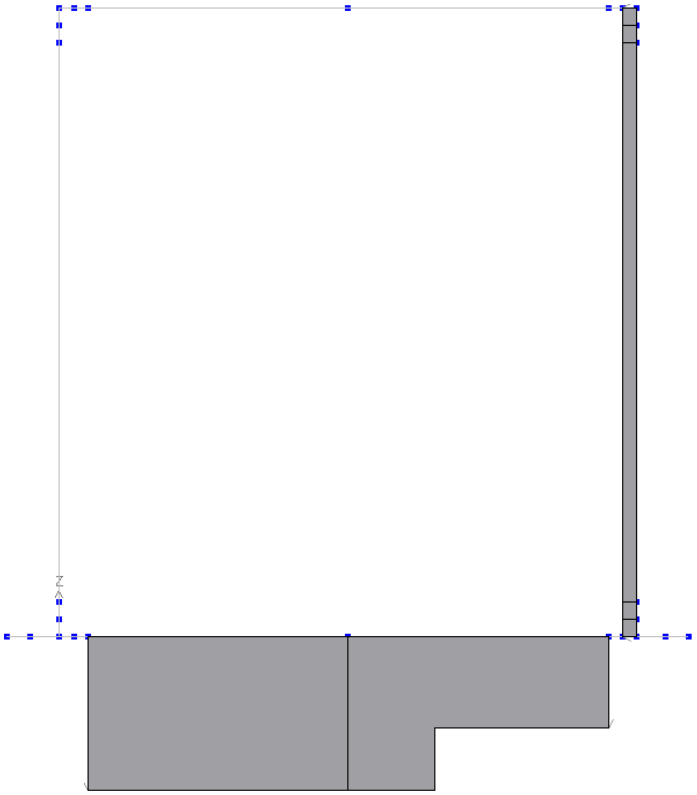


FIGURA 7.2-13 - SPINTA DEL SOVRACCARICO 20 KN/M2 SUL PIEDRITTO DESTRO E SOVRACCARICO ACCIDENTALE SULLA SOLETTA DI FONDAZIONE (CDC 13)

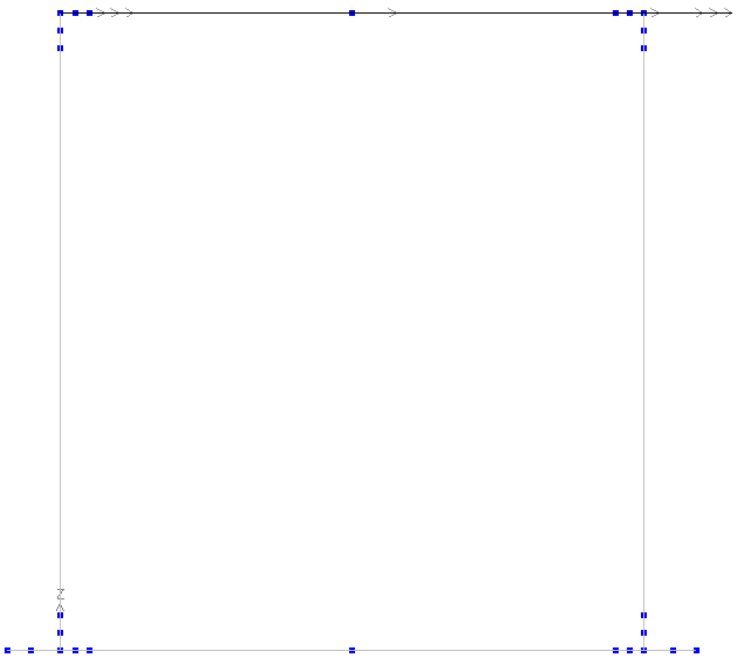


FIGURA 7.2-14 - FRENATURA (CDC 14)

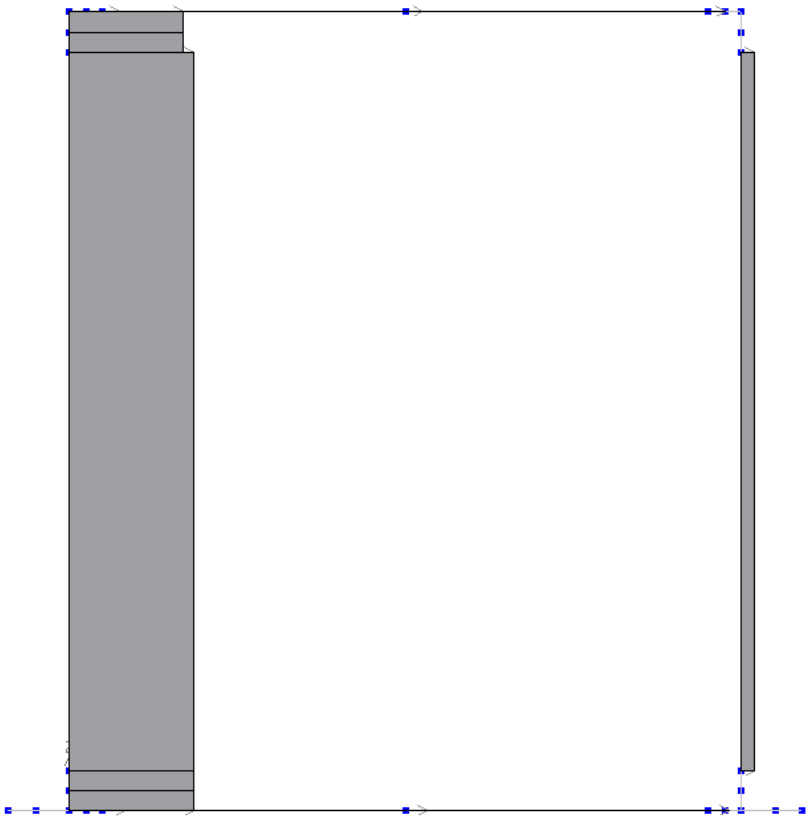


FIGURA 7.2-15 - AZIONE SISMICA ORIZZONTALE (CDC 15)

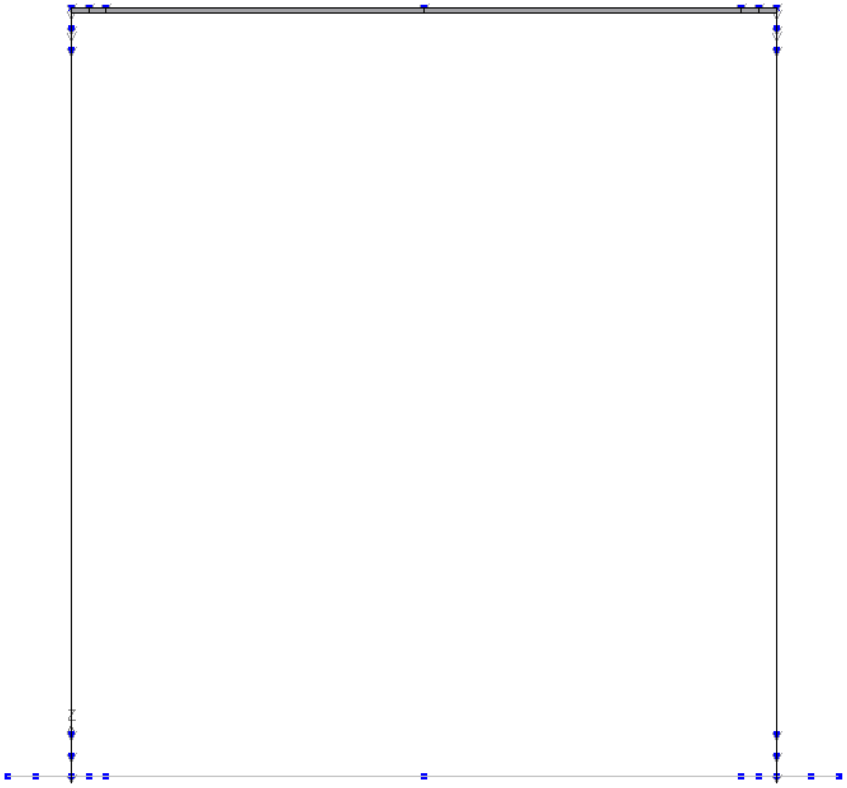


FIGURA 7.2-16 - AZIONE SISMICA VERTICALE (CDC 16)

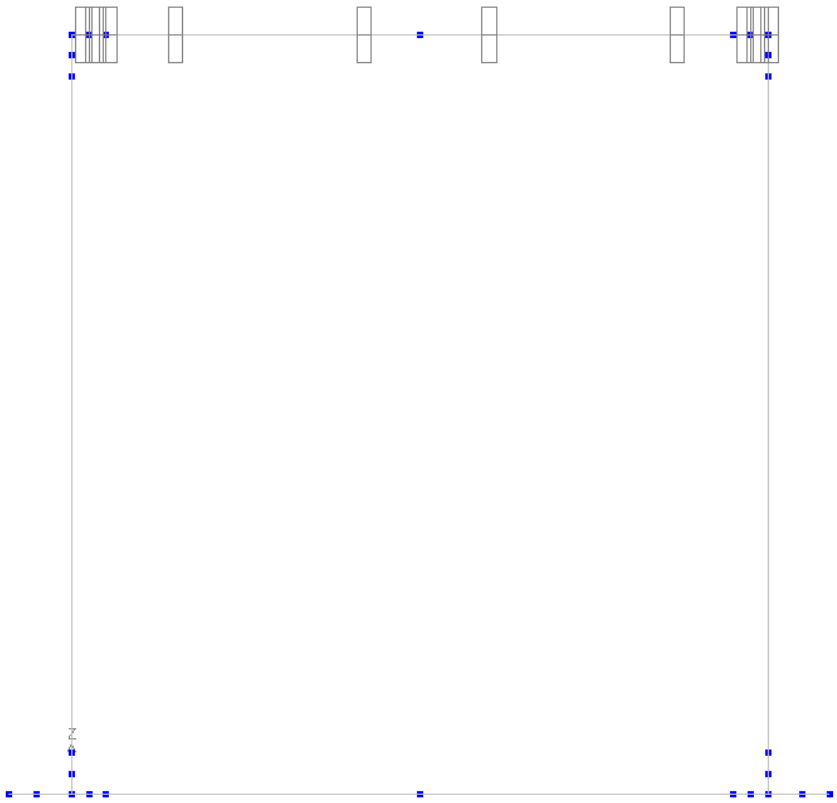


FIGURA 7.2-17 - CARICO TERMICO UNIFORME (CDC 17)

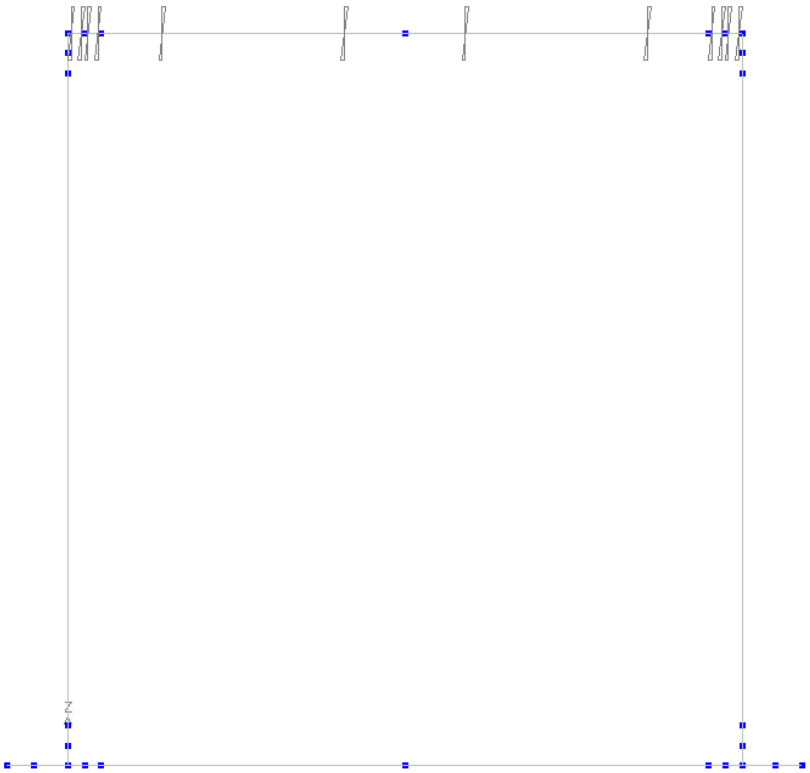


FIGURA 7.2-18 - CARICO TERMICO A FARFALLA (CDC 18)

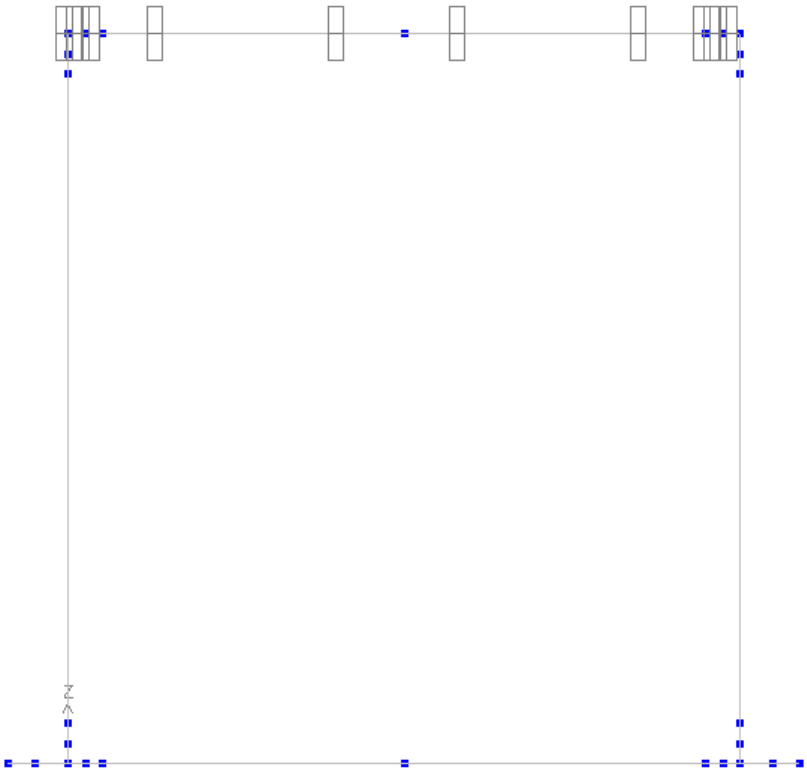


FIGURA 7.2-19 - RITIRO (CDC 19)

7.2.2. Peso proprio e carichi permanenti portati

Soletta superiore

peso proprio	0.40	*	25.00	=	10.00	kN/m^2
peso pavimentazione	0.15	*	22.00	=	3.30	
totale					13.30	kN/m^2

Soletta inferiore

peso proprio	0.60	*	25.00	=	15.00	kN/m^2
peso sovrastruttura stradale	0.50	*	20.00	=	10.00	kN/m^2
totale					25.00	kN/m^2

Piedritti

peso proprio	0.50	*	25.00	=	12.50	kN/m^2

Tali carichi vengono considerati nelle condizioni di carico elementari CDC 1-2, in particolare nella CDC1 sono presenti i pesi propri della struttura, nella condizione di carico CDC2 i carichi permanenti portati.

7.2.3. Spinta delle terre

Il reinterro a ridosso dello scatolare verrà realizzato tramite materiale di buone caratteristiche meccaniche, in accordo a quanto riportato al paragrafo 5 del presente documento.

La spinta del terreno assume un andamento lineare con la profondità secondo la legge:

$p_h = \lambda \gamma_t z$

dove si considera come coefficiente di spinta λ il coefficiente di spinta attiva o a riposo a seconda dell'elemento strutturale di cui si vogliono massimizzare le sollecitazioni

1) In presenza di falda esterna allo scatolare

Le pressioni del terreno relative alla <u>spinta a riposo</u>, in corrispondenza dei nodi caratteristici dei piedritti, risultano essere le seguenti:

p_2 = (22.00 * 0.15 + 19.5 * 0.20) * 0.384 = 2.77 kN/m^2

p_{12} = p_2 + (19.50 * 0.20) * 0.384 = 6.60. kN/m^2

p_w = p_{12} + (19.50 * 6.00) * 0.384 = 49.23 kN/m^2

p_1 = p_w + (9.50 * 0.30) * 0.384 + (10.000 * 0.300) = 51.48 kN/m^2

Tali spinte vengono considerate nella Condizione Elementare (CDC 3) sul piedritto sx e nella Condizione Elementare (CDC 4) sul piedritto dx.

Le pressioni del terreno relative alla <u>spinta attiva</u>, in corrispondenza dei nodi caratteristici dei piedritti, risultano essere le seguenti:

p_2 = (22.00 * 0.15 + 19.5 * 0.20) * 0.238 = 1.71 kN/m^2

p_{12} = p_2 + (19.50 * 0.20) * 0.238 = 4.09 kN/m^2

p_w = p_{12} + (19.50 * 6.00) * 0.238 = 31.40 kN/m^2

p_1 = p_w + (9.50 * 0.30) * 0.238 + (10.000 * 0.300) = 35.08 kN/m^2

Tali spinte vengono considerate nella Condizione Elementare (CDC 5) sul piedritto sx e nella Condizione Elementare (CDC 6) sul piedritto dx.

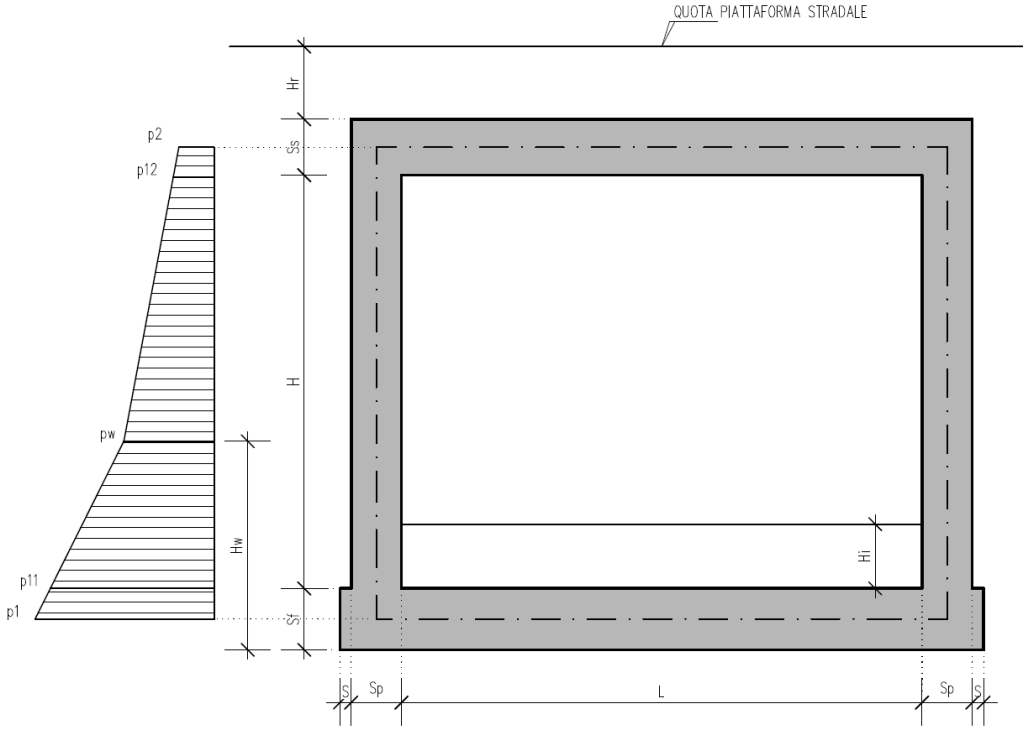


Figura 7.2-20 – Spinta delle Terre

Nelle combinazioni di carico verranno considerate:

1) Spinta a riposo su entrambi i piedritti;
2) Spinta attiva su ambo i piedritti;
3) Spinta a riposo su piedritto sx e spinta attiva su piedritto dx;

La condizione di spinta 3) serve a mettere in conto possibili situazioni (anche temporanee) di disomogeneità nei costipamenti o altre condizioni che possano generare situazioni di spinte asimmetriche sull'opera. La condizione di spinta attiva, sebbene poco realistica considerando le caratteristiche dell'opera, viene comunque considerata a favore di sicurezza per massimizzare i valori delle sollecitazioni flessionali in corrispondenza delle mezzerie delle solette.

Naturalmente queste spinte saranno opportunamente combinate, utilizzando i valori dei coefficienti parziali delle azioni da assumere nell'analisi per la determinazione degli effetti delle azioni nelle verifiche agli stati limite ultimi.

7.2.4. Spinta della falda interna allo scatolare

Assente

(Condizione Elementare CDC 7)

7.2.5. Carichi veicolari sulla soletta superiore

I casi di carico CDC8, CDC9, CDC10 e CDC11 sono relativi agli effetti indotti sulla soletta superiore dai carichi veicolari agenti in corrispondenza della sovrastruttura stradale. I carichi di riferimento sono descritti nel paragrafo 5.1.3.3 del D.M. 14/01/2008.

In particolare lo schema di carico 1 è costituito da carichi concentrati su due assi in tandem e da carichi uniformemente distribuiti ; i carichi concentrati sono pari a:

Q_{1k} = 300 kN ad asse (300 + 300 = 600 kN) su corsia n.1 di larghezza convenzionale pari a 3 m ;

Q_{2k} = 200 kN ad asse (200 + 200 = 400 kN) su corsia n.2 di larghezza convenzionale pari a 3 m ;

Q_{3k} = 100 kN ad asse (100 + 100 = 200 kN) su corsia n.3 di larghezza convenzionale pari a 3 m ;

Si ipotizza che tali carichi siano applicati su un'impronta rettangolare pari a 2.4 x 1.60 m (1.6 m sviluppo parallelo alla corsia di traffico, 2.4 m sviluppo perpendicolare), ovvero pari all'ingombro complessivo esterno del tandem. Per quanto riguarda i carichi uniformemente distribuiti (associati ai carichi tandem) si considera prudenzialmente il carico q_{1k} = 9 kN/m^2 applicato a tutte le colonne di carico (la norma prevede l'applicazione dalla seconda alla n-esima corsia di un carico ridotto da 2.5 kN/m^2).

I carichi tandem vengono posizionati ortogonalmente all'asse del sottovia e vengono ripartiti sia in direzione longitudinale che trasversale dal piano stradale al piano medio della soletta superiore. Si assume che la diffusione avvenga con un angolo di 30° attraverso il rilevato stradale (in accordo al punto C5.1.3.3.7.1 della circolare ministeriale del 02/02/2009) e con un angolo di 45° nella soletta superiore del tombino. L'effetto dei carichi tandem sulla soletta superiore viene pertanto messo in conto attraverso la determinazione di un carico equivalente distribuito q_{eq} a cui si somma il carico uniforme q_{1k} = 9 kN/m^2.

7.2.5.1 Diffusione del carico tandem in direzione longitunale (parallela all'asse stradale)

La larghezza di diffusione del carico tandem in direzione longitudinale è pari a:

L_{dl} = 1.6 m + 2x [tan30°x H_r + tan45°xS_s/2]

Nel caso in esame risulta:

L_{dl} = 1.60 + 2 * (0.25 * tg30° + 0.20) = 2.17 m

7.2.5.2 Diffusione del carico tandem in direzione trasversale (ortogonale all'asse stradale)

In direzione trasversale alla strada detta L_{dt} la *larghezza di diffusione del carico trasversale* dal piano stradale alla quota del piano medio della soletta superiore, assumendo che detta diffusione avvenga con angolo di diffusione di 30° attraverso il rilevato stradale e di 45° sino al piano medio della soletta superiore

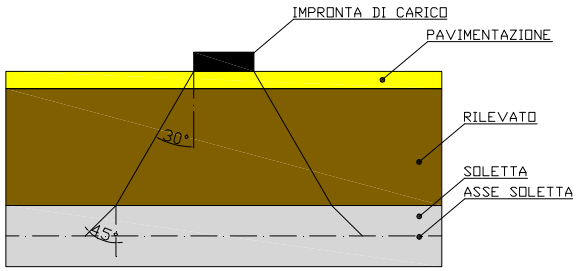


Figura 7.2-21 – Angoli di diffusione del carico Tandem

risulta:

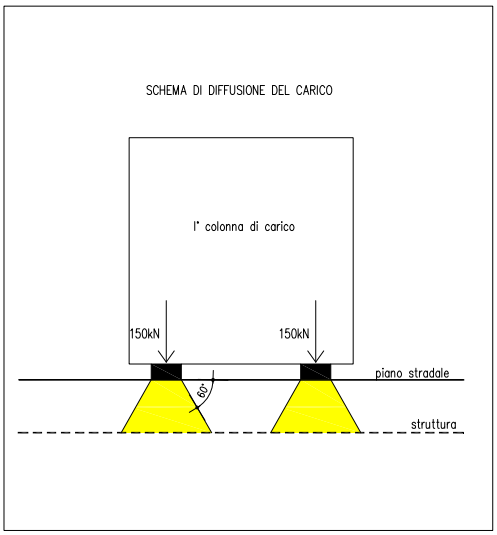
L_{dt} = 2.40 + 2 * (0.25 * tg30° + 0.20) = 2.97 m

Il valore di L_{dt} viene poi limitato in base alle seguenti circostanze:

presenza della seconda colonna di carico: il carico della 1° colonna, in corrispondenza dell'adiacenza alla 2° colonna, può essere diffuso al massimo fino a 0.30m all'esterno dell'impronta del carico;

posizionando il carico in adiacenza al cordolo, ne consegue che la massima diffusione lato cordolo è pari a:

$L_{d,\ cordolo}$ = tan30 x Hr + tan45 x Ss/2



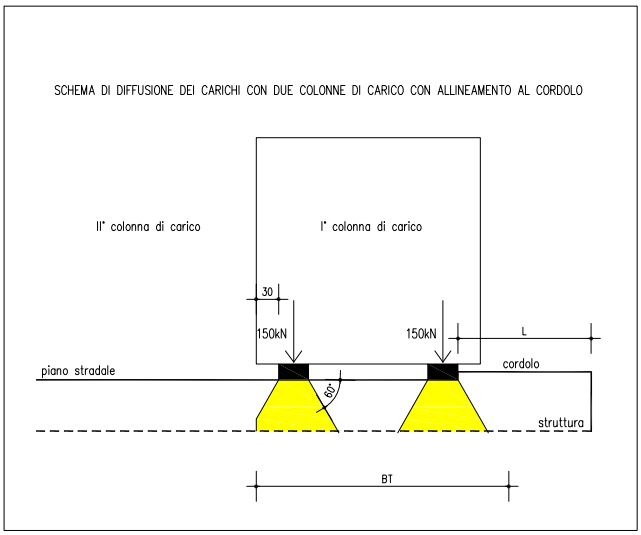


Figura 7.2-22 - Figura 7.2-23 – Schemi di Diffusione Trasversale e Longitudinale del carico Tandem

pertanto la larghezza di diffusione trasversale non può risultare superiore al valore di:

$L_{dt,max}$ = 2.40 + 0.30 + (0.25 * tg30° + 0.20) = 2.97 m

7.2.5.3 Calcolo del carico distribuito equivalente al tandem

Avendo definito L_{dl} e L_{dt} si può valutare l'intensità del carico q_{eq} equivalente all'effetto indotto dai carichi tandem sulla soletta superiore:

Considerando il carico tandem dovuto alla prima colonna di carico

$q_{eq} = 2 \times Q_{1k} / (L_{dl} \times L_{dt,max}) = 92.86$ kN/m

cui si sovrappone il carico q = 9 kN/m uniforme su tutta la soletta (corrispondente al carico q_{1k}).

La posizione del carico q_{eq} equivalente al tandem viene variata su tutta la soletta nei casi di carico CDC8-10 per massimizzare:

CDC 8: il momento in mezzeria soletta;

CDC 9: il taglio nella soletta a filo piedritto destro;

CDC 10: il taglio nella soletta a filo piedritto sinistro.

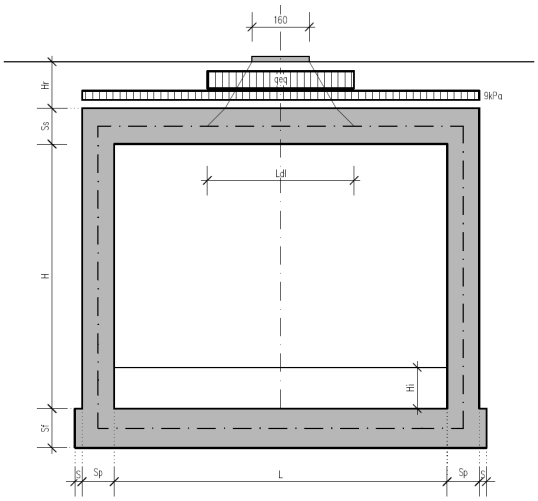


Figura 7.2-24 – Schema di Diffusione del carico da traffico – Carico Tandem Centrato

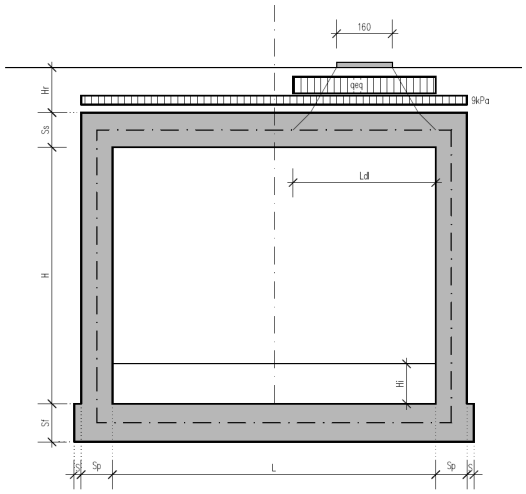


Figura 7.2-25 - Schema di Diffusione del carico da traffico – Carico Tandem filo Piedritto Destro

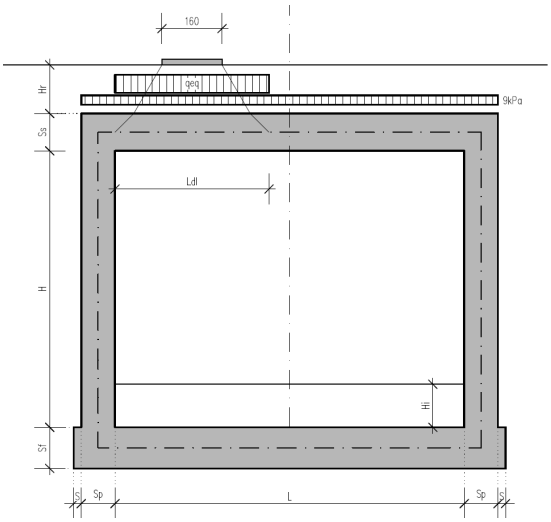


Figura 7.2-26 - Schema di Diffusione del carico da traffico – Carico Tandem filo Piedritto Sinistro

Si noti che se $L_{dl} > L + 2 \times S_p$ (larghezza netta interna + spessore dei piedritti) allora il carico equivalente è applicato a tutte le aste della soletta superiore nei tre casi di carico CDC 8-10 che vengono a coincidere tra di loro.

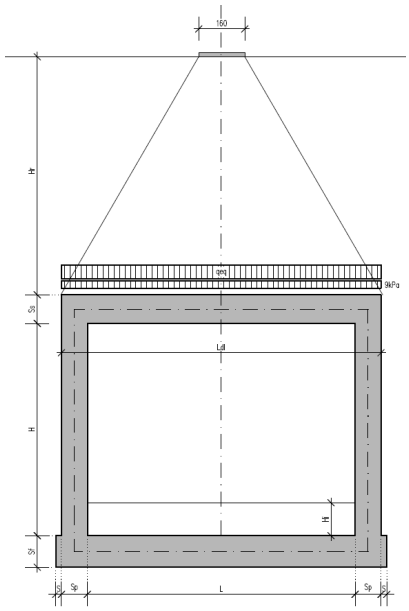


Figura 7.2-27 - Schema di Diffusione del carico da traffico – Caso con carichi Tandem coincidenti

7.2.5.4 <u>Sovraccarico uniforme da 20kN/m2</u>

Poiché il valore del sovraccarico uniforme è inferiore al valore del carico tandem distribuito equivalente qeq si ritiene trascurabile questo contributo.

7.2.6. <u>Spinte sui piedritti indotte dai sovraccarichi accidentali</u>

In accordo con il punto C5.1.3.3.7.1 della circolare ministeriale 02/02/2009 per il calcolo delle spinte generate dal sovraccarico sul rilevato si può considerare applicato lo schema di carico 1, in cui per semplicità i carichi tandem possono essere sostituiti da carichi uniformemente distribuiti equivalenti, applicati su una superficie rettangolare larga 3.0 m e lunga 2.20 m. Anche in questo caso si tiene in conto la diffusione del carico attraverso il rilevato sia in direzione longitudinale che trasversale. Al tandem si somma il carico uniformemente distribuito agente sulla i-esima corsia di carico $q_{ik} = 9$ kN/m^2 .

7.2.6.1 Diffusione del carico tandem in direzione longitudinale (parallela all'asse stradale)

Il carico tandem trasformato in carico uniformemente distribuito assume il valore:

$600/(3.00x2.20)=90.91kN/m^2$

La larghezza di diffusione del carico tandem in direzione longitudinale è pari a:

$L_{dl,sup}$= 2.2 m + [tan30°x (2 x H_r + S_s/2)] **=** 2.66m (piano medio sol. sup.)

$L_{dl,inf}$ = 2.2 m + [tan30°x (2 x H_r + S_s/2 + H + S_f/2)] **=** 6.10m (piano medio sol. inf.)

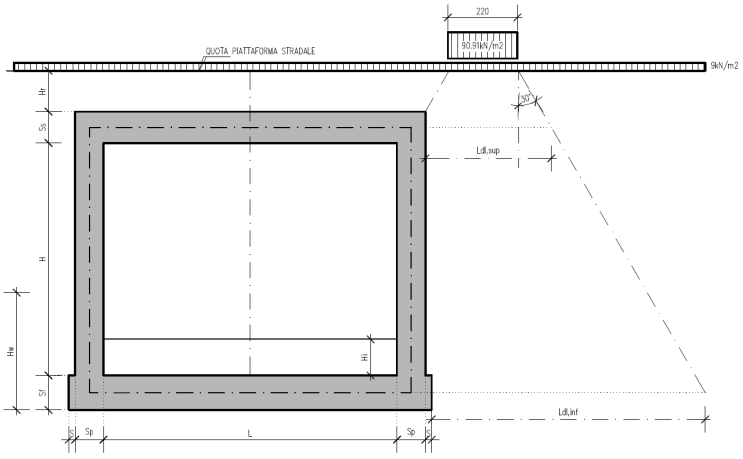


Figura 7.2-28 – Schema di diffusione del Carico Tandem in direzione Longitudinale

7.2.6.2 Diffusione del carico tandem in direzione trasversale (ortogonale all'asse stradale)

In direzione trasversale, consederando due colonne di carico e la ripartizione trasversale del carico distribuito, si ottiene quanto riportato nella figura seguente:

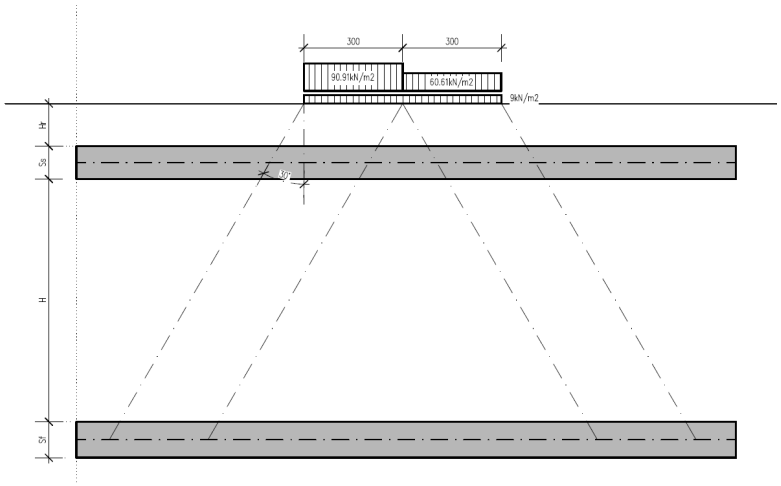


Figura 7.2-29 – Schema di diffusione del Carico Tandem in direzione Trasversale

Per il calcolo delle azioni agenti sulle pareti dello scatolare, si considera il carico distribuito dovuto alla colonna di carico 1, limitando la diffusione del carico sul lato della seconda colonna di carico come schema seguente:

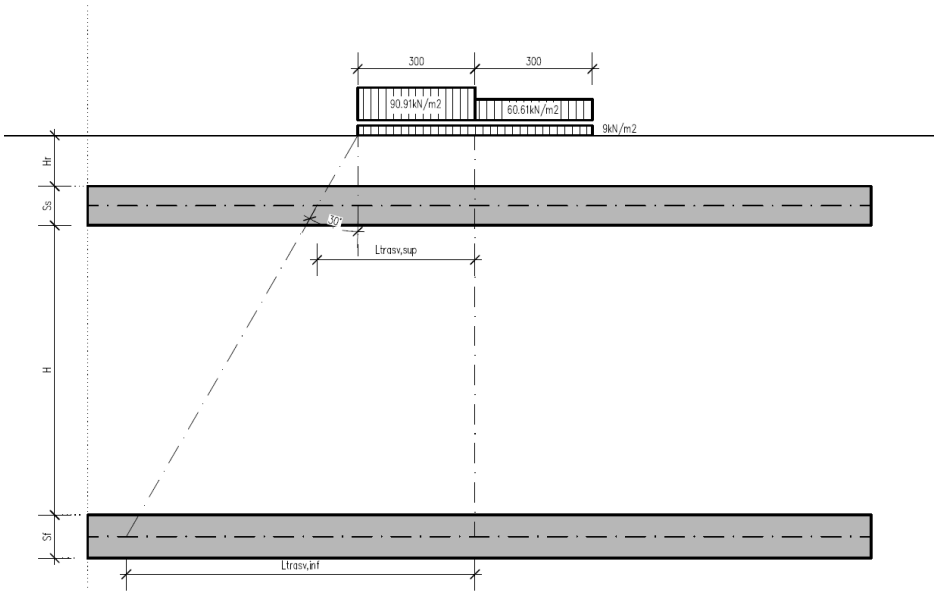


Figura 7.2-30 – Schema di diffusione del Carico Tandem in direzione Longitudinale

La larghezza di diffusione del carico tandem in direzione longitudinale è pari a:

$L_{dt,sup}$= 3 m + [tan30° x (H_r + S_s/2)] **=** 3.20m (piano medio sol. sup.)

$L_{dt,inf}$ = 3 m + 2 x [tan30° x (H_r + S_s+ H+S_f/2)] **=** 6.95m (piano medio sol. inf.)

7.2.6.3 Definizione dei carichi di progetto

Il diagramma di spinta applicato ai piedritti varia linearmente fra i valori qacc,sup2 e qacc,sup1 come esemplificato nella immagine seguente (spinta a riposo).

Il contributo dei carichi Tandem vale:

Qacc,sup = 2 x Q1,k x (Ldt,sup x Ldl,sup) x k0 = 28.94 kN/m

Qacc,inf = 2 x Q1,k x (Ldt,inf x Ldl,inf) x k0 = 6.24 kN/m

A questi valori si somma il contributo del carico distribuito q1k = 9 kN/m2:

qacc,sup = Qacc,sup + k0 x q1k = Qacc,sup + 0.384 x 9 = 32.397 kN/m

qacc,inf = Qacc,inf + k0 x q1k = Qacc,inf + 0.384 x 9 = 8.771 kN/m

Le spinte sui piedritti generate dai sovraccarichi da traffico (Q1k + q1k) vengono inserite nei casi di carico CDC10-11 agenti rispettivamente sul piedritto sinistro e destro

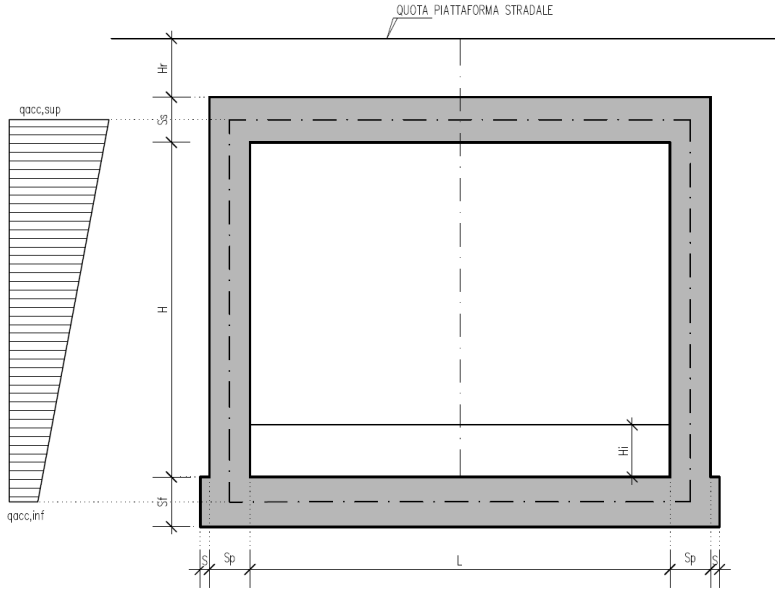


FIGURA 7.2-31 – SPINTA SUL PIEDRITTO GENERATA DAL CARICO DA TRAFFICO

CDC 12-13: spinta sul piedritto generata dal sovraccarico da 20kN/m2 sul rilevato

Nello scenario di carico da traffico alternativo allo Schema di Carico 1 si considera, ai fini del calcolo della spinta sui piedritti, un carico qacc sul terrapieno pari a 20 kN/m2 .

Tale carico genera spinte pari a:

p = k0 x qacc = 0.384 x 20 = 7.69 kN/m (spinta a riposo, CDC 12 e 13, piedritto sinistro/destro)

7.2.7. Sovraccarichi accidentali sulla soletta di fondazione

Sulla soletta di fondazione si applica il carico tandem corrispondente a ciascuna colonna di carico $Q_{i.k}$, ripartito su una larghezza pari all'ingombro della colonna di carico convenzionale (3m), e una lunghezza ottenuta dalla ripartizione del carico fino al piano medio della soletta attraverso il ricoprimenmto, assumendo che detta diffusione avvenga con angolo di diffusione di 30° attraverso il rilevato stradale e di 45° sino al piano medio della soletta.

Base collaborante trasversale: B_T =3.00m

Ingombro longitudinale: L_L = 1.60+2 ∗ (0.50*tan30°+0.60/2)=2.78m

$q'_{acc,1}$= 600/3.00/2.78+9 =81.01kN/m^2 (carico distribuito equivalente alla prima colonna di carico)

$q'_{acc,2}$= 400/3.00/2.78+2.5=50.51kN/m^2 (carico distribuito equivalente alla seconda colonna di carico)

(Condizioni Elementari CDC 15÷17)

7.2.8. Frenatura

La forza di frenatura q_3 è funzione del carico totale agente sulla corsia convenzionale n.1 e risulta pari a (si veda il paragrafo 5.1.3.5 del D.M. 14/01/2008):

180 kN ≤ q_3 = 0.6 x 2 x Q_{1k} + 0.10 q_{1k} x w_1 x L ≤ 900 kN

dove:

Q_{1k} = 300 kN

q_{1k}= 9 kN/m_2

w_1 = 3.00 m (larghezza della corsia)

L = 2 x S_p + B_i (larghezza della soletta compresi i piedritti)

Nel caso in esame risulta:

q_3 = 374.85 kN

L'azione di cui sopra, viene distribuita sulla soletta superiore dello scatolare; il valore della frenatura equivalente da applicare alla soletta, si ottiene distribuendo il valore del carico frenante, alla lunghezza della soletta e alla larghezza di diffusione del carico (L_{dt}), con la seguente relazione:

$q_{3,dis}$ = 374.85 / (5.00 * 2.97) = 25.21 kN/m^2

(applicata nel CDC 18)

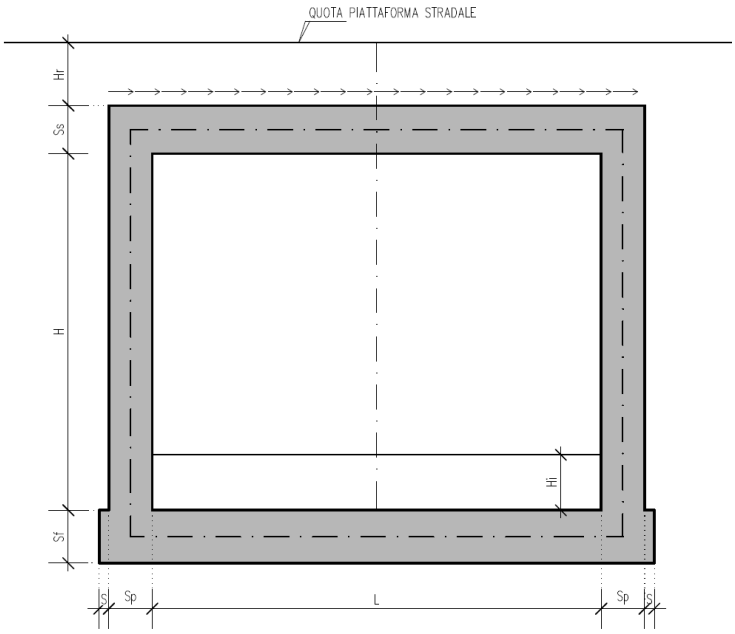


FIGURA 7.2-32 – AZIONE DELLA FRENATURA

7.2.9. Azioni sismiche

(CDC elementari 15-16)

Stato limite di salvaguardia della vita (SLV)

La risultante delle forze inerziali orizzontali indotte dal sisma viene valutata con la seguente espressione:

$F_h = P^* k_h$

$$k_h=\beta_m \cdot \frac{a\max}{g}$$

(SLV) $k_h=\beta_m \cdot \frac{a\max}{g}$ =0.373 $k_v=\pm 0.5^* k_h$=0.186

P = peso proprio;

k = coefficienti sismici;

Nel caso di sisma orizzontale si considera la spinta derivante dall'oscillazione del cuneo di terreno spingente con l'applicazione del diagramma triangolare di pressioni, tipico dei muri di sostegno, avente la risultante a 1/3 dell'altezza. Per tener conto dell'incremento di spinta del terreno dovuta al sisma si fa riferimento all'EC8, in cui l'incremento di spinta sismica ΔP per la condizione a riposo viene valutato:

$\Delta Pd = S \cdot a_g/g \cdot \gamma \cdot h_{tot}^2$

La risultante di tale incremento di spinta viene applicata ad h/2 del piedritto.

7.2.9.1 Ai fini delle azioni verticali, non considerando i carichi accidentali

sulla Soletta superiore si ha:

Peso proprio soletta	15.00	kN/m2	Inerzia Soletta	15.00	*	0.187	=2.80	kN/m2
Carichi permanenti	5.504	kN/m2	Inerzia Permanenti	5.50	*	0.187	=1.02	kN/m2
			Totale				=3.82	kN/m2

Sui piedritti si ha:

Peso proprio piedritto	12.50	kN/m2	Inerzia piedritto	12.50	*	0.187	=2.33	kN/m2

7.2.9.2 Ai fini delle azioni orizzontali

sui piedritti si considera il contributo della sovraspinta sismica dovuto al sisma oscillatorio e le spinte inerziali agenti sui piedritti, mentre sulla soletta superiore si considera l'inerzia della stessa nonchè i permanenti portati.

Spinta inerziale sulla soletta superiore:

Peso proprio*k_h	=	5.59	kN/m2
Peso permanente* k_h	=	2.05	kN/m2

Spinta inerziale sui piedritti:

Peso proprio*k_h	=	4.66	kN/m2

Spinta inerziale sulla soletta inferiore:

Peso proprio*k_h	=	5.59	kN/m2
Peso permanente* k_h	=	4.10	kN/m2

Sovraspinta sismica del terreno laterale:

h_{tot}	=	6.80	m
$\Delta Pd = amax /g \cdot \gamma \cdot h_{tot}^2$	=	335.92	kN/m
H scatolare	=	6.55	m
Sovraspinta sismica = $\Delta Pd /H$	=	51.29	kN/m2

dove si indica con h_{tot} l'altezza totale del tombino compresi gli spessori delle solette superiore e inferiore più l'altezza di ricoprimento totale del tombino. Si fa osservare che tale metodologia porta ad azioni eccessivamente prudenziali, soprattutto per tombini con altezza di ricoprimento elevata.

7.2.10. Azioni termiche

Sono stati considerati gli effetti dovuti alle variazioni termiche. In particolare, è stata considerata una variazione termica uniforme di ±10°C sulla soletta superiore (CDC 17) ed un salto termico di 5°C sulla soletta superiore e sui piedritti, analizzando nelle combinazioni di carico i due casi di intradosso più caldo dell'estradosso e viceversa agendo sul segno della sollecitazione, con andamento lineare nello spessore della soletta superiore e sui piedritti (CDC 18).

Per il coefficiente di dilatazione termica si assume:

$\alpha = 10 * 10\text{-}6 = 0.00001$ °C-1

7.2.11. Ritiro

Si considera soggetta a fenomeni di ritiro la sola soletta superiore. (CDC 19)

La deformazione totale da ritiro si può esprimere come:

$\varepsilon cs = \varepsilon cd + \varepsilon ca$

dove:

εcs è la deformazione totale per ritiro

εcd è la deformazione per ritiro da essiccamento

εca è la deformazione per ritiro autogeno.

Il valore medio a tempo infinito della deformazione per ritiro da essiccamento:

$\varepsilon cd,\infty = kh * \varepsilon c0$

può essere valutato mediante i valori delle seguenti Tab. 11.2.Va-b (NTC) in funzione della resistenza caratteristica a compressione, dell'umidità relativa e del parametro h0:

	Deformazione da ritiro per essiccamento (in ‰)					
fck	Umidità relativa (in %)					
	20.00	40.00	60.00	80.00	90.00	100.00
20.00	-0.62	-0.58	-0.49	-0.30	-0.17	0.00
25.00	-0.59	-0.55	-0.46	-0.29	-0.16	0.00
28.00	-0.56	-0.53	-0.45	-0.28	-0.15	0.00
32.00	-0.54	-0.51	-0.42	-0.26	-0.15	0.00
40.00	-0.48	-0.46	-0.38	-0.24	-0.13	0.00
60.00	-0.38	-0.36	-0.30	-0.19	0.10	0.00
80.00	-0.30	-0.28	-0.24	-0.15	-0.07	0.00

TABELLA 7.2-1- VALORI DI εc0

h0 (mm)	kh
100	1
200	0.85
300	0.75
400	0.725
500	0.7

Tabella 7.2-2– Valori di kh

I valori intermedi dei parametri indicati in tabella si ottengono per l'interpolazione lineare.

Il valore medio a tempo infinito della deformazione per ritiro autogeno εca,∞ può essere valutato mediante l'espressione:

εca,∞ =-2.5*(fck-10)*10-6 (con fck in N/mm2)

Assumendo come umidità relativa

Ur=70%

Si hanno i seguenti risultati:

coefficiente kh = 0.72

deformazione effettiva εc0 = -0.357 ‰

ritiro da essiccamento εcd,∝ = -0.257 ‰

deformazione per ritiro autogeno $\varepsilon ca,\infty$ = -0.048 ‰

ritiro totale εcs = -0.305 ‰

si determina quindi la variazione termica equivalente:

coeff. espansione termica α = 0.00001

variazione termica $\Delta T = \varepsilon cs/\alpha$ ΔT = -30.51 °C

Il modulo viscoso a tempo infinito, in considerazione del valore di h0, della resistenza del calcestruzzo e della U.R., può cautelativamente essere assunto pari a Φ (t = ∞) = 1.6. Di conseguenza la variazione termica negativa equivalente applicata sarà:

variazione termica equivalente ΔTeq = -11.73 °C

7.3. COMBINAZIONI DI CARICO ADOTTATE

I carichi caratteristici sopra elencati (CDC), al fine di ottenere le sollecitazioni di progetto per effettuare le successive verifiche, sono opportunamente combinati fra loro.

7.3.1. Combinazioni per lo STATO LIMITE ULTIMO

$\gamma G1$ G1 + $\gamma\varepsilon 2$ R + $\gamma Q1$Qk1 + $\gamma\varepsilon 3$ $\psi 0$ $\varepsilon 3$ T (carico da traffico veicolare Qk1 principale)

$\gamma G1$ G1 + $\gamma\varepsilon 2$ R + $\gamma\varepsilon 3$ T + $\gamma Q1$ $\psi 01$ Qk1 (azioni termiche T principali)

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Termica Uniforme	Termica farfalla +	Ritiro
SLU	1	1.35	1.35	0	0	1	1	1.35	0	0	0	0	0	0	0	0	0	0.72	0.72	1.2
	2	1.35	1.35	0	0	1	1	0	0	0	0	0	0	0	0	0	0	0.72	0.72	1.2
	3	1.35	1.35	0	0	1	1	1.01	0	0	0	0	0	0	0	0	0	1.2	1.2	1.2
	4	1.35	1.35	0	0	1	1	0	0	0	0	0	0	0	0	0	0	1.2	1.2	1.2
	5	1.35	1.35	1.35	0	0	1	1.01	0	0	0	0	0	0	1.35	0	0	-0.72	-0.72	0
	6	1.35	1.35	1.35	0	0	1	0	0	0	0	0	1.01	0	1.35	0	0	-0.72	-0.72	0
	7	1.35	1.35	1.35	0	0	1	0	0	0	1.01	0	0	0	1.35	0	0	-0.72	-0.72	0
	8	1.35	1.35	1.35	0	0	1	1.01	0	0	0	0	0	0	0	0	0	-1.2	-1.2	0
	9	1.35	1.35	1.35	0	0	1	0	0	0	0	0	1.01	0	0	0	0	-1.2	-1.2	0
	10	1.35	1.35	1.35	0	0	1	0	0	0	1.01	0	0	0	0	0	0	-1.2	-1.2	0
	11	1.35	1.35	0	0	1	1	1.35	0	0	0	0	0	0	0	0	0	-0.72	0.72	0
	12	1.35	1.35	0	0	1	1	0	0	0	0	0	0	0	0	0	0	-0.72	0.72	0
	13	1.35	1.35	0	0	1	1	1.01	0	0	0	0	0	0	0	0	0	-1.2	1.2	0
	14	1.35	1.35	0	0	1	1	0	0	0	0	0	0	0	0	0	0	-1.2	1.2	0
	15	1.35	1.35	1.35	0	0	1	1.01	0	0	0	0	0	0	1.35	0	0	0.72	-0.72	1.2
	16	1.35	1.35	1.35	0	0	1	0	0	0	0	0	1.01	0	1.35	0	0	0.72	-0.72	1.2
	17	1.35	1.35	1.35	0	0	1	0	0	0	1.01	0	0	0	1.35	0	0	0.72	-0.72	1.2
	18	1.35	1.35	1.35	0	0	1	1.01	0	0	0	0	0	0	0	0	0	1.2	-1.2	1.2
	19	1.35	1.35	1.35	0	0	1	0	0	0	0	0	1.01	0	0	0	0	1.2	-1.2	1.2
	20	1.35	1.35	1.35	0	0	1	0	0	0	1.01	0	0	0	0	0	0	1.2	-1.2	1.2
	21	1.35	1.35	1.35	0	0	1	0	0	1.01	0	0	0	0	1.35	0	0	0.72	-0.72	1.2
	22	1.35	1.35	1.35	0	0	1	0	0	1.01	0	0	0	0	0	0	0	1.2	-1.2	1.2
	23	1	1	1.35	0	0	1	0	0	0	1.01	0	0	0	1.35	0	0	0.72	0.72	1.2
	24	1	1	1.35	0	0	1	0	0	0	1.01	0	0	0	0	0	0	1.2	1.2	1.2
	25	1.35	1.35	1.35	0	0	1	0	1.01	0	0	0	0	0	1.35	0	0	0	0	0
	26	1.35	1.35	1.35	0	0	1	0	0	0	0	0	1.01	0	1.35	0	0	0	0	0
	27	1.35	1.35	1.35	0	0	1	0	0	1.35	0	0	0	0	0	0	0	0.72	-0.72	1.2
	28	1.35	1.35	1.35	0	0	1	0	0	0	0	0	1.01	0	0	0	0	0.72	-0.72	1.2
	29	1.35	1.35	1.35	0	0	1	0	0	0	1.01	0	0	0	1.35	0	0	0.72	0.72	1.2
	30	1	1	1.35	1.35	0	0	1.01	0	0	0	0	0	0	1.35	0	0	-0.72	-0.72	0
	31	1	1	1.35	1.35	0	0	0	0	0	0	0	1.01	1.01	1.35	0	0	-0.72	-0.72	0
	32	1	1	1.35	1.35	0	0	0	0	0	1.01	1.01	0	0	1.35	0	0	-0.72	-0.72	0

	33	1.35	1.35	1.35	0	0	1	0	0	0	1.01	0	0	0	1.35	0	0	-0.72	-0.72	1.2

7.3.2. Combinazioni per gli stati limite di esercizio: combinazione rara

G1 + R + Qk1 + ψ0ε3 T (carico da traffico veicolare Qk1 principale)

G1 + R + T + ψ01 Qk1 (azioni termiche T principali)

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Termica Uniforme	Termica farfalla +	Ritiro
SLE RAR	46	1	1	0	0	1	1	1	0	0	0	0	0	0	0	0	0	0.6	0.6	1
	47	1	1	0	0	1	1	0	0	0	0	0	0	0	0	0	0	0.6	0.6	1
	48	1	1	0	0	1	1	0.75	0	0	0	0	0	0	0	0	0	1	1	1
	49	1	1	0	0	1	1	0	0	0	0	0	0	0	0	0	0	1	1	1
	50	1	1	1	0	0	1	0.75	0	0	0	0	0	0	1	0	0	-0.6	-0.6	0
	51	1	1	1	0	0	1	0	0	0	0	0	0.75	0	1	0	0	-0.6	-0.6	0
	52	1	1	1	0	0	1	0	0	0	0.75	0	0	0	1	0	0	-0.6	-0.6	0
	53	1	1	1	0	0	1	0.75	0	0	0	0	0	0	0	0	0	-1	-1	0
	54	1	1	1	0	0	1	0	0	0	0	0	0.75	0	0	0	0	-1	-1	0
	55	1	1	1	0	0	1	0	0	0	0.75	0	0	0	0	0	0	-1	-1	0
	56	1	1	0	0	1	1	1	0	0	0	0	0	0	0	0	0	-0.6	0.6	1
	57	1	1	0	0	1	1	0	0	0	0	0	0	0	0	0	0	-0.6	0.6	1
	58	1	1	0	0	1	1	0.75	0	0	0	0	0	0	0	0	0	-1	1	1
	59	1	1	0	0	1	1	0	0	0	0	0	0	0	0	0	0	-1	1	1
	60	1	1	1	0	0	1	0.75	0	0	0	0	0	0	1	0	0	0.6	-0.6	1
	61	1	1	1	0	0	1	0	0	0	0	0	0.75	0	1	0	0	0.6	-0.6	1
	62	1	1	1	0	0	1	0	0	0	0.75	0	0	0	1	0	0	0.6	-0.6	1
	63	1	1	1	0	0	1	0.75	0	0	0	0	0	0	0	0	0	1	-1	1
	64	1	1	1	0	0	1	0	0	0	0	0	0.75	0	0	0	0	1	-1	1
	65	1	1	1	0	0	1	0	0	0	0.75	0	0	0	0	0	0	1	-1	1
	66	1	1	1	0	0	1	0	0	0.75	0	0	0	0	1	0	0	0.6	-0.6	1
	67	1	1	1	0	0	1	0	0	0.75	0	0	0	0	0	0	0	1	-1	1

	68	1	1	1	0	0	1	0	0	0	0.75	0	0	0	1	0	0	0.6	0.6	1
	69	1	1	1	0	0	1	0	0	0	0.75	0	0	0	0	0	0	1	1	1

7.3.3. Combinazioni per gli stati limite di esercizio: combinazione frequente

G1 + R + ψ11 Qk1 + ψ2ε3 T (carico da traffico veicolare Qk1 principale)

		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Spinta idrodinamica	Termica Uniforme	Termica farfalla +	Ritiro
SLE FR	34	1	1	0	0	1	1	0.75	0	0	0	0	0	0	0	0	0	0.6	0.6	1	1
	35	1	1	0	0	1	1	0	0	0	0	0	0.75	0	0	0	0	0.6	0.6	1	1
	36	1	1	1	0	0	1	0.75	0	0	0	0	0	0	0	0	0	-0.6	-0.6	0	1
	37	1	1	1	0	0	1	0	0	0	0	0	0.75	0	0	0	0	-0.6	-0.6	0	1
	38	1	1	1	0	0	1	0	0	0	0.75	0	0	0	0	0	0	-0.6	-0.6	0	1
	39	1	1	0	0	1	1	0.75	0	0	0	0	0	0	0	0	0	-0.6	0.6	0	1
	40	1	1	0	0	1	1	0	0	0	0	0	0	0	0	0	0	-0.6	0.6	0	1
	41	1	1	1	0	0	1	0.75	0	0	0	0	0	0	0	0	0	0.6	-0.6	1	1
	42	1	1	1	0	0	1	0	0	0	0	0	0.75	0	0	0	0	0.6	-0.6	1	1
	43	1	1	1	0	0	1	0	0	0	0.75	0	0	0	0	0	0	0.6	-0.6	1	1
	44	1	1	1	0	0	1	0	0	0.75	0.75	0	0	0	0	0	0	0.6	-0.6	1	1
	45	1	1	1	0	0	1	0	0	0	0.75	0	0	0	0	0	0	0.6	0.6	1	1

7.3.4. Combinazioni per gli stati limite di esercizio: combinazione quasi permanente

G1 + R + ψ21 Qk1 + ψ2ε3 T

		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Spinta idrodinamica	Termica Uniforme	Termica farfalla +	Ritiro
SLE QP	70	1	1	0	0	1	1	0	0	0	0	0	0	0	0	0	0	0.5	0.5	1	1
	71	1	1	1	0	0	1	0	0	0	0	0	0	0	0	0	0	-0.5	-0.5	0	1
	72	1	1	0	0	1	1	0	0	0	0	0	0	0	0	0	0	-0.5	0.5	0	1

	73	1	1	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0.5	-0.5	1	1
	74	1	1	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0.5	0.5	1	1

7.3.5. Combinazioni per lo stato limite ultimo di Salvaguardia della vita

Si considera il sisma agente nella direzione trasversale dello scatolare (gli effetti del sisma agente nella direzione longitudinale del manufatto sono poco rilevanti), associato al sisma in direzione verticale (considerando in alternativa entrambi i versi d'azione). La non contemporaneità della massima azione verticale e orizzontale viene tenuta in conto, come prescritto dalle NTC 2008 (Par. 7.3.5), considerando i 4 seguenti scenari:

E1 = 1.00 EH + 0.30 EV + (sisma orizzontale al 100%, sisma verticale verso l'alto al 30%)

E2 = 1.00 EH + 0.30 EV - (sisma orizzontale al 100%, sisma verticale verso il basso al 30%)

E3 = 0.30 EH + 1.00 EV + (sisma orizzontale al 30%, sisma verticale verso l'alto al 100%)

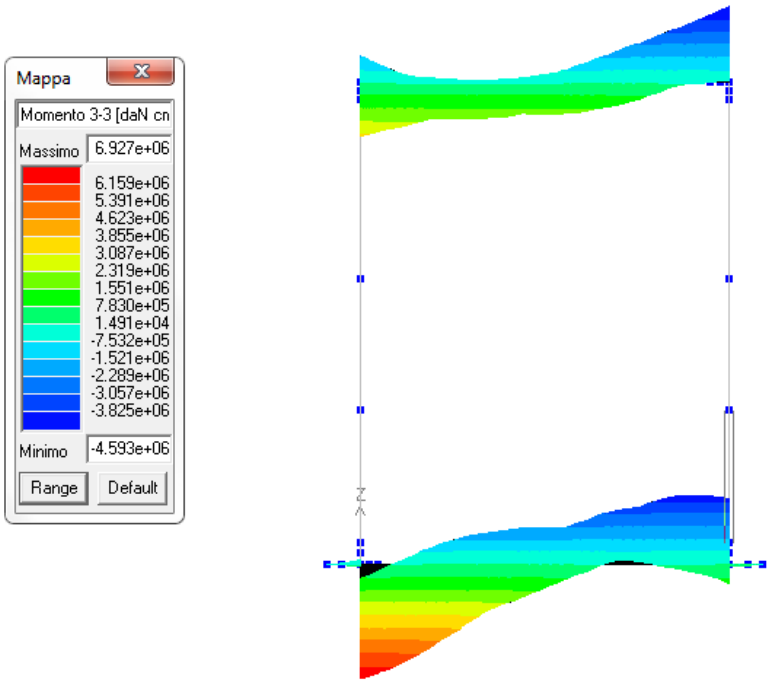
E4 = 0.30 EH + 1.00 EV - (sisma orizzontale al 30%, sisma verticale verso il basso al 100%)

G1 + E + $\psi 21$ Qk1 + $\psi 2\varepsilon 3$ T

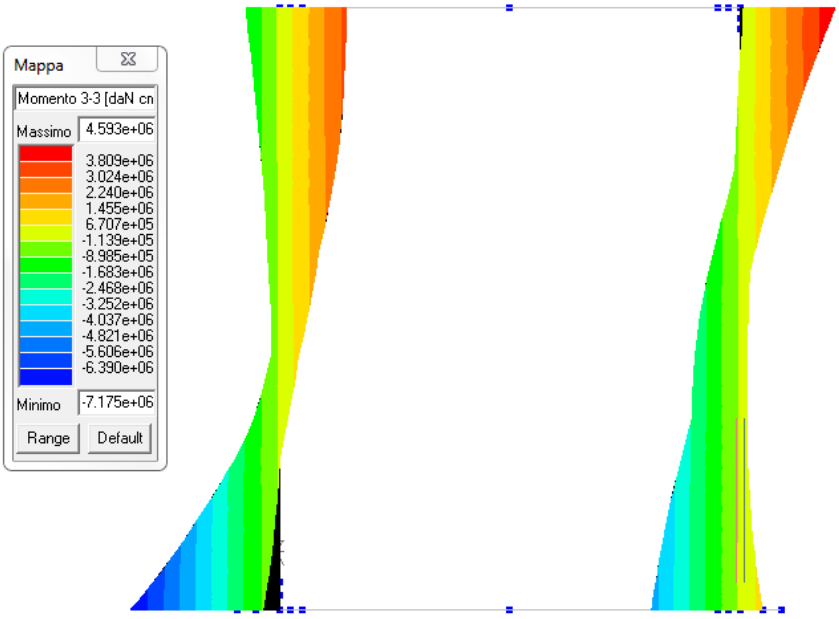
		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Termica Uniforme	Termica farfalla +	Ritiro
SISMA	75	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0.3	1	0.5	0.5	1
	76	1	1	1	1	0	0	0	0	0	0	0	0	0	0	1	0.3	-0.5	-0.5	0
	77	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0.3	1	-0.5	0.5	0
	78	1	1	1	1	0	0	0	0	0	0	0	0	0	0	1	0.3	0.5	-0.5	1
	79	1	1	1	1	0	0	0	0	0	0	0	0	0	0	1	-0.3	0.5	0.5	1

7.4. DIAGRAMMI DELLE CARATTERISTICHE DELLA SOLLECITAZIONE

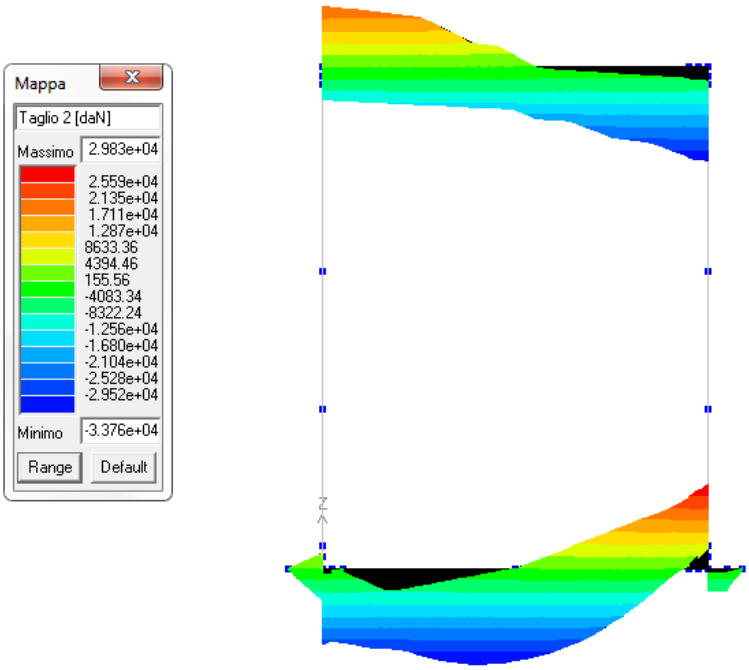
7.4.1. InviluppoSLU/SLV momento flettente soletta superiore e soletta di fondazione



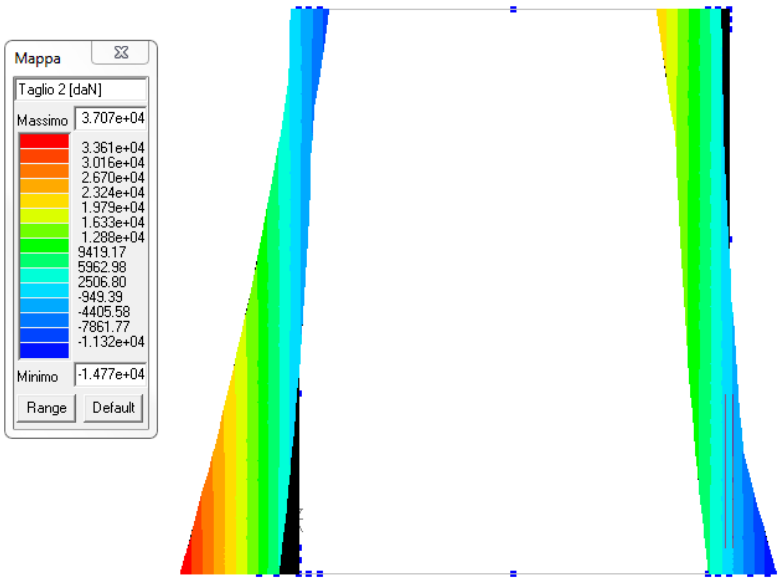
7.4.2. InviluppoSLU/SLV momento flettente piedritti



7.4.3. Inviluppo taglio SLU/SLV soletta superiore e soletta di fondazione



7.4.4. Inviluppo taglio SLU/SLV piedritti



7.5. VERIFICHE DI RESISTENZA E A FESSURAZIONE

I calcoli di verifica di resistenza sono effettuati con il metodo degli Stati Limite, applicando il combinato D. M.14.01.2008 con l'UNI EN 1992 (Eurocodice 2).

Le verifiche a fessurazione sono state condotte considerando:

Verifica di formazione delle fessure: la verifica si esegue per la sezione interamente reagente e per le sollecitazioni di esercizio si determina la massima trazione nel calcestruzzo σ_{ct}, confrontandola con la resistenza caratteristica a trazione per flessione f_{cfk}: se risulta $\sigma_{ct}<f_{cfk}$ la verifica è soddisfatta, altrimenti si procede alla verifica di apertura delle fessure.

Verifica di apertura delle fessure: l'apertura convenzionale delle fessure è calcolata con le modalità indicate nell'EC2, come richiesto dal D. M. Min. II. TT. del 14 gennaio 2008, e valutata con le sollecitazioni relative alle Combinazioni FR o QP della normativa vigente sui ponti stradali". La massima apertura ammissibile risulta rispettivamente per le strutture in ambiente ordinario ed armature poco sensibili:

1) combinazione di carico Frequente:

$w_k \leq w_3 = 0.40mm$

2) combinazione di carico quasi permanente:

$w_k \leq w_2 = 0.30mm$

Verifica delle tensioni di esercizio: si eseguono per la condizione di carico Quasi Permanente e Rara, verificando rispettivamente che le tensioni di lavoro siano inferiori ai seguenti limiti:

1) per la condizione QP si verifica che le massime tensioni presenti nel calcestruzzo siano inferiori a $\sigma_c < 0.45\ f_{ck}$;

2) per la condizione rara si verifica che le massime tensioni presenti nel calcestruzzo siano inferiori a $\sigma_c < 0.60\ f_{ck}$, mentre quelle dell'acciaio $\sigma_s < 0.80\ f_{yk}$.

7.5.1. Verifiche di resistenza delle solette

La verifica a pressoflessione e taglio delle solette viene eseguita automaticamente dal programma di calcolo. Nella sezione di calcolo "assegnazione dati di progetto", il programma consente mediante una finestra d'inserimento dati, di assegnare l'armatura longitudinale ad ogni singola soletta, successivamente esegue le verifiche per ogni combinazione di carico; il quantitativo di armatura trasversale (cmq/m) viene calcolato automaticamente dal programma in funzione del diametro delle barre e delle tipologia di staffe (2br., 4br., ecc.) inseriti nella finestra d'inserimento dati.

ARMATURE:

Si dispongono le armature trasversali di seguito elencate:

SOLETTA SUPERIORE:

armatura superiore	ϕ 22/10
armatura inferiore	ϕ 22/10

PARETI:

armatura interna per 2m fino a estradosso soletta superiore	ϕ 20/10
armatura interna per 2m fino a estradosso soletta superiore	ϕ 20/10
armatura esterna per 2m nella mezzeria delle pareti	ϕ20/20
armatura interna per 2m nella mezzeria delle pareti	ϕ 20/20
armatura esterna per 2m da intradosso soletta inferiore	ϕ 24/10
armatura interna per 2m da intradosso soletta inferiore	ϕ 24/10

SOLETTA DI FONDAZIONE:

armatura superiore	ϕ 20/10
armatura inferiore	ϕ 20/10

Si precisa che come da diagramma armature sotto riportato,all'incastro nella soletta di copertura in fase di esecutivo,andrà aggiunto uno spezzone di barra d'armatura (ora trascurato ai fini dell'incidenza).

Come armatura di ripartizione longitudinale si dispongono ϕ 14/20 sulla soletta di fondazione e sulle pareti, ad eccezione della soletta superiore dove si dispongono ϕ 14/15.

L'armatura disposta nelle solette viene riportata mediante diagrammi.

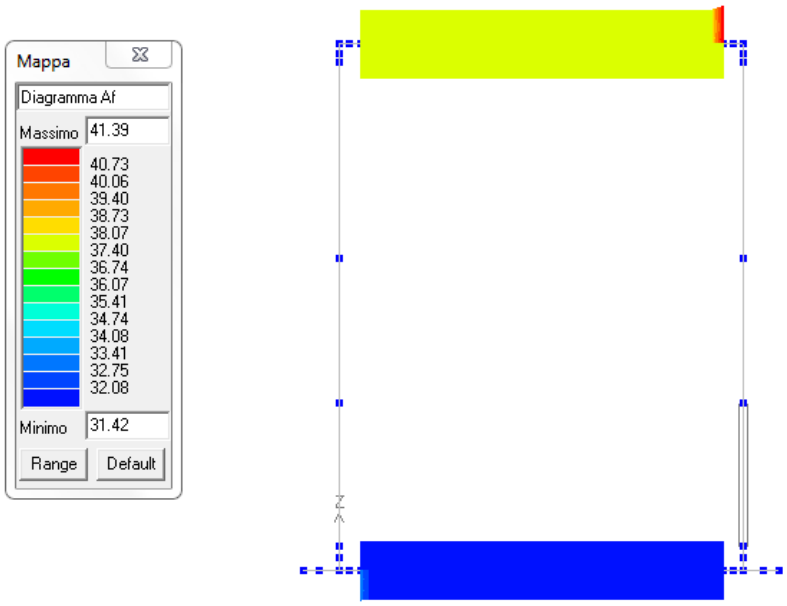
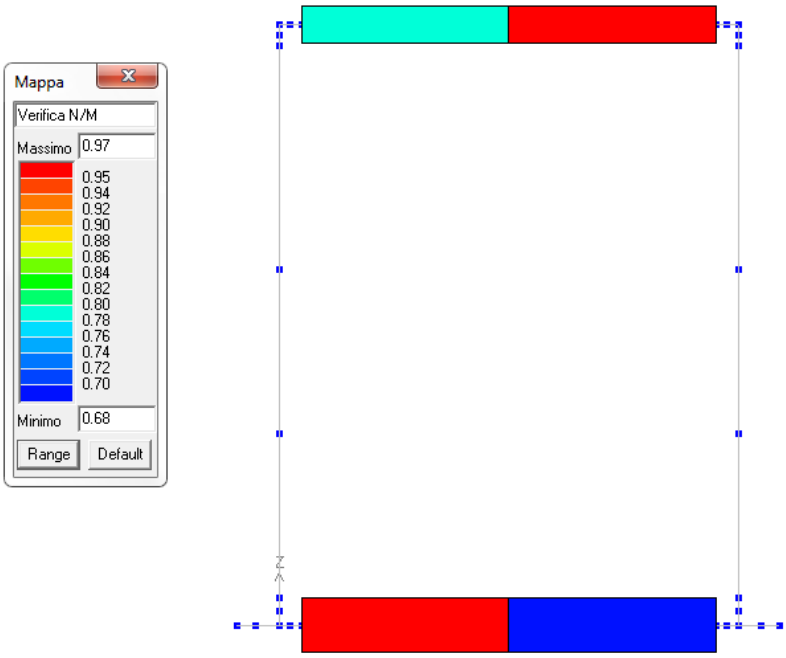


FIGURA 7.5-1 – DIAGRAMMA DEL QUANTATIVO DI ARMATURA LONGITUDINALE NELLE SOLETTE (CMQ)

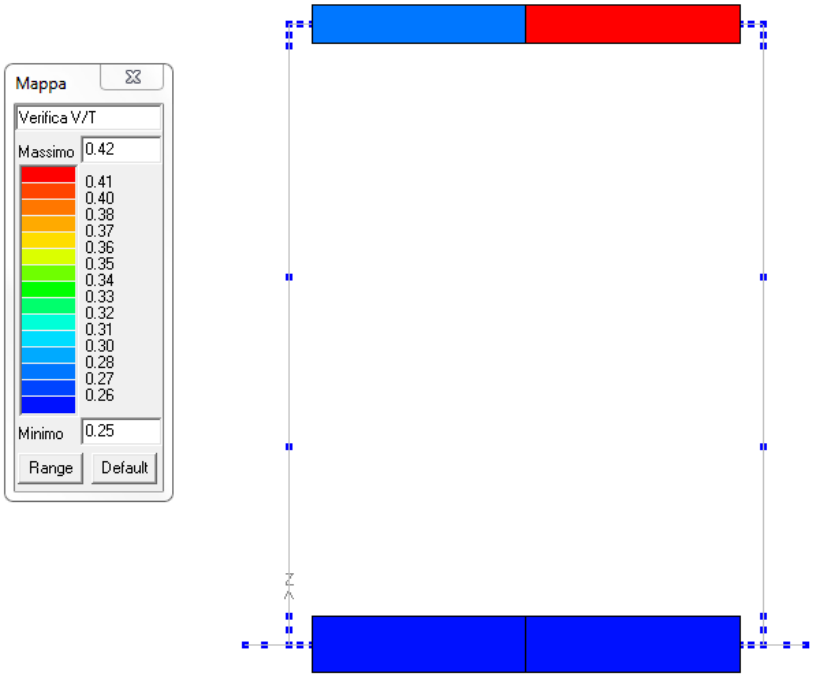
Nel seguito si riportano gli elementi grafici di visualizzazione delle verifiche eseguite secondo quanto previsto dal D.M. 14/01/2008 al paragrafo 4.1.2.1, e nel dettaglio:

- Verifica N/M Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Mrd/Med con sollecitazioni ultime proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Sd = sollecitazione di progetto, Su = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.2.4).

- Verifica (V/T) Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Vrd/Ved con sollecitazioni taglianti e torcenti proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Sd = sollecitazione di progetto, Su = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.3.2/4.1.2.1.4).



Verifica N/M Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Mrd/*Med* con sollecitazioni ultime proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Mrd = sollecitazione di progetto, Med = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.2.4).



Verifica (V/T) Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Vrd/Ved con sollecitazioni taglianti e torcenti proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Vrd = sollecitazione di progetto, Ved = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.3.2).

7.5.2. Verifiche di resistenza dei piedritti

La verifica a pressoflessione e taglio dei piedritti viene eseguita automaticamente dal programma di calcolo. Nella sezione di calcolo "assegnazione dati di progetto", il programma consente mediante una finestra d'inserimento dati, di assegnare l'armatura longitudinale e trasversale ad ogni singolo piedritto, successivamente esegue le verifiche per ogni combinazione di carico.

L'armatura disposta nei piedritti viene riportata mediante diagrammi.

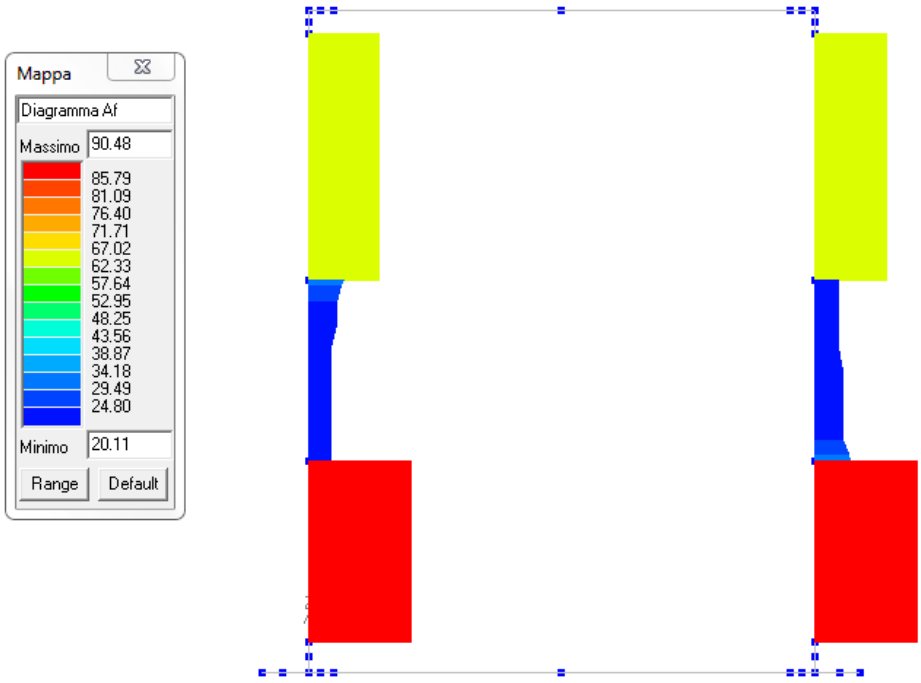


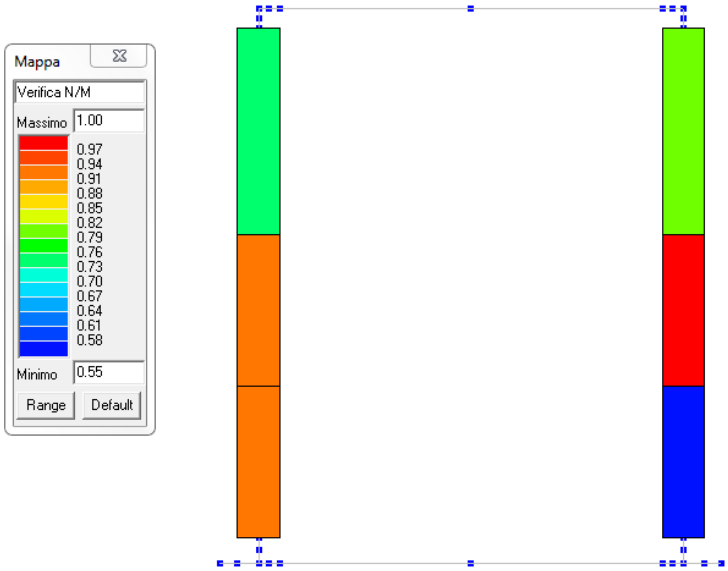
FIGURA 7.5-2 – DIAGRAMMA DEL QUANTATIVO DI ARMATURA TRASVERSALE NEI PIEDRITTI (CMQ/M)

Nel seguito si riportano gli elementi grafici di visualizzazione delle verifiche eseguite secondo quanto previsto dal D.M. 14/01/2008 al paragrafo 4.1.2.1, e nel dettaglio:

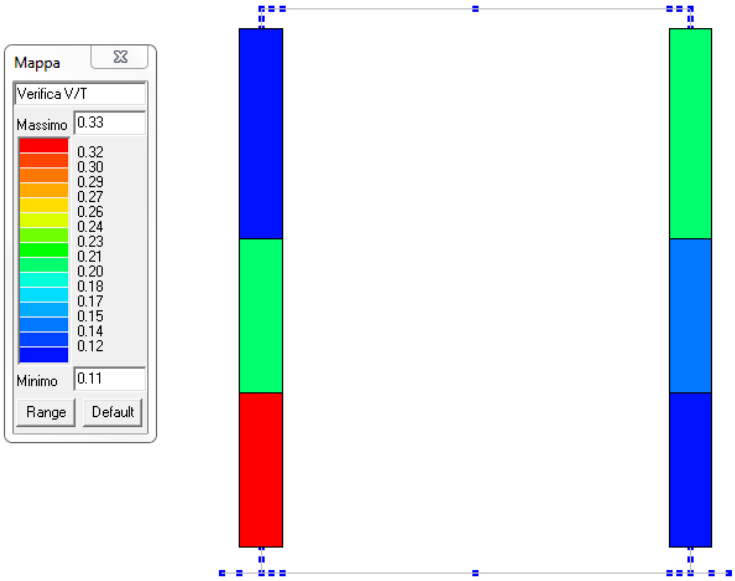
- Verifica N/M Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Mrd/Med con sollecitazioni ultime proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Mrd = sollecitazione di progetto, Med = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.2.4).

- Verifica (V/T) Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Vrd/Ved con sollecitazioni taglianti e torcenti proporzionali; il valore del rapporto deve essere minore o

uguale a 1 per verifica positiva (Vrd = sollecitazione di progetto, Ved = sollecitazione ultima) D.M. 14/01/2008 par. 4.1.2.1.3.2/4.1.2.1.4).



Verifica N/M Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Mrd/*Med* con sollecitazioni ultime proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Mrd = sollecitazione di progetto, Med = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.2.4).



Verifica (V/T) Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Vrd/Ved con sollecitazioni taglianti e torcenti proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Vrd = sollecitazione di progetto, Ved = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.3.2).

7.5.3. Verifica stato limite di esercizio per c.c. rare

La massima tensione di compressione del calcestruzzo deve rispettare la limitazione seguente: $\sigma_c<0.60f_{ck}$.

La massima tensione dell'acciaio deve rispettare la limitazione seguente: $\sigma_s<0.80f_{yk}$.

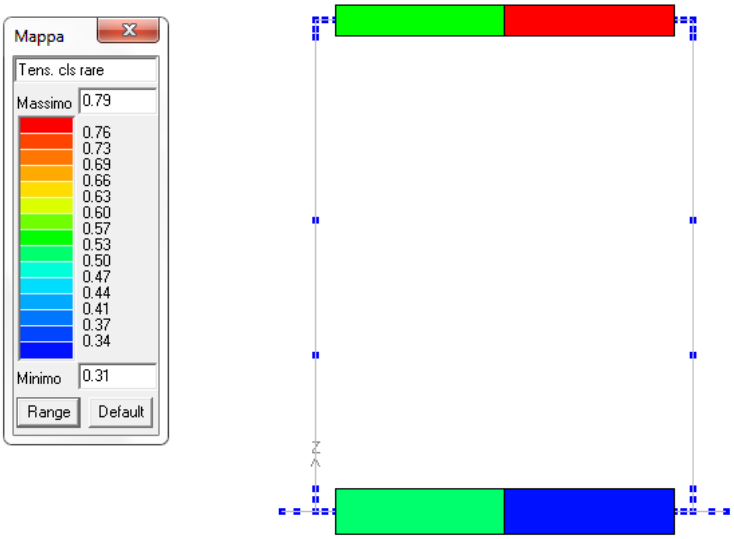


FIGURA 7.5-3 VERIFICA DELLA TENSIONE NEL CALCESTRUZZO (SLE RARE) – SOLETTA INFERIORE E SUPERIORE

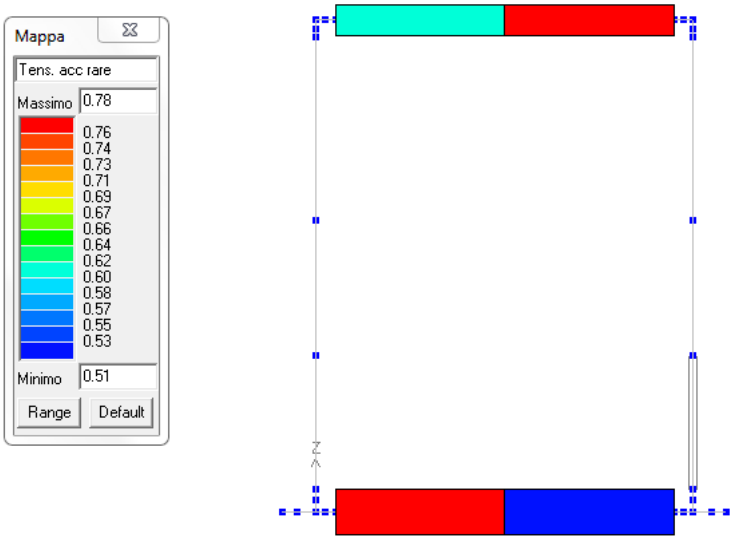


FIGURA 7.5-4 VERIFICA DELLA TENSIONE NELL'ACCIAIO (SLE RARE) – SOLETTA INFERIORE E SUPERIORE

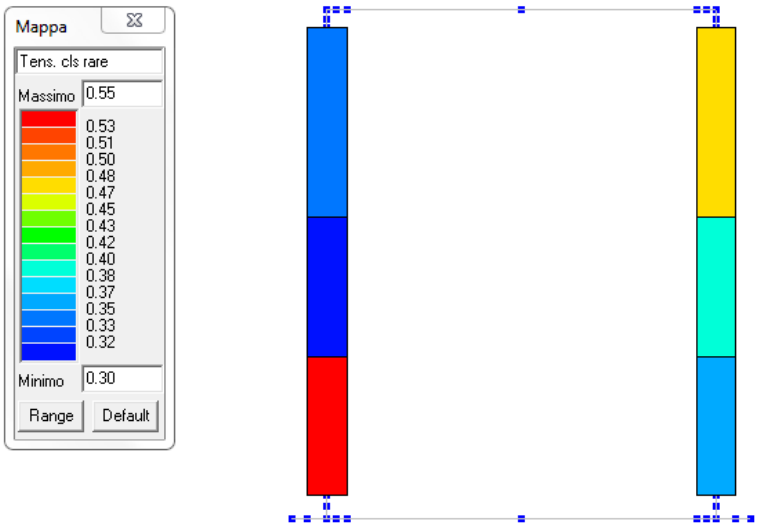


FIGURA 7.5-5 VERIFICA DELLA TENSIONE NEL CALCESTRUZZO (SLE RARE) – PIEDRITTI

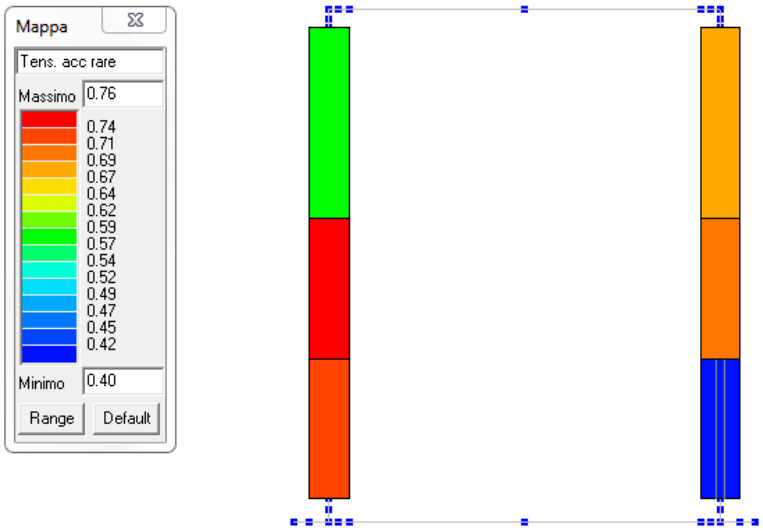


FIGURA 7.5-6 VERIFICA DELLA TENSIONE NELL'ACCIAIO (SLE RARE) – PIEDRITTI

7.5.4. Verifica stato limite di esercizio per c.c. frequenti

Il valore di calcolo di apertura delle fessure non deve superare i valori nominali (w1,w2,w3) secondo quanto riportato nella Tab. 4.1.IV del vigente D.M. 14/01/2008.

Nel caso in esame si hanno :

Condizioni ambientali	Combinazione delle azioni	Armature poco sensibili	
		Stato Limite	wd
Ordinarie	Frequente	Ap. fessure	< 0.4mm
	Quasi permanente	Ap. fessure	< 0.3mm

Di seguito si riportano le verifiche condotte agli Stati Limite di Esercizio.

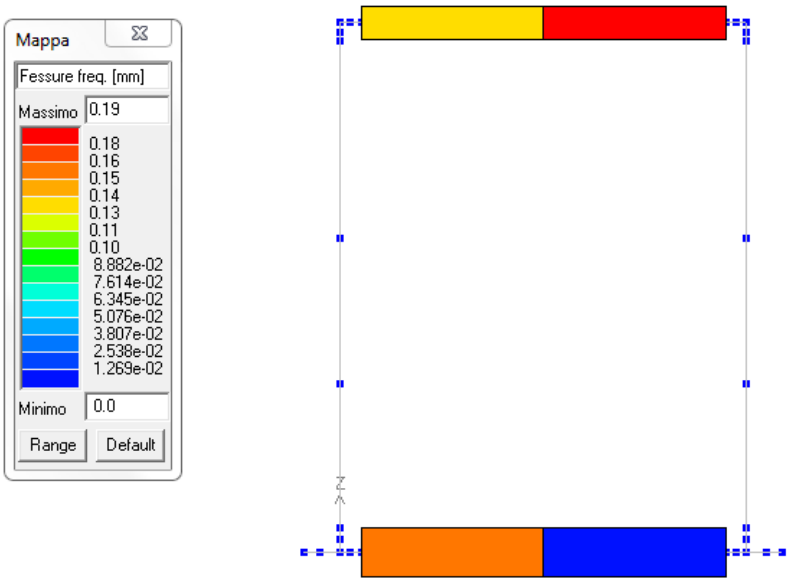


FIGURA 7.5-7 VERIFICA A FESSURAZIONE (SLE FREQUENTI) – SOLETTA INFERIORE E SUPERIORE

7.5.5. Verifica stato limite di esercizio per c.c. quasi permanenti

La massima tensione di compressione del calcestruzzo deve rispettare la limitazione seguente: $\sigma_c<0.45f_{ck}$.

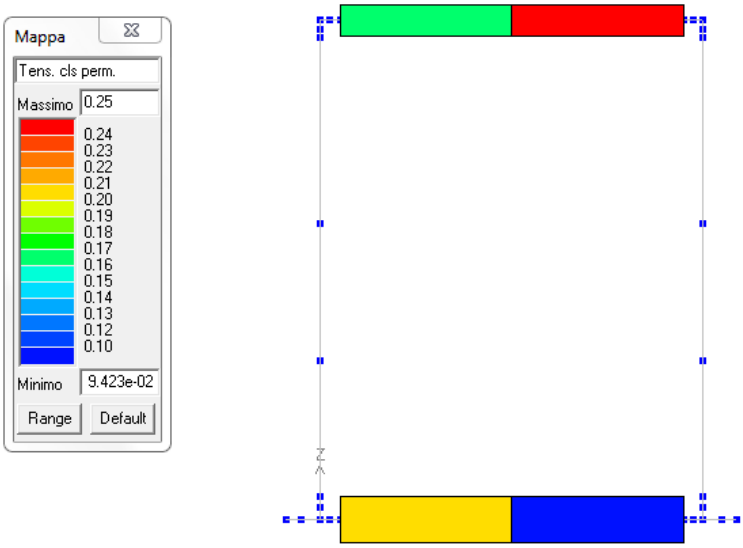


FIGURA 7.5-8 VERIFICA DELLA TENSIONE NEL CALCESTRUZZO (SLE QUASI PERMANENTI) – SOLETTA INFERIORE E SUPERIORE

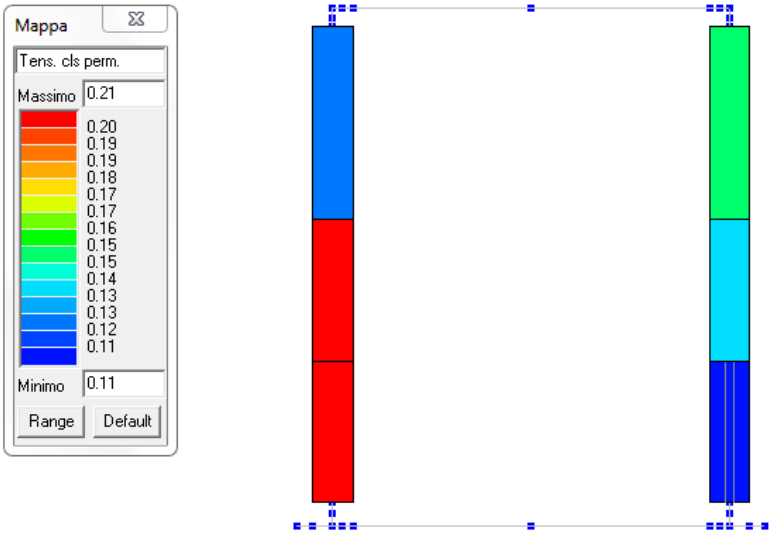


FIGURA 7.5-9 VERIFICA DELLA TENSIONE NEL CALCESTRUZZO (SLE QUASI PERMANENTI) – PIEDRITTI

Il valore di calcolo di apertura delle fessure non deve superare i valori nominali (w1,w2,w3) secondo quanto riportato nella Tab. 4.1.IV del vigente D.M. 14/01/2008.

Nel caso in esame si hanno :

Condizioni ambientali	Combinazione delle azioni	Armature poco sensibili	
		Stato Limite	wd
Ordinarie	Frequente	Ap. fessure	< 0.4mm
	Quasi permanente	Ap. fessure	< 0.3mm

Di seguito si riportano le verifiche condotte agli Stati Limite di Esercizio.

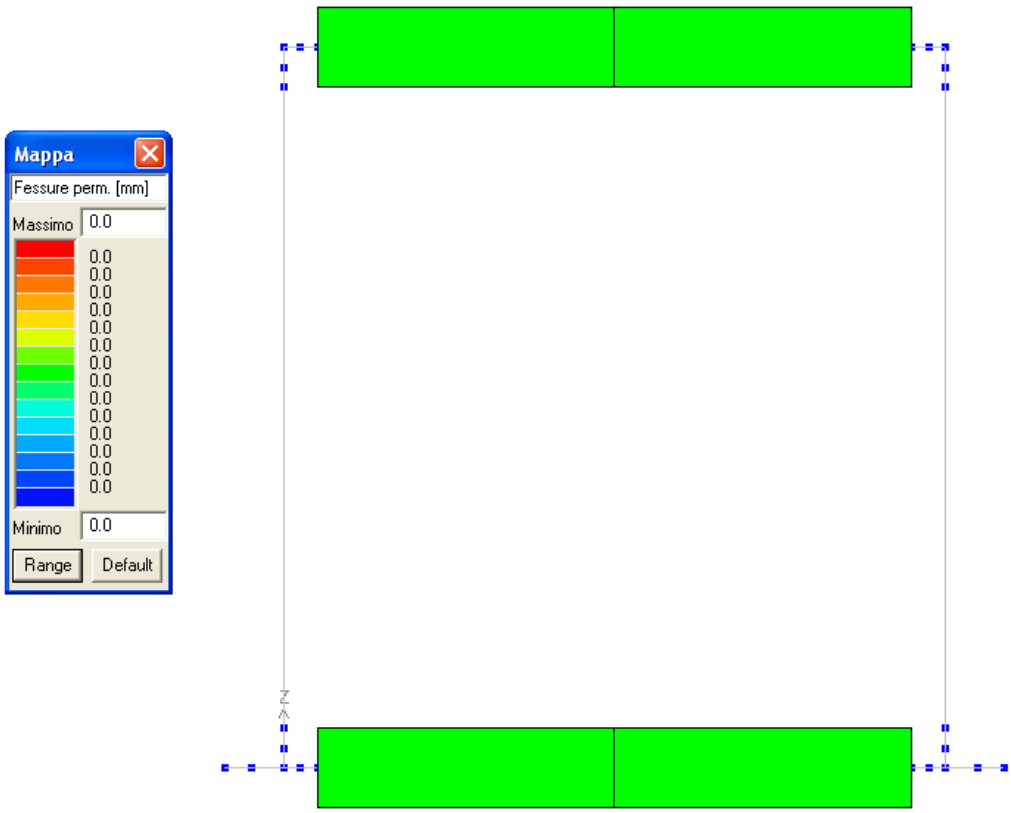


FIGURA 7.5-10 VERIFICA A FESSURAZIONE (SLE QUASI-PERMANENTI) – SOLETTA INFERIORE E SUPERIORE

7.5.6. Armatura di ripartizione dello scatolare

L'armatura di ripartizione nelle solette e nelle pareti dello scatolare (direzione y) viene posta in misura non inferiore al 20% dell'armatura principale (direzione x) (EC2 § 9.3).

L'armatura di ripartizione viene disposta non uniformemente, ma leggermente maggiorata nei punti in cui è maggiore anche l'armatura principale, punti in cui, peraltro, risultano maggiori le sollecitazioni trasversali alla luce di calcolo dello scatolare. Ad esempio, l'armatura di ripartizione viene posta in quantità maggiore all'intradosso della sezione di mezzeria della soletta superiore che è il punto dove si hanno i maggiori momenti secondari dovuti ai carichi mobili stradali ed alla sovrastruttura stradale (gli unici carichi non uniformemente distribuiti sulla larghezza dello scatolare e quindi gli unici carichi che danno azioni flessionali trasversali). Essendo tali carichi ubicati al centro dello scatolare, essi generano azioni flessionali che tendono le fibre poste all'intradosso, dove viene appunto incrementata l'armatura di ripartizione.

Semplici valutazioni consentono di provare che l'armatura di ripartizione pari al 20% della principale è sicuramente sufficiente per assorbire le azioni flessionali trasversali secondarie, ovvero nella direzione ortogonale a quella di massima inflessione della soletta.

Come già osservato la massima azione flessionale secondaria si ha nella soletta superiore, perché solo qui sono applicate azioni non uniformemente distribuite su un intero elemento strutturale; tali azioni localizzate sono i carichi mobili stradali ed il peso della sovrastruttura.

Schematizzando, la soletta superiore come una lastra infinitamente lunga in direzione y, appoggiata sui bordi distanti l_x =5.50m, si valuta con l'ausilio di risultati tabellati (formule di BITTNER, vedi Allegato C) il massimo momento flettente in direzione y sotto l'effetto di una fascia caricata di larghezza t_y=11.25 m (larghezza caricata) per i carichi permanenti e variabili, e di lunghezza $t_{x\text{-}var}$ = 2.49m (lunghezza di diffusione longitudinale dei carichi da traffico) per i carichi variabili, mentre per i carichi permanenti $t_{x\text{-}perm}$ = 5.00m.

Contributo dei carichi permanenti:

p_{perm}= 22.00*0.25 = 5.5 kN/m^2

$p_{perm\text{-}SLU}$= (22.00*0.25) *1.35= 7.425 kN/m^2

P = p* t_y*l_x = 5.50 *5.00*11.25 = 309.38 kN

P_{SLU} = p_{SLU}* t_y*l_x = 417.66 kN

$l_y = \infty$ t_y/l_x = 2.25 $\Rightarrow$1 t_y/l_x = 1.00 α_{ym} = 0.0210

Il massimo momento trasversale risulta:

$M_{ym;SLE} = \alpha_{ym} * P$ = 6.50 kNm/m

$M_{ym,SLU} = \alpha_{ym} * P_{SLU} = 8.77$ kNm/m

Contributo dei carichi variabili:

$p_{var} = 85.68$ kN/m^2

$p_{var\text{-}SLU} = 85.68 * 1.35 = 115.67$ kN/m^2

$P = p^* t_y * l_x = 85.68 * 11.25 * 5.00 = 4819.50$ kN

$P_{SLU} = p_{SLU} * t_y * l_x = 6506.44$ kN

$l_y = \infty \quad t_x/l_x = 0.498 \Rightarrow 1 \qquad t_x/l_x = 0.50 \qquad \alpha_{ym} = 0.0299$

Il massimo momento trasversale risulta:

$M_{ym;SLE} = \alpha_{ym} * P = 144.10$ kNm/m

$M_{ym,SLU} = \alpha_{ym} * P_{SLU} = 194.54$ kNm/m

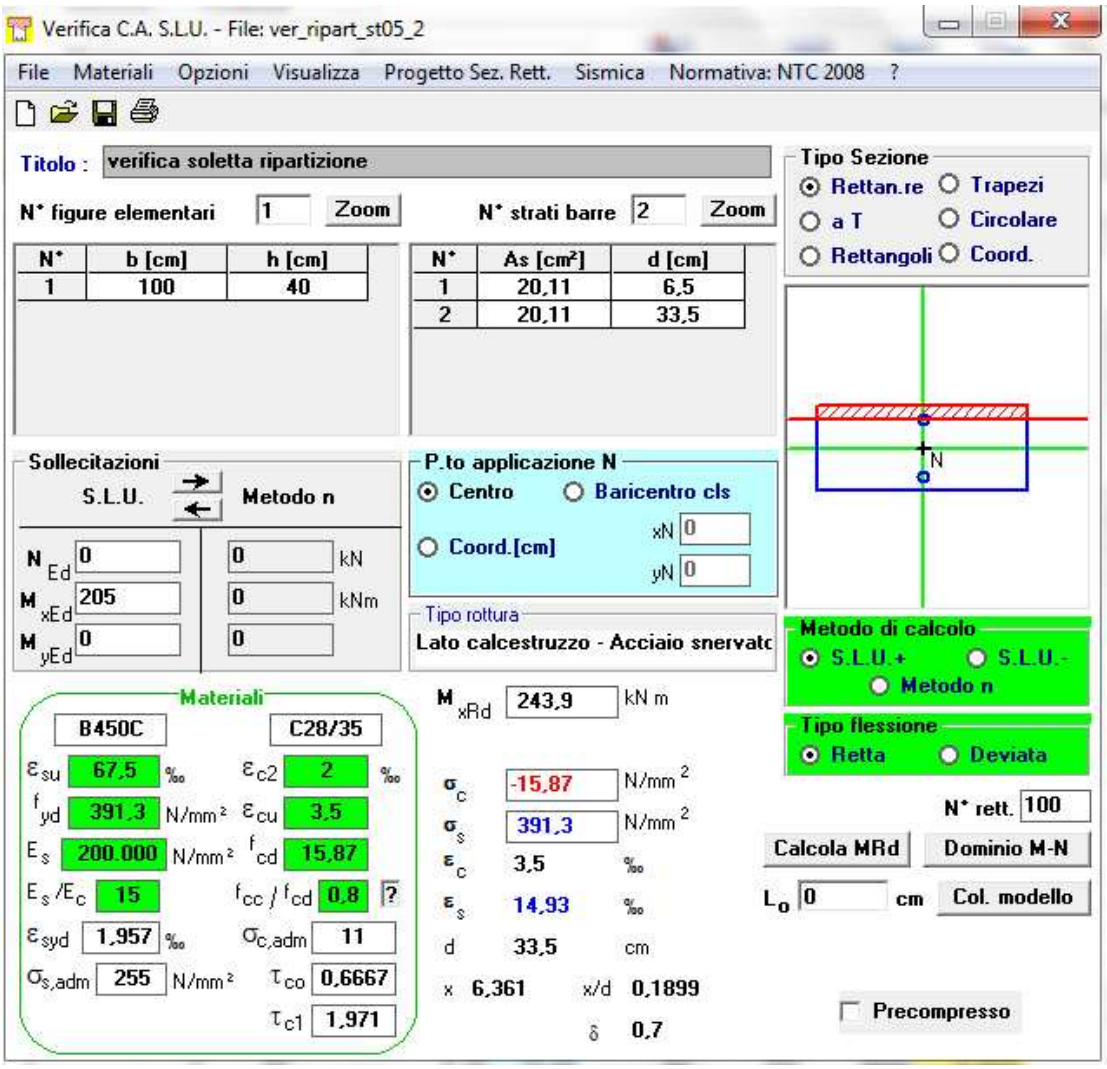
Sollecitazioni totali:

$M_{ym;SLE} = 150.60$ kNm/m

$M_{ym,SLU} = 203.31$ kNm/m

Nella soletta superiore dello scatolare si dispone un'armatura di ripartizione longitudinale pari a ϕ 14/15.

7.5.6.1 Verifiche allo stato limite ultimo per flessione



8. MURI AD "U"

Si riporta di seguito la verifica relativa al primo metro di muro ad "U" vicino allo scatolare; si ritiene che tale sezione sia la più sfavorevole in quanto abbiamo le pareti più alte.

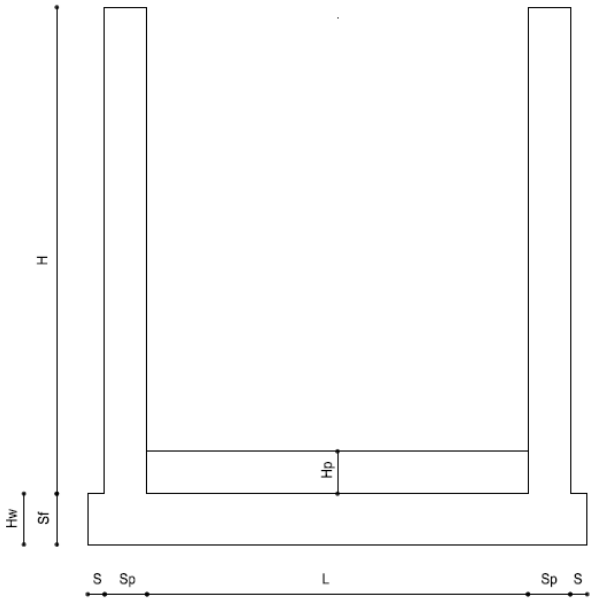


Figura 8-1 – Sezione tipologica

Dimensioni geometriche (sezione in retto):

L	=	4.50	m
H	=	5.90	m
Sp	=	0.50	m
S	=	0.20	m
Sf	=	0.60	m
Hp	=	0.50	m
Falda		si	
Hw	=	0.6	m
rispetto ad intradosso soletta			

Tabella 8-1- Dimensioni geometriche (sezione in retto)

8.1. PROGRAMMI DI CALCOLO UTILIZZATI

L'analisi della struttura scatolare è stata condotta con un programma agli elementi finiti (PRO_SAP prodotto dalla 2S.I. Software e Servizi per l'Ingegneria S.r.l. P.tta Schiatti 8/b 44100 Ferrara)) schematizzando i vari setti con elementi "beam".

8.1.1. Modellazione adottata

La struttura viene schematizzata attraverso un modello analitico agli elementi finiti. Si è assunto lo schema statico di telaio chiuso. La mesh è composta da 20 beam elements e da 21 nodi (figure 2a e 2b); l'output di calcolo viene raccolto nell'allegato.

L'analisi strutturale e' condotta con il metodo degli spostamenti per la valutazione dello stato tenso-deformativo indotto da carichi statici.

Il suolo viene modellato facendo ricorso all'usuale artificio delle molle elastiche alla Winkler.

Nel caso in esame il valore della costante di sottofondo si assume pari a:Ks = 3500 kN/m3

Agli effetti delle caratteristiche geometriche delle varie aste si è quindi assunto:

una sezione rettangolare b x h = 100 x Ss cm per la soletta superiore

una sezione rettangolare b x h = 100 x Sf cm per la soletta di fondazione

una sezione rettangolare b x h = 100 x Sp cm per i piedritti

Per le aste del reticolo si è assunto:

Ec = 31447 / 32588 N/mm² ; modulo elastico del calcestruzzo rispettivamente per classe di resistenza C25/30 e C28/35.

Lo schema statico della struttura e la relativa numerazione dei nodi e delle aste sono riportati nelle figure seguenti:

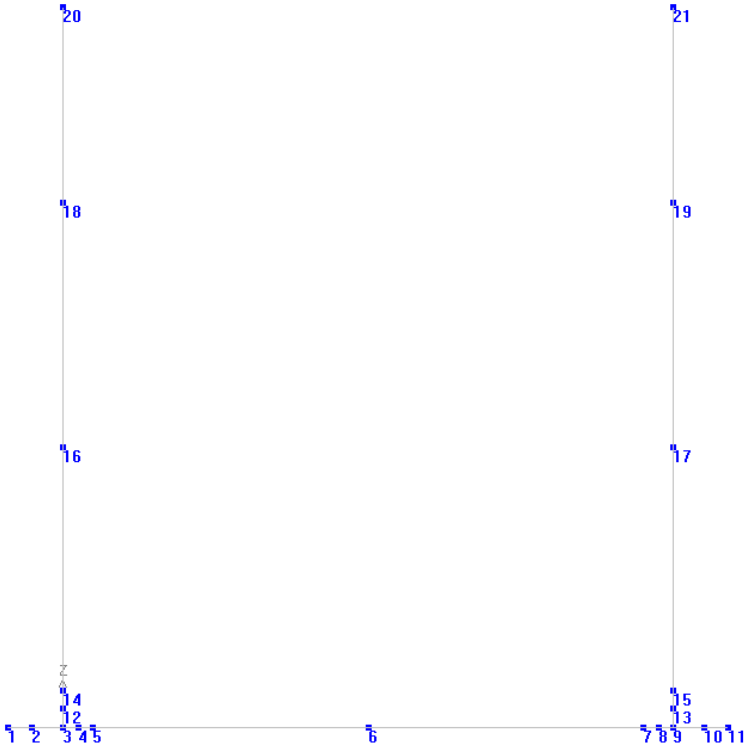


FIG. 2A - NUMERAZIONE DEI NODI

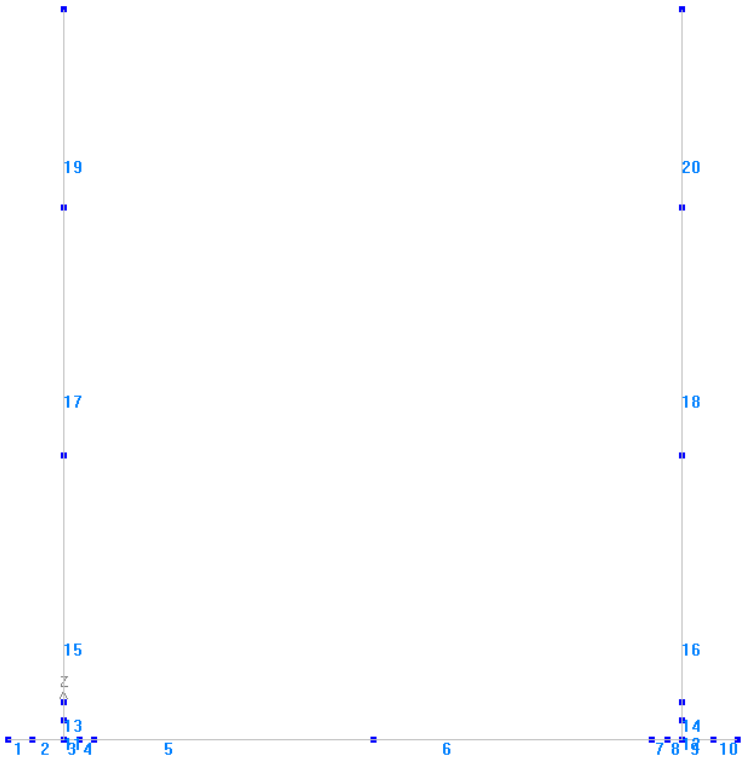


FIG. 2B - NUMERAZIONE DELLE ASTE

8.2. ANALISI DEI CARICHI

Nel seguente paragrafo si descrivono i carichi elementari da assumere per le verifiche algi stati limite ultimi e agli stati limite di eserciazio.

Vengono prese in considerazione le stesse 19 Condizioni Elementari di carico (CDC1÷ CDC 19) del Sottovia.

I dettagli relativi a ciascuna condizione di carico sono riportati nel paragrafo di analisi dei carichi.

CDC	Tipo	Sigla Id
1	Ggk	CDC=Ggk (peso proprio della struttura)
2	Gk	CDC=Gk (permanenti portati)
3	Gk	CDC=Gk (spinta a riposo piedritto sx)
4	Gk	CDC=Gk (spinta a riposo piedritto dx)
5	Gk	CDC=Gk (spinta attiva piedritto sx)
6	Gk	CDC=Gk (spinta attiva piedritto dx)
7	Qk	CDC=Qk (Q1k centrato)
8	Qk	CDC=Qk (Q1k filo piedritto dx)
9	Qk	CDC=Qk (Q1k filo piedritto sx)
10	Qk	CDC=Qk (Accidentale su piedritto sx)
11	Qk	CDC=Qk (Accidentale su piedritto dx)
12	Qk	CDC=Qk (Accidentale 20kPa su piedritto sx)
13	Qk	CDC=Qk (Accidentale 20kPa su piedritto dx)
14	Qk	CDC=Qk (frenatura)
15	Qk	CDC=Qk (Sisma orizzontale)
16	Qk	CDC=Qk (Sisma verticale)
17	Qk	CDC=Qk (Variazione termica uniforme)
18	Qk	CDC=Qk (Variazione termica lineare su soletta e piedritti)
19	Qk	CDC=Qk (Ritiro differenziale soletta)

Tali Combinazioni Elementari saranno opportunamente combinate secondo quanto previsto dalla normativa vigente.

Per i materiali si assumono i seguenti pesi specifici:

calcestruzzo armato:	25 kN/m³
rilevato	20 kN/m³
pavimentazione (spessore 0.50m)	22 kN/m³

8.2.1. Carichi elementari applicati:

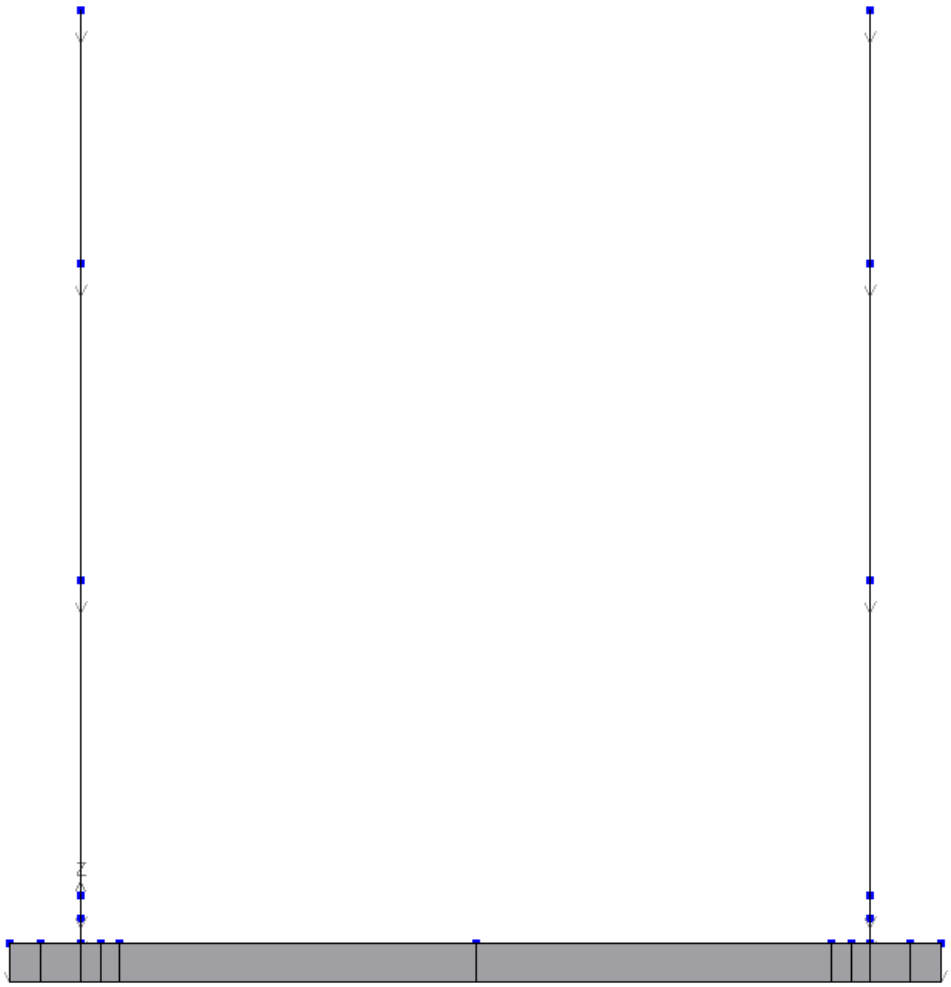


FIGURA 8.2-1 - PESO PROPRIO DELLA STRUTTURA (CARICO AUTOMATICO, CDC 1)

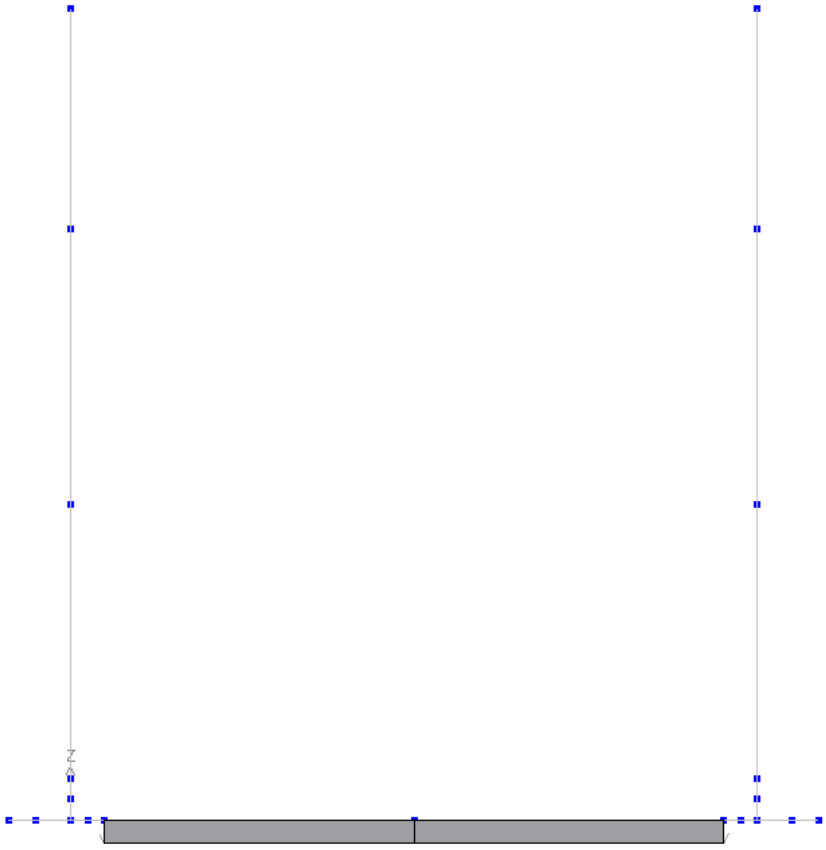


FIGURA 8.2-2 - CARICHI PERMANENTI (CDC 2)

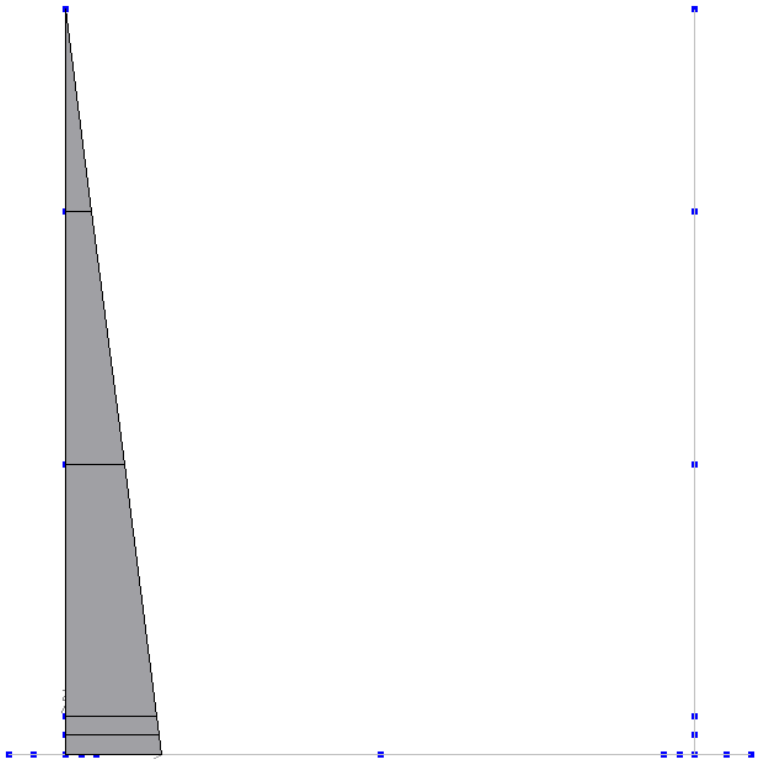


FIGURA 8.2-3 - SPINTA A RIPOSO DELLE TERRE SUL PIEDRITTO SINISTRO (CDC 3)

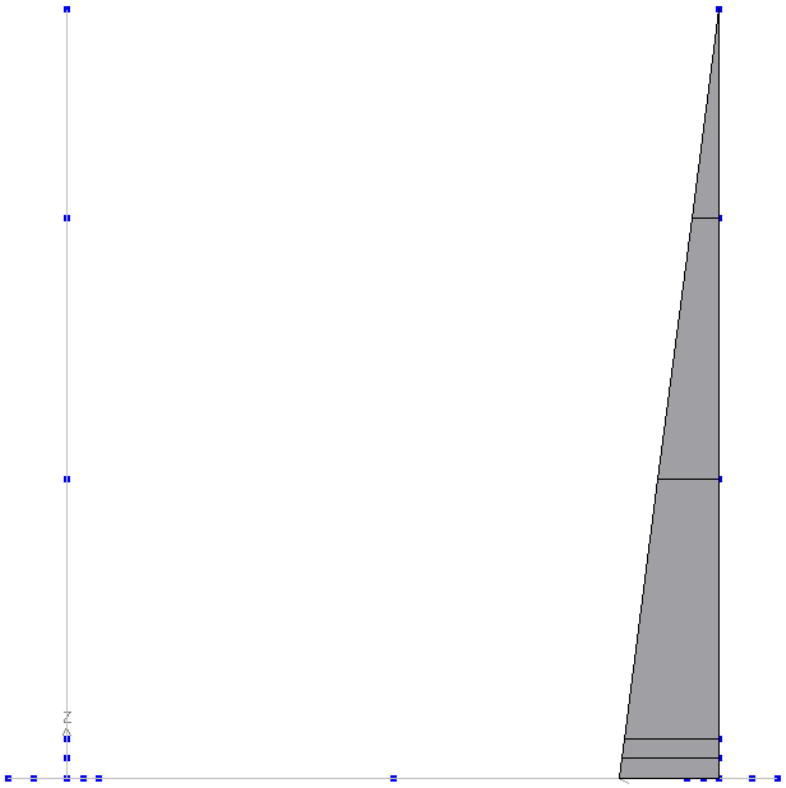


FIGURA 8.2-4 - SPINTA A RIPOSO DELLE TERRE SUL PIEDRITTO DESTRO (CDC 4)

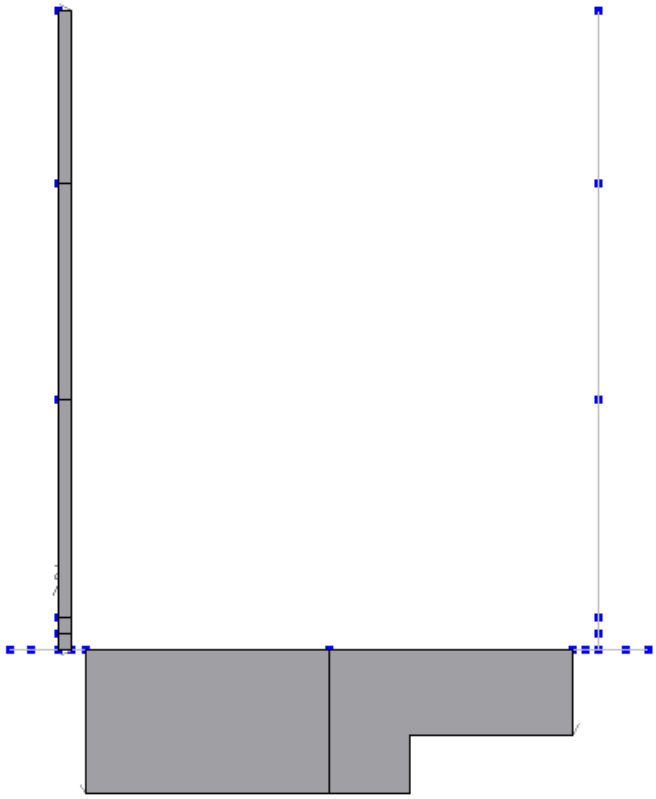


FIGURA 8.2-5 - SPINTA DEL SOVRACCARICO 20 KN/M2 SUL PIEDRITTO SINISTRO E SOVRACCARICO ACCIDENTALE SULLA SOLETTA DI FONDAZIONE (CDC 12)

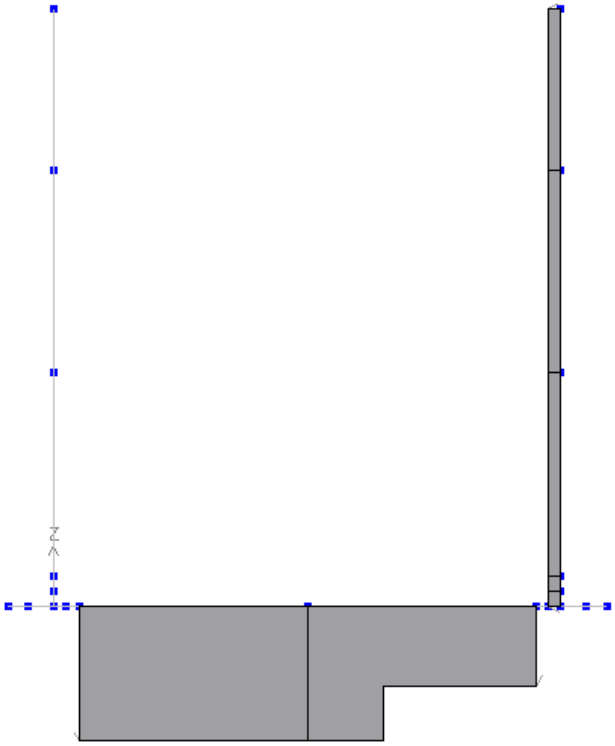


Figura 8.2-6 - Spinta del sovraccarico 20 kN/m2 sul piedritto destro e Sovraccarico accidentale sulla soletta di Fondazione (CDC 13)

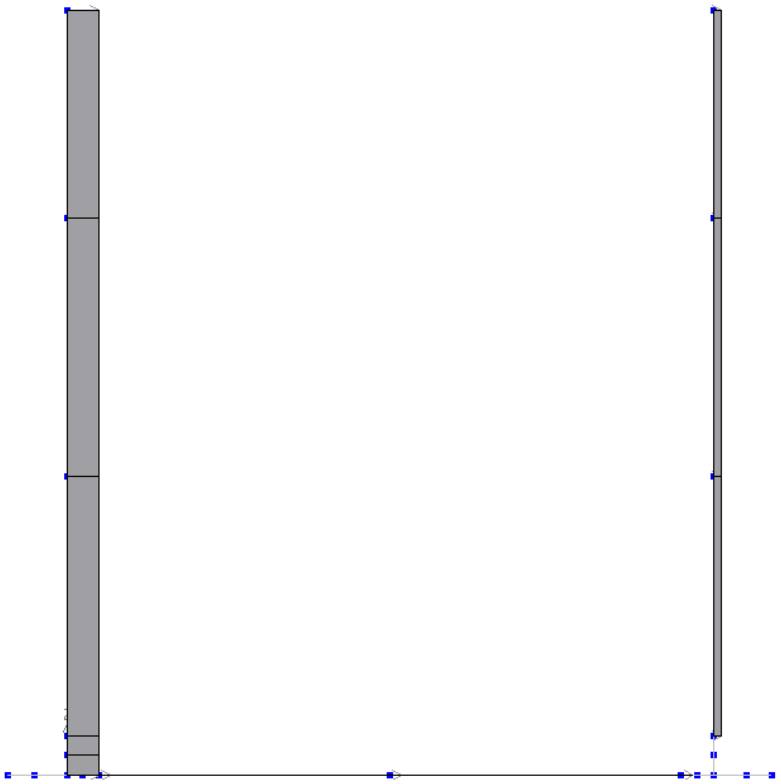


FIGURA 8.2-7 - AZIONE SISMICA ORIZZONTALE (CDC 15)

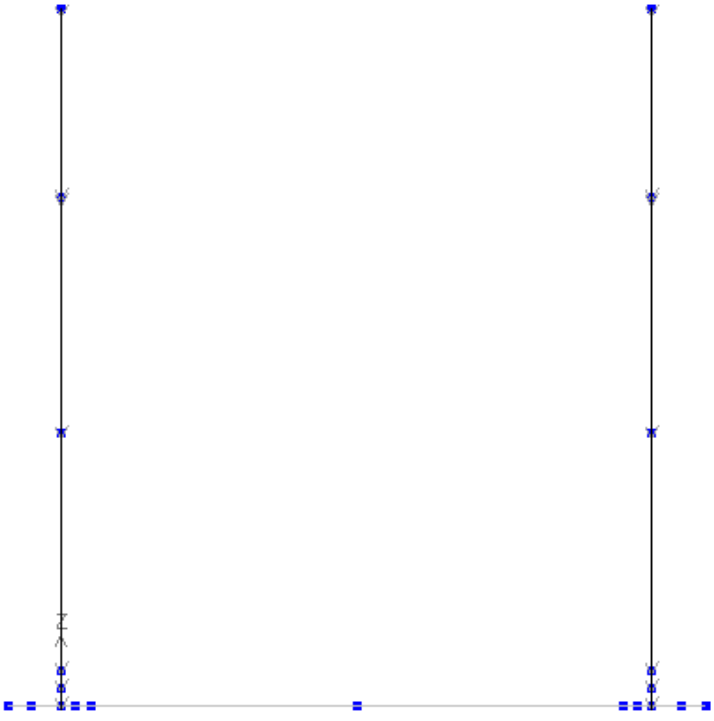


FIGURA 8.2-8 - AZIONE SISMICA VERTICALE (CDC 16)

8.2.2. Peso proprio e carichi permanenti portati

Piedritti						
peso proprio	0.50	*	25.00	=	12.50	kN/m2
Soletta inferiore						
peso proprio	0.60	*	25.00	=	15.00	kN/m2
peso sovrastruttura stradale	0.50	*	20.00	=	10.00	kN/m2
totale					25.00	kN/m2

Tali carichi vengono considerati nelle condizioni di carico elementari CDC 1-2, in particolare nella CDC1 sono presenti i pesi propri della struttura, nella condizione di carico CDC2 i carichi permanenti portati.

8.2.3. Spinta delle terre

Il reinterro a ridosso dello scatolare verrà realizzato tramite materiale di buone caratteristiche meccaniche, in accordo a quanto riportato al paragrafo 5 del presente documento.

La spinta del terreno assume un andamento lineare con la profondità secondo la legge:

$ph = \lambda \square t\ z$

dove si considera come coefficiente di spinta λ il coefficiente di spinta attiva o a riposo a seconda dell'elemento strutturale di cui si vogliono massimizzare le sollecitazioni

1) In presenza di falda esterna al muro:

Le pressioni del terreno relative alla spinta a riposo, in corrispondenza dei nodi caratteristici dei piedritti, risultano essere le seguenti:

p2	=													=	0	kN/m2
pw	=	p2	+	(	19.50	*	5.90	)	*	0.384				=	44.18	kN/m2
p1	=	pw	+	(	9.50	*	0.300	)	*	0.384	+	(10.00	* 0.300)	=	48.27	kN/m2

Tali spinte vengono considerate nella Condizione Elementare (CDC 3) sul piedritto sx e nella Condizione Elementare (CDC 4) sul piedritto dx.

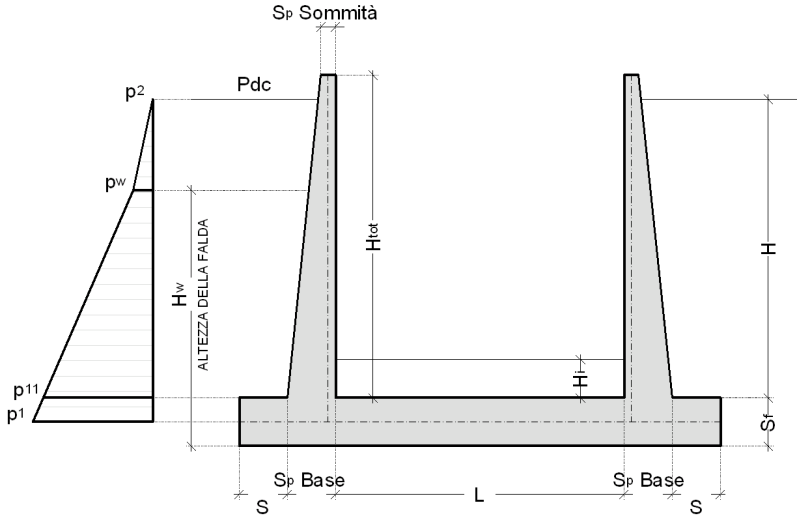


FIGURA 8.2-9 – SPINTA DELLE TERRE

Nelle combinazioni di carico verranno considerate:

Spinta a riposo su entrambi i piedritti;

8.2.4. Spinte sui piedritti indotte dai sovraccarichi accidentali

CDC 12-13: spinta sul piedritto generata dal sovraccarico da 20kN/m2 sul rilevato

Si considera, ai fini del calcolo della spinta sui piedritti, un carico qacc sul terrapieno pari a 20 kN/m2 .

Tale carico genera spinte pari a:

p = k0 x qacc = 0.384 x 20 = 7.69 kN/m (spinta a riposo, CDC 12 e 13, piedritto sinistro/destro)

8.2.5. Sovraccarichi accidentali sulla soletta di fondazione del muro

Sulla soletta di fondazione si applica il carico tandem corrispondente a ciascuna colonna di carico Qi.k, ripartito su una larghezza pari all'ingombro della colonna di carico convenzionale (3m), e una lunghezza ottenuta dalla ripartizione del carico fino al piano medio della soletta attraverso il ricoprimenmto, assumendo che detta diffusione avvenga con angolo di diffusione di 30° attraverso il rilevato stradale e di 45° sino al piano medio della soletta.

Base collaborante trasversale: BT =3.00m

Ingombro longitudinale: LL = 1.60+2 ∗ (0.50*tan30°+0.6/2)=2.78m

q'acc,1= 600/3.00/2.78+9 = 81.01kN/m2 (carico distribuito equivalente alla prima colonna di carico)

q'acc,2= 400/3.00/2.78+2.5= 50.51kN/m2 (carico distribuito equivalente alla seconda colonna di carico)

I sovraccarichi accidentali sulla soletta di fondazione vengono inserite nei casi di carico CDC12-13.

8.2.6. Azioni sismiche

(CDC elementari 15-16)

Stato limite di salvaguardia della vita (SLV)

La risultante delle forze inerziali orizzontali indotte dal sisma viene valutata con la seguente espressione:

Fh = P* kh

$$kh=\beta m \cdot \frac{a\max}{g}$$

(SLV) $kh=\beta m \cdot \frac{a\max}{g} = 0.2664$ kv=± 0.5* kh=0.1332

P = peso proprio;

k = coefficienti sismici;

Per tener conto dell'incremento di spinta del terreno dovuta al sisma si farà riferimento alla (4-6) e (4-7) e si adotterà il seguente procedimento:

si calcola la spinta attiva in condizioni statiche ($S_{A,S}$)

si calcola la quota parte efficace di spinta sismica Ed dovuta alla terra:

$$S_{A,E}= \tfrac{1}{2}\gamma^{*}(1\pm k_v)K_{A,E}\mathrm{H}^2$$

si calcola l'incremento di spinta dovuto alla terra in caso di sisma (componente efficace):

$$\Delta S_A= S_{A,E} - S_{A,S}$$

Si assume che tale azione si distribuisca uniformemente sulla parete, il che equivale ad applicare un carico uniformemente distribuito pari a:

$$q = \Delta S_A / H$$

8.2.6.1 Ai fini delle azioni verticali, non considerando i carichi accidentali

Sui piedritti si ha:

Peso proprio	12.50	kN/m^2	Inerzia piedritto	12.50	*	0.1332	1.67	kN/m^2

piedritto

8.2.6.2 Ai fini delle azioni orizzontali,

sui piedritti si considera il contributo della sovraspinta sismica dovuto al sisma oscillatorio e le spinte inerziali agenti sui piedritti, mentre sulla soletta inferiore si considera l'inerzia della stessa nonchè i permanenti portati.

Spinta inerziale sui piedritti:

Peso proprio*kh = 3.33 kN/m2

Spinta inerziale sulla soletta inferiore:

Peso proprio*kh = 3.99 kN/m2

Peso permanente* kh = 1.47 kN/m2

Sovraspinta sismica del terreno laterale:

β	ϕ	Ψ	δ	γw	γ*	γ*v	γ*h
°	°	°	°	*kN/m3*	*kN/m3*	*kN/m3*	*kN/m3*
0	38.00	90.00	0.0	10.00	19.50	0.00	0.00

Ews	Ewd	$S_{AS\ fuori\ falda}$	$S_{AS\ sotto\ falda}$	S_{AS}
kN/m	*kN/m*	*kN/m*	*kN/m*	*kN/m*
0	0	0	0.00	89.05

	Θ	ϕ–Θ	K_{AE}+sism	S_{AE}Ed	S_{AE}	Δ_{AS}	q_{AS} +
+kv	°	°	0.379	*kN/m*	*kN/m*	*kN/m*	*kN/m²*
	13.23	24.77		161.04	161.04	71.98	11.61
	Θ	ϕ–Θ	K_{AE}-sism	S_{AE}Ed	S_{AE}	Δ_{AS}	q_{AS} -
-kv	°	°	0.436	*kN/m*	*kN/m*	*kN/m*	*kN/m²*
	17.08	20.92		141.73	141.73	52.68	8.50

All'interno del modello di calcolo è stato inserito il carico qAS più gravoso.

8.3. COMBINAZIONI DI CARICO ADOTTATE

I carichi caratteristici sopra elencati (CDC), al fine di ottenere le sollecitazioni di progetto per effettuare le successive verifiche, sono opportunamente combinati fra loro.

8.3.1. Combinazioni per lo STATO LIMITE ULTIMO

γ_{G1} G1 + $\gamma_{\varepsilon 2}$ R + $\gamma_{Q1} Q_{k1}$ + $\gamma_{\varepsilon 3}$ $\psi_{0\,\varepsilon 3}$ T (carico da traffico veicolare Qk1 principale)

γ_{G1} G1 + $\gamma_{\varepsilon 2}$ R + $\gamma_{\varepsilon 3}$ T + γ_{Q1} ψ_{01} Q_{k1} (azioni termiche T principali)

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Termica Uniforme	Termica farfalla +	Ritiro
SLU	1	1.35	1.35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	2	1.35	1.35	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	3	1.35	1.35	1.35	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	4	1.35	1.35	1.35	1	0	0	0	0	0	0	0	1.01	0	0	0	0	0	0	0
	5	1	1	1.35	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	6	1	1	1.35	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	7	1	1	1.35	1.35	0	0	0	0	0	0	0	1.01	1.01	0	0	0	0	0	0
	8	1	1	1.35	1.35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

8.3.2. Combinazioni per gli stati limite di esercizio: combinazione rara

$G_1 + R + Q_{k1} + \psi_{0\varepsilon 3} T$ (carico da traffico veicolare Qk1 principale)

$G_1 + R + T + \psi_{0i} Q_{k1}$ (azioni termiche T principali)

		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Termica Uniforme	Termica farfalla +	Ritiro
SLE RAR	12	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	13	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	14	1	1	1	1	0	0	0	0	0	0	0	0.75	0	0	0	0	0	0	0

8.3.3. Combinazioni per gli stati limite di esercizio: combinazione frequente

$G_1 + R + \psi_{11} Q_{k1} + \psi_{2\varepsilon 3} T$ (carico da traffico veicolare Qk1 principale)

		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Termica Uniforme	Termica farfalla +	Ritiro
SLE FR	9	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	10	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	11	1	1	1	1	0	0	0	0	0	0	0	0.75	0	0	0	0	0	0	0

8.3.4. Combinazioni per gli stati limite di esercizio: combinazione quasi permanente

$G_1 + R + \psi_{21} Q_{k1} + \psi_{2\varepsilon 3} T$

		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Termica Uniforme	Termica farfalla +	Ritiro
SLE QP	15	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	16	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

8.3.5. Combinazioni per lo stato limite ultimo di Salvaguardia della vita

Si considera il sisma agente nella direzione trasversale dello scatolare (gli effetti del sisma agente nella direzione longitudinale del manufatto sono poco rilevanti), associato al sisma in direzione verticale (considerando in alternativa entrambi i versi d'azione). La non contemporaneità della massima azione verticale e orizzontale viene tenuta in conto, come prescritto dalle NTC 2008 (Par. 7.3.5), considerando i 4 seguenti scenari:

$E_1 = 1.00\ E_H + 0.30\ E_{V+}$ (sisma orizzontale al 100%, sisma verticale verso l'alto al 30%)

$E_2 = 1.00\ E_H + 0.30\ E_{V-}$ (sisma orizzontale al 100%, sisma verticale verso il basso al 30%)

$E_3 = 0.30\ E_H + 1.00\ E_{V+}$ (sisma orizzontale al 30%, sisma verticale verso l'alto al 100%)

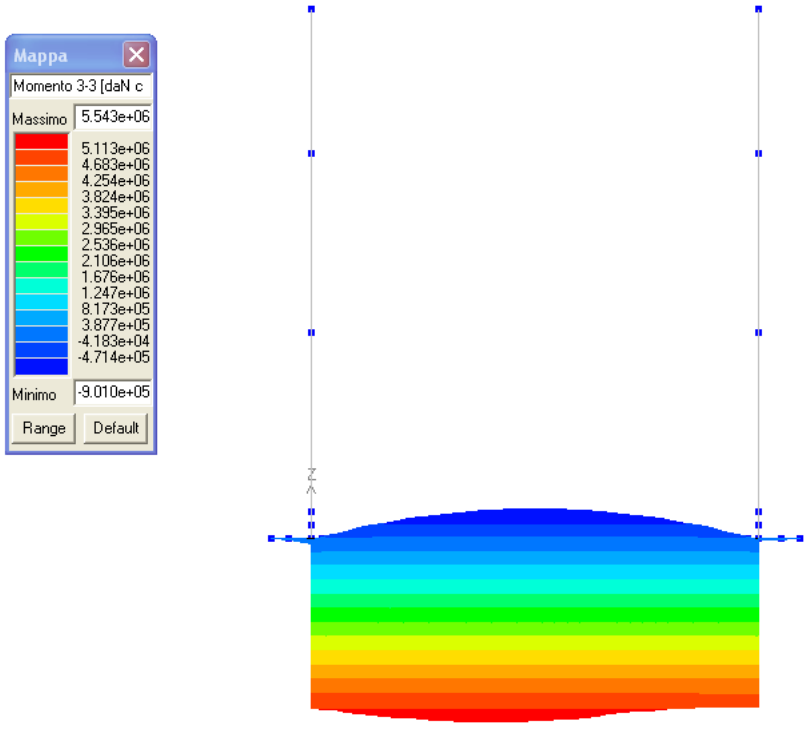
$E_4 = 0.30\ E_H + 1.00\ E_{V-}$ (sisma orizzontale al 30%, sisma verticale verso il basso al 100%)

$G_1 + E + \psi_{21} Qk1 + \psi_{2\varepsilon 3} T$

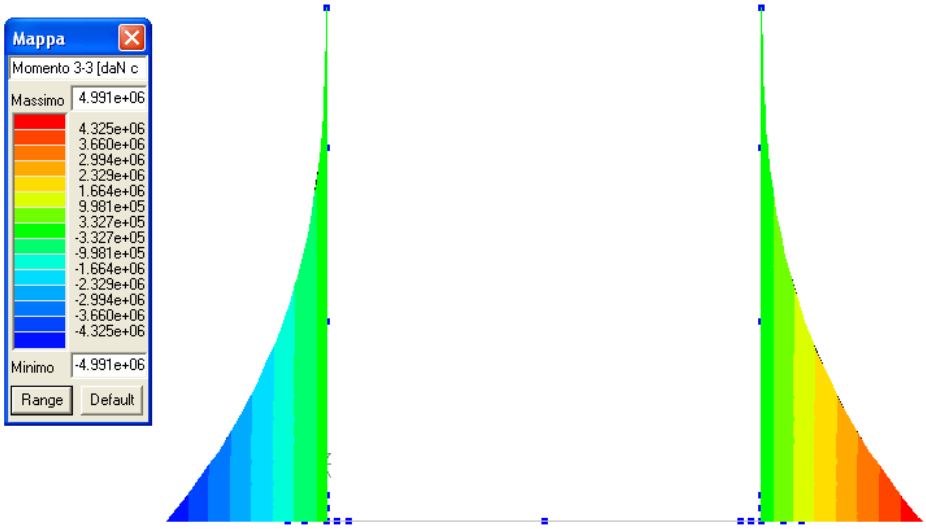
		Peso proprio	Permanenti portati	Spinta a riposo piedritto sx	Spinta riposo piedritto dx	Spinta attiva piedritto sx	Spinta attiva piedritto dx	Q1k centrato	Q1k filo piedritto dx	Q1k filo piedritto sx	Accidentale su piedritto sx	Accidentale su piedritto dx	Accidentale 20kPa piedritto sx	Accidentale 20kPa piedritto dx	Frenatura	Sisma orizzontale	Sisma verticale	Termica Uniforme	Termica farfalla +	Ritiro
SISMA	17	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0.3	1	0	0	0
	18	1	1	1	1	0	0	0	0	0	0	0	0	0	0	1	0.3	0	0	0
	19	1	1	1	1	0	0	0	0	0	0	0	0	0	0	0.3	1	0	0	0
	20	1	1	1	1	0	0	0	0	0	0	0	0	0	0	1	0.3	0	0	0
	21	1	1	1	1	0	0	0	0	0	0	0	0	0	0	1	-0.3	0	0	0

8.4. DIAGRAMMI DELLE CARATTERISTICHE DELLA SOLLECITAZIONE

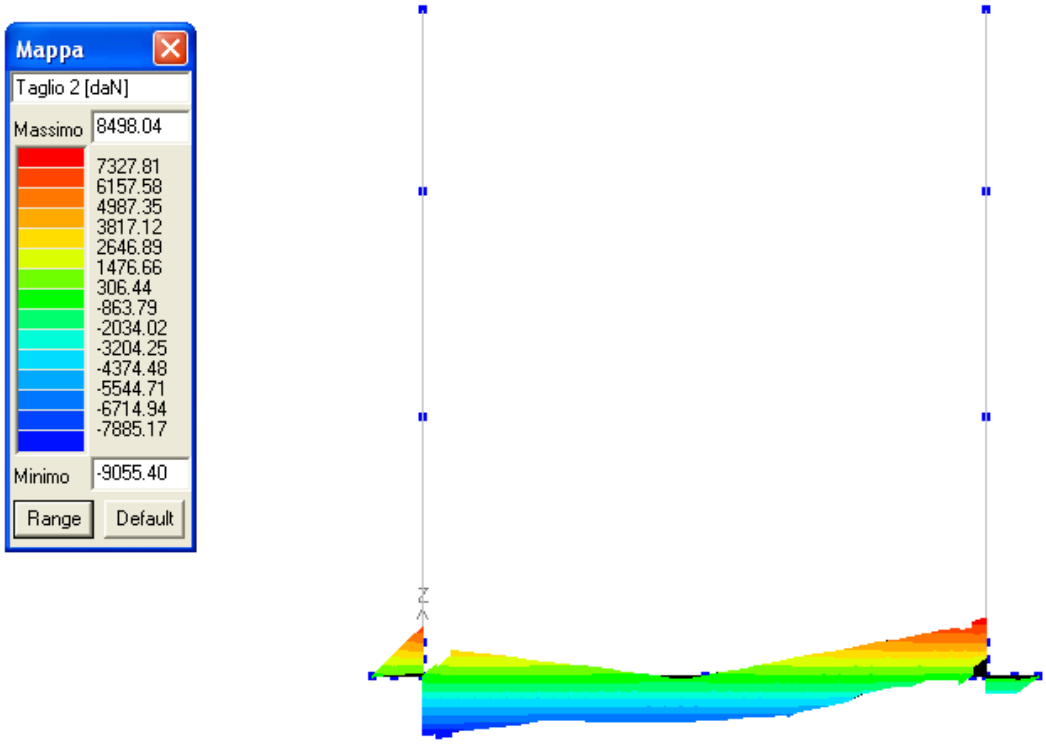
8.4.1. InviluppoSLU/SLV momento flettente soletta di fondazione



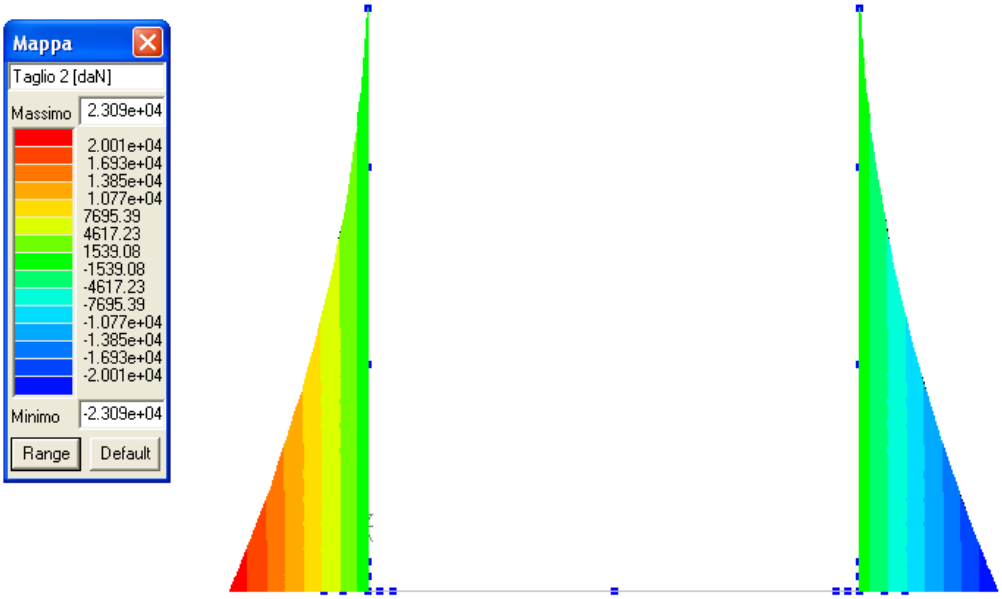
8.4.2. InviluppoSLU/SLV momento flettente piedritti



8.4.3. Inviluppo taglio SLU/SLV soletta di fondazione



8.4.4. Inviluppo taglio SLU/SLV piedritti



8.5. VERIFICHE DI RESISTENZA E A FESSURAZIONE

I calcoli di verifica di resistenza sono effettuati con il metodo degli Stati Limite, applicando il combinato D. M.14.01.2008 con l'UNI EN 1992 (Eurocodice 2).

Le verifiche a fessurazione sono state condotte considerando:

Verifica di formazione delle fessure: la verifica si esegue per la sezione interamente reagente e per le sollecitazioni di esercizio si determina la massima trazione nel calcestruzzo σ_{ct}, confrontandola con la resistenza caratteristica a trazione per flessione f_{cfk}: se risulta $\sigma_{ct}<f_{cfk}$ la verifica è soddisfatta, altrimenti si procede alla verifica di apertura delle fessure.

Verifica di apertura delle fessure: l'apertura convenzionale delle fessure è calcolata con le modalità indicate nell'EC2, come richiesto dal D. M. Min. II. TT. del 14 gennaio 2008, e valutata con le sollecitazioni relative alle Combinazioni FR o QP della normativa vigente sui ponti stradali". La massima apertura ammissibile risulta rispettivamente per le strutture in ambiente ordinario ed armature poco sensibili:

1) combinazione di carico Frequente:

$w_k \leq w_3 = 0.40mm$

2) combinazione di carico quasi permanente:

$w_k \leq w_2 = 0.30mm$

Verifica delle tensioni di esercizio: si eseguono per la condizione di carico Quasi Permanente e Rara, verificando rispettivamente che le tensioni di lavoro siano inferiori ai seguenti limiti:

1) per la condizione QP si verifica che le massime tensioni presenti nel calcestruzzo siano inferiori a $\sigma_c < 0.45\ f_{ck}$;

2) per la condizione rara si verifica che le massime tensioni presenti nel calcestruzzo siano inferiori a $\sigma_c < 0.60\ f_{ck}$, mentre quelle dell'acciaio $\sigma_s < 0.80\ f_{yk}$.

8.5.1. Verifiche di resistenza della soletta di fondazione

La verifica a pressoflessione e taglio delle solette viene eseguita automaticamente dal programma di calcolo. Nella sezione di calcolo "assegnazione dati di progetto", il programma consente mediante una finestra d'inserimento dati, di assegnare l'armatura longitudinale ad ogni singola soletta, successivamente esegue le verifiche per ogni combinazione di carico; il quantitativo di armatura trasversale (cmq/m) viene calcolato

automaticamente dal programma in funzione del diametro delle barre e delle tipologia di staffe (2br., 4br., ecc.) inseriti nella finestra d'inserimento dati.

ARMATURE:

Si dispongono le armature trasversali di seguito elencate:

PARETI:

armatura esterna per 2m da intradosso soletta inferiore	ϕ 20/10
armatura esterna per la restante lunghezza delle pareti	ϕ 16/20
armatura interna per 2m da intradosso soletta inferiore	ϕ 20/10
armatura interna per la restante lunghezza delle pareti	ϕ 16/20

SOLETTA DI FONDAZIONE:

armatura superiore	ϕ 20/10
armatura inferiore	ϕ 20/10

L'armatura di ripartizione longitudinale nelle solette e nelle pareti viene posta in misura non inferiore al 20% dell'armatura principale (direzione x) (EC2 § 9.3);si dispongono cioè ϕ 14/20.

L'armatura disposta nelle solette viene riportata mediante diagrammi.

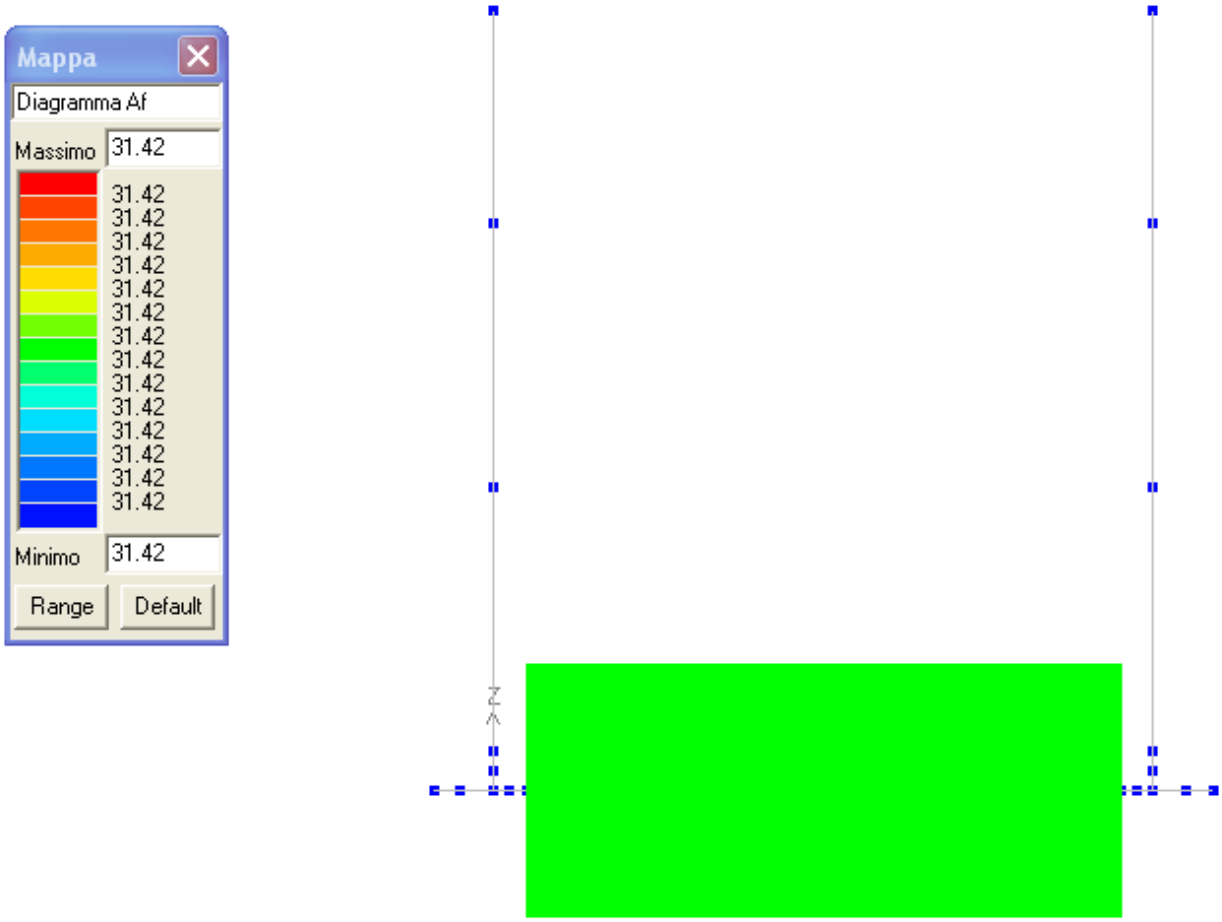
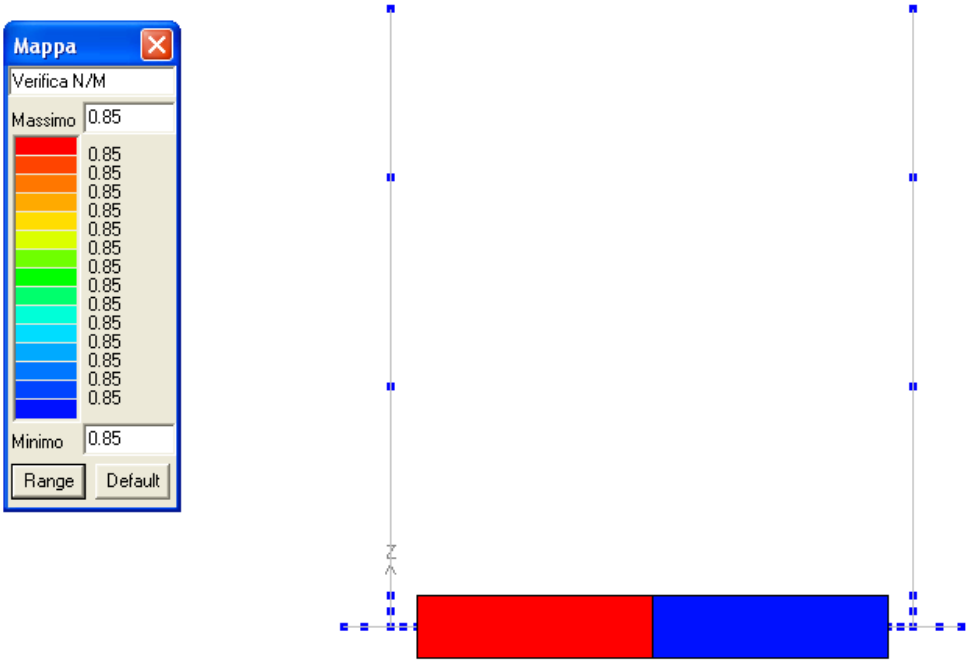


FIGURA 8.5-1 – DIAGRAMMA DEL QUANTATIVO DI ARMATURA LONGITUDINALE NELLE SOLETTE (CMQ)

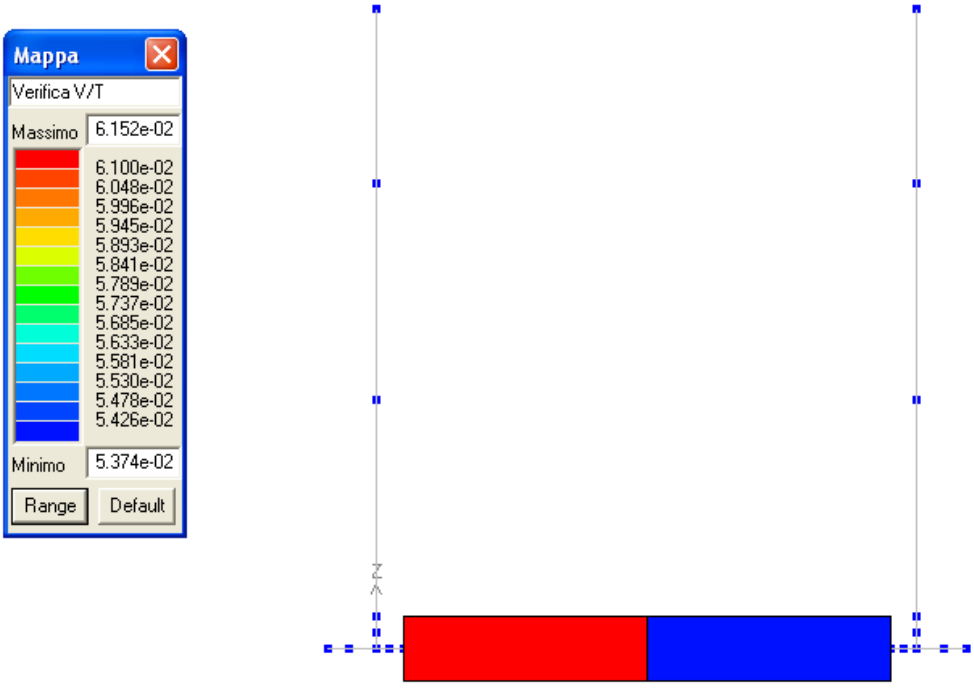
Nel seguito si riportano gli elementi grafici di visualizzazione delle verifiche eseguite secondo quanto previsto dal D.M. 14/01/2008 al paragrafo 4.1.2.1, e nel dettaglio:

- Verifica N/M Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Mrd/Med con sollecitazioni ultime proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Sd = sollecitazione di progetto, Su = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.2.4).

- Verifica (V/T) Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Vrd/Ved con sollecitazioni taglianti e torcenti proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Sd = sollecitazione di progetto, Su = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.3.2/4.1.2.1.4).



Verifica N/M Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto M*rd/Med* con sollecitazioni ultime proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Mrd = sollecitazione di progetto, Med = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.2.4).



Verifica (V/T) Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Vrd/Ved con sollecitazioni taglianti e torcenti proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Vrd = sollecitazione di progetto, Ved = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.3.2).

8.5.2. Verifiche di resistenza dei piedritti

La verifica a pressoflessione e taglio dei piedritti viene eseguita automaticamente dal programma di calcolo. Nella sezione di calcolo "assegnazione dati di progetto", il programma consente mediante una finestra d'inserimento dati, di assegnare l'armatura longitudinale e trasversale ad ogni singolo piedritto, successivamente esegue le verifiche per ogni combinazione di carico.

L'armatura disposta nei piedritti viene riportata mediante diagrammi.

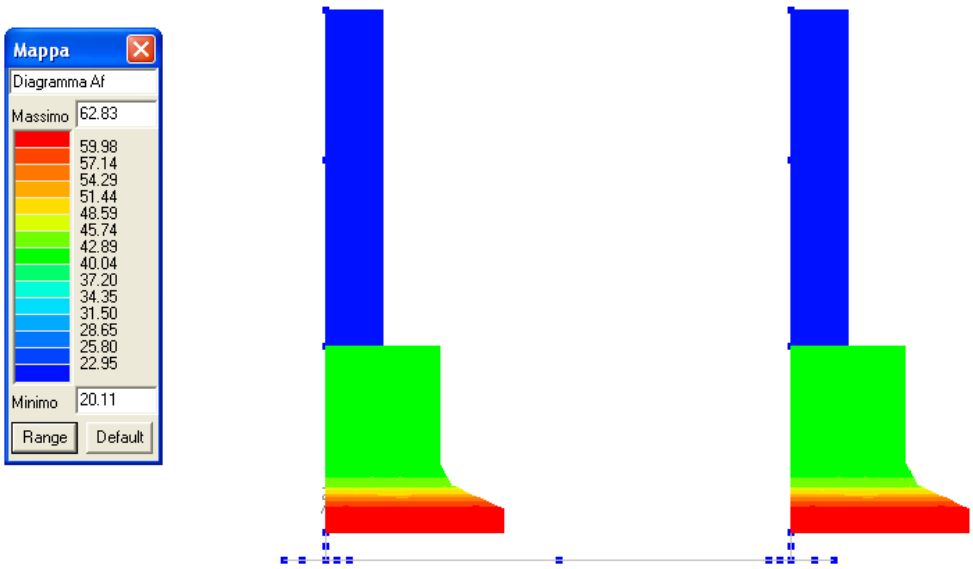
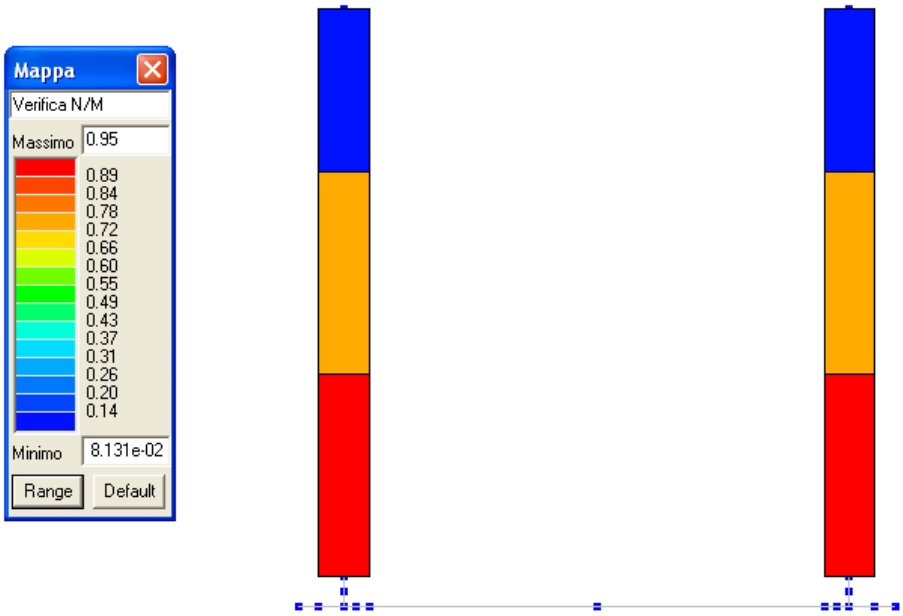


FIGURA 8.5-2 – DIAGRAMMA DEL QUANTATIVO DI ARMATURA TRASVERSALE NEI PIEDRITTI (CMQ/M)

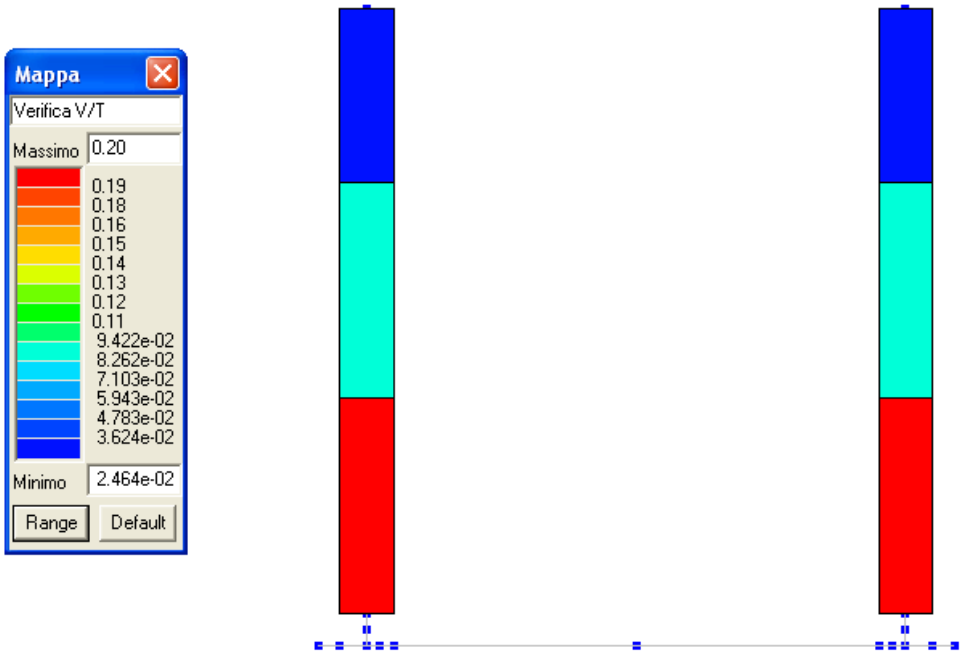
Nel seguito si riportano gli elementi grafici di visualizzazione delle verifiche eseguite secondo quanto previsto dal D.M. 14/01/2008 al paragrafo 4.1.2.1, e nel dettaglio:

- Verifica N/M Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Mrd/Med con sollecitazioni ultime proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Mrd = sollecitazione di progetto, Med = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.2.4).

- Verifica (V/T) Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Vrd/Ved con sollecitazioni taglianti e torcenti proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Vrd = sollecitazione di progetto, Ved = sollecitazione ultima) D.M. 14/01/2008 par. 4.1.2.1.3.2/4.1.2.1.4).



Verifica N/M Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Mrd/*Med* con sollecitazioni ultime proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Mrd = sollecitazione di progetto, Med = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.2.4).



Verifica (V/T) Permette la visualizzazione, mediante mappa di colore, dei valori massimi del rapporto Vrd/Ved con sollecitazioni taglianti e torcenti proporzionali; il valore del rapporto deve essere minore o uguale a 1 per verifica positiva (Vrd = sollecitazione di progetto, Ved = sollecitazione ultima) (D.M. 14/01/2008 par. 4.1.2.1.3.2).

8.5.3. Verifica stato limite di esercizio per c.c. rare

La massima tensione di compressione del calcestruzzo deve rispettare la limitazione seguente: $\sigma_c<0.60f_{ck}$.

La massima tensione dell'acciaio deve rispettare la limitazione seguente: $\sigma_s<0.80f_{yk}$.

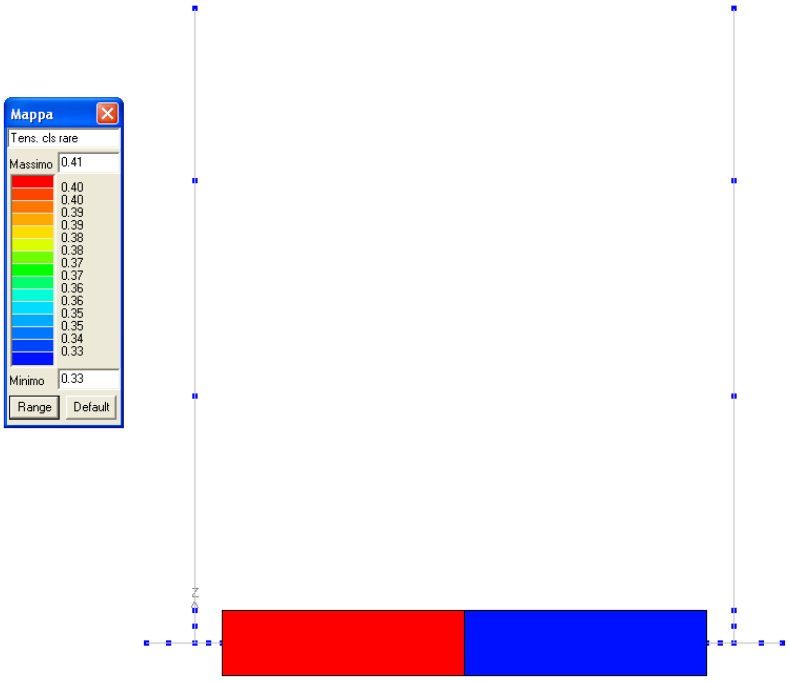


FIGURA 8.5-3 VERIFICA DELLA TENSIONE NEL CALCESTRUZZO (SLE RARE) – SOLETTA INFERIORE

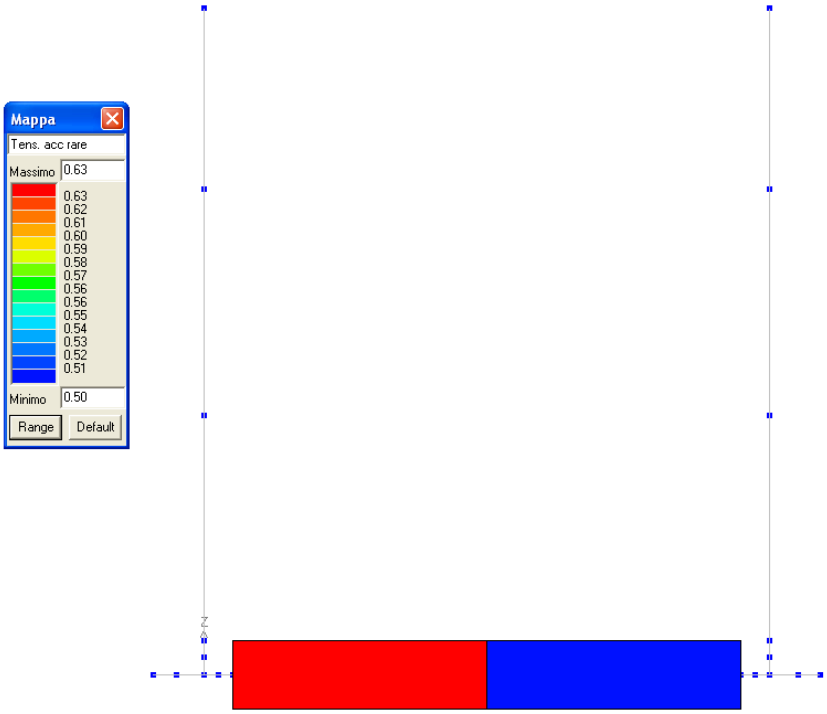


FIGURA 8.5-4 VERIFICA DELLA TENSIONE NELL'ACCIAIO (SLE RARE) – SOLETTA INFERIORE

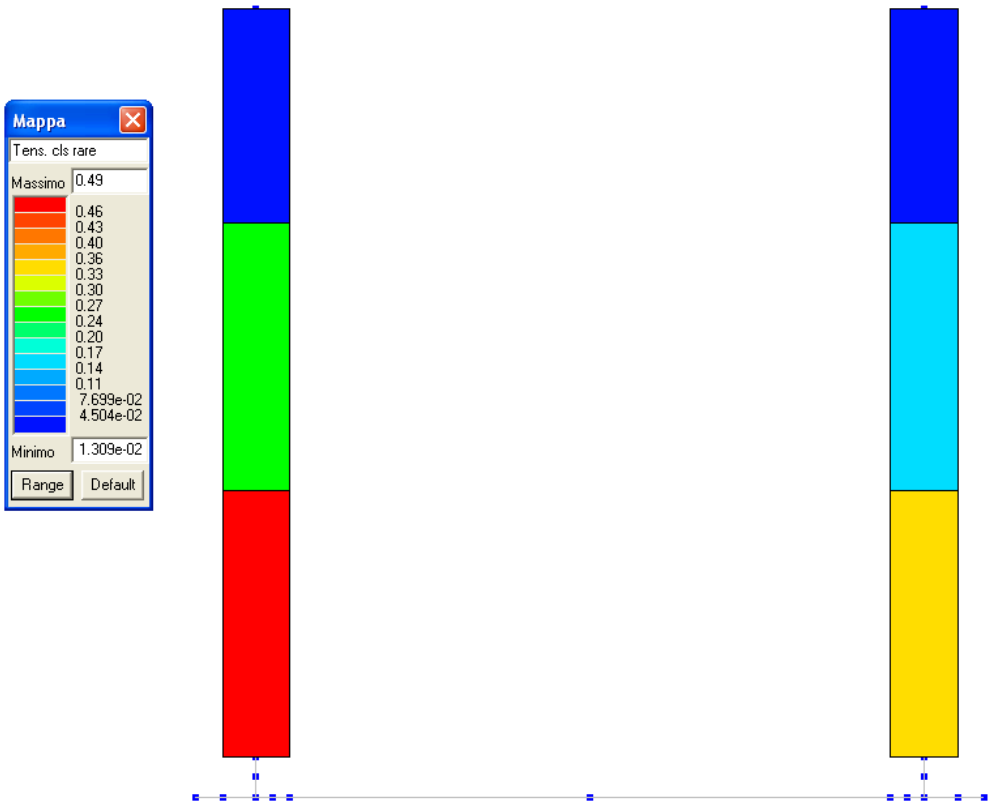


FIGURA 8.5-5 VERIFICA DELLA TENSIONE NEL CALCESTRUZZO (SLE RARE) – PIEDRITTI

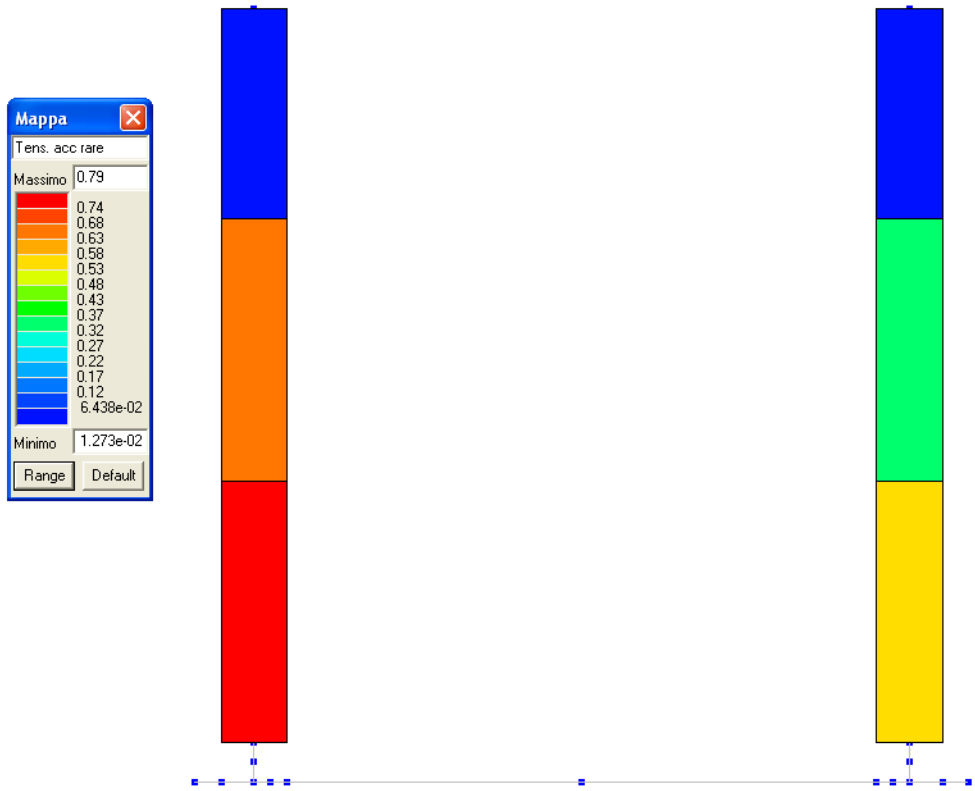


FIGURA 8.5-6 VERIFICA DELLA TENSIONE NELL'ACCIAIO (SLE RARE) – PIEDRITTI

8.5.4. Verifica stato limite di esercizio per c.c. frequenti

Il valore di calcolo di apertura delle fessure non deve superare i valori nominali (w1,w2,w3) secondo quanto riportato nella Tab. 4.1.IV del vigente D.M. 14/01/2008.

Nel caso in esame si hanno :

Condizioni ambientali	Combinazione delle azioni	Armature poco sensibili	
		Stato Limite	wd
Ordinarie	Frequente	Ap. fessure	< 0.4mm
	Quasi permanente	Ap. fessure	< 0.3mm

Di seguito si riportano le verifiche condotte agli Stati Limite di Esercizio.

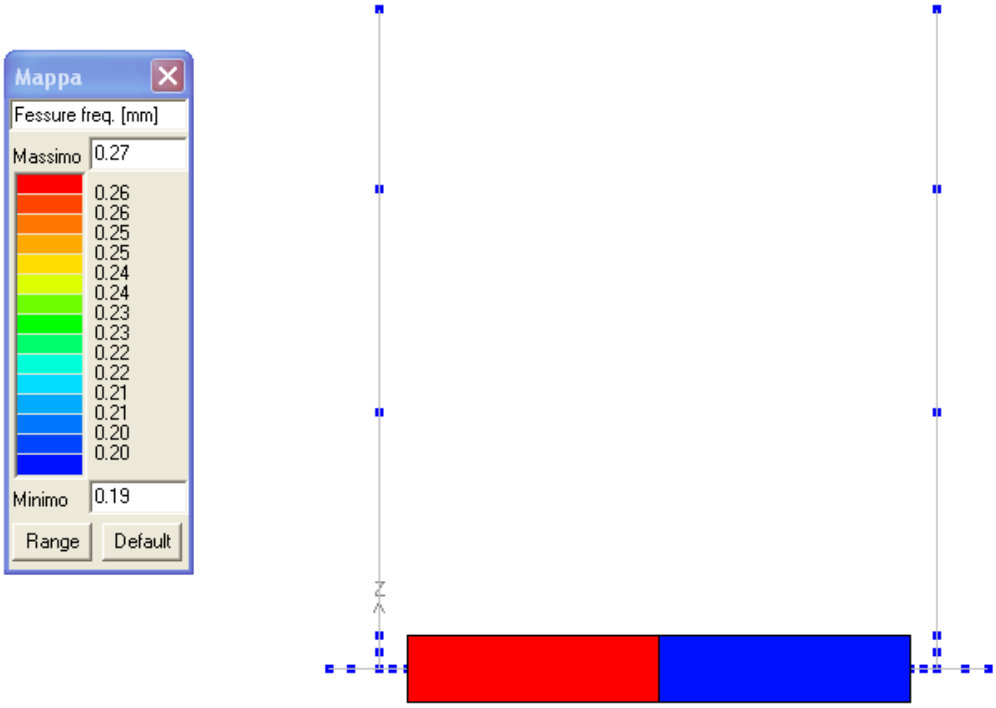


FIGURA 8.5-7 VERIFICA A FESSURAZIONE (SLE FREQUENTI) – SOLETTA INFERIORE

8.5.5. Verifica stato limite di esercizio per c.c. quasi permanenti

La massima tensione di compressione del calcestruzzo deve rispettare la limitazione seguente: $\sigma_c<0.45f_{ck}$.

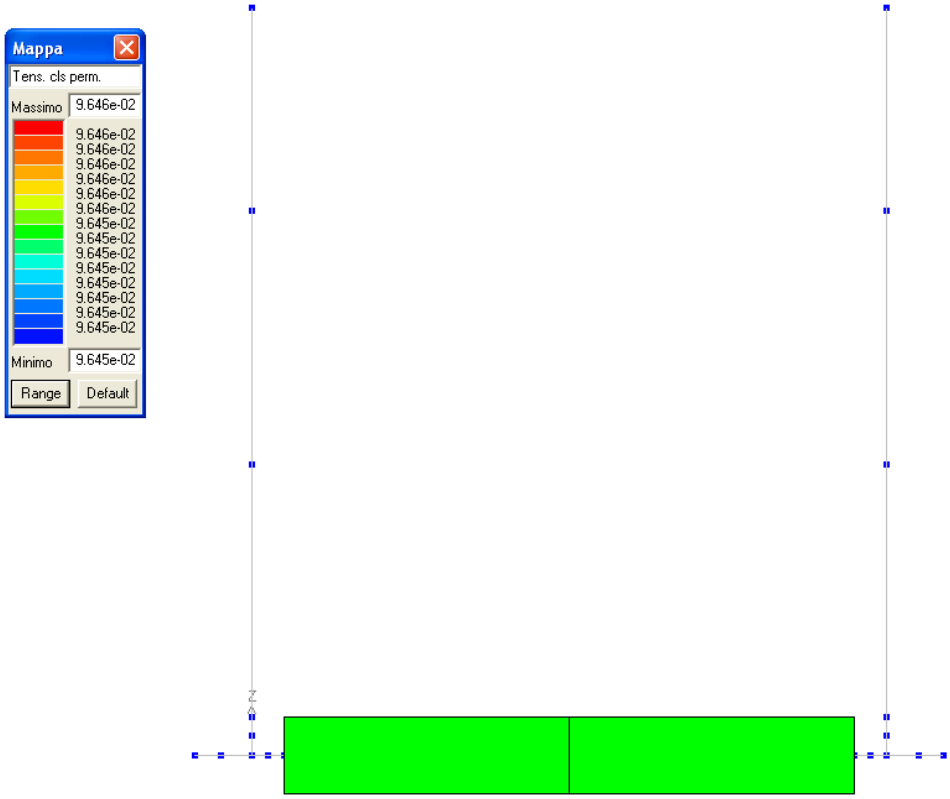


FIGURA 8.5-8 VERIFICA DELLA TENSIONE NEL CALCESTRUZZO (SLE QUASI PERMANENTI) – SOLETTA INFERIORE

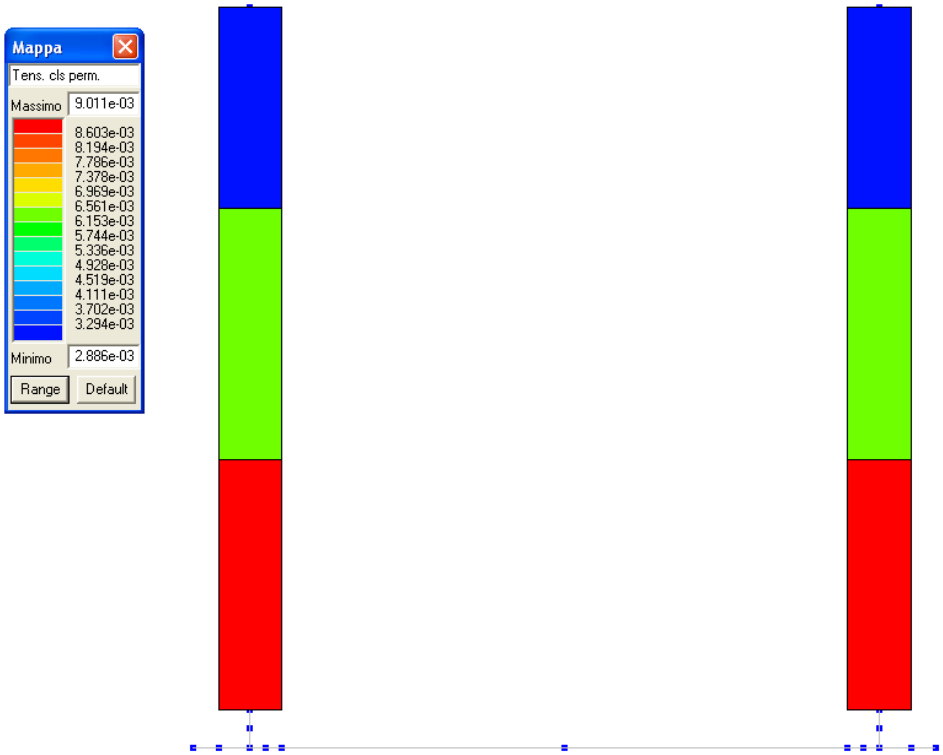


FIGURA 8.5-9 VERIFICA DELLA TENSIONE NEL CALCESTRUZZO (SLE QUASI PERMANENTI) – PIEDRITTI

Il valore di calcolo di apertura delle fessure non deve superare i valori nominali (w1,w2,w3) secondo quanto riportato nella Tab. 4.1.IV del vigente D.M. 14/01/2008.

Nel caso in esame si hanno :

Condizioni ambientali	Combinazione delle azioni	Armature poco sensibili	
		Stato Limite	wd
Ordinarie	Frequente	Ap. fessure	< 0.4mm
	Quasi permanente	Ap. fessure	< 0.3mm

Di seguito si riportano le verifiche condotte agli Stati Limite di Esercizio.

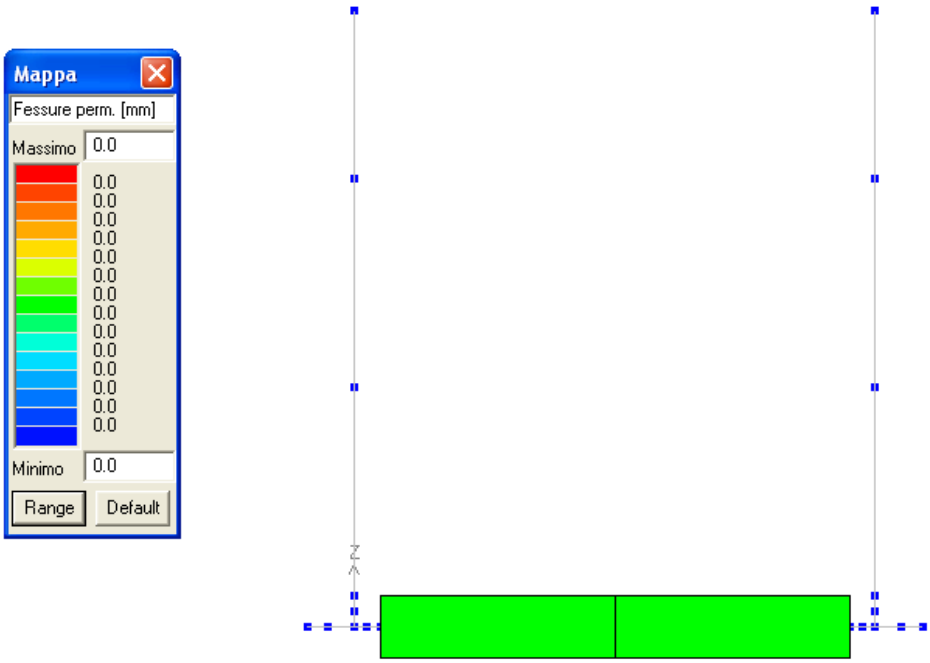


FIGURA 8.5-10 VERIFICA A FESSURAZIONE (SLE QUASI-PERMANENTI) – SOLETTA INFERIORE

9. VERIFICHE GEOTECNICHE

9.1. VERIFICA DELLA CAPACITA' PORTANTE

Considerando il tipo di struttura, ai fini della verifica della portanza del terreno stesso, non si ritengono significativi gli squilibri dovuti a spinte orizzontali non simmetriche o ad azioni orizzontali applicate alla sommità dello scatolare quali frenatura o sisma.

Al proposito si fa notare che dette spinte (o azioni) sono state applicate sul telaio piano schematizzante la canna scatolare senza considerare in alcun modo l'effetto di contenimento laterale esercitato dal terreno di rinfianco al fine di massimizzare gli effetti flessionali agenti sui piedritti (e sulle solette) del tombino.

Pertanto nel seguito le pressioni agenti sul terreno di fondazione vengono calcolate in presenza dei soli carichi verticali:

- peso proprio sezione scatolare
- peso terreno di ricoprimento e pavimentazione stradale
- carichi accidentali da traffico
- peso ricoprimento interno allo scatolare senza tenere in conto la presenza di azioni orizzontali.
- Carichi accidentali da traffico sulla soletta inferiore

Ai fini della combinazione dei carichi verranno utilizzati i seguenti coefficienti di norma:

A1-STR: $1.35 (G_1 + G_2 + G_3) + 1.35\ Q$

A2-GEO: $G_1 + G_2 + G_3 + 1.15\ Q$

Fra i carichi accidentali elencati:

- Carico mobile veicolare sulla soletta superiore, posizione per massimo momento in mezzeria soletta superiore
- Carico mobile veicolare sulla soletta superiore, posizione per massimo taglio all'attacco del piedritto dx
- Sovraccarico uniforme da 20kPa sulle soletta superiore

verrà considerato di volta in volta il carico più sfavorevole ai fini della determinazione:

- del massimo carico verticale agente ad intradosso fondazione ;

- della massima pressione di contatto terreno/fondazione.

Nelle tabelle seguenti, si fornisce per entrambi gli scenari di norma elencati e per ognuna delle due "condizioni di verifica" sopra descritte:

- nella prima colonna il carico considerato ;

- nella seconda colonna la reazione verticale (agente su un metro di fondazione) indotta dal carico in esame (N, [kN]);

- nella terza colonna il momento (agente su un metro di fondazione) indotto dal carico in esame (M, [kN.m]);

- nella quarta colonna l'eccentricità della reazione verticale (e=M/N, [m]);

- nella quinta colonna il coefficiente di combinazione del carico in esame.

Si riportano quindi nell'ultima riga:

- il carico N_{tot} agente ad intradosso fondazione (ogni metro di canna) nella combinazione in esame ;

- il momento M_{tot} agente ad intradosso fondazione (ogni metro di canna) nella combinazione in esame ;

- l'eccentricità della reazione verticale $e = M_{tot} / N_{tot}$;

- la pressione di contatto terreno/fondazione valutate con la teoria di *Mayerhof* :

$\sigma_{terr} = N_{tot} / (B_i + 2 \times S_p + 2 \times S_b - 2 \times e)$ [kPa]

Combinazione A1-STR				
Carico	N (KN)	M (KN)	e (m)	coefff
peso proprio	304.75	0	0	1.35
peso ricoprimento	175.66	0	0	1.35
1) veicolari max soletta	559.1135376	0	0	1.35
2) veicolari max taglio	559.1135376	145.7424955	0.260667084	1.35
3) veicolari 20KPa	318.7943309	0	0	1.35
	Ntot (KN)	Mtot (KN)	e (m)	sigma (KPa)
1) Risultante	1403.356776	0	0	237.8570806
2) Risultante	1403.356776	196.7523689	0.140201246	249.7254961
3) Risultante	1078.925847	0	0	182.8687876

Combinazione A2-GEO				
Carico	N (KN)	M (KN)	e (m)	coefff
peso proprio	304.75	0	0	1
peso ricoprimento	175.66	0	0	1
1) veicolari max soletta	559.1135376	0	0	1.15
2) veicolari max taglio	559.1135376	145.7424955	0.260667084	1.15
3) veicolari 20KPa	318.7943309	0	0	1.15
	Ntot (KN)	Mtot (KN)	e (m)	sigma (KPa)
1) Risultante	1123.390568	0	0	190.405181
2) Risultante	1123.390568	145.7424955	0.129734484	199.1639726
3) Risultante	847.0234806	0	0	143.5633018

9.2. VERIFICA A GALLEGGIAMENTO SCATOLARE

La verifica viene eseguita in condizione di esercizio (ovviamente in assenza di sovraccarichi accidentali), considerando il battente alla sua altezza massima.

Per la stabilità al sollevamento deve risultare che il valore di progetto dell'azione instabilizzante $V_{inst,d}$, combinazione di azioni permanenti ($G_{inst,d}$), sia non maggiore della combinazione dei valori di progetto delle azioni stabilizzanti ($G_{stb,d}$) e delle resistenze (R_d):

$$V_{inst,d} \leq G_{stb,d} + R_d \qquad \text{dove} \quad V_{inst,d} = G_{inst,d}$$

Le verifiche agli stati limite ultimi sono eseguite in riferimento alla seguente combinazione:

1. combinazione 2 → (A2+M2) → GEO (galleggiamento)

TABELLA 6.2.III - COEFFICIENTI PARZIALI PER LE AZIONI O PER L'EFFETTO DELLE AZIONI

CARICHI	EFFETTO	SIMBOLO γ_F	(A2) STR
Permanente	favorevole	γ_{G1}	0.9
	sfavorevole		1.1
Permanente non strutturali	favorevole	γ_{G2}	0.0
	sfavorevole		1.1

TABELLA 6.2.II - COEFFICIENTI PARZIALI PER I PARAMETRI DEL TERRENO

PARAMETRO	GRANDEZZA ALLA QUALE APPLICARE IL COEFF. PARZIALE	COEFFICIENTE PARZIALE γ_M	M_2
Tangente dell'angolo di resistenza al taglio	$\tan \varphi'_k$	$\gamma_{\varphi'}$	1.25
Coesione efficace	c'_k	$\gamma_{c'}$	1.25
Resistenza non drenata	c'_{uk}	γ_{cu}	1.4
Peso dell'unità di volume	γ	γ_γ	1

Dato il livello di falda di progetto, la spinta di galleggiamento risulta:

Verifica Galleggiamento in Esercizio

VERIFICA A GALLEGGIAMENTO		
Hw falda quota di appoggio fond.	0.6	m
Altezza totale scatolare	6.55	m
Larghezza fondazione senza ali	5.50	m
Lunghezza ala di fondazione	0.20	m
Spessore soletta fondazione	0.60	m
Volume immerso	3.54	mc
Peso specifico Liquido	10	KN/mc
Sottospinta idraulica di galleggiamento	35.4	KN
$\gamma_{G,inst}$	1.1	m
Ginst,d	38.94	KN
Peso proprio strutture	304.75	KN
γ_{G1}	0.9	
Peso permanente soletta superiore	30.25	KN
γ_{G1}	0.9	
Peso permanente soletta inferiore	0.00	KN
γ_{G1}	0.9	
Peso Terreno su di fondazione	41.73	KN
γ_{G1}	0.9	
Ginst,d	339.057	KN
Coefficiente di Sicurezza	8.707164869	

La verifica risulta soddisfatta senza considerare il contributo favorevole svolto dalla resistenza di attrito lungo le pareti dello scatolare (azione stabilizzante R_d).

9.3. VERIFICA A GALLEGGIAMENTO MURO AD "U"

La verifica viene eseguita in condizione di esercizio (ovviamente in assenza di sovraccarichi accidentali), considerando il battente alla sua altezza massima.

Per la stabilità al sollevamento deve risultare che il valore di progetto dell'azione instabilizzante $V_{inst,d}$, combinazione di azioni permanenti ($G_{inst,d}$), sia non maggiore della combinazione dei valori di progetto delle azioni stabilizzanti ($G_{stb,d}$) e delle resistenze (R_d):

$$V_{inst,d} \leq G_{stb,d} + R_d \qquad \text{dove } V_{inst,d} = G_{inst,d}$$

Le verifiche agli stati limite ultimi sono eseguite in riferimento alla seguente combinazione:

2. combinazione 2 → (A2+M2) → GEO (galleggiamento)

TABELLA 6.2.III - COEFFICIENTI PARZIALI PER LE AZIONI O PER L'EFFETTO DELLE AZIONI

CARICHI	EFFETTO	SIMBOLO γF	(A2) STR
Permanente	favorevole	γ_{G1}	0.9
	sfavorevole		1.1
Permanente non strutturali	favorevole	γ_{G2}	0.0
	sfavorevole		1.1

TABELLA 6.2.II - COEFFICIENTI PARZIALI PER I PARAMETRI DEL TERRENO

PARAMETRO	GRANDEZZA ALLA QUALE APPLICARE IL COEFF. PARZIALE	COEFFICIENTE PARZIALE γ_M	M_2
Tangente dell'angolo di resistenza al taglio	$\tan \varphi'_k$	$\gamma_{\varphi'}$	1.25
Coesione efficace	c'_k	$\gamma_{c'}$	1.25
Resistenza non drenata	c'_{uk}	γ_{cu}	1.4
Peso dell'unità di volume	γ	γ_γ	1

Dato il livello di falda di progetto, la spinta di galleggiamento risulta:

Verifica Galleggiamento in Esercizio

VERIFICA A GALLEGGIAMENTO		
Hw falda quota di appoggio fond.	0.6	m
Altezza totale scatolare	6.50	m
Larghezza fondazione senza ali	5.50	m
Lunghezza ala di fondazione	0.20	m
Spessore soletta fondazione	0.60	m
Volume immerso	3.54	mc
Peso specifico Liquido	10	KN/mc
Sottospinta idraulica di galleggiamento	35.4	KN
$\gamma_{G,inst}$	1.1	m
Ginst,d	38.94	KN
Peso proprio strutture	295	KN
γ_{G1}	0.9	
Peso permanente soletta superiore	0.00	KN
γ_{G1}	0.9	
Peso permanente soletta inferiore	0.00	KN
γ_{G1}	0.9	
Peso Terreno su di fondazione	46.02	KN
γ_{G1}	0.9	
Ginst,d	306.918	KN
Coefficiente di Sicurezza	7.881818182	

La verifica risulta soddisfatta senza considerare il contributo favorevole svolto dalla resistenza di attrito lungo le pareti del muro ad "U" (azione stabilizzante R_d).

10. ALLEGATO A. –SCATOLARE - CALCOLO FEM - OUTPUT

PRO_SAP
PROFESSIONAL STRUCTURAL ANALYSIS PROGRAM

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste nel D.M. 14 Gennaio 2008 cap. 10 "Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo"

2S.I. SOFTWARE E SERVIZI PER L'INGEGNERIA SRL
P.tta Schiatti 8/b
44100 FERRARA (ITALY)
tel. 39 532 200091 – fax 39 532 200086
www.2si.it **info@2si.it**

D.M. 14/01/08 cap. 10.2 Affidabilità dei codici utilizzati:
www.2si.it/software/Affidabilità.htm

10.1. RISULTATI NODALI

Il controllo dei risultati delle analisi condotte, per quanto concerne i nodi strutturali, è possibile in relazione alle tabelle sottoriportate.

Una prima tabella riporta infatti per ogni nodo e per ogni combinazione (o caso di carico) gli spostamenti nodali.

Una seconda tabella, infine riassume per ogni nodo le sei combinazioni in cui si attingono i valori minimi e massimi della reazione Fz, della reazione Mx e della reazione My.

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm2	daN/cm2
1	1	-0.65	-0.65	-0.65	2	-0.61	-0.62	-0.62	3	-0.44	-0.46	-0.46
	4	-0.85	-0.88	-0.88	5	-0.27	-0.29	-0.29	6	-0.27	-0.29	-0.29
	7	-1.73	-1.72	-1.73	8	-0.43	-0.44	-0.44	9	-0.48	-0.48	-0.48
	10	-0.44	-0.45	-0.45	11	-0.75	-0.76	-0.76	12	-0.48	-0.48	-0.48
	13	-0.44	-0.45	-0.45	14	-0.75	-0.76	-0.76	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.32	-0.34	-0.34	18	0.11	0.07	0.11
	19	-0.32	-0.34	-0.34	20	0.11	0.07	0.11	21	0.14	0.09	0.14
2	1	-0.65	-0.65	-0.65	2	-0.62	-0.62	-0.62	3	-0.46	-0.48	-0.48
	4	-0.88	-0.92	-0.92	5	-0.29	-0.31	-0.31	6	-0.29	-0.31	-0.31
	7	-1.72	-1.72	-1.72	8	-0.44	-0.45	-0.45	9	-0.48	-0.48	-0.48
	10	-0.45	-0.46	-0.46	11	-0.76	-0.78	-0.78	12	-0.48	-0.48	-0.48
	13	-0.45	-0.46	-0.46	14	-0.76	-0.78	-0.78	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.34	-0.36	-0.36	18	0.07	6.15e-03	0.06
	19	-0.34	-0.36	-0.36	20	0.07	6.15e-03	0.06	21	0.09	0.03	0.09
3	1	-0.65	-0.65	-0.65	2	-0.62	-0.63	-0.63	3	-0.48	-0.49	-0.49
	4	-0.92	-0.94	-0.94	5	-0.31	-0.32	-0.32	6	-0.31	-0.32	-0.32
	7	-1.72	-1.72	-1.72	8	-0.45	-0.45	-0.45	9	-0.48	-0.48	-0.48
	10	-0.46	-0.46	-0.46	11	-0.78	-0.79	-0.79	12	-0.48	-0.48	-0.48
	13	-0.46	-0.46	-0.46	14	-0.78	-0.79	-0.79	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.36	-0.37	-0.37	18	6.15e-03	-0.02	-0.02
	19	-0.36	-0.37	-0.37	20	6.15e-03	-0.02	-0.02	21	0.03	4.30e-03	0.03
4	1	-0.65	-0.65	-0.65	2	-0.63	-0.63	-0.63	3	-0.49	-0.50	-0.50
	4	-0.94	-0.96	-0.96	5	-0.32	-0.34	-0.34	6	-0.32	-0.34	-0.34
	7	-1.72	-1.72	-1.72	8	-0.45	-0.46	-0.46	9	-0.48	-0.48	-0.48
	10	-0.46	-0.46	-0.46	11	-0.79	-0.80	-0.80	12	-0.48	-0.48	-0.48
	13	-0.46	-0.46	-0.46	14	-0.79	-0.80	-0.80	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.37	-0.38	-0.38	18	-0.02	-0.05	-0.05
	19	-0.37	-0.38	-0.38	20	-0.02	-0.05	-0.05	21	4.30e-03	-0.03	-0.03
5	1	-0.65	-0.64	-0.65	2	-0.63	-0.66	-0.66	3	-0.50	-0.66	-0.66
	4	-0.96	-1.21	-1.21	5	-0.34	-0.50	-0.50	6	-0.34	-0.50	-0.50
	7	-1.72	-1.60	-1.72	8	-0.46	-0.50	-0.50	9	-0.48	-0.47	-0.48
	10	-0.46	-0.49	-0.49	11	-0.80	-0.90	-0.90	12	-0.48	-0.47	-0.48
	13	-0.46	-0.49	-0.49	14	-0.80	-0.90	-0.90	15	-0.48	-0.47	-0.48
	16	-0.48	-0.47	-0.48	17	-0.38	-0.54	-0.54	18	-0.05	-0.52	-0.52
	19	-0.38	-0.54	-0.54	20	-0.05	-0.52	-0.52	21	-0.03	-0.49	-0.49
6	1	-0.64	-0.65	-0.65	2	-0.66	-0.63	-0.66	3	-0.66	-0.75	-0.75
	4	-1.21	-1.36	-1.36	5	-0.50	-0.58	-0.58	6	-0.50	-0.58	-0.58

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
	7	-1.60	-1.32	-1.59	8	-0.50	-0.46	-0.50	9	-0.47	-0.48	-0.48
	10	-0.49	-0.46	-0.49	11	-0.90	-0.92	-0.92	12	-0.47	-0.48	-0.48
	13	-0.49	-0.46	-0.49	14	-0.90	-0.92	-0.92	15	-0.47	-0.48	-0.48
	16	-0.47	-0.48	-0.48	17	-0.54	-0.63	-0.63	18	-0.52	-0.89	-0.89
	19	-0.54	-0.63	-0.63	20	-0.52	-0.89	-0.89	21	-0.49	-0.86	-0.86
7	1	-0.65	-0.65	-0.65	2	-0.63	-0.63	-0.63	3	-0.75	-0.76	-0.76
	4	-1.36	-1.37	-1.37	5	-0.58	-0.59	-0.59	6	-0.58	-0.59	-0.59
	7	-1.32	-1.30	-1.32	8	-0.46	-0.45	-0.46	9	-0.48	-0.48	-0.48
	10	-0.46	-0.46	-0.46	11	-0.92	-0.92	-0.92	12	-0.48	-0.48	-0.48
	13	-0.46	-0.46	-0.46	14	-0.92	-0.92	-0.92	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.63	-0.64	-0.64	18	-0.89	-0.91	-0.91
	19	-0.63	-0.64	-0.64	20	-0.89	-0.91	-0.91	21	-0.86	-0.88	-0.88
8	1	-0.65	-0.65	-0.65	2	-0.63	-0.62	-0.63	3	-0.76	-0.76	-0.76
	4	-1.37	-1.37	-1.37	5	-0.59	-0.59	-0.59	6	-0.59	-0.59	-0.59
	7	-1.30	-1.28	-1.30	8	-0.45	-0.45	-0.45	9	-0.48	-0.48	-0.48
	10	-0.46	-0.46	-0.46	11	-0.92	-0.91	-0.92	12	-0.48	-0.48	-0.48
	13	-0.46	-0.46	-0.46	14	-0.92	-0.91	-0.92	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.64	-0.64	-0.64	18	-0.91	-0.93	-0.93
	19	-0.64	-0.64	-0.64	20	-0.91	-0.93	-0.93	21	-0.88	-0.90	-0.90
9	1	-0.65	-0.65	-0.65	2	-0.62	-0.62	-0.62	3	-0.76	-0.76	-0.76
	4	-1.37	-1.39	-1.39	5	-0.59	-0.59	-0.59	6	-0.59	-0.59	-0.59
	7	-1.28	-1.24	-1.28	8	-0.45	-0.44	-0.45	9	-0.48	-0.48	-0.48
	10	-0.46	-0.45	-0.46	11	-0.91	-0.91	-0.91	12	-0.48	-0.48	-0.48
	13	-0.46	-0.45	-0.46	14	-0.91	-0.91	-0.91	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.64	-0.65	-0.65	18	-0.93	-0.96	-0.96
	19	-0.64	-0.65	-0.65	20	-0.93	-0.96	-0.96	21	-0.90	-0.94	-0.94
10	1	-0.65	-0.65	-0.65	2	-0.62	-0.61	-0.62	3	-0.76	-0.77	-0.77
	4	-1.39	-1.39	-1.39	5	-0.59	-0.60	-0.60	6	-0.59	-0.60	-0.60
	7	-1.24	-1.21	-1.24	8	-0.44	-0.43	-0.43	9	-0.48	-0.48	-0.48
	10	-0.45	-0.44	-0.45	11	-0.91	-0.91	-0.91	12	-0.48	-0.48	-0.48
	13	-0.45	-0.44	-0.45	14	-0.91	-0.91	-0.91	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.65	-0.65	-0.65	18	-0.96	-0.99	-0.99
	19	-0.65	-0.65	-0.65	20	-0.96	-0.99	-0.99	21	-0.94	-0.96	-0.96
Elem.		**Pt ini**	**Pt fin**	**Pt max**		**Pt ini**	**Pt fin**	**Pt max**		**Pt ini**	**Pt fin**	**Pt max**
		-1.73										
		0.14										

10.2. RISULTATI ELEMENTI TIPO TRAVE

Il controllo dei risultati delle analisi condotte, per quanto concerne gli elementi tipo trave, è possibile in relazione alle tabelle sottoriportate.

Gli elementi vengono suddivisi, in relazione alle proprietà in elementi:

- tipo **pilastro**
- tipo **trave in elevazione**

- tipo **trave in fondazione**

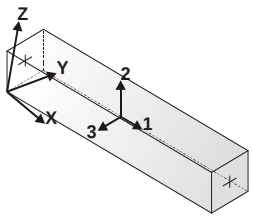
Per ogni elemento, e per ogni combinazione (o caso di carico) vengono riportati i risultati più significativi.

Per gli elementi tipo *pilastro* sono riportati in tabella i seguenti valori:

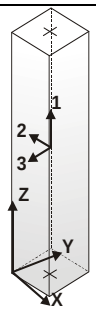
Pilas.	numero dell'elemento pilastro
Cmb	combinazione in cui si verificano i valori riportati
M3 mx/mn	momento flettente in campata M3 max (prima riga) / min (seconda riga)
M2 mx/mn	momento flettente in campata M2 max (prima riga) / min (seconda riga)
D2/D3	freccia massima in direzione 2 (prima riga) / direzione 3 (seconda riga)
Q2/Q3	carico totale in direzione 2 (prima riga) / direzione 3 (seconda riga)
Pos.	ascissa del punto iniziale e finale dell'elemento
N, V2, ecc..	sei componenti di sollecitazione al piede ed in sommità dell'elemento

Per gli elementi tipo *trave in elevazione* sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri.

Per gli elementi tipo *trave in fondazione* (trave f.) sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri e la massima pressione sul terreno.



orientamento elementi 2D non verticali



orientamento elementi 2D verticali

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		daN cm	daN cm	cm	daN	cm	daN	daN	daN	daN cm	daN cm	daN cm
11	1	-9.339e+05	0.0	6.33e-03	-449.28	0.0	-3.255e+04	6026.92	0.0	0.0	0.0	-1.021e+06
		-1.021e+06	0.0	0.0	0.0	15.0	-3.230e+04	5577.64	0.0	0.0	0.0	-9.339e+05
11	2	-6.910e+05	0.0	1.93e-03	-449.28	0.0	-1.814e+04	6623.74	0.0	0.0	0.0	-7.870e+05
		-7.870e+05	0.0	0.0	0.0	15.0	-1.789e+04	6174.46	0.0	0.0	0.0	-6.910e+05
11	3	-8.164e+05	0.0	5.62e-03	-449.28	0.0	-2.892e+04	5837.44	0.0	0.0	0.0	-9.006e+05
		-9.006e+05	0.0	0.0	0.0	15.0	-2.867e+04	5388.15	0.0	0.0	0.0	-8.164e+05
11	4	-6.346e+05	0.0	2.33e-03	-449.28	0.0	-1.814e+04	6283.94	0.0	0.0	0.0	-7.255e+05
		-7.255e+05	0.0	0.0	0.0	15.0	-1.789e+04	5834.66	0.0	0.0	0.0	-6.346e+05
11	5	-4.165e+06	0.0	-0.31	-979.96	0.0	-1.772e+04	2.456e+04	0.0	0.0	0.0	-4.526e+06
		-4.526e+06	0.0	0.0	0.0	15.0	-1.747e+04	2.358e+04	0.0	0.0	0.0	-4.165e+06
11	6	-4.259e+06	0.0	-0.33	-1096.41	0.0	-5930.65	2.806e+04	0.0	0.0	0.0	-4.671e+06
		-4.671e+06	0.0	0.0	0.0	15.0	-5677.52	2.696e+04	0.0	0.0	0.0	-4.259e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
11	7	-5.313e+06	0.0	-0.42	-1129.23	0.0	-3816.27	3.330e+04	0.0	0.0	0.0	-5.804e+06
		-5.804e+06	0.0	0.0	0.0	15.0	-3563.15	3.217e+04	0.0	0.0	0.0	-5.313e+06
11	8	-1.955e+06	0.0	-0.06	-979.96	0.0	-2.740e+04	1.682e+04	0.0	0.0	0.0	-2.200e+06
		-2.200e+06	0.0	0.0	0.0	15.0	-2.715e+04	1.584e+04	0.0	0.0	0.0	-1.955e+06
11	9	-2.049e+06	0.0	-0.08	-1096.41	0.0	-1.561e+04	2.032e+04	0.0	0.0	0.0	-2.345e+06
		-2.345e+06	0.0	0.0	0.0	15.0	-1.536e+04	1.922e+04	0.0	0.0	0.0	-2.049e+06
11	10	-3.103e+06	0.0	-0.17	-1129.23	0.0	-1.350e+04	2.556e+04	0.0	0.0	0.0	-3.478e+06
		-3.478e+06	0.0	0.0	0.0	15.0	-1.324e+04	2.443e+04	0.0	0.0	0.0	-3.103e+06
11	11	-9.360e+05	0.0	6.31e-03	-449.28	0.0	-3.255e+04	6034.25	0.0	0.0	0.0	-1.023e+06
		-1.023e+06	0.0	0.0	0.0	15.0	-3.230e+04	5584.97	0.0	0.0	0.0	-9.360e+05
11	12	-6.931e+05	0.0	1.92e-03	-449.28	0.0	-1.814e+04	6631.07	0.0	0.0	0.0	-7.891e+05
		-7.891e+05	0.0	0.0	0.0	15.0	-1.789e+04	6181.79	0.0	0.0	0.0	-6.931e+05
11	13	-1.017e+06	0.0	4.19e-03	-449.28	0.0	-2.892e+04	7250.36	0.0	0.0	0.0	-1.123e+06
		-1.123e+06	0.0	0.0	0.0	15.0	-2.867e+04	6801.08	0.0	0.0	0.0	-1.017e+06
11	14	-8.355e+05	0.0	-9.02e-04	-449.28	0.0	-1.814e+04	7696.87	0.0	0.0	0.0	-9.476e+05
		-9.476e+05	0.0	0.0	0.0	15.0	-1.789e+04	7247.59	0.0	0.0	0.0	-8.355e+05
11	15	-4.077e+06	0.0	-0.31	-979.96	0.0	-1.772e+04	2.383e+04	0.0	0.0	0.0	-4.427e+06
		-4.427e+06	0.0	0.0	0.0	15.0	-1.747e+04	2.285e+04	0.0	0.0	0.0	-4.077e+06
11	16	-4.171e+06	0.0	-0.33	-1096.41	0.0	-5930.65	2.733e+04	0.0	0.0	0.0	-4.572e+06
		-4.572e+06	0.0	0.0	0.0	15.0	-5677.52	2.623e+04	0.0	0.0	0.0	-4.171e+06
11	17	-5.225e+06	0.0	-0.42	-1129.23	0.0	-3816.27	3.256e+04	0.0	0.0	0.0	-5.705e+06
		-5.705e+06	0.0	0.0	0.0	15.0	-3563.15	3.144e+04	0.0	0.0	0.0	-5.225e+06
11	18	-1.898e+06	0.0	-0.06	-979.96	0.0	-2.740e+04	1.662e+04	0.0	0.0	0.0	-2.140e+06
		-2.140e+06	0.0	0.0	0.0	15.0	-2.715e+04	1.564e+04	0.0	0.0	0.0	-1.898e+06
11	19	-1.991e+06	0.0	-0.08	-1096.41	0.0	-1.561e+04	2.012e+04	0.0	0.0	0.0	-2.285e+06
		-2.285e+06	0.0	0.0	0.0	15.0	-1.536e+04	1.902e+04	0.0	0.0	0.0	-1.991e+06
11	20	-3.045e+06	0.0	-0.17	-1129.23	0.0	-1.350e+04	2.536e+04	0.0	0.0	0.0	-3.417e+06
		-3.417e+06	0.0	0.0	0.0	15.0	-1.324e+04	2.423e+04	0.0	0.0	0.0	-3.045e+06
11	21	-4.163e+06	0.0	-0.35	-979.96	0.0	-1.422e+04	2.473e+04	0.0	0.0	0.0	-4.527e+06
		-4.527e+06	0.0	0.0	0.0	15.0	-1.397e+04	2.375e+04	0.0	0.0	0.0	-4.163e+06
11	22	-1.898e+06	0.0	-0.10	-979.96	0.0	-2.390e+04	1.679e+04	0.0	0.0	0.0	-2.142e+06
		-2.142e+06	0.0	0.0	0.0	15.0	-2.365e+04	1.581e+04	0.0	0.0	0.0	-1.898e+06
11	23	-5.114e+06	0.0	-0.42	-1129.23	0.0	886.85	3.245e+04	0.0	0.0	0.0	-5.593e+06
		-5.593e+06	0.0	0.0	0.0	15.0	1074.35	3.132e+04	0.0	0.0	0.0	-5.114e+06
11	24	-2.791e+06	0.0	-0.17	-1129.23	0.0	-8791.93	2.403e+04	0.0	0.0	0.0	-3.143e+06
		-3.143e+06	0.0	0.0	0.0	15.0	-8604.43	2.290e+04	0.0	0.0	0.0	-2.791e+06
11	25	-4.121e+06	0.0	-0.27	-979.96	0.0	-2.123e+04	2.422e+04	0.0	0.0	0.0	-4.477e+06
		-4.477e+06	0.0	0.0	0.0	15.0	-2.097e+04	2.324e+04	0.0	0.0	0.0	-4.121e+06
11	26	-4.174e+06	0.0	-0.33	-1096.41	0.0	-5930.65	2.755e+04	0.0	0.0	0.0	-4.579e+06
		-4.579e+06	0.0	0.0	0.0	15.0	-5677.52	2.645e+04	0.0	0.0	0.0	-4.174e+06
11	27	-1.958e+06	0.0	-0.12	-979.96	0.0	-2.635e+04	1.655e+04	0.0	0.0	0.0	-2.199e+06
		-2.199e+06	0.0	0.0	0.0	15.0	-2.610e+04	1.557e+04	0.0	0.0	0.0	-1.958e+06
11	28	-1.990e+06	0.0	-0.08	-1096.41	0.0	-1.561e+04	1.997e+04	0.0	0.0	0.0	-2.282e+06
		-2.282e+06	0.0	0.0	0.0	15.0	-1.536e+04	1.888e+04	0.0	0.0	0.0	-1.990e+06
11	29	-5.225e+06	0.0	-0.42	-1129.23	0.0	-3816.27	3.256e+04	0.0	0.0	0.0	-5.705e+06
		-5.705e+06	0.0	0.0	0.0	15.0	-3563.15	3.144e+04	0.0	0.0	0.0	-5.225e+06
11	30	-3.435e+06	0.0	-0.25	-979.96	0.0	-1.454e+04	2.242e+04	0.0	0.0	0.0	-3.764e+06
		-3.764e+06	0.0	0.0	0.0	15.0	-1.435e+04	2.144e+04	0.0	0.0	0.0	-3.435e+06
11	31	-2.994e+06	0.0	-0.22	-1096.41	0.0	-3720.02	2.435e+04	0.0	0.0	0.0	-3.351e+06
		-3.351e+06	0.0	0.0	0.0	15.0	-3532.52	2.325e+04	0.0	0.0	0.0	-2.994e+06
11	32	-3.553e+06	0.0	-0.25	-1129.23	0.0	-3758.72	2.767e+04	0.0	0.0	0.0	-3.960e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-3.960e+06	0.0	0.0	0.0	15.0	-3571.22	2.655e+04	0.0	0.0	0.0	-3.553e+06
11	33	-5.394e+06	0.0	-0.42	-1129.23	0.0	-3816.27	3.358e+04	0.0	0.0	0.0	-5.889e+06
		-5.889e+06	0.0	0.0	0.0	15.0	-3563.15	3.246e+04	0.0	0.0	0.0	-5.394e+06
11	34	-6.923e+05	0.0	3.45e-03	-449.28	0.0	-2.144e+04	6009.09	0.0	0.0	0.0	-7.791e+05
		-7.791e+05	0.0	0.0	0.0	15.0	-2.126e+04	5559.81	0.0	0.0	0.0	-6.923e+05
11	35	-7.619e+05	0.0	-0.01	-535.76	0.0	-1.269e+04	8605.97	0.0	0.0	0.0	-8.869e+05
		-8.869e+05	0.0	0.0	0.0	15.0	-1.250e+04	8070.21	0.0	0.0	0.0	-7.619e+05
11	36	-1.310e+06	0.0	-0.03	-725.89	0.0	-2.065e+04	1.175e+04	0.0	0.0	0.0	-1.481e+06
		-1.481e+06	0.0	0.0	0.0	15.0	-2.046e+04	1.102e+04	0.0	0.0	0.0	-1.310e+06
11	37	-1.380e+06	0.0	-0.05	-812.37	0.0	-1.189e+04	1.434e+04	0.0	0.0	0.0	-1.589e+06
		-1.589e+06	0.0	0.0	0.0	15.0	-1.171e+04	1.353e+04	0.0	0.0	0.0	-1.380e+06
11	38	-2.162e+06	0.0	-0.11	-836.74	0.0	-1.032e+04	1.823e+04	0.0	0.0	0.0	-2.430e+06
		-2.430e+06	0.0	0.0	0.0	15.0	-1.014e+04	1.740e+04	0.0	0.0	0.0	-2.162e+06
11	39	-7.521e+05	0.0	3.02e-03	-449.28	0.0	-2.144e+04	6513.26	0.0	0.0	0.0	-8.464e+05
		-8.464e+05	0.0	0.0	0.0	15.0	-2.126e+04	6063.98	0.0	0.0	0.0	-7.521e+05
11	40	-6.171e+05	0.0	-5.76e-04	-449.28	0.0	-1.344e+04	6844.82	0.0	0.0	0.0	-7.164e+05
		-7.164e+05	0.0	0.0	0.0	15.0	-1.325e+04	6395.54	0.0	0.0	0.0	-6.171e+05
11	41	-1.250e+06	0.0	-0.03	-725.89	0.0	-2.065e+04	1.124e+04	0.0	0.0	0.0	-1.414e+06
		-1.414e+06	0.0	0.0	0.0	15.0	-2.046e+04	1.052e+04	0.0	0.0	0.0	-1.250e+06
11	42	-1.320e+06	0.0	-0.05	-812.37	0.0	-1.189e+04	1.384e+04	0.0	0.0	0.0	-1.521e+06
		-1.521e+06	0.0	0.0	0.0	15.0	-1.171e+04	1.303e+04	0.0	0.0	0.0	-1.320e+06
11	43	-2.103e+06	0.0	-0.11	-836.74	0.0	-1.032e+04	1.773e+04	0.0	0.0	0.0	-2.362e+06
		-2.362e+06	0.0	0.0	0.0	15.0	-1.014e+04	1.689e+04	0.0	0.0	0.0	-2.103e+06
11	44	-2.238e+06	0.0	-0.14	-836.74	0.0	-1.573e+04	1.753e+04	0.0	0.0	0.0	-2.494e+06
		-2.494e+06	0.0	0.0	0.0	15.0	-1.554e+04	1.669e+04	0.0	0.0	0.0	-2.238e+06
11	45	-2.033e+06	0.0	-0.11	-836.74	0.0	-1.032e+04	1.749e+04	0.0	0.0	0.0	-2.289e+06
		-2.289e+06	0.0	0.0	0.0	15.0	-1.014e+04	1.665e+04	0.0	0.0	0.0	-2.033e+06
11	46	-7.612e+05	0.0	4.09e-03	-449.28	0.0	-2.411e+04	6100.23	0.0	0.0	0.0	-8.494e+05
		-8.494e+05	0.0	0.0	0.0	15.0	-2.393e+04	5650.95	0.0	0.0	0.0	-7.612e+05
11	47	-5.813e+05	0.0	-8.36e-04	-449.28	0.0	-1.344e+04	6542.32	0.0	0.0	0.0	-6.760e+05
		-6.760e+05	0.0	0.0	0.0	15.0	-1.325e+04	6093.04	0.0	0.0	0.0	-5.813e+05
11	48	-6.693e+05	0.0	3.61e-03	-449.28	0.0	-2.144e+04	5927.60	0.0	0.0	0.0	-7.548e+05
		-7.548e+05	0.0	0.0	0.0	15.0	-2.126e+04	5478.31	0.0	0.0	0.0	-6.693e+05
11	49	-5.343e+05	0.0	-1.16e-03	-449.28	0.0	-1.344e+04	6259.16	0.0	0.0	0.0	-6.248e+05
		-6.248e+05	0.0	0.0	0.0	15.0	-1.325e+04	5809.88	0.0	0.0	0.0	-5.343e+05
11	50	-2.957e+06	0.0	-0.22	-725.89	0.0	-1.348e+04	1.780e+04	0.0	0.0	0.0	-3.219e+06
		-3.219e+06	0.0	0.0	0.0	15.0	-1.329e+04	1.707e+04	0.0	0.0	0.0	-2.957e+06
11	51	-3.027e+06	0.0	-0.23	-812.37	0.0	-4724.96	2.039e+04	0.0	0.0	0.0	-3.327e+06
		-3.327e+06	0.0	0.0	0.0	15.0	-4537.46	1.958e+04	0.0	0.0	0.0	-3.027e+06
11	52	-3.810e+06	0.0	-0.30	-836.74	0.0	-3154.88	2.428e+04	0.0	0.0	0.0	-4.168e+06
		-4.168e+06	0.0	0.0	0.0	15.0	-2967.38	2.345e+04	0.0	0.0	0.0	-3.810e+06
11	53	-1.326e+06	0.0	-0.03	-725.89	0.0	-2.065e+04	1.209e+04	0.0	0.0	0.0	-1.501e+06
		-1.501e+06	0.0	0.0	0.0	15.0	-2.046e+04	1.137e+04	0.0	0.0	0.0	-1.326e+06
11	54	-1.395e+06	0.0	-0.05	-812.37	0.0	-1.189e+04	1.469e+04	0.0	0.0	0.0	-1.609e+06
		-1.609e+06	0.0	0.0	0.0	15.0	-1.171e+04	1.388e+04	0.0	0.0	0.0	-1.395e+06
11	55	-2.178e+06	0.0	-0.11	-836.74	0.0	-1.032e+04	1.858e+04	0.0	0.0	0.0	-2.450e+06
		-2.450e+06	0.0	0.0	0.0	15.0	-1.014e+04	1.775e+04	0.0	0.0	0.0	-2.178e+06
11	56	-8.304e+05	0.0	3.62e-03	-449.28	0.0	-2.411e+04	6344.71	0.0	0.0	0.0	-9.222e+05
		-9.222e+05	0.0	0.0	0.0	15.0	-2.393e+04	5895.43	0.0	0.0	0.0	-8.304e+05
11	57	-6.505e+05	0.0	-3.68e-04	-449.28	0.0	-1.344e+04	6786.80	0.0	0.0	0.0	-7.489e+05
		-7.489e+05	0.0	0.0	0.0	15.0	-1.325e+04	6337.52	0.0	0.0	0.0	-6.505e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
11	58	-7.846e+05	0.0	2.83e-03	-449.28	0.0	-2.144e+04	6335.06	0.0	0.0	0.0	-8.762e+05
		-8.762e+05	0.0	0.0	0.0	15.0	-2.126e+04	5885.78	0.0	0.0	0.0	-7.846e+05
11	59	-6.496e+05	0.0	-3.85e-04	-449.28	0.0	-1.344e+04	6666.63	0.0	0.0	0.0	-7.462e+05
		-7.462e+05	0.0	0.0	0.0	15.0	-1.325e+04	6217.35	0.0	0.0	0.0	-6.496e+05
11	60	-2.956e+06	0.0	-0.22	-725.89	0.0	-1.348e+04	1.779e+04	0.0	0.0	0.0	-3.217e+06
		-3.217e+06	0.0	0.0	0.0	15.0	-1.329e+04	1.706e+04	0.0	0.0	0.0	-2.956e+06
11	61	-3.025e+06	0.0	-0.23	-812.37	0.0	-4724.96	2.039e+04	0.0	0.0	0.0	-3.325e+06
		-3.325e+06	0.0	0.0	0.0	15.0	-4537.46	1.957e+04	0.0	0.0	0.0	-3.025e+06
11	62	-3.808e+06	0.0	-0.30	-836.74	0.0	-3154.88	2.428e+04	0.0	0.0	0.0	-4.166e+06
		-4.166e+06	0.0	0.0	0.0	15.0	-2967.38	2.344e+04	0.0	0.0	0.0	-3.808e+06
11	63	-1.278e+06	0.0	-0.03	-725.89	0.0	-2.065e+04	1.193e+04	0.0	0.0	0.0	-1.451e+06
		-1.451e+06	0.0	0.0	0.0	15.0	-2.046e+04	1.120e+04	0.0	0.0	0.0	-1.278e+06
11	64	-1.347e+06	0.0	-0.05	-812.37	0.0	-1.189e+04	1.452e+04	0.0	0.0	0.0	-1.559e+06
		-1.559e+06	0.0	0.0	0.0	15.0	-1.171e+04	1.371e+04	0.0	0.0	0.0	-1.347e+06
11	65	-2.130e+06	0.0	-0.11	-836.74	0.0	-1.032e+04	1.841e+04	0.0	0.0	0.0	-2.400e+06
		-2.400e+06	0.0	0.0	0.0	15.0	-1.014e+04	1.758e+04	0.0	0.0	0.0	-2.130e+06
11	66	-2.956e+06	0.0	-0.25	-725.89	0.0	-1.088e+04	1.792e+04	0.0	0.0	0.0	-3.219e+06
		-3.219e+06	0.0	0.0	0.0	15.0	-1.069e+04	1.719e+04	0.0	0.0	0.0	-2.956e+06
11	67	-1.278e+06	0.0	-0.06	-725.89	0.0	-1.805e+04	1.205e+04	0.0	0.0	0.0	-1.453e+06
		-1.453e+06	0.0	0.0	0.0	15.0	-1.786e+04	1.133e+04	0.0	0.0	0.0	-1.278e+06
11	68	-3.736e+06	0.0	-0.30	-836.74	0.0	-3154.88	2.367e+04	0.0	0.0	0.0	-4.085e+06
		-4.085e+06	0.0	0.0	0.0	15.0	-2967.38	2.284e+04	0.0	0.0	0.0	-3.736e+06
11	69	-2.010e+06	0.0	-0.11	-836.74	0.0	-1.032e+04	1.740e+04	0.0	0.0	0.0	-2.265e+06
		-2.265e+06	0.0	0.0	0.0	15.0	-1.014e+04	1.657e+04	0.0	0.0	0.0	-2.010e+06
11	70	-5.631e+05	0.0	-9.70e-04	-449.28	0.0	-1.344e+04	6361.03	0.0	0.0	0.0	-6.552e+05
		-6.552e+05	0.0	0.0	0.0	15.0	-1.325e+04	5911.75	0.0	0.0	0.0	-5.631e+05
11	71	-1.169e+06	0.0	-0.03	-725.89	0.0	-1.264e+04	1.206e+04	0.0	0.0	0.0	-1.345e+06
		-1.345e+06	0.0	0.0	0.0	15.0	-1.246e+04	1.133e+04	0.0	0.0	0.0	-1.169e+06
11	72	-6.229e+05	0.0	-5.37e-04	-449.28	0.0	-1.344e+04	6865.20	0.0	0.0	0.0	-7.225e+05
		-7.225e+05	0.0	0.0	0.0	15.0	-1.325e+04	6415.91	0.0	0.0	0.0	-6.229e+05
11	73	-1.110e+06	0.0	-0.03	-725.89	0.0	-1.264e+04	1.155e+04	0.0	0.0	0.0	-1.277e+06
		-1.277e+06	0.0	0.0	0.0	15.0	-1.246e+04	1.083e+04	0.0	0.0	0.0	-1.110e+06
11	74	-1.052e+06	0.0	-0.03	-725.89	0.0	-1.264e+04	1.135e+04	0.0	0.0	0.0	-1.217e+06
		-1.217e+06	0.0	0.0	0.0	15.0	-1.246e+04	1.062e+04	0.0	0.0	0.0	-1.052e+06
12	1	1.021e+06	0.0	-6.33e-03	449.28	0.0	-3.255e+04	-6026.92	0.0	0.0	0.0	1.021e+06
		9.339e+05	0.0	0.0	0.0	15.0	-3.230e+04	-5577.64	0.0	0.0	0.0	9.339e+05
12	2	7.870e+05	0.0	-1.93e-03	449.28	0.0	-1.814e+04	-6623.74	0.0	0.0	0.0	7.870e+05
		6.910e+05	0.0	0.0	0.0	15.0	-1.789e+04	-6174.46	0.0	0.0	0.0	6.910e+05
12	3	9.006e+05	0.0	-5.62e-03	449.28	0.0	-2.892e+04	-5837.44	0.0	0.0	0.0	9.006e+05
		8.164e+05	0.0	0.0	0.0	15.0	-2.867e+04	-5388.15	0.0	0.0	0.0	8.164e+05
12	4	7.255e+05	0.0	-2.33e-03	449.28	0.0	-1.814e+04	-6283.94	0.0	0.0	0.0	7.255e+05
		6.346e+05	0.0	0.0	0.0	15.0	-1.789e+04	-5834.66	0.0	0.0	0.0	6.346e+05
12	5	-1.926e+06	0.0	-0.32	449.28	0.0	-4.012e+04	3193.97	0.0	0.0	0.0	-1.977e+06
		-1.977e+06	0.0	0.0	0.0	15.0	-3.987e+04	3643.26	0.0	0.0	0.0	-1.926e+06
12	6	-2.633e+06	0.0	-0.33	449.28	0.0	-3.035e+04	4316.34	0.0	0.0	0.0	-2.701e+06
		-2.701e+06	0.0	0.0	0.0	15.0	-3.010e+04	4765.62	0.0	0.0	0.0	-2.633e+06
12	7	-3.137e+06	0.0	-0.42	449.28	0.0	-3.246e+04	6227.68	0.0	0.0	0.0	-3.234e+06
		-3.234e+06	0.0	0.0	0.0	15.0	-3.221e+04	6676.96	0.0	0.0	0.0	-3.137e+06
12	8	4.723e+05	0.0	-0.07	449.28	0.0	-3.044e+04	-5225.94	0.0	0.0	0.0	4.723e+05
		3.973e+05	0.0	0.0	0.0	15.0	-3.019e+04	-4776.65	0.0	0.0	0.0	3.973e+05
12	9	-2.514e+05	0.0	-0.08	449.28	0.0	-2.067e+04	-4103.57	0.0	0.0	0.0	-2.514e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-3.096e+05	0.0	0.0	0.0	15.0	-2.042e+04	-3654.29	0.0	0.0	0.0	-3.096e+05
12	10	-7.844e+05	0.0	-0.17	449.28	0.0	-2.279e+04	-2192.23	0.0	0.0	0.0	-7.844e+05
		-8.139e+05	0.0	0.0	0.0	15.0	-2.253e+04	-1742.95	0.0	0.0	0.0	-8.139e+05
12	11	1.023e+06	0.0	-6.31e-03	449.28	0.0	-3.255e+04	-6034.25	0.0	0.0	0.0	1.023e+06
		9.360e+05	0.0	0.0	0.0	15.0	-3.230e+04	-5584.97	0.0	0.0	0.0	9.360e+05
12	12	7.891e+05	0.0	-1.92e-03	449.28	0.0	-1.814e+04	-6631.07	0.0	0.0	0.0	7.891e+05
		6.931e+05	0.0	0.0	0.0	15.0	-1.789e+04	-6181.79	0.0	0.0	0.0	6.931e+05
12	13	1.123e+06	0.0	-4.19e-03	449.28	0.0	-2.892e+04	-7250.36	0.0	0.0	0.0	1.123e+06
		1.017e+06	0.0	0.0	0.0	15.0	-2.867e+04	-6801.08	0.0	0.0	0.0	1.017e+06
12	14	9.476e+05	0.0	9.02e-04	449.28	0.0	-1.814e+04	-7696.87	0.0	0.0	0.0	9.476e+05
		8.355e+05	0.0	0.0	0.0	15.0	-1.789e+04	-7247.59	0.0	0.0	0.0	8.355e+05
12	15	-2.014e+06	0.0	-0.32	449.28	0.0	-4.012e+04	3927.31	0.0	0.0	0.0	-2.076e+06
		-2.076e+06	0.0	0.0	0.0	15.0	-3.987e+04	4376.59	0.0	0.0	0.0	-2.014e+06
12	16	-2.721e+06	0.0	-0.33	449.28	0.0	-3.035e+04	5049.67	0.0	0.0	0.0	-2.800e+06
		-2.800e+06	0.0	0.0	0.0	15.0	-3.010e+04	5498.96	0.0	0.0	0.0	-2.721e+06
12	17	-3.225e+06	0.0	-0.42	449.28	0.0	-3.246e+04	6961.02	0.0	0.0	0.0	-3.333e+06
		-3.333e+06	0.0	0.0	0.0	15.0	-3.221e+04	7410.30	0.0	0.0	0.0	-3.225e+06
12	18	4.118e+05	0.0	-0.07	449.28	0.0	-3.044e+04	-5023.02	0.0	0.0	0.0	4.118e+05
		3.399e+05	0.0	0.0	0.0	15.0	-3.019e+04	-4573.74	0.0	0.0	0.0	3.399e+05
12	19	-3.119e+05	0.0	-0.08	449.28	0.0	-2.067e+04	-3900.65	0.0	0.0	0.0	-3.119e+05
		-3.670e+05	0.0	0.0	0.0	15.0	-2.042e+04	-3451.37	0.0	0.0	0.0	-3.670e+05
12	20	-8.449e+05	0.0	-0.17	449.28	0.0	-2.279e+04	-1989.31	0.0	0.0	0.0	-8.449e+05
		-8.713e+05	0.0	0.0	0.0	15.0	-2.253e+04	-1540.03	0.0	0.0	0.0	-8.713e+05
12	21	-1.887e+06	0.0	-0.36	449.28	0.0	-4.362e+04	3029.96	0.0	0.0	0.0	-1.936e+06
		-1.936e+06	0.0	0.0	0.0	15.0	-4.337e+04	3479.24	0.0	0.0	0.0	-1.887e+06
12	22	4.551e+05	0.0	-0.11	449.28	0.0	-3.395e+04	-5194.36	0.0	0.0	0.0	4.551e+05
		3.805e+05	0.0	0.0	0.0	15.0	-3.369e+04	-4745.08	0.0	0.0	0.0	3.805e+05
12	23	-3.335e+06	0.0	-0.42	449.28	0.0	-2.776e+04	7079.71	0.0	0.0	0.0	-3.445e+06
		-3.445e+06	0.0	0.0	0.0	15.0	-2.757e+04	7528.99	0.0	0.0	0.0	-3.335e+06
12	24	-1.119e+06	0.0	-0.17	449.28	0.0	-1.808e+04	-660.62	0.0	0.0	0.0	-1.119e+06
		-1.125e+06	0.0	0.0	0.0	15.0	-1.790e+04	-211.33	0.0	0.0	0.0	-1.125e+06
12	25	-2.010e+06	0.0	-0.27	449.28	0.0	-3.662e+04	3532.32	0.0	0.0	0.0	-2.067e+06
		-2.067e+06	0.0	0.0	0.0	15.0	-3.637e+04	3981.60	0.0	0.0	0.0	-2.010e+06
12	26	-2.717e+06	0.0	-0.33	449.28	0.0	-3.035e+04	4826.03	0.0	0.0	0.0	-2.793e+06
		-2.793e+06	0.0	0.0	0.0	15.0	-3.010e+04	5275.31	0.0	0.0	0.0	-2.717e+06
12	27	5.254e+05	0.0	-0.13	449.28	0.0	-3.875e+04	-4957.53	0.0	0.0	0.0	5.254e+05
		4.544e+05	0.0	0.0	0.0	15.0	-3.850e+04	-4508.25	0.0	0.0	0.0	4.544e+05
12	28	-3.151e+05	0.0	-0.08	449.28	0.0	-2.067e+04	-3756.45	0.0	0.0	0.0	-3.151e+05
		-3.680e+05	0.0	0.0	0.0	15.0	-2.042e+04	-3307.16	0.0	0.0	0.0	-3.680e+05
12	29	-3.225e+06	0.0	-0.42	449.28	0.0	-3.246e+04	6961.02	0.0	0.0	0.0	-3.333e+06
		-3.333e+06	0.0	0.0	0.0	15.0	-3.221e+04	7410.30	0.0	0.0	0.0	-3.225e+06
12	30	-1.012e+06	0.0	-0.25	979.96	0.0	-3.390e+04	-6258.85	0.0	0.0	0.0	-1.012e+06
		-1.098e+06	0.0	0.0	0.0	15.0	-3.371e+04	-5278.90	0.0	0.0	0.0	-1.098e+06
12	31	-1.405e+06	0.0	-0.20	1096.41	0.0	-2.315e+04	-8187.12	0.0	0.0	0.0	-1.405e+06
		-1.520e+06	0.0	0.0	0.0	15.0	-2.297e+04	-7090.71	0.0	0.0	0.0	-1.520e+06
12	32	-8.158e+05	0.0	-0.24	1129.23	0.0	-2.312e+04	-1.152e+04	0.0	0.0	0.0	-8.158e+05
		-9.801e+05	0.0	0.0	0.0	15.0	-2.293e+04	-1.039e+04	0.0	0.0	0.0	-9.801e+05
12	33	-3.056e+06	0.0	-0.42	449.28	0.0	-3.246e+04	5941.64	0.0	0.0	0.0	-3.148e+06
		-3.148e+06	0.0	0.0	0.0	15.0	-3.221e+04	6390.92	0.0	0.0	0.0	-3.056e+06
12	34	7.791e+05	0.0	-3.45e-03	449.28	0.0	-2.144e+04	-6009.09	0.0	0.0	0.0	7.791e+05
		6.923e+05	0.0	0.0	0.0	15.0	-2.126e+04	-5559.81	0.0	0.0	0.0	6.923e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
12	35	2.417e+05	0.0	-0.01	449.28	0.0	-1.419e+04	-5175.65	0.0	0.0	0.0	2.417e+05
		1.674e+05	0.0	0.0	0.0	15.0	-1.400e+04	-4726.37	0.0	0.0	0.0	1.674e+05
12	36	5.803e+05	0.0	-0.04	449.28	0.0	-2.224e+04	-5702.52	0.0	0.0	0.0	5.803e+05
		4.981e+05	0.0	0.0	0.0	15.0	-2.205e+04	-5253.24	0.0	0.0	0.0	4.981e+05
12	37	4.289e+04	0.0	-0.04	449.28	0.0	-1.498e+04	-4869.09	0.0	0.0	0.0	4.289e+04
		-2.676e+04	0.0	0.0	0.0	15.0	-1.479e+04	-4419.81	0.0	0.0	0.0	-2.676e+04
12	38	-3.529e+05	0.0	-0.11	449.28	0.0	-1.655e+04	-3449.77	0.0	0.0	0.0	-3.529e+05
		-4.013e+05	0.0	0.0	0.0	15.0	-1.636e+04	-3000.49	0.0	0.0	0.0	-4.013e+05
12	39	8.464e+05	0.0	-3.02e-03	449.28	0.0	-2.144e+04	-6513.26	0.0	0.0	0.0	8.464e+05
		7.521e+05	0.0	0.0	0.0	15.0	-2.126e+04	-6063.98	0.0	0.0	0.0	7.521e+05
12	40	7.164e+05	0.0	5.76e-04	449.28	0.0	-1.344e+04	-6844.82	0.0	0.0	0.0	7.164e+05
		6.171e+05	0.0	0.0	0.0	15.0	-1.325e+04	-6395.54	0.0	0.0	0.0	6.171e+05
12	41	5.130e+05	0.0	-0.04	449.28	0.0	-2.224e+04	-5198.36	0.0	0.0	0.0	5.130e+05
		4.384e+05	0.0	0.0	0.0	15.0	-2.205e+04	-4749.07	0.0	0.0	0.0	4.384e+05
12	42	-2.446e+04	0.0	-0.04	449.28	0.0	-1.498e+04	-4364.92	0.0	0.0	0.0	-2.446e+04
		-8.655e+04	0.0	0.0	0.0	15.0	-1.479e+04	-3915.64	0.0	0.0	0.0	-8.655e+04
12	43	-4.202e+05	0.0	-0.11	449.28	0.0	-1.655e+04	-2945.60	0.0	0.0	0.0	-4.202e+05
		-4.610e+05	0.0	0.0	0.0	15.0	-1.636e+04	-2496.32	0.0	0.0	0.0	-4.610e+05
12	44	-2.581e+05	0.0	-0.15	449.28	0.0	-2.716e+04	-2741.28	0.0	0.0	0.0	-2.581e+05
		-2.959e+05	0.0	0.0	0.0	15.0	-2.697e+04	-2291.99	0.0	0.0	0.0	-2.959e+05
12	45	-4.931e+05	0.0	-0.11	449.28	0.0	-1.655e+04	-2701.12	0.0	0.0	0.0	-4.931e+05
		-5.302e+05	0.0	0.0	0.0	15.0	-1.636e+04	-2251.84	0.0	0.0	0.0	-5.302e+05
12	46	8.494e+05	0.0	-4.09e-03	449.28	0.0	-2.411e+04	-6100.23	0.0	0.0	0.0	8.494e+05
		7.612e+05	0.0	0.0	0.0	15.0	-2.393e+04	-5650.95	0.0	0.0	0.0	7.612e+05
12	47	6.760e+05	0.0	8.36e-04	449.28	0.0	-1.344e+04	-6542.32	0.0	0.0	0.0	6.760e+05
		5.813e+05	0.0	0.0	0.0	15.0	-1.325e+04	-6093.04	0.0	0.0	0.0	5.813e+05
12	48	7.548e+05	0.0	-3.61e-03	449.28	0.0	-2.144e+04	-5927.60	0.0	0.0	0.0	7.548e+05
		6.693e+05	0.0	0.0	0.0	15.0	-2.126e+04	-5478.31	0.0	0.0	0.0	6.693e+05
12	49	6.248e+05	0.0	1.16e-03	449.28	0.0	-1.344e+04	-6259.16	0.0	0.0	0.0	6.248e+05
		5.343e+05	0.0	0.0	0.0	15.0	-1.325e+04	-5809.88	0.0	0.0	0.0	5.343e+05
12	50	-1.212e+06	0.0	-0.22	449.28	0.0	-2.941e+04	218.61	0.0	0.0	0.0	-1.219e+06
		-1.219e+06	0.0	0.0	0.0	15.0	-2.922e+04	667.90	0.0	0.0	0.0	-1.212e+06
12	51	-1.737e+06	0.0	-0.23	449.28	0.0	-2.215e+04	1052.05	0.0	0.0	0.0	-1.757e+06
		-1.757e+06	0.0	0.0	0.0	15.0	-2.196e+04	1501.33	0.0	0.0	0.0	-1.737e+06
12	52	-2.112e+06	0.0	-0.29	449.28	0.0	-2.372e+04	2471.37	0.0	0.0	0.0	-2.152e+06
		-2.152e+06	0.0	0.0	0.0	15.0	-2.353e+04	2920.65	0.0	0.0	0.0	-2.112e+06
12	53	6.009e+05	0.0	-0.04	449.28	0.0	-2.224e+04	-6049.82	0.0	0.0	0.0	6.009e+05
		5.135e+05	0.0	0.0	0.0	15.0	-2.205e+04	-5600.54	0.0	0.0	0.0	5.135e+05
12	54	6.349e+04	0.0	-0.04	449.28	0.0	-1.498e+04	-5216.38	0.0	0.0	0.0	6.349e+04
		-1.138e+04	0.0	0.0	0.0	15.0	-1.479e+04	-4767.10	0.0	0.0	0.0	-1.138e+04
12	55	-3.323e+05	0.0	-0.11	449.28	0.0	-1.655e+04	-3797.07	0.0	0.0	0.0	-3.323e+05
		-3.859e+05	0.0	0.0	0.0	15.0	-1.636e+04	-3347.78	0.0	0.0	0.0	-3.859e+05
12	56	9.222e+05	0.0	-3.62e-03	449.28	0.0	-2.411e+04	-6344.71	0.0	0.0	0.0	9.222e+05
		8.304e+05	0.0	0.0	0.0	15.0	-2.393e+04	-5895.43	0.0	0.0	0.0	8.304e+05
12	57	7.489e+05	0.0	3.68e-04	449.28	0.0	-1.344e+04	-6786.80	0.0	0.0	0.0	7.489e+05
		6.505e+05	0.0	0.0	0.0	15.0	-1.325e+04	-6337.52	0.0	0.0	0.0	6.505e+05
12	58	8.762e+05	0.0	-2.83e-03	449.28	0.0	-2.144e+04	-6335.06	0.0	0.0	0.0	8.762e+05
		7.846e+05	0.0	0.0	0.0	15.0	-2.126e+04	-5885.78	0.0	0.0	0.0	7.846e+05
12	59	7.462e+05	0.0	3.85e-04	449.28	0.0	-1.344e+04	-6666.63	0.0	0.0	0.0	7.462e+05
		6.496e+05	0.0	0.0	0.0	15.0	-1.325e+04	-6217.35	0.0	0.0	0.0	6.496e+05
12	60	-1.214e+06	0.0	-0.22	449.28	0.0	-2.941e+04	224.73	0.0	0.0	0.0	-1.221e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-1.221e+06	0.0	0.0	0.0	15.0	-2.922e+04	674.01	0.0	0.0	0.0	-1.214e+06
12	61	-1.739e+06	0.0	-0.23	449.28	0.0	-2.215e+04	1058.16	0.0	0.0	0.0	-1.758e+06
		-1.758e+06	0.0	0.0	0.0	15.0	-2.196e+04	1507.45	0.0	0.0	0.0	-1.739e+06
12	62	-2.114e+06	0.0	-0.29	449.28	0.0	-2.372e+04	2477.48	0.0	0.0	0.0	-2.154e+06
		-2.154e+06	0.0	0.0	0.0	15.0	-2.353e+04	2926.76	0.0	0.0	0.0	-2.114e+06
12	63	5.505e+05	0.0	-0.04	449.28	0.0	-2.224e+04	-5880.72	0.0	0.0	0.0	5.505e+05
		4.657e+05	0.0	0.0	0.0	15.0	-2.205e+04	-5431.44	0.0	0.0	0.0	4.657e+05
12	64	1.309e+04	0.0	-0.04	449.28	0.0	-1.498e+04	-5047.28	0.0	0.0	0.0	1.309e+04
		-5.924e+04	0.0	0.0	0.0	15.0	-1.479e+04	-4598.00	0.0	0.0	0.0	-5.924e+04
12	65	-3.827e+05	0.0	-0.11	449.28	0.0	-1.655e+04	-3627.97	0.0	0.0	0.0	-3.827e+05
		-4.337e+05	0.0	0.0	0.0	15.0	-1.636e+04	-3178.68	0.0	0.0	0.0	-4.337e+05
12	66	-1.184e+06	0.0	-0.25	449.28	0.0	-3.201e+04	97.49	0.0	0.0	0.0	-1.189e+06
		-1.189e+06	0.0	0.0	0.0	15.0	-3.182e+04	546.77	0.0	0.0	0.0	-1.184e+06
12	67	5.826e+05	0.0	-0.07	449.28	0.0	-2.484e+04	-6007.96	0.0	0.0	0.0	5.826e+05
		4.959e+05	0.0	0.0	0.0	15.0	-2.465e+04	-5558.68	0.0	0.0	0.0	4.959e+05
12	68	-2.185e+06	0.0	-0.30	449.28	0.0	-2.372e+04	3082.48	0.0	0.0	0.0	-2.235e+06
		-2.235e+06	0.0	0.0	0.0	15.0	-2.353e+04	3531.76	0.0	0.0	0.0	-2.185e+06
12	69	-5.174e+05	0.0	-0.11	449.28	0.0	-1.655e+04	-2619.63	0.0	0.0	0.0	-5.174e+05
		-5.533e+05	0.0	0.0	0.0	15.0	-1.636e+04	-2170.35	0.0	0.0	0.0	-5.533e+05
12	70	6.552e+05	0.0	9.70e-04	449.28	0.0	-1.344e+04	-6361.03	0.0	0.0	0.0	6.552e+05
		5.631e+05	0.0	0.0	0.0	15.0	-1.325e+04	-5911.75	0.0	0.0	0.0	5.631e+05
12	71	4.442e+05	0.0	-0.03	449.28	0.0	-1.423e+04	-6013.72	0.0	0.0	0.0	4.442e+05
		3.574e+05	0.0	0.0	0.0	15.0	-1.404e+04	-5564.44	0.0	0.0	0.0	3.574e+05
12	72	7.225e+05	0.0	5.37e-04	449.28	0.0	-1.344e+04	-6865.20	0.0	0.0	0.0	7.225e+05
		6.229e+05	0.0	0.0	0.0	15.0	-1.325e+04	-6415.91	0.0	0.0	0.0	6.229e+05
12	73	3.769e+05	0.0	-0.03	449.28	0.0	-1.423e+04	-5509.55	0.0	0.0	0.0	3.769e+05
		2.976e+05	0.0	0.0	0.0	15.0	-1.404e+04	-5060.27	0.0	0.0	0.0	2.976e+05
12	74	3.162e+05	0.0	-0.03	449.28	0.0	-1.423e+04	-5305.82	0.0	0.0	0.0	3.162e+05
		2.400e+05	0.0	0.0	0.0	15.0	-1.404e+04	-4856.53	0.0	0.0	0.0	2.400e+05
13	1	-8.536e+05	0.0	5.73e-03	-438.84	0.0	-3.230e+04	5577.64	0.0	0.0	0.0	-9.339e+05
		-9.339e+05	0.0	0.0	0.0	15.0	-3.205e+04	5138.79	0.0	0.0	0.0	-8.536e+05
13	2	-6.017e+05	0.0	1.49e-03	-438.84	0.0	-1.789e+04	6174.46	0.0	0.0	0.0	-6.910e+05
		-6.910e+05	0.0	0.0	0.0	15.0	-1.763e+04	5735.61	0.0	0.0	0.0	-6.017e+05
13	3	-7.389e+05	0.0	5.09e-03	-438.84	0.0	-2.867e+04	5388.15	0.0	0.0	0.0	-8.164e+05
		-8.164e+05	0.0	0.0	0.0	15.0	-2.842e+04	4949.31	0.0	0.0	0.0	-7.389e+05
13	4	-5.504e+05	0.0	1.92e-03	-438.84	0.0	-1.789e+04	5834.66	0.0	0.0	0.0	-6.346e+05
		-6.346e+05	0.0	0.0	0.0	15.0	-1.763e+04	5395.82	0.0	0.0	0.0	-5.504e+05
13	5	-3.819e+06	0.0	-0.31	-957.19	0.0	-1.747e+04	2.358e+04	0.0	0.0	0.0	-4.165e+06
		-4.165e+06	0.0	0.0	0.0	15.0	-1.722e+04	2.262e+04	0.0	0.0	0.0	-3.819e+06
13	6	-3.862e+06	0.0	-0.33	-1073.65	0.0	-5677.52	2.696e+04	0.0	0.0	0.0	-4.259e+06
		-4.259e+06	0.0	0.0	0.0	15.0	-5424.40	2.589e+04	0.0	0.0	0.0	-3.862e+06
13	7	-4.839e+06	0.0	-0.42	-1114.09	0.0	-3563.15	3.217e+04	0.0	0.0	0.0	-5.313e+06
		-5.313e+06	0.0	0.0	0.0	15.0	-3310.02	3.105e+04	0.0	0.0	0.0	-4.839e+06
13	8	-1.725e+06	0.0	-0.06	-957.19	0.0	-2.715e+04	1.584e+04	0.0	0.0	0.0	-1.955e+06
		-1.955e+06	0.0	0.0	0.0	15.0	-2.690e+04	1.488e+04	0.0	0.0	0.0	-1.725e+06
13	9	-1.769e+06	0.0	-0.09	-1073.65	0.0	-1.536e+04	1.922e+04	0.0	0.0	0.0	-2.049e+06
		-2.049e+06	0.0	0.0	0.0	15.0	-1.510e+04	1.815e+04	0.0	0.0	0.0	-1.769e+06
13	10	-2.745e+06	0.0	-0.17	-1114.09	0.0	-1.324e+04	2.443e+04	0.0	0.0	0.0	-3.103e+06
		-3.103e+06	0.0	0.0	0.0	15.0	-1.299e+04	2.332e+04	0.0	0.0	0.0	-2.745e+06
13	11	-8.555e+05	0.0	5.71e-03	-438.84	0.0	-3.230e+04	5584.97	0.0	0.0	0.0	-9.360e+05
		-9.360e+05	0.0	0.0	0.0	15.0	-3.205e+04	5146.13	0.0	0.0	0.0	-8.555e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
13	12	-6.036e+05	0.0	1.47e-03	-438.84	0.0	-1.789e+04	6181.79	0.0	0.0	0.0	-6.931e+05
		-6.931e+05	0.0	0.0	0.0	15.0	-1.763e+04	5742.95	0.0	0.0	0.0	-6.036e+05
13	13	-9.186e+05	0.0	3.54e-03	-438.84	0.0	-2.867e+04	6801.08	0.0	0.0	0.0	-1.017e+06
		-1.017e+06	0.0	0.0	0.0	15.0	-2.842e+04	6362.23	0.0	0.0	0.0	-9.186e+05
13	14	-7.301e+05	0.0	3.66e-04	-438.84	0.0	-1.789e+04	7247.59	0.0	0.0	0.0	-8.355e+05
		-8.355e+05	0.0	0.0	0.0	15.0	-1.763e+04	6808.74	0.0	0.0	0.0	-7.301e+05
13	15	-3.742e+06	0.0	-0.31	-957.19	0.0	-1.747e+04	2.285e+04	0.0	0.0	0.0	-4.077e+06
		-4.077e+06	0.0	0.0	0.0	15.0	-1.722e+04	2.189e+04	0.0	0.0	0.0	-3.742e+06
13	16	-3.785e+06	0.0	-0.33	-1073.65	0.0	-5677.52	2.623e+04	0.0	0.0	0.0	-4.171e+06
		-4.171e+06	0.0	0.0	0.0	15.0	-5424.40	2.516e+04	0.0	0.0	0.0	-3.785e+06
13	17	-4.761e+06	0.0	-0.42	-1114.09	0.0	-3563.15	3.144e+04	0.0	0.0	0.0	-5.225e+06
		-5.225e+06	0.0	0.0	0.0	15.0	-3310.02	3.032e+04	0.0	0.0	0.0	-4.761e+06
13	18	-1.670e+06	0.0	-0.06	-957.19	0.0	-2.715e+04	1.564e+04	0.0	0.0	0.0	-1.898e+06
		-1.898e+06	0.0	0.0	0.0	15.0	-2.690e+04	1.468e+04	0.0	0.0	0.0	-1.670e+06
13	19	-1.714e+06	0.0	-0.08	-1073.65	0.0	-1.536e+04	1.902e+04	0.0	0.0	0.0	-1.991e+06
		-1.991e+06	0.0	0.0	0.0	15.0	-1.510e+04	1.795e+04	0.0	0.0	0.0	-1.714e+06
13	20	-2.690e+06	0.0	-0.17	-1114.09	0.0	-1.324e+04	2.423e+04	0.0	0.0	0.0	-3.045e+06
		-3.045e+06	0.0	0.0	0.0	15.0	-1.299e+04	2.311e+04	0.0	0.0	0.0	-2.690e+06
13	21	-3.814e+06	0.0	-0.36	-957.19	0.0	-1.397e+04	2.375e+04	0.0	0.0	0.0	-4.163e+06
		-4.163e+06	0.0	0.0	0.0	15.0	-1.372e+04	2.279e+04	0.0	0.0	0.0	-3.814e+06
13	22	-1.668e+06	0.0	-0.11	-957.19	0.0	-2.365e+04	1.581e+04	0.0	0.0	0.0	-1.898e+06
		-1.898e+06	0.0	0.0	0.0	15.0	-2.339e+04	1.485e+04	0.0	0.0	0.0	-1.668e+06
13	23	-4.653e+06	0.0	-0.42	-1114.09	0.0	1074.35	3.132e+04	0.0	0.0	0.0	-5.114e+06
		-5.114e+06	0.0	0.0	0.0	15.0	1261.85	3.020e+04	0.0	0.0	0.0	-4.653e+06
13	24	-2.456e+06	0.0	-0.17	-1114.09	0.0	-8604.43	2.290e+04	0.0	0.0	0.0	-2.791e+06
		-2.791e+06	0.0	0.0	0.0	15.0	-8416.93	2.178e+04	0.0	0.0	0.0	-2.456e+06
13	25	-3.780e+06	0.0	-0.27	-957.19	0.0	-2.097e+04	2.324e+04	0.0	0.0	0.0	-4.121e+06
		-4.121e+06	0.0	0.0	0.0	15.0	-2.072e+04	2.229e+04	0.0	0.0	0.0	-3.780e+06
13	26	-3.786e+06	0.0	-0.33	-1073.65	0.0	-5677.52	2.645e+04	0.0	0.0	0.0	-4.174e+06
		-4.174e+06	0.0	0.0	0.0	15.0	-5424.40	2.538e+04	0.0	0.0	0.0	-3.786e+06
13	27	-1.731e+06	0.0	-0.12	-957.19	0.0	-2.610e+04	1.557e+04	0.0	0.0	0.0	-1.958e+06
		-1.958e+06	0.0	0.0	0.0	15.0	-2.584e+04	1.462e+04	0.0	0.0	0.0	-1.731e+06
13	28	-1.715e+06	0.0	-0.08	-1073.65	0.0	-1.536e+04	1.888e+04	0.0	0.0	0.0	-1.990e+06
		-1.990e+06	0.0	0.0	0.0	15.0	-1.510e+04	1.780e+04	0.0	0.0	0.0	-1.715e+06
13	29	-4.761e+06	0.0	-0.42	-1114.09	0.0	-3563.15	3.144e+04	0.0	0.0	0.0	-5.225e+06
		-5.225e+06	0.0	0.0	0.0	15.0	-3310.02	3.032e+04	0.0	0.0	0.0	-4.761e+06
13	30	-3.121e+06	0.0	-0.25	-957.19	0.0	-1.435e+04	2.144e+04	0.0	0.0	0.0	-3.435e+06
		-3.435e+06	0.0	0.0	0.0	15.0	-1.417e+04	2.048e+04	0.0	0.0	0.0	-3.121e+06
13	31	-2.653e+06	0.0	-0.22	-1073.65	0.0	-3532.52	2.325e+04	0.0	0.0	0.0	-2.994e+06
		-2.994e+06	0.0	0.0	0.0	15.0	-3345.02	2.218e+04	0.0	0.0	0.0	-2.653e+06
13	32	-3.163e+06	0.0	-0.26	-1114.09	0.0	-3571.22	2.655e+04	0.0	0.0	0.0	-3.553e+06
		-3.553e+06	0.0	0.0	0.0	15.0	-3383.72	2.543e+04	0.0	0.0	0.0	-3.163e+06
13	33	-4.915e+06	0.0	-0.42	-1114.09	0.0	-3563.15	3.246e+04	0.0	0.0	0.0	-5.394e+06
		-5.394e+06	0.0	0.0	0.0	15.0	-3310.02	3.134e+04	0.0	0.0	0.0	-4.915e+06
13	34	-6.122e+05	0.0	3.01e-03	-438.84	0.0	-2.126e+04	5559.81	0.0	0.0	0.0	-6.923e+05
		-6.923e+05	0.0	0.0	0.0	15.0	-2.107e+04	5120.96	0.0	0.0	0.0	-6.122e+05
13	35	-6.448e+05	0.0	-0.01	-525.32	0.0	-1.250e+04	8070.21	0.0	0.0	0.0	-7.619e+05
		-7.619e+05	0.0	0.0	0.0	15.0	-1.231e+04	7544.89	0.0	0.0	0.0	-6.448e+05
13	36	-1.150e+06	0.0	-0.03	-709.03	0.0	-2.046e+04	1.102e+04	0.0	0.0	0.0	-1.310e+06
		-1.310e+06	0.0	0.0	0.0	15.0	-2.028e+04	1.031e+04	0.0	0.0	0.0	-1.150e+06
13	37	-1.183e+06	0.0	-0.05	-795.51	0.0	-1.171e+04	1.353e+04	0.0	0.0	0.0	-1.380e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-1.380e+06	0.0	0.0	0.0	15.0	-1.152e+04	1.274e+04	0.0	0.0	0.0	-1.183e+06
13	38	-1.908e+06	0.0	-0.12	-825.54	0.0	-1.014e+04	1.740e+04	0.0	0.0	0.0	-2.162e+06
		-2.162e+06	0.0	0.0	0.0	15.0	-9949.35	1.657e+04	0.0	0.0	0.0	-1.908e+06
13	39	-6.645e+05	0.0	2.54e-03	-438.84	0.0	-2.126e+04	6063.98	0.0	0.0	0.0	-7.521e+05
		-7.521e+05	0.0	0.0	0.0	15.0	-2.107e+04	5625.13	0.0	0.0	0.0	-6.645e+05
13	40	-5.245e+05	0.0	-1.81e-04	-438.84	0.0	-1.325e+04	6395.54	0.0	0.0	0.0	-6.171e+05
		-6.171e+05	0.0	0.0	0.0	15.0	-1.306e+04	5956.70	0.0	0.0	0.0	-5.245e+05
13	41	-1.098e+06	0.0	-0.03	-709.03	0.0	-2.046e+04	1.052e+04	0.0	0.0	0.0	-1.250e+06
		-1.250e+06	0.0	0.0	0.0	15.0	-2.028e+04	9807.74	0.0	0.0	0.0	-1.098e+06
13	42	-1.130e+06	0.0	-0.05	-795.51	0.0	-1.171e+04	1.303e+04	0.0	0.0	0.0	-1.320e+06
		-1.320e+06	0.0	0.0	0.0	15.0	-1.152e+04	1.223e+04	0.0	0.0	0.0	-1.130e+06
13	43	-1.855e+06	0.0	-0.12	-825.54	0.0	-1.014e+04	1.689e+04	0.0	0.0	0.0	-2.103e+06
		-2.103e+06	0.0	0.0	0.0	15.0	-9949.35	1.607e+04	0.0	0.0	0.0	-1.855e+06
13	44	-1.993e+06	0.0	-0.14	-825.54	0.0	-1.554e+04	1.669e+04	0.0	0.0	0.0	-2.238e+06
		-2.238e+06	0.0	0.0	0.0	15.0	-1.536e+04	1.586e+04	0.0	0.0	0.0	-1.993e+06
13	45	-1.790e+06	0.0	-0.11	-825.54	0.0	-1.014e+04	1.665e+04	0.0	0.0	0.0	-2.033e+06
		-2.033e+06	0.0	0.0	0.0	15.0	-9949.35	1.582e+04	0.0	0.0	0.0	-1.790e+06
13	46	-6.798e+05	0.0	3.60e-03	-438.84	0.0	-2.393e+04	5650.95	0.0	0.0	0.0	-7.612e+05
		-7.612e+05	0.0	0.0	0.0	15.0	-2.374e+04	5212.11	0.0	0.0	0.0	-6.798e+05
13	47	-4.932e+05	0.0	4.63e-04	-438.84	0.0	-1.325e+04	6093.04	0.0	0.0	0.0	-5.813e+05
		-5.813e+05	0.0	0.0	0.0	15.0	-1.306e+04	5654.20	0.0	0.0	0.0	-4.932e+05
13	48	-5.904e+05	0.0	3.18e-03	-438.84	0.0	-2.126e+04	5478.31	0.0	0.0	0.0	-6.693e+05
		-6.693e+05	0.0	0.0	0.0	15.0	-2.107e+04	5039.47	0.0	0.0	0.0	-5.904e+05
13	49	-4.504e+05	0.0	8.22e-04	-438.84	0.0	-1.325e+04	5809.88	0.0	0.0	0.0	-5.343e+05
		-5.343e+05	0.0	0.0	0.0	15.0	-1.306e+04	5371.03	0.0	0.0	0.0	-4.504e+05
13	50	-2.707e+06	0.0	-0.22	-709.03	0.0	-1.329e+04	1.707e+04	0.0	0.0	0.0	-2.957e+06
		-2.957e+06	0.0	0.0	0.0	15.0	-1.311e+04	1.636e+04	0.0	0.0	0.0	-2.707e+06
13	51	-2.739e+06	0.0	-0.23	-795.51	0.0	-4537.46	1.958e+04	0.0	0.0	0.0	-3.027e+06
		-3.027e+06	0.0	0.0	0.0	15.0	-4349.96	1.878e+04	0.0	0.0	0.0	-2.739e+06
13	52	-3.464e+06	0.0	-0.30	-825.54	0.0	-2967.38	2.345e+04	0.0	0.0	0.0	-3.810e+06
		-3.810e+06	0.0	0.0	0.0	15.0	-2779.88	2.262e+04	0.0	0.0	0.0	-3.464e+06
13	53	-1.160e+06	0.0	-0.03	-709.03	0.0	-2.046e+04	1.137e+04	0.0	0.0	0.0	-1.326e+06
		-1.326e+06	0.0	0.0	0.0	15.0	-2.028e+04	1.066e+04	0.0	0.0	0.0	-1.160e+06
13	54	-1.193e+06	0.0	-0.05	-795.51	0.0	-1.171e+04	1.388e+04	0.0	0.0	0.0	-1.395e+06
		-1.395e+06	0.0	0.0	0.0	15.0	-1.152e+04	1.308e+04	0.0	0.0	0.0	-1.193e+06
13	55	-1.918e+06	0.0	-0.12	-825.54	0.0	-1.014e+04	1.775e+04	0.0	0.0	0.0	-2.178e+06
		-2.178e+06	0.0	0.0	0.0	15.0	-9949.35	1.692e+04	0.0	0.0	0.0	-1.918e+06
13	56	-7.453e+05	0.0	3.09e-03	-438.84	0.0	-2.393e+04	5895.43	0.0	0.0	0.0	-8.304e+05
		-8.304e+05	0.0	0.0	0.0	15.0	-2.374e+04	5456.59	0.0	0.0	0.0	-7.453e+05
13	57	-5.587e+05	0.0	-4.92e-05	-438.84	0.0	-1.325e+04	6337.52	0.0	0.0	0.0	-6.505e+05
		-6.505e+05	0.0	0.0	0.0	15.0	-1.306e+04	5898.68	0.0	0.0	0.0	-5.587e+05
13	58	-6.996e+05	0.0	2.32e-03	-438.84	0.0	-2.126e+04	5885.78	0.0	0.0	0.0	-7.846e+05
		-7.846e+05	0.0	0.0	0.0	15.0	-2.107e+04	5446.94	0.0	0.0	0.0	-6.996e+05
13	59	-5.597e+05	0.0	3.37e-05	-438.84	0.0	-1.325e+04	6217.35	0.0	0.0	0.0	-6.496e+05
		-6.496e+05	0.0	0.0	0.0	15.0	-1.306e+04	5778.50	0.0	0.0	0.0	-5.597e+05
13	60	-2.705e+06	0.0	-0.22	-709.03	0.0	-1.329e+04	1.706e+04	0.0	0.0	0.0	-2.956e+06
		-2.956e+06	0.0	0.0	0.0	15.0	-1.311e+04	1.635e+04	0.0	0.0	0.0	-2.705e+06
13	61	-2.738e+06	0.0	-0.23	-795.51	0.0	-4537.46	1.957e+04	0.0	0.0	0.0	-3.025e+06
		-3.025e+06	0.0	0.0	0.0	15.0	-4349.96	1.878e+04	0.0	0.0	0.0	-2.738e+06
13	62	-3.462e+06	0.0	-0.30	-825.54	0.0	-2967.38	2.344e+04	0.0	0.0	0.0	-3.808e+06
		-3.808e+06	0.0	0.0	0.0	15.0	-2779.88	2.262e+04	0.0	0.0	0.0	-3.462e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
13	63	-1.115e+06	0.0	-0.03	-709.03	0.0	-2.046e+04	1.120e+04	0.0	0.0	0.0	-1.278e+06
		-1.278e+06	0.0	0.0	0.0	15.0	-2.028e+04	1.049e+04	0.0	0.0	0.0	-1.115e+06
13	64	-1.148e+06	0.0	-0.05	-795.51	0.0	-1.171e+04	1.371e+04	0.0	0.0	0.0	-1.347e+06
		-1.347e+06	0.0	0.0	0.0	15.0	-1.152e+04	1.291e+04	0.0	0.0	0.0	-1.148e+06
13	65	-1.872e+06	0.0	-0.12	-825.54	0.0	-1.014e+04	1.758e+04	0.0	0.0	0.0	-2.130e+06
		-2.130e+06	0.0	0.0	0.0	15.0	-9949.35	1.675e+04	0.0	0.0	0.0	-1.872e+06
13	66	-2.703e+06	0.0	-0.25	-709.03	0.0	-1.069e+04	1.719e+04	0.0	0.0	0.0	-2.956e+06
		-2.956e+06	0.0	0.0	0.0	15.0	-1.051e+04	1.648e+04	0.0	0.0	0.0	-2.703e+06
13	67	-1.113e+06	0.0	-0.06	-709.03	0.0	-1.786e+04	1.133e+04	0.0	0.0	0.0	-1.278e+06
		-1.278e+06	0.0	0.0	0.0	15.0	-1.768e+04	1.062e+04	0.0	0.0	0.0	-1.113e+06
13	68	-3.400e+06	0.0	-0.30	-825.54	0.0	-2967.38	2.284e+04	0.0	0.0	0.0	-3.736e+06
		-3.736e+06	0.0	0.0	0.0	15.0	-2779.88	2.201e+04	0.0	0.0	0.0	-3.400e+06
13	69	-1.768e+06	0.0	-0.11	-825.54	0.0	-1.014e+04	1.657e+04	0.0	0.0	0.0	-2.010e+06
		-2.010e+06	0.0	0.0	0.0	15.0	-9949.35	1.574e+04	0.0	0.0	0.0	-1.768e+06
13	70	-4.778e+05	0.0	6.09e-04	-438.84	0.0	-1.325e+04	5911.75	0.0	0.0	0.0	-5.631e+05
		-5.631e+05	0.0	0.0	0.0	15.0	-1.306e+04	5472.90	0.0	0.0	0.0	-4.778e+05
13	71	-1.005e+06	0.0	-0.04	-709.03	0.0	-1.246e+04	1.133e+04	0.0	0.0	0.0	-1.169e+06
		-1.169e+06	0.0	0.0	0.0	15.0	-1.227e+04	1.062e+04	0.0	0.0	0.0	-1.005e+06
13	72	-5.300e+05	0.0	-1.38e-04	-438.84	0.0	-1.325e+04	6415.91	0.0	0.0	0.0	-6.229e+05
		-6.229e+05	0.0	0.0	0.0	15.0	-1.306e+04	5977.07	0.0	0.0	0.0	-5.300e+05
13	73	-9.526e+05	0.0	-0.03	-709.03	0.0	-1.246e+04	1.083e+04	0.0	0.0	0.0	-1.110e+06
		-1.110e+06	0.0	0.0	0.0	15.0	-1.227e+04	1.012e+04	0.0	0.0	0.0	-9.526e+05
13	74	-8.979e+05	0.0	-0.03	-709.03	0.0	-1.246e+04	1.062e+04	0.0	0.0	0.0	-1.052e+06
		-1.052e+06	0.0	0.0	0.0	15.0	-1.227e+04	9915.20	0.0	0.0	0.0	-8.979e+05
14	1	9.339e+05	0.0	-5.73e-03	438.84	0.0	-3.230e+04	-5577.64	0.0	0.0	0.0	9.339e+05
		8.536e+05	0.0	0.0	0.0	15.0	-3.205e+04	-5138.79	0.0	0.0	0.0	8.536e+05
14	2	6.910e+05	0.0	-1.49e-03	438.84	0.0	-1.789e+04	-6174.46	0.0	0.0	0.0	6.910e+05
		6.017e+05	0.0	0.0	0.0	15.0	-1.763e+04	-5735.61	0.0	0.0	0.0	6.017e+05
14	3	8.164e+05	0.0	-5.09e-03	438.84	0.0	-2.867e+04	-5388.15	0.0	0.0	0.0	8.164e+05
		7.389e+05	0.0	0.0	0.0	15.0	-2.842e+04	-4949.31	0.0	0.0	0.0	7.389e+05
14	4	6.346e+05	0.0	-1.92e-03	438.84	0.0	-1.789e+04	-5834.66	0.0	0.0	0.0	6.346e+05
		5.504e+05	0.0	0.0	0.0	15.0	-1.763e+04	-5395.82	0.0	0.0	0.0	5.504e+05
14	5	-1.868e+06	0.0	-0.32	438.84	0.0	-3.987e+04	3643.26	0.0	0.0	0.0	-1.926e+06
		-1.926e+06	0.0	0.0	0.0	15.0	-3.962e+04	4082.10	0.0	0.0	0.0	-1.868e+06
14	6	-2.558e+06	0.0	-0.33	438.84	0.0	-3.010e+04	4765.62	0.0	0.0	0.0	-2.633e+06
		-2.633e+06	0.0	0.0	0.0	15.0	-2.984e+04	5204.46	0.0	0.0	0.0	-2.558e+06
14	7	-3.033e+06	0.0	-0.42	438.84	0.0	-3.221e+04	6676.96	0.0	0.0	0.0	-3.137e+06
		-3.137e+06	0.0	0.0	0.0	15.0	-3.196e+04	7115.81	0.0	0.0	0.0	-3.033e+06
14	8	3.973e+05	0.0	-0.07	438.84	0.0	-3.019e+04	-4776.65	0.0	0.0	0.0	3.973e+05
		3.290e+05	0.0	0.0	0.0	15.0	-2.994e+04	-4337.81	0.0	0.0	0.0	3.290e+05
14	9	-3.096e+05	0.0	-0.08	438.84	0.0	-2.042e+04	-3654.29	0.0	0.0	0.0	-3.096e+05
		-3.611e+05	0.0	0.0	0.0	15.0	-2.017e+04	-3215.45	0.0	0.0	0.0	-3.611e+05
14	10	-8.139e+05	0.0	-0.17	438.84	0.0	-2.253e+04	-1742.95	0.0	0.0	0.0	-8.139e+05
		-8.367e+05	0.0	0.0	0.0	15.0	-2.228e+04	-1304.10	0.0	0.0	0.0	-8.367e+05
14	11	9.360e+05	0.0	-5.71e-03	438.84	0.0	-3.230e+04	-5584.97	0.0	0.0	0.0	9.360e+05
		8.555e+05	0.0	0.0	0.0	15.0	-3.205e+04	-5146.13	0.0	0.0	0.0	8.555e+05
14	12	6.931e+05	0.0	-1.47e-03	438.84	0.0	-1.789e+04	-6181.79	0.0	0.0	0.0	6.931e+05
		6.036e+05	0.0	0.0	0.0	15.0	-1.763e+04	-5742.95	0.0	0.0	0.0	6.036e+05
14	13	1.017e+06	0.0	-3.54e-03	438.84	0.0	-2.867e+04	-6801.08	0.0	0.0	0.0	1.017e+06
		9.186e+05	0.0	0.0	0.0	15.0	-2.842e+04	-6362.23	0.0	0.0	0.0	9.186e+05
14	14	8.355e+05	0.0	-3.66e-04	438.84	0.0	-1.789e+04	-7247.59	0.0	0.0	0.0	8.355e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		7.301e+05	0.0	0.0	0.0	15.0	-1.763e+04	-6808.74	0.0	0.0	0.0	7.301e+05
14	15	-1.945e+06	0.0	-0.32	438.84	0.0	-3.987e+04	4376.59	0.0	0.0	0.0	-2.014e+06
		-2.014e+06	0.0	0.0	0.0	15.0	-3.962e+04	4815.44	0.0	0.0	0.0	-1.945e+06
14	16	-2.635e+06	0.0	-0.33	438.84	0.0	-3.010e+04	5498.96	0.0	0.0	0.0	-2.721e+06
		-2.721e+06	0.0	0.0	0.0	15.0	-2.984e+04	5937.80	0.0	0.0	0.0	-2.635e+06
14	17	-3.111e+06	0.0	-0.42	438.84	0.0	-3.221e+04	7410.30	0.0	0.0	0.0	-3.225e+06
		-3.225e+06	0.0	0.0	0.0	15.0	-3.196e+04	7849.15	0.0	0.0	0.0	-3.111e+06
14	18	3.399e+05	0.0	-0.07	438.84	0.0	-3.019e+04	-4573.74	0.0	0.0	0.0	3.399e+05
		2.746e+05	0.0	0.0	0.0	15.0	-2.994e+04	-4134.89	0.0	0.0	0.0	2.746e+05
14	19	-3.670e+05	0.0	-0.08	438.84	0.0	-2.042e+04	-3451.37	0.0	0.0	0.0	-3.670e+05
		-4.155e+05	0.0	0.0	0.0	15.0	-2.017e+04	-3012.53	0.0	0.0	0.0	-4.155e+05
14	20	-8.713e+05	0.0	-0.17	438.84	0.0	-2.253e+04	-1540.03	0.0	0.0	0.0	-8.713e+05
		-8.911e+05	0.0	0.0	0.0	15.0	-2.228e+04	-1101.18	0.0	0.0	0.0	-8.911e+05
14	21	-1.832e+06	0.0	-0.36	438.84	0.0	-4.337e+04	3479.24	0.0	0.0	0.0	-1.887e+06
		-1.887e+06	0.0	0.0	0.0	15.0	-4.312e+04	3918.09	0.0	0.0	0.0	-1.832e+06
14	22	3.805e+05	0.0	-0.11	438.84	0.0	-3.369e+04	-4745.08	0.0	0.0	0.0	3.805e+05
		3.127e+05	0.0	0.0	0.0	15.0	-3.344e+04	-4306.24	0.0	0.0	0.0	3.127e+05
14	23	-3.219e+06	0.0	-0.42	438.84	0.0	-2.757e+04	7528.99	0.0	0.0	0.0	-3.335e+06
		-3.335e+06	0.0	0.0	0.0	15.0	-2.739e+04	7967.84	0.0	0.0	0.0	-3.219e+06
14	24	-1.125e+06	0.0	-0.17	438.84	0.0	-1.790e+04	-211.33	0.0	0.0	0.0	-1.125e+06
		-1.126e+06	0.0	0.0	0.0	15.0	-1.771e+04	227.51	0.0	0.0	0.0	-1.125e+06
14	25	-1.947e+06	0.0	-0.27	438.84	0.0	-3.637e+04	3981.60	0.0	0.0	0.0	-2.010e+06
		-2.010e+06	0.0	0.0	0.0	15.0	-3.611e+04	4420.44	0.0	0.0	0.0	-1.947e+06
14	26	-2.635e+06	0.0	-0.33	438.84	0.0	-3.010e+04	5275.31	0.0	0.0	0.0	-2.717e+06
		-2.717e+06	0.0	0.0	0.0	15.0	-2.984e+04	5714.15	0.0	0.0	0.0	-2.635e+06
14	27	4.544e+05	0.0	-0.13	438.84	0.0	-3.850e+04	-4508.25	0.0	0.0	0.0	4.544e+05
		3.901e+05	0.0	0.0	0.0	15.0	-3.825e+04	-4069.40	0.0	0.0	0.0	3.901e+05
14	28	-3.680e+05	0.0	-0.08	438.84	0.0	-2.042e+04	-3307.16	0.0	0.0	0.0	-3.680e+05
		-4.143e+05	0.0	0.0	0.0	15.0	-2.017e+04	-2868.32	0.0	0.0	0.0	-4.143e+05
14	29	-3.111e+06	0.0	-0.42	438.84	0.0	-3.221e+04	7410.30	0.0	0.0	0.0	-3.225e+06
		-3.225e+06	0.0	0.0	0.0	15.0	-3.196e+04	7849.15	0.0	0.0	0.0	-3.111e+06
14	30	-1.098e+06	0.0	-0.25	957.19	0.0	-3.371e+04	-5278.89	0.0	0.0	0.0	-1.098e+06
		-1.170e+06	0.0	0.0	0.0	15.0	-3.352e+04	-4321.70	0.0	0.0	0.0	-1.170e+06
14	31	-1.520e+06	0.0	-0.21	1073.65	0.0	-2.297e+04	-7090.71	0.0	0.0	0.0	-1.520e+06
		-1.618e+06	0.0	0.0	0.0	15.0	-2.278e+04	-6017.06	0.0	0.0	0.0	-1.618e+06
14	32	-9.801e+05	0.0	-0.24	1114.09	0.0	-2.293e+04	-1.039e+04	0.0	0.0	0.0	-9.801e+05
		-1.127e+06	0.0	0.0	0.0	15.0	-2.274e+04	-9272.12	0.0	0.0	0.0	-1.127e+06
14	33	-2.957e+06	0.0	-0.42	438.84	0.0	-3.221e+04	6390.92	0.0	0.0	0.0	-3.056e+06
		-3.056e+06	0.0	0.0	0.0	15.0	-3.196e+04	6829.77	0.0	0.0	0.0	-2.957e+06
14	34	6.923e+05	0.0	-3.01e-03	438.84	0.0	-2.126e+04	-5559.81	0.0	0.0	0.0	6.923e+05
		6.122e+05	0.0	0.0	0.0	15.0	-2.107e+04	-5120.96	0.0	0.0	0.0	6.122e+05
14	35	1.674e+05	0.0	-0.01	438.84	0.0	-1.400e+04	-4726.37	0.0	0.0	0.0	1.674e+05
		9.983e+04	0.0	0.0	0.0	15.0	-1.381e+04	-4287.52	0.0	0.0	0.0	9.983e+04
14	36	4.981e+05	0.0	-0.04	438.84	0.0	-2.205e+04	-5253.24	0.0	0.0	0.0	4.981e+05
		4.227e+05	0.0	0.0	0.0	15.0	-2.186e+04	-4814.40	0.0	0.0	0.0	4.227e+05
14	37	-2.676e+04	0.0	-0.04	438.84	0.0	-1.479e+04	-4419.81	0.0	0.0	0.0	-2.676e+04
		-8.975e+04	0.0	0.0	0.0	15.0	-1.461e+04	-3980.96	0.0	0.0	0.0	-8.975e+04
14	38	-4.013e+05	0.0	-0.11	438.84	0.0	-1.636e+04	-3000.49	0.0	0.0	0.0	-4.013e+05
		-4.430e+05	0.0	0.0	0.0	15.0	-1.618e+04	-2561.65	0.0	0.0	0.0	-4.430e+05
14	39	7.521e+05	0.0	-2.54e-03	438.84	0.0	-2.126e+04	-6063.98	0.0	0.0	0.0	7.521e+05
		6.645e+05	0.0	0.0	0.0	15.0	-2.107e+04	-5625.13	0.0	0.0	0.0	6.645e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
14	40	6.171e+05	0.0	1.81e-04	438.84	0.0	-1.325e+04	-6395.54	0.0	0.0	0.0	6.171e+05
		5.245e+05	0.0	0.0	0.0	15.0	-1.306e+04	-5956.70	0.0	0.0	0.0	5.245e+05
14	41	4.384e+05	0.0	-0.04	438.84	0.0	-2.205e+04	-4749.07	0.0	0.0	0.0	4.384e+05
		3.704e+05	0.0	0.0	0.0	15.0	-2.186e+04	-4310.23	0.0	0.0	0.0	3.704e+05
14	42	-8.655e+04	0.0	-0.04	438.84	0.0	-1.479e+04	-3915.64	0.0	0.0	0.0	-8.655e+04
		-1.420e+05	0.0	0.0	0.0	15.0	-1.461e+04	-3476.79	0.0	0.0	0.0	-1.420e+05
14	43	-4.610e+05	0.0	-0.11	438.84	0.0	-1.636e+04	-2496.32	0.0	0.0	0.0	-4.610e+05
		-4.952e+05	0.0	0.0	0.0	15.0	-1.618e+04	-2057.48	0.0	0.0	0.0	-4.952e+05
14	44	-2.959e+05	0.0	-0.15	438.84	0.0	-2.697e+04	-2291.99	0.0	0.0	0.0	-2.959e+05
		-3.269e+05	0.0	0.0	0.0	15.0	-2.678e+04	-1853.15	0.0	0.0	0.0	-3.269e+05
14	45	-5.302e+05	0.0	-0.11	438.84	0.0	-1.636e+04	-2251.84	0.0	0.0	0.0	-5.302e+05
		-5.607e+05	0.0	0.0	0.0	15.0	-1.618e+04	-1813.00	0.0	0.0	0.0	-5.607e+05
14	46	7.612e+05	0.0	-3.60e-03	438.84	0.0	-2.393e+04	-5650.95	0.0	0.0	0.0	7.612e+05
		6.798e+05	0.0	0.0	0.0	15.0	-2.374e+04	-5212.11	0.0	0.0	0.0	6.798e+05
14	47	5.813e+05	0.0	-4.63e-04	438.84	0.0	-1.325e+04	-6093.04	0.0	0.0	0.0	5.813e+05
		4.932e+05	0.0	0.0	0.0	15.0	-1.306e+04	-5654.20	0.0	0.0	0.0	4.932e+05
14	48	6.693e+05	0.0	-3.18e-03	438.84	0.0	-2.126e+04	-5478.31	0.0	0.0	0.0	6.693e+05
		5.904e+05	0.0	0.0	0.0	15.0	-2.107e+04	-5039.47	0.0	0.0	0.0	5.904e+05
14	49	5.343e+05	0.0	-8.22e-04	438.84	0.0	-1.325e+04	-5809.88	0.0	0.0	0.0	5.343e+05
		4.504e+05	0.0	0.0	0.0	15.0	-1.306e+04	-5371.03	0.0	0.0	0.0	4.504e+05
14	50	-1.199e+06	0.0	-0.22	438.84	0.0	-2.922e+04	667.90	0.0	0.0	0.0	-1.212e+06
		-1.212e+06	0.0	0.0	0.0	15.0	-2.903e+04	1106.74	0.0	0.0	0.0	-1.199e+06
14	51	-1.712e+06	0.0	-0.23	438.84	0.0	-2.196e+04	1501.33	0.0	0.0	0.0	-1.737e+06
		-1.737e+06	0.0	0.0	0.0	15.0	-2.178e+04	1940.18	0.0	0.0	0.0	-1.712e+06
14	52	-2.065e+06	0.0	-0.30	438.84	0.0	-2.353e+04	2920.65	0.0	0.0	0.0	-2.112e+06
		-2.112e+06	0.0	0.0	0.0	15.0	-2.335e+04	3359.49	0.0	0.0	0.0	-2.065e+06
14	53	5.135e+05	0.0	-0.04	438.84	0.0	-2.205e+04	-5600.54	0.0	0.0	0.0	5.135e+05
		4.328e+05	0.0	0.0	0.0	15.0	-2.186e+04	-5161.69	0.0	0.0	0.0	4.328e+05
14	54	-1.138e+04	0.0	-0.04	438.84	0.0	-1.479e+04	-4767.10	0.0	0.0	0.0	-1.138e+04
		-7.958e+04	0.0	0.0	0.0	15.0	-1.461e+04	-4328.25	0.0	0.0	0.0	-7.958e+04
14	55	-3.859e+05	0.0	-0.11	438.84	0.0	-1.636e+04	-3347.78	0.0	0.0	0.0	-3.859e+05
		-4.328e+05	0.0	0.0	0.0	15.0	-1.618e+04	-2908.94	0.0	0.0	0.0	-4.328e+05
14	56	8.304e+05	0.0	-3.09e-03	438.84	0.0	-2.393e+04	-5895.43	0.0	0.0	0.0	8.304e+05
		7.453e+05	0.0	0.0	0.0	15.0	-2.374e+04	-5456.59	0.0	0.0	0.0	7.453e+05
14	57	6.505e+05	0.0	4.92e-05	438.84	0.0	-1.325e+04	-6337.52	0.0	0.0	0.0	6.505e+05
		5.587e+05	0.0	0.0	0.0	15.0	-1.306e+04	-5898.68	0.0	0.0	0.0	5.587e+05
14	58	7.846e+05	0.0	-2.32e-03	438.84	0.0	-2.126e+04	-5885.78	0.0	0.0	0.0	7.846e+05
		6.996e+05	0.0	0.0	0.0	15.0	-2.107e+04	-5446.94	0.0	0.0	0.0	6.996e+05
14	59	6.496e+05	0.0	-3.37e-05	438.84	0.0	-1.325e+04	-6217.35	0.0	0.0	0.0	6.496e+05
		5.597e+05	0.0	0.0	0.0	15.0	-1.306e+04	-5778.50	0.0	0.0	0.0	5.597e+05
14	60	-1.201e+06	0.0	-0.22	438.84	0.0	-2.922e+04	674.01	0.0	0.0	0.0	-1.214e+06
		-1.214e+06	0.0	0.0	0.0	15.0	-2.903e+04	1112.85	0.0	0.0	0.0	-1.201e+06
14	61	-1.713e+06	0.0	-0.23	438.84	0.0	-2.196e+04	1507.45	0.0	0.0	0.0	-1.739e+06
		-1.739e+06	0.0	0.0	0.0	15.0	-2.178e+04	1946.29	0.0	0.0	0.0	-1.713e+06
14	62	-2.066e+06	0.0	-0.30	438.84	0.0	-2.353e+04	2926.76	0.0	0.0	0.0	-2.114e+06
		-2.114e+06	0.0	0.0	0.0	15.0	-2.335e+04	3365.61	0.0	0.0	0.0	-2.066e+06
14	63	4.657e+05	0.0	-0.04	438.84	0.0	-2.205e+04	-5431.44	0.0	0.0	0.0	4.657e+05
		3.875e+05	0.0	0.0	0.0	15.0	-2.186e+04	-4992.59	0.0	0.0	0.0	3.875e+05
14	64	-5.924e+04	0.0	-0.04	438.84	0.0	-1.479e+04	-4598.00	0.0	0.0	0.0	-5.924e+04
		-1.249e+05	0.0	0.0	0.0	15.0	-1.461e+04	-4159.16	0.0	0.0	0.0	-1.249e+05
14	65	-4.337e+05	0.0	-0.11	438.84	0.0	-1.636e+04	-3178.68	0.0	0.0	0.0	-4.337e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-4.781e+05	0.0	0.0	0.0	15.0	-1.618e+04	-2739.84	0.0	0.0	0.0	-4.781e+05
14	66	-1.172e+06	0.0	-0.25	438.84	0.0	-3.182e+04	546.77	0.0	0.0	0.0	-1.184e+06
		-1.184e+06	0.0	0.0	0.0	15.0	-3.163e+04	985.61	0.0	0.0	0.0	-1.172e+06
14	67	4.959e+05	0.0	-0.07	438.84	0.0	-2.465e+04	-5558.68	0.0	0.0	0.0	4.959e+05
		4.158e+05	0.0	0.0	0.0	15.0	-2.446e+04	-5119.83	0.0	0.0	0.0	4.158e+05
14	68	-2.129e+06	0.0	-0.30	438.84	0.0	-2.353e+04	3531.76	0.0	0.0	0.0	-2.185e+06
		-2.185e+06	0.0	0.0	0.0	15.0	-2.335e+04	3970.61	0.0	0.0	0.0	-2.129e+06
14	69	-5.533e+05	0.0	-0.11	438.84	0.0	-1.636e+04	-2170.35	0.0	0.0	0.0	-5.533e+05
		-5.826e+05	0.0	0.0	0.0	15.0	-1.618e+04	-1731.50	0.0	0.0	0.0	-5.826e+05
14	70	5.631e+05	0.0	-6.09e-04	438.84	0.0	-1.325e+04	-5911.75	0.0	0.0	0.0	5.631e+05
		4.778e+05	0.0	0.0	0.0	15.0	-1.306e+04	-5472.90	0.0	0.0	0.0	4.778e+05
14	71	3.574e+05	0.0	-0.03	438.84	0.0	-1.404e+04	-5564.44	0.0	0.0	0.0	3.574e+05
		2.772e+05	0.0	0.0	0.0	15.0	-1.386e+04	-5125.59	0.0	0.0	0.0	2.772e+05
14	72	6.229e+05	0.0	1.38e-04	438.84	0.0	-1.325e+04	-6415.91	0.0	0.0	0.0	6.229e+05
		5.300e+05	0.0	0.0	0.0	15.0	-1.306e+04	-5977.07	0.0	0.0	0.0	5.300e+05
14	73	2.976e+05	0.0	-0.03	438.84	0.0	-1.404e+04	-5060.27	0.0	0.0	0.0	2.976e+05
		2.250e+05	0.0	0.0	0.0	15.0	-1.386e+04	-4621.42	0.0	0.0	0.0	2.250e+05
14	74	2.400e+05	0.0	-0.03	438.84	0.0	-1.404e+04	-4856.53	0.0	0.0	0.0	2.400e+05
		1.704e+05	0.0	0.0	0.0	15.0	-1.386e+04	-4417.69	0.0	0.0	0.0	1.704e+05
15	1	-3.530e+05	0.0	0.04	-4417.72	0.0	-3.205e+04	5138.79	0.0	0.0	0.0	-8.536e+05
		-8.536e+05	0.0	0.0	0.0	178.3	-2.904e+04	721.07	0.0	0.0	0.0	-3.530e+05
15	2	5339.17	0.0	2.68e-03	-4417.72	0.0	-1.763e+04	5735.61	0.0	0.0	0.0	-6.017e+05
		-6.017e+05	0.0	0.0	0.0	178.3	-1.463e+04	1317.89	0.0	0.0	0.0	5339.17
15	3	-2.721e+05	0.0	0.03	-4417.72	0.0	-2.842e+04	4949.31	0.0	0.0	0.0	-7.389e+05
		-7.389e+05	0.0	0.0	0.0	178.3	-2.541e+04	531.59	0.0	0.0	0.0	-2.721e+05
15	4	-3977.69	0.0	6.98e-03	-4417.72	0.0	-1.763e+04	5395.82	0.0	0.0	0.0	-5.504e+05
		-5.504e+05	0.0	0.0	0.0	178.3	-1.462e+04	978.10	0.0	0.0	0.0	-3977.69
15	5	-6.910e+05	0.0	-3.84	-9635.76	0.0	-1.722e+04	2.262e+04	0.0	0.0	0.0	-3.819e+06
		-3.819e+06	0.0	0.0	0.0	178.3	-1.421e+04	1.299e+04	0.0	0.0	0.0	-6.910e+05
15	6	-2.762e+05	0.0	-4.10	-1.102e+04	0.0	-5424.40	2.589e+04	0.0	0.0	0.0	-3.862e+06
		-3.862e+06	0.0	0.0	0.0	178.3	-2415.02	1.487e+04	0.0	0.0	0.0	-2.762e+05
15	7	-4.099e+05	0.0	-5.20	-1.209e+04	0.0	-3310.02	3.105e+04	0.0	0.0	0.0	-4.839e+06
		-4.839e+06	0.0	0.0	0.0	178.3	-300.65	1.897e+04	0.0	0.0	0.0	-4.099e+05
15	8	2.272e+04	0.0	-0.80	-9635.76	0.0	-2.690e+04	1.488e+04	0.0	0.0	0.0	-1.725e+06
		-1.725e+06	0.0	0.0	0.0	178.3	-2.389e+04	5248.97	0.0	0.0	0.0	2.272e+04
15	9	4.376e+05	0.0	-1.06	-1.102e+04	0.0	-1.510e+04	1.815e+04	0.0	0.0	0.0	-1.769e+06
		-1.769e+06	0.0	0.0	0.0	178.3	-1.209e+04	7128.64	0.0	0.0	0.0	4.376e+05
15	10	3.038e+05	0.0	-2.16	-1.209e+04	0.0	-1.299e+04	2.332e+04	0.0	0.0	0.0	-2.745e+06
		-2.745e+06	0.0	0.0	0.0	178.3	-9979.43	1.123e+04	0.0	0.0	0.0	3.038e+05
15	11	-3.537e+05	0.0	0.04	-4417.72	0.0	-3.205e+04	5146.13	0.0	0.0	0.0	-8.555e+05
		-8.555e+05	0.0	0.0	0.0	178.3	-2.904e+04	728.41	0.0	0.0	0.0	-3.537e+05
15	12	4681.21	0.0	2.61e-03	-4417.72	0.0	-1.763e+04	5742.95	0.0	0.0	0.0	-6.036e+05
		-6.036e+05	0.0	0.0	0.0	178.3	-1.463e+04	1325.22	0.0	0.0	0.0	4681.21
15	13	-1.998e+05	0.0	0.01	-4417.72	0.0	-2.842e+04	6362.23	0.0	0.0	0.0	-9.186e+05
		-9.186e+05	0.0	0.0	0.0	178.3	-2.541e+04	1944.51	0.0	0.0	0.0	-1.998e+05
15	14	6.827e+04	0.0	-0.02	-4417.72	0.0	-1.763e+04	6808.74	0.0	0.0	0.0	-7.301e+05
		-7.301e+05	0.0	0.0	0.0	178.3	-1.463e+04	2391.02	0.0	0.0	0.0	6.827e+04
15	15	-7.446e+05	0.0	-3.83	-9635.76	0.0	-1.722e+04	2.189e+04	0.0	0.0	0.0	-3.742e+06
		-3.742e+06	0.0	0.0	0.0	178.3	-1.421e+04	1.226e+04	0.0	0.0	0.0	-7.446e+05
15	16	-3.298e+05	0.0	-4.09	-1.102e+04	0.0	-5424.40	2.516e+04	0.0	0.0	0.0	-3.785e+06
		-3.785e+06	0.0	0.0	0.0	178.3	-2415.02	1.413e+04	0.0	0.0	0.0	-3.298e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
15	17	-4.636e+05	0.0	-5.19	-1.209e+04	0.0	-3310.02	3.032e+04	0.0	0.0	0.0	-4.761e+06
		-4.761e+06	0.0	0.0	0.0	178.3	-300.65	1.824e+04	0.0	0.0	0.0	-4.636e+05
15	18	4.092e+04	0.0	-0.80	-9635.76	0.0	-2.690e+04	1.468e+04	0.0	0.0	0.0	-1.670e+06
		-1.670e+06	0.0	0.0	0.0	178.3	-2.389e+04	5046.05	0.0	0.0	0.0	4.092e+04
15	19	4.558e+05	0.0	-1.05	-1.102e+04	0.0	-1.510e+04	1.795e+04	0.0	0.0	0.0	-1.714e+06
		-1.714e+06	0.0	0.0	0.0	178.3	-1.209e+04	6925.72	0.0	0.0	0.0	4.558e+05
15	20	3.220e+05	0.0	-2.15	-1.209e+04	0.0	-1.299e+04	2.311e+04	0.0	0.0	0.0	-2.690e+06
		-2.690e+06	0.0	0.0	0.0	178.3	-9979.43	1.103e+04	0.0	0.0	0.0	3.220e+05
15	21	-6.572e+05	0.0	-4.36	-9635.76	0.0	-1.372e+04	2.279e+04	0.0	0.0	0.0	-3.814e+06
		-3.814e+06	0.0	0.0	0.0	178.3	-1.071e+04	1.315e+04	0.0	0.0	0.0	-6.572e+05
15	22	7.408e+04	0.0	-1.31	-9635.76	0.0	-2.339e+04	1.485e+04	0.0	0.0	0.0	-1.668e+06
		-1.668e+06	0.0	0.0	0.0	178.3	-2.038e+04	5217.40	0.0	0.0	0.0	7.408e+04
15	23	-3.762e+05	0.0	-5.20	-1.209e+04	0.0	1261.85	3.020e+04	0.0	0.0	0.0	-4.653e+06
		-4.653e+06	0.0	0.0	0.0	178.3	3491.02	1.812e+04	0.0	0.0	0.0	-3.762e+05
15	24	3.189e+05	0.0	-2.14	-1.209e+04	0.0	-8416.93	2.178e+04	0.0	0.0	0.0	-2.456e+06
		-2.456e+06	0.0	0.0	0.0	178.3	-6187.76	9698.26	0.0	0.0	0.0	3.189e+05
15	25	-7.125e+05	0.0	-3.33	-9635.76	0.0	-2.072e+04	2.229e+04	0.0	0.0	0.0	-3.780e+06
		-3.780e+06	0.0	0.0	0.0	178.3	-1.771e+04	1.265e+04	0.0	0.0	0.0	-7.125e+05
15	26	-2.901e+05	0.0	-4.09	-1.102e+04	0.0	-5424.40	2.538e+04	0.0	0.0	0.0	-3.786e+06
		-3.786e+06	0.0	0.0	0.0	178.3	-2415.02	1.436e+04	0.0	0.0	0.0	-2.901e+05
15	27	-3.187e+04	0.0	-1.47	-9635.76	0.0	-2.584e+04	1.462e+04	0.0	0.0	0.0	-1.731e+06
		-1.731e+06	0.0	0.0	0.0	178.3	-2.284e+04	4980.56	0.0	0.0	0.0	-3.187e+04
15	28	4.289e+05	0.0	-1.05	-1.102e+04	0.0	-1.510e+04	1.780e+04	0.0	0.0	0.0	-1.715e+06
		-1.715e+06	0.0	0.0	0.0	178.3	-1.209e+04	6781.51	0.0	0.0	0.0	4.289e+05
15	29	-4.636e+05	0.0	-5.19	-1.209e+04	0.0	-3310.02	3.032e+04	0.0	0.0	0.0	-4.761e+06
		-4.761e+06	0.0	0.0	0.0	178.3	-300.65	1.824e+04	0.0	0.0	0.0	-4.636e+05
15	30	-3.751e+05	0.0	-3.07	-9635.76	0.0	-1.417e+04	2.048e+04	0.0	0.0	0.0	-3.121e+06
		-3.121e+06	0.0	0.0	0.0	178.3	-1.194e+04	1.085e+04	0.0	0.0	0.0	-3.751e+05
15	31	2.713e+05	0.0	-2.68	-1.102e+04	0.0	-3345.02	2.218e+04	0.0	0.0	0.0	-2.653e+06
		-2.653e+06	0.0	0.0	0.0	178.3	-1115.86	1.116e+04	0.0	0.0	0.0	2.713e+05
15	32	2.626e+05	0.0	-3.13	-1.209e+04	0.0	-3383.72	2.543e+04	0.0	0.0	0.0	-3.163e+06
		-3.163e+06	0.0	0.0	0.0	178.3	-1154.55	1.335e+04	0.0	0.0	0.0	2.626e+05
15	33	-4.356e+05	0.0	-5.21	-1.209e+04	0.0	-3310.02	3.134e+04	0.0	0.0	0.0	-4.915e+06
		-4.915e+06	0.0	0.0	0.0	178.3	-300.65	1.926e+04	0.0	0.0	0.0	-4.356e+05
15	34	-1.148e+05	0.0	0.02	-4417.72	0.0	-2.107e+04	5120.96	0.0	0.0	0.0	-6.122e+05
		-6.122e+05	0.0	0.0	0.0	178.3	-1.884e+04	703.24	0.0	0.0	0.0	-1.148e+05
15	35	1.932e+05	0.0	-0.18	-5445.86	0.0	-1.231e+04	7544.89	0.0	0.0	0.0	-6.448e+05
		-6.448e+05	0.0	0.0	0.0	178.3	-1.008e+04	2099.03	0.0	0.0	0.0	1.932e+05
15	36	1.692e+04	0.0	-0.42	-7137.60	0.0	-2.028e+04	1.031e+04	0.0	0.0	0.0	-1.150e+06
		-1.150e+06	0.0	0.0	0.0	178.3	-1.805e+04	3174.31	0.0	0.0	0.0	1.692e+04
15	37	3.250e+05	0.0	-0.62	-8165.73	0.0	-1.152e+04	1.274e+04	0.0	0.0	0.0	-1.183e+06
		-1.183e+06	0.0	0.0	0.0	178.3	-9290.26	4570.10	0.0	0.0	0.0	3.250e+05
15	38	2.257e+05	0.0	-1.43	-8956.70	0.0	-9949.35	1.657e+04	0.0	0.0	0.0	-1.908e+06
		-1.908e+06	0.0	0.0	0.0	178.3	-7720.18	7615.58	0.0	0.0	0.0	2.257e+05
15	39	-7.715e+04	0.0	9.31e-03	-4417.72	0.0	-2.107e+04	5625.13	0.0	0.0	0.0	-6.645e+05
		-6.645e+05	0.0	0.0	0.0	178.3	-1.884e+04	1207.41	0.0	0.0	0.0	-7.715e+04
15	40	1.219e+05	0.0	-0.01	-4417.72	0.0	-1.306e+04	5956.70	0.0	0.0	0.0	-5.245e+05
		-5.245e+05	0.0	0.0	0.0	178.3	-1.083e+04	1538.98	0.0	0.0	0.0	1.219e+05
15	41	-2.077e+04	0.0	-0.42	-7137.60	0.0	-2.028e+04	9807.74	0.0	0.0	0.0	-1.098e+06
		-1.098e+06	0.0	0.0	0.0	178.3	-1.805e+04	2670.14	0.0	0.0	0.0	-2.077e+04
15	42	2.873e+05	0.0	-0.61	-8165.73	0.0	-1.152e+04	1.223e+04	0.0	0.0	0.0	-1.130e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-1.130e+06	0.0	0.0	0.0	178.3	-9290.26	4065.94	0.0	0.0	0.0	2.873e+05
15	43	1.880e+05	0.0	-1.42	-8956.70	0.0	-9949.35	1.607e+04	0.0	0.0	0.0	-1.855e+06
		-1.855e+06	0.0	0.0	0.0	178.3	-7720.18	7111.41	0.0	0.0	0.0	1.880e+05
15	44	1.351e+04	0.0	-1.78	-8956.70	0.0	-1.536e+04	1.586e+04	0.0	0.0	0.0	-1.993e+06
		-1.993e+06	0.0	0.0	0.0	178.3	-1.313e+04	6907.08	0.0	0.0	0.0	1.351e+04
15	45	2.099e+05	0.0	-1.41	-8956.70	0.0	-9949.35	1.582e+04	0.0	0.0	0.0	-1.790e+06
		-1.790e+06	0.0	0.0	0.0	178.3	-7720.18	6866.93	0.0	0.0	0.0	2.099e+05
15	46	-1.661e+05	0.0	0.02	-4417.72	0.0	-2.374e+04	5212.11	0.0	0.0	0.0	-6.798e+05
		-6.798e+05	0.0	0.0	0.0	178.3	-2.151e+04	794.39	0.0	0.0	0.0	-1.661e+05
15	47	9.931e+04	0.0	-6.86e-03	-4417.72	0.0	-1.306e+04	5654.20	0.0	0.0	0.0	-4.932e+05
		-4.932e+05	0.0	0.0	0.0	178.3	-1.083e+04	1236.47	0.0	0.0	0.0	9.931e+04
15	48	-1.075e+05	0.0	0.02	-4417.72	0.0	-2.107e+04	5039.47	0.0	0.0	0.0	-5.904e+05
		-5.904e+05	0.0	0.0	0.0	178.3	-1.884e+04	621.75	0.0	0.0	0.0	-1.075e+05
15	49	9.155e+04	0.0	2.19e-03	-4417.72	0.0	-1.306e+04	5371.04	0.0	0.0	0.0	-4.504e+05
		-4.504e+05	0.0	0.0	0.0	178.3	-1.083e+04	953.31	0.0	0.0	0.0	9.155e+04
15	50	-4.609e+05	0.0	-2.68	-7137.60	0.0	-1.311e+04	1.636e+04	0.0	0.0	0.0	-2.707e+06
		-2.707e+06	0.0	0.0	0.0	178.3	-1.088e+04	9223.17	0.0	0.0	0.0	-4.609e+05
15	51	-1.528e+05	0.0	-2.87	-8165.73	0.0	-4349.96	1.878e+04	0.0	0.0	0.0	-2.739e+06
		-2.739e+06	0.0	0.0	0.0	178.3	-2120.79	1.062e+04	0.0	0.0	0.0	-1.528e+05
15	52	-2.522e+05	0.0	-3.68	-8956.70	0.0	-2779.88	2.262e+04	0.0	0.0	0.0	-3.464e+06
		-3.464e+06	0.0	0.0	0.0	178.3	-550.71	1.366e+04	0.0	0.0	0.0	-2.522e+05
15	53	6.867e+04	0.0	-0.42	-7137.60	0.0	-2.028e+04	1.066e+04	0.0	0.0	0.0	-1.160e+06
		-1.160e+06	0.0	0.0	0.0	178.3	-1.805e+04	3521.60	0.0	0.0	0.0	6.867e+04
15	54	3.767e+05	0.0	-0.62	-8165.73	0.0	-1.152e+04	1.308e+04	0.0	0.0	0.0	-1.193e+06
		-1.193e+06	0.0	0.0	0.0	178.3	-9290.26	4917.40	0.0	0.0	0.0	3.767e+05
15	55	2.774e+05	0.0	-1.43	-8956.70	0.0	-9949.35	1.692e+04	0.0	0.0	0.0	-1.918e+06
		-1.918e+06	0.0	0.0	0.0	178.3	-7720.18	7962.87	0.0	0.0	0.0	2.774e+05
15	56	-1.881e+05	0.0	0.01	-4417.72	0.0	-2.374e+04	5456.59	0.0	0.0	0.0	-7.453e+05
		-7.453e+05	0.0	0.0	0.0	178.3	-2.151e+04	1038.87	0.0	0.0	0.0	-1.881e+05
15	57	7.738e+04	0.0	-0.02	-4417.72	0.0	-1.306e+04	5898.68	0.0	0.0	0.0	-5.587e+05
		-5.587e+05	0.0	0.0	0.0	178.3	-1.083e+04	1480.95	0.0	0.0	0.0	7.738e+04
15	58	-1.441e+05	0.0	6.26e-03	-4417.72	0.0	-2.107e+04	5446.94	0.0	0.0	0.0	-6.996e+05
		-6.996e+05	0.0	0.0	0.0	178.3	-1.884e+04	1029.21	0.0	0.0	0.0	-1.441e+05
15	59	5.499e+04	0.0	-0.02	-4417.72	0.0	-1.306e+04	5778.50	0.0	0.0	0.0	-5.597e+05
		-5.597e+05	0.0	0.0	0.0	178.3	-1.083e+04	1360.78	0.0	0.0	0.0	5.499e+04
15	60	-4.603e+05	0.0	-2.68	-7137.60	0.0	-1.311e+04	1.635e+04	0.0	0.0	0.0	-2.705e+06
		-2.705e+06	0.0	0.0	0.0	178.3	-1.088e+04	9217.06	0.0	0.0	0.0	-4.603e+05
15	61	-1.523e+05	0.0	-2.87	-8165.73	0.0	-4349.96	1.878e+04	0.0	0.0	0.0	-2.738e+06
		-2.738e+06	0.0	0.0	0.0	178.3	-2120.79	1.061e+04	0.0	0.0	0.0	-1.523e+05
15	62	-2.516e+05	0.0	-3.68	-8956.70	0.0	-2779.88	2.262e+04	0.0	0.0	0.0	-3.462e+06
		-3.462e+06	0.0	0.0	0.0	178.3	-550.71	1.366e+04	0.0	0.0	0.0	-2.516e+05
15	63	8.384e+04	0.0	-0.42	-7137.60	0.0	-2.028e+04	1.049e+04	0.0	0.0	0.0	-1.115e+06
		-1.115e+06	0.0	0.0	0.0	178.3	-1.805e+04	3352.51	0.0	0.0	0.0	8.384e+04
15	64	3.919e+05	0.0	-0.61	-8165.73	0.0	-1.152e+04	1.291e+04	0.0	0.0	0.0	-1.148e+06
		-1.148e+06	0.0	0.0	0.0	178.3	-9290.26	4748.30	0.0	0.0	0.0	3.919e+05
15	65	2.926e+05	0.0	-1.42	-8956.70	0.0	-9949.35	1.675e+04	0.0	0.0	0.0	-1.872e+06
		-1.872e+06	0.0	0.0	0.0	178.3	-7720.18	7793.77	0.0	0.0	0.0	2.926e+05
15	66	-4.357e+05	0.0	-3.06	-7137.60	0.0	-1.051e+04	1.648e+04	0.0	0.0	0.0	-2.703e+06
		-2.703e+06	0.0	0.0	0.0	178.3	-8277.27	9344.30	0.0	0.0	0.0	-4.357e+05
15	67	1.085e+05	0.0	-0.80	-7137.60	0.0	-1.768e+04	1.062e+04	0.0	0.0	0.0	-1.113e+06
		-1.113e+06	0.0	0.0	0.0	178.3	-1.545e+04	3479.74	0.0	0.0	0.0	1.085e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
15	68	-2.968e+05	0.0	-3.67	-8956.70	0.0	-2779.88	2.201e+04	0.0	0.0	0.0	-3.400e+06
		-3.400e+06	0.0	0.0	0.0	178.3	-550.71	1.305e+04	0.0	0.0	0.0	-2.968e+05
15	69	2.172e+05	0.0	-1.41	-8956.70	0.0	-9949.35	1.574e+04	0.0	0.0	0.0	-1.768e+06
		-1.768e+06	0.0	0.0	0.0	178.3	-7720.18	6785.43	0.0	0.0	0.0	2.172e+05
15	70	8.241e+04	0.0	-4.85e-03	-4417.72	0.0	-1.306e+04	5472.90	0.0	0.0	0.0	-4.778e+05
		-4.778e+05	0.0	0.0	0.0	178.3	-1.083e+04	1055.18	0.0	0.0	0.0	8.241e+04
15	71	2.178e+05	0.0	-0.44	-7137.60	0.0	-1.227e+04	1.062e+04	0.0	0.0	0.0	-1.005e+06
		-1.005e+06	0.0	0.0	0.0	178.3	-1.004e+04	3485.50	0.0	0.0	0.0	2.178e+05
15	72	1.201e+05	0.0	-0.01	-4417.72	0.0	-1.306e+04	5977.07	0.0	0.0	0.0	-5.300e+05
		-5.300e+05	0.0	0.0	0.0	178.3	-1.083e+04	1559.35	0.0	0.0	0.0	1.201e+05
15	73	1.801e+05	0.0	-0.44	-7137.60	0.0	-1.227e+04	1.012e+04	0.0	0.0	0.0	-9.526e+05
		-9.526e+05	0.0	0.0	0.0	178.3	-1.004e+04	2981.34	0.0	0.0	0.0	1.801e+05
15	74	1.984e+05	0.0	-0.43	-7137.60	0.0	-1.227e+04	9915.20	0.0	0.0	0.0	-8.979e+05
		-8.979e+05	0.0	0.0	0.0	178.3	-1.004e+04	2777.60	0.0	0.0	0.0	1.984e+05
16	1	8.536e+05	0.0	-0.04	4417.72	0.0	-3.205e+04	-5138.79	0.0	0.0	0.0	8.536e+05
		3.530e+05	0.0	0.0	0.0	178.3	-2.904e+04	-721.07	0.0	0.0	0.0	3.530e+05
16	2	6.017e+05	0.0	-2.68e-03	4417.72	0.0	-1.763e+04	-5735.61	0.0	0.0	0.0	6.017e+05
		-5339.17	0.0	0.0	0.0	178.3	-1.462e+04	-1317.89	0.0	0.0	0.0	-5339.17
16	3	7.389e+05	0.0	-0.03	4417.72	0.0	-2.842e+04	-4949.31	0.0	0.0	0.0	7.389e+05
		2.721e+05	0.0	0.0	0.0	178.3	-2.541e+04	-531.59	0.0	0.0	0.0	2.721e+05
16	4	5.504e+05	0.0	-6.98e-03	4417.72	0.0	-1.763e+04	-5395.82	0.0	0.0	0.0	5.504e+05
		3977.69	0.0	0.0	0.0	178.3	-1.463e+04	-978.10	0.0	0.0	0.0	3977.69
16	5	-7.240e+05	0.0	-3.85	4417.72	0.0	-3.962e+04	4082.10	0.0	0.0	0.0	-1.868e+06
		-1.868e+06	0.0	0.0	0.0	178.3	-3.661e+04	8499.82	0.0	0.0	0.0	-7.240e+05
16	6	-1.214e+06	0.0	-4.03	4417.72	0.0	-2.984e+04	5204.46	0.0	0.0	0.0	-2.558e+06
		-2.558e+06	0.0	0.0	0.0	178.3	-2.683e+04	9622.18	0.0	0.0	0.0	-1.214e+06
16	7	-1.349e+06	0.0	-5.12	4417.72	0.0	-3.196e+04	7115.81	0.0	0.0	0.0	-3.033e+06
		-3.033e+06	0.0	0.0	0.0	178.3	-2.895e+04	1.153e+04	0.0	0.0	0.0	-1.349e+06
16	8	3.290e+05	0.0	-0.79	4417.72	0.0	-2.994e+04	-4337.81	0.0	0.0	0.0	3.290e+05
		-2.879e+04	0.0	0.0	0.0	178.3	-2.693e+04	79.91	0.0	0.0	0.0	-2.879e+04
16	9	-3.611e+05	0.0	-0.97	4417.72	0.0	-2.017e+04	-3215.45	0.0	0.0	0.0	-3.611e+05
		-5.511e+05	0.0	0.0	0.0	178.3	-1.716e+04	1202.27	0.0	0.0	0.0	-5.187e+05
16	10	-6.535e+05	0.0	-2.06	4417.72	0.0	-2.228e+04	-1304.10	0.0	0.0	0.0	-8.367e+05
		-8.668e+05	0.0	0.0	0.0	178.3	-1.927e+04	3113.62	0.0	0.0	0.0	-6.535e+05
16	11	8.555e+05	0.0	-0.04	4417.72	0.0	-3.205e+04	-5146.13	0.0	0.0	0.0	8.555e+05
		3.537e+05	0.0	0.0	0.0	178.3	-2.904e+04	-728.41	0.0	0.0	0.0	3.537e+05
16	12	6.036e+05	0.0	-2.61e-03	4417.72	0.0	-1.763e+04	-5742.95	0.0	0.0	0.0	6.036e+05
		-4681.21	0.0	0.0	0.0	178.3	-1.462e+04	-1325.22	0.0	0.0	0.0	-4681.21
16	13	9.186e+05	0.0	-0.01	4417.72	0.0	-2.842e+04	-6362.23	0.0	0.0	0.0	9.186e+05
		1.998e+05	0.0	0.0	0.0	178.3	-2.541e+04	-1944.51	0.0	0.0	0.0	1.998e+05
16	14	7.301e+05	0.0	0.02	4417.72	0.0	-1.763e+04	-6808.74	0.0	0.0	0.0	7.301e+05
		-6.827e+04	0.0	0.0	0.0	178.3	-1.462e+04	-2391.02	0.0	0.0	0.0	-6.827e+04
16	15	-6.704e+05	0.0	-3.86	4417.72	0.0	-3.962e+04	4815.44	0.0	0.0	0.0	-1.945e+06
		-1.945e+06	0.0	0.0	0.0	178.3	-3.661e+04	9233.16	0.0	0.0	0.0	-6.704e+05
16	16	-1.160e+06	0.0	-4.04	4417.72	0.0	-2.984e+04	5937.80	0.0	0.0	0.0	-2.635e+06
		-2.635e+06	0.0	0.0	0.0	178.3	-2.683e+04	1.036e+04	0.0	0.0	0.0	-1.160e+06
16	17	-1.295e+06	0.0	-5.13	4417.72	0.0	-3.196e+04	7849.15	0.0	0.0	0.0	-3.111e+06
		-3.111e+06	0.0	0.0	0.0	178.3	-2.895e+04	1.227e+04	0.0	0.0	0.0	-1.295e+06
16	18	2.746e+05	0.0	-0.80	4417.72	0.0	-2.994e+04	-4134.89	0.0	0.0	0.0	2.746e+05
		-4.808e+04	0.0	0.0	0.0	178.3	-2.693e+04	282.83	0.0	0.0	0.0	-4.699e+04
16	19	-4.155e+05	0.0	-0.98	4417.72	0.0	-2.017e+04	-3012.53	0.0	0.0	0.0	-4.155e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-5.824e+05	0.0	0.0	0.0	178.3	-1.716e+04	1405.19	0.0	0.0	0.0	-5.369e+05
16	20	-6.717e+05	0.0	-2.07	4417.72	0.0	-2.228e+04	-1101.18	0.0	0.0	0.0	-8.911e+05
		-9.122e+05	0.0	0.0	0.0	178.3	-1.927e+04	3316.54	0.0	0.0	0.0	-6.717e+05
16	21	-7.171e+05	0.0	-4.35	4417.72	0.0	-4.312e+04	3918.09	0.0	0.0	0.0	-1.832e+06
		-1.832e+06	0.0	0.0	0.0	178.3	-4.011e+04	8335.81	0.0	0.0	0.0	-7.171e+05
16	22	3.127e+05	0.0	-1.31	4417.72	0.0	-3.344e+04	-4306.24	0.0	0.0	0.0	3.127e+05
		-3.945e+04	0.0	0.0	0.0	178.3	-3.043e+04	111.48	0.0	0.0	0.0	-3.945e+04
16	23	-1.382e+06	0.0	-5.12	4417.72	0.0	-2.739e+04	7967.84	0.0	0.0	0.0	-3.219e+06
		-3.219e+06	0.0	0.0	0.0	178.3	-2.516e+04	1.239e+04	0.0	0.0	0.0	-1.382e+06
16	24	-6.686e+05	0.0	-2.08	4417.72	0.0	-1.771e+04	227.51	0.0	0.0	0.0	-1.125e+06
		-1.125e+06	0.0	0.0	0.0	178.3	-1.548e+04	4645.23	0.0	0.0	0.0	-6.686e+05
16	25	-7.432e+05	0.0	-3.35	4417.72	0.0	-3.611e+04	4420.44	0.0	0.0	0.0	-1.947e+06
		-1.947e+06	0.0	0.0	0.0	178.3	-3.310e+04	8838.16	0.0	0.0	0.0	-7.432e+05
16	26	-1.200e+06	0.0	-4.04	4417.72	0.0	-2.984e+04	5714.15	0.0	0.0	0.0	-2.635e+06
		-2.635e+06	0.0	0.0	0.0	178.3	-2.683e+04	1.013e+04	0.0	0.0	0.0	-1.200e+06
16	27	3.901e+05	0.0	-1.49	4417.72	0.0	-3.825e+04	-4069.40	0.0	0.0	0.0	3.901e+05
		7.764e+04	0.0	0.0	0.0	178.3	-3.524e+04	348.32	0.0	0.0	0.0	8.019e+04
16	28	-4.143e+05	0.0	-0.98	4417.72	0.0	-2.017e+04	-2868.32	0.0	0.0	0.0	-4.143e+05
		-5.652e+05	0.0	0.0	0.0	178.3	-1.716e+04	1549.40	0.0	0.0	0.0	-5.100e+05
16	29	-1.295e+06	0.0	-5.13	4417.72	0.0	-3.196e+04	7849.15	0.0	0.0	0.0	-3.111e+06
		-3.111e+06	0.0	0.0	0.0	178.3	-2.895e+04	1.227e+04	0.0	0.0	0.0	-1.295e+06
16	30	-1.034e+06	0.0	-3.03	9635.76	0.0	-3.352e+04	-4321.70	0.0	0.0	0.0	-1.170e+06
		-1.323e+06	0.0	0.0	0.0	178.3	-3.129e+04	5314.05	0.0	0.0	0.0	-1.034e+06
16	31	-1.618e+06	0.0	-2.53	1.102e+04	0.0	-2.278e+04	-6017.06	0.0	0.0	0.0	-1.618e+06
		-1.885e+06	0.0	0.0	0.0	178.3	-2.055e+04	5003.26	0.0	0.0	0.0	-1.661e+06
16	32	-1.127e+06	0.0	-2.97	1.209e+04	0.0	-2.274e+04	-9272.12	0.0	0.0	0.0	-1.127e+06
		-1.735e+06	0.0	0.0	0.0	178.3	-2.051e+04	2813.36	0.0	0.0	0.0	-1.672e+06
16	33	-1.323e+06	0.0	-5.11	4417.72	0.0	-3.196e+04	6829.77	0.0	0.0	0.0	-2.957e+06
		-2.957e+06	0.0	0.0	0.0	178.3	-2.895e+04	1.125e+04	0.0	0.0	0.0	-1.323e+06
16	34	6.122e+05	0.0	-0.02	4417.72	0.0	-2.107e+04	-5120.96	0.0	0.0	0.0	6.122e+05
		1.148e+05	0.0	0.0	0.0	178.3	-1.884e+04	-703.24	0.0	0.0	0.0	1.148e+05
16	35	9.983e+04	0.0	-0.15	4417.72	0.0	-1.381e+04	-4287.52	0.0	0.0	0.0	9.983e+04
		-2.489e+05	0.0	0.0	0.0	178.3	-1.158e+04	130.20	0.0	0.0	0.0	-2.489e+05
16	36	4.227e+05	0.0	-0.41	4417.72	0.0	-2.186e+04	-4814.40	0.0	0.0	0.0	4.227e+05
		-2.008e+04	0.0	0.0	0.0	178.3	-1.963e+04	-396.68	0.0	0.0	0.0	-2.008e+04
16	37	-8.975e+04	0.0	-0.54	4417.72	0.0	-1.461e+04	-3980.96	0.0	0.0	0.0	-8.975e+04
		-3.884e+05	0.0	0.0	0.0	178.3	-1.238e+04	436.76	0.0	0.0	0.0	-3.839e+05
16	38	-4.430e+05	0.0	-1.35	4417.72	0.0	-1.618e+04	-2561.65	0.0	0.0	0.0	-4.430e+05
		-5.619e+05	0.0	0.0	0.0	178.3	-1.395e+04	1856.08	0.0	0.0	0.0	-4.839e+05
16	39	6.645e+05	0.0	-9.31e-03	4417.72	0.0	-2.107e+04	-5625.13	0.0	0.0	0.0	6.645e+05
		7.715e+04	0.0	0.0	0.0	178.3	-1.884e+04	-1207.41	0.0	0.0	0.0	7.715e+04
16	40	5.245e+05	0.0	0.01	4417.72	0.0	-1.306e+04	-5956.70	0.0	0.0	0.0	5.245e+05
		-1.219e+05	0.0	0.0	0.0	178.3	-1.083e+04	-1538.98	0.0	0.0	0.0	-1.219e+05
16	41	3.704e+05	0.0	-0.42	4417.72	0.0	-2.186e+04	-4310.23	0.0	0.0	0.0	3.704e+05
		1.761e+04	0.0	0.0	0.0	178.3	-1.963e+04	107.49	0.0	0.0	0.0	1.761e+04
16	42	-1.420e+05	0.0	-0.55	4417.72	0.0	-1.461e+04	-3476.79	0.0	0.0	0.0	-1.420e+05
		-3.669e+05	0.0	0.0	0.0	178.3	-1.238e+04	940.93	0.0	0.0	0.0	-3.462e+05
16	43	-4.463e+05	0.0	-1.36	4417.72	0.0	-1.618e+04	-2057.48	0.0	0.0	0.0	-4.952e+05
		-5.704e+05	0.0	0.0	0.0	178.3	-1.395e+04	2360.24	0.0	0.0	0.0	-4.463e+05
16	44	-2.416e+05	0.0	-1.75	4417.72	0.0	-2.678e+04	-1853.15	0.0	0.0	0.0	-3.269e+05
		-3.885e+05	0.0	0.0	0.0	178.3	-2.455e+04	2564.57	0.0	0.0	0.0	-2.416e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
16	45	-4.682e+05	0.0	-1.37	4417.72	0.0	-1.618e+04	-1813.00	0.0	0.0	0.0	-5.607e+05
		-6.196e+05	0.0	0.0	0.0	178.3	-1.395e+04	2604.72	0.0	0.0	0.0	-4.682e+05
16	46	6.798e+05	0.0	-0.02	4417.72	0.0	-2.374e+04	-5212.11	0.0	0.0	0.0	6.798e+05
		1.661e+05	0.0	0.0	0.0	178.3	-2.151e+04	-794.39	0.0	0.0	0.0	1.661e+05
16	47	4.932e+05	0.0	6.86e-03	4417.72	0.0	-1.306e+04	-5654.20	0.0	0.0	0.0	4.932e+05
		-9.931e+04	0.0	0.0	0.0	178.3	-1.083e+04	-1236.47	0.0	0.0	0.0	-9.931e+04
16	48	5.904e+05	0.0	-0.02	4417.72	0.0	-2.107e+04	-5039.47	0.0	0.0	0.0	5.904e+05
		1.075e+05	0.0	0.0	0.0	178.3	-1.884e+04	-621.75	0.0	0.0	0.0	1.075e+05
16	49	4.504e+05	0.0	-2.19e-03	4417.72	0.0	-1.306e+04	-5371.04	0.0	0.0	0.0	4.504e+05
		-9.155e+04	0.0	0.0	0.0	178.3	-1.083e+04	-953.31	0.0	0.0	0.0	-9.155e+04
16	50	-5.859e+05	0.0	-2.67	4417.72	0.0	-2.903e+04	1106.74	0.0	0.0	0.0	-1.199e+06
		-1.199e+06	0.0	0.0	0.0	178.3	-2.680e+04	5524.46	0.0	0.0	0.0	-5.859e+05
16	51	-9.497e+05	0.0	-2.80	4417.72	0.0	-2.178e+04	1940.18	0.0	0.0	0.0	-1.712e+06
		-1.712e+06	0.0	0.0	0.0	178.3	-1.955e+04	6357.90	0.0	0.0	0.0	-9.497e+05
16	52	-1.050e+06	0.0	-3.61	4417.72	0.0	-2.335e+04	3359.49	0.0	0.0	0.0	-2.065e+06
		-2.065e+06	0.0	0.0	0.0	178.3	-2.112e+04	7777.22	0.0	0.0	0.0	-1.050e+06
16	53	4.328e+05	0.0	-0.41	4417.72	0.0	-2.186e+04	-5161.69	0.0	0.0	0.0	4.328e+05
		-7.184e+04	0.0	0.0	0.0	178.3	-1.963e+04	-743.97	0.0	0.0	0.0	-7.184e+04
16	54	-7.958e+04	0.0	-0.54	4417.72	0.0	-1.461e+04	-4328.25	0.0	0.0	0.0	-7.958e+04
		-4.356e+05	0.0	0.0	0.0	178.3	-1.238e+04	89.47	0.0	0.0	0.0	-4.356e+05
16	55	-4.328e+05	0.0	-1.35	4417.72	0.0	-1.618e+04	-2908.94	0.0	0.0	0.0	-4.328e+05
		-5.882e+05	0.0	0.0	0.0	178.3	-1.395e+04	1508.78	0.0	0.0	0.0	-5.357e+05
16	56	7.453e+05	0.0	-0.01	4417.72	0.0	-2.374e+04	-5456.59	0.0	0.0	0.0	7.453e+05
		1.881e+05	0.0	0.0	0.0	178.3	-2.151e+04	-1038.87	0.0	0.0	0.0	1.881e+05
16	57	5.587e+05	0.0	0.02	4417.72	0.0	-1.306e+04	-5898.68	0.0	0.0	0.0	5.587e+05
		-7.738e+04	0.0	0.0	0.0	178.3	-1.083e+04	-1480.95	0.0	0.0	0.0	-7.738e+04
16	58	6.996e+05	0.0	-6.26e-03	4417.72	0.0	-2.107e+04	-5446.94	0.0	0.0	0.0	6.996e+05
		1.441e+05	0.0	0.0	0.0	178.3	-1.884e+04	-1029.21	0.0	0.0	0.0	1.441e+05
16	59	5.597e+05	0.0	0.02	4417.72	0.0	-1.306e+04	-5778.50	0.0	0.0	0.0	5.597e+05
		-5.499e+04	0.0	0.0	0.0	178.3	-1.083e+04	-1360.78	0.0	0.0	0.0	-5.499e+04
16	60	-5.865e+05	0.0	-2.67	4417.72	0.0	-2.903e+04	1112.85	0.0	0.0	0.0	-1.201e+06
		-1.201e+06	0.0	0.0	0.0	178.3	-2.680e+04	5530.57	0.0	0.0	0.0	-5.865e+05
16	61	-9.503e+05	0.0	-2.80	4417.72	0.0	-2.178e+04	1946.29	0.0	0.0	0.0	-1.713e+06
		-1.713e+06	0.0	0.0	0.0	178.3	-1.955e+04	6364.01	0.0	0.0	0.0	-9.503e+05
16	62	-1.050e+06	0.0	-3.61	4417.72	0.0	-2.335e+04	3365.61	0.0	0.0	0.0	-2.066e+06
		-2.066e+06	0.0	0.0	0.0	178.3	-2.112e+04	7783.33	0.0	0.0	0.0	-1.050e+06
16	63	3.875e+05	0.0	-0.41	4417.72	0.0	-2.186e+04	-4992.59	0.0	0.0	0.0	3.875e+05
		-8.701e+04	0.0	0.0	0.0	178.3	-1.963e+04	-574.87	0.0	0.0	0.0	-8.701e+04
16	64	-1.249e+05	0.0	-0.55	4417.72	0.0	-1.461e+04	-4159.16	0.0	0.0	0.0	-1.249e+05
		-4.513e+05	0.0	0.0	0.0	178.3	-1.238e+04	258.57	0.0	0.0	0.0	-4.508e+05
16	65	-4.781e+05	0.0	-1.35	4417.72	0.0	-1.618e+04	-2739.84	0.0	0.0	0.0	-4.781e+05
		-6.146e+05	0.0	0.0	0.0	178.3	-1.395e+04	1677.88	0.0	0.0	0.0	-5.509e+05
16	66	-5.809e+05	0.0	-3.05	4417.72	0.0	-3.163e+04	985.61	0.0	0.0	0.0	-1.172e+06
		-1.172e+06	0.0	0.0	0.0	178.3	-2.940e+04	5403.34	0.0	0.0	0.0	-5.809e+05
16	67	4.158e+05	0.0	-0.79	4417.72	0.0	-2.446e+04	-5119.83	0.0	0.0	0.0	4.158e+05
		-8.141e+04	0.0	0.0	0.0	178.3	-2.223e+04	-702.11	0.0	0.0	0.0	-8.141e+04
16	68	-1.005e+06	0.0	-3.62	4417.72	0.0	-2.335e+04	3970.61	0.0	0.0	0.0	-2.129e+06
		-2.129e+06	0.0	0.0	0.0	178.3	-2.112e+04	8388.33	0.0	0.0	0.0	-1.005e+06
16	69	-4.755e+05	0.0	-1.37	4417.72	0.0	-1.618e+04	-1731.50	0.0	0.0	0.0	-5.826e+05
		-6.360e+05	0.0	0.0	0.0	178.3	-1.395e+04	2686.22	0.0	0.0	0.0	-4.755e+05
16	70	4.778e+05	0.0	4.85e-03	4417.72	0.0	-1.306e+04	-5472.90	0.0	0.0	0.0	4.778e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-8.241e+04	0.0	0.0	0.0	178.3	-1.083e+04	-1055.18	0.0	0.0	0.0	-8.241e+04
16	71	2.772e+05	0.0	-0.39	4417.72	0.0	-1.386e+04	-5125.59	0.0	0.0	0.0	2.772e+05
		-2.210e+05	0.0	0.0	0.0	178.3	-1.163e+04	-707.87	0.0	0.0	0.0	-2.210e+05
16	72	5.300e+05	0.0	0.01	4417.72	0.0	-1.306e+04	-5977.07	0.0	0.0	0.0	5.300e+05
		-1.201e+05	0.0	0.0	0.0	178.3	-1.083e+04	-1559.35	0.0	0.0	0.0	-1.201e+05
16	73	2.250e+05	0.0	-0.40	4417.72	0.0	-1.386e+04	-4621.42	0.0	0.0	0.0	2.250e+05
		-1.833e+05	0.0	0.0	0.0	178.3	-1.163e+04	-203.70	0.0	0.0	0.0	-1.833e+05
16	74	1.704e+05	0.0	-0.40	4417.72	0.0	-1.386e+04	-4417.69	0.0	0.0	0.0	1.704e+05
		-2.016e+05	0.0	0.0	0.0	178.3	-1.163e+04	0.03	0.0	0.0	0.0	-2.016e+05
17	1	-3.407e+05	0.0	4.37e-03	-2942.50	0.0	-2.904e+04	721.07	0.0	0.0	0.0	-3.530e+05
		-5.087e+05	0.0	0.0	0.0	178.3	-2.603e+04	-2221.43	0.0	0.0	0.0	-5.087e+05
17	2	4.964e+04	0.0	4.22e-03	-2942.50	0.0	-1.462e+04	1317.89	0.0	0.0	0.0	5339.17
		-4.393e+04	0.0	0.0	0.0	178.3	-1.162e+04	-1624.61	0.0	0.0	0.0	-4.393e+04
17	3	-2.653e+05	0.0	6.34e-03	-2942.50	0.0	-2.541e+04	531.59	0.0	0.0	0.0	-2.721e+05
		-4.616e+05	0.0	0.0	0.0	178.3	-2.240e+04	-2410.91	0.0	0.0	0.0	-4.616e+05
17	4	1.981e+04	0.0	1.67e-03	-2942.50	0.0	-1.462e+04	978.10	0.0	0.0	0.0	-3977.69
		-1.138e+05	0.0	0.0	0.0	178.3	-1.162e+04	-1964.40	0.0	0.0	0.0	-1.138e+05
17	5	1.005e+06	0.0	-3.92	-6418.03	0.0	-1.421e+04	1.299e+04	0.0	0.0	0.0	-6.910e+05
		-6.910e+05	0.0	0.0	0.0	178.3	-1.120e+04	6570.53	0.0	0.0	0.0	1.005e+06
17	6	1.632e+06	0.0	-4.14	-7802.59	0.0	-2415.02	1.487e+04	0.0	0.0	0.0	-2.762e+05
		-2.762e+05	0.0	0.0	0.0	178.3	594.36	7065.64	0.0	0.0	0.0	1.632e+06
17	7	2.054e+06	0.0	-5.25	-9945.89	0.0	-300.65	1.897e+04	0.0	0.0	0.0	-4.099e+05
		-4.099e+05	0.0	0.0	0.0	178.3	2708.73	9023.58	0.0	0.0	0.0	2.054e+06
17	8	3.625e+05	0.0	-0.81	-6418.03	0.0	-2.389e+04	5248.97	0.0	0.0	0.0	2.272e+04
		2.272e+04	0.0	0.0	0.0	178.3	-2.088e+04	-1169.06	0.0	0.0	0.0	3.387e+05
17	9	9.715e+05	0.0	-1.03	-7802.59	0.0	-1.209e+04	7128.64	0.0	0.0	0.0	4.376e+05
		4.376e+05	0.0	0.0	0.0	178.3	-9084.43	-673.95	0.0	0.0	0.0	9.653e+05
17	10	1.388e+06	0.0	-2.14	-9945.89	0.0	-9979.43	1.123e+04	0.0	0.0	0.0	3.038e+05
		3.038e+05	0.0	0.0	0.0	178.3	-6970.05	1283.99	0.0	0.0	0.0	1.388e+06
17	11	-3.410e+05	0.0	4.53e-03	-2942.50	0.0	-2.904e+04	728.41	0.0	0.0	0.0	-3.537e+05
		-5.081e+05	0.0	0.0	0.0	178.3	-2.603e+04	-2214.09	0.0	0.0	0.0	-5.081e+05
17	12	4.947e+04	0.0	4.54e-03	-2942.50	0.0	-1.462e+04	1325.22	0.0	0.0	0.0	4681.21
		-4.328e+04	0.0	0.0	0.0	178.3	-1.162e+04	-1617.28	0.0	0.0	0.0	-4.328e+04
17	13	-1.006e+05	0.0	0.01	-2942.50	0.0	-2.541e+04	1944.51	0.0	0.0	0.0	-1.998e+05
		-1.998e+05	0.0	0.0	0.0	178.3	-2.240e+04	-997.99	0.0	0.0	0.0	-1.373e+05
17	14	2.220e+05	0.0	-0.02	-2942.50	0.0	-1.462e+04	2391.02	0.0	0.0	0.0	6.827e+04
		6.827e+04	0.0	0.0	0.0	178.3	-1.162e+04	-551.48	0.0	0.0	0.0	2.104e+05
17	15	8.208e+05	0.0	-3.91	-6418.03	0.0	-1.421e+04	1.226e+04	0.0	0.0	0.0	-7.446e+05
		-7.446e+05	0.0	0.0	0.0	178.3	-1.120e+04	5837.19	0.0	0.0	0.0	8.208e+05
17	16	1.447e+06	0.0	-4.14	-7802.59	0.0	-2415.02	1.413e+04	0.0	0.0	0.0	-3.298e+05
		-3.298e+05	0.0	0.0	0.0	178.3	594.36	6332.30	0.0	0.0	0.0	1.447e+06
17	17	1.870e+06	0.0	-5.25	-9945.89	0.0	-300.65	1.824e+04	0.0	0.0	0.0	-4.636e+05
		-4.636e+05	0.0	0.0	0.0	178.3	2708.73	8290.24	0.0	0.0	0.0	1.870e+06
17	18	3.536e+05	0.0	-0.80	-6418.03	0.0	-2.389e+04	5046.05	0.0	0.0	0.0	4.092e+04
		4.092e+04	0.0	0.0	0.0	178.3	-2.088e+04	-1371.98	0.0	0.0	0.0	3.207e+05
17	19	9.581e+05	0.0	-1.03	-7802.59	0.0	-1.209e+04	6925.72	0.0	0.0	0.0	4.558e+05
		4.558e+05	0.0	0.0	0.0	178.3	-9084.43	-876.87	0.0	0.0	0.0	9.473e+05
17	20	1.370e+06	0.0	-2.14	-9945.89	0.0	-9979.43	1.103e+04	0.0	0.0	0.0	3.220e+05
		3.220e+05	0.0	0.0	0.0	178.3	-6970.05	1081.07	0.0	0.0	0.0	1.370e+06
17	21	1.068e+06	0.0	-4.43	-6418.03	0.0	-1.071e+04	1.315e+04	0.0	0.0	0.0	-6.572e+05
		-6.572e+05	0.0	0.0	0.0	178.3	-7696.37	6734.54	0.0	0.0	0.0	1.068e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
17	22	4.097e+05	0.0	-1.31	-6418.03	0.0	-2.038e+04	5217.40	0.0	0.0	0.0	7.408e+04
		7.408e+04	0.0	0.0	0.0	178.3	-1.738e+04	-1200.63	0.0	0.0	0.0	3.844e+05
17	23	1.936e+06	0.0	-5.24	-9945.89	0.0	3491.02	1.812e+04	0.0	0.0	0.0	-3.762e+05
		-3.762e+05	0.0	0.0	0.0	178.3	5720.19	8171.55	0.0	0.0	0.0	1.936e+06
17	24	1.130e+06	0.0	-2.13	-9945.89	0.0	-6187.76	9698.26	0.0	0.0	0.0	3.189e+05
		3.189e+05	0.0	0.0	0.0	178.3	-3958.59	-247.63	0.0	0.0	0.0	1.130e+06
17	25	9.233e+05	0.0	-3.40	-6418.03	0.0	-1.771e+04	1.265e+04	0.0	0.0	0.0	-7.125e+05
		-7.125e+05	0.0	0.0	0.0	178.3	-1.470e+04	6232.19	0.0	0.0	0.0	9.233e+05
17	26	1.527e+06	0.0	-4.13	-7802.59	0.0	-2415.02	1.436e+04	0.0	0.0	0.0	-2.901e+05
		-2.901e+05	0.0	0.0	0.0	178.3	594.36	6555.95	0.0	0.0	0.0	1.527e+06
17	27	2.720e+05	0.0	-1.49	-6418.03	0.0	-2.284e+04	4980.56	0.0	0.0	0.0	-3.187e+04
		-3.187e+04	0.0	0.0	0.0	178.3	-1.983e+04	-1437.47	0.0	0.0	0.0	2.362e+05
17	28	9.087e+05	0.0	-1.03	-7802.59	0.0	-1.209e+04	6781.51	0.0	0.0	0.0	4.289e+05
		4.289e+05	0.0	0.0	0.0	178.3	-9084.43	-1021.08	0.0	0.0	0.0	8.948e+05
17	29	1.870e+06	0.0	-5.25	-9945.89	0.0	-300.65	1.824e+04	0.0	0.0	0.0	-4.636e+05
		-4.636e+05	0.0	0.0	0.0	178.3	2708.73	8290.24	0.0	0.0	0.0	1.870e+06
17	30	9.390e+05	0.0	-3.11	-6418.03	0.0	-1.194e+04	1.085e+04	0.0	0.0	0.0	-3.751e+05
		-3.751e+05	0.0	0.0	0.0	178.3	-9707.68	4427.41	0.0	0.0	0.0	9.390e+05
17	31	1.517e+06	0.0	-2.67	-7802.59	0.0	-1115.86	1.116e+04	0.0	0.0	0.0	2.713e+05
		2.713e+05	0.0	0.0	0.0	178.3	1113.31	3353.65	0.0	0.0	0.0	1.517e+06
17	32	1.724e+06	0.0	-3.12	-9945.89	0.0	-1154.55	1.335e+04	0.0	0.0	0.0	2.626e+05
		2.626e+05	0.0	0.0	0.0	178.3	1074.62	3400.25	0.0	0.0	0.0	1.724e+06
17	33	2.080e+06	0.0	-5.26	-9945.89	0.0	-300.65	1.926e+04	0.0	0.0	0.0	-4.356e+05
		-4.356e+05	0.0	0.0	0.0	178.3	2708.73	9309.62	0.0	0.0	0.0	2.080e+06
17	34	-1.033e+05	0.0	2.06e-03	-2942.50	0.0	-1.884e+04	703.24	0.0	0.0	0.0	-1.148e+05
		-2.737e+05	0.0	0.0	0.0	178.3	-1.661e+04	-2239.26	0.0	0.0	0.0	-2.737e+05
17	35	2.809e+05	0.0	-0.16	-3970.64	0.0	-1.008e+04	2099.03	0.0	0.0	0.0	1.932e+05
		1.916e+05	0.0	0.0	0.0	178.3	-7853.61	-1871.60	0.0	0.0	0.0	1.916e+05
17	36	1.809e+05	0.0	-0.43	-4754.10	0.0	-1.805e+04	3174.31	0.0	0.0	0.0	1.692e+04
		1.692e+04	0.0	0.0	0.0	178.3	-1.582e+04	-1579.79	0.0	0.0	0.0	1.237e+05
17	37	6.163e+05	0.0	-0.60	-5782.24	0.0	-9290.26	4570.10	0.0	0.0	0.0	3.250e+05
		3.250e+05	0.0	0.0	0.0	178.3	-7061.09	-1212.13	0.0	0.0	0.0	5.890e+05
17	38	9.027e+05	0.0	-1.42	-7373.79	0.0	-7720.18	7615.58	0.0	0.0	0.0	2.257e+05
		2.257e+05	0.0	0.0	0.0	178.3	-5491.01	241.78	0.0	0.0	0.0	9.027e+05
17	39	-4.024e+04	0.0	2.62e-03	-2942.50	0.0	-1.884e+04	1207.41	0.0	0.0	0.0	-7.715e+04
		-1.461e+05	0.0	0.0	0.0	178.3	-1.661e+04	-1735.09	0.0	0.0	0.0	-1.461e+05
17	40	1.826e+05	0.0	-5.05e-03	-2942.50	0.0	-1.083e+04	1538.98	0.0	0.0	0.0	1.219e+05
		1.121e+05	0.0	0.0	0.0	178.3	-8604.17	-1403.52	0.0	0.0	0.0	1.121e+05
17	41	9.363e+04	0.0	-0.43	-4754.10	0.0	-1.805e+04	2670.14	0.0	0.0	0.0	-2.077e+04
		-2.077e+04	0.0	0.0	0.0	178.3	-1.582e+04	-2083.96	0.0	0.0	0.0	-3924.97
17	42	5.149e+05	0.0	-0.59	-5782.24	0.0	-9290.26	4065.93	0.0	0.0	0.0	2.873e+05
		2.873e+05	0.0	0.0	0.0	178.3	-7061.09	-1716.30	0.0	0.0	0.0	4.614e+05
17	43	7.751e+05	0.0	-1.42	-7373.79	0.0	-7720.18	7111.41	0.0	0.0	0.0	1.880e+05
		1.880e+05	0.0	0.0	0.0	178.3	-5491.01	-262.39	0.0	0.0	0.0	7.751e+05
17	44	5.654e+05	0.0	-1.79	-7373.79	0.0	-1.313e+04	6907.08	0.0	0.0	0.0	1.351e+04
		1.351e+04	0.0	0.0	0.0	178.3	-1.090e+04	-466.71	0.0	0.0	0.0	5.642e+05
17	45	7.555e+05	0.0	-1.41	-7373.79	0.0	-7720.18	6866.93	0.0	0.0	0.0	2.099e+05
		2.099e+05	0.0	0.0	0.0	178.3	-5491.01	-506.87	0.0	0.0	0.0	7.535e+05
17	46	-1.505e+05	0.0	2.16e-03	-2942.50	0.0	-2.151e+04	794.39	0.0	0.0	0.0	-1.661e+05
		-3.088e+05	0.0	0.0	0.0	178.3	-1.928e+04	-2148.11	0.0	0.0	0.0	-3.088e+05
17	47	1.382e+05	0.0	-3.07e-03	-2942.50	0.0	-1.083e+04	1236.47	0.0	0.0	0.0	9.931e+04

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		3.552e+04	0.0	0.0	0.0	178.3	-8604.17	-1706.03	0.0	0.0	0.0	3.552e+04
17	48	-9.871e+04	0.0	4.62e-03	-2942.50	0.0	-1.884e+04	621.75	0.0	0.0	0.0	-1.075e+05
		-2.809e+05	0.0	0.0	0.0	178.3	-1.661e+04	-2320.75	0.0	0.0	0.0	-2.809e+05
17	49	1.142e+05	0.0	2.09e-03	-2942.50	0.0	-1.083e+04	953.31	0.0	0.0	0.0	9.155e+04
		-2.274e+04	0.0	0.0	0.0	178.3	-8604.17	-1989.19	0.0	0.0	0.0	-2.274e+04
17	50	7.246e+05	0.0	-2.73	-4754.10	0.0	-1.088e+04	9223.17	0.0	0.0	0.0	-4.609e+05
		-4.609e+05	0.0	0.0	0.0	178.3	-8648.83	4469.07	0.0	0.0	0.0	7.246e+05
17	51	1.190e+06	0.0	-2.89	-5782.24	0.0	-2120.79	1.062e+04	0.0	0.0	0.0	-1.528e+05
		-1.528e+05	0.0	0.0	0.0	178.3	108.38	4836.73	0.0	0.0	0.0	1.190e+06
17	52	1.504e+06	0.0	-3.72	-7373.79	0.0	-550.71	1.366e+04	0.0	0.0	0.0	-2.522e+05
		-2.522e+05	0.0	0.0	0.0	178.3	1678.46	6290.64	0.0	0.0	0.0	1.504e+06
17	53	2.714e+05	0.0	-0.43	-4754.10	0.0	-1.805e+04	3521.60	0.0	0.0	0.0	6.867e+04
		6.867e+04	0.0	0.0	0.0	178.3	-1.582e+04	-1232.49	0.0	0.0	0.0	2.374e+05
17	54	7.154e+05	0.0	-0.59	-5782.24	0.0	-9290.26	4917.40	0.0	0.0	0.0	3.767e+05
		3.767e+05	0.0	0.0	0.0	178.3	-7061.09	-864.84	0.0	0.0	0.0	7.027e+05
17	55	1.016e+06	0.0	-1.42	-7373.79	0.0	-7720.18	7962.87	0.0	0.0	0.0	2.774e+05
		2.774e+05	0.0	0.0	0.0	178.3	-5491.01	589.08	0.0	0.0	0.0	1.016e+06
17	56	-1.616e+05	0.0	0.01	-2942.50	0.0	-2.151e+04	1038.87	0.0	0.0	0.0	-1.881e+05
		-2.871e+05	0.0	0.0	0.0	178.3	-1.928e+04	-1903.63	0.0	0.0	0.0	-2.871e+05
17	57	1.329e+05	0.0	-0.01	-2942.50	0.0	-1.083e+04	1480.95	0.0	0.0	0.0	7.738e+04
		5.719e+04	0.0	0.0	0.0	178.3	-8604.17	-1461.55	0.0	0.0	0.0	5.719e+04
17	58	-1.180e+05	0.0	0.01	-2942.50	0.0	-1.884e+04	1029.21	0.0	0.0	0.0	-1.441e+05
		-2.448e+05	0.0	0.0	0.0	178.3	-1.661e+04	-1913.29	0.0	0.0	0.0	-2.448e+05
17	59	1.022e+05	0.0	-0.02	-2942.50	0.0	-1.083e+04	1360.78	0.0	0.0	0.0	5.499e+04
		1.337e+04	0.0	0.0	0.0	178.3	-8604.17	-1581.72	0.0	0.0	0.0	1.337e+04
17	60	7.240e+05	0.0	-2.73	-4754.10	0.0	-1.088e+04	9217.06	0.0	0.0	0.0	-4.603e+05
		-4.603e+05	0.0	0.0	0.0	178.3	-8648.83	4462.96	0.0	0.0	0.0	7.240e+05
17	61	1.189e+06	0.0	-2.89	-5782.24	0.0	-2120.79	1.061e+04	0.0	0.0	0.0	-1.523e+05
		-1.523e+05	0.0	0.0	0.0	178.3	108.38	4830.62	0.0	0.0	0.0	1.189e+06
17	62	1.503e+06	0.0	-3.72	-7373.79	0.0	-550.71	1.366e+04	0.0	0.0	0.0	-2.516e+05
		-2.516e+05	0.0	0.0	0.0	178.3	1678.46	6284.53	0.0	0.0	0.0	1.503e+06
17	63	2.677e+05	0.0	-0.42	-4754.10	0.0	-1.805e+04	3352.51	0.0	0.0	0.0	8.384e+04
		8.384e+04	0.0	0.0	0.0	178.3	-1.582e+04	-1401.59	0.0	0.0	0.0	2.224e+05
17	64	7.071e+05	0.0	-0.58	-5782.24	0.0	-9290.26	4748.30	0.0	0.0	0.0	3.919e+05
		3.919e+05	0.0	0.0	0.0	178.3	-7061.09	-1033.94	0.0	0.0	0.0	6.877e+05
17	65	1.001e+06	0.0	-1.41	-7373.79	0.0	-7720.18	7793.77	0.0	0.0	0.0	2.926e+05
		2.926e+05	0.0	0.0	0.0	178.3	-5491.01	419.98	0.0	0.0	0.0	1.001e+06
17	66	7.713e+05	0.0	-3.10	-4754.10	0.0	-8277.27	9344.30	0.0	0.0	0.0	-4.357e+05
		-4.357e+05	0.0	0.0	0.0	178.3	-6048.10	4590.20	0.0	0.0	0.0	7.713e+05
17	67	3.065e+05	0.0	-0.80	-4754.10	0.0	-1.545e+04	3479.74	0.0	0.0	0.0	1.085e+05
		1.085e+05	0.0	0.0	0.0	178.3	-1.322e+04	-1274.36	0.0	0.0	0.0	2.697e+05
17	68	1.350e+06	0.0	-3.71	-7373.79	0.0	-550.71	1.305e+04	0.0	0.0	0.0	-2.968e+05
		-2.968e+05	0.0	0.0	0.0	178.3	1678.46	5679.53	0.0	0.0	0.0	1.350e+06
17	69	7.501e+05	0.0	-1.40	-7373.79	0.0	-7720.18	6785.43	0.0	0.0	0.0	2.172e+05
		2.172e+05	0.0	0.0	0.0	178.3	-5491.01	-588.36	0.0	0.0	0.0	7.463e+05
17	70	1.096e+05	0.0	-2.41e-03	-2942.50	0.0	-1.083e+04	1055.18	0.0	0.0	0.0	8.241e+04
		-1.371e+04	0.0	0.0	0.0	178.3	-8604.17	-1887.32	0.0	0.0	0.0	-1.371e+04
17	71	4.165e+05	0.0	-0.43	-4754.10	0.0	-1.004e+04	3485.50	0.0	0.0	0.0	2.178e+05
		2.178e+05	0.0	0.0	0.0	178.3	-7811.65	-1268.60	0.0	0.0	0.0	3.801e+05
17	72	1.826e+05	0.0	-5.83e-03	-2942.50	0.0	-1.083e+04	1559.35	0.0	0.0	0.0	1.201e+05
		1.139e+05	0.0	0.0	0.0	178.3	-8604.17	-1383.15	0.0	0.0	0.0	1.139e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
17	73	3.226e+05	0.0	-0.43	-4754.10	0.0	-1.004e+04	2981.33	0.0	0.0	0.0	1.801e+05
		1.801e+05	0.0	0.0	0.0	178.3	-7811.65	-1772.76	0.0	0.0	0.0	2.525e+05
17	74	3.224e+05	0.0	-0.42	-4754.10	0.0	-1.004e+04	2777.60	0.0	0.0	0.0	1.984e+05
		1.984e+05	0.0	0.0	0.0	178.3	-7811.65	-1976.50	0.0	0.0	0.0	2.344e+05
18	1	5.087e+05	0.0	-4.37e-03	2942.50	0.0	-2.904e+04	-721.07	0.0	0.0	0.0	3.530e+05
		3.407e+05	0.0	0.0	0.0	178.3	-2.603e+04	2221.43	0.0	0.0	0.0	5.087e+05
18	2	4.393e+04	0.0	-4.22e-03	2942.50	0.0	-1.462e+04	-1317.89	0.0	0.0	0.0	-5339.17
		-4.964e+04	0.0	0.0	0.0	178.3	-1.162e+04	1624.61	0.0	0.0	0.0	4.393e+04
18	3	4.616e+05	0.0	-6.34e-03	2942.50	0.0	-2.541e+04	-531.59	0.0	0.0	0.0	2.721e+05
		2.653e+05	0.0	0.0	0.0	178.3	-2.240e+04	2410.91	0.0	0.0	0.0	4.616e+05
18	4	1.138e+05	0.0	-1.67e-03	2942.50	0.0	-1.462e+04	-978.10	0.0	0.0	0.0	3977.69
		-1.981e+04	0.0	0.0	0.0	178.3	-1.162e+04	1964.40	0.0	0.0	0.0	1.138e+05
18	5	1.076e+06	0.0	-3.91	2942.50	0.0	-3.661e+04	8499.82	0.0	0.0	0.0	-7.240e+05
		-7.240e+05	0.0	0.0	0.0	178.3	-3.360e+04	1.144e+04	0.0	0.0	0.0	1.076e+06
18	6	7.864e+05	0.0	-4.13	2942.50	0.0	-2.683e+04	9622.18	0.0	0.0	0.0	-1.214e+06
		-1.214e+06	0.0	0.0	0.0	178.3	-2.383e+04	1.256e+04	0.0	0.0	0.0	7.864e+05
18	7	9.925e+05	0.0	-5.23	2942.50	0.0	-2.895e+04	1.153e+04	0.0	0.0	0.0	-1.349e+06
		-1.349e+06	0.0	0.0	0.0	178.3	-2.594e+04	1.448e+04	0.0	0.0	0.0	9.925e+05
18	8	2.698e+05	0.0	-0.79	2942.50	0.0	-2.693e+04	79.91	0.0	0.0	0.0	-2.879e+04
		-2.879e+04	0.0	0.0	0.0	178.3	-2.392e+04	3022.41	0.0	0.0	0.0	2.698e+05
18	9	-1.997e+04	0.0	-1.01	2942.50	0.0	-1.716e+04	1202.27	0.0	0.0	0.0	-5.187e+05
		-5.187e+05	0.0	0.0	0.0	178.3	-1.415e+04	4144.77	0.0	0.0	0.0	-1.997e+04
18	10	1.861e+05	0.0	-2.12	2942.50	0.0	-1.927e+04	3113.62	0.0	0.0	0.0	-6.535e+05
		-6.535e+05	0.0	0.0	0.0	178.3	-1.626e+04	6056.12	0.0	0.0	0.0	1.861e+05
18	11	5.081e+05	0.0	-4.53e-03	2942.50	0.0	-2.904e+04	-728.41	0.0	0.0	0.0	3.537e+05
		3.410e+05	0.0	0.0	0.0	178.3	-2.603e+04	2214.09	0.0	0.0	0.0	5.081e+05
18	12	4.328e+04	0.0	-4.54e-03	2942.50	0.0	-1.462e+04	-1325.22	0.0	0.0	0.0	-4681.21
		-4.947e+04	0.0	0.0	0.0	178.3	-1.162e+04	1617.28	0.0	0.0	0.0	4.328e+04
18	13	1.998e+05	0.0	-0.01	2942.50	0.0	-2.541e+04	-1944.51	0.0	0.0	0.0	1.998e+05
		1.006e+05	0.0	0.0	0.0	178.3	-2.240e+04	997.99	0.0	0.0	0.0	1.373e+05
18	14	-6.827e+04	0.0	0.02	2942.50	0.0	-1.462e+04	-2391.02	0.0	0.0	0.0	-6.827e+04
		-2.220e+05	0.0	0.0	0.0	178.3	-1.162e+04	551.48	0.0	0.0	0.0	-2.104e+05
18	15	1.261e+06	0.0	-3.91	2942.50	0.0	-3.661e+04	9233.16	0.0	0.0	0.0	-6.704e+05
		-6.704e+05	0.0	0.0	0.0	178.3	-3.360e+04	1.218e+04	0.0	0.0	0.0	1.261e+06
18	16	9.708e+05	0.0	-4.14	2942.50	0.0	-2.683e+04	1.036e+04	0.0	0.0	0.0	-1.160e+06
		-1.160e+06	0.0	0.0	0.0	178.3	-2.383e+04	1.330e+04	0.0	0.0	0.0	9.708e+05
18	17	1.177e+06	0.0	-5.24	2942.50	0.0	-2.895e+04	1.227e+04	0.0	0.0	0.0	-1.295e+06
		-1.295e+06	0.0	0.0	0.0	178.3	-2.594e+04	1.521e+04	0.0	0.0	0.0	1.177e+06
18	18	2.877e+05	0.0	-0.80	2942.50	0.0	-2.693e+04	282.83	0.0	0.0	0.0	-4.699e+04
		-4.699e+04	0.0	0.0	0.0	178.3	-2.392e+04	3225.33	0.0	0.0	0.0	2.877e+05
18	19	-1989.42	0.0	-1.02	2942.50	0.0	-1.716e+04	1405.19	0.0	0.0	0.0	-5.369e+05
		-5.369e+05	0.0	0.0	0.0	178.3	-1.415e+04	4347.69	0.0	0.0	0.0	-1989.42
18	20	2.041e+05	0.0	-2.12	2942.50	0.0	-1.927e+04	3316.54	0.0	0.0	0.0	-6.717e+05
		-6.717e+05	0.0	0.0	0.0	178.3	-1.626e+04	6259.04	0.0	0.0	0.0	2.041e+05
18	21	1.054e+06	0.0	-4.41	2942.50	0.0	-4.011e+04	8335.81	0.0	0.0	0.0	-7.171e+05
		-7.171e+05	0.0	0.0	0.0	178.3	-3.710e+04	1.128e+04	0.0	0.0	0.0	1.054e+06
18	22	2.647e+05	0.0	-1.31	2942.50	0.0	-3.043e+04	111.48	0.0	0.0	0.0	-3.945e+04
		-3.945e+04	0.0	0.0	0.0	178.3	-2.742e+04	3053.98	0.0	0.0	0.0	2.647e+05
18	23	1.111e+06	0.0	-5.24	2942.50	0.0	-2.516e+04	1.239e+04	0.0	0.0	0.0	-1.382e+06
		-1.382e+06	0.0	0.0	0.0	178.3	-2.293e+04	1.533e+04	0.0	0.0	0.0	1.111e+06
18	24	4.441e+05	0.0	-2.13	2942.50	0.0	-1.548e+04	4645.23	0.0	0.0	0.0	-6.686e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-6.686e+05	0.0	0.0	0.0	178.3	-1.325e+04	7587.73	0.0	0.0	0.0	4.441e+05
18	25	1.117e+06	0.0	-3.41	2942.50	0.0	-3.310e+04	8838.16	0.0	0.0	0.0	-7.432e+05
		-7.432e+05	0.0	0.0	0.0	178.3	-3.009e+04	1.178e+04	0.0	0.0	0.0	1.117e+06
18	26	8.913e+05	0.0	-4.14	2942.50	0.0	-2.683e+04	1.013e+04	0.0	0.0	0.0	-1.200e+06
		-1.200e+06	0.0	0.0	0.0	178.3	-2.383e+04	1.307e+04	0.0	0.0	0.0	8.913e+05
18	27	4.266e+05	0.0	-1.47	2942.50	0.0	-3.524e+04	348.32	0.0	0.0	0.0	8.019e+04
		8.019e+04	0.0	0.0	0.0	178.3	-3.223e+04	3290.82	0.0	0.0	0.0	4.266e+05
18	28	5.059e+04	0.0	-1.02	2942.50	0.0	-1.716e+04	1549.40	0.0	0.0	0.0	-5.100e+05
		-5.100e+05	0.0	0.0	0.0	178.3	-1.415e+04	4491.90	0.0	0.0	0.0	5.059e+04
18	29	1.177e+06	0.0	-5.24	2942.50	0.0	-2.895e+04	1.227e+04	0.0	0.0	0.0	-1.295e+06
		-1.295e+06	0.0	0.0	0.0	178.3	-2.594e+04	1.521e+04	0.0	0.0	0.0	1.177e+06
18	30	5.339e+05	0.0	-3.11	6418.03	0.0	-3.129e+04	5314.05	0.0	0.0	0.0	-1.034e+06
		-1.034e+06	0.0	0.0	0.0	178.3	-2.907e+04	1.173e+04	0.0	0.0	0.0	5.339e+05
18	31	-2.508e+04	0.0	-2.67	7802.59	0.0	-2.055e+04	5003.26	0.0	0.0	0.0	-1.661e+06
		-1.661e+06	0.0	0.0	0.0	178.3	-1.832e+04	1.281e+04	0.0	0.0	0.0	-2.508e+04
18	32	-2.512e+05	0.0	-3.10	9945.89	0.0	-2.051e+04	2813.36	0.0	0.0	0.0	-1.672e+06
		-1.672e+06	0.0	0.0	0.0	178.3	-1.828e+04	1.276e+04	0.0	0.0	0.0	-2.512e+05
18	33	9.671e+05	0.0	-5.22	2942.50	0.0	-2.895e+04	1.125e+04	0.0	0.0	0.0	-1.323e+06
		-1.323e+06	0.0	0.0	0.0	178.3	-2.594e+04	1.419e+04	0.0	0.0	0.0	9.671e+05
18	34	2.737e+05	0.0	-2.06e-03	2942.50	0.0	-1.884e+04	-703.24	0.0	0.0	0.0	1.148e+05
		1.033e+05	0.0	0.0	0.0	178.3	-1.661e+04	2239.26	0.0	0.0	0.0	2.737e+05
18	35	5.858e+04	0.0	-0.17	2942.50	0.0	-1.158e+04	130.20	0.0	0.0	0.0	-2.489e+05
		-2.489e+05	0.0	0.0	0.0	178.3	-9354.72	3072.70	0.0	0.0	0.0	5.858e+04
18	36	1.935e+05	0.0	-0.41	2942.50	0.0	-1.963e+04	-396.68	0.0	0.0	0.0	-2.008e+04
		-2.388e+04	0.0	0.0	0.0	178.3	-1.740e+04	2545.82	0.0	0.0	0.0	1.935e+05
18	37	-2.167e+04	0.0	-0.57	2942.50	0.0	-1.238e+04	436.76	0.0	0.0	0.0	-3.839e+05
		-3.839e+05	0.0	0.0	0.0	178.3	-1.015e+04	3379.26	0.0	0.0	0.0	-2.167e+04
18	38	1.313e+05	0.0	-1.39	2942.50	0.0	-1.395e+04	1856.08	0.0	0.0	0.0	-4.839e+05
		-4.839e+05	0.0	0.0	0.0	178.3	-1.172e+04	4798.58	0.0	0.0	0.0	1.313e+05
18	39	1.461e+05	0.0	-2.62e-03	2942.50	0.0	-1.884e+04	-1207.41	0.0	0.0	0.0	7.715e+04
		4.024e+04	0.0	0.0	0.0	178.3	-1.661e+04	1735.09	0.0	0.0	0.0	1.461e+05
18	40	-1.121e+05	0.0	5.05e-03	2942.50	0.0	-1.083e+04	-1538.98	0.0	0.0	0.0	-1.219e+05
		-1.826e+05	0.0	0.0	0.0	178.3	-8604.17	1403.52	0.0	0.0	0.0	-1.121e+05
18	41	3.211e+05	0.0	-0.41	2942.50	0.0	-1.963e+04	107.49	0.0	0.0	0.0	1.761e+04
		1.761e+04	0.0	0.0	0.0	178.3	-1.740e+04	3049.99	0.0	0.0	0.0	3.211e+05
18	42	1.059e+05	0.0	-0.57	2942.50	0.0	-1.238e+04	940.93	0.0	0.0	0.0	-3.462e+05
		-3.462e+05	0.0	0.0	0.0	178.3	-1.015e+04	3883.43	0.0	0.0	0.0	1.059e+05
18	43	2.589e+05	0.0	-1.39	2942.50	0.0	-1.395e+04	2360.24	0.0	0.0	0.0	-4.463e+05
		-4.463e+05	0.0	0.0	0.0	178.3	-1.172e+04	5302.74	0.0	0.0	0.0	2.589e+05
18	44	5.001e+05	0.0	-1.77	2942.50	0.0	-2.455e+04	2564.57	0.0	0.0	0.0	-2.416e+05
		-2.416e+05	0.0	0.0	0.0	178.3	-2.232e+04	5507.07	0.0	0.0	0.0	5.001e+05
18	45	2.806e+05	0.0	-1.40	2942.50	0.0	-1.395e+04	2604.72	0.0	0.0	0.0	-4.682e+05
		-4.682e+05	0.0	0.0	0.0	178.3	-1.172e+04	5547.22	0.0	0.0	0.0	2.806e+05
18	46	3.088e+05	0.0	-2.16e-03	2942.50	0.0	-2.151e+04	-794.39	0.0	0.0	0.0	1.661e+05
		1.505e+05	0.0	0.0	0.0	178.3	-1.928e+04	2148.11	0.0	0.0	0.0	3.088e+05
18	47	-3.552e+04	0.0	3.07e-03	2942.50	0.0	-1.083e+04	-1236.47	0.0	0.0	0.0	-9.931e+04
		-1.382e+05	0.0	0.0	0.0	178.3	-8604.17	1706.03	0.0	0.0	0.0	-3.552e+04
18	48	2.809e+05	0.0	-4.62e-03	2942.50	0.0	-1.884e+04	-621.75	0.0	0.0	0.0	1.075e+05
		9.871e+04	0.0	0.0	0.0	178.3	-1.661e+04	2320.75	0.0	0.0	0.0	2.809e+05
18	49	2.274e+04	0.0	-2.09e-03	2942.50	0.0	-1.083e+04	-953.31	0.0	0.0	0.0	-9.155e+04
		-1.142e+05	0.0	0.0	0.0	178.3	-8604.17	1989.19	0.0	0.0	0.0	2.274e+04

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
18	50	6.836e+05	0.0	-2.72	2942.50	0.0	-2.680e+04	5524.46	0.0	0.0	0.0	-5.859e+05
		-5.859e+05	0.0	0.0	0.0	178.3	-2.457e+04	8466.96	0.0	0.0	0.0	6.836e+05
18	51	4.684e+05	0.0	-2.88	2942.50	0.0	-1.955e+04	6357.90	0.0	0.0	0.0	-9.497e+05
		-9.497e+05	0.0	0.0	0.0	178.3	-1.732e+04	9300.40	0.0	0.0	0.0	4.684e+05
18	52	6.214e+05	0.0	-3.70	2942.50	0.0	-2.112e+04	7777.22	0.0	0.0	0.0	-1.050e+06
		-1.050e+06	0.0	0.0	0.0	178.3	-1.889e+04	1.072e+04	0.0	0.0	0.0	6.214e+05
18	53	7.979e+04	0.0	-0.41	2942.50	0.0	-1.963e+04	-743.97	0.0	0.0	0.0	-7.184e+04
		-8.518e+04	0.0	0.0	0.0	178.3	-1.740e+04	2198.53	0.0	0.0	0.0	7.979e+04
18	54	-1.354e+05	0.0	-0.57	2942.50	0.0	-1.238e+04	89.47	0.0	0.0	0.0	-4.356e+05
		-4.356e+05	0.0	0.0	0.0	178.3	-1.015e+04	3031.97	0.0	0.0	0.0	-1.354e+05
18	55	1.765e+04	0.0	-1.39	2942.50	0.0	-1.395e+04	1508.78	0.0	0.0	0.0	-5.357e+05
		-5.357e+05	0.0	0.0	0.0	178.3	-1.172e+04	4451.28	0.0	0.0	0.0	1.765e+04
18	56	2.871e+05	0.0	-0.01	2942.50	0.0	-2.151e+04	-1038.87	0.0	0.0	0.0	1.881e+05
		1.616e+05	0.0	0.0	0.0	178.3	-1.928e+04	1903.63	0.0	0.0	0.0	2.871e+05
18	57	-5.719e+04	0.0	0.01	2942.50	0.0	-1.083e+04	-1480.95	0.0	0.0	0.0	-7.738e+04
		-1.329e+05	0.0	0.0	0.0	178.3	-8604.17	1461.55	0.0	0.0	0.0	-5.719e+04
18	58	2.448e+05	0.0	-0.01	2942.50	0.0	-1.884e+04	-1029.21	0.0	0.0	0.0	1.441e+05
		1.180e+05	0.0	0.0	0.0	178.3	-1.661e+04	1913.29	0.0	0.0	0.0	2.448e+05
18	59	-1.337e+04	0.0	0.02	2942.50	0.0	-1.083e+04	-1360.78	0.0	0.0	0.0	-5.499e+04
		-1.022e+05	0.0	0.0	0.0	178.3	-8604.17	1581.72	0.0	0.0	0.0	-1.337e+04
18	60	6.841e+05	0.0	-2.72	2942.50	0.0	-2.680e+04	5530.57	0.0	0.0	0.0	-5.865e+05
		-5.865e+05	0.0	0.0	0.0	178.3	-2.457e+04	8473.07	0.0	0.0	0.0	6.841e+05
18	61	4.690e+05	0.0	-2.88	2942.50	0.0	-1.955e+04	6364.01	0.0	0.0	0.0	-9.503e+05
		-9.503e+05	0.0	0.0	0.0	178.3	-1.732e+04	9306.51	0.0	0.0	0.0	4.690e+05
18	62	6.220e+05	0.0	-3.70	2942.50	0.0	-2.112e+04	7783.33	0.0	0.0	0.0	-1.050e+06
		-1.050e+06	0.0	0.0	0.0	178.3	-1.889e+04	1.073e+04	0.0	0.0	0.0	6.220e+05
18	63	9.477e+04	0.0	-0.42	2942.50	0.0	-1.963e+04	-574.87	0.0	0.0	0.0	-8.701e+04
		-9.478e+04	0.0	0.0	0.0	178.3	-1.740e+04	2367.63	0.0	0.0	0.0	9.477e+04
18	64	-1.204e+05	0.0	-0.58	2942.50	0.0	-1.238e+04	258.57	0.0	0.0	0.0	-4.508e+05
		-4.508e+05	0.0	0.0	0.0	178.3	-1.015e+04	3201.07	0.0	0.0	0.0	-1.204e+05
18	65	3.264e+04	0.0	-1.40	2942.50	0.0	-1.395e+04	1677.88	0.0	0.0	0.0	-5.509e+05
		-5.509e+05	0.0	0.0	0.0	178.3	-1.172e+04	4620.38	0.0	0.0	0.0	3.264e+04
18	66	6.670e+05	0.0	-3.09	2942.50	0.0	-2.940e+04	5403.34	0.0	0.0	0.0	-5.809e+05
		-5.809e+05	0.0	0.0	0.0	178.3	-2.717e+04	8345.84	0.0	0.0	0.0	6.670e+05
18	67	7.768e+04	0.0	-0.79	2942.50	0.0	-2.223e+04	-702.11	0.0	0.0	0.0	-8.141e+04
		-9.289e+04	0.0	0.0	0.0	178.3	-2.000e+04	2240.39	0.0	0.0	0.0	7.768e+04
18	68	7.751e+05	0.0	-3.71	2942.50	0.0	-2.112e+04	8388.33	0.0	0.0	0.0	-1.005e+06
		-1.005e+06	0.0	0.0	0.0	178.3	-1.889e+04	1.133e+04	0.0	0.0	0.0	7.751e+05
18	69	2.878e+05	0.0	-1.41	2942.50	0.0	-1.395e+04	2686.22	0.0	0.0	0.0	-4.755e+05
		-4.755e+05	0.0	0.0	0.0	178.3	-1.172e+04	5628.72	0.0	0.0	0.0	2.878e+05
18	70	1.371e+04	0.0	2.41e-03	2942.50	0.0	-1.083e+04	-1055.18	0.0	0.0	0.0	-8.241e+04
		-1.096e+05	0.0	0.0	0.0	178.3	-8604.17	1887.32	0.0	0.0	0.0	1.371e+04
18	71	-6.292e+04	0.0	-0.40	2942.50	0.0	-1.163e+04	-707.87	0.0	0.0	0.0	-2.210e+05
		-2.327e+05	0.0	0.0	0.0	178.3	-9396.69	2234.63	0.0	0.0	0.0	-6.292e+04
18	72	-1.139e+05	0.0	5.83e-03	2942.50	0.0	-1.083e+04	-1559.35	0.0	0.0	0.0	-1.201e+05
		-1.826e+05	0.0	0.0	0.0	178.3	-8604.17	1383.15	0.0	0.0	0.0	-1.139e+05
18	73	6.467e+04	0.0	-0.41	2942.50	0.0	-1.163e+04	-203.70	0.0	0.0	0.0	-1.833e+05
		-1.833e+05	0.0	0.0	0.0	178.3	-9396.69	2738.80	0.0	0.0	0.0	6.467e+04
18	74	8.273e+04	0.0	-0.42	2942.50	0.0	-1.163e+04	0.03	0.0	0.0	0.0	-2.016e+05
		-2.016e+05	0.0	0.0	0.0	178.3	-9396.69	2942.53	0.0	0.0	0.0	8.273e+04
19	1	-5.087e+05	0.0	0.05	-1467.28	0.0	-2.603e+04	-2221.43	0.0	0.0	0.0	-5.087e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-1.058e+06	0.0	0.0	0.0	178.3	-2.302e+04	-3688.71	0.0	0.0	0.0	-1.058e+06
19	2	-4.393e+04	0.0	-0.01	-1467.28	0.0	-1.162e+04	-1624.61	0.0	0.0	0.0	-4.393e+04
		-4.864e+05	0.0	0.0	0.0	178.3	-8606.25	-3091.89	0.0	0.0	0.0	-4.864e+05
19	3	-4.616e+05	0.0	0.04	-1467.28	0.0	-2.240e+04	-2410.91	0.0	0.0	0.0	-4.616e+05
		-1.044e+06	0.0	0.0	0.0	178.3	-1.939e+04	-3878.19	0.0	0.0	0.0	-1.044e+06
19	4	-1.138e+05	0.0	0.01	-1467.28	0.0	-1.162e+04	-1964.40	0.0	0.0	0.0	-1.138e+05
		-6.169e+05	0.0	0.0	0.0	178.3	-8606.25	-3431.68	0.0	0.0	0.0	-6.169e+05
19	5	1.844e+06	0.0	-3.83	-3200.31	0.0	-1.120e+04	6570.53	0.0	0.0	0.0	1.005e+06
		1.005e+06	0.0	0.0	0.0	178.3	-8189.31	3370.22	0.0	0.0	0.0	1.844e+06
19	6	2.435e+06	0.0	-4.00	-4584.87	0.0	594.35	7065.64	0.0	0.0	0.0	1.632e+06
		1.632e+06	0.0	0.0	0.0	178.3	3603.73	2480.77	0.0	0.0	0.0	2.435e+06
19	7	2.936e+06	0.0	-5.08	-7806.29	0.0	2708.73	9023.58	0.0	0.0	0.0	2.054e+06
		2.054e+06	0.0	0.0	0.0	178.3	5718.10	1217.28	0.0	0.0	0.0	2.936e+06
19	8	3.387e+05	0.0	-0.79	-3200.31	0.0	-2.088e+04	-1169.06	0.0	0.0	0.0	3.387e+05
		-2.030e+05	0.0	0.0	0.0	178.3	-1.787e+04	-4369.37	0.0	0.0	0.0	-2.030e+05
19	9	9.653e+05	0.0	-0.96	-4584.87	0.0	-9084.43	-673.95	0.0	0.0	0.0	9.653e+05
		3.885e+05	0.0	0.0	0.0	178.3	-6075.05	-5258.82	0.0	0.0	0.0	3.885e+05
19	10	1.404e+06	0.0	-2.03	-7806.29	0.0	-6970.05	1283.99	0.0	0.0	0.0	1.388e+06
		8.890e+05	0.0	0.0	0.0	178.3	-3960.68	-6522.30	0.0	0.0	0.0	8.890e+05
19	11	-5.081e+05	0.0	0.05	-1467.28	0.0	-2.603e+04	-2214.09	0.0	0.0	0.0	-5.081e+05
		-1.056e+06	0.0	0.0	0.0	178.3	-2.302e+04	-3681.37	0.0	0.0	0.0	-1.056e+06
19	12	-4.328e+04	0.0	-0.01	-1467.28	0.0	-1.162e+04	-1617.28	0.0	0.0	0.0	-4.328e+04
		-4.845e+05	0.0	0.0	0.0	178.3	-8606.25	-3084.55	0.0	0.0	0.0	-4.845e+05
19	13	-1.373e+05	0.0	-0.03	-1467.28	0.0	-2.240e+04	-997.99	0.0	0.0	0.0	-1.373e+05
		-4.681e+05	0.0	0.0	0.0	178.3	-1.939e+04	-2465.27	0.0	0.0	0.0	-4.681e+05
19	14	2.104e+05	0.0	-1.76e-03	-1467.28	0.0	-1.162e+04	-551.48	0.0	0.0	0.0	2.104e+05
		-4.073e+04	0.0	0.0	0.0	178.3	-8606.25	-2018.76	0.0	0.0	0.0	-4.073e+04
19	15	1.529e+06	0.0	-3.84	-3200.31	0.0	-1.120e+04	5837.19	0.0	0.0	0.0	8.208e+05
		8.208e+05	0.0	0.0	0.0	178.3	-8189.31	2636.88	0.0	0.0	0.0	1.529e+06
19	16	2.120e+06	0.0	-4.01	-4584.87	0.0	594.35	6332.30	0.0	0.0	0.0	1.447e+06
		1.447e+06	0.0	0.0	0.0	178.3	3603.73	1747.43	0.0	0.0	0.0	2.120e+06
19	17	2.620e+06	0.0	-5.09	-7806.29	0.0	2708.73	8290.24	0.0	0.0	0.0	1.870e+06
		1.870e+06	0.0	0.0	0.0	178.3	5718.10	483.95	0.0	0.0	0.0	2.620e+06
19	18	3.207e+05	0.0	-0.78	-3200.31	0.0	-2.088e+04	-1371.98	0.0	0.0	0.0	3.207e+05
		-2.571e+05	0.0	0.0	0.0	178.3	-1.787e+04	-4572.29	0.0	0.0	0.0	-2.571e+05
19	19	9.473e+05	0.0	-0.95	-4584.87	0.0	-9084.43	-876.87	0.0	0.0	0.0	9.473e+05
		3.343e+05	0.0	0.0	0.0	178.3	-6075.05	-5461.74	0.0	0.0	0.0	3.343e+05
19	20	1.382e+06	0.0	-2.02	-7806.29	0.0	-6970.05	1081.07	0.0	0.0	0.0	1.370e+06
		8.348e+05	0.0	0.0	0.0	178.3	-3960.68	-6725.22	0.0	0.0	0.0	8.348e+05
19	21	1.936e+06	0.0	-4.34	-3200.31	0.0	-7696.37	6734.54	0.0	0.0	0.0	1.068e+06
		1.068e+06	0.0	0.0	0.0	178.3	-4687.00	3534.23	0.0	0.0	0.0	1.936e+06
19	22	3.844e+05	0.0	-1.28	-3200.31	0.0	-1.738e+04	-1200.63	0.0	0.0	0.0	3.844e+05
		-1.629e+05	0.0	0.0	0.0	178.3	-1.437e+04	-4400.94	0.0	0.0	0.0	-1.629e+05
19	23	2.666e+06	0.0	-5.08	-7806.29	0.0	5720.19	8171.55	0.0	0.0	0.0	1.936e+06
		1.936e+06	0.0	0.0	0.0	178.3	7949.35	365.26	0.0	0.0	0.0	2.666e+06
19	24	1.130e+06	0.0	-2.04	-7806.29	0.0	-3958.60	-247.63	0.0	0.0	0.0	1.130e+06
		3.578e+05	0.0	0.0	0.0	178.3	-1729.43	-8053.92	0.0	0.0	0.0	3.578e+05
19	25	1.702e+06	0.0	-3.33	-3200.31	0.0	-1.470e+04	6232.19	0.0	0.0	0.0	9.233e+05
		9.233e+05	0.0	0.0	0.0	178.3	-1.169e+04	3031.87	0.0	0.0	0.0	1.702e+06
19	26	2.239e+06	0.0	-4.00	-4584.87	0.0	594.35	6555.95	0.0	0.0	0.0	1.527e+06
		1.527e+06	0.0	0.0	0.0	178.3	3603.73	1971.08	0.0	0.0	0.0	2.239e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
19	27	2.362e+05	0.0	-1.47	-3200.31	0.0	-1.983e+04	-1437.47	0.0	0.0	0.0	2.362e+05
		-3.533e+05	0.0	0.0	0.0	178.3	-1.682e+04	-4637.78	0.0	0.0	0.0	-3.533e+05
19	28	8.948e+05	0.0	-0.96	-4584.87	0.0	-9084.43	-1021.08	0.0	0.0	0.0	8.948e+05
		2.560e+05	0.0	0.0	0.0	178.3	-6075.05	-5605.95	0.0	0.0	0.0	2.560e+05
19	29	2.620e+06	0.0	-5.09	-7806.29	0.0	2708.73	8290.24	0.0	0.0	0.0	1.870e+06
		1.870e+06	0.0	0.0	0.0	178.3	5718.10	483.95	0.0	0.0	0.0	2.620e+06
19	30	1.395e+06	0.0	-3.04	-3200.31	0.0	-9707.68	4427.41	0.0	0.0	0.0	9.390e+05
		9.390e+05	0.0	0.0	0.0	178.3	-7478.51	1227.10	0.0	0.0	0.0	1.395e+06
19	31	1.699e+06	0.0	-2.54	-4584.87	0.0	1113.31	3353.65	0.0	0.0	0.0	1.517e+06
		1.517e+06	0.0	0.0	0.0	178.3	3342.48	-1231.22	0.0	0.0	0.0	1.659e+06
19	32	1.843e+06	0.0	-2.98	-7806.29	0.0	1074.61	3400.25	0.0	0.0	0.0	1.724e+06
		1.603e+06	0.0	0.0	0.0	178.3	3303.78	-4406.04	0.0	0.0	0.0	1.603e+06
19	33	3.012e+06	0.0	-5.09	-7806.29	0.0	2708.73	9309.62	0.0	0.0	0.0	2.080e+06
		2.080e+06	0.0	0.0	0.0	178.3	5718.10	1503.33	0.0	0.0	0.0	3.012e+06
19	34	-2.737e+05	0.0	0.03	-1467.28	0.0	-1.661e+04	-2239.26	0.0	0.0	0.0	-2.737e+05
		-8.258e+05	0.0	0.0	0.0	178.3	-1.438e+04	-3706.54	0.0	0.0	0.0	-8.258e+05
19	35	1.916e+05	0.0	-0.15	-2495.41	0.0	-7853.61	-1871.60	0.0	0.0	0.0	1.916e+05
		-3.866e+05	0.0	0.0	0.0	178.3	-5624.45	-4367.02	0.0	0.0	0.0	-3.866e+05
19	36	1.237e+05	0.0	-0.42	-2370.60	0.0	-1.582e+04	-1579.79	0.0	0.0	0.0	1.237e+05
		-4.049e+05	0.0	0.0	0.0	178.3	-1.359e+04	-3950.39	0.0	0.0	0.0	-4.049e+05
19	37	5.890e+05	0.0	-0.55	-3398.74	0.0	-7061.09	-1212.13	0.0	0.0	0.0	5.890e+05
		3.435e+04	0.0	0.0	0.0	178.3	-4831.93	-4610.87	0.0	0.0	0.0	3.435e+04
19	38	9.027e+05	0.0	-1.35	-5790.88	0.0	-5491.01	241.78	0.0	0.0	0.0	9.027e+05
		4.060e+05	0.0	0.0	0.0	178.3	-3261.85	-5549.10	0.0	0.0	0.0	4.060e+05
19	39	-1.461e+05	0.0	0.02	-1467.28	0.0	-1.661e+04	-1735.09	0.0	0.0	0.0	-1.461e+05
		-6.083e+05	0.0	0.0	0.0	178.3	-1.438e+04	-3202.37	0.0	0.0	0.0	-6.083e+05
19	40	1.121e+05	0.0	-2.32e-03	-1467.28	0.0	-8604.17	-1403.52	0.0	0.0	0.0	1.121e+05
		-2.910e+05	0.0	0.0	0.0	178.3	-6375.00	-2870.80	0.0	0.0	0.0	-2.910e+05
19	41	-3924.97	0.0	-0.43	-2370.60	0.0	-1.582e+04	-2083.96	0.0	0.0	0.0	-3924.97
		-6.224e+05	0.0	0.0	0.0	178.3	-1.359e+04	-4454.56	0.0	0.0	0.0	-6.224e+05
19	42	4.614e+05	0.0	-0.56	-3398.74	0.0	-7061.09	-1716.30	0.0	0.0	0.0	4.614e+05
		-1.832e+05	0.0	0.0	0.0	178.3	-4831.93	-5115.04	0.0	0.0	0.0	-1.832e+05
19	43	7.751e+05	0.0	-1.36	-5790.88	0.0	-5491.01	-262.39	0.0	0.0	0.0	7.751e+05
		1.885e+05	0.0	0.0	0.0	178.3	-3261.85	-6053.27	0.0	0.0	0.0	1.885e+05
19	44	5.642e+05	0.0	-1.75	-5790.88	0.0	-1.090e+04	-466.71	0.0	0.0	0.0	5.642e+05
		-5.886e+04	0.0	0.0	0.0	178.3	-8667.77	-6257.60	0.0	0.0	0.0	-5.886e+04
19	45	7.535e+05	0.0	-1.35	-5790.88	0.0	-5491.01	-506.87	0.0	0.0	0.0	7.535e+05
		1.232e+05	0.0	0.0	0.0	178.3	-3261.85	-6297.75	0.0	0.0	0.0	1.232e+05
19	46	-3.088e+05	0.0	0.03	-1467.28	0.0	-1.928e+04	-2148.11	0.0	0.0	0.0	-3.088e+05
		-8.446e+05	0.0	0.0	0.0	178.3	-1.705e+04	-3615.39	0.0	0.0	0.0	-8.446e+05
19	47	3.552e+04	0.0	-2.57e-03	-1467.28	0.0	-8604.17	-1706.03	0.0	0.0	0.0	3.552e+04
		-4.215e+05	0.0	0.0	0.0	178.3	-6375.00	-3173.30	0.0	0.0	0.0	-4.215e+05
19	48	-2.809e+05	0.0	0.02	-1467.28	0.0	-1.661e+04	-2320.75	0.0	0.0	0.0	-2.809e+05
		-8.476e+05	0.0	0.0	0.0	178.3	-1.438e+04	-3788.03	0.0	0.0	0.0	-8.476e+05
19	49	-2.274e+04	0.0	4.30e-03	-1467.28	0.0	-8604.17	-1989.19	0.0	0.0	0.0	-2.274e+04
		-5.302e+05	0.0	0.0	0.0	178.3	-6375.00	-3456.47	0.0	0.0	0.0	-5.302e+05
19	50	1.275e+06	0.0	-2.67	-2370.60	0.0	-8648.83	4469.07	0.0	0.0	0.0	7.246e+05
		7.246e+05	0.0	0.0	0.0	178.3	-6419.67	2098.47	0.0	0.0	0.0	1.275e+06
19	51	1.714e+06	0.0	-2.79	-3398.74	0.0	108.38	4836.73	0.0	0.0	0.0	1.190e+06
		1.190e+06	0.0	0.0	0.0	178.3	2337.54	1437.99	0.0	0.0	0.0	1.714e+06
19	52	2.086e+06	0.0	-3.59	-5790.88	0.0	1678.45	6290.64	0.0	0.0	0.0	1.504e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		1.504e+06	0.0	0.0	0.0	178.3	3907.62	499.76	0.0	0.0	0.0	2.086e+06
19	53	2.374e+05	0.0	-0.41	-2370.60	0.0	-1.582e+04	-1232.49	0.0	0.0	0.0	2.374e+05
		-2.292e+05	0.0	0.0	0.0	178.3	-1.359e+04	-3603.10	0.0	0.0	0.0	-2.292e+05
19	54	7.027e+05	0.0	-0.53	-3398.74	0.0	-7061.09	-864.84	0.0	0.0	0.0	7.027e+05
		2.100e+05	0.0	0.0	0.0	178.3	-4831.93	-4263.58	0.0	0.0	0.0	2.100e+05
19	55	1.020e+06	0.0	-1.33	-5790.88	0.0	-5491.01	589.08	0.0	0.0	0.0	1.016e+06
		5.816e+05	0.0	0.0	0.0	178.3	-3261.85	-5201.81	0.0	0.0	0.0	5.816e+05
19	56	-2.871e+05	0.0	-0.04	-1467.28	0.0	-1.928e+04	-1903.63	0.0	0.0	0.0	-2.871e+05
		-7.793e+05	0.0	0.0	0.0	178.3	-1.705e+04	-3370.91	0.0	0.0	0.0	-7.793e+05
19	57	5.719e+04	0.0	-0.01	-1467.28	0.0	-8604.17	-1461.55	0.0	0.0	0.0	5.719e+04
		-3.562e+05	0.0	0.0	0.0	178.3	-6375.00	-2928.82	0.0	0.0	0.0	-3.562e+05
19	58	-2.448e+05	0.0	-0.04	-1467.28	0.0	-1.661e+04	-1913.29	0.0	0.0	0.0	-2.448e+05
		-7.388e+05	0.0	0.0	0.0	178.3	-1.438e+04	-3380.56	0.0	0.0	0.0	-7.388e+05
19	59	1.337e+04	0.0	-0.02	-1467.28	0.0	-8604.17	-1581.72	0.0	0.0	0.0	1.337e+04
		-4.215e+05	0.0	0.0	0.0	178.3	-6375.00	-3049.00	0.0	0.0	0.0	-4.215e+05
19	60	1.273e+06	0.0	-2.67	-2370.60	0.0	-8648.83	4462.96	0.0	0.0	0.0	7.240e+05
		7.240e+05	0.0	0.0	0.0	178.3	-6419.67	2092.36	0.0	0.0	0.0	1.273e+06
19	61	1.712e+06	0.0	-2.79	-3398.74	0.0	108.38	4830.62	0.0	0.0	0.0	1.189e+06
		1.189e+06	0.0	0.0	0.0	178.3	2337.54	1431.88	0.0	0.0	0.0	1.712e+06
19	62	2.084e+06	0.0	-3.59	-5790.88	0.0	1678.45	6284.53	0.0	0.0	0.0	1.503e+06
		1.503e+06	0.0	0.0	0.0	178.3	3907.62	493.65	0.0	0.0	0.0	2.084e+06
19	63	2.224e+05	0.0	-0.40	-2370.60	0.0	-1.582e+04	-1401.59	0.0	0.0	0.0	2.224e+05
		-2.744e+05	0.0	0.0	0.0	178.3	-1.359e+04	-3772.19	0.0	0.0	0.0	-2.744e+05
19	64	6.877e+05	0.0	-0.53	-3398.74	0.0	-7061.09	-1033.94	0.0	0.0	0.0	6.877e+05
		1.648e+05	0.0	0.0	0.0	178.3	-4831.93	-4432.67	0.0	0.0	0.0	1.648e+05
19	65	1.002e+06	0.0	-1.33	-5790.88	0.0	-5491.01	419.98	0.0	0.0	0.0	1.001e+06
		5.365e+05	0.0	0.0	0.0	178.3	-3261.85	-5370.91	0.0	0.0	0.0	5.365e+05
19	66	1.343e+06	0.0	-3.04	-2370.60	0.0	-6048.10	4590.20	0.0	0.0	0.0	7.713e+05
		7.713e+05	0.0	0.0	0.0	178.3	-3818.94	2219.60	0.0	0.0	0.0	1.343e+06
19	67	2.697e+05	0.0	-0.78	-2370.60	0.0	-1.322e+04	-1274.36	0.0	0.0	0.0	2.697e+05
		-2.044e+05	0.0	0.0	0.0	178.3	-1.099e+04	-3644.96	0.0	0.0	0.0	-2.044e+05
19	68	1.823e+06	0.0	-3.60	-5790.88	0.0	1678.45	5679.53	0.0	0.0	0.0	1.350e+06
		1.350e+06	0.0	0.0	0.0	178.3	3907.62	-111.35	0.0	0.0	0.0	1.823e+06
19	69	7.463e+05	0.0	-1.34	-5790.88	0.0	-5491.01	-588.36	0.0	0.0	0.0	7.463e+05
		1.015e+05	0.0	0.0	0.0	178.3	-3261.85	-6379.24	0.0	0.0	0.0	1.015e+05
19	70	-1.371e+04	0.0	-6.55e-03	-1467.28	0.0	-8604.17	-1887.32	0.0	0.0	0.0	-1.371e+04
		-5.030e+05	0.0	0.0	0.0	178.3	-6375.00	-3354.60	0.0	0.0	0.0	-5.030e+05
19	71	3.801e+05	0.0	-0.40	-2370.60	0.0	-7811.65	-1268.60	0.0	0.0	0.0	3.801e+05
		-9.296e+04	0.0	0.0	0.0	178.3	-5582.48	-3639.20	0.0	0.0	0.0	-9.296e+04
19	72	1.139e+05	0.0	-1.60e-03	-1467.28	0.0	-8604.17	-1383.15	0.0	0.0	0.0	1.139e+05
		-2.855e+05	0.0	0.0	0.0	178.3	-6375.00	-2850.43	0.0	0.0	0.0	-2.855e+05
19	73	2.525e+05	0.0	-0.41	-2370.60	0.0	-7811.65	-1772.76	0.0	0.0	0.0	2.525e+05
		-3.105e+05	0.0	0.0	0.0	178.3	-5582.48	-4143.37	0.0	0.0	0.0	-3.105e+05
19	74	2.344e+05	0.0	-0.40	-2370.60	0.0	-7811.65	-1976.50	0.0	0.0	0.0	2.344e+05
		-3.649e+05	0.0	0.0	0.0	178.3	-5582.48	-4347.10	0.0	0.0	0.0	-3.649e+05
20	1	1.058e+06	0.0	-0.05	1467.28	0.0	-2.603e+04	2221.43	0.0	0.0	0.0	5.087e+05
		5.087e+05	0.0	0.0	0.0	178.3	-2.302e+04	3688.71	0.0	0.0	0.0	1.058e+06
20	2	4.864e+05	0.0	0.01	1467.28	0.0	-1.162e+04	1624.61	0.0	0.0	0.0	4.393e+04
		4.393e+04	0.0	0.0	0.0	178.3	-8606.25	3091.89	0.0	0.0	0.0	4.864e+05
20	3	1.044e+06	0.0	-0.04	1467.28	0.0	-2.240e+04	2410.91	0.0	0.0	0.0	4.616e+05
		4.616e+05	0.0	0.0	0.0	178.3	-1.939e+04	3878.19	0.0	0.0	0.0	1.044e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
20	4	6.169e+05	0.0	-0.01	1467.28	0.0	-1.162e+04	1964.40	0.0	0.0	0.0	1.138e+05
		1.138e+05	0.0	0.0	0.0	178.3	-8606.25	3431.68	0.0	0.0	0.0	6.169e+05
20	5	3.269e+06	0.0	-3.81	1467.28	0.0	-3.360e+04	1.144e+04	0.0	0.0	0.0	1.076e+06
		1.076e+06	0.0	0.0	0.0	178.3	-3.059e+04	1.291e+04	0.0	0.0	0.0	3.269e+06
20	6	3.180e+06	0.0	-4.06	1467.28	0.0	-2.383e+04	1.256e+04	0.0	0.0	0.0	7.864e+05
		7.864e+05	0.0	0.0	0.0	178.3	-2.082e+04	1.403e+04	0.0	0.0	0.0	3.180e+06
20	7	3.727e+06	0.0	-5.14	1467.28	0.0	-2.594e+04	1.448e+04	0.0	0.0	0.0	9.925e+05
		9.925e+05	0.0	0.0	0.0	178.3	-2.293e+04	1.594e+04	0.0	0.0	0.0	3.727e+06
20	8	9.615e+05	0.0	-0.76	1467.28	0.0	-2.392e+04	3022.41	0.0	0.0	0.0	2.698e+05
		2.698e+05	0.0	0.0	0.0	178.3	-2.091e+04	4489.69	0.0	0.0	0.0	9.615e+05
20	9	8.719e+05	0.0	-1.01	1467.28	0.0	-1.415e+04	4144.77	0.0	0.0	0.0	-1.997e+04
		-1.997e+04	0.0	0.0	0.0	178.3	-1.114e+04	5612.05	0.0	0.0	0.0	8.719e+05
20	10	1.419e+06	0.0	-2.10	1467.28	0.0	-1.626e+04	6056.12	0.0	0.0	0.0	1.861e+05
		1.861e+05	0.0	0.0	0.0	178.3	-1.325e+04	7523.40	0.0	0.0	0.0	1.419e+06
20	11	1.056e+06	0.0	-0.05	1467.28	0.0	-2.603e+04	2214.09	0.0	0.0	0.0	5.081e+05
		5.081e+05	0.0	0.0	0.0	178.3	-2.302e+04	3681.37	0.0	0.0	0.0	1.056e+06
20	12	4.845e+05	0.0	0.01	1467.28	0.0	-1.162e+04	1617.28	0.0	0.0	0.0	4.328e+04
		4.328e+04	0.0	0.0	0.0	178.3	-8606.25	3084.55	0.0	0.0	0.0	4.845e+05
20	13	4.681e+05	0.0	0.03	1467.28	0.0	-2.240e+04	997.99	0.0	0.0	0.0	1.373e+05
		1.373e+05	0.0	0.0	0.0	178.3	-1.939e+04	2465.27	0.0	0.0	0.0	4.681e+05
20	14	4.073e+04	0.0	1.76e-03	1467.28	0.0	-1.162e+04	551.48	0.0	0.0	0.0	-2.104e+05
		-2.104e+05	0.0	0.0	0.0	178.3	-8606.25	2018.76	0.0	0.0	0.0	4.073e+04
20	15	3.585e+06	0.0	-3.80	1467.28	0.0	-3.360e+04	1.218e+04	0.0	0.0	0.0	1.261e+06
		1.261e+06	0.0	0.0	0.0	178.3	-3.059e+04	1.364e+04	0.0	0.0	0.0	3.585e+06
20	16	3.495e+06	0.0	-4.04	1467.28	0.0	-2.383e+04	1.330e+04	0.0	0.0	0.0	9.708e+05
		9.708e+05	0.0	0.0	0.0	178.3	-2.082e+04	1.477e+04	0.0	0.0	0.0	3.495e+06
20	17	4.042e+06	0.0	-5.13	1467.28	0.0	-2.594e+04	1.521e+04	0.0	0.0	0.0	1.177e+06
		1.177e+06	0.0	0.0	0.0	178.3	-2.293e+04	1.668e+04	0.0	0.0	0.0	4.042e+06
20	18	1.016e+06	0.0	-0.77	1467.28	0.0	-2.392e+04	3225.33	0.0	0.0	0.0	2.877e+05
		2.877e+05	0.0	0.0	0.0	178.3	-2.091e+04	4692.61	0.0	0.0	0.0	1.016e+06
20	19	9.261e+05	0.0	-1.02	1467.28	0.0	-1.415e+04	4347.69	0.0	0.0	0.0	-1989.45
		-1989.45	0.0	0.0	0.0	178.3	-1.114e+04	5814.97	0.0	0.0	0.0	9.261e+05
20	20	1.473e+06	0.0	-2.10	1467.28	0.0	-1.626e+04	6259.04	0.0	0.0	0.0	2.041e+05
		2.041e+05	0.0	0.0	0.0	178.3	-1.325e+04	7726.32	0.0	0.0	0.0	1.473e+06
20	21	3.218e+06	0.0	-4.32	1467.28	0.0	-3.710e+04	1.128e+04	0.0	0.0	0.0	1.054e+06
		1.054e+06	0.0	0.0	0.0	178.3	-3.409e+04	1.275e+04	0.0	0.0	0.0	3.218e+06
20	22	9.621e+05	0.0	-1.28	1467.28	0.0	-2.742e+04	3053.98	0.0	0.0	0.0	2.647e+05
		2.647e+05	0.0	0.0	0.0	178.3	-2.441e+04	4521.26	0.0	0.0	0.0	9.621e+05
20	23	3.997e+06	0.0	-5.14	1467.28	0.0	-2.293e+04	1.533e+04	0.0	0.0	0.0	1.111e+06
		1.111e+06	0.0	0.0	0.0	178.3	-2.070e+04	1.680e+04	0.0	0.0	0.0	3.997e+06
20	24	1.950e+06	0.0	-2.09	1467.28	0.0	-1.325e+04	7587.73	0.0	0.0	0.0	4.441e+05
		4.441e+05	0.0	0.0	0.0	178.3	-1.102e+04	9055.01	0.0	0.0	0.0	1.950e+06
20	25	3.371e+06	0.0	-3.30	1467.28	0.0	-3.009e+04	1.178e+04	0.0	0.0	0.0	1.117e+06
		1.117e+06	0.0	0.0	0.0	178.3	-2.709e+04	1.325e+04	0.0	0.0	0.0	3.371e+06
20	26	3.376e+06	0.0	-4.06	1467.28	0.0	-2.383e+04	1.307e+04	0.0	0.0	0.0	8.913e+05
		8.913e+05	0.0	0.0	0.0	178.3	-2.082e+04	1.454e+04	0.0	0.0	0.0	3.376e+06
20	27	1.166e+06	0.0	-1.43	1467.28	0.0	-3.223e+04	3290.82	0.0	0.0	0.0	4.266e+05
		4.266e+05	0.0	0.0	0.0	178.3	-2.922e+04	4758.10	0.0	0.0	0.0	1.166e+06
20	28	1.004e+06	0.0	-1.01	1467.28	0.0	-1.415e+04	4491.90	0.0	0.0	0.0	5.059e+04
		5.059e+04	0.0	0.0	0.0	178.3	-1.114e+04	5959.18	0.0	0.0	0.0	1.004e+06
20	29	4.042e+06	0.0	-5.13	1467.28	0.0	-2.594e+04	1.521e+04	0.0	0.0	0.0	1.177e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		1.177e+06	0.0	0.0	0.0	178.3	-2.293e+04	1.668e+04	0.0	0.0	0.0	4.042e+06
20	30	2.959e+06	0.0	-3.05	3200.31	0.0	-2.907e+04	1.173e+04	0.0	0.0	0.0	5.339e+05
		5.339e+05	0.0	0.0	0.0	178.3	-2.684e+04	1.493e+04	0.0	0.0	0.0	2.959e+06
20	31	2.715e+06	0.0	-2.66	4584.87	0.0	-1.832e+04	1.281e+04	0.0	0.0	0.0	-2.508e+04
		-2.508e+04	0.0	0.0	0.0	178.3	-1.609e+04	1.739e+04	0.0	0.0	0.0	2.715e+06
20	32	2.752e+06	0.0	-3.11	7806.29	0.0	-1.828e+04	1.276e+04	0.0	0.0	0.0	-2.512e+05
		-2.512e+05	0.0	0.0	0.0	178.3	-1.605e+04	2.057e+04	0.0	0.0	0.0	2.752e+06
20	33	3.650e+06	0.0	-5.13	1467.28	0.0	-2.594e+04	1.419e+04	0.0	0.0	0.0	9.671e+05
		9.671e+05	0.0	0.0	0.0	178.3	-2.293e+04	1.566e+04	0.0	0.0	0.0	3.650e+06
20	34	8.258e+05	0.0	-0.03	1467.28	0.0	-1.661e+04	2239.26	0.0	0.0	0.0	2.737e+05
		2.737e+05	0.0	0.0	0.0	178.3	-1.438e+04	3706.54	0.0	0.0	0.0	8.258e+05
20	35	7.593e+05	0.0	-0.16	1467.28	0.0	-9354.72	3072.70	0.0	0.0	0.0	5.858e+04
		5.858e+04	0.0	0.0	0.0	178.3	-7125.56	4539.98	0.0	0.0	0.0	7.593e+05
20	36	8.002e+05	0.0	-0.38	1467.28	0.0	-1.740e+04	2545.82	0.0	0.0	0.0	1.935e+05
		1.935e+05	0.0	0.0	0.0	178.3	-1.517e+04	4013.10	0.0	0.0	0.0	8.002e+05
20	37	7.337e+05	0.0	-0.57	1467.28	0.0	-1.015e+04	3379.26	0.0	0.0	0.0	-2.167e+04
		-2.167e+04	0.0	0.0	0.0	178.3	-7918.07	4846.54	0.0	0.0	0.0	7.337e+05
20	38	1.140e+06	0.0	-1.37	1467.28	0.0	-1.172e+04	4798.58	0.0	0.0	0.0	1.313e+05
		1.313e+05	0.0	0.0	0.0	178.3	-9488.15	6265.85	0.0	0.0	0.0	1.140e+06
20	39	6.083e+05	0.0	-0.02	1467.28	0.0	-1.661e+04	1735.09	0.0	0.0	0.0	1.461e+05
		1.461e+05	0.0	0.0	0.0	178.3	-1.438e+04	3202.37	0.0	0.0	0.0	6.083e+05
20	40	2.910e+05	0.0	2.32e-03	1467.28	0.0	-8604.17	1403.52	0.0	0.0	0.0	-1.121e+05
		-1.121e+05	0.0	0.0	0.0	178.3	-6375.00	2870.80	0.0	0.0	0.0	2.910e+05
20	41	1.018e+06	0.0	-0.38	1467.28	0.0	-1.740e+04	3049.99	0.0	0.0	0.0	3.211e+05
		3.211e+05	0.0	0.0	0.0	178.3	-1.517e+04	4517.27	0.0	0.0	0.0	1.018e+06
20	42	9.512e+05	0.0	-0.56	1467.28	0.0	-1.015e+04	3883.43	0.0	0.0	0.0	1.059e+05
		1.059e+05	0.0	0.0	0.0	178.3	-7918.07	5350.71	0.0	0.0	0.0	9.512e+05
20	43	1.357e+06	0.0	-1.37	1467.28	0.0	-1.172e+04	5302.74	0.0	0.0	0.0	2.589e+05
		2.589e+05	0.0	0.0	0.0	178.3	-9488.15	6770.02	0.0	0.0	0.0	1.357e+06
20	44	1.635e+06	0.0	-1.72	1467.28	0.0	-2.232e+04	5507.07	0.0	0.0	0.0	5.001e+05
		5.001e+05	0.0	0.0	0.0	178.3	-2.010e+04	6974.35	0.0	0.0	0.0	1.635e+06
20	45	1.423e+06	0.0	-1.37	1467.28	0.0	-1.172e+04	5547.22	0.0	0.0	0.0	2.806e+05
		2.806e+05	0.0	0.0	0.0	178.3	-9488.15	7014.50	0.0	0.0	0.0	1.423e+06
20	46	8.446e+05	0.0	-0.03	1467.28	0.0	-1.928e+04	2148.11	0.0	0.0	0.0	3.088e+05
		3.088e+05	0.0	0.0	0.0	178.3	-1.705e+04	3615.39	0.0	0.0	0.0	8.446e+05
20	47	4.215e+05	0.0	2.57e-03	1467.28	0.0	-8604.17	1706.03	0.0	0.0	0.0	-3.552e+04
		-3.552e+04	0.0	0.0	0.0	178.3	-6375.00	3173.30	0.0	0.0	0.0	4.215e+05
20	48	8.476e+05	0.0	-0.02	1467.28	0.0	-1.661e+04	2320.75	0.0	0.0	0.0	2.809e+05
		2.809e+05	0.0	0.0	0.0	178.3	-1.438e+04	3788.03	0.0	0.0	0.0	8.476e+05
20	49	5.302e+05	0.0	-4.30e-03	1467.28	0.0	-8604.17	1989.19	0.0	0.0	0.0	2.274e+04
		2.274e+04	0.0	0.0	0.0	178.3	-6375.00	3456.47	0.0	0.0	0.0	5.302e+05
20	50	2.346e+06	0.0	-2.65	1467.28	0.0	-2.457e+04	8466.96	0.0	0.0	0.0	6.836e+05
		6.836e+05	0.0	0.0	0.0	178.3	-2.234e+04	9934.24	0.0	0.0	0.0	2.346e+06
20	51	2.280e+06	0.0	-2.84	1467.28	0.0	-1.732e+04	9300.40	0.0	0.0	0.0	4.684e+05
		4.684e+05	0.0	0.0	0.0	178.3	-1.509e+04	1.077e+04	0.0	0.0	0.0	2.280e+06
20	52	2.686e+06	0.0	-3.64	1467.28	0.0	-1.889e+04	1.072e+04	0.0	0.0	0.0	6.214e+05
		6.214e+05	0.0	0.0	0.0	178.3	-1.666e+04	1.219e+04	0.0	0.0	0.0	2.686e+06
20	53	6.246e+05	0.0	-0.40	1467.28	0.0	-1.740e+04	2198.53	0.0	0.0	0.0	7.979e+04
		7.979e+04	0.0	0.0	0.0	178.3	-1.517e+04	3665.81	0.0	0.0	0.0	6.246e+05
20	54	5.581e+05	0.0	-0.58	1467.28	0.0	-1.015e+04	3031.97	0.0	0.0	0.0	-1.354e+05
		-1.354e+05	0.0	0.0	0.0	178.3	-7918.07	4499.25	0.0	0.0	0.0	5.581e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
20	55	9.642e+05	0.0	-1.39	1467.28	0.0	-1.172e+04	4451.28	0.0	0.0	0.0	1.765e+04
		1.765e+04	0.0	0.0	0.0	178.3	-9488.15	5918.56	0.0	0.0	0.0	9.642e+05
20	56	7.793e+05	0.0	0.04	1467.28	0.0	-1.928e+04	1903.63	0.0	0.0	0.0	2.871e+05
		2.871e+05	0.0	0.0	0.0	178.3	-1.705e+04	3370.91	0.0	0.0	0.0	7.793e+05
20	57	3.562e+05	0.0	0.01	1467.28	0.0	-8604.17	1461.55	0.0	0.0	0.0	-5.719e+04
		-5.719e+04	0.0	0.0	0.0	178.3	-6375.00	2928.82	0.0	0.0	0.0	3.562e+05
20	58	7.388e+05	0.0	0.04	1467.28	0.0	-1.661e+04	1913.29	0.0	0.0	0.0	2.448e+05
		2.448e+05	0.0	0.0	0.0	178.3	-1.438e+04	3380.56	0.0	0.0	0.0	7.388e+05
20	59	4.215e+05	0.0	0.02	1467.28	0.0	-8604.17	1581.72	0.0	0.0	0.0	-1.337e+04
		-1.337e+04	0.0	0.0	0.0	178.3	-6375.00	3049.00	0.0	0.0	0.0	4.215e+05
20	60	2.348e+06	0.0	-2.65	1467.28	0.0	-2.457e+04	8473.07	0.0	0.0	0.0	6.841e+05
		6.841e+05	0.0	0.0	0.0	178.3	-2.234e+04	9940.35	0.0	0.0	0.0	2.348e+06
20	61	2.281e+06	0.0	-2.84	1467.28	0.0	-1.732e+04	9306.51	0.0	0.0	0.0	4.690e+05
		4.690e+05	0.0	0.0	0.0	178.3	-1.509e+04	1.077e+04	0.0	0.0	0.0	2.281e+06
20	62	2.688e+06	0.0	-3.64	1467.28	0.0	-1.889e+04	1.073e+04	0.0	0.0	0.0	6.220e+05
		6.220e+05	0.0	0.0	0.0	178.3	-1.666e+04	1.219e+04	0.0	0.0	0.0	2.688e+06
20	63	6.698e+05	0.0	-0.40	1467.28	0.0	-1.740e+04	2367.63	0.0	0.0	0.0	9.477e+04
		9.477e+04	0.0	0.0	0.0	178.3	-1.517e+04	3834.91	0.0	0.0	0.0	6.698e+05
20	64	6.032e+05	0.0	-0.59	1467.28	0.0	-1.015e+04	3201.07	0.0	0.0	0.0	-1.204e+05
		-1.204e+05	0.0	0.0	0.0	178.3	-7918.07	4668.34	0.0	0.0	0.0	6.032e+05
20	65	1.009e+06	0.0	-1.39	1467.28	0.0	-1.172e+04	4620.38	0.0	0.0	0.0	3.264e+04
		3.264e+04	0.0	0.0	0.0	178.3	-9488.15	6087.66	0.0	0.0	0.0	1.009e+06
20	66	2.308e+06	0.0	-3.03	1467.28	0.0	-2.717e+04	8345.84	0.0	0.0	0.0	6.670e+05
		6.670e+05	0.0	0.0	0.0	178.3	-2.494e+04	9813.11	0.0	0.0	0.0	2.308e+06
20	67	6.300e+05	0.0	-0.78	1467.28	0.0	-2.000e+04	2240.39	0.0	0.0	0.0	7.768e+04
		7.768e+04	0.0	0.0	0.0	178.3	-1.777e+04	3707.67	0.0	0.0	0.0	6.300e+05
20	68	2.949e+06	0.0	-3.63	1467.28	0.0	-1.889e+04	1.133e+04	0.0	0.0	0.0	7.751e+05
		7.751e+05	0.0	0.0	0.0	178.3	-1.666e+04	1.280e+04	0.0	0.0	0.0	2.949e+06
20	69	1.444e+06	0.0	-1.38	1467.28	0.0	-1.172e+04	5628.72	0.0	0.0	0.0	2.878e+05
		2.878e+05	0.0	0.0	0.0	178.3	-9488.15	7096.00	0.0	0.0	0.0	1.444e+06
20	70	5.030e+05	0.0	6.55e-03	1467.28	0.0	-8604.17	1887.32	0.0	0.0	0.0	1.371e+04
		1.371e+04	0.0	0.0	0.0	178.3	-6375.00	3354.60	0.0	0.0	0.0	5.030e+05
20	71	4.883e+05	0.0	-0.41	1467.28	0.0	-9396.69	2234.63	0.0	0.0	0.0	-6.292e+04
		-6.292e+04	0.0	0.0	0.0	178.3	-7167.52	3701.91	0.0	0.0	0.0	4.883e+05
20	72	2.855e+05	0.0	1.60e-03	1467.28	0.0	-8604.17	1383.15	0.0	0.0	0.0	-1.139e+05
		-1.139e+05	0.0	0.0	0.0	178.3	-6375.00	2850.43	0.0	0.0	0.0	2.855e+05
20	73	7.058e+05	0.0	-0.40	1467.28	0.0	-9396.69	2738.80	0.0	0.0	0.0	6.467e+04
		6.467e+04	0.0	0.0	0.0	178.3	-7167.52	4206.08	0.0	0.0	0.0	7.058e+05
20	74	7.602e+05	0.0	-0.41	1467.28	0.0	-9396.69	2942.53	0.0	0.0	0.0	8.273e+04
		8.273e+04	0.0	0.0	0.0	178.3	-7167.52	4409.81	0.0	0.0	0.0	7.602e+05
21	1	-1.058e+06	0.0	-7.73e-03	-56.16	0.0	-2.302e+04	-3688.71	0.0	0.0	0.0	-1.058e+06
		-1.113e+06	0.0	0.0	0.0	15.0	-2.277e+04	-3744.86	0.0	0.0	0.0	-1.113e+06
21	2	-4.864e+05	0.0	-2.31e-03	-56.16	0.0	-8606.25	-3091.89	0.0	0.0	0.0	-4.864e+05
		-5.332e+05	0.0	0.0	0.0	15.0	-8353.13	-3148.04	0.0	0.0	0.0	-5.332e+05
21	3	-1.044e+06	0.0	6.87e-03	-56.16	0.0	-1.939e+04	-3878.19	0.0	0.0	0.0	-1.044e+06
		-1.103e+06	0.0	0.0	0.0	15.0	-1.914e+04	-3934.35	0.0	0.0	0.0	-1.103e+06
21	4	-6.169e+05	0.0	-2.81e-03	-56.16	0.0	-8606.25	-3431.68	0.0	0.0	0.0	-6.169e+05
		-6.688e+05	0.0	0.0	0.0	15.0	-8353.12	-3487.84	0.0	0.0	0.0	-6.688e+05
21	5	1.893e+06	0.0	-0.32	-122.48	0.0	-8189.31	3370.22	0.0	0.0	0.0	1.844e+06
		1.844e+06	0.0	0.0	0.0	15.0	-7936.19	3247.74	0.0	0.0	0.0	1.893e+06
21	6	2.471e+06	0.0	-0.33	-238.94	0.0	3603.73	2480.77	0.0	0.0	0.0	2.435e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		2.435e+06	0.0	0.0	0.0	15.0	3856.85	2241.83	0.0	0.0	0.0	2.471e+06
21	7	2.950e+06	0.0	-0.42	-559.05	0.0	5718.10	1217.28	0.0	0.0	0.0	2.936e+06
		2.936e+06	0.0	0.0	0.0	15.0	5971.23	658.23	0.0	0.0	0.0	2.950e+06
21	8	-2.030e+05	0.0	-0.07	-122.48	0.0	-1.787e+04	-4369.37	0.0	0.0	0.0	-2.030e+05
		-2.695e+05	0.0	0.0	0.0	15.0	-1.761e+04	-4491.85	0.0	0.0	0.0	-2.695e+05
21	9	3.885e+05	0.0	-0.08	-238.94	0.0	-6075.05	-5258.82	0.0	0.0	0.0	3.885e+05
		3.078e+05	0.0	0.0	0.0	15.0	-5821.93	-5497.76	0.0	0.0	0.0	3.078e+05
21	10	8.890e+05	0.0	-0.17	-559.05	0.0	-3960.68	-6522.30	0.0	0.0	0.0	8.890e+05
		7.869e+05	0.0	0.0	0.0	15.0	-3707.55	-7081.36	0.0	0.0	0.0	7.869e+05
21	11	-1.056e+06	0.0	-7.75e-03	-56.16	0.0	-2.302e+04	-3681.37	0.0	0.0	0.0	-1.056e+06
		-1.111e+06	0.0	0.0	0.0	15.0	-2.277e+04	-3737.53	0.0	0.0	0.0	-1.111e+06
21	12	-4.845e+05	0.0	-2.33e-03	-56.16	0.0	-8606.25	-3084.55	0.0	0.0	0.0	-4.845e+05
		-5.312e+05	0.0	0.0	0.0	15.0	-8353.13	-3140.71	0.0	0.0	0.0	-5.312e+05
21	13	-4.681e+05	0.0	-3.77e-03	-56.16	0.0	-1.939e+04	-2465.27	0.0	0.0	0.0	-4.681e+05
		-5.055e+05	0.0	0.0	0.0	15.0	-1.914e+04	-2521.42	0.0	0.0	0.0	-5.055e+05
21	14	-4.073e+04	0.0	-2.91e-04	-56.16	0.0	-8606.25	-2018.76	0.0	0.0	0.0	-4.073e+04
		-7.145e+04	0.0	0.0	0.0	15.0	-8353.13	-2074.91	0.0	0.0	0.0	-7.145e+04
21	15	1.567e+06	0.0	-0.32	-122.48	0.0	-8189.31	2636.88	0.0	0.0	0.0	1.529e+06
		1.529e+06	0.0	0.0	0.0	15.0	-7936.19	2514.40	0.0	0.0	0.0	1.567e+06
21	16	2.144e+06	0.0	-0.33	-238.94	0.0	3603.73	1747.43	0.0	0.0	0.0	2.120e+06
		2.120e+06	0.0	0.0	0.0	15.0	3856.85	1508.50	0.0	0.0	0.0	2.144e+06
21	17	2.624e+06	0.0	-0.42	-559.05	0.0	5718.10	483.95	0.0	0.0	0.0	2.620e+06
		2.620e+06	0.0	0.0	0.0	15.0	5971.23	-75.10	0.0	0.0	0.0	2.624e+06
21	18	-2.571e+05	0.0	-0.07	-122.48	0.0	-1.787e+04	-4572.29	0.0	0.0	0.0	-2.571e+05
		-3.267e+05	0.0	0.0	0.0	15.0	-1.761e+04	-4694.77	0.0	0.0	0.0	-3.267e+05
21	19	3.343e+05	0.0	-0.08	-238.94	0.0	-6075.05	-5461.74	0.0	0.0	0.0	3.343e+05
		2.506e+05	0.0	0.0	0.0	15.0	-5821.93	-5700.67	0.0	0.0	0.0	2.506e+05
21	20	8.348e+05	0.0	-0.17	-559.05	0.0	-3960.68	-6725.22	0.0	0.0	0.0	8.348e+05
		7.297e+05	0.0	0.0	0.0	15.0	-3707.55	-7284.28	0.0	0.0	0.0	7.297e+05
21	21	1.988e+06	0.0	-0.36	-122.48	0.0	-4687.00	3534.23	0.0	0.0	0.0	1.936e+06
		1.936e+06	0.0	0.0	0.0	15.0	-4433.87	3411.75	0.0	0.0	0.0	1.988e+06
21	22	-1.629e+05	0.0	-0.11	-122.48	0.0	-1.437e+04	-4400.94	0.0	0.0	0.0	-1.629e+05
		-2.298e+05	0.0	0.0	0.0	15.0	-1.411e+04	-4523.42	0.0	0.0	0.0	-2.298e+05
21	23	2.667e+06	0.0	-0.42	-559.05	0.0	7949.35	365.26	0.0	0.0	0.0	2.666e+06
		2.666e+06	0.0	0.0	0.0	15.0	8136.85	-193.79	0.0	0.0	0.0	2.667e+06
21	24	3.578e+05	0.0	-0.17	-559.05	0.0	-1729.43	-8053.92	0.0	0.0	0.0	3.578e+05
		2.328e+05	0.0	0.0	0.0	15.0	-1541.93	-8612.97	0.0	0.0	0.0	2.328e+05
21	25	1.746e+06	0.0	-0.27	-122.48	0.0	-1.169e+04	3031.87	0.0	0.0	0.0	1.702e+06
		1.702e+06	0.0	0.0	0.0	15.0	-1.144e+04	2909.40	0.0	0.0	0.0	1.746e+06
21	26	2.267e+06	0.0	-0.33	-238.94	0.0	3603.73	1971.08	0.0	0.0	0.0	2.239e+06
		2.239e+06	0.0	0.0	0.0	15.0	3856.85	1732.14	0.0	0.0	0.0	2.267e+06
21	27	-3.533e+05	0.0	-0.12	-122.48	0.0	-1.682e+04	-4637.78	0.0	0.0	0.0	-3.533e+05
		-4.238e+05	0.0	0.0	0.0	15.0	-1.656e+04	-4760.26	0.0	0.0	0.0	-4.238e+05
21	28	2.560e+05	0.0	-0.08	-238.94	0.0	-6075.05	-5605.95	0.0	0.0	0.0	2.560e+05
		1.701e+05	0.0	0.0	0.0	15.0	-5821.93	-5844.88	0.0	0.0	0.0	1.701e+05
21	29	2.624e+06	0.0	-0.42	-559.05	0.0	5718.10	483.95	0.0	0.0	0.0	2.620e+06
		2.620e+06	0.0	0.0	0.0	15.0	5971.23	-75.10	0.0	0.0	0.0	2.624e+06
21	30	1.413e+06	0.0	-0.25	-122.48	0.0	-7478.51	1227.10	0.0	0.0	0.0	1.395e+06
		1.395e+06	0.0	0.0	0.0	15.0	-7291.01	1104.62	0.0	0.0	0.0	1.413e+06
21	31	1.659e+06	0.0	-0.21	-238.94	0.0	3342.48	-1231.22	0.0	0.0	0.0	1.659e+06
		1.638e+06	0.0	0.0	0.0	15.0	3529.98	-1470.15	0.0	0.0	0.0	1.638e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
21	32	1.603e+06	0.0	-0.24	-559.05	0.0	3303.78	-4406.04	0.0	0.0	0.0	1.603e+06
		1.532e+06	0.0	0.0	0.0	15.0	3491.28	-4965.10	0.0	0.0	0.0	1.532e+06
21	33	3.030e+06	0.0	-0.42	-559.05	0.0	5718.10	1503.33	0.0	0.0	0.0	3.012e+06
		3.012e+06	0.0	0.0	0.0	15.0	5971.23	944.27	0.0	0.0	0.0	3.030e+06
21	34	-8.258e+05	0.0	-4.90e-03	-56.16	0.0	-1.438e+04	-3706.54	0.0	0.0	0.0	-8.258e+05
		-8.818e+05	0.0	0.0	0.0	15.0	-1.419e+04	-3762.69	0.0	0.0	0.0	-8.818e+05
21	35	-3.866e+05	0.0	-0.01	-142.63	0.0	-5624.45	-4367.02	0.0	0.0	0.0	-3.866e+05
		-4.532e+05	0.0	0.0	0.0	15.0	-5436.95	-4509.65	0.0	0.0	0.0	-4.532e+05
21	36	-4.049e+05	0.0	-0.04	-90.72	0.0	-1.359e+04	-3950.39	0.0	0.0	0.0	-4.049e+05
		-4.648e+05	0.0	0.0	0.0	15.0	-1.340e+04	-4041.11	0.0	0.0	0.0	-4.648e+05
21	37	3.435e+04	0.0	-0.05	-177.20	0.0	-4831.93	-4610.87	0.0	0.0	0.0	3.435e+04
		-3.617e+04	0.0	0.0	0.0	15.0	-4644.43	-4788.07	0.0	0.0	0.0	-3.617e+04
21	38	4.060e+05	0.0	-0.11	-414.91	0.0	-3261.85	-5549.10	0.0	0.0	0.0	4.060e+05
		3.196e+05	0.0	0.0	0.0	15.0	-3074.35	-5964.01	0.0	0.0	0.0	3.196e+05
21	39	-6.083e+05	0.0	-3.43e-03	-56.16	0.0	-1.438e+04	-3202.37	0.0	0.0	0.0	-6.083e+05
		-6.568e+05	0.0	0.0	0.0	15.0	-1.419e+04	-3258.52	0.0	0.0	0.0	-6.568e+05
21	40	-2.910e+05	0.0	-4.19e-04	-56.16	0.0	-6375.00	-2870.80	0.0	0.0	0.0	-2.910e+05
		-3.345e+05	0.0	0.0	0.0	15.0	-6187.50	-2926.96	0.0	0.0	0.0	-3.345e+05
21	41	-6.224e+05	0.0	-0.04	-90.72	0.0	-1.359e+04	-4454.56	0.0	0.0	0.0	-6.224e+05
		-6.899e+05	0.0	0.0	0.0	15.0	-1.340e+04	-4545.28	0.0	0.0	0.0	-6.899e+05
21	42	-1.832e+05	0.0	-0.05	-177.20	0.0	-4831.93	-5115.04	0.0	0.0	0.0	-1.832e+05
		-2.612e+05	0.0	0.0	0.0	15.0	-4644.43	-5292.24	0.0	0.0	0.0	-2.612e+05
21	43	1.885e+05	0.0	-0.11	-414.91	0.0	-3261.85	-6053.27	0.0	0.0	0.0	1.885e+05
		9.455e+04	0.0	0.0	0.0	15.0	-3074.35	-6468.18	0.0	0.0	0.0	9.455e+04
21	44	-5.886e+04	0.0	-0.15	-414.91	0.0	-8667.77	-6257.60	0.0	0.0	0.0	-5.886e+04
		-1.558e+05	0.0	0.0	0.0	15.0	-8480.27	-6672.51	0.0	0.0	0.0	-1.558e+05
21	45	1.232e+05	0.0	-0.11	-414.91	0.0	-3261.85	-6297.75	0.0	0.0	0.0	1.232e+05
		2.562e+04	0.0	0.0	0.0	15.0	-3074.35	-6712.66	0.0	0.0	0.0	2.562e+04
21	46	-8.446e+05	0.0	-5.32e-03	-56.16	0.0	-1.705e+04	-3615.39	0.0	0.0	0.0	-8.446e+05
		-8.993e+05	0.0	0.0	0.0	15.0	-1.686e+04	-3671.55	0.0	0.0	0.0	-8.993e+05
21	47	-4.215e+05	0.0	-1.30e-03	-56.16	0.0	-6375.00	-3173.30	0.0	0.0	0.0	-4.215e+05
		-4.695e+05	0.0	0.0	0.0	15.0	-6187.50	-3229.46	0.0	0.0	0.0	-4.695e+05
21	48	-8.476e+05	0.0	4.73e-03	-56.16	0.0	-1.438e+04	-3788.03	0.0	0.0	0.0	-8.476e+05
		-9.048e+05	0.0	0.0	0.0	15.0	-1.419e+04	-3844.19	0.0	0.0	0.0	-9.048e+05
21	49	-5.302e+05	0.0	-1.72e-03	-56.16	0.0	-6375.00	-3456.47	0.0	0.0	0.0	-5.302e+05
		-5.825e+05	0.0	0.0	0.0	15.0	-6187.50	-3512.62	0.0	0.0	0.0	-5.825e+05
21	50	1.306e+06	0.0	-0.22	-90.72	0.0	-6419.67	2098.47	0.0	0.0	0.0	1.275e+06
		1.275e+06	0.0	0.0	0.0	15.0	-6232.17	2007.75	0.0	0.0	0.0	1.306e+06
21	51	1.734e+06	0.0	-0.23	-177.20	0.0	2337.54	1437.99	0.0	0.0	0.0	1.714e+06
		1.714e+06	0.0	0.0	0.0	15.0	2525.04	1260.79	0.0	0.0	0.0	1.734e+06
21	52	2.090e+06	0.0	-0.29	-414.91	0.0	3907.62	499.76	0.0	0.0	0.0	2.086e+06
		2.086e+06	0.0	0.0	0.0	15.0	4095.12	84.85	0.0	0.0	0.0	2.090e+06
21	53	-2.292e+05	0.0	-0.03	-90.72	0.0	-1.359e+04	-3603.10	0.0	0.0	0.0	-2.292e+05
		-2.840e+05	0.0	0.0	0.0	15.0	-1.340e+04	-3693.82	0.0	0.0	0.0	-2.840e+05
21	54	2.100e+05	0.0	-0.04	-177.20	0.0	-4831.93	-4263.58	0.0	0.0	0.0	2.100e+05
		1.447e+05	0.0	0.0	0.0	15.0	-4644.43	-4440.78	0.0	0.0	0.0	1.447e+05
21	55	5.816e+05	0.0	-0.11	-414.91	0.0	-3261.85	-5201.81	0.0	0.0	0.0	5.816e+05
		5.005e+05	0.0	0.0	0.0	15.0	-3074.35	-5616.72	0.0	0.0	0.0	5.005e+05
21	56	-7.793e+05	0.0	-5.83e-03	-56.16	0.0	-1.705e+04	-3370.91	0.0	0.0	0.0	-7.793e+05
		-8.303e+05	0.0	0.0	0.0	15.0	-1.686e+04	-3427.07	0.0	0.0	0.0	-8.303e+05
21	57	-3.562e+05	0.0	-1.82e-03	-56.16	0.0	-6375.00	-2928.82	0.0	0.0	0.0	-3.562e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-4.006e+05	0.0	0.0	0.0	15.0	-6187.50	-2984.98	0.0	0.0	0.0	-4.006e+05
21	58	-7.388e+05	0.0	-5.59e-03	-56.16	0.0	-1.438e+04	-3380.56	0.0	0.0	0.0	-7.388e+05
		-7.899e+05	0.0	0.0	0.0	15.0	-1.419e+04	-3436.72	0.0	0.0	0.0	-7.899e+05
21	59	-4.215e+05	0.0	-2.58e-03	-56.16	0.0	-6375.00	-3049.00	0.0	0.0	0.0	-4.215e+05
		-4.676e+05	0.0	0.0	0.0	15.0	-6187.50	-3105.15	0.0	0.0	0.0	-4.676e+05
21	60	1.304e+06	0.0	-0.22	-90.72	0.0	-6419.67	2092.36	0.0	0.0	0.0	1.273e+06
		1.273e+06	0.0	0.0	0.0	15.0	-6232.17	2001.63	0.0	0.0	0.0	1.304e+06
21	61	1.732e+06	0.0	-0.23	-177.20	0.0	2337.54	1431.88	0.0	0.0	0.0	1.712e+06
		1.712e+06	0.0	0.0	0.0	15.0	2525.04	1254.68	0.0	0.0	0.0	1.732e+06
21	62	2.088e+06	0.0	-0.29	-414.91	0.0	3907.62	493.65	0.0	0.0	0.0	2.084e+06
		2.084e+06	0.0	0.0	0.0	15.0	4095.12	78.73	0.0	0.0	0.0	2.088e+06
21	63	-2.744e+05	0.0	-0.03	-90.72	0.0	-1.359e+04	-3772.19	0.0	0.0	0.0	-2.744e+05
		-3.317e+05	0.0	0.0	0.0	15.0	-1.340e+04	-3862.92	0.0	0.0	0.0	-3.317e+05
21	64	1.648e+05	0.0	-0.04	-177.20	0.0	-4831.93	-4432.67	0.0	0.0	0.0	1.648e+05
		9.699e+04	0.0	0.0	0.0	15.0	-4644.43	-4609.88	0.0	0.0	0.0	9.699e+04
21	65	5.365e+05	0.0	-0.11	-414.91	0.0	-3261.85	-5370.91	0.0	0.0	0.0	5.365e+05
		4.528e+05	0.0	0.0	0.0	15.0	-3074.35	-5785.82	0.0	0.0	0.0	4.528e+05
21	66	1.376e+06	0.0	-0.25	-90.72	0.0	-3818.94	2219.60	0.0	0.0	0.0	1.343e+06
		1.343e+06	0.0	0.0	0.0	15.0	-3631.44	2128.87	0.0	0.0	0.0	1.376e+06
21	67	-2.044e+05	0.0	-0.07	-90.72	0.0	-1.099e+04	-3644.96	0.0	0.0	0.0	-2.044e+05
		-2.597e+05	0.0	0.0	0.0	15.0	-1.080e+04	-3735.68	0.0	0.0	0.0	-2.597e+05
21	68	1.823e+06	0.0	-0.30	-414.91	0.0	3907.62	-111.35	0.0	0.0	0.0	1.823e+06
		1.818e+06	0.0	0.0	0.0	15.0	4095.12	-526.27	0.0	0.0	0.0	1.818e+06
21	69	1.015e+05	0.0	-0.11	-414.91	0.0	-3261.85	-6379.24	0.0	0.0	0.0	1.015e+05
		2641.19	0.0	0.0	0.0	15.0	-3074.35	-6794.16	0.0	0.0	0.0	2641.19
21	70	-5.030e+05	0.0	-1.93e-03	-56.16	0.0	-6375.00	-3354.60	0.0	0.0	0.0	-5.030e+05
		-5.538e+05	0.0	0.0	0.0	15.0	-6187.50	-3410.75	0.0	0.0	0.0	-5.538e+05
21	71	-9.296e+04	0.0	-0.03	-90.72	0.0	-5582.48	-3639.20	0.0	0.0	0.0	-9.296e+04
		-1.482e+05	0.0	0.0	0.0	15.0	-5394.98	-3729.92	0.0	0.0	0.0	-1.482e+05
21	72	-2.855e+05	0.0	-4.61e-04	-56.16	0.0	-6375.00	-2850.43	0.0	0.0	0.0	-2.855e+05
		-3.287e+05	0.0	0.0	0.0	15.0	-6187.50	-2906.59	0.0	0.0	0.0	-3.287e+05
21	73	-3.105e+05	0.0	-0.03	-90.72	0.0	-5582.48	-4143.37	0.0	0.0	0.0	-3.105e+05
		-3.733e+05	0.0	0.0	0.0	15.0	-5394.98	-4234.09	0.0	0.0	0.0	-3.733e+05
21	74	-3.649e+05	0.0	-0.03	-90.72	0.0	-5582.48	-4347.10	0.0	0.0	0.0	-3.649e+05
		-4.308e+05	0.0	0.0	0.0	15.0	-5394.98	-4437.82	0.0	0.0	0.0	-4.308e+05
22	1	1.113e+06	0.0	7.73e-03	56.16	0.0	-2.302e+04	3688.71	0.0	0.0	0.0	1.058e+06
		1.058e+06	0.0	0.0	0.0	15.0	-2.277e+04	3744.86	0.0	0.0	0.0	1.113e+06
22	2	5.332e+05	0.0	2.31e-03	56.16	0.0	-8606.25	3091.89	0.0	0.0	0.0	4.864e+05
		4.864e+05	0.0	0.0	0.0	15.0	-8353.12	3148.04	0.0	0.0	0.0	5.332e+05
22	3	1.103e+06	0.0	-6.87e-03	56.16	0.0	-1.939e+04	3878.19	0.0	0.0	0.0	1.044e+06
		1.044e+06	0.0	0.0	0.0	15.0	-1.914e+04	3934.35	0.0	0.0	0.0	1.103e+06
22	4	6.688e+05	0.0	2.81e-03	56.16	0.0	-8606.25	3431.68	0.0	0.0	0.0	6.169e+05
		6.169e+05	0.0	0.0	0.0	15.0	-8353.13	3487.84	0.0	0.0	0.0	6.688e+05
22	5	3.464e+06	0.0	-0.31	56.16	0.0	-3.059e+04	1.291e+04	0.0	0.0	0.0	3.269e+06
		3.269e+06	0.0	0.0	0.0	15.0	-3.033e+04	1.297e+04	0.0	0.0	0.0	3.464e+06
22	6	3.391e+06	0.0	-0.33	56.16	0.0	-2.082e+04	1.403e+04	0.0	0.0	0.0	3.180e+06
		3.180e+06	0.0	0.0	0.0	15.0	-2.056e+04	1.409e+04	0.0	0.0	0.0	3.391e+06
22	7	3.966e+06	0.0	-0.42	56.16	0.0	-2.293e+04	1.594e+04	0.0	0.0	0.0	3.727e+06
		3.727e+06	0.0	0.0	0.0	15.0	-2.268e+04	1.600e+04	0.0	0.0	0.0	3.966e+06
22	8	1.029e+06	0.0	-0.06	56.16	0.0	-2.091e+04	4489.69	0.0	0.0	0.0	9.615e+05
		9.615e+05	0.0	0.0	0.0	15.0	-2.066e+04	4545.85	0.0	0.0	0.0	1.029e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
22	9	9.565e+05	0.0	-0.08	56.16	0.0	-1.114e+04	5612.05	0.0	0.0	0.0	8.719e+05
		8.719e+05	0.0	0.0	0.0	15.0	-1.088e+04	5668.21	0.0	0.0	0.0	9.565e+05
22	10	1.532e+06	0.0	-0.17	56.16	0.0	-1.325e+04	7523.40	0.0	0.0	0.0	1.419e+06
		1.419e+06	0.0	0.0	0.0	15.0	-1.300e+04	7579.55	0.0	0.0	0.0	1.532e+06
22	11	1.111e+06	0.0	7.75e-03	56.16	0.0	-2.302e+04	3681.37	0.0	0.0	0.0	1.056e+06
		1.056e+06	0.0	0.0	0.0	15.0	-2.277e+04	3737.53	0.0	0.0	0.0	1.111e+06
22	12	5.312e+05	0.0	2.33e-03	56.16	0.0	-8606.25	3084.55	0.0	0.0	0.0	4.845e+05
		4.845e+05	0.0	0.0	0.0	15.0	-8353.12	3140.71	0.0	0.0	0.0	5.312e+05
22	13	5.055e+05	0.0	3.77e-03	56.16	0.0	-1.939e+04	2465.27	0.0	0.0	0.0	4.681e+05
		4.681e+05	0.0	0.0	0.0	15.0	-1.914e+04	2521.42	0.0	0.0	0.0	5.055e+05
22	14	7.145e+04	0.0	2.91e-04	56.16	0.0	-8606.25	2018.76	0.0	0.0	0.0	4.073e+04
		4.073e+04	0.0	0.0	0.0	15.0	-8353.12	2074.91	0.0	0.0	0.0	7.145e+04
22	15	3.790e+06	0.0	-0.31	56.16	0.0	-3.059e+04	1.364e+04	0.0	0.0	0.0	3.585e+06
		3.585e+06	0.0	0.0	0.0	15.0	-3.033e+04	1.370e+04	0.0	0.0	0.0	3.790e+06
22	16	3.717e+06	0.0	-0.33	56.16	0.0	-2.082e+04	1.477e+04	0.0	0.0	0.0	3.495e+06
		3.495e+06	0.0	0.0	0.0	15.0	-2.056e+04	1.482e+04	0.0	0.0	0.0	3.717e+06
22	17	4.293e+06	0.0	-0.42	56.16	0.0	-2.293e+04	1.668e+04	0.0	0.0	0.0	4.042e+06
		4.042e+06	0.0	0.0	0.0	15.0	-2.268e+04	1.673e+04	0.0	0.0	0.0	4.293e+06
22	18	1.087e+06	0.0	-0.06	56.16	0.0	-2.091e+04	4692.61	0.0	0.0	0.0	1.016e+06
		1.016e+06	0.0	0.0	0.0	15.0	-2.066e+04	4748.76	0.0	0.0	0.0	1.087e+06
22	19	1.014e+06	0.0	-0.08	56.16	0.0	-1.114e+04	5814.97	0.0	0.0	0.0	9.261e+05
		9.261e+05	0.0	0.0	0.0	15.0	-1.088e+04	5871.13	0.0	0.0	0.0	1.014e+06
22	20	1.589e+06	0.0	-0.17	56.16	0.0	-1.325e+04	7726.32	0.0	0.0	0.0	1.473e+06
		1.473e+06	0.0	0.0	0.0	15.0	-1.300e+04	7782.47	0.0	0.0	0.0	1.589e+06
22	21	3.409e+06	0.0	-0.35	56.16	0.0	-3.409e+04	1.275e+04	0.0	0.0	0.0	3.218e+06
		3.218e+06	0.0	0.0	0.0	15.0	-3.384e+04	1.280e+04	0.0	0.0	0.0	3.409e+06
22	22	1.030e+06	0.0	-0.10	56.16	0.0	-2.441e+04	4521.26	0.0	0.0	0.0	9.621e+05
		9.621e+05	0.0	0.0	0.0	15.0	-2.416e+04	4577.42	0.0	0.0	0.0	1.030e+06
22	23	4.249e+06	0.0	-0.42	56.16	0.0	-2.070e+04	1.680e+04	0.0	0.0	0.0	3.997e+06
		3.997e+06	0.0	0.0	0.0	15.0	-2.051e+04	1.685e+04	0.0	0.0	0.0	4.249e+06
22	24	2.086e+06	0.0	-0.17	56.16	0.0	-1.102e+04	9055.01	0.0	0.0	0.0	1.950e+06
		1.950e+06	0.0	0.0	0.0	15.0	-1.083e+04	9111.17	0.0	0.0	0.0	2.086e+06
22	25	3.570e+06	0.0	-0.27	56.16	0.0	-2.709e+04	1.325e+04	0.0	0.0	0.0	3.371e+06
		3.371e+06	0.0	0.0	0.0	15.0	-2.683e+04	1.330e+04	0.0	0.0	0.0	3.570e+06
22	26	3.594e+06	0.0	-0.33	56.16	0.0	-2.082e+04	1.454e+04	0.0	0.0	0.0	3.376e+06
		3.376e+06	0.0	0.0	0.0	15.0	-2.056e+04	1.460e+04	0.0	0.0	0.0	3.594e+06
22	27	1.238e+06	0.0	-0.12	56.16	0.0	-2.922e+04	4758.10	0.0	0.0	0.0	1.166e+06
		1.166e+06	0.0	0.0	0.0	15.0	-2.897e+04	4814.25	0.0	0.0	0.0	1.238e+06
22	28	1.094e+06	0.0	-0.08	56.16	0.0	-1.114e+04	5959.18	0.0	0.0	0.0	1.004e+06
		1.004e+06	0.0	0.0	0.0	15.0	-1.088e+04	6015.34	0.0	0.0	0.0	1.094e+06
22	29	4.293e+06	0.0	-0.42	56.16	0.0	-2.293e+04	1.668e+04	0.0	0.0	0.0	4.042e+06
		4.042e+06	0.0	0.0	0.0	15.0	-2.268e+04	1.673e+04	0.0	0.0	0.0	4.293e+06
22	30	3.184e+06	0.0	-0.25	122.48	0.0	-2.684e+04	1.493e+04	0.0	0.0	0.0	2.959e+06
		2.959e+06	0.0	0.0	0.0	15.0	-2.665e+04	1.505e+04	0.0	0.0	0.0	3.184e+06
22	31	2.978e+06	0.0	-0.22	238.94	0.0	-1.609e+04	1.739e+04	0.0	0.0	0.0	2.715e+06
		2.715e+06	0.0	0.0	0.0	15.0	-1.590e+04	1.763e+04	0.0	0.0	0.0	2.978e+06
22	32	3.065e+06	0.0	-0.25	559.05	0.0	-1.605e+04	2.057e+04	0.0	0.0	0.0	2.752e+06
		2.752e+06	0.0	0.0	0.0	15.0	-1.587e+04	2.112e+04	0.0	0.0	0.0	3.065e+06
22	33	3.886e+06	0.0	-0.42	56.16	0.0	-2.293e+04	1.566e+04	0.0	0.0	0.0	3.650e+06
		3.650e+06	0.0	0.0	0.0	15.0	-2.268e+04	1.571e+04	0.0	0.0	0.0	3.886e+06
22	34	8.818e+05	0.0	4.90e-03	56.16	0.0	-1.438e+04	3706.54	0.0	0.0	0.0	8.258e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		8.258e+05	0.0	0.0	0.0	15.0	-1.419e+04	3762.69	0.0	0.0	0.0	8.818e+05
22	35	8.278e+05	0.0	-0.01	56.16	0.0	-7125.55	4539.98	0.0	0.0	0.0	7.593e+05
		7.593e+05	0.0	0.0	0.0	15.0	-6938.05	4596.13	0.0	0.0	0.0	8.278e+05
22	36	8.609e+05	0.0	-0.03	56.16	0.0	-1.517e+04	4013.10	0.0	0.0	0.0	8.002e+05
		8.002e+05	0.0	0.0	0.0	15.0	-1.499e+04	4069.26	0.0	0.0	0.0	8.609e+05
22	37	8.069e+05	0.0	-0.05	56.16	0.0	-7918.07	4846.54	0.0	0.0	0.0	7.337e+05
		7.337e+05	0.0	0.0	0.0	15.0	-7730.57	4902.69	0.0	0.0	0.0	8.069e+05
22	38	1.234e+06	0.0	-0.11	56.16	0.0	-9488.15	6265.85	0.0	0.0	0.0	1.140e+06
		1.140e+06	0.0	0.0	0.0	15.0	-9300.65	6322.01	0.0	0.0	0.0	1.234e+06
22	39	6.568e+05	0.0	3.43e-03	56.16	0.0	-1.438e+04	3202.37	0.0	0.0	0.0	6.083e+05
		6.083e+05	0.0	0.0	0.0	15.0	-1.419e+04	3258.52	0.0	0.0	0.0	6.568e+05
22	40	3.345e+05	0.0	4.19e-04	56.16	0.0	-6375.00	2870.80	0.0	0.0	0.0	2.910e+05
		2.910e+05	0.0	0.0	0.0	15.0	-6187.50	2926.96	0.0	0.0	0.0	3.345e+05
22	41	1.086e+06	0.0	-0.03	56.16	0.0	-1.517e+04	4517.27	0.0	0.0	0.0	1.018e+06
		1.018e+06	0.0	0.0	0.0	15.0	-1.499e+04	4573.43	0.0	0.0	0.0	1.086e+06
22	42	1.032e+06	0.0	-0.04	56.16	0.0	-7918.07	5350.71	0.0	0.0	0.0	9.512e+05
		9.512e+05	0.0	0.0	0.0	15.0	-7730.57	5406.86	0.0	0.0	0.0	1.032e+06
22	43	1.459e+06	0.0	-0.11	56.16	0.0	-9488.15	6770.02	0.0	0.0	0.0	1.357e+06
		1.357e+06	0.0	0.0	0.0	15.0	-9300.65	6826.18	0.0	0.0	0.0	1.459e+06
22	44	1.740e+06	0.0	-0.14	56.16	0.0	-2.010e+04	6974.35	0.0	0.0	0.0	1.635e+06
		1.635e+06	0.0	0.0	0.0	15.0	-1.991e+04	7030.51	0.0	0.0	0.0	1.740e+06
22	45	1.528e+06	0.0	-0.11	56.16	0.0	-9488.15	7014.50	0.0	0.0	0.0	1.423e+06
		1.423e+06	0.0	0.0	0.0	15.0	-9300.65	7070.66	0.0	0.0	0.0	1.528e+06
22	46	8.993e+05	0.0	5.32e-03	56.16	0.0	-1.705e+04	3615.39	0.0	0.0	0.0	8.446e+05
		8.446e+05	0.0	0.0	0.0	15.0	-1.686e+04	3671.55	0.0	0.0	0.0	8.993e+05
22	47	4.695e+05	0.0	1.30e-03	56.16	0.0	-6375.00	3173.30	0.0	0.0	0.0	4.215e+05
		4.215e+05	0.0	0.0	0.0	15.0	-6187.50	3229.46	0.0	0.0	0.0	4.695e+05
22	48	9.048e+05	0.0	-4.73e-03	56.16	0.0	-1.438e+04	3788.03	0.0	0.0	0.0	8.476e+05
		8.476e+05	0.0	0.0	0.0	15.0	-1.419e+04	3844.19	0.0	0.0	0.0	9.048e+05
22	49	5.825e+05	0.0	1.72e-03	56.16	0.0	-6375.00	3456.47	0.0	0.0	0.0	5.302e+05
		5.302e+05	0.0	0.0	0.0	15.0	-6187.50	3512.62	0.0	0.0	0.0	5.825e+05
22	50	2.496e+06	0.0	-0.22	56.16	0.0	-2.234e+04	9934.24	0.0	0.0	0.0	2.346e+06
		2.346e+06	0.0	0.0	0.0	15.0	-2.216e+04	9990.40	0.0	0.0	0.0	2.496e+06
22	51	2.442e+06	0.0	-0.23	56.16	0.0	-1.509e+04	1.077e+04	0.0	0.0	0.0	2.280e+06
		2.280e+06	0.0	0.0	0.0	15.0	-1.490e+04	1.082e+04	0.0	0.0	0.0	2.442e+06
22	52	2.869e+06	0.0	-0.30	56.16	0.0	-1.666e+04	1.219e+04	0.0	0.0	0.0	2.686e+06
		2.686e+06	0.0	0.0	0.0	15.0	-1.647e+04	1.224e+04	0.0	0.0	0.0	2.869e+06
22	53	6.800e+05	0.0	-0.03	56.16	0.0	-1.517e+04	3665.81	0.0	0.0	0.0	6.246e+05
		6.246e+05	0.0	0.0	0.0	15.0	-1.499e+04	3721.96	0.0	0.0	0.0	6.800e+05
22	54	6.260e+05	0.0	-0.05	56.16	0.0	-7918.07	4499.25	0.0	0.0	0.0	5.581e+05
		5.581e+05	0.0	0.0	0.0	15.0	-7730.57	4555.40	0.0	0.0	0.0	6.260e+05
22	55	1.053e+06	0.0	-0.11	56.16	0.0	-9488.15	5918.56	0.0	0.0	0.0	9.642e+05
		9.642e+05	0.0	0.0	0.0	15.0	-9300.65	5974.72	0.0	0.0	0.0	1.053e+06
22	56	8.303e+05	0.0	5.83e-03	56.16	0.0	-1.705e+04	3370.91	0.0	0.0	0.0	7.793e+05
		7.793e+05	0.0	0.0	0.0	15.0	-1.686e+04	3427.07	0.0	0.0	0.0	8.303e+05
22	57	4.006e+05	0.0	1.82e-03	56.16	0.0	-6375.00	2928.82	0.0	0.0	0.0	3.562e+05
		3.562e+05	0.0	0.0	0.0	15.0	-6187.50	2984.98	0.0	0.0	0.0	4.006e+05
22	58	7.899e+05	0.0	5.59e-03	56.16	0.0	-1.438e+04	3380.56	0.0	0.0	0.0	7.388e+05
		7.388e+05	0.0	0.0	0.0	15.0	-1.419e+04	3436.72	0.0	0.0	0.0	7.899e+05
22	59	4.676e+05	0.0	2.58e-03	56.16	0.0	-6375.00	3049.00	0.0	0.0	0.0	4.215e+05
		4.215e+05	0.0	0.0	0.0	15.0	-6187.50	3105.15	0.0	0.0	0.0	4.676e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
22	60	2.497e+06	0.0	-0.22	56.16	0.0	-2.234e+04	9940.35	0.0	0.0	0.0	2.348e+06
		2.348e+06	0.0	0.0	0.0	15.0	-2.216e+04	9996.51	0.0	0.0	0.0	2.497e+06
22	61	2.443e+06	0.0	-0.23	56.16	0.0	-1.509e+04	1.077e+04	0.0	0.0	0.0	2.281e+06
		2.281e+06	0.0	0.0	0.0	15.0	-1.490e+04	1.083e+04	0.0	0.0	0.0	2.443e+06
22	62	2.871e+06	0.0	-0.30	56.16	0.0	-1.666e+04	1.219e+04	0.0	0.0	0.0	2.688e+06
		2.688e+06	0.0	0.0	0.0	15.0	-1.647e+04	1.225e+04	0.0	0.0	0.0	2.871e+06
22	63	7.277e+05	0.0	-0.03	56.16	0.0	-1.517e+04	3834.91	0.0	0.0	0.0	6.698e+05
		6.698e+05	0.0	0.0	0.0	15.0	-1.499e+04	3891.06	0.0	0.0	0.0	7.277e+05
22	64	6.737e+05	0.0	-0.05	56.16	0.0	-7918.07	4668.34	0.0	0.0	0.0	6.032e+05
		6.032e+05	0.0	0.0	0.0	15.0	-7730.57	4724.50	0.0	0.0	0.0	6.737e+05
22	65	1.101e+06	0.0	-0.11	56.16	0.0	-9488.15	6087.66	0.0	0.0	0.0	1.009e+06
		1.009e+06	0.0	0.0	0.0	15.0	-9300.65	6143.82	0.0	0.0	0.0	1.101e+06
22	66	2.456e+06	0.0	-0.25	56.16	0.0	-2.494e+04	9813.11	0.0	0.0	0.0	2.308e+06
		2.308e+06	0.0	0.0	0.0	15.0	-2.476e+04	9869.27	0.0	0.0	0.0	2.456e+06
22	67	6.860e+05	0.0	-0.06	56.16	0.0	-1.777e+04	3707.67	0.0	0.0	0.0	6.300e+05
		6.300e+05	0.0	0.0	0.0	15.0	-1.759e+04	3763.82	0.0	0.0	0.0	6.860e+05
22	68	3.141e+06	0.0	-0.30	56.16	0.0	-1.666e+04	1.280e+04	0.0	0.0	0.0	2.949e+06
		2.949e+06	0.0	0.0	0.0	15.0	-1.647e+04	1.285e+04	0.0	0.0	0.0	3.141e+06
22	69	1.551e+06	0.0	-0.11	56.16	0.0	-9488.15	7096.00	0.0	0.0	0.0	1.444e+06
		1.444e+06	0.0	0.0	0.0	15.0	-9300.65	7152.15	0.0	0.0	0.0	1.551e+06
22	70	5.538e+05	0.0	1.93e-03	56.16	0.0	-6375.00	3354.60	0.0	0.0	0.0	5.030e+05
		5.030e+05	0.0	0.0	0.0	15.0	-6187.50	3410.75	0.0	0.0	0.0	5.538e+05
22	71	5.443e+05	0.0	-0.03	56.16	0.0	-7167.52	3701.91	0.0	0.0	0.0	4.883e+05
		4.883e+05	0.0	0.0	0.0	15.0	-6980.02	3758.06	0.0	0.0	0.0	5.443e+05
22	72	3.287e+05	0.0	4.61e-04	56.16	0.0	-6375.00	2850.43	0.0	0.0	0.0	2.855e+05
		2.855e+05	0.0	0.0	0.0	15.0	-6187.50	2906.59	0.0	0.0	0.0	3.287e+05
22	73	7.694e+05	0.0	-0.03	56.16	0.0	-7167.52	4206.08	0.0	0.0	0.0	7.058e+05
		7.058e+05	0.0	0.0	0.0	15.0	-6980.02	4262.23	0.0	0.0	0.0	7.694e+05
22	74	8.268e+05	0.0	-0.03	56.16	0.0	-7167.52	4409.81	0.0	0.0	0.0	7.602e+05
		7.602e+05	0.0	0.0	0.0	15.0	-6980.02	4465.97	0.0	0.0	0.0	8.268e+05
23	1	-1.113e+06	0.0	-8.45e-03	-45.72	0.0	-2.277e+04	-3744.86	0.0	0.0	0.0	-1.113e+06
		-1.170e+06	0.0	0.0	0.0	15.0	-2.251e+04	-3790.58	0.0	0.0	0.0	-1.170e+06
23	2	-5.332e+05	0.0	-2.65e-03	-45.72	0.0	-8353.13	-3148.04	0.0	0.0	0.0	-5.332e+05
		-5.808e+05	0.0	0.0	0.0	15.0	-8100.00	-3193.76	0.0	0.0	0.0	-5.808e+05
23	3	-1.103e+06	0.0	-7.57e-03	-45.72	0.0	-1.914e+04	-3934.35	0.0	0.0	0.0	-1.103e+06
		-1.162e+06	0.0	0.0	0.0	15.0	-1.888e+04	-3980.06	0.0	0.0	0.0	-1.162e+06
23	4	-6.688e+05	0.0	-3.24e-03	-45.72	0.0	-8353.12	-3487.84	0.0	0.0	0.0	-6.688e+05
		-7.215e+05	0.0	0.0	0.0	15.0	-8100.00	-3533.56	0.0	0.0	0.0	-7.215e+05
23	5	1.941e+06	0.0	-0.31	-99.71	0.0	-7936.19	3247.74	0.0	0.0	0.0	1.893e+06
		1.893e+06	0.0	0.0	0.0	15.0	-7683.06	3148.02	0.0	0.0	0.0	1.941e+06
23	6	2.503e+06	0.0	-0.33	-216.17	0.0	3856.85	2241.83	0.0	0.0	0.0	2.471e+06
		2.471e+06	0.0	0.0	0.0	15.0	4109.98	2025.66	0.0	0.0	0.0	2.503e+06
23	7	2.955e+06	0.0	-0.41	-543.91	0.0	5971.23	658.23	0.0	0.0	0.0	2.950e+06
		2.950e+06	0.0	0.0	0.0	15.0	6224.35	114.32	0.0	0.0	0.0	2.955e+06
23	8	-2.695e+05	0.0	-0.07	-99.71	0.0	-1.761e+04	-4491.85	0.0	0.0	0.0	-2.695e+05
		-3.376e+05	0.0	0.0	0.0	15.0	-1.736e+04	-4591.56	0.0	0.0	0.0	-3.376e+05
23	9	3.078e+05	0.0	-0.08	-216.17	0.0	-5821.93	-5497.76	0.0	0.0	0.0	3.078e+05
		2.237e+05	0.0	0.0	0.0	15.0	-5568.80	-5713.93	0.0	0.0	0.0	2.237e+05
23	10	7.869e+05	0.0	-0.17	-543.91	0.0	-3707.55	-7081.36	0.0	0.0	0.0	7.869e+05
		6.766e+05	0.0	0.0	0.0	15.0	-3454.43	-7625.27	0.0	0.0	0.0	6.766e+05
23	11	-1.111e+06	0.0	-8.46e-03	-45.72	0.0	-2.277e+04	-3737.53	0.0	0.0	0.0	-1.111e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-1.168e+06	0.0	0.0	0.0	15.0	-2.251e+04	-3783.25	0.0	0.0	0.0	-1.168e+06
23	12	-5.312e+05	0.0	-2.67e-03	-45.72	0.0	-8353.13	-3140.71	0.0	0.0	0.0	-5.312e+05
		-5.786e+05	0.0	0.0	0.0	15.0	-8100.00	-3186.43	0.0	0.0	0.0	-5.786e+05
23	13	-5.055e+05	0.0	-4.09e-03	-45.72	0.0	-1.914e+04	-2521.42	0.0	0.0	0.0	-5.055e+05
		-5.437e+05	0.0	0.0	0.0	15.0	-1.888e+04	-2567.14	0.0	0.0	0.0	-5.437e+05
23	14	-7.145e+04	0.0	-2.45e-04	-45.72	0.0	-8353.13	-2074.91	0.0	0.0	0.0	-7.145e+04
		-1.029e+05	0.0	0.0	0.0	15.0	-8100.00	-2120.63	0.0	0.0	0.0	-1.029e+05
23	15	1.604e+06	0.0	-0.32	-99.71	0.0	-7936.19	2514.40	0.0	0.0	0.0	1.567e+06
		1.567e+06	0.0	0.0	0.0	15.0	-7683.06	2414.69	0.0	0.0	0.0	1.604e+06
23	16	2.165e+06	0.0	-0.33	-216.17	0.0	3856.85	1508.50	0.0	0.0	0.0	2.144e+06
		2.144e+06	0.0	0.0	0.0	15.0	4109.98	1292.33	0.0	0.0	0.0	2.165e+06
23	17	2.624e+06	0.0	-0.42	-543.91	0.0	5971.23	-75.10	0.0	0.0	0.0	2.624e+06
		2.618e+06	0.0	0.0	0.0	15.0	6224.35	-619.02	0.0	0.0	0.0	2.618e+06
23	18	-3.267e+05	0.0	-0.07	-99.71	0.0	-1.761e+04	-4694.77	0.0	0.0	0.0	-3.267e+05
		-3.979e+05	0.0	0.0	0.0	15.0	-1.736e+04	-4794.48	0.0	0.0	0.0	-3.979e+05
23	19	2.506e+05	0.0	-0.08	-216.17	0.0	-5821.93	-5700.67	0.0	0.0	0.0	2.506e+05
		1.634e+05	0.0	0.0	0.0	15.0	-5568.80	-5916.85	0.0	0.0	0.0	1.634e+05
23	20	7.297e+05	0.0	-0.17	-543.91	0.0	-3707.55	-7284.28	0.0	0.0	0.0	7.297e+05
		6.163e+05	0.0	0.0	0.0	15.0	-3454.43	-7828.19	0.0	0.0	0.0	6.163e+05
23	21	2.039e+06	0.0	-0.36	-99.71	0.0	-4433.87	3411.75	0.0	0.0	0.0	1.988e+06
		1.988e+06	0.0	0.0	0.0	15.0	-4180.75	3312.04	0.0	0.0	0.0	2.039e+06
23	22	-2.298e+05	0.0	-0.11	-99.71	0.0	-1.411e+04	-4523.42	0.0	0.0	0.0	-2.298e+05
		-2.985e+05	0.0	0.0	0.0	15.0	-1.386e+04	-4623.14	0.0	0.0	0.0	-2.985e+05
23	23	2.667e+06	0.0	-0.42	-543.91	0.0	8136.85	-193.80	0.0	0.0	0.0	2.667e+06
		2.660e+06	0.0	0.0	0.0	15.0	8324.35	-737.71	0.0	0.0	0.0	2.660e+06
23	24	2.328e+05	0.0	-0.17	-543.91	0.0	-1541.93	-8612.97	0.0	0.0	0.0	2.328e+05
		9.950e+04	0.0	0.0	0.0	15.0	-1354.43	-9156.89	0.0	0.0	0.0	9.950e+04
23	25	1.789e+06	0.0	-0.27	-99.71	0.0	-1.144e+04	2909.40	0.0	0.0	0.0	1.746e+06
		1.746e+06	0.0	0.0	0.0	15.0	-1.119e+04	2809.68	0.0	0.0	0.0	1.789e+06
23	26	2.291e+06	0.0	-0.33	-216.17	0.0	3856.85	1732.14	0.0	0.0	0.0	2.267e+06
		2.267e+06	0.0	0.0	0.0	15.0	4109.98	1515.97	0.0	0.0	0.0	2.291e+06
23	27	-4.238e+05	0.0	-0.12	-99.71	0.0	-1.656e+04	-4760.26	0.0	0.0	0.0	-4.238e+05
		-4.960e+05	0.0	0.0	0.0	15.0	-1.631e+04	-4859.97	0.0	0.0	0.0	-4.960e+05
23	28	1.701e+05	0.0	-0.08	-216.17	0.0	-5821.93	-5844.88	0.0	0.0	0.0	1.701e+05
		8.079e+04	0.0	0.0	0.0	15.0	-5568.80	-6061.05	0.0	0.0	0.0	8.079e+04
23	29	2.624e+06	0.0	-0.42	-543.91	0.0	5971.23	-75.10	0.0	0.0	0.0	2.624e+06
		2.618e+06	0.0	0.0	0.0	15.0	6224.35	-619.02	0.0	0.0	0.0	2.618e+06
23	30	1.429e+06	0.0	-0.25	-99.71	0.0	-7291.01	1104.62	0.0	0.0	0.0	1.413e+06
		1.413e+06	0.0	0.0	0.0	15.0	-7103.51	1004.91	0.0	0.0	0.0	1.429e+06
23	31	1.638e+06	0.0	-0.21	-216.17	0.0	3529.98	-1470.15	0.0	0.0	0.0	1.638e+06
		1.615e+06	0.0	0.0	0.0	15.0	3717.48	-1686.32	0.0	0.0	0.0	1.615e+06
23	32	1.532e+06	0.0	-0.24	-543.91	0.0	3491.28	-4965.10	0.0	0.0	0.0	1.532e+06
		1.454e+06	0.0	0.0	0.0	15.0	3678.78	-5509.01	0.0	0.0	0.0	1.454e+06
23	33	3.040e+06	0.0	-0.41	-543.91	0.0	5971.23	944.27	0.0	0.0	0.0	3.030e+06
		3.030e+06	0.0	0.0	0.0	15.0	6224.35	400.36	0.0	0.0	0.0	3.040e+06
23	34	-8.818e+05	0.0	-5.47e-03	-45.72	0.0	-1.419e+04	-3762.69	0.0	0.0	0.0	-8.818e+05
		-9.386e+05	0.0	0.0	0.0	15.0	-1.401e+04	-3808.41	0.0	0.0	0.0	-9.386e+05
23	35	-4.532e+05	0.0	-0.01	-132.20	0.0	-5436.95	-4509.65	0.0	0.0	0.0	-4.532e+05
		-5.219e+05	0.0	0.0	0.0	15.0	-5249.45	-4641.85	0.0	0.0	0.0	-5.219e+05
23	36	-4.648e+05	0.0	-0.04	-73.86	0.0	-1.340e+04	-4041.11	0.0	0.0	0.0	-4.648e+05
		-5.260e+05	0.0	0.0	0.0	15.0	-1.321e+04	-4114.98	0.0	0.0	0.0	-5.260e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
23	37	-3.617e+04	0.0	-0.05	-160.34	0.0	-4644.43	-4788.07	0.0	0.0	0.0	-3.617e+04
		-1.092e+05	0.0	0.0	0.0	15.0	-4456.93	-4948.41	0.0	0.0	0.0	-1.092e+05
23	38	3.196e+05	0.0	-0.11	-403.71	0.0	-3074.35	-5964.01	0.0	0.0	0.0	3.196e+05
		2.271e+05	0.0	0.0	0.0	15.0	-2886.85	-6367.73	0.0	0.0	0.0	2.271e+05
23	39	-6.568e+05	0.0	-3.85e-03	-45.72	0.0	-1.419e+04	-3258.52	0.0	0.0	0.0	-6.568e+05
		-7.060e+05	0.0	0.0	0.0	15.0	-1.401e+04	-3304.24	0.0	0.0	0.0	-7.060e+05
23	40	-3.345e+05	0.0	-6.33e-04	-45.72	0.0	-6187.50	-2926.96	0.0	0.0	0.0	-3.345e+05
		-3.787e+05	0.0	0.0	0.0	15.0	-6000.00	-2972.68	0.0	0.0	0.0	-3.787e+05
23	41	-6.899e+05	0.0	-0.04	-73.86	0.0	-1.340e+04	-4545.28	0.0	0.0	0.0	-6.899e+05
		-7.586e+05	0.0	0.0	0.0	15.0	-1.321e+04	-4619.14	0.0	0.0	0.0	-7.586e+05
23	42	-2.612e+05	0.0	-0.05	-160.34	0.0	-4644.43	-5292.24	0.0	0.0	0.0	-2.612e+05
		-3.418e+05	0.0	0.0	0.0	15.0	-4456.93	-5452.58	0.0	0.0	0.0	-3.418e+05
23	43	9.455e+04	0.0	-0.11	-403.71	0.0	-3074.35	-6468.18	0.0	0.0	0.0	9.455e+04
		-5512.67	0.0	0.0	0.0	15.0	-2886.85	-6871.90	0.0	0.0	0.0	-5512.67
23	44	-1.558e+05	0.0	-0.15	-403.71	0.0	-8480.27	-6672.51	0.0	0.0	0.0	-1.558e+05
		-2.590e+05	0.0	0.0	0.0	15.0	-8292.77	-7076.22	0.0	0.0	0.0	-2.590e+05
23	45	2.562e+04	0.0	-0.11	-403.71	0.0	-3074.35	-6712.66	0.0	0.0	0.0	2.562e+04
		-7.811e+04	0.0	0.0	0.0	15.0	-2886.85	-7116.38	0.0	0.0	0.0	-7.811e+04
23	46	-8.993e+05	0.0	-5.89e-03	-45.72	0.0	-1.686e+04	-3671.55	0.0	0.0	0.0	-8.993e+05
		-9.547e+05	0.0	0.0	0.0	15.0	-1.668e+04	-3717.27	0.0	0.0	0.0	-9.547e+05
23	47	-4.695e+05	0.0	-1.60e-03	-45.72	0.0	-6187.50	-3229.46	0.0	0.0	0.0	-4.695e+05
		-5.183e+05	0.0	0.0	0.0	15.0	-6000.00	-3275.18	0.0	0.0	0.0	-5.183e+05
23	48	-9.048e+05	0.0	-5.31e-03	-45.72	0.0	-1.419e+04	-3844.19	0.0	0.0	0.0	-9.048e+05
		-9.628e+05	0.0	0.0	0.0	15.0	-1.401e+04	-3889.91	0.0	0.0	0.0	-9.628e+05
23	49	-5.825e+05	0.0	-2.09e-03	-45.72	0.0	-6187.50	-3512.62	0.0	0.0	0.0	-5.825e+05
		-6.356e+05	0.0	0.0	0.0	15.0	-6000.00	-3558.34	0.0	0.0	0.0	-6.356e+05
23	50	1.335e+06	0.0	-0.22	-73.86	0.0	-6232.17	2007.75	0.0	0.0	0.0	1.306e+06
		1.306e+06	0.0	0.0	0.0	15.0	-6044.67	1933.88	0.0	0.0	0.0	1.335e+06
23	51	1.752e+06	0.0	-0.23	-160.34	0.0	2525.04	1260.79	0.0	0.0	0.0	1.734e+06
		1.734e+06	0.0	0.0	0.0	15.0	2712.54	1100.45	0.0	0.0	0.0	1.752e+06
23	52	2.090e+06	0.0	-0.29	-403.71	0.0	4095.12	84.85	0.0	0.0	0.0	2.090e+06
		2.088e+06	0.0	0.0	0.0	15.0	4282.62	-318.87	0.0	0.0	0.0	2.088e+06
23	53	-2.840e+05	0.0	-0.03	-73.86	0.0	-1.340e+04	-3693.82	0.0	0.0	0.0	-2.840e+05
		-3.400e+05	0.0	0.0	0.0	15.0	-1.321e+04	-3767.68	0.0	0.0	0.0	-3.400e+05
23	54	1.447e+05	0.0	-0.04	-160.34	0.0	-4644.43	-4440.78	0.0	0.0	0.0	1.447e+05
		7.683e+04	0.0	0.0	0.0	15.0	-4456.93	-4601.12	0.0	0.0	0.0	7.683e+04
23	55	5.005e+05	0.0	-0.11	-403.71	0.0	-3074.35	-5616.72	0.0	0.0	0.0	5.005e+05
		4.132e+05	0.0	0.0	0.0	15.0	-2886.85	-6020.44	0.0	0.0	0.0	4.132e+05
23	56	-8.303e+05	0.0	-6.36e-03	-45.72	0.0	-1.686e+04	-3427.07	0.0	0.0	0.0	-8.303e+05
		-8.821e+05	0.0	0.0	0.0	15.0	-1.668e+04	-3472.79	0.0	0.0	0.0	-8.821e+05
23	57	-4.006e+05	0.0	-2.07e-03	-45.72	0.0	-6187.50	-2984.98	0.0	0.0	0.0	-4.006e+05
		-4.457e+05	0.0	0.0	0.0	15.0	-6000.00	-3030.70	0.0	0.0	0.0	-4.457e+05
23	58	-7.899e+05	0.0	-6.09e-03	-45.72	0.0	-1.419e+04	-3436.72	0.0	0.0	0.0	-7.899e+05
		-8.418e+05	0.0	0.0	0.0	15.0	-1.401e+04	-3482.44	0.0	0.0	0.0	-8.418e+05
23	59	-4.676e+05	0.0	-2.88e-03	-45.72	0.0	-6187.50	-3105.15	0.0	0.0	0.0	-4.676e+05
		-5.146e+05	0.0	0.0	0.0	15.0	-6000.00	-3150.87	0.0	0.0	0.0	-5.146e+05
23	60	1.333e+06	0.0	-0.22	-73.86	0.0	-6232.17	2001.63	0.0	0.0	0.0	1.304e+06
		1.304e+06	0.0	0.0	0.0	15.0	-6044.67	1927.77	0.0	0.0	0.0	1.333e+06
23	61	1.750e+06	0.0	-0.23	-160.34	0.0	2525.04	1254.68	0.0	0.0	0.0	1.732e+06
		1.732e+06	0.0	0.0	0.0	15.0	2712.54	1094.34	0.0	0.0	0.0	1.750e+06
23	62	2.088e+06	0.0	-0.29	-403.71	0.0	4095.12	78.73	0.0	0.0	0.0	2.088e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		2.086e+06	0.0	0.0	0.0	15.0	4282.62	-324.98	0.0	0.0	0.0	2.086e+06
23	63	-3.317e+05	0.0	-0.03	-73.86	0.0	-1.340e+04	-3862.92	0.0	0.0	0.0	-3.317e+05
		-3.902e+05	0.0	0.0	0.0	15.0	-1.321e+04	-3936.78	0.0	0.0	0.0	-3.902e+05
23	64	9.699e+04	0.0	-0.04	-160.34	0.0	-4644.43	-4609.88	0.0	0.0	0.0	9.699e+04
		2.662e+04	0.0	0.0	0.0	15.0	-4456.93	-4770.22	0.0	0.0	0.0	2.662e+04
23	65	4.528e+05	0.0	-0.11	-403.71	0.0	-3074.35	-5785.82	0.0	0.0	0.0	4.528e+05
		3.630e+05	0.0	0.0	0.0	15.0	-2886.85	-6189.53	0.0	0.0	0.0	3.630e+05
23	66	1.407e+06	0.0	-0.25	-73.86	0.0	-3631.44	2128.87	0.0	0.0	0.0	1.376e+06
		1.376e+06	0.0	0.0	0.0	15.0	-3443.94	2055.01	0.0	0.0	0.0	1.407e+06
23	67	-2.597e+05	0.0	-0.07	-73.86	0.0	-1.080e+04	-3735.68	0.0	0.0	0.0	-2.597e+05
		-3.164e+05	0.0	0.0	0.0	15.0	-1.061e+04	-3809.54	0.0	0.0	0.0	-3.164e+05
23	68	1.818e+06	0.0	-0.29	-403.71	0.0	4095.12	-526.27	0.0	0.0	0.0	1.818e+06
		1.807e+06	0.0	0.0	0.0	15.0	4282.62	-929.98	0.0	0.0	0.0	1.807e+06
23	69	2641.19	0.0	-0.11	-403.71	0.0	-3074.35	-6794.16	0.0	0.0	0.0	2641.19
		-1.023e+05	0.0	0.0	0.0	15.0	-2886.85	-7197.87	0.0	0.0	0.0	-1.023e+05
23	70	-5.538e+05	0.0	-2.29e-03	-45.72	0.0	-6187.50	-3410.75	0.0	0.0	0.0	-5.538e+05
		-6.053e+05	0.0	0.0	0.0	15.0	-6000.00	-3456.47	0.0	0.0	0.0	-6.053e+05
23	71	-1.482e+05	0.0	-0.03	-73.86	0.0	-5394.98	-3729.92	0.0	0.0	0.0	-1.482e+05
		-2.048e+05	0.0	0.0	0.0	15.0	-5207.48	-3803.78	0.0	0.0	0.0	-2.048e+05
23	72	-3.287e+05	0.0	-6.72e-04	-45.72	0.0	-6187.50	-2906.59	0.0	0.0	0.0	-3.287e+05
		-3.727e+05	0.0	0.0	0.0	15.0	-6000.00	-2952.30	0.0	0.0	0.0	-3.727e+05
23	73	-3.733e+05	0.0	-0.04	-73.86	0.0	-5394.98	-4234.09	0.0	0.0	0.0	-3.733e+05
		-4.374e+05	0.0	0.0	0.0	15.0	-5207.48	-4307.95	0.0	0.0	0.0	-4.374e+05
23	74	-4.308e+05	0.0	-0.03	-73.86	0.0	-5394.98	-4437.82	0.0	0.0	0.0	-4.308e+05
		-4.979e+05	0.0	0.0	0.0	15.0	-5207.48	-4511.68	0.0	0.0	0.0	-4.979e+05
24	1	1.170e+06	0.0	8.45e-03	45.72	0.0	-2.277e+04	3744.86	0.0	0.0	0.0	1.113e+06
		1.113e+06	0.0	0.0	0.0	15.0	-2.251e+04	3790.58	0.0	0.0	0.0	1.170e+06
24	2	5.808e+05	0.0	2.65e-03	45.72	0.0	-8353.12	3148.04	0.0	0.0	0.0	5.332e+05
		5.332e+05	0.0	0.0	0.0	15.0	-8100.00	3193.76	0.0	0.0	0.0	5.808e+05
24	3	1.162e+06	0.0	7.57e-03	45.72	0.0	-1.914e+04	3934.35	0.0	0.0	0.0	1.103e+06
		1.103e+06	0.0	0.0	0.0	15.0	-1.888e+04	3980.06	0.0	0.0	0.0	1.162e+06
24	4	7.215e+05	0.0	3.24e-03	45.72	0.0	-8353.13	3487.84	0.0	0.0	0.0	6.688e+05
		6.688e+05	0.0	0.0	0.0	15.0	-8100.00	3533.56	0.0	0.0	0.0	7.215e+05
24	5	3.658e+06	0.0	-0.31	45.72	0.0	-3.033e+04	1.297e+04	0.0	0.0	0.0	3.464e+06
		3.464e+06	0.0	0.0	0.0	15.0	-3.008e+04	1.301e+04	0.0	0.0	0.0	3.658e+06
24	6	3.602e+06	0.0	-0.33	45.72	0.0	-2.056e+04	1.409e+04	0.0	0.0	0.0	3.391e+06
		3.391e+06	0.0	0.0	0.0	15.0	-2.031e+04	1.413e+04	0.0	0.0	0.0	3.602e+06
24	7	4.207e+06	0.0	-0.42	45.72	0.0	-2.268e+04	1.600e+04	0.0	0.0	0.0	3.966e+06
		3.966e+06	0.0	0.0	0.0	15.0	-2.242e+04	1.605e+04	0.0	0.0	0.0	4.207e+06
24	8	1.098e+06	0.0	-0.06	45.72	0.0	-2.066e+04	4545.85	0.0	0.0	0.0	1.029e+06
		1.029e+06	0.0	0.0	0.0	15.0	-2.040e+04	4591.56	0.0	0.0	0.0	1.098e+06
24	9	1.042e+06	0.0	-0.08	45.72	0.0	-1.088e+04	5668.21	0.0	0.0	0.0	9.565e+05
		9.565e+05	0.0	0.0	0.0	15.0	-1.063e+04	5713.93	0.0	0.0	0.0	1.042e+06
24	10	1.646e+06	0.0	-0.17	45.72	0.0	-1.300e+04	7579.55	0.0	0.0	0.0	1.532e+06
		1.532e+06	0.0	0.0	0.0	15.0	-1.275e+04	7625.27	0.0	0.0	0.0	1.646e+06
24	11	1.168e+06	0.0	8.46e-03	45.72	0.0	-2.277e+04	3737.53	0.0	0.0	0.0	1.111e+06
		1.111e+06	0.0	0.0	0.0	15.0	-2.251e+04	3783.25	0.0	0.0	0.0	1.168e+06
24	12	5.786e+05	0.0	2.67e-03	45.72	0.0	-8353.12	3140.71	0.0	0.0	0.0	5.312e+05
		5.312e+05	0.0	0.0	0.0	15.0	-8100.00	3186.43	0.0	0.0	0.0	5.786e+05
24	13	5.437e+05	0.0	4.09e-03	45.72	0.0	-1.914e+04	2521.42	0.0	0.0	0.0	5.055e+05
		5.055e+05	0.0	0.0	0.0	15.0	-1.888e+04	2567.14	0.0	0.0	0.0	5.437e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
24	14	1.029e+05	0.0	2.45e-04	45.72	0.0	-8353.12	2074.91	0.0	0.0	0.0	7.145e+04
		7.145e+04	0.0	0.0	0.0	15.0	-8100.00	2120.63	0.0	0.0	0.0	1.029e+05
24	15	3.996e+06	0.0	-0.31	45.72	0.0	-3.033e+04	1.370e+04	0.0	0.0	0.0	3.790e+06
		3.790e+06	0.0	0.0	0.0	15.0	-3.008e+04	1.374e+04	0.0	0.0	0.0	3.996e+06
24	16	3.940e+06	0.0	-0.33	45.72	0.0	-2.056e+04	1.482e+04	0.0	0.0	0.0	3.717e+06
		3.717e+06	0.0	0.0	0.0	15.0	-2.031e+04	1.487e+04	0.0	0.0	0.0	3.940e+06
24	17	4.544e+06	0.0	-0.42	45.72	0.0	-2.268e+04	1.673e+04	0.0	0.0	0.0	4.293e+06
		4.293e+06	0.0	0.0	0.0	15.0	-2.242e+04	1.678e+04	0.0	0.0	0.0	4.544e+06
24	18	1.158e+06	0.0	-0.06	45.72	0.0	-2.066e+04	4748.76	0.0	0.0	0.0	1.087e+06
		1.087e+06	0.0	0.0	0.0	15.0	-2.040e+04	4794.48	0.0	0.0	0.0	1.158e+06
24	19	1.102e+06	0.0	-0.08	45.72	0.0	-1.088e+04	5871.13	0.0	0.0	0.0	1.014e+06
		1.014e+06	0.0	0.0	0.0	15.0	-1.063e+04	5916.85	0.0	0.0	0.0	1.102e+06
24	20	1.706e+06	0.0	-0.17	45.72	0.0	-1.300e+04	7782.47	0.0	0.0	0.0	1.589e+06
		1.589e+06	0.0	0.0	0.0	15.0	-1.275e+04	7828.19	0.0	0.0	0.0	1.706e+06
24	21	3.602e+06	0.0	-0.35	45.72	0.0	-3.384e+04	1.280e+04	0.0	0.0	0.0	3.409e+06
		3.409e+06	0.0	0.0	0.0	15.0	-3.358e+04	1.285e+04	0.0	0.0	0.0	3.602e+06
24	22	1.099e+06	0.0	-0.10	45.72	0.0	-2.416e+04	4577.42	0.0	0.0	0.0	1.030e+06
		1.030e+06	0.0	0.0	0.0	15.0	-2.391e+04	4623.14	0.0	0.0	0.0	1.099e+06
24	23	4.502e+06	0.0	-0.42	45.72	0.0	-2.051e+04	1.685e+04	0.0	0.0	0.0	4.249e+06
		4.249e+06	0.0	0.0	0.0	15.0	-2.032e+04	1.690e+04	0.0	0.0	0.0	4.502e+06
24	24	2.223e+06	0.0	-0.17	45.72	0.0	-1.083e+04	9111.17	0.0	0.0	0.0	2.086e+06
		2.086e+06	0.0	0.0	0.0	15.0	-1.065e+04	9156.89	0.0	0.0	0.0	2.223e+06
24	25	3.770e+06	0.0	-0.26	45.72	0.0	-2.683e+04	1.330e+04	0.0	0.0	0.0	3.570e+06
		3.570e+06	0.0	0.0	0.0	15.0	-2.658e+04	1.335e+04	0.0	0.0	0.0	3.770e+06
24	26	3.813e+06	0.0	-0.33	45.72	0.0	-2.056e+04	1.460e+04	0.0	0.0	0.0	3.594e+06
		3.594e+06	0.0	0.0	0.0	15.0	-2.031e+04	1.464e+04	0.0	0.0	0.0	3.813e+06
24	27	1.311e+06	0.0	-0.12	45.72	0.0	-2.897e+04	4814.25	0.0	0.0	0.0	1.238e+06
		1.238e+06	0.0	0.0	0.0	15.0	-2.871e+04	4859.97	0.0	0.0	0.0	1.311e+06
24	28	1.185e+06	0.0	-0.08	45.72	0.0	-1.088e+04	6015.34	0.0	0.0	0.0	1.094e+06
		1.094e+06	0.0	0.0	0.0	15.0	-1.063e+04	6061.05	0.0	0.0	0.0	1.185e+06
24	29	4.544e+06	0.0	-0.42	45.72	0.0	-2.268e+04	1.673e+04	0.0	0.0	0.0	4.293e+06
		4.293e+06	0.0	0.0	0.0	15.0	-2.242e+04	1.678e+04	0.0	0.0	0.0	4.544e+06
24	30	3.411e+06	0.0	-0.25	99.71	0.0	-2.665e+04	1.505e+04	0.0	0.0	0.0	3.184e+06
		3.184e+06	0.0	0.0	0.0	15.0	-2.646e+04	1.515e+04	0.0	0.0	0.0	3.411e+06
24	31	3.244e+06	0.0	-0.21	216.17	0.0	-1.590e+04	1.763e+04	0.0	0.0	0.0	2.978e+06
		2.978e+06	0.0	0.0	0.0	15.0	-1.572e+04	1.785e+04	0.0	0.0	0.0	3.244e+06
24	32	3.386e+06	0.0	-0.25	543.91	0.0	-1.587e+04	2.112e+04	0.0	0.0	0.0	3.065e+06
		3.065e+06	0.0	0.0	0.0	15.0	-1.568e+04	2.167e+04	0.0	0.0	0.0	3.386e+06
24	33	4.122e+06	0.0	-0.42	45.72	0.0	-2.268e+04	1.571e+04	0.0	0.0	0.0	3.886e+06
		3.886e+06	0.0	0.0	0.0	15.0	-2.242e+04	1.576e+04	0.0	0.0	0.0	4.122e+06
24	34	9.386e+05	0.0	5.47e-03	45.72	0.0	-1.419e+04	3762.69	0.0	0.0	0.0	8.818e+05
		8.818e+05	0.0	0.0	0.0	15.0	-1.401e+04	3808.41	0.0	0.0	0.0	9.386e+05
24	35	8.971e+05	0.0	-0.01	45.72	0.0	-6938.05	4596.13	0.0	0.0	0.0	8.278e+05
		8.278e+05	0.0	0.0	0.0	15.0	-6750.55	4641.85	0.0	0.0	0.0	8.971e+05
24	36	9.223e+05	0.0	-0.03	45.72	0.0	-1.499e+04	4069.26	0.0	0.0	0.0	8.609e+05
		8.609e+05	0.0	0.0	0.0	15.0	-1.480e+04	4114.98	0.0	0.0	0.0	9.223e+05
24	37	8.807e+05	0.0	-0.05	45.72	0.0	-7730.57	4902.69	0.0	0.0	0.0	8.069e+05
		8.069e+05	0.0	0.0	0.0	15.0	-7543.07	4948.41	0.0	0.0	0.0	8.807e+05
24	38	1.329e+06	0.0	-0.11	45.72	0.0	-9300.65	6322.01	0.0	0.0	0.0	1.234e+06
		1.234e+06	0.0	0.0	0.0	15.0	-9113.15	6367.73	0.0	0.0	0.0	1.329e+06
24	39	7.060e+05	0.0	3.85e-03	45.72	0.0	-1.419e+04	3258.52	0.0	0.0	0.0	6.568e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		6.568e+05	0.0	0.0	0.0	15.0	-1.401e+04	3304.24	0.0	0.0	0.0	7.060e+05
24	40	3.787e+05	0.0	6.33e-04	45.72	0.0	-6187.50	2926.96	0.0	0.0	0.0	3.345e+05
		3.345e+05	0.0	0.0	0.0	15.0	-6000.00	2972.68	0.0	0.0	0.0	3.787e+05
24	41	1.155e+06	0.0	-0.03	45.72	0.0	-1.499e+04	4573.43	0.0	0.0	0.0	1.086e+06
		1.086e+06	0.0	0.0	0.0	15.0	-1.480e+04	4619.14	0.0	0.0	0.0	1.155e+06
24	42	1.113e+06	0.0	-0.04	45.72	0.0	-7730.57	5406.86	0.0	0.0	0.0	1.032e+06
		1.032e+06	0.0	0.0	0.0	15.0	-7543.07	5452.58	0.0	0.0	0.0	1.113e+06
24	43	1.562e+06	0.0	-0.11	45.72	0.0	-9300.65	6826.18	0.0	0.0	0.0	1.459e+06
		1.459e+06	0.0	0.0	0.0	15.0	-9113.15	6871.90	0.0	0.0	0.0	1.562e+06
24	44	1.846e+06	0.0	-0.14	45.72	0.0	-1.991e+04	7030.51	0.0	0.0	0.0	1.740e+06
		1.740e+06	0.0	0.0	0.0	15.0	-1.972e+04	7076.22	0.0	0.0	0.0	1.846e+06
24	45	1.635e+06	0.0	-0.11	45.72	0.0	-9300.65	7070.66	0.0	0.0	0.0	1.528e+06
		1.528e+06	0.0	0.0	0.0	15.0	-9113.15	7116.38	0.0	0.0	0.0	1.635e+06
24	46	9.547e+05	0.0	5.89e-03	45.72	0.0	-1.686e+04	3671.55	0.0	0.0	0.0	8.993e+05
		8.993e+05	0.0	0.0	0.0	15.0	-1.668e+04	3717.27	0.0	0.0	0.0	9.547e+05
24	47	5.183e+05	0.0	1.60e-03	45.72	0.0	-6187.50	3229.46	0.0	0.0	0.0	4.695e+05
		4.695e+05	0.0	0.0	0.0	15.0	-6000.00	3275.18	0.0	0.0	0.0	5.183e+05
24	48	9.628e+05	0.0	5.31e-03	45.72	0.0	-1.419e+04	3844.19	0.0	0.0	0.0	9.048e+05
		9.048e+05	0.0	0.0	0.0	15.0	-1.401e+04	3889.91	0.0	0.0	0.0	9.628e+05
24	49	6.356e+05	0.0	2.09e-03	45.72	0.0	-6187.50	3512.62	0.0	0.0	0.0	5.825e+05
		5.825e+05	0.0	0.0	0.0	15.0	-6000.00	3558.34	0.0	0.0	0.0	6.356e+05
24	50	2.646e+06	0.0	-0.21	45.72	0.0	-2.216e+04	9990.40	0.0	0.0	0.0	2.496e+06
		2.496e+06	0.0	0.0	0.0	15.0	-2.197e+04	1.004e+04	0.0	0.0	0.0	2.646e+06
24	51	2.604e+06	0.0	-0.23	45.72	0.0	-1.490e+04	1.082e+04	0.0	0.0	0.0	2.442e+06
		2.442e+06	0.0	0.0	0.0	15.0	-1.471e+04	1.087e+04	0.0	0.0	0.0	2.604e+06
24	52	3.053e+06	0.0	-0.30	45.72	0.0	-1.647e+04	1.224e+04	0.0	0.0	0.0	2.869e+06
		2.869e+06	0.0	0.0	0.0	15.0	-1.628e+04	1.229e+04	0.0	0.0	0.0	3.053e+06
24	53	7.362e+05	0.0	-0.03	45.72	0.0	-1.499e+04	3721.96	0.0	0.0	0.0	6.800e+05
		6.800e+05	0.0	0.0	0.0	15.0	-1.480e+04	3767.68	0.0	0.0	0.0	7.362e+05
24	54	6.947e+05	0.0	-0.05	45.72	0.0	-7730.57	4555.40	0.0	0.0	0.0	6.260e+05
		6.260e+05	0.0	0.0	0.0	15.0	-7543.07	4601.12	0.0	0.0	0.0	6.947e+05
24	55	1.143e+06	0.0	-0.11	45.72	0.0	-9300.65	5974.72	0.0	0.0	0.0	1.053e+06
		1.053e+06	0.0	0.0	0.0	15.0	-9113.15	6020.44	0.0	0.0	0.0	1.143e+06
24	56	8.821e+05	0.0	6.36e-03	45.72	0.0	-1.686e+04	3427.07	0.0	0.0	0.0	8.303e+05
		8.303e+05	0.0	0.0	0.0	15.0	-1.668e+04	3472.79	0.0	0.0	0.0	8.821e+05
24	57	4.457e+05	0.0	2.07e-03	45.72	0.0	-6187.50	2984.98	0.0	0.0	0.0	4.006e+05
		4.006e+05	0.0	0.0	0.0	15.0	-6000.00	3030.70	0.0	0.0	0.0	4.457e+05
24	58	8.418e+05	0.0	6.09e-03	45.72	0.0	-1.419e+04	3436.72	0.0	0.0	0.0	7.899e+05
		7.899e+05	0.0	0.0	0.0	15.0	-1.401e+04	3482.44	0.0	0.0	0.0	8.418e+05
24	59	5.146e+05	0.0	2.88e-03	45.72	0.0	-6187.50	3105.15	0.0	0.0	0.0	4.676e+05
		4.676e+05	0.0	0.0	0.0	15.0	-6000.00	3150.87	0.0	0.0	0.0	5.146e+05
24	60	2.648e+06	0.0	-0.21	45.72	0.0	-2.216e+04	9996.51	0.0	0.0	0.0	2.497e+06
		2.497e+06	0.0	0.0	0.0	15.0	-2.197e+04	1.004e+04	0.0	0.0	0.0	2.648e+06
24	61	2.606e+06	0.0	-0.23	45.72	0.0	-1.490e+04	1.083e+04	0.0	0.0	0.0	2.443e+06
		2.443e+06	0.0	0.0	0.0	15.0	-1.471e+04	1.088e+04	0.0	0.0	0.0	2.606e+06
24	62	3.055e+06	0.0	-0.30	45.72	0.0	-1.647e+04	1.225e+04	0.0	0.0	0.0	2.871e+06
		2.871e+06	0.0	0.0	0.0	15.0	-1.628e+04	1.229e+04	0.0	0.0	0.0	3.055e+06
24	63	7.864e+05	0.0	-0.03	45.72	0.0	-1.499e+04	3891.06	0.0	0.0	0.0	7.277e+05
		7.277e+05	0.0	0.0	0.0	15.0	-1.480e+04	3936.78	0.0	0.0	0.0	7.864e+05
24	64	7.449e+05	0.0	-0.05	45.72	0.0	-7730.57	4724.50	0.0	0.0	0.0	6.737e+05
		6.737e+05	0.0	0.0	0.0	15.0	-7543.07	4770.22	0.0	0.0	0.0	7.449e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
24	65	1.194e+06	0.0	-0.11	45.72	0.0	-9300.65	6143.82	0.0	0.0	0.0	1.101e+06
		1.101e+06	0.0	0.0	0.0	15.0	-9113.15	6189.53	0.0	0.0	0.0	1.194e+06
24	66	2.604e+06	0.0	-0.25	45.72	0.0	-2.476e+04	9869.27	0.0	0.0	0.0	2.456e+06
		2.456e+06	0.0	0.0	0.0	15.0	-2.457e+04	9914.99	0.0	0.0	0.0	2.604e+06
24	67	7.428e+05	0.0	-0.06	45.72	0.0	-1.759e+04	3763.82	0.0	0.0	0.0	6.860e+05
		6.860e+05	0.0	0.0	0.0	15.0	-1.740e+04	3809.54	0.0	0.0	0.0	7.428e+05
24	68	3.334e+06	0.0	-0.29	45.72	0.0	-1.647e+04	1.285e+04	0.0	0.0	0.0	3.141e+06
		3.141e+06	0.0	0.0	0.0	15.0	-1.628e+04	1.290e+04	0.0	0.0	0.0	3.334e+06
24	69	1.659e+06	0.0	-0.11	45.72	0.0	-9300.65	7152.15	0.0	0.0	0.0	1.551e+06
		1.551e+06	0.0	0.0	0.0	15.0	-9113.15	7197.87	0.0	0.0	0.0	1.659e+06
24	70	6.053e+05	0.0	2.29e-03	45.72	0.0	-6187.50	3410.75	0.0	0.0	0.0	5.538e+05
		5.538e+05	0.0	0.0	0.0	15.0	-6000.00	3456.47	0.0	0.0	0.0	6.053e+05
24	71	6.010e+05	0.0	-0.03	45.72	0.0	-6980.02	3758.06	0.0	0.0	0.0	5.443e+05
		5.443e+05	0.0	0.0	0.0	15.0	-6792.52	3803.78	0.0	0.0	0.0	6.010e+05
24	72	3.727e+05	0.0	6.72e-04	45.72	0.0	-6187.50	2906.59	0.0	0.0	0.0	3.287e+05
		3.287e+05	0.0	0.0	0.0	15.0	-6000.00	2952.30	0.0	0.0	0.0	3.727e+05
24	73	8.337e+05	0.0	-0.03	45.72	0.0	-6980.02	4262.23	0.0	0.0	0.0	7.694e+05
		7.694e+05	0.0	0.0	0.0	15.0	-6792.52	4307.95	0.0	0.0	0.0	8.337e+05
24	74	8.942e+05	0.0	-0.03	45.72	0.0	-6980.02	4465.97	0.0	0.0	0.0	8.268e+05
		8.268e+05	0.0	0.0	0.0	15.0	-6792.52	4511.68	0.0	0.0	0.0	8.942e+05
Pilas.		**M3 mx/mn**	**M2 mx/mn**	**D 2 / D 3**	**Q 2 / Q 3**		**N**	**V 2**	**V 3**	**T**		
		-5.889e+06	0.0	-5.26	-1.209e+04		-4.362e+04	-1.152e+04	0.0	0.0		
		4.544e+06	0.0	0.05	1.209e+04		8324.35	3.358e+04	0.0	0.0		

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		daN cm	daN cm	cm	daN	cm	daN	daN	daN	daN cm	daN cm	daN cm
25	1	-8.920e+05	0.0	-7.81e-03	-556.88	0.0	-3790.57	2.251e+04	0.0	0.0	0.0	-1.170e+06
		-1.170e+06	0.0	0.0	0.0	12.5	-3790.57	2.196e+04	0.0	0.0	0.0	-8.920e+05
25	2	-4.821e+05	0.0	-2.51e-03	-405.00	0.0	-3193.75	8100.00	0.0	0.0	0.0	-5.808e+05
		-5.808e+05	0.0	0.0	0.0	12.5	-3193.75	7695.00	0.0	0.0	0.0	-4.821e+05
25	3	-9.295e+05	0.0	-6.99e-03	-518.63	0.0	-3980.06	1.888e+04	0.0	0.0	0.0	-1.162e+06
		-1.162e+06	0.0	0.0	0.0	12.5	-3980.06	1.836e+04	0.0	0.0	0.0	-9.295e+05
25	4	-6.228e+05	0.0	-3.03e-03	-405.00	0.0	-3533.55	8100.00	0.0	0.0	0.0	-7.215e+05
		-7.215e+05	0.0	0.0	0.0	12.5	-3533.55	7695.00	0.0	0.0	0.0	-6.228e+05
25	5	2.034e+06	0.0	0.26	-518.63	0.0	3148.03	7683.06	0.0	0.0	0.0	1.941e+06
		1.941e+06	0.0	0.0	0.0	12.5	2763.28	7164.44	0.0	0.0	0.0	2.034e+06
25	6	2.503e+06	0.0	0.27	-405.00	0.0	2025.66	-4109.98	0.0	0.0	0.0	2.503e+06
		2.449e+06	0.0	0.0	0.0	12.5	1640.91	-4514.98	0.0	0.0	0.0	2.449e+06
25	7	2.955e+06	0.0	0.34	-405.00	0.0	114.32	-6224.35	0.0	0.0	0.0	2.955e+06
		2.875e+06	0.0	0.0	0.0	12.5	-270.43	-6629.35	0.0	0.0	0.0	2.875e+06
25	8	-1.238e+05	0.0	-0.06	-518.63	0.0	-4591.56	1.736e+04	0.0	0.0	0.0	-3.376e+05
		-3.376e+05	0.0	0.0	0.0	12.5	-4591.56	1.684e+04	0.0	0.0	0.0	-1.238e+05
25	9	2.907e+05	0.0	-0.06	-405.00	0.0	-5713.93	5568.80	0.0	0.0	0.0	2.237e+05
		2.237e+05	0.0	0.0	0.0	12.5	-5713.93	5163.80	0.0	0.0	0.0	2.907e+05
25	10	7.172e+05	0.0	0.14	-405.00	0.0	-7625.27	3454.43	0.0	0.0	0.0	6.766e+05
		6.766e+05	0.0	0.0	0.0	12.5	-7625.27	3049.43	0.0	0.0	0.0	7.172e+05
25	11	-8.898e+05	0.0	-7.82e-03	-556.88	0.0	-3783.25	2.251e+04	0.0	0.0	0.0	-1.168e+06
		-1.168e+06	0.0	0.0	0.0	12.5	-3783.25	2.196e+04	0.0	0.0	0.0	-8.898e+05
25	12	-4.799e+05	0.0	-2.53e-03	-405.00	0.0	-3186.43	8100.00	0.0	0.0	0.0	-5.786e+05
		-5.786e+05	0.0	0.0	0.0	12.5	-3186.43	7695.00	0.0	0.0	0.0	-4.799e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
25	13	-3.109e+05	0.0	-4.00e-03	-518.63	0.0	-2567.14	1.888e+04	0.0	0.0	0.0	-5.437e+05
		-5.437e+05	0.0	0.0	0.0	12.5	-2567.14	1.836e+04	0.0	0.0	0.0	-3.109e+05
25	14	-4210.17	0.0	-3.86e-05	-405.00	0.0	-2120.63	8100.00	0.0	0.0	0.0	-1.029e+05
		-1.029e+05	0.0	0.0	0.0	12.5	-2120.63	7695.00	0.0	0.0	0.0	-4210.17
25	15	1.697e+06	0.0	0.26	-518.63	0.0	2414.70	7683.06	0.0	0.0	0.0	1.604e+06
		1.604e+06	0.0	0.0	0.0	12.5	2029.95	7164.44	0.0	0.0	0.0	1.697e+06
25	16	2.165e+06	0.0	0.27	-405.00	0.0	1292.33	-4109.98	0.0	0.0	0.0	2.165e+06
		2.111e+06	0.0	0.0	0.0	12.5	907.58	-4514.98	0.0	0.0	0.0	2.111e+06
25	17	2.618e+06	0.0	0.35	-405.00	0.0	-619.01	-6224.35	0.0	0.0	0.0	2.618e+06
		2.538e+06	0.0	0.0	0.0	12.5	-1003.76	-6629.35	0.0	0.0	0.0	2.538e+06
25	18	-1.841e+05	0.0	-0.06	-518.63	0.0	-4794.48	1.736e+04	0.0	0.0	0.0	-3.979e+05
		-3.979e+05	0.0	0.0	0.0	12.5	-4794.48	1.684e+04	0.0	0.0	0.0	-1.841e+05
25	19	2.305e+05	0.0	-0.06	-405.00	0.0	-5916.84	5568.80	0.0	0.0	0.0	1.634e+05
		1.634e+05	0.0	0.0	0.0	12.5	-5916.84	5163.80	0.0	0.0	0.0	2.305e+05
25	20	6.570e+05	0.0	0.14	-405.00	0.0	-7828.18	3454.43	0.0	0.0	0.0	6.163e+05
		6.163e+05	0.0	0.0	0.0	12.5	-7828.18	3049.43	0.0	0.0	0.0	6.570e+05
25	21	2.088e+06	0.0	0.30	-518.63	0.0	3312.05	4180.75	0.0	0.0	0.0	2.039e+06
		2.039e+06	0.0	0.0	0.0	12.5	2927.30	3662.12	0.0	0.0	0.0	2.088e+06
25	22	-1.285e+05	0.0	-0.09	-518.63	0.0	-4623.13	1.386e+04	0.0	0.0	0.0	-2.985e+05
		-2.985e+05	0.0	0.0	0.0	12.5	-4623.13	1.334e+04	0.0	0.0	0.0	-1.285e+05
25	23	2.660e+06	0.0	0.34	-300.00	0.0	-737.70	-8324.35	0.0	0.0	0.0	2.660e+06
		2.554e+06	0.0	0.0	0.0	12.5	-1122.45	-8624.35	0.0	0.0	0.0	2.554e+06
25	24	1.146e+05	0.0	0.14	-300.00	0.0	-9156.88	1354.43	0.0	0.0	0.0	9.950e+04
		9.950e+04	0.0	0.0	0.0	12.5	-9156.88	1054.43	0.0	0.0	0.0	1.146e+05
25	25	1.926e+06	0.0	0.23	-518.63	0.0	2809.68	1.119e+04	0.0	0.0	0.0	1.789e+06
		1.789e+06	0.0	0.0	0.0	12.5	2424.93	1.067e+04	0.0	0.0	0.0	1.926e+06
25	26	2.291e+06	0.0	0.27	-405.00	0.0	1515.97	-4109.98	0.0	0.0	0.0	2.291e+06
		2.238e+06	0.0	0.0	0.0	12.5	1131.22	-4514.98	0.0	0.0	0.0	2.238e+06
25	27	-2.956e+05	0.0	-0.10	-556.88	0.0	-4859.97	1.631e+04	0.0	0.0	0.0	-4.960e+05
		-4.960e+05	0.0	0.0	0.0	12.5	-4859.97	1.575e+04	0.0	0.0	0.0	-2.956e+05
25	28	1.479e+05	0.0	-0.07	-405.00	0.0	-6061.05	5568.80	0.0	0.0	0.0	8.079e+04
		8.079e+04	0.0	0.0	0.0	12.5	-6061.05	5163.80	0.0	0.0	0.0	1.479e+05
25	29	2.618e+06	0.0	0.35	-405.00	0.0	-619.01	-6224.35	0.0	0.0	0.0	2.618e+06
		2.538e+06	0.0	0.0	0.0	12.5	-1003.76	-6629.35	0.0	0.0	0.0	2.538e+06
25	30	1.515e+06	0.0	0.21	-413.63	0.0	1004.91	7103.51	0.0	0.0	0.0	1.429e+06
		1.429e+06	0.0	0.0	0.0	12.5	620.16	6689.89	0.0	0.0	0.0	1.515e+06
25	31	1.615e+06	0.0	-0.17	-300.00	0.0	-1686.32	-3717.48	0.0	0.0	0.0	1.615e+06
		1.566e+06	0.0	0.0	0.0	12.5	-2071.07	-4017.48	0.0	0.0	0.0	1.566e+06
25	32	1.454e+06	0.0	0.20	-300.00	0.0	-5509.01	-3678.78	0.0	0.0	0.0	1.454e+06
		1.406e+06	0.0	0.0	0.0	12.5	-5893.76	-3978.78	0.0	0.0	0.0	1.406e+06
25	33	3.040e+06	0.0	0.34	-405.00	0.0	400.37	-6224.35	0.0	0.0	0.0	3.040e+06
		2.960e+06	0.0	0.0	0.0	12.5	15.62	-6629.35	0.0	0.0	0.0	2.960e+06
25	34	-7.660e+05	0.0	-5.08e-03	-384.38	0.0	-3808.41	1.401e+04	0.0	0.0	0.0	-9.386e+05
		-9.386e+05	0.0	0.0	0.0	12.5	-3808.41	1.362e+04	0.0	0.0	0.0	-7.660e+05
25	35	-4.581e+05	0.0	-0.01	-300.00	0.0	-4641.84	5249.45	0.0	0.0	0.0	-5.219e+05
		-5.219e+05	0.0	0.0	0.0	12.5	-4641.84	4949.45	0.0	0.0	0.0	-4.581e+05
25	36	-3.632e+05	0.0	-0.03	-384.38	0.0	-4114.97	1.321e+04	0.0	0.0	0.0	-5.260e+05
		-5.260e+05	0.0	0.0	0.0	12.5	-4114.97	1.283e+04	0.0	0.0	0.0	-3.632e+05
25	37	-5.538e+04	0.0	-0.04	-300.00	0.0	-4948.41	4456.93	0.0	0.0	0.0	-1.092e+05
		-1.092e+05	0.0	0.0	0.0	12.5	-4948.41	4156.93	0.0	0.0	0.0	-5.538e+04
25	38	2.613e+05	0.0	-0.09	-300.00	0.0	-6367.72	2886.85	0.0	0.0	0.0	2.271e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		2.271e+05	0.0	0.0	0.0	12.5	-6367.72	2586.85	0.0	0.0	0.0	2.613e+05
25	39	-5.333e+05	0.0	-3.71e-03	-384.38	0.0	-3304.24	1.401e+04	0.0	0.0	0.0	-7.060e+05
		-7.060e+05	0.0	0.0	0.0	12.5	-3304.24	1.362e+04	0.0	0.0	0.0	-5.333e+05
25	40	-3.056e+05	0.0	-7.67e-04	-300.00	0.0	-2972.67	6000.00	0.0	0.0	0.0	-3.787e+05
		-3.787e+05	0.0	0.0	0.0	12.5	-2972.67	5700.00	0.0	0.0	0.0	-3.056e+05
25	41	-5.959e+05	0.0	-0.03	-384.38	0.0	-4619.14	1.321e+04	0.0	0.0	0.0	-7.586e+05
		-7.586e+05	0.0	0.0	0.0	12.5	-4619.14	1.283e+04	0.0	0.0	0.0	-5.959e+05
25	42	-2.880e+05	0.0	-0.04	-300.00	0.0	-5452.57	4456.93	0.0	0.0	0.0	-3.418e+05
		-3.418e+05	0.0	0.0	0.0	12.5	-5452.57	4156.93	0.0	0.0	0.0	-2.880e+05
25	43	2.870e+04	0.0	-0.09	-300.00	0.0	-6871.89	2886.85	0.0	0.0	0.0	-5512.67
		-5512.67	0.0	0.0	0.0	12.5	-6871.89	2586.85	0.0	0.0	0.0	2.870e+04
25	44	-1.577e+05	0.0	-0.12	-384.38	0.0	-7076.22	8292.77	0.0	0.0	0.0	-2.590e+05
		-2.590e+05	0.0	0.0	0.0	12.5	-7076.22	7908.40	0.0	0.0	0.0	-1.577e+05
25	45	-4.390e+04	0.0	-0.09	-300.00	0.0	-7116.37	2886.85	0.0	0.0	0.0	-7.811e+04
		-7.811e+04	0.0	0.0	0.0	12.5	-7116.37	2586.85	0.0	0.0	0.0	-4.390e+04
25	46	-7.488e+05	0.0	-5.51e-03	-412.50	0.0	-3717.26	1.668e+04	0.0	0.0	0.0	-9.547e+05
		-9.547e+05	0.0	0.0	0.0	12.5	-3717.26	1.626e+04	0.0	0.0	0.0	-7.488e+05
25	47	-4.452e+05	0.0	-1.59e-03	-300.00	0.0	-3275.17	6000.00	0.0	0.0	0.0	-5.183e+05
		-5.183e+05	0.0	0.0	0.0	12.5	-3275.17	5700.00	0.0	0.0	0.0	-4.452e+05
25	48	-7.902e+05	0.0	-4.96e-03	-384.38	0.0	-3889.90	1.401e+04	0.0	0.0	0.0	-9.628e+05
		-9.628e+05	0.0	0.0	0.0	12.5	-3889.90	1.362e+04	0.0	0.0	0.0	-7.902e+05
25	49	-5.624e+05	0.0	-2.02e-03	-300.00	0.0	-3558.33	6000.00	0.0	0.0	0.0	-6.356e+05
		-6.356e+05	0.0	0.0	0.0	12.5	-3558.33	5700.00	0.0	0.0	0.0	-5.624e+05
25	50	1.408e+06	0.0	0.18	-384.38	0.0	1933.89	6044.67	0.0	0.0	0.0	1.335e+06
		1.335e+06	0.0	0.0	0.0	12.5	1648.89	5660.29	0.0	0.0	0.0	1.408e+06
25	51	1.752e+06	0.0	0.19	-300.00	0.0	1100.45	-2712.54	0.0	0.0	0.0	1.752e+06
		1.716e+06	0.0	0.0	0.0	12.5	815.45	-3012.54	0.0	0.0	0.0	1.716e+06
25	52	2.088e+06	0.0	0.24	-300.00	0.0	-318.87	-4282.62	0.0	0.0	0.0	2.088e+06
		2.033e+06	0.0	0.0	0.0	12.5	-603.87	-4582.62	0.0	0.0	0.0	2.033e+06
25	53	-1.772e+05	0.0	-0.03	-384.38	0.0	-3767.68	1.321e+04	0.0	0.0	0.0	-3.400e+05
		-3.400e+05	0.0	0.0	0.0	12.5	-3767.68	1.283e+04	0.0	0.0	0.0	-1.772e+05
25	54	1.307e+05	0.0	-0.04	-300.00	0.0	-4601.12	4456.93	0.0	0.0	0.0	7.683e+04
		7.683e+04	0.0	0.0	0.0	12.5	-4601.12	4156.93	0.0	0.0	0.0	1.307e+05
25	55	4.474e+05	0.0	-0.09	-300.00	0.0	-6020.43	2886.85	0.0	0.0	0.0	4.132e+05
		4.132e+05	0.0	0.0	0.0	12.5	-6020.43	2586.85	0.0	0.0	0.0	4.474e+05
25	56	-6.762e+05	0.0	-5.87e-03	-412.50	0.0	-3472.78	1.668e+04	0.0	0.0	0.0	-8.821e+05
		-8.821e+05	0.0	0.0	0.0	12.5	-3472.78	1.626e+04	0.0	0.0	0.0	-6.762e+05
25	57	-3.726e+05	0.0	-1.95e-03	-300.00	0.0	-3030.69	6000.00	0.0	0.0	0.0	-4.457e+05
		-4.457e+05	0.0	0.0	0.0	12.5	-3030.69	5700.00	0.0	0.0	0.0	-3.726e+05
25	58	-6.692e+05	0.0	-5.56e-03	-384.38	0.0	-3482.43	1.401e+04	0.0	0.0	0.0	-8.418e+05
		-8.418e+05	0.0	0.0	0.0	12.5	-3482.43	1.362e+04	0.0	0.0	0.0	-6.692e+05
25	59	-4.414e+05	0.0	-2.62e-03	-300.00	0.0	-3150.86	6000.00	0.0	0.0	0.0	-5.146e+05
		-5.146e+05	0.0	0.0	0.0	12.5	-3150.86	5700.00	0.0	0.0	0.0	-4.414e+05
25	60	1.406e+06	0.0	0.18	-384.38	0.0	1927.78	6044.67	0.0	0.0	0.0	1.333e+06
		1.333e+06	0.0	0.0	0.0	12.5	1642.78	5660.29	0.0	0.0	0.0	1.406e+06
25	61	1.750e+06	0.0	0.19	-300.00	0.0	1094.34	-2712.54	0.0	0.0	0.0	1.750e+06
		1.714e+06	0.0	0.0	0.0	12.5	809.34	-3012.54	0.0	0.0	0.0	1.714e+06
25	62	2.086e+06	0.0	0.24	-300.00	0.0	-324.97	-4282.62	0.0	0.0	0.0	2.086e+06
		2.031e+06	0.0	0.0	0.0	12.5	-609.97	-4582.62	0.0	0.0	0.0	2.031e+06
25	63	-2.274e+05	0.0	-0.03	-384.38	0.0	-3936.77	1.321e+04	0.0	0.0	0.0	-3.902e+05
		-3.902e+05	0.0	0.0	0.0	12.5	-3936.77	1.283e+04	0.0	0.0	0.0	-2.274e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
25	64	8.046e+04	0.0	-0.04	-300.00	0.0	-4770.21	4456.93	0.0	0.0	0.0	2.662e+04
		2.662e+04	0.0	0.0	0.0	12.5	-4770.21	4156.93	0.0	0.0	0.0	8.046e+04
25	65	3.972e+05	0.0	-0.09	-300.00	0.0	-6189.53	2886.85	0.0	0.0	0.0	3.630e+05
		3.630e+05	0.0	0.0	0.0	12.5	-6189.53	2586.85	0.0	0.0	0.0	3.972e+05
25	66	1.448e+06	0.0	0.21	-384.38	0.0	2055.02	3443.94	0.0	0.0	0.0	1.407e+06
		1.407e+06	0.0	0.0	0.0	12.5	1770.02	3059.56	0.0	0.0	0.0	1.448e+06
25	67	-1.861e+05	0.0	-0.06	-384.38	0.0	-3809.54	1.061e+04	0.0	0.0	0.0	-3.164e+05
		-3.164e+05	0.0	0.0	0.0	12.5	-3809.54	1.023e+04	0.0	0.0	0.0	-1.861e+05
25	68	1.807e+06	0.0	0.24	-300.00	0.0	-929.98	-4282.62	0.0	0.0	0.0	1.807e+06
		1.752e+06	0.0	0.0	0.0	12.5	-1214.98	-4582.62	0.0	0.0	0.0	1.752e+06
25	69	-6.810e+04	0.0	-0.09	-300.00	0.0	-7197.86	2886.85	0.0	0.0	0.0	-1.023e+05
		-1.023e+05	0.0	0.0	0.0	12.5	-7197.86	2586.85	0.0	0.0	0.0	-6.810e+04
25	70	-5.322e+05	0.0	-2.17e-03	-300.00	0.0	-3456.47	6000.00	0.0	0.0	0.0	-6.053e+05
		-6.053e+05	0.0	0.0	0.0	12.5	-3456.47	5700.00	0.0	0.0	0.0	-5.322e+05
25	71	-1.416e+05	0.0	-0.03	-300.00	0.0	-3803.78	5207.48	0.0	0.0	0.0	-2.048e+05
		-2.048e+05	0.0	0.0	0.0	12.5	-3803.78	4907.48	0.0	0.0	0.0	-1.416e+05
25	72	-2.996e+05	0.0	-7.97e-04	-300.00	0.0	-2952.30	6000.00	0.0	0.0	0.0	-3.727e+05
		-3.727e+05	0.0	0.0	0.0	12.5	-2952.30	5700.00	0.0	0.0	0.0	-2.996e+05
25	73	-3.742e+05	0.0	-0.03	-300.00	0.0	-4307.94	5207.48	0.0	0.0	0.0	-4.374e+05
		-4.374e+05	0.0	0.0	0.0	12.5	-4307.94	4907.48	0.0	0.0	0.0	-3.742e+05
25	74	-4.347e+05	0.0	-0.03	-300.00	0.0	-4511.68	5207.48	0.0	0.0	0.0	-4.979e+05
		-4.979e+05	0.0	0.0	0.0	12.5	-4511.68	4907.48	0.0	0.0	0.0	-4.347e+05
26	1	-6.210e+05	0.0	-7.93e-03	-556.88	0.0	-3790.57	2.196e+04	0.0	0.0	0.0	-8.920e+05
		-8.920e+05	0.0	0.0	0.0	12.5	-3790.57	2.140e+04	0.0	0.0	0.0	-6.210e+05
26	2	-3.884e+05	0.0	-2.54e-03	-405.00	0.0	-3193.75	7695.00	0.0	0.0	0.0	-4.821e+05
		-4.821e+05	0.0	0.0	0.0	12.5	-3193.75	7290.00	0.0	0.0	0.0	-3.884e+05
26	3	-7.032e+05	0.0	-7.06e-03	-518.63	0.0	-3980.06	1.836e+04	0.0	0.0	0.0	-9.295e+05
		-9.295e+05	0.0	0.0	0.0	12.5	-3980.06	1.785e+04	0.0	0.0	0.0	-7.032e+05
26	4	-5.291e+05	0.0	-3.02e-03	-405.00	0.0	-3533.55	7695.00	0.0	0.0	0.0	-6.228e+05
		-6.228e+05	0.0	0.0	0.0	12.5	-3533.55	7290.00	0.0	0.0	0.0	-5.291e+05
26	5	2.120e+06	0.0	0.26	-518.63	0.0	2763.28	7164.44	0.0	0.0	0.0	2.034e+06
		2.034e+06	0.0	0.0	0.0	12.5	2378.53	6645.81	0.0	0.0	0.0	2.120e+06
26	6	2.449e+06	0.0	0.27	-405.00	0.0	1640.91	-4514.98	0.0	0.0	0.0	2.449e+06
		2.390e+06	0.0	0.0	0.0	12.5	1256.16	-4919.98	0.0	0.0	0.0	2.390e+06
26	7	2.875e+06	0.0	0.34	-405.00	0.0	-270.43	-6629.35	0.0	0.0	0.0	2.875e+06
		2.790e+06	0.0	0.0	0.0	12.5	-655.18	-7034.35	0.0	0.0	0.0	2.790e+06
26	8	8.347e+04	0.0	-0.06	-518.63	0.0	-4591.56	1.684e+04	0.0	0.0	0.0	-1.238e+05
		-1.238e+05	0.0	0.0	0.0	12.5	-4591.56	1.632e+04	0.0	0.0	0.0	8.347e+04
26	9	3.528e+05	0.0	-0.06	-405.00	0.0	-5713.93	5163.80	0.0	0.0	0.0	2.907e+05
		2.907e+05	0.0	0.0	0.0	12.5	-5713.93	4758.80	0.0	0.0	0.0	3.528e+05
26	10	7.528e+05	0.0	-0.14	-405.00	0.0	-7625.27	3049.43	0.0	0.0	0.0	7.172e+05
		7.172e+05	0.0	0.0	0.0	12.5	-7625.27	2644.43	0.0	0.0	0.0	7.528e+05
26	11	-6.189e+05	0.0	-7.94e-03	-556.88	0.0	-3783.25	2.196e+04	0.0	0.0	0.0	-8.898e+05
		-8.898e+05	0.0	0.0	0.0	12.5	-3783.25	2.140e+04	0.0	0.0	0.0	-6.189e+05
26	12	-3.862e+05	0.0	-2.55e-03	-405.00	0.0	-3186.43	7695.00	0.0	0.0	0.0	-4.799e+05
		-4.799e+05	0.0	0.0	0.0	12.5	-3186.43	7290.00	0.0	0.0	0.0	-3.862e+05
26	13	-8.458e+04	0.0	-4.23e-03	-518.63	0.0	-2567.14	1.836e+04	0.0	0.0	0.0	-3.109e+05
		-3.109e+05	0.0	0.0	0.0	12.5	-2567.14	1.785e+04	0.0	0.0	0.0	-8.458e+04
26	14	8.945e+04	0.0	-1.89e-04	-405.00	0.0	-2120.63	7695.00	0.0	0.0	0.0	-4210.17
		-4210.17	0.0	0.0	0.0	12.5	-2120.63	7290.00	0.0	0.0	0.0	8.945e+04
26	15	1.783e+06	0.0	0.26	-518.63	0.0	2029.95	7164.44	0.0	0.0	0.0	1.697e+06

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		1.697e+06	0.0	0.0	0.0	12.5	1645.20	6645.81	0.0	0.0	0.0	1.783e+06
26	16	2.111e+06	0.0	0.27	-405.00	0.0	907.58	-4514.98	0.0	0.0	0.0	2.111e+06
		2.053e+06	0.0	0.0	0.0	12.5	522.83	-4919.98	0.0	0.0	0.0	2.053e+06
26	17	2.538e+06	0.0	0.34	-405.00	0.0	-1003.76	-6629.35	0.0	0.0	0.0	2.538e+06
		2.453e+06	0.0	0.0	0.0	12.5	-1388.51	-7034.35	0.0	0.0	0.0	2.453e+06
26	18	2.321e+04	0.0	-0.06	-518.63	0.0	-4794.48	1.684e+04	0.0	0.0	0.0	-1.841e+05
		-1.841e+05	0.0	0.0	0.0	12.5	-4794.48	1.632e+04	0.0	0.0	0.0	2.321e+04
26	19	2.925e+05	0.0	-0.06	-405.00	0.0	-5916.84	5163.80	0.0	0.0	0.0	2.305e+05
		2.305e+05	0.0	0.0	0.0	12.5	-5916.84	4758.80	0.0	0.0	0.0	2.925e+05
26	20	6.926e+05	0.0	-0.14	-405.00	0.0	-7828.18	3049.43	0.0	0.0	0.0	6.570e+05
		6.570e+05	0.0	0.0	0.0	12.5	-7828.18	2644.43	0.0	0.0	0.0	6.926e+05
26	21	2.130e+06	0.0	0.30	-518.63	0.0	2927.30	3662.12	0.0	0.0	0.0	2.088e+06
		2.088e+06	0.0	0.0	0.0	12.5	2542.55	3143.50	0.0	0.0	0.0	2.130e+06
26	22	3.506e+04	0.0	-0.09	-518.63	0.0	-4623.13	1.334e+04	0.0	0.0	0.0	-1.285e+05
		-1.285e+05	0.0	0.0	0.0	12.5	-4623.13	1.282e+04	0.0	0.0	0.0	3.506e+04
26	23	2.554e+06	0.0	0.34	-300.00	0.0	-1122.45	-8624.35	0.0	0.0	0.0	2.554e+06
		2.444e+06	0.0	0.0	0.0	12.5	-1507.20	-8924.35	0.0	0.0	0.0	2.444e+06
26	24	1.259e+05	0.0	0.14	-300.00	0.0	-9156.88	1054.43	0.0	0.0	0.0	1.146e+05
		1.146e+05	0.0	0.0	0.0	12.5	-9156.88	754.43	0.0	0.0	0.0	1.259e+05
26	25	2.056e+06	0.0	0.23	-518.63	0.0	2424.93	1.067e+04	0.0	0.0	0.0	1.926e+06
		1.926e+06	0.0	0.0	0.0	12.5	2040.18	1.015e+04	0.0	0.0	0.0	2.056e+06
26	26	2.238e+06	0.0	0.27	-405.00	0.0	1131.22	-4514.98	0.0	0.0	0.0	2.238e+06
		2.179e+06	0.0	0.0	0.0	12.5	746.47	-4919.98	0.0	0.0	0.0	2.179e+06
26	27	-1.022e+05	0.0	-0.10	-556.88	0.0	-4859.97	1.575e+04	0.0	0.0	0.0	-2.956e+05
		-2.956e+05	0.0	0.0	0.0	12.5	-4859.97	1.520e+04	0.0	0.0	0.0	-1.022e+05
26	28	2.099e+05	0.0	-0.07	-405.00	0.0	-6061.05	5163.80	0.0	0.0	0.0	1.479e+05
		1.479e+05	0.0	0.0	0.0	12.5	-6061.05	4758.80	0.0	0.0	0.0	2.099e+05
26	29	2.538e+06	0.0	0.34	-405.00	0.0	-1003.76	-6629.35	0.0	0.0	0.0	2.538e+06
		2.453e+06	0.0	0.0	0.0	12.5	-1388.51	-7034.35	0.0	0.0	0.0	2.453e+06
26	30	1.596e+06	0.0	0.21	-413.63	0.0	620.16	6689.89	0.0	0.0	0.0	1.515e+06
		1.515e+06	0.0	0.0	0.0	12.5	235.41	6276.26	0.0	0.0	0.0	1.596e+06
26	31	1.566e+06	0.0	-0.17	-300.00	0.0	-2071.07	-4017.48	0.0	0.0	0.0	1.566e+06
		1.514e+06	0.0	0.0	0.0	12.5	-2455.82	-4317.48	0.0	0.0	0.0	1.514e+06
26	32	1.406e+06	0.0	0.20	-300.00	0.0	-5893.76	-3978.78	0.0	0.0	0.0	1.406e+06
		1.354e+06	0.0	0.0	0.0	12.5	-6278.51	-4278.78	0.0	0.0	0.0	1.354e+06
26	33	2.960e+06	0.0	0.34	-405.00	0.0	15.62	-6629.35	0.0	0.0	0.0	2.960e+06
		2.875e+06	0.0	0.0	0.0	12.5	-369.13	-7034.35	0.0	0.0	0.0	2.875e+06
26	34	-5.981e+05	0.0	-5.14e-03	-384.38	0.0	-3808.41	1.362e+04	0.0	0.0	0.0	-7.660e+05
		-7.660e+05	0.0	0.0	0.0	12.5	-3808.41	1.324e+04	0.0	0.0	0.0	-5.981e+05
26	35	-3.981e+05	0.0	-0.01	-300.00	0.0	-4641.84	4949.45	0.0	0.0	0.0	-4.581e+05
		-4.581e+05	0.0	0.0	0.0	12.5	-4641.84	4649.45	0.0	0.0	0.0	-3.981e+05
26	36	-2.053e+05	0.0	-0.03	-384.38	0.0	-4114.97	1.283e+04	0.0	0.0	0.0	-3.632e+05
		-3.632e+05	0.0	0.0	0.0	12.5	-4114.97	1.245e+04	0.0	0.0	0.0	-2.053e+05
26	37	-5289.52	0.0	-0.04	-300.00	0.0	-4948.41	4156.93	0.0	0.0	0.0	-5.538e+04
		-5.538e+04	0.0	0.0	0.0	12.5	-4948.41	3856.93	0.0	0.0	0.0	-5289.52
26	38	2.918e+05	0.0	-0.09	-300.00	0.0	-6367.72	2586.85	0.0	0.0	0.0	2.613e+05
		2.613e+05	0.0	0.0	0.0	12.5	-6367.72	2286.85	0.0	0.0	0.0	2.918e+05
26	39	-3.655e+05	0.0	-3.84e-03	-384.38	0.0	-3304.24	1.362e+04	0.0	0.0	0.0	-5.333e+05
		-5.333e+05	0.0	0.0	0.0	12.5	-3304.24	1.324e+04	0.0	0.0	0.0	-3.655e+05
26	40	-2.362e+05	0.0	-8.41e-04	-300.00	0.0	-2972.67	5700.00	0.0	0.0	0.0	-3.056e+05
		-3.056e+05	0.0	0.0	0.0	12.5	-2972.67	5400.00	0.0	0.0	0.0	-2.362e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
26	41	-4.379e+05	0.0	-0.03	-384.38	0.0	-4619.14	1.283e+04	0.0	0.0	0.0	-5.959e+05
		-5.959e+05	0.0	0.0	0.0	12.5	-4619.14	1.245e+04	0.0	0.0	0.0	-4.379e+05
26	42	-2.379e+05	0.0	-0.04	-300.00	0.0	-5452.57	4156.93	0.0	0.0	0.0	-2.880e+05
		-2.880e+05	0.0	0.0	0.0	12.5	-5452.57	3856.93	0.0	0.0	0.0	-2.379e+05
26	43	5.916e+04	0.0	-0.09	-300.00	0.0	-6871.89	2586.85	0.0	0.0	0.0	2.870e+04
		2.870e+04	0.0	0.0	0.0	12.5	-6871.89	2286.85	0.0	0.0	0.0	5.916e+04
26	44	-6.127e+04	0.0	-0.12	-384.38	0.0	-7076.22	7908.40	0.0	0.0	0.0	-1.577e+05
		-1.577e+05	0.0	0.0	0.0	12.5	-7076.22	7524.02	0.0	0.0	0.0	-6.127e+04
26	45	-1.344e+04	0.0	-0.09	-300.00	0.0	-7116.37	2586.85	0.0	0.0	0.0	-4.390e+04
		-4.390e+04	0.0	0.0	0.0	12.5	-7116.37	2286.85	0.0	0.0	0.0	-1.344e+04
26	46	-5.481e+05	0.0	-5.62e-03	-412.50	0.0	-3717.26	1.626e+04	0.0	0.0	0.0	-7.488e+05
		-7.488e+05	0.0	0.0	0.0	12.5	-3717.26	1.585e+04	0.0	0.0	0.0	-5.481e+05
26	47	-3.758e+05	0.0	-1.62e-03	-300.00	0.0	-3275.17	5700.00	0.0	0.0	0.0	-4.452e+05
		-4.452e+05	0.0	0.0	0.0	12.5	-3275.17	5400.00	0.0	0.0	0.0	-3.758e+05
26	48	-6.223e+05	0.0	-5.02e-03	-384.38	0.0	-3889.90	1.362e+04	0.0	0.0	0.0	-7.902e+05
		-7.902e+05	0.0	0.0	0.0	12.5	-3889.90	1.324e+04	0.0	0.0	0.0	-6.223e+05
26	49	-4.931e+05	0.0	-2.03e-03	-300.00	0.0	-3558.33	5700.00	0.0	0.0	0.0	-5.624e+05
		-5.624e+05	0.0	0.0	0.0	12.5	-3558.33	5400.00	0.0	0.0	0.0	-4.931e+05
26	50	1.477e+06	0.0	0.18	-384.38	0.0	1648.89	5660.29	0.0	0.0	0.0	1.408e+06
		1.408e+06	0.0	0.0	0.0	12.5	1363.89	5275.92	0.0	0.0	0.0	1.477e+06
26	51	1.716e+06	0.0	0.19	-300.00	0.0	815.45	-3012.54	0.0	0.0	0.0	1.716e+06
		1.677e+06	0.0	0.0	0.0	12.5	530.45	-3312.54	0.0	0.0	0.0	1.677e+06
26	52	2.033e+06	0.0	0.24	-300.00	0.0	-603.87	-4582.62	0.0	0.0	0.0	2.033e+06
		1.974e+06	0.0	0.0	0.0	12.5	-888.87	-4882.62	0.0	0.0	0.0	1.974e+06
26	53	-1.922e+04	0.0	-0.03	-384.38	0.0	-3767.68	1.283e+04	0.0	0.0	0.0	-1.772e+05
		-1.772e+05	0.0	0.0	0.0	12.5	-3767.68	1.245e+04	0.0	0.0	0.0	-1.922e+04
26	54	1.808e+05	0.0	-0.04	-300.00	0.0	-4601.12	4156.93	0.0	0.0	0.0	1.307e+05
		1.307e+05	0.0	0.0	0.0	12.5	-4601.12	3856.93	0.0	0.0	0.0	1.808e+05
26	55	4.778e+05	0.0	-0.09	-300.00	0.0	-6020.43	2586.85	0.0	0.0	0.0	4.474e+05
		4.474e+05	0.0	0.0	0.0	12.5	-6020.43	2286.85	0.0	0.0	0.0	4.778e+05
26	56	-4.755e+05	0.0	-5.96e-03	-412.50	0.0	-3472.78	1.626e+04	0.0	0.0	0.0	-6.762e+05
		-6.762e+05	0.0	0.0	0.0	12.5	-3472.78	1.585e+04	0.0	0.0	0.0	-4.755e+05
26	57	-3.032e+05	0.0	-1.97e-03	-300.00	0.0	-3030.69	5700.00	0.0	0.0	0.0	-3.726e+05
		-3.726e+05	0.0	0.0	0.0	12.5	-3030.69	5400.00	0.0	0.0	0.0	-3.032e+05
26	58	-5.013e+05	0.0	-5.60e-03	-384.38	0.0	-3482.43	1.362e+04	0.0	0.0	0.0	-6.692e+05
		-6.692e+05	0.0	0.0	0.0	12.5	-3482.43	1.324e+04	0.0	0.0	0.0	-5.013e+05
26	59	-3.721e+05	0.0	-2.60e-03	-300.00	0.0	-3150.86	5700.00	0.0	0.0	0.0	-4.414e+05
		-4.414e+05	0.0	0.0	0.0	12.5	-3150.86	5400.00	0.0	0.0	0.0	-3.721e+05
26	60	1.475e+06	0.0	0.18	-384.38	0.0	1642.78	5660.29	0.0	0.0	0.0	1.406e+06
		1.406e+06	0.0	0.0	0.0	12.5	1357.78	5275.92	0.0	0.0	0.0	1.475e+06
26	61	1.714e+06	0.0	0.19	-300.00	0.0	809.34	-3012.54	0.0	0.0	0.0	1.714e+06
		1.675e+06	0.0	0.0	0.0	12.5	524.34	-3312.54	0.0	0.0	0.0	1.675e+06
26	62	2.031e+06	0.0	0.24	-300.00	0.0	-609.97	-4582.62	0.0	0.0	0.0	2.031e+06
		1.972e+06	0.0	0.0	0.0	12.5	-894.97	-4882.62	0.0	0.0	0.0	1.972e+06
26	63	-6.943e+04	0.0	-0.03	-384.38	0.0	-3936.77	1.283e+04	0.0	0.0	0.0	-2.274e+05
		-2.274e+05	0.0	0.0	0.0	12.5	-3936.77	1.245e+04	0.0	0.0	0.0	-6.943e+04
26	64	1.305e+05	0.0	-0.04	-300.00	0.0	-4770.21	4156.93	0.0	0.0	0.0	8.046e+04
		8.046e+04	0.0	0.0	0.0	12.5	-4770.21	3856.93	0.0	0.0	0.0	1.305e+05
26	65	4.276e+05	0.0	-0.09	-300.00	0.0	-6189.53	2586.85	0.0	0.0	0.0	3.972e+05
		3.972e+05	0.0	0.0	0.0	12.5	-6189.53	2286.85	0.0	0.0	0.0	4.276e+05
26	66	1.484e+06	0.0	0.21	-384.38	0.0	1770.02	3059.56	0.0	0.0	0.0	1.448e+06

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		1.448e+06	0.0	0.0	0.0	12.5	1485.02	2675.19	0.0	0.0	0.0	1.484e+06
26	67	-6.063e+04	0.0	-0.06	-384.38	0.0	-3809.54	1.023e+04	0.0	0.0	0.0	-1.861e+05
		-1.861e+05	0.0	0.0	0.0	12.5	-3809.54	9844.65	0.0	0.0	0.0	-6.063e+04
26	68	1.752e+06	0.0	0.24	-300.00	0.0	-1214.98	-4582.62	0.0	0.0	0.0	1.752e+06
		1.693e+06	0.0	0.0	0.0	12.5	-1499.98	-4882.62	0.0	0.0	0.0	1.693e+06
26	69	-3.764e+04	0.0	-0.09	-300.00	0.0	-7197.86	2586.85	0.0	0.0	0.0	-6.810e+04
		-6.810e+04	0.0	0.0	0.0	12.5	-7197.86	2286.85	0.0	0.0	0.0	-3.764e+04
26	70	-4.628e+05	0.0	-2.17e-03	-300.00	0.0	-3456.47	5700.00	0.0	0.0	0.0	-5.322e+05
		-5.322e+05	0.0	0.0	0.0	12.5	-3456.47	5400.00	0.0	0.0	0.0	-4.628e+05
26	71	-8.209e+04	0.0	-0.03	-300.00	0.0	-3803.78	4907.48	0.0	0.0	0.0	-1.416e+05
		-1.416e+05	0.0	0.0	0.0	12.5	-3803.78	4607.48	0.0	0.0	0.0	-8.209e+04
26	72	-2.302e+05	0.0	-8.70e-04	-300.00	0.0	-2952.30	5700.00	0.0	0.0	0.0	-2.996e+05
		-2.996e+05	0.0	0.0	0.0	12.5	-2952.30	5400.00	0.0	0.0	0.0	-2.302e+05
26	73	-3.147e+05	0.0	-0.03	-300.00	0.0	-4307.94	4907.48	0.0	0.0	0.0	-3.742e+05
		-3.742e+05	0.0	0.0	0.0	12.5	-4307.94	4607.48	0.0	0.0	0.0	-3.147e+05
26	74	-3.752e+05	0.0	-0.03	-300.00	0.0	-4511.68	4907.48	0.0	0.0	0.0	-4.347e+05
		-4.347e+05	0.0	0.0	0.0	12.5	-4511.68	4607.48	0.0	0.0	0.0	-3.752e+05
27	1	2.358e+06	0.0	-0.09	-2.140e+04	0.0	-3790.57	2.140e+04	0.0	0.0	0.0	-6.210e+05
		-6.210e+05	0.0	0.0	0.0	225.0	-3790.57	-5.27e-04	0.0	0.0	0.0	2.358e+06
27	2	4.317e+05	0.0	-0.03	-7290.00	0.0	-3193.75	7290.00	0.0	0.0	0.0	-3.884e+05
		-3.884e+05	0.0	0.0	0.0	225.0	-3193.75	0.0	0.0	0.0	0.0	4.317e+05
27	3	1.732e+06	0.0	-0.08	-1.785e+04	0.0	-3980.06	1.785e+04	0.0	0.0	0.0	-7.032e+05
		-7.032e+05	0.0	0.0	0.0	225.0	-3980.06	-3.95e-04	0.0	0.0	0.0	1.732e+06
27	4	2.910e+05	0.0	-0.03	-7290.00	0.0	-3533.55	7290.00	0.0	0.0	0.0	-5.291e+05
		-5.291e+05	0.0	0.0	0.0	225.0	-3533.55	0.0	0.0	0.0	0.0	2.910e+05
27	5	2.606e+06	0.0	-4.61	-1.785e+04	0.0	2378.53	6645.81	0.0	0.0	0.0	2.120e+06
		2.036e+06	0.0	0.0	0.0	225.0	-4546.97	-1.120e+04	0.0	0.0	0.0	2.036e+06
27	6	2.390e+06	0.0	-4.79	-7290.00	0.0	1256.16	-4919.98	0.0	0.0	0.0	2.390e+06
		4.626e+05	0.0	0.0	0.0	225.0	-5669.34	-1.221e+04	0.0	0.0	0.0	4.626e+05
27	7	2.790e+06	0.0	6.09	-7290.00	0.0	-655.18	-7034.35	0.0	0.0	0.0	2.790e+06
		3.869e+05	0.0	0.0	0.0	225.0	-7580.68	-1.432e+04	0.0	0.0	0.0	3.869e+05
27	8	2.187e+06	0.0	-0.99	-1.785e+04	0.0	-4591.56	1.632e+04	0.0	0.0	0.0	8.347e+04
		8.347e+04	0.0	0.0	0.0	225.0	-4591.56	-1520.45	0.0	0.0	0.0	2.177e+06
27	9	7.016e+05	0.0	-1.17	-7290.00	0.0	-5713.93	4758.80	0.0	0.0	0.0	3.528e+05
		3.528e+05	0.0	0.0	0.0	225.0	-5713.93	-2531.20	0.0	0.0	0.0	6.034e+05
27	10	8.606e+05	0.0	-2.47	-7290.00	0.0	-7625.27	2644.43	0.0	0.0	0.0	7.528e+05
		5.277e+05	0.0	0.0	0.0	225.0	-7625.27	-4645.57	0.0	0.0	0.0	5.277e+05
27	11	2.360e+06	0.0	-0.09	-2.140e+04	0.0	-3783.25	2.140e+04	0.0	0.0	0.0	-6.189e+05
		-6.189e+05	0.0	0.0	0.0	225.0	-3783.25	-5.27e-04	0.0	0.0	0.0	2.360e+06
27	12	4.339e+05	0.0	-0.03	-7290.00	0.0	-3186.43	7290.00	0.0	0.0	0.0	-3.862e+05
		-3.862e+05	0.0	0.0	0.0	225.0	-3186.43	0.0	0.0	0.0	0.0	4.339e+05
27	13	2.351e+06	0.0	-0.06	-1.785e+04	0.0	-2567.14	1.785e+04	0.0	0.0	0.0	-8.458e+04
		-8.458e+04	0.0	0.0	0.0	225.0	-2567.14	-3.95e-04	0.0	0.0	0.0	2.351e+06
27	14	9.096e+05	0.0	-8.01e-03	-7290.00	0.0	-2120.63	7290.00	0.0	0.0	0.0	8.945e+04
		8.945e+04	0.0	0.0	0.0	225.0	-2120.63	0.0	0.0	0.0	0.0	9.096e+05
27	15	2.269e+06	0.0	-4.62	-1.785e+04	0.0	1645.20	6645.81	0.0	0.0	0.0	1.783e+06
		1.699e+06	0.0	0.0	0.0	225.0	-5280.30	-1.120e+04	0.0	0.0	0.0	1.699e+06
27	16	2.053e+06	0.0	-4.80	-7290.00	0.0	522.83	-4919.98	0.0	0.0	0.0	2.053e+06
		1.254e+05	0.0	0.0	0.0	225.0	-6402.67	-1.221e+04	0.0	0.0	0.0	1.254e+05
27	17	2.453e+06	0.0	6.11	-7290.00	0.0	-1388.51	-7034.35	0.0	0.0	0.0	2.453e+06
		4.972e+04	0.0	0.0	0.0	225.0	-8314.01	-1.432e+04	0.0	0.0	0.0	4.972e+04

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
27	18	2.127e+06	0.0	-0.98	-1.785e+04	0.0	-4794.48	1.632e+04	0.0	0.0	0.0	2.321e+04
		2.321e+04	0.0	0.0	0.0	225.0	-4794.48	-1520.45	0.0	0.0	0.0	2.116e+06
27	19	6.414e+05	0.0	-1.17	-7290.00	0.0	-5916.84	4758.80	0.0	0.0	0.0	2.925e+05
		2.925e+05	0.0	0.0	0.0	225.0	-5916.84	-2531.20	0.0	0.0	0.0	5.431e+05
27	20	8.004e+05	0.0	-2.47	-7290.00	0.0	-7828.18	2644.43	0.0	0.0	0.0	6.926e+05
		4.674e+05	0.0	0.0	0.0	225.0	-7828.18	-4645.57	0.0	0.0	0.0	4.674e+05
27	21	2.249e+06	0.0	-5.24	-1.098e+04	0.0	2542.55	3143.50	0.0	0.0	0.0	2.130e+06
		1.767e+06	0.0	0.0	0.0	225.0	-4382.95	-7832.20	0.0	0.0	0.0	1.767e+06
27	22	1.850e+06	0.0	-1.62	-1.098e+04	0.0	-4623.13	1.282e+04	0.0	0.0	0.0	3.506e+04
		3.506e+04	0.0	0.0	0.0	225.0	-4623.13	1846.59	0.0	0.0	0.0	1.850e+06
27	23	2.444e+06	0.0	6.10	-5400.00	0.0	-1507.20	-8924.35	0.0	0.0	0.0	2.444e+06
		-1.713e+05	0.0	0.0	0.0	225.0	-8432.70	-1.432e+04	0.0	0.0	0.0	-1.713e+05
27	24	1.376e+05	0.0	-2.49	-5400.00	0.0	-9156.88	754.43	0.0	0.0	0.0	1.259e+05
		-3.119e+05	0.0	0.0	0.0	225.0	-9156.88	-4645.57	0.0	0.0	0.0	-3.119e+05
27	25	2.522e+06	0.0	-3.96	-2.471e+04	0.0	2040.18	1.015e+04	0.0	0.0	0.0	2.056e+06
		1.559e+06	0.0	0.0	0.0	225.0	-4885.32	-1.457e+04	0.0	0.0	0.0	1.559e+06
27	26	2.179e+06	0.0	-4.79	-7290.00	0.0	746.47	-4919.98	0.0	0.0	0.0	2.179e+06
		2.515e+05	0.0	0.0	0.0	225.0	-6179.03	-1.221e+04	0.0	0.0	0.0	2.515e+05
27	27	2.163e+06	0.0	-1.86	-1.222e+04	0.0	-4859.97	1.520e+04	0.0	0.0	0.0	-1.022e+05
		-1.022e+05	0.0	0.0	0.0	225.0	-4859.97	2980.04	0.0	0.0	0.0	2.163e+06
27	28	5.587e+05	0.0	-1.17	-7290.00	0.0	-6061.05	4758.80	0.0	0.0	0.0	2.099e+05
		2.099e+05	0.0	0.0	0.0	225.0	-6061.05	-2531.20	0.0	0.0	0.0	4.605e+05
27	29	2.453e+06	0.0	6.11	-7290.00	0.0	-1388.51	-7034.35	0.0	0.0	0.0	2.453e+06
		4.972e+04	0.0	0.0	0.0	225.0	-8314.01	-1.432e+04	0.0	0.0	0.0	4.972e+04
27	30	2.102e+06	0.0	-3.66	-1.596e+04	0.0	235.41	6276.26	0.0	0.0	0.0	1.596e+06
		1.596e+06	0.0	0.0	0.0	225.0	-6690.09	-9678.78	0.0	0.0	0.0	1.641e+06
27	31	1.514e+06	0.0	-3.03	-5400.00	0.0	-2455.82	-4317.48	0.0	0.0	0.0	1.514e+06
		-6.467e+04	0.0	0.0	0.0	225.0	-9381.32	-9717.48	0.0	0.0	0.0	-6.467e+04
27	32	1.354e+06	0.0	-3.59	-5400.00	0.0	-6278.51	-4278.78	0.0	0.0	0.0	1.354e+06
		-2.160e+05	0.0	0.0	0.0	225.0	-1.320e+04	-9678.78	0.0	0.0	0.0	-2.160e+05
27	33	2.875e+06	0.0	6.09	-7290.00	0.0	-369.13	-7034.35	0.0	0.0	0.0	2.875e+06
		4.718e+05	0.0	0.0	0.0	225.0	-7294.63	-1.432e+04	0.0	0.0	0.0	4.718e+05
27	34	1.209e+06	0.0	-0.06	-1.324e+04	0.0	-3808.41	1.324e+04	0.0	0.0	0.0	-5.981e+05
		-5.981e+05	0.0	0.0	0.0	225.0	-3808.41	-2.93e-04	0.0	0.0	0.0	1.209e+06
27	35	5.213e+04	0.0	-0.19	-5400.00	0.0	-4641.84	4649.45	0.0	0.0	0.0	-3.981e+05
		-3.981e+05	0.0	0.0	0.0	225.0	-4641.84	-750.55	0.0	0.0	0.0	4.051e+04
27	36	1.426e+06	0.0	-0.54	-1.324e+04	0.0	-4114.97	1.245e+04	0.0	0.0	0.0	-2.053e+05
		-2.053e+05	0.0	0.0	0.0	225.0	-4114.97	-792.52	0.0	0.0	0.0	1.423e+06
27	37	3.042e+05	0.0	-0.67	-5400.00	0.0	-4948.41	3856.93	0.0	0.0	0.0	-5289.52
		-5289.52	0.0	0.0	0.0	225.0	-4948.41	-1543.07	0.0	0.0	0.0	2.550e+05
27	38	4.006e+05	0.0	-1.64	-5400.00	0.0	-6367.72	2286.85	0.0	0.0	0.0	2.918e+05
		1.988e+05	0.0	0.0	0.0	225.0	-6367.72	-3113.15	0.0	0.0	0.0	1.988e+05
27	39	1.441e+06	0.0	-0.05	-1.324e+04	0.0	-3304.24	1.324e+04	0.0	0.0	0.0	-3.655e+05
		-3.655e+05	0.0	0.0	0.0	225.0	-3304.24	-2.93e-04	0.0	0.0	0.0	1.441e+06
27	40	3.713e+05	0.0	-0.01	-5400.00	0.0	-2972.67	5400.00	0.0	0.0	0.0	-2.362e+05
		-2.362e+05	0.0	0.0	0.0	225.0	-2972.67	0.0	0.0	0.0	0.0	3.713e+05
27	41	1.194e+06	0.0	-0.55	-1.324e+04	0.0	-4619.14	1.245e+04	0.0	0.0	0.0	-4.379e+05
		-4.379e+05	0.0	0.0	0.0	225.0	-4619.14	-792.52	0.0	0.0	0.0	1.191e+06
27	42	7.156e+04	0.0	-0.68	-5400.00	0.0	-5452.57	3856.93	0.0	0.0	0.0	-2.379e+05
		-2.379e+05	0.0	0.0	0.0	225.0	-5452.57	-1543.07	0.0	0.0	0.0	2.239e+04
27	43	1.680e+05	0.0	-1.65	-5400.00	0.0	-6871.89	2286.85	0.0	0.0	0.0	5.916e+04

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-3.380e+04	0.0	0.0	0.0	225.0	-6871.89	-3113.15	0.0	0.0	0.0	-3.380e+04
27	44	8.392e+05	0.0	-2.16	-8136.90	0.0	-7076.22	7524.02	0.0	0.0	0.0	-6.127e+04
		-6.127e+04	0.0	0.0	0.0	225.0	-7076.22	-612.88	0.0	0.0	0.0	8.387e+05
27	45	9.539e+04	0.0	-1.65	-5400.00	0.0	-7116.37	2286.85	0.0	0.0	0.0	-1.344e+04
		-1.064e+05	0.0	0.0	0.0	225.0	-7116.37	-3113.15	0.0	0.0	0.0	-1.064e+05
27	46	1.658e+06	0.0	-0.07	-1.585e+04	0.0	-3717.26	1.585e+04	0.0	0.0	0.0	-5.481e+05
		-5.481e+05	0.0	0.0	0.0	225.0	-3717.26	-3.91e-04	0.0	0.0	0.0	1.658e+06
27	47	2.317e+05	0.0	-0.02	-5400.00	0.0	-3275.17	5400.00	0.0	0.0	0.0	-3.758e+05
		-3.758e+05	0.0	0.0	0.0	225.0	-3275.17	0.0	0.0	0.0	0.0	2.317e+05
27	48	1.185e+06	0.0	-0.06	-1.324e+04	0.0	-3889.90	1.324e+04	0.0	0.0	0.0	-6.223e+05
		-6.223e+05	0.0	0.0	0.0	225.0	-3889.90	-2.93e-04	0.0	0.0	0.0	1.185e+06
27	49	1.144e+05	0.0	-0.02	-5400.00	0.0	-3558.33	5400.00	0.0	0.0	0.0	-4.931e+05
		-4.931e+05	0.0	0.0	0.0	225.0	-3558.33	0.0	0.0	0.0	0.0	1.144e+05
27	50	1.881e+06	0.0	-3.20	-1.324e+04	0.0	1363.89	5275.92	0.0	0.0	0.0	1.477e+06
		1.477e+06	0.0	0.0	0.0	225.0	-3766.11	-7961.99	0.0	0.0	0.0	1.492e+06
27	51	1.677e+06	0.0	-3.34	-5400.00	0.0	530.45	-3312.54	0.0	0.0	0.0	1.677e+06
		3.237e+05	0.0	0.0	0.0	225.0	-4599.55	-8712.54	0.0	0.0	0.0	3.237e+05
27	52	1.974e+06	0.0	4.31	-5400.00	0.0	-888.87	-4882.62	0.0	0.0	0.0	1.974e+06
		2.675e+05	0.0	0.0	0.0	225.0	-6018.87	-1.028e+04	0.0	0.0	0.0	2.675e+05
27	53	1.612e+06	0.0	-0.52	-1.324e+04	0.0	-3767.68	1.245e+04	0.0	0.0	0.0	-1.922e+04
		-1.922e+04	0.0	0.0	0.0	225.0	-3767.68	-792.52	0.0	0.0	0.0	1.609e+06
27	54	4.902e+05	0.0	-0.66	-5400.00	0.0	-4601.12	3856.93	0.0	0.0	0.0	1.808e+05
		1.808e+05	0.0	0.0	0.0	225.0	-4601.12	-1543.07	0.0	0.0	0.0	4.411e+05
27	55	5.867e+05	0.0	-1.62	-5400.00	0.0	-6020.43	2286.85	0.0	0.0	0.0	4.778e+05
		3.849e+05	0.0	0.0	0.0	225.0	-6020.43	-3113.15	0.0	0.0	0.0	3.849e+05
27	56	1.731e+06	0.0	-0.07	-1.585e+04	0.0	-3472.78	1.585e+04	0.0	0.0	0.0	-4.755e+05
		-4.755e+05	0.0	0.0	0.0	225.0	-3472.78	-3.91e-04	0.0	0.0	0.0	1.731e+06
27	57	3.043e+05	0.0	-0.02	-5400.00	0.0	-3030.69	5400.00	0.0	0.0	0.0	-3.032e+05
		-3.032e+05	0.0	0.0	0.0	225.0	-3030.69	0.0	0.0	0.0	0.0	3.043e+05
27	58	1.306e+06	0.0	-0.06	-1.324e+04	0.0	-3482.43	1.324e+04	0.0	0.0	0.0	-5.013e+05
		-5.013e+05	0.0	0.0	0.0	225.0	-3482.43	-2.93e-04	0.0	0.0	0.0	1.306e+06
27	59	2.354e+05	0.0	-0.03	-5400.00	0.0	-3150.86	5400.00	0.0	0.0	0.0	-3.721e+05
		-3.721e+05	0.0	0.0	0.0	225.0	-3150.86	0.0	0.0	0.0	0.0	2.354e+05
27	60	1.879e+06	0.0	-3.20	-1.324e+04	0.0	1357.78	5275.92	0.0	0.0	0.0	1.475e+06
		1.475e+06	0.0	0.0	0.0	225.0	-3772.22	-7961.99	0.0	0.0	0.0	1.490e+06
27	61	1.675e+06	0.0	-3.34	-5400.00	0.0	524.34	-3312.54	0.0	0.0	0.0	1.675e+06
		3.219e+05	0.0	0.0	0.0	225.0	-4605.66	-8712.54	0.0	0.0	0.0	3.219e+05
27	62	1.972e+06	0.0	4.31	-5400.00	0.0	-894.97	-4882.62	0.0	0.0	0.0	1.972e+06
		2.657e+05	0.0	0.0	0.0	225.0	-6024.97	-1.028e+04	0.0	0.0	0.0	2.657e+05
27	63	1.562e+06	0.0	-0.52	-1.324e+04	0.0	-3936.77	1.245e+04	0.0	0.0	0.0	-6.943e+04
		-6.943e+04	0.0	0.0	0.0	225.0	-3936.77	-792.52	0.0	0.0	0.0	1.559e+06
27	64	4.400e+05	0.0	-0.66	-5400.00	0.0	-4770.21	3856.93	0.0	0.0	0.0	1.305e+05
		1.305e+05	0.0	0.0	0.0	225.0	-4770.21	-1543.07	0.0	0.0	0.0	3.909e+05
27	65	5.365e+05	0.0	-1.62	-5400.00	0.0	-6189.53	2286.85	0.0	0.0	0.0	4.276e+05
		3.347e+05	0.0	0.0	0.0	225.0	-6189.53	-3113.15	0.0	0.0	0.0	3.347e+05
27	66	1.600e+06	0.0	-3.68	-8136.90	0.0	1485.02	2675.19	0.0	0.0	0.0	1.484e+06
		1.293e+06	0.0	0.0	0.0	225.0	-3644.98	-5461.71	0.0	0.0	0.0	1.293e+06
27	67	1.361e+06	0.0	-0.99	-8136.90	0.0	-3809.54	9844.65	0.0	0.0	0.0	-6.063e+04
		-6.063e+04	0.0	0.0	0.0	225.0	-3809.54	1707.75	0.0	0.0	0.0	1.361e+06
27	68	1.693e+06	0.0	4.32	-5400.00	0.0	-1499.98	-4882.62	0.0	0.0	0.0	1.693e+06
		-1.343e+04	0.0	0.0	0.0	225.0	-6629.98	-1.028e+04	0.0	0.0	0.0	-1.343e+04

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
27	69	7.119e+04	0.0	-1.65	-5400.00	0.0	-7197.86	2286.85	0.0	0.0	0.0	-3.764e+04
		-1.306e+05	0.0	0.0	0.0	225.0	-7197.86	-3113.15	0.0	0.0	0.0	-1.306e+05
27	70	1.447e+05	0.0	-0.02	-5400.00	0.0	-3456.47	5400.00	0.0	0.0	0.0	-4.628e+05
		-4.628e+05	0.0	0.0	0.0	225.0	-3456.47	0.0	0.0	0.0	0.0	1.447e+05
27	71	3.599e+05	0.0	-0.50	-5400.00	0.0	-3803.78	4607.48	0.0	0.0	0.0	-8.209e+04
		-8.209e+04	0.0	0.0	0.0	225.0	-3803.78	-792.52	0.0	0.0	0.0	3.471e+05
27	72	3.773e+05	0.0	-0.01	-5400.00	0.0	-2952.30	5400.00	0.0	0.0	0.0	-2.302e+05
		-2.302e+05	0.0	0.0	0.0	225.0	-2952.30	0.0	0.0	0.0	0.0	3.773e+05
27	73	1.273e+05	0.0	-0.51	-5400.00	0.0	-4307.94	4607.48	0.0	0.0	0.0	-3.147e+05
		-3.147e+05	0.0	0.0	0.0	225.0	-4307.94	-792.52	0.0	0.0	0.0	1.145e+05
27	74	6.676e+04	0.0	-0.51	-5400.00	0.0	-4511.68	4607.48	0.0	0.0	0.0	-3.752e+05
		-3.752e+05	0.0	0.0	0.0	225.0	-4511.68	-792.52	0.0	0.0	0.0	5.397e+04
28	1	2.358e+06	0.0	-0.09	-2.140e+04	0.0	-3790.57	0.0	0.0	0.0	0.0	2.358e+06
		-6.210e+05	0.0	0.0	0.0	225.0	-3790.57	-2.140e+04	0.0	0.0	0.0	-6.210e+05
28	2	4.317e+05	0.0	-0.03	-7290.00	0.0	-3193.75	0.0	0.0	0.0	0.0	4.317e+05
		-3.884e+05	0.0	0.0	0.0	225.0	-3193.75	-7290.00	0.0	0.0	0.0	-3.884e+05
28	3	1.732e+06	0.0	-0.08	-1.785e+04	0.0	-3980.06	0.0	0.0	0.0	0.0	1.732e+06
		-7.032e+05	0.0	0.0	0.0	225.0	-3980.06	-1.785e+04	0.0	0.0	0.0	-7.032e+05
28	4	2.910e+05	0.0	-0.03	-7290.00	0.0	-3533.55	0.0	0.0	0.0	0.0	2.910e+05
		-5.291e+05	0.0	0.0	0.0	225.0	-3533.55	-7290.00	0.0	0.0	0.0	-5.291e+05
28	5	2.036e+06	0.0	-4.50	-1.785e+04	0.0	-4546.97	-1.120e+04	0.0	0.0	0.0	2.036e+06
		-2.919e+06	0.0	0.0	0.0	225.0	-1.147e+04	-2.904e+04	0.0	0.0	0.0	-2.919e+06
28	6	4.626e+05	0.0	-4.79	-7290.00	0.0	-5669.34	-1.221e+04	0.0	0.0	0.0	4.626e+05
		-3.105e+06	0.0	0.0	0.0	225.0	-1.259e+04	-1.950e+04	0.0	0.0	0.0	-3.105e+06
28	7	3.869e+05	0.0	-6.10	-7290.00	0.0	-7580.68	-1.432e+04	0.0	0.0	0.0	3.869e+05
		-3.656e+06	0.0	0.0	0.0	225.0	-1.451e+04	-2.161e+04	0.0	0.0	0.0	-3.656e+06
28	8	2.177e+06	0.0	-0.89	-1.785e+04	0.0	-4591.56	-1520.45	0.0	0.0	0.0	2.177e+06
		-6.007e+05	0.0	0.0	0.0	225.0	-4591.56	-1.937e+04	0.0	0.0	0.0	-6.007e+05
28	9	6.034e+05	0.0	-1.18	-7290.00	0.0	-5713.93	-2531.20	0.0	0.0	0.0	6.034e+05
		-7.863e+05	0.0	0.0	0.0	225.0	-5713.93	-9821.20	0.0	0.0	0.0	-7.863e+05
28	10	5.277e+05	0.0	-2.49	-7290.00	0.0	-7625.27	-4645.57	0.0	0.0	0.0	5.277e+05
		-1.338e+06	0.0	0.0	0.0	225.0	-7625.27	-1.194e+04	0.0	0.0	0.0	-1.338e+06
28	11	2.360e+06	0.0	-0.09	-2.140e+04	0.0	-3783.25	0.0	0.0	0.0	0.0	2.360e+06
		-6.189e+05	0.0	0.0	0.0	225.0	-3783.25	-2.140e+04	0.0	0.0	0.0	-6.189e+05
28	12	4.339e+05	0.0	-0.03	-7290.00	0.0	-3186.43	0.0	0.0	0.0	0.0	4.339e+05
		-3.862e+05	0.0	0.0	0.0	225.0	-3186.43	-7290.00	0.0	0.0	0.0	-3.862e+05
28	13	2.351e+06	0.0	-0.06	-1.785e+04	0.0	-2567.14	0.0	0.0	0.0	0.0	2.351e+06
		-8.458e+04	0.0	0.0	0.0	225.0	-2567.14	-1.785e+04	0.0	0.0	0.0	-8.458e+04
28	14	9.096e+05	0.0	-8.01e-03	-7290.00	0.0	-2120.63	0.0	0.0	0.0	0.0	9.096e+05
		8.945e+04	0.0	0.0	0.0	225.0	-2120.63	-7290.00	0.0	0.0	0.0	8.945e+04
28	15	1.699e+06	0.0	-4.48	-1.785e+04	0.0	-5280.30	-1.120e+04	0.0	0.0	0.0	1.699e+06
		-3.256e+06	0.0	0.0	0.0	225.0	-1.221e+04	-2.904e+04	0.0	0.0	0.0	-3.256e+06
28	16	1.254e+05	0.0	-4.77	-7290.00	0.0	-6402.67	-1.221e+04	0.0	0.0	0.0	1.254e+05
		-3.442e+06	0.0	0.0	0.0	225.0	-1.333e+04	-1.950e+04	0.0	0.0	0.0	-3.442e+06
28	17	4.972e+04	0.0	-6.08	-7290.00	0.0	-8314.01	-1.432e+04	0.0	0.0	0.0	4.972e+04
		-3.993e+06	0.0	0.0	0.0	225.0	-1.524e+04	-2.161e+04	0.0	0.0	0.0	-3.993e+06
28	18	2.116e+06	0.0	-0.89	-1.785e+04	0.0	-4794.48	-1520.45	0.0	0.0	0.0	2.116e+06
		-6.610e+05	0.0	0.0	0.0	225.0	-4794.48	-1.937e+04	0.0	0.0	0.0	-6.610e+05
28	19	5.431e+05	0.0	-1.18	-7290.00	0.0	-5916.84	-2531.20	0.0	0.0	0.0	5.431e+05
		-8.465e+05	0.0	0.0	0.0	225.0	-5916.84	-9821.20	0.0	0.0	0.0	-8.465e+05
28	20	4.674e+05	0.0	-2.49	-7290.00	0.0	-7828.18	-4645.57	0.0	0.0	0.0	4.674e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-1.398e+06	0.0	0.0	0.0	225.0	-7828.18	-1.194e+04	0.0	0.0	0.0	-1.398e+06
28	21	1.767e+06	0.0	-5.15	-2.471e+04	0.0	-4382.95	-7832.20	0.0	0.0	0.0	1.767e+06
		-2.775e+06	0.0	0.0	0.0	225.0	-1.131e+04	-3.255e+04	0.0	0.0	0.0	-2.775e+06
28	22	1.865e+06	0.0	-1.54	-2.471e+04	0.0	-4623.13	1846.59	0.0	0.0	0.0	1.850e+06
		-5.147e+05	0.0	0.0	0.0	225.0	-4623.13	-2.287e+04	0.0	0.0	0.0	-5.147e+05
28	23	-1.713e+05	0.0	-6.09	-5400.00	0.0	-8432.70	-1.432e+04	0.0	0.0	0.0	-1.713e+05
		-4.002e+06	0.0	0.0	0.0	225.0	-1.536e+04	-1.972e+04	0.0	0.0	0.0	-4.002e+06
28	24	-3.119e+05	0.0	-2.47	-5400.00	0.0	-9156.88	-4645.57	0.0	0.0	0.0	-3.119e+05
		-1.965e+06	0.0	0.0	0.0	225.0	-9156.88	-1.005e+04	0.0	0.0	0.0	-1.965e+06
28	25	1.559e+06	0.0	-3.86	-1.098e+04	0.0	-4885.32	-1.457e+04	0.0	0.0	0.0	1.559e+06
		-3.118e+06	0.0	0.0	0.0	225.0	-1.181e+04	-2.554e+04	0.0	0.0	0.0	-3.118e+06
28	26	2.515e+05	0.0	-4.78	-7290.00	0.0	-6179.03	-1.221e+04	0.0	0.0	0.0	2.515e+05
		-3.316e+06	0.0	0.0	0.0	225.0	-1.310e+04	-1.950e+04	0.0	0.0	0.0	-3.316e+06
28	27	2.195e+06	0.0	-1.74	-3.058e+04	0.0	-4859.97	2980.04	0.0	0.0	0.0	2.163e+06
		-6.067e+05	0.0	0.0	0.0	225.0	-4859.97	-2.760e+04	0.0	0.0	0.0	-6.067e+05
28	28	4.605e+05	0.0	-1.17	-7290.00	0.0	-6061.05	-2531.20	0.0	0.0	0.0	4.605e+05
		-9.292e+05	0.0	0.0	0.0	225.0	-6061.05	-9821.20	0.0	0.0	0.0	-9.292e+05
28	29	4.972e+04	0.0	-6.08	-7290.00	0.0	-8314.01	-1.432e+04	0.0	0.0	0.0	4.972e+04
		-3.993e+06	0.0	0.0	0.0	225.0	-1.524e+04	-2.161e+04	0.0	0.0	0.0	-3.993e+06
28	30	1.641e+06	0.0	-3.58	-1.596e+04	0.0	-6690.09	-9678.78	0.0	0.0	0.0	1.641e+06
		-2.760e+06	0.0	0.0	0.0	225.0	-1.362e+04	-2.563e+04	0.0	0.0	0.0	-2.760e+06
28	31	-6.467e+04	0.0	-3.07	-5400.00	0.0	-9381.32	-9717.48	0.0	0.0	0.0	-6.467e+04
		-2.859e+06	0.0	0.0	0.0	225.0	-1.631e+04	-1.512e+04	0.0	0.0	0.0	-2.859e+06
28	32	-2.160e+05	0.0	-3.64	-5400.00	0.0	-1.320e+04	-9678.78	0.0	0.0	0.0	-2.160e+05
		-3.001e+06	0.0	0.0	0.0	225.0	-2.013e+04	-1.508e+04	0.0	0.0	0.0	-3.001e+06
28	33	4.718e+05	0.0	-6.09	-7290.00	0.0	-7294.63	-1.432e+04	0.0	0.0	0.0	4.718e+05
		-3.571e+06	0.0	0.0	0.0	225.0	-1.422e+04	-2.161e+04	0.0	0.0	0.0	-3.571e+06
28	34	1.209e+06	0.0	-0.06	-1.324e+04	0.0	-3808.41	0.0	0.0	0.0	0.0	1.209e+06
		-5.981e+05	0.0	0.0	0.0	225.0	-3808.41	-1.324e+04	0.0	0.0	0.0	-5.981e+05
28	35	4.051e+04	0.0	-0.16	-5400.00	0.0	-4641.84	-750.55	0.0	0.0	0.0	4.051e+04
		-7.359e+05	0.0	0.0	0.0	225.0	-4641.84	-6150.55	0.0	0.0	0.0	-7.359e+05
28	36	1.423e+06	0.0	-0.44	-1.324e+04	0.0	-4114.97	-792.52	0.0	0.0	0.0	1.423e+06
		-5.619e+05	0.0	0.0	0.0	225.0	-4114.97	-1.403e+04	0.0	0.0	0.0	-5.619e+05
28	37	2.550e+05	0.0	-0.66	-5400.00	0.0	-4948.41	-1543.07	0.0	0.0	0.0	2.550e+05
		-6.997e+05	0.0	0.0	0.0	225.0	-4948.41	-6943.07	0.0	0.0	0.0	-6.997e+05
28	38	1.988e+05	0.0	-1.63	-5400.00	0.0	-6367.72	-3113.15	0.0	0.0	0.0	1.988e+05
		-1.109e+06	0.0	0.0	0.0	225.0	-6367.72	-8513.15	0.0	0.0	0.0	-1.109e+06
28	39	1.441e+06	0.0	-0.05	-1.324e+04	0.0	-3304.24	0.0	0.0	0.0	0.0	1.441e+06
		-3.655e+05	0.0	0.0	0.0	225.0	-3304.24	-1.324e+04	0.0	0.0	0.0	-3.655e+05
28	40	3.713e+05	0.0	-0.01	-5400.00	0.0	-2972.67	0.0	0.0	0.0	0.0	3.713e+05
		-2.362e+05	0.0	0.0	0.0	225.0	-2972.67	-5400.00	0.0	0.0	0.0	-2.362e+05
28	41	1.191e+06	0.0	-0.43	-1.324e+04	0.0	-4619.14	-792.52	0.0	0.0	0.0	1.191e+06
		-7.945e+05	0.0	0.0	0.0	225.0	-4619.14	-1.403e+04	0.0	0.0	0.0	-7.945e+05
28	42	2.239e+04	0.0	-0.64	-5400.00	0.0	-5452.57	-1543.07	0.0	0.0	0.0	2.239e+04
		-9.323e+05	0.0	0.0	0.0	225.0	-5452.57	-6943.07	0.0	0.0	0.0	-9.323e+05
28	43	-3.380e+04	0.0	-1.62	-5400.00	0.0	-6871.89	-3113.15	0.0	0.0	0.0	-3.380e+04
		-1.342e+06	0.0	0.0	0.0	225.0	-6871.89	-8513.15	0.0	0.0	0.0	-1.342e+06
28	44	8.387e+05	0.0	-2.07	-1.834e+04	0.0	-7076.22	-612.88	0.0	0.0	0.0	8.387e+05
		-1.362e+06	0.0	0.0	0.0	225.0	-7076.22	-1.895e+04	0.0	0.0	0.0	-1.362e+06
28	45	-1.064e+05	0.0	-1.62	-5400.00	0.0	-7116.37	-3113.15	0.0	0.0	0.0	-1.064e+05
		-1.414e+06	0.0	0.0	0.0	225.0	-7116.37	-8513.15	0.0	0.0	0.0	-1.414e+06

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
28	46	1.658e+06	0.0	-0.07	-1.585e+04	0.0	-3717.26	0.0	0.0	0.0	0.0	1.658e+06
		-5.481e+05	0.0	0.0	0.0	225.0	-3717.26	-1.585e+04	0.0	0.0	0.0	-5.481e+05
28	47	2.317e+05	0.0	-0.02	-5400.00	0.0	-3275.17	0.0	0.0	0.0	0.0	2.317e+05
		-3.758e+05	0.0	0.0	0.0	225.0	-3275.17	-5400.00	0.0	0.0	0.0	-3.758e+05
28	48	1.185e+06	0.0	-0.06	-1.324e+04	0.0	-3889.90	0.0	0.0	0.0	0.0	1.185e+06
		-6.223e+05	0.0	0.0	0.0	225.0	-3889.90	-1.324e+04	0.0	0.0	0.0	-6.223e+05
28	49	1.144e+05	0.0	-0.02	-5400.00	0.0	-3558.33	0.0	0.0	0.0	0.0	1.144e+05
		-4.931e+05	0.0	0.0	0.0	225.0	-3558.33	-5400.00	0.0	0.0	0.0	-4.931e+05
28	50	1.492e+06	0.0	-3.13	-1.324e+04	0.0	-3766.11	-7961.99	0.0	0.0	0.0	1.492e+06
		-2.106e+06	0.0	0.0	0.0	225.0	-8896.11	-2.120e+04	0.0	0.0	0.0	-2.106e+06
28	51	3.237e+05	0.0	-3.34	-5400.00	0.0	-4599.55	-8712.54	0.0	0.0	0.0	3.237e+05
		-2.244e+06	0.0	0.0	0.0	225.0	-9729.55	-1.411e+04	0.0	0.0	0.0	-2.244e+06
28	52	2.675e+05	0.0	-4.32	-5400.00	0.0	-6018.87	-1.028e+04	0.0	0.0	0.0	2.675e+05
		-2.654e+06	0.0	0.0	0.0	225.0	-1.115e+04	-1.568e+04	0.0	0.0	0.0	-2.654e+06
28	53	1.609e+06	0.0	-0.45	-1.324e+04	0.0	-3767.68	-792.52	0.0	0.0	0.0	1.609e+06
		-3.758e+05	0.0	0.0	0.0	225.0	-3767.68	-1.403e+04	0.0	0.0	0.0	-3.758e+05
28	54	4.411e+05	0.0	-0.67	-5400.00	0.0	-4601.12	-1543.07	0.0	0.0	0.0	4.411e+05
		-5.136e+05	0.0	0.0	0.0	225.0	-4601.12	-6943.07	0.0	0.0	0.0	-5.136e+05
28	55	3.849e+05	0.0	-1.64	-5400.00	0.0	-6020.43	-3113.15	0.0	0.0	0.0	3.849e+05
		-9.231e+05	0.0	0.0	0.0	225.0	-6020.43	-8513.15	0.0	0.0	0.0	-9.231e+05
28	56	1.731e+06	0.0	-0.07	-1.585e+04	0.0	-3472.78	0.0	0.0	0.0	0.0	1.731e+06
		-4.755e+05	0.0	0.0	0.0	225.0	-3472.78	-1.585e+04	0.0	0.0	0.0	-4.755e+05
28	57	3.043e+05	0.0	-0.02	-5400.00	0.0	-3030.69	0.0	0.0	0.0	0.0	3.043e+05
		-3.032e+05	0.0	0.0	0.0	225.0	-3030.69	-5400.00	0.0	0.0	0.0	-3.032e+05
28	58	1.306e+06	0.0	-0.06	-1.324e+04	0.0	-3482.43	0.0	0.0	0.0	0.0	1.306e+06
		-5.013e+05	0.0	0.0	0.0	225.0	-3482.43	-1.324e+04	0.0	0.0	0.0	-5.013e+05
28	59	2.354e+05	0.0	-0.03	-5400.00	0.0	-3150.86	0.0	0.0	0.0	0.0	2.354e+05
		-3.721e+05	0.0	0.0	0.0	225.0	-3150.86	-5400.00	0.0	0.0	0.0	-3.721e+05
28	60	1.490e+06	0.0	-3.13	-1.324e+04	0.0	-3772.22	-7961.99	0.0	0.0	0.0	1.490e+06
		-2.108e+06	0.0	0.0	0.0	225.0	-8902.22	-2.120e+04	0.0	0.0	0.0	-2.108e+06
28	61	3.219e+05	0.0	-3.34	-5400.00	0.0	-4605.66	-8712.54	0.0	0.0	0.0	3.219e+05
		-2.246e+06	0.0	0.0	0.0	225.0	-9735.66	-1.411e+04	0.0	0.0	0.0	-2.246e+06
28	62	2.657e+05	0.0	-4.32	-5400.00	0.0	-6024.97	-1.028e+04	0.0	0.0	0.0	2.657e+05
		-2.655e+06	0.0	0.0	0.0	225.0	-1.115e+04	-1.568e+04	0.0	0.0	0.0	-2.655e+06
28	63	1.559e+06	0.0	-0.46	-1.324e+04	0.0	-3936.77	-792.52	0.0	0.0	0.0	1.559e+06
		-4.261e+05	0.0	0.0	0.0	225.0	-3936.77	-1.403e+04	0.0	0.0	0.0	-4.261e+05
28	64	3.909e+05	0.0	-0.67	-5400.00	0.0	-4770.21	-1543.07	0.0	0.0	0.0	3.909e+05
		-5.638e+05	0.0	0.0	0.0	225.0	-4770.21	-6943.07	0.0	0.0	0.0	-5.638e+05
28	65	3.347e+05	0.0	-1.64	-5400.00	0.0	-6189.53	-3113.15	0.0	0.0	0.0	3.347e+05
		-9.733e+05	0.0	0.0	0.0	225.0	-6189.53	-8513.15	0.0	0.0	0.0	-9.733e+05
28	66	1.293e+06	0.0	-3.61	-1.834e+04	0.0	-3644.98	-5461.71	0.0	0.0	0.0	1.293e+06
		-2.000e+06	0.0	0.0	0.0	225.0	-8774.98	-2.380e+04	0.0	0.0	0.0	-2.000e+06
28	67	1.379e+06	0.0	-0.94	-1.834e+04	0.0	-3809.54	1707.75	0.0	0.0	0.0	1.361e+06
		-3.174e+05	0.0	0.0	0.0	225.0	-3809.54	-1.663e+04	0.0	0.0	0.0	-3.174e+05
28	68	-1.343e+04	0.0	-4.30	-5400.00	0.0	-6629.98	-1.028e+04	0.0	0.0	0.0	-1.343e+04
		-2.935e+06	0.0	0.0	0.0	225.0	-1.176e+04	-1.568e+04	0.0	0.0	0.0	-2.935e+06
28	69	-1.306e+05	0.0	-1.62	-5400.00	0.0	-7197.86	-3113.15	0.0	0.0	0.0	-1.306e+05
		-1.439e+06	0.0	0.0	0.0	225.0	-7197.86	-8513.15	0.0	0.0	0.0	-1.439e+06
28	70	1.447e+05	0.0	-0.02	-5400.00	0.0	-3456.47	0.0	0.0	0.0	0.0	1.447e+05
		-4.628e+05	0.0	0.0	0.0	225.0	-3456.47	-5400.00	0.0	0.0	0.0	-4.628e+05
28	71	3.471e+05	0.0	-0.48	-5400.00	0.0	-3803.78	-792.52	0.0	0.0	0.0	3.471e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-4.387e+05	0.0	0.0	0.0	225.0	-3803.78	-6192.52	0.0	0.0	0.0	-4.387e+05
28	72	3.773e+05	0.0	-0.01	-5400.00	0.0	-2952.30	0.0	0.0	0.0	0.0	3.773e+05
		-2.302e+05	0.0	0.0	0.0	225.0	-2952.30	-5400.00	0.0	0.0	0.0	-2.302e+05
28	73	1.145e+05	0.0	-0.47	-5400.00	0.0	-4307.94	-792.52	0.0	0.0	0.0	1.145e+05
		-6.714e+05	0.0	0.0	0.0	225.0	-4307.94	-6192.52	0.0	0.0	0.0	-6.714e+05
28	74	5.397e+04	0.0	-0.47	-5400.00	0.0	-4511.68	-792.52	0.0	0.0	0.0	5.397e+04
		-7.319e+05	0.0	0.0	0.0	225.0	-4511.68	-6192.52	0.0	0.0	0.0	-7.319e+05
29	1	-6.210e+05	0.0	-7.93e-03	-556.88	0.0	-3790.57	-2.140e+04	0.0	0.0	0.0	-6.210e+05
		-8.920e+05	0.0	0.0	0.0	12.5	-3790.57	-2.196e+04	0.0	0.0	0.0	-8.920e+05
29	2	-3.884e+05	0.0	-2.54e-03	-405.00	0.0	-3193.75	-7290.00	0.0	0.0	0.0	-3.884e+05
		-4.821e+05	0.0	0.0	0.0	12.5	-3193.75	-7695.00	0.0	0.0	0.0	-4.821e+05
29	3	-7.032e+05	0.0	-7.06e-03	-518.63	0.0	-3980.06	-1.785e+04	0.0	0.0	0.0	-7.032e+05
		-9.295e+05	0.0	0.0	0.0	12.5	-3980.06	-1.836e+04	0.0	0.0	0.0	-9.295e+05
29	4	-5.291e+05	0.0	-3.02e-03	-405.00	0.0	-3533.55	-7290.00	0.0	0.0	0.0	-5.291e+05
		-6.228e+05	0.0	0.0	0.0	12.5	-3533.55	-7695.00	0.0	0.0	0.0	-6.228e+05
29	5	-2.919e+06	0.0	-0.25	-518.63	0.0	-1.147e+04	-2.904e+04	0.0	0.0	0.0	-2.919e+06
		-3.286e+06	0.0	0.0	0.0	12.5	-1.224e+04	-2.956e+04	0.0	0.0	0.0	-3.286e+06
29	6	-3.105e+06	0.0	-0.27	-405.00	0.0	-1.259e+04	-1.950e+04	0.0	0.0	0.0	-3.105e+06
		-3.351e+06	0.0	0.0	0.0	12.5	-1.336e+04	-1.990e+04	0.0	0.0	0.0	-3.351e+06
29	7	-3.656e+06	0.0	-0.35	-405.00	0.0	-1.451e+04	-2.161e+04	0.0	0.0	0.0	-3.656e+06
		-3.929e+06	0.0	0.0	0.0	12.5	-1.528e+04	-2.202e+04	0.0	0.0	0.0	-3.929e+06
29	8	-6.007e+05	0.0	-0.05	-518.63	0.0	-4591.56	-1.937e+04	0.0	0.0	0.0	-6.007e+05
		-8.460e+05	0.0	0.0	0.0	12.5	-4591.56	-1.988e+04	0.0	0.0	0.0	-8.460e+05
29	9	-7.863e+05	0.0	-0.07	-405.00	0.0	-5713.93	-9821.20	0.0	0.0	0.0	-7.863e+05
		-9.116e+05	0.0	0.0	0.0	12.5	-5713.93	-1.023e+04	0.0	0.0	0.0	-9.116e+05
29	10	-1.338e+06	0.0	-0.14	-405.00	0.0	-7625.27	-1.194e+04	0.0	0.0	0.0	-1.338e+06
		-1.489e+06	0.0	0.0	0.0	12.5	-7625.27	-1.234e+04	0.0	0.0	0.0	-1.489e+06
29	11	-6.189e+05	0.0	-7.94e-03	-556.88	0.0	-3783.25	-2.140e+04	0.0	0.0	0.0	-6.189e+05
		-8.898e+05	0.0	0.0	0.0	12.5	-3783.25	-2.196e+04	0.0	0.0	0.0	-8.898e+05
29	12	-3.862e+05	0.0	-2.55e-03	-405.00	0.0	-3186.43	-7290.00	0.0	0.0	0.0	-3.862e+05
		-4.799e+05	0.0	0.0	0.0	12.5	-3186.43	-7695.00	0.0	0.0	0.0	-4.799e+05
29	13	-8.458e+04	0.0	-4.23e-03	-518.63	0.0	-2567.14	-1.785e+04	0.0	0.0	0.0	-8.458e+04
		-3.109e+05	0.0	0.0	0.0	12.5	-2567.14	-1.836e+04	0.0	0.0	0.0	-3.109e+05
29	14	8.945e+04	0.0	-1.89e-04	-405.00	0.0	-2120.63	-7290.00	0.0	0.0	0.0	8.945e+04
		-4210.17	0.0	0.0	0.0	12.5	-2120.63	-7695.00	0.0	0.0	0.0	-4210.17
29	15	-3.256e+06	0.0	-0.25	-518.63	0.0	-1.221e+04	-2.904e+04	0.0	0.0	0.0	-3.256e+06
		-3.623e+06	0.0	0.0	0.0	12.5	-1.298e+04	-2.956e+04	0.0	0.0	0.0	-3.623e+06
29	16	-3.442e+06	0.0	-0.27	-405.00	0.0	-1.333e+04	-1.950e+04	0.0	0.0	0.0	-3.442e+06
		-3.688e+06	0.0	0.0	0.0	12.5	-1.410e+04	-1.990e+04	0.0	0.0	0.0	-3.688e+06
29	17	-3.993e+06	0.0	-0.34	-405.00	0.0	-1.524e+04	-2.161e+04	0.0	0.0	0.0	-3.993e+06
		-4.266e+06	0.0	0.0	0.0	12.5	-1.601e+04	-2.202e+04	0.0	0.0	0.0	-4.266e+06
29	18	-6.610e+05	0.0	-0.05	-518.63	0.0	-4794.48	-1.937e+04	0.0	0.0	0.0	-6.610e+05
		-9.063e+05	0.0	0.0	0.0	12.5	-4794.48	-1.988e+04	0.0	0.0	0.0	-9.063e+05
29	19	-8.465e+05	0.0	-0.07	-405.00	0.0	-5916.84	-9821.20	0.0	0.0	0.0	-8.465e+05
		-9.718e+05	0.0	0.0	0.0	12.5	-5916.84	-1.023e+04	0.0	0.0	0.0	-9.718e+05
29	20	-1.398e+06	0.0	-0.14	-405.00	0.0	-7828.18	-1.194e+04	0.0	0.0	0.0	-1.398e+06
		-1.550e+06	0.0	0.0	0.0	12.5	-7828.18	-1.234e+04	0.0	0.0	0.0	-1.550e+06
29	21	-2.775e+06	0.0	-0.29	-518.62	0.0	-1.131e+04	-3.255e+04	0.0	0.0	0.0	-2.775e+06
		-3.185e+06	0.0	0.0	0.0	12.5	-1.208e+04	-3.307e+04	0.0	0.0	0.0	-3.185e+06
29	22	-5.147e+05	0.0	-0.09	-518.63	0.0	-4623.13	-2.287e+04	0.0	0.0	0.0	-5.147e+05
		-8.038e+05	0.0	0.0	0.0	12.5	-4623.13	-2.339e+04	0.0	0.0	0.0	-8.038e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
29	23	-4.002e+06	0.0	-0.34	-300.00	0.0	-1.536e+04	-1.972e+04	0.0	0.0	0.0	-4.002e+06
		-4.250e+06	0.0	0.0	0.0	12.5	-1.613e+04	-2.002e+04	0.0	0.0	0.0	-4.250e+06
29	24	-1.965e+06	0.0	-0.14	-300.00	0.0	-9156.88	-1.005e+04	0.0	0.0	0.0	-1.965e+06
		-2.092e+06	0.0	0.0	0.0	12.5	-9156.88	-1.035e+04	0.0	0.0	0.0	-2.092e+06
29	25	-3.118e+06	0.0	-0.22	-518.63	0.0	-1.181e+04	-2.554e+04	0.0	0.0	0.0	-3.118e+06
		-3.441e+06	0.0	0.0	0.0	12.5	-1.258e+04	-2.606e+04	0.0	0.0	0.0	-3.441e+06
29	26	-3.316e+06	0.0	-0.27	-405.00	0.0	-1.310e+04	-1.950e+04	0.0	0.0	0.0	-3.316e+06
		-3.562e+06	0.0	0.0	0.0	12.5	-1.387e+04	-1.990e+04	0.0	0.0	0.0	-3.562e+06
29	27	-6.067e+05	0.0	-0.10	-556.88	0.0	-4859.97	-2.760e+04	0.0	0.0	0.0	-6.067e+05
		-9.552e+05	0.0	0.0	0.0	12.5	-4859.97	-2.816e+04	0.0	0.0	0.0	-9.552e+05
29	28	-9.292e+05	0.0	-0.07	-405.00	0.0	-6061.05	-9821.20	0.0	0.0	0.0	-9.292e+05
		-1.054e+06	0.0	0.0	0.0	12.5	-6061.05	-1.023e+04	0.0	0.0	0.0	-1.054e+06
29	29	-3.993e+06	0.0	-0.34	-405.00	0.0	-1.524e+04	-2.161e+04	0.0	0.0	0.0	-3.993e+06
		-4.266e+06	0.0	0.0	0.0	12.5	-1.601e+04	-2.202e+04	0.0	0.0	0.0	-4.266e+06
29	30	-2.760e+06	0.0	-0.20	-413.63	0.0	-1.362e+04	-2.563e+04	0.0	0.0	0.0	-2.760e+06
		-3.083e+06	0.0	0.0	0.0	12.5	-1.439e+04	-2.605e+04	0.0	0.0	0.0	-3.083e+06
29	31	-2.859e+06	0.0	-0.18	-300.00	0.0	-1.631e+04	-1.512e+04	0.0	0.0	0.0	-2.859e+06
		-3.049e+06	0.0	0.0	0.0	12.5	-1.708e+04	-1.542e+04	0.0	0.0	0.0	-3.049e+06
29	32	-3.001e+06	0.0	-0.21	-300.00	0.0	-2.013e+04	-1.508e+04	0.0	0.0	0.0	-3.001e+06
		-3.192e+06	0.0	0.0	0.0	12.5	-2.090e+04	-1.538e+04	0.0	0.0	0.0	-3.192e+06
29	33	-3.571e+06	0.0	-0.34	-405.00	0.0	-1.422e+04	-2.161e+04	0.0	0.0	0.0	-3.571e+06
		-3.844e+06	0.0	0.0	0.0	12.5	-1.499e+04	-2.202e+04	0.0	0.0	0.0	-3.844e+06
29	34	-5.981e+05	0.0	-5.14e-03	-384.38	0.0	-3808.41	-1.324e+04	0.0	0.0	0.0	-5.981e+05
		-7.660e+05	0.0	0.0	0.0	12.5	-3808.41	-1.362e+04	0.0	0.0	0.0	-7.660e+05
29	35	-7.359e+05	0.0	-8.34e-03	-300.00	0.0	-4641.84	-6150.55	0.0	0.0	0.0	-7.359e+05
		-8.146e+05	0.0	0.0	0.0	12.5	-4641.84	-6450.55	0.0	0.0	0.0	-8.146e+05
29	36	-5.619e+05	0.0	-0.02	-384.38	0.0	-4114.97	-1.403e+04	0.0	0.0	0.0	-5.619e+05
		-7.397e+05	0.0	0.0	0.0	12.5	-4114.97	-1.441e+04	0.0	0.0	0.0	-7.397e+05
29	37	-6.997e+05	0.0	-0.04	-300.00	0.0	-4948.41	-6943.07	0.0	0.0	0.0	-6.997e+05
		-7.883e+05	0.0	0.0	0.0	12.5	-4948.41	-7243.07	0.0	0.0	0.0	-7.883e+05
29	38	-1.109e+06	0.0	-0.09	-300.00	0.0	-6367.72	-8513.15	0.0	0.0	0.0	-1.109e+06
		-1.217e+06	0.0	0.0	0.0	12.5	-6367.72	-8813.15	0.0	0.0	0.0	-1.217e+06
29	39	-3.655e+05	0.0	-3.84e-03	-384.38	0.0	-3304.24	-1.324e+04	0.0	0.0	0.0	-3.655e+05
		-5.333e+05	0.0	0.0	0.0	12.5	-3304.24	-1.362e+04	0.0	0.0	0.0	-5.333e+05
29	40	-2.362e+05	0.0	-8.41e-04	-300.00	0.0	-2972.67	-5400.00	0.0	0.0	0.0	-2.362e+05
		-3.056e+05	0.0	0.0	0.0	12.5	-2972.67	-5700.00	0.0	0.0	0.0	-3.056e+05
29	41	-7.945e+05	0.0	-0.02	-384.38	0.0	-4619.14	-1.403e+04	0.0	0.0	0.0	-7.945e+05
		-9.723e+05	0.0	0.0	0.0	12.5	-4619.14	-1.441e+04	0.0	0.0	0.0	-9.723e+05
29	42	-9.323e+05	0.0	-0.04	-300.00	0.0	-5452.57	-6943.07	0.0	0.0	0.0	-9.323e+05
		-1.021e+06	0.0	0.0	0.0	12.5	-5452.57	-7243.07	0.0	0.0	0.0	-1.021e+06
29	43	-1.342e+06	0.0	-0.09	-300.00	0.0	-6871.89	-8513.15	0.0	0.0	0.0	-1.342e+06
		-1.450e+06	0.0	0.0	0.0	12.5	-6871.89	-8813.15	0.0	0.0	0.0	-1.450e+06
29	44	-1.362e+06	0.0	-0.11	-384.38	0.0	-7076.22	-1.895e+04	0.0	0.0	0.0	-1.362e+06
		-1.602e+06	0.0	0.0	0.0	12.5	-7076.22	-1.934e+04	0.0	0.0	0.0	-1.602e+06
29	45	-1.414e+06	0.0	-0.09	-300.00	0.0	-7116.37	-8513.15	0.0	0.0	0.0	-1.414e+06
		-1.523e+06	0.0	0.0	0.0	12.5	-7116.37	-8813.15	0.0	0.0	0.0	-1.523e+06
29	46	-5.481e+05	0.0	-5.62e-03	-412.50	0.0	-3717.26	-1.585e+04	0.0	0.0	0.0	-5.481e+05
		-7.488e+05	0.0	0.0	0.0	12.5	-3717.26	-1.626e+04	0.0	0.0	0.0	-7.488e+05
29	47	-3.758e+05	0.0	-1.62e-03	-300.00	0.0	-3275.17	-5400.00	0.0	0.0	0.0	-3.758e+05
		-4.452e+05	0.0	0.0	0.0	12.5	-3275.17	-5700.00	0.0	0.0	0.0	-4.452e+05
29	48	-6.223e+05	0.0	-5.02e-03	-384.38	0.0	-3889.90	-1.324e+04	0.0	0.0	0.0	-6.223e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-7.902e+05	0.0	0.0	0.0	12.5	-3889.90	-1.362e+04	0.0	0.0	0.0	-7.902e+05
29	49	-4.931e+05	0.0	-2.03e-03	-300.00	0.0	-3558.33	-5400.00	0.0	0.0	0.0	-4.931e+05
		-5.624e+05	0.0	0.0	0.0	12.5	-3558.33	-5700.00	0.0	0.0	0.0	-5.624e+05
29	50	-2.106e+06	0.0	-0.18	-384.38	0.0	-8896.11	-2.120e+04	0.0	0.0	0.0	-2.106e+06
		-2.374e+06	0.0	0.0	0.0	12.5	-9466.11	-2.158e+04	0.0	0.0	0.0	-2.374e+06
29	51	-2.244e+06	0.0	-0.19	-300.00	0.0	-9729.55	-1.411e+04	0.0	0.0	0.0	-2.244e+06
		-2.422e+06	0.0	0.0	0.0	12.5	-1.030e+04	-1.441e+04	0.0	0.0	0.0	-2.422e+06
29	52	-2.654e+06	0.0	-0.24	-300.00	0.0	-1.115e+04	-1.568e+04	0.0	0.0	0.0	-2.654e+06
		-2.851e+06	0.0	0.0	0.0	12.5	-1.172e+04	-1.598e+04	0.0	0.0	0.0	-2.851e+06
29	53	-3.758e+05	0.0	-0.03	-384.38	0.0	-3767.68	-1.403e+04	0.0	0.0	0.0	-3.758e+05
		-5.536e+05	0.0	0.0	0.0	12.5	-3767.68	-1.441e+04	0.0	0.0	0.0	-5.536e+05
29	54	-5.136e+05	0.0	-0.04	-300.00	0.0	-4601.12	-6943.07	0.0	0.0	0.0	-5.136e+05
		-6.023e+05	0.0	0.0	0.0	12.5	-4601.12	-7243.07	0.0	0.0	0.0	-6.023e+05
29	55	-9.231e+05	0.0	-0.09	-300.00	0.0	-6020.43	-8513.15	0.0	0.0	0.0	-9.231e+05
		-1.031e+06	0.0	0.0	0.0	12.5	-6020.43	-8813.15	0.0	0.0	0.0	-1.031e+06
29	56	-4.755e+05	0.0	-5.96e-03	-412.50	0.0	-3472.78	-1.585e+04	0.0	0.0	0.0	-4.755e+05
		-6.762e+05	0.0	0.0	0.0	12.5	-3472.78	-1.626e+04	0.0	0.0	0.0	-6.762e+05
29	57	-3.032e+05	0.0	-1.97e-03	-300.00	0.0	-3030.69	-5400.00	0.0	0.0	0.0	-3.032e+05
		-3.726e+05	0.0	0.0	0.0	12.5	-3030.69	-5700.00	0.0	0.0	0.0	-3.726e+05
29	58	-5.013e+05	0.0	-5.60e-03	-384.38	0.0	-3482.43	-1.324e+04	0.0	0.0	0.0	-5.013e+05
		-6.692e+05	0.0	0.0	0.0	12.5	-3482.43	-1.362e+04	0.0	0.0	0.0	-6.692e+05
29	59	-3.721e+05	0.0	-2.60e-03	-300.00	0.0	-3150.86	-5400.00	0.0	0.0	0.0	-3.721e+05
		-4.414e+05	0.0	0.0	0.0	12.5	-3150.86	-5700.00	0.0	0.0	0.0	-4.414e+05
29	60	-2.108e+06	0.0	-0.18	-384.38	0.0	-8902.22	-2.120e+04	0.0	0.0	0.0	-2.108e+06
		-2.376e+06	0.0	0.0	0.0	12.5	-9472.22	-2.158e+04	0.0	0.0	0.0	-2.376e+06
29	61	-2.246e+06	0.0	-0.19	-300.00	0.0	-9735.66	-1.411e+04	0.0	0.0	0.0	-2.246e+06
		-2.424e+06	0.0	0.0	0.0	12.5	-1.031e+04	-1.441e+04	0.0	0.0	0.0	-2.424e+06
29	62	-2.655e+06	0.0	-0.24	-300.00	0.0	-1.115e+04	-1.568e+04	0.0	0.0	0.0	-2.655e+06
		-2.853e+06	0.0	0.0	0.0	12.5	-1.172e+04	-1.598e+04	0.0	0.0	0.0	-2.853e+06
29	63	-4.261e+05	0.0	-0.03	-384.38	0.0	-3936.77	-1.403e+04	0.0	0.0	0.0	-4.261e+05
		-6.038e+05	0.0	0.0	0.0	12.5	-3936.77	-1.441e+04	0.0	0.0	0.0	-6.038e+05
29	64	-5.638e+05	0.0	-0.04	-300.00	0.0	-4770.21	-6943.07	0.0	0.0	0.0	-5.638e+05
		-6.525e+05	0.0	0.0	0.0	12.5	-4770.21	-7243.07	0.0	0.0	0.0	-6.525e+05
29	65	-9.733e+05	0.0	-0.09	-300.00	0.0	-6189.53	-8513.15	0.0	0.0	0.0	-9.733e+05
		-1.082e+06	0.0	0.0	0.0	12.5	-6189.53	-8813.15	0.0	0.0	0.0	-1.082e+06
29	66	-2.000e+06	0.0	-0.20	-384.38	0.0	-8774.98	-2.380e+04	0.0	0.0	0.0	-2.000e+06
		-2.299e+06	0.0	0.0	0.0	12.5	-9344.98	-2.418e+04	0.0	0.0	0.0	-2.299e+06
29	67	-3.174e+05	0.0	-0.05	-384.38	0.0	-3809.54	-1.663e+04	0.0	0.0	0.0	-3.174e+05
		-5.277e+05	0.0	0.0	0.0	12.5	-3809.54	-1.702e+04	0.0	0.0	0.0	-5.277e+05
29	68	-2.935e+06	0.0	-0.24	-300.00	0.0	-1.176e+04	-1.568e+04	0.0	0.0	0.0	-2.935e+06
		-3.132e+06	0.0	0.0	0.0	12.5	-1.233e+04	-1.598e+04	0.0	0.0	0.0	-3.132e+06
29	69	-1.439e+06	0.0	-0.09	-300.00	0.0	-7197.86	-8513.15	0.0	0.0	0.0	-1.439e+06
		-1.547e+06	0.0	0.0	0.0	12.5	-7197.86	-8813.15	0.0	0.0	0.0	-1.547e+06
29	70	-4.628e+05	0.0	-2.17e-03	-300.00	0.0	-3456.47	-5400.00	0.0	0.0	0.0	-4.628e+05
		-5.322e+05	0.0	0.0	0.0	12.5	-3456.47	-5700.00	0.0	0.0	0.0	-5.322e+05
29	71	-4.387e+05	0.0	-0.03	-300.00	0.0	-3803.78	-6192.52	0.0	0.0	0.0	-4.387e+05
		-5.180e+05	0.0	0.0	0.0	12.5	-3803.78	-6492.52	0.0	0.0	0.0	-5.180e+05
29	72	-2.302e+05	0.0	-8.70e-04	-300.00	0.0	-2952.30	-5400.00	0.0	0.0	0.0	-2.302e+05
		-2.996e+05	0.0	0.0	0.0	12.5	-2952.30	-5700.00	0.0	0.0	0.0	-2.996e+05
29	73	-6.714e+05	0.0	-0.03	-300.00	0.0	-4307.94	-6192.52	0.0	0.0	0.0	-6.714e+05
		-7.506e+05	0.0	0.0	0.0	12.5	-4307.94	-6492.52	0.0	0.0	0.0	-7.506e+05

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
29	74	-7.319e+05	0.0	-0.03	-300.00	0.0	-4511.68	-6192.52	0.0	0.0	0.0	-7.319e+05
		-8.111e+05	0.0	0.0	0.0	12.5	-4511.68	-6492.52	0.0	0.0	0.0	-8.111e+05
30	1	-8.920e+05	0.0	-7.81e-03	-556.88	0.0	-3790.57	-2.196e+04	0.0	0.0	0.0	-8.920e+05
		-1.170e+06	0.0	0.0	0.0	12.5	-3790.57	-2.251e+04	0.0	0.0	0.0	-1.170e+06
30	2	-4.821e+05	0.0	-2.51e-03	-405.00	0.0	-3193.75	-7695.00	0.0	0.0	0.0	-4.821e+05
		-5.808e+05	0.0	0.0	0.0	12.5	-3193.75	-8100.00	0.0	0.0	0.0	-5.808e+05
30	3	-9.295e+05	0.0	-6.99e-03	-518.63	0.0	-3980.06	-1.836e+04	0.0	0.0	0.0	-9.295e+05
		-1.162e+06	0.0	0.0	0.0	12.5	-3980.06	-1.888e+04	0.0	0.0	0.0	-1.162e+06
30	4	-6.228e+05	0.0	-3.03e-03	-405.00	0.0	-3533.55	-7695.00	0.0	0.0	0.0	-6.228e+05
		-7.215e+05	0.0	0.0	0.0	12.5	-3533.55	-8100.00	0.0	0.0	0.0	-7.215e+05
30	5	-3.286e+06	0.0	-0.25	-518.63	0.0	-1.224e+04	-2.956e+04	0.0	0.0	0.0	-3.286e+06
		-3.658e+06	0.0	0.0	0.0	12.5	-1.301e+04	-3.008e+04	0.0	0.0	0.0	-3.658e+06
30	6	-3.351e+06	0.0	-0.27	-405.00	0.0	-1.336e+04	-1.990e+04	0.0	0.0	0.0	-3.351e+06
		-3.602e+06	0.0	0.0	0.0	12.5	-1.413e+04	-2.031e+04	0.0	0.0	0.0	-3.602e+06
30	7	-3.929e+06	0.0	-0.35	-405.00	0.0	-1.528e+04	-2.202e+04	0.0	0.0	0.0	-3.929e+06
		-4.207e+06	0.0	0.0	0.0	12.5	-1.605e+04	-2.242e+04	0.0	0.0	0.0	-4.207e+06
30	8	-8.460e+05	0.0	-0.05	-518.63	0.0	-4591.56	-1.988e+04	0.0	0.0	0.0	-8.460e+05
		-1.098e+06	0.0	0.0	0.0	12.5	-4591.56	-2.040e+04	0.0	0.0	0.0	-1.098e+06
30	9	-9.116e+05	0.0	-0.07	-405.00	0.0	-5713.93	-1.023e+04	0.0	0.0	0.0	-9.116e+05
		-1.042e+06	0.0	0.0	0.0	12.5	-5713.93	-1.063e+04	0.0	0.0	0.0	-1.042e+06
30	10	-1.489e+06	0.0	-0.14	-405.00	0.0	-7625.27	-1.234e+04	0.0	0.0	0.0	-1.489e+06
		-1.646e+06	0.0	0.0	0.0	12.5	-7625.27	-1.275e+04	0.0	0.0	0.0	-1.646e+06
30	11	-8.898e+05	0.0	-7.82e-03	-556.88	0.0	-3783.25	-2.196e+04	0.0	0.0	0.0	-8.898e+05
		-1.168e+06	0.0	0.0	0.0	12.5	-3783.25	-2.251e+04	0.0	0.0	0.0	-1.168e+06
30	12	-4.799e+05	0.0	-2.53e-03	-405.00	0.0	-3186.43	-7695.00	0.0	0.0	0.0	-4.799e+05
		-5.786e+05	0.0	0.0	0.0	12.5	-3186.43	-8100.00	0.0	0.0	0.0	-5.786e+05
30	13	-3.109e+05	0.0	-4.00e-03	-518.63	0.0	-2567.14	-1.836e+04	0.0	0.0	0.0	-3.109e+05
		-5.437e+05	0.0	0.0	0.0	12.5	-2567.14	-1.888e+04	0.0	0.0	0.0	-5.437e+05
30	14	-4210.17	0.0	-3.86e-05	-405.00	0.0	-2120.63	-7695.00	0.0	0.0	0.0	-4210.17
		-1.029e+05	0.0	0.0	0.0	12.5	-2120.63	-8100.00	0.0	0.0	0.0	-1.029e+05
30	15	-3.623e+06	0.0	-0.25	-518.63	0.0	-1.298e+04	-2.956e+04	0.0	0.0	0.0	-3.623e+06
		-3.996e+06	0.0	0.0	0.0	12.5	-1.374e+04	-3.008e+04	0.0	0.0	0.0	-3.996e+06
30	16	-3.688e+06	0.0	-0.27	-405.00	0.0	-1.410e+04	-1.990e+04	0.0	0.0	0.0	-3.688e+06
		-3.940e+06	0.0	0.0	0.0	12.5	-1.487e+04	-2.031e+04	0.0	0.0	0.0	-3.940e+06
30	17	-4.266e+06	0.0	-0.34	-405.00	0.0	-1.601e+04	-2.202e+04	0.0	0.0	0.0	-4.266e+06
		-4.544e+06	0.0	0.0	0.0	12.5	-1.678e+04	-2.242e+04	0.0	0.0	0.0	-4.544e+06
30	18	-9.063e+05	0.0	-0.05	-518.63	0.0	-4794.48	-1.988e+04	0.0	0.0	0.0	-9.063e+05
		-1.158e+06	0.0	0.0	0.0	12.5	-4794.48	-2.040e+04	0.0	0.0	0.0	-1.158e+06
30	19	-9.718e+05	0.0	-0.07	-405.00	0.0	-5916.84	-1.023e+04	0.0	0.0	0.0	-9.718e+05
		-1.102e+06	0.0	0.0	0.0	12.5	-5916.84	-1.063e+04	0.0	0.0	0.0	-1.102e+06
30	20	-1.550e+06	0.0	-0.14	-405.00	0.0	-7828.18	-1.234e+04	0.0	0.0	0.0	-1.550e+06
		-1.706e+06	0.0	0.0	0.0	12.5	-7828.18	-1.275e+04	0.0	0.0	0.0	-1.706e+06
30	21	-3.185e+06	0.0	-0.29	-518.63	0.0	-1.208e+04	-3.307e+04	0.0	0.0	0.0	-3.185e+06
		-3.602e+06	0.0	0.0	0.0	12.5	-1.285e+04	-3.358e+04	0.0	0.0	0.0	-3.602e+06
30	22	-8.038e+05	0.0	-0.09	-518.63	0.0	-4623.13	-2.339e+04	0.0	0.0	0.0	-8.038e+05
		-1.099e+06	0.0	0.0	0.0	12.5	-4623.13	-2.391e+04	0.0	0.0	0.0	-1.099e+06
30	23	-4.250e+06	0.0	-0.35	-300.00	0.0	-1.613e+04	-2.002e+04	0.0	0.0	0.0	-4.250e+06
		-4.502e+06	0.0	0.0	0.0	12.5	-1.690e+04	-2.032e+04	0.0	0.0	0.0	-4.502e+06
30	24	-2.092e+06	0.0	-0.14	-300.00	0.0	-9156.88	-1.035e+04	0.0	0.0	0.0	-2.092e+06
		-2.223e+06	0.0	0.0	0.0	12.5	-9156.88	-1.065e+04	0.0	0.0	0.0	-2.223e+06
30	25	-3.441e+06	0.0	-0.22	-518.63	0.0	-1.258e+04	-2.606e+04	0.0	0.0	0.0	-3.441e+06

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-3.770e+06	0.0	0.0	0.0	12.5	-1.335e+04	-2.658e+04	0.0	0.0	0.0	-3.770e+06
30	26	-3.562e+06	0.0	-0.27	-405.00	0.0	-1.387e+04	-1.990e+04	0.0	0.0	0.0	-3.562e+06
		-3.813e+06	0.0	0.0	0.0	12.5	-1.464e+04	-2.031e+04	0.0	0.0	0.0	-3.813e+06
30	27	-9.552e+05	0.0	-0.10	-556.88	0.0	-4859.97	-2.816e+04	0.0	0.0	0.0	-9.552e+05
		-1.311e+06	0.0	0.0	0.0	12.5	-4859.97	-2.871e+04	0.0	0.0	0.0	-1.311e+06
30	28	-1.054e+06	0.0	-0.07	-405.00	0.0	-6061.05	-1.023e+04	0.0	0.0	0.0	-1.054e+06
		-1.185e+06	0.0	0.0	0.0	12.5	-6061.05	-1.063e+04	0.0	0.0	0.0	-1.185e+06
30	29	-4.266e+06	0.0	-0.34	-405.00	0.0	-1.601e+04	-2.202e+04	0.0	0.0	0.0	-4.266e+06
		-4.544e+06	0.0	0.0	0.0	12.5	-1.678e+04	-2.242e+04	0.0	0.0	0.0	-4.544e+06
30	30	-3.083e+06	0.0	-0.20	-413.63	0.0	-1.439e+04	-2.605e+04	0.0	0.0	0.0	-3.083e+06
		-3.411e+06	0.0	0.0	0.0	12.5	-1.515e+04	-2.646e+04	0.0	0.0	0.0	-3.411e+06
30	31	-3.049e+06	0.0	-0.18	-300.00	0.0	-1.708e+04	-1.542e+04	0.0	0.0	0.0	-3.049e+06
		-3.244e+06	0.0	0.0	0.0	12.5	-1.785e+04	-1.572e+04	0.0	0.0	0.0	-3.244e+06
30	32	-3.192e+06	0.0	-0.21	-300.00	0.0	-2.090e+04	-1.538e+04	0.0	0.0	0.0	-3.192e+06
		-3.386e+06	0.0	0.0	0.0	12.5	-2.167e+04	-1.568e+04	0.0	0.0	0.0	-3.386e+06
30	33	-3.844e+06	0.0	-0.35	-405.00	0.0	-1.499e+04	-2.202e+04	0.0	0.0	0.0	-3.844e+06
		-4.122e+06	0.0	0.0	0.0	12.5	-1.576e+04	-2.242e+04	0.0	0.0	0.0	-4.122e+06
30	34	-7.660e+05	0.0	-5.08e-03	-384.38	0.0	-3808.41	-1.362e+04	0.0	0.0	0.0	-7.660e+05
		-9.386e+05	0.0	0.0	0.0	12.5	-3808.41	-1.401e+04	0.0	0.0	0.0	-9.386e+05
30	35	-8.146e+05	0.0	-8.41e-03	-300.00	0.0	-4641.84	-6450.55	0.0	0.0	0.0	-8.146e+05
		-8.971e+05	0.0	0.0	0.0	12.5	-4641.84	-6750.55	0.0	0.0	0.0	-8.971e+05
30	36	-7.397e+05	0.0	-0.02	-384.38	0.0	-4114.97	-1.441e+04	0.0	0.0	0.0	-7.397e+05
		-9.223e+05	0.0	0.0	0.0	12.5	-4114.97	-1.480e+04	0.0	0.0	0.0	-9.223e+05
30	37	-7.883e+05	0.0	-0.04	-300.00	0.0	-4948.41	-7243.07	0.0	0.0	0.0	-7.883e+05
		-8.807e+05	0.0	0.0	0.0	12.5	-4948.41	-7543.07	0.0	0.0	0.0	-8.807e+05
30	38	-1.217e+06	0.0	-0.09	-300.00	0.0	-6367.72	-8813.15	0.0	0.0	0.0	-1.217e+06
		-1.329e+06	0.0	0.0	0.0	12.5	-6367.72	-9113.15	0.0	0.0	0.0	-1.329e+06
30	39	-5.333e+05	0.0	-3.71e-03	-384.38	0.0	-3304.24	-1.362e+04	0.0	0.0	0.0	-5.333e+05
		-7.060e+05	0.0	0.0	0.0	12.5	-3304.24	-1.401e+04	0.0	0.0	0.0	-7.060e+05
30	40	-3.056e+05	0.0	-7.67e-04	-300.00	0.0	-2972.67	-5700.00	0.0	0.0	0.0	-3.056e+05
		-3.787e+05	0.0	0.0	0.0	12.5	-2972.67	-6000.00	0.0	0.0	0.0	-3.787e+05
30	41	-9.723e+05	0.0	-0.02	-384.38	0.0	-4619.14	-1.441e+04	0.0	0.0	0.0	-9.723e+05
		-1.155e+06	0.0	0.0	0.0	12.5	-4619.14	-1.480e+04	0.0	0.0	0.0	-1.155e+06
30	42	-1.021e+06	0.0	-0.04	-300.00	0.0	-5452.57	-7243.07	0.0	0.0	0.0	-1.021e+06
		-1.113e+06	0.0	0.0	0.0	12.5	-5452.57	-7543.07	0.0	0.0	0.0	-1.113e+06
30	43	-1.450e+06	0.0	-0.09	-300.00	0.0	-6871.89	-8813.15	0.0	0.0	0.0	-1.450e+06
		-1.562e+06	0.0	0.0	0.0	12.5	-6871.89	-9113.15	0.0	0.0	0.0	-1.562e+06
30	44	-1.602e+06	0.0	-0.11	-384.38	0.0	-7076.22	-1.934e+04	0.0	0.0	0.0	-1.602e+06
		-1.846e+06	0.0	0.0	0.0	12.5	-7076.22	-1.972e+04	0.0	0.0	0.0	-1.846e+06
30	45	-1.523e+06	0.0	-0.09	-300.00	0.0	-7116.37	-8813.15	0.0	0.0	0.0	-1.523e+06
		-1.635e+06	0.0	0.0	0.0	12.5	-7116.37	-9113.15	0.0	0.0	0.0	-1.635e+06
30	46	-7.488e+05	0.0	-5.51e-03	-412.50	0.0	-3717.26	-1.626e+04	0.0	0.0	0.0	-7.488e+05
		-9.547e+05	0.0	0.0	0.0	12.5	-3717.26	-1.668e+04	0.0	0.0	0.0	-9.547e+05
30	47	-4.452e+05	0.0	-1.59e-03	-300.00	0.0	-3275.17	-5700.00	0.0	0.0	0.0	-4.452e+05
		-5.183e+05	0.0	0.0	0.0	12.5	-3275.17	-6000.00	0.0	0.0	0.0	-5.183e+05
30	48	-7.902e+05	0.0	-4.96e-03	-384.38	0.0	-3889.90	-1.362e+04	0.0	0.0	0.0	-7.902e+05
		-9.628e+05	0.0	0.0	0.0	12.5	-3889.90	-1.401e+04	0.0	0.0	0.0	-9.628e+05
30	49	-5.624e+05	0.0	-2.02e-03	-300.00	0.0	-3558.33	-5700.00	0.0	0.0	0.0	-5.624e+05
		-6.356e+05	0.0	0.0	0.0	12.5	-3558.33	-6000.00	0.0	0.0	0.0	-6.356e+05
30	50	-2.374e+06	0.0	-0.18	-384.38	0.0	-9466.11	-2.158e+04	0.0	0.0	0.0	-2.374e+06
		-2.646e+06	0.0	0.0	0.0	12.5	-1.004e+04	-2.197e+04	0.0	0.0	0.0	-2.646e+06

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
30	51	-2.422e+06	0.0	-0.19	-300.00	0.0	-1.030e+04	-1.441e+04	0.0	0.0	0.0	-2.422e+06
		-2.604e+06	0.0	0.0	0.0	12.5	-1.087e+04	-1.471e+04	0.0	0.0	0.0	-2.604e+06
30	52	-2.851e+06	0.0	-0.25	-300.00	0.0	-1.172e+04	-1.598e+04	0.0	0.0	0.0	-2.851e+06
		-3.053e+06	0.0	0.0	0.0	12.5	-1.229e+04	-1.628e+04	0.0	0.0	0.0	-3.053e+06
30	53	-5.536e+05	0.0	-0.03	-384.38	0.0	-3767.68	-1.441e+04	0.0	0.0	0.0	-5.536e+05
		-7.362e+05	0.0	0.0	0.0	12.5	-3767.68	-1.480e+04	0.0	0.0	0.0	-7.362e+05
30	54	-6.023e+05	0.0	-0.04	-300.00	0.0	-4601.12	-7243.07	0.0	0.0	0.0	-6.023e+05
		-6.947e+05	0.0	0.0	0.0	12.5	-4601.12	-7543.07	0.0	0.0	0.0	-6.947e+05
30	55	-1.031e+06	0.0	-0.09	-300.00	0.0	-6020.43	-8813.15	0.0	0.0	0.0	-1.031e+06
		-1.143e+06	0.0	0.0	0.0	12.5	-6020.43	-9113.15	0.0	0.0	0.0	-1.143e+06
30	56	-6.762e+05	0.0	-5.87e-03	-412.50	0.0	-3472.78	-1.626e+04	0.0	0.0	0.0	-6.762e+05
		-8.821e+05	0.0	0.0	0.0	12.5	-3472.78	-1.668e+04	0.0	0.0	0.0	-8.821e+05
30	57	-3.726e+05	0.0	-1.95e-03	-300.00	0.0	-3030.69	-5700.00	0.0	0.0	0.0	-3.726e+05
		-4.457e+05	0.0	0.0	0.0	12.5	-3030.69	-6000.00	0.0	0.0	0.0	-4.457e+05
30	58	-6.692e+05	0.0	-5.56e-03	-384.38	0.0	-3482.43	-1.362e+04	0.0	0.0	0.0	-6.692e+05
		-8.418e+05	0.0	0.0	0.0	12.5	-3482.43	-1.401e+04	0.0	0.0	0.0	-8.418e+05
30	59	-4.414e+05	0.0	-2.62e-03	-300.00	0.0	-3150.86	-5700.00	0.0	0.0	0.0	-4.414e+05
		-5.146e+05	0.0	0.0	0.0	12.5	-3150.86	-6000.00	0.0	0.0	0.0	-5.146e+05
30	60	-2.376e+06	0.0	-0.18	-384.38	0.0	-9472.22	-2.158e+04	0.0	0.0	0.0	-2.376e+06
		-2.648e+06	0.0	0.0	0.0	12.5	-1.004e+04	-2.197e+04	0.0	0.0	0.0	-2.648e+06
30	61	-2.424e+06	0.0	-0.19	-300.00	0.0	-1.031e+04	-1.441e+04	0.0	0.0	0.0	-2.424e+06
		-2.606e+06	0.0	0.0	0.0	12.5	-1.088e+04	-1.471e+04	0.0	0.0	0.0	-2.606e+06
30	62	-2.853e+06	0.0	-0.25	-300.00	0.0	-1.172e+04	-1.598e+04	0.0	0.0	0.0	-2.853e+06
		-3.055e+06	0.0	0.0	0.0	12.5	-1.229e+04	-1.628e+04	0.0	0.0	0.0	-3.055e+06
30	63	-6.038e+05	0.0	-0.03	-384.38	0.0	-3936.77	-1.441e+04	0.0	0.0	0.0	-6.038e+05
		-7.864e+05	0.0	0.0	0.0	12.5	-3936.77	-1.480e+04	0.0	0.0	0.0	-7.864e+05
30	64	-6.525e+05	0.0	-0.04	-300.00	0.0	-4770.21	-7243.07	0.0	0.0	0.0	-6.525e+05
		-7.449e+05	0.0	0.0	0.0	12.5	-4770.21	-7543.07	0.0	0.0	0.0	-7.449e+05
30	65	-1.082e+06	0.0	-0.09	-300.00	0.0	-6189.53	-8813.15	0.0	0.0	0.0	-1.082e+06
		-1.194e+06	0.0	0.0	0.0	12.5	-6189.53	-9113.15	0.0	0.0	0.0	-1.194e+06
30	66	-2.299e+06	0.0	-0.20	-384.38	0.0	-9344.98	-2.418e+04	0.0	0.0	0.0	-2.299e+06
		-2.604e+06	0.0	0.0	0.0	12.5	-9914.98	-2.457e+04	0.0	0.0	0.0	-2.604e+06
30	67	-5.277e+05	0.0	-0.05	-384.38	0.0	-3809.54	-1.702e+04	0.0	0.0	0.0	-5.277e+05
		-7.428e+05	0.0	0.0	0.0	12.5	-3809.54	-1.740e+04	0.0	0.0	0.0	-7.428e+05
30	68	-3.132e+06	0.0	-0.24	-300.00	0.0	-1.233e+04	-1.598e+04	0.0	0.0	0.0	-3.132e+06
		-3.334e+06	0.0	0.0	0.0	12.5	-1.290e+04	-1.628e+04	0.0	0.0	0.0	-3.334e+06
30	69	-1.547e+06	0.0	-0.09	-300.00	0.0	-7197.86	-8813.15	0.0	0.0	0.0	-1.547e+06
		-1.659e+06	0.0	0.0	0.0	12.5	-7197.86	-9113.15	0.0	0.0	0.0	-1.659e+06
30	70	-5.322e+05	0.0	-2.17e-03	-300.00	0.0	-3456.47	-5700.00	0.0	0.0	0.0	-5.322e+05
		-6.053e+05	0.0	0.0	0.0	12.5	-3456.47	-6000.00	0.0	0.0	0.0	-6.053e+05
30	71	-5.180e+05	0.0	-0.03	-300.00	0.0	-3803.78	-6492.52	0.0	0.0	0.0	-5.180e+05
		-6.010e+05	0.0	0.0	0.0	12.5	-3803.78	-6792.52	0.0	0.0	0.0	-6.010e+05
30	72	-2.996e+05	0.0	-7.97e-04	-300.00	0.0	-2952.30	-5700.00	0.0	0.0	0.0	-2.996e+05
		-3.727e+05	0.0	0.0	0.0	12.5	-2952.30	-6000.00	0.0	0.0	0.0	-3.727e+05
30	73	-7.506e+05	0.0	-0.03	-300.00	0.0	-4307.94	-6492.52	0.0	0.0	0.0	-7.506e+05
		-8.337e+05	0.0	0.0	0.0	12.5	-4307.94	-6792.52	0.0	0.0	0.0	-8.337e+05
30	74	-8.111e+05	0.0	-0.03	-300.00	0.0	-4511.68	-6492.52	0.0	0.0	0.0	-8.111e+05
		-8.942e+05	0.0	0.0	0.0	12.5	-4511.68	-6792.52	0.0	0.0	0.0	-8.942e+05
Trave		M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3		N	V 2	V 3	T		
		-4.544e+06	0.0	-6.10	-3.058e+04		-2.167e+04	-3.358e+04	0.0	0.0		

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		3.040e+06	0.0	6.11	0.0		3312.05	2.251e+04	0.0	0.0		

10.3. RISULTATI OPERE DI FONDAZIONE

Il controllo dei risultati delle analisi condotte, per quanto concerne le opere di fondazione, è possibile in relazione alle tabelle sottoriportate.

La tabella è riferita alle fondazioni tipo trave su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni alle estremità dell'elemento e la massima (in valore assoluto) pressione lungo lo sviluppo dell'elemento.

Vengono inoltre riportati, con funzione statistica, i valori massimo e minimo delle pressioni che compaiono nella tabella.

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm2	daN/cm2
1	1	-1.43	-1.43	-1.43	2	-0.93	-0.93	-0.93	3	-1.31	-1.30	-1.31
	4	-0.93	-0.93	-0.93	5	0.80	0.66	0.79	6	0.75	0.60	0.74
	7	1.89	1.70	1.88	8	-0.87	-0.89	-0.89	9	-0.91	-0.95	-0.95
	10	0.22	0.14	0.22	11	-1.43	-1.43	-1.43	12	-0.93	-0.93	-0.93
	13	-1.30	-1.30	-1.30	14	-0.93	-0.93	-0.93	15	0.80	0.66	0.79
	16	0.75	0.60	0.74	17	1.89	1.69	1.88	18	-0.87	-0.90	-0.90
	19	-0.92	-0.95	-0.95	20	0.22	0.14	0.22	21	1.10	0.93	1.09
	22	-0.57	-0.62	-0.62	23	2.13	1.94	2.12	24	0.46	0.38	0.46
	25	0.50	0.38	0.50	26	0.75	0.60	0.74	27	-0.60	-0.65	-0.65
	28	-0.92	-0.95	-0.95	29	1.89	1.69	1.88	30	0.61	0.50	0.61
	31	-0.34	-0.44	-0.44	32	1.00	0.88	0.99	33	1.89	1.70	1.88
	34	-0.97	-0.96	-0.97	35	-1.00	-1.01	-1.01	36	-0.74	-0.75	-0.75
	37	-0.77	-0.79	-0.79	38	0.07	0.02	0.07	39	-0.96	-0.96	-0.96
	40	-0.69	-0.69	-0.69	41	-0.74	-0.75	-0.75	42	-0.77	-0.80	-0.80
	43	0.07	0.02	0.07	44	0.01	-0.05	-0.05	45	0.07	0.02	0.07
	46	-1.06	-1.06	-1.06	47	-0.69	-0.69	-0.69	48	-0.97	-0.96	-0.97
	49	-0.69	-0.69	-0.69	50	0.50	0.40	0.49	51	0.46	0.35	0.46
	52	1.31	1.17	1.30	53	-0.74	-0.75	-0.75	54	-0.77	-0.79	-0.79
	55	0.07	0.02	0.07	56	-1.06	-1.06	-1.06	57	-0.69	-0.68	-0.69
	58	-0.96	-0.96	-0.96	59	-0.69	-0.68	-0.69	60	0.50	0.40	0.49
	61	0.46	0.35	0.46	62	1.31	1.17	1.30	63	-0.74	-0.75	-0.75
	64	-0.77	-0.79	-0.79	65	0.07	0.02	0.07	66	0.72	0.60	0.71
	67	-0.52	-0.55	-0.55	68	1.31	1.17	1.30	69	0.07	0.02	0.07
	70	-0.69	-0.69	-0.69	71	-0.46	-0.47	-0.47	72	-0.69	-0.69	-0.69
	73	-0.46	-0.47	-0.47	74	-0.46	-0.48	-0.48				
2	1	-1.43	-1.42	-1.43	2	-0.93	-0.93	-0.93	3	-1.30	-1.30	-1.30
	4	-0.93	-0.93	-0.93	5	0.66	0.48	0.65	6	0.60	0.41	0.59
	7	1.70	1.45	1.68	8	-0.89	-0.93	-0.93	9	-0.95	-1.00	-1.00
	10	0.14	0.04	0.14	11	-1.43	-1.42	-1.43	12	-0.93	-0.93	-0.93
	13	-1.30	-1.30	-1.30	14	-0.93	-0.92	-0.93	15	0.66	0.48	0.64
	16	0.60	0.40	0.58	17	1.69	1.45	1.68	18	-0.90	-0.93	-0.93
	19	-0.95	-1.00	-1.00	20	0.14	0.04	0.14	21	0.93	0.73	0.92
	22	-0.62	-0.68	-0.68	23	1.94	1.69	1.92	24	0.38	0.28	0.38
	25	0.38	0.23	0.37	26	0.60	0.40	0.58	27	-0.65	-0.72	-0.72

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
	28	-0.95	-1.00	-1.00	29	1.69	1.45	1.68	30	0.50	0.36	0.49
	31	-0.44	-0.56	-0.56	32	0.88	0.73	0.87	33	1.70	1.45	1.68
	34	-0.96	-0.96	-0.96	35	-1.01	-1.01	-1.01	36	-0.75	-0.77	-0.77
	37	-0.79	-0.82	-0.82	38	0.02	-0.05	-0.05	39	-0.96	-0.96	-0.96
	40	-0.69	-0.68	-0.69	41	-0.75	-0.77	-0.77	42	-0.80	-0.82	-0.82
	43	0.02	-0.05	-0.05	44	-0.05	-0.14	-0.14	45	0.02	-0.05	-0.05
	46	-1.06	-1.05	-1.06	47	-0.69	-0.69	-0.69	48	-0.96	-0.96	-0.96
	49	-0.69	-0.69	-0.69	50	0.40	0.27	0.39	51	0.35	0.22	0.35
	52	1.17	1.00	1.16	53	-0.75	-0.77	-0.77	54	-0.79	-0.82	-0.82
	55	0.02	-0.05	-0.05	56	-1.06	-1.05	-1.06	57	-0.68	-0.68	-0.68
	58	-0.96	-0.96	-0.96	59	-0.68	-0.68	-0.68	60	0.40	0.27	0.39
	61	0.35	0.22	0.35	62	1.17	1.00	1.16	63	-0.75	-0.77	-0.77
	64	-0.79	-0.82	-0.82	65	0.02	-0.05	-0.05	66	0.60	0.46	0.59
	67	-0.55	-0.58	-0.58	68	1.17	1.00	1.16	69	0.02	-0.05	-0.05
	70	-0.69	-0.69	-0.69	71	-0.47	-0.49	-0.49	72	-0.69	-0.68	-0.69
	73	-0.47	-0.49	-0.49	74	-0.48	-0.49	-0.49				
3	1	-1.42	-1.42	-1.42	2	-0.93	-0.93	-0.93	3	-1.30	-1.30	-1.30
	4	-0.93	-0.93	-0.93	5	0.48	0.39	0.47	6	0.41	0.31	0.40
	7	1.45	1.33	1.44	8	-0.93	-0.95	-0.95	9	-1.00	-1.03	-1.03
	10	0.04	-6.14e-03	0.04	11	-1.42	-1.42	-1.42	12	-0.93	-0.93	-0.93
	13	-1.30	-1.30	-1.30	14	-0.92	-0.92	-0.92	15	0.48	0.39	0.47
	16	0.40	0.31	0.40	17	1.45	1.33	1.44	18	-0.93	-0.95	-0.95
	19	-1.00	-1.03	-1.03	20	0.04	-6.61e-03	0.04	21	0.73	0.62	0.72
	22	-0.68	-0.71	-0.71	23	1.69	1.57	1.68	24	0.28	0.23	0.28
	25	0.23	0.15	0.22	26	0.40	0.31	0.40	27	-0.72	-0.76	-0.76
	28	-1.00	-1.03	-1.03	29	1.45	1.33	1.44	30	0.36	0.28	0.35
	31	-0.56	-0.63	-0.63	32	0.73	0.66	0.73	33	1.45	1.33	1.44
	34	-0.96	-0.96	-0.96	35	-1.01	-1.02	-1.02	36	-0.77	-0.78	-0.78
	37	-0.82	-0.84	-0.84	38	-0.05	-0.08	-0.08	39	-0.96	-0.96	-0.96
	40	-0.68	-0.68	-0.68	41	-0.77	-0.78	-0.78	42	-0.82	-0.84	-0.84
	43	-0.05	-0.08	-0.08	44	-0.14	-0.18	-0.18	45	-0.05	-0.08	-0.08
	46	-1.05	-1.05	-1.05	47	-0.69	-0.68	-0.69	48	-0.96	-0.96	-0.96
	49	-0.69	-0.69	-0.69	50	0.27	0.21	0.27	51	0.22	0.15	0.22
	52	1.00	0.91	0.99	53	-0.77	-0.78	-0.78	54	-0.82	-0.84	-0.84
	55	-0.05	-0.08	-0.08	56	-1.05	-1.05	-1.05	57	-0.68	-0.68	-0.68
	58	-0.96	-0.96	-0.96	59	-0.68	-0.68	-0.68	60	0.27	0.21	0.27
	61	0.22	0.15	0.22	62	1.00	0.91	0.99	63	-0.77	-0.78	-0.78
	64	-0.82	-0.84	-0.84	65	-0.05	-0.08	-0.08	66	0.46	0.39	0.45
	67	-0.58	-0.60	-0.60	68	1.00	0.91	0.99	69	-0.05	-0.08	-0.08
	70	-0.69	-0.69	-0.69	71	-0.49	-0.50	-0.50	72	-0.68	-0.68	-0.68
	73	-0.49	-0.50	-0.50	74	-0.49	-0.50	-0.50				
4	1	-1.42	-1.42	-1.42	2	-0.93	-0.92	-0.93	3	-1.30	-1.30	-1.30
	4	-0.93	-0.93	-0.93	5	0.39	0.30	0.38	6	0.31	0.21	0.30
	7	1.33	1.21	1.32	8	-0.95	-0.97	-0.97	9	-1.03	-1.05	-1.05
	10	-6.14e-03	-0.06	-0.06	11	-1.42	-1.42	-1.42	12	-0.93	-0.92	-0.93
	13	-1.30	-1.29	-1.30	14	-0.92	-0.92	-0.92	15	0.39	0.30	0.38
	16	0.31	0.21	0.30	17	1.33	1.21	1.32	18	-0.95	-0.97	-0.97
	19	-1.03	-1.05	-1.05	20	-6.61e-03	-0.06	-0.06	21	0.62	0.52	0.62
	22	-0.71	-0.74	-0.74	23	1.57	1.45	1.56	24	0.23	0.18	0.23
	25	0.15	0.07	0.14	26	0.31	0.21	0.30	27	-0.76	-0.79	-0.79
	28	-1.03	-1.05	-1.05	29	1.33	1.21	1.32	30	0.28	0.21	0.28

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
	31	-0.63	-0.69	-0.69	32	0.66	0.59	0.65	33	1.33	1.21	1.32
	34	-0.96	-0.96	-0.96	35	-1.02	-1.02	-1.02	36	-0.78	-0.79	-0.79
	37	-0.84	-0.85	-0.85	38	-0.08	-0.11	-0.11	39	-0.96	-0.96	-0.96
	40	-0.68	-0.68	-0.68	41	-0.78	-0.79	-0.79	42	-0.84	-0.85	-0.85
	43	-0.08	-0.11	-0.11	44	-0.18	-0.22	-0.22	45	-0.08	-0.11	-0.11
	46	-1.05	-1.05	-1.05	47	-0.68	-0.68	-0.68	48	-0.96	-0.96	-0.96
	49	-0.69	-0.68	-0.69	50	0.21	0.15	0.21	51	0.15	0.09	0.15
	52	0.91	0.82	0.90	53	-0.78	-0.79	-0.79	54	-0.84	-0.85	-0.85
	55	-0.08	-0.11	-0.11	56	-1.05	-1.05	-1.05	57	-0.68	-0.68	-0.68
	58	-0.96	-0.96	-0.96	59	-0.68	-0.68	-0.68	60	0.21	0.15	0.21
	61	0.15	0.09	0.15	62	0.91	0.82	0.90	63	-0.78	-0.79	-0.79
	64	-0.84	-0.85	-0.85	65	-0.08	-0.11	-0.11	66	0.39	0.32	0.38
	67	-0.60	-0.62	-0.62	68	0.91	0.82	0.90	69	-0.08	-0.11	-0.11
	70	-0.69	-0.68	-0.69	71	-0.50	-0.51	-0.51	72	-0.68	-0.68	-0.68
	73	-0.50	-0.51	-0.51	74	-0.50	-0.51	-0.51				
5	1	-1.42	-1.39	-1.42	2	-0.92	-0.91	-0.92	3	-1.30	-1.27	-1.29
	4	-0.93	-0.91	-0.92	5	0.30	-1.28	-1.28	6	0.21	-1.46	-1.46
	7	1.21	-0.92	1.07	8	-0.97	-1.28	-1.28	9	-1.05	-1.46	-1.46
	10	-0.06	-0.92	-0.92	11	-1.42	-1.39	-1.42	12	-0.92	-0.91	-0.92
	13	-1.29	-1.27	-1.29	14	-0.92	-0.92	-0.92	15	0.30	-1.28	-1.28
	16	0.21	-1.46	-1.46	17	1.21	-0.92	1.07	18	-0.97	-1.28	-1.28
	19	-1.05	-1.46	-1.46	20	-0.06	-0.92	-0.92	21	0.52	-1.28	-1.28
	22	-0.74	-1.28	-1.28	23	1.45	-0.68	1.31	24	0.18	-0.68	-0.68
	25	0.07	-1.28	-1.28	26	0.21	-1.46	-1.46	27	-0.79	-1.40	-1.40
	28	-1.05	-1.46	-1.46	29	1.21	-0.92	1.07	30	0.21	-1.04	-1.04
	31	-0.69	-1.77	-1.77	32	0.59	-0.69	-0.69	33	1.21	-0.92	1.07
	34	-0.96	-0.94	-0.96	35	-1.02	-1.08	-1.08	36	-0.79	-0.95	-0.95
	37	-0.85	-1.08	-1.08	38	-0.11	-0.68	-0.68	39	-0.96	-0.95	-0.96
	40	-0.68	-0.68	-0.68	41	-0.79	-0.95	-0.95	42	-0.85	-1.08	-1.08
	43	-0.11	-0.68	-0.68	44	-0.22	-0.95	-0.95	45	-0.11	-0.68	-0.68
	46	-1.05	-1.03	-1.05	47	-0.68	-0.68	-0.68	48	-0.96	-0.94	-0.96
	49	-0.68	-0.68	-0.68	50	0.15	-0.95	-0.95	51	0.09	-1.08	-1.08
	52	0.82	-0.68	0.73	53	-0.79	-0.95	-0.95	54	-0.85	-1.08	-1.08
	55	-0.11	-0.68	-0.68	56	-1.05	-1.03	-1.05	57	-0.68	-0.68	-0.68
	58	-0.96	-0.95	-0.96	59	-0.68	-0.68	-0.68	60	0.15	-0.95	-0.95
	61	0.09	-1.08	-1.08	62	0.82	-0.68	0.73	63	-0.79	-0.95	-0.95
	64	-0.85	-1.08	-1.08	65	-0.11	-0.68	-0.68	66	0.32	-0.95	-0.95
	67	-0.62	-0.95	-0.95	68	0.82	-0.68	0.73	69	-0.11	-0.68	-0.68
	70	-0.68	-0.68	-0.68	71	-0.51	-0.68	-0.68	72	-0.68	-0.68	-0.68
	73	-0.51	-0.68	-0.68	74	-0.51	-0.68	-0.68				
6	1	-1.39	-1.42	-1.42	2	-0.91	-0.92	-0.92	3	-1.27	-1.30	-1.30
	4	-0.91	-0.93	-0.93	5	-1.28	-2.88	-2.88	6	-1.46	-3.13	-3.13
	7	-0.92	-3.05	-3.05	8	-1.28	-1.62	-1.62	9	-1.46	-1.87	-1.87
	10	-0.92	-1.79	-1.79	11	-1.39	-1.42	-1.42	12	-0.91	-0.92	-0.92
	13	-1.27	-1.29	-1.29	14	-0.92	-0.92	-0.92	15	-1.28	-2.89	-2.89
	16	-1.46	-3.13	-3.13	17	-0.92	-3.05	-3.05	18	-1.28	-1.62	-1.62
	19	-1.46	-1.87	-1.87	20	-0.92	-1.79	-1.79	21	-1.28	-3.11	-3.11
	22	-1.28	-1.85	-1.85	23	-0.68	-2.81	-2.81	24	-0.68	-1.55	-1.55
	25	-1.28	-2.66	-2.66	26	-1.46	-3.13	-3.13	27	-1.40	-2.05	-2.05
	28	-1.46	-1.87	-1.87	29	-0.92	-3.05	-3.05	30	-1.04	-2.32	-2.32
	31	-1.77	-2.82	-2.82	32	-0.69	-1.94	-1.94	33	-0.92	-3.05	-3.05

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
	34	-0.94	-0.96	-0.96	35	-1.08	-1.14	-1.14	36	-0.95	-1.13	-1.13
	37	-1.08	-1.31	-1.31	38	-0.68	-1.25	-1.25	39	-0.95	-0.96	-0.96
	40	-0.68	-0.68	-0.68	41	-0.95	-1.13	-1.13	42	-1.08	-1.31	-1.31
	43	-0.68	-1.25	-1.25	44	-0.95	-1.70	-1.70	45	-0.68	-1.25	-1.25
	46	-1.03	-1.05	-1.05	47	-0.68	-0.68	-0.68	48	-0.94	-0.96	-0.96
	49	-0.68	-0.68	-0.68	50	-0.95	-2.07	-2.07	51	-1.08	-2.25	-2.25
	52	-0.68	-2.19	-2.19	53	-0.95	-1.13	-1.13	54	-1.08	-1.31	-1.31
	55	-0.68	-1.25	-1.25	56	-1.03	-1.05	-1.05	57	-0.68	-0.68	-0.68
	58	-0.95	-0.96	-0.96	59	-0.68	-0.68	-0.68	60	-0.95	-2.07	-2.07
	61	-1.08	-2.25	-2.25	62	-0.68	-2.19	-2.19	63	-0.95	-1.13	-1.13
	64	-1.08	-1.31	-1.31	65	-0.68	-1.25	-1.25	66	-0.95	-2.23	-2.23
	67	-0.95	-1.30	-1.30	68	-0.68	-2.19	-2.19	69	-0.68	-1.25	-1.25
	70	-0.68	-0.68	-0.68	71	-0.68	-0.85	-0.85	72	-0.68	-0.68	-0.68
	73	-0.68	-0.85	-0.85	74	-0.68	-0.85	-0.85				
7	1	-1.42	-1.42	-1.42	2	-0.92	-0.93	-0.93	3	-1.30	-1.30	-1.30
	4	-0.93	-0.93	-0.93	5	-2.88	-2.98	-2.98	6	-3.13	-3.23	-3.23
	7	-3.05	-3.17	-3.17	8	-1.62	-1.64	-1.64	9	-1.87	-1.89	-1.89
	10	-1.79	-1.84	-1.84	11	-1.42	-1.42	-1.42	12	-0.92	-0.93	-0.93
	13	-1.29	-1.30	-1.30	14	-0.92	-0.92	-0.92	15	-2.89	-2.98	-2.98
	16	-3.13	-3.23	-3.23	17	-3.05	-3.17	-3.17	18	-1.62	-1.64	-1.64
	19	-1.87	-1.89	-1.89	20	-1.79	-1.84	-1.84	21	-3.11	-3.21	-3.21
	22	-1.85	-1.88	-1.88	23	-2.81	-2.93	-2.93	24	-1.55	-1.60	-1.60
	25	-2.66	-2.74	-2.74	26	-3.13	-3.23	-3.23	27	-2.05	-2.08	-2.08
	28	-1.87	-1.89	-1.89	29	-3.05	-3.17	-3.17	30	-2.32	-2.39	-2.39
	31	-2.82	-2.88	-2.88	32	-1.94	-2.01	-2.01	33	-3.05	-3.17	-3.17
	34	-0.96	-0.96	-0.96	35	-1.14	-1.15	-1.15	36	-1.13	-1.14	-1.14
	37	-1.31	-1.33	-1.33	38	-1.25	-1.29	-1.29	39	-0.96	-0.96	-0.96
	40	-0.68	-0.68	-0.68	41	-1.13	-1.14	-1.14	42	-1.31	-1.33	-1.33
	43	-1.25	-1.29	-1.29	44	-1.70	-1.74	-1.74	45	-1.25	-1.29	-1.29
	46	-1.05	-1.05	-1.05	47	-0.68	-0.68	-0.68	48	-0.96	-0.96	-0.96
	49	-0.68	-0.69	-0.69	50	-2.07	-2.13	-2.13	51	-2.25	-2.32	-2.32
	52	-2.19	-2.27	-2.27	53	-1.13	-1.14	-1.14	54	-1.31	-1.33	-1.33
	55	-1.25	-1.28	-1.28	56	-1.05	-1.05	-1.05	57	-0.68	-0.68	-0.68
	58	-0.96	-0.96	-0.96	59	-0.68	-0.68	-0.68	60	-2.07	-2.13	-2.13
	61	-2.25	-2.32	-2.32	62	-2.19	-2.27	-2.27	63	-1.13	-1.14	-1.14
	64	-1.31	-1.33	-1.33	65	-1.25	-1.29	-1.29	66	-2.23	-2.31	-2.31
	67	-1.30	-1.32	-1.32	68	-2.19	-2.28	-2.28	69	-1.25	-1.29	-1.29
	70	-0.68	-0.69	-0.69	71	-0.85	-0.86	-0.86	72	-0.68	-0.68	-0.68
	73	-0.85	-0.86	-0.86	74	-0.85	-0.86	-0.86				
8	1	-1.42	-1.42	-1.42	2	-0.93	-0.93	-0.93	3	-1.30	-1.30	-1.30
	4	-0.93	-0.93	-0.93	5	-2.98	-3.07	-3.07	6	-3.23	-3.32	-3.32
	7	-3.17	-3.29	-3.29	8	-1.64	-1.66	-1.66	9	-1.89	-1.91	-1.91
	10	-1.84	-1.89	-1.89	11	-1.42	-1.42	-1.42	12	-0.93	-0.93	-0.93
	13	-1.30	-1.30	-1.30	14	-0.92	-0.92	-0.92	15	-2.98	-3.07	-3.07
	16	-3.23	-3.32	-3.32	17	-3.17	-3.29	-3.29	18	-1.64	-1.66	-1.66
	19	-1.89	-1.92	-1.92	20	-1.84	-1.89	-1.89	21	-3.21	-3.32	-3.32
	22	-1.88	-1.91	-1.91	23	-2.93	-3.05	-3.05	24	-1.60	-1.65	-1.65
	25	-2.74	-2.82	-2.82	26	-3.23	-3.32	-3.32	27	-2.08	-2.12	-2.12
	28	-1.89	-1.92	-1.92	29	-3.17	-3.29	-3.29	30	-2.39	-2.46	-2.46
	31	-2.88	-2.94	-2.94	32	-2.01	-2.08	-2.08	33	-3.17	-3.29	-3.29
	34	-0.96	-0.96	-0.96	35	-1.15	-1.15	-1.15	36	-1.14	-1.15	-1.15

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
	37	-1.33	-1.34	-1.34	38	-1.29	-1.32	-1.32	39	-0.96	-0.96	-0.96
	40	-0.68	-0.68	-0.68	41	-1.14	-1.15	-1.15	42	-1.33	-1.34	-1.34
	43	-1.29	-1.32	-1.32	44	-1.74	-1.78	-1.78	45	-1.29	-1.32	-1.32
	46	-1.05	-1.05	-1.05	47	-0.68	-0.69	-0.69	48	-0.96	-0.96	-0.96
	49	-0.69	-0.69	-0.69	50	-2.13	-2.19	-2.19	51	-2.32	-2.38	-2.38
	52	-2.27	-2.36	-2.36	53	-1.14	-1.15	-1.15	54	-1.33	-1.34	-1.34
	55	-1.28	-1.32	-1.32	56	-1.05	-1.05	-1.05	57	-0.68	-0.68	-0.68
	58	-0.96	-0.96	-0.96	59	-0.68	-0.68	-0.68	60	-2.13	-2.19	-2.19
	61	-2.32	-2.38	-2.38	62	-2.27	-2.36	-2.36	63	-1.14	-1.15	-1.15
	64	-1.33	-1.34	-1.34	65	-1.29	-1.32	-1.32	66	-2.31	-2.38	-2.38
	67	-1.32	-1.34	-1.34	68	-2.28	-2.36	-2.36	69	-1.29	-1.32	-1.32
	70	-0.69	-0.69	-0.69	71	-0.86	-0.87	-0.87	72	-0.68	-0.68	-0.68
	73	-0.86	-0.87	-0.87	74	-0.86	-0.87	-0.87				
9	1	-1.42	-1.43	-1.43	2	-0.93	-0.93	-0.93	3	-1.30	-1.30	-1.30
	4	-0.93	-0.93	-0.93	5	-3.07	-3.25	-3.25	6	-3.32	-3.51	-3.51
	7	-3.29	-3.54	-3.54	8	-1.66	-1.70	-1.70	9	-1.91	-1.96	-1.96
	10	-1.89	-1.98	-1.98	11	-1.42	-1.43	-1.43	12	-0.93	-0.93	-0.93
	13	-1.30	-1.30	-1.30	14	-0.92	-0.93	-0.93	15	-3.07	-3.25	-3.25
	16	-3.32	-3.52	-3.52	17	-3.29	-3.54	-3.54	18	-1.66	-1.70	-1.70
	19	-1.92	-1.96	-1.96	20	-1.89	-1.99	-1.99	21	-3.32	-3.53	-3.53
	22	-1.91	-1.97	-1.97	23	-3.05	-3.30	-3.30	24	-1.65	-1.75	-1.75
	25	-2.82	-2.98	-2.98	26	-3.32	-3.51	-3.51	27	-2.12	-2.19	-2.19
	28	-1.92	-1.96	-1.96	29	-3.29	-3.54	-3.54	30	-2.46	-2.61	-2.61
	31	-2.94	-3.06	-3.06	32	-2.08	-2.23	-2.23	33	-3.29	-3.54	-3.54
	34	-0.96	-0.96	-0.96	35	-1.15	-1.16	-1.16	36	-1.15	-1.17	-1.17
	37	-1.34	-1.36	-1.36	38	-1.32	-1.38	-1.38	39	-0.96	-0.96	-0.96
	40	-0.68	-0.69	-0.69	41	-1.15	-1.17	-1.17	42	-1.34	-1.37	-1.37
	43	-1.32	-1.38	-1.38	44	-1.78	-1.86	-1.86	45	-1.32	-1.38	-1.38
	46	-1.05	-1.06	-1.06	47	-0.69	-0.69	-0.69	48	-0.96	-0.96	-0.96
	49	-0.69	-0.69	-0.69	50	-2.19	-2.32	-2.32	51	-2.38	-2.51	-2.51
	52	-2.36	-2.53	-2.53	53	-1.15	-1.17	-1.17	54	-1.34	-1.36	-1.36
	55	-1.32	-1.38	-1.38	56	-1.05	-1.06	-1.06	57	-0.68	-0.68	-0.68
	58	-0.96	-0.96	-0.96	59	-0.68	-0.68	-0.68	60	-2.19	-2.32	-2.32
	61	-2.38	-2.51	-2.51	62	-2.36	-2.53	-2.53	63	-1.15	-1.17	-1.17
	64	-1.34	-1.37	-1.37	65	-1.32	-1.38	-1.38	66	-2.38	-2.52	-2.52
	67	-1.34	-1.37	-1.37	68	-2.36	-2.53	-2.53	69	-1.32	-1.38	-1.38
	70	-0.69	-0.69	-0.69	71	-0.87	-0.89	-0.89	72	-0.68	-0.69	-0.69
	73	-0.87	-0.89	-0.89	74	-0.87	-0.89	-0.89				
10	1	-1.43	-1.43	-1.43	2	-0.93	-0.93	-0.93	3	-1.30	-1.31	-1.31
	4	-0.93	-0.93	-0.93	5	-3.25	-3.40	-3.40	6	-3.51	-3.67	-3.67
	7	-3.54	-3.73	-3.73	8	-1.70	-1.73	-1.73	9	-1.96	-2.00	-2.00
	10	-1.98	-2.06	-2.06	11	-1.43	-1.43	-1.43	12	-0.93	-0.93	-0.93
	13	-1.30	-1.30	-1.30	14	-0.93	-0.93	-0.93	15	-3.25	-3.40	-3.40
	16	-3.52	-3.67	-3.67	17	-3.54	-3.73	-3.73	18	-1.70	-1.73	-1.73
	19	-1.96	-2.00	-2.00	20	-1.99	-2.06	-2.06	21	-3.53	-3.69	-3.69
	22	-1.97	-2.03	-2.03	23	-3.30	-3.49	-3.49	24	-1.75	-1.82	-1.82
	25	-2.98	-3.10	-3.10	26	-3.51	-3.67	-3.67	27	-2.19	-2.25	-2.25
	28	-1.96	-2.00	-2.00	29	-3.54	-3.73	-3.73	30	-2.61	-2.72	-2.72
	31	-3.06	-3.15	-3.15	32	-2.23	-2.34	-2.34	33	-3.54	-3.73	-3.73
	34	-0.96	-0.97	-0.97	35	-1.16	-1.16	-1.16	36	-1.17	-1.19	-1.19
	37	-1.36	-1.39	-1.39	38	-1.38	-1.43	-1.43	39	-0.96	-0.96	-0.96

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
	40	-0.69	-0.69	-0.69	41	-1.17	-1.19	-1.19	42	-1.37	-1.39	-1.39
	43	-1.38	-1.44	-1.44	44	-1.86	-1.93	-1.93	45	-1.38	-1.44	-1.44
	46	-1.06	-1.06	-1.06	47	-0.69	-0.69	-0.69	48	-0.96	-0.97	-0.97
	49	-0.69	-0.69	-0.69	50	-2.32	-2.42	-2.42	51	-2.51	-2.62	-2.62
	52	-2.53	-2.67	-2.67	53	-1.17	-1.19	-1.19	54	-1.36	-1.39	-1.39
	55	-1.38	-1.43	-1.43	56	-1.06	-1.06	-1.06	57	-0.68	-0.69	-0.69
	58	-0.96	-0.96	-0.96	59	-0.68	-0.69	-0.69	60	-2.32	-2.42	-2.42
	61	-2.51	-2.62	-2.62	62	-2.53	-2.67	-2.67	63	-1.17	-1.19	-1.19
	64	-1.37	-1.39	-1.39	65	-1.38	-1.43	-1.43	66	-2.52	-2.64	-2.64
	67	-1.37	-1.41	-1.41	68	-2.53	-2.67	-2.67	69	-1.38	-1.44	-1.44
	70	-0.69	-0.69	-0.69	71	-0.89	-0.91	-0.91	72	-0.69	-0.69	-0.69
	73	-0.89	-0.91	-0.91	74	-0.89	-0.91	-0.91				
Elem.		**Pt ini**	**Pt fin**	**Pt max**		**Pt ini**	**Pt fin**	**Pt max**		**Pt ini**	**Pt fin**	**Pt max**
		-3.73										
		2.13										

11. ALLEGATO B. – MURO AD U - CALCOLO FEM - OUTPUT

PRO_SAP
PROFESSIONAL STRUCTURAL ANALYSIS PROGRAM

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste nel D.M. 14 Gennaio 2008 cap. 10 "Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo"

2S.I. SOFTWARE E SERVIZI PER L'INGEGNERIA SRL
P.tta Schiatti 8/b
44100 FERRARA (ITALY)
tel. 39 532 200091 – fax 39 532 200086
www.2si.it **info@2si.it**

D.M. 14/01/08 cap. 10.2 Affidabilità dei codici utilizzati:
www.2si.it/software/Affidabilità.htm

11.1. RISULTATI NODALI

Il controllo dei risultati delle analisi condotte, per quanto concerne i nodi strutturali, è possibile in relazione alle tabelle sottoriportate.

Una prima tabella riporta infatti per ogni nodo e per ogni combinazione (o caso di carico) gli spostamenti nodali.

Una seconda tabella, infine riassume per ogni nodo le sei combinazioni in cui si attingono i valori minimi e massimi della reazione Fz, della reazione Mx e della reazione My.

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
		cm	cm	cm			
1	1	0.0	0.0	-1.87	2.41e-04	0.0	0.0
1	2	0.0	1.69e-03	-1.74	-8.57e-04	0.0	0.0
1	3	0.0	0.08	-1.25	-2.70e-03	0.0	0.0
1	4	0.0	0.16	-2.44	-4.27e-03	0.0	0.0
1	5	0.0	0.08	-0.77	-2.76e-03	0.0	0.0
1	6	0.0	0.08	-0.77	-2.76e-03	0.0	0.0
1	7	0.0	2.85e-03	-4.93	2.84e-04	0.0	0.0
1	8	0.0	2.28e-03	-1.22	-1.30e-03	0.0	0.0
1	9	0.0	0.0	-1.38	1.78e-04	0.0	0.0
1	10	0.0	1.69e-03	-1.26	-9.19e-04	0.0	0.0
1	11	0.0	0.06	-2.14	-2.09e-03	0.0	0.0
1	12	0.0	0.0	-1.38	1.78e-04	0.0	0.0
1	13	0.0	1.69e-03	-1.26	-9.19e-04	0.0	0.0
1	14	0.0	0.06	-2.14	-2.09e-03	0.0	0.0
1	15	0.0	0.0	-1.38	1.78e-04	0.0	0.0
1	16	0.0	0.0	-1.38	1.78e-04	0.0	0.0
1	17	0.0	0.07	-0.91	-2.68e-03	0.0	0.0
1	18	0.0	0.22	0.33	-6.88e-03	0.0	0.0
1	19	0.0	0.07	-0.91	-2.68e-03	0.0	0.0
1	20	0.0	0.22	0.33	-6.88e-03	0.0	0.0
1	21	0.0	0.22	0.41	-6.91e-03	0.0	0.0
2	1	0.0	0.0	-1.86	2.41e-04	0.0	0.0
2	2	0.0	1.69e-03	-1.76	-8.57e-04	0.0	0.0
2	3	0.0	0.08	-1.31	-2.70e-03	0.0	0.0
2	4	0.0	0.16	-2.52	-4.27e-03	0.0	0.0
2	5	0.0	0.08	-0.82	-2.76e-03	0.0	0.0
2	6	0.0	0.08	-0.82	-2.76e-03	0.0	0.0
2	7	0.0	2.85e-03	-4.93	2.84e-04	0.0	0.0
2	8	0.0	2.28e-03	-1.24	-1.30e-03	0.0	0.0
2	9	0.0	0.0	-1.38	1.79e-04	0.0	0.0
2	10	0.0	1.69e-03	-1.28	-9.19e-04	0.0	0.0
2	11	0.0	0.06	-2.18	-2.09e-03	0.0	0.0
2	12	0.0	0.0	-1.38	1.79e-04	0.0	0.0
2	13	0.0	1.69e-03	-1.28	-9.19e-04	0.0	0.0
2	14	0.0	0.06	-2.18	-2.09e-03	0.0	0.0
2	15	0.0	0.0	-1.38	1.79e-04	0.0	0.0
2	16	0.0	0.0	-1.38	1.79e-04	0.0	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
2	17	0.0	0.07	-0.96	-2.68e-03	0.0	0.0
2	18	0.0	0.22	0.19	-6.88e-03	0.0	0.0
2	19	0.0	0.07	-0.96	-2.68e-03	0.0	0.0
2	20	0.0	0.22	0.19	-6.88e-03	0.0	0.0
2	21	0.0	0.22	0.27	-6.91e-03	0.0	0.0
3	1	0.0	0.0	-1.86	2.42e-04	0.0	0.0
3	2	0.0	1.69e-03	-1.78	-8.56e-04	0.0	0.0
3	3	0.0	0.08	-1.38	-2.70e-03	0.0	0.0
3	4	0.0	0.16	-2.63	-4.27e-03	0.0	0.0
3	5	0.0	0.08	-0.89	-2.76e-03	0.0	0.0
3	6	0.0	0.08	-0.89	-2.76e-03	0.0	0.0
3	7	0.0	2.85e-03	-4.92	2.88e-04	0.0	0.0
3	8	0.0	2.28e-03	-1.28	-1.30e-03	0.0	0.0
3	9	0.0	0.0	-1.38	1.79e-04	0.0	0.0
3	10	0.0	1.69e-03	-1.30	-9.19e-04	0.0	0.0
3	11	0.0	0.06	-2.23	-2.09e-03	0.0	0.0
3	12	0.0	0.0	-1.38	1.79e-04	0.0	0.0
3	13	0.0	1.69e-03	-1.30	-9.19e-04	0.0	0.0
3	14	0.0	0.06	-2.23	-2.09e-03	0.0	0.0
3	15	0.0	0.0	-1.38	1.79e-04	0.0	0.0
3	16	0.0	0.0	-1.38	1.79e-04	0.0	0.0
3	17	0.0	0.07	-1.03	-2.68e-03	0.0	0.0
3	18	0.0	0.22	0.02	-6.89e-03	0.0	0.0
3	19	0.0	0.07	-1.03	-2.68e-03	0.0	0.0
3	20	0.0	0.22	0.02	-6.89e-03	0.0	0.0
3	21	0.0	0.22	0.10	-6.91e-03	0.0	0.0
4	1	0.0	0.0	-1.85	2.42e-04	0.0	0.0
4	2	0.0	1.61e-03	-1.79	-8.01e-04	0.0	0.0
4	3	0.0	0.08	-1.41	-2.63e-03	0.0	0.0
4	4	0.0	0.16	-2.68	-4.17e-03	0.0	0.0
4	5	0.0	0.08	-0.93	-2.69e-03	0.0	0.0
4	6	0.0	0.08	-0.93	-2.69e-03	0.0	0.0
4	7	0.0	2.71e-03	-4.91	3.94e-04	0.0	0.0
4	8	0.0	2.17e-03	-1.29	-1.23e-03	0.0	0.0
4	9	0.0	0.0	-1.37	1.79e-04	0.0	0.0
4	10	0.0	1.61e-03	-1.31	-8.63e-04	0.0	0.0
4	11	0.0	0.06	-2.26	-2.01e-03	0.0	0.0
4	12	0.0	0.0	-1.37	1.79e-04	0.0	0.0
4	13	0.0	1.61e-03	-1.31	-8.63e-04	0.0	0.0
4	14	0.0	0.06	-2.26	-2.01e-03	0.0	0.0
4	15	0.0	0.0	-1.37	1.79e-04	0.0	0.0
4	16	0.0	0.0	-1.37	1.79e-04	0.0	0.0
4	17	0.0	0.07	-1.06	-2.60e-03	0.0	0.0
4	18	0.0	0.22	-0.07	-6.78e-03	0.0	0.0
4	19	0.0	0.07	-1.06	-2.60e-03	0.0	0.0
4	20	0.0	0.22	-0.07	-6.78e-03	0.0	0.0
4	21	0.0	0.22	0.01	-6.80e-03	0.0	0.0
5	1	0.0	0.0	-1.85	2.40e-04	0.0	0.0
5	2	0.0	1.52e-03	-1.80	-7.47e-04	0.0	0.0
5	3	0.0	0.08	-1.44	-2.55e-03	0.0	0.0
5	4	0.0	0.16	-2.73	-4.07e-03	0.0	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
5	5	0.0	0.08	-0.96	-2.62e-03	0.0	0.0
5	6	0.0	0.08	-0.96	-2.62e-03	0.0	0.0
5	7	0.0	2.56e-03	-4.91	5.00e-04	0.0	0.0
5	8	0.0	2.05e-03	-1.31	-1.15e-03	0.0	0.0
5	9	0.0	0.0	-1.37	1.78e-04	0.0	0.0
5	10	0.0	1.52e-03	-1.32	-8.09e-04	0.0	0.0
5	11	0.0	0.06	-2.28	-1.93e-03	0.0	0.0
5	12	0.0	0.0	-1.37	1.78e-04	0.0	0.0
5	13	0.0	1.52e-03	-1.32	-8.09e-04	0.0	0.0
5	14	0.0	0.06	-2.28	-1.93e-03	0.0	0.0
5	15	0.0	0.0	-1.37	1.78e-04	0.0	0.0
5	16	0.0	0.0	-1.37	1.78e-04	0.0	0.0
5	17	0.0	0.07	-1.09	-2.54e-03	0.0	0.0
5	18	0.0	0.22	-0.15	-6.67e-03	0.0	0.0
5	19	0.0	0.07	-1.09	-2.54e-03	0.0	0.0
5	20	0.0	0.22	-0.15	-6.67e-03	0.0	0.0
5	21	0.0	0.22	-0.07	-6.69e-03	0.0	0.0
6	1	0.0	0.0	-1.82	0.0	0.0	0.0
6	2	0.0	0.0	-1.88	0.0	0.0	0.0
6	3	0.0	0.08	-1.89	-1.54e-03	0.0	0.0
6	4	0.0	0.16	-3.46	-2.50e-03	0.0	0.0
6	5	0.0	0.08	-1.42	-1.54e-03	0.0	0.0
6	6	0.0	0.08	-1.42	-1.54e-03	0.0	0.0
6	7	0.0	0.0	-4.57	2.52e-03	0.0	0.0
6	8	0.0	0.0	-1.43	0.0	0.0	0.0
6	9	0.0	0.0	-1.35	0.0	0.0	0.0
6	10	0.0	0.0	-1.41	0.0	0.0	0.0
6	11	0.0	0.06	-2.58	-7.07e-04	0.0	0.0
6	12	0.0	0.0	-1.35	0.0	0.0	0.0
6	13	0.0	0.0	-1.41	0.0	0.0	0.0
6	14	0.0	0.06	-2.58	-7.07e-04	0.0	0.0
6	15	0.0	0.0	-1.35	0.0	0.0	0.0
6	16	0.0	0.0	-1.35	0.0	0.0	0.0
6	17	0.0	0.07	-1.55	-1.56e-03	0.0	0.0
6	18	0.0	0.22	-1.47	-5.20e-03	0.0	0.0
6	19	0.0	0.07	-1.55	-1.56e-03	0.0	0.0
6	20	0.0	0.22	-1.47	-5.20e-03	0.0	0.0
6	21	0.0	0.22	-1.40	-5.20e-03	0.0	0.0
7	1	0.0	0.0	-1.85	-2.40e-04	0.0	0.0
7	2	0.0	-1.52e-03	-1.80	7.47e-04	0.0	0.0
7	3	0.0	0.08	-2.15	-7.14e-04	0.0	0.0
7	4	0.0	0.16	-3.89	-1.40e-03	0.0	0.0
7	5	0.0	0.08	-1.67	-6.52e-04	0.0	0.0
7	6	0.0	0.08	-1.67	-6.52e-04	0.0	0.0
7	7	0.0	-2.56e-03	-3.78	4.47e-03	0.0	0.0
7	8	0.0	-2.05e-03	-1.31	1.15e-03	0.0	0.0
7	9	0.0	0.0	-1.37	-1.78e-04	0.0	0.0
7	10	0.0	-1.52e-03	-1.32	8.09e-04	0.0	0.0
7	11	0.0	0.06	-2.62	3.02e-04	0.0	0.0
7	12	0.0	0.0	-1.37	-1.78e-04	0.0	0.0
7	13	0.0	-1.52e-03	-1.32	8.09e-04	0.0	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
7	14	0.0	0.06	-2.62	3.02e-04	0.0	0.0
7	15	0.0	0.0	-1.37	-1.78e-04	0.0	0.0
7	16	0.0	0.0	-1.37	-1.78e-04	0.0	0.0
7	17	0.0	0.06	-1.81	-7.67e-04	0.0	0.0
7	18	0.0	0.22	-2.54	-4.33e-03	0.0	0.0
7	19	0.0	0.06	-1.81	-7.67e-04	0.0	0.0
7	20	0.0	0.22	-2.54	-4.33e-03	0.0	0.0
7	21	0.0	0.22	-2.46	-4.31e-03	0.0	0.0
8	1	0.0	0.0	-1.85	-2.42e-04	0.0	0.0
8	2	0.0	-1.61e-03	-1.79	8.01e-04	0.0	0.0
8	3	0.0	0.08	-2.16	-6.60e-04	0.0	0.0
8	4	0.0	0.16	-3.91	-1.34e-03	0.0	0.0
8	5	0.0	0.08	-1.68	-5.97e-04	0.0	0.0
8	6	0.0	0.08	-1.68	-5.97e-04	0.0	0.0
8	7	0.0	-2.71e-03	-3.73	4.57e-03	0.0	0.0
8	8	0.0	-2.17e-03	-1.29	1.23e-03	0.0	0.0
8	9	0.0	0.0	-1.37	-1.79e-04	0.0	0.0
8	10	0.0	-1.61e-03	-1.31	8.63e-04	0.0	0.0
8	11	0.0	0.06	-2.62	3.58e-04	0.0	0.0
8	12	0.0	0.0	-1.37	-1.79e-04	0.0	0.0
8	13	0.0	-1.61e-03	-1.31	8.63e-04	0.0	0.0
8	14	0.0	0.06	-2.62	3.58e-04	0.0	0.0
8	15	0.0	0.0	-1.37	-1.79e-04	0.0	0.0
8	16	0.0	0.0	-1.37	-1.79e-04	0.0	0.0
8	17	0.0	0.06	-1.82	-7.16e-04	0.0	0.0
8	18	0.0	0.22	-2.59	-4.29e-03	0.0	0.0
8	19	0.0	0.06	-1.82	-7.16e-04	0.0	0.0
8	20	0.0	0.22	-2.59	-4.29e-03	0.0	0.0
8	21	0.0	0.22	-2.51	-4.27e-03	0.0	0.0
9	1	0.0	0.0	-1.86	-2.42e-04	0.0	0.0
9	2	0.0	-1.69e-03	-1.78	8.56e-04	0.0	0.0
9	3	0.0	0.08	-2.17	-6.04e-04	0.0	0.0
9	4	0.0	0.16	-3.93	-1.28e-03	0.0	0.0
9	5	0.0	0.08	-1.68	-5.41e-04	0.0	0.0
9	6	0.0	0.08	-1.68	-5.41e-04	0.0	0.0
9	7	0.0	-2.85e-03	-3.67	4.68e-03	0.0	0.0
9	8	0.0	-2.28e-03	-1.28	1.30e-03	0.0	0.0
9	9	0.0	0.0	-1.38	-1.79e-04	0.0	0.0
9	10	0.0	-1.69e-03	-1.30	9.19e-04	0.0	0.0
9	11	0.0	0.06	-2.61	4.15e-04	0.0	0.0
9	12	0.0	0.0	-1.38	-1.79e-04	0.0	0.0
9	13	0.0	-1.69e-03	-1.30	9.19e-04	0.0	0.0
9	14	0.0	0.06	-2.61	4.15e-04	0.0	0.0
9	15	0.0	0.0	-1.38	-1.79e-04	0.0	0.0
9	16	0.0	0.0	-1.38	-1.79e-04	0.0	0.0
9	17	0.0	0.06	-1.83	-6.64e-04	0.0	0.0
9	18	0.0	0.22	-2.65	-4.25e-03	0.0	0.0
9	19	0.0	0.06	-1.83	-6.64e-04	0.0	0.0
9	20	0.0	0.22	-2.65	-4.25e-03	0.0	0.0
9	21	0.0	0.22	-2.57	-4.22e-03	0.0	0.0
10	1	0.0	0.0	-1.86	-2.41e-04	0.0	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
10	2	0.0	-1.69e-03	-1.76	8.57e-04	0.0	0.0
10	3	0.0	0.08	-2.18	-6.03e-04	0.0	0.0
10	4	0.0	0.16	-3.96	-1.28e-03	0.0	0.0
10	5	0.0	0.08	-1.70	-5.40e-04	0.0	0.0
10	6	0.0	0.08	-1.70	-5.40e-04	0.0	0.0
10	7	0.0	-2.85e-03	-3.55	4.68e-03	0.0	0.0
10	8	0.0	-2.28e-03	-1.24	1.30e-03	0.0	0.0
10	9	0.0	0.0	-1.38	-1.79e-04	0.0	0.0
10	10	0.0	-1.69e-03	-1.28	9.19e-04	0.0	0.0
10	11	0.0	0.06	-2.60	4.16e-04	0.0	0.0
10	12	0.0	0.0	-1.38	-1.79e-04	0.0	0.0
10	13	0.0	-1.69e-03	-1.28	9.19e-04	0.0	0.0
10	14	0.0	0.06	-2.60	4.16e-04	0.0	0.0
10	15	0.0	0.0	-1.38	-1.79e-04	0.0	0.0
10	16	0.0	0.0	-1.38	-1.79e-04	0.0	0.0
10	17	0.0	0.06	-1.84	-6.63e-04	0.0	0.0
10	18	0.0	0.22	-2.75	-4.24e-03	0.0	0.0
10	19	0.0	0.06	-1.84	-6.63e-04	0.0	0.0
10	20	0.0	0.22	-2.75	-4.24e-03	0.0	0.0
10	21	0.0	0.22	-2.67	-4.22e-03	0.0	0.0
11	1	0.0	0.0	-1.87	-2.41e-04	0.0	0.0
11	2	0.0	-1.69e-03	-1.74	8.57e-04	0.0	0.0
11	3	0.0	0.08	-2.19	-6.03e-04	0.0	0.0
11	4	0.0	0.16	-3.99	-1.28e-03	0.0	0.0
11	5	0.0	0.08	-1.71	-5.40e-04	0.0	0.0
11	6	0.0	0.08	-1.71	-5.40e-04	0.0	0.0
11	7	0.0	-2.85e-03	-3.46	4.68e-03	0.0	0.0
11	8	0.0	-2.28e-03	-1.22	1.30e-03	0.0	0.0
11	9	0.0	0.0	-1.38	-1.78e-04	0.0	0.0
11	10	0.0	-1.69e-03	-1.26	9.19e-04	0.0	0.0
11	11	0.0	0.06	-2.59	4.17e-04	0.0	0.0
11	12	0.0	0.0	-1.38	-1.78e-04	0.0	0.0
11	13	0.0	-1.69e-03	-1.26	9.19e-04	0.0	0.0
11	14	0.0	0.06	-2.59	4.17e-04	0.0	0.0
11	15	0.0	0.0	-1.38	-1.78e-04	0.0	0.0
11	16	0.0	0.0	-1.38	-1.78e-04	0.0	0.0
11	17	0.0	0.06	-1.86	-6.63e-04	0.0	0.0
11	18	0.0	0.22	-2.84	-4.24e-03	0.0	0.0
11	19	0.0	0.06	-1.86	-6.63e-04	0.0	0.0
11	20	0.0	0.22	-2.84	-4.24e-03	0.0	0.0
11	21	0.0	0.22	-2.76	-4.22e-03	0.0	0.0
12	1	0.0	-3.63e-03	-1.86	2.42e-04	0.0	0.0
12	2	0.0	0.02	-1.78	-9.67e-04	0.0	0.0
12	3	0.0	0.13	-1.38	-2.85e-03	0.0	0.0
12	4	0.0	0.23	-2.63	-4.48e-03	0.0	0.0
12	5	0.0	0.13	-0.89	-2.91e-03	0.0	0.0
12	6	0.0	0.13	-0.89	-2.91e-03	0.0	0.0
12	7	0.0	9.34e-05	-4.92	8.20e-05	0.0	0.0
12	8	0.0	0.02	-1.28	-1.45e-03	0.0	0.0
12	9	0.0	-2.69e-03	-1.38	1.79e-04	0.0	0.0
12	10	0.0	0.02	-1.30	-1.03e-03	0.0	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
12	11	0.0	0.09	-2.23	-2.24e-03	0.0	0.0
12	12	0.0	-2.69e-03	-1.38	1.79e-04	0.0	0.0
12	13	0.0	0.02	-1.30	-1.03e-03	0.0	0.0
12	14	0.0	0.09	-2.23	-2.24e-03	0.0	0.0
12	15	0.0	-2.69e-03	-1.38	1.79e-04	0.0	0.0
12	16	0.0	-2.69e-03	-1.38	1.79e-04	0.0	0.0
12	17	0.0	0.11	-1.03	-2.82e-03	0.0	0.0
12	18	0.0	0.33	0.02	-7.10e-03	0.0	0.0
12	19	0.0	0.11	-1.03	-2.82e-03	0.0	0.0
12	20	0.0	0.33	0.02	-7.10e-03	0.0	0.0
12	21	0.0	0.33	0.10	-7.13e-03	0.0	0.0
13	1	0.0	3.63e-03	-1.86	-2.42e-04	0.0	0.0
13	2	0.0	-0.02	-1.78	9.67e-04	0.0	0.0
13	3	0.0	0.09	-2.17	-4.93e-04	0.0	0.0
13	4	0.0	0.18	-3.93	-1.17e-03	0.0	0.0
13	5	0.0	0.09	-1.68	-4.31e-04	0.0	0.0
13	6	0.0	0.09	-1.68	-4.31e-04	0.0	0.0
13	7	0.0	-0.07	-3.67	4.88e-03	0.0	0.0
13	8	0.0	-0.02	-1.28	1.45e-03	0.0	0.0
13	9	0.0	2.69e-03	-1.38	-1.79e-04	0.0	0.0
13	10	0.0	-0.02	-1.30	1.03e-03	0.0	0.0
13	11	0.0	0.05	-2.61	5.25e-04	0.0	0.0
13	12	0.0	2.69e-03	-1.38	-1.79e-04	0.0	0.0
13	13	0.0	-0.02	-1.30	1.03e-03	0.0	0.0
13	14	0.0	0.05	-2.61	5.25e-04	0.0	0.0
13	15	0.0	2.69e-03	-1.38	-1.79e-04	0.0	0.0
13	16	0.0	2.69e-03	-1.38	-1.79e-04	0.0	0.0
13	17	0.0	0.07	-1.83	-5.61e-04	0.0	0.0
13	18	0.0	0.28	-2.65	-4.16e-03	0.0	0.0
13	19	0.0	0.07	-1.83	-5.61e-04	0.0	0.0
13	20	0.0	0.28	-2.65	-4.16e-03	0.0	0.0
13	21	0.0	0.28	-2.57	-4.14e-03	0.0	0.0
14	1	0.0	-7.26e-03	-1.86	2.42e-04	0.0	0.0
14	2	0.0	0.03	-1.78	-1.07e-03	0.0	0.0
14	3	0.0	0.17	-1.38	-2.99e-03	0.0	0.0
14	4	0.0	0.30	-2.63	-4.67e-03	0.0	0.0
14	5	0.0	0.17	-0.89	-3.05e-03	0.0	0.0
14	6	0.0	0.17	-0.89	-3.05e-03	0.0	0.0
14	7	0.0	3.19e-04	-4.92	-1.10e-04	0.0	0.0
14	8	0.0	0.05	-1.28	-1.59e-03	0.0	0.0
14	9	0.0	-5.38e-03	-1.38	1.79e-04	0.0	0.0
14	10	0.0	0.03	-1.30	-1.13e-03	0.0	0.0
14	11	0.0	0.13	-2.23	-2.38e-03	0.0	0.0
14	12	0.0	-5.38e-03	-1.38	1.79e-04	0.0	0.0
14	13	0.0	0.03	-1.30	-1.13e-03	0.0	0.0
14	14	0.0	0.13	-2.23	-2.38e-03	0.0	0.0
14	15	0.0	-5.38e-03	-1.38	1.79e-04	0.0	0.0
14	16	0.0	-5.38e-03	-1.38	1.79e-04	0.0	0.0
14	17	0.0	0.15	-1.03	-2.95e-03	0.0	0.0
14	18	0.0	0.44	0.02	-7.31e-03	0.0	0.0
14	19	0.0	0.15	-1.03	-2.95e-03	0.0	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
14	20	0.0	0.44	0.02	-7.31e-03	0.0	0.0
14	21	0.0	0.44	0.10	-7.33e-03	0.0	0.0
15	1	0.0	7.26e-03	-1.86	-2.42e-04	0.0	0.0
15	2	0.0	-0.03	-1.78	1.07e-03	0.0	0.0
15	3	0.0	0.09	-2.17	-3.91e-04	0.0	0.0
15	4	0.0	0.19	-3.93	-1.07e-03	0.0	0.0
15	5	0.0	0.09	-1.68	-3.28e-04	0.0	0.0
15	6	0.0	0.09	-1.68	-3.28e-04	0.0	0.0
15	7	0.0	-0.15	-3.67	5.08e-03	0.0	0.0
15	8	0.0	-0.05	-1.28	1.59e-03	0.0	0.0
15	9	0.0	5.38e-03	-1.38	-1.79e-04	0.0	0.0
15	10	0.0	-0.03	-1.30	1.13e-03	0.0	0.0
15	11	0.0	0.04	-2.61	6.28e-04	0.0	0.0
15	12	0.0	5.38e-03	-1.38	-1.79e-04	0.0	0.0
15	13	0.0	-0.03	-1.30	1.13e-03	0.0	0.0
15	14	0.0	0.04	-2.61	6.28e-04	0.0	0.0
15	15	0.0	5.38e-03	-1.38	-1.79e-04	0.0	0.0
15	16	0.0	5.38e-03	-1.38	-1.79e-04	0.0	0.0
15	17	0.0	0.08	-1.83	-4.65e-04	0.0	0.0
15	18	0.0	0.34	-2.65	-4.08e-03	0.0	0.0
15	19	0.0	0.08	-1.83	-4.65e-04	0.0	0.0
15	20	0.0	0.34	-2.65	-4.08e-03	0.0	0.0
15	21	0.0	0.34	-2.57	-4.06e-03	0.0	0.0
16	1	0.0	-0.06	-1.86	2.42e-04	0.0	0.0
16	2	0.0	0.34	-1.78	-1.83e-03	0.0	0.0
16	3	0.0	0.89	-1.38	-4.02e-03	0.0	0.0
16	4	0.0	1.41	-2.63	-6.17e-03	0.0	0.0
16	5	0.0	0.91	-0.89	-4.08e-03	0.0	0.0
16	6	0.0	0.91	-0.89	-4.08e-03	0.0	0.0
16	7	0.0	0.20	-4.92	-1.61e-03	0.0	0.0
16	8	0.0	0.49	-1.28	-2.62e-03	0.0	0.0
16	9	0.0	-0.04	-1.38	1.79e-04	0.0	0.0
16	10	0.0	0.35	-1.30	-1.89e-03	0.0	0.0
16	11	0.0	0.74	-2.23	-3.49e-03	0.0	0.0
16	12	0.0	-0.04	-1.38	1.79e-04	0.0	0.0
16	13	0.0	0.35	-1.30	-1.89e-03	0.0	0.0
16	14	0.0	0.74	-2.23	-3.49e-03	0.0	0.0
16	15	0.0	-0.04	-1.38	1.79e-04	0.0	0.0
16	16	0.0	-0.04	-1.38	1.79e-04	0.0	0.0
16	17	0.0	0.87	-1.03	-3.99e-03	0.0	0.0
16	18	0.0	2.10	0.02	-8.98e-03	0.0	0.0
16	19	0.0	0.87	-1.03	-3.99e-03	0.0	0.0
16	20	0.0	2.10	0.02	-8.98e-03	0.0	0.0
16	21	0.0	2.10	0.10	-9.01e-03	0.0	0.0
17	1	0.0	0.06	-1.86	-2.42e-04	0.0	0.0
17	2	0.0	-0.34	-1.78	1.83e-03	0.0	0.0
17	3	0.0	0.08	-2.17	3.71e-04	0.0	0.0
17	4	0.0	0.31	-3.93	-3.08e-04	0.0	0.0
17	5	0.0	0.07	-1.69	4.33e-04	0.0	0.0
17	6	0.0	0.07	-1.69	4.33e-04	0.0	0.0
17	7	0.0	-1.34	-3.67	6.58e-03	0.0	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
17	8	0.0	-0.49	-1.28	2.62e-03	0.0	0.0
17	9	0.0	0.04	-1.38	-1.79e-04	0.0	0.0
17	10	0.0	-0.35	-1.30	1.89e-03	0.0	0.0
17	11	0.0	-0.18	-2.61	1.39e-03	0.0	0.0
17	12	0.0	0.04	-1.38	-1.79e-04	0.0	0.0
17	13	0.0	-0.35	-1.30	1.89e-03	0.0	0.0
17	14	0.0	-0.18	-2.61	1.39e-03	0.0	0.0
17	15	0.0	0.04	-1.38	-1.79e-04	0.0	0.0
17	16	0.0	0.04	-1.38	-1.79e-04	0.0	0.0
17	17	0.0	0.09	-1.83	2.35e-04	0.0	0.0
17	18	0.0	1.09	-2.65	-3.52e-03	0.0	0.0
17	19	0.0	0.09	-1.83	2.35e-04	0.0	0.0
17	20	0.0	1.09	-2.65	-3.52e-03	0.0	0.0
17	21	0.0	1.09	-2.57	-3.50e-03	0.0	0.0
18	1	0.0	-0.10	-1.86	2.42e-04	0.0	0.0
18	2	0.0	0.72	-1.78	-1.98e-03	0.0	0.0
18	3	0.0	1.72	-1.38	-4.22e-03	0.0	0.0
18	4	0.0	2.69	-2.63	-6.53e-03	0.0	0.0
18	5	0.0	1.75	-0.89	-4.28e-03	0.0	0.0
18	6	0.0	1.75	-0.89	-4.28e-03	0.0	0.0
18	7	0.0	0.57	-4.92	-1.97e-03	0.0	0.0
18	8	0.0	1.04	-1.28	-2.82e-03	0.0	0.0
18	9	0.0	-0.08	-1.38	1.79e-04	0.0	0.0
18	10	0.0	0.75	-1.30	-2.04e-03	0.0	0.0
18	11	0.0	1.47	-2.24	-3.76e-03	0.0	0.0
18	12	0.0	-0.08	-1.38	1.79e-04	0.0	0.0
18	13	0.0	0.75	-1.30	-2.04e-03	0.0	0.0
18	14	0.0	1.47	-2.24	-3.76e-03	0.0	0.0
18	15	0.0	-0.08	-1.38	1.79e-04	0.0	0.0
18	16	0.0	-0.08	-1.38	1.79e-04	0.0	0.0
18	17	0.0	1.70	-1.03	-4.23e-03	0.0	0.0
18	18	0.0	3.95	0.02	-9.44e-03	0.0	0.0
18	19	0.0	1.70	-1.03	-4.23e-03	0.0	0.0
18	20	0.0	3.95	0.02	-9.44e-03	0.0	0.0
18	21	0.0	3.96	0.10	-9.46e-03	0.0	0.0
19	1	0.0	0.10	-1.86	-2.42e-04	0.0	0.0
19	2	0.0	-0.72	-1.78	1.98e-03	0.0	0.0
19	3	0.0	-0.01	-2.17	5.21e-04	0.0	0.0
19	4	0.0	0.36	-3.93	-1.57e-04	0.0	0.0
19	5	0.0	-0.04	-1.69	5.84e-04	0.0	0.0
19	6	0.0	-0.04	-1.69	5.84e-04	0.0	0.0
19	7	0.0	-2.71	-3.67	6.94e-03	0.0	0.0
19	8	0.0	-1.04	-1.28	2.82e-03	0.0	0.0
19	9	0.0	0.08	-1.38	-1.79e-04	0.0	0.0
19	10	0.0	-0.75	-1.30	2.04e-03	0.0	0.0
19	11	0.0	-0.48	-2.61	1.54e-03	0.0	0.0
19	12	0.0	0.08	-1.38	-1.79e-04	0.0	0.0
19	13	0.0	-0.75	-1.30	2.04e-03	0.0	0.0
19	14	0.0	-0.48	-2.61	1.54e-03	0.0	0.0
19	15	0.0	0.08	-1.38	-1.79e-04	0.0	0.0
19	16	0.0	0.08	-1.38	-1.79e-04	0.0	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
19	17	0.0	0.02	-1.83	3.66e-04	0.0	0.0
19	18	0.0	1.78	-2.65	-3.44e-03	0.0	0.0
19	19	0.0	0.02	-1.83	3.66e-04	0.0	0.0
19	20	0.0	1.78	-2.65	-3.44e-03	0.0	0.0
19	21	0.0	1.77	-2.57	-3.42e-03	0.0	0.0
20	1	0.0	-0.14	-1.86	2.42e-04	0.0	0.0
20	2	0.0	1.04	-1.79	-1.99e-03	0.0	0.0
20	3	0.0	2.40	-1.38	-4.23e-03	0.0	0.0
20	4	0.0	3.74	-2.63	-6.56e-03	0.0	0.0
20	5	0.0	2.43	-0.89	-4.29e-03	0.0	0.0
20	6	0.0	2.43	-0.89	-4.29e-03	0.0	0.0
20	7	0.0	0.89	-4.92	-2.00e-03	0.0	0.0
20	8	0.0	1.49	-1.28	-2.83e-03	0.0	0.0
20	9	0.0	-0.11	-1.38	1.79e-04	0.0	0.0
20	10	0.0	1.08	-1.30	-2.05e-03	0.0	0.0
20	11	0.0	2.07	-2.24	-3.78e-03	0.0	0.0
20	12	0.0	-0.11	-1.38	1.79e-04	0.0	0.0
20	13	0.0	1.08	-1.30	-2.05e-03	0.0	0.0
20	14	0.0	2.07	-2.24	-3.78e-03	0.0	0.0
20	15	0.0	-0.11	-1.38	1.79e-04	0.0	0.0
20	16	0.0	-0.11	-1.38	1.79e-04	0.0	0.0
20	17	0.0	2.37	-1.03	-4.24e-03	0.0	0.0
20	18	0.0	5.46	0.02	-9.47e-03	0.0	0.0
20	19	0.0	2.37	-1.03	-4.24e-03	0.0	0.0
20	20	0.0	5.46	0.02	-9.47e-03	0.0	0.0
20	21	0.0	5.48	0.10	-9.49e-03	0.0	0.0
21	1	0.0	0.14	-1.86	-2.42e-04	0.0	0.0
21	2	0.0	-1.04	-1.79	1.99e-03	0.0	0.0
21	3	0.0	-0.10	-2.17	5.28e-04	0.0	0.0
21	4	0.0	0.38	-3.93	-1.51e-04	0.0	0.0
21	5	0.0	-0.14	-1.69	5.90e-04	0.0	0.0
21	6	0.0	-0.14	-1.69	5.90e-04	0.0	0.0
21	7	0.0	-3.82	-3.67	6.96e-03	0.0	0.0
21	8	0.0	-1.49	-1.28	2.83e-03	0.0	0.0
21	9	0.0	0.11	-1.38	-1.79e-04	0.0	0.0
21	10	0.0	-1.08	-1.30	2.05e-03	0.0	0.0
21	11	0.0	-0.72	-2.61	1.55e-03	0.0	0.0
21	12	0.0	0.11	-1.38	-1.79e-04	0.0	0.0
21	13	0.0	-1.08	-1.30	2.05e-03	0.0	0.0
21	14	0.0	-0.72	-2.61	1.55e-03	0.0	0.0
21	15	0.0	0.11	-1.38	-1.79e-04	0.0	0.0
21	16	0.0	0.11	-1.38	-1.79e-04	0.0	0.0
21	17	0.0	-0.03	-1.83	3.70e-04	0.0	0.0
21	18	0.0	2.33	-2.65	-3.44e-03	0.0	0.0
21	19	0.0	-0.03	-1.83	3.70e-04	0.0	0.0
21	20	0.0	2.33	-2.65	-3.44e-03	0.0	0.0
21	21	0.0	2.32	-2.57	-3.42e-03	0.0	0.0
Nodo		**Traslazione X**	**Traslazione Y**	**Traslazione Z**	**Rotazione X**	**Rotazione Y**	**Rotazione Z**
		0.0	-3.82	-4.93	-9.49e-03	0.0	0.0
		0.0	5.48	0.41	6.96e-03	0.0	0.0

11.2. RISULTATI ELEMENTI TIPO TRAVE

Il controllo dei risultati delle analisi condotte, per quanto concerne gli elementi tipo trave, è possibile in relazione alle tabelle sottoriportate.

Gli elementi vengono suddivisi, in relazione alle proprietà in elementi:

- tipo **pilastro**
- tipo **trave in elevazione**
- tipo **trave in fondazione**

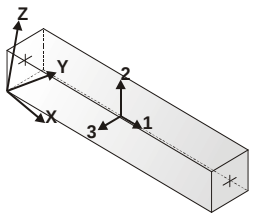
Per ogni elemento, e per ogni combinazione (o caso di carico) vengono riportati i risultati più significativi.

Per gli elementi tipo *pilastro* sono riportati in tabella i seguenti valori:

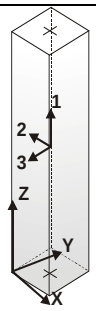
Pilas.	numero dell'elemento pilastro
Cmb	combinazione in cui si verificano i valori riportati
M3 mx/mn	momento flettente in campata M3 max (prima riga) / min (seconda riga)
M2 mx/mn	momento flettente in campata M2 max (prima riga) / min (seconda riga)
D2/D3	freccia massima in direzione 2 (prima riga) / direzione 3 (seconda riga)
Q2/Q3	carico totale in direzione 2 (prima riga) / direzione 3 (seconda riga)
Pos.	ascissa del punto iniziale e finale dell'elemento
N, V2, ecc..	sei componenti di sollecitazione al piede ed in sommità dell'elemento

Per gli elementi tipo *trave in elevazione* sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri.

Per gli elementi tipo *trave in fondazione* (trave f.) sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri e la massima pressione sul terreno.



orientamento elementi 2D non verticali



orientamento elementi 2D verticali

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		daN cm	daN cm	cm	daN	cm	daN	daN	daN	daN cm	daN cm	daN cm
11	1	0.0	0.0	3.63e-03	0.0	0.0	-9956.25	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-9703.13	0.0	0.0	0.0	0.0	0.0
11	2	-2.495e+06	0.0	-0.01	-688.14	0.0	-9956.25	1.371e+04	0.0	0.0	0.0	-2.696e+06
		-2.696e+06	0.0	0.0	0.0	15.0	-9703.12	1.302e+04	0.0	0.0	0.0	-2.495e+06
11	3	-3.369e+06	0.0	-0.04	-929.00	0.0	-9956.25	1.851e+04	0.0	0.0	0.0	-3.639e+06
		-3.639e+06	0.0	0.0	0.0	15.0	-9703.12	1.758e+04	0.0	0.0	0.0	-3.369e+06
11	4	-4.652e+06	0.0	-0.07	-1045.45	0.0	-9956.25	2.309e+04	0.0	0.0	0.0	-4.991e+06
		-4.991e+06	0.0	0.0	0.0	15.0	-9703.12	2.204e+04	0.0	0.0	0.0	-4.652e+06
11	5	-3.369e+06	0.0	-0.04	-929.00	0.0	-7375.00	1.851e+04	0.0	0.0	0.0	-3.639e+06
		-3.639e+06	0.0	0.0	0.0	15.0	-7187.50	1.758e+04	0.0	0.0	0.0	-3.369e+06
11	6	-3.369e+06	0.0	-0.04	-929.00	0.0	-7375.00	1.851e+04	0.0	0.0	0.0	-3.639e+06
		-3.639e+06	0.0	0.0	0.0	15.0	-7187.50	1.758e+04	0.0	0.0	0.0	-3.369e+06
11	7	-4.652e+06	0.0	-2.75e-03	-1045.45	0.0	-7375.00	2.309e+04	0.0	0.0	0.0	-4.991e+06
		-4.991e+06	0.0	0.0	0.0	15.0	-7187.50	2.204e+04	0.0	0.0	0.0	-4.652e+06
11	8	-3.369e+06	0.0	-0.02	-929.00	0.0	-7375.00	1.851e+04	0.0	0.0	0.0	-3.639e+06
		-3.639e+06	0.0	0.0	0.0	15.0	-7187.50	1.758e+04	0.0	0.0	0.0	-3.369e+06
11	9	0.0	0.0	2.69e-03	0.0	0.0	-7375.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7187.50	0.0	0.0	0.0	0.0	0.0
11	10	-2.495e+06	0.0	-0.01	-688.14	0.0	-7375.00	1.371e+04	0.0	0.0	0.0	-2.696e+06
		-2.696e+06	0.0	0.0	0.0	15.0	-7187.50	1.302e+04	0.0	0.0	0.0	-2.495e+06
11	11	-3.448e+06	0.0	-0.03	-774.62	0.0	-7375.00	1.711e+04	0.0	0.0	0.0	-3.699e+06
		-3.699e+06	0.0	0.0	0.0	15.0	-7187.50	1.633e+04	0.0	0.0	0.0	-3.448e+06
11	12	0.0	0.0	2.69e-03	0.0	0.0	-7375.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7187.50	0.0	0.0	0.0	0.0	0.0
11	13	-2.495e+06	0.0	-0.01	-688.14	0.0	-7375.00	1.371e+04	0.0	0.0	0.0	-2.696e+06
		-2.696e+06	0.0	0.0	0.0	15.0	-7187.50	1.302e+04	0.0	0.0	0.0	-2.495e+06
11	14	-3.448e+06	0.0	-0.03	-774.62	0.0	-7375.00	1.711e+04	0.0	0.0	0.0	-3.699e+06
		-3.699e+06	0.0	0.0	0.0	15.0	-7187.50	1.633e+04	0.0	0.0	0.0	-3.448e+06
11	15	0.0	0.0	2.69e-03	0.0	0.0	-7375.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7187.50	0.0	0.0	0.0	0.0	0.0
11	16	0.0	0.0	2.69e-03	0.0	0.0	-7375.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7187.50	0.0	0.0	0.0	0.0	0.0
11	17	-3.236e+06	0.0	-0.04	-755.37	0.0	-8727.20	1.635e+04	0.0	0.0	0.0	-3.476e+06
		-3.476e+06	0.0	0.0	0.0	15.0	-8514.80	1.560e+04	0.0	0.0	0.0	-3.236e+06
11	18	-4.965e+06	0.0	-0.10	-912.24	0.0	-7780.66	2.252e+04	0.0	0.0	0.0	-5.296e+06
		-5.296e+06	0.0	0.0	0.0	15.0	-7585.69	2.161e+04	0.0	0.0	0.0	-4.965e+06
11	19	-3.236e+06	0.0	-0.04	-755.37	0.0	-8727.20	1.635e+04	0.0	0.0	0.0	-3.476e+06
		-3.476e+06	0.0	0.0	0.0	15.0	-8514.80	1.560e+04	0.0	0.0	0.0	-3.236e+06
11	20	-4.965e+06	0.0	-0.10	-912.24	0.0	-7780.66	2.252e+04	0.0	0.0	0.0	-5.296e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-5.296e+06	0.0	0.0	0.0	15.0	-7585.69	2.161e+04	0.0	0.0	0.0	-4.965e+06
11	21	-4.965e+06	0.0	-0.11	-912.24	0.0	-6969.34	2.252e+04	0.0	0.0	0.0	-5.296e+06
		-5.296e+06	0.0	0.0	0.0	15.0	-6789.31	2.161e+04	0.0	0.0	0.0	-4.965e+06
12	1	0.0	0.0	-3.63e-03	0.0	0.0	-9956.25	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-9703.13	0.0	0.0	0.0	0.0	0.0
12	2	2.696e+06	0.0	0.01	688.14	0.0	-9956.25	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-9703.13	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	3	2.696e+06	0.0	-8.22e-03	688.14	0.0	-9956.25	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-9703.13	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	4	2.696e+06	0.0	-0.02	688.14	0.0	-9956.25	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-9703.13	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	5	2.696e+06	0.0	-7.28e-03	688.14	0.0	-7375.00	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	6	2.696e+06	0.0	-7.28e-03	688.14	0.0	-7375.00	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	7	4.991e+06	0.0	0.07	1045.45	0.0	-7375.00	-2.309e+04	0.0	0.0	0.0	4.991e+06
		4.652e+06	0.0	0.0	0.0	15.0	-7187.50	-2.204e+04	0.0	0.0	0.0	4.652e+06
12	8	3.639e+06	0.0	0.02	929.00	0.0	-7375.00	-1.851e+04	0.0	0.0	0.0	3.639e+06
		3.369e+06	0.0	0.0	0.0	15.0	-7187.50	-1.758e+04	0.0	0.0	0.0	3.369e+06
12	9	0.0	0.0	-2.69e-03	0.0	0.0	-7375.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7187.50	0.0	0.0	0.0	0.0	0.0
12	10	2.696e+06	0.0	0.01	688.14	0.0	-7375.00	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	11	2.696e+06	0.0	-7.06e-03	688.14	0.0	-7375.00	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	12	0.0	0.0	-2.69e-03	0.0	0.0	-7375.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7187.50	0.0	0.0	0.0	0.0	0.0
12	13	2.696e+06	0.0	0.01	688.14	0.0	-7375.00	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	14	2.696e+06	0.0	-7.06e-03	688.14	0.0	-7375.00	-1.371e+04	0.0	0.0	0.0	2.696e+06
		2.495e+06	0.0	0.0	0.0	15.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
12	15	0.0	0.0	-2.69e-03	0.0	0.0	-7375.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7187.50	0.0	0.0	0.0	0.0	0.0
12	16	0.0	0.0	-2.69e-03	0.0	0.0	-7375.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7187.50	0.0	0.0	0.0	0.0	0.0
12	17	2.522e+06	0.0	-9.18e-03	688.14	0.0	-8727.20	-1.315e+04	0.0	0.0	0.0	2.522e+06
		2.330e+06	0.0	0.0	0.0	15.0	-8514.80	-1.246e+04	0.0	0.0	0.0	2.330e+06
12	18	2.118e+06	0.0	-0.06	688.14	0.0	-7780.66	-1.184e+04	0.0	0.0	0.0	2.118e+06
		1.945e+06	0.0	0.0	0.0	15.0	-7585.69	-1.115e+04	0.0	0.0	0.0	1.945e+06
12	19	2.522e+06	0.0	-9.18e-03	688.14	0.0	-8727.20	-1.315e+04	0.0	0.0	0.0	2.522e+06
		2.330e+06	0.0	0.0	0.0	15.0	-8514.80	-1.246e+04	0.0	0.0	0.0	2.330e+06
12	20	2.118e+06	0.0	-0.06	688.14	0.0	-7780.66	-1.184e+04	0.0	0.0	0.0	2.118e+06
		1.945e+06	0.0	0.0	0.0	15.0	-7585.69	-1.115e+04	0.0	0.0	0.0	1.945e+06
12	21	2.118e+06	0.0	-0.06	688.14	0.0	-6969.34	-1.184e+04	0.0	0.0	0.0	2.118e+06
		1.945e+06	0.0	0.0	0.0	15.0	-6789.31	-1.115e+04	0.0	0.0	0.0	1.945e+06
13	1	0.0	0.0	3.63e-03	0.0	0.0	-9703.13	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-9450.00	0.0	0.0	0.0	0.0	0.0
13	2	-2.305e+06	0.0	-0.02	-670.42	0.0	-9703.13	1.302e+04	0.0	0.0	0.0	-2.495e+06
		-2.495e+06	0.0	0.0	0.0	15.0	-9450.00	1.235e+04	0.0	0.0	0.0	-2.305e+06
13	3	-3.112e+06	0.0	-0.04	-905.07	0.0	-9703.13	1.758e+04	0.0	0.0	0.0	-3.369e+06
		-3.369e+06	0.0	0.0	0.0	15.0	-9450.00	1.667e+04	0.0	0.0	0.0	-3.112e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
13	4	-4.329e+06	0.0	-0.07	-1021.53	0.0	-9703.13	2.204e+04	0.0	0.0	0.0	-4.652e+06
		-4.652e+06	0.0	0.0	0.0	15.0	-9450.00	2.102e+04	0.0	0.0	0.0	-4.329e+06
13	5	-3.112e+06	0.0	-0.04	-905.07	0.0	-7187.50	1.758e+04	0.0	0.0	0.0	-3.369e+06
		-3.369e+06	0.0	0.0	0.0	15.0	-7000.00	1.667e+04	0.0	0.0	0.0	-3.112e+06
13	6	-3.112e+06	0.0	-0.04	-905.07	0.0	-7187.50	1.758e+04	0.0	0.0	0.0	-3.369e+06
		-3.369e+06	0.0	0.0	0.0	15.0	-7000.00	1.667e+04	0.0	0.0	0.0	-3.112e+06
13	7	-4.329e+06	0.0	2.54e-04	-1021.53	0.0	-7187.50	2.204e+04	0.0	0.0	0.0	-4.652e+06
		-4.652e+06	0.0	0.0	0.0	15.0	-7000.00	2.102e+04	0.0	0.0	0.0	-4.329e+06
13	8	-3.112e+06	0.0	-0.02	-905.07	0.0	-7187.50	1.758e+04	0.0	0.0	0.0	-3.369e+06
		-3.369e+06	0.0	0.0	0.0	15.0	-7000.00	1.667e+04	0.0	0.0	0.0	-3.112e+06
13	9	0.0	0.0	2.69e-03	0.0	0.0	-7187.50	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7000.00	0.0	0.0	0.0	0.0	0.0
13	10	-2.305e+06	0.0	-0.02	-670.42	0.0	-7187.50	1.302e+04	0.0	0.0	0.0	-2.495e+06
		-2.495e+06	0.0	0.0	0.0	15.0	-7000.00	1.235e+04	0.0	0.0	0.0	-2.305e+06
13	11	-3.209e+06	0.0	-0.03	-756.90	0.0	-7187.50	1.633e+04	0.0	0.0	0.0	-3.448e+06
		-3.448e+06	0.0	0.0	0.0	15.0	-7000.00	1.558e+04	0.0	0.0	0.0	-3.209e+06
13	12	0.0	0.0	2.69e-03	0.0	0.0	-7187.50	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7000.00	0.0	0.0	0.0	0.0	0.0
13	13	-2.305e+06	0.0	-0.02	-670.42	0.0	-7187.50	1.302e+04	0.0	0.0	0.0	-2.495e+06
		-2.495e+06	0.0	0.0	0.0	15.0	-7000.00	1.235e+04	0.0	0.0	0.0	-2.305e+06
13	14	-3.209e+06	0.0	-0.03	-756.90	0.0	-7187.50	1.633e+04	0.0	0.0	0.0	-3.448e+06
		-3.448e+06	0.0	0.0	0.0	15.0	-7000.00	1.558e+04	0.0	0.0	0.0	-3.209e+06
13	15	0.0	0.0	2.69e-03	0.0	0.0	-7187.50	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7000.00	0.0	0.0	0.0	0.0	0.0
13	16	0.0	0.0	2.69e-03	0.0	0.0	-7187.50	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7000.00	0.0	0.0	0.0	0.0	0.0
13	17	-3.008e+06	0.0	-0.04	-737.65	0.0	-8514.80	1.560e+04	0.0	0.0	0.0	-3.236e+06
		-3.236e+06	0.0	0.0	0.0	15.0	-8302.40	1.486e+04	0.0	0.0	0.0	-3.008e+06
13	18	-4.648e+06	0.0	-0.11	-894.52	0.0	-7585.69	2.161e+04	0.0	0.0	0.0	-4.965e+06
		-4.965e+06	0.0	0.0	0.0	15.0	-7390.72	2.072e+04	0.0	0.0	0.0	-4.648e+06
13	19	-3.008e+06	0.0	-0.04	-737.65	0.0	-8514.80	1.560e+04	0.0	0.0	0.0	-3.236e+06
		-3.236e+06	0.0	0.0	0.0	15.0	-8302.40	1.486e+04	0.0	0.0	0.0	-3.008e+06
13	20	-4.648e+06	0.0	-0.11	-894.52	0.0	-7585.69	2.161e+04	0.0	0.0	0.0	-4.965e+06
		-4.965e+06	0.0	0.0	0.0	15.0	-7390.72	2.072e+04	0.0	0.0	0.0	-4.648e+06
13	21	-4.648e+06	0.0	-0.11	-894.52	0.0	-6789.31	2.161e+04	0.0	0.0	0.0	-4.965e+06
		-4.965e+06	0.0	0.0	0.0	15.0	-6609.28	2.072e+04	0.0	0.0	0.0	-4.648e+06
14	1	0.0	0.0	-3.63e-03	0.0	0.0	-9703.13	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-9450.00	0.0	0.0	0.0	0.0	0.0
14	2	2.495e+06	0.0	0.02	670.42	0.0	-9703.13	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-9450.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	3	2.495e+06	0.0	-6.62e-03	670.42	0.0	-9703.13	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-9450.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	4	2.495e+06	0.0	-0.02	670.42	0.0	-9703.13	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-9450.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	5	2.495e+06	0.0	-5.68e-03	670.42	0.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	6	2.495e+06	0.0	-5.68e-03	670.42	0.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	7	4.652e+06	0.0	0.07	1021.53	0.0	-7187.50	-2.204e+04	0.0	0.0	0.0	4.652e+06
		4.329e+06	0.0	0.0	0.0	15.0	-7000.00	-2.102e+04	0.0	0.0	0.0	4.329e+06
14	8	3.369e+06	0.0	0.02	905.07	0.0	-7187.50	-1.758e+04	0.0	0.0	0.0	3.369e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		3.112e+06	0.0	0.0	0.0	15.0	-7000.00	-1.667e+04	0.0	0.0	0.0	3.112e+06
14	9	0.0	0.0	-2.69e-03	0.0	0.0	-7187.50	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7000.00	0.0	0.0	0.0	0.0	0.0
14	10	2.495e+06	0.0	0.02	670.42	0.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	11	2.495e+06	0.0	-8.66e-03	670.42	0.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	12	0.0	0.0	-2.69e-03	0.0	0.0	-7187.50	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7000.00	0.0	0.0	0.0	0.0	0.0
14	13	2.495e+06	0.0	0.02	670.42	0.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	14	2.495e+06	0.0	-8.66e-03	670.42	0.0	-7187.50	-1.302e+04	0.0	0.0	0.0	2.495e+06
		2.305e+06	0.0	0.0	0.0	15.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
14	15	0.0	0.0	-2.69e-03	0.0	0.0	-7187.50	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7000.00	0.0	0.0	0.0	0.0	0.0
14	16	0.0	0.0	-2.69e-03	0.0	0.0	-7187.50	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	15.0	-7000.00	0.0	0.0	0.0	0.0	0.0
14	17	2.330e+06	0.0	-7.68e-03	670.42	0.0	-8514.80	-1.246e+04	0.0	0.0	0.0	2.330e+06
		2.149e+06	0.0	0.0	0.0	15.0	-8302.40	-1.179e+04	0.0	0.0	0.0	2.149e+06
14	18	1.945e+06	0.0	-0.06	670.42	0.0	-7585.69	-1.115e+04	0.0	0.0	0.0	1.945e+06
		1.783e+06	0.0	0.0	0.0	15.0	-7390.72	-1.048e+04	0.0	0.0	0.0	1.783e+06
14	19	2.330e+06	0.0	-7.68e-03	670.42	0.0	-8514.80	-1.246e+04	0.0	0.0	0.0	2.330e+06
		2.149e+06	0.0	0.0	0.0	15.0	-8302.40	-1.179e+04	0.0	0.0	0.0	2.149e+06
14	20	1.945e+06	0.0	-0.06	670.42	0.0	-7585.69	-1.115e+04	0.0	0.0	0.0	1.945e+06
		1.783e+06	0.0	0.0	0.0	15.0	-7390.72	-1.048e+04	0.0	0.0	0.0	1.783e+06
14	21	1.945e+06	0.0	-0.06	670.42	0.0	-6789.31	-1.115e+04	0.0	0.0	0.0	1.945e+06
		1.783e+06	0.0	0.0	0.0	15.0	-6609.28	-1.048e+04	0.0	0.0	0.0	1.783e+06
15	1	0.0	0.0	0.05	0.0	0.0	-9450.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-6075.00	0.0	0.0	0.0	0.0	0.0
15	2	-6.124e+05	0.0	-0.31	-7245.70	0.0	-9450.00	1.235e+04	0.0	0.0	0.0	-2.305e+06
		-2.305e+06	0.0	0.0	0.0	200.0	-6075.00	5103.49	0.0	0.0	0.0	-6.124e+05
15	3	-8.268e+05	0.0	-0.72	-9781.70	0.0	-9450.00	1.667e+04	0.0	0.0	0.0	-3.112e+06
		-3.112e+06	0.0	0.0	0.0	200.0	-6075.00	6889.72	0.0	0.0	0.0	-8.268e+05
15	4	-1.330e+06	0.0	-1.11	-1.133e+04	0.0	-9450.00	2.102e+04	0.0	0.0	0.0	-4.329e+06
		-4.329e+06	0.0	0.0	0.0	200.0	-6075.00	9684.71	0.0	0.0	0.0	-1.330e+06
15	5	-8.268e+05	0.0	-0.73	-9781.70	0.0	-7000.00	1.667e+04	0.0	0.0	0.0	-3.112e+06
		-3.112e+06	0.0	0.0	0.0	200.0	-4500.00	6889.72	0.0	0.0	0.0	-8.268e+05
15	6	-8.268e+05	0.0	-0.73	-9781.70	0.0	-7000.00	1.667e+04	0.0	0.0	0.0	-3.112e+06
		-3.112e+06	0.0	0.0	0.0	200.0	-4500.00	6889.72	0.0	0.0	0.0	-8.268e+05
15	7	-1.330e+06	0.0	-0.20	-1.133e+04	0.0	-7000.00	2.102e+04	0.0	0.0	0.0	-4.329e+06
		-4.329e+06	0.0	0.0	0.0	200.0	-4500.00	9684.71	0.0	0.0	0.0	-1.330e+06
15	8	-8.268e+05	0.0	-0.44	-9781.70	0.0	-7000.00	1.667e+04	0.0	0.0	0.0	-3.112e+06
		-3.112e+06	0.0	0.0	0.0	200.0	-4500.00	6889.72	0.0	0.0	0.0	-8.268e+05
15	9	0.0	0.0	0.04	0.0	0.0	-7000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-4500.00	0.0	0.0	0.0	0.0	0.0
15	10	-6.124e+05	0.0	-0.32	-7245.70	0.0	-7000.00	1.235e+04	0.0	0.0	0.0	-2.305e+06
		-2.305e+06	0.0	0.0	0.0	200.0	-4500.00	5103.49	0.0	0.0	0.0	-6.124e+05
15	11	-9.860e+05	0.0	-0.61	-8398.75	0.0	-7000.00	1.558e+04	0.0	0.0	0.0	-3.209e+06
		-3.209e+06	0.0	0.0	0.0	200.0	-4500.00	7178.98	0.0	0.0	0.0	-9.860e+05
15	12	0.0	0.0	0.04	0.0	0.0	-7000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-4500.00	0.0	0.0	0.0	0.0	0.0

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
15	13	-6.124e+05	0.0	-0.32	-7245.70	0.0	-7000.00	1.235e+04	0.0	0.0	0.0	-2.305e+06
		-2.305e+06	0.0	0.0	0.0	200.0	-4500.00	5103.49	0.0	0.0	0.0	-6.124e+05
15	14	-9.860e+05	0.0	-0.61	-8398.75	0.0	-7000.00	1.558e+04	0.0	0.0	0.0	-3.209e+06
		-3.209e+06	0.0	0.0	0.0	200.0	-4500.00	7178.98	0.0	0.0	0.0	-9.860e+05
15	15	0.0	0.0	0.04	0.0	0.0	-7000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-4500.00	0.0	0.0	0.0	0.0	0.0
15	16	0.0	0.0	0.04	0.0	0.0	-7000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-4500.00	0.0	0.0	0.0	0.0	0.0
15	17	-9.029e+05	0.0	-0.71	-8142.10	0.0	-8302.40	1.486e+04	0.0	0.0	0.0	-3.008e+06
		-3.008e+06	0.0	0.0	0.0	200.0	-5470.40	6717.01	0.0	0.0	0.0	-9.029e+05
15	18	-1.581e+06	0.0	-1.66	-1.023e+04	0.0	-7390.72	2.072e+04	0.0	0.0	0.0	-4.648e+06
		-4.648e+06	0.0	0.0	0.0	200.0	-4791.12	1.048e+04	0.0	0.0	0.0	-1.581e+06
15	19	-9.029e+05	0.0	-0.71	-8142.10	0.0	-8302.40	1.486e+04	0.0	0.0	0.0	-3.008e+06
		-3.008e+06	0.0	0.0	0.0	200.0	-5470.40	6717.01	0.0	0.0	0.0	-9.029e+05
15	20	-1.581e+06	0.0	-1.66	-1.023e+04	0.0	-7390.72	2.072e+04	0.0	0.0	0.0	-4.648e+06
		-4.648e+06	0.0	0.0	0.0	200.0	-4791.12	1.048e+04	0.0	0.0	0.0	-1.581e+06
15	21	-1.581e+06	0.0	-1.66	-1.023e+04	0.0	-6609.28	2.072e+04	0.0	0.0	0.0	-4.648e+06
		-4.648e+06	0.0	0.0	0.0	200.0	-4208.88	1.048e+04	0.0	0.0	0.0	-1.581e+06
16	1	0.0	0.0	-0.05	0.0	0.0	-9450.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-6075.00	0.0	0.0	0.0	0.0	0.0
16	2	2.305e+06	0.0	0.31	7245.70	0.0	-9450.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-6075.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	3	2.305e+06	0.0	-0.03	7245.70	0.0	-9450.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-6075.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	4	2.305e+06	0.0	-0.12	7245.70	0.0	-9450.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-6075.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	5	2.305e+06	0.0	-0.04	7245.70	0.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	6	2.305e+06	0.0	-0.04	7245.70	0.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	7	4.329e+06	0.0	1.19	1.133e+04	0.0	-7000.00	-2.102e+04	0.0	0.0	0.0	4.329e+06
		1.330e+06	0.0	0.0	0.0	200.0	-4500.00	-9684.71	0.0	0.0	0.0	1.330e+06
16	8	3.112e+06	0.0	0.44	9781.70	0.0	-7000.00	-1.667e+04	0.0	0.0	0.0	3.112e+06
		8.268e+05	0.0	0.0	0.0	200.0	-4500.00	-6889.72	0.0	0.0	0.0	8.268e+05
16	9	0.0	0.0	-0.04	0.0	0.0	-7000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-4500.00	0.0	0.0	0.0	0.0	0.0
16	10	2.305e+06	0.0	0.32	7245.70	0.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	11	2.305e+06	0.0	0.22	7245.70	0.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	12	0.0	0.0	-0.04	0.0	0.0	-7000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-4500.00	0.0	0.0	0.0	0.0	0.0
16	13	2.305e+06	0.0	0.32	7245.70	0.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	14	2.305e+06	0.0	0.22	7245.70	0.0	-7000.00	-1.235e+04	0.0	0.0	0.0	2.305e+06
		6.124e+05	0.0	0.0	0.0	200.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
16	15	0.0	0.0	-0.04	0.0	0.0	-7000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-4500.00	0.0	0.0	0.0	0.0	0.0
16	16	0.0	0.0	-0.04	0.0	0.0	-7000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-4500.00	0.0	0.0	0.0	0.0	0.0
16	17	2.149e+06	0.0	-0.02	7045.90	0.0	-8302.40	-1.179e+04	0.0	0.0	0.0	2.149e+06

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		5.477e+05	0.0	0.0	0.0	200.0	-5470.40	-4743.85	0.0	0.0	0.0	5.477e+05
16	18	1.783e+06	0.0	-0.75	6579.70	0.0	-7390.72	-1.048e+04	0.0	0.0	0.0	1.783e+06
		3.966e+05	0.0	0.0	0.0	200.0	-4791.12	-3904.69	0.0	0.0	0.0	3.966e+05
16	19	2.149e+06	0.0	-0.02	7045.90	0.0	-8302.40	-1.179e+04	0.0	0.0	0.0	2.149e+06
		5.477e+05	0.0	0.0	0.0	200.0	-5470.40	-4743.85	0.0	0.0	0.0	5.477e+05
16	20	1.783e+06	0.0	-0.75	6579.70	0.0	-7390.72	-1.048e+04	0.0	0.0	0.0	1.783e+06
		3.966e+05	0.0	0.0	0.0	200.0	-4791.12	-3904.69	0.0	0.0	0.0	3.966e+05
16	21	1.783e+06	0.0	-0.74	6579.70	0.0	-6609.28	-1.048e+04	0.0	0.0	0.0	1.783e+06
		3.966e+05	0.0	0.0	0.0	200.0	-4208.88	-3904.69	0.0	0.0	0.0	3.966e+05
17	1	0.0	0.0	0.05	0.0	0.0	-6075.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2700.00	0.0	0.0	0.0	0.0	0.0
17	2	-5.377e+04	0.0	-0.39	-4095.40	0.0	-6075.00	5103.49	0.0	0.0	0.0	-6.124e+05
		-6.124e+05	0.0	0.0	0.0	200.0	-2700.00	1008.10	0.0	0.0	0.0	-5.377e+04
17	3	-7.258e+04	0.0	-0.83	-5528.79	0.0	-6075.00	6889.72	0.0	0.0	0.0	-8.268e+05
		-8.268e+05	0.0	0.0	0.0	200.0	-2700.00	1360.93	0.0	0.0	0.0	-7.258e+04
17	4	-1.720e+05	0.0	-1.28	-7081.56	0.0	-6075.00	9684.71	0.0	0.0	0.0	-1.330e+06
		-1.330e+06	0.0	0.0	0.0	200.0	-2700.00	2603.15	0.0	0.0	0.0	-1.720e+05
17	5	-7.258e+04	0.0	-0.84	-5528.79	0.0	-4500.00	6889.72	0.0	0.0	0.0	-8.268e+05
		-8.268e+05	0.0	0.0	0.0	200.0	-2000.00	1360.93	0.0	0.0	0.0	-7.258e+04
17	6	-7.258e+04	0.0	-0.84	-5528.79	0.0	-4500.00	6889.72	0.0	0.0	0.0	-8.268e+05
		-8.268e+05	0.0	0.0	0.0	200.0	-2000.00	1360.93	0.0	0.0	0.0	-7.258e+04
17	7	-1.720e+05	0.0	-0.37	-7081.56	0.0	-4500.00	9684.71	0.0	0.0	0.0	-1.330e+06
		-1.330e+06	0.0	0.0	0.0	200.0	-2000.00	2603.15	0.0	0.0	0.0	-1.720e+05
17	8	-7.258e+04	0.0	-0.55	-5528.79	0.0	-4500.00	6889.72	0.0	0.0	0.0	-8.268e+05
		-8.268e+05	0.0	0.0	0.0	200.0	-2000.00	1360.93	0.0	0.0	0.0	-7.258e+04
17	9	0.0	0.0	0.04	0.0	0.0	-4500.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2000.00	0.0	0.0	0.0	0.0	0.0
17	10	-5.377e+04	0.0	-0.40	-4095.40	0.0	-4500.00	5103.49	0.0	0.0	0.0	-6.124e+05
		-6.124e+05	0.0	0.0	0.0	200.0	-2000.00	1008.10	0.0	0.0	0.0	-5.377e+04
17	11	-1.276e+05	0.0	-0.73	-5248.45	0.0	-4500.00	7178.98	0.0	0.0	0.0	-9.860e+05
		-9.860e+05	0.0	0.0	0.0	200.0	-2000.00	1930.54	0.0	0.0	0.0	-1.276e+05
17	12	0.0	0.0	0.04	0.0	0.0	-4500.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2000.00	0.0	0.0	0.0	0.0	0.0
17	13	-5.377e+04	0.0	-0.40	-4095.40	0.0	-4500.00	5103.49	0.0	0.0	0.0	-6.124e+05
		-6.124e+05	0.0	0.0	0.0	200.0	-2000.00	1008.10	0.0	0.0	0.0	-5.377e+04
17	14	-1.276e+05	0.0	-0.73	-5248.45	0.0	-4500.00	7178.98	0.0	0.0	0.0	-9.860e+05
		-9.860e+05	0.0	0.0	0.0	200.0	-2000.00	1930.54	0.0	0.0	0.0	-1.276e+05
17	15	0.0	0.0	0.04	0.0	0.0	-4500.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2000.00	0.0	0.0	0.0	0.0	0.0
17	16	0.0	0.0	0.04	0.0	0.0	-4500.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2000.00	0.0	0.0	0.0	0.0	0.0
17	17	-1.111e+05	0.0	-0.83	-4991.80	0.0	-5470.40	6717.01	0.0	0.0	0.0	-9.029e+05
		-9.029e+05	0.0	0.0	0.0	200.0	-2638.40	1725.22	0.0	0.0	0.0	-1.111e+05
17	18	-2.450e+05	0.0	-1.85	-7083.40	0.0	-4791.12	1.048e+04	0.0	0.0	0.0	-1.581e+06
		-1.581e+06	0.0	0.0	0.0	200.0	-2191.52	3398.50	0.0	0.0	0.0	-2.450e+05
17	19	-1.111e+05	0.0	-0.83	-4991.80	0.0	-5470.40	6717.01	0.0	0.0	0.0	-9.029e+05
		-9.029e+05	0.0	0.0	0.0	200.0	-2638.40	1725.22	0.0	0.0	0.0	-1.111e+05
17	20	-2.450e+05	0.0	-1.85	-7083.40	0.0	-4791.12	1.048e+04	0.0	0.0	0.0	-1.581e+06
		-1.581e+06	0.0	0.0	0.0	200.0	-2191.52	3398.50	0.0	0.0	0.0	-2.450e+05
17	21	-2.450e+05	0.0	-1.86	-7083.40	0.0	-4208.88	1.048e+04	0.0	0.0	0.0	-1.581e+06
		-1.581e+06	0.0	0.0	0.0	200.0	-1808.48	3398.50	0.0	0.0	0.0	-2.450e+05

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
18	1	0.0	0.0	-0.05	0.0	0.0	-6075.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2700.00	0.0	0.0	0.0	0.0	0.0
18	2	6.124e+05	0.0	0.39	4095.40	0.0	-6075.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2700.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	3	6.124e+05	0.0	-0.09	4095.40	0.0	-6075.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2700.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	4	6.124e+05	0.0	-0.04	4095.40	0.0	-6075.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2700.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	5	6.124e+05	0.0	-0.11	4095.40	0.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	6	6.124e+05	0.0	-0.11	4095.40	0.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	7	1.330e+06	0.0	1.36	7081.56	0.0	-4500.00	-9684.71	0.0	0.0	0.0	1.330e+06
		1.720e+05	0.0	0.0	0.0	200.0	-2000.00	-2603.15	0.0	0.0	0.0	1.720e+05
18	8	8.268e+05	0.0	0.55	5528.79	0.0	-4500.00	-6889.72	0.0	0.0	0.0	8.268e+05
		7.258e+04	0.0	0.0	0.0	200.0	-2000.00	-1360.93	0.0	0.0	0.0	7.258e+04
18	9	0.0	0.0	-0.04	0.0	0.0	-4500.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2000.00	0.0	0.0	0.0	0.0	0.0
18	10	6.124e+05	0.0	0.40	4095.40	0.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	11	6.124e+05	0.0	0.30	4095.40	0.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	12	0.0	0.0	-0.04	0.0	0.0	-4500.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2000.00	0.0	0.0	0.0	0.0	0.0
18	13	6.124e+05	0.0	0.40	4095.40	0.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	14	6.124e+05	0.0	0.30	4095.40	0.0	-4500.00	-5103.49	0.0	0.0	0.0	6.124e+05
		5.377e+04	0.0	0.0	0.0	200.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
18	15	0.0	0.0	-0.04	0.0	0.0	-4500.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2000.00	0.0	0.0	0.0	0.0	0.0
18	16	0.0	0.0	-0.04	0.0	0.0	-4500.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	200.0	-2000.00	0.0	0.0	0.0	0.0	0.0
18	17	5.477e+05	0.0	-0.06	3895.60	0.0	-5470.40	-4743.85	0.0	0.0	0.0	5.477e+05
		4.098e+04	0.0	0.0	0.0	200.0	-2638.40	-848.26	0.0	0.0	0.0	4.098e+04
18	18	3.966e+05	0.0	-0.69	3429.40	0.0	-4791.12	-3904.69	0.0	0.0	0.0	3.966e+05
		1.114e+04	0.0	0.0	0.0	200.0	-2191.52	-475.30	0.0	0.0	0.0	1.114e+04
18	19	5.477e+05	0.0	-0.06	3895.60	0.0	-5470.40	-4743.85	0.0	0.0	0.0	5.477e+05
		4.098e+04	0.0	0.0	0.0	200.0	-2638.40	-848.26	0.0	0.0	0.0	4.098e+04
18	20	3.966e+05	0.0	-0.69	3429.40	0.0	-4791.12	-3904.69	0.0	0.0	0.0	3.966e+05
		1.114e+04	0.0	0.0	0.0	200.0	-2191.52	-475.30	0.0	0.0	0.0	1.114e+04
18	21	3.966e+05	0.0	-0.69	3429.40	0.0	-4208.88	-3904.69	0.0	0.0	0.0	3.966e+05
		1.114e+04	0.0	0.0	0.0	200.0	-1808.48	-475.30	0.0	0.0	0.0	1.114e+04
19	1	0.0	0.0	0.04	0.0	0.0	-2700.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
19	2	0.0	0.0	-0.32	-1008.10	0.0	-2700.00	1008.10	0.0	0.0	0.0	-5.377e+04
		-5.377e+04	0.0	0.0	0.0	160.0	0.0	2.91e-05	0.0	0.0	0.0	0.0
19	3	0.0	0.0	-0.68	-1360.93	0.0	-2700.00	1360.93	0.0	0.0	0.0	-7.258e+04
		-7.258e+04	0.0	0.0	0.0	160.0	0.0	3.93e-05	0.0	0.0	0.0	0.0
19	4	0.0	0.0	-1.05	-2603.15	0.0	-2700.00	2603.15	0.0	0.0	0.0	-1.720e+05
		-1.720e+05	0.0	0.0	0.0	160.0	0.0	8.37e-05	0.0	0.0	0.0	0.0
19	5	0.0	0.0	-0.69	-1360.93	0.0	-2000.00	1360.93	0.0	0.0	0.0	-7.258e+04

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		-7.258e+04	0.0	0.0	0.0	160.0	0.0	3.93e-05	0.0	0.0	0.0	0.0
19	6	0.0	0.0	-0.69	-1360.93	0.0	-2000.00	1360.93	0.0	0.0	0.0	-7.258e+04
		-7.258e+04	0.0	0.0	0.0	160.0	0.0	3.93e-05	0.0	0.0	0.0	0.0
19	7	0.0	0.0	-0.32	-2603.15	0.0	-2000.00	2603.15	0.0	0.0	0.0	-1.720e+05
		-1.720e+05	0.0	0.0	0.0	160.0	0.0	8.37e-05	0.0	0.0	0.0	0.0
19	8	0.0	0.0	-0.45	-1360.93	0.0	-2000.00	1360.93	0.0	0.0	0.0	-7.258e+04
		-7.258e+04	0.0	0.0	0.0	160.0	0.0	3.93e-05	0.0	0.0	0.0	0.0
19	9	0.0	0.0	0.03	0.0	0.0	-2000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
19	10	0.0	0.0	-0.33	-1008.10	0.0	-2000.00	1008.10	0.0	0.0	0.0	-5.377e+04
		-5.377e+04	0.0	0.0	0.0	160.0	0.0	2.91e-05	0.0	0.0	0.0	0.0
19	11	0.0	0.0	-0.60	-1930.54	0.0	-2000.00	1930.54	0.0	0.0	0.0	-1.276e+05
		-1.276e+05	0.0	0.0	0.0	160.0	0.0	6.21e-05	0.0	0.0	0.0	0.0
19	12	0.0	0.0	0.03	0.0	0.0	-2000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
19	13	0.0	0.0	-0.33	-1008.10	0.0	-2000.00	1008.10	0.0	0.0	0.0	-5.377e+04
		-5.377e+04	0.0	0.0	0.0	160.0	0.0	2.91e-05	0.0	0.0	0.0	0.0
19	14	0.0	0.0	-0.60	-1930.54	0.0	-2000.00	1930.54	0.0	0.0	0.0	-1.276e+05
		-1.276e+05	0.0	0.0	0.0	160.0	0.0	6.21e-05	0.0	0.0	0.0	0.0
19	15	0.0	0.0	0.03	0.0	0.0	-2000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
19	16	0.0	0.0	0.03	0.0	0.0	-2000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
19	17	0.0	0.0	-0.68	-1725.22	0.0	-2638.40	1725.22	0.0	0.0	0.0	-1.111e+05
		-1.111e+05	0.0	0.0	0.0	160.0	-2.44e-05	0.0	0.0	0.0	0.0	0.0
19	18	0.0	0.0	-1.51	-3398.50	0.0	-2191.52	3398.50	0.0	0.0	0.0	-2.450e+05
		-2.450e+05	0.0	0.0	0.0	160.0	-7.32e-06	-6.85e-05	0.0	0.0	0.0	0.0
19	19	0.0	0.0	-0.68	-1725.22	0.0	-2638.40	1725.22	0.0	0.0	0.0	-1.111e+05
		-1.111e+05	0.0	0.0	0.0	160.0	-2.44e-05	0.0	0.0	0.0	0.0	0.0
19	20	0.0	0.0	-1.51	-3398.50	0.0	-2191.52	3398.50	0.0	0.0	0.0	-2.450e+05
		-2.450e+05	0.0	0.0	0.0	160.0	-7.32e-06	-6.85e-05	0.0	0.0	0.0	0.0
19	21	0.0	0.0	-1.52	-3398.50	0.0	-1808.48	3398.50	0.0	0.0	0.0	-2.450e+05
		-2.450e+05	0.0	0.0	0.0	160.0	7.32e-06	-6.85e-05	0.0	0.0	0.0	0.0
20	1	0.0	0.0	-0.04	0.0	0.0	-2700.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
20	2	5.377e+04	0.0	0.32	1008.10	0.0	-2700.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	3	5.377e+04	0.0	0.08	1008.10	0.0	-2700.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	4	5.377e+04	0.0	-0.02	1008.10	0.0	-2700.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	5	5.377e+04	0.0	0.09	1008.10	0.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	6	5.377e+04	0.0	0.09	1008.10	0.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	7	1.720e+05	0.0	1.11	2603.15	0.0	-2000.00	-2603.15	0.0	0.0	0.0	1.720e+05
		0.0	0.0	0.0	0.0	160.0	0.0	-8.37e-05	0.0	0.0	0.0	0.0
20	8	7.258e+04	0.0	0.45	1360.93	0.0	-2000.00	-1360.93	0.0	0.0	0.0	7.258e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-3.93e-05	0.0	0.0	0.0	0.0
20	9	0.0	0.0	-0.03	0.0	0.0	-2000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0

Pilas.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
20	10	5.377e+04	0.0	0.33	1008.10	0.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	11	5.377e+04	0.0	0.25	1008.10	0.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	12	0.0	0.0	-0.03	0.0	0.0	-2000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
20	13	5.377e+04	0.0	0.33	1008.10	0.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	14	5.377e+04	0.0	0.25	1008.10	0.0	-2000.00	-1008.10	0.0	0.0	0.0	5.377e+04
		0.0	0.0	0.0	0.0	160.0	0.0	-2.91e-05	0.0	0.0	0.0	0.0
20	15	0.0	0.0	-0.03	0.0	0.0	-2000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
20	16	0.0	0.0	-0.03	0.0	0.0	-2000.00	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	160.0	0.0	0.0	0.0	0.0	0.0	0.0
20	17	4.098e+04	0.0	0.06	848.26	0.0	-2638.40	-848.26	0.0	0.0	0.0	4.098e+04
		-94.79	0.0	0.0	0.0	160.0	-2.44e-05	-3.28e-05	0.0	0.0	0.0	0.0
20	18	1.114e+04	0.0	-0.55	475.30	0.0	-2191.52	-475.30	0.0	0.0	0.0	1.114e+04
		-3935.35	0.0	0.0	0.0	160.0	-7.32e-06	-4.13e-05	0.0	0.0	0.0	0.0
20	19	4.098e+04	0.0	0.06	848.26	0.0	-2638.40	-848.26	0.0	0.0	0.0	4.098e+04
		-94.79	0.0	0.0	0.0	160.0	-2.44e-05	-3.28e-05	0.0	0.0	0.0	0.0
20	20	1.114e+04	0.0	-0.55	475.30	0.0	-2191.52	-475.30	0.0	0.0	0.0	1.114e+04
		-3935.35	0.0	0.0	0.0	160.0	-7.32e-06	-4.13e-05	0.0	0.0	0.0	0.0
20	21	1.114e+04	0.0	-0.55	475.30	0.0	-1808.48	-475.30	0.0	0.0	0.0	1.114e+04
		-3935.35	0.0	0.0	0.0	160.0	7.32e-06	-4.13e-05	0.0	0.0	0.0	0.0
Pilas.		**M3 mx/mn**	**M2 mx/mn**	**D 2 / D 3**	**Q 2 / Q 3**		**N**	**V 2**	**V 3**	**T**		
		-5.296e+06	0.0	-1.86	-1.133e+04		-9956.25	-2.309e+04	0.0	0.0		
		4.991e+06	0.0	1.36	1.133e+04		7.32e-06	2.309e+04	0.0	0.0		

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		daN cm	daN cm	cm	daN/cm2	cm	daN	daN	daN	daN cm	daN cm	daN cm
1	1	8198.01	0.0	4.82e-03	-0.65	0.0	0.0	-81.57	0.0	0.0	0.0	815.84
		749.13	0.0	0.0		20.0	0.0	819.22	0.0	0.0	0.0	8198.01
1	2	8346.87	0.0	0.02	-0.62	0.0	1.69	15.14	0.0	0.0	0.0	-159.67
		-159.67	0.0	0.0		20.0	1.69	837.51	0.0	0.0	0.0	8346.87
1	3	5152.30	0.0	0.05	-0.46	0.0	83.37	31.28	0.0	0.0	0.0	-323.92
		-323.92	0.0	0.0		20.0	83.37	522.64	0.0	0.0	0.0	5152.30
1	4	1.327e+04	0.0	0.09	-0.88	0.0	161.36	6.59	0.0	0.0	0.0	-75.24
		-75.24	0.0	0.0		20.0	161.36	1337.90	0.0	0.0	0.0	1.327e+04
1	5	3026.89	0.0	0.06	-0.29	0.0	83.37	52.43	0.0	0.0	0.0	-535.44
		-535.44	0.0	0.0		20.0	83.37	310.25	0.0	0.0	0.0	3026.89
1	6	3026.89	0.0	0.06	-0.29	0.0	83.37	52.43	0.0	0.0	0.0	-535.44
		-535.44	0.0	0.0		20.0	83.37	310.25	0.0	0.0	0.0	3026.89
1	7	3.132e+04	0.0	5.68e-03	-1.73	0.0	2.85	-18.07	0.0	0.0	0.0	171.46
		171.46	0.0	0.0		20.0	2.85	3132.02	0.0	0.0	0.0	3.132e+04
1	8	6273.56	0.0	0.03	-0.44	0.0	2.28	70.13	0.0	0.0	0.0	-712.61
		-712.61	0.0	0.0		20.0	2.28	631.53	0.0	0.0	0.0	6273.56
1	9	6072.60	0.0	3.57e-03	-0.48	0.0	0.0	-60.42	0.0	0.0	0.0	604.33
		554.91	0.0	0.0		20.0	0.0	606.83	0.0	0.0	0.0	6072.60
1	10	6221.46	0.0	0.02	-0.45	0.0	1.69	36.29	0.0	0.0	0.0	-371.18
		-371.18	0.0	0.0		20.0	1.69	625.12	0.0	0.0	0.0	6221.46

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
1	11	1.225e+04	0.0	0.04	-0.76	0.0	59.60	17.95	0.0	0.0	0.0	-186.52
		-186.52	0.0	0.0		20.0	59.60	1230.51	0.0	0.0	0.0	1.225e+04
1	12	6072.60	0.0	3.57e-03	-0.48	0.0	0.0	-60.42	0.0	0.0	0.0	604.33
		554.91	0.0	0.0		20.0	0.0	606.83	0.0	0.0	0.0	6072.60
1	13	6221.46	0.0	0.02	-0.45	0.0	1.69	36.29	0.0	0.0	0.0	-371.18
		-371.18	0.0	0.0		20.0	1.69	625.12	0.0	0.0	0.0	6221.46
1	14	1.225e+04	0.0	0.04	-0.76	0.0	59.60	17.95	0.0	0.0	0.0	-186.52
		-186.52	0.0	0.0		20.0	59.60	1230.51	0.0	0.0	0.0	1.225e+04
1	15	6072.60	0.0	3.57e-03	-0.48	0.0	0.0	-60.42	0.0	0.0	0.0	604.33
		554.91	0.0	0.0		20.0	0.0	606.83	0.0	0.0	0.0	6072.60
1	16	6072.60	0.0	3.57e-03	-0.48	0.0	0.0	-60.42	0.0	0.0	0.0	604.33
		554.91	0.0	0.0		20.0	0.0	606.83	0.0	0.0	0.0	6072.60
1	17	3838.97	0.0	0.05	-0.34	0.0	68.36	36.91	0.0	0.0	0.0	-377.56
		-377.56	0.0	0.0		20.0	68.36	390.98	0.0	0.0	0.0	3838.97
1	18	-168.70	0.0	-0.14	0.11	0.0	223.93	16.00	0.0	0.0	0.0	-168.70
		-4819.02	0.0	0.0		20.0	223.93	-464.97	0.0	0.0	0.0	-4819.02
1	19	3838.97	0.0	0.05	-0.34	0.0	68.36	36.91	0.0	0.0	0.0	-377.56
		-377.56	0.0	0.0		20.0	68.36	390.98	0.0	0.0	0.0	3838.97
1	20	-168.70	0.0	-0.14	0.11	0.0	223.93	16.00	0.0	0.0	0.0	-168.70
		-4819.02	0.0	0.0		20.0	223.93	-464.97	0.0	0.0	0.0	-4819.02
1	21	-124.45	0.0	-0.14	0.14	0.0	223.93	11.57	0.0	0.0	0.0	-124.45
		-5431.98	0.0	0.0		20.0	223.93	-526.21	0.0	0.0	0.0	-5431.98
2	1	4.622e+04	0.0	6.04e-03	-0.65	0.0	0.0	953.93	0.0	0.0	0.0	8349.23
		8349.23	0.0	0.0		25.0	0.0	2075.17	0.0	0.0	0.0	4.622e+04
2	2	4.233e+04	0.0	-0.02	-0.62	0.0	5.50	866.13	0.0	0.0	0.0	7653.24
		7653.24	0.0	0.0		25.0	5.50	1910.97	0.0	0.0	0.0	4.233e+04
2	3	2.582e+04	0.0	-0.07	-0.48	0.0	270.96	529.18	0.0	0.0	0.0	4375.09
		4375.09	0.0	0.0		25.0	270.96	1196.55	0.0	0.0	0.0	2.582e+04
2	4	6.896e+04	0.0	-0.11	-0.92	0.0	524.42	1395.84	0.0	0.0	0.0	1.240e+04
		1.240e+04	0.0	0.0		25.0	524.42	3144.09	0.0	0.0	0.0	6.896e+04
2	5	1.384e+04	0.0	-0.07	-0.31	0.0	270.96	281.86	0.0	0.0	0.0	2210.48
		2210.48	0.0	0.0		25.0	270.96	658.55	0.0	0.0	0.0	1.384e+04
2	6	1.384e+04	0.0	-0.07	-0.31	0.0	270.96	281.86	0.0	0.0	0.0	2210.48
		2210.48	0.0	0.0		25.0	270.96	658.55	0.0	0.0	0.0	1.384e+04
2	7	1.603e+05	0.0	-7.14e-03	-1.72	0.0	9.26	3224.70	0.0	0.0	0.0	3.057e+04
		3.057e+04	0.0	0.0		25.0	9.26	7156.72	0.0	0.0	0.0	1.603e+05
2	8	2.898e+04	0.0	-0.03	-0.45	0.0	7.42	588.09	0.0	0.0	0.0	5245.03
		5245.03	0.0	0.0		25.0	7.42	1315.50	0.0	0.0	0.0	2.898e+04
2	9	3.424e+04	0.0	4.47e-03	-0.48	0.0	0.0	706.61	0.0	0.0	0.0	6184.61
		6184.61	0.0	0.0		25.0	0.0	1537.16	0.0	0.0	0.0	3.424e+04
2	10	3.034e+04	0.0	-0.02	-0.46	0.0	5.50	618.82	0.0	0.0	0.0	5488.63
		5488.63	0.0	0.0		25.0	5.50	1372.97	0.0	0.0	0.0	3.034e+04
2	11	6.237e+04	0.0	-0.05	-0.78	0.0	193.71	1262.38	0.0	0.0	0.0	1.145e+04
		1.145e+04	0.0	0.0		25.0	193.71	2819.16	0.0	0.0	0.0	6.237e+04
2	12	3.424e+04	0.0	4.47e-03	-0.48	0.0	0.0	706.61	0.0	0.0	0.0	6184.61
		6184.61	0.0	0.0		25.0	0.0	1537.16	0.0	0.0	0.0	3.424e+04
2	13	3.034e+04	0.0	-0.02	-0.46	0.0	5.50	618.82	0.0	0.0	0.0	5488.63
		5488.63	0.0	0.0		25.0	5.50	1372.97	0.0	0.0	0.0	3.034e+04
2	14	6.237e+04	0.0	-0.05	-0.78	0.0	193.71	1262.38	0.0	0.0	0.0	1.145e+04
		1.145e+04	0.0	0.0		25.0	193.71	2819.16	0.0	0.0	0.0	6.237e+04
2	15	3.424e+04	0.0	4.47e-03	-0.48	0.0	0.0	706.61	0.0	0.0	0.0	6184.61

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		6184.61	0.0	0.0		25.0	0.0	1537.16	0.0	0.0	0.0	3.424e+04
2	16	3.424e+04	0.0	4.47e-03	-0.48	0.0	0.0	706.61	0.0	0.0	0.0	6184.61
		6184.61	0.0	0.0		25.0	0.0	1537.16	0.0	0.0	0.0	3.424e+04
2	17	1.871e+04	0.0	-0.07	-0.36	0.0	222.18	379.35	0.0	0.0	0.0	3157.36
		3157.36	0.0	0.0		25.0	222.18	874.61	0.0	0.0	0.0	1.871e+04
2	18	-5148.31	0.0	-0.17	0.07	0.0	727.76	-467.38	0.0	0.0	0.0	-5148.31
		-2.297e+04	0.0	0.0		25.0	727.76	-933.04	0.0	0.0	0.0	-2.297e+04
2	19	1.871e+04	0.0	-0.07	-0.36	0.0	222.18	379.35	0.0	0.0	0.0	3157.36
		3157.36	0.0	0.0		25.0	222.18	874.61	0.0	0.0	0.0	1.871e+04
2	20	-5148.31	0.0	-0.17	0.07	0.0	727.76	-467.38	0.0	0.0	0.0	-5148.31
		-2.297e+04	0.0	0.0		25.0	727.76	-933.04	0.0	0.0	0.0	-2.297e+04
2	21	-5715.22	0.0	-0.17	0.09	0.0	727.76	-524.33	0.0	0.0	0.0	-5715.22
		-2.584e+04	0.0	0.0		25.0	727.76	-1060.59	0.0	0.0	0.0	-2.584e+04
3	1	4.613e+04	0.0	-3.03e-03	-0.65	0.0	0.0	-8025.25	0.0	0.0	0.0	4.613e+04
		-5.069e+04	0.0	0.0		12.5	0.0	-7466.61	0.0	0.0	0.0	-5.069e+04
3	2	2.737e+06	0.0	-0.01	-0.63	0.0	-1.370e+04	-8056.92	0.0	0.0	0.0	2.737e+06
		2.640e+06	0.0	0.0		12.5	-1.370e+04	-7527.53	0.0	0.0	0.0	2.640e+06
3	3	3.664e+06	0.0	-0.03	-0.49	0.0	-1.808e+04	-8658.95	0.0	0.0	0.0	3.664e+06
		3.558e+06	0.0	0.0		12.5	-1.808e+04	-8303.17	0.0	0.0	0.0	3.558e+06
3	4	5.058e+06	0.0	-0.05	-0.94	0.0	-2.226e+04	-6773.29	0.0	0.0	0.0	5.058e+06
		4.979e+06	0.0	0.0		12.5	-2.226e+04	-5864.22	0.0	0.0	0.0	4.979e+06
3	5	3.652e+06	0.0	-0.03	-0.32	0.0	-1.808e+04	-6578.33	0.0	0.0	0.0	3.652e+06
		3.571e+06	0.0	0.0		12.5	-1.808e+04	-6367.39	0.0	0.0	0.0	3.571e+06
3	6	3.652e+06	0.0	-0.03	-0.32	0.0	-1.808e+04	-6578.33	0.0	0.0	0.0	3.652e+06
		3.571e+06	0.0	0.0		12.5	-1.808e+04	-6367.39	0.0	0.0	0.0	3.571e+06
3	7	5.159e+06	0.0	-4.26e-03	-1.72	0.0	-2.307e+04	-181.90	0.0	0.0	0.0	5.149e+06
		5.149e+06	0.0	0.0		12.5	-2.307e+04	1781.66	0.0	0.0	0.0	5.159e+06
3	8	3.667e+06	0.0	-0.02	-0.45	0.0	-1.849e+04	-5987.39	0.0	0.0	0.0	3.667e+06
		3.595e+06	0.0	0.0		12.5	-1.849e+04	-5613.07	0.0	0.0	0.0	3.595e+06
3	9	3.417e+04	0.0	-2.24e-03	-0.48	0.0	0.0	-5944.63	0.0	0.0	0.0	3.417e+04
		-3.755e+04	0.0	0.0		12.5	0.0	-5530.82	0.0	0.0	0.0	-3.755e+04
3	10	2.726e+06	0.0	-0.01	-0.46	0.0	-1.370e+04	-5976.31	0.0	0.0	0.0	2.726e+06
		2.653e+06	0.0	0.0		12.5	-1.370e+04	-5591.74	0.0	0.0	0.0	2.653e+06
3	11	3.761e+06	0.0	-0.03	-0.79	0.0	-1.680e+04	-4576.07	0.0	0.0	0.0	3.761e+06
		3.709e+06	0.0	0.0		12.5	-1.680e+04	-3780.64	0.0	0.0	0.0	3.709e+06
3	12	3.417e+04	0.0	-2.24e-03	-0.48	0.0	0.0	-5944.63	0.0	0.0	0.0	3.417e+04
		-3.755e+04	0.0	0.0		12.5	0.0	-5530.82	0.0	0.0	0.0	-3.755e+04
3	13	2.726e+06	0.0	-0.01	-0.46	0.0	-1.370e+04	-5976.31	0.0	0.0	0.0	2.726e+06
		2.653e+06	0.0	0.0		12.5	-1.370e+04	-5591.74	0.0	0.0	0.0	2.653e+06
3	14	3.761e+06	0.0	-0.03	-0.79	0.0	-1.680e+04	-4576.07	0.0	0.0	0.0	3.761e+06
		3.709e+06	0.0	0.0		12.5	-1.680e+04	-3780.64	0.0	0.0	0.0	3.709e+06
3	15	3.417e+04	0.0	-2.24e-03	-0.48	0.0	0.0	-5944.63	0.0	0.0	0.0	3.417e+04
		-3.755e+04	0.0	0.0		12.5	0.0	-5530.82	0.0	0.0	0.0	-3.755e+04
3	16	3.417e+04	0.0	-2.24e-03	-0.48	0.0	0.0	-5944.63	0.0	0.0	0.0	3.417e+04
		-3.755e+04	0.0	0.0		12.5	0.0	-5530.82	0.0	0.0	0.0	-3.755e+04
3	17	3.494e+06	0.0	-0.03	-0.37	0.0	-1.600e+04	-7746.78	0.0	0.0	0.0	3.494e+06
		3.398e+06	0.0	0.0		12.5	-1.600e+04	-7477.27	0.0	0.0	0.0	3.398e+06
3	18	5.271e+06	0.0	-0.09	-0.02	0.0	-2.137e+04	-8460.29	0.0	0.0	0.0	5.271e+06
		5.164e+06	0.0	0.0		12.5	-2.137e+04	-8636.74	0.0	0.0	0.0	5.164e+06
3	19	3.494e+06	0.0	-0.03	-0.37	0.0	-1.600e+04	-7746.78	0.0	0.0	0.0	3.494e+06
		3.398e+06	0.0	0.0		12.5	-1.600e+04	-7477.27	0.0	0.0	0.0	3.398e+06

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
3	20	5.271e+06	0.0	-0.09	-0.02	0.0	-2.137e+04	-8460.29	0.0	0.0	0.0	5.271e+06
		5.164e+06	0.0	0.0		12.5	-2.137e+04	-8636.74	0.0	0.0	0.0	5.164e+06
3	21	5.269e+06	0.0	-0.09	0.03	0.0	-2.137e+04	-7784.28	0.0	0.0	0.0	5.269e+06
		5.170e+06	0.0	0.0		12.5	-2.137e+04	-7995.84	0.0	0.0	0.0	5.170e+06
4	1	-4.768e+04	0.0	3.02e-03	-0.65	0.0	0.0	-7767.57	0.0	0.0	0.0	-4.768e+04
		-1.413e+05	0.0	0.0		12.5	0.0	-7210.25	0.0	0.0	0.0	-1.413e+05
4	2	2.643e+06	0.0	9.67e-03	-0.63	0.0	-1.370e+04	-8096.47	0.0	0.0	0.0	2.643e+06
		2.545e+06	0.0	0.0		12.5	-1.370e+04	-7562.70	0.0	0.0	0.0	2.545e+06
4	3	3.561e+06	0.0	-0.03	-0.50	0.0	-1.797e+04	-9055.40	0.0	0.0	0.0	3.561e+06
		3.450e+06	0.0	0.0		12.5	-1.797e+04	-8685.27	0.0	0.0	0.0	3.450e+06
4	4	4.984e+06	0.0	-0.05	-0.96	0.0	-2.206e+04	-6755.90	0.0	0.0	0.0	4.984e+06
		4.905e+06	0.0	0.0		12.5	-2.206e+04	-5824.03	0.0	0.0	0.0	4.905e+06
4	5	3.573e+06	0.0	-0.03	-0.34	0.0	-1.797e+04	-7041.59	0.0	0.0	0.0	3.573e+06
		3.487e+06	0.0	0.0		12.5	-1.797e+04	-6815.94	0.0	0.0	0.0	3.487e+06
4	6	3.573e+06	0.0	-0.03	-0.34	0.0	-1.797e+04	-7041.59	0.0	0.0	0.0	3.573e+06
		3.487e+06	0.0	0.0		12.5	-1.797e+04	-6815.94	0.0	0.0	0.0	3.487e+06
4	7	5.187e+06	0.0	-5.59e-03	-1.72	0.0	-2.307e+04	949.05	0.0	0.0	0.0	5.163e+06
		5.163e+06	0.0	0.0		12.5	-2.307e+04	2910.45	0.0	0.0	0.0	5.187e+06
4	8	3.597e+06	0.0	-0.01	-0.46	0.0	-1.849e+04	-6197.77	0.0	0.0	0.0	3.597e+06
		3.522e+06	0.0	0.0		12.5	-1.849e+04	-5816.73	0.0	0.0	0.0	3.522e+06
4	9	-3.532e+04	0.0	2.23e-03	-0.48	0.0	0.0	-5753.75	0.0	0.0	0.0	-3.532e+04
		-1.047e+05	0.0	0.0		12.5	0.0	-5340.93	0.0	0.0	0.0	-1.047e+05
4	10	2.656e+06	0.0	-0.01	-0.46	0.0	-1.370e+04	-6082.66	0.0	0.0	0.0	2.656e+06
		2.582e+06	0.0	0.0		12.5	-1.370e+04	-5693.37	0.0	0.0	0.0	2.582e+06
4	11	3.712e+06	0.0	-0.02	-0.80	0.0	-1.673e+04	-4375.10	0.0	0.0	0.0	3.712e+06
		3.662e+06	0.0	0.0		12.5	-1.673e+04	-3568.69	0.0	0.0	0.0	3.662e+06
4	12	-3.532e+04	0.0	2.23e-03	-0.48	0.0	0.0	-5753.75	0.0	0.0	0.0	-3.532e+04
		-1.047e+05	0.0	0.0		12.5	0.0	-5340.93	0.0	0.0	0.0	-1.047e+05
4	13	2.656e+06	0.0	-0.01	-0.46	0.0	-1.370e+04	-6082.66	0.0	0.0	0.0	2.656e+06
		2.582e+06	0.0	0.0		12.5	-1.370e+04	-5693.37	0.0	0.0	0.0	2.582e+06
4	14	3.712e+06	0.0	-0.02	-0.80	0.0	-1.673e+04	-4375.10	0.0	0.0	0.0	3.712e+06
		3.662e+06	0.0	0.0		12.5	-1.673e+04	-3568.69	0.0	0.0	0.0	3.662e+06
4	15	-3.532e+04	0.0	2.23e-03	-0.48	0.0	0.0	-5753.75	0.0	0.0	0.0	-3.532e+04
		-1.047e+05	0.0	0.0		12.5	0.0	-5340.93	0.0	0.0	0.0	-1.047e+05
4	16	-3.532e+04	0.0	2.23e-03	-0.48	0.0	0.0	-5753.75	0.0	0.0	0.0	-3.532e+04
		-1.047e+05	0.0	0.0		12.5	0.0	-5340.93	0.0	0.0	0.0	-1.047e+05
4	17	3.401e+06	0.0	-0.03	-0.38	0.0	-1.592e+04	-8177.81	0.0	0.0	0.0	3.401e+06
		3.301e+06	0.0	0.0		12.5	-1.592e+04	-7894.06	0.0	0.0	0.0	3.301e+06
4	18	5.167e+06	0.0	-0.08	-0.05	0.0	-2.109e+04	-9646.31	0.0	0.0	0.0	5.167e+06
		5.046e+06	0.0	0.0		12.5	-2.109e+04	-9785.70	0.0	0.0	0.0	5.046e+06
4	19	3.401e+06	0.0	-0.03	-0.38	0.0	-1.592e+04	-8177.81	0.0	0.0	0.0	3.401e+06
		3.301e+06	0.0	0.0		12.5	-1.592e+04	-7894.06	0.0	0.0	0.0	3.301e+06
4	20	5.167e+06	0.0	-0.08	-0.05	0.0	-2.109e+04	-9646.31	0.0	0.0	0.0	5.167e+06
		5.046e+06	0.0	0.0		12.5	-2.109e+04	-9785.70	0.0	0.0	0.0	5.046e+06
4	21	5.173e+06	0.0	-0.08	-0.03	0.0	-2.109e+04	-8969.79	0.0	0.0	0.0	5.173e+06
		5.059e+06	0.0	0.0		12.5	-2.109e+04	-9144.17	0.0	0.0	0.0	5.059e+06
5	1	-1.388e+05	0.0	0.03	-0.65	0.0	0.0	-6818.25	0.0	0.0	0.0	-1.388e+05
		-9.010e+05	0.0	0.0		225.0	0.0	0.02	0.0	0.0	0.0	-9.010e+05
5	2	2.549e+06	0.0	0.08	-0.66	0.0	-1.368e+04	-7025.84	0.0	0.0	0.0	2.549e+06
		1.747e+06	0.0	0.0		225.0	-1.368e+04	0.04	0.0	0.0	0.0	1.747e+06
5	3	3.454e+06	0.0	0.45	-0.66	0.0	-1.699e+04	-8071.56	0.0	0.0	0.0	3.454e+06

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		2.210e+06	0.0	0.0		225.0	-1.699e+04	-2391.12	0.0	0.0	0.0	2.210e+06
5	4	4.910e+06	0.0	0.73	-1.21	0.0	-2.015e+04	-5035.69	0.0	0.0	0.0	4.910e+06
		3.515e+06	0.0	0.0		225.0	-2.015e+04	-6407.40	0.0	0.0	0.0	3.515e+06
5	5	3.490e+06	0.0	0.46	-0.50	0.0	-1.699e+04	-6303.86	0.0	0.0	0.0	3.490e+06
		2.444e+06	0.0	0.0		225.0	-1.699e+04	-2391.12	0.0	0.0	0.0	2.444e+06
5	6	3.490e+06	0.0	0.46	-0.50	0.0	-1.699e+04	-6303.86	0.0	0.0	0.0	3.490e+06
		2.444e+06	0.0	0.0		225.0	-1.699e+04	-2391.12	0.0	0.0	0.0	2.444e+06
5	7	5.543e+06	0.0	0.34	-1.72	0.0	-2.305e+04	3632.13	0.0	0.0	0.0	5.192e+06
		5.192e+06	0.0	0.0		225.0	-2.305e+04	-1183.58	0.0	0.0	0.0	5.517e+06
5	8	3.525e+06	0.0	0.13	-0.50	0.0	-1.847e+04	-5330.80	0.0	0.0	0.0	3.525e+06
		2.907e+06	0.0	0.0		225.0	-1.847e+04	0.04	0.0	0.0	0.0	2.907e+06
5	9	-1.028e+05	0.0	0.02	-0.48	0.0	0.0	-5050.56	0.0	0.0	0.0	-1.028e+05
		-6.674e+05	0.0	0.0		225.0	0.0	0.01	0.0	0.0	0.0	-6.674e+05
5	10	2.585e+06	0.0	0.09	-0.49	0.0	-1.368e+04	-5258.14	0.0	0.0	0.0	2.585e+06
		1.980e+06	0.0	0.0		225.0	-1.368e+04	0.03	0.0	0.0	0.0	1.980e+06
5	11	3.666e+06	0.0	0.29	-0.90	0.0	-1.603e+04	-3003.78	0.0	0.0	0.0	3.666e+06
		2.949e+06	0.0	0.0		225.0	-1.603e+04	-2982.36	0.0	0.0	0.0	2.949e+06
5	12	-1.028e+05	0.0	0.02	-0.48	0.0	0.0	-5050.56	0.0	0.0	0.0	-1.028e+05
		-6.674e+05	0.0	0.0		225.0	0.0	0.01	0.0	0.0	0.0	-6.674e+05
5	13	2.585e+06	0.0	0.09	-0.49	0.0	-1.368e+04	-5258.14	0.0	0.0	0.0	2.585e+06
		1.980e+06	0.0	0.0		225.0	-1.368e+04	0.03	0.0	0.0	0.0	1.980e+06
5	14	3.666e+06	0.0	0.29	-0.90	0.0	-1.603e+04	-3003.78	0.0	0.0	0.0	3.666e+06
		2.949e+06	0.0	0.0		225.0	-1.603e+04	-2982.36	0.0	0.0	0.0	2.949e+06
5	15	-1.028e+05	0.0	0.02	-0.48	0.0	0.0	-5050.56	0.0	0.0	0.0	-1.028e+05
		-6.674e+05	0.0	0.0		225.0	0.0	0.01	0.0	0.0	0.0	-6.674e+05
5	16	-1.028e+05	0.0	0.02	-0.48	0.0	0.0	-5050.56	0.0	0.0	0.0	-1.028e+05
		-6.674e+05	0.0	0.0		225.0	0.0	0.01	0.0	0.0	0.0	-6.674e+05
5	17	3.304e+06	0.0	0.45	-0.54	0.0	-1.511e+04	-7324.58	0.0	0.0	0.0	3.304e+06
		2.142e+06	0.0	0.0		225.0	-1.547e+04	-2416.39	0.0	0.0	0.0	2.142e+06
5	18	5.051e+06	0.0	1.32	-0.52	0.0	-1.845e+04	-9043.11	0.0	0.0	0.0	5.051e+06
		2.933e+06	0.0	0.0		225.0	-1.965e+04	-8054.70	0.0	0.0	0.0	2.933e+06
5	19	3.304e+06	0.0	0.45	-0.54	0.0	-1.511e+04	-7324.58	0.0	0.0	0.0	3.304e+06
		2.142e+06	0.0	0.0		225.0	-1.547e+04	-2416.39	0.0	0.0	0.0	2.142e+06
5	20	5.051e+06	0.0	1.32	-0.52	0.0	-1.845e+04	-9043.11	0.0	0.0	0.0	5.051e+06
		2.933e+06	0.0	0.0		225.0	-1.965e+04	-8054.70	0.0	0.0	0.0	2.933e+06
5	21	5.064e+06	0.0	1.32	-0.49	0.0	-1.845e+04	-8429.30	0.0	0.0	0.0	5.064e+06
		3.014e+06	0.0	0.0		225.0	-1.965e+04	-8054.70	0.0	0.0	0.0	3.014e+06
6	1	-1.388e+05	0.0	-0.03	-0.65	0.0	0.0	0.09	0.0	0.0	0.0	-9.010e+05
		-9.010e+05	0.0	0.0		225.0	0.0	6818.36	0.0	0.0	0.0	-1.388e+05
6	2	2.549e+06	0.0	-0.08	-0.66	0.0	-1.368e+04	0.07	0.0	0.0	0.0	1.747e+06
		1.747e+06	0.0	0.0		225.0	-1.368e+04	7025.94	0.0	0.0	0.0	2.549e+06
6	3	2.584e+06	0.0	-0.26	-0.75	0.0	-1.517e+04	-2391.09	0.0	0.0	0.0	2.210e+06
		2.125e+06	0.0	0.0		225.0	-1.517e+04	6052.88	0.0	0.0	0.0	2.584e+06
6	4	3.515e+06	0.0	-0.43	-1.36	0.0	-1.658e+04	-6407.55	0.0	0.0	0.0	3.515e+06
		2.710e+06	0.0	0.0		225.0	-1.658e+04	1718.90	0.0	0.0	0.0	2.736e+06
6	5	2.620e+06	0.0	-0.25	-0.58	0.0	-1.517e+04	-2391.12	0.0	0.0	0.0	2.444e+06
		2.335e+06	0.0	0.0		225.0	-1.517e+04	4285.15	0.0	0.0	0.0	2.620e+06
6	6	2.620e+06	0.0	-0.25	-0.58	0.0	-1.517e+04	-2391.12	0.0	0.0	0.0	2.444e+06
		2.335e+06	0.0	0.0		225.0	-1.517e+04	4285.15	0.0	0.0	0.0	2.620e+06
6	7	5.517e+06	0.0	-0.79	-1.60	0.0	-2.305e+04	-1183.72	0.0	0.0	0.0	5.517e+06
		5.075e+06	0.0	0.0		225.0	-2.305e+04	-445.68	0.0	0.0	0.0	5.075e+06

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
6	8	3.525e+06	0.0	-0.13	-0.50	0.0	-1.847e+04	0.04	0.0	0.0	0.0	2.907e+06
		2.907e+06	0.0	0.0		225.0	-1.847e+04	5330.87	0.0	0.0	0.0	3.525e+06
6	9	-1.028e+05	0.0	-0.02	-0.48	0.0	0.0	0.06	0.0	0.0	0.0	-6.674e+05
		-6.674e+05	0.0	0.0		225.0	0.0	5050.63	0.0	0.0	0.0	-1.028e+05
6	10	2.585e+06	0.0	-0.09	-0.49	0.0	-1.368e+04	0.04	0.0	0.0	0.0	1.980e+06
		1.980e+06	0.0	0.0		225.0	-1.368e+04	5258.22	0.0	0.0	0.0	2.585e+06
6	11	2.949e+06	0.0	-0.04	-0.92	0.0	-1.473e+04	-2982.47	0.0	0.0	0.0	2.949e+06
		2.631e+06	0.0	0.0		225.0	-1.473e+04	2039.92	0.0	0.0	0.0	2.698e+06
6	12	-1.028e+05	0.0	-0.02	-0.48	0.0	0.0	0.06	0.0	0.0	0.0	-6.674e+05
		-6.674e+05	0.0	0.0		225.0	0.0	5050.63	0.0	0.0	0.0	-1.028e+05
6	13	2.585e+06	0.0	-0.09	-0.49	0.0	-1.368e+04	0.04	0.0	0.0	0.0	1.980e+06
		1.980e+06	0.0	0.0		225.0	-1.368e+04	5258.22	0.0	0.0	0.0	2.585e+06
6	14	2.949e+06	0.0	-0.04	-0.92	0.0	-1.473e+04	-2982.47	0.0	0.0	0.0	2.949e+06
		2.631e+06	0.0	0.0		225.0	-1.473e+04	2039.92	0.0	0.0	0.0	2.698e+06
6	15	-1.028e+05	0.0	-0.02	-0.48	0.0	0.0	0.06	0.0	0.0	0.0	-6.674e+05
		-6.674e+05	0.0	0.0		225.0	0.0	5050.63	0.0	0.0	0.0	-1.028e+05
6	16	-1.028e+05	0.0	-0.02	-0.48	0.0	0.0	0.06	0.0	0.0	0.0	-6.674e+05
		-6.674e+05	0.0	0.0		225.0	0.0	5050.63	0.0	0.0	0.0	-1.028e+05
6	17	2.425e+06	0.0	-0.26	-0.63	0.0	-1.398e+04	-2416.39	0.0	0.0	0.0	2.142e+06
		2.046e+06	0.0	0.0		225.0	-1.434e+04	5284.52	0.0	0.0	0.0	2.425e+06
6	18	2.933e+06	0.0	1.07	-0.89	0.0	-1.466e+04	-8054.72	0.0	0.0	0.0	2.933e+06
		2.082e+06	0.0	0.0		225.0	-1.586e+04	2242.75	0.0	0.0	0.0	2.121e+06
6	19	2.425e+06	0.0	-0.26	-0.63	0.0	-1.398e+04	-2416.39	0.0	0.0	0.0	2.142e+06
		2.046e+06	0.0	0.0		225.0	-1.434e+04	5284.52	0.0	0.0	0.0	2.425e+06
6	20	2.933e+06	0.0	1.07	-0.89	0.0	-1.466e+04	-8054.72	0.0	0.0	0.0	2.933e+06
		2.082e+06	0.0	0.0		225.0	-1.586e+04	2242.75	0.0	0.0	0.0	2.121e+06
6	21	3.014e+06	0.0	-1.06	-0.86	0.0	-1.466e+04	-8054.72	0.0	0.0	0.0	3.014e+06
		2.112e+06	0.0	0.0		225.0	-1.586e+04	1628.94	0.0	0.0	0.0	2.135e+06
7	1	-5.192e+04	0.0	-3.01e-03	-0.65	0.0	0.0	6531.20	0.0	0.0	0.0	-1.370e+05
		-1.370e+05	0.0	0.0		12.5	0.0	7088.51	0.0	0.0	0.0	-5.192e+04
7	2	2.636e+06	0.0	-9.67e-03	-0.63	0.0	-1.370e+04	6439.09	0.0	0.0	0.0	2.552e+06
		2.552e+06	0.0	0.0		12.5	-1.370e+04	6972.86	0.0	0.0	0.0	2.636e+06
7	3	2.660e+06	0.0	-8.59e-03	-0.76	0.0	-1.421e+04	5439.88	0.0	0.0	0.0	2.588e+06
		2.588e+06	0.0	0.0		12.5	-1.421e+04	6129.05	0.0	0.0	0.0	2.660e+06
7	4	2.763e+06	0.0	0.02	-1.37	0.0	-1.471e+04	1094.93	0.0	0.0	0.0	2.740e+06
		2.740e+06	0.0	0.0		12.5	-1.471e+04	2549.45	0.0	0.0	0.0	2.763e+06
7	5	2.674e+06	0.0	-7.81e-03	-0.59	0.0	-1.421e+04	3746.61	0.0	0.0	0.0	2.624e+06
		2.624e+06	0.0	0.0		12.5	-1.421e+04	4291.29	0.0	0.0	0.0	2.674e+06
7	6	2.674e+06	0.0	-7.81e-03	-0.59	0.0	-1.421e+04	3746.61	0.0	0.0	0.0	2.624e+06
		2.624e+06	0.0	0.0		12.5	-1.421e+04	4291.29	0.0	0.0	0.0	2.674e+06
7	7	5.080e+06	0.0	0.06	-1.32	0.0	-2.307e+04	-1197.48	0.0	0.0	0.0	5.080e+06
		5.074e+06	0.0	0.0		12.5	-2.307e+04	257.37	0.0	0.0	0.0	5.074e+06
7	8	3.590e+06	0.0	0.01	-0.46	0.0	-1.849e+04	4713.58	0.0	0.0	0.0	3.529e+06
		3.529e+06	0.0	0.0		12.5	-1.849e+04	5094.62	0.0	0.0	0.0	3.590e+06
7	9	-3.846e+04	0.0	-2.23e-03	-0.48	0.0	0.0	4837.93	0.0	0.0	0.0	-1.015e+05
		-1.015e+05	0.0	0.0		12.5	0.0	5250.75	0.0	0.0	0.0	-3.846e+04
7	10	2.650e+06	0.0	-0.01	-0.46	0.0	-1.370e+04	4745.82	0.0	0.0	0.0	2.588e+06
		2.588e+06	0.0	0.0		12.5	-1.370e+04	5135.10	0.0	0.0	0.0	2.650e+06
7	11	2.726e+06	0.0	4.13e-03	-0.92	0.0	-1.406e+04	1519.37	0.0	0.0	0.0	2.701e+06
		2.701e+06	0.0	0.0		12.5	-1.406e+04	2476.99	0.0	0.0	0.0	2.726e+06
7	12	-3.846e+04	0.0	-2.23e-03	-0.48	0.0	0.0	4837.93	0.0	0.0	0.0	-1.015e+05

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		-1.015e+05	0.0	0.0		12.5	0.0	5250.75	0.0	0.0	0.0	-3.846e+04
7	13	2.650e+06	0.0	-0.01	-0.46	0.0	-1.370e+04	4745.82	0.0	0.0	0.0	2.588e+06
		2.588e+06	0.0	0.0		12.5	-1.370e+04	5135.10	0.0	0.0	0.0	2.650e+06
7	14	2.726e+06	0.0	4.13e-03	-0.92	0.0	-1.406e+04	1519.37	0.0	0.0	0.0	2.701e+06
		2.701e+06	0.0	0.0		12.5	-1.406e+04	2476.99	0.0	0.0	0.0	2.726e+06
7	15	-3.846e+04	0.0	-2.23e-03	-0.48	0.0	0.0	4837.93	0.0	0.0	0.0	-1.015e+05
		-1.015e+05	0.0	0.0		12.5	0.0	5250.75	0.0	0.0	0.0	-3.846e+04
7	16	-3.846e+04	0.0	-2.23e-03	-0.48	0.0	0.0	4837.93	0.0	0.0	0.0	-1.015e+05
		-1.015e+05	0.0	0.0		12.5	0.0	5250.75	0.0	0.0	0.0	-3.846e+04
7	17	2.492e+06	0.0	9.27e-03	-0.64	0.0	-1.356e+04	4819.98	0.0	0.0	0.0	2.428e+06
		2.428e+06	0.0	0.0		12.5	-1.356e+04	5426.13	0.0	0.0	0.0	2.492e+06
7	18	2.152e+06	0.0	0.05	-0.91	0.0	-1.324e+04	1750.51	0.0	0.0	0.0	2.124e+06
		2.124e+06	0.0	0.0		12.5	-1.324e+04	2685.80	0.0	0.0	0.0	2.152e+06
7	19	2.492e+06	0.0	9.27e-03	-0.64	0.0	-1.356e+04	4819.98	0.0	0.0	0.0	2.428e+06
		2.428e+06	0.0	0.0		12.5	-1.356e+04	5426.13	0.0	0.0	0.0	2.492e+06
7	20	2.152e+06	0.0	0.05	-0.91	0.0	-1.324e+04	1750.51	0.0	0.0	0.0	2.124e+06
		2.124e+06	0.0	0.0		12.5	-1.324e+04	2685.80	0.0	0.0	0.0	2.152e+06
7	21	2.157e+06	0.0	0.05	-0.88	0.0	-1.324e+04	1109.14	0.0	0.0	0.0	2.138e+06
		2.138e+06	0.0	0.0		12.5	-1.324e+04	2009.43	0.0	0.0	0.0	2.157e+06
8	1	4.611e+04	0.0	-3.03e-03	-0.65	0.0	0.0	7463.18	0.0	0.0	0.0	-5.067e+04
		-5.067e+04	0.0	0.0		12.5	0.0	8021.81	0.0	0.0	0.0	4.611e+04
8	2	2.740e+06	0.0	0.01	-0.63	0.0	-1.370e+04	7968.65	0.0	0.0	0.0	2.637e+06
		2.637e+06	0.0	0.0		12.5	-1.370e+04	8498.04	0.0	0.0	0.0	2.740e+06
8	3	2.756e+06	0.0	7.90e-03	-0.76	0.0	-1.411e+04	7214.33	0.0	0.0	0.0	2.661e+06
		2.661e+06	0.0	0.0		12.5	-1.411e+04	7907.11	0.0	0.0	0.0	2.756e+06
8	4	2.818e+06	0.0	0.02	-1.37	0.0	-1.451e+04	3574.61	0.0	0.0	0.0	2.765e+06
		2.765e+06	0.0	0.0		12.5	-1.451e+04	5036.46	0.0	0.0	0.0	2.818e+06
8	5	2.744e+06	0.0	7.12e-03	-0.59	0.0	-1.411e+04	5279.43	0.0	0.0	0.0	2.674e+06
		2.674e+06	0.0	0.0		12.5	-1.411e+04	5827.38	0.0	0.0	0.0	2.744e+06
8	6	2.744e+06	0.0	7.12e-03	-0.59	0.0	-1.411e+04	5279.43	0.0	0.0	0.0	2.674e+06
		2.674e+06	0.0	0.0		12.5	-1.411e+04	5827.38	0.0	0.0	0.0	2.744e+06
8	7	5.103e+06	0.0	0.06	-1.30	0.0	-2.307e+04	1450.79	0.0	0.0	0.0	5.076e+06
		5.076e+06	0.0	0.0		12.5	-2.307e+04	2880.64	0.0	0.0	0.0	5.103e+06
8	8	3.671e+06	0.0	0.02	-0.45	0.0	-1.849e+04	6210.67	0.0	0.0	0.0	3.591e+06
		3.591e+06	0.0	0.0		12.5	-1.849e+04	6584.99	0.0	0.0	0.0	3.671e+06
8	9	3.415e+04	0.0	-2.24e-03	-0.48	0.0	0.0	5528.28	0.0	0.0	0.0	-3.754e+04
		-3.754e+04	0.0	0.0		12.5	0.0	5942.08	0.0	0.0	0.0	3.415e+04
8	10	2.728e+06	0.0	0.01	-0.46	0.0	-1.370e+04	6033.75	0.0	0.0	0.0	2.650e+06
		2.650e+06	0.0	0.0		12.5	-1.370e+04	6418.31	0.0	0.0	0.0	2.728e+06
8	11	2.775e+06	0.0	4.83e-03	-0.92	0.0	-1.399e+04	3330.99	0.0	0.0	0.0	2.727e+06
		2.727e+06	0.0	0.0		12.5	-1.399e+04	4286.65	0.0	0.0	0.0	2.775e+06
8	12	3.415e+04	0.0	-2.24e-03	-0.48	0.0	0.0	5528.28	0.0	0.0	0.0	-3.754e+04
		-3.754e+04	0.0	0.0		12.5	0.0	5942.08	0.0	0.0	0.0	3.415e+04
8	13	2.728e+06	0.0	0.01	-0.46	0.0	-1.370e+04	6033.75	0.0	0.0	0.0	2.650e+06
		2.650e+06	0.0	0.0		12.5	-1.370e+04	6418.31	0.0	0.0	0.0	2.728e+06
8	14	2.775e+06	0.0	4.83e-03	-0.92	0.0	-1.399e+04	3330.99	0.0	0.0	0.0	2.727e+06
		2.727e+06	0.0	0.0		12.5	-1.399e+04	4286.65	0.0	0.0	0.0	2.775e+06
8	15	3.415e+04	0.0	-2.24e-03	-0.48	0.0	0.0	5528.28	0.0	0.0	0.0	-3.754e+04
		-3.754e+04	0.0	0.0		12.5	0.0	5942.08	0.0	0.0	0.0	3.415e+04
8	16	3.415e+04	0.0	-2.24e-03	-0.48	0.0	0.0	5528.28	0.0	0.0	0.0	-3.754e+04
		-3.754e+04	0.0	0.0		12.5	0.0	5942.08	0.0	0.0	0.0	3.415e+04

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
8	17	2.575e+06	0.0	8.63e-03	-0.64	0.0	-1.348e+04	6331.48	0.0	0.0	0.0	2.493e+06
		2.493e+06	0.0	0.0		12.5	-1.348e+04	6941.55	0.0	0.0	0.0	2.575e+06
8	18	2.205e+06	0.0	0.05	-0.93	0.0	-1.297e+04	3786.84	0.0	0.0	0.0	2.151e+06
		2.151e+06	0.0	0.0		12.5	-1.297e+04	4745.59	0.0	0.0	0.0	2.205e+06
8	19	2.575e+06	0.0	8.63e-03	-0.64	0.0	-1.348e+04	6331.48	0.0	0.0	0.0	2.493e+06
		2.493e+06	0.0	0.0		12.5	-1.348e+04	6941.55	0.0	0.0	0.0	2.575e+06
8	20	2.205e+06	0.0	0.05	-0.93	0.0	-1.297e+04	3786.84	0.0	0.0	0.0	2.151e+06
		2.151e+06	0.0	0.0		12.5	-1.297e+04	4745.59	0.0	0.0	0.0	2.205e+06
8	21	2.202e+06	0.0	0.05	-0.90	0.0	-1.297e+04	3146.10	0.0	0.0	0.0	2.157e+06
		2.157e+06	0.0	0.0		12.5	-1.297e+04	4069.74	0.0	0.0	0.0	2.202e+06
9	1	4.530e+04	0.0	-6.04e-03	-0.65	0.0	0.0	-2000.99	0.0	0.0	0.0	4.530e+04
		9276.46	0.0	0.0		25.0	0.0	-879.75	0.0	0.0	0.0	9276.46
9	2	4.140e+04	0.0	-0.02	-0.62	0.0	5.50	-1836.80	0.0	0.0	0.0	4.140e+04
		8580.47	0.0	0.0		25.0	5.50	-791.96	0.0	0.0	0.0	8580.47
9	3	5.654e+04	0.0	-0.02	-0.76	0.0	-258.04	-2493.75	0.0	0.0	0.0	5.654e+04
		1.162e+04	0.0	0.0		25.0	-258.04	-1098.19	0.0	0.0	0.0	1.162e+04
9	4	1.194e+05	0.0	-0.03	-1.39	0.0	-509.66	-5264.60	0.0	0.0	0.0	1.194e+05
		2.449e+04	0.0	0.0		25.0	-509.66	-2319.76	0.0	0.0	0.0	2.449e+04
9	5	4.480e+04	0.0	-0.01	-0.59	0.0	-258.04	-1974.97	0.0	0.0	0.0	4.480e+04
		9210.02	0.0	0.0		25.0	-258.04	-870.11	0.0	0.0	0.0	9210.02
9	6	4.480e+04	0.0	-0.01	-0.59	0.0	-258.04	-1974.97	0.0	0.0	0.0	4.480e+04
		9210.02	0.0	0.0		25.0	-258.04	-870.11	0.0	0.0	0.0	9210.02
9	7	1.091e+05	0.0	-0.12	-1.28	0.0	9.26	-4882.47	0.0	0.0	0.0	1.091e+05
		2.208e+04	0.0	0.0		25.0	9.26	-2099.36	0.0	0.0	0.0	2.208e+04
9	8	2.829e+04	0.0	-0.03	-0.45	0.0	7.42	-1260.55	0.0	0.0	0.0	2.829e+04
		5931.87	0.0	0.0		25.0	7.42	-533.15	0.0	0.0	0.0	5931.87
9	9	3.355e+04	0.0	-4.47e-03	-0.48	0.0	0.0	-1482.22	0.0	0.0	0.0	3.355e+04
		6871.45	0.0	0.0		25.0	0.0	-651.67	0.0	0.0	0.0	6871.45
9	10	2.966e+04	0.0	-0.02	-0.46	0.0	5.50	-1318.02	0.0	0.0	0.0	2.966e+04
		6175.46	0.0	0.0		25.0	5.50	-563.88	0.0	0.0	0.0	6175.46
9	11	7.630e+04	0.0	-0.01	-0.91	0.0	-181.35	-3375.59	0.0	0.0	0.0	7.630e+04
		1.574e+04	0.0	0.0		25.0	-181.35	-1470.98	0.0	0.0	0.0	1.574e+04
9	12	3.355e+04	0.0	-4.47e-03	-0.48	0.0	0.0	-1482.22	0.0	0.0	0.0	3.355e+04
		6871.45	0.0	0.0		25.0	0.0	-651.67	0.0	0.0	0.0	6871.45
9	13	2.966e+04	0.0	-0.02	-0.46	0.0	5.50	-1318.02	0.0	0.0	0.0	2.966e+04
		6175.46	0.0	0.0		25.0	5.50	-563.88	0.0	0.0	0.0	6175.46
9	14	7.630e+04	0.0	-0.01	-0.91	0.0	-181.35	-3375.59	0.0	0.0	0.0	7.630e+04
		1.574e+04	0.0	0.0		25.0	-181.35	-1470.98	0.0	0.0	0.0	1.574e+04
9	15	3.355e+04	0.0	-4.47e-03	-0.48	0.0	0.0	-1482.22	0.0	0.0	0.0	3.355e+04
		6871.45	0.0	0.0		25.0	0.0	-651.67	0.0	0.0	0.0	6871.45
9	16	3.355e+04	0.0	-4.47e-03	-0.48	0.0	0.0	-1482.22	0.0	0.0	0.0	3.355e+04
		6871.45	0.0	0.0		25.0	0.0	-651.67	0.0	0.0	0.0	6871.45
9	17	4.996e+04	0.0	-0.02	-0.65	0.0	-210.35	-2201.79	0.0	0.0	0.0	4.996e+04
		1.027e+04	0.0	0.0		25.0	-210.35	-970.65	0.0	0.0	0.0	1.027e+04
9	18	8.280e+04	0.0	-0.11	-0.96	0.0	-713.99	-3618.82	0.0	0.0	0.0	8.280e+04
		1.697e+04	0.0	0.0		25.0	-713.99	-1631.59	0.0	0.0	0.0	1.697e+04
9	19	4.996e+04	0.0	-0.02	-0.65	0.0	-210.35	-2201.79	0.0	0.0	0.0	4.996e+04
		1.027e+04	0.0	0.0		25.0	-210.35	-970.65	0.0	0.0	0.0	1.027e+04
9	20	8.280e+04	0.0	-0.11	-0.96	0.0	-713.99	-3618.82	0.0	0.0	0.0	8.280e+04
		1.697e+04	0.0	0.0		25.0	-713.99	-1631.59	0.0	0.0	0.0	1.697e+04
9	21	7.992e+04	0.0	-0.11	-0.94	0.0	-713.99	-3491.22	0.0	0.0	0.0	7.992e+04

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		1.641e+04	0.0	0.0		25.0	-713.99	-1574.58	0.0	0.0	0.0	1.641e+04
10	1	9494.22	0.0	-4.82e-03	-0.65	0.0	0.0	-948.90	0.0	0.0	0.0	9494.22
		-481.55	0.0	0.0		20.0	0.0	-48.11	0.0	0.0	0.0	-481.55
10	2	9643.07	0.0	-0.02	-0.62	0.0	1.69	-967.19	0.0	0.0	0.0	9643.07
		-1457.07	0.0	0.0		20.0	1.69	-144.82	0.0	0.0	0.0	-1457.07
10	3	1.289e+04	0.0	-0.01	-0.77	0.0	-79.40	-1288.47	0.0	0.0	0.0	1.289e+04
		-1634.24	0.0	0.0		20.0	-79.40	-162.53	0.0	0.0	0.0	-1634.24
10	4	2.489e+04	0.0	-0.03	-1.39	0.0	-156.82	-2486.56	0.0	0.0	0.0	2.489e+04
		-1114.22	0.0	0.0		20.0	-156.82	-110.53	0.0	0.0	0.0	-1114.22
10	5	1.043e+04	0.0	-0.01	-0.60	0.0	-79.40	-1042.46	0.0	0.0	0.0	1.043e+04
		-1509.40	0.0	0.0		20.0	-79.40	-150.05	0.0	0.0	0.0	-1509.40
10	6	1.043e+04	0.0	-0.01	-0.60	0.0	-79.40	-1042.46	0.0	0.0	0.0	1.043e+04
		-1509.40	0.0	0.0		20.0	-79.40	-150.05	0.0	0.0	0.0	-1509.40
10	7	2.240e+04	0.0	-0.09	-1.24	0.0	2.85	-2252.73	0.0	0.0	0.0	2.240e+04
		-1016.76	0.0	0.0		20.0	2.85	-99.95	0.0	0.0	0.0	-1016.76
10	8	7233.71	0.0	-0.03	-0.44	0.0	2.28	-727.58	0.0	0.0	0.0	7233.71
		-1673.65	0.0	0.0		20.0	2.28	-166.19	0.0	0.0	0.0	-1673.65
10	9	7032.75	0.0	-3.57e-03	-0.48	0.0	0.0	-702.89	0.0	0.0	0.0	7032.75
		-356.71	0.0	0.0		20.0	0.0	-35.64	0.0	0.0	0.0	-356.71
10	10	7181.61	0.0	-0.02	-0.45	0.0	1.69	-721.18	0.0	0.0	0.0	7181.61
		-1332.22	0.0	0.0		20.0	1.69	-132.35	0.0	0.0	0.0	-1332.22
10	11	1.609e+04	0.0	-8.33e-03	-0.91	0.0	-55.80	-1610.86	0.0	0.0	0.0	1.609e+04
		-946.07	0.0	0.0		20.0	-55.80	-93.73	0.0	0.0	0.0	-946.07
10	12	7032.75	0.0	-3.57e-03	-0.48	0.0	0.0	-702.89	0.0	0.0	0.0	7032.75
		-356.71	0.0	0.0		20.0	0.0	-35.64	0.0	0.0	0.0	-356.71
10	13	7181.61	0.0	-0.02	-0.45	0.0	1.69	-721.18	0.0	0.0	0.0	7181.61
		-1332.22	0.0	0.0		20.0	1.69	-132.35	0.0	0.0	0.0	-1332.22
10	14	1.609e+04	0.0	-8.33e-03	-0.91	0.0	-55.80	-1610.86	0.0	0.0	0.0	1.609e+04
		-946.07	0.0	0.0		20.0	-55.80	-93.73	0.0	0.0	0.0	-946.07
10	15	7032.75	0.0	-3.57e-03	-0.48	0.0	0.0	-702.89	0.0	0.0	0.0	7032.75
		-356.71	0.0	0.0		20.0	0.0	-35.64	0.0	0.0	0.0	-356.71
10	16	7032.75	0.0	-3.57e-03	-0.48	0.0	0.0	-702.89	0.0	0.0	0.0	7032.75
		-356.71	0.0	0.0		20.0	0.0	-35.64	0.0	0.0	0.0	-356.71
10	17	1.152e+04	0.0	-0.01	-0.65	0.0	-64.72	-1151.38	0.0	0.0	0.0	1.152e+04
		-1570.81	0.0	0.0		20.0	-64.72	-156.03	0.0	0.0	0.0	-1570.81
10	18	1.854e+04	0.0	-0.08	-0.99	0.0	-219.69	-1845.15	0.0	0.0	0.0	1.854e+04
		-1899.77	0.0	0.0		20.0	-219.69	-188.51	0.0	0.0	0.0	-1899.77
10	19	1.152e+04	0.0	-0.01	-0.65	0.0	-64.72	-1151.38	0.0	0.0	0.0	1.152e+04
		-1570.81	0.0	0.0		20.0	-64.72	-156.03	0.0	0.0	0.0	-1570.81
10	20	1.854e+04	0.0	-0.08	-0.99	0.0	-219.69	-1845.15	0.0	0.0	0.0	1.854e+04
		-1899.77	0.0	0.0		20.0	-219.69	-188.51	0.0	0.0	0.0	-1899.77
10	21	1.792e+04	0.0	-0.08	-0.96	0.0	-219.69	-1783.82	0.0	0.0	0.0	1.792e+04
		-1854.72	0.0	0.0		20.0	-219.69	-184.00	0.0	0.0	0.0	-1854.72
Trave f.		**M3 mx/mn**	**M2 mx/mn**	**D 2 / D 3**	**Pt**		**N**	**V 2**	**V 3**	**T**		
		-9.010e+05	0.0	-1.06	-1.73		-2.307e+04	-9785.70	0.0	0.0		
		5.543e+06	0.0	1.32	0.14		727.76	8498.04	0.0	0.0		

11.3. RISULTATI OPERE DI FONDAZIONE

Il controllo dei risultati delle analisi condotte, per quanto concerne le opere di fondazione, è possibile in relazione alle tabelle sottoriportate.

La tabella è riferita alle fondazioni tipo trave su suolo elastico.

Per questo tipo di fondazione vengono riportate le pressioni alle estremità dell'elemento e la massima (in valore assoluto) pressione lungo lo sviluppo dell'elemento.

Vengono inoltre riportati, con funzione statistica, i valori massimo e minimo delle pressioni che compaiono nella tabella.

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm2	daN/cm2
1	1	-0.65	-0.65	-0.65	2	-0.61	-0.62	-0.62	3	-0.44	-0.46	-0.46
	4	-0.85	-0.88	-0.88	5	-0.27	-0.29	-0.29	6	-0.27	-0.29	-0.29
	7	-1.73	-1.72	-1.73	8	-0.43	-0.44	-0.44	9	-0.48	-0.48	-0.48
	10	-0.44	-0.45	-0.45	11	-0.75	-0.76	-0.76	12	-0.48	-0.48	-0.48
	13	-0.44	-0.45	-0.45	14	-0.75	-0.76	-0.76	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.32	-0.34	-0.34	18	0.11	0.07	0.11
	19	-0.32	-0.34	-0.34	20	0.11	0.07	0.11	21	0.14	0.09	0.14
2	1	-0.65	-0.65	-0.65	2	-0.62	-0.62	-0.62	3	-0.46	-0.48	-0.48
	4	-0.88	-0.92	-0.92	5	-0.29	-0.31	-0.31	6	-0.29	-0.31	-0.31
	7	-1.72	-1.72	-1.72	8	-0.44	-0.45	-0.45	9	-0.48	-0.48	-0.48
	10	-0.45	-0.46	-0.46	11	-0.76	-0.78	-0.78	12	-0.48	-0.48	-0.48
	13	-0.45	-0.46	-0.46	14	-0.76	-0.78	-0.78	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.34	-0.36	-0.36	18	0.07	6.15e-03	0.06
	19	-0.34	-0.36	-0.36	20	0.07	6.15e-03	0.06	21	0.09	0.03	0.09
3	1	-0.65	-0.65	-0.65	2	-0.62	-0.63	-0.63	3	-0.48	-0.49	-0.49
	4	-0.92	-0.94	-0.94	5	-0.31	-0.32	-0.32	6	-0.31	-0.32	-0.32
	7	-1.72	-1.72	-1.72	8	-0.45	-0.45	-0.45	9	-0.48	-0.48	-0.48
	10	-0.46	-0.46	-0.46	11	-0.78	-0.79	-0.79	12	-0.48	-0.48	-0.48
	13	-0.46	-0.46	-0.46	14	-0.78	-0.79	-0.79	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.36	-0.37	-0.37	18	6.15e-03	-0.02	-0.02
	19	-0.36	-0.37	-0.37	20	6.15e-03	-0.02	-0.02	21	0.03	4.30e-03	0.03
4	1	-0.65	-0.65	-0.65	2	-0.63	-0.63	-0.63	3	-0.49	-0.50	-0.50
	4	-0.94	-0.96	-0.96	5	-0.32	-0.34	-0.34	6	-0.32	-0.34	-0.34
	7	-1.72	-1.72	-1.72	8	-0.45	-0.46	-0.46	9	-0.48	-0.48	-0.48
	10	-0.46	-0.46	-0.46	11	-0.79	-0.80	-0.80	12	-0.48	-0.48	-0.48
	13	-0.46	-0.46	-0.46	14	-0.79	-0.80	-0.80	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.37	-0.38	-0.38	18	-0.02	-0.05	-0.05
	19	-0.37	-0.38	-0.38	20	-0.02	-0.05	-0.05	21	4.30e-03	-0.03	-0.03
5	1	-0.65	-0.64	-0.65	2	-0.63	-0.66	-0.66	3	-0.50	-0.66	-0.66
	4	-0.96	-1.21	-1.21	5	-0.34	-0.50	-0.50	6	-0.34	-0.50	-0.50
	7	-1.72	-1.60	-1.72	8	-0.46	-0.50	-0.50	9	-0.48	-0.47	-0.48
	10	-0.46	-0.49	-0.49	11	-0.80	-0.90	-0.90	12	-0.48	-0.47	-0.48
	13	-0.46	-0.49	-0.49	14	-0.80	-0.90	-0.90	15	-0.48	-0.47	-0.48
	16	-0.48	-0.47	-0.48	17	-0.38	-0.54	-0.54	18	-0.05	-0.52	-0.52
	19	-0.38	-0.54	-0.54	20	-0.05	-0.52	-0.52	21	-0.03	-0.49	-0.49
6	1	-0.64	-0.65	-0.65	2	-0.66	-0.63	-0.66	3	-0.66	-0.75	-0.75
	4	-1.21	-1.36	-1.36	5	-0.50	-0.58	-0.58	6	-0.50	-0.58	-0.58
	7	-1.60	-1.32	-1.59	8	-0.50	-0.46	-0.50	9	-0.47	-0.48	-0.48
	10	-0.49	-0.46	-0.49	11	-0.90	-0.92	-0.92	12	-0.47	-0.48	-0.48

Elem.	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max	Cmb	Pt ini	Pt fin	Pt max
	13	-0.49	-0.46	-0.49	14	-0.90	-0.92	-0.92	15	-0.47	-0.48	-0.48
	16	-0.47	-0.48	-0.48	17	-0.54	-0.63	-0.63	18	-0.52	-0.89	-0.89
	19	-0.54	-0.63	-0.63	20	-0.52	-0.89	-0.89	21	-0.49	-0.86	-0.86
7	1	-0.65	-0.65	-0.65	2	-0.63	-0.63	-0.63	3	-0.75	-0.76	-0.76
	4	-1.36	-1.37	-1.37	5	-0.58	-0.59	-0.59	6	-0.58	-0.59	-0.59
	7	-1.32	-1.30	-1.32	8	-0.46	-0.45	-0.46	9	-0.48	-0.48	-0.48
	10	-0.46	-0.46	-0.46	11	-0.92	-0.92	-0.92	12	-0.48	-0.48	-0.48
	13	-0.46	-0.46	-0.46	14	-0.92	-0.92	-0.92	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.63	-0.64	-0.64	18	-0.89	-0.91	-0.91
	19	-0.63	-0.64	-0.64	20	-0.89	-0.91	-0.91	21	-0.86	-0.88	-0.88
8	1	-0.65	-0.65	-0.65	2	-0.63	-0.62	-0.63	3	-0.76	-0.76	-0.76
	4	-1.37	-1.37	-1.37	5	-0.59	-0.59	-0.59	6	-0.59	-0.59	-0.59
	7	-1.30	-1.28	-1.30	8	-0.45	-0.45	-0.45	9	-0.48	-0.48	-0.48
	10	-0.46	-0.46	-0.46	11	-0.92	-0.91	-0.92	12	-0.48	-0.48	-0.48
	13	-0.46	-0.46	-0.46	14	-0.92	-0.91	-0.92	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.64	-0.64	-0.64	18	-0.91	-0.93	-0.93
	19	-0.64	-0.64	-0.64	20	-0.91	-0.93	-0.93	21	-0.88	-0.90	-0.90
9	1	-0.65	-0.65	-0.65	2	-0.62	-0.62	-0.62	3	-0.76	-0.76	-0.76
	4	-1.37	-1.39	-1.39	5	-0.59	-0.59	-0.59	6	-0.59	-0.59	-0.59
	7	-1.28	-1.24	-1.28	8	-0.45	-0.44	-0.45	9	-0.48	-0.48	-0.48
	10	-0.46	-0.45	-0.46	11	-0.91	-0.91	-0.91	12	-0.48	-0.48	-0.48
	13	-0.46	-0.45	-0.46	14	-0.91	-0.91	-0.91	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.64	-0.65	-0.65	18	-0.93	-0.96	-0.96
	19	-0.64	-0.65	-0.65	20	-0.93	-0.96	-0.96	21	-0.90	-0.94	-0.94
10	1	-0.65	-0.65	-0.65	2	-0.62	-0.61	-0.62	3	-0.76	-0.77	-0.77
	4	-1.39	-1.39	-1.39	5	-0.59	-0.60	-0.60	6	-0.59	-0.60	-0.60
	7	-1.24	-1.21	-1.24	8	-0.44	-0.43	-0.43	9	-0.48	-0.48	-0.48
	10	-0.45	-0.44	-0.45	11	-0.91	-0.91	-0.91	12	-0.48	-0.48	-0.48
	13	-0.45	-0.44	-0.45	14	-0.91	-0.91	-0.91	15	-0.48	-0.48	-0.48
	16	-0.48	-0.48	-0.48	17	-0.65	-0.65	-0.65	18	-0.96	-0.99	-0.99
	19	-0.65	-0.65	-0.65	20	-0.96	-0.99	-0.99	21	-0.94	-0.96	-0.96
Elem.		**Pt ini**	**Pt fin**	**Pt max**		**Pt ini**	**Pt fin**	**Pt max**		**Pt ini**	**Pt fin**	**Pt max**
		-1.73										
		0.14										

12. ALLEGATO C. – TABELLE SOLLECITAZIONI TRASVERSALI NELLA SOLETTA SUPERIORE

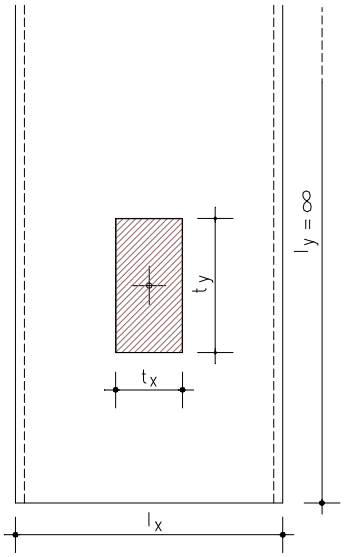


FIGURA 12-1– SCHEMA PER IL CALCOLO DELLE SOLLECITAZIONI TRASVERSALI

Piastra rettangolare appoggiata sui quattro lati caricata uniformemente su una zona rettangolare centrale

t_x/l_x t_y/l_x	1.00	0.90	0.80	0.70	0.60	0.50	0.40	0.30	0.20	0.10	0.05
1.00	0.0210	0.0230	0.0250	0.0268	0.0285	0.0299	0.0312	0.0322	0.0330	0.0334	0.0335
0.90	0.0245	0.0269	0.0292	0.0313	0.0333	0.0351	0.0366	0.0378	0.0388	0.0393	0.0395
0.80	0.0286	0.0314	0.0341	0.0366	0.0390	0.0411	0.0430	0.0445	0.0456	0.0463	0.0465
0.70	0.0333	0.0366	0.0398	0.0428	0.0457	0.0483	0.0506	0.0525	0.0539	0.0548	0.0550
0.60	0.0388	0.0427	0.0464	0.0501	0.0535	0.0567	0.0596	0.0620	0.0639	0.0651	0.0654
0.50	0.0452	0.0496	0.0541	0.0585	0.0627	0.0667	0.0704	0.0736	0.0761	0.0778	0.0782
0.40	0.0525	0.0578	0.0630	0.0683	0.0735	0.0786	0.0834	0.0878	0.0914	0.0938	0.0945
0.30	0.0608	0.0670	0.0732	0.0796	0.0861	0.0927	0.0993	0.1055	0.1111	0.1150	0.1161
0.20	0.0703	0.0774	0.0849	0.0926	0.1008	0.1095	0.1186	0.1280	0.1372	0.1449	0.1471
0.10	0.0809	0.0892	0.0981	0.1075	0.1179	0.1293	0.1422	0.1569	0.1739	0.1921	0.1993
0.05	0.0867	0.0957	0.1053	0.1157	0.1273	0.1405	0.1558	0.1745	0.1979	0.2290	0.2472

TABELLA 12-1- VALORI DI α_{YM}

$l_y = \infty$ $\quad P = p * t_x * t_y \quad$ $M_{ym} = \alpha_{ym} * P$