REGIONE CAMPANIA
PROVINCIA DI CASERTA
COMUNE DI CANCELLO ED ARNONE

PROGETTO PER LA REALIZZAZIONE DI UN IMPIANTO FOTOVOLTAICO DENOMINATO "LA FOSSA" DELLA POTENZA DI 43.410 kWp -40.000 kVA

STARENERGIA

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Struttura di base/Fondazione Cabina di Vettoriamento - Cabina di consegna
Relazione illustrativa e di calcolo

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RELAZIONE ILLUSTRATIVA E DI CALCOLO
STRUTTURA DI BASE CABINA DI VETTORIAMENTO

1. DESCRIZIONE

La presente relazione è relativa alla progettazione strutturale della struttura di base sulla quale sarà posizionata la "Cabina di Vettoriamento", la quale deve essere posizionata ad una quota pari a +1.50 m dal piano campagna.

La struttura di base della "Cabina di Vettoriamento" è così costituita:

- dimensioni in pianta pari a 2026x490 cm, per un'altezza al piano campagna pari a 1500 mm;
- pilastri costituiti da profili HEB140;
- travi costituite da profili HEB140;
- controventi costituiti da profili 2UPN50;
- impalcato costituito da solaio HI-BOND tipo A55/P600 H=100 mm, spessore lamiera 10/10;
- fondazione costituita da una platea in c.a. di dimensioni in pianta pari a 2126x590 cm e spessore pari a 30 cm, armata inferiormente e superiormente con Φ16/25 cm disposti lungo le due direzioni principali.

2. NORMATIVA DI RIFERIMENTO

Disciplina delle opere

- Legge n. 1086 del 5 Novembre 1971. "Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso, ed a struttura metallica".
- Circolare del 14 febbraio 1974 n. 11951. "Istruzioni per l'applicazione delle «Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso, ed a struttura metallica» di cui alla Legge n. 1086 del 5 Novembre 1971".

Azioni

- D.M. 17 Gennaio 2018 "Aggiornamento delle Norme Tecniche per le Costruzioni".
- Eurocodice 1. "Basi della progettazione ed azioni sulle strutture".

Strutture in acciaio e c.a.

- D.M. 17 Gennaio 2018 "Aggiornamento delle Norme Tecniche per le Costruzioni".
- Eurocodice 2. "Progettazione delle strutture di calcestruzzo".
- Eurocodice 3. "Progettazione delle strutture di acciaio".

Zone sismiche

- Legge n. 64 del 2 febbraio 1974. "Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche".
- D.M. 17 Gennaio 2018 "Aggiornamento delle Norme Tecniche per le Costruzioni".
- Eurocodice 8. "Regole progettuali per le strutture antisismiche".

Opere di fondazione

- D.M. 17 Gennaio 2018 “Aggiornamento delle Norme Tecniche per le Costruzioni”.
- Eurocodice 7. “Progettazione geotecnica”.

3. CARATTERISTICHE DEI MATERIALI UTILIZZATI

CALCESTRUZZO

C25/30

ACCIAIO PER CALCESTRUZZO ARMATO

B450C

ACCIAIO S275JR

Gli elementi che sono progettati con l’acciaio S275 JR sono i seguenti

- Tubolare principale 120x120x3mm;
- profili per fissaggio pannelli Ω34x33x24x2mm;
- profili per fissaggio pannelli Z30x24x3mm;
- piastrame;
- Palo verticale Ω101x108x40x4mm;

Caratteristiche meccaniche:

- $f_y \geq 275$ N/mm^2 Limite di snervamento;
- $f_t \geq 430$ N/mm^2 Limite di rottura;
- $A_{\%} \geq 25$ % Allungamento minimo;
- R ≤ 27J Resilienza a 20°C;
- E=210000 N/mm^2 Modulo Elastico;
- G=E/[2(1+v)] = 80769 N/mm^2 Modulo Tangenziale;
- $\alpha = 12x10^{-6}$per °C^{-1} Coefficiente di espansione termica lineare.

BULLONI

I bulloni - conformi per le caratteristiche dimensionali alle norme UNI EN ISO 4016:2002 e UNI 5592:1968 devono appartenere alle sottoindicate classi della norma UNI EN ISO 898- 1:2001.

Vite 8.8 - Dado 8	f_{yb}=649 N/mm^2	f_{tb}=800 N/mm^2

SALDATURE

Eventuali saldature dell'acciaio dovranno avvenire con uno dei procedimenti all’arco elettrico codificati secondo la norma UNI EN ISO 4063:2001. È ammesso l’uso di procedimenti diversi purché sostenuti da adeguata documentazione teorica e sperimentale.

4. ANALISI DEI CARICHI

Carichi permanenti

Peso proprio solaio HI-BOND	190 dN/m^2
Peso proprio Cabina di Vettoriamento	300 dN/m^2

Carichi variabili

Carico manutenzione	100 dN/m^2
Carico neve – Zona III	50 dN/m^2
Carico vento – Zona 3	70 dN/m^2

Parametri di calcolo Analisi Dinamica

INTESTAZIONE E DATI CARATTERISTICI DELLA STRUTTURA

Tipo di struttura	Nello Spazio
Tipo di analisi	Statica e Dinamica
Tipo di soluzione	Lineare
Unita' di misura delle forze	daN
Unita' di misura delle lunghezze	cm
Normativa	NTC-2018

NORMATIVA

Vita nominale costruzione	50 anni
Classe d'uso costruzione	IV
Vita di riferimento	100 anni
Luogo	Cancello ed Arnone (CE)
Categoria del suolo	C
Fattore topografico	1

PARAMETRI SISMICI

	TR	ag/g	FO	TC*	CC	Ss	Pga (ag/g*S)
SLO	60	0.053	2.43	0.33	1.51	1.50	0.079
SLD	101	0.063	2.50	0.35	1.48	1.50	0.095
SLV	949	0.126	2.69	0.47	1.35	1.50	0.189
SLC	1950	0.150	2.78	0.51	1.31	1.45	0.217

Comportamento strutturale NON Dissipativo

PARAMETRI SISMICI

Angolo del sisma nel piano orizzontale	0
Sisma verticale	Assente
Combinazione dei modi	CQC
Combinazione componenti azioni sismiche	NTC - Eurocodice 8
λ	0.3

μ 0.3

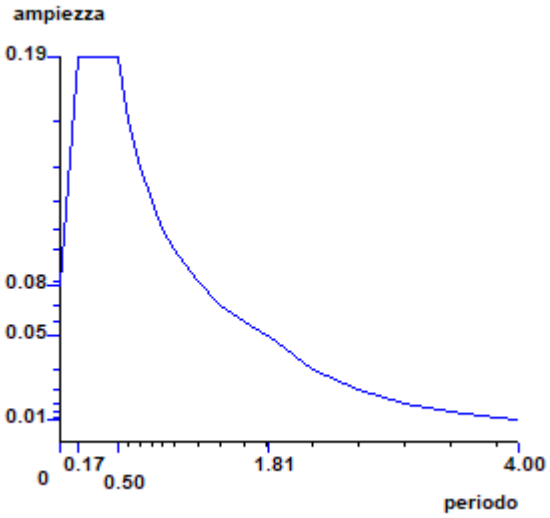


Grafico spettro SLO

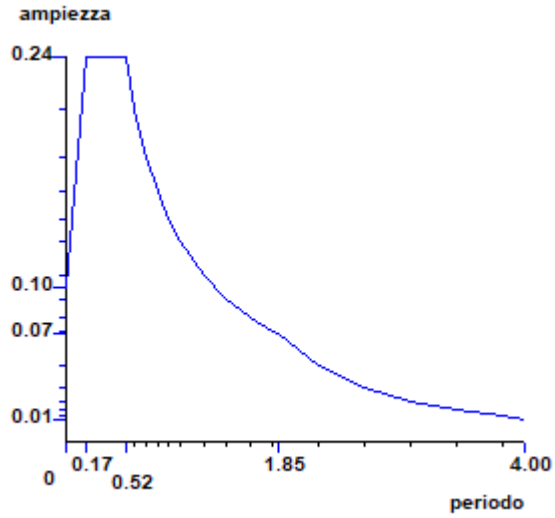


Grafico spettro SLD

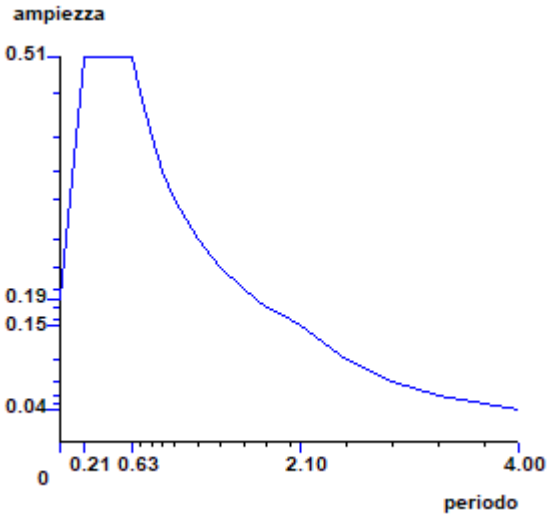


Grafico spettro SLV

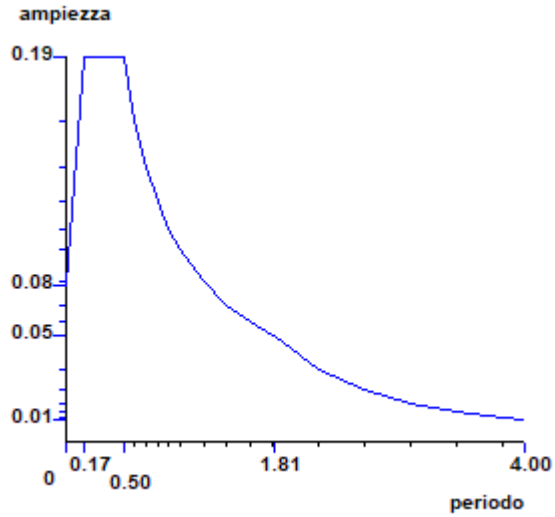


Grafico spettro SLC

5. COMBINAZIONE DEI CARICHI

NORMATIVA: NORME TECNICHE PER LE COSTRUZIONI 2018

COMBINAZIONI PER LE VERIFICHE ALLO STATO LIMITE ULTIMO

Num.	Descrizione	Parametri	Tipo azione/categoria	Condizione	Moltiplicatore
1	Dinamica	Azione sismica: Presente	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variabile: Domestici e residenziali	Condizione 2	0.300
2	SLU: permanenti (1.30) + variabile manutenzione (1.50)	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.300
			Variabile: Manutenzionei	Condizione 2	1.500

Num.	Descrizione	Parametri	Tipo azione/categoria	Condizione	Moltiplicatore
3	SLU: permanenti (1.30) + neve (1.50)	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.300
			Variabile: Neve	Condizione 3	1.500
4	SLU: permanenti (1.30) + vento direzione X (1.50)	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.300
			Variabile: Vento	Condizione 4	1.500
5	SLU: permanenti (1.30) + vento direzione Y (1.50)	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.300
			Variabile: Vento	Condizione 5	1.500

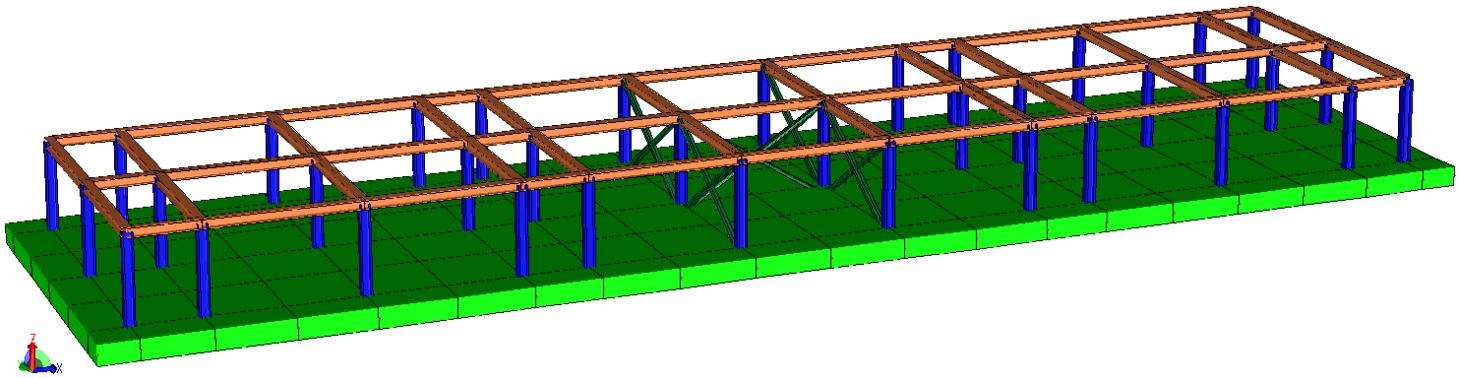
COMBINAZIONI PER LE VERIFICHE ALLO STATO LIMITE D'ESERCIZIO

Num.	Descrizione	Parametri	Tipo azione/categoria	Condizione	Moltiplicatore
6	SLE: permanenti (1.00) + variabile manutenzione (1.00)	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variabile: Manutenzione	Condizione 2	1.000
7	SLE: permanenti (1.00) + neve (1.00)	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variabile: Neve	Condizione 3	1.000
8	SLE: permanenti (1.00) + vento direzione X (1.00)	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variabile: Vento	Condizione 4	1.000
9	SLE: permanenti (1.00) + vento direzione Y (1.00)	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variabile: Vento	Condizione 5	1.000
10	SLE: permanenti (1.00) + vento direzione X (0.60)	Tipologia: Frequente	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variabile: Vento	Condizione 4	0.600
11	SLE: permanenti (1.00) + vento direzione Y (0.60)	Tipologia: Frequente	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variabile: Vento	Condizione 5	0.600
12	SLE: permanenti (1.00)	Tipologia: Quasi permanente	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000

COMBINAZIONI PER LE VERIFICHE ALLO STATO LIMITE DI DANNO

Num.	Descrizione	Parametri	Tipo azione/categoria	Condizione	Moltiplicatore
13	S.L.D.	Azione sismica: Presente	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variabile: Manutenzione	Condizione 2	0.300

6. SCHEMA GEOMETRICO E MODELLO CON ELEMENTI FINITI



RIEPILOGO DELLE SEZIONI UTILIZZATE NEL MODELLO STRUTTURALE

SEZIONE PROFILO SEMPLICE

Codice	Codice sezione	Asse Y capovolto
1	HEB 140	No

SEZIONE PROFILO DOPPIO

Codice	Codice sezione	Tipo accoppiamento	Distanza	Ali	Lati
2	U 50X 38		1.000	esterne	

CARICHI PER ELEMENTI TRAVE, TRAVE DI FONDAZIONE E RETICOLARE

Carico distribuito con riferimento globale X

Descrizione	Cod.	Cond. carico	Tipo Azione/categoria	Val. iniz.	Dist. iniz. nodo I	Val. finale	Dist.fin. nodo I	Aliq.inerz.	Aliq.inerz. SLD
Vento Zona 3 - Direzione X	5	Condizione 4	Variabile: Vento	0.007000	0.000	0.007000	0.000	0.0000	0.0000

Carico distribuito con riferimento globale Y

Descrizione	Cod.	Cond. carico	Tipo Azione/categoria	Val. iniz.	Dist. iniz. nodo I	Val. finale	Dist.fin. nodo I	Aliq.inerz.	Aliq.inerz. SLD
Vento Zona 3 - Direzione Y	6	Condizione 5	Variabile: Vento	0.007000	0.000	0.007000	0.000	0.0000	0.0000

Carico distribuito con riferimento globale Z

Descrizione	Cod.	Cond. carico	Tipo Azione/categoria	Val. iniz.	Dist. iniz. nodo I	Val. finale	Dist.fin. nodo I	Aliq.inerz.	Aliq.inerz. SLD
Neve Zona III	4	Condizione 3	Variabile: Neve	-0.005000	0.000	-0.005000	0.000	0.0000	0.0000

Carico distribuito con riferimento globale Z, agente sulla lunghezza reale

Descrizione	Cod.	Cond. carico	Tipo Azione/categoria	Val. iniz.	Dist.iniz. nodo I	Val. finale	Dist.fin. nodo I	Aliq.inerz.	Aliq.inerz. SLD
Peso proprio solaio	1	Condizione 1	Permanente: Permanente	-0.019000	0.000	-0.019000	0.000	1.0000	1.0000

Descrizione	Cod.	Cond. carico	Tipo Azione/categoria	Val. iniz.	Dist.iniz. nodo I	Val. finale	Dist.fin. nodo I	Aliq.inerz.	Aliq.inerz. SLD
solaio HI-BOND			portato						
Peso proprio Cabina di Vettoriamento	2	Condizione 1	Permanente: Permanente portato	-0.030000	0.000	-0.030000	0.000	1.0000	1.0000
Carico per manutenzione	3	Condizione 2	Variabile: Manutenzione	-0.010000	0.000	-0.010000	0.000	0.0000	0.0000

LISTA MATERIALI UTILIZZATI

Codice	Descrizione	Mod. elast.	Coef. Poisson	Peso unit.	Dil. term.	Aliq. inerz.	Rigid. taglio	Rigid. fless.
1	Calcestruzzo C25/30 (Rck 300)	+3.21e+005	0.120	0.00250	+1.00e-005	1.000	+1.00e+000	+1.00e+000
2	Acciaio	+2.10e+006	0.300	0.00785	+1.20e-005	1.000	+1.00e+000	+1.00e+000

GRUPPI DELLA STRUTTURA

ELEMENTO FINITO: TRAVE

Numero gruppo	Descrizione gruppo	
1	Pilastri	
2	Traversi	
3	Controventi	

ELEMENTO FINITO: PIASTRA

Numero gruppo	Descrizione gruppo	
1	Platea di fondazione	

ELEMENTO FINITO: VINCOLO

Numero gruppo	Descrizione gruppo	
1	Vincoli di platea cost. sottofondo = 2	

NODI DEL MODELLO

Nodo	Coord. X	Coord. Y	Coord. Z	Temper.	uX	uY	uZ	rX	rY	rZ
1	0.000	-5.000	0.000	0.000	0	0	0	0	0	0
2	329.000	-5.000	0.000	0.000	0	0	0	0	0	0
3	556.000	-5.000	0.000	0.000	0	0	0	0	0	0
4	889.000	-5.000	0.000	0.000	0	0	0	0	0	0
5	1123.000	-5.000	0.000	0.000	0	0	0	0	0	0
6	1356.000	-5.000	0.000	0.000	0	0	0	0	0	0
7	1683.000	-5.000	0.000	0.000	0	0	0	0	0	0
8	1683.000	233.000	0.000	0.000	0	0	0	0	0	0
9	1356.000	233.000	0.000	0.000	0	0	0	0	0	0

Nodo	Coord. X	Coord. Y	Coord. Z	Temper.	uX	uY	uZ	rX	rY	rZ
10	1123.000	233.000	0.000	0.000	0	0	0	0	0	0
11	889.000	233.000	0.000	0.000	0	0	0	0	0	0
12	556.000	233.000	0.000	0.000	0	0	0	0	0	0
13	329.000	233.000	0.000	0.000	0	0	0	0	0	0
14	0.000	233.000	0.000	0.000	0	0	0	0	0	0
15	1683.000	471.000	0.000	0.000	0	0	0	0	0	0
16	1356.000	471.000	0.000	0.000	0	0	0	0	0	0
17	1123.000	471.000	0.000	0.000	0	0	0	0	0	0
18	889.000	471.000	0.000	0.000	0	0	0	0	0	0
19	556.000	471.000	0.000	0.000	0	0	0	0	0	0
20	329.000	471.000	0.000	0.000	0	0	0	0	0	0
21	0.000	471.000	0.000	0.000	0	0	0	0	0	0
22	0.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
23	329.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
24	556.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
25	889.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
26	1123.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
27	1356.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
28	1683.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
29	0.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
30	329.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
31	556.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
32	889.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
33	1123.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
34	1356.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
35	1683.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
36	1683.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
37	1356.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
38	1123.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
39	889.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
40	556.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
41	329.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
42	0.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
43	1683.000	528.000	0.000	0.000	0	0	0	0	0	0
44	1910.000	528.000	0.000	0.000	0	0	0	0	0	0
45	2012.000	528.000	0.000	0.000	0	0	0	0	0	0
46	0.000	-62.000	0.000	0.000	0	0	0	0	0	0
47	102.000	-62.000	0.000	0.000	0	0	0	0	0	0
48	329.000	-62.000	0.000	0.000	0	0	0	0	0	0
49	556.000	-62.000	0.000	0.000	0	0	0	0	0	0
50	-57.000	-5.000	0.000	0.000	0	0	0	0	0	0
51	-57.000	233.000	0.000	0.000	0	0	0	0	0	0
52	2069.000	-62.000	0.000	0.000	0	0	0	0	0	0

Nodo	Coord. X	Coord. Y	Coord. Z	Temper.	uX	uY	uZ	rX	rY	rZ
53	2069.000	528.000	0.000	0.000	0	0	0	0	0	0
54	2069.000	471.000	0.000	0.000	0	0	0	0	0	0
55	2069.000	-5.000	0.000	0.000	0	0	0	0	0	0
56	2069.000	233.000	0.000	0.000	0	0	0	0	0	0
57	-57.000	352.000	0.000	0.000	0	0	0	0	0	0
58	656.000	-62.000	0.000	0.000	0	0	0	0	0	0
59	889.000	-62.000	0.000	0.000	0	0	0	0	0	0
60	1123.000	-62.000	0.000	0.000	0	0	0	0	0	0
61	1356.000	-62.000	0.000	0.000	0	0	0	0	0	0
62	-57.000	114.000	0.000	0.000	0	0	0	0	0	0
63	1456.000	-62.000	0.000	0.000	0	0	0	0	0	0
64	656.000	528.000	0.000	0.000	0	0	0	0	0	0
65	889.000	528.000	0.000	0.000	0	0	0	0	0	0
66	1123.000	528.000	0.000	0.000	0	0	0	0	0	0
67	1683.000	-62.000	0.000	0.000	0	0	0	0	0	0
68	1910.000	-62.000	0.000	0.000	0	0	0	0	0	0
69	1356.000	528.000	0.000	0.000	0	0	0	0	0	0
70	1910.000	471.000	0.000	0.000	0	0	0	0	0	0
71	2012.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
72	2012.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
73	2012.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
74	2012.000	471.000	0.000	0.000	0	0	0	0	0	0
75	2012.000	233.000	0.000	0.000	0	0	0	0	0	0
76	2012.000	-5.000	0.000	0.000	0	0	0	0	0	0
77	1456.000	528.000	0.000	0.000	0	0	0	0	0	0
78	1456.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
79	1456.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
80	1456.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
81	1456.000	-5.000	0.000	0.000	0	0	0	0	0	0
82	1456.000	233.000	0.000	0.000	0	0	0	0	0	0
83	1456.000	471.000	0.000	0.000	0	0	0	0	0	0
84	1910.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
85	2069.000	352.000	0.000	0.000	0	0	0	0	0	0
86	0.000	352.000	0.000	0.000	0	0	0	0	0	0
87	102.000	352.000	0.000	0.000	0	0	0	0	0	0
88	329.000	352.000	0.000	0.000	0	0	0	0	0	0
89	1910.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
90	0.000	528.000	0.000	0.000	0	0	0	0	0	0
91	2012.000	-62.000	0.000	0.000	0	0	0	0	0	0
92	102.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
93	102.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
94	102.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
95	1910.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]

Nodo	Coord. X	Coord. Y	Coord. Z	Temper.	uX	uY	uZ	rX	rY	rZ
96	102.000	528.000	0.000	0.000	0	0	0	0	0	0
97	-57.000	-62.000	0.000	0.000	0	0	0	0	0	0
98	102.000	471.000	0.000	0.000	0	0	0	0	0	0
99	102.000	233.000	0.000	0.000	0	0	0	0	0	0
100	102.000	-5.000	0.000	0.000	0	0	0	0	0	0
101	1910.000	-5.000	0.000	0.000	0	0	0	0	0	0
102	329.000	528.000	0.000	0.000	0	0	0	0	0	0
103	-57.000	528.000	0.000	0.000	0	0	0	0	0	0
104	656.000	233.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
105	656.000	471.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
106	656.000	-5.000	148.000	0.000	PXY[184]	PXY[184]	0	0	0	PXY[184]
107	1910.000	233.000	0.000	0.000	0	0	0	0	0	0
108	556.000	528.000	0.000	0.000	0	0	0	0	0	0
109	-57.000	471.000	0.000	0.000	0	0	0	0	0	0
110	656.000	-5.000	0.000	0.000	0	0	0	0	0	0
111	656.000	233.000	0.000	0.000	0	0	0	0	0	0
112	656.000	471.000	0.000	0.000	0	0	0	0	0	0
113	556.000	352.000	0.000	0.000	0	0	0	0	0	0
114	656.000	352.000	0.000	0.000	0	0	0	0	0	0
115	889.000	352.000	0.000	0.000	0	0	0	0	0	0
116	1123.000	352.000	0.000	0.000	0	0	0	0	0	0
117	1356.000	352.000	0.000	0.000	0	0	0	0	0	0
118	1456.000	352.000	0.000	0.000	0	0	0	0	0	0
119	1683.000	352.000	0.000	0.000	0	0	0	0	0	0
120	1910.000	352.000	0.000	0.000	0	0	0	0	0	0
121	2012.000	352.000	0.000	0.000	0	0	0	0	0	0
122	2069.000	114.000	0.000	0.000	0	0	0	0	0	0
123	0.000	114.000	0.000	0.000	0	0	0	0	0	0
124	102.000	114.000	0.000	0.000	0	0	0	0	0	0
125	329.000	114.000	0.000	0.000	0	0	0	0	0	0
126	556.000	114.000	0.000	0.000	0	0	0	0	0	0
127	656.000	114.000	0.000	0.000	0	0	0	0	0	0
128	889.000	114.000	0.000	0.000	0	0	0	0	0	0
129	1123.000	114.000	0.000	0.000	0	0	0	0	0	0
130	1356.000	114.000	0.000	0.000	0	0	0	0	0	0
131	1456.000	114.000	0.000	0.000	0	0	0	0	0	0
132	1683.000	114.000	0.000	0.000	0	0	0	0	0	0
133	1910.000	114.000	0.000	0.000	0	0	0	0	0	0
134	2012.000	114.000	0.000	0.000	0	0	0	0	0	0
135	215.500	528.000	0.000	0.000	0	0	0	0	0	0
136	442.500	528.000	0.000	0.000	0	0	0	0	0	0
137	772.500	528.000	0.000	0.000	0	0	0	0	0	0
138	1006.000	528.000	0.000	0.000	0	0	0	0	0	0

Nodo	Coord. X	Coord. Y	Coord. Z	Temper.	uX	uY	uZ	rX	rY	rZ
139	1239.500	528.000	0.000	0.000	0	0	0	0	0	0
140	1569.500	528.000	0.000	0.000	0	0	0	0	0	0
141	1796.500	528.000	0.000	0.000	0	0	0	0	0	0
142	215.500	114.000	0.000	0.000	0	0	0	0	0	0
143	215.500	352.000	0.000	0.000	0	0	0	0	0	0
144	215.500	-62.000	0.000	0.000	0	0	0	0	0	0
145	215.500	471.000	0.000	0.000	0	0	0	0	0	0
146	215.500	-5.000	0.000	0.000	0	0	0	0	0	0
147	215.500	233.000	0.000	0.000	0	0	0	0	0	0
148	442.500	114.000	0.000	0.000	0	0	0	0	0	0
149	442.500	352.000	0.000	0.000	0	0	0	0	0	0
150	442.500	-62.000	0.000	0.000	0	0	0	0	0	0
151	442.500	471.000	0.000	0.000	0	0	0	0	0	0
152	442.500	-5.000	0.000	0.000	0	0	0	0	0	0
153	442.500	233.000	0.000	0.000	0	0	0	0	0	0
154	772.500	114.000	0.000	0.000	0	0	0	0	0	0
155	772.500	352.000	0.000	0.000	0	0	0	0	0	0
156	772.500	-62.000	0.000	0.000	0	0	0	0	0	0
157	772.500	471.000	0.000	0.000	0	0	0	0	0	0
158	772.500	-5.000	0.000	0.000	0	0	0	0	0	0
159	772.500	233.000	0.000	0.000	0	0	0	0	0	0
160	1006.000	114.000	0.000	0.000	0	0	0	0	0	0
161	1006.000	352.000	0.000	0.000	0	0	0	0	0	0
162	1006.000	-62.000	0.000	0.000	0	0	0	0	0	0
163	1006.000	471.000	0.000	0.000	0	0	0	0	0	0
164	1006.000	-5.000	0.000	0.000	0	0	0	0	0	0
165	1006.000	233.000	0.000	0.000	0	0	0	0	0	0
166	1239.500	114.000	0.000	0.000	0	0	0	0	0	0
167	1239.500	352.000	0.000	0.000	0	0	0	0	0	0
168	1239.500	-62.000	0.000	0.000	0	0	0	0	0	0
169	1239.500	471.000	0.000	0.000	0	0	0	0	0	0
170	1239.500	-5.000	0.000	0.000	0	0	0	0	0	0
171	1239.500	233.000	0.000	0.000	0	0	0	0	0	0
172	1569.500	114.000	0.000	0.000	0	0	0	0	0	0
173	1569.500	352.000	0.000	0.000	0	0	0	0	0	0
174	1569.500	-62.000	0.000	0.000	0	0	0	0	0	0
175	1569.500	471.000	0.000	0.000	0	0	0	0	0	0
176	1569.500	-5.000	0.000	0.000	0	0	0	0	0	0
177	1569.500	233.000	0.000	0.000	0	0	0	0	0	0
178	1796.500	114.000	0.000	0.000	0	0	0	0	0	0
179	1796.500	352.000	0.000	0.000	0	0	0	0	0	0
180	1796.500	-62.000	0.000	0.000	0	0	0	0	0	0
181	1796.500	471.000	0.000	0.000	0	0	0	0	0	0

Nodo	Coord. X	Coord. Y	Coord. Z	Temper.	uX	uY	uZ	rX	rY	rZ
182	1796.500	-5.000	0.000	0.000	0	0	0	0	0	0
183	1796.500	233.000	0.000	0.000	0	0	0	0	0	0

Legenda: descrizione della simbologia adottata per i gradi di liberta'

Simbolo	Descrizione del Grado di Liberta'
0	libero
1	bloccato
MASTER	Master di una o piu' relazioni
PXY[nnn]	Slave di piano rigido XY [nnn = nodo master, e' stato assegnato automaticamente in fase di calcolo]

PROSPETTO RIASSUNTIVO CENTRI DELLE MASSE E DELLE RIGIDEZZE

	CENTRI DELLE MASSE				CENTRI DELLE RIGIDEZZE		ECCENTRICITA' RELATIVE	
Nodo	Coord. X	Coord. Y	Coord. Z	Nodi master automatici	Coord. X	Coord. Y	Coord. X	Coord. Y
184	1006.001	233.000	148.000	-2	1006.001	233.000	-0.000	0.000

GRUPPI ELEMENTO FINITO TRAVE

GRUPPO NUMERO: 1 - DESCRIZIONE: PILASTRI

	Nodi			Connessioni				Offset strutturali/Conci rigidi
Asta	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
1	1	42	0	Rigida	Rigida	2	1	
2	2	41	0	Rigida	Rigida	2	1	
3	3	40	0	Rigida	Rigida	2	1	
4	4	39	0	Rigida	Rigida	2	1	
5	5	38	0	Rigida	Rigida	2	1	
6	6	37	0	Rigida	Rigida	2	1	
7	7	36	0	Rigida	Rigida	2	1	
8	14	29	0	Rigida	Rigida	2	1	
9	13	30	0	Rigida	Rigida	2	1	
10	12	31	0	Rigida	Rigida	2	1	
11	11	32	0	Rigida	Rigida	2	1	
12	10	33	0	Rigida	Rigida	2	1	
13	9	34	0	Rigida	Rigida	2	1	
14	8	35	0	Rigida	Rigida	2	1	

	Nodi			Connessioni				Offset strutturali/Conci rigidi
Asta	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
15	21	22	0	Rigida	Rigida	2	1	
16	20	23	0	Rigida	Rigida	2	1	
17	19	24	0	Rigida	Rigida	2	1	
18	18	25	0	Rigida	Rigida	2	1	
19	17	26	0	Rigida	Rigida	2	1	
20	16	27	0	Rigida	Rigida	2	1	
21	15	28	0	Rigida	Rigida	2	1	
22	98	94	0	Rigida	Rigida	2	1	
23	99	93	0	Rigida	Rigida	2	1	
24	100	92	0	Rigida	Rigida	2	1	
25	110	106	0	Rigida	Rigida	2	1	
26	111	104	0	Rigida	Rigida	2	1	
27	112	105	0	Rigida	Rigida	2	1	
28	81	80	0	Rigida	Rigida	2	1	
29	82	78	0	Rigida	Rigida	2	1	
30	83	79	0	Rigida	Rigida	2	1	
31	101	95	0	Rigida	Rigida	2	1	
32	107	84	0	Rigida	Rigida	2	1	
33	70	89	0	Rigida	Rigida	2	1	
34	74	73	0	Rigida	Rigida	2	1	
35	75	72	0	Rigida	Rigida	2	1	
36	76	71	0	Rigida	Rigida	2	1	

GRUPPO NUMERO: 2 - DESCRIZIONE: TRAVERSI

	Nodi			Connessioni				Offset strutturali/Conci rigidi
Asta	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
1	78	35	0	Rigida	Rigida	2	1	

	Nodi			Connessioni				Offset strutturali/Conci rigidi
Asta	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
2	33	34	0	Rigida	Rigida	2	1	
3	32	33	0	Rigida	Rigida	2	1	
4	104	32	0	Rigida	Rigida	2	1	
5	30	31	0	Rigida	Rigida	2	1	
6	93	30	0	Rigida	Rigida	2	1	
7	34	27	0	Rigida	Rigida	2	1	
8	37	34	0	Rigida	Rigida	2	1	
9	33	26	0	Rigida	Rigida	2	1	
10	38	33	0	Rigida	Rigida	2	1	
11	32	25	0	Rigida	Rigida	2	1	
12	39	32	0	Rigida	Rigida	2	1	
13	31	24	0	Rigida	Rigida	2	1	
14	40	31	0	Rigida	Rigida	2	1	
15	30	23	0	Rigida	Rigida	2	1	
16	41	30	0	Rigida	Rigida	2	1	
17	35	28	0	Rigida	Rigida	2	1	
18	36	35	0	Rigida	Rigida	2	1	
19	79	28	0	Rigida	Rigida	2	1	
20	26	27	0	Rigida	Rigida	2	1	
21	25	26	0	Rigida	Rigida	2	1	
22	105	25	0	Rigida	Rigida	2	1	
23	23	24	0	Rigida	Rigida	2	1	
24	94	23	0	Rigida	Rigida	2	1	
25	29	22	0	Rigida	Rigida	2	1	
26	42	29	0	Rigida	Rigida	2	1	
27	36	95	0	Rigida	Rigida	2	1	

	Nodi			Connessioni				Offset strutturali/Conci rigidi
Asta	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
28	38	37	0	Rigida	Rigida	2	1	
29	39	38	0	Rigida	Rigida	2	1	
30	106	39	0	Rigida	Rigida	2	1	
31	41	40	0	Rigida	Rigida	2	1	
32	92	41	0	Rigida	Rigida	2	1	
33	92	93	0	Rigida	Rigida	2	1	
34	93	94	0	Rigida	Rigida	2	1	
35	104	105	0	Rigida	Rigida	2	1	
36	106	104	0	Rigida	Rigida	2	1	
37	78	79	0	Rigida	Rigida	2	1	
38	80	78	0	Rigida	Rigida	2	1	
39	84	89	0	Rigida	Rigida	2	1	
40	95	84	0	Rigida	Rigida	2	1	
41	71	72	0	Rigida	Rigida	2	1	
42	72	73	0	Rigida	Rigida	2	1	
43	42	92	0	Rigida	Rigida	2	1	
44	40	106	0	Rigida	Rigida	2	1	
45	37	80	0	Rigida	Rigida	2	1	
46	80	36	0	Rigida	Rigida	2	1	
47	95	71	0	Rigida	Rigida	2	1	
48	84	72	0	Rigida	Rigida	2	1	
49	89	73	0	Rigida	Rigida	2	1	
50	28	89	0	Rigida	Rigida	2	1	
51	35	84	0	Rigida	Rigida	2	1	
52	34	78	0	Rigida	Rigida	2	1	
53	27	79	0	Rigida	Rigida	2	1	

	Nodi			Connessioni				Offset strutturali/Conci rigidi
Asta	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
54	24	105	0	Rigida	Rigida	2	1	
55	31	104	0	Rigida	Rigida	2	1	
56	29	93	0	Rigida	Rigida	2	1	
57	22	94	0	Rigida	Rigida	2	1	

GRUPPO NUMERO: 3 - DESCRIZIONE: CONTROVENTI

	Nodi			Connessioni				Offset strutturali/Conci rigidi
Asta	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
1	11	33	0	Rigida	Rigida	2	2	
2	10	32	0	Rigida	Rigida	2	2	
3	4	32	0	Rigida	Rigida	2	2	
4	11	39	0	Rigida	Rigida	2	2	
5	11	25	0	Rigida	Rigida	2	2	
6	18	32	0	Rigida	Rigida	2	2	
7	17	33	0	Rigida	Rigida	2	2	
8	10	26	0	Rigida	Rigida	2	2	
9	10	38	0	Rigida	Rigida	2	2	
10	5	33	0	Rigida	Rigida	2	2	

GRUPPI ELEMENTO FINITO PIASTRA

GRUPPO NUMERO: 1 DESCRIZIONE: PLATEA DI FONDAZIONE

Elem.	Nodo I	Nodo J	Nodo K	Nodo L	Spessore	Materiale
1	103	109	21	90	50.00	1
2	90	21	98	96	50.00	1
3	96	98	145	135	50.00	1
4	135	145	20	102	50.00	1
5	102	20	151	136	50.00	1
6	136	151	19	108	50.00	1
7	108	19	112	64	50.00	1
8	64	112	157	137	50.00	1
9	137	157	18	65	50.00	1
10	65	18	163	138	50.00	1

Elem.	Nodo I	Nodo J	Nodo K	Nodo L	Spessore	Materiale
11	138	163	17	66	50.00	1
12	66	17	169	139	50.00	1
13	139	169	16	69	50.00	1
14	69	16	83	77	50.00	1
15	77	83	175	140	50.00	1
16	140	175	15	43	50.00	1
17	43	15	181	141	50.00	1
18	141	181	70	44	50.00	1
19	44	70	74	45	50.00	1
20	45	74	54	53	50.00	1
21	109	57	86	21	50.00	1
22	21	86	87	98	50.00	1
23	98	87	143	145	50.00	1
24	145	143	88	20	50.00	1
25	20	88	149	151	50.00	1
26	151	149	113	19	50.00	1
27	19	113	114	112	50.00	1
28	112	114	155	157	50.00	1
29	157	155	115	18	50.00	1
30	18	115	161	163	50.00	1
31	163	161	116	17	50.00	1
32	17	116	167	169	50.00	1
33	169	167	117	16	50.00	1
34	16	117	118	83	50.00	1
35	83	118	173	175	50.00	1
36	175	173	119	15	50.00	1
37	15	119	179	181	50.00	1
38	181	179	120	70	50.00	1
39	70	120	121	74	50.00	1
40	74	121	85	54	50.00	1
41	57	51	14	86	50.00	1
42	86	14	99	87	50.00	1
43	87	99	147	143	50.00	1
44	143	147	13	88	50.00	1
45	88	13	153	149	50.00	1
46	149	153	12	113	50.00	1
47	113	12	111	114	50.00	1
48	114	111	159	155	50.00	1
49	155	159	11	115	50.00	1
50	115	11	165	161	50.00	1
51	161	165	10	116	50.00	1
52	116	10	171	167	50.00	1
53	167	171	9	117	50.00	1

Elem.	Nodo I	Nodo J	Nodo K	Nodo L	Spessore	Materiale
54	117	9	82	118	50.00	1
55	118	82	177	173	50.00	1
56	173	177	8	119	50.00	1
57	119	8	183	179	50.00	1
58	179	183	107	120	50.00	1
59	120	107	75	121	50.00	1
60	121	75	56	85	50.00	1
61	51	62	123	14	50.00	1
62	14	123	124	99	50.00	1
63	99	124	142	147	50.00	1
64	147	142	125	13	50.00	1
65	13	125	148	153	50.00	1
66	153	148	126	12	50.00	1
67	12	126	127	111	50.00	1
68	111	127	154	159	50.00	1
69	159	154	128	11	50.00	1
70	11	128	160	165	50.00	1
71	165	160	129	10	50.00	1
72	10	129	166	171	50.00	1
73	171	166	130	9	50.00	1
74	9	130	131	82	50.00	1
75	82	131	172	177	50.00	1
76	177	172	132	8	50.00	1
77	8	132	178	183	50.00	1
78	183	178	133	107	50.00	1
79	107	133	134	75	50.00	1
80	75	134	122	56	50.00	1
81	62	50	1	123	50.00	1
82	123	1	100	124	50.00	1
83	124	100	146	142	50.00	1
84	142	146	2	125	50.00	1
85	125	2	152	148	50.00	1
86	148	152	3	126	50.00	1
87	126	3	110	127	50.00	1
88	127	110	158	154	50.00	1
89	154	158	4	128	50.00	1
90	128	4	164	160	50.00	1
91	160	164	5	129	50.00	1
92	129	5	170	166	50.00	1
93	166	170	6	130	50.00	1
94	130	6	81	131	50.00	1
95	131	81	176	172	50.00	1
96	172	176	7	132	50.00	1

Elem.	Nodo I	Nodo J	Nodo K	Nodo L	Spessore	Materiale
97	132	7	182	178	50.00	1
98	178	182	101	133	50.00	1
99	133	101	76	134	50.00	1
100	134	76	55	122	50.00	1
101	50	97	46	1	50.00	1
102	1	46	47	100	50.00	1
103	100	47	144	146	50.00	1
104	146	144	48	2	50.00	1
105	2	48	150	152	50.00	1
106	152	150	49	3	50.00	1
107	3	49	58	110	50.00	1
108	110	58	156	158	50.00	1
109	158	156	59	4	50.00	1
110	4	59	162	164	50.00	1
111	164	162	60	5	50.00	1
112	5	60	168	170	50.00	1
113	170	168	61	6	50.00	1
114	6	61	63	81	50.00	1
115	81	63	174	176	50.00	1
116	176	174	67	7	50.00	1
117	7	67	180	182	50.00	1
118	182	180	68	101	50.00	1
119	101	68	91	76	50.00	1
120	76	91	52	55	50.00	1

GRUPPI ELEMENTO FINITO VINCOLO

GRUPPO NUMERO: 1 - DESCRIZIONE: VINCOLI DI PLATEA COST. SOTTOFONDO = 2

VINCOLI STANDARD

Nodo	Rigid. Trasl. X	Rigid. Rotaz. X	Rigid. Trasl. Y	Rigid. Rotaz. Y	Rigid. Trasl. Z	Rigid. Rotaz. Z
1					+1.40e+004	
2					+2.00e+004	
3					+1.88e+004	
4					+2.05e+004	
5					+2.05e+004	
6					+1.91e+004	
7					+2.00e+004	
8					+2.70e+004	

Nodo	Rigid. Trasl. X	Rigid. Rotaz. X	Rigid. Trasl. Y	Rigid. Rotaz. Y	Rigid. Trasl. Z	Rigid. Rotaz. Z
9					+2.58e+004	
10					+2.78e+004	
11					+2.78e+004	
12					+2.54e+004	
13					+2.70e+004	
14					+1.89e+004	
15					+2.00e+004	
16					+1.91e+004	
17					+2.05e+004	
18					+2.05e+004	
19					+1.88e+004	
20					+2.00e+004	
21					+1.40e+004	
43					+6.47e+003	
44					+6.14e+003	
45					+4.53e+003	
46					+4.53e+003	
47					+6.14e+003	
48					+6.47e+003	
49					+6.08e+003	
50					+5.02e+003	
51					+6.78e+003	
52					+1.62e+003	
53					+1.62e+003	
54					+5.02e+003	
55					+5.02e+003	
56					+6.78e+003	

Nodo	Rigid. Trasl. X	Rigid. Rotaz. X	Rigid. Trasl. Y	Rigid. Rotaz. Y	Rigid. Trasl. Z	Rigid. Rotaz. Z
57					+6.78e+003	
58					+6.17e+003	
59					+6.65e+003	
60					+6.65e+003	
61					+6.17e+003	
62					+6.78e+003	
63					+6.08e+003	
64					+6.17e+003	
65					+6.65e+003	
66					+6.65e+003	
67					+6.47e+003	
68					+6.14e+003	
69					+6.17e+003	
70					+1.90e+004	
74					+1.40e+004	
75					+1.89e+004	
76					+1.40e+004	
77					+6.08e+003	
81					+1.88e+004	
82					+2.54e+004	
83					+1.88e+004	
85					+6.78e+003	
86					+1.89e+004	
87					+2.56e+004	
88					+2.70e+004	
90					+4.53e+003	
91					+4.53e+003	

Nodo	Rigid. Trasl. X	Rigid. Rotaz. X	Rigid. Trasl. Y	Rigid. Rotaz. Y	Rigid. Trasl. Z	Rigid. Rotaz. Z
96					+6.14e+003	
97					+1.62e+003	
98					+1.90e+004	
99					+2.56e+004	
100					+1.90e+004	
101					+1.90e+004	
102					+6.47e+003	
103					+1.62e+003	
107					+2.56e+004	
108					+6.08e+003	
109					+5.02e+003	
110					+1.91e+004	
111					+2.58e+004	
112					+1.91e+004	
113					+2.54e+004	
114					+2.58e+004	
115					+2.78e+004	
116					+2.78e+004	
117					+2.58e+004	
118					+2.54e+004	
119					+2.70e+004	
120					+2.56e+004	
121					+1.89e+004	
122					+6.78e+003	
123					+1.89e+004	
124					+2.56e+004	
125					+2.70e+004	

Nodo	Rigid. Trasl. X	Rigid. Rotaz. X	Rigid. Trasl. Y	Rigid. Rotaz. Y	Rigid. Trasl. Z	Rigid. Rotaz. Z
126					+2.54e+004	
127					+2.58e+004	
128					+2.78e+004	
129					+2.78e+004	
130					+2.58e+004	
131					+2.54e+004	
132					+2.70e+004	
133					+2.56e+004	
134					+1.89e+004	
135					+6.47e+003	
136					+6.47e+003	
137					+6.64e+003	
138					+6.67e+003	
139					+6.64e+003	
140					+6.47e+003	
141					+6.47e+003	
142					+2.70e+004	
143					+2.70e+004	
144					+6.47e+003	
145					+2.00e+004	
146					+2.00e+004	
147					+2.70e+004	
148					+2.70e+004	
149					+2.70e+004	
150					+6.47e+003	
151					+2.00e+004	
152					+2.00e+004	

Nodo	Rigid. Trasl. X	Rigid. Rotaz. X	Rigid. Trasl. Y	Rigid. Rotaz. Y	Rigid. Trasl. Z	Rigid. Rotaz. Z
153					+2.70e+004	
154					+2.77e+004	
155					+2.77e+004	
156					+6.64e+003	
157					+2.05e+004	
158					+2.05e+004	
159					+2.77e+004	
160					+2.78e+004	
161					+2.78e+004	
162					+6.67e+003	
163					+2.06e+004	
164					+2.06e+004	
165					+2.78e+004	
166					+2.77e+004	
167					+2.77e+004	
168					+6.64e+003	
169					+2.05e+004	
170					+2.05e+004	
171					+2.77e+004	
172					+2.70e+004	
173					+2.70e+004	
174					+6.47e+003	
175					+2.00e+004	
176					+2.00e+004	
177					+2.70e+004	
178					+2.70e+004	
179					+2.70e+004	

Nodo	Rigid. Trasl. X	Rigid. Rotaz. X	Rigid. Trasl. Y	Rigid. Rotaz. Y	Rigid. Trasl. Z	Rigid. Rotaz. Z
180					+6.47e+003	
181					+2.00e+004	
182					+2.00e+004	
183					+2.70e+004	

GRUPPI ELEMENTO FINITO TRAVE - ELEMENTI CON CARICO APPLICATO

GRUPPO NUMERO: 1- DESCRIZIONE: PILASTRI

Asta		Carichi	
1	Codice carico	5	6
	Moltiplicatore	119.00	51.00
2	Codice carico	6	
	Moltiplicatore	227.00	
3	Codice carico	6	
	Moltiplicatore	163.50	
4	Codice carico	6	
	Moltiplicatore	233.50	
5	Codice carico	6	
	Moltiplicatore	233.50	
6	Codice carico	6	
	Moltiplicatore	166.50	
7	Codice carico	6	
	Moltiplicatore	227.00	
8	Codice carico	5	
	Moltiplicatore	238.00	
15	Codice carico	5	
	Moltiplicatore	119.00	
24	Codice carico	6	

Asta						Carichi
	Moltiplicatore	164.00				
25	Codice carico	6				
	Moltiplicatore	166.50				
28	Codice carico	6				
	Moltiplicatore	163.50				
31	Codice carico	6				
	Moltiplicatore	164.50				

GRUPPO NUMERO: 2- DESCRIZIONE: TRAVERSI

Asta						Carichi
1	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
2	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
3	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
4	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
5	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
6	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
19	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
20	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
21	Codice carico	1	2	3	4	

Asta						Carichi
	Moltiplicatore	119.00	119.00	119.00	119.00	
22	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
23	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
24	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
27	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
28	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
29	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
30	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
31	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
32	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
43	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
44	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
45	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
46	Codice carico	1	2	3	4	

Asta						Carichi
	Moltiplicatore	119.00	119.00	119.00	119.00	
47	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
48	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
49	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
50	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
51	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
52	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
53	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
54	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	
55	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
56	Codice carico	1	2	3	4	
	Moltiplicatore	238.00	238.00	238.00	238.00	
57	Codice carico	1	2	3	4	
	Moltiplicatore	119.00	119.00	119.00	119.00	

SPOSTAMENTI/ROTAZIONI NODI NON BLOCCATI

COMBINAZIONE DI CARICO: 1 - DESCRIZIONE: DINAMICA

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+5.28e-009	+2.32e-008	-9.12e-002	+3.58e-005	-2.54e-004	-1.08e-012	+9.12e-002
Nodo	22	22	32	25	34	22	32

COMBINAZIONE DI CARICO: 2 - DESCRIZIONE: SLU: PERMANENTI (1.30) + VARIABILE MANUTENZIONE (1.50)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+6.91e-009	+3.50e-008	-1.24e-001	-4.83e-005	-3.83e-004	-1.66e-012	+1.24e-001
Nodo	22	22	32	38	34	22	32

COMBINAZIONE DI CARICO: 3 - DESCRIZIONE: SLU: PERMANENTI (1.30) + NEVE (1.50)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+6.88e-009	+3.17e-008	-1.20e-001	-4.71e-005	-3.47e-004	-1.49e-012	+1.20e-001
Nodo	22	22	32	38	34	22	32

COMBINAZIONE DI CARICO: 4 - DESCRIZIONE: SLU: PERMANENTI (1.30) + VENTO DIREZIONE X (1.50)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+8.41e-004	+2.97e-008	-1.17e-001	-4.61e-005	+3.14e-004	-2.47e-012	+1.17e-001
Nodo	22	22	33	38	104	22	33

COMBINAZIONE DI CARICO: 5 - DESCRIZIONE: SLU: PERMANENTI (1.30) + VENTO DIREZIONE Y (1.50)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+1.26e-004	+3.18e-003	-1.17e-001	-3.75e-005	-3.12e-004	-5.29e-007	+1.17e-001
Nodo	22	22	32	71	34	22	32

COMBINAZIONE DI CARICO: 6 - DESCRIZIONE: SLE: PERMANENTI (1.00) + VARIABILE MANUTENZIONE (1.00)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+5.31e-009	+2.63e-008	-9.47e-002	+3.69e-005	-2.87e-004	-1.24e-012	+9.47e-002
Nodo	22	22	32	25	34	22	32

COMBINAZIONE DI CARICO: 7 - DESCRIZIONE: SLE: PERMANENTI (1.00) + NEVE (1.00)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+5.29e-009	+2.41e-008	-9.22e-002	+3.61e-005	-2.63e-004	-1.13e-012	+9.22e-002
Nodo	22	22	32	25	34	22	32

COMBINAZIONE DI CARICO: 8 - DESCRIZIONE: SLE: PERMANENTI (1.00) + VENTO DIREZIONE X (1.00)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+5.61e-004	+2.27e-008	-8.98e-002	+3.54e-005	+2.41e-004	-1.78e-012	+8.98e-002
Nodo	22	22	33	26	104	22	33

COMBINAZIONE DI CARICO: 9 - DESCRIZIONE: SLE: PERMANENTI (1.00) + VENTO DIREZIONE Y (1.00)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+8.39e-005	+2.12e-003	-8.97e-002	+2.93e-005	-2.40e-004	-3.53e-007	+8.97e-002
Nodo	22	22	32	26	34	22	32

COMBINAZIONE DI CARICO: 10 - DESCRIZIONE: SLE: PERMANENTI (1.00) + VENTO DIREZIONE X (0.60)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+3.36e-004	+2.24e-008	-8.97e-002	+3.54e-005	+2.40e-004	-1.47e-012	+8.97e-002
Nodo	22	22	33	26	104	22	33

COMBINAZIONE DI CARICO: 11 - DESCRIZIONE: SLE: PERMANENTI (1.00) + VENTO DIREZIONE Y (0.60)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+5.03e-005	+1.27e-003	-8.97e-002	+3.17e-005	-2.40e-004	-2.12e-007	+8.97e-002
Nodo	22	22	32	26	34	22	32

COMBINAZIONE DI CARICO: 12 - DESCRIZIONE: SLE: PERMANENTI (1.00)

MASSIME DEFORMAZIONI NODALI

	Trasl.X	Trasl.Y	Trasl.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
Deform. nodali	+5.26e-009	+2.19e-008	-8.97e-002	+3.53e-005	-2.40e-004	-1.02e-012	+8.97e-002
Nodo	22	22	32	25	34	22	32

TABELLA FREQUENZE, COEFF. MODALI E RISPOSTA SPETTRALE

FREQUENZE PROPRIE DI OSCILLAZIONE

Numero	Pulsazione	Frequenza	Periodo	Precisione
1	5.832e+001	9.282e+000	1.077e-001	5.682e-026
2	8.614e+001	1.371e+001	7.294e-002	5.573e-015
3	8.726e+001	1.389e+001	7.201e-002	4.997e-014

COEFFICIENTI DI PARTECIPAZIONE MODALE

Modo	Direzione X	Direzione Y
1	-1.447e-011	-1.197e-007
2	-7.121e+000	8.366e-006
3	1.022e-005	5.677e+000

COMBINAZIONE QUADRATICA COMPLETA (CQC) - SISMA LUNGO X

Tralaz. X/Nodo	Tralaz.Y/Nodo	Tralaz.Z/Nodo	Rotaz.X/Nodo	Rotaz.Y/Nodo	Rotaz.Z/Nodo	DL max/Nodo
+3.78e-002	+8.19e-009	+7.97e-003	+1.16e-005	+1.55e-004	+3.42e-016	+3.85e-002
22	28	50	25	22	22	29

COMBINAZIONE QUADRATICA COMPLETA (CQC) - SISMA LUNGO Y

Tralaz. X/Nodo	Tralaz.Y/Nodo	Tralaz.Z/Nodo	Rotaz.X/Nodo	Rotaz.Y/Nodo	Rotaz.Z/Nodo	DL max/Nodo
+8.23e-009	+2.33e-002	+2.19e-002	+1.20e-004	+1.92e-005	+2.75e-012	+2.98e-002
36	22	138	25	137	22	25

TABELLA INVILUPPI

MEDIA QUADRATICA DEI RISULTATI DINAMICI (EX+λ*EY)

MASSIME DEFORMAZIONI NODALI/ NODI CORRISPONDENTI

Traslaz.X	Traslaz.Y	Traslaz.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
+3.78e-002	+6.98e-003	+1.09e-002	+4.75e-005	+1.56e-004	+8.26e-013	+3.96e-002
Nodo: 22	Nodo: 22	Nodo: 52	Nodo: 25	Nodo: 22	Nodo: 22	Nodo: 22

MEDIA QUADRATICA DEI RISULTATI DINAMICI (λ*EX+EY)

MASSIME DEFORMAZIONI NODALI/ NODI CORRISPONDENTI

Traslaz.X	Traslaz.Y	Traslaz.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
+1.13e-002	+2.33e-002	+2.19e-002	+1.23e-004	+4.84e-005	+2.75e-012	+3.22e-002
Nodo: 22	Nodo: 22	Nodo: 138	Nodo: 25	Nodo: 22	Nodo: 22	Nodo: 25

TABELLA INVILUPPI SLU

MEDIA QUADRATICA DEI RISULTATI DINAMICI (QOR1 * EX + QOR2 * λ * EY)

MASSIME DEFORMAZIONI NODALI/ NODI CORRISPONDENTI

Traslaz.X	Traslaz.Y	Traslaz.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
+3.78e-002	+6.98e-003	+1.09e-002	+4.75e-005	+1.56e-004	+8.26e-013	+3.96e-002
Nodo: 22	Nodo: 22	Nodo: 52	Nodo: 25	Nodo: 22	Nodo: 22	Nodo: 22

MEDIA QUADRATICA DEI RISULTATI DINAMICI (QOR1 * λ * EX + QOR2 * EY)

MASSIME DEFORMAZIONI NODALI/ NODI CORRISPONDENTI

Traslaz.X	Traslaz.Y	Traslaz.Z	Rotaz.X	Rotaz.Y	Rotaz.Z	DLMax
+1.13e-002	+2.33e-002	+2.19e-002	+1.23e-004	+4.84e-005	+2.75e-012	+3.22e-002
Nodo: 22	Nodo: 22	Nodo: 138	Nodo: 25	Nodo: 22	Nodo: 22	Nodo: 25

TABELLA MASSE ECCITATE

MASSA ECCITATA PER QUOTA Z MAGGIORE DI :0.00

Modo	Direz.X	%	Direz.Y	%
Modo: 1	+2.07e+001	18	+9.54e+000	18
Modo: 2	+5.07e+001	96	+3.22e+001	61
Modo: 3	+5.07e+001	96	+4.82e+001	91

7. VERIFICA FONDAZIONE IN C.A.

Elem.: **GUSCIO (piastra)** Gruppo: **1** Tabella: **Tabella gusci**
Descrizione: **Platea di fondazione**
Rck: **300.00** daN/cmq fyk: **4580.0** daN/cmq Copriferro sup.: **4.0** cm Copriferro inf.: **4.0** cm
Coeff. di partecipazione Mxy: **0.50** Coeff. di partecipazione Sxy: **0.50**
dxx base sup.: **16** mm dxx base inf.: **16** mm pxx: **25** cm dxx agg.: **16** mm pxx agg.: **25** cm
dyy base sup.: **16** mm dyy base inf.: **16** mm pyy: **25** cm dyy agg.: **16** mm pyy agg.: **25** cm
Orientamento armature: **rif._globale** Angolo di posa delle armature: **0.00** gradi
Le armature longitudinali aggiuntive, riferite al proprio passo, vanno aggiunte all'armatura di base: vedere riga riassuntiva

El.	comb.	Nxx	Mxx	Nyy	Myy	Vz(Mxx)	Vz(Myy)	Axx inf.	Axx sup.	Ayy inf.	Ayy sup.	Indice di resistenza		
		daN/25 cm	daN*m/25 cm	daN/25 cm	daN*m/25 cm	daN/m		cmq /25 cm		cmq /25 cm		N, M	txy	Vz/Vrd1
1	1A	0	-98	0	-135	2221	1018	2.01	2.01	2.01	2.01	0.07	0.00	0.18
1	1B	0	-98	0	-135	2221	1018	2.01	2.01	2.01	2.01	0.07	0.00	0.18
1	1C	0	118	0	169	62	422	2.01	2.01	2.01	2.01	0.08	0.00	0.03
1	1D	0	118	0	169	62	422	2.01	2.01	2.01	2.01	0.08	0.00	0.03
1	1I	0	-69	0	-116	3026	1326	2.01	2.01	2.01	2.01	0.06	0.00	0.25
1	1J	0	-69	0	-116	3026	1326	2.01	2.01	2.01	2.01	0.06	0.00	0.25
1	1K	0	89	0	151	648	122	2.01	2.01	2.01	2.01	0.07	0.00	0.05
1	1L	0	89	0	151	648	122	2.01	2.01	2.01	2.01	0.07	0.00	0.05
1	2	0	8	0	15	2116	74	2.01	2.01	2.01	2.01	0.01	0.00	0.18
1	3	0	5	0	10	2405	24	2.01	2.01	2.01	2.01	0.01	0.00	0.20
1	4	0	7	0	10	2232	36	2.01	2.01	2.01	2.01	0.01	0.00	0.18
1	5	0	18	0	30	1457	295	2.01	2.01	2.01	2.01	0.01	0.00	0.12
Spess.= 50.0 cm		Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
2	1A	0	-1022	0	-430	8553	1313	2.01	2.01	2.01	2.01	0.50	0.00	0.71
2	1B	0	-1022	0	-430	8553	1313	2.01	2.01	2.01	2.01	0.50	0.00	0.71
2	1C	0	692	0	299	3302	310	2.01	2.01	2.01	2.01	0.34	0.00	0.27
2	1D	0	692	0	299	3302	310	2.01	2.01	2.01	2.01	0.34	0.00	0.27
2	1I	0	-695	0	-381	4324	1117	2.01	2.01	2.01	2.01	0.34	0.00	0.36
2	1J	0	-695	0	-381	4324	1117	2.01	2.01	2.01	2.01	0.34	0.00	0.36
2	1K	0	365	0	249	56	28	2.01	2.01	2.01	2.01	0.18	0.00	0.00
2	1L	0	365	0	249	56	28	2.01	2.01	2.01	2.01	0.18	0.00	0.00
2	2	0	-184	0	-56	1529	504	2.01	2.01	2.01	2.01	0.09	0.00	0.13
2	3	0	-144	0	-38	1944	341	2.01	2.01	2.01	2.01	0.07	0.00	0.16
2	4	0	-164	0	-39	1246	375	2.01	2.01	2.01	2.01	0.08	0.00	0.10
2	5	0	-255	0	-121	2679	961	2.01	2.01	2.01	2.01	0.12	0.00	0.22
Spess.= 50.0 cm		Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
3	1A	0	-223	0	-344	13776	1161	2.01	4.02	2.01	2.01	0.17	0.00	0.92
3	1B	0	-223	0	-344	13776	1161	2.01	4.02	2.01	2.01	0.17	0.00	0.92
3	1C	0	200	0	254	6083	1256	2.01	2.01	2.01	2.01	0.12	0.00	0.50
3	1D	0	200	0	254	6083	1256	2.01	2.01	2.01	2.01	0.12	0.00	0.50
3	1I	0	-182	0	-270	9222	281	2.01	2.01	2.01	2.01	0.13	0.00	0.76
3	1J	0	-182	0	-270	9222	281	2.01	2.01	2.01	2.01	0.13	0.00	0.76
3	1K	0	159	0	179	1944	1023	2.01	2.01	2.01	2.01	0.09	0.00	0.16
3	1L	0	159	0	179	1944	1023	2.01	2.01	2.01	2.01	0.09	0.00	0.16
3	2	0	-12	0	-33	3829	171	2.01	2.01	2.01	2.01	0.02	0.00	0.32
3	3	0	3	0	-11	3379	28	2.01	2.01	2.01	2.01	0.01	0.00	0.28

3	4	0	-7	0	-20	3421	155	2.01	2.01	2.01	2.01	0.01	0.00	0.28
3	5	0	-21	0	-88	5274	177	2.01	2.01	2.01	2.01	0.04	0.00	0.44
Spess.= 50.0 cm Axxinf= -- Axxsup= 1 d 16/25 Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
4	1A	0	-636	0	-370	5260	998	2.01	2.01	2.01	2.01	0.31	0.00	0.44
4	1B	0	-636	0	-370	5260	998	2.01	2.01	2.01	2.01	0.31	0.00	0.44
4	1C	0	380	0	388	2728	107	2.01	2.01	2.01	2.01	0.19	0.00	0.23
4	1D	0	380	0	388	2728	107	2.01	2.01	2.01	2.01	0.19	0.00	0.23
4	1I	0	-431	0	-190	2699	1063	2.01	2.01	2.01	2.01	0.21	0.00	0.22
4	1J	0	-431	0	-190	2699	1063	2.01	2.01	2.01	2.01	0.21	0.00	0.22
4	1K	0	175	0	208	97	379	2.01	2.01	2.01	2.01	0.10	0.00	0.03
4	1L	0	175	0	208	97	379	2.01	2.01	2.01	2.01	0.10	0.00	0.03
4	2	0	-154	0	-17	1136	470	2.01	2.01	2.01	2.01	0.08	0.00	0.09
4	3	0	-135	0	-11	1337	226	2.01	2.01	2.01	2.01	0.07	0.00	0.11
4	4	0	-142	0	-15	939	325	2.01	2.01	2.01	2.01	0.07	0.00	0.08
4	5	0	-184	0	24	1869	1042	2.01	2.01	2.01	2.01	0.09	0.00	0.15
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
5	1A	0	-477	0	-106	2448	272	2.01	2.01	2.01	2.01	0.23	0.00	0.20
5	1B	0	-477	0	-106	2448	272	2.01	2.01	2.01	2.01	0.23	0.00	0.20
5	1C	0	251	0	208	3313	341	2.01	2.01	2.01	2.01	0.12	0.00	0.27
5	1D	0	251	0	208	3313	341	2.01	2.01	2.01	2.01	0.12	0.00	0.27
5	1I	0	-320	0	-82	885	167	2.01	2.01	2.01	2.01	0.16	0.00	0.07
5	1J	0	-320	0	-82	885	167	2.01	2.01	2.01	2.01	0.16	0.00	0.07
5	1K	0	95	0	184	1069	179	2.01	2.01	2.01	2.01	0.09	0.00	0.09
5	1L	0	95	0	184	1069	179	2.01	2.01	2.01	2.01	0.09	0.00	0.09
5	2	0	-138	0	38	126	13	2.01	2.01	2.01	2.01	0.07	0.00	0.01
5	3	0	-154	0	16	550	24	2.01	2.01	2.01	2.01	0.08	0.00	0.05
5	4	0	-132	0	23	235	9	2.01	2.01	2.01	2.01	0.06	0.00	0.02
5	5	0	-157	0	102	330	42	2.01	2.01	2.01	2.01	0.08	0.00	0.03
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
6	1A	0	-489	0	-286	5076	526	2.01	2.01	2.01	2.01	0.24	0.00	0.42
6	1B	0	-489	0	-286	5076	526	2.01	2.01	2.01	2.01	0.24	0.00	0.42
6	1C	0	214	0	202	2729	274	2.01	2.01	2.01	2.01	0.10	0.00	0.23
6	1D	0	214	0	202	2729	274	2.01	2.01	2.01	2.01	0.10	0.00	0.23
6	1I	0	-401	0	-234	2678	498	2.01	2.01	2.01	2.01	0.20	0.00	0.22
6	1J	0	-401	0	-234	2678	498	2.01	2.01	2.01	2.01	0.20	0.00	0.22
6	1K	0	126	0	150	662	140	2.01	2.01	2.01	2.01	0.07	0.00	0.05
6	1L	0	126	0	150	662	140	2.01	2.01	2.01	2.01	0.07	0.00	0.05
6	2	0	-159	0	-43	1110	363	2.01	2.01	2.01	2.01	0.08	0.00	0.09
6	3	0	-140	0	-32	1266	160	2.01	2.01	2.01	2.01	0.07	0.00	0.10
6	4	0	-149	0	-30	991	293	2.01	2.01	2.01	2.01	0.07	0.00	0.08
6	5	0	-203	0	-73	1850	811	2.01	2.01	2.01	2.01	0.10	0.00	0.15
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
7	1A	0	-360	0	-324	6722	1113	2.01	2.01	2.01	2.01	0.18	0.00	0.56
7	1B	0	-360	0	-324	6722	1113	2.01	2.01	2.01	2.01	0.18	0.00	0.56
7	1C	0	345	0	360	3568	1759	2.01	2.01	2.01	2.01	0.18	0.00	0.30
7	1D	0	345	0	360	3568	1759	2.01	2.01	2.01	2.01	0.18	0.00	0.30
7	1I	0	-219	0	-161	4302	184	2.01	2.01	2.01	2.01	0.11	0.00	0.36
7	1J	0	-219	0	-161	4302	184	2.01	2.01	2.01	2.01	0.11	0.00	0.36
7	1K	0	205	0	197	1007	722	2.01	2.01	2.01	2.01	0.10	0.00	0.08
7	1L	0	205	0	197	1007	722	2.01	2.01	2.01	2.01	0.10	0.00	0.08
7	2	0	-7	0	13	2354	226	2.01	2.01	2.01	2.01	0.01	0.00	0.19
7	3	0	5	0	16	2551	24	2.01	2.01	2.01	2.01	0.01	0.00	0.21
7	4	0	-4	0	8	2556	158	2.01	2.01	2.01	2.01	0.01	0.00	0.21
7	5	0	-13	0	34	1694	478	2.01	2.01	2.01	2.01	0.02	0.00	0.14
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
8	1A	0	-148	0	-90	3632	951	2.01	2.01	2.01	2.01	0.07	0.00	0.30
8	1B	0	-148	0	-90	3632	951	2.01	2.01	2.01	2.01	0.07	0.00	0.30

8	1C	0	98	0	209	2475	1039	2.01	2.01	2.01	2.01	0.10	0.00	0.20
8	1D	0	98	0	209	2475	1039	2.01	2.01	2.01	2.01	0.10	0.00	0.20
8	1I	0	-172	0	-69	2027	573	2.01	2.01	2.01	2.01	0.08	0.00	0.17
8	1J	0	-172	0	-69	2027	573	2.01	2.01	2.01	2.01	0.08	0.00	0.17
8	1K	0	122	0	188	387	532	2.01	2.01	2.01	2.01	0.09	0.00	0.04
8	1L	0	122	0	188	387	532	2.01	2.01	2.01	2.01	0.09	0.00	0.04
8	2	0	-22	0	50	1780	3	2.01	2.01	2.01	2.01	0.02	0.00	0.15
8	3	0	-14	0	29	1045	18	2.01	2.01	2.01	2.01	0.01	0.00	0.09
8	4	0	-14	0	36	2056	2	2.01	2.01	2.01	2.01	0.02	0.00	0.17
8	5	0	-47	0	111	300	25	2.01	2.01	2.01	2.01	0.05	0.00	0.02
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
9	1A	0	-248	0	-298	6984	2041	2.01	2.01	2.01	2.01	0.15	0.00	0.58
9	1B	0	-248	0	-298	6984	2041	2.01	2.01	2.01	2.01	0.15	0.00	0.58
9	1C	0	307	0	236	2675	1517	2.01	2.01	2.01	2.01	0.15	0.00	0.22
9	1D	0	307	0	236	2675	1517	2.01	2.01	2.01	2.01	0.15	0.00	0.22
9	1I	0	-149	0	-218	5070	1329	2.01	2.01	2.01	2.01	0.11	0.00	0.42
9	1J	0	-149	0	-218	5070	1329	2.01	2.01	2.01	2.01	0.11	0.00	0.42
9	1K	0	208	0	156	949	807	2.01	2.01	2.01	2.01	0.10	0.00	0.08
9	1L	0	208	0	156	949	807	2.01	2.01	2.01	2.01	0.10	0.00	0.08
9	2	0	25	0	-28	2762	192	2.01	2.01	2.01	2.01	0.01	0.00	0.23
9	3	0	19	0	21	2983	13	2.01	2.01	2.01	2.01	0.01	0.00	0.25
9	4	0	17	0	17	2701	152	2.01	2.01	2.01	2.01	0.01	0.00	0.22
9	5	0	55	0	-59	2666	426	2.01	2.01	2.01	2.01	0.03	0.00	0.22
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
10	1A	0	-987	0	-454	6081	2025	2.01	2.01	2.01	2.01	0.48	0.00	0.50
10	1B	0	-987	0	-454	6081	2025	2.01	2.01	2.01	2.01	0.48	0.00	0.50
10	1C	0	723	0	333	3096	1071	2.01	2.01	2.01	2.01	0.35	0.00	0.26
10	1D	0	723	0	333	3096	1071	2.01	2.01	2.01	2.01	0.35	0.00	0.26
10	1I	0	-692	0	-395	3371	1700	2.01	2.01	2.01	2.01	0.34	0.00	0.28
10	1J	0	-692	0	-395	3371	1700	2.01	2.01	2.01	2.01	0.34	0.00	0.28
10	1K	0	428	0	274	983	1289	2.01	2.01	2.01	2.01	0.21	0.00	0.11
10	1L	0	428	0	274	983	1289	2.01	2.01	2.01	2.01	0.21	0.00	0.11
10	2	0	-154	0	-58	1418	666	2.01	2.01	2.01	2.01	0.08	0.00	0.12
10	3	0	-115	0	-32	1537	435	2.01	2.01	2.01	2.01	0.06	0.00	0.13
10	4	0	-149	0	-52	1210	549	2.01	2.01	2.01	2.01	0.07	0.00	0.10
10	5	0	-193	0	-105	2488	1476	2.01	2.01	2.01	2.01	0.09	0.00	0.21
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
11	1A	0	-425	0	-1101	4437	3666	2.01	2.01	2.01	2.01	0.54	0.00	0.37
11	1B	0	-425	0	-1101	4437	3666	2.01	2.01	2.01	2.01	0.54	0.00	0.37
11	1C	0	325	0	886	2928	3344	2.01	2.01	2.01	2.01	0.43	0.00	0.28
11	1D	0	325	0	886	2928	3344	2.01	2.01	2.01	2.01	0.43	0.00	0.28
11	1I	0	-663	0	-1450	382	8421	2.01	2.01	2.01	2.01	0.71	0.00	0.70
11	1J	0	-663	0	-1450	382	8421	2.01	2.01	2.01	2.01	0.71	0.00	0.70
11	1K	0	563	0	1235	1040	6352	2.01	2.01	2.01	2.01	0.60	0.00	0.53
11	1L	0	563	0	1235	1040	6352	2.01	2.01	2.01	2.01	0.60	0.00	0.53
11	2	0	-39	0	-86	635	1377	2.01	2.01	2.01	2.01	0.04	0.00	0.11
11	3	0	-35	0	-88	1945	1566	2.01	2.01	2.01	2.01	0.04	0.00	0.16
11	4	0	-5	0	-14	606	1051	2.01	2.01	2.01	2.01	0.01	0.00	0.09
11	5	0	-96	0	-205	918	2946	2.01	2.01	2.01	2.01	0.10	0.00	0.24
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
12	1A	0	-990	0	-841	1273	4209	2.01	2.01	2.01	2.01	0.48	0.00	0.35
12	1B	0	-990	0	-841	1273	4209	2.01	2.01	2.01	2.01	0.48	0.00	0.35
12	1C	0	911	0	1047	951	2641	2.01	2.01	2.01	2.01	0.51	0.00	0.22
12	1D	0	911	0	1047	951	2641	2.01	2.01	2.01	2.01	0.51	0.00	0.22
12	1I	0	-719	0	-898	13	6086	2.01	2.01	2.01	2.01	0.44	0.00	0.50
12	1J	0	-719	0	-898	13	6086	2.01	2.01	2.01	2.01	0.44	0.00	0.50
12	1K	0	640	0	1104	2595	3336	2.01	2.01	2.01	2.01	0.54	0.00	0.28

12	1L	0	640	0	1104	2595	3336	2.01	2.01	2.01	2.01	0.54	0.00	0.28
12	2	0	-33	0	83	767	1475	2.01	2.01	2.01	2.01	0.04	0.00	0.12
12	3	0	-47	0	88	93	1576	2.01	2.01	2.01	2.01	0.04	0.00	0.13
12	4	0	-12	0	-11	256	948	2.01	2.01	2.01	2.01	0.01	0.00	0.08
12	5	0	-74	0	195	1817	3194	2.01	2.01	2.01	2.01	0.10	0.00	0.26
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
13	1A	0	-243	0	-236	2227	2419	2.01	2.01	2.01	2.01	0.12	0.00	0.20
13	1B	0	-243	0	-236	2227	2419	2.01	2.01	2.01	2.01	0.12	0.00	0.20
13	1C	0	293	0	636	1279	2525	2.01	2.01	2.01	2.01	0.31	0.00	0.21
13	1D	0	293	0	636	1279	2525	2.01	2.01	2.01	2.01	0.31	0.00	0.21
13	1I	0	-235	0	-271	1328	3159	2.01	2.01	2.01	2.01	0.13	0.00	0.26
13	1J	0	-235	0	-271	1328	3159	2.01	2.01	2.01	2.01	0.13	0.00	0.26
13	1K	0	284	0	670	1375	3313	2.01	2.01	2.01	2.01	0.33	0.00	0.27
13	1L	0	284	0	670	1375	3313	2.01	2.01	2.01	2.01	0.33	0.00	0.27
13	2	0	21	0	171	3147	84	2.01	2.01	2.01	2.01	0.08	0.00	0.26
13	3	0	28	0	166	4092	157	2.01	2.01	2.01	2.01	0.08	0.00	0.34
13	4	0	29	0	146	2466	208	2.01	2.01	2.01	2.01	0.07	0.00	0.20
13	5	0	47	0	374	6572	167	2.01	2.01	2.01	2.01	0.18	0.00	0.54
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
14	1A	0	-1054	0	-933	4019	9380	2.01	2.01	2.01	2.01	0.52	0.00	0.78
14	1B	0	-1054	0	-933	4019	9380	2.01	2.01	2.01	2.01	0.52	0.00	0.78
14	1C	0	981	0	1130	1893	7437	2.01	2.01	2.01	2.01	0.55	0.00	0.62
14	1D	0	981	0	1130	1893	7437	2.01	2.01	2.01	2.01	0.55	0.00	0.62
14	1I	0	-691	0	-958	2760	12613	2.01	2.01	2.01	4.02	0.34	0.00	0.84
14	1J	0	-691	0	-958	2760	12613	2.01	2.01	2.01	4.02	0.34	0.00	0.84
14	1K	0	618	0	1155	304	9771	2.01	2.01	2.01	2.01	0.57	0.00	0.81
14	1L	0	618	0	1155	304	9771	2.01	2.01	2.01	2.01	0.57	0.00	0.81
14	2	0	-36	0	82	682	1311	2.01	2.01	2.01	2.01	0.04	0.00	0.11
14	3	0	-49	0	87	300	1195	2.01	2.01	2.01	2.01	0.04	0.00	0.10
14	4	0	43	0	124	1039	1310	2.01	2.01	2.01	2.01	0.06	0.00	0.11
14	5	0	-66	0	185	1761	2684	2.01	2.01	2.01	2.01	0.09	0.00	0.22
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= 1 d 16/25 (e arm. base nelle due direz.)														
15	1A	0	-470	0	-1212	5685	7198	2.01	2.01	2.01	2.01	0.59	0.00	0.60
15	1B	0	-470	0	-1212	5685	7198	2.01	2.01	2.01	2.01	0.59	0.00	0.60
15	1C	0	387	0	1027	6382	5814	2.01	2.01	2.01	2.01	0.50	0.00	0.53
15	1D	0	387	0	1027	6382	5814	2.01	2.01	2.01	2.01	0.50	0.00	0.53
15	1I	0	-696	0	-1463	1201	12362	2.01	2.01	2.01	4.02	0.37	0.00	0.82
15	1J	0	-696	0	-1463	1201	12362	2.01	2.01	2.01	4.02	0.37	0.00	0.82
15	1K	0	613	0	1279	2807	9750	2.01	2.01	2.01	2.01	0.63	0.00	0.81
15	1L	0	613	0	1279	2807	9750	2.01	2.01	2.01	2.01	0.63	0.00	0.81
15	2	0	-38	0	-85	932	1447	2.01	2.01	2.01	2.01	0.04	0.00	0.12
15	3	0	-28	0	-79	2585	1661	2.01	2.01	2.01	2.01	0.04	0.00	0.21
15	4	0	-60	0	-125	497	1108	2.01	2.01	2.01	2.01	0.06	0.00	0.09
15	5	0	-77	0	-170	1910	2703	2.01	2.01	2.01	2.01	0.08	0.00	0.22
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= 1 d 16/25 (e arm. base nelle due direz.)														
16	1A	0	-753	0	-529	931	664	2.01	2.01	2.01	2.01	0.37	0.00	0.08
16	1B	0	-753	0	-529	931	664	2.01	2.01	2.01	2.01	0.37	0.00	0.08
16	1C	0	978	0	388	578	440	2.01	2.01	2.01	2.01	0.48	0.00	0.05
16	1D	0	978	0	388	578	440	2.01	2.01	2.01	2.01	0.48	0.00	0.05
16	1I	0	-656	0	-892	1329	77	2.01	2.01	2.01	2.01	0.44	0.00	0.11
16	1J	0	-656	0	-892	1329	77	2.01	2.01	2.01	2.01	0.44	0.00	0.11
16	1K	0	880	0	750	1704	392	2.01	2.01	2.01	2.01	0.43	0.00	0.14
16	1L	0	880	0	750	1704	392	2.01	2.01	2.01	2.01	0.43	0.00	0.14
16	2	0	100	0	-56	1079	633	2.01	2.01	2.01	2.01	0.05	0.00	0.09
16	3	0	135	0	-55	1037	623	2.01	2.01	2.01	2.01	0.07	0.00	0.09
16	4	0	68	0	-13	679	455	2.01	2.01	2.01	2.01	0.03	0.00	0.06
16	5	0	207	0	-135	2333	1381	2.01	2.01	2.01	2.01	0.10	0.00	0.19

Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
17	1A	0	-54	0	-83	993	335	2.01	2.01	2.01	2.01	0.04	0.00	0.08
17	1B	0	-54	0	-83	993	335	2.01	2.01	2.01	2.01	0.04	0.00	0.08
17	1C	0	649	0	125	1217	121	2.01	2.01	2.01	2.01	0.32	0.00	0.10
17	1D	0	649	0	125	1217	121	2.01	2.01	2.01	2.01	0.32	0.00	0.10
17	1I	0	-139	0	-154	1848	618	2.01	2.01	2.01	2.01	0.08	0.00	0.15
17	1J	0	-139	0	-154	1848	618	2.01	2.01	2.01	2.01	0.08	0.00	0.15
17	1K	0	734	0	197	1919	155	2.01	2.01	2.01	2.01	0.36	0.00	0.16
17	1L	0	734	0	197	1919	155	2.01	2.01	2.01	2.01	0.36	0.00	0.16
17	2	0	258	0	16	49	22	2.01	2.01	2.01	2.01	0.13	0.00	0.00
17	3	0	217	0	16	166	25	2.01	2.01	2.01	2.01	0.11	0.00	0.01
17	4	0	181	0	10	22	1	2.01	2.01	2.01	2.01	0.09	0.00	0.00
17	5	0	553	0	41	79	48	2.01	2.01	2.01	2.01	0.27	0.00	0.01
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
18	1A	0	-309	0	-145	656	671	2.01	2.01	2.01	2.01	0.15	0.00	0.06
18	1B	0	-309	0	-145	656	671	2.01	2.01	2.01	2.01	0.15	0.00	0.06
18	1C	0	877	0	213	2184	462	2.01	2.01	2.01	2.01	0.43	0.00	0.18
18	1D	0	877	0	213	2184	462	2.01	2.01	2.01	2.01	0.43	0.00	0.18
18	1I	0	-277	0	-232	2253	992	2.01	2.01	2.01	2.01	0.14	0.00	0.19
18	1J	0	-277	0	-232	2253	992	2.01	2.01	2.01	2.01	0.14	0.00	0.19
18	1K	0	845	0	299	2771	218	2.01	2.01	2.01	2.01	0.41	0.00	0.23
18	1L	0	845	0	299	2771	218	2.01	2.01	2.01	2.01	0.41	0.00	0.23
18	2	0	248	0	26	273	38	2.01	2.01	2.01	2.01	0.12	0.00	0.02
18	3	0	238	0	27	154	9	2.01	2.01	2.01	2.01	0.12	0.00	0.01
18	4	0	160	0	1	188	2	2.01	2.01	2.01	2.01	0.08	0.00	0.02
18	5	0	528	0	64	596	101	2.01	2.01	2.01	2.01	0.26	0.00	0.05
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
19	1A	0	-226	0	-75	969	24	2.01	2.01	2.01	2.01	0.11	0.00	0.08
19	1B	0	-226	0	-75	969	24	2.01	2.01	2.01	2.01	0.11	0.00	0.08
19	1C	0	746	0	109	83	90	2.01	2.01	2.01	2.01	0.36	0.00	0.01
19	1D	0	746	0	109	83	90	2.01	2.01	2.01	2.01	0.36	0.00	0.01
19	1I	0	-176	0	-105	787	231	2.01	2.01	2.01	2.01	0.09	0.00	0.07
19	1J	0	-176	0	-105	787	231	2.01	2.01	2.01	2.01	0.09	0.00	0.07
19	1K	0	695	0	140	644	133	2.01	2.01	2.01	2.01	0.34	0.00	0.05
19	1L	0	695	0	140	644	133	2.01	2.01	2.01	2.01	0.34	0.00	0.05
19	2	0	225	0	16	257	71	2.01	2.01	2.01	2.01	0.11	0.00	0.02
19	3	0	150	0	10	356	46	2.01	2.01	2.01	2.01	0.07	0.00	0.03
19	4	0	157	0	13	191	36	2.01	2.01	2.01	2.01	0.08	0.00	0.02
19	5	0	488	0	32	454	168	2.01	2.01	2.01	2.01	0.24	0.00	0.04
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
20	1A	0	-527	0	-683	412	1538	2.01	2.01	2.01	2.01	0.33	0.00	0.13
20	1B	0	-527	0	-683	412	1538	2.01	2.01	2.01	2.01	0.33	0.00	0.13
20	1C	0	782	0	874	111	1083	2.01	2.01	2.01	2.01	0.43	0.00	0.09
20	1D	0	782	0	874	111	1083	2.01	2.01	2.01	2.01	0.43	0.00	0.09
20	1I	0	-313	0	-850	2	1983	2.01	2.01	2.01	2.01	0.42	0.00	0.16
20	1J	0	-313	0	-850	2	1983	2.01	2.01	2.01	2.01	0.42	0.00	0.16
20	1K	0	569	0	1041	447	666	2.01	2.01	2.01	2.01	0.51	0.00	0.06
20	1L	0	569	0	1041	447	666	2.01	2.01	2.01	2.01	0.51	0.00	0.06
20	2	0	113	0	78	728	817	2.01	2.01	2.01	2.01	0.06	0.00	0.07
20	3	0	142	0	83	658	761	2.01	2.01	2.01	2.01	0.07	0.00	0.06
20	4	0	67	0	15	552	586	2.01	2.01	2.01	2.01	0.03	0.00	0.05
20	5	0	236	0	181	1534	1777	2.01	2.01	2.01	2.01	0.12	0.00	0.15
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
21	1A	0	-358	0	-249	1797	62	2.01	2.01	2.01	2.01	0.18	0.00	0.15
21	1B	0	-358	0	-249	1797	62	2.01	2.01	2.01	2.01	0.18	0.00	0.15
21	1C	0	561	0	575	1514	534	2.01	2.01	2.01	2.01	0.28	0.00	0.13
21	1D	0	561	0	575	1514	534	2.01	2.01	2.01	2.01	0.28	0.00	0.13

21	1I	0	-220	0	-289	2073	22	2.01	2.01	2.01	2.01	0.14	0.00	0.17
21	1J	0	-220	0	-289	2073	22	2.01	2.01	2.01	2.01	0.14	0.00	0.17
21	1K	0	424	0	615	1819	712	2.01	2.01	2.01	2.01	0.30	0.00	0.15
21	1L	0	424	0	615	1819	712	2.01	2.01	2.01	2.01	0.30	0.00	0.15
21	2	0	90	0	139	529	26	2.01	2.01	2.01	2.01	0.07	0.00	0.04
21	3	0	103	0	133	564	40	2.01	2.01	2.01	2.01	0.07	0.00	0.05
21	4	0	82	0	120	422	105	2.01	2.01	2.01	2.01	0.06	0.00	0.03
21	5	0	189	0	306	1085	55	2.01	2.01	2.01	2.01	0.15	0.00	0.09
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
22	1A	0	-257	0	-221	94	388	2.01	2.01	2.01	2.01	0.13	0.00	0.03
22	1B	0	-257	0	-221	94	388	2.01	2.01	2.01	2.01	0.13	0.00	0.03
22	1C	0	780	0	376	977	505	2.01	2.01	2.01	2.01	0.38	0.00	0.08
22	1D	0	780	0	376	977	505	2.01	2.01	2.01	2.01	0.38	0.00	0.08
22	1I	0	-172	0	-358	821	428	2.01	2.01	2.01	2.01	0.18	0.00	0.07
22	1J	0	-172	0	-358	821	428	2.01	2.01	2.01	2.01	0.18	0.00	0.07
22	1K	0	696	0	512	1106	176	2.01	2.01	2.01	2.01	0.34	0.00	0.09
22	1L	0	696	0	512	1106	176	2.01	2.01	2.01	2.01	0.34	0.00	0.09
22	2	0	229	0	63	157	236	2.01	2.01	2.01	2.01	0.11	0.00	0.02
22	3	0	221	0	61	43	221	2.01	2.01	2.01	2.01	0.11	0.00	0.02
22	4	0	155	0	23	128	200	2.01	2.01	2.01	2.01	0.08	0.00	0.02
22	5	0	486	0	146	333	505	2.01	2.01	2.01	2.01	0.24	0.00	0.04
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
23	1A	0	-884	0	-355	242	1948	2.01	2.01	2.01	2.01	0.43	0.00	0.16
23	1B	0	-884	0	-355	242	1948	2.01	2.01	2.01	2.01	0.43	0.00	0.16
23	1C	0	1126	0	524	108	1292	2.01	2.01	2.01	2.01	0.55	0.00	0.11
23	1D	0	1126	0	524	108	1292	2.01	2.01	2.01	2.01	0.55	0.00	0.11
23	1I	0	-705	0	-618	117	2605	2.01	2.01	2.01	2.01	0.34	0.00	0.22
23	1J	0	-705	0	-618	117	2605	2.01	2.01	2.01	2.01	0.34	0.00	0.22
23	1K	0	947	0	786	481	1198	2.01	2.01	2.01	2.01	0.46	0.00	0.10
23	1L	0	947	0	786	481	1198	2.01	2.01	2.01	2.01	0.46	0.00	0.10
23	2	0	111	0	71	685	752	2.01	2.01	2.01	2.01	0.05	0.00	0.06
23	3	0	139	0	70	617	655	2.01	2.01	2.01	2.01	0.07	0.00	0.05
23	4	0	112	0	106	559	628	2.01	2.01	2.01	2.01	0.05	0.00	0.05
23	5	0	222	0	158	1386	1554	2.01	2.01	2.01	2.01	0.11	0.00	0.13
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
24	1A	0	-31	0	-114	10	611	2.01	2.01	2.01	2.01	0.06	0.00	0.05
24	1B	0	-31	0	-114	10	611	2.01	2.01	2.01	2.01	0.06	0.00	0.05
24	1C	0	581	0	218	195	695	2.01	2.01	2.01	2.01	0.28	0.00	0.06
24	1D	0	581	0	218	195	695	2.01	2.01	2.01	2.01	0.28	0.00	0.06
24	1I	0	-59	0	-219	130	1037	2.01	2.01	2.01	2.01	0.11	0.00	0.09
24	1J	0	-59	0	-219	130	1037	2.01	2.01	2.01	2.01	0.11	0.00	0.09
24	1K	0	609	0	322	197	1004	2.01	2.01	2.01	2.01	0.30	0.00	0.08
24	1L	0	609	0	322	197	1004	2.01	2.01	2.01	2.01	0.30	0.00	0.08
24	2	0	240	0	41	72	109	2.01	2.01	2.01	2.01	0.12	0.00	0.01
24	3	0	202	0	39	186	105	2.01	2.01	2.01	2.01	0.10	0.00	0.02
24	4	0	176	0	26	52	118	2.01	2.01	2.01	2.01	0.09	0.00	0.01
24	5	0	512	0	98	120	233	2.01	2.01	2.01	2.01	0.25	0.00	0.02
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
25	1A	0	-18	0	-66	135	501	2.01	2.01	2.01	2.01	0.03	0.00	0.04
25	1B	0	-18	0	-66	135	501	2.01	2.01	2.01	2.01	0.03	0.00	0.04
25	1C	0	517	0	204	177	415	2.01	2.01	2.01	2.01	0.25	0.00	0.03
25	1D	0	517	0	204	177	415	2.01	2.01	2.01	2.01	0.25	0.00	0.03
25	1I	0	33	0	-106	124	1023	2.01	2.01	2.01	2.01	0.05	0.00	0.08
25	1J	0	33	0	-106	124	1023	2.01	2.01	2.01	2.01	0.05	0.00	0.08
25	1K	0	466	0	244	12	680	2.01	2.01	2.01	2.01	0.23	0.00	0.06
25	1L	0	466	0	244	12	680	2.01	2.01	2.01	2.01	0.23	0.00	0.06
25	2	0	224	0	60	87	54	2.01	2.01	2.01	2.01	0.11	0.00	0.01

25	3	0	184	0	54	201	34	2.01	2.01	2.01	2.01	0.09	0.00	0.02
25	4	0	180	0	53	74	38	2.01	2.01	2.01	2.01	0.09	0.00	0.01
25	5	0	461	0	128	149	125	2.01	2.01	2.01	2.01	0.23	0.00	0.01
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
26	1A	0	-185	0	-71	338	190	2.01	2.01	2.01	2.01	0.09	0.00	0.03
26	1B	0	-185	0	-71	338	190	2.01	2.01	2.01	2.01	0.09	0.00	0.03
26	1C	0	668	0	155	466	143	2.01	2.01	2.01	2.01	0.33	0.00	0.04
26	1D	0	668	0	155	466	143	2.01	2.01	2.01	2.01	0.33	0.00	0.04
26	1I	0	-86	0	-160	151	159	2.01	2.01	2.01	2.01	0.08	0.00	0.01
26	1J	0	-86	0	-160	151	159	2.01	2.01	2.01	2.01	0.08	0.00	0.01
26	1K	0	569	0	245	349	54	2.01	2.01	2.01	2.01	0.28	0.00	0.03
26	1L	0	569	0	245	349	54	2.01	2.01	2.01	2.01	0.28	0.00	0.03
26	2	0	209	0	36	236	71	2.01	2.01	2.01	2.01	0.10	0.00	0.02
26	3	0	138	0	27	335	77	2.01	2.01	2.01	2.01	0.07	0.00	0.03
26	4	0	151	0	26	195	83	2.01	2.01	2.01	2.01	0.07	0.00	0.02
26	5	0	453	0	79	398	158	2.01	2.01	2.01	2.01	0.22	0.00	0.03
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
27	1A	0	-111	0	-109	427	109	2.01	2.01	2.01	2.01	0.05	0.00	0.04
27	1B	0	-111	0	-109	427	109	2.01	2.01	2.01	2.01	0.05	0.00	0.04
27	1C	0	625	0	201	789	63	2.01	2.01	2.01	2.01	0.31	0.00	0.07
27	1D	0	625	0	201	789	63	2.01	2.01	2.01	2.01	0.31	0.00	0.07
27	1I	0	-72	0	-141	958	38	2.01	2.01	2.01	2.01	0.07	0.00	0.08
27	1J	0	-72	0	-141	958	38	2.01	2.01	2.01	2.01	0.07	0.00	0.08
27	1K	0	586	0	233	927	77	2.01	2.01	2.01	2.01	0.29	0.00	0.08
27	1L	0	586	0	233	927	77	2.01	2.01	2.01	2.01	0.29	0.00	0.08
27	2	0	232	0	41	105	118	2.01	2.01	2.01	2.01	0.11	0.00	0.01
27	3	0	189	0	35	216	103	2.01	2.01	2.01	2.01	0.09	0.00	0.02
27	4	0	200	0	47	112	30	2.01	2.01	2.01	2.01	0.10	0.00	0.01
27	5	0	475	0	85	186	269	2.01	2.01	2.01	2.01	0.23	0.00	0.02
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
28	1A	0	-205	0	-101	1358	370	2.01	2.01	2.01	2.01	0.10	0.00	0.11
28	1B	0	-205	0	-101	1358	370	2.01	2.01	2.01	2.01	0.10	0.00	0.11
28	1C	0	652	0	312	217	62	2.01	2.01	2.01	2.01	0.32	0.00	0.02
28	1D	0	652	0	312	217	62	2.01	2.01	2.01	2.01	0.32	0.00	0.02
28	1I	0	-83	0	-141	1399	504	2.01	2.01	2.01	2.01	0.07	0.00	0.12
28	1J	0	-83	0	-141	1399	504	2.01	2.01	2.01	2.01	0.07	0.00	0.12
28	1K	0	529	0	352	889	133	2.01	2.01	2.01	2.01	0.26	0.00	0.07
28	1L	0	529	0	352	889	133	2.01	2.01	2.01	2.01	0.26	0.00	0.07
28	2	0	199	0	90	147	52	2.01	2.01	2.01	2.01	0.10	0.00	0.01
28	3	0	191	0	83	24	39	2.01	2.01	2.01	2.01	0.09	0.00	0.00
28	4	0	166	0	80	122	80	2.01	2.01	2.01	2.01	0.08	0.00	0.01
28	5	0	413	0	198	309	121	2.01	2.01	2.01	2.01	0.20	0.00	0.03
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
29	1A	0	-382	0	-147	377	15	2.01	2.01	2.01	2.01	0.19	0.00	0.03
29	1B	0	-382	0	-147	377	15	2.01	2.01	2.01	2.01	0.19	0.00	0.03
29	1C	0	870	0	280	1444	28	2.01	2.01	2.01	2.01	0.43	0.00	0.12
29	1D	0	870	0	280	1444	28	2.01	2.01	2.01	2.01	0.43	0.00	0.12
29	1I	0	-228	0	-217	496	42	2.01	2.01	2.01	2.01	0.11	0.00	0.04
29	1J	0	-228	0	-217	496	42	2.01	2.01	2.01	2.01	0.11	0.00	0.04
29	1K	0	715	0	350	1619	315	2.01	2.01	2.01	2.01	0.35	0.00	0.13
29	1L	0	715	0	350	1619	315	2.01	2.01	2.01	2.01	0.35	0.00	0.13
29	2	0	222	0	58	104	237	2.01	2.01	2.01	2.01	0.11	0.00	0.02
29	3	0	211	0	53	1	197	2.01	2.01	2.01	2.01	0.10	0.00	0.02
29	4	0	197	0	71	41	133	2.01	2.01	2.01	2.01	0.10	0.00	0.01
29	5	0	449	0	123	202	515	2.01	2.01	2.01	2.01	0.22	0.00	0.04
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
30	1A	0	-130	0	-37	846	5	2.01	2.01	2.01	2.01	0.06	0.00	0.07

30	1B	0	-130	0	-37	846	5	2.01	2.01	2.01	2.01	0.06	0.00	0.07
30	1C	0	571	0	162	264	47	2.01	2.01	2.01	2.01	0.28	0.00	0.02
30	1D	0	571	0	162	264	47	2.01	2.01	2.01	2.01	0.28	0.00	0.02
30	1I	0	26	0	-64	795	17	2.01	2.01	2.01	2.01	0.03	0.00	0.07
30	1J	0	26	0	-64	795	17	2.01	2.01	2.01	2.01	0.03	0.00	0.07
30	1K	0	415	0	189	640	240	2.01	2.01	2.01	2.01	0.20	0.00	0.05
30	1L	0	415	0	189	640	240	2.01	2.01	2.01	2.01	0.20	0.00	0.05
30	2	0	193	0	53	254	59	2.01	2.01	2.01	2.01	0.09	0.00	0.02
30	3	0	125	0	45	339	35	2.01	2.01	2.01	2.01	0.06	0.00	0.03
30	4	0	148	0	43	216	13	2.01	2.01	2.01	2.01	0.07	0.00	0.02
30	5	0	414	0	116	434	136	2.01	2.01	2.01	2.01	0.20	0.00	0.04
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
31	1A	0	-213	0	-74	829	17	2.01	2.01	2.01	2.01	0.10	0.00	0.07
31	1B	0	-213	0	-74	829	17	2.01	2.01	2.01	2.01	0.10	0.00	0.07
31	1C	0	632	0	143	532	297	2.01	2.01	2.01	2.01	0.31	0.00	0.04
31	1D	0	632	0	143	532	297	2.01	2.01	2.01	2.01	0.31	0.00	0.04
31	1I	0	-144	0	-91	851	117	2.01	2.01	2.01	2.01	0.07	0.00	0.07
31	1J	0	-144	0	-91	851	117	2.01	2.01	2.01	2.01	0.07	0.00	0.07
31	1K	0	563	0	161	769	384	2.01	2.01	2.01	2.01	0.28	0.00	0.06
31	1L	0	563	0	161	769	384	2.01	2.01	2.01	2.01	0.28	0.00	0.06
31	2	0	185	0	29	309	118	2.01	2.01	2.01	2.01	0.09	0.00	0.03
31	3	0	115	0	24	392	110	2.01	2.01	2.01	2.01	0.06	0.00	0.03
31	4	0	154	0	30	275	40	2.01	2.01	2.01	2.01	0.08	0.00	0.02
31	5	0	394	0	64	556	265	2.01	2.01	2.01	2.01	0.19	0.00	0.05
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
32	1A	0	-914	0	-554	673	559	2.01	2.01	2.01	2.01	0.45	0.00	0.06
32	1B	0	-914	0	-554	673	559	2.01	2.01	2.01	2.01	0.45	0.00	0.06
32	1C	0	1145	0	435	1106	91	2.01	2.01	2.01	2.01	0.56	0.00	0.09
32	1D	0	1145	0	435	1106	91	2.01	2.01	2.01	2.01	0.56	0.00	0.09
32	1I	0	-791	0	-919	1323	1432	2.01	2.01	2.01	2.01	0.45	0.00	0.12
32	1J	0	-791	0	-919	1323	1432	2.01	2.01	2.01	2.01	0.45	0.00	0.12
32	1K	0	1022	0	800	755	32	2.01	2.01	2.01	2.01	0.50	0.00	0.06
32	1L	0	1022	0	800	755	32	2.01	2.01	2.01	2.01	0.50	0.00	0.06
32	2	0	106	0	-56	1020	592	2.01	2.01	2.01	2.01	0.05	0.00	0.08
32	3	0	148	0	-46	938	489	2.01	2.01	2.01	2.01	0.07	0.00	0.08
32	4	0	102	0	-84	1047	503	2.01	2.01	2.01	2.01	0.05	0.00	0.09
32	5	0	211	0	-110	2085	1133	2.01	2.01	2.01	2.01	0.10	0.00	0.17
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
33	1A	0	-156	0	-111	100	8	2.01	2.01	2.01	2.01	0.08	0.00	0.01
33	1B	0	-156	0	-111	100	8	2.01	2.01	2.01	2.01	0.08	0.00	0.01
33	1C	0	696	0	148	168	10	2.01	2.01	2.01	2.01	0.34	0.00	0.01
33	1D	0	696	0	148	168	10	2.01	2.01	2.01	2.01	0.34	0.00	0.01
33	1I	0	-120	0	-155	301	259	2.01	2.01	2.01	2.01	0.08	0.00	0.02
33	1J	0	-120	0	-155	301	259	2.01	2.01	2.01	2.01	0.08	0.00	0.02
33	1K	0	660	0	193	47	255	2.01	2.01	2.01	2.01	0.32	0.00	0.02
33	1L	0	660	0	193	47	255	2.01	2.01	2.01	2.01	0.32	0.00	0.02
33	2	0	243	0	19	77	63	2.01	2.01	2.01	2.01	0.12	0.00	0.01
33	3	0	199	0	12	179	21	2.01	2.01	2.01	2.01	0.10	0.00	0.01
33	4	0	218	0	27	84	67	2.01	2.01	2.01	2.01	0.11	0.00	0.01
33	5	0	499	0	34	110	149	2.01	2.01	2.01	2.01	0.24	0.00	0.01
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
34	1A	0	-376	0	-185	1311	215	2.01	2.01	2.01	2.01	0.18	0.00	0.11
34	1B	0	-376	0	-185	1311	215	2.01	2.01	2.01	2.01	0.18	0.00	0.11
34	1C	0	903	0	242	832	259	2.01	2.01	2.01	2.01	0.44	0.00	0.07
34	1D	0	903	0	242	832	259	2.01	2.01	2.01	2.01	0.44	0.00	0.07
34	1I	0	-243	0	-243	955	409	2.01	2.01	2.01	2.01	0.12	0.00	0.08
34	1J	0	-243	0	-243	955	409	2.01	2.01	2.01	2.01	0.12	0.00	0.08

34	1K	0	771	0	300	484	647	2.01	2.01	2.01	2.01	0.38	0.00	0.05
34	1L	0	771	0	300	484	647	2.01	2.01	2.01	2.01	0.38	0.00	0.05
34	2	0	239	0	27	231	96	2.01	2.01	2.01	2.01	0.12	0.00	0.02
34	3	0	230	0	23	104	39	2.01	2.01	2.01	2.01	0.11	0.00	0.01
34	4	0	223	0	42	220	149	2.01	2.01	2.01	2.01	0.11	0.00	0.02
34	5	0	485	0	53	475	235	2.01	2.01	2.01	2.01	0.24	0.00	0.04

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

35	1A	0	-450	0	-188	490	149	2.01	2.01	2.01	2.01	0.22	0.00	0.04
35	1B	0	-450	0	-188	490	149	2.01	2.01	2.01	2.01	0.22	0.00	0.04
35	1C	0	870	0	214	694	794	2.01	2.01	2.01	2.01	0.43	0.00	0.07
35	1D	0	870	0	214	694	794	2.01	2.01	2.01	2.01	0.43	0.00	0.07
35	1I	0	-341	0	-177	529	129	2.01	2.01	2.01	2.01	0.17	0.00	0.04
35	1J	0	-341	0	-177	529	129	2.01	2.01	2.01	2.01	0.17	0.00	0.04
35	1K	0	761	0	203	658	933	2.01	2.01	2.01	2.01	0.37	0.00	0.08
35	1L	0	761	0	203	658	933	2.01	2.01	2.01	2.01	0.37	0.00	0.08
35	2	0	188	0	10	401	66	2.01	2.01	2.01	2.01	0.09	0.00	0.03
35	3	0	117	0	17	529	20	2.01	2.01	2.01	2.01	0.06	0.00	0.04
35	4	0	164	0	15	342	77	2.01	2.01	2.01	2.01	0.08	0.00	0.03
35	5	0	396	0	24	786	91	2.01	2.01	2.01	2.01	0.19	0.00	0.07

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

36	1A	0	-339	0	-145	1399	150	2.01	2.01	2.01	2.01	0.17	0.00	0.12
36	1B	0	-339	0	-145	1399	150	2.01	2.01	2.01	2.01	0.17	0.00	0.12
36	1C	0	795	0	189	1330	315	2.01	2.01	2.01	2.01	0.39	0.00	0.11
36	1D	0	795	0	189	1330	315	2.01	2.01	2.01	2.01	0.39	0.00	0.11
36	1I	0	-194	0	-167	43	163	2.01	2.01	2.01	2.01	0.09	0.00	0.01
36	1J	0	-194	0	-167	43	163	2.01	2.01	2.01	2.01	0.09	0.00	0.01
36	1K	0	649	0	211	13	45	2.01	2.01	2.01	2.01	0.32	0.00	0.00
36	1L	0	649	0	211	13	45	2.01	2.01	2.01	2.01	0.32	0.00	0.00
36	2	0	190	0	20	447	56	2.01	2.01	2.01	2.01	0.09	0.00	0.04
36	3	0	95	0	10	509	34	2.01	2.01	2.01	2.01	0.05	0.00	0.04
36	4	0	124	0	14	359	20	2.01	2.01	2.01	2.01	0.06	0.00	0.03
36	5	0	435	0	40	796	106	2.01	2.01	2.01	2.01	0.21	0.00	0.07

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

37	1A	0	-557	0	-193	1358	18	2.01	2.01	2.01	2.01	0.27	0.00	0.11
37	1B	0	-557	0	-193	1358	18	2.01	2.01	2.01	2.01	0.27	0.00	0.11
37	1C	0	854	0	152	1974	776	2.01	2.01	2.01	2.01	0.42	0.00	0.16
37	1D	0	854	0	152	1974	776	2.01	2.01	2.01	2.01	0.42	0.00	0.16
37	1I	0	-279	0	-129	275	364	2.01	2.01	2.01	2.01	0.14	0.00	0.03
37	1J	0	-279	0	-129	275	364	2.01	2.01	2.01	2.01	0.14	0.00	0.03
37	1K	0	575	0	87	356	532	2.01	2.01	2.01	2.01	0.28	0.00	0.04
37	1L	0	575	0	87	356	532	2.01	2.01	2.01	2.01	0.28	0.00	0.04
37	2	0	114	0	-20	769	9	2.01	2.01	2.01	2.01	0.06	0.00	0.06
37	3	0	15	0	-16	783	13	2.01	2.01	2.01	2.01	0.01	0.00	0.06
37	4	0	64	0	-16	584	3	2.01	2.01	2.01	2.01	0.03	0.00	0.05
37	5	0	296	0	-38	1444	84	2.01	2.01	2.01	2.01	0.15	0.00	0.12

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

38	1A	0	-1299	0	-552	42	1046	2.01	2.01	2.01	2.01	0.64	0.00	0.09
38	1B	0	-1299	0	-552	42	1046	2.01	2.01	2.01	2.01	0.64	0.00	0.09
38	1C	0	1138	0	445	211	465	2.01	2.01	2.01	2.01	0.56	0.00	0.04
38	1D	0	1138	0	445	211	465	2.01	2.01	2.01	2.01	0.56	0.00	0.04
38	1I	0	-640	0	-366	682	462	2.01	2.01	2.01	2.01	0.31	0.00	0.06
38	1J	0	-640	0	-366	682	462	2.01	2.01	2.01	2.01	0.31	0.00	0.06
38	1K	0	479	0	260	316	424	2.01	2.01	2.01	2.01	0.23	0.00	0.04
38	1L	0	479	0	260	316	424	2.01	2.01	2.01	2.01	0.23	0.00	0.04
38	2	0	-97	0	-45	1432	467	2.01	2.01	2.01	2.01	0.05	0.00	0.12
38	3	0	-167	0	-37	827	461	2.01	2.01	2.01	2.01	0.08	0.00	0.07
38	4	0	-92	0	-31	1062	330	2.01	2.01	2.01	2.01	0.05	0.00	0.09

38	5	0	-114	0	-98	2794	987	2.01	2.01	2.01	2.01	0.06	0.00	0.23
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
39	1A	0	-289	0	-69	1433	294	2.01	2.01	2.01	2.01	0.14	0.00	0.12
39	1B	0	-289	0	-69	1433	294	2.01	2.01	2.01	2.01	0.14	0.00	0.12
39	1C	0	698	0	160	874	80	2.01	2.01	2.01	2.01	0.34	0.00	0.07
39	1D	0	698	0	160	874	80	2.01	2.01	2.01	2.01	0.34	0.00	0.07
39	1I	0	-121	0	-108	374	77	2.01	2.01	2.01	2.01	0.06	0.00	0.03
39	1J	0	-121	0	-108	374	77	2.01	2.01	2.01	2.01	0.06	0.00	0.03
39	1K	0	530	0	199	132	85	2.01	2.01	2.01	2.01	0.26	0.00	0.01
39	1L	0	530	0	199	132	85	2.01	2.01	2.01	2.01	0.26	0.00	0.01
39	2	0	171	0	38	462	22	2.01	2.01	2.01	2.01	0.08	0.00	0.04
39	3	0	84	0	25	490	65	2.01	2.01	2.01	2.01	0.04	0.00	0.04
39	4	0	116	0	25	375	60	2.01	2.01	2.01	2.01	0.06	0.00	0.03
39	5	0	391	0	86	811	52	2.01	2.01	2.01	2.01	0.19	0.00	0.07
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
40	1A	0	-223	0	-28	1312	465	2.01	2.01	2.01	2.01	0.11	0.00	0.11
40	1B	0	-223	0	-28	1312	465	2.01	2.01	2.01	2.01	0.11	0.00	0.11
40	1C	0	579	0	158	154	417	2.01	2.01	2.01	2.01	0.28	0.00	0.03
40	1D	0	579	0	158	154	417	2.01	2.01	2.01	2.01	0.28	0.00	0.03
40	1I	0	-27	0	-44	581	393	2.01	2.01	2.01	2.01	0.02	0.00	0.05
40	1J	0	-27	0	-44	581	393	2.01	2.01	2.01	2.01	0.02	0.00	0.05
40	1K	0	383	0	174	617	192	2.01	2.01	2.01	2.01	0.19	0.00	0.05
40	1L	0	383	0	174	617	192	2.01	2.01	2.01	2.01	0.19	0.00	0.05
40	2	0	149	0	54	455	76	2.01	2.01	2.01	2.01	0.07	0.00	0.04
40	3	0	70	0	44	469	46	2.01	2.01	2.01	2.01	0.03	0.00	0.04
40	4	0	108	0	40	384	1	2.01	2.01	2.01	2.01	0.05	0.00	0.03
40	5	0	341	0	123	797	178	2.01	2.01	2.01	2.01	0.17	0.00	0.07
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
41	1A	0	-259	0	-47	883	293	2.01	2.01	2.01	2.01	0.13	0.00	0.07
41	1B	0	-259	0	-47	883	293	2.01	2.01	2.01	2.01	0.13	0.00	0.07
41	1C	0	558	0	112	747	777	2.01	2.01	2.01	2.01	0.27	0.00	0.06
41	1D	0	558	0	112	747	777	2.01	2.01	2.01	2.01	0.27	0.00	0.06
41	1I	0	-114	0	-69	219	404	2.01	2.01	2.01	2.01	0.06	0.00	0.03
41	1J	0	-114	0	-69	219	404	2.01	2.01	2.01	2.01	0.06	0.00	0.03
41	1K	0	414	0	134	1443	825	2.01	2.01	2.01	2.01	0.20	0.00	0.12
41	1L	0	414	0	134	1443	825	2.01	2.01	2.01	2.01	0.20	0.00	0.12
41	2	0	127	0	25	564	250	2.01	2.01	2.01	2.01	0.06	0.00	0.05
41	3	0	54	0	21	480	239	2.01	2.01	2.01	2.01	0.03	0.00	0.04
41	4	0	100	0	23	498	124	2.01	2.01	2.01	2.01	0.05	0.00	0.04
41	5	0	289	0	61	1036	581	2.01	2.01	2.01	2.01	0.14	0.00	0.09
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
42	1A	0	-512	0	-139	1250	696	2.01	2.01	2.01	2.01	0.25	0.00	0.10
42	1B	0	-512	0	-139	1250	696	2.01	2.01	2.01	2.01	0.25	0.00	0.10
42	1C	0	788	0	227	704	130	2.01	2.01	2.01	2.01	0.39	0.00	0.06
42	1D	0	788	0	227	704	130	2.01	2.01	2.01	2.01	0.39	0.00	0.06
42	1I	0	-217	0	-128	483	298	2.01	2.01	2.01	2.01	0.11	0.00	0.04
42	1J	0	-217	0	-128	483	298	2.01	2.01	2.01	2.01	0.11	0.00	0.04
42	1K	0	493	0	216	131	32	2.01	2.01	2.01	2.01	0.24	0.00	0.01
42	1L	0	493	0	216	131	32	2.01	2.01	2.01	2.01	0.24	0.00	0.01
42	2	0	106	0	35	646	134	2.01	2.01	2.01	2.01	0.05	0.00	0.05
42	3	0	15	0	19	622	166	2.01	2.01	2.01	2.01	0.01	0.00	0.05
42	4	0	62	0	22	515	114	2.01	2.01	2.01	2.01	0.03	0.00	0.04
42	5	0	277	0	84	1147	307	2.01	2.01	2.01	2.01	0.14	0.00	0.09
Spess.=	50.0 cm	Axxinf= --		Axxsup= --		Ayyinf= --		Ayysup= --		(e arm. base nelle due direz.)				
43	1A	0	-958	0	-249	458	1539	2.01	2.01	2.01	2.01	0.47	0.00	0.13
43	1B	0	-958	0	-249	458	1539	2.01	2.01	2.01	2.01	0.47	0.00	0.13
43	1C	0	865	0	306	1159	573	2.01	2.01	2.01	2.01	0.42	0.00	0.10

43	1D	0	865	0	306	1159	573	2.01	2.01	2.01	2.01	0.42	0.00	0.10
43	1I	0	-469	0	-157	780	1038	2.01	2.01	2.01	2.01	0.23	0.00	0.09
43	1J	0	-469	0	-157	780	1038	2.01	2.01	2.01	2.01	0.23	0.00	0.09
43	1K	0	376	0	214	896	475	2.01	2.01	2.01	2.01	0.18	0.00	0.07
43	1L	0	376	0	214	896	475	2.01	2.01	2.01	2.01	0.18	0.00	0.07
43	2	0	-70	0	19	1169	411	2.01	2.01	2.01	2.01	0.03	0.00	0.10
43	3	0	-124	0	-4	786	411	2.01	2.01	2.01	2.01	0.06	0.00	0.07
43	4	0	-73	0	-12	904	291	2.01	2.01	2.01	2.01	0.04	0.00	0.07
43	5	0	-49	0	58	2178	920	2.01	2.01	2.01	2.01	0.03	0.00	0.18
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
44	1A	0	-322	0	-26	1337	243	2.01	2.01	2.01	2.01	0.16	0.00	0.11
44	1B	0	-322	0	-26	1337	243	2.01	2.01	2.01	2.01	0.16	0.00	0.11
44	1C	0	555	0	160	198	248	2.01	2.01	2.01	2.01	0.27	0.00	0.02
44	1D	0	555	0	160	198	248	2.01	2.01	2.01	2.01	0.27	0.00	0.02
44	1I	0	-98	0	-43	778	196	2.01	2.01	2.01	2.01	0.05	0.00	0.06
44	1J	0	-98	0	-43	778	196	2.01	2.01	2.01	2.01	0.05	0.00	0.06
44	1K	0	331	0	178	503	39	2.01	2.01	2.01	2.01	0.16	0.00	0.04
44	1L	0	331	0	178	503	39	2.01	2.01	2.01	2.01	0.16	0.00	0.04
44	2	0	88	0	54	599	75	2.01	2.01	2.01	2.01	0.04	0.00	0.05
44	3	0	10	0	42	594	33	2.01	2.01	2.01	2.01	0.02	0.00	0.05
44	4	0	55	0	39	502	12	2.01	2.01	2.01	2.01	0.03	0.00	0.04
44	5	0	237	0	128	1043	176	2.01	2.01	2.01	2.01	0.12	0.00	0.09
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
45	1A	0	-413	0	-151	1921	646	2.01	2.01	2.01	2.01	0.20	0.00	0.16
45	1B	0	-413	0	-151	1921	646	2.01	2.01	2.01	2.01	0.20	0.00	0.16
45	1C	0	589	0	205	231	56	2.01	2.01	2.01	2.01	0.29	0.00	0.02
45	1D	0	589	0	205	231	56	2.01	2.01	2.01	2.01	0.29	0.00	0.02
45	1I	0	-177	0	-97	1191	486	2.01	2.01	2.01	2.01	0.09	0.00	0.10
45	1J	0	-177	0	-97	1191	486	2.01	2.01	2.01	2.01	0.09	0.00	0.10
45	1K	0	352	0	152	538	99	2.01	2.01	2.01	2.01	0.17	0.00	0.04
45	1L	0	352	0	152	538	99	2.01	2.01	2.01	2.01	0.17	0.00	0.04
45	2	0	65	0	19	529	240	2.01	2.01	2.01	2.01	0.03	0.00	0.04
45	3	0	-15	0	12	500	207	2.01	2.01	2.01	2.01	0.01	0.00	0.04
45	4	0	44	0	17	470	156	2.01	2.01	2.01	2.01	0.02	0.00	0.04
45	5	0	182	0	52	888	537	2.01	2.01	2.01	2.01	0.09	0.00	0.07
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
46	1A	0	-519	0	-64	596	206	2.01	2.01	2.01	2.01	0.25	0.00	0.05
46	1B	0	-519	0	-64	596	206	2.01	2.01	2.01	2.01	0.25	0.00	0.05
46	1C	0	467	0	187	1520	197	2.01	2.01	2.01	2.01	0.23	0.00	0.13
46	1D	0	467	0	187	1520	197	2.01	2.01	2.01	2.01	0.23	0.00	0.13
46	1I	0	-266	0	-61	645	129	2.01	2.01	2.01	2.01	0.13	0.00	0.05
46	1J	0	-266	0	-61	645	129	2.01	2.01	2.01	2.01	0.13	0.00	0.05
46	1K	0	214	0	185	858	27	2.01	2.01	2.01	2.01	0.10	0.00	0.07
46	1L	0	214	0	185	858	27	2.01	2.01	2.01	2.01	0.10	0.00	0.07
46	2	0	-52	0	48	705	24	2.01	2.01	2.01	2.01	0.03	0.00	0.06
46	3	0	-91	0	31	481	8	2.01	2.01	2.01	2.01	0.04	0.00	0.04
46	4	0	-57	0	32	608	1	2.01	2.01	2.01	2.01	0.03	0.00	0.05
46	5	0	52	0	120	1181	56	2.01	2.01	2.01	2.01	0.06	0.00	0.10
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
47	1A	0	-805	0	-184	1191	625	2.01	2.01	2.01	2.01	0.39	0.00	0.10
47	1B	0	-805	0	-184	1191	625	2.01	2.01	2.01	2.01	0.39	0.00	0.10
47	1C	0	685	0	140	1422	385	2.01	2.01	2.01	2.01	0.34	0.00	0.12
47	1D	0	685	0	140	1422	385	2.01	2.01	2.01	2.01	0.34	0.00	0.12
47	1I	0	-465	0	-158	1509	481	2.01	2.01	2.01	2.01	0.23	0.00	0.12
47	1J	0	-465	0	-158	1509	481	2.01	2.01	2.01	2.01	0.23	0.00	0.12
47	1K	0	346	0	114	1300	58	2.01	2.01	2.01	2.01	0.17	0.00	0.11
47	1L	0	346	0	114	1300	58	2.01	2.01	2.01	2.01	0.17	0.00	0.11

47	2	0	-77	0	-25	1016	435	2.01	2.01	2.01	2.01	0.04	0.00	0.08
47	3	0	-136	0	-26	732	406	2.01	2.01	2.01	2.01	0.07	0.00	0.06
47	4	0	-75	0	-15	877	327	2.01	2.01	2.01	2.01	0.04	0.00	0.07
47	5	0	-76	0	-37	1865	984	2.01	2.01	2.01	2.01	0.04	0.00	0.15
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
48	1A	0	-102	0	-315	9482	1659	2.01	2.01	2.01	2.01	0.15	0.00	0.78
48	1B	0	-102	0	-315	9482	1659	2.01	2.01	2.01	2.01	0.15	0.00	0.78
48	1C	0	142	0	238	3942	3013	2.01	2.01	2.01	2.01	0.12	0.00	0.33
48	1D	0	142	0	238	3942	3013	2.01	2.01	2.01	2.01	0.12	0.00	0.33
48	1I	0	-85	0	-273	7194	430	2.01	2.01	2.01	2.01	0.13	0.00	0.60
48	1J	0	-85	0	-273	7194	430	2.01	2.01	2.01	2.01	0.13	0.00	0.60
48	1K	0	125	0	195	2204	1125	2.01	2.01	2.01	2.01	0.10	0.00	0.18
48	1L	0	125	0	195	2204	1125	2.01	2.01	2.01	2.01	0.10	0.00	0.18
48	2	0	16	0	-34	3214	181	2.01	2.01	2.01	2.01	0.02	0.00	0.27
48	3	0	10	0	-16	3643	96	2.01	2.01	2.01	2.01	0.01	0.00	0.30
48	4	0	10	0	-30	3106	167	2.01	2.01	2.01	2.01	0.01	0.00	0.26
48	5	0	37	0	-71	3802	365	2.01	2.01	2.01	2.01	0.03	0.00	0.31
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
49	1A	0	-321	0	-136	2668	1015	2.01	2.01	2.01	2.01	0.16	0.00	0.22
49	1B	0	-321	0	-136	2668	1015	2.01	2.01	2.01	2.01	0.16	0.00	0.22
49	1C	0	107	0	101	2516	156	2.01	2.01	2.01	2.01	0.05	0.00	0.21
49	1D	0	107	0	101	2516	156	2.01	2.01	2.01	2.01	0.05	0.00	0.21
49	1I	0	-254	0	-116	1573	780	2.01	2.01	2.01	2.01	0.12	0.00	0.13
49	1J	0	-254	0	-116	1573	780	2.01	2.01	2.01	2.01	0.12	0.00	0.13
49	1K	0	40	0	81	996	58	2.01	2.01	2.01	2.01	0.04	0.00	0.08
49	1L	0	40	0	81	996	58	2.01	2.01	2.01	2.01	0.04	0.00	0.08
49	2	0	-132	0	-20	480	56	2.01	2.01	2.01	2.01	0.06	0.00	0.04
49	3	0	-134	0	-13	739	21	2.01	2.01	2.01	2.01	0.07	0.00	0.06
49	4	0	-130	0	-14	480	42	2.01	2.01	2.01	2.01	0.06	0.00	0.04
49	5	0	-146	0	34	429	125	2.01	2.01	2.01	2.01	0.07	0.00	0.04
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
50	1A	0	-244	0	-112	623	75	2.01	2.01	2.01	2.01	0.12	0.00	0.05
50	1B	0	-244	0	-112	623	75	2.01	2.01	2.01	2.01	0.12	0.00	0.05
50	1C	0	66	0	65	777	212	2.01	2.01	2.01	2.01	0.03	0.00	0.06
50	1D	0	66	0	65	777	212	2.01	2.01	2.01	2.01	0.03	0.00	0.06
50	1I	0	-189	0	-120	454	144	2.01	2.01	2.01	2.01	0.09	0.00	0.04
50	1J	0	-189	0	-120	454	144	2.01	2.01	2.01	2.01	0.09	0.00	0.04
50	1K	0	11	0	74	458	298	2.01	2.01	2.01	2.01	0.04	0.00	0.04
50	1L	0	11	0	74	458	298	2.01	2.01	2.01	2.01	0.04	0.00	0.04
50	2	0	-118	0	-21	341	62	2.01	2.01	2.01	2.01	0.06	0.00	0.03
50	3	0	-125	0	-16	561	52	2.01	2.01	2.01	2.01	0.06	0.00	0.05
50	4	0	-121	0	-15	448	1	2.01	2.01	2.01	2.01	0.06	0.00	0.04
50	5	0	-113	0	-40	198	62	2.01	2.01	2.01	2.01	0.06	0.00	0.02
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
51	1A	0	-290	0	-238	207	265	2.01	2.01	2.01	2.01	0.14	0.00	0.02
51	1B	0	-290	0	-238	207	265	2.01	2.01	2.01	2.01	0.14	0.00	0.02
51	1C	0	509	0	270	1283	1655	2.01	2.01	2.01	2.01	0.25	0.00	0.14
51	1D	0	509	0	270	1283	1655	2.01	2.01	2.01	2.01	0.25	0.00	0.14
51	1I	0	-254	0	-274	573	426	2.01	2.01	2.01	2.01	0.13	0.00	0.05
51	1J	0	-254	0	-274	573	426	2.01	2.01	2.01	2.01	0.13	0.00	0.05
51	1K	0	474	0	306	1691	1734	2.01	2.01	2.01	2.01	0.23	0.00	0.14
51	1L	0	474	0	306	1691	1734	2.01	2.01	2.01	2.01	0.23	0.00	0.14
51	2	0	96	0	8	584	358	2.01	2.01	2.01	2.01	0.05	0.00	0.05
51	3	0	32	0	17	514	232	2.01	2.01	2.01	2.01	0.02	0.00	0.04
51	4	0	82	0	11	494	263	2.01	2.01	2.01	2.01	0.04	0.00	0.04
51	5	0	214	0	29	1153	767	2.01	2.01	2.01	2.01	0.10	0.00	0.10
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														

52	1A	0	-363	0	-141	1656	655	2.01	2.01	2.01	2.01	0.18	0.00	0.14
52	1B	0	-363	0	-141	1656	655	2.01	2.01	2.01	2.01	0.18	0.00	0.14
52	1C	0	504	0	101	1079	167	2.01	2.01	2.01	2.01	0.25	0.00	0.09
52	1D	0	504	0	101	1079	167	2.01	2.01	2.01	2.01	0.25	0.00	0.09
52	1I	0	-246	0	-132	743	839	2.01	2.01	2.01	2.01	0.12	0.00	0.07
52	1J	0	-246	0	-132	743	839	2.01	2.01	2.01	2.01	0.12	0.00	0.07
52	1K	0	386	0	92	15	124	2.01	2.01	2.01	2.01	0.19	0.00	0.01
52	1L	0	386	0	92	15	124	2.01	2.01	2.01	2.01	0.19	0.00	0.01
52	2	0	51	0	-23	501	112	2.01	2.01	2.01	2.01	0.03	0.00	0.04
52	3	0	-36	0	-22	534	66	2.01	2.01	2.01	2.01	0.02	0.00	0.04
52	4	0	37	0	-13	468	84	2.01	2.01	2.01	2.01	0.02	0.00	0.04
52	5	0	148	0	-35	868	212	2.01	2.01	2.01	2.01	0.07	0.00	0.07
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
53	1A	0	-1203	0	-596	1239	1421	2.01	2.01	2.01	2.01	0.59	0.00	0.12
53	1B	0	-1203	0	-596	1239	1421	2.01	2.01	2.01	2.01	0.59	0.00	0.12
53	1C	0	1028	0	481	848	1054	2.01	2.01	2.01	2.01	0.50	0.00	0.09
53	1D	0	1028	0	481	848	1054	2.01	2.01	2.01	2.01	0.50	0.00	0.09
53	1I	0	-671	0	-356	1507	962	2.01	2.01	2.01	2.01	0.33	0.00	0.12
53	1J	0	-671	0	-356	1507	962	2.01	2.01	2.01	2.01	0.33	0.00	0.12
53	1K	0	496	0	241	1044	1016	2.01	2.01	2.01	2.01	0.24	0.00	0.09
53	1L	0	496	0	241	1044	1016	2.01	2.01	2.01	2.01	0.24	0.00	0.09
53	2	0	-99	0	-54	1035	458	2.01	2.01	2.01	2.01	0.05	0.00	0.09
53	3	0	-150	0	-49	735	540	2.01	2.01	2.01	2.01	0.07	0.00	0.06
53	4	0	-91	0	-42	935	379	2.01	2.01	2.01	2.01	0.04	0.00	0.08
53	5	0	-129	0	-104	1912	1043	2.01	2.01	2.01	2.01	0.06	0.00	0.16
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
54	1A	0	-142	0	-89	5721	814	2.01	2.01	2.01	2.01	0.07	0.00	0.47
54	1B	0	-142	0	-89	5721	814	2.01	2.01	2.01	2.01	0.07	0.00	0.47
54	1C	0	172	0	141	1725	1742	2.01	2.01	2.01	2.01	0.08	0.00	0.14
54	1D	0	172	0	141	1725	1742	2.01	2.01	2.01	2.01	0.08	0.00	0.14
54	1I	0	-90	0	-59	4535	96	2.01	2.01	2.01	2.01	0.04	0.00	0.38
54	1J	0	-90	0	-59	4535	96	2.01	2.01	2.01	2.01	0.04	0.00	0.38
54	1K	0	119	0	111	349	855	2.01	2.01	2.01	2.01	0.06	0.00	0.07
54	1L	0	119	0	111	349	855	2.01	2.01	2.01	2.01	0.06	0.00	0.07
54	2	0	11	0	20	2882	28	2.01	2.01	2.01	2.01	0.01	0.00	0.24
54	3	0	-5	0	10	2512	5	2.01	2.01	2.01	2.01	0.01	0.00	0.21
54	4	0	-8	0	18	2815	27	2.01	2.01	2.01	2.01	0.01	0.00	0.23
54	5	0	27	0	48	3069	37	2.01	2.01	2.01	2.01	0.02	0.00	0.25
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
55	1A	0	-119	0	-50	2913	234	2.01	2.01	2.01	2.01	0.06	0.00	0.24
55	1B	0	-119	0	-50	2913	234	2.01	2.01	2.01	2.01	0.06	0.00	0.24
55	1C	0	145	0	78	1263	122	2.01	2.01	2.01	2.01	0.07	0.00	0.10
55	1D	0	145	0	78	1263	122	2.01	2.01	2.01	2.01	0.07	0.00	0.10
55	1I	0	-93	0	-53	2872	441	2.01	2.01	2.01	2.01	0.05	0.00	0.24
55	1J	0	-93	0	-53	2872	441	2.01	2.01	2.01	2.01	0.05	0.00	0.24
55	1K	0	120	0	81	1445	49	2.01	2.01	2.01	2.01	0.06	0.00	0.12
55	1L	0	120	0	81	1445	49	2.01	2.01	2.01	2.01	0.06	0.00	0.12
55	2	0	11	0	14	2919	75	2.01	2.01	2.01	2.01	0.01	0.00	0.24
55	3	0	-5	0	10	2718	53	2.01	2.01	2.01	2.01	0.01	0.00	0.22
55	4	0	8	0	15	2846	61	2.01	2.01	2.01	2.01	0.01	0.00	0.24
55	5	0	25	0	23	3110	103	2.01	2.01	2.01	2.01	0.01	0.00	0.26
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
56	1A	0	-323	0	-408	699	551	2.01	2.01	2.01	2.01	0.20	0.00	0.06
56	1B	0	-323	0	-408	699	551	2.01	2.01	2.01	2.01	0.20	0.00	0.06
56	1C	0	407	0	390	45	143	2.01	2.01	2.01	2.01	0.20	0.00	0.01
56	1D	0	407	0	390	45	143	2.01	2.01	2.01	2.01	0.20	0.00	0.01
56	1I	0	-289	0	-386	1041	568	2.01	2.01	2.01	2.01	0.19	0.00	0.09

56	1J	0	-289	0	-386	1041	568	2.01	2.01	2.01	2.01	0.19	0.00	0.09
56	1K	0	373	0	368	165	280	2.01	2.01	2.01	2.01	0.18	0.00	0.02
56	1L	0	373	0	368	165	280	2.01	2.01	2.01	2.01	0.18	0.00	0.02
56	2	0	35	0	-13	227	252	2.01	2.01	2.01	2.01	0.02	0.00	0.02
56	3	0	-16	0	16	174	319	2.01	2.01	2.01	2.01	0.01	0.00	0.03
56	4	0	30	0	-4	180	165	2.01	2.01	2.01	2.01	0.01	0.00	0.01
56	5	0	82	0	-13	311	709	2.01	2.01	2.01	2.01	0.04	0.00	0.06

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

57	1A	0	-116	0	-169	1095	213	2.01	2.01	2.01	2.01	0.08	0.00	0.09
57	1B	0	-116	0	-169	1095	213	2.01	2.01	2.01	2.01	0.08	0.00	0.09
57	1C	0	71	0	26	35	1129	2.01	2.01	2.01	2.01	0.03	0.00	0.09
57	1D	0	71	0	26	35	1129	2.01	2.01	2.01	2.01	0.03	0.00	0.09
57	1I	0	-123	0	-215	753	406	2.01	2.01	2.01	2.01	0.11	0.00	0.06
57	1J	0	-123	0	-215	753	406	2.01	2.01	2.01	2.01	0.11	0.00	0.06
57	1K	0	78	0	72	342	1077	2.01	2.01	2.01	2.01	0.04	0.00	0.09
57	1L	0	78	0	72	342	1077	2.01	2.01	2.01	2.01	0.04	0.00	0.09
57	2	0	-15	0	-44	79	247	2.01	2.01	2.01	2.01	0.02	0.00	0.02
57	3	0	-22	0	-44	89	149	2.01	2.01	2.01	2.01	0.02	0.00	0.01
57	4	0	-11	0	-34	79	240	2.01	2.01	2.01	2.01	0.02	0.00	0.02
57	5	0	-41	0	-139	139	808	2.01	2.01	2.01	2.01	0.07	0.00	0.07

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

58	1A	0	-299	0	-217	668	40	2.01	2.01	2.01	2.01	0.15	0.00	0.06
58	1B	0	-299	0	-217	668	40	2.01	2.01	2.01	2.01	0.15	0.00	0.06
58	1C	0	381	0	169	760	767	2.01	2.01	2.01	2.01	0.19	0.00	0.06
58	1D	0	381	0	169	760	767	2.01	2.01	2.01	2.01	0.19	0.00	0.06
58	1I	0	-204	0	-216	26	321	2.01	2.01	2.01	2.01	0.11	0.00	0.03
58	1J	0	-204	0	-216	26	321	2.01	2.01	2.01	2.01	0.11	0.00	0.03
58	1K	0	286	0	169	258	682	2.01	2.01	2.01	2.01	0.14	0.00	0.06
58	1L	0	286	0	169	258	682	2.01	2.01	2.01	2.01	0.14	0.00	0.06
58	2	0	25	0	-24	283	93	2.01	2.01	2.01	2.01	0.01	0.00	0.02
58	3	0	-45	0	-19	337	41	2.01	2.01	2.01	2.01	0.02	0.00	0.03
58	4	0	17	0	-14	280	65	2.01	2.01	2.01	2.01	0.01	0.00	0.02
58	5	0	91	0	-42	350	282	2.01	2.01	2.01	2.01	0.04	0.00	0.03

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

59	1A	0	-214	0	-172	606	27	2.01	2.01	2.01	2.01	0.10	0.00	0.05
59	1B	0	-214	0	-172	606	27	2.01	2.01	2.01	2.01	0.10	0.00	0.05
59	1C	0	174	0	59	72	591	2.01	2.01	2.01	2.01	0.09	0.00	0.05
59	1D	0	174	0	59	72	591	2.01	2.01	2.01	2.01	0.09	0.00	0.05
59	1I	0	-175	0	-173	491	189	2.01	2.01	2.01	2.01	0.09	0.00	0.04
59	1J	0	-175	0	-173	491	189	2.01	2.01	2.01	2.01	0.09	0.00	0.04
59	1K	0	136	0	60	259	614	2.01	2.01	2.01	2.01	0.07	0.00	0.05
59	1L	0	136	0	60	259	614	2.01	2.01	2.01	2.01	0.07	0.00	0.05
59	2	0	-22	0	-36	56	117	2.01	2.01	2.01	2.01	0.02	0.00	0.01
59	3	0	-43	0	-34	133	71	2.01	2.01	2.01	2.01	0.02	0.00	0.01
59	4	0	-19	0	-27	71	123	2.01	2.01	2.01	2.01	0.01	0.00	0.01
59	5	0	-24	0	-109	322	430	2.01	2.01	2.01	2.01	0.05	0.00	0.04

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

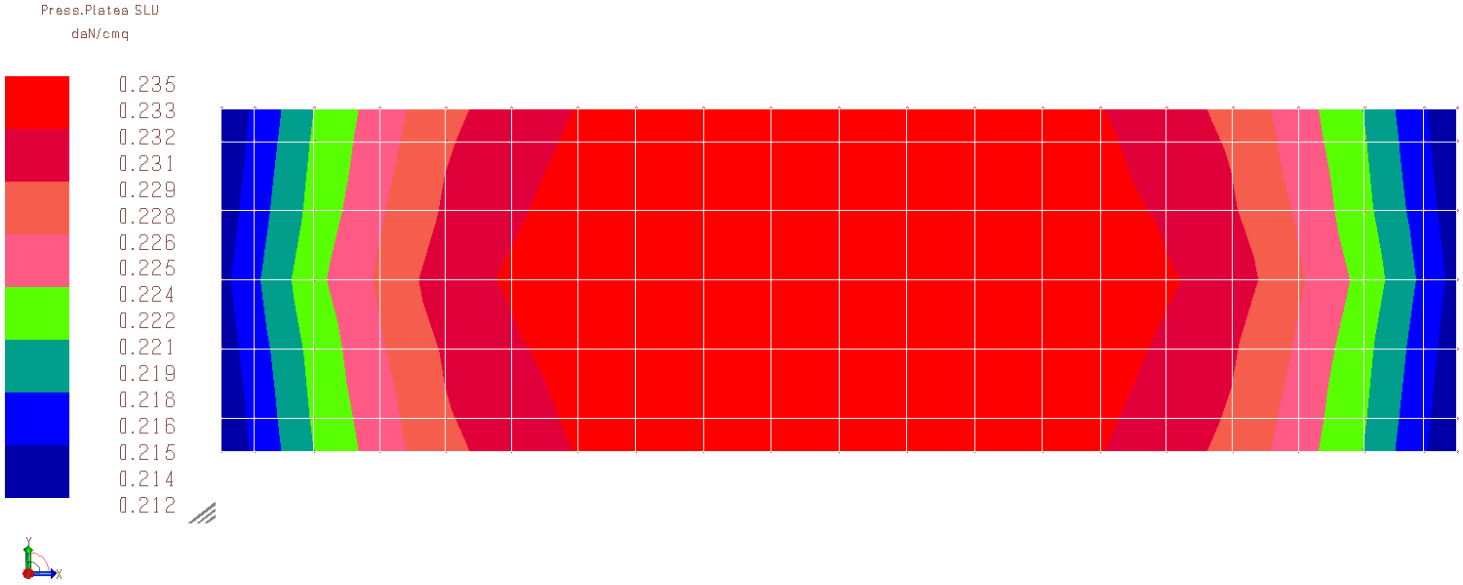
60	1A	0	-454	0	-169	253	965	2.01	2.01	2.01	2.01	0.22	0.00	0.08
60	1B	0	-454	0	-169	253	965	2.01	2.01	2.01	2.01	0.22	0.00	0.08
60	1C	0	322	0	118	310	269	2.01	2.01	2.01	2.01	0.16	0.00	0.03
60	1D	0	322	0	118	310	269	2.01	2.01	2.01	2.01	0.16	0.00	0.03
60	1I	0	-302	0	-144	126	438	2.01	2.01	2.01	2.01	0.15	0.00	0.04
60	1J	0	-302	0	-144	126	438	2.01	2.01	2.01	2.01	0.15	0.00	0.04
60	1K	0	170	0	94	127	183	2.01	2.01	2.01	2.01	0.08	0.00	0.02
60	1L	0	170	0	94	127	183	2.01	2.01	2.01	2.01	0.08	0.00	0.02
60	2	0	-81	0	-26	497	10	2.01	2.01	2.01	2.01	0.04	0.00	0.04
60	3	0	-110	0	-18	376	81	2.01	2.01	2.01	2.01	0.05	0.00	0.03

60	4	0	-78	0	-17	500	9	2.01	2.01	2.01	2.01	0.04	0.00	0.04
60	5	0	-89	0	-43	651	21	2.01	2.01	2.01	2.01	0.04	0.00	0.05
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
61	1A	0	-246	0	-154	545	172	2.01	2.01	2.01	2.01	0.12	0.00	0.05
61	1B	0	-246	0	-154	545	172	2.01	2.01	2.01	2.01	0.12	0.00	0.05
61	1C	0	150	0	91	866	8	2.01	2.01	2.01	2.01	0.07	0.00	0.07
61	1D	0	150	0	91	866	8	2.01	2.01	2.01	2.01	0.07	0.00	0.07
61	1I	0	-202	0	-148	626	11	2.01	2.01	2.01	2.01	0.10	0.00	0.05
61	1J	0	-202	0	-148	626	11	2.01	2.01	2.01	2.01	0.10	0.00	0.05
61	1K	0	106	0	85	770	36	2.01	2.01	2.01	2.01	0.05	0.00	0.06
61	1L	0	106	0	85	770	36	2.01	2.01	2.01	2.01	0.05	0.00	0.06
61	2	0	-66	0	-24	387	22	2.01	2.01	2.01	2.01	0.03	0.00	0.03
61	3	0	-86	0	-19	341	46	2.01	2.01	2.01	2.01	0.04	0.00	0.03
61	4	0	-68	0	-17	444	24	2.01	2.01	2.01	2.01	0.03	0.00	0.04
61	5	0	-55	0	-58	422	28	2.01	2.01	2.01	2.01	0.03	0.00	0.03
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
62	1A	0	-258	0	-109	365	400	2.01	2.01	2.01	2.01	0.13	0.00	0.03
62	1B	0	-258	0	-109	365	400	2.01	2.01	2.01	2.01	0.13	0.00	0.03
62	1C	0	104	0	96	442	898	2.01	2.01	2.01	2.01	0.05	0.00	0.07
62	1D	0	104	0	96	442	898	2.01	2.01	2.01	2.01	0.05	0.00	0.07
62	1I	0	-296	0	-212	461	85	2.01	2.01	2.01	2.01	0.14	0.00	0.04
62	1J	0	-296	0	-212	461	85	2.01	2.01	2.01	2.01	0.14	0.00	0.04
62	1K	0	142	0	199	473	1302	2.01	2.01	2.01	2.01	0.10	0.00	0.11
62	1L	0	142	0	199	473	1302	2.01	2.01	2.01	2.01	0.10	0.00	0.11
62	2	0	-108	0	-9	524	185	2.01	2.01	2.01	2.01	0.05	0.00	0.04
62	3	0	-116	0	-8	644	186	2.01	2.01	2.01	2.01	0.06	0.00	0.05
62	4	0	-118	0	-13	733	169	2.01	2.01	2.01	2.01	0.06	0.00	0.06
62	5	0	-90	0	13	549	404	2.01	2.01	2.01	2.01	0.04	0.00	0.05
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
63	1A	0	-86	0	-105	1010	975	2.01	2.01	2.01	2.01	0.05	0.00	0.08
63	1B	0	-86	0	-105	1010	975	2.01	2.01	2.01	2.01	0.05	0.00	0.08
63	1C	0	71	0	89	128	955	2.01	2.01	2.01	2.01	0.04	0.00	0.08
63	1D	0	71	0	89	128	955	2.01	2.01	2.01	2.01	0.04	0.00	0.08
63	1I	0	-103	0	-155	863	672	2.01	2.01	2.01	2.01	0.08	0.00	0.07
63	1J	0	-103	0	-155	863	672	2.01	2.01	2.01	2.01	0.08	0.00	0.07
63	1K	0	89	0	139	174	718	2.01	2.01	2.01	2.01	0.07	0.00	0.06
63	1L	0	89	0	139	174	718	2.01	2.01	2.01	2.01	0.07	0.00	0.06
63	2	0	-7	0	-7	61	681	2.01	2.01	2.01	2.01	0.01	0.00	0.06
63	3	0	-11	0	-9	138	707	2.01	2.01	2.01	2.01	0.01	0.00	0.06
63	4	0	-3	0	-2	25	601	2.01	2.01	2.01	2.01	0.01	0.00	0.05
63	5	0	-11	0	-14	76	2472	2.01	2.01	2.01	2.01	0.01	0.00	0.20
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
64	1A	0	-163	0	-51	775	505	2.01	2.01	2.01	2.01	0.08	0.00	0.06
64	1B	0	-163	0	-51	775	505	2.01	2.01	2.01	2.01	0.08	0.00	0.06
64	1C	0	147	0	45	235	41	2.01	2.01	2.01	2.01	0.07	0.00	0.02
64	1D	0	147	0	45	235	41	2.01	2.01	2.01	2.01	0.07	0.00	0.02
64	1I	0	-155	0	-64	987	256	2.01	2.01	2.01	2.01	0.08	0.00	0.08
64	1J	0	-155	0	-64	987	256	2.01	2.01	2.01	2.01	0.08	0.00	0.08
64	1K	0	139	0	58	541	68	2.01	2.01	2.01	2.01	0.07	0.00	0.04
64	1L	0	139	0	58	541	68	2.01	2.01	2.01	2.01	0.07	0.00	0.04
64	2	0	-16	0	-3	7	224	2.01	2.01	2.01	2.01	0.01	0.00	0.02
64	3	0	-30	0	-2	52	236	2.01	2.01	2.01	2.01	0.01	0.00	0.02
64	4	0	-15	0	-2	14	187	2.01	2.01	2.01	2.01	0.01	0.00	0.02
64	5	0	5	0	-7	447	786	2.01	2.01	2.01	2.01	0.01	0.00	0.07
Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)														
65	1A	0	-216	0	-80	924	589	2.01	2.01	2.01	2.01	0.11	0.00	0.08
65	1B	0	-216	0	-80	924	589	2.01	2.01	2.01	2.01	0.11	0.00	0.08

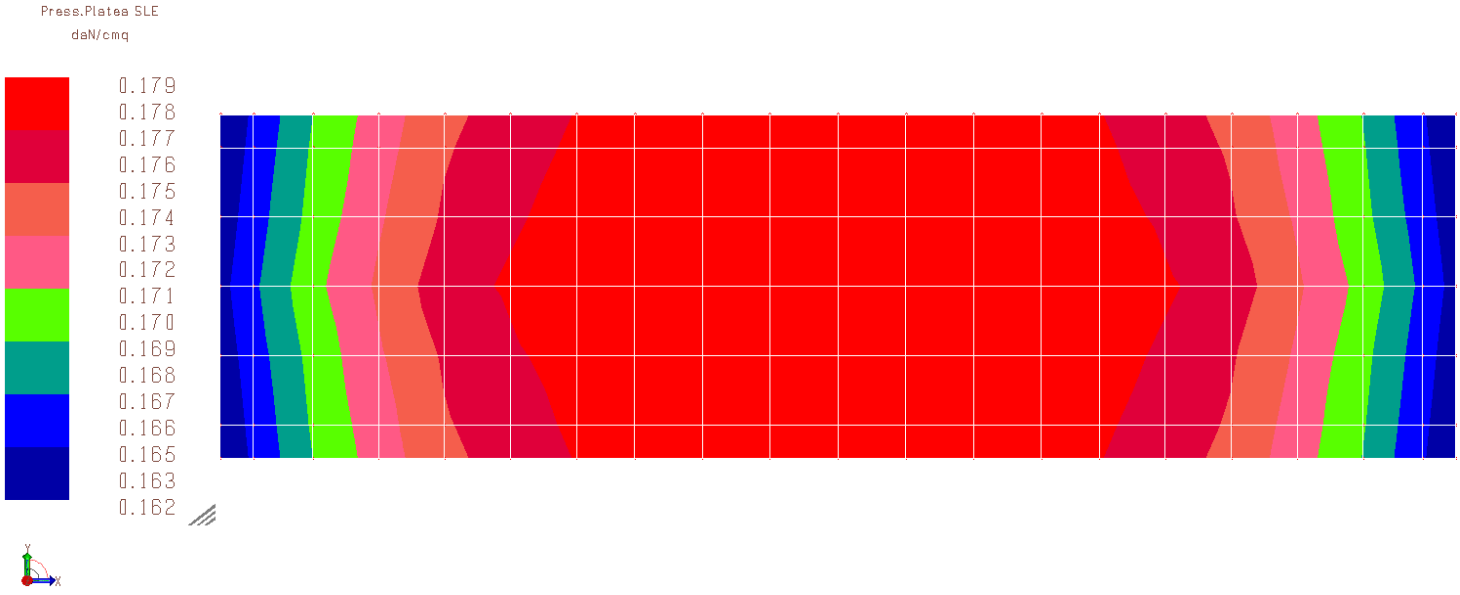
65	1C	0	133	0	53	904	129	2.01	2.01	2.01	2.01	0.07	0.00	0.07
65	1D	0	133	0	53	904	129	2.01	2.01	2.01	2.01	0.07	0.00	0.07
65	1I	0	-230	0	-120	1258	309	2.01	2.01	2.01	2.01	0.11	0.00	0.10
65	1J	0	-230	0	-120	1258	309	2.01	2.01	2.01	2.01	0.11	0.00	0.10
65	1K	0	148	0	93	969	512	2.01	2.01	2.01	2.01	0.07	0.00	0.08
65	1L	0	148	0	93	969	512	2.01	2.01	2.01	2.01	0.07	0.00	0.08
65	2	0	-62	0	-10	280	112	2.01	2.01	2.01	2.01	0.03	0.00	0.02
65	3	0	-78	0	-8	269	141	2.01	2.01	2.01	2.01	0.04	0.00	0.02
65	4	0	-66	0	-9	414	165	2.01	2.01	2.01	2.01	0.03	0.00	0.03
65	5	0	-43	0	-25	136	349	2.01	2.01	2.01	2.01	0.02	0.00	0.03

Spess.= 50.0 cm Axxinf= -- Axxsup= -- Ayyinf= -- Ayysup= -- (e arm. base nelle due direz.)

Dalle figure seguenti, in cui sono riportati gli inviluppi della pressione sul terreno allo stato limite ultimo e di esercizio, si evince che la fondazione di che trattasi risulta rispettare il fattore di sicurezza imposto dal D.M. 2018 nel caso del carico limite relativo al collasso del complesso fondazione – terreno.



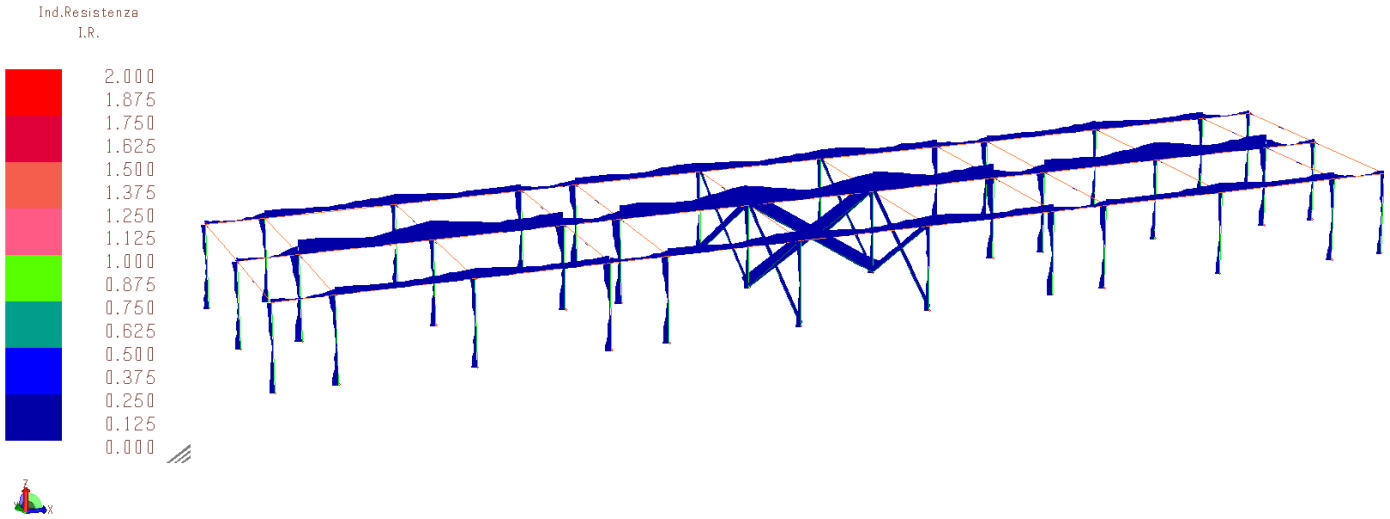
Inviluppo delle pressioni sul terreno allo SLU



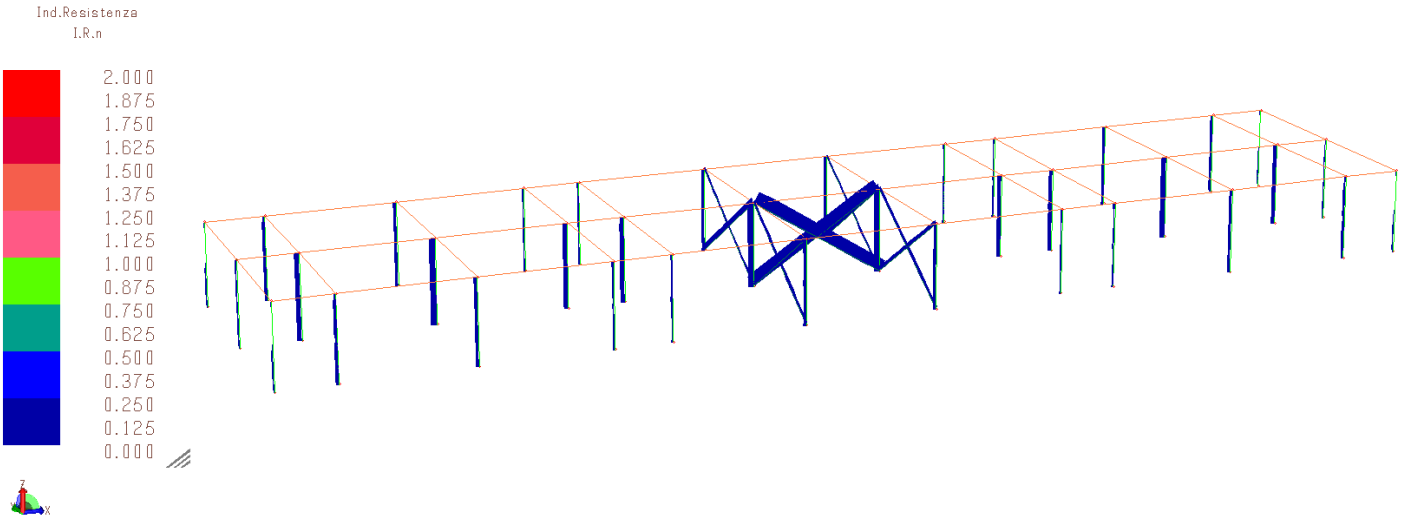
Inviluppo delle pressioni sul terreno allo SLE

8. VERIFICA STRUTTURA IN ELEVAZIONE

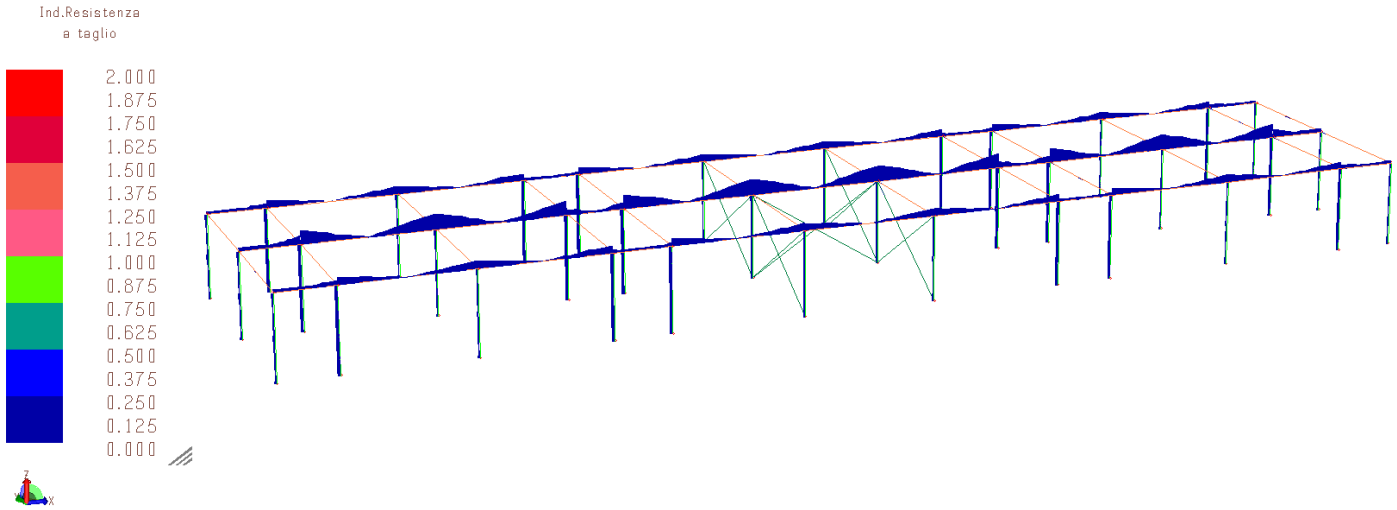
- Verifiche di resistenza



I.R.: Indice di Resistenza

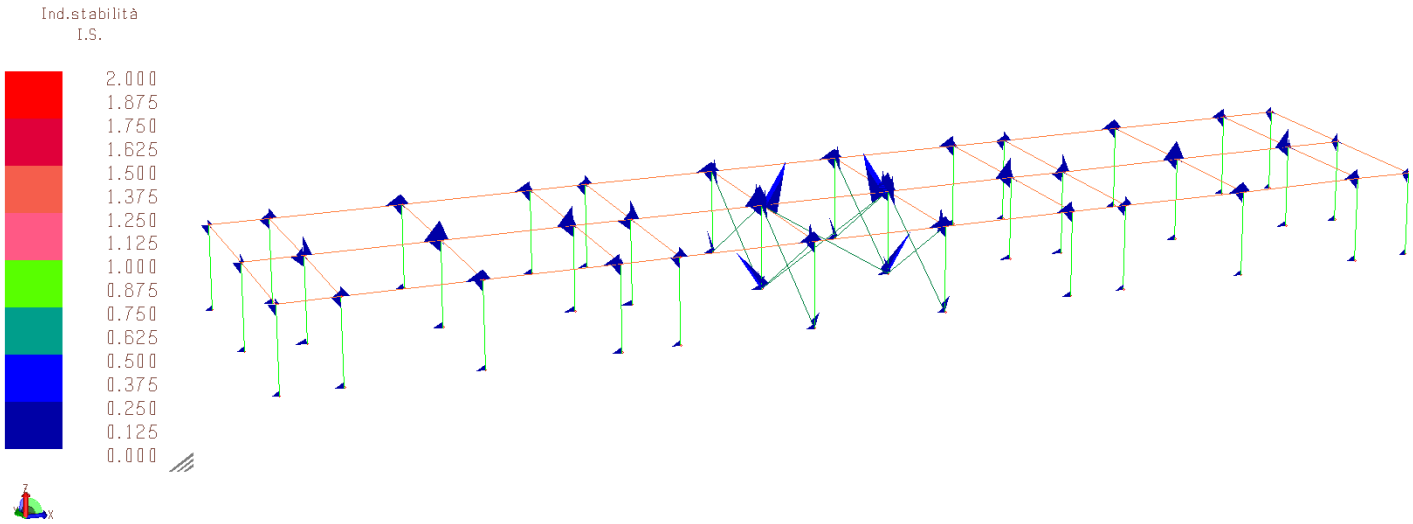


I.R.n.: Indice di Resistenza Sforzo Normale

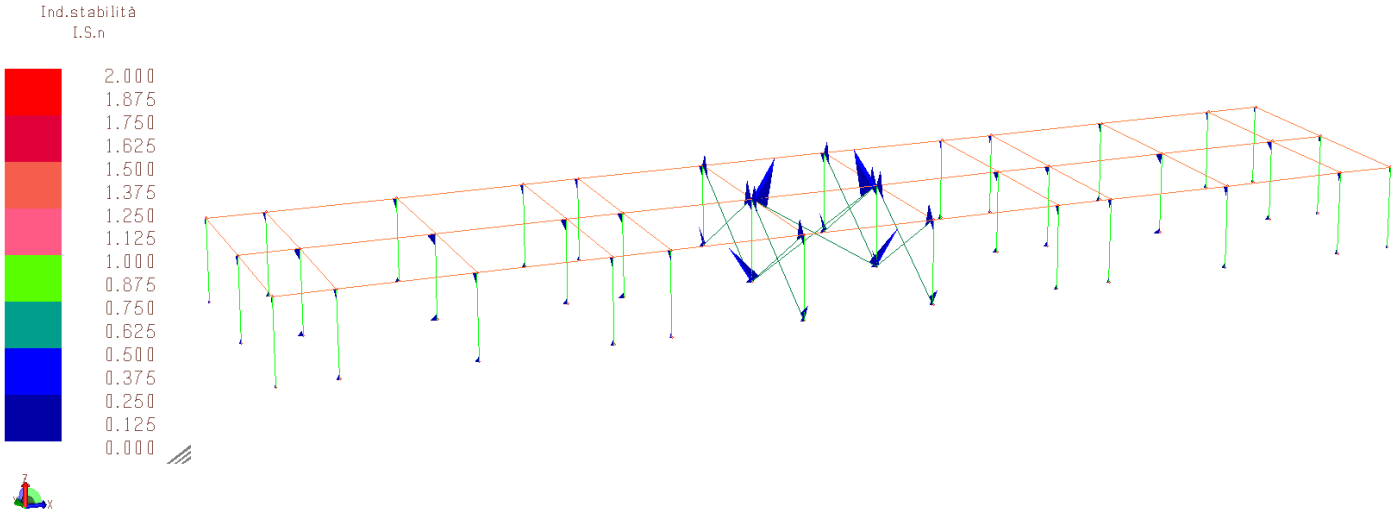


I.V.T.: Indice di Resistenza Taglio e Torsione

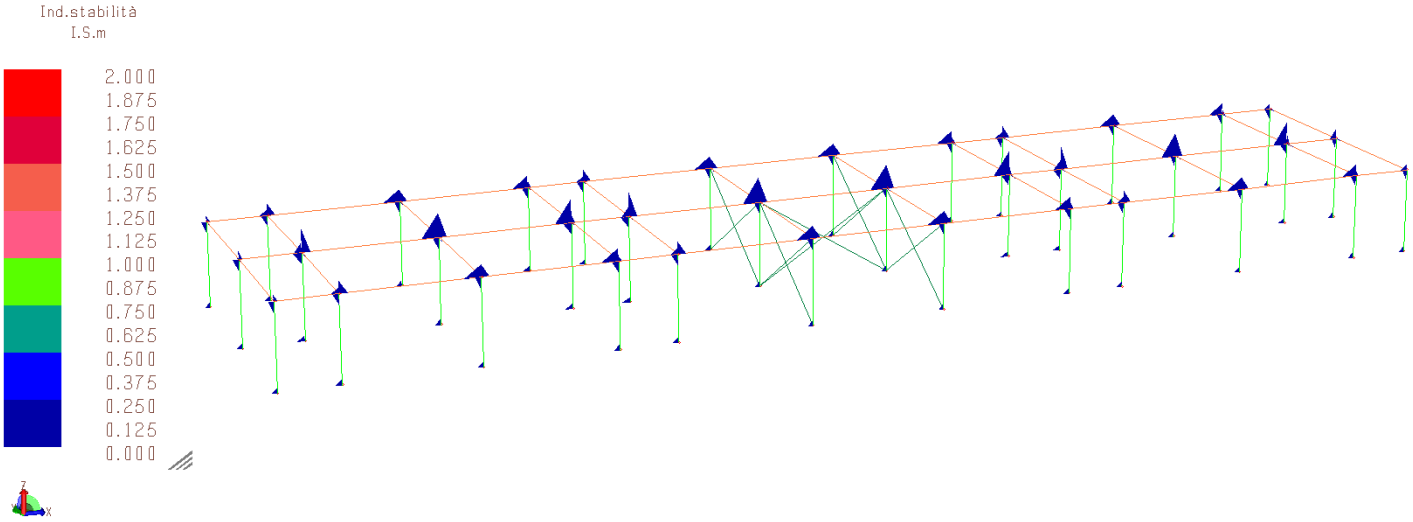
- Verifiche di stabilità



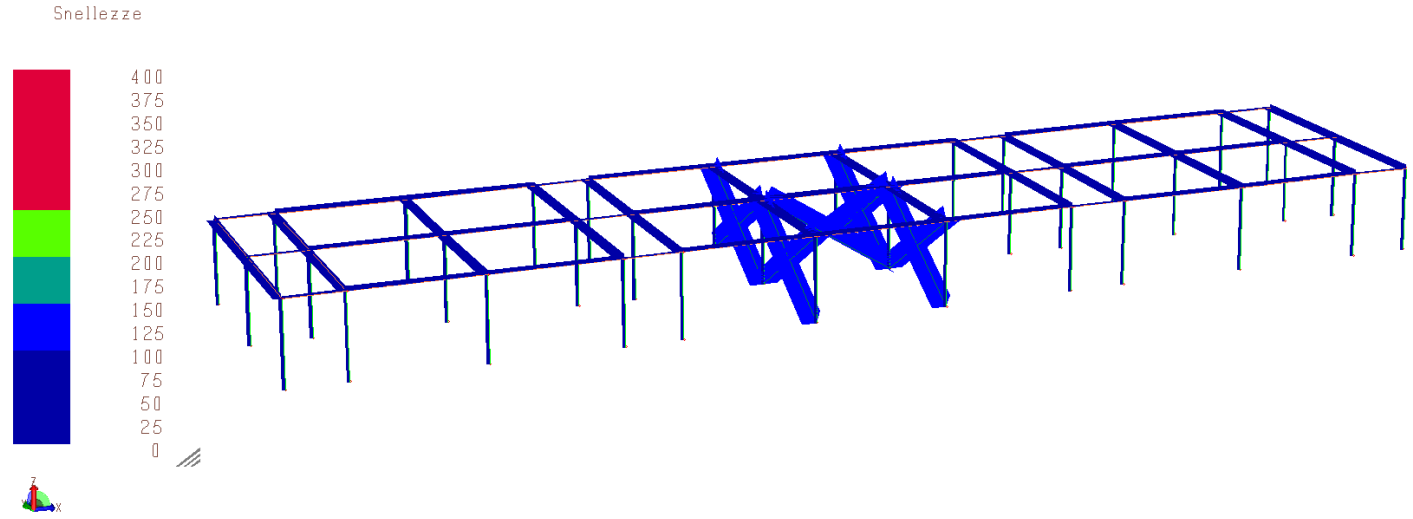
I.S.: Indice di Svergolamento interazione tra Sforzo Normale e Momento Flettente



I.S.n.: Indice di Svergolamento Sforzo Normale



I.S.m.: Indice di Svergolamento dovuto allo Sforzo Normale



Snellezze

Di seguito si riporta uno stralcio del tabulato dei calcoli.

Elemento: **TRAVE** Metodo di verifica: **Eurocodice 3 - NTC 2018**

Gruppo: **2** Descrizione: **Traversi**

Tabella: **Tabella travi**

Tipo acciaio: **S 275** Beta piano 'yx': **1.000** Beta piano 'zx': **1.000**

Coeff. k: **1.000** Coeff. kw: **1.000** Carico all'estradosso della trave

Coeff. riduzione dell'area: **0.000** Tipologia sismica: **Senza prescrizioni aggiuntive**

γM0: **1.050** γM1': **1.050** γM1'': **1.050** γM2: **1.250** γrv: **0.000** γM0 Pf: **1.000** γM1 Pf: **1.000**

Tipo collegamento: **bullonato**

ASTA NUM. 1 NI 78 NF 35 Lungh. 227.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	1292	-0	0	-0	-345	1	0.06	0.00	0.05	
1B	0	-0	1442	-0	0	-0	-508	1	0.07	0.00	0.08	
1C	0	-0	1292	-0	0	-0	-345	1	0.06	0.00	0.05	

1D	0	-0	1442	-0	0	-0	-508	1	0.07	0.00	0.08
1E	0	-0	1292	-0	0	-0	-345	1	0.06	0.00	0.05
1F	0	-0	1442	-0	0	-0	-508	1	0.07	0.00	0.08
1G	0	-0	1292	-0	0	-0	-345	1	0.06	0.00	0.05
1H	0	-0	1442	-0	0	-0	-508	1	0.07	0.00	0.08
1I	0	-0	1344	-0	0	-0	-402	1	0.07	0.00	0.06
1J	0	-0	1390	-0	0	-0	-451	1	0.07	0.00	0.07
1K	0	-0	1344	-0	0	-0	-402	1	0.07	0.00	0.06
1L	0	-0	1390	-0	0	-0	-451	1	0.07	0.00	0.07
1M	0	-0	1344	-0	0	-0	-402	1	0.07	0.00	0.06
1N	0	-0	1390	-0	0	-0	-451	1	0.07	0.00	0.07
1O	0	-0	1344	-0	0	-0	-402	1	0.07	0.00	0.06
1P	0	-0	1390	-0	0	-0	-451	1	0.07	0.00	0.07
2	0	-0	2062	-0	0	-0	-643	1	0.10	0.00	0.10
3	0	-0	1870	-0	0	-0	-583	1	0.09	0.00	0.09
4	0	-0	1676	-0	0	-0	-521	1	0.08	0.00	0.08
5	0	-0	1678	-0	0	-0	-523	1	0.08	0.00	0.08
1A	114	-0	-151	-0	0	-0	303	1	0.01	0.00	0.05
1B	114	-0	-1	-0	0	-0	311	1	0.00	0.00	0.05
1C	114	-0	-151	-0	0	-0	303	1	0.01	0.00	0.05
1D	114	-0	-1	-0	0	-0	311	1	0.00	0.00	0.05
1E	114	-0	-151	-0	0	-0	303	1	0.01	0.00	0.05
1F	114	-0	-1	-0	0	-0	311	1	0.00	0.00	0.05
1G	114	-0	-151	-0	0	-0	303	1	0.01	0.00	0.05
1H	114	-0	-1	-0	0	-0	311	1	0.00	0.00	0.05
1I	114	-0	-99	-0	0	-0	306	1	0.00	0.00	0.05
1J	114	-0	-53	-0	0	-0	308	1	0.00	0.00	0.05
1K	114	-0	-99	-0	0	-0	306	1	0.00	0.00	0.05
1L	114	-0	-53	-0	0	-0	308	1	0.00	0.00	0.05
1M	114	-0	-99	-0	0	-0	306	1	0.00	0.00	0.05
1N	114	-0	-53	-0	0	-0	308	1	0.00	0.00	0.05
1O	114	-0	-99	-0	0	-0	306	1	0.00	0.00	0.05
1P	114	-0	-53	-0	0	-0	308	1	0.00	0.00	0.05
2	114	-0	-114	-0	0	-0	463	1	0.01	0.00	0.07
3	114	-0	-103	-0	0	-0	420	1	0.01	0.00	0.06
4	114	-0	-95	-0	0	-0	377	1	0.00	0.00	0.06
5	114	-0	-93	-0	0	-0	377	1	0.00	0.00	0.06
1A	227	-0	-1594	-0	0	-0	-687	1	0.08	0.00	0.10
1B	227	-0	-1444	-0	0	-0	-508	1	0.07	0.00	0.08
1C	227	-0	-1594	-0	0	0	-687	1	0.08	0.00	0.10
1D	227	-0	-1444	-0	0	0	-508	1	0.07	0.00	0.08
1E	227	-0	-1594	-0	0	-0	-687	1	0.08	0.00	0.10
1F	227	-0	-1444	-0	0	-0	-508	1	0.07	0.00	0.08
1G	227	-0	-1594	-0	0	0	-687	1	0.08	0.00	0.10
1H	227	-0	-1444	-0	0	0	-508	1	0.07	0.00	0.08
1I	227	-0	-1542	-0	0	0	-625	1	0.08	0.00	0.10
1J	227	-0	-1496	-0	0	0	-571	1	0.07	0.00	0.09
1K	227	-0	-1542	-0	0	0	-625	1	0.08	0.00	0.10
1L	227	-0	-1496	-0	0	0	-571	1	0.07	0.00	0.09
1M	227	-0	-1542	-0	0	0	-625	1	0.08	0.00	0.10
1N	227	-0	-1496	-0	0	0	-571	1	0.07	0.00	0.09
1O	227	-0	-1542	-0	0	0	-625	1	0.08	0.00	0.10
1P	227	-0	-1496	-0	0	0	-571	1	0.07	0.00	0.09
2	227	-0	-2290	-0	0	0	-901	1	0.11	0.00	0.14
3	227	-0	-2076	-0	0	0	-817	1	0.10	0.00	0.12
4	227	-0	-1865	-0	0	0	-735	1	0.09	0.00	0.11
5	227	-0	-1863	-0	0	0	-733	1	0.09	0.00	0.11

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	0	-0	-687	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
1B	0	-0	-508	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
1C	0	-0	-687	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
1D	0	-0	-508	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
1E	0	-0	-687	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
1F	0	-0	-508	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
1G	0	-0	-687	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
1H	0	-0	-508	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
1I	0	-0	-625	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1J	0	-0	-571	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1K	0	-0	-625	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1L	0	-0	-571	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1M	0	-0	-625	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1N	0	-0	-571	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1O	0	-0	-625	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1P	0	-0	-571	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
2	0	-0	-901	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.17	--	Snell. 'zx'= 63
3	0	-0	-817	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.15	--	Snell. 'zx'= 63
4	0	-0	-735	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.14	--	Snell. 'zx'= 63
5	0	-0	-733	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.14	--	Snell. 'zx'= 63

ASTA NUM. 2 NI 33 NF 34 Lungh. 233.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	1472	0	0	0	-521	1	0.07	0.00	0.08	
1B	0	-0	1628	0	0	0	-714	1	0.08	0.00	0.11	
1C	0	-0	1472	-0	0	-0	-521	1	0.07	0.00	0.08	
1D	0	-0	1628	-0	0	-0	-714	1	0.08	0.00	0.11	
1E	0	-0	1472	0	0	0	-521	1	0.07	0.00	0.08	
1F	0	-0	1628	0	0	0	-714	1	0.08	0.00	0.11	
1G	0	-0	1472	-0	0	-0	-521	1	0.07	0.00	0.08	
1H	0	-0	1628	-0	0	-0	-714	1	0.08	0.00	0.11	
1I	0	-0	1527	0	0	0	-588	1	0.08	0.00	0.09	
1J	0	-0	1573	0	0	0	-646	1	0.08	0.00	0.10	
1K	0	-0	1527	0	0	0	-588	1	0.08	0.00	0.09	
1L	0	-0	1573	0	0	0	-646	1	0.08	0.00	0.10	
1M	0	-0	1527	0	0	0	-588	1	0.08	0.00	0.09	
1N	0	-0	1573	0	0	0	-646	1	0.08	0.00	0.10	
1O	0	-0	1527	0	0	0	-588	1	0.08	0.00	0.09	
1P	0	-0	1573	0	0	0	-646	1	0.08	0.00	0.10	
2	0	-0	2337	0	0	0	-930	1	0.12	0.00	0.14	
3	0	-0	2120	0	0	0	-844	1	0.10	0.00	0.13	
4	0	-0	1901	0	0	0	-755	1	0.09	0.00	0.12	
5	0	-0	1902	0	-0	0	-757	1	0.09	0.00	0.12	
1A	117	-0	-9	0	0	-0	332	1	0.00	0.00	0.05	
1B	117	-0	147	0	0	-0	320	1	0.01	0.00	0.05	
1C	117	-0	-9	-0	0	-0	332	1	0.00	0.00	0.05	

1D	117	-0	147	-0	0	-0	320	1	0.01	0.00	0.05
1E	117	-0	-9	0	0	-0	332	1	0.00	0.00	0.05
1F	117	-0	147	0	0	-0	320	1	0.01	0.00	0.05
1G	117	-0	-9	-0	0	-0	332	1	0.00	0.00	0.05
1H	117	-0	147	-0	0	-0	320	1	0.01	0.00	0.05
1I	117	-0	46	0	0	-0	328	1	0.00	0.00	0.05
1J	117	-0	92	0	0	-0	325	1	0.00	0.00	0.05
1K	117	-0	46	0	0	-0	328	1	0.00	0.00	0.05
1L	117	-0	92	0	0	-0	325	1	0.00	0.00	0.05
1M	117	-0	46	0	0	-0	328	1	0.00	0.00	0.05
1N	117	-0	92	0	0	-0	325	1	0.00	0.00	0.05
1O	117	-0	46	0	0	-0	328	1	0.00	0.00	0.05
1P	117	-0	92	0	0	-0	325	1	0.00	0.00	0.05
2	117	-0	104	0	0	-0	492	1	0.01	0.00	0.08
3	117	-0	95	0	0	-0	446	1	0.00	0.00	0.07
4	117	-0	83	0	0	-0	400	1	0.00	0.00	0.06
5	117	-0	85	0	-0	-0	400	1	0.00	0.00	0.06
1A	233	-0	-1490	0	0	-0	-541	1	0.07	0.00	0.08
1B	233	-0	-1334	0	0	-0	-371	1	0.07	0.00	0.06
1C	233	-0	-1490	-0	0	-0	-541	1	0.07	0.00	0.08
1D	233	-0	-1334	-0	0	-0	-371	1	0.07	0.00	0.06
1E	233	-0	-1490	0	0	-0	-541	1	0.07	0.00	0.08
1F	233	-0	-1334	0	0	-0	-371	1	0.07	0.00	0.06
1G	233	-0	-1490	-0	0	-0	-541	1	0.07	0.00	0.08
1H	233	-0	-1334	-0	0	-0	-371	1	0.07	0.00	0.06
1I	233	-0	-1435	0	0	-0	-481	1	0.07	0.00	0.07
1J	233	-0	-1389	0	0	-0	-430	1	0.07	0.00	0.07
1K	233	-0	-1435	0	0	-0	-481	1	0.07	0.00	0.07
1L	233	-0	-1389	0	0	-0	-430	1	0.07	0.00	0.07
1M	233	-0	-1435	0	0	-0	-481	1	0.07	0.00	0.07
1N	233	-0	-1389	0	0	-0	-430	1	0.07	0.00	0.07
1O	233	-0	-1435	0	0	-0	-481	1	0.07	0.00	0.07
1P	233	-0	-1389	0	0	-0	-430	1	0.07	0.00	0.07
2	233	-0	-2129	0	0	-0	-687	1	0.11	0.00	0.10
3	233	-0	-1931	0	0	-0	-623	1	0.10	0.00	0.10
4	233	-0	-1734	0	0	-0	-561	1	0.09	0.00	0.09
5	233	-0	-1732	0	-0	-0	-559	1	0.09	0.00	0.09

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	0	-0	-541	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.10	--	Snell. 'zx'= 65
1B	0	-0	-714	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.13	--	Snell. 'zx'= 65
1C	0	-0	-541	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.10	--	Snell. 'zx'= 65
1D	0	-0	-714	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.13	--	Snell. 'zx'= 65
1E	0	-0	-541	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.10	--	Snell. 'zx'= 65
1F	0	-0	-714	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.13	--	Snell. 'zx'= 65
1G	0	-0	-541	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.10	--	Snell. 'zx'= 65
1H	0	-0	-714	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.13	--	Snell. 'zx'= 65
1I	0	-0	-588	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.11	--	Snell. 'zx'= 65
1J	0	-0	-646	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.12	--	Snell. 'zx'= 65
1K	0	-0	-588	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.11	--	Snell. 'zx'= 65
1L	0	-0	-646	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.12	--	Snell. 'zx'= 65
1M	0	-0	-588	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.11	--	Snell. 'zx'= 65

1N	0	-0	-646	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.12	--	Snell. 'zx'= 65
1O	0	-0	-588	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.11	--	Snell. 'zx'= 65
1P	0	-0	-646	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.12	--	Snell. 'zx'= 65
2	0	-0	-930	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.17	--	Snell. 'zx'= 65
3	0	-0	-844	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.16	--	Snell. 'zx'= 65
4	0	-0	-755	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.14	--	Snell. 'zx'= 65
5	0	-0	-757	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.14	--	Snell. 'zx'= 65

ASTA NUM. 3 NI 32 NF 33 Lungh. 234.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm		daN			daN*m						
1A	0	-0	1429	0	0	0	-520	1	0.07	0.00	0.08	
1B	0	-0	1545	0	0	0	-656	1	0.08	0.00	0.10	
1C	0	-0	1429	-0	0	-0	-520	1	0.07	0.00	0.08	
1D	0	-0	1545	-0	0	-0	-656	1	0.08	0.00	0.10	
1E	0	-0	1429	0	0	0	-520	1	0.07	0.00	0.08	
1F	0	-0	1545	0	0	0	-656	1	0.08	0.00	0.10	
1G	0	-0	1429	-0	0	-0	-520	1	0.07	0.00	0.08	
1H	0	-0	1545	-0	0	-0	-656	1	0.08	0.00	0.10	
1I	0	-0	1470	0	0	0	-568	1	0.07	0.00	0.09	
1J	0	-0	1504	0	0	0	-609	1	0.07	0.00	0.09	
1K	0	-0	1470	-0	0	-0	-568	1	0.07	0.00	0.09	
1L	0	-0	1504	-0	0	-0	-609	1	0.07	0.00	0.09	
1M	0	-0	1470	0	0	0	-568	1	0.07	0.00	0.09	
1N	0	-0	1504	0	0	0	-609	1	0.07	0.00	0.09	
1O	0	-0	1470	-0	0	-0	-568	1	0.07	0.00	0.09	
1P	0	-0	1504	-0	0	-0	-609	1	0.07	0.00	0.09	
2	0	-0	2243	-0	0	0	-887	1	0.11	0.00	0.14	
3	0	-0	2034	-0	0	0	-805	1	0.10	0.00	0.12	
4	0	-0	1824	-0	0	0	-720	1	0.09	0.00	0.11	
5	0	-0	1825	-0	-0	0	-722	1	0.09	0.00	0.11	
1A	117	-0	-58	0	0	-0	282	1	0.00	0.00	0.04	
1B	117	-0	58	0	0	-0	282	1	0.00	0.00	0.04	
1C	117	-0	-58	-0	0	-0	282	1	0.00	0.00	0.04	
1D	117	-0	58	-0	0	-0	282	1	0.00	0.00	0.04	
1E	117	-0	-58	0	0	-0	282	1	0.00	0.00	0.04	
1F	117	-0	58	0	0	-0	282	1	0.00	0.00	0.04	
1G	117	-0	-58	-0	0	-0	282	1	0.00	0.00	0.04	
1H	117	-0	58	-0	0	-0	282	1	0.00	0.00	0.04	
1I	117	-0	-17	0	0	-0	282	1	0.00	0.00	0.04	
1J	117	-0	17	0	0	-0	282	1	0.00	0.00	0.04	
1K	117	-0	-17	-0	0	-0	282	1	0.00	0.00	0.04	
1L	117	-0	17	-0	0	-0	282	1	0.00	0.00	0.04	
1M	117	-0	-17	0	0	-0	282	1	0.00	0.00	0.04	
1N	117	-0	17	0	0	-0	282	1	0.00	0.00	0.04	
1O	117	-0	-17	-0	0	-0	282	1	0.00	0.00	0.04	
1P	117	-0	17	-0	0	-0	282	1	0.00	0.00	0.04	
2	117	-0	-0	-0	0	-0	425	1	0.00	0.00	0.06	
3	117	-0	-0	-0	0	-0	385	1	0.00	0.00	0.06	
4	117	-0	-1	-0	0	-0	346	1	0.00	0.00	0.05	
5	117	-0	0	-0	-0	-0	346	1	0.00	0.00	0.05	
1A	234	-0	-1545	0	0	-0	-656	1	0.08	0.00	0.10	
1B	234	-0	-1429	0	0	-0	-520	1	0.07	0.00	0.08	
1C	234	-0	-1545	-0	0	0	-656	1	0.08	0.00	0.10	

1D	234	-0	-1429	-0	0	0	-520	1	0.07	0.00	0.08
1E	234	-0	-1545	0	0	-0	-656	1	0.08	0.00	0.10
1F	234	-0	-1429	0	0	-0	-520	1	0.07	0.00	0.08
1G	234	-0	-1545	-0	0	0	-656	1	0.08	0.00	0.10
1H	234	-0	-1429	-0	0	0	-520	1	0.07	0.00	0.08
1I	234	-0	-1504	0	0	-0	-609	1	0.07	0.00	0.09
1J	234	-0	-1470	0	0	-0	-568	1	0.07	0.00	0.09
1K	234	-0	-1504	-0	0	0	-609	1	0.07	0.00	0.09
1L	234	-0	-1470	-0	0	0	-568	1	0.07	0.00	0.09
1M	234	-0	-1504	0	0	-0	-609	1	0.07	0.00	0.09
1N	234	-0	-1470	0	0	-0	-568	1	0.07	0.00	0.09
1O	234	-0	-1504	-0	0	0	-609	1	0.07	0.00	0.09
1P	234	-0	-1470	-0	0	0	-568	1	0.07	0.00	0.09
2	234	-0	-2243	0	0	0	-887	1	0.11	0.00	0.14
3	234	-0	-2034	0	0	0	-805	1	0.10	0.00	0.12
4	234	-0	-1826	-0	0	0	-723	1	0.09	0.00	0.11
5	234	-0	-1825	-0	-0	0	-722	1	0.09	0.00	0.11

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	0	0	-656	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.12	--	Snell. 'zx'= 65
1B	0	0	-656	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.12	--	Snell. 'zx'= 65
1C	0	0	-656	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.12	--	Snell. 'zx'= 65
1D	0	0	-656	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.12	--	Snell. 'zx'= 65
1E	0	0	-656	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.12	--	Snell. 'zx'= 65
1F	0	0	-656	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.12	--	Snell. 'zx'= 65
1G	0	0	-656	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.12	--	Snell. 'zx'= 65
1H	0	0	-656	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.12	--	Snell. 'zx'= 65
1I	0	-0	-609	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.11	--	Snell. 'zx'= 65
1J	0	-0	-609	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.11	--	Snell. 'zx'= 65
1K	0	-0	-609	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.11	--	Snell. 'zx'= 65
1L	0	-0	-609	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.11	--	Snell. 'zx'= 65
1M	0	-0	-609	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.11	--	Snell. 'zx'= 65
1N	0	-0	-609	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.11	--	Snell. 'zx'= 65
1O	0	-0	-609	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.11	--	Snell. 'zx'= 65
1P	0	-0	-609	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.11	--	Snell. 'zx'= 65
2	0	-0	-887	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.17	--	Snell. 'zx'= 65
3	0	-0	-805	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.15	--	Snell. 'zx'= 65
4	0	-0	-723	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.13	--	Snell. 'zx'= 65
5	0	-0	-722	1	0.6867	1.0000	1.0000	1.0000	0.8203	--	0.13	--	Snell. 'zx'= 65

ASTA NUM. 4 NI 104 NF 32 Lungh. 233.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	1334	0	0	-0	-371	1	0.07	0.00	0.06	
1B	0	-0	1490	0	0	-0	-541	1	0.07	0.00	0.08	
1C	0	-0	1334	-0	0	-0	-371	1	0.07	0.00	0.06	
1D	0	-0	1490	-0	0	-0	-541	1	0.07	0.00	0.08	
1E	0	-0	1334	0	0	-0	-371	1	0.07	0.00	0.06	
1F	0	-0	1490	0	0	-0	-541	1	0.07	0.00	0.08	

1G	0	-0	1334	-0	0	-0	-371	1	0.07	0.00	0.06
1H	0	-0	1490	-0	0	-0	-541	1	0.07	0.00	0.08
1I	0	-0	1389	-0	0	-0	-430	1	0.07	0.00	0.07
1J	0	-0	1435	-0	0	-0	-481	1	0.07	0.00	0.07
1K	0	-0	1389	-0	0	-0	-430	1	0.07	0.00	0.07
1L	0	-0	1435	-0	0	-0	-481	1	0.07	0.00	0.07
1M	0	-0	1389	-0	0	-0	-430	1	0.07	0.00	0.07
1N	0	-0	1435	-0	0	-0	-481	1	0.07	0.00	0.07
1O	0	-0	1389	-0	0	-0	-430	1	0.07	0.00	0.07
1P	0	-0	1435	-0	0	-0	-481	1	0.07	0.00	0.07
2	0	-0	2129	-0	0	-0	-687	1	0.11	0.00	0.10
3	0	-0	1931	-0	0	-0	-623	1	0.10	0.00	0.10
4	0	-0	1731	-0	0	-0	-557	1	0.09	0.00	0.09
5	0	-0	1732	-0	0	-0	-559	1	0.09	0.00	0.09
1A	117	-0	-147	0	0	-0	320	1	0.01	0.00	0.05
1B	117	-0	9	0	0	-0	332	1	0.00	0.00	0.05
1C	117	-0	-147	-0	0	-0	320	1	0.01	0.00	0.05
1D	117	-0	9	-0	0	-0	332	1	0.00	0.00	0.05
1E	117	-0	-147	0	0	-0	320	1	0.01	0.00	0.05
1F	117	-0	9	0	0	-0	332	1	0.00	0.00	0.05
1G	117	-0	-147	-0	0	-0	320	1	0.01	0.00	0.05
1H	117	-0	9	-0	0	-0	332	1	0.00	0.00	0.05
1I	117	-0	-92	-0	0	-0	325	1	0.00	0.00	0.05
1J	117	-0	-46	-0	0	-0	328	1	0.00	0.00	0.05
1K	117	-0	-92	-0	0	-0	325	1	0.00	0.00	0.05
1L	117	-0	-46	-0	0	-0	328	1	0.00	0.00	0.05
1M	117	-0	-92	-0	0	-0	325	1	0.00	0.00	0.05
1N	117	-0	-46	-0	0	-0	328	1	0.00	0.00	0.05
1O	117	-0	-92	-0	0	-0	325	1	0.00	0.00	0.05
1P	117	-0	-46	-0	0	-0	328	1	0.00	0.00	0.05
2	117	-0	-104	-0	0	-0	492	1	0.01	0.00	0.08
3	117	-0	-94	-0	0	-0	446	1	0.00	0.00	0.07
4	117	-0	-87	-0	0	-0	400	1	0.00	0.00	0.06
5	117	-0	-85	-0	0	-0	400	1	0.00	0.00	0.06
1A	233	-0	-1628	0	0	-0	-714	1	0.08	0.00	0.11
1B	233	-0	-1472	0	0	-0	-521	1	0.07	0.00	0.08
1C	233	-0	-1628	-0	0	0	-714	1	0.08	0.00	0.11
1D	233	-0	-1472	-0	0	0	-521	1	0.07	0.00	0.08
1E	233	-0	-1628	0	0	-0	-714	1	0.08	0.00	0.11
1F	233	-0	-1472	0	0	-0	-521	1	0.07	0.00	0.08
1G	233	-0	-1628	-0	0	0	-714	1	0.08	0.00	0.11
1H	233	-0	-1472	-0	0	0	-521	1	0.07	0.00	0.08
1I	233	-0	-1573	-0	0	0	-646	1	0.08	0.00	0.10
1J	233	-0	-1527	-0	0	0	-588	1	0.08	0.00	0.09
1K	233	-0	-1573	-0	0	0	-646	1	0.08	0.00	0.10
1L	233	-0	-1527	-0	0	0	-588	1	0.08	0.00	0.09
1M	233	-0	-1573	-0	0	0	-646	1	0.08	0.00	0.10
1N	233	-0	-1527	-0	0	0	-588	1	0.08	0.00	0.09
1O	233	-0	-1573	-0	0	0	-646	1	0.08	0.00	0.10
1P	233	-0	-1527	-0	0	0	-588	1	0.08	0.00	0.09
2	233	-0	-2337	-0	0	0	-930	1	0.12	0.00	0.14
3	233	-0	-2120	-0	0	0	-844	1	0.10	0.00	0.13
4	233	-0	-1904	-0	0	0	-760	1	0.09	0.00	0.12
5	233	-0	-1902	-0	0	0	-757	1	0.09	0.00	0.12

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	0	-0	-714	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.13	--	Snell. 'zx'= 65
1B	0	-0	-541	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.10	--	Snell. 'zx'= 65
1C	0	-0	-714	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.13	--	Snell. 'zx'= 65
1D	0	-0	-541	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.10	--	Snell. 'zx'= 65
1E	0	-0	-714	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.13	--	Snell. 'zx'= 65
1F	0	-0	-541	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.10	--	Snell. 'zx'= 65
1G	0	-0	-714	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.13	--	Snell. 'zx'= 65
1H	0	-0	-541	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.10	--	Snell. 'zx'= 65
1I	0	-0	-646	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.12	--	Snell. 'zx'= 65
1J	0	-0	-588	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.11	--	Snell. 'zx'= 65
1K	0	-0	-646	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.12	--	Snell. 'zx'= 65
1L	0	-0	-588	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.11	--	Snell. 'zx'= 65
1M	0	-0	-646	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.12	--	Snell. 'zx'= 65
1N	0	-0	-588	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.11	--	Snell. 'zx'= 65
1O	0	-0	-646	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.12	--	Snell. 'zx'= 65
1P	0	-0	-588	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.11	--	Snell. 'zx'= 65
2	0	-0	-930	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.17	--	Snell. 'zx'= 65
3	0	-0	-844	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.16	--	Snell. 'zx'= 65
4	0	-0	-760	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.14	--	Snell. 'zx'= 65
5	0	-0	-757	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.14	--	Snell. 'zx'= 65

ASTA NUM. 5 NI 30 NF 31 Lungh. 227.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	1444	0	0	0	-508	1	0.07	0.00	0.08	
1B	0	-0	1594	0	0	0	-687	1	0.08	0.00	0.10	
1C	0	-0	1444	0	0	-0	-508	1	0.07	0.00	0.08	
1D	0	-0	1594	0	0	-0	-687	1	0.08	0.00	0.10	
1E	0	-0	1444	0	0	0	-508	1	0.07	0.00	0.08	
1F	0	-0	1594	0	0	0	-687	1	0.08	0.00	0.10	
1G	0	-0	1444	0	0	-0	-508	1	0.07	0.00	0.08	
1H	0	-0	1594	0	0	-0	-687	1	0.08	0.00	0.10	
1I	0	-0	1496	0	0	0	-571	1	0.07	0.00	0.09	
1J	0	-0	1542	0	0	0	-625	1	0.08	0.00	0.10	
1K	0	-0	1496	0	0	0	-571	1	0.07	0.00	0.09	
1L	0	-0	1542	0	0	0	-625	1	0.08	0.00	0.10	
1M	0	-0	1496	0	0	0	-571	1	0.07	0.00	0.09	
1N	0	-0	1542	0	0	0	-625	1	0.08	0.00	0.10	
1O	0	-0	1496	0	0	0	-571	1	0.07	0.00	0.09	
1P	0	-0	1542	0	0	0	-625	1	0.08	0.00	0.10	
2	0	-0	2290	0	0	0	-901	1	0.11	0.00	0.14	
3	0	-0	2076	0	0	0	-817	1	0.10	0.00	0.12	
4	0	-0	1862	0	0	0	-732	1	0.09	0.00	0.11	
5	0	-0	1863	0	-0	0	-733	1	0.09	0.00	0.11	
1A	114	-0	1	0	0	-0	311	1	0.00	0.00	0.05	
1B	114	-0	151	0	0	-0	303	1	0.01	0.00	0.05	
1C	114	-0	1	0	0	-0	311	1	0.00	0.00	0.05	
1D	114	-0	151	0	0	-0	303	1	0.01	0.00	0.05	
1E	114	-0	1	0	0	-0	311	1	0.00	0.00	0.05	

1F	114	-0	151	0	0	-0	303	1	0.01	0.00	0.05
1G	114	-0	1	0	0	-0	311	1	0.00	0.00	0.05
1H	114	-0	151	0	0	-0	303	1	0.01	0.00	0.05
1I	114	-0	53	0	0	-0	308	1	0.00	0.00	0.05
1J	114	-0	99	0	0	-0	306	1	0.00	0.00	0.05
1K	114	-0	53	0	0	-0	308	1	0.00	0.00	0.05
1L	114	-0	99	0	0	-0	306	1	0.00	0.00	0.05
1M	114	-0	53	0	0	-0	308	1	0.00	0.00	0.05
1N	114	-0	99	0	0	-0	306	1	0.00	0.00	0.05
1O	114	-0	53	0	0	-0	308	1	0.00	0.00	0.05
1P	114	-0	99	0	0	-0	306	1	0.00	0.00	0.05
2	114	-0	114	0	0	-0	463	1	0.01	0.00	0.07
3	114	-0	103	0	0	-0	420	1	0.01	0.00	0.06
4	114	-0	92	0	0	-0	377	1	0.00	0.00	0.06
5	114	-0	93	0	-0	-0	377	1	0.00	0.00	0.06
1A	227	-0	-1442	0	0	-0	-508	1	0.07	0.00	0.08
1B	227	-0	-1292	0	0	-0	-345	1	0.06	0.00	0.05
1C	227	-0	-1442	0	0	-0	-508	1	0.07	0.00	0.08
1D	227	-0	-1292	0	0	-0	-345	1	0.06	0.00	0.05
1E	227	-0	-1442	0	0	-0	-508	1	0.07	0.00	0.08
1F	227	-0	-1292	0	0	-0	-345	1	0.06	0.00	0.05
1G	227	-0	-1442	0	0	-0	-508	1	0.07	0.00	0.08
1H	227	-0	-1292	0	0	-0	-345	1	0.06	0.00	0.05
1I	227	-0	-1390	0	0	-0	-451	1	0.07	0.00	0.07
1J	227	-0	-1344	0	0	-0	-402	1	0.07	0.00	0.06
1K	227	-0	-1390	0	0	-0	-451	1	0.07	0.00	0.07
1L	227	-0	-1344	0	0	-0	-402	1	0.07	0.00	0.06
1M	227	-0	-1390	0	0	-0	-451	1	0.07	0.00	0.07
1N	227	-0	-1344	0	0	-0	-402	1	0.07	0.00	0.06
1O	227	-0	-1390	0	0	-0	-451	1	0.07	0.00	0.07
1P	227	-0	-1344	0	0	-0	-402	1	0.07	0.00	0.06
2	227	-0	-2062	0	0	-0	-643	1	0.10	0.00	0.10
3	227	-0	-1870	0	0	-0	-583	1	0.09	0.00	0.09
4	227	-0	-1679	0	0	-0	-525	1	0.08	0.00	0.08
5	227	-0	-1678	0	-0	-0	-523	1	0.08	0.00	0.08

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	0	-0	-508	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
1B	0	-0	-687	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
1C	0	-0	-508	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
1D	0	-0	-687	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
1E	0	-0	-508	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
1F	0	-0	-687	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
1G	0	-0	-508	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
1H	0	-0	-687	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
1I	0	-0	-571	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1J	0	-0	-625	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1K	0	-0	-571	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1L	0	-0	-625	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1M	0	-0	-571	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1N	0	-0	-625	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1O	0	-0	-571	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63

1P	0	-0	-625	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'=	63
2	0	-0	-901	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.17	--	Snell. 'zx'=	63
3	0	-0	-817	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.15	--	Snell. 'zx'=	63
4	0	-0	-731	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.14	--	Snell. 'zx'=	63
5	0	-0	-733	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.14	--	Snell. 'zx'=	63

ASTA NUM. 6 NI 93 NF 30 Lungh. 227.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	1307	0	0	-0	-366	1	0.06	0.00	0.06	
1B	0	-0	1449	0	0	-0	-519	1	0.07	0.00	0.08	
1C	0	-0	1307	-0	0	-0	-366	1	0.06	0.00	0.06	
1D	0	-0	1449	-0	0	-0	-519	1	0.07	0.00	0.08	
1E	0	-0	1307	0	0	-0	-366	1	0.06	0.00	0.06	
1F	0	-0	1449	0	0	-0	-519	1	0.07	0.00	0.08	
1G	0	-0	1307	-0	0	-0	-366	1	0.06	0.00	0.06	
1H	0	-0	1449	-0	0	-0	-519	1	0.07	0.00	0.08	
1I	0	-0	1357	-0	0	-0	-420	1	0.07	0.00	0.06	
1J	0	-0	1399	-0	0	-0	-466	1	0.07	0.00	0.07	
1K	0	-0	1357	-0	0	-0	-420	1	0.07	0.00	0.06	
1L	0	-0	1399	-0	0	-0	-466	1	0.07	0.00	0.07	
1M	0	-0	1357	-0	0	-0	-420	1	0.07	0.00	0.06	
1N	0	-0	1399	-0	0	-0	-466	1	0.07	0.00	0.07	
1O	0	-0	1357	-0	0	-0	-420	1	0.07	0.00	0.06	
1P	0	-0	1399	-0	0	-0	-466	1	0.07	0.00	0.07	
2	0	-0	2078	-0	0	-0	-668	1	0.10	0.00	0.10	
3	0	-0	1885	-0	0	-0	-605	1	0.09	0.00	0.09	
4	0	-0	1688	-0	0	-0	-540	1	0.08	0.00	0.08	
5	0	-0	1691	-0	0	-0	-543	1	0.08	0.00	0.08	
1A	114	-0	-136	0	0	-0	299	1	0.01	0.00	0.05	
1B	114	-0	6	0	0	-0	306	1	0.00	0.00	0.05	
1C	114	-0	-136	-0	0	-0	299	1	0.01	0.00	0.05	
1D	114	-0	6	-0	0	-0	306	1	0.00	0.00	0.05	
1E	114	-0	-136	0	0	-0	299	1	0.01	0.00	0.05	
1F	114	-0	6	0	0	-0	306	1	0.00	0.00	0.05	
1G	114	-0	-136	-0	0	-0	299	1	0.01	0.00	0.05	
1H	114	-0	6	-0	0	-0	306	1	0.00	0.00	0.05	
1I	114	-0	-86	-0	0	-0	302	1	0.00	0.00	0.05	
1J	114	-0	-44	-0	0	-0	304	1	0.00	0.00	0.05	
1K	114	-0	-86	-0	0	-0	302	1	0.00	0.00	0.05	
1L	114	-0	-44	-0	0	-0	304	1	0.00	0.00	0.05	
1M	114	-0	-86	-0	0	-0	302	1	0.00	0.00	0.05	
1N	114	-0	-44	-0	0	-0	304	1	0.00	0.00	0.05	
1O	114	-0	-86	-0	0	-0	302	1	0.00	0.00	0.05	
1P	114	-0	-44	-0	0	-0	304	1	0.00	0.00	0.05	
2	114	-0	-98	-0	0	-0	456	1	0.00	0.00	0.07	
3	114	-0	-89	-0	0	-0	414	1	0.00	0.00	0.06	
4	114	-0	-83	-0	0	-0	372	1	0.00	0.00	0.06	
5	114	-0	-80	-0	0	-0	371	1	0.00	0.00	0.06	
1A	227	-0	-1579	0	0	-0	-674	1	0.08	0.00	0.10	
1B	227	-0	-1437	0	0	-0	-506	1	0.07	0.00	0.08	
1C	227	-0	-1579	-0	0	0	-674	1	0.08	0.00	0.10	
1D	227	-0	-1437	-0	0	0	-506	1	0.07	0.00	0.08	
1E	227	-0	-1579	0	0	-0	-674	1	0.08	0.00	0.10	

1F	227	-0	-1437	0	0	-0	-506	1	0.07	0.00	0.08
1G	227	-0	-1579	-0	0	0	-674	1	0.08	0.00	0.10
1H	227	-0	-1437	-0	0	0	-506	1	0.07	0.00	0.08
1I	227	-0	-1529	-0	0	0	-615	1	0.08	0.00	0.09
1J	227	-0	-1487	-0	0	0	-565	1	0.07	0.00	0.09
1K	227	-0	-1529	-0	0	0	-615	1	0.08	0.00	0.09
1L	227	-0	-1487	-0	0	0	-565	1	0.07	0.00	0.09
1M	227	-0	-1529	-0	0	0	-615	1	0.08	0.00	0.09
1N	227	-0	-1487	-0	0	0	-565	1	0.07	0.00	0.09
1O	227	-0	-1529	-0	0	0	-615	1	0.08	0.00	0.09
1P	227	-0	-1487	-0	0	0	-565	1	0.07	0.00	0.09
2	227	-0	-2273	-0	0	0	-889	1	0.11	0.00	0.14
3	227	-0	-2062	-0	0	0	-807	1	0.10	0.00	0.12
4	227	-0	-1853	-0	0	0	-726	1	0.09	0.00	0.11
5	227	-0	-1850	-0	0	0	-724	1	0.09	0.00	0.11

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	0	-0	-674	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1B	0	-0	-519	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.10	--	Snell. 'zx'= 63
1C	0	-0	-674	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1D	0	-0	-519	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.10	--	Snell. 'zx'= 63
1E	0	-0	-674	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1F	0	-0	-519	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.10	--	Snell. 'zx'= 63
1G	0	-0	-674	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.12	--	Snell. 'zx'= 63
1H	0	-0	-519	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.10	--	Snell. 'zx'= 63
1I	0	-0	-615	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1J	0	-0	-565	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.10	--	Snell. 'zx'= 63
1K	0	-0	-615	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1L	0	-0	-565	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.10	--	Snell. 'zx'= 63
1M	0	-0	-615	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1N	0	-0	-565	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.10	--	Snell. 'zx'= 63
1O	0	-0	-615	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.11	--	Snell. 'zx'= 63
1P	0	-0	-565	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.10	--	Snell. 'zx'= 63
2	0	-0	-889	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.16	--	Snell. 'zx'= 63
3	0	-0	-807	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.15	--	Snell. 'zx'= 63
4	0	-0	-726	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63
5	0	-0	-724	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.13	--	Snell. 'zx'= 63

ASTA NUM. 7 NI 34 NF 27 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--	----------			----------			------	----------			
	cm	daN			daN*m							
1A	0	-0	36	0	-0	0	-8	1	0.00	0.00	0.00	
1B	0	-0	50	0	-0	0	-23	1	0.00	0.00	0.00	
1C	0	-0	36	-0	-0	-0	-8	1	0.00	0.00	0.00	
1D	0	-0	50	-0	-0	-0	-23	1	0.00	0.00	0.00	
1E	0	-0	36	0	-0	0	-8	1	0.00	0.00	0.00	

1F	0	-0	50	0	-0	0	-23	1	0.00	0.00	0.00
1G	0	-0	36	-0	-0	-0	-8	1	0.00	0.00	0.00
1H	0	-0	50	-0	-0	-0	-23	1	0.00	0.00	0.00
1I	0	-0	22	0	-0	0	5	1	0.00	0.00	0.00
1J	0	-0	64	0	-0	0	-36	1	0.00	0.00	0.01
1K	0	-0	22	-0	-0	-0	5	1	0.00	0.00	0.00
1L	0	-0	64	-0	-0	-0	-36	1	0.00	0.00	0.01
1M	0	-0	22	0	-0	0	5	1	0.00	0.00	0.00
1N	0	-0	64	0	-0	0	-36	1	0.00	0.00	0.01
1O	0	-0	22	-0	-0	-0	5	1	0.00	0.00	0.00
1P	0	-0	64	-0	-0	-0	-36	1	0.00	0.00	0.01
2	0	-0	55	-0	-0	0	-19	1	0.00	0.00	0.00
3	0	-0	56	-0	-0	0	-20	1	0.00	0.00	0.00
4	0	-0	56	-0	-0	0	-20	1	0.00	0.00	0.00
5	0	-0	51	0	-0	0	-14	1	0.00	0.00	0.00
1A	119	-0	-4	0	-0	0	11	1	0.00	0.00	0.00
1B	119	-0	10	0	-0	0	13	1	0.00	0.00	0.00
1C	119	-0	-4	-0	-0	0	11	1	0.00	0.00	0.00
1D	119	-0	10	-0	-0	0	13	1	0.00	0.00	0.00
1E	119	-0	-4	0	-0	0	11	1	0.00	0.00	0.00
1F	119	-0	10	0	-0	0	13	1	0.00	0.00	0.00
1G	119	-0	-4	-0	-0	0	11	1	0.00	0.00	0.00
1H	119	-0	10	-0	-0	0	13	1	0.00	0.00	0.00
1I	119	-0	-18	0	-0	0	7	1	0.00	0.00	0.00
1J	119	-0	24	0	-0	0	16	1	0.00	0.00	0.00
1K	119	-0	-18	-0	-0	0	7	1	0.00	0.00	0.00
1L	119	-0	24	-0	-0	0	16	1	0.00	0.00	0.00
1M	119	-0	-18	0	-0	0	7	1	0.00	0.00	0.00
1N	119	-0	24	0	-0	0	16	1	0.00	0.00	0.00
1O	119	-0	-18	-0	-0	0	7	1	0.00	0.00	0.00
1P	119	-0	24	-0	-0	0	16	1	0.00	0.00	0.00
2	119	-0	3	-0	-0	0	16	1	0.00	0.00	0.00
3	119	-0	3	-0	-0	0	15	1	0.00	0.00	0.00
4	119	-0	4	-0	-0	0	15	1	0.00	0.00	0.00
5	119	-0	-1	0	-0	0	16	1	0.00	0.00	0.00
1A	238	-0	-45	0	-0	-0	-19	1	0.00	0.00	0.00
1B	238	-0	-30	0	-0	-0	1	1	0.00	0.00	0.00
1C	238	-0	-45	-0	-0	0	-19	1	0.00	0.00	0.00
1D	238	-0	-30	-0	-0	0	1	1	0.00	0.00	0.00
1E	238	-0	-45	0	-0	-0	-19	1	0.00	0.00	0.00
1F	238	-0	-30	0	-0	-0	1	1	0.00	0.00	0.00
1G	238	-0	-45	-0	-0	0	-19	1	0.00	0.00	0.00
1H	238	-0	-30	-0	-0	0	1	1	0.00	0.00	0.00
1I	238	-0	-58	0	-0	-0	-38	1	0.00	0.00	0.01
1J	238	-0	-16	0	-0	-0	21	1	0.00	0.00	0.00
1K	238	-0	-58	-0	-0	0	-38	1	0.00	0.00	0.01
1L	238	-0	-16	-0	-0	0	21	1	0.00	0.00	0.00
1M	238	-0	-58	0	-0	-0	-38	1	0.00	0.00	0.01
1N	238	-0	-16	0	-0	-0	21	1	0.00	0.00	0.00
1O	238	-0	-58	-0	-0	0	-38	1	0.00	0.00	0.01
1P	238	-0	-16	-0	-0	0	21	1	0.00	0.00	0.00
2	238	-0	-49	-0	-0	0	-12	1	0.00	0.00	0.00
3	238	-0	-49	-0	-0	0	-12	1	0.00	0.00	0.00
4	238	-0	-48	-0	-0	0	-11	1	0.00	0.00	0.00
5	238	-0	-53	0	-0	0	-16	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9326	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9527	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9326	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9527	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9326	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9527	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9326	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9527	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-38	1	0.6785	1.0000	1.0000	1.0000	0.9566	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9693	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-38	1	0.6785	1.0000	1.0000	1.0000	0.9566	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9693	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-38	1	0.6785	1.0000	1.0000	1.0000	0.9566	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9693	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-38	1	0.6785	1.0000	1.0000	1.0000	0.9566	--	0.01	--	Snell. 'zx'= 67
1P	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9693	--	0.01	--	Snell. 'zx'= 67
2	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9229	--	0.00	--	Snell. 'zx'= 67
3	0	0	-20	1	0.6785	1.0000	1.0000	1.0000	0.9249	--	0.00	--	Snell. 'zx'= 67
4	0	0	-20	1	0.6785	1.0000	1.0000	1.0000	0.9267	--	0.00	--	Snell. 'zx'= 67
5	0	0	-16	1	0.6785	1.0000	1.0000	1.0000	0.9112	--	0.00	--	Snell. 'zx'= 67

ASTA NUM. 8 NI 37 NF 34 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	30	0	0	0	1	1	0.00	0.00	0.00	
1B	0	-0	45	0	0	0	-19	1	0.00	0.00	0.00	
1C	0	-0	30	-0	0	-0	1	1	0.00	0.00	0.00	
1D	0	-0	45	-0	0	-0	-19	1	0.00	0.00	0.00	
1E	0	-0	30	0	0	0	1	1	0.00	0.00	0.00	
1F	0	-0	45	0	0	0	-19	1	0.00	0.00	0.00	
1G	0	-0	30	-0	0	-0	1	1	0.00	0.00	0.00	
1H	0	-0	45	-0	0	-0	-19	1	0.00	0.00	0.00	
1I	0	-0	16	0	0	0	21	1	0.00	0.00	0.00	
1J	0	-0	58	0	0	0	-38	1	0.00	0.00	0.01	
1K	0	-0	16	-0	0	-0	21	1	0.00	0.00	0.00	
1L	0	-0	58	-0	0	-0	-38	1	0.00	0.00	0.01	
1M	0	-0	16	0	0	0	21	1	0.00	0.00	0.00	
1N	0	-0	58	0	0	0	-38	1	0.00	0.00	0.01	
1O	0	-0	16	-0	0	-0	21	1	0.00	0.00	0.00	
1P	0	-0	58	-0	0	-0	-38	1	0.00	0.00	0.01	
2	0	-0	49	0	0	0	-12	1	0.00	0.00	0.00	
3	0	-0	49	0	0	0	-12	1	0.00	0.00	0.00	
4	0	-0	48	0	0	0	-11	1	0.00	0.00	0.00	
5	0	-0	56	-0	0	-0	-27	1	0.00	0.00	0.00	
1A	119	-0	-10	0	0	0	13	1	0.00	0.00	0.00	
1B	119	-0	4	0	0	0	11	1	0.00	0.00	0.00	
1C	119	-0	-10	-0	0	0	13	1	0.00	0.00	0.00	
1D	119	-0	4	-0	0	0	11	1	0.00	0.00	0.00	
1E	119	-0	-10	0	0	0	13	1	0.00	0.00	0.00	

1F	119	-0	4	0	0	0	11	1	0.00	0.00	0.00
1G	119	-0	-10	-0	0	0	13	1	0.00	0.00	0.00
1H	119	-0	4	-0	0	0	11	1	0.00	0.00	0.00
1I	119	-0	-24	0	0	0	16	1	0.00	0.00	0.00
1J	119	-0	18	0	0	0	7	1	0.00	0.00	0.00
1K	119	-0	-24	-0	0	0	16	1	0.00	0.00	0.00
1L	119	-0	18	-0	0	0	7	1	0.00	0.00	0.00
1M	119	-0	-24	0	0	0	16	1	0.00	0.00	0.00
1N	119	-0	18	0	0	0	7	1	0.00	0.00	0.00
1O	119	-0	-24	-0	0	0	16	1	0.00	0.00	0.00
1P	119	-0	18	-0	0	0	7	1	0.00	0.00	0.00
2	119	-0	-3	0	0	0	16	1	0.00	0.00	0.00
3	119	-0	-3	0	0	0	15	1	0.00	0.00	0.00
4	119	-0	-4	0	0	0	15	1	0.00	0.00	0.00
5	119	-0	4	-0	0	0	9	1	0.00	0.00	0.00
1A	238	-0	-50	0	0	-0	-23	1	0.00	0.00	0.00
1B	238	-0	-36	0	0	-0	-8	1	0.00	0.00	0.00
1C	238	-0	-50	-0	0	0	-23	1	0.00	0.00	0.00
1D	238	-0	-36	-0	0	0	-8	1	0.00	0.00	0.00
1E	238	-0	-50	0	0	-0	-23	1	0.00	0.00	0.00
1F	238	-0	-36	0	0	-0	-8	1	0.00	0.00	0.00
1G	238	-0	-50	-0	0	0	-23	1	0.00	0.00	0.00
1H	238	-0	-36	-0	0	0	-8	1	0.00	0.00	0.00
1I	238	-0	-64	0	0	-0	-36	1	0.00	0.00	0.01
1J	238	-0	-22	0	0	-0	5	1	0.00	0.00	0.00
1K	238	-0	-64	-0	0	0	-36	1	0.00	0.00	0.01
1L	238	-0	-22	-0	0	0	5	1	0.00	0.00	0.00
1M	238	-0	-64	0	0	-0	-36	1	0.00	0.00	0.01
1N	238	-0	-22	0	0	-0	5	1	0.00	0.00	0.00
1O	238	-0	-64	-0	0	0	-36	1	0.00	0.00	0.01
1P	238	-0	-22	-0	0	0	5	1	0.00	0.00	0.00
2	238	-0	-55	0	0	0	-19	1	0.00	0.00	0.00
3	238	-0	-56	0	0	0	-20	1	0.00	0.00	0.00
4	238	-0	-56	0	0	0	-20	1	0.00	0.00	0.00
5	238	-0	-48	-0	0	0	-17	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	--	--										
	daN	daN*m											
1A	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9527	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9326	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9527	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9326	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9527	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9326	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9527	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9326	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9693	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-38	1	0.6785	1.0000	1.0000	1.0000	0.9566	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9693	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-38	1	0.6785	1.0000	1.0000	1.0000	0.9566	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9693	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-38	1	0.6785	1.0000	1.0000	1.0000	0.9566	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9693	--	0.01	--	Snell. 'zx'= 67

1P	0	0	-38	1	0.6785	1.0000	1.0000	1.0000	0.9566	--	0.01	--	Snell. 'zx'=	67
2	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9229	--	0.00	--	Snell. 'zx'=	67
3	0	0	-20	1	0.6785	1.0000	1.0000	1.0000	0.9249	--	0.00	--	Snell. 'zx'=	67
4	0	0	-20	1	0.6785	1.0000	1.0000	1.0000	0.9267	--	0.00	--	Snell. 'zx'=	67
5	0	0	-27	1	0.6785	1.0000	1.0000	1.0000	0.9228	--	0.00	--	Snell. 'zx'=	67

ASTA NUM. 9 NI 33 NF 26 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	35	0	0	0	-4	1	0.00	0.00	0.00	
1B	0	-0	55	0	0	0	-29	1	0.00	0.00	0.00	
1C	0	-0	35	-0	0	-0	-4	1	0.00	0.00	0.00	
1D	0	-0	55	-0	0	-0	-29	1	0.00	0.00	0.00	
1E	0	-0	35	0	0	0	-4	1	0.00	0.00	0.00	
1F	0	-0	55	0	0	0	-29	1	0.00	0.00	0.00	
1G	0	-0	35	-0	0	-0	-4	1	0.00	0.00	0.00	
1H	0	-0	55	-0	0	-0	-29	1	0.00	0.00	0.00	
1I	0	-0	26	0	0	0	2	1	0.00	0.00	0.00	
1J	0	-0	63	0	0	0	-36	1	0.00	0.00	0.01	
1K	0	-0	26	-0	0	-0	2	1	0.00	0.00	0.00	
1L	0	-0	63	-0	0	-0	-36	1	0.00	0.00	0.01	
1M	0	-0	26	0	0	0	2	1	0.00	0.00	0.00	
1N	0	-0	63	0	0	0	-36	1	0.00	0.00	0.01	
1O	0	-0	26	-0	0	-0	2	1	0.00	0.00	0.00	
1P	0	-0	63	-0	0	-0	-36	1	0.00	0.00	0.01	
2	0	-0	58	-0	0	-0	-21	1	0.00	0.00	0.00	
3	0	-0	58	-0	0	-0	-21	1	0.00	0.00	0.00	
4	0	-0	58	-0	0	-0	-22	1	0.00	0.00	0.00	
5	0	-0	54	-0	0	0	-15	1	0.00	0.00	0.00	
1A	119	-0	-5	0	0	0	13	1	0.00	0.00	0.00	
1B	119	-0	15	0	0	0	12	1	0.00	0.00	0.00	
1C	119	-0	-5	-0	0	0	13	1	0.00	0.00	0.00	
1D	119	-0	15	-0	0	0	12	1	0.00	0.00	0.00	
1E	119	-0	-5	0	0	0	13	1	0.00	0.00	0.00	
1F	119	-0	15	0	0	0	12	1	0.00	0.00	0.00	
1G	119	-0	-5	-0	0	0	13	1	0.00	0.00	0.00	
1H	119	-0	15	-0	0	0	12	1	0.00	0.00	0.00	
1I	119	-0	-14	0	0	0	10	1	0.00	0.00	0.00	
1J	119	-0	23	0	0	0	16	1	0.00	0.00	0.00	
1K	119	-0	-14	-0	0	0	10	1	0.00	0.00	0.00	
1L	119	-0	23	-0	0	0	16	1	0.00	0.00	0.00	
1M	119	-0	-14	0	0	0	10	1	0.00	0.00	0.00	
1N	119	-0	23	0	0	0	16	1	0.00	0.00	0.00	
1O	119	-0	-14	-0	0	0	10	1	0.00	0.00	0.00	
1P	119	-0	23	-0	0	0	16	1	0.00	0.00	0.00	
2	119	-0	5	-0	0	0	17	1	0.00	0.00	0.00	
3	119	-0	6	-0	0	0	17	1	0.00	0.00	0.00	
4	119	-0	6	-0	0	0	16	1	0.00	0.00	0.00	
5	119	-0	1	-0	0	0	18	1	0.00	0.00	0.00	
1A	238	-0	-45	0	0	-0	-17	1	0.00	0.00	0.00	
1B	238	-0	-26	0	0	-0	6	1	0.00	0.00	0.00	
1C	238	-0	-45	-0	0	0	-17	1	0.00	0.00	0.00	
1D	238	-0	-26	-0	0	0	6	1	0.00	0.00	0.00	
1E	238	-0	-45	0	0	-0	-17	1	0.00	0.00	0.00	

1F	238	-0	-26	0	0	-0	6	1	0.00	0.00	0.00
1G	238	-0	-45	-0	0	0	-17	1	0.00	0.00	0.00
1H	238	-0	-26	-0	0	0	6	1	0.00	0.00	0.00
1I	238	-0	-54	0	0	-0	-31	1	0.00	0.00	0.00
1J	238	-0	-17	0	0	-0	20	1	0.00	0.00	0.00
1K	238	-0	-54	-0	0	0	-31	1	0.00	0.00	0.00
1L	238	-0	-17	-0	0	0	20	1	0.00	0.00	0.00
1M	238	-0	-54	0	0	-0	-31	1	0.00	0.00	0.00
1N	238	-0	-17	0	0	-0	20	1	0.00	0.00	0.00
1O	238	-0	-54	-0	0	0	-31	1	0.00	0.00	0.00
1P	238	-0	-17	-0	0	0	20	1	0.00	0.00	0.00
2	238	-0	-47	-0	0	0	-8	1	0.00	0.00	0.00
3	238	-0	-46	-0	0	0	-8	1	0.00	0.00	0.00
4	238	-0	-46	-0	0	0	-7	1	0.00	0.00	0.00
5	238	-0	-51	-0	0	0	-12	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1J	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1L	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1N	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1P	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
2	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9347	--	0.00	--	Snell. 'zx'= 67
3	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9362	--	0.00	--	Snell. 'zx'= 67
4	0	0	-22	1	0.6785	1.0000	1.0000	1.0000	0.9373	--	0.00	--	Snell. 'zx'= 67
5	0	0	18	1	0.6785	1.0000	1.0000	1.0000	0.9168	--	0.00	--	Snell. 'zx'= 67

ASTA NUM. 10 NI 38 NF 33 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--	----------			----------			------	----------			
	cm	daN			daN*m							
1A	0	-0	26	0	-0	0	6	1	0.00	0.00	0.00	
1B	0	-0	45	0	-0	0	-17	1	0.00	0.00	0.00	
1C	0	-0	26	-0	-0	-0	6	1	0.00	0.00	0.00	
1D	0	-0	45	-0	-0	-0	-17	1	0.00	0.00	0.00	
1E	0	-0	26	0	-0	0	6	1	0.00	0.00	0.00	

1F	0	-0	45	0	-0	0	-17	1	0.00	0.00	0.00
1G	0	-0	26	-0	-0	-0	6	1	0.00	0.00	0.00
1H	0	-0	45	-0	-0	-0	-17	1	0.00	0.00	0.00
1I	0	-0	17	0	-0	0	20	1	0.00	0.00	0.00
1J	0	-0	54	0	-0	0	-31	1	0.00	0.00	0.00
1K	0	-0	17	-0	-0	-0	20	1	0.00	0.00	0.00
1L	0	-0	54	-0	-0	-0	-31	1	0.00	0.00	0.00
1M	0	-0	17	0	-0	0	20	1	0.00	0.00	0.00
1N	0	-0	54	0	-0	0	-31	1	0.00	0.00	0.00
1O	0	-0	17	-0	-0	-0	20	1	0.00	0.00	0.00
1P	0	-0	54	-0	-0	-0	-31	1	0.00	0.00	0.00
2	0	-0	47	0	-0	0	-8	1	0.00	0.00	0.00
3	0	-0	46	0	-0	0	-8	1	0.00	0.00	0.00
4	0	-0	46	0	-0	0	-7	1	0.00	0.00	0.00
5	0	-0	58	-0	-0	-0	-30	1	0.00	0.00	0.00
1A	119	-0	-15	0	-0	0	12	1	0.00	0.00	0.00
1B	119	-0	5	0	-0	0	13	1	0.00	0.00	0.00
1C	119	-0	-15	-0	-0	0	12	1	0.00	0.00	0.00
1D	119	-0	5	-0	-0	0	13	1	0.00	0.00	0.00
1E	119	-0	-15	0	-0	0	12	1	0.00	0.00	0.00
1F	119	-0	5	0	-0	0	13	1	0.00	0.00	0.00
1G	119	-0	-15	-0	-0	0	12	1	0.00	0.00	0.00
1H	119	-0	5	-0	-0	0	13	1	0.00	0.00	0.00
1I	119	-0	-23	0	-0	0	16	1	0.00	0.00	0.00
1J	119	-0	14	0	-0	0	10	1	0.00	0.00	0.00
1K	119	-0	-23	-0	-0	0	16	1	0.00	0.00	0.00
1L	119	-0	14	-0	-0	0	10	1	0.00	0.00	0.00
1M	119	-0	-23	0	-0	0	16	1	0.00	0.00	0.00
1N	119	-0	14	0	-0	0	10	1	0.00	0.00	0.00
1O	119	-0	-23	-0	-0	0	16	1	0.00	0.00	0.00
1P	119	-0	14	-0	-0	0	10	1	0.00	0.00	0.00
2	119	-0	-5	0	-0	0	17	1	0.00	0.00	0.00
3	119	-0	-6	0	-0	0	17	1	0.00	0.00	0.00
4	119	-0	-6	0	-0	0	16	1	0.00	0.00	0.00
5	119	-0	6	-0	-0	0	8	1	0.00	0.00	0.00
1A	238	-0	-55	0	-0	-0	-29	1	0.00	0.00	0.00
1B	238	-0	-35	0	-0	-0	-4	1	0.00	0.00	0.00
1C	238	-0	-55	-0	-0	0	-29	1	0.00	0.00	0.00
1D	238	-0	-35	-0	-0	0	-4	1	0.00	0.00	0.00
1E	238	-0	-55	0	-0	-0	-29	1	0.00	0.00	0.00
1F	238	-0	-35	0	-0	-0	-4	1	0.00	0.00	0.00
1G	238	-0	-55	-0	-0	0	-29	1	0.00	0.00	0.00
1H	238	-0	-35	-0	-0	0	-4	1	0.00	0.00	0.00
1I	238	-0	-63	0	-0	-0	-36	1	0.00	0.00	0.01
1J	238	-0	-26	0	-0	-0	2	1	0.00	0.00	0.00
1K	238	-0	-63	-0	-0	0	-36	1	0.00	0.00	0.01
1L	238	-0	-26	-0	-0	0	2	1	0.00	0.00	0.00
1M	238	-0	-63	0	-0	-0	-36	1	0.00	0.00	0.01
1N	238	-0	-26	0	-0	-0	2	1	0.00	0.00	0.00
1O	238	-0	-63	-0	-0	0	-36	1	0.00	0.00	0.01
1P	238	-0	-26	-0	-0	0	2	1	0.00	0.00	0.00
2	238	-0	-58	0	-0	-0	-21	1	0.00	0.00	0.00
3	238	-0	-58	0	-0	-0	-21	1	0.00	0.00	0.00
4	238	-0	-58	0	-0	-0	-22	1	0.00	0.00	0.00
5	238	-0	-47	-0	-0	0	-16	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	--	--										
	daN	daN*m											
1A	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1K	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1M	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1O	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1P	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
2	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9347	--	0.00	--	Snell. 'zx'= 67
3	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9362	--	0.00	--	Snell. 'zx'= 67
4	0	0	-22	1	0.6785	1.0000	1.0000	1.0000	0.9373	--	0.00	--	Snell. 'zx'= 67
5	0	0	-30	1	0.6785	1.0000	1.0000	1.0000	0.9271	--	0.00	--	Snell. 'zx'= 67

ASTA NUM. 11 NI 32 NF 25 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--	--	--	--	--	--	--	------	--	--	--	
	cm	daN			daN*m							
1A	0	-0	35	0	-0	0	-4	1	0.00	0.00	0.00	
1B	0	-0	55	0	-0	0	-29	1	0.00	0.00	0.00	
1C	0	-0	35	-0	-0	-0	-4	1	0.00	0.00	0.00	
1D	0	-0	55	-0	-0	-0	-29	1	0.00	0.00	0.00	
1E	0	-0	35	0	-0	0	-4	1	0.00	0.00	0.00	
1F	0	-0	55	0	-0	0	-29	1	0.00	0.00	0.00	
1G	0	-0	35	-0	-0	-0	-4	1	0.00	0.00	0.00	
1H	0	-0	55	-0	-0	-0	-29	1	0.00	0.00	0.00	
1I	0	-0	26	0	-0	0	2	1	0.00	0.00	0.00	
1J	0	-0	63	0	-0	0	-36	1	0.00	0.00	0.01	
1K	0	-0	26	-0	-0	-0	2	1	0.00	0.00	0.00	
1L	0	-0	63	-0	-0	-0	-36	1	0.00	0.00	0.01	
1M	0	-0	26	0	-0	0	2	1	0.00	0.00	0.00	
1N	0	-0	63	0	-0	0	-36	1	0.00	0.00	0.01	
1O	0	-0	26	-0	-0	-0	2	1	0.00	0.00	0.00	
1P	0	-0	63	-0	-0	-0	-36	1	0.00	0.00	0.01	
2	0	-0	58	-0	-0	-0	-21	1	0.00	0.00	0.00	
3	0	-0	58	-0	-0	-0	-21	1	0.00	0.00	0.00	
4	0	-0	59	-0	-0	-0	-22	1	0.00	0.00	0.00	
5	0	-0	54	-0	-0	0	-15	1	0.00	0.00	0.00	
1A	119	-0	-5	0	-0	0	13	1	0.00	0.00	0.00	
1B	119	-0	15	0	-0	0	12	1	0.00	0.00	0.00	
1C	119	-0	-5	-0	-0	0	13	1	0.00	0.00	0.00	
1D	119	-0	15	-0	-0	0	12	1	0.00	0.00	0.00	
1E	119	-0	-5	0	-0	0	13	1	0.00	0.00	0.00	

1F	119	-0	15	0	-0	0	12	1	0.00	0.00	0.00
1G	119	-0	-5	-0	-0	0	13	1	0.00	0.00	0.00
1H	119	-0	15	-0	-0	0	12	1	0.00	0.00	0.00
1I	119	-0	-14	0	-0	0	10	1	0.00	0.00	0.00
1J	119	-0	23	0	-0	0	16	1	0.00	0.00	0.00
1K	119	-0	-14	-0	-0	0	10	1	0.00	0.00	0.00
1L	119	-0	23	-0	-0	0	16	1	0.00	0.00	0.00
1M	119	-0	-14	0	-0	0	10	1	0.00	0.00	0.00
1N	119	-0	23	0	-0	0	16	1	0.00	0.00	0.00
1O	119	-0	-14	-0	-0	0	10	1	0.00	0.00	0.00
1P	119	-0	23	-0	-0	0	16	1	0.00	0.00	0.00
2	119	-0	5	-0	-0	0	17	1	0.00	0.00	0.00
3	119	-0	6	-0	-0	0	17	1	0.00	0.00	0.00
4	119	-0	6	-0	-0	0	16	1	0.00	0.00	0.00
5	119	-0	1	-0	-0	0	18	1	0.00	0.00	0.00
1A	238	-0	-45	0	-0	-0	-17	1	0.00	0.00	0.00
1B	238	-0	-26	0	-0	-0	6	1	0.00	0.00	0.00
1C	238	-0	-45	-0	-0	0	-17	1	0.00	0.00	0.00
1D	238	-0	-26	-0	-0	0	6	1	0.00	0.00	0.00
1E	238	-0	-45	0	-0	-0	-17	1	0.00	0.00	0.00
1F	238	-0	-26	0	-0	-0	6	1	0.00	0.00	0.00
1G	238	-0	-45	-0	-0	0	-17	1	0.00	0.00	0.00
1H	238	-0	-26	-0	-0	0	6	1	0.00	0.00	0.00
1I	238	-0	-54	0	-0	-0	-31	1	0.00	0.00	0.00
1J	238	-0	-17	0	-0	-0	20	1	0.00	0.00	0.00
1K	238	-0	-54	-0	-0	0	-31	1	0.00	0.00	0.00
1L	238	-0	-17	-0	-0	0	20	1	0.00	0.00	0.00
1M	238	-0	-54	0	-0	-0	-31	1	0.00	0.00	0.00
1N	238	-0	-17	0	-0	-0	20	1	0.00	0.00	0.00
1O	238	-0	-54	-0	-0	0	-31	1	0.00	0.00	0.00
1P	238	-0	-17	-0	-0	0	20	1	0.00	0.00	0.00
2	238	-0	-47	-0	-0	0	-8	1	0.00	0.00	0.00
3	238	-0	-46	-0	-0	0	-8	1	0.00	0.00	0.00
4	238	-0	-46	-0	-0	0	-7	1	0.00	0.00	0.00
5	238	-0	-51	-0	-0	0	-12	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1J	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1L	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1N	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67

1P	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'=	67
2	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9347	--	0.00	--	Snell. 'zx'=	67
3	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9362	--	0.00	--	Snell. 'zx'=	67
4	0	0	-22	1	0.6785	1.0000	1.0000	1.0000	0.9379	--	0.00	--	Snell. 'zx'=	67
5	0	0	18	1	0.6785	1.0000	1.0000	1.0000	0.9158	--	0.00	--	Snell. 'zx'=	67

ASTA NUM. 12 NI 39 NF 32 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	26	0	0	0	6	1	0.00	0.00	0.00	
1B	0	-0	45	0	0	0	-17	1	0.00	0.00	0.00	
1C	0	-0	26	-0	0	-0	6	1	0.00	0.00	0.00	
1D	0	-0	45	-0	0	-0	-17	1	0.00	0.00	0.00	
1E	0	-0	26	0	0	0	6	1	0.00	0.00	0.00	
1F	0	-0	45	0	0	0	-17	1	0.00	0.00	0.00	
1G	0	-0	26	-0	0	-0	6	1	0.00	0.00	0.00	
1H	0	-0	45	-0	0	-0	-17	1	0.00	0.00	0.00	
1I	0	-0	17	0	0	0	20	1	0.00	0.00	0.00	
1J	0	-0	54	0	0	0	-31	1	0.00	0.00	0.00	
1K	0	-0	17	-0	0	-0	20	1	0.00	0.00	0.00	
1L	0	-0	54	-0	0	-0	-31	1	0.00	0.00	0.00	
1M	0	-0	17	0	0	0	20	1	0.00	0.00	0.00	
1N	0	-0	54	0	0	0	-31	1	0.00	0.00	0.00	
1O	0	-0	17	-0	0	-0	20	1	0.00	0.00	0.00	
1P	0	-0	54	-0	0	-0	-31	1	0.00	0.00	0.00	
2	0	-0	47	0	0	0	-8	1	0.00	0.00	0.00	
3	0	-0	46	0	0	0	-8	1	0.00	0.00	0.00	
4	0	-0	46	0	0	0	-7	1	0.00	0.00	0.00	
5	0	-0	58	-0	0	-0	-30	1	0.00	0.00	0.00	
1A	119	-0	-15	0	0	0	12	1	0.00	0.00	0.00	
1B	119	-0	5	0	0	0	13	1	0.00	0.00	0.00	
1C	119	-0	-15	-0	0	0	12	1	0.00	0.00	0.00	
1D	119	-0	5	-0	0	0	13	1	0.00	0.00	0.00	
1E	119	-0	-15	0	0	0	12	1	0.00	0.00	0.00	
1F	119	-0	5	0	0	0	13	1	0.00	0.00	0.00	
1G	119	-0	-15	-0	0	0	12	1	0.00	0.00	0.00	
1H	119	-0	5	-0	0	0	13	1	0.00	0.00	0.00	
1I	119	-0	-23	0	0	0	16	1	0.00	0.00	0.00	
1J	119	-0	14	0	0	0	10	1	0.00	0.00	0.00	
1K	119	-0	-23	-0	0	0	16	1	0.00	0.00	0.00	
1L	119	-0	14	-0	0	0	10	1	0.00	0.00	0.00	
1M	119	-0	-23	0	0	0	16	1	0.00	0.00	0.00	
1N	119	-0	14	0	0	0	10	1	0.00	0.00	0.00	
1O	119	-0	-23	-0	0	0	16	1	0.00	0.00	0.00	
1P	119	-0	14	-0	0	0	10	1	0.00	0.00	0.00	
2	119	-0	-5	0	0	0	17	1	0.00	0.00	0.00	
3	119	-0	-6	0	0	0	17	1	0.00	0.00	0.00	
4	119	-0	-6	0	0	0	16	1	0.00	0.00	0.00	
5	119	-0	6	-0	0	0	8	1	0.00	0.00	0.00	
1A	238	-0	-55	0	0	-0	-29	1	0.00	0.00	0.00	
1B	238	-0	-35	0	0	-0	-4	1	0.00	0.00	0.00	
1C	238	-0	-55	-0	0	0	-29	1	0.00	0.00	0.00	
1D	238	-0	-35	-0	0	0	-4	1	0.00	0.00	0.00	
1E	238	-0	-55	0	0	-0	-29	1	0.00	0.00	0.00	

1F	238	-0	-35	0	0	-0	-4	1	0.00	0.00	0.00
1G	238	-0	-55	-0	0	0	-29	1	0.00	0.00	0.00
1H	238	-0	-35	-0	0	0	-4	1	0.00	0.00	0.00
1I	238	-0	-63	0	0	-0	-36	1	0.00	0.00	0.01
1J	238	-0	-26	0	0	-0	2	1	0.00	0.00	0.00
1K	238	-0	-63	-0	0	0	-36	1	0.00	0.00	0.01
1L	238	-0	-26	-0	0	0	2	1	0.00	0.00	0.00
1M	238	-0	-63	0	0	-0	-36	1	0.00	0.00	0.01
1N	238	-0	-26	0	0	-0	2	1	0.00	0.00	0.00
1O	238	-0	-63	-0	0	0	-36	1	0.00	0.00	0.01
1P	238	-0	-26	-0	0	0	2	1	0.00	0.00	0.00
2	238	-0	-58	0	0	-0	-21	1	0.00	0.00	0.00
3	238	-0	-58	0	0	-0	-21	1	0.00	0.00	0.00
4	238	-0	-59	0	0	-0	-22	1	0.00	0.00	0.00
5	238	-0	-47	-0	0	0	-17	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-29	1	0.6785	1.0000	1.0000	1.0000	0.9591	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9400	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1K	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1M	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
1O	0	0	-36	1	0.6785	1.0000	1.0000	1.0000	0.9690	--	0.01	--	Snell. 'zx'= 67
1P	0	0	-31	1	0.6785	1.0000	1.0000	1.0000	0.9544	--	0.00	--	Snell. 'zx'= 67
2	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9347	--	0.00	--	Snell. 'zx'= 67
3	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9362	--	0.00	--	Snell. 'zx'= 67
4	0	0	-22	1	0.6785	1.0000	1.0000	1.0000	0.9379	--	0.00	--	Snell. 'zx'= 67
5	0	0	-30	1	0.6785	1.0000	1.0000	1.0000	0.9267	--	0.00	--	Snell. 'zx'= 67

ASTA NUM. 13 NI 31 NF 24 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--	----------			----------			------	----------			
	cm	daN			daN*m							
1A	0	-0	36	0	-0	0	-8	1	0.00	0.00	0.00	
1B	0	-0	50	0	-0	0	-23	1	0.00	0.00	0.00	
1C	0	-0	36	-0	-0	-0	-8	1	0.00	0.00	0.00	
1D	0	-0	50	-0	-0	-0	-23	1	0.00	0.00	0.00	
1E	0	-0	36	0	-0	0	-8	1	0.00	0.00	0.00	

1F	0	-0	50	0	-0	0	-23	1	0.00	0.00	0.00
1G	0	-0	36	-0	-0	-0	-8	1	0.00	0.00	0.00
1H	0	-0	50	-0	-0	-0	-23	1	0.00	0.00	0.00
1I	0	-0	21	0	-0	0	6	1	0.00	0.00	0.00
1J	0	-0	65	0	-0	0	-37	1	0.00	0.00	0.01
1K	0	-0	21	-0	-0	-0	6	1	0.00	0.00	0.00
1L	0	-0	65	-0	-0	-0	-37	1	0.00	0.00	0.01
1M	0	-0	21	0	-0	0	6	1	0.00	0.00	0.00
1N	0	-0	65	0	-0	0	-37	1	0.00	0.00	0.01
1O	0	-0	21	-0	-0	-0	6	1	0.00	0.00	0.00
1P	0	-0	65	-0	-0	-0	-37	1	0.00	0.00	0.01
2	0	-0	55	-0	-0	0	-19	1	0.00	0.00	0.00
3	0	-0	56	-0	-0	0	-20	1	0.00	0.00	0.00
4	0	-0	56	-0	-0	0	-21	1	0.00	0.00	0.00
5	0	-0	51	0	-0	0	-14	1	0.00	0.00	0.00
1A	119	-0	-4	0	-0	0	10	1	0.00	0.00	0.00
1B	119	-0	10	0	-0	0	13	1	0.00	0.00	0.00
1C	119	-0	-4	-0	-0	0	10	1	0.00	0.00	0.00
1D	119	-0	10	-0	-0	0	13	1	0.00	0.00	0.00
1E	119	-0	-4	0	-0	0	10	1	0.00	0.00	0.00
1F	119	-0	10	0	-0	0	13	1	0.00	0.00	0.00
1G	119	-0	-4	-0	-0	0	10	1	0.00	0.00	0.00
1H	119	-0	10	-0	-0	0	13	1	0.00	0.00	0.00
1I	119	-0	-19	0	-0	0	7	1	0.00	0.00	0.00
1J	119	-0	25	0	-0	0	17	1	0.00	0.00	0.00
1K	119	-0	-19	-0	-0	0	7	1	0.00	0.00	0.00
1L	119	-0	25	-0	-0	0	17	1	0.00	0.00	0.00
1M	119	-0	-19	0	-0	0	7	1	0.00	0.00	0.00
1N	119	-0	25	0	-0	0	17	1	0.00	0.00	0.00
1O	119	-0	-19	-0	-0	0	7	1	0.00	0.00	0.00
1P	119	-0	25	-0	-0	0	17	1	0.00	0.00	0.00
2	119	-0	3	-0	-0	0	15	1	0.00	0.00	0.00
3	119	-0	3	-0	-0	0	15	1	0.00	0.00	0.00
4	119	-0	4	-0	-0	0	15	1	0.00	0.00	0.00
5	119	-0	-1	0	-0	0	16	1	0.00	0.00	0.00
1A	238	-0	-45	0	-0	-0	-19	1	0.00	0.00	0.00
1B	238	-0	-30	0	-0	-0	1	1	0.00	0.00	0.00
1C	238	-0	-45	-0	-0	0	-19	1	0.00	0.00	0.00
1D	238	-0	-30	-0	-0	0	1	1	0.00	0.00	0.00
1E	238	-0	-45	0	-0	-0	-19	1	0.00	0.00	0.00
1F	238	-0	-30	0	-0	-0	1	1	0.00	0.00	0.00
1G	238	-0	-45	-0	-0	0	-19	1	0.00	0.00	0.00
1H	238	-0	-30	-0	-0	0	1	1	0.00	0.00	0.00
1I	238	-0	-60	0	-0	-0	-40	1	0.00	0.00	0.01
1J	238	-0	-15	0	-0	-0	22	1	0.00	0.00	0.00
1K	238	-0	-60	-0	-0	0	-40	1	0.00	0.00	0.01
1L	238	-0	-15	-0	-0	0	22	1	0.00	0.00	0.00
1M	238	-0	-60	0	-0	-0	-40	1	0.00	0.00	0.01
1N	238	-0	-15	0	-0	-0	22	1	0.00	0.00	0.00
1O	238	-0	-60	-0	-0	0	-40	1	0.00	0.00	0.01
1P	238	-0	-15	-0	-0	0	22	1	0.00	0.00	0.00
2	238	-0	-49	-0	-0	0	-12	1	0.00	0.00	0.00
3	238	-0	-49	-0	-0	0	-12	1	0.00	0.00	0.00
4	238	-0	-48	-0	-0	0	-11	1	0.00	0.00	0.00
5	238	-0	-54	0	-0	0	-17	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	--------											
	daN	daN*m											
1A	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9324	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9533	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9324	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9533	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9324	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9533	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9324	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9533	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-40	1	0.6785	1.0000	1.0000	1.0000	0.9574	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9697	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-40	1	0.6785	1.0000	1.0000	1.0000	0.9574	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9697	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-40	1	0.6785	1.0000	1.0000	1.0000	0.9574	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9697	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-40	1	0.6785	1.0000	1.0000	1.0000	0.9574	--	0.01	--	Snell. 'zx'= 67
1P	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9697	--	0.01	--	Snell. 'zx'= 67
2	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9232	--	0.00	--	Snell. 'zx'= 67
3	0	0	-20	1	0.6785	1.0000	1.0000	1.0000	0.9252	--	0.00	--	Snell. 'zx'= 67
4	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9270	--	0.00	--	Snell. 'zx'= 67
5	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9149	--	0.00	--	Snell. 'zx'= 67

ASTA NUM. 14 NI 40 NF 31 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--	----------			----------			------	----------			
	cm	daN			daN*m							
1A	0	-0	30	0	0	0	1	1	0.00	0.00	0.00	
1B	0	-0	45	0	0	0	-19	1	0.00	0.00	0.00	
1C	0	-0	30	-0	0	-0	1	1	0.00	0.00	0.00	
1D	0	-0	45	-0	0	-0	-19	1	0.00	0.00	0.00	
1E	0	-0	30	0	0	0	1	1	0.00	0.00	0.00	
1F	0	-0	45	0	0	0	-19	1	0.00	0.00	0.00	
1G	0	-0	30	-0	0	-0	1	1	0.00	0.00	0.00	
1H	0	-0	45	-0	0	-0	-19	1	0.00	0.00	0.00	
1I	0	-0	15	0	0	0	22	1	0.00	0.00	0.00	
1J	0	-0	60	0	0	0	-40	1	0.00	0.00	0.01	
1K	0	-0	15	-0	0	-0	22	1	0.00	0.00	0.00	
1L	0	-0	60	-0	0	-0	-40	1	0.00	0.00	0.01	
1M	0	-0	15	0	0	0	22	1	0.00	0.00	0.00	
1N	0	-0	60	0	0	0	-40	1	0.00	0.00	0.01	
1O	0	-0	15	-0	0	-0	22	1	0.00	0.00	0.00	
1P	0	-0	60	-0	0	-0	-40	1	0.00	0.00	0.01	
2	0	-0	49	0	0	0	-12	1	0.00	0.00	0.00	
3	0	-0	49	0	0	0	-12	1	0.00	0.00	0.00	
4	0	-0	48	0	0	0	-11	1	0.00	0.00	0.00	
5	0	-0	55	-0	0	-0	-25	1	0.00	0.00	0.00	
1A	119	-0	-10	0	0	0	13	1	0.00	0.00	0.00	
1B	119	-0	4	0	0	0	10	1	0.00	0.00	0.00	
1C	119	-0	-10	-0	0	0	13	1	0.00	0.00	0.00	
1D	119	-0	4	-0	0	0	10	1	0.00	0.00	0.00	
1E	119	-0	-10	0	0	0	13	1	0.00	0.00	0.00	

1F	119	-0	4	0	0	0	10	1	0.00	0.00	0.00
1G	119	-0	-10	-0	0	0	13	1	0.00	0.00	0.00
1H	119	-0	4	-0	0	0	10	1	0.00	0.00	0.00
1I	119	-0	-25	0	0	0	17	1	0.00	0.00	0.00
1J	119	-0	19	0	0	0	7	1	0.00	0.00	0.00
1K	119	-0	-25	-0	0	0	17	1	0.00	0.00	0.00
1L	119	-0	19	-0	0	0	7	1	0.00	0.00	0.00
1M	119	-0	-25	0	0	0	17	1	0.00	0.00	0.00
1N	119	-0	19	0	0	0	7	1	0.00	0.00	0.00
1O	119	-0	-25	-0	0	0	17	1	0.00	0.00	0.00
1P	119	-0	19	-0	0	0	7	1	0.00	0.00	0.00
2	119	-0	-3	0	0	0	15	1	0.00	0.00	0.00
3	119	-0	-3	0	0	0	15	1	0.00	0.00	0.00
4	119	-0	-4	0	0	0	15	1	0.00	0.00	0.00
5	119	-0	3	-0	0	0	9	1	0.00	0.00	0.00
1A	238	-0	-50	0	0	-0	-23	1	0.00	0.00	0.00
1B	238	-0	-36	0	0	-0	-8	1	0.00	0.00	0.00
1C	238	-0	-50	-0	0	0	-23	1	0.00	0.00	0.00
1D	238	-0	-36	-0	0	0	-8	1	0.00	0.00	0.00
1E	238	-0	-50	0	0	-0	-23	1	0.00	0.00	0.00
1F	238	-0	-36	0	0	-0	-8	1	0.00	0.00	0.00
1G	238	-0	-50	-0	0	0	-23	1	0.00	0.00	0.00
1H	238	-0	-36	-0	0	0	-8	1	0.00	0.00	0.00
1I	238	-0	-65	0	0	-0	-37	1	0.00	0.00	0.01
1J	238	-0	-21	0	0	-0	6	1	0.00	0.00	0.00
1K	238	-0	-65	-0	0	0	-37	1	0.00	0.00	0.01
1L	238	-0	-21	-0	0	0	6	1	0.00	0.00	0.00
1M	238	-0	-65	0	0	-0	-37	1	0.00	0.00	0.01
1N	238	-0	-21	0	0	-0	6	1	0.00	0.00	0.00
1O	238	-0	-65	-0	0	0	-37	1	0.00	0.00	0.01
1P	238	-0	-21	-0	0	0	6	1	0.00	0.00	0.00
2	238	-0	-55	0	0	0	-19	1	0.00	0.00	0.00
3	238	-0	-56	0	0	0	-20	1	0.00	0.00	0.00
4	238	-0	-56	0	0	0	-21	1	0.00	0.00	0.00
5	238	-0	-49	-0	0	0	-18	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9533	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9324	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9533	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9324	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9533	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9324	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-23	1	0.6785	1.0000	1.0000	1.0000	0.9533	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9324	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9697	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-40	1	0.6785	1.0000	1.0000	1.0000	0.9574	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9697	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-40	1	0.6785	1.0000	1.0000	1.0000	0.9574	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9697	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-40	1	0.6785	1.0000	1.0000	1.0000	0.9574	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9697	--	0.01	--	Snell. 'zx'= 67

1P	0	0	-40	1	0.6785	1.0000	1.0000	1.0000	0.9574	--	0.01	--	Snell. 'zx'=	67
2	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9232	--	0.00	--	Snell. 'zx'=	67
3	0	0	-20	1	0.6785	1.0000	1.0000	1.0000	0.9252	--	0.00	--	Snell. 'zx'=	67
4	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9270	--	0.00	--	Snell. 'zx'=	67
5	0	0	-25	1	0.6785	1.0000	1.0000	1.0000	0.9193	--	0.00	--	Snell. 'zx'=	67

ASTA NUM. 15 NI 30 NF 23 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	34	0	0	0	-6	1	0.00	0.00	0.00	
1B	0	-0	50	0	0	0	-21	1	0.00	0.00	0.00	
1C	0	-0	34	-0	0	-0	-6	1	0.00	0.00	0.00	
1D	0	-0	50	-0	0	-0	-21	1	0.00	0.00	0.00	
1E	0	-0	34	0	0	0	-6	1	0.00	0.00	0.00	
1F	0	-0	50	0	0	0	-21	1	0.00	0.00	0.00	
1G	0	-0	34	-0	0	-0	-6	1	0.00	0.00	0.00	
1H	0	-0	50	-0	0	-0	-21	1	0.00	0.00	0.00	
1I	0	-0	17	0	0	0	10	1	0.00	0.00	0.00	
1J	0	-0	66	0	0	0	-37	1	0.00	0.00	0.01	
1K	0	-0	17	-0	0	-0	10	1	0.00	0.00	0.00	
1L	0	-0	66	-0	0	-0	-37	1	0.00	0.00	0.01	
1M	0	-0	17	0	0	0	10	1	0.00	0.00	0.00	
1N	0	-0	66	0	0	0	-37	1	0.00	0.00	0.01	
1O	0	-0	17	-0	0	-0	10	1	0.00	0.00	0.00	
1P	0	-0	66	-0	0	-0	-37	1	0.00	0.00	0.01	
2	0	-0	53	-0	0	0	-16	1	0.00	0.00	0.00	
3	0	-0	54	-0	0	0	-17	1	0.00	0.00	0.00	
4	0	-0	55	-0	0	0	-18	1	0.00	0.00	0.00	
5	0	-0	48	0	0	0	-10	1	0.00	0.00	0.00	
1A	119	-0	-6	0	0	0	11	1	0.00	0.00	0.00	
1B	119	-0	9	0	0	0	14	1	0.00	0.00	0.00	
1C	119	-0	-6	-0	0	0	11	1	0.00	0.00	0.00	
1D	119	-0	9	-0	0	0	14	1	0.00	0.00	0.00	
1E	119	-0	-6	0	0	0	11	1	0.00	0.00	0.00	
1F	119	-0	9	0	0	0	14	1	0.00	0.00	0.00	
1G	119	-0	-6	-0	0	0	11	1	0.00	0.00	0.00	
1H	119	-0	9	-0	0	0	14	1	0.00	0.00	0.00	
1I	119	-0	-23	0	0	0	7	1	0.00	0.00	0.00	
1J	119	-0	26	0	0	0	18	1	0.00	0.00	0.00	
1K	119	-0	-23	-0	0	0	7	1	0.00	0.00	0.00	
1L	119	-0	26	-0	0	0	18	1	0.00	0.00	0.00	
1M	119	-0	-23	0	0	0	7	1	0.00	0.00	0.00	
1N	119	-0	26	0	0	0	18	1	0.00	0.00	0.00	
1O	119	-0	-23	-0	0	0	7	1	0.00	0.00	0.00	
1P	119	-0	26	-0	0	0	18	1	0.00	0.00	0.00	
2	119	-0	1	-0	0	0	16	1	0.00	0.00	0.00	
3	119	-0	2	-0	0	0	16	1	0.00	0.00	0.00	
4	119	-0	2	-0	0	0	16	1	0.00	0.00	0.00	
5	119	-0	-4	0	0	0	17	1	0.00	0.00	0.00	
1A	238	-0	-46	0	0	-0	-21	1	0.00	0.00	0.00	
1B	238	-0	-31	0	0	-0	1	1	0.00	0.00	0.00	
1C	238	-0	-46	-0	0	0	-21	1	0.00	0.00	0.00	
1D	238	-0	-31	-0	0	0	1	1	0.00	0.00	0.00	
1E	238	-0	-46	0	0	-0	-21	1	0.00	0.00	0.00	

1F	238	-0	-31	0	0	-0	1	1	0.00	0.00	0.00
1G	238	-0	-46	-0	0	0	-21	1	0.00	0.00	0.00
1H	238	-0	-31	-0	0	0	1	1	0.00	0.00	0.00
1I	238	-0	-63	0	0	-0	-44	1	0.00	0.00	0.01
1J	238	-0	-14	0	0	-0	25	1	0.00	0.00	0.00
1K	238	-0	-63	-0	0	0	-44	1	0.00	0.00	0.01
1L	238	-0	-14	-0	0	0	25	1	0.00	0.00	0.00
1M	238	-0	-63	0	0	-0	-44	1	0.00	0.00	0.01
1N	238	-0	-14	0	0	-0	25	1	0.00	0.00	0.00
1O	238	-0	-63	-0	0	0	-44	1	0.00	0.00	0.01
1P	238	-0	-14	-0	0	0	25	1	0.00	0.00	0.00
2	238	-0	-51	-0	0	0	-14	1	0.00	0.00	0.00
3	238	-0	-50	-0	0	0	-13	1	0.00	0.00	0.00
4	238	-0	-50	-0	0	0	-12	1	0.00	0.00	0.00
5	238	-0	-56	0	0	0	-19	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1P	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
2	0	0	-16	1	0.6785	1.0000	1.0000	1.0000	0.9141	--	0.00	--	Snell. 'zx'= 67
3	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9175	--	0.00	--	Snell. 'zx'= 67
4	0	0	-18	1	0.6785	1.0000	1.0000	1.0000	0.9211	--	0.00	--	Snell. 'zx'= 67
5	0	0	-19	1	0.6785	1.0000	1.0000	1.0000	0.9282	--	0.00	--	Snell. 'zx'= 67

ASTA NUM. 16 NI 41 NF 30 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--	----------			----------			------	----------			
	cm	daN			daN*m							
1A	0	-0	31	0	-0	0	1	1	0.00	0.00	0.00	
1B	0	-0	46	0	-0	0	-21	1	0.00	0.00	0.00	
1C	0	-0	31	-0	-0	-0	1	1	0.00	0.00	0.00	
1D	0	-0	46	-0	-0	-0	-21	1	0.00	0.00	0.00	
1E	0	-0	31	0	-0	0	1	1	0.00	0.00	0.00	

1F	0	-0	46	0	-0	0	-21	1	0.00	0.00	0.00
1G	0	-0	31	-0	-0	-0	1	1	0.00	0.00	0.00
1H	0	-0	46	-0	-0	-0	-21	1	0.00	0.00	0.00
1I	0	-0	14	0	-0	0	25	1	0.00	0.00	0.00
1J	0	-0	63	0	-0	0	-44	1	0.00	0.00	0.01
1K	0	-0	14	-0	-0	-0	25	1	0.00	0.00	0.00
1L	0	-0	63	-0	-0	-0	-44	1	0.00	0.00	0.01
1M	0	-0	14	0	-0	0	25	1	0.00	0.00	0.00
1N	0	-0	63	0	-0	0	-44	1	0.00	0.00	0.01
1O	0	-0	14	-0	-0	-0	25	1	0.00	0.00	0.00
1P	0	-0	63	-0	-0	-0	-44	1	0.00	0.00	0.01
2	0	-0	51	0	-0	0	-14	1	0.00	0.00	0.00
3	0	-0	50	0	-0	0	-13	1	0.00	0.00	0.00
4	0	-0	50	0	-0	0	-12	1	0.00	0.00	0.00
5	0	-0	60	-0	-0	-0	-33	1	0.00	0.00	0.01
1A	119	-0	-9	0	-0	0	14	1	0.00	0.00	0.00
1B	119	-0	6	0	-0	0	11	1	0.00	0.00	0.00
1C	119	-0	-9	-0	-0	0	14	1	0.00	0.00	0.00
1D	119	-0	6	-0	-0	0	11	1	0.00	0.00	0.00
1E	119	-0	-9	0	-0	0	14	1	0.00	0.00	0.00
1F	119	-0	6	0	-0	0	11	1	0.00	0.00	0.00
1G	119	-0	-9	-0	-0	0	14	1	0.00	0.00	0.00
1H	119	-0	6	-0	-0	0	11	1	0.00	0.00	0.00
1I	119	-0	-26	0	-0	0	18	1	0.00	0.00	0.00
1J	119	-0	23	0	-0	0	7	1	0.00	0.00	0.00
1K	119	-0	-26	-0	-0	0	18	1	0.00	0.00	0.00
1L	119	-0	23	-0	-0	0	7	1	0.00	0.00	0.00
1M	119	-0	-26	0	-0	0	18	1	0.00	0.00	0.00
1N	119	-0	23	0	-0	0	7	1	0.00	0.00	0.00
1O	119	-0	-26	-0	-0	0	18	1	0.00	0.00	0.00
1P	119	-0	23	-0	-0	0	7	1	0.00	0.00	0.00
2	119	-0	-1	0	-0	0	16	1	0.00	0.00	0.00
3	119	-0	-2	0	-0	0	16	1	0.00	0.00	0.00
4	119	-0	-2	0	-0	0	16	1	0.00	0.00	0.00
5	119	-0	8	-0	-0	0	7	1	0.00	0.00	0.00
1A	238	-0	-50	0	-0	-0	-21	1	0.00	0.00	0.00
1B	238	-0	-34	0	-0	-0	-6	1	0.00	0.00	0.00
1C	238	-0	-50	-0	-0	0	-21	1	0.00	0.00	0.00
1D	238	-0	-34	-0	-0	0	-6	1	0.00	0.00	0.00
1E	238	-0	-50	0	-0	-0	-21	1	0.00	0.00	0.00
1F	238	-0	-34	0	-0	-0	-6	1	0.00	0.00	0.00
1G	238	-0	-50	-0	-0	0	-21	1	0.00	0.00	0.00
1H	238	-0	-34	-0	-0	0	-6	1	0.00	0.00	0.00
1I	238	-0	-66	0	-0	-0	-37	1	0.00	0.00	0.01
1J	238	-0	-17	0	-0	-0	10	1	0.00	0.00	0.00
1K	238	-0	-66	-0	-0	0	-37	1	0.00	0.00	0.01
1L	238	-0	-17	-0	-0	0	10	1	0.00	0.00	0.00
1M	238	-0	-66	0	-0	-0	-37	1	0.00	0.00	0.01
1N	238	-0	-17	0	-0	-0	10	1	0.00	0.00	0.00
1O	238	-0	-66	-0	-0	0	-37	1	0.00	0.00	0.01
1P	238	-0	-17	-0	-0	0	10	1	0.00	0.00	0.00
2	238	-0	-53	0	-0	0	-16	1	0.00	0.00	0.00
3	238	-0	-54	0	-0	0	-17	1	0.00	0.00	0.00
4	238	-0	-55	0	-0	0	-18	1	0.00	0.00	0.00
5	238	-0	-44	-0	-0	0	-14	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	--	--										
	daN	daN*m											
1A	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1P	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
2	0	0	-16	1	0.6785	1.0000	1.0000	1.0000	0.9141	--	0.00	--	Snell. 'zx'= 67
3	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9175	--	0.00	--	Snell. 'zx'= 67
4	0	0	-18	1	0.6785	1.0000	1.0000	1.0000	0.9211	--	0.00	--	Snell. 'zx'= 67
5	0	0	-33	1	0.6785	1.0000	1.0000	1.0000	0.9330	--	0.01	--	Snell. 'zx'= 67

ASTA NUM. 17 NI 35 NF 28 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--											
	cm	daN			daN*m							
1A	0	-0	34	0	-0	0	-6	1	0.00	0.00	0.00	
1B	0	-0	50	0	-0	0	-21	1	0.00	0.00	0.00	
1C	0	-0	34	-0	-0	-0	-6	1	0.00	0.00	0.00	
1D	0	-0	50	-0	-0	-0	-21	1	0.00	0.00	0.00	
1E	0	-0	34	0	-0	0	-6	1	0.00	0.00	0.00	
1F	0	-0	50	0	-0	0	-21	1	0.00	0.00	0.00	
1G	0	-0	34	-0	-0	-0	-6	1	0.00	0.00	0.00	
1H	0	-0	50	-0	-0	-0	-21	1	0.00	0.00	0.00	
1I	0	-0	17	0	-0	0	10	1	0.00	0.00	0.00	
1J	0	-0	66	0	-0	0	-37	1	0.00	0.00	0.01	
1K	0	-0	17	-0	-0	-0	10	1	0.00	0.00	0.00	
1L	0	-0	66	-0	-0	-0	-37	1	0.00	0.00	0.01	
1M	0	-0	17	0	-0	0	10	1	0.00	0.00	0.00	
1N	0	-0	66	0	-0	0	-37	1	0.00	0.00	0.01	
1O	0	-0	17	-0	-0	-0	10	1	0.00	0.00	0.00	
1P	0	-0	66	-0	-0	-0	-37	1	0.00	0.00	0.01	
2	0	-0	53	-0	-0	0	-16	1	0.00	0.00	0.00	
3	0	-0	54	-0	-0	0	-17	1	0.00	0.00	0.00	
4	0	-0	55	-0	-0	0	-18	1	0.00	0.00	0.00	
5	0	-0	49	0	-0	0	-11	1	0.00	0.00	0.00	
1A	119	-0	-6	0	-0	0	11	1	0.00	0.00	0.00	
1B	119	-0	9	0	-0	0	14	1	0.00	0.00	0.00	
1C	119	-0	-6	-0	-0	0	11	1	0.00	0.00	0.00	
1D	119	-0	9	-0	-0	0	14	1	0.00	0.00	0.00	
1E	119	-0	-6	0	-0	0	11	1	0.00	0.00	0.00	

1F	119	-0	9	0	-0	0	14	1	0.00	0.00	0.00
1G	119	-0	-6	-0	-0	0	11	1	0.00	0.00	0.00
1H	119	-0	9	-0	-0	0	14	1	0.00	0.00	0.00
1I	119	-0	-23	0	-0	0	7	1	0.00	0.00	0.00
1J	119	-0	26	0	-0	0	18	1	0.00	0.00	0.00
1K	119	-0	-23	-0	-0	0	7	1	0.00	0.00	0.00
1L	119	-0	26	-0	-0	0	18	1	0.00	0.00	0.00
1M	119	-0	-23	0	-0	0	7	1	0.00	0.00	0.00
1N	119	-0	26	0	-0	0	18	1	0.00	0.00	0.00
1O	119	-0	-23	-0	-0	0	7	1	0.00	0.00	0.00
1P	119	-0	26	-0	-0	0	18	1	0.00	0.00	0.00
2	119	-0	1	-0	-0	0	16	1	0.00	0.00	0.00
3	119	-0	2	-0	-0	0	16	1	0.00	0.00	0.00
4	119	-0	2	-0	-0	0	16	1	0.00	0.00	0.00
5	119	-0	-3	0	-0	0	17	1	0.00	0.00	0.00
1A	238	-0	-46	0	-0	-0	-21	1	0.00	0.00	0.00
1B	238	-0	-31	0	-0	-0	1	1	0.00	0.00	0.00
1C	238	-0	-46	-0	-0	0	-21	1	0.00	0.00	0.00
1D	238	-0	-31	-0	-0	0	1	1	0.00	0.00	0.00
1E	238	-0	-46	0	-0	-0	-21	1	0.00	0.00	0.00
1F	238	-0	-31	0	-0	-0	1	1	0.00	0.00	0.00
1G	238	-0	-46	-0	-0	0	-21	1	0.00	0.00	0.00
1H	238	-0	-31	-0	-0	0	1	1	0.00	0.00	0.00
1I	238	-0	-63	0	-0	-0	-44	1	0.00	0.00	0.01
1J	238	-0	-14	0	-0	-0	25	1	0.00	0.00	0.00
1K	238	-0	-63	-0	-0	0	-44	1	0.00	0.00	0.01
1L	238	-0	-14	-0	-0	0	25	1	0.00	0.00	0.00
1M	238	-0	-63	0	-0	-0	-44	1	0.00	0.00	0.01
1N	238	-0	-14	0	-0	-0	25	1	0.00	0.00	0.00
1O	238	-0	-63	-0	-0	0	-44	1	0.00	0.00	0.01
1P	238	-0	-14	-0	-0	0	25	1	0.00	0.00	0.00
2	238	-0	-51	-0	-0	0	-14	1	0.00	0.00	0.00
3	238	-0	-50	-0	-0	0	-13	1	0.00	0.00	0.00
4	238	-0	-50	-0	-0	0	-13	1	0.00	0.00	0.00
5	238	-0	-55	0	-0	0	-18	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67

1P	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'=	67
2	0	0	-16	1	0.6785	1.0000	1.0000	1.0000	0.9141	--	0.00	--	Snell. 'zx'=	67
3	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9175	--	0.00	--	Snell. 'zx'=	67
4	0	0	-18	1	0.6785	1.0000	1.0000	1.0000	0.9210	--	0.00	--	Snell. 'zx'=	67
5	0	0	-18	1	0.6785	1.0000	1.0000	1.0000	0.9240	--	0.00	--	Snell. 'zx'=	67

ASTA NUM. 18 NI 36 NF 35 Lungh. 238.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-0	31	0	0	0	1	1	0.00	0.00	0.00	
1B	0	-0	46	0	0	0	-21	1	0.00	0.00	0.00	
1C	0	-0	31	-0	0	-0	1	1	0.00	0.00	0.00	
1D	0	-0	46	-0	0	-0	-21	1	0.00	0.00	0.00	
1E	0	-0	31	0	0	0	1	1	0.00	0.00	0.00	
1F	0	-0	46	0	0	0	-21	1	0.00	0.00	0.00	
1G	0	-0	31	-0	0	-0	1	1	0.00	0.00	0.00	
1H	0	-0	46	-0	0	-0	-21	1	0.00	0.00	0.00	
1I	0	-0	14	0	0	0	25	1	0.00	0.00	0.00	
1J	0	-0	63	0	0	0	-44	1	0.00	0.00	0.01	
1K	0	-0	14	-0	0	-0	25	1	0.00	0.00	0.00	
1L	0	-0	63	-0	0	-0	-44	1	0.00	0.00	0.01	
1M	0	-0	14	0	0	0	25	1	0.00	0.00	0.00	
1N	0	-0	63	0	0	0	-44	1	0.00	0.00	0.01	
1O	0	-0	14	-0	0	-0	25	1	0.00	0.00	0.00	
1P	0	-0	63	-0	0	-0	-44	1	0.00	0.00	0.01	
2	0	-0	51	0	0	0	-14	1	0.00	0.00	0.00	
3	0	-0	50	0	0	0	-13	1	0.00	0.00	0.00	
4	0	-0	50	0	0	0	-13	1	0.00	0.00	0.00	
5	0	-0	61	-0	0	-0	-35	1	0.00	0.00	0.01	
1A	119	-0	-9	0	0	0	14	1	0.00	0.00	0.00	
1B	119	-0	6	0	0	0	11	1	0.00	0.00	0.00	
1C	119	-0	-9	-0	0	0	14	1	0.00	0.00	0.00	
1D	119	-0	6	-0	0	0	11	1	0.00	0.00	0.00	
1E	119	-0	-9	0	0	0	14	1	0.00	0.00	0.00	
1F	119	-0	6	0	0	0	11	1	0.00	0.00	0.00	
1G	119	-0	-9	-0	0	0	14	1	0.00	0.00	0.00	
1H	119	-0	6	-0	0	0	11	1	0.00	0.00	0.00	
1I	119	-0	-26	0	0	0	18	1	0.00	0.00	0.00	
1J	119	-0	23	0	0	0	7	1	0.00	0.00	0.00	
1K	119	-0	-26	-0	0	0	18	1	0.00	0.00	0.00	
1L	119	-0	23	-0	0	0	7	1	0.00	0.00	0.00	
1M	119	-0	-26	0	0	0	18	1	0.00	0.00	0.00	
1N	119	-0	23	0	0	0	7	1	0.00	0.00	0.00	
1O	119	-0	-26	-0	0	0	18	1	0.00	0.00	0.00	
1P	119	-0	23	-0	0	0	7	1	0.00	0.00	0.00	
2	119	-0	-1	0	0	0	16	1	0.00	0.00	0.00	
3	119	-0	-2	0	0	0	16	1	0.00	0.00	0.00	
4	119	-0	-2	0	0	0	16	1	0.00	0.00	0.00	
5	119	-0	9	-0	0	0	7	1	0.00	0.00	0.00	
1A	238	-0	-50	0	0	-0	-21	1	0.00	0.00	0.00	
1B	238	-0	-34	0	0	-0	-6	1	0.00	0.00	0.00	
1C	238	-0	-50	-0	0	0	-21	1	0.00	0.00	0.00	
1D	238	-0	-34	-0	0	0	-6	1	0.00	0.00	0.00	
1E	238	-0	-50	0	0	-0	-21	1	0.00	0.00	0.00	

1F	238	-0	-34	0	0	-0	-6	1	0.00	0.00	0.00
1G	238	-0	-50	-0	0	0	-21	1	0.00	0.00	0.00
1H	238	-0	-34	-0	0	0	-6	1	0.00	0.00	0.00
1I	238	-0	-66	0	0	-0	-37	1	0.00	0.00	0.01
1J	238	-0	-17	0	0	-0	10	1	0.00	0.00	0.00
1K	238	-0	-66	-0	0	0	-37	1	0.00	0.00	0.01
1L	238	-0	-17	-0	0	0	10	1	0.00	0.00	0.00
1M	238	-0	-66	0	0	-0	-37	1	0.00	0.00	0.01
1N	238	-0	-17	0	0	-0	10	1	0.00	0.00	0.00
1O	238	-0	-66	-0	0	0	-37	1	0.00	0.00	0.01
1P	238	-0	-17	-0	0	0	10	1	0.00	0.00	0.00
2	238	-0	-53	0	0	0	-16	1	0.00	0.00	0.00
3	238	-0	-54	0	0	0	-17	1	0.00	0.00	0.00
4	238	-0	-55	0	0	0	-18	1	0.00	0.00	0.00
5	238	-0	-43	-0	0	0	-13	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1B	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1C	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1D	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1E	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1F	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1G	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9530	--	0.00	--	Snell. 'zx'= 67
1H	0	0	-21	1	0.6785	1.0000	1.0000	1.0000	0.9387	--	0.00	--	Snell. 'zx'= 67
1I	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1J	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1K	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1L	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1M	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1N	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
1O	0	0	-37	1	0.6785	1.0000	1.0000	1.0000	0.9704	--	0.01	--	Snell. 'zx'= 67
1P	0	0	-44	1	0.6785	1.0000	1.0000	1.0000	0.9601	--	0.01	--	Snell. 'zx'= 67
2	0	0	-16	1	0.6785	1.0000	1.0000	1.0000	0.9141	--	0.00	--	Snell. 'zx'= 67
3	0	0	-17	1	0.6785	1.0000	1.0000	1.0000	0.9175	--	0.00	--	Snell. 'zx'= 67
4	0	0	-18	1	0.6785	1.0000	1.0000	1.0000	0.9210	--	0.00	--	Snell. 'zx'= 67
5	0	0	-35	1	0.6785	1.0000	1.0000	1.0000	0.9350	--	0.01	--	Snell. 'zx'= 67

ASTA NUM. 19 NI 79 NF 28 Lungh. 227.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--	----------			----------			------	----------			
	cm	daN			daN*m							
1A	0	-0	625	0	-0	0	-135	1	0.03	0.00	0.02	
1B	0	-0	777	0	-0	0	-300	1	0.04	0.00	0.05	
1C	0	-0	625	-0	-0	-0	-135	1	0.03	0.00	0.02	
1D	0	-0	777	-0	-0	-0	-300	1	0.04	0.00	0.05	
1E	0	-0	625	0	-0	0	-135	1	0.03	0.00	0.02	

1F	0	-0	777	0	-0	0	-300	1	0.04	0.00	0.05
1G	0	-0	625	-0	-0	-0	-135	1	0.03	0.00	0.02
1H	0	-0	777	-0	-0	-0	-300	1	0.04	0.00	0.05
1I	0	-0	675	-0	-0	-0	-190	1	0.03	0.00	0.03
1J	0	-0	727	-0	-0	-0	-245	1	0.04	0.00	0.04
1K	0	-0	675	-0	-0	-0	-190	1	0.03	0.00	0.03
1L	0	-0	727	-0	-0	-0	-245	1	0.04	0.00	0.04
1M	0	-0	675	-0	-0	-0	-190	1	0.03	0.00	0.03
1N	0	-0	727	-0	-0	-0	-245	1	0.04	0.00	0.04
1O	0	-0	675	-0	-0	-0	-190	1	0.03	0.00	0.03
1P	0	-0	727	-0	-0	-0	-245	1	0.04	0.00	0.04
2	0	-0	1053	-0	-0	-0	-327	1	0.05	0.00	0.05
3	0	-0	958	-0	-0	-0	-297	1	0.05	0.00	0.05
4	0	-0	860	-0	-0	-0	-266	1	0.04	0.00	0.04
5	0	-0	861	-0	-0	-0	-267	1	0.04	0.00	0.04
1A	114	-0	-116	0	-0	-0	153	1	0.01	0.00	0.02
1B	114	-0	37	0	-0	-0	162	1	0.00	0.00	0.02
1C	114	-0	-116	-0	-0	-0	153	1	0.01	0.00	0.02
1D	114	-0	37	-0	-0	-0	162	1	0.00	0.00	0.02
1E	114	-0	-116	0	-0	-0	153	1	0.01	0.00	0.02
1F	114	-0	37	0	-0	-0	162	1	0.00	0.00	0.02
1G	114	-0	-116	-0	-0	-0	153	1	0.01	0.00	0.02
1H	114	-0	37	-0	-0	-0	162	1	0.00	0.00	0.02
1I	114	-0	-65	-0	-0	-0	156	1	0.00	0.00	0.02
1J	114	-0	-14	-0	-0	-0	159	1	0.00	0.00	0.02
1K	114	-0	-65	-0	-0	-0	156	1	0.00	0.00	0.02
1L	114	-0	-14	-0	-0	-0	159	1	0.00	0.00	0.02
1M	114	-0	-65	-0	-0	-0	156	1	0.00	0.00	0.02
1N	114	-0	-14	-0	-0	-0	159	1	0.00	0.00	0.02
1O	114	-0	-65	-0	-0	-0	156	1	0.00	0.00	0.02
1P	114	-0	-14	-0	-0	-0	159	1	0.00	0.00	0.02
2	114	-0	-59	-0	-0	-0	237	1	0.00	0.00	0.04
3	114	-0	-54	-0	-0	-0	215	1	0.00	0.00	0.03
4	114	-0	-50	-0	-0	-0	194	1	0.00	0.00	0.03
5	114	-0	-49	-0	-0	-0	194	1	0.00	0.00	0.03
1A	227	-0	-856	0	-0	-0	-398	1	0.04	0.00	0.06
1B	227	-0	-704	0	-0	-0	-217	1	0.03	0.00	0.03
1C	227	-0	-856	-0	-0	0	-398	1	0.04	0.00	0.06
1D	227	-0	-704	-0	-0	0	-217	1	0.03	0.00	0.03
1E	227	-0	-856	0	-0	-0	-398	1	0.04	0.00	0.06
1F	227	-0	-704	0	-0	-0	-217	1	0.03	0.00	0.03
1G	227	-0	-856	-0	-0	0	-398	1	0.04	0.00	0.06
1H	227	-0	-704	-0	-0	0	-217	1	0.03	0.00	0.03
1I	227	-0	-806	-0	-0	-0	-339	1	0.04	0.00	0.05
1J	227	-0	-754	-0	-0	-0	-276	1	0.04	0.00	0.04
1K	227	-0	-806	-0	-0	0	-339	1	0.04	0.00	0.05
1L	227	-0	-754	-0	-0	0	-276	1	0.04	0.00	0.04
1M	227	-0	-806	-0	-0	-0	-339	1	0.04	0.00	0.05
1N	227	-0	-754	-0	-0	-0	-276	1	0.04	0.00	0.04
1O	227	-0	-806	-0	-0	0	-339	1	0.04	0.00	0.05
1P	227	-0	-754	-0	-0	0	-276	1	0.04	0.00	0.04
2	227	-0	-1172	-0	-0	0	-462	1	0.06	0.00	0.07
3	227	-0	-1065	-0	-0	0	-420	1	0.05	0.00	0.06
4	227	-0	-961	-0	-0	0	-380	1	0.05	0.00	0.06
5	227	-0	-959	-0	-0	0	-379	1	0.05	0.00	0.06

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	--------------											
	daN	daN*m											
1A	0	-0	-398	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.07	--	Snell. 'zx'= 63
1B	0	-0	-300	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.06	--	Snell. 'zx'= 63
1C	0	-0	-398	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.07	--	Snell. 'zx'= 63
1D	0	-0	-300	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.06	--	Snell. 'zx'= 63
1E	0	-0	-398	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.07	--	Snell. 'zx'= 63
1F	0	-0	-300	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.06	--	Snell. 'zx'= 63
1G	0	-0	-398	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.07	--	Snell. 'zx'= 63
1H	0	-0	-300	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.06	--	Snell. 'zx'= 63
1I	0	-0	-339	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.06	--	Snell. 'zx'= 63
1J	0	-0	-276	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.05	--	Snell. 'zx'= 63
1K	0	-0	-339	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.06	--	Snell. 'zx'= 63
1L	0	-0	-276	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.05	--	Snell. 'zx'= 63
1M	0	-0	-339	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.06	--	Snell. 'zx'= 63
1N	0	-0	-276	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.05	--	Snell. 'zx'= 63
1O	0	-0	-339	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.06	--	Snell. 'zx'= 63
1P	0	-0	-276	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.05	--	Snell. 'zx'= 63
2	0	-0	-462	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.09	--	Snell. 'zx'= 63
3	0	-0	-420	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.08	--	Snell. 'zx'= 63
4	0	-0	-380	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.07	--	Snell. 'zx'= 63
5	0	-0	-379	1	0.7009	1.0000	1.0000	1.0000	0.8256	--	0.07	--	Snell. 'zx'= 63

ASTA NUM. 20 NI 26 NF 27 Lungh. 233.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	--	----------			----------			------	----------			
	cm	daN			daN*m							
1A	0	-0	723	0	0	0	-227	1	0.04	0.00	0.03	
1B	0	-0	867	0	0	0	-404	1	0.04	0.00	0.06	
1C	0	-0	723	-0	0	-0	-227	1	0.04	0.00	0.03	
1D	0	-0	867	-0	0	-0	-404	1	0.04	0.00	0.06	
1E	0	-0	723	0	0	0	-227	1	0.04	0.00	0.03	
1F	0	-0	867	0	0	0	-404	1	0.04	0.00	0.06	
1G	0	-0	723	-0	0	-0	-227	1	0.04	0.00	0.03	
1H	0	-0	867	-0	0	-0	-404	1	0.04	0.00	0.06	
1I	0	-0	767	0	0	0	-281	1	0.04	0.00	0.04	
1J	0	-0	823	0	0	0	-350	1	0.04	0.00	0.05	
1K	0	-0	767	0	0	-0	-281	1	0.04	0.00	0.04	
1L	0	-0	823	0	0	-0	-350	1	0.04	0.00	0.05	
1M	0	-0	767	0	0	0	-281	1	0.04	0.00	0.04	
1N	0	-0	823	0	0	0	-350	1	0.04	0.00	0.05	
1O	0	-0	767	0	0	-0	-281	1	0.04	0.00	0.04	
1P	0	-0	823	0	0	-0	-350	1	0.04	0.00	0.05	
2	0	-0	1194	0	0	0	-474	1	0.06	0.00	0.07	
3	0	-0	1085	0	0	0	-431	1	0.05	0.00	0.07	
4	0	-0	975	0	0	0	-385	1	0.05	0.00	0.06	
5	0	-0	976	0	0	0	-386	1	0.05	0.00	0.06	
1A	117	-0	-38	0	0	-0	172	1	0.00	0.00	0.03	
1B	117	-0	107	0	0	-0	163	1	0.01	0.00	0.02	
1C	117	-0	-38	-0	0	-0	172	1	0.00	0.00	0.03	
1D	117	-0	107	-0	0	-0	163	1	0.01	0.00	0.02	
1E	117	-0	-38	0	0	-0	172	1	0.00	0.00	0.03	

1F	117	-0	107	0	0	-0	163	1	0.01	0.00	0.02
1G	117	-0	-38	-0	0	-0	172	1	0.00	0.00	0.03
1H	117	-0	107	-0	0	-0	163	1	0.01	0.00	0.02
1I	117	-0	7	0	0	-0	170	1	0.00	0.00	0.03
1J	117	-0	63	0	0	-0	166	1	0.00	0.00	0.03
1K	117	-0	7	0	0	-0	170	1	0.00	0.00	0.03
1L	117	-0	63	0	0	-0	166	1	0.00	0.00	0.03
1M	117	-0	7	0	0	-0	170	1	0.00	0.00	0.03
1N	117	-0	63	0	0	-0	166	1	0.00	0.00	0.03
1O	117	-0	7	0	0	-0	170	1	0.00	0.00	0.03
1P	117	-0	63	0	0	-0	166	1	0.00	0.00	0.03
2	117	-0	52	0	0	-0	252	1	0.00	0.00	0.04
3	117	-0	47	0	0	-0	229	1	0.00	0.00	0.03
4	117	-0	41	0	0	-0	206	1	0.00	0.00	0.03
5	117	-0	41	0	0	-0	206	1	0.00	0.00	0.03
1A	233	-0	-798	0	0	-0	-315	1	0.04	0.00	0.05
1B	233	-0	-653	0	0	-0	-155	1	0.03	0.00	0.02
1C	233	-0	-798	-0	0	0	-315	1	0.04	0.00	0.05
1D	233	-0	-653	-0	0	0	-155	1	0.03	0.00	0.02
1E	233	-0	-798	0	0	-0	-315	1	0.04	0.00	0.05
1F	233	-0	-653	0	0	-0	-155	1	0.03	0.00	0.02
1G	233	-0	-798	-0	0	0	-315	1	0.04	0.00	0.05
1H	233	-0	-653	-0	0	0	-155	1	0.03	0.00	0.02
1I	233	-0	-754	0	0	-0	-266	1	0.04	0.00	0.04
1J	233	-0	-698	0	0	-0	-204	1	0.03	0.00	0.03
1K	233	-0	-754	0	0	-0	-266	1	0.04	0.00	0.04
1L	233	-0	-698	0	0	-0	-204	1	0.03	0.00	0.03
1M	233	-0	-754	0	0	-0	-266	1	0.04	0.00	0.04
1N	233	-0	-698	0	0	-0	-204	1	0.03	0.00	0.03
1O	233	-0	-754	0	0	-0	-266	1	0.04	0.00	0.04
1P	233	-0	-698	0	0	-0	-204	1	0.03	0.00	0.03
2	233	-0	-1090	0	0	-0	-353	1	0.05	0.00	0.05
3	233	-0	-991	0	0	-0	-321	1	0.05	0.00	0.05
4	233	-0	-893	0	0	-0	-290	1	0.04	0.00	0.04
5	233	-0	-893	0	0	-0	-290	1	0.04	0.00	0.04

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	0	-0	-315	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.06	--	Snell. 'zx'= 65
1B	0	-0	-404	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.08	--	Snell. 'zx'= 65
1C	0	-0	-315	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.06	--	Snell. 'zx'= 65
1D	0	-0	-404	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.08	--	Snell. 'zx'= 65
1E	0	-0	-315	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.06	--	Snell. 'zx'= 65
1F	0	-0	-404	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.08	--	Snell. 'zx'= 65
1G	0	-0	-315	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.06	--	Snell. 'zx'= 65
1H	0	-0	-404	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.08	--	Snell. 'zx'= 65
1I	0	-0	-281	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.05	--	Snell. 'zx'= 65
1J	0	-0	-350	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.07	--	Snell. 'zx'= 65
1K	0	-0	-281	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.05	--	Snell. 'zx'= 65
1L	0	-0	-350	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.07	--	Snell. 'zx'= 65
1M	0	-0	-281	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.05	--	Snell. 'zx'= 65
1N	0	-0	-350	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.07	--	Snell. 'zx'= 65
1O	0	-0	-281	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.05	--	Snell. 'zx'= 65

1P	0	-0	-350	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.07	--	Snell. 'zx'= 65
2	0	-0	-474	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.09	--	Snell. 'zx'= 65
3	0	-0	-431	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.08	--	Snell. 'zx'= 65
4	0	-0	-385	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.07	--	Snell. 'zx'= 65
5	0	-0	-386	1	0.6887	1.0000	1.0000	1.0000	0.8211	--	0.07	--	Snell. 'zx'= 65

Elemento: **TRAVE** Metodo di verifica: **NTC 2018**

Gruppo: **3** Descrizione: **Controventi**

Tabella: **Tabella controventi**

Tipo acciaio: **S 275** Beta piano 'yx': **1.000** Beta piano 'zx': **1.000**

Coeff. riduzione dell'area: **0.000** Tipologia sismica: **Senza prescrizioni aggiuntive**

γM0: **1.050** γM1': **1.050** γM1'': **1.050** γM2: **1.250** γrv: **0.000** γM0 Pf: **1.000** γM1 Pf: **1.000**

Tipo collegamento: **bullonato**

ASTA NUM. 1 NI 11 NF 33 Lungh. 276.9 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-3260	13	0	0	0	-5	1	0.00	0.09	0.09	
1B	0	-3260	13	0	0	0	-7	1	0.00	0.09	0.10	
1C	0	-3260	13	-0	0	-0	-5	1	0.00	0.09	0.09	
1D	0	-3260	13	-0	0	-0	-7	1	0.00	0.09	0.10	
1E	0	2722	13	0	0	0	-5	1	0.00	0.07	0.08	
1F	0	2722	13	0	0	0	-7	1	0.00	0.07	0.08	
1G	0	2722	13	-0	0	-0	-5	1	0.00	0.07	0.08	
1H	0	2722	13	-0	0	-0	-7	1	0.00	0.07	0.08	
1I	0	-1167	13	1	0	1	-6	1	0.00	0.03	0.04	
1J	0	-1167	13	1	0	1	-6	1	0.00	0.03	0.04	
1K	0	-1167	13	-1	0	-1	-6	1	0.00	0.03	0.04	
1L	0	-1167	13	-1	0	-1	-6	1	0.00	0.03	0.04	
1M	0	628	13	1	0	1	-6	1	0.00	0.02	0.03	
1N	0	628	13	1	0	1	-6	1	0.00	0.02	0.03	
1O	0	628	13	-1	0	-1	-6	1	0.00	0.02	0.03	
1P	0	628	13	-1	0	-1	-6	1	0.00	0.02	0.03	
2	0	-402	17	-0	0	-0	-8	1	0.00	0.01	0.02	
3	0	-367	17	-0	0	-0	-8	1	0.00	0.01	0.02	
4	0	-264	17	-0	0	-0	-8	1	0.00	0.01	0.02	
5	0	-331	17	-0	0	-0	-8	1	0.00	0.01	0.02	
1A	138	-3252	-0	0	0	0	3	1	0.00	0.09	0.09	
1B	138	-3252	0	0	0	0	2	1	0.00	0.09	0.09	
1C	138	-3252	-0	-0	0	-0	3	1	0.00	0.09	0.09	
1D	138	-3252	0	-0	0	-0	2	1	0.00	0.09	0.09	

1E	138	2730	-0	0	0	0	3	1	0.00	0.07	0.08
1F	138	2730	0	0	0	0	2	1	0.00	0.07	0.08
1G	138	2730	-0	-0	0	-0	3	1	0.00	0.07	0.08
1H	138	2730	0	-0	0	-0	2	1	0.00	0.07	0.08
1I	138	-1158	-0	1	0	0	3	1	0.00	0.03	0.03
1J	138	-1158	0	1	0	0	3	1	0.00	0.03	0.03
1K	138	-1158	-0	-1	0	-0	3	1	0.00	0.03	0.03
1L	138	-1158	0	-1	0	-0	3	1	0.00	0.03	0.03
1M	138	636	-0	1	0	0	3	1	0.00	0.02	0.02
1N	138	636	0	1	0	0	3	1	0.00	0.02	0.02
1O	138	636	-0	-1	0	-0	3	1	0.00	0.02	0.02
1P	138	636	0	-1	0	-0	3	1	0.00	0.02	0.02
2	138	-391	-0	-0	0	-0	4	1	0.00	0.01	0.02
3	138	-356	-0	-0	0	-0	4	1	0.00	0.01	0.01
4	138	-253	-0	-0	0	-0	4	1	0.00	0.01	0.01
5	138	-320	-0	-0	0	-0	4	1	0.00	0.01	0.01
1A	277	-3244	-13	0	0	-0	-6	1	0.00	0.09	0.09
1B	277	-3244	-13	0	0	-0	-6	1	0.00	0.09	0.09
1C	277	-3244	-13	-0	0	0	-6	1	0.00	0.09	0.09
1D	277	-3244	-13	-0	0	0	-6	1	0.00	0.09	0.09
1E	277	2738	-13	0	0	-0	-6	1	0.00	0.07	0.08
1F	277	2738	-13	0	0	-0	-6	1	0.00	0.07	0.08
1G	277	2738	-13	-0	0	0	-6	1	0.00	0.07	0.08
1H	277	2738	-13	-0	0	0	-6	1	0.00	0.07	0.08
1I	277	-1150	-13	1	0	-1	-6	1	0.00	0.03	0.04
1J	277	-1150	-13	1	0	-1	-6	1	0.00	0.03	0.04
1K	277	-1150	-13	-1	0	1	-6	1	0.00	0.03	0.04
1L	277	-1150	-13	-1	0	1	-6	1	0.00	0.03	0.04
1M	277	644	-13	1	0	-1	-6	1	0.00	0.02	0.03
1N	277	644	-13	1	0	-1	-6	1	0.00	0.02	0.03
1O	277	644	-13	-1	0	1	-6	1	0.00	0.02	0.03
1P	277	644	-13	-1	0	1	-6	1	0.00	0.02	0.03
2	277	-380	-17	-0	0	0	-8	1	0.00	0.01	0.02
3	277	-345	-17	-0	0	0	-8	1	0.00	0.01	0.02
4	277	-242	-17	-0	0	0	-8	1	0.00	0.01	0.02
5	277	-309	-17	-0	0	0	-8	1	0.00	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	-3260	0	-6	1	0.2655	0.7726	1.5000	--	--	0.32	--	0.34	Snell. 'yx'= 144
1B	-3260	0	-7	1	0.2655	0.7726	1.5000	--	--	0.32	--	0.34	Snell. 'yx'= 144
1C	-3260	-0	-6	1	0.2655	0.7726	1.5000	--	--	0.32	--	0.34	Snell. 'yx'= 144
1D	-3260	-0	-7	1	0.2655	0.7726	1.5000	--	--	0.32	--	0.34	Snell. 'yx'= 144
1I	-1167	1	-6	1	0.2655	0.9186	1.2132	--	--	0.12	--	0.13	Snell. 'yx'= 144
1J	-1167	1	-6	1	0.2655	0.9186	1.2110	--	--	0.12	--	0.13	Snell. 'yx'= 144
1K	-1167	-1	-6	1	0.2655	0.9186	1.2132	--	--	0.12	--	0.13	Snell. 'yx'= 144
1L	-1167	-1	-6	1	0.2655	0.9186	1.2110	--	--	0.12	--	0.13	Snell. 'yx'= 144
2	-402	-0	-8	1	0.2655	1.0946	1.0790	--	--	0.04	--	0.05	Snell. 'yx'= 144
3	-367	-0	-8	1	0.2655	1.0838	1.0722	--	--	0.04	--	0.05	Snell. 'yx'= 144
4	-264	-0	-8	1	0.2655	1.0582	1.0518	--	--	0.03	--	0.04	Snell. 'yx'= 144
5	-331	-0	-8	1	0.2655	0.9769	1.0650	--	--	0.03	--	0.04	Snell. 'yx'= 144

ASTA NUM. 2 NI 10 NF 32 Lungh. 276.9 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm		daN			daN*m						
1A	0	-3260	13	0	0	0	-5	1	0.00	0.09	0.09	
1B	0	-3260	13	0	0	0	-7	1	0.00	0.09	0.10	
1C	0	-3260	13	-0	0	-0	-5	1	0.00	0.09	0.09	
1D	0	-3260	13	-0	0	-0	-7	1	0.00	0.09	0.10	
1E	0	2722	13	0	0	0	-5	1	0.00	0.07	0.08	
1F	0	2722	13	0	0	0	-7	1	0.00	0.07	0.08	
1G	0	2722	13	-0	0	-0	-5	1	0.00	0.07	0.08	
1H	0	2722	13	-0	0	-0	-7	1	0.00	0.07	0.08	
1I	0	-1167	13	1	0	1	-6	1	0.00	0.03	0.04	
1J	0	-1167	13	1	0	1	-6	1	0.00	0.03	0.04	
1K	0	-1167	13	-1	0	-1	-6	1	0.00	0.03	0.04	
1L	0	-1167	13	-1	0	-1	-6	1	0.00	0.03	0.04	
1M	0	628	13	1	0	1	-6	1	0.00	0.02	0.03	
1N	0	628	13	1	0	1	-6	1	0.00	0.02	0.03	
1O	0	628	13	-1	0	-1	-6	1	0.00	0.02	0.03	
1P	0	628	13	-1	0	-1	-6	1	0.00	0.02	0.03	
2	0	-402	17	0	0	0	-8	1	0.00	0.01	0.02	
3	0	-367	17	0	0	0	-8	1	0.00	0.01	0.02	
4	0	-401	17	0	0	0	-8	1	0.00	0.01	0.02	
5	0	-331	17	0	0	0	-8	1	0.00	0.01	0.02	
1A	138	-3252	-0	0	0	0	3	1	0.00	0.09	0.09	
1B	138	-3252	0	0	0	0	2	1	0.00	0.09	0.09	
1C	138	-3252	-0	-0	0	-0	3	1	0.00	0.09	0.09	
1D	138	-3252	0	-0	0	-0	2	1	0.00	0.09	0.09	
1E	138	2730	-0	0	0	0	3	1	0.00	0.07	0.08	
1F	138	2730	0	0	0	0	2	1	0.00	0.07	0.08	
1G	138	2730	-0	-0	0	-0	3	1	0.00	0.07	0.08	
1H	138	2730	0	-0	0	-0	2	1	0.00	0.07	0.08	
1I	138	-1158	-0	1	0	0	3	1	0.00	0.03	0.03	
1J	138	-1158	0	1	0	0	3	1	0.00	0.03	0.03	
1K	138	-1158	-0	-1	0	-0	3	1	0.00	0.03	0.03	
1L	138	-1158	0	-1	0	-0	3	1	0.00	0.03	0.03	
1M	138	636	-0	1	0	0	3	1	0.00	0.02	0.02	
1N	138	636	0	1	0	0	3	1	0.00	0.02	0.02	
1O	138	636	-0	-1	0	-0	3	1	0.00	0.02	0.02	
1P	138	636	0	-1	0	-0	3	1	0.00	0.02	0.02	
2	138	-391	-0	0	0	0	4	1	0.00	0.01	0.02	
3	138	-356	-0	0	0	0	4	1	0.00	0.01	0.01	
4	138	-390	-0	0	0	0	4	1	0.00	0.01	0.02	
5	138	-320	-0	0	0	0	4	1	0.00	0.01	0.01	
1A	277	-3244	-13	0	0	-0	-6	1	0.00	0.09	0.09	
1B	277	-3244	-13	0	0	-0	-6	1	0.00	0.09	0.09	
1C	277	-3244	-13	-0	0	0	-6	1	0.00	0.09	0.09	
1D	277	-3244	-13	-0	0	0	-6	1	0.00	0.09	0.09	
1E	277	2738	-13	0	0	-0	-6	1	0.00	0.07	0.08	
1F	277	2738	-13	0	0	-0	-6	1	0.00	0.07	0.08	
1G	277	2738	-13	-0	0	0	-6	1	0.00	0.07	0.08	
1H	277	2738	-13	-0	0	0	-6	1	0.00	0.07	0.08	
1I	277	-1150	-13	1	0	-1	-6	1	0.00	0.03	0.04	
1J	277	-1150	-13	1	0	-1	-6	1	0.00	0.03	0.04	
1K	277	-1150	-13	-1	0	1	-6	1	0.00	0.03	0.04	
1L	277	-1150	-13	-1	0	1	-6	1	0.00	0.03	0.04	

1M	277	644	-13	1	0	-1	-6	1	0.00	0.02	0.03
1N	277	644	-13	1	0	-1	-6	1	0.00	0.02	0.03
1O	277	644	-13	-1	0	1	-6	1	0.00	0.02	0.03
1P	277	644	-13	-1	0	1	-6	1	0.00	0.02	0.03
2	277	-380	-17	0	0	-0	-8	1	0.00	0.01	0.02
3	277	-345	-17	0	0	-0	-8	1	0.00	0.01	0.02
4	277	-379	-17	0	0	-0	-8	1	0.00	0.01	0.02
5	277	-309	-17	0	0	-0	-8	1	0.00	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-3260	0	-6	1	0.2655	0.7726	1.5000	--	--	0.32	--	0.34	Snell. 'yx'= 144
1B	-3260	0	-7	1	0.2655	0.7726	1.5000	--	--	0.32	--	0.34	Snell. 'yx'= 144
1C	-3260	-0	-6	1	0.2655	0.7726	1.5000	--	--	0.32	--	0.34	Snell. 'yx'= 144
1D	-3260	-0	-7	1	0.2655	0.7726	1.5000	--	--	0.32	--	0.34	Snell. 'yx'= 144
1I	-1167	1	-6	1	0.2655	0.9186	1.2132	--	--	0.12	--	0.13	Snell. 'yx'= 144
1J	-1167	1	-6	1	0.2655	0.9186	1.2110	--	--	0.12	--	0.13	Snell. 'yx'= 144
1K	-1167	-1	-6	1	0.2655	0.9186	1.2132	--	--	0.12	--	0.13	Snell. 'yx'= 144
1L	-1167	-1	-6	1	0.2655	0.9186	1.2110	--	--	0.12	--	0.13	Snell. 'yx'= 144
2	-402	0	-8	1	0.2655	1.0940	1.0790	--	--	0.04	--	0.05	Snell. 'yx'= 144
3	-367	0	-8	1	0.2655	1.0833	1.0722	--	--	0.04	--	0.05	Snell. 'yx'= 144
4	-401	0	-8	1	0.2655	1.0881	1.0788	--	--	0.04	--	0.05	Snell. 'yx'= 144
5	-331	0	-8	1	0.2655	0.9769	1.0650	--	--	0.03	--	0.04	Snell. 'yx'= 144

ASTA NUM. 3 NI 4 NF 32 Lungh. 280.3 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-819	13	2	0	3	-6	1	0.00	0.02	0.04	
1B	0	-819	14	2	0	3	-7	1	0.00	0.02	0.04	
1C	0	-819	13	-2	0	-3	-6	1	0.00	0.02	0.03	
1D	0	-819	14	-2	0	-3	-7	1	0.00	0.02	0.04	
1E	0	235	13	2	0	3	-6	1	0.00	0.01	0.02	
1F	0	235	14	2	0	3	-7	1	0.00	0.01	0.02	
1G	0	235	13	-2	0	-3	-6	1	0.00	0.01	0.02	
1H	0	235	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1I	0	-1485	13	1	0	1	-6	1	0.00	0.04	0.05	
1J	0	-1485	14	1	0	1	-7	1	0.00	0.04	0.05	
1K	0	-1485	13	-1	0	-1	-6	1	0.00	0.04	0.05	
1L	0	-1485	14	-1	0	-1	-7	1	0.00	0.04	0.05	
1M	0	901	13	1	0	1	-6	1	0.00	0.02	0.03	
1N	0	901	14	1	0	1	-7	1	0.00	0.02	0.04	
1O	0	901	13	-1	0	-1	-6	1	0.00	0.02	0.03	
1P	0	901	14	-1	0	-1	-7	1	0.00	0.02	0.03	
2	0	-436	18	0	0	0	-9	1	0.00	0.01	0.02	
3	0	-398	18	0	0	0	-9	1	0.00	0.01	0.02	
4	0	-356	18	0	0	0	-8	1	0.00	0.01	0.02	
5	0	-186	18	0	0	0	-8	1	0.00	0.00	0.02	
1A	140	-811	0	2	0	0	3	1	0.00	0.02	0.03	
1B	140	-811	0	2	0	0	3	1	0.00	0.02	0.03	
1C	140	-811	0	-2	0	-0	3	1	0.00	0.02	0.03	

1D	140	-811	0	-2	0	-0	3	1	0.00	0.02	0.03
1E	140	244	0	2	0	0	3	1	0.00	0.01	0.01
1F	140	244	0	2	0	0	3	1	0.00	0.01	0.01
1G	140	244	0	-2	0	-0	3	1	0.00	0.01	0.01
1H	140	244	0	-2	0	-0	3	1	0.00	0.01	0.01
1I	140	-1477	-0	1	0	0	3	1	0.00	0.04	0.04
1J	140	-1477	1	1	0	0	3	1	0.00	0.04	0.04
1K	140	-1477	-0	-1	0	-0	3	1	0.00	0.04	0.04
1L	140	-1477	1	-1	0	-0	3	1	0.00	0.04	0.04
1M	140	909	-0	1	0	0	3	1	0.00	0.02	0.03
1N	140	909	1	1	0	0	3	1	0.00	0.02	0.03
1O	140	909	-0	-1	0	-0	3	1	0.00	0.02	0.03
1P	140	909	1	-1	0	-0	3	1	0.00	0.02	0.03
2	140	-425	0	0	0	-0	4	1	0.00	0.01	0.02
3	140	-387	0	0	0	-0	4	1	0.00	0.01	0.02
4	140	-345	0	0	0	-0	4	1	0.00	0.01	0.01
5	140	-175	0	0	0	-0	4	1	0.00	0.00	0.01
1A	280	-803	-13	2	0	-3	-6	1	0.00	0.02	0.03
1B	280	-803	-13	2	0	-3	-6	1	0.00	0.02	0.03
1C	280	-803	-13	-2	0	2	-6	1	0.00	0.02	0.03
1D	280	-803	-13	-2	0	2	-6	1	0.00	0.02	0.03
1E	280	252	-13	2	0	-3	-6	1	0.00	0.01	0.02
1F	280	252	-13	2	0	-3	-6	1	0.00	0.01	0.02
1G	280	252	-13	-2	0	2	-6	1	0.00	0.01	0.02
1H	280	252	-13	-2	0	2	-6	1	0.00	0.01	0.02
1I	280	-1468	-13	1	0	-1	-6	1	0.00	0.04	0.05
1J	280	-1468	-13	1	0	-1	-6	1	0.00	0.04	0.05
1K	280	-1468	-13	-1	0	0	-6	1	0.00	0.04	0.05
1L	280	-1468	-13	-1	0	0	-6	1	0.00	0.04	0.05
1M	280	917	-13	1	0	-1	-6	1	0.00	0.02	0.03
1N	280	917	-13	1	0	-1	-6	1	0.00	0.02	0.03
1O	280	917	-13	-1	0	0	-6	1	0.00	0.02	0.03
1P	280	917	-13	-1	0	0	-6	1	0.00	0.02	0.03
2	280	-415	-17	0	0	-0	-8	1	0.00	0.01	0.02
3	280	-376	-17	0	0	-0	-8	1	0.00	0.01	0.02
4	280	-334	-17	0	0	-0	-8	1	0.00	0.01	0.02
5	280	-164	-17	0	0	-0	-8	1	0.00	0.00	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-819	3	-6	1	0.2603	0.9418	1.1515	--	--	0.08	--	0.10	Snell. 'yx'= 145
1B	-819	3	-7	1	0.2603	0.9418	1.1625	--	--	0.08	--	0.10	Snell. 'yx'= 145
1C	-819	-3	-6	1	0.2603	0.9418	1.1515	--	--	0.08	--	0.10	Snell. 'yx'= 145
1D	-819	-3	-7	1	0.2603	0.9418	1.1625	--	--	0.08	--	0.10	Snell. 'yx'= 145
1I	-1485	1	-6	1	0.2603	0.8945	1.2746	--	--	0.15	--	0.16	Snell. 'yx'= 145
1J	-1485	1	-7	1	0.2603	0.8945	1.2963	--	--	0.15	--	0.16	Snell. 'yx'= 145
1K	-1485	-1	-6	1	0.2603	0.8945	1.2746	--	--	0.15	--	0.16	Snell. 'yx'= 145
1L	-1485	-1	-7	1	0.2603	0.8945	1.2963	--	--	0.15	--	0.16	Snell. 'yx'= 145
2	-436	-0	-9	1	0.2603	0.9690	1.0892	--	--	0.04	--	0.06	Snell. 'yx'= 145
3	-398	-0	-9	1	0.2603	0.9717	1.0814	--	--	0.04	--	0.05	Snell. 'yx'= 145
4	-356	-0	-8	1	0.2603	0.9747	1.0728	--	--	0.04	--	0.05	Snell. 'yx'= 145
5	-186	-0	-8	1	0.2603	0.9868	1.0380	--	--	0.02	--	0.03	Snell. 'yx'= 145

ASTA NUM. 4 NI 11 NF 39 Lungh. 280.3 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-488	14	2	0	3	-7	1	0.00	0.01	0.03	
1B	0	-488	14	2	0	3	-7	1	0.00	0.01	0.03	
1C	0	-488	14	-2	0	-3	-7	1	0.00	0.01	0.03	
1D	0	-488	14	-2	0	-3	-7	1	0.00	0.01	0.03	
1E	0	239	14	2	0	3	-7	1	0.00	0.01	0.02	
1F	0	239	14	2	0	3	-7	1	0.00	0.01	0.02	
1G	0	239	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1H	0	239	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1I	0	-1202	14	1	0	1	-6	1	0.00	0.03	0.04	
1J	0	-1202	14	1	0	1	-7	1	0.00	0.03	0.04	
1K	0	-1202	14	-1	0	-1	-6	1	0.00	0.03	0.04	
1L	0	-1202	14	-1	0	-1	-7	1	0.00	0.03	0.04	
1M	0	953	14	1	0	1	-6	1	0.00	0.03	0.04	
1N	0	953	14	1	0	1	-7	1	0.00	0.03	0.04	
1O	0	953	14	-1	0	-1	-6	1	0.00	0.03	0.04	
1P	0	953	14	-1	0	-1	-7	1	0.00	0.03	0.04	
2	0	-184	18	-0	0	-0	-9	1	0.00	0.00	0.02	
3	0	-169	18	-0	0	-0	-9	1	0.00	0.00	0.02	
4	0	-155	18	-0	0	-0	-9	1	0.00	0.00	0.02	
5	0	-320	17	-0	0	-0	-8	1	0.00	0.01	0.02	
1A	140	-480	0	2	0	0	3	1	0.00	0.01	0.02	
1B	140	-480	0	2	0	0	3	1	0.00	0.01	0.02	
1C	140	-480	0	-2	0	-0	3	1	0.00	0.01	0.02	
1D	140	-480	0	-2	0	-0	3	1	0.00	0.01	0.02	
1E	140	247	0	2	0	0	3	1	0.00	0.01	0.01	
1F	140	247	0	2	0	0	3	1	0.00	0.01	0.01	
1G	140	247	0	-2	0	-0	3	1	0.00	0.01	0.01	
1H	140	247	0	-2	0	-0	3	1	0.00	0.01	0.01	
1I	140	-1194	0	1	0	0	3	1	0.00	0.03	0.04	
1J	140	-1194	0	1	0	0	3	1	0.00	0.03	0.04	
1K	140	-1194	0	-1	0	-0	3	1	0.00	0.03	0.04	
1L	140	-1194	0	-1	0	-0	3	1	0.00	0.03	0.04	
1M	140	961	0	1	0	0	3	1	0.00	0.03	0.03	
1N	140	961	0	1	0	0	3	1	0.00	0.03	0.03	
1O	140	961	0	-1	0	-0	3	1	0.00	0.03	0.03	
1P	140	961	0	-1	0	-0	3	1	0.00	0.03	0.03	
2	140	-173	1	-0	0	0	4	1	0.00	0.00	0.01	
3	140	-158	1	-0	0	0	4	1	0.00	0.00	0.01	
4	140	-145	1	-0	0	0	4	1	0.00	0.00	0.01	
5	140	-309	0	-0	0	0	4	1	0.00	0.01	0.01	
1A	280	-471	-13	2	0	-2	-6	1	0.00	0.01	0.02	
1B	280	-471	-13	2	0	-2	-5	1	0.00	0.01	0.02	
1C	280	-471	-13	-2	0	3	-6	1	0.00	0.01	0.02	
1D	280	-471	-13	-2	0	3	-5	1	0.00	0.01	0.02	
1E	280	255	-13	2	0	-2	-6	1	0.00	0.01	0.02	
1F	280	255	-13	2	0	-2	-5	1	0.00	0.01	0.02	
1G	280	255	-13	-2	0	3	-6	1	0.00	0.01	0.02	
1H	280	255	-13	-2	0	3	-5	1	0.00	0.01	0.02	
1I	280	-1185	-13	1	0	-1	-5	1	0.00	0.03	0.04	
1J	280	-1185	-13	1	0	-1	-6	1	0.00	0.03	0.04	
1K	280	-1185	-13	-1	0	1	-5	1	0.00	0.03	0.04	

1L	280	-1185	-13	-1	0	1	-6	1	0.00	0.03	0.04
1M	280	969	-13	1	0	-1	-5	1	0.00	0.03	0.03
1N	280	969	-13	1	0	-1	-6	1	0.00	0.03	0.03
1O	280	969	-13	-1	0	1	-5	1	0.00	0.03	0.03
1P	280	969	-13	-1	0	1	-6	1	0.00	0.03	0.03
2	280	-162	-17	-0	0	0	-7	1	0.00	0.00	0.01
3	280	-148	-17	-0	0	0	-7	1	0.00	0.00	0.01
4	280	-134	-17	-0	0	0	-7	1	0.00	0.00	0.01
5	280	-299	-17	-0	0	0	-8	1	0.00	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-488	3	-7	1	0.2603	0.9653	1.0950	--	--	0.05	--	0.06	Snell. 'yx'= 145
1B	-488	3	-7	1	0.2603	0.9653	1.0973	--	--	0.05	--	0.06	Snell. 'yx'= 145
1C	-488	-3	-7	1	0.2603	0.9653	1.0950	--	--	0.05	--	0.06	Snell. 'yx'= 145
1D	-488	-3	-7	1	0.2603	0.9653	1.0973	--	--	0.05	--	0.06	Snell. 'yx'= 145
1I	-1202	1	-6	1	0.2603	0.9146	1.2356	--	--	0.12	--	0.13	Snell. 'yx'= 145
1J	-1202	1	-7	1	0.2603	0.9146	1.2384	--	--	0.12	--	0.13	Snell. 'yx'= 145
1K	-1202	-1	-6	1	0.2603	0.9146	1.2356	--	--	0.12	--	0.13	Snell. 'yx'= 145
1L	-1202	-1	-7	1	0.2603	0.9146	1.2384	--	--	0.12	--	0.13	Snell. 'yx'= 145
2	-184	0	-9	1	0.2603	0.9869	1.0376	--	--	0.02	--	0.03	Snell. 'yx'= 145
3	-169	0	-9	1	0.2603	0.9880	1.0346	--	--	0.02	--	0.03	Snell. 'yx'= 145
4	-155	0	-9	1	0.2603	0.9890	1.0318	--	--	0.02	--	0.03	Snell. 'yx'= 145
5	-320	0	-8	1	0.2603	0.9773	1.0650	--	--	0.03	--	0.04	Snell. 'yx'= 145

ASTA NUM. 5 NI 11 NF 25 Lungh. 280.3 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-488	14	2	0	3	-7	1	0.00	0.01	0.03	
1B	0	-488	14	2	0	3	-7	1	0.00	0.01	0.03	
1C	0	-488	14	-2	0	-3	-7	1	0.00	0.01	0.03	
1D	0	-488	14	-2	0	-3	-7	1	0.00	0.01	0.03	
1E	0	239	14	2	0	3	-7	1	0.00	0.01	0.02	
1F	0	239	14	2	0	3	-7	1	0.00	0.01	0.02	
1G	0	239	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1H	0	239	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1I	0	-1202	14	1	0	1	-6	1	0.00	0.03	0.04	
1J	0	-1202	14	1	0	1	-7	1	0.00	0.03	0.04	
1K	0	-1202	14	-1	0	-1	-6	1	0.00	0.03	0.04	
1L	0	-1202	14	-1	0	-1	-7	1	0.00	0.03	0.04	
1M	0	953	14	1	0	1	-6	1	0.00	0.03	0.04	
1N	0	953	14	1	0	1	-7	1	0.00	0.03	0.04	
1O	0	953	14	-1	0	-1	-6	1	0.00	0.03	0.04	
1P	0	953	14	-1	0	-1	-7	1	0.00	0.03	0.04	
2	0	-184	18	0	0	0	-9	1	0.00	0.00	0.02	
3	0	-169	18	0	0	0	-9	1	0.00	0.00	0.02	
4	0	-155	18	0	0	0	-9	1	0.00	0.00	0.02	
5	0	14	18	0	0	0	-9	1	0.00	0.00	0.01	
1A	140	-480	0	2	0	0	3	1	0.00	0.01	0.02	
1B	140	-480	0	2	0	0	3	1	0.00	0.01	0.02	

1C	140	-480	0	-2	0	-0	3	1	0.00	0.01	0.02
1D	140	-480	0	-2	0	-0	3	1	0.00	0.01	0.02
1E	140	247	0	2	0	0	3	1	0.00	0.01	0.01
1F	140	247	0	2	0	0	3	1	0.00	0.01	0.01
1G	140	247	0	-2	0	-0	3	1	0.00	0.01	0.01
1H	140	247	0	-2	0	-0	3	1	0.00	0.01	0.01
1I	140	-1194	0	1	0	0	3	1	0.00	0.03	0.04
1J	140	-1194	0	1	0	0	3	1	0.00	0.03	0.04
1K	140	-1194	0	-1	0	-0	3	1	0.00	0.03	0.04
1L	140	-1194	0	-1	0	-0	3	1	0.00	0.03	0.04
1M	140	961	0	1	0	0	3	1	0.00	0.03	0.03
1N	140	961	0	1	0	0	3	1	0.00	0.03	0.03
1O	140	961	0	-1	0	-0	3	1	0.00	0.03	0.03
1P	140	961	0	-1	0	-0	3	1	0.00	0.03	0.03
2	140	-173	1	0	0	-0	4	1	0.00	0.00	0.01
3	140	-158	1	0	0	-0	4	1	0.00	0.00	0.01
4	140	-145	1	0	0	-0	4	1	0.00	0.00	0.01
5	140	24	1	0	0	-0	4	1	0.00	0.00	0.01
1A	280	-471	-13	2	0	-3	-6	1	0.00	0.01	0.02
1B	280	-471	-13	2	0	-3	-5	1	0.00	0.01	0.02
1C	280	-471	-13	-2	0	2	-6	1	0.00	0.01	0.02
1D	280	-471	-13	-2	0	2	-5	1	0.00	0.01	0.02
1E	280	255	-13	2	0	-3	-6	1	0.00	0.01	0.02
1F	280	255	-13	2	0	-3	-5	1	0.00	0.01	0.02
1G	280	255	-13	-2	0	2	-6	1	0.00	0.01	0.02
1H	280	255	-13	-2	0	2	-5	1	0.00	0.01	0.02
1I	280	-1185	-13	1	0	-1	-5	1	0.00	0.03	0.04
1J	280	-1185	-13	1	0	-1	-6	1	0.00	0.03	0.04
1K	280	-1185	-13	-1	0	1	-5	1	0.00	0.03	0.04
1L	280	-1185	-13	-1	0	1	-6	1	0.00	0.03	0.04
1M	280	969	-13	1	0	-1	-5	1	0.00	0.03	0.03
1N	280	969	-13	1	0	-1	-6	1	0.00	0.03	0.03
1O	280	969	-13	-1	0	1	-5	1	0.00	0.03	0.03
1P	280	969	-13	-1	0	1	-6	1	0.00	0.03	0.03
2	280	-162	-17	0	0	-0	-7	1	0.00	0.00	0.01
3	280	-148	-17	0	0	-0	-7	1	0.00	0.00	0.01
4	280	-134	-17	0	0	-0	-7	1	0.00	0.00	0.01
5	280	35	-17	0	0	-0	-7	1	0.00	0.00	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	-488	3	-7	1	0.2603	0.9653	1.0950	--	--	0.05	--	0.06	Snell. 'yx'= 145
1B	-488	3	-7	1	0.2603	0.9653	1.0973	--	--	0.05	--	0.06	Snell. 'yx'= 145
1C	-488	-3	-7	1	0.2603	0.9653	1.0950	--	--	0.05	--	0.06	Snell. 'yx'= 145
1D	-488	-3	-7	1	0.2603	0.9653	1.0973	--	--	0.05	--	0.06	Snell. 'yx'= 145
1I	-1202	1	-6	1	0.2603	0.9146	1.2356	--	--	0.12	--	0.13	Snell. 'yx'= 145
1J	-1202	1	-7	1	0.2603	0.9146	1.2384	--	--	0.12	--	0.13	Snell. 'yx'= 145
1K	-1202	-1	-6	1	0.2603	0.9146	1.2356	--	--	0.12	--	0.13	Snell. 'yx'= 145
1L	-1202	-1	-7	1	0.2603	0.9146	1.2384	--	--	0.12	--	0.13	Snell. 'yx'= 145
2	-184	-0	-9	1	0.2603	0.9869	1.0376	--	--	0.02	--	0.03	Snell. 'yx'= 145
3	-169	-0	-9	1	0.2603	0.9880	1.0346	--	--	0.02	--	0.03	Snell. 'yx'= 145
4	-155	-0	-9	1	0.2603	0.9890	1.0318	--	--	0.02	--	0.03	Snell. 'yx'= 145

ASTA NUM. 6 NI 18 NF 32 Lungh. 280.3 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-819	13	2	0	3	-6	1	0.00	0.02	0.03	
1B	0	-819	14	2	0	3	-7	1	0.00	0.02	0.04	
1C	0	-819	13	-2	0	-3	-6	1	0.00	0.02	0.04	
1D	0	-819	14	-2	0	-3	-7	1	0.00	0.02	0.04	
1E	0	235	13	2	0	3	-6	1	0.00	0.01	0.02	
1F	0	235	14	2	0	3	-7	1	0.00	0.01	0.02	
1G	0	235	13	-2	0	-3	-6	1	0.00	0.01	0.02	
1H	0	235	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1I	0	-1485	13	1	0	1	-6	1	0.00	0.04	0.05	
1J	0	-1485	14	1	0	1	-7	1	0.00	0.04	0.05	
1K	0	-1485	13	-1	0	-1	-6	1	0.00	0.04	0.05	
1L	0	-1485	14	-1	0	-1	-7	1	0.00	0.04	0.05	
1M	0	901	13	1	0	1	-6	1	0.00	0.02	0.03	
1N	0	901	14	1	0	1	-7	1	0.00	0.02	0.03	
1O	0	901	13	-1	0	-1	-6	1	0.00	0.02	0.03	
1P	0	901	14	-1	0	-1	-7	1	0.00	0.02	0.04	
2	0	-436	18	-0	0	-0	-9	1	0.00	0.01	0.02	
3	0	-398	18	-0	0	-0	-9	1	0.00	0.01	0.02	
4	0	-356	18	-0	0	-0	-8	1	0.00	0.01	0.02	
5	0	-535	18	-0	0	-0	-9	1	0.00	0.01	0.03	
1A	140	-811	0	2	0	0	3	1	0.00	0.02	0.03	
1B	140	-811	0	2	0	0	3	1	0.00	0.02	0.03	
1C	140	-811	0	-2	0	-0	3	1	0.00	0.02	0.03	
1D	140	-811	0	-2	0	-0	3	1	0.00	0.02	0.03	
1E	140	244	0	2	0	0	3	1	0.00	0.01	0.01	
1F	140	244	0	2	0	0	3	1	0.00	0.01	0.01	
1G	140	244	0	-2	0	-0	3	1	0.00	0.01	0.01	
1H	140	244	0	-2	0	-0	3	1	0.00	0.01	0.01	
1I	140	-1477	-0	1	0	0	3	1	0.00	0.04	0.04	
1J	140	-1477	1	1	0	0	3	1	0.00	0.04	0.04	
1K	140	-1477	-0	-1	0	-0	3	1	0.00	0.04	0.04	
1L	140	-1477	1	-1	0	-0	3	1	0.00	0.04	0.04	
1M	140	909	-0	1	0	0	3	1	0.00	0.02	0.03	
1N	140	909	1	1	0	0	3	1	0.00	0.02	0.03	
1O	140	909	-0	-1	0	-0	3	1	0.00	0.02	0.03	
1P	140	909	1	-1	0	-0	3	1	0.00	0.02	0.03	
2	140	-425	0	-0	0	0	4	1	0.00	0.01	0.02	
3	140	-387	0	-0	0	0	4	1	0.00	0.01	0.02	
4	140	-345	0	-0	0	0	4	1	0.00	0.01	0.01	
5	140	-524	0	-0	0	0	4	1	0.00	0.01	0.02	
1A	280	-803	-13	2	0	-2	-6	1	0.00	0.02	0.03	
1B	280	-803	-13	2	0	-2	-6	1	0.00	0.02	0.03	
1C	280	-803	-13	-2	0	3	-6	1	0.00	0.02	0.03	
1D	280	-803	-13	-2	0	3	-6	1	0.00	0.02	0.03	
1E	280	252	-13	2	0	-2	-6	1	0.00	0.01	0.02	
1F	280	252	-13	2	0	-2	-6	1	0.00	0.01	0.02	
1G	280	252	-13	-2	0	3	-6	1	0.00	0.01	0.02	
1H	280	252	-13	-2	0	3	-6	1	0.00	0.01	0.02	
1I	280	-1468	-13	1	0	-0	-6	1	0.00	0.04	0.05	
1J	280	-1468	-13	1	0	-0	-6	1	0.00	0.04	0.05	
1K	280	-1468	-13	-1	0	1	-6	1	0.00	0.04	0.05	

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1L	280	-1468	-13	-1	0	1	-6	1	0.00	0.04	0.05
1M	280	917	-13	1	0	-0	-6	1	0.00	0.02	0.03
1N	280	917	-13	1	0	-0	-6	1	0.00	0.02	0.03
1O	280	917	-13	-1	0	1	-6	1	0.00	0.02	0.03
1P	280	917	-13	-1	0	1	-6	1	0.00	0.02	0.03
2	280	-415	-17	-0	0	0	-8	1	0.00	0.01	0.02
3	280	-376	-17	-0	0	0	-8	1	0.00	0.01	0.02
4	280	-334	-17	-0	0	0	-8	1	0.00	0.01	0.02
5	280	-513	-17	-0	0	0	-8	1	0.00	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-819	3	-6	1	0.2603	0.9418	1.1515	--	--	0.08	--	0.10	Snell. 'yx'= 145
1B	-819	3	-7	1	0.2603	0.9418	1.1625	--	--	0.08	--	0.10	Snell. 'yx'= 145
1C	-819	-3	-6	1	0.2603	0.9418	1.1515	--	--	0.08	--	0.10	Snell. 'yx'= 145
1D	-819	-3	-7	1	0.2603	0.9418	1.1625	--	--	0.08	--	0.10	Snell. 'yx'= 145
1I	-1485	1	-6	1	0.2603	0.8945	1.2746	--	--	0.15	--	0.16	Snell. 'yx'= 145
1J	-1485	1	-7	1	0.2603	0.8945	1.2963	--	--	0.15	--	0.16	Snell. 'yx'= 145
1K	-1485	-1	-6	1	0.2603	0.8945	1.2746	--	--	0.15	--	0.16	Snell. 'yx'= 145
1L	-1485	-1	-7	1	0.2603	0.8945	1.2963	--	--	0.15	--	0.16	Snell. 'yx'= 145
2	-436	0	-9	1	0.2603	0.9690	1.0892	--	--	0.04	--	0.06	Snell. 'yx'= 145
3	-398	0	-9	1	0.2603	0.9717	1.0814	--	--	0.04	--	0.05	Snell. 'yx'= 145
4	-356	0	-8	1	0.2603	0.9747	1.0728	--	--	0.04	--	0.05	Snell. 'yx'= 145
5	-535	0	-9	1	0.2603	0.9620	1.1094	--	--	0.05	--	0.07	Snell. 'yx'= 145

ASTA NUM. 7 NI 17 NF 33 Lungh. 280.3 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-819	13	2	0	3	-6	1	0.00	0.02	0.04	
1B	0	-819	14	2	0	3	-7	1	0.00	0.02	0.04	
1C	0	-819	13	-2	0	-3	-6	1	0.00	0.02	0.03	
1D	0	-819	14	-2	0	-3	-7	1	0.00	0.02	0.04	
1E	0	235	13	2	0	3	-6	1	0.00	0.01	0.02	
1F	0	235	14	2	0	3	-7	1	0.00	0.01	0.02	
1G	0	235	13	-2	0	-3	-6	1	0.00	0.01	0.02	
1H	0	235	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1I	0	-1485	13	1	0	1	-6	1	0.00	0.04	0.05	
1J	0	-1485	14	1	0	1	-7	1	0.00	0.04	0.05	
1K	0	-1485	13	-1	0	-1	-6	1	0.00	0.04	0.05	
1L	0	-1485	14	-1	0	-1	-7	1	0.00	0.04	0.05	
1M	0	901	13	1	0	1	-6	1	0.00	0.02	0.03	
1N	0	901	14	1	0	1	-7	1	0.00	0.02	0.04	
1O	0	901	13	-1	0	-1	-6	1	0.00	0.02	0.03	
1P	0	901	14	-1	0	-1	-7	1	0.00	0.02	0.03	
2	0	-436	18	0	0	0	-9	1	0.00	0.01	0.02	
3	0	-398	18	0	0	0	-9	1	0.00	0.01	0.02	
4	0	-364	18	0	0	0	-9	1	0.00	0.01	0.02	
5	0	-525	18	0	0	0	-9	1	0.00	0.01	0.03	
1A	140	-811	0	2	0	0	3	1	0.00	0.02	0.03	
1B	140	-811	0	2	0	0	3	1	0.00	0.02	0.03	

1C	140	-811	0	-2	0	-0	3	1	0.00	0.02	0.03
1D	140	-811	0	-2	0	-0	3	1	0.00	0.02	0.03
1E	140	244	0	2	0	0	3	1	0.00	0.01	0.01
1F	140	244	0	2	0	0	3	1	0.00	0.01	0.01
1G	140	244	0	-2	0	-0	3	1	0.00	0.01	0.01
1H	140	244	0	-2	0	-0	3	1	0.00	0.01	0.01
1I	140	-1477	-0	1	0	0	3	1	0.00	0.04	0.04
1J	140	-1477	1	1	0	0	3	1	0.00	0.04	0.04
1K	140	-1477	-0	-1	0	-0	3	1	0.00	0.04	0.04
1L	140	-1477	1	-1	0	-0	3	1	0.00	0.04	0.04
1M	140	909	-0	1	0	0	3	1	0.00	0.02	0.03
1N	140	909	1	1	0	0	3	1	0.00	0.02	0.03
1O	140	909	-0	-1	0	-0	3	1	0.00	0.02	0.03
1P	140	909	1	-1	0	-0	3	1	0.00	0.02	0.03
2	140	-425	0	0	0	-0	4	1	0.00	0.01	0.02
3	140	-387	0	0	0	-0	4	1	0.00	0.01	0.02
4	140	-353	0	0	0	-0	4	1	0.00	0.01	0.02
5	140	-514	0	0	0	-0	4	1	0.00	0.01	0.02
1A	280	-803	-13	2	0	-3	-6	1	0.00	0.02	0.03
1B	280	-803	-13	2	0	-3	-6	1	0.00	0.02	0.03
1C	280	-803	-13	-2	0	2	-6	1	0.00	0.02	0.03
1D	280	-803	-13	-2	0	2	-6	1	0.00	0.02	0.03
1E	280	252	-13	2	0	-3	-6	1	0.00	0.01	0.02
1F	280	252	-13	2	0	-3	-6	1	0.00	0.01	0.02
1G	280	252	-13	-2	0	2	-6	1	0.00	0.01	0.02
1H	280	252	-13	-2	0	2	-6	1	0.00	0.01	0.02
1I	280	-1468	-13	1	0	-1	-6	1	0.00	0.04	0.05
1J	280	-1468	-13	1	0	-1	-6	1	0.00	0.04	0.05
1K	280	-1468	-13	-1	0	0	-6	1	0.00	0.04	0.05
1L	280	-1468	-13	-1	0	0	-6	1	0.00	0.04	0.05
1M	280	917	-13	1	0	-1	-6	1	0.00	0.02	0.03
1N	280	917	-13	1	0	-1	-6	1	0.00	0.02	0.03
1O	280	917	-13	-1	0	0	-6	1	0.00	0.02	0.03
1P	280	917	-13	-1	0	0	-6	1	0.00	0.02	0.03
2	280	-415	-17	0	0	-0	-8	1	0.00	0.01	0.02
3	280	-376	-17	0	0	-0	-8	1	0.00	0.01	0.02
4	280	-342	-17	0	0	-0	-8	1	0.00	0.01	0.02
5	280	-503	-17	0	0	-0	-8	1	0.00	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	-819	3	-6	1	0.2603	0.9418	1.1515	--	--	0.08	--	0.10	Snell. 'yx'= 145
1B	-819	3	-7	1	0.2603	0.9418	1.1625	--	--	0.08	--	0.10	Snell. 'yx'= 145
1C	-819	-3	-6	1	0.2603	0.9418	1.1515	--	--	0.08	--	0.10	Snell. 'yx'= 145
1D	-819	-3	-7	1	0.2603	0.9418	1.1625	--	--	0.08	--	0.10	Snell. 'yx'= 145
1I	-1485	1	-6	1	0.2603	0.8945	1.2746	--	--	0.15	--	0.16	Snell. 'yx'= 145
1J	-1485	1	-7	1	0.2603	0.8945	1.2963	--	--	0.15	--	0.16	Snell. 'yx'= 145
1K	-1485	-1	-6	1	0.2603	0.8945	1.2746	--	--	0.15	--	0.16	Snell. 'yx'= 145
1L	-1485	-1	-7	1	0.2603	0.8945	1.2963	--	--	0.15	--	0.16	Snell. 'yx'= 145
2	-436	-0	-9	1	0.2603	0.9690	1.0892	--	--	0.04	--	0.06	Snell. 'yx'= 145
3	-398	-0	-9	1	0.2603	0.9717	1.0814	--	--	0.04	--	0.05	Snell. 'yx'= 145
4	-364	-0	-9	1	0.2603	0.9760	1.0744	--	--	0.04	--	0.05	Snell. 'yx'= 145
5	-525	-0	-9	1	0.2603	0.9627	1.1073	--	--	0.05	--	0.07	Snell. 'yx'= 145

ASTA NUM. 8 NI 10 NF 26 Lungh. 280.3 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-488	14	2	0	3	-7	1	0.00	0.01	0.03	
1B	0	-488	14	2	0	3	-7	1	0.00	0.01	0.03	
1C	0	-488	14	-2	0	-3	-7	1	0.00	0.01	0.03	
1D	0	-488	14	-2	0	-3	-7	1	0.00	0.01	0.03	
1E	0	239	14	2	0	3	-7	1	0.00	0.01	0.02	
1F	0	239	14	2	0	3	-7	1	0.00	0.01	0.02	
1G	0	239	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1H	0	239	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1I	0	-1202	14	1	0	1	-6	1	0.00	0.03	0.04	
1J	0	-1202	14	1	0	1	-7	1	0.00	0.03	0.04	
1K	0	-1202	14	-1	0	-1	-6	1	0.00	0.03	0.04	
1L	0	-1202	14	-1	0	-1	-7	1	0.00	0.03	0.04	
1M	0	953	14	1	0	1	-6	1	0.00	0.03	0.04	
1N	0	953	14	1	0	1	-7	1	0.00	0.03	0.04	
1O	0	953	14	-1	0	-1	-6	1	0.00	0.03	0.04	
1P	0	953	14	-1	0	-1	-7	1	0.00	0.03	0.04	
2	0	-184	18	-0	0	-0	-9	1	0.00	0.00	0.02	
3	0	-169	18	-0	0	-0	-9	1	0.00	0.00	0.02	
4	0	-153	18	-0	0	-0	-9	1	0.00	0.00	0.02	
5	0	4	18	-0	0	-0	-9	1	0.00	0.00	0.01	
1A	140	-480	0	2	0	0	3	1	0.00	0.01	0.02	
1B	140	-480	0	2	0	0	3	1	0.00	0.01	0.02	
1C	140	-480	0	-2	0	-0	3	1	0.00	0.01	0.02	
1D	140	-480	0	-2	0	-0	3	1	0.00	0.01	0.02	
1E	140	247	0	2	0	0	3	1	0.00	0.01	0.01	
1F	140	247	0	2	0	0	3	1	0.00	0.01	0.01	
1G	140	247	0	-2	0	-0	3	1	0.00	0.01	0.01	
1H	140	247	0	-2	0	-0	3	1	0.00	0.01	0.01	
1I	140	-1194	0	1	0	0	3	1	0.00	0.03	0.04	
1J	140	-1194	0	1	0	0	3	1	0.00	0.03	0.04	
1K	140	-1194	0	-1	0	-0	3	1	0.00	0.03	0.04	
1L	140	-1194	0	-1	0	-0	3	1	0.00	0.03	0.04	
1M	140	961	0	1	0	0	3	1	0.00	0.03	0.03	
1N	140	961	0	1	0	0	3	1	0.00	0.03	0.03	
1O	140	961	0	-1	0	-0	3	1	0.00	0.03	0.03	
1P	140	961	0	-1	0	-0	3	1	0.00	0.03	0.03	
2	140	-173	1	-0	0	0	4	1	0.00	0.00	0.01	
3	140	-158	1	-0	0	0	4	1	0.00	0.00	0.01	
4	140	-143	1	-0	0	0	4	1	0.00	0.00	0.01	
5	140	15	1	-0	0	0	4	1	0.00	0.00	0.01	
1A	280	-471	-13	2	0	-2	-6	1	0.00	0.01	0.02	
1B	280	-471	-13	2	0	-2	-5	1	0.00	0.01	0.02	
1C	280	-471	-13	-2	0	3	-6	1	0.00	0.01	0.02	
1D	280	-471	-13	-2	0	3	-5	1	0.00	0.01	0.02	
1E	280	255	-13	2	0	-2	-6	1	0.00	0.01	0.02	
1F	280	255	-13	2	0	-2	-5	1	0.00	0.01	0.02	
1G	280	255	-13	-2	0	3	-6	1	0.00	0.01	0.02	
1H	280	255	-13	-2	0	3	-5	1	0.00	0.01	0.02	
1I	280	-1185	-13	1	0	-1	-5	1	0.00	0.03	0.04	
1J	280	-1185	-13	1	0	-1	-6	1	0.00	0.03	0.04	

1K	280	-1185	-13	-1	0	1	-5	1	0.00	0.03	0.04
1L	280	-1185	-13	-1	0	1	-6	1	0.00	0.03	0.04
1M	280	969	-13	1	0	-1	-5	1	0.00	0.03	0.03
1N	280	969	-13	1	0	-1	-6	1	0.00	0.03	0.03
1O	280	969	-13	-1	0	1	-5	1	0.00	0.03	0.03
1P	280	969	-13	-1	0	1	-6	1	0.00	0.03	0.03
2	280	-162	-17	-0	0	0	-7	1	0.00	0.00	0.01
3	280	-148	-17	-0	0	0	-7	1	0.00	0.00	0.01
4	280	-132	-17	-0	0	0	-7	1	0.00	0.00	0.01
5	280	25	-17	-0	0	0	-7	1	0.00	0.00	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-488	3	-7	1	0.2603	0.9653	1.0950	--	--	0.05	--	0.06	Snell. 'yx'= 145
1B	-488	3	-7	1	0.2603	0.9653	1.0973	--	--	0.05	--	0.06	Snell. 'yx'= 145
1C	-488	-3	-7	1	0.2603	0.9653	1.0950	--	--	0.05	--	0.06	Snell. 'yx'= 145
1D	-488	-3	-7	1	0.2603	0.9653	1.0973	--	--	0.05	--	0.06	Snell. 'yx'= 145
1I	-1202	1	-6	1	0.2603	0.9146	1.2356	--	--	0.12	--	0.13	Snell. 'yx'= 145
1J	-1202	1	-7	1	0.2603	0.9146	1.2384	--	--	0.12	--	0.13	Snell. 'yx'= 145
1K	-1202	-1	-6	1	0.2603	0.9146	1.2356	--	--	0.12	--	0.13	Snell. 'yx'= 145
1L	-1202	-1	-7	1	0.2603	0.9146	1.2384	--	--	0.12	--	0.13	Snell. 'yx'= 145
2	-184	0	-9	1	0.2603	0.9869	1.0376	--	--	0.02	--	0.03	Snell. 'yx'= 145
3	-169	0	-9	1	0.2603	0.9880	1.0346	--	--	0.02	--	0.03	Snell. 'yx'= 145
4	-153	0	-9	1	0.2603	0.9931	1.0314	--	--	0.02	--	0.03	Snell. 'yx'= 145

ASTA NUM. 9 NI 10 NF 38 Lungh. 280.3 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-488	14	2	0	3	-7	1	0.00	0.01	0.03	
1B	0	-488	14	2	0	3	-7	1	0.00	0.01	0.03	
1C	0	-488	14	-2	0	-3	-7	1	0.00	0.01	0.03	
1D	0	-488	14	-2	0	-3	-7	1	0.00	0.01	0.03	
1E	0	239	14	2	0	3	-7	1	0.00	0.01	0.02	
1F	0	239	14	2	0	3	-7	1	0.00	0.01	0.02	
1G	0	239	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1H	0	239	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1I	0	-1202	14	1	0	1	-6	1	0.00	0.03	0.04	
1J	0	-1202	14	1	0	1	-7	1	0.00	0.03	0.04	
1K	0	-1202	14	-1	0	-1	-6	1	0.00	0.03	0.04	
1L	0	-1202	14	-1	0	-1	-7	1	0.00	0.03	0.04	
1M	0	953	14	1	0	1	-6	1	0.00	0.03	0.04	
1N	0	953	14	1	0	1	-7	1	0.00	0.03	0.04	
1O	0	953	14	-1	0	-1	-6	1	0.00	0.03	0.04	
1P	0	953	14	-1	0	-1	-7	1	0.00	0.03	0.04	
2	0	-184	18	0	0	0	-9	1	0.00	0.00	0.02	
3	0	-169	18	0	0	0	-9	1	0.00	0.00	0.02	
4	0	-153	18	0	0	0	-9	1	0.00	0.00	0.02	
5	0	-310	17	0	0	0	-8	1	0.00	0.01	0.02	
1A	140	-480	0	2	0	0	3	1	0.00	0.01	0.02	
1B	140	-480	0	2	0	0	3	1	0.00	0.01	0.02	

1C	140	-480	0	-2	0	-0	3	1	0.00	0.01	0.02
1D	140	-480	0	-2	0	-0	3	1	0.00	0.01	0.02
1E	140	247	0	2	0	0	3	1	0.00	0.01	0.01
1F	140	247	0	2	0	0	3	1	0.00	0.01	0.01
1G	140	247	0	-2	0	-0	3	1	0.00	0.01	0.01
1H	140	247	0	-2	0	-0	3	1	0.00	0.01	0.01
1I	140	-1194	0	1	0	0	3	1	0.00	0.03	0.04
1J	140	-1194	0	1	0	0	3	1	0.00	0.03	0.04
1K	140	-1194	0	-1	0	-0	3	1	0.00	0.03	0.04
1L	140	-1194	0	-1	0	-0	3	1	0.00	0.03	0.04
1M	140	961	0	1	0	0	3	1	0.00	0.03	0.03
1N	140	961	0	1	0	0	3	1	0.00	0.03	0.03
1O	140	961	0	-1	0	-0	3	1	0.00	0.03	0.03
1P	140	961	0	-1	0	-0	3	1	0.00	0.03	0.03
2	140	-173	1	0	0	-0	4	1	0.00	0.00	0.01
3	140	-158	1	0	0	-0	4	1	0.00	0.00	0.01
4	140	-143	1	0	0	-0	4	1	0.00	0.00	0.01
5	140	-300	0	0	0	-0	4	1	0.00	0.01	0.01
1A	280	-471	-13	2	0	-3	-6	1	0.00	0.01	0.02
1B	280	-471	-13	2	0	-3	-5	1	0.00	0.01	0.02
1C	280	-471	-13	-2	0	2	-6	1	0.00	0.01	0.02
1D	280	-471	-13	-2	0	2	-5	1	0.00	0.01	0.02
1E	280	255	-13	2	0	-3	-6	1	0.00	0.01	0.02
1F	280	255	-13	2	0	-3	-5	1	0.00	0.01	0.02
1G	280	255	-13	-2	0	2	-6	1	0.00	0.01	0.02
1H	280	255	-13	-2	0	2	-5	1	0.00	0.01	0.02
1I	280	-1185	-13	1	0	-1	-5	1	0.00	0.03	0.04
1J	280	-1185	-13	1	0	-1	-6	1	0.00	0.03	0.04
1K	280	-1185	-13	-1	0	1	-5	1	0.00	0.03	0.04
1L	280	-1185	-13	-1	0	1	-6	1	0.00	0.03	0.04
1M	280	969	-13	1	0	-1	-5	1	0.00	0.03	0.03
1N	280	969	-13	1	0	-1	-6	1	0.00	0.03	0.03
1O	280	969	-13	-1	0	1	-5	1	0.00	0.03	0.03
1P	280	969	-13	-1	0	1	-6	1	0.00	0.03	0.03
2	280	-162	-17	0	0	-0	-7	1	0.00	0.00	0.01
3	280	-148	-17	0	0	-0	-7	1	0.00	0.00	0.01
4	280	-132	-17	0	0	-0	-7	1	0.00	0.00	0.01
5	280	-289	-17	0	0	-0	-8	1	0.00	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-488	3	-7	1	0.2603	0.9653	1.0950	--	--	0.05	--	0.06	Snell. 'yx'= 145
1B	-488	3	-7	1	0.2603	0.9653	1.0973	--	--	0.05	--	0.06	Snell. 'yx'= 145
1C	-488	-3	-7	1	0.2603	0.9653	1.0950	--	--	0.05	--	0.06	Snell. 'yx'= 145
1D	-488	-3	-7	1	0.2603	0.9653	1.0973	--	--	0.05	--	0.06	Snell. 'yx'= 145
1I	-1202	1	-6	1	0.2603	0.9146	1.2356	--	--	0.12	--	0.13	Snell. 'yx'= 145
1J	-1202	1	-7	1	0.2603	0.9146	1.2384	--	--	0.12	--	0.13	Snell. 'yx'= 145
1K	-1202	-1	-6	1	0.2603	0.9146	1.2356	--	--	0.12	--	0.13	Snell. 'yx'= 145
1L	-1202	-1	-7	1	0.2603	0.9146	1.2384	--	--	0.12	--	0.13	Snell. 'yx'= 145
2	-184	-0	-9	1	0.2603	0.9869	1.0376	--	--	0.02	--	0.03	Snell. 'yx'= 145
3	-169	-0	-9	1	0.2603	0.9880	1.0346	--	--	0.02	--	0.03	Snell. 'yx'= 145
4	-153	-0	-9	1	0.2603	0.9931	1.0314	--	--	0.02	--	0.03	Snell. 'yx'= 145
5	-310	-0	-8	1	0.2603	0.9779	1.0631	--	--	0.03	--	0.04	Snell. 'yx'= 145

ASTA NUM. 10 NI 5 NF 33 Lungh. 280.3 cm SEZ. 2 Pd U 50X 38 Dist.= 1.0 cm ali esterne

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-819	13	2	0	3	-6	1	0.00	0.02	0.03	
1B	0	-819	14	2	0	3	-7	1	0.00	0.02	0.04	
1C	0	-819	13	-2	0	-3	-6	1	0.00	0.02	0.04	
1D	0	-819	14	-2	0	-3	-7	1	0.00	0.02	0.04	
1E	0	235	13	2	0	3	-6	1	0.00	0.01	0.02	
1F	0	235	14	2	0	3	-7	1	0.00	0.01	0.02	
1G	0	235	13	-2	0	-3	-6	1	0.00	0.01	0.02	
1H	0	235	14	-2	0	-3	-7	1	0.00	0.01	0.02	
1I	0	-1485	13	1	0	1	-6	1	0.00	0.04	0.05	
1J	0	-1485	14	1	0	1	-7	1	0.00	0.04	0.05	
1K	0	-1485	13	-1	0	-1	-6	1	0.00	0.04	0.05	
1L	0	-1485	14	-1	0	-1	-7	1	0.00	0.04	0.05	
1M	0	901	13	1	0	1	-6	1	0.00	0.02	0.03	
1N	0	901	14	1	0	1	-7	1	0.00	0.02	0.03	
1O	0	901	13	-1	0	-1	-6	1	0.00	0.02	0.03	
1P	0	901	14	-1	0	-1	-7	1	0.00	0.02	0.04	
2	0	-436	18	-0	0	-0	-9	1	0.00	0.01	0.02	
3	0	-398	18	-0	0	-0	-9	1	0.00	0.01	0.02	
4	0	-364	18	-0	0	-0	-9	1	0.00	0.01	0.02	
5	0	-196	18	-0	0	-0	-8	1	0.00	0.01	0.02	
1A	140	-811	0	2	0	0	3	1	0.00	0.02	0.03	
1B	140	-811	0	2	0	0	3	1	0.00	0.02	0.03	
1C	140	-811	0	-2	0	-0	3	1	0.00	0.02	0.03	
1D	140	-811	0	-2	0	-0	3	1	0.00	0.02	0.03	
1E	140	244	0	2	0	0	3	1	0.00	0.01	0.01	
1F	140	244	0	2	0	0	3	1	0.00	0.01	0.01	
1G	140	244	0	-2	0	-0	3	1	0.00	0.01	0.01	
1H	140	244	0	-2	0	-0	3	1	0.00	0.01	0.01	
1I	140	-1477	-0	1	0	0	3	1	0.00	0.04	0.04	
1J	140	-1477	1	1	0	0	3	1	0.00	0.04	0.04	
1K	140	-1477	-0	-1	0	-0	3	1	0.00	0.04	0.04	
1L	140	-1477	1	-1	0	-0	3	1	0.00	0.04	0.04	
1M	140	909	-0	1	0	0	3	1	0.00	0.02	0.03	
1N	140	909	1	1	0	0	3	1	0.00	0.02	0.03	
1O	140	909	-0	-1	0	-0	3	1	0.00	0.02	0.03	
1P	140	909	1	-1	0	-0	3	1	0.00	0.02	0.03	
2	140	-425	0	-0	0	0	4	1	0.00	0.01	0.02	
3	140	-387	0	-0	0	0	4	1	0.00	0.01	0.02	
4	140	-353	0	-0	0	0	4	1	0.00	0.01	0.02	
5	140	-185	0	-0	0	0	4	1	0.00	0.00	0.01	
1A	280	-803	-13	2	0	-2	-6	1	0.00	0.02	0.03	
1B	280	-803	-13	2	0	-2	-6	1	0.00	0.02	0.03	
1C	280	-803	-13	-2	0	3	-6	1	0.00	0.02	0.03	
1D	280	-803	-13	-2	0	3	-6	1	0.00	0.02	0.03	
1E	280	252	-13	2	0	-2	-6	1	0.00	0.01	0.02	
1F	280	252	-13	2	0	-2	-6	1	0.00	0.01	0.02	
1G	280	252	-13	-2	0	3	-6	1	0.00	0.01	0.02	
1H	280	252	-13	-2	0	3	-6	1	0.00	0.01	0.02	
1I	280	-1468	-13	1	0	-0	-6	1	0.00	0.04	0.05	
1J	280	-1468	-13	1	0	-0	-6	1	0.00	0.04	0.05	

1K	280	-1468	-13	-1	0	1	-6	1	0.00	0.04	0.05
1L	280	-1468	-13	-1	0	1	-6	1	0.00	0.04	0.05
1M	280	917	-13	1	0	-0	-6	1	0.00	0.02	0.03
1N	280	917	-13	1	0	-0	-6	1	0.00	0.02	0.03
1O	280	917	-13	-1	0	1	-6	1	0.00	0.02	0.03
1P	280	917	-13	-1	0	1	-6	1	0.00	0.02	0.03
2	280	-415	-17	-0	0	0	-8	1	0.00	0.01	0.02
3	280	-376	-17	-0	0	0	-8	1	0.00	0.01	0.02
4	280	-342	-17	-0	0	0	-8	1	0.00	0.01	0.02
5	280	-174	-17	-0	0	0	-8	1	0.00	0.00	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-819	3	-6	1	0.2603	0.9418	1.1515	--	--	0.08	--	0.10	Snell. 'yx'= 145
1B	-819	3	-7	1	0.2603	0.9418	1.1625	--	--	0.08	--	0.10	Snell. 'yx'= 145
1C	-819	-3	-6	1	0.2603	0.9418	1.1515	--	--	0.08	--	0.10	Snell. 'yx'= 145
1D	-819	-3	-7	1	0.2603	0.9418	1.1625	--	--	0.08	--	0.10	Snell. 'yx'= 145
1I	-1485	1	-6	1	0.2603	0.8945	1.2746	--	--	0.15	--	0.16	Snell. 'yx'= 145
1J	-1485	1	-7	1	0.2603	0.8945	1.2963	--	--	0.15	--	0.16	Snell. 'yx'= 145
1K	-1485	-1	-6	1	0.2603	0.8945	1.2746	--	--	0.15	--	0.16	Snell. 'yx'= 145
1L	-1485	-1	-7	1	0.2603	0.8945	1.2963	--	--	0.15	--	0.16	Snell. 'yx'= 145
2	-436	0	-9	1	0.2603	0.9690	1.0892	--	--	0.04	--	0.06	Snell. 'yx'= 145
3	-398	0	-9	1	0.2603	0.9717	1.0814	--	--	0.04	--	0.05	Snell. 'yx'= 145
4	-364	0	-9	1	0.2603	0.9760	1.0744	--	--	0.04	--	0.05	Snell. 'yx'= 145
5	-196	0	-8	1	0.2603	0.9861	1.0400	--	--	0.02	--	0.03	Snell. 'yx'= 145

Elemento: **TRAVE** Metodo di verifica: **NTC 2018**
Gruppo: **1** Descrizione: **Pilastri**
Tabella: **Tabella pilastri**
Tipo acciaio: **S 275** Beta piano 'yx': **1.000** Beta piano 'zx': **1.000**
Coeff. k: **1.000** Coeff. kw: **1.000** Carico all'estradosso della trave
Coeff. riduzione dell'area: **0.000** Tipologia sismica yx: **Senza prescrizioni aggiuntive**
Tipologia sismica zx: **Senza prescrizioni aggiuntive**
γM0: **1.050** γM1': **1.050** γM1'': **1.050** γM2: **1.250** γrv: **0.000** γM0 Pf: **1.000** γM1 Pf: **1.000**
Tipo collegamento: **bullonato**
ASTA NUM. 1 NI 1 NF 42 Lungh. 148.0 cm SEZ. 1 Ps HEB 140
Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-602	-273	24	0	18	228	1	0.01	0.01	0.03	
1B	0	-602	202	24	0	18	-182	1	0.01	0.01	0.03	
1C	0	-602	-273	-9	0	-10	228	1	0.01	0.01	0.03	
1D	0	-602	202	-9	0	-10	-182	1	0.01	0.01	0.03	
1E	0	-22	-273	24	0	18	228	1	0.01	0.00	0.03	
1F	0	-22	202	24	0	18	-182	1	0.01	0.00	0.03	
1G	0	-22	-273	-9	0	-10	228	1	0.01	0.00	0.03	
1H	0	-22	202	-9	0	-10	-182	1	0.01	0.00	0.03	
1I	0	-448	-110	64	0	50	87	1	0.01	0.00	0.02	
1J	0	-448	39	64	0	50	-41	1	0.00	0.00	0.02	
1K	0	-448	-110	-48	0	-42	87	1	0.01	0.00	0.01	

1L	0	-448	39	-48	0	-42	-41	1	0.00	0.00	0.01
1M	0	-176	-110	64	0	50	87	1	0.01	0.00	0.02
1N	0	-176	39	64	0	50	-41	1	0.00	0.00	0.02
1O	0	-176	-110	-48	0	-42	87	1	0.01	0.00	0.01
1P	0	-176	39	-48	0	-42	-41	1	0.00	0.00	0.01
2	0	-452	-53	10	0	5	35	1	0.00	0.00	0.01
3	0	-421	-48	10	0	5	32	1	0.00	0.00	0.00
4	0	-398	64	10	0	5	-3	1	0.00	0.00	0.00
5	0	-389	-44	-43	0	-14	29	1	0.00	0.00	0.00
1A	74	-577	-273	24	0	-0	26	1	0.01	0.01	0.00
1B	74	-577	202	24	0	-0	-32	1	0.01	0.01	0.00
1C	74	-577	-273	-9	0	-3	26	1	0.01	0.01	0.00
1D	74	-577	202	-9	0	-3	-32	1	0.01	0.01	0.00
1E	74	3	-273	24	0	-0	26	1	0.01	0.00	0.00
1F	74	3	202	24	0	-0	-32	1	0.01	0.00	0.00
1G	74	3	-273	-9	0	-3	26	1	0.01	0.00	0.00
1H	74	3	202	-9	0	-3	-32	1	0.01	0.00	0.00
1I	74	-423	-110	64	0	3	6	1	0.01	0.00	0.00
1J	74	-423	39	64	0	3	-12	1	0.00	0.00	0.00
1K	74	-423	-110	-48	0	-7	6	1	0.01	0.00	0.00
1L	74	-423	39	-48	0	-7	-12	1	0.00	0.00	0.00
1M	74	-151	-110	64	0	3	6	1	0.01	0.00	0.00
1N	74	-151	39	64	0	3	-12	1	0.00	0.00	0.00
1O	74	-151	-110	-48	0	-7	6	1	0.01	0.00	0.00
1P	74	-151	39	-48	0	-7	-12	1	0.00	0.00	0.00
2	74	-420	-53	10	0	-2	-4	1	0.00	0.00	0.00
3	74	-388	-48	10	0	-2	-4	1	0.00	0.00	0.00
4	74	-366	-28	10	0	-2	10	1	0.00	0.00	0.00
5	74	-356	-44	-3	0	3	-4	1	0.00	0.00	0.00
1A	148	-552	-273	24	0	-18	-176	1	0.01	0.00	0.03
1B	148	-552	202	24	0	-18	118	1	0.01	0.00	0.02
1C	148	-552	-273	-9	0	4	-176	1	0.01	0.00	0.03
1D	148	-552	202	-9	0	4	118	1	0.01	0.00	0.02
1E	148	28	-273	24	0	-18	-176	1	0.01	0.00	0.03
1F	148	28	202	24	0	-18	118	1	0.01	0.00	0.02
1G	148	28	-273	-9	0	4	-176	1	0.01	0.00	0.03
1H	148	28	202	-9	0	4	118	1	0.01	0.00	0.02
1I	148	-398	-110	64	0	-44	-75	1	0.01	0.00	0.01
1J	148	-398	39	64	0	-44	17	1	0.00	0.00	0.01
1K	148	-398	-110	-48	0	29	-75	1	0.01	0.00	0.01
1L	148	-398	39	-48	0	29	17	1	0.00	0.00	0.01
1M	148	-126	-110	64	0	-44	-75	1	0.01	0.00	0.01
1N	148	-126	39	64	0	-44	17	1	0.00	0.00	0.01
1O	148	-126	-110	-48	0	29	-75	1	0.01	0.00	0.01
1P	148	-126	39	-48	0	29	17	1	0.00	0.00	0.01
2	148	-387	-53	10	0	-10	-44	1	0.00	0.00	0.01
3	148	-356	-48	10	0	-10	-40	1	0.00	0.00	0.01
4	148	-333	-121	10	0	-9	-45	1	0.01	0.00	0.01
5	148	-324	-44	36	0	-9	-36	1	0.00	0.00	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-602	-18	228	1	0.8534	0.9968	0.9985	0.9999	0.9931	0.01	0.04	0.05	Snell. 'zx'= 41

1B	-602	-18	-182	1	0.8534	0.9968	0.9989	1.0000	0.9925	0.01	0.03	0.04	Snell. 'zx'= 41
1C	-602	-10	228	1	0.8534	1.0011	0.9985	0.9999	0.9931	0.01	0.04	0.04	Snell. 'zx'= 41
1D	-602	-10	-182	1	0.8534	1.0011	0.9989	1.0000	0.9925	0.01	0.03	0.04	Snell. 'zx'= 41
1E	-22	-18	228	1	0.8534	0.9999	0.9999	1.0000	0.9931	0.00	0.04	0.04	Snell. 'zx'= 41
1F	-22	-18	-182	1	0.8534	0.9999	1.0000	1.0000	0.9925	0.00	0.03	0.03	Snell. 'zx'= 41
1G	-22	-10	228	1	0.8534	1.0000	0.9999	1.0000	0.9931	0.00	0.04	0.04	Snell. 'zx'= 41
1H	-22	-10	-182	1	0.8534	1.0000	1.0000	1.0000	0.9925	0.00	0.03	0.03	Snell. 'zx'= 41
1I	-448	50	87	1	0.8534	0.9967	0.9991	0.9999	0.9926	0.00	0.01	0.03	Snell. 'zx'= 41
1J	-448	50	-41	1	0.8534	0.9967	1.0003	0.9999	0.9898	0.00	0.01	0.03	Snell. 'zx'= 41
1K	-448	-42	87	1	0.8534	0.9973	0.9991	1.0000	0.9926	0.00	0.01	0.03	Snell. 'zx'= 41
1L	-448	-42	-41	1	0.8534	0.9973	1.0003	1.0000	0.9898	0.00	0.01	0.02	Snell. 'zx'= 41
1M	-176	50	87	1	0.8534	0.9987	0.9996	1.0000	0.9926	0.00	0.01	0.03	Snell. 'zx'= 41
1N	-176	50	-41	1	0.8534	0.9987	1.0001	1.0000	0.9898	0.00	0.01	0.02	Snell. 'zx'= 41
1O	-176	-42	87	1	0.8534	0.9989	0.9996	1.0000	0.9926	0.00	0.01	0.03	Snell. 'zx'= 41
1P	-176	-42	-41	1	0.8534	0.9989	1.0001	1.0000	0.9898	0.00	0.01	0.02	Snell. 'zx'= 41
2	-452	-10	-44	1	0.8534	1.0005	0.9997	1.0000	0.9929	0.00	0.01	0.01	Snell. 'zx'= 41
3	-421	-10	-40	1	0.8534	1.0005	0.9998	1.0000	0.9930	0.00	0.01	0.01	Snell. 'zx'= 41
4	-398	-9	-45	1	0.8534	1.0006	1.0006	1.0000	0.8921	0.00	0.01	0.01	Snell. 'zx'= 41
5	-389	-14	-36	1	0.8534	1.0005	0.9999	1.0000	0.9929	0.00	0.01	0.01	Snell. 'zx'= 41

ASTA NUM. 2 NI 2 NF 41 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1723	-282	27	0	19	235	1	0.01	0.02	0.04	
1B	0	-1723	263	27	0	19	-220	1	0.01	0.02	0.03	
1C	0	-1723	-282	-6	0	-8	235	1	0.01	0.02	0.04	
1D	0	-1723	263	-6	0	-8	-220	1	0.01	0.02	0.03	
1E	0	-1559	-282	27	0	19	235	1	0.01	0.01	0.04	
1F	0	-1559	263	27	0	19	-220	1	0.01	0.01	0.03	
1G	0	-1559	-282	-6	0	-8	235	1	0.01	0.01	0.04	
1H	0	-1559	263	-6	0	-8	-220	1	0.01	0.01	0.03	
1I	0	-1792	-100	63	0	49	83	1	0.00	0.02	0.02	
1J	0	-1792	80	63	0	49	-68	1	0.00	0.02	0.02	
1K	0	-1792	-100	-43	0	-39	83	1	0.00	0.02	0.01	
1L	0	-1792	80	-43	0	-39	-68	1	0.00	0.02	0.01	
1M	0	-1490	-100	63	0	49	83	1	0.00	0.01	0.02	
1N	0	-1490	80	63	0	49	-68	1	0.00	0.01	0.02	
1O	0	-1490	-100	-43	0	-39	83	1	0.00	0.01	0.01	
1P	0	-1490	80	-43	0	-39	-68	1	0.00	0.01	0.01	
2	0	-2449	-15	14	0	7	12	1	0.00	0.02	0.00	
3	0	-2236	-13	13	0	7	10	1	0.00	0.02	0.00	
4	0	-2023	-6	13	0	7	4	1	0.00	0.02	0.00	
5	0	-2033	-12	-189	0	-52	9	1	0.00	0.02	0.02	
1A	74	-1698	-282	27	0	-1	27	1	0.01	0.01	0.00	
1B	74	-1698	263	27	0	-1	-26	1	0.01	0.01	0.00	
1C	74	-1698	-282	-6	0	-4	27	1	0.01	0.01	0.00	
1D	74	-1698	263	-6	0	-4	-26	1	0.01	0.01	0.00	
1E	74	-1534	-282	27	0	-1	27	1	0.01	0.01	0.00	
1F	74	-1534	263	27	0	-1	-26	1	0.01	0.01	0.00	
1G	74	-1534	-282	-6	0	-4	27	1	0.01	0.01	0.00	
1H	74	-1534	263	-6	0	-4	-26	1	0.01	0.01	0.00	
1I	74	-1767	-100	63	0	2	9	1	0.00	0.02	0.00	
1J	74	-1767	80	63	0	2	-8	1	0.00	0.02	0.00	
1K	74	-1767	-100	-43	0	-7	9	1	0.00	0.02	0.00	

1L	74	-1767	80	-43	0	-7	-8	1	0.00	0.02	0.00
1M	74	-1465	-100	63	0	2	9	1	0.00	0.01	0.00
1N	74	-1465	80	63	0	2	-8	1	0.00	0.01	0.00
1O	74	-1465	-100	-43	0	-7	9	1	0.00	0.01	0.00
1P	74	-1465	80	-43	0	-7	-8	1	0.00	0.01	0.00
2	74	-2417	-15	14	0	-3	1	1	0.00	0.02	0.00
3	74	-2204	-13	13	0	-3	1	1	0.00	0.02	0.00
4	74	-1991	-6	13	0	-3	0	1	0.00	0.02	0.00
5	74	-2001	-12	-13	0	23	1	1	0.00	0.02	0.01
1A	148	-1673	-282	27	0	-21	-182	1	0.01	0.01	0.03
1B	148	-1673	263	27	0	-21	169	1	0.01	0.01	0.03
1C	148	-1673	-282	-6	0	1	-182	1	0.01	0.01	0.03
1D	148	-1673	263	-6	0	1	169	1	0.01	0.01	0.03
1E	148	-1509	-282	27	0	-21	-182	1	0.01	0.01	0.03
1F	148	-1509	263	27	0	-21	169	1	0.01	0.01	0.03
1G	148	-1509	-282	-6	0	1	-182	1	0.01	0.01	0.03
1H	148	-1509	263	-6	0	1	169	1	0.01	0.01	0.03
1I	148	-1742	-100	63	0	-44	-65	1	0.00	0.02	0.01
1J	148	-1742	80	63	0	-44	51	1	0.00	0.02	0.01
1K	148	-1742	-100	-43	0	25	-65	1	0.00	0.02	0.01
1L	148	-1742	80	-43	0	25	51	1	0.00	0.02	0.01
1M	148	-1440	-100	63	0	-44	-65	1	0.00	0.01	0.01
1N	148	-1440	80	63	0	-44	51	1	0.00	0.01	0.01
1O	148	-1440	-100	-43	0	25	-65	1	0.00	0.01	0.01
1P	148	-1440	80	-43	0	25	51	1	0.00	0.01	0.01
2	148	-2384	-15	14	0	-14	-10	1	0.00	0.02	0.00
3	148	-2171	-13	13	0	-13	-9	1	0.00	0.02	0.00
4	148	-1958	-6	13	0	-12	-4	1	0.00	0.02	0.00
5	148	-1968	-12	164	0	-33	-8	1	0.00	0.02	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-1723	-21	235	1	0.8534	1.0144	0.9951	0.9997	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1B	-1723	-21	-220	1	0.8534	1.0144	0.9951	0.9997	0.9932	0.02	0.03	0.06	Snell. 'zx'= 41
1C	-1723	-8	235	1	0.8534	1.0577	0.9951	0.9997	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1D	-1723	-8	-220	1	0.8534	1.0577	0.9951	0.9997	0.9932	0.02	0.03	0.05	Snell. 'zx'= 41
1E	-1559	-21	235	1	0.8534	1.0130	0.9955	0.9997	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1F	-1559	-21	-220	1	0.8534	1.0130	0.9956	0.9997	0.9932	0.02	0.03	0.06	Snell. 'zx'= 41
1G	-1559	-8	235	1	0.8534	1.0522	0.9955	0.9997	0.9931	0.02	0.04	0.05	Snell. 'zx'= 41
1H	-1559	-8	-220	1	0.8534	1.0522	0.9956	0.9997	0.9932	0.02	0.03	0.05	Snell. 'zx'= 41
1I	-1792	49	83	1	0.8534	0.9967	0.9948	0.9997	0.9931	0.02	0.01	0.05	Snell. 'zx'= 41
1J	-1792	49	-68	1	0.8534	0.9967	0.9950	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1K	-1792	-39	83	1	0.8534	1.0029	0.9948	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
1L	-1792	-39	-68	1	0.8534	1.0029	0.9950	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1M	-1490	49	83	1	0.8534	0.9973	0.9957	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
1N	-1490	49	-68	1	0.8534	0.9973	0.9958	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1O	-1490	-39	83	1	0.8534	1.0024	0.9957	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
1P	-1490	-39	-68	1	0.8534	1.0024	0.9958	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
2	-2449	-14	11	1	0.8534	1.0460	0.9920	0.9994	0.9924	0.02	0.00	0.03	Snell. 'zx'= 41
3	-2236	-13	10	1	0.8534	1.0444	0.9927	0.9995	0.9924	0.02	0.00	0.03	Snell. 'zx'= 41
4	-2023	-12	-4	1	0.8534	1.0426	0.9926	0.9994	0.9917	0.02	0.00	0.03	Snell. 'zx'= 41
5	-2033	-52	9	1	0.8534	1.0026	0.9934	0.9995	0.9924	0.02	0.00	0.04	Snell. 'zx'= 41

ASTA NUM. 3 NI 3 NF 40 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1332	-215	24	0	17	206	1	0.01	0.01	0.03	
1B	0	-1332	379	24	0	17	-275	1	0.02	0.01	0.04	
1C	0	-1332	-215	-6	0	-8	206	1	0.01	0.01	0.03	
1D	0	-1332	379	-6	0	-8	-275	1	0.02	0.01	0.04	
1E	0	-882	-215	24	0	17	206	1	0.01	0.01	0.03	
1F	0	-882	379	24	0	17	-275	1	0.02	0.01	0.04	
1G	0	-882	-215	-6	0	-8	206	1	0.01	0.01	0.03	
1H	0	-882	379	-6	0	-8	-275	1	0.02	0.01	0.04	
1I	0	-1299	-21	57	0	45	50	1	0.00	0.01	0.01	
1J	0	-1299	186	57	0	45	-118	1	0.01	0.01	0.02	
1K	0	-1299	-21	-39	0	-35	50	1	0.00	0.01	0.01	
1L	0	-1299	186	-39	0	-35	-118	1	0.01	0.01	0.02	
1M	0	-915	-21	57	0	45	50	1	0.00	0.01	0.01	
1N	0	-915	186	57	0	45	-118	1	0.01	0.01	0.02	
1O	0	-915	-21	-39	0	-35	50	1	0.00	0.01	0.01	
1P	0	-915	186	-39	0	-35	-118	1	0.01	0.01	0.02	
2	0	-1646	124	13	0	7	-51	1	0.01	0.01	0.01	
3	0	-1506	112	12	0	6	-47	1	0.01	0.01	0.01	
4	0	-1362	108	12	0	6	-47	1	0.01	0.01	0.01	
5	0	-1372	102	-135	0	-37	-42	1	0.01	0.01	0.01	
1A	74	-1307	-215	24	0	-1	47	1	0.01	0.01	0.01	
1B	74	-1307	379	24	0	-1	6	1	0.02	0.01	0.00	
1C	74	-1307	-215	-6	0	-3	47	1	0.01	0.01	0.01	
1D	74	-1307	379	-6	0	-3	6	1	0.02	0.01	0.00	
1E	74	-857	-215	24	0	-1	47	1	0.01	0.01	0.01	
1F	74	-857	379	24	0	-1	6	1	0.02	0.01	0.00	
1G	74	-857	-215	-6	0	-3	47	1	0.01	0.01	0.01	
1H	74	-857	379	-6	0	-3	6	1	0.02	0.01	0.00	
1I	74	-1274	-21	57	0	2	34	1	0.00	0.01	0.01	
1J	74	-1274	186	57	0	2	19	1	0.01	0.01	0.00	
1K	74	-1274	-21	-39	0	-6	34	1	0.00	0.01	0.01	
1L	74	-1274	186	-39	0	-6	19	1	0.01	0.01	0.00	
1M	74	-890	-21	57	0	2	34	1	0.00	0.01	0.01	
1N	74	-890	186	57	0	2	19	1	0.01	0.01	0.00	
1O	74	-890	-21	-39	0	-6	34	1	0.00	0.01	0.01	
1P	74	-890	186	-39	0	-6	19	1	0.01	0.01	0.00	
2	74	-1614	124	13	0	-3	40	1	0.01	0.01	0.01	
3	74	-1474	112	12	0	-3	36	1	0.01	0.01	0.01	
4	74	-1330	108	12	0	-3	32	1	0.01	0.01	0.00	
5	74	-1340	102	-8	0	16	33	1	0.01	0.01	0.00	
1A	148	-1282	-215	24	0	-19	-112	1	0.01	0.01	0.02	
1B	148	-1282	379	24	0	-19	287	1	0.02	0.01	0.04	
1C	148	-1282	-215	-6	0	1	-112	1	0.01	0.01	0.02	
1D	148	-1282	379	-6	0	1	287	1	0.02	0.01	0.04	
1E	148	-832	-215	24	0	-19	-112	1	0.01	0.01	0.02	
1F	148	-832	379	24	0	-19	287	1	0.02	0.01	0.04	
1G	148	-832	-215	-6	0	1	-112	1	0.01	0.01	0.02	
1H	148	-832	379	-6	0	1	287	1	0.02	0.01	0.04	
1I	148	-1249	-21	57	0	-40	18	1	0.00	0.01	0.01	
1J	148	-1249	186	57	0	-40	157	1	0.01	0.01	0.02	
1K	148	-1249	-21	-39	0	22	18	1	0.00	0.01	0.01	

1L	148	-1249	186	-39	0	22	157	1	0.01	0.01	0.02
1M	148	-865	-21	57	0	-40	18	1	0.00	0.01	0.01
1N	148	-865	186	57	0	-40	157	1	0.01	0.01	0.02
1O	148	-865	-21	-39	0	22	18	1	0.00	0.01	0.01
1P	148	-865	186	-39	0	22	157	1	0.01	0.01	0.02
2	148	-1581	124	13	0	-12	132	1	0.01	0.01	0.02
3	148	-1441	112	12	0	-12	120	1	0.01	0.01	0.02
4	148	-1297	108	12	0	-11	112	1	0.01	0.01	0.02
5	148	-1308	102	119	0	-25	108	1	0.01	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-1332	-19	206	1	0.8534	1.0060	0.9973	0.9999	0.9915	0.01	0.03	0.05	Snell. 'zx'= 41
1B	-1332	-19	287	1	0.8534	1.0060	0.9953	0.9996	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1C	-1332	-8	206	1	0.8534	1.0333	0.9973	0.9999	0.9915	0.01	0.03	0.05	Snell. 'zx'= 41
1D	-1332	-8	287	1	0.8534	1.0333	0.9953	0.9996	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1E	-882	-19	206	1	0.8534	1.0040	0.9982	0.9999	0.9915	0.01	0.03	0.05	Snell. 'zx'= 41
1F	-882	-19	287	1	0.8534	1.0040	0.9969	0.9998	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1G	-882	-8	206	1	0.8534	1.0220	0.9982	0.9999	0.9915	0.01	0.03	0.04	Snell. 'zx'= 41
1H	-882	-8	287	1	0.8534	1.0220	0.9969	0.9998	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1I	-1299	45	50	1	0.8534	0.9956	1.0014	1.0000	0.9710	0.01	0.01	0.03	Snell. 'zx'= 41
1J	-1299	45	157	1	0.8534	0.9956	0.9964	0.9998	0.9932	0.01	0.02	0.05	Snell. 'zx'= 41
1K	-1299	-35	50	1	0.8534	0.9996	1.0014	1.0000	0.9710	0.01	0.01	0.03	Snell. 'zx'= 41
1L	-1299	-35	157	1	0.8534	0.9996	0.9964	0.9998	0.9932	0.01	0.02	0.05	Snell. 'zx'= 41
1M	-915	45	50	1	0.8534	0.9969	1.0010	1.0000	0.9710	0.01	0.01	0.03	Snell. 'zx'= 41
1N	-915	45	157	1	0.8534	0.9969	0.9974	0.9998	0.9932	0.01	0.02	0.05	Snell. 'zx'= 41
1O	-915	-35	50	1	0.8534	0.9997	1.0010	1.0000	0.9710	0.01	0.01	0.03	Snell. 'zx'= 41
1P	-915	-35	157	1	0.8534	0.9997	0.9974	0.9998	0.9932	0.01	0.02	0.04	Snell. 'zx'= 41
2	-1646	-12	132	1	0.8534	1.0226	0.9975	1.0000	0.9893	0.02	0.02	0.04	Snell. 'zx'= 41
3	-1506	-12	120	1	0.8534	1.0218	0.9977	1.0000	0.9893	0.02	0.02	0.04	Snell. 'zx'= 41
4	-1362	-11	112	1	0.8534	1.0208	0.9978	1.0000	0.9898	0.01	0.02	0.03	Snell. 'zx'= 41
5	-1372	-37	108	1	0.8534	1.0018	0.9979	1.0000	0.9893	0.01	0.02	0.04	Snell. 'zx'= 41

ASTA NUM. 4 NI 4 NF 39 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
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	cm	daN			daN*m							
1A	0	-1887	-251	27	0	18	214	1	0.01	0.02	0.03	
1B	0	-1887	275	27	0	18	-225	1	0.01	0.02	0.03	
1C	0	-1887	-251	-4	0	-6	214	1	0.01	0.02	0.03	
1D	0	-1887	275	-4	0	-6	-225	1	0.01	0.02	0.03	
1E	0	-1309	-251	27	0	18	214	1	0.01	0.01	0.03	
1F	0	-1309	275	27	0	18	-225	1	0.01	0.01	0.03	
1G	0	-1309	-251	-4	0	-6	214	1	0.01	0.01	0.03	
1H	0	-1309	275	-4	0	-6	-225	1	0.01	0.01	0.03	
1I	0	-2404	-77	50	0	38	68	1	0.00	0.02	0.01	
1J	0	-2404	101	50	0	38	-79	1	0.00	0.02	0.01	
1K	0	-2404	-77	-28	0	-27	68	1	0.00	0.02	0.01	
1L	0	-2404	101	-28	0	-27	-79	1	0.00	0.02	0.01	
1M	0	-792	-77	50	0	38	68	1	0.00	0.01	0.01	
1N	0	-792	101	50	0	38	-79	1	0.00	0.01	0.01	

1O	0	-792	-77	-28	0	-27	68	1	0.00	0.01	0.01
1P	0	-792	101	-28	0	-27	-79	1	0.00	0.01	0.01
2	0	-2382	18	15	0	8	-8	1	0.00	0.02	0.00
3	0	-2176	16	15	0	8	-7	1	0.00	0.02	0.00
4	0	-1969	21	14	0	7	-11	1	0.00	0.02	0.00
5	0	-1896	15	-190	0	-51	-7	1	0.00	0.02	0.02
1A	74	-1862	-251	27	0	-2	29	1	0.01	0.02	0.00
1B	74	-1862	275	27	0	-2	-21	1	0.01	0.02	0.00
1C	74	-1862	-251	-4	0	-3	29	1	0.01	0.02	0.00
1D	74	-1862	275	-4	0	-3	-21	1	0.01	0.02	0.00
1E	74	-1284	-251	27	0	-2	29	1	0.01	0.01	0.00
1F	74	-1284	275	27	0	-2	-21	1	0.01	0.01	0.00
1G	74	-1284	-251	-4	0	-3	29	1	0.01	0.01	0.00
1H	74	-1284	275	-4	0	-3	-21	1	0.01	0.01	0.00
1I	74	-2379	-77	50	0	1	12	1	0.00	0.02	0.00
1J	74	-2379	101	50	0	1	-4	1	0.00	0.02	0.00
1K	74	-2379	-77	-28	0	-6	12	1	0.00	0.02	0.00
1L	74	-2379	101	-28	0	-6	-4	1	0.00	0.02	0.00
1M	74	-767	-77	50	0	1	12	1	0.00	0.01	0.00
1N	74	-767	101	50	0	1	-4	1	0.00	0.01	0.00
1O	74	-767	-77	-28	0	-6	12	1	0.00	0.01	0.00
1P	74	-767	101	-28	0	-6	-4	1	0.00	0.01	0.00
2	74	-2350	18	15	0	-4	6	1	0.00	0.02	0.00
3	74	-2144	16	15	0	-4	5	1	0.00	0.02	0.00
4	74	-1937	21	14	0	-3	4	1	0.00	0.02	0.00
5	74	-1864	15	-9	0	23	5	1	0.00	0.02	0.01
1A	148	-1837	-251	27	0	-22	-157	1	0.01	0.02	0.02
1B	148	-1837	275	27	0	-22	183	1	0.01	0.02	0.03
1C	148	-1837	-251	-4	0	0	-157	1	0.01	0.02	0.02
1D	148	-1837	275	-4	0	0	183	1	0.01	0.02	0.03
1E	148	-1259	-251	27	0	-22	-157	1	0.01	0.01	0.02
1F	148	-1259	275	27	0	-22	183	1	0.01	0.01	0.03
1G	148	-1259	-251	-4	0	0	-157	1	0.01	0.01	0.02
1H	148	-1259	275	-4	0	0	183	1	0.01	0.01	0.03
1I	148	-2354	-77	50	0	-37	-45	1	0.00	0.02	0.01
1J	148	-2354	101	50	0	-37	70	1	0.00	0.02	0.01
1K	148	-2354	-77	-28	0	14	-45	1	0.00	0.02	0.01
1L	148	-2354	101	-28	0	14	70	1	0.00	0.02	0.01
1M	148	-742	-77	50	0	-37	-45	1	0.00	0.01	0.01
1N	148	-742	101	50	0	-37	70	1	0.00	0.01	0.01
1O	148	-742	-77	-28	0	14	-45	1	0.00	0.01	0.01
1P	148	-742	101	-28	0	14	70	1	0.00	0.01	0.01
2	148	-2317	18	15	0	-15	19	1	0.00	0.02	0.00
3	148	-2111	16	15	0	-15	17	1	0.00	0.02	0.00
4	148	-1904	21	14	0	-14	19	1	0.00	0.02	0.00
5	148	-1831	15	173	0	-38	16	1	0.00	0.02	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	-1887	-22	214	1	0.8534	1.0150	0.9949	0.9997	0.9931	0.02	0.03	0.06	Snell. 'zx'= 41
1B	-1887	-22	-225	1	0.8534	1.0150	0.9943	0.9996	0.9929	0.02	0.03	0.06	Snell. 'zx'= 41
1C	-1887	-6	214	1	0.8534	1.0872	0.9949	0.9997	0.9931	0.02	0.03	0.05	Snell. 'zx'= 41
1D	-1887	-6	-225	1	0.8534	1.0872	0.9943	0.9996	0.9929	0.02	0.03	0.06	Snell. 'zx'= 41

1E	-1309	-22	214	1	0.8534	1.0104	0.9964	0.9998	0.9931	0.01	0.03	0.05	Snell. 'zx'= 41
1F	-1309	-22	-225	1	0.8534	1.0104	0.9961	0.9997	0.9929	0.01	0.03	0.05	Snell. 'zx'= 41
1G	-1309	-6	214	1	0.8534	1.0605	0.9964	0.9998	0.9931	0.01	0.03	0.05	Snell. 'zx'= 41
1H	-1309	-6	-225	1	0.8534	1.0605	0.9961	0.9997	0.9929	0.01	0.03	0.05	Snell. 'zx'= 41
1I	-2404	38	68	1	0.8534	1.0006	0.9941	0.9997	0.9925	0.02	0.01	0.05	Snell. 'zx'= 41
1J	-2404	38	-79	1	0.8534	1.0006	0.9921	0.9994	0.9924	0.02	0.01	0.05	Snell. 'zx'= 41
1K	-2404	-27	68	1	0.8534	1.0158	0.9941	0.9997	0.9925	0.02	0.01	0.04	Snell. 'zx'= 41
1L	-2404	-27	-79	1	0.8534	1.0158	0.9921	0.9994	0.9924	0.02	0.01	0.04	Snell. 'zx'= 41
1M	-792	38	68	1	0.8534	1.0002	0.9981	0.9999	0.9925	0.01	0.01	0.03	Snell. 'zx'= 41
1N	-792	38	-79	1	0.8534	1.0002	0.9974	0.9998	0.9924	0.01	0.01	0.03	Snell. 'zx'= 41
1O	-792	-27	68	1	0.8534	1.0052	0.9981	0.9999	0.9925	0.01	0.01	0.03	Snell. 'zx'= 41
1P	-792	-27	-79	1	0.8534	1.0052	0.9974	0.9998	0.9924	0.01	0.01	0.03	Snell. 'zx'= 41
2	-2382	-15	19	1	0.8534	1.0404	0.9962	1.0000	0.9896	0.02	0.00	0.03	Snell. 'zx'= 41
3	-2176	-15	17	1	0.8534	1.0384	0.9965	1.0000	0.9896	0.02	0.00	0.03	Snell. 'zx'= 41
4	-1969	-14	19	1	0.8534	1.0364	0.9957	0.9998	0.9919	0.02	0.00	0.03	Snell. 'zx'= 41
5	-1896	-51	16	1	0.8534	1.0026	0.9969	1.0000	0.9897	0.02	0.00	0.04	Snell. 'zx'= 41

ASTA NUM. 5 NI 5 NF 38 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1887	-275	27	0	18	225	1	0.01	0.02	0.03	
1B	0	-1887	251	27	0	18	-214	1	0.01	0.02	0.03	
1C	0	-1887	-275	-4	0	-6	225	1	0.01	0.02	0.03	
1D	0	-1887	251	-4	0	-6	-214	1	0.01	0.02	0.03	
1E	0	-1309	-275	27	0	18	225	1	0.01	0.01	0.03	
1F	0	-1309	251	27	0	18	-214	1	0.01	0.01	0.03	
1G	0	-1309	-275	-4	0	-6	225	1	0.01	0.01	0.03	
1H	0	-1309	251	-4	0	-6	-214	1	0.01	0.01	0.03	
1I	0	-2404	-101	50	0	38	79	1	0.00	0.02	0.01	
1J	0	-2404	77	50	0	38	-68	1	0.00	0.02	0.01	
1K	0	-2404	-101	-28	0	-27	79	1	0.00	0.02	0.01	
1L	0	-2404	77	-28	0	-27	-68	1	0.00	0.02	0.01	
1M	0	-792	-101	50	0	38	79	1	0.00	0.01	0.01	
1N	0	-792	77	50	0	38	-68	1	0.00	0.01	0.01	
1O	0	-792	-101	-28	0	-27	79	1	0.00	0.01	0.01	
1P	0	-792	77	-28	0	-27	-68	1	0.00	0.01	0.01	
2	0	-2382	-18	15	0	8	8	1	0.00	0.02	0.00	
3	0	-2176	-16	15	0	8	7	1	0.00	0.02	0.00	
4	0	-1971	-9	15	0	7	1	1	0.00	0.02	0.00	
5	0	-1901	-17	-190	0	-50	8	1	0.00	0.02	0.02	
1A	74	-1862	-275	27	0	-2	21	1	0.01	0.02	0.00	
1B	74	-1862	251	27	0	-2	-29	1	0.01	0.02	0.00	
1C	74	-1862	-275	-4	0	-3	21	1	0.01	0.02	0.00	
1D	74	-1862	251	-4	0	-3	-29	1	0.01	0.02	0.00	
1E	74	-1284	-275	27	0	-2	21	1	0.01	0.01	0.00	
1F	74	-1284	251	27	0	-2	-29	1	0.01	0.01	0.00	
1G	74	-1284	-275	-4	0	-3	21	1	0.01	0.01	0.00	
1H	74	-1284	251	-4	0	-3	-29	1	0.01	0.01	0.00	
1I	74	-2379	-101	50	0	1	4	1	0.00	0.02	0.00	
1J	74	-2379	77	50	0	1	-12	1	0.00	0.02	0.00	
1K	74	-2379	-101	-28	0	-6	4	1	0.00	0.02	0.00	
1L	74	-2379	77	-28	0	-6	-12	1	0.00	0.02	0.00	
1M	74	-767	-101	50	0	1	4	1	0.00	0.01	0.00	

1N	74	-767	77	50	0	1	-12	1	0.00	0.01	0.00
1O	74	-767	-101	-28	0	-6	4	1	0.00	0.01	0.00
1P	74	-767	77	-28	0	-6	-12	1	0.00	0.01	0.00
2	74	-2350	-18	15	0	-4	-6	1	0.00	0.02	0.00
3	74	-2144	-16	15	0	-4	-5	1	0.00	0.02	0.00
4	74	-1939	-9	15	0	-3	-5	1	0.00	0.02	0.00
5	74	-1869	-17	-8	0	23	-4	1	0.00	0.02	0.01
1A	148	-1837	-275	27	0	-22	-183	1	0.01	0.02	0.03
1B	148	-1837	251	27	0	-22	157	1	0.01	0.02	0.02
1C	148	-1837	-275	-4	0	0	-183	1	0.01	0.02	0.03
1D	148	-1837	251	-4	0	0	157	1	0.01	0.02	0.02
1E	148	-1259	-275	27	0	-22	-183	1	0.01	0.01	0.03
1F	148	-1259	251	27	0	-22	157	1	0.01	0.01	0.02
1G	148	-1259	-275	-4	0	0	-183	1	0.01	0.01	0.03
1H	148	-1259	251	-4	0	0	157	1	0.01	0.01	0.02
1I	148	-2354	-101	50	0	-37	-70	1	0.00	0.02	0.01
1J	148	-2354	77	50	0	-37	45	1	0.00	0.02	0.01
1K	148	-2354	-101	-28	0	14	-70	1	0.00	0.02	0.01
1L	148	-2354	77	-28	0	14	45	1	0.00	0.02	0.01
1M	148	-742	-101	50	0	-37	-70	1	0.00	0.01	0.01
1N	148	-742	77	50	0	-37	45	1	0.00	0.01	0.01
1O	148	-742	-101	-28	0	14	-70	1	0.00	0.01	0.01
1P	148	-742	77	-28	0	14	45	1	0.00	0.01	0.01
2	148	-2317	-18	15	0	-15	-19	1	0.00	0.02	0.00
3	148	-2111	-16	15	0	-15	-17	1	0.00	0.02	0.00
4	148	-1906	-9	15	0	-14	-12	1	0.00	0.02	0.00
5	148	-1836	-17	173	0	-38	-17	1	0.00	0.02	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	-1887	-22	225	1	0.8534	1.0150	0.9943	0.9996	0.9929	0.02	0.03	0.06	Snell. 'zx'= 41
1B	-1887	-22	-214	1	0.8534	1.0150	0.9949	0.9997	0.9931	0.02	0.03	0.06	Snell. 'zx'= 41
1C	-1887	-6	225	1	0.8534	1.0872	0.9943	0.9996	0.9929	0.02	0.03	0.06	Snell. 'zx'= 41
1D	-1887	-6	-214	1	0.8534	1.0872	0.9949	0.9997	0.9931	0.02	0.03	0.05	Snell. 'zx'= 41
1E	-1309	-22	225	1	0.8534	1.0104	0.9961	0.9997	0.9929	0.01	0.03	0.05	Snell. 'zx'= 41
1F	-1309	-22	-214	1	0.8534	1.0104	0.9964	0.9998	0.9931	0.01	0.03	0.05	Snell. 'zx'= 41
1G	-1309	-6	225	1	0.8534	1.0605	0.9961	0.9997	0.9929	0.01	0.03	0.05	Snell. 'zx'= 41
1H	-1309	-6	-214	1	0.8534	1.0605	0.9964	0.9998	0.9931	0.01	0.03	0.05	Snell. 'zx'= 41
1I	-2404	38	79	1	0.8534	1.0006	0.9921	0.9994	0.9924	0.02	0.01	0.05	Snell. 'zx'= 41
1J	-2404	38	-68	1	0.8534	1.0006	0.9941	0.9997	0.9925	0.02	0.01	0.05	Snell. 'zx'= 41
1K	-2404	-27	79	1	0.8534	1.0158	0.9921	0.9994	0.9924	0.02	0.01	0.04	Snell. 'zx'= 41
1L	-2404	-27	-68	1	0.8534	1.0158	0.9941	0.9997	0.9925	0.02	0.01	0.04	Snell. 'zx'= 41
1M	-792	38	79	1	0.8534	1.0002	0.9974	0.9998	0.9924	0.01	0.01	0.03	Snell. 'zx'= 41
1N	-792	38	-68	1	0.8534	1.0002	0.9981	0.9999	0.9925	0.01	0.01	0.03	Snell. 'zx'= 41
1O	-792	-27	79	1	0.8534	1.0052	0.9974	0.9998	0.9924	0.01	0.01	0.03	Snell. 'zx'= 41
1P	-792	-27	-68	1	0.8534	1.0052	0.9981	0.9999	0.9925	0.01	0.01	0.03	Snell. 'zx'= 41
2	-2382	-15	-19	1	0.8534	1.0404	0.9962	1.0000	0.9896	0.02	0.00	0.03	Snell. 'zx'= 41
3	-2176	-15	-17	1	0.8534	1.0384	0.9965	1.0000	0.9896	0.02	0.00	0.03	Snell. 'zx'= 41
4	-1971	-14	-12	1	0.8534	1.0358	0.9989	1.0000	0.9834	0.02	0.00	0.03	Snell. 'zx'= 41
5	-1901	-50	-17	1	0.8534	1.0026	0.9965	0.9999	0.9908	0.02	0.00	0.04	Snell. 'zx'= 41

ASTA NUM. 6 NI 6 NF 37 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

STARENERGIA

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm		daN			daN*m						
1A	0	-1323	-203	24	0	17	199	1	0.01	0.01	0.03	
1B	0	-1323	388	24	0	17	-279	1	0.02	0.01	0.04	
1C	0	-1323	-203	-6	0	-8	199	1	0.01	0.01	0.03	
1D	0	-1323	388	-6	0	-8	-279	1	0.02	0.01	0.04	
1E	0	-971	-203	24	0	17	199	1	0.01	0.01	0.03	
1F	0	-971	388	24	0	17	-279	1	0.02	0.01	0.04	
1G	0	-971	-203	-6	0	-8	199	1	0.01	0.01	0.03	
1H	0	-971	388	-6	0	-8	-279	1	0.02	0.01	0.04	
1I	0	-1321	-14	55	0	42	45	1	0.00	0.01	0.01	
1J	0	-1321	198	55	0	42	-126	1	0.01	0.01	0.02	
1K	0	-1321	-14	-36	0	-33	45	1	0.00	0.01	0.01	
1L	0	-1321	198	-36	0	-33	-126	1	0.01	0.01	0.02	
1M	0	-973	-14	55	0	42	45	1	0.00	0.01	0.01	
1N	0	-973	198	55	0	42	-126	1	0.01	0.01	0.02	
1O	0	-973	-14	-36	0	-33	45	1	0.00	0.01	0.01	
1P	0	-973	198	-36	0	-33	-126	1	0.01	0.01	0.02	
2	0	-1707	139	13	0	7	-60	1	0.01	0.01	0.01	
3	0	-1561	126	12	0	6	-55	1	0.01	0.01	0.01	
4	0	-1412	120	12	0	6	-54	1	0.01	0.01	0.01	
5	0	-1425	110	-136	0	-37	-47	1	0.01	0.01	0.01	
1A	74	-1298	-203	24	0	-1	49	1	0.01	0.01	0.01	
1B	74	-1298	388	24	0	-1	7	1	0.02	0.01	0.00	
1C	74	-1298	-203	-6	0	-3	49	1	0.01	0.01	0.01	
1D	74	-1298	388	-6	0	-3	7	1	0.02	0.01	0.00	
1E	74	-946	-203	24	0	-1	49	1	0.01	0.01	0.01	
1F	74	-946	388	24	0	-1	7	1	0.02	0.01	0.00	
1G	74	-946	-203	-6	0	-3	49	1	0.01	0.01	0.01	
1H	74	-946	388	-6	0	-3	7	1	0.02	0.01	0.00	
1I	74	-1296	-14	55	0	2	35	1	0.00	0.01	0.01	
1J	74	-1296	198	55	0	2	21	1	0.01	0.01	0.00	
1K	74	-1296	-14	-36	0	-6	35	1	0.00	0.01	0.01	
1L	74	-1296	198	-36	0	-6	21	1	0.01	0.01	0.00	
1M	74	-948	-14	55	0	2	35	1	0.00	0.01	0.01	
1N	74	-948	198	55	0	2	21	1	0.01	0.01	0.00	
1O	74	-948	-14	-36	0	-6	35	1	0.00	0.01	0.01	
1P	74	-948	198	-36	0	-6	21	1	0.01	0.01	0.00	
2	74	-1675	139	13	0	-3	43	1	0.01	0.01	0.01	
3	74	-1529	126	12	0	-3	39	1	0.01	0.01	0.01	
4	74	-1380	120	12	0	-3	34	1	0.01	0.01	0.01	
5	74	-1393	110	-7	0	16	35	1	0.01	0.01	0.01	
1A	148	-1273	-203	24	0	-19	-101	1	0.01	0.01	0.02	
1B	148	-1273	388	24	0	-19	294	1	0.02	0.01	0.04	
1C	148	-1273	-203	-6	0	1	-101	1	0.01	0.01	0.02	
1D	148	-1273	388	-6	0	1	294	1	0.02	0.01	0.04	
1E	148	-921	-203	24	0	-19	-101	1	0.01	0.01	0.02	
1F	148	-921	388	24	0	-19	294	1	0.02	0.01	0.04	
1G	148	-921	-203	-6	0	1	-101	1	0.01	0.01	0.02	
1H	148	-921	388	-6	0	1	294	1	0.02	0.01	0.04	
1I	148	-1271	-14	55	0	-38	25	1	0.00	0.01	0.01	
1J	148	-1271	198	55	0	-38	168	1	0.01	0.01	0.03	
1K	148	-1271	-14	-36	0	21	25	1	0.00	0.01	0.01	
1L	148	-1271	198	-36	0	21	168	1	0.01	0.01	0.03	
1M	148	-923	-14	55	0	-38	25	1	0.00	0.01	0.01	

1N	148	-923	198	55	0	-38	168	1	0.01	0.01	0.03
1O	148	-923	-14	-36	0	21	25	1	0.00	0.01	0.01
1P	148	-923	198	-36	0	21	168	1	0.01	0.01	0.03
2	148	-1642	139	13	0	-12	145	1	0.01	0.01	0.02
3	148	-1496	126	12	0	-12	132	1	0.01	0.01	0.02
4	148	-1347	120	12	0	-11	123	1	0.01	0.01	0.02
5	148	-1360	110	123	0	-27	117	1	0.01	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-1323	-19	199	1	0.8534	1.0066	0.9974	0.9999	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41
1B	-1323	-19	294	1	0.8534	1.0066	0.9954	0.9996	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1C	-1323	-8	199	1	0.8534	1.0353	0.9974	0.9999	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41
1D	-1323	-8	294	1	0.8534	1.0353	0.9954	0.9996	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1E	-971	-19	199	1	0.8534	1.0048	0.9981	0.9999	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41
1F	-971	-19	294	1	0.8534	1.0048	0.9966	0.9997	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1G	-971	-8	199	1	0.8534	1.0259	0.9981	0.9999	0.9913	0.01	0.03	0.04	Snell. 'zx'= 41
1H	-971	-8	294	1	0.8534	1.0259	0.9966	0.9997	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1I	-1321	42	45	1	0.8534	0.9960	1.0024	1.0000	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1J	-1321	42	168	1	0.8534	0.9960	0.9963	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1K	-1321	-33	45	1	0.8534	1.0005	1.0024	1.0000	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1L	-1321	-33	168	1	0.8534	1.0005	0.9963	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1M	-973	42	45	1	0.8534	0.9971	1.0017	1.0000	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1N	-973	42	168	1	0.8534	0.9971	0.9973	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1O	-973	-33	45	1	0.8534	1.0004	1.0017	1.0000	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1P	-973	-33	168	1	0.8534	1.0004	0.9973	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
2	-1707	-12	145	1	0.8534	1.0240	0.9972	1.0000	0.9897	0.02	0.02	0.04	Snell. 'zx'= 41
3	-1561	-12	132	1	0.8534	1.0231	0.9975	1.0000	0.9897	0.02	0.02	0.04	Snell. 'zx'= 41
4	-1412	-11	123	1	0.8534	1.0220	0.9976	1.0000	0.9902	0.01	0.02	0.04	Snell. 'zx'= 41
5	-1425	-37	117	1	0.8534	1.0019	0.9978	1.0000	0.9894	0.01	0.02	0.04	Snell. 'zx'= 41

ASTA NUM. 7 NI 7 NF 36 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1723	-263	27	0	19	220	1	0.01	0.02	0.03	
1B	0	-1723	282	27	0	19	-235	1	0.01	0.02	0.04	
1C	0	-1723	-263	-6	0	-8	220	1	0.01	0.02	0.03	
1D	0	-1723	282	-6	0	-8	-235	1	0.01	0.02	0.04	
1E	0	-1559	-263	27	0	19	220	1	0.01	0.01	0.03	
1F	0	-1559	282	27	0	19	-235	1	0.01	0.01	0.04	
1G	0	-1559	-263	-6	0	-8	220	1	0.01	0.01	0.03	
1H	0	-1559	282	-6	0	-8	-235	1	0.01	0.01	0.04	
1I	0	-1792	-80	63	0	49	68	1	0.00	0.02	0.02	
1J	0	-1792	100	63	0	49	-83	1	0.00	0.02	0.02	
1K	0	-1792	-80	-43	0	-39	68	1	0.00	0.02	0.01	
1L	0	-1792	100	-43	0	-39	-83	1	0.00	0.02	0.01	
1M	0	-1490	-80	63	0	49	68	1	0.00	0.01	0.02	
1N	0	-1490	100	63	0	49	-83	1	0.00	0.01	0.02	
1O	0	-1490	-80	-43	0	-39	68	1	0.00	0.01	0.01	
1P	0	-1490	100	-43	0	-39	-83	1	0.00	0.01	0.01	

2	0	-2449	15	14	0	7	-12	1	0.00	0.02	0.00
3	0	-2236	13	13	0	7	-10	1	0.00	0.02	0.00
4	0	-2023	18	13	0	7	-14	1	0.00	0.02	0.00
5	0	-2034	10	-187	0	-50	-8	1	0.00	0.02	0.02
1A	74	-1698	-263	27	0	-1	26	1	0.01	0.01	0.00
1B	74	-1698	282	27	0	-1	-27	1	0.01	0.01	0.00
1C	74	-1698	-263	-6	0	-4	26	1	0.01	0.01	0.00
1D	74	-1698	282	-6	0	-4	-27	1	0.01	0.01	0.00
1E	74	-1534	-263	27	0	-1	26	1	0.01	0.01	0.00
1F	74	-1534	282	27	0	-1	-27	1	0.01	0.01	0.00
1G	74	-1534	-263	-6	0	-4	26	1	0.01	0.01	0.00
1H	74	-1534	282	-6	0	-4	-27	1	0.01	0.01	0.00
1I	74	-1767	-80	63	0	2	8	1	0.00	0.02	0.00
1J	74	-1767	100	63	0	2	-9	1	0.00	0.02	0.00
1K	74	-1767	-80	-43	0	-7	8	1	0.00	0.02	0.00
1L	74	-1767	100	-43	0	-7	-9	1	0.00	0.02	0.00
1M	74	-1465	-80	63	0	2	8	1	0.00	0.01	0.00
1N	74	-1465	100	63	0	2	-9	1	0.00	0.01	0.00
1O	74	-1465	-80	-43	0	-7	8	1	0.00	0.01	0.00
1P	74	-1465	100	-43	0	-7	-9	1	0.00	0.01	0.00
2	74	-2417	15	14	0	-3	-1	1	0.00	0.02	0.00
3	74	-2204	13	13	0	-3	-1	1	0.00	0.02	0.00
4	74	-1991	18	13	0	-3	-1	1	0.00	0.02	0.00
5	74	-2002	10	-11	0	23	-0	1	0.00	0.02	0.01
1A	148	-1673	-263	27	0	-21	-169	1	0.01	0.01	0.03
1B	148	-1673	282	27	0	-21	182	1	0.01	0.01	0.03
1C	148	-1673	-263	-6	0	1	-169	1	0.01	0.01	0.03
1D	148	-1673	282	-6	0	1	182	1	0.01	0.01	0.03
1E	148	-1509	-263	27	0	-21	-169	1	0.01	0.01	0.03
1F	148	-1509	282	27	0	-21	182	1	0.01	0.01	0.03
1G	148	-1509	-263	-6	0	1	-169	1	0.01	0.01	0.03
1H	148	-1509	282	-6	0	1	182	1	0.01	0.01	0.03
1I	148	-1742	-80	63	0	-44	-51	1	0.00	0.02	0.01
1J	148	-1742	100	63	0	-44	65	1	0.00	0.02	0.01
1K	148	-1742	-80	-43	0	25	-51	1	0.00	0.02	0.01
1L	148	-1742	100	-43	0	25	65	1	0.00	0.02	0.01
1M	148	-1440	-80	63	0	-44	-51	1	0.00	0.01	0.01
1N	148	-1440	100	63	0	-44	65	1	0.00	0.01	0.01
1O	148	-1440	-80	-43	0	25	-51	1	0.00	0.01	0.01
1P	148	-1440	100	-43	0	25	65	1	0.00	0.01	0.01
2	148	-2384	15	14	0	-14	10	1	0.00	0.02	0.00
3	148	-2171	13	13	0	-13	9	1	0.00	0.02	0.00
4	148	-1958	18	13	0	-13	12	1	0.00	0.02	0.00
5	148	-1969	10	166	0	-35	7	1	0.00	0.02	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-1723	-21	220	1	0.8534	1.0144	0.9951	0.9997	0.9932	0.02	0.03	0.06	Snell. 'zx'= 41
1B	-1723	-21	-235	1	0.8534	1.0144	0.9951	0.9997	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1C	-1723	-8	220	1	0.8534	1.0577	0.9951	0.9997	0.9932	0.02	0.03	0.05	Snell. 'zx'= 41
1D	-1723	-8	-235	1	0.8534	1.0577	0.9951	0.9997	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1E	-1559	-21	220	1	0.8534	1.0130	0.9956	0.9997	0.9932	0.02	0.03	0.06	Snell. 'zx'= 41
1F	-1559	-21	-235	1	0.8534	1.0130	0.9955	0.9997	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41

1G	-1559	-8	220	1	0.8534	1.0522	0.9956	0.9997	0.9932	0.02	0.03	0.05	Snell. 'zx'=	41
1H	-1559	-8	-235	1	0.8534	1.0522	0.9955	0.9997	0.9931	0.02	0.04	0.05	Snell. 'zx'=	41
1I	-1792	49	68	1	0.8534	0.9967	0.9950	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'=	41
1J	-1792	49	-83	1	0.8534	0.9967	0.9948	0.9997	0.9931	0.02	0.01	0.05	Snell. 'zx'=	41
1K	-1792	-39	68	1	0.8534	1.0029	0.9950	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'=	41
1L	-1792	-39	-83	1	0.8534	1.0029	0.9948	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'=	41
1M	-1490	49	68	1	0.8534	0.9973	0.9958	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'=	41
1N	-1490	49	-83	1	0.8534	0.9973	0.9957	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'=	41
1O	-1490	-39	68	1	0.8534	1.0024	0.9958	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'=	41
1P	-1490	-39	-83	1	0.8534	1.0024	0.9957	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'=	41
2	-2449	-14	-11	1	0.8534	1.0460	0.9920	0.9994	0.9924	0.02	0.00	0.03	Snell. 'zx'=	41
3	-2236	-13	-10	1	0.8534	1.0444	0.9927	0.9995	0.9924	0.02	0.00	0.03	Snell. 'zx'=	41
4	-2023	-13	-14	1	0.8534	1.0425	0.9937	0.9996	0.9927	0.02	0.00	0.03	Snell. 'zx'=	41
5	-2034	-50	-8	1	0.8534	1.0027	0.9932	0.9995	0.9923	0.02	0.00	0.04	Snell. 'zx'=	41

ASTA NUM. 8 NI 14 NF 29 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-858	-290	21	0	16	236	1	0.01	0.01	0.04	
1B	0	-858	185	21	0	16	-174	1	0.01	0.01	0.03	
1C	0	-858	-290	-21	0	-16	236	1	0.01	0.01	0.04	
1D	0	-858	185	-21	0	-16	-174	1	0.01	0.01	0.03	
1E	0	-269	-290	21	0	16	236	1	0.01	0.00	0.04	
1F	0	-269	185	21	0	16	-174	1	0.01	0.00	0.03	
1G	0	-269	-290	-21	0	-16	236	1	0.01	0.00	0.04	
1H	0	-269	185	-21	0	-16	-174	1	0.01	0.00	0.03	
1I	0	-652	-124	70	0	53	92	1	0.01	0.01	0.02	
1J	0	-652	19	70	0	53	-31	1	0.00	0.01	0.02	
1K	0	-652	-124	-70	0	-53	92	1	0.01	0.01	0.02	
1L	0	-652	19	-70	0	-53	-31	1	0.00	0.01	0.02	
1M	0	-475	-124	70	0	53	92	1	0.01	0.00	0.02	
1N	0	-475	19	70	0	53	-31	1	0.00	0.00	0.02	
1O	0	-475	-124	-70	0	-53	92	1	0.01	0.00	0.02	
1P	0	-475	19	-70	0	-53	-31	1	0.00	0.00	0.02	
2	0	-820	-79	-0	0	-0	47	1	0.00	0.01	0.01	
3	0	-761	-72	-0	0	-0	42	1	0.00	0.01	0.01	
4	0	-725	146	-0	0	-0	-21	1	0.01	0.01	0.00	
5	0	-698	-64	-11	0	-8	38	1	0.00	0.01	0.01	
1A	74	-833	-290	21	0	0	21	1	0.01	0.01	0.00	
1B	74	-833	185	21	0	0	-37	1	0.01	0.01	0.01	
1C	74	-833	-290	-21	0	-0	21	1	0.01	0.01	0.00	
1D	74	-833	185	-21	0	-0	-37	1	0.01	0.01	0.01	
1E	74	-244	-290	21	0	0	21	1	0.01	0.00	0.00	
1F	74	-244	185	21	0	0	-37	1	0.01	0.00	0.01	
1G	74	-244	-290	-21	0	-0	21	1	0.01	0.00	0.00	
1H	74	-244	185	-21	0	-0	-37	1	0.01	0.00	0.01	
1I	74	-627	-124	70	0	2	1	1	0.01	0.01	0.00	
1J	74	-627	19	70	0	2	-17	1	0.00	0.01	0.00	
1K	74	-627	-124	-70	0	-2	1	1	0.01	0.01	0.00	
1L	74	-627	19	-70	0	-2	-17	1	0.00	0.01	0.00	
1M	74	-450	-124	70	0	2	1	1	0.01	0.00	0.00	

1N	74	-450	19	70	0	2	-17	1	0.00	0.00	0.00
1O	74	-450	-124	-70	0	-2	1	1	0.01	0.00	0.00
1P	74	-450	19	-70	0	-2	-17	1	0.00	0.00	0.00
2	74	-788	-79	-0	0	-0	-12	1	0.00	0.01	0.00
3	74	-728	-72	-0	0	-0	-11	1	0.00	0.01	0.00
4	74	-692	-39	-0	0	-0	19	1	0.00	0.01	0.00
5	74	-665	-64	-11	0	-0	-10	1	0.00	0.01	0.00
1A	148	-808	-290	21	0	-15	-194	1	0.01	0.01	0.03
1B	148	-808	185	21	0	-15	100	1	0.01	0.01	0.02
1C	148	-808	-290	-21	0	15	-194	1	0.01	0.01	0.03
1D	148	-808	185	-21	0	15	100	1	0.01	0.01	0.02
1E	148	-219	-290	21	0	-15	-194	1	0.01	0.00	0.03
1F	148	-219	185	21	0	-15	100	1	0.01	0.00	0.02
1G	148	-219	-290	-21	0	15	-194	1	0.01	0.00	0.03
1H	148	-219	185	-21	0	15	100	1	0.01	0.00	0.02
1I	148	-602	-124	70	0	-50	-91	1	0.01	0.01	0.02
1J	148	-602	19	70	0	-50	-3	1	0.00	0.01	0.02
1K	148	-602	-124	-70	0	50	-91	1	0.01	0.01	0.02
1L	148	-602	19	-70	0	50	-3	1	0.00	0.01	0.02
1M	148	-425	-124	70	0	-50	-91	1	0.01	0.00	0.02
1N	148	-425	19	70	0	-50	-3	1	0.00	0.00	0.02
1O	148	-425	-124	-70	0	50	-91	1	0.01	0.00	0.02
1P	148	-425	19	-70	0	50	-3	1	0.00	0.00	0.02
2	148	-755	-79	-0	0	0	-71	1	0.00	0.01	0.01
3	148	-696	-72	-0	0	0	-64	1	0.00	0.01	0.01
4	148	-660	-224	-0	0	0	-79	1	0.01	0.01	0.01
5	148	-633	-64	-11	0	7	-57	1	0.00	0.01	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-858	16	236	1	0.8534	0.9925	0.9981	0.9998	0.9928	0.01	0.04	0.05	Snell. 'zx'= 41
1B	-858	16	-174	1	0.8534	0.9925	0.9991	0.9998	0.9919	0.01	0.03	0.04	Snell. 'zx'= 41
1C	-858	-16	236	1	0.8534	0.9925	0.9981	0.9998	0.9928	0.01	0.04	0.05	Snell. 'zx'= 41
1D	-858	-16	-174	1	0.8534	0.9925	0.9991	0.9998	0.9919	0.01	0.03	0.04	Snell. 'zx'= 41
1E	-269	16	236	1	0.8534	0.9976	0.9994	0.9999	0.9928	0.00	0.04	0.04	Snell. 'zx'= 41
1F	-269	16	-174	1	0.8534	0.9976	0.9997	0.9999	0.9919	0.00	0.03	0.03	Snell. 'zx'= 41
1G	-269	-16	236	1	0.8534	0.9976	0.9994	0.9999	0.9928	0.00	0.04	0.04	Snell. 'zx'= 41
1H	-269	-16	-174	1	0.8534	0.9976	0.9997	0.9999	0.9919	0.00	0.03	0.03	Snell. 'zx'= 41
1I	-652	53	92	1	0.8534	0.9943	0.9991	0.9998	0.9918	0.01	0.01	0.04	Snell. 'zx'= 41
1J	-652	53	-31	1	0.8534	0.9943	1.0033	0.9998	0.9783	0.01	0.00	0.03	Snell. 'zx'= 41
1K	-652	-53	92	1	0.8534	0.9943	0.9991	0.9998	0.9918	0.01	0.01	0.04	Snell. 'zx'= 41
1L	-652	-53	-31	1	0.8534	0.9943	1.0033	0.9998	0.9783	0.01	0.00	0.03	Snell. 'zx'= 41
1M	-475	53	92	1	0.8534	0.9958	0.9993	0.9999	0.9918	0.00	0.01	0.04	Snell. 'zx'= 41
1N	-475	53	-31	1	0.8534	0.9958	1.0024	0.9999	0.9783	0.00	0.00	0.03	Snell. 'zx'= 41
1O	-475	-53	92	1	0.8534	0.9958	0.9993	0.9999	0.9918	0.00	0.01	0.04	Snell. 'zx'= 41
1P	-475	-53	-31	1	0.8534	0.9958	1.0024	0.9999	0.9783	0.00	0.00	0.03	Snell. 'zx'= 41
2	-820	-0	-71	1	0.8534	1.0110	1.0003	1.0000	0.9926	0.01	0.01	0.02	Snell. 'zx'= 41
3	-761	-0	-64	1	0.8534	1.0102	1.0005	1.0000	0.9926	0.01	0.01	0.02	Snell. 'zx'= 41
4	-725	-0	-79	1	0.8534	1.0097	1.0013	1.0000	0.8921	0.01	0.02	0.02	Snell. 'zx'= 41
5	-698	-8	-57	1	0.8534	0.9939	1.0007	0.9998	0.9926	0.01	0.01	0.02	Snell. 'zx'= 41

ASTA NUM. 9 NI 13 NF 30 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm		daN			daN*m						
1A	0	-3237	-281	20	0	15	234	1	0.01	0.03	0.04	
1B	0	-3237	259	20	0	15	-218	1	0.01	0.03	0.03	
1C	0	-3237	-281	-20	0	-15	234	1	0.01	0.03	0.04	
1D	0	-3237	259	-20	0	-15	-218	1	0.01	0.03	0.03	
1E	0	-3083	-281	20	0	15	234	1	0.01	0.03	0.04	
1F	0	-3083	259	20	0	15	-218	1	0.01	0.03	0.03	
1G	0	-3083	-281	-20	0	-15	234	1	0.01	0.03	0.04	
1H	0	-3083	259	-20	0	-15	-218	1	0.01	0.03	0.03	
1I	0	-3183	-92	66	0	50	76	1	0.00	0.03	0.02	
1J	0	-3183	70	66	0	50	-60	1	0.00	0.03	0.02	
1K	0	-3183	-92	-66	0	-50	76	1	0.00	0.03	0.02	
1L	0	-3183	70	-66	0	-50	-60	1	0.00	0.03	0.02	
1M	0	-3137	-92	66	0	50	76	1	0.00	0.03	0.02	
1N	0	-3137	70	66	0	50	-60	1	0.00	0.03	0.02	
1O	0	-3137	-92	-66	0	-50	76	1	0.00	0.03	0.02	
1P	0	-3137	70	-66	0	-50	-60	1	0.00	0.03	0.02	
2	0	-4735	-16	-0	0	-0	12	1	0.00	0.04	0.00	
3	0	-4311	-15	-0	0	-0	11	1	0.00	0.04	0.00	
4	0	-3889	-7	-0	0	-0	5	1	0.00	0.03	0.00	
5	0	-3871	-13	-7	0	-6	10	1	0.00	0.03	0.00	
1A	74	-3212	-281	20	0	0	26	1	0.01	0.03	0.00	
1B	74	-3212	259	20	0	0	-26	1	0.01	0.03	0.00	
1C	74	-3212	-281	-20	0	-0	26	1	0.01	0.03	0.00	
1D	74	-3212	259	-20	0	-0	-26	1	0.01	0.03	0.00	
1E	74	-3058	-281	20	0	0	26	1	0.01	0.03	0.00	
1F	74	-3058	259	20	0	0	-26	1	0.01	0.03	0.00	
1G	74	-3058	-281	-20	0	-0	26	1	0.01	0.03	0.00	
1H	74	-3058	259	-20	0	-0	-26	1	0.01	0.03	0.00	
1I	74	-3158	-92	66	0	2	8	1	0.00	0.03	0.00	
1J	74	-3158	70	66	0	2	-8	1	0.00	0.03	0.00	
1K	74	-3158	-92	-66	0	-2	8	1	0.00	0.03	0.00	
1L	74	-3158	70	-66	0	-2	-8	1	0.00	0.03	0.00	
1M	74	-3112	-92	66	0	2	8	1	0.00	0.03	0.00	
1N	74	-3112	70	66	0	2	-8	1	0.00	0.03	0.00	
1O	74	-3112	-92	-66	0	-2	8	1	0.00	0.03	0.00	
1P	74	-3112	70	-66	0	-2	-8	1	0.00	0.03	0.00	
2	74	-4703	-16	-0	0	-0	0	1	0.00	0.04	0.00	
3	74	-4279	-15	-0	0	-0	0	1	0.00	0.04	0.00	
4	74	-3857	-7	-0	0	-0	-0	1	0.00	0.03	0.00	
5	74	-3839	-13	-7	0	-1	0	1	0.00	0.03	0.00	
1A	148	-3187	-281	20	0	-14	-182	1	0.01	0.03	0.03	
1B	148	-3187	259	20	0	-14	166	1	0.01	0.03	0.03	
1C	148	-3187	-281	-20	0	14	-182	1	0.01	0.03	0.03	
1D	148	-3187	259	-20	0	14	166	1	0.01	0.03	0.03	
1E	148	-3033	-281	20	0	-14	-182	1	0.01	0.03	0.03	
1F	148	-3033	259	20	0	-14	166	1	0.01	0.03	0.03	
1G	148	-3033	-281	-20	0	14	-182	1	0.01	0.03	0.03	
1H	148	-3033	259	-20	0	14	166	1	0.01	0.03	0.03	
1I	148	-3133	-92	66	0	-47	-60	1	0.00	0.03	0.01	
1J	148	-3133	70	66	0	-47	44	1	0.00	0.03	0.01	
1K	148	-3133	-92	-66	0	47	-60	1	0.00	0.03	0.01	
1L	148	-3133	70	-66	0	47	44	1	0.00	0.03	0.01	
1M	148	-3087	-92	66	0	-47	-60	1	0.00	0.03	0.01	

1N	148	-3087	70	66	0	-47	44	1	0.00	0.03	0.01
1O	148	-3087	-92	-66	0	47	-60	1	0.00	0.03	0.01
1P	148	-3087	70	-66	0	47	44	1	0.00	0.03	0.01
2	148	-4670	-16	-0	0	0	-12	1	0.00	0.04	0.00
3	148	-4246	-15	-0	0	0	-11	1	0.00	0.04	0.00
4	148	-3824	-7	-0	0	0	-5	1	0.00	0.03	0.00
5	148	-3806	-13	-7	0	4	-10	1	0.00	0.03	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-3237	15	234	1	0.8534	0.9717	0.9907	0.9991	0.9931	0.03	0.04	0.07	Snell. 'zx'= 41
1B	-3237	15	-218	1	0.8534	0.9717	0.9908	0.9991	0.9932	0.03	0.03	0.07	Snell. 'zx'= 41
1C	-3237	-15	234	1	0.8534	0.9717	0.9907	0.9991	0.9931	0.03	0.04	0.07	Snell. 'zx'= 41
1D	-3237	-15	-218	1	0.8534	0.9717	0.9908	0.9991	0.9932	0.03	0.03	0.07	Snell. 'zx'= 41
1E	-3083	15	234	1	0.8534	0.9730	0.9911	0.9992	0.9931	0.03	0.04	0.07	Snell. 'zx'= 41
1F	-3083	15	-218	1	0.8534	0.9730	0.9913	0.9992	0.9932	0.03	0.03	0.07	Snell. 'zx'= 41
1G	-3083	-15	234	1	0.8534	0.9730	0.9911	0.9992	0.9931	0.03	0.04	0.07	Snell. 'zx'= 41
1H	-3083	-15	-218	1	0.8534	0.9730	0.9913	0.9992	0.9932	0.03	0.03	0.07	Snell. 'zx'= 41
1I	-3183	50	76	1	0.8534	0.9722	0.9907	0.9992	0.9930	0.03	0.01	0.06	Snell. 'zx'= 41
1J	-3183	50	-60	1	0.8534	0.9722	0.9912	0.9992	0.9932	0.03	0.01	0.06	Snell. 'zx'= 41
1K	-3183	-50	76	1	0.8534	0.9722	0.9907	0.9992	0.9930	0.03	0.01	0.06	Snell. 'zx'= 41
1L	-3183	-50	-60	1	0.8534	0.9722	0.9912	0.9992	0.9932	0.03	0.01	0.06	Snell. 'zx'= 41
1M	-3137	50	76	1	0.8534	0.9726	0.9908	0.9992	0.9930	0.03	0.01	0.06	Snell. 'zx'= 41
1N	-3137	50	-60	1	0.8534	0.9726	0.9913	0.9992	0.9932	0.03	0.01	0.06	Snell. 'zx'= 41
1O	-3137	-50	76	1	0.8534	0.9726	0.9908	0.9992	0.9930	0.03	0.01	0.06	Snell. 'zx'= 41
1P	-3137	-50	-60	1	0.8534	0.9726	0.9913	0.9992	0.9932	0.03	0.01	0.06	Snell. 'zx'= 41
2	-4735	-0	12	1	0.8534	1.0629	0.9833	0.9987	0.9919	0.05	0.00	0.05	Snell. 'zx'= 41
3	-4311	-0	11	1	0.8534	1.0572	0.9848	0.9988	0.9919	0.04	0.00	0.05	Snell. 'zx'= 41
4	-3889	-0	-5	1	0.8534	1.0515	0.9874	0.9991	0.9924	0.04	0.00	0.04	Snell. 'zx'= 41
5	-3871	-6	10	1	0.8534	0.9705	0.9863	0.9989	0.9919	0.04	0.00	0.04	Snell. 'zx'= 41

ASTA NUM. 10 NI 12 NF 31 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
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	cm	daN			daN*m							
1A	0	-2335	-130	18	0	14	168	1	0.01	0.02	0.03	
1B	0	-2335	457	18	0	14	-308	1	0.02	0.02	0.05	
1C	0	-2335	-130	-18	0	-14	168	1	0.01	0.02	0.03	
1D	0	-2335	457	-18	0	-14	-308	1	0.02	0.02	0.05	
1E	0	-1911	-130	18	0	14	168	1	0.01	0.02	0.03	
1F	0	-1911	457	18	0	14	-308	1	0.02	0.02	0.05	
1G	0	-1911	-130	-18	0	-14	168	1	0.01	0.02	0.03	
1H	0	-1911	457	-18	0	-14	-308	1	0.02	0.02	0.05	
1I	0	-2187	76	60	0	46	2	1	0.00	0.02	0.01	
1J	0	-2187	252	60	0	46	-141	1	0.01	0.02	0.02	
1K	0	-2187	76	-60	0	-46	2	1	0.00	0.02	0.01	
1L	0	-2187	252	-60	0	-46	-141	1	0.01	0.02	0.02	
1M	0	-2059	76	60	0	46	2	1	0.00	0.02	0.01	
1N	0	-2059	252	60	0	46	-141	1	0.01	0.02	0.02	
1O	0	-2059	76	-60	0	-46	2	1	0.00	0.02	0.01	
1P	0	-2059	252	-60	0	-46	-141	1	0.01	0.02	0.02	

2	0	-3172	247	-0	0	-0	-105	1	0.01	0.03	0.02
3	0	-2894	224	-0	0	-0	-95	1	0.01	0.03	0.01
4	0	-2612	207	-0	0	-0	-91	1	0.01	0.02	0.01
5	0	-2604	201	-7	0	-6	-85	1	0.01	0.02	0.01
1A	74	-2310	-130	18	0	0	72	1	0.01	0.02	0.01
1B	74	-2310	457	18	0	0	31	1	0.02	0.02	0.00
1C	74	-2310	-130	-18	0	-0	72	1	0.01	0.02	0.01
1D	74	-2310	457	-18	0	-0	31	1	0.02	0.02	0.00
1E	74	-1886	-130	18	0	0	72	1	0.01	0.02	0.01
1F	74	-1886	457	18	0	0	31	1	0.02	0.02	0.00
1G	74	-1886	-130	-18	0	-0	72	1	0.01	0.02	0.01
1H	74	-1886	457	-18	0	-0	31	1	0.02	0.02	0.00
1I	74	-2162	76	60	0	1	58	1	0.00	0.02	0.01
1J	74	-2162	252	60	0	1	45	1	0.01	0.02	0.01
1K	74	-2162	76	-60	0	-1	58	1	0.00	0.02	0.01
1L	74	-2162	252	-60	0	-1	45	1	0.01	0.02	0.01
1M	74	-2034	76	60	0	1	58	1	0.00	0.02	0.01
1N	74	-2034	252	60	0	1	45	1	0.01	0.02	0.01
1O	74	-2034	76	-60	0	-1	58	1	0.00	0.02	0.01
1P	74	-2034	252	-60	0	-1	45	1	0.01	0.02	0.01
2	74	-3140	247	-0	0	-0	78	1	0.01	0.03	0.01
3	74	-2862	224	-0	0	-0	71	1	0.01	0.02	0.01
4	74	-2580	207	-0	0	-0	63	1	0.01	0.02	0.01
5	74	-2572	201	-7	0	-1	63	1	0.01	0.02	0.01
1A	148	-2285	-130	18	0	-13	-24	1	0.01	0.02	0.00
1B	148	-2285	457	18	0	-13	369	1	0.02	0.02	0.06
1C	148	-2285	-130	-18	0	13	-24	1	0.01	0.02	0.00
1D	148	-2285	457	-18	0	13	369	1	0.02	0.02	0.06
1E	148	-1861	-130	18	0	-13	-24	1	0.01	0.02	0.00
1F	148	-1861	457	18	0	-13	369	1	0.02	0.02	0.06
1G	148	-1861	-130	-18	0	13	-24	1	0.01	0.02	0.00
1H	148	-1861	457	-18	0	13	369	1	0.02	0.02	0.06
1I	148	-2137	76	60	0	-43	114	1	0.00	0.02	0.02
1J	148	-2137	252	60	0	-43	232	1	0.01	0.02	0.04
1K	148	-2137	76	-60	0	43	114	1	0.00	0.02	0.02
1L	148	-2137	252	-60	0	43	232	1	0.01	0.02	0.04
1M	148	-2009	76	60	0	-43	114	1	0.00	0.02	0.02
1N	148	-2009	252	60	0	-43	232	1	0.01	0.02	0.04
1O	148	-2009	76	-60	0	43	114	1	0.00	0.02	0.02
1P	148	-2009	252	-60	0	43	232	1	0.01	0.02	0.04
2	148	-3107	247	-0	0	0	260	1	0.01	0.03	0.04
3	148	-2829	224	-0	0	0	236	1	0.01	0.02	0.04
4	148	-2547	207	-0	0	0	216	1	0.01	0.02	0.03
5	148	-2539	201	-7	0	4	212	1	0.01	0.02	0.03

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-2335	14	168	1	0.8534	0.9796	0.9984	0.9994	0.9840	0.02	0.03	0.05	Snell. 'zx'= 41
1B	-2335	14	369	1	0.8534	0.9796	0.9928	0.9994	0.9928	0.02	0.06	0.08	Snell. 'zx'= 41
1C	-2335	-14	168	1	0.8534	0.9796	0.9984	0.9994	0.9840	0.02	0.03	0.05	Snell. 'zx'= 41
1D	-2335	-14	369	1	0.8534	0.9796	0.9928	0.9994	0.9928	0.02	0.06	0.08	Snell. 'zx'= 41
1E	-1911	14	168	1	0.8534	0.9833	0.9987	0.9995	0.9840	0.02	0.03	0.05	Snell. 'zx'= 41
1F	-1911	14	369	1	0.8534	0.9833	0.9941	0.9995	0.9928	0.02	0.06	0.08	Snell. 'zx'= 41

1G	-1911	-14	168	1	0.8534	0.9833	0.9987	0.9995	0.9840	0.02	0.03	0.05	Snell. 'zx'= 41
1H	-1911	-14	369	1	0.8534	0.9833	0.9941	0.9995	0.9928	0.02	0.06	0.08	Snell. 'zx'= 41
1I	-2187	46	114	1	0.8534	0.9809	0.9998	0.9994	0.9800	0.02	0.02	0.05	Snell. 'zx'= 41
1J	-2187	46	232	1	0.8534	0.9809	0.9950	0.9994	0.9921	0.02	0.04	0.07	Snell. 'zx'= 41
1K	-2187	-46	114	1	0.8534	0.9809	0.9998	0.9994	0.9800	0.02	0.02	0.05	Snell. 'zx'= 41
1L	-2187	-46	232	1	0.8534	0.9809	0.9950	0.9994	0.9921	0.02	0.04	0.07	Snell. 'zx'= 41
1M	-2059	46	114	1	0.8534	0.9820	0.9998	0.9995	0.9800	0.02	0.02	0.05	Snell. 'zx'= 41
1N	-2059	46	232	1	0.8534	0.9820	0.9953	0.9995	0.9921	0.02	0.04	0.07	Snell. 'zx'= 41
1O	-2059	-46	114	1	0.8534	0.9820	0.9998	0.9995	0.9800	0.02	0.02	0.05	Snell. 'zx'= 41
1P	-2059	-46	232	1	0.8534	0.9820	0.9953	0.9995	0.9921	0.02	0.04	0.07	Snell. 'zx'= 41
2	-3172	-0	260	1	0.8534	1.0408	0.9950	1.0000	0.9895	0.03	0.04	0.07	Snell. 'zx'= 41
3	-2894	-0	236	1	0.8534	1.0370	0.9954	1.0000	0.9895	0.03	0.04	0.07	Snell. 'zx'= 41
4	-2612	-0	216	1	0.8534	1.0333	0.9957	1.0000	0.9898	0.03	0.03	0.06	Snell. 'zx'= 41
5	-2604	-6	212	1	0.8534	0.9790	0.9959	0.9996	0.9895	0.03	0.03	0.06	Snell. 'zx'= 41

ASTA NUM. 11 NI 11 NF 32 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-4273	-231	14	0	11	203	1	0.01	0.04	0.03	
1B	0	-4273	274	14	0	11	-222	1	0.01	0.04	0.03	
1C	0	-4273	-231	-14	0	-11	203	1	0.01	0.04	0.03	
1D	0	-4273	274	-14	0	-11	-222	1	0.01	0.04	0.03	
1E	0	-1297	-231	14	0	11	203	1	0.01	0.01	0.03	
1F	0	-1297	274	14	0	11	-222	1	0.01	0.01	0.03	
1G	0	-1297	-231	-14	0	-11	203	1	0.01	0.01	0.03	
1H	0	-1297	274	-14	0	-11	-222	1	0.01	0.01	0.03	
1I	0	-3231	-54	46	0	36	54	1	0.00	0.03	0.01	
1J	0	-3231	97	46	0	36	-73	1	0.00	0.03	0.01	
1K	0	-3231	-54	-46	0	-36	54	1	0.00	0.03	0.01	
1L	0	-3231	97	-46	0	-36	-73	1	0.00	0.03	0.01	
1M	0	-2339	-54	46	0	36	54	1	0.00	0.02	0.01	
1N	0	-2339	97	46	0	36	-73	1	0.00	0.02	0.01	
1O	0	-2339	-54	-46	0	-36	54	1	0.00	0.02	0.01	
1P	0	-2339	97	-46	0	-36	-73	1	0.00	0.02	0.01	
2	0	-4162	33	-0	0	-0	-14	1	0.00	0.04	0.00	
3	0	-3796	29	-0	0	-0	-13	1	0.00	0.03	0.00	
4	0	-3398	32	-0	0	-0	-16	1	0.00	0.03	0.00	
5	0	-3413	26	-4	0	-4	-11	1	0.00	0.03	0.00	
1A	74	-4248	-231	14	0	0	32	1	0.01	0.04	0.00	
1B	74	-4248	274	14	0	0	-19	1	0.01	0.04	0.00	
1C	74	-4248	-231	-14	0	-0	32	1	0.01	0.04	0.00	
1D	74	-4248	274	-14	0	-0	-19	1	0.01	0.04	0.00	
1E	74	-1272	-231	14	0	0	32	1	0.01	0.01	0.00	
1F	74	-1272	274	14	0	0	-19	1	0.01	0.01	0.00	
1G	74	-1272	-231	-14	0	-0	32	1	0.01	0.01	0.00	
1H	74	-1272	274	-14	0	-0	-19	1	0.01	0.01	0.00	
1I	74	-3206	-54	46	0	2	14	1	0.00	0.03	0.00	
1J	74	-3206	97	46	0	2	-1	1	0.00	0.03	0.00	
1K	74	-3206	-54	-46	0	-2	14	1	0.00	0.03	0.00	
1L	74	-3206	97	-46	0	-2	-1	1	0.00	0.03	0.00	
1M	74	-2314	-54	46	0	2	14	1	0.00	0.02	0.00	

1N	74	-2314	97	46	0	2	-1	1	0.00	0.02	0.00
1O	74	-2314	-54	-46	0	-2	14	1	0.00	0.02	0.00
1P	74	-2314	97	-46	0	-2	-1	1	0.00	0.02	0.00
2	74	-4130	33	-0	0	-0	10	1	0.00	0.04	0.00
3	74	-3764	29	-0	0	-0	9	1	0.00	0.03	0.00
4	74	-3366	32	-0	0	-0	7	1	0.00	0.03	0.00
5	74	-3381	26	-4	0	-1	8	1	0.00	0.03	0.00
1A	148	-4223	-231	14	0	-10	-139	1	0.01	0.04	0.02
1B	148	-4223	274	14	0	-10	184	1	0.01	0.04	0.03
1C	148	-4223	-231	-14	0	10	-139	1	0.01	0.04	0.02
1D	148	-4223	274	-14	0	10	184	1	0.01	0.04	0.03
1E	148	-1247	-231	14	0	-10	-139	1	0.01	0.01	0.02
1F	148	-1247	274	14	0	-10	184	1	0.01	0.01	0.03
1G	148	-1247	-231	-14	0	10	-139	1	0.01	0.01	0.02
1H	148	-1247	274	-14	0	10	184	1	0.01	0.01	0.03
1I	148	-3181	-54	46	0	-33	-26	1	0.00	0.03	0.01
1J	148	-3181	97	46	0	-33	71	1	0.00	0.03	0.01
1K	148	-3181	-54	-46	0	33	-26	1	0.00	0.03	0.01
1L	148	-3181	97	-46	0	33	71	1	0.00	0.03	0.01
1M	148	-2289	-54	46	0	-33	-26	1	0.00	0.02	0.01
1N	148	-2289	97	46	0	-33	71	1	0.00	0.02	0.01
1O	148	-2289	-54	-46	0	33	-26	1	0.00	0.02	0.01
1P	148	-2289	97	-46	0	33	71	1	0.00	0.02	0.01
2	148	-4098	33	-0	0	0	34	1	0.00	0.04	0.01
3	148	-3731	29	-0	0	0	31	1	0.00	0.03	0.00
4	148	-3333	32	-0	0	0	31	1	0.00	0.03	0.00
5	148	-3348	26	-4	0	2	27	1	0.00	0.03	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-4273	11	203	1	0.8534	0.9626	0.9890	0.9989	0.9928	0.04	0.03	0.08	Snell. 'zx'= 41
1B	-4273	11	-222	1	0.8534	0.9626	0.9869	0.9989	0.9928	0.04	0.03	0.08	Snell. 'zx'= 41
1C	-4273	-11	203	1	0.8534	0.9626	0.9890	0.9989	0.9928	0.04	0.03	0.08	Snell. 'zx'= 41
1D	-4273	-11	-222	1	0.8534	0.9626	0.9869	0.9989	0.9928	0.04	0.03	0.08	Snell. 'zx'= 41
1E	-1297	11	203	1	0.8534	0.9887	0.9967	0.9997	0.9928	0.01	0.03	0.05	Snell. 'zx'= 41
1F	-1297	11	-222	1	0.8534	0.9887	0.9960	0.9997	0.9928	0.01	0.03	0.05	Snell. 'zx'= 41
1G	-1297	-11	203	1	0.8534	0.9887	0.9967	0.9997	0.9928	0.01	0.03	0.05	Snell. 'zx'= 41
1H	-1297	-11	-222	1	0.8534	0.9887	0.9960	0.9997	0.9928	0.01	0.03	0.05	Snell. 'zx'= 41
1I	-3231	36	54	1	0.8534	0.9717	0.9940	0.9992	0.9909	0.03	0.01	0.05	Snell. 'zx'= 41
1J	-3231	36	-73	1	0.8534	0.9717	0.9885	0.9991	0.9919	0.03	0.01	0.05	Snell. 'zx'= 41
1K	-3231	-36	54	1	0.8534	0.9717	0.9940	0.9992	0.9909	0.03	0.01	0.05	Snell. 'zx'= 41
1L	-3231	-36	-73	1	0.8534	0.9717	0.9885	0.9991	0.9919	0.03	0.01	0.05	Snell. 'zx'= 41
1M	-2339	36	54	1	0.8534	0.9795	0.9957	0.9994	0.9909	0.02	0.01	0.04	Snell. 'zx'= 41
1N	-2339	36	-73	1	0.8534	0.9795	0.9917	0.9993	0.9919	0.02	0.01	0.05	Snell. 'zx'= 41
1O	-2339	-36	54	1	0.8534	0.9795	0.9957	0.9994	0.9909	0.02	0.01	0.04	Snell. 'zx'= 41
1P	-2339	-36	-73	1	0.8534	0.9795	0.9917	0.9993	0.9919	0.02	0.01	0.05	Snell. 'zx'= 41
2	-4162	-0	34	1	0.8534	1.0550	0.9932	1.0000	0.9897	0.04	0.01	0.05	Snell. 'zx'= 41
3	-3796	-0	31	1	0.8534	1.0500	0.9938	1.0000	0.9897	0.04	0.00	0.04	Snell. 'zx'= 41
4	-3398	-0	31	1	0.8534	1.0446	0.9932	0.9998	0.9914	0.03	0.00	0.04	Snell. 'zx'= 41
5	-3413	-4	27	1	0.8534	0.9781	0.9945	0.9999	0.9897	0.03	0.00	0.04	Snell. 'zx'= 41

ASTA NUM. 12 NI 10 NF 33 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm		daN			daN*m						
1A	0	-4273	-274	14	0	11	222	1	0.01	0.04	0.03	
1B	0	-4273	231	14	0	11	-203	1	0.01	0.04	0.03	
1C	0	-4273	-274	-14	0	-11	222	1	0.01	0.04	0.03	
1D	0	-4273	231	-14	0	-11	-203	1	0.01	0.04	0.03	
1E	0	-1297	-274	14	0	11	222	1	0.01	0.01	0.03	
1F	0	-1297	231	14	0	11	-203	1	0.01	0.01	0.03	
1G	0	-1297	-274	-14	0	-11	222	1	0.01	0.01	0.03	
1H	0	-1297	231	-14	0	-11	-203	1	0.01	0.01	0.03	
1I	0	-3231	-97	46	0	36	73	1	0.00	0.03	0.01	
1J	0	-3231	54	46	0	36	-54	1	0.00	0.03	0.01	
1K	0	-3231	-97	-46	0	-36	73	1	0.00	0.03	0.01	
1L	0	-3231	54	-46	0	-36	-54	1	0.00	0.03	0.01	
1M	0	-2339	-97	46	0	36	73	1	0.00	0.02	0.01	
1N	0	-2339	54	46	0	36	-54	1	0.00	0.02	0.01	
1O	0	-2339	-97	-46	0	-36	73	1	0.00	0.02	0.01	
1P	0	-2339	54	-46	0	-36	-54	1	0.00	0.02	0.01	
2	0	-4162	-33	-0	0	-0	14	1	0.00	0.04	0.00	
3	0	-3796	-29	-0	0	-0	13	1	0.00	0.03	0.00	
4	0	-3461	-20	-0	0	-0	6	1	0.00	0.03	0.00	
5	0	-3413	-26	-4	0	-4	11	1	0.00	0.03	0.00	
1A	74	-4248	-274	14	0	0	19	1	0.01	0.04	0.00	
1B	74	-4248	231	14	0	0	-32	1	0.01	0.04	0.00	
1C	74	-4248	-274	-14	0	-0	19	1	0.01	0.04	0.00	
1D	74	-4248	231	-14	0	-0	-32	1	0.01	0.04	0.00	
1E	74	-1272	-274	14	0	0	19	1	0.01	0.01	0.00	
1F	74	-1272	231	14	0	0	-32	1	0.01	0.01	0.00	
1G	74	-1272	-274	-14	0	-0	19	1	0.01	0.01	0.00	
1H	74	-1272	231	-14	0	-0	-32	1	0.01	0.01	0.00	
1I	74	-3206	-97	46	0	2	1	1	0.00	0.03	0.00	
1J	74	-3206	54	46	0	2	-14	1	0.00	0.03	0.00	
1K	74	-3206	-97	-46	0	-2	1	1	0.00	0.03	0.00	
1L	74	-3206	54	-46	0	-2	-14	1	0.00	0.03	0.00	
1M	74	-2314	-97	46	0	2	1	1	0.00	0.02	0.00	
1N	74	-2314	54	46	0	2	-14	1	0.00	0.02	0.00	
1O	74	-2314	-97	-46	0	-2	1	1	0.00	0.02	0.00	
1P	74	-2314	54	-46	0	-2	-14	1	0.00	0.02	0.00	
2	74	-4130	-33	-0	0	-0	-10	1	0.00	0.04	0.00	
3	74	-3764	-29	-0	0	-0	-9	1	0.00	0.03	0.00	
4	74	-3429	-20	-0	0	-0	-9	1	0.00	0.03	0.00	
5	74	-3381	-26	-4	0	-1	-8	1	0.00	0.03	0.00	
1A	148	-4223	-274	14	0	-10	-184	1	0.01	0.04	0.03	
1B	148	-4223	231	14	0	-10	139	1	0.01	0.04	0.02	
1C	148	-4223	-274	-14	0	10	-184	1	0.01	0.04	0.03	
1D	148	-4223	231	-14	0	10	139	1	0.01	0.04	0.02	
1E	148	-1247	-274	14	0	-10	-184	1	0.01	0.01	0.03	
1F	148	-1247	231	14	0	-10	139	1	0.01	0.01	0.02	
1G	148	-1247	-274	-14	0	10	-184	1	0.01	0.01	0.03	
1H	148	-1247	231	-14	0	10	139	1	0.01	0.01	0.02	
1I	148	-3181	-97	46	0	-33	-71	1	0.00	0.03	0.01	
1J	148	-3181	54	46	0	-33	26	1	0.00	0.03	0.01	
1K	148	-3181	-97	-46	0	33	-71	1	0.00	0.03	0.01	
1L	148	-3181	54	-46	0	33	26	1	0.00	0.03	0.01	
1M	148	-2289	-97	46	0	-33	-71	1	0.00	0.02	0.01	

1N	148	-2289	54	46	0	-33	26	1	0.00	0.02	0.01
1O	148	-2289	-97	-46	0	33	-71	1	0.00	0.02	0.01
1P	148	-2289	54	-46	0	33	26	1	0.00	0.02	0.01
2	148	-4098	-33	-0	0	0	-34	1	0.00	0.04	0.01
3	148	-3731	-29	-0	0	0	-31	1	0.00	0.03	0.00
4	148	-3396	-20	-0	0	0	-23	1	0.00	0.03	0.00
5	148	-3348	-26	-4	0	2	-27	1	0.00	0.03	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-4273	11	222	1	0.8534	0.9626	0.9869	0.9989	0.9928	0.04	0.03	0.08	Snell. 'zx'= 41
1B	-4273	11	-203	1	0.8534	0.9626	0.9890	0.9989	0.9928	0.04	0.03	0.08	Snell. 'zx'= 41
1C	-4273	-11	222	1	0.8534	0.9626	0.9869	0.9989	0.9928	0.04	0.03	0.08	Snell. 'zx'= 41
1D	-4273	-11	-203	1	0.8534	0.9626	0.9890	0.9989	0.9928	0.04	0.03	0.08	Snell. 'zx'= 41
1E	-1297	11	222	1	0.8534	0.9887	0.9960	0.9997	0.9928	0.01	0.03	0.05	Snell. 'zx'= 41
1F	-1297	11	-203	1	0.8534	0.9887	0.9967	0.9997	0.9928	0.01	0.03	0.05	Snell. 'zx'= 41
1G	-1297	-11	222	1	0.8534	0.9887	0.9960	0.9997	0.9928	0.01	0.03	0.05	Snell. 'zx'= 41
1H	-1297	-11	-203	1	0.8534	0.9887	0.9967	0.9997	0.9928	0.01	0.03	0.05	Snell. 'zx'= 41
1I	-3231	36	73	1	0.8534	0.9717	0.9885	0.9991	0.9919	0.03	0.01	0.05	Snell. 'zx'= 41
1J	-3231	36	-54	1	0.8534	0.9717	0.9940	0.9992	0.9909	0.03	0.01	0.05	Snell. 'zx'= 41
1K	-3231	-36	73	1	0.8534	0.9717	0.9885	0.9991	0.9919	0.03	0.01	0.05	Snell. 'zx'= 41
1L	-3231	-36	-54	1	0.8534	0.9717	0.9940	0.9992	0.9909	0.03	0.01	0.05	Snell. 'zx'= 41
1M	-2339	36	73	1	0.8534	0.9795	0.9917	0.9993	0.9919	0.02	0.01	0.05	Snell. 'zx'= 41
1N	-2339	36	-54	1	0.8534	0.9795	0.9957	0.9994	0.9909	0.02	0.01	0.04	Snell. 'zx'= 41
1O	-2339	-36	73	1	0.8534	0.9795	0.9917	0.9993	0.9919	0.02	0.01	0.05	Snell. 'zx'= 41
1P	-2339	-36	-54	1	0.8534	0.9795	0.9957	0.9994	0.9909	0.02	0.01	0.04	Snell. 'zx'= 41
2	-4162	-0	-34	1	0.8534	1.0559	0.9932	1.0000	0.9897	0.04	0.01	0.05	Snell. 'zx'= 41
3	-3796	-0	-31	1	0.8534	1.0510	0.9938	1.0000	0.9897	0.04	0.00	0.04	Snell. 'zx'= 41
4	-3461	-0	-23	1	0.8534	1.0464	0.9961	1.0000	0.9869	0.04	0.00	0.04	Snell. 'zx'= 41
5	-3413	-4	-27	1	0.8534	0.9790	0.9945	0.9999	0.9897	0.03	0.00	0.04	Snell. 'zx'= 41

ASTA NUM. 13 NI 9 NF 34 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
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	cm	daN			daN*m							
1A	0	-2297	-117	17	0	13	161	1	0.01	0.02	0.02	
1B	0	-2297	473	17	0	13	-315	1	0.02	0.02	0.05	
1C	0	-2297	-117	-17	0	-13	161	1	0.01	0.02	0.02	
1D	0	-2297	473	-17	0	-13	-315	1	0.02	0.02	0.05	
1E	0	-2101	-117	17	0	13	161	1	0.01	0.02	0.02	
1F	0	-2101	473	17	0	13	-315	1	0.02	0.02	0.05	
1G	0	-2101	-117	-17	0	-13	161	1	0.01	0.02	0.02	
1H	0	-2101	473	-17	0	-13	-315	1	0.02	0.02	0.05	
1I	0	-2228	90	56	0	43	-6	1	0.00	0.02	0.01	
1J	0	-2228	267	56	0	43	-149	1	0.01	0.02	0.02	
1K	0	-2228	90	-56	0	-43	-6	1	0.00	0.02	0.01	
1L	0	-2228	267	-56	0	-43	-149	1	0.01	0.02	0.02	
1M	0	-2170	90	56	0	43	-6	1	0.00	0.02	0.01	
1N	0	-2170	267	56	0	43	-149	1	0.01	0.02	0.02	
1O	0	-2170	90	-56	0	-43	-6	1	0.00	0.02	0.01	
1P	0	-2170	267	-56	0	-43	-149	1	0.01	0.02	0.02	

2	0	-3286	269	-0	0	-0	-116	1	0.01	0.03	0.02
3	0	-2997	244	-0	0	-0	-106	1	0.01	0.03	0.02
4	0	-2705	225	-0	0	-0	-100	1	0.01	0.02	0.02
5	0	-2696	219	-5	0	-5	-95	1	0.01	0.02	0.01
1A	74	-2272	-117	17	0	0	75	1	0.01	0.02	0.01
1B	74	-2272	473	17	0	0	35	1	0.02	0.02	0.01
1C	74	-2272	-117	-17	0	-0	75	1	0.01	0.02	0.01
1D	74	-2272	473	-17	0	-0	35	1	0.02	0.02	0.01
1E	74	-2076	-117	17	0	0	75	1	0.01	0.02	0.01
1F	74	-2076	473	17	0	0	35	1	0.02	0.02	0.01
1G	74	-2076	-117	-17	0	-0	75	1	0.01	0.02	0.01
1H	74	-2076	473	-17	0	-0	35	1	0.02	0.02	0.01
1I	74	-2203	90	56	0	1	61	1	0.00	0.02	0.01
1J	74	-2203	267	56	0	1	49	1	0.01	0.02	0.01
1K	74	-2203	90	-56	0	-1	61	1	0.00	0.02	0.01
1L	74	-2203	267	-56	0	-1	49	1	0.01	0.02	0.01
1M	74	-2145	90	56	0	1	61	1	0.00	0.02	0.01
1N	74	-2145	267	56	0	1	49	1	0.01	0.02	0.01
1O	74	-2145	90	-56	0	-1	61	1	0.00	0.02	0.01
1P	74	-2145	267	-56	0	-1	49	1	0.01	0.02	0.01
2	74	-3254	269	-0	0	-0	83	1	0.01	0.03	0.01
3	74	-2965	244	-0	0	-0	75	1	0.01	0.03	0.01
4	74	-2673	225	-0	0	-0	67	1	0.01	0.02	0.01
5	74	-2664	219	-5	0	-1	67	1	0.01	0.02	0.01
1A	148	-2247	-117	17	0	-12	-12	1	0.01	0.02	0.00
1B	148	-2247	473	17	0	-12	385	1	0.02	0.02	0.06
1C	148	-2247	-117	-17	0	12	-12	1	0.01	0.02	0.00
1D	148	-2247	473	-17	0	12	385	1	0.02	0.02	0.06
1E	148	-2051	-117	17	0	-12	-12	1	0.01	0.02	0.00
1F	148	-2051	473	17	0	-12	385	1	0.02	0.02	0.06
1G	148	-2051	-117	-17	0	12	-12	1	0.01	0.02	0.00
1H	148	-2051	473	-17	0	12	385	1	0.02	0.02	0.06
1I	148	-2178	90	56	0	-40	127	1	0.00	0.02	0.02
1J	148	-2178	267	56	0	-40	246	1	0.01	0.02	0.04
1K	148	-2178	90	-56	0	40	127	1	0.00	0.02	0.02
1L	148	-2178	267	-56	0	40	246	1	0.01	0.02	0.04
1M	148	-2120	90	56	0	-40	127	1	0.00	0.02	0.02
1N	148	-2120	267	56	0	-40	246	1	0.01	0.02	0.04
1O	148	-2120	90	-56	0	40	127	1	0.00	0.02	0.02
1P	148	-2120	267	-56	0	40	246	1	0.01	0.02	0.04
2	148	-3221	269	-0	0	0	281	1	0.01	0.03	0.04
3	148	-2932	244	-0	0	0	255	1	0.01	0.03	0.04
4	148	-2640	225	-0	0	0	234	1	0.01	0.02	0.04
5	148	-2631	219	-5	0	3	229	1	0.01	0.02	0.03

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-2297	13	161	1	0.8534	0.9799	0.9990	0.9994	0.9823	0.02	0.03	0.05	Snell. 'zx'= 41
1B	-2297	13	385	1	0.8534	0.9799	0.9930	0.9994	0.9928	0.02	0.06	0.09	Snell. 'zx'= 41
1C	-2297	-13	161	1	0.8534	0.9799	0.9990	0.9994	0.9823	0.02	0.03	0.05	Snell. 'zx'= 41
1D	-2297	-13	385	1	0.8534	0.9799	0.9930	0.9994	0.9928	0.02	0.06	0.09	Snell. 'zx'= 41
1E	-2101	13	161	1	0.8534	0.9816	0.9991	0.9994	0.9823	0.02	0.03	0.05	Snell. 'zx'= 41
1F	-2101	13	385	1	0.8534	0.9816	0.9936	0.9994	0.9928	0.02	0.06	0.08	Snell. 'zx'= 41

1G	-2101	-13	161	1	0.8534	0.9816	0.9991	0.9994	0.9823	0.02	0.03	0.05	Snell. 'zx'=	41
1H	-2101	-13	385	1	0.8534	0.9816	0.9936	0.9994	0.9928	0.02	0.06	0.08	Snell. 'zx'=	41
1I	-2228	43	127	1	0.8534	0.9805	0.9993	0.9994	0.9816	0.02	0.02	0.06	Snell. 'zx'=	41
1J	-2228	43	246	1	0.8534	0.9805	0.9949	0.9994	0.9921	0.02	0.04	0.07	Snell. 'zx'=	41
1K	-2228	-43	127	1	0.8534	0.9805	0.9993	0.9994	0.9816	0.02	0.02	0.06	Snell. 'zx'=	41
1L	-2228	-43	246	1	0.8534	0.9805	0.9949	0.9994	0.9921	0.02	0.04	0.07	Snell. 'zx'=	41
1M	-2170	43	127	1	0.8534	0.9810	0.9993	0.9994	0.9816	0.02	0.02	0.05	Snell. 'zx'=	41
1N	-2170	43	246	1	0.8534	0.9810	0.9951	0.9994	0.9921	0.02	0.04	0.07	Snell. 'zx'=	41
1O	-2170	-43	127	1	0.8534	0.9810	0.9993	0.9994	0.9816	0.02	0.02	0.05	Snell. 'zx'=	41
1P	-2170	-43	246	1	0.8534	0.9810	0.9951	0.9994	0.9921	0.02	0.04	0.07	Snell. 'zx'=	41
2	-3286	-0	281	1	0.8534	1.0431	0.9947	1.0000	0.9897	0.03	0.04	0.08	Snell. 'zx'=	41
3	-2997	-0	255	1	0.8534	1.0392	0.9952	1.0000	0.9897	0.03	0.04	0.07	Snell. 'zx'=	41
4	-2705	-0	234	1	0.8534	1.0352	0.9955	1.0000	0.9900	0.03	0.04	0.06	Snell. 'zx'=	41
5	-2696	-5	229	1	0.8534	0.9796	0.9957	0.9997	0.9897	0.03	0.04	0.06	Snell. 'zx'=	41

ASTA NUM. 14 NI 8 NF 35 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-3237	-259	20	0	15	218	1	0.01	0.03	0.03	
1B	0	-3237	281	20	0	15	-234	1	0.01	0.03	0.04	
1C	0	-3237	-259	-20	0	-15	218	1	0.01	0.03	0.03	
1D	0	-3237	281	-20	0	-15	-234	1	0.01	0.03	0.04	
1E	0	-3083	-259	20	0	15	218	1	0.01	0.03	0.03	
1F	0	-3083	281	20	0	15	-234	1	0.01	0.03	0.04	
1G	0	-3083	-259	-20	0	-15	218	1	0.01	0.03	0.03	
1H	0	-3083	281	-20	0	-15	-234	1	0.01	0.03	0.04	
1I	0	-3183	-70	66	0	50	60	1	0.00	0.03	0.02	
1J	0	-3183	92	66	0	50	-76	1	0.00	0.03	0.02	
1K	0	-3183	-70	-66	0	-50	60	1	0.00	0.03	0.02	
1L	0	-3183	92	-66	0	-50	-76	1	0.00	0.03	0.02	
1M	0	-3137	-70	66	0	50	60	1	0.00	0.03	0.02	
1N	0	-3137	92	66	0	50	-76	1	0.00	0.03	0.02	
1O	0	-3137	-70	-66	0	-50	60	1	0.00	0.03	0.02	
1P	0	-3137	92	-66	0	-50	-76	1	0.00	0.03	0.02	
2	0	-4735	16	-0	0	-0	-12	1	0.00	0.04	0.00	
3	0	-4311	15	-0	0	-0	-11	1	0.00	0.04	0.00	
4	0	-3888	19	-0	0	-0	-15	1	0.00	0.03	0.00	
5	0	-3871	13	-4	0	-4	-10	1	0.00	0.03	0.00	
1A	74	-3212	-259	20	0	0	26	1	0.01	0.03	0.00	
1B	74	-3212	281	20	0	0	-26	1	0.01	0.03	0.00	
1C	74	-3212	-259	-20	0	-0	26	1	0.01	0.03	0.00	
1D	74	-3212	281	-20	0	-0	-26	1	0.01	0.03	0.00	
1E	74	-3058	-259	20	0	0	26	1	0.01	0.03	0.00	
1F	74	-3058	281	20	0	0	-26	1	0.01	0.03	0.00	
1G	74	-3058	-259	-20	0	-0	26	1	0.01	0.03	0.00	
1H	74	-3058	281	-20	0	-0	-26	1	0.01	0.03	0.00	
1I	74	-3158	-70	66	0	2	8	1	0.00	0.03	0.00	
1J	74	-3158	92	66	0	2	-8	1	0.00	0.03	0.00	
1K	74	-3158	-70	-66	0	-2	8	1	0.00	0.03	0.00	
1L	74	-3158	92	-66	0	-2	-8	1	0.00	0.03	0.00	
1M	74	-3112	-70	66	0	2	8	1	0.00	0.03	0.00	

1N	74	-3112	92	66	0	2	-8	1	0.00	0.03	0.00
1O	74	-3112	-70	-66	0	-2	8	1	0.00	0.03	0.00
1P	74	-3112	92	-66	0	-2	-8	1	0.00	0.03	0.00
2	74	-4703	16	-0	0	-0	-0	1	0.00	0.04	0.00
3	74	-4279	15	-0	0	-0	-0	1	0.00	0.04	0.00
4	74	-3856	19	-0	0	-0	-1	1	0.00	0.03	0.00
5	74	-3839	13	-4	0	-1	-0	1	0.00	0.03	0.00
1A	148	-3187	-259	20	0	-14	-166	1	0.01	0.03	0.03
1B	148	-3187	281	20	0	-14	182	1	0.01	0.03	0.03
1C	148	-3187	-259	-20	0	14	-166	1	0.01	0.03	0.03
1D	148	-3187	281	-20	0	14	182	1	0.01	0.03	0.03
1E	148	-3033	-259	20	0	-14	-166	1	0.01	0.03	0.03
1F	148	-3033	281	20	0	-14	182	1	0.01	0.03	0.03
1G	148	-3033	-259	-20	0	14	-166	1	0.01	0.03	0.03
1H	148	-3033	281	-20	0	14	182	1	0.01	0.03	0.03
1I	148	-3133	-70	66	0	-47	-44	1	0.00	0.03	0.01
1J	148	-3133	92	66	0	-47	60	1	0.00	0.03	0.01
1K	148	-3133	-70	-66	0	47	-44	1	0.00	0.03	0.01
1L	148	-3133	92	-66	0	47	60	1	0.00	0.03	0.01
1M	148	-3087	-70	66	0	-47	-44	1	0.00	0.03	0.01
1N	148	-3087	92	66	0	-47	60	1	0.00	0.03	0.01
1O	148	-3087	-70	-66	0	47	-44	1	0.00	0.03	0.01
1P	148	-3087	92	-66	0	47	60	1	0.00	0.03	0.01
2	148	-4670	16	-0	0	0	12	1	0.00	0.04	0.00
3	148	-4246	15	-0	0	0	11	1	0.00	0.04	0.00
4	148	-3823	19	-0	0	0	14	1	0.00	0.03	0.00
5	148	-3806	13	-4	0	2	10	1	0.00	0.03	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-3237	15	218	1	0.8534	0.9717	0.9908	0.9991	0.9932	0.03	0.03	0.07	Snell. 'zx'= 41
1B	-3237	15	-234	1	0.8534	0.9717	0.9907	0.9991	0.9931	0.03	0.04	0.07	Snell. 'zx'= 41
1C	-3237	-15	218	1	0.8534	0.9717	0.9908	0.9991	0.9932	0.03	0.03	0.07	Snell. 'zx'= 41
1D	-3237	-15	-234	1	0.8534	0.9717	0.9907	0.9991	0.9931	0.03	0.04	0.07	Snell. 'zx'= 41
1E	-3083	15	218	1	0.8534	0.9730	0.9913	0.9992	0.9932	0.03	0.03	0.07	Snell. 'zx'= 41
1F	-3083	15	-234	1	0.8534	0.9730	0.9911	0.9992	0.9931	0.03	0.04	0.07	Snell. 'zx'= 41
1G	-3083	-15	218	1	0.8534	0.9730	0.9913	0.9992	0.9932	0.03	0.03	0.07	Snell. 'zx'= 41
1H	-3083	-15	-234	1	0.8534	0.9730	0.9911	0.9992	0.9931	0.03	0.04	0.07	Snell. 'zx'= 41
1I	-3183	50	60	1	0.8534	0.9722	0.9912	0.9992	0.9932	0.03	0.01	0.06	Snell. 'zx'= 41
1J	-3183	50	-76	1	0.8534	0.9722	0.9907	0.9992	0.9930	0.03	0.01	0.06	Snell. 'zx'= 41
1K	-3183	-50	60	1	0.8534	0.9722	0.9912	0.9992	0.9932	0.03	0.01	0.06	Snell. 'zx'= 41
1L	-3183	-50	-76	1	0.8534	0.9722	0.9907	0.9992	0.9930	0.03	0.01	0.06	Snell. 'zx'= 41
1M	-3137	50	60	1	0.8534	0.9726	0.9913	0.9992	0.9932	0.03	0.01	0.06	Snell. 'zx'= 41
1N	-3137	50	-76	1	0.8534	0.9726	0.9908	0.9992	0.9930	0.03	0.01	0.06	Snell. 'zx'= 41
1O	-3137	-50	60	1	0.8534	0.9726	0.9913	0.9992	0.9932	0.03	0.01	0.06	Snell. 'zx'= 41
1P	-3137	-50	-76	1	0.8534	0.9726	0.9908	0.9992	0.9930	0.03	0.01	0.06	Snell. 'zx'= 41
2	-4735	-0	-12	1	0.8534	1.0606	0.9833	0.9987	0.9919	0.05	0.00	0.05	Snell. 'zx'= 41
3	-4311	-0	-11	1	0.8534	1.0549	0.9848	0.9988	0.9919	0.04	0.00	0.05	Snell. 'zx'= 41
4	-3888	-0	-15	1	0.8534	1.0491	0.9871	0.9990	0.9923	0.04	0.00	0.04	Snell. 'zx'= 41
5	-3871	-4	-10	1	0.8534	0.9738	0.9863	0.9989	0.9919	0.04	0.00	0.04	Snell. 'zx'= 41

ASTA NUM. 15 NI 21 NF 22 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-602	-273	9	0	10	228	1	0.01	0.01	0.03	
1B	0	-602	202	9	0	10	-182	1	0.01	0.01	0.03	
1C	0	-602	-273	-24	0	-18	228	1	0.01	0.01	0.03	
1D	0	-602	202	-24	0	-18	-182	1	0.01	0.01	0.03	
1E	0	-22	-273	9	0	10	228	1	0.01	0.00	0.03	
1F	0	-22	202	9	0	10	-182	1	0.01	0.00	0.03	
1G	0	-22	-273	-24	0	-18	228	1	0.01	0.00	0.03	
1H	0	-22	202	-24	0	-18	-182	1	0.01	0.00	0.03	
1I	0	-448	-110	48	0	42	87	1	0.01	0.00	0.01	
1J	0	-448	39	48	0	42	-41	1	0.00	0.00	0.01	
1K	0	-448	-110	-64	0	-50	87	1	0.01	0.00	0.02	
1L	0	-448	39	-64	0	-50	-41	1	0.00	0.00	0.02	
1M	0	-176	-110	48	0	42	87	1	0.01	0.00	0.01	
1N	0	-176	39	48	0	42	-41	1	0.00	0.00	0.01	
1O	0	-176	-110	-64	0	-50	87	1	0.01	0.00	0.02	
1P	0	-176	39	-64	0	-50	-41	1	0.00	0.00	0.02	
2	0	-452	-53	-10	0	-5	35	1	0.00	0.00	0.01	
3	0	-421	-48	-10	0	-5	32	1	0.00	0.00	0.00	
4	0	-398	64	-10	0	-5	-3	1	0.00	0.00	0.00	
5	0	-393	-43	-19	0	-13	28	1	0.00	0.00	0.00	
1A	74	-577	-273	9	0	3	26	1	0.01	0.01	0.00	
1B	74	-577	202	9	0	3	-32	1	0.01	0.01	0.00	
1C	74	-577	-273	-24	0	0	26	1	0.01	0.01	0.00	
1D	74	-577	202	-24	0	0	-32	1	0.01	0.01	0.00	
1E	74	3	-273	9	0	3	26	1	0.01	0.00	0.00	
1F	74	3	202	9	0	3	-32	1	0.01	0.00	0.00	
1G	74	3	-273	-24	0	0	26	1	0.01	0.00	0.00	
1H	74	3	202	-24	0	0	-32	1	0.01	0.00	0.00	
1I	74	-423	-110	48	0	7	6	1	0.01	0.00	0.00	
1J	74	-423	39	48	0	7	-12	1	0.00	0.00	0.00	
1K	74	-423	-110	-64	0	-3	6	1	0.01	0.00	0.00	
1L	74	-423	39	-64	0	-3	-12	1	0.00	0.00	0.00	
1M	74	-151	-110	48	0	7	6	1	0.01	0.00	0.00	
1N	74	-151	39	48	0	7	-12	1	0.00	0.00	0.00	
1O	74	-151	-110	-64	0	-3	6	1	0.01	0.00	0.00	
1P	74	-151	39	-64	0	-3	-12	1	0.00	0.00	0.00	
2	74	-420	-53	-10	0	2	-4	1	0.00	0.00	0.00	
3	74	-388	-48	-10	0	2	-4	1	0.00	0.00	0.00	
4	74	-366	-28	-10	0	2	10	1	0.00	0.00	0.00	
5	74	-361	-43	-19	0	1	-4	1	0.00	0.00	0.00	
1A	148	-552	-273	9	0	-4	-176	1	0.01	0.00	0.03	
1B	148	-552	202	9	0	-4	118	1	0.01	0.00	0.02	
1C	148	-552	-273	-24	0	18	-176	1	0.01	0.00	0.03	
1D	148	-552	202	-24	0	18	118	1	0.01	0.00	0.02	
1E	148	28	-273	9	0	-4	-176	1	0.01	0.00	0.03	
1F	148	28	202	9	0	-4	118	1	0.01	0.00	0.02	
1G	148	28	-273	-24	0	18	-176	1	0.01	0.00	0.03	
1H	148	28	202	-24	0	18	118	1	0.01	0.00	0.02	
1I	148	-398	-110	48	0	-29	-75	1	0.01	0.00	0.01	
1J	148	-398	39	48	0	-29	17	1	0.00	0.00	0.01	
1K	148	-398	-110	-64	0	44	-75	1	0.01	0.00	0.01	
1L	148	-398	39	-64	0	44	17	1	0.00	0.00	0.01	
1M	148	-126	-110	48	0	-29	-75	1	0.01	0.00	0.01	

1N	148	-126	39	48	0	-29	17	1	0.00	0.00	0.01
1O	148	-126	-110	-64	0	44	-75	1	0.01	0.00	0.01
1P	148	-126	39	-64	0	44	17	1	0.00	0.00	0.01
2	148	-387	-53	-10	0	10	-44	1	0.00	0.00	0.01
3	148	-356	-48	-10	0	10	-40	1	0.00	0.00	0.01
4	148	-333	-121	-10	0	9	-45	1	0.01	0.00	0.01
5	148	-328	-43	-19	0	16	-35	1	0.00	0.00	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	-602	10	228	1	0.8534	0.9965	0.9985	0.9999	0.9931	0.01	0.04	0.04	Snell. 'zx'= 41
1B	-602	10	-182	1	0.8534	0.9965	0.9989	1.0000	0.9925	0.01	0.03	0.04	Snell. 'zx'= 41
1C	-602	18	228	1	0.8534	0.9947	0.9985	0.9998	0.9931	0.01	0.04	0.05	Snell. 'zx'= 41
1D	-602	18	-182	1	0.8534	0.9947	0.9989	0.9998	0.9925	0.01	0.03	0.04	Snell. 'zx'= 41
1E	-22	10	228	1	0.8534	0.9999	0.9999	1.0000	0.9931	0.00	0.04	0.04	Snell. 'zx'= 41
1F	-22	10	-182	1	0.8534	0.9999	1.0000	1.0000	0.9925	0.00	0.03	0.03	Snell. 'zx'= 41
1G	-22	18	228	1	0.8534	0.9998	0.9999	1.0000	0.9931	0.00	0.04	0.04	Snell. 'zx'= 41
1H	-22	18	-182	1	0.8534	0.9998	1.0000	1.0000	0.9925	0.00	0.03	0.03	Snell. 'zx'= 41
1I	-448	42	87	1	0.8534	0.9965	0.9991	0.9999	0.9926	0.00	0.01	0.03	Snell. 'zx'= 41
1J	-448	42	-41	1	0.8534	0.9965	1.0003	0.9999	0.9898	0.00	0.01	0.02	Snell. 'zx'= 41
1K	-448	-50	87	1	0.8534	0.9961	0.9991	0.9999	0.9926	0.00	0.01	0.03	Snell. 'zx'= 41
1L	-448	-50	-41	1	0.8534	0.9961	1.0003	0.9999	0.9898	0.00	0.01	0.03	Snell. 'zx'= 41
1M	-176	42	87	1	0.8534	0.9986	0.9996	1.0000	0.9926	0.00	0.01	0.03	Snell. 'zx'= 41
1N	-176	42	-41	1	0.8534	0.9986	1.0001	1.0000	0.9898	0.00	0.01	0.02	Snell. 'zx'= 41
1O	-176	-50	87	1	0.8534	0.9985	0.9996	1.0000	0.9926	0.00	0.01	0.03	Snell. 'zx'= 41
1P	-176	-50	-41	1	0.8534	0.9985	1.0001	1.0000	0.9898	0.00	0.01	0.02	Snell. 'zx'= 41
2	-452	10	-44	1	0.8534	0.9969	0.9997	1.0000	0.9929	0.00	0.01	0.01	Snell. 'zx'= 41
3	-421	10	-40	1	0.8534	0.9971	0.9998	1.0000	0.9930	0.00	0.01	0.01	Snell. 'zx'= 41
4	-398	9	-45	1	0.8534	0.9973	1.0006	1.0000	0.8921	0.00	0.01	0.01	Snell. 'zx'= 41
5	-393	16	-35	1	0.8534	0.9966	1.0000	0.9999	0.9930	0.00	0.01	0.01	Snell. 'zx'= 41

ASTA NUM. 16 NI 20 NF 23 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
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	cm	daN			daN*m							
1A	0	-1723	-282	6	0	8	235	1	0.01	0.02	0.04	
1B	0	-1723	263	6	0	8	-220	1	0.01	0.02	0.03	
1C	0	-1723	-282	-27	0	-19	235	1	0.01	0.02	0.04	
1D	0	-1723	263	-27	0	-19	-220	1	0.01	0.02	0.03	
1E	0	-1559	-282	6	0	8	235	1	0.01	0.01	0.04	
1F	0	-1559	263	6	0	8	-220	1	0.01	0.01	0.03	
1G	0	-1559	-282	-27	0	-19	235	1	0.01	0.01	0.04	
1H	0	-1559	263	-27	0	-19	-220	1	0.01	0.01	0.03	
1I	0	-1792	-100	43	0	39	83	1	0.00	0.02	0.01	
1J	0	-1792	80	43	0	39	-68	1	0.00	0.02	0.01	
1K	0	-1792	-100	-63	0	-49	83	1	0.00	0.02	0.02	
1L	0	-1792	80	-63	0	-49	-68	1	0.00	0.02	0.02	
1M	0	-1490	-100	43	0	39	83	1	0.00	0.01	0.01	
1N	0	-1490	80	43	0	39	-68	1	0.00	0.01	0.01	
1O	0	-1490	-100	-63	0	-49	83	1	0.00	0.01	0.02	
1P	0	-1490	80	-63	0	-49	-68	1	0.00	0.01	0.02	

2	0	-2449	-15	-14	0	-7	12	1	0.00	0.02	0.00
3	0	-2236	-13	-13	0	-7	10	1	0.00	0.02	0.00
4	0	-2023	-6	-13	0	-7	4	1	0.00	0.02	0.00
5	0	-2029	-12	-22	0	-14	9	1	0.00	0.02	0.00
1A	74	-1698	-282	6	0	4	27	1	0.01	0.01	0.00
1B	74	-1698	263	6	0	4	-26	1	0.01	0.01	0.00
1C	74	-1698	-282	-27	0	1	27	1	0.01	0.01	0.00
1D	74	-1698	263	-27	0	1	-26	1	0.01	0.01	0.00
1E	74	-1534	-282	6	0	4	27	1	0.01	0.01	0.00
1F	74	-1534	263	6	0	4	-26	1	0.01	0.01	0.00
1G	74	-1534	-282	-27	0	1	27	1	0.01	0.01	0.00
1H	74	-1534	263	-27	0	1	-26	1	0.01	0.01	0.00
1I	74	-1767	-100	43	0	7	9	1	0.00	0.02	0.00
1J	74	-1767	80	43	0	7	-8	1	0.00	0.02	0.00
1K	74	-1767	-100	-63	0	-2	9	1	0.00	0.02	0.00
1L	74	-1767	80	-63	0	-2	-8	1	0.00	0.02	0.00
1M	74	-1465	-100	43	0	7	9	1	0.00	0.01	0.00
1N	74	-1465	80	43	0	7	-8	1	0.00	0.01	0.00
1O	74	-1465	-100	-63	0	-2	9	1	0.00	0.01	0.00
1P	74	-1465	80	-63	0	-2	-8	1	0.00	0.01	0.00
2	74	-2417	-15	-14	0	3	1	1	0.00	0.02	0.00
3	74	-2204	-13	-13	0	3	1	1	0.00	0.02	0.00
4	74	-1991	-6	-13	0	3	0	1	0.00	0.02	0.00
5	74	-1997	-12	-22	0	2	1	1	0.00	0.02	0.00
1A	148	-1673	-282	6	0	-1	-182	1	0.01	0.01	0.03
1B	148	-1673	263	6	0	-1	169	1	0.01	0.01	0.03
1C	148	-1673	-282	-27	0	21	-182	1	0.01	0.01	0.03
1D	148	-1673	263	-27	0	21	169	1	0.01	0.01	0.03
1E	148	-1509	-282	6	0	-1	-182	1	0.01	0.01	0.03
1F	148	-1509	263	6	0	-1	169	1	0.01	0.01	0.03
1G	148	-1509	-282	-27	0	21	-182	1	0.01	0.01	0.03
1H	148	-1509	263	-27	0	21	169	1	0.01	0.01	0.03
1I	148	-1742	-100	43	0	-25	-65	1	0.00	0.02	0.01
1J	148	-1742	80	43	0	-25	51	1	0.00	0.02	0.01
1K	148	-1742	-100	-63	0	44	-65	1	0.00	0.02	0.01
1L	148	-1742	80	-63	0	44	51	1	0.00	0.02	0.01
1M	148	-1440	-100	43	0	-25	-65	1	0.00	0.01	0.01
1N	148	-1440	80	43	0	-25	51	1	0.00	0.01	0.01
1O	148	-1440	-100	-63	0	44	-65	1	0.00	0.01	0.01
1P	148	-1440	80	-63	0	44	51	1	0.00	0.01	0.01
2	148	-2384	-15	-14	0	14	-10	1	0.00	0.02	0.00
3	148	-2171	-13	-13	0	13	-9	1	0.00	0.02	0.00
4	148	-1958	-6	-13	0	12	-4	1	0.00	0.02	0.00
5	148	-1964	-12	-22	0	19	-8	1	0.00	0.02	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-1723	8	235	1	0.8534	0.9931	0.9951	0.9997	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1B	-1723	8	-220	1	0.8534	0.9931	0.9951	0.9997	0.9932	0.02	0.03	0.05	Snell. 'zx'= 41
1C	-1723	21	235	1	0.8534	0.9849	0.9951	0.9996	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1D	-1723	21	-220	1	0.8534	0.9849	0.9951	0.9996	0.9932	0.02	0.03	0.06	Snell. 'zx'= 41
1E	-1559	8	235	1	0.8534	0.9937	0.9955	0.9997	0.9931	0.02	0.04	0.05	Snell. 'zx'= 41
1F	-1559	8	-220	1	0.8534	0.9937	0.9956	0.9997	0.9932	0.02	0.03	0.05	Snell. 'zx'= 41

1G	-1559	21	235	1	0.8534	0.9864	0.9955	0.9996	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1H	-1559	21	-220	1	0.8534	0.9864	0.9956	0.9996	0.9932	0.02	0.03	0.06	Snell. 'zx'= 41
1I	-1792	39	83	1	0.8534	0.9865	0.9948	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
1J	-1792	39	-68	1	0.8534	0.9865	0.9950	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1K	-1792	-49	83	1	0.8534	0.9843	0.9948	0.9996	0.9931	0.02	0.01	0.05	Snell. 'zx'= 41
1L	-1792	-49	-68	1	0.8534	0.9843	0.9950	0.9996	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1M	-1490	39	83	1	0.8534	0.9888	0.9957	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
1N	-1490	39	-68	1	0.8534	0.9888	0.9958	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1O	-1490	-49	83	1	0.8534	0.9870	0.9957	0.9996	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
1P	-1490	-49	-68	1	0.8534	0.9870	0.9958	0.9996	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
2	-2449	14	11	1	0.8534	0.9833	0.9920	0.9994	0.9924	0.02	0.00	0.03	Snell. 'zx'= 41
3	-2236	13	10	1	0.8534	0.9848	0.9927	0.9995	0.9924	0.02	0.00	0.03	Snell. 'zx'= 41
4	-2023	12	-4	1	0.8534	0.9863	0.9926	0.9994	0.9917	0.02	0.00	0.03	Snell. 'zx'= 41
5	-2029	19	9	1	0.8534	0.9834	0.9934	0.9995	0.9924	0.02	0.00	0.03	Snell. 'zx'= 41

ASTA NUM. 17 NI 19 NF 24 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1332	-215	6	0	8	206	1	0.01	0.01	0.03	
1B	0	-1332	379	6	0	8	-275	1	0.02	0.01	0.04	
1C	0	-1332	-215	-24	0	-17	206	1	0.01	0.01	0.03	
1D	0	-1332	379	-24	0	-17	-275	1	0.02	0.01	0.04	
1E	0	-882	-215	6	0	8	206	1	0.01	0.01	0.03	
1F	0	-882	379	6	0	8	-275	1	0.02	0.01	0.04	
1G	0	-882	-215	-24	0	-17	206	1	0.01	0.01	0.03	
1H	0	-882	379	-24	0	-17	-275	1	0.02	0.01	0.04	
1I	0	-1299	-21	39	0	35	50	1	0.00	0.01	0.01	
1J	0	-1299	186	39	0	35	-118	1	0.01	0.01	0.02	
1K	0	-1299	-21	-57	0	-45	50	1	0.00	0.01	0.01	
1L	0	-1299	186	-57	0	-45	-118	1	0.01	0.01	0.02	
1M	0	-915	-21	39	0	35	50	1	0.00	0.01	0.01	
1N	0	-915	186	39	0	35	-118	1	0.01	0.01	0.02	
1O	0	-915	-21	-57	0	-45	50	1	0.00	0.01	0.01	
1P	0	-915	186	-57	0	-45	-118	1	0.01	0.01	0.02	
2	0	-1646	124	-13	0	-7	-51	1	0.01	0.01	0.01	
3	0	-1506	112	-12	0	-6	-47	1	0.01	0.01	0.01	
4	0	-1362	108	-12	0	-6	-47	1	0.01	0.01	0.01	
5	0	-1372	100	-20	0	-13	-41	1	0.00	0.01	0.01	
1A	74	-1307	-215	6	0	3	47	1	0.01	0.01	0.01	
1B	74	-1307	379	6	0	3	6	1	0.02	0.01	0.00	
1C	74	-1307	-215	-24	0	1	47	1	0.01	0.01	0.01	
1D	74	-1307	379	-24	0	1	6	1	0.02	0.01	0.00	
1E	74	-857	-215	6	0	3	47	1	0.01	0.01	0.01	
1F	74	-857	379	6	0	3	6	1	0.02	0.01	0.00	
1G	74	-857	-215	-24	0	1	47	1	0.01	0.01	0.01	
1H	74	-857	379	-24	0	1	6	1	0.02	0.01	0.00	
1I	74	-1274	-21	39	0	6	34	1	0.00	0.01	0.01	
1J	74	-1274	186	39	0	6	19	1	0.01	0.01	0.00	
1K	74	-1274	-21	-57	0	-2	34	1	0.00	0.01	0.01	
1L	74	-1274	186	-57	0	-2	19	1	0.01	0.01	0.00	
1M	74	-890	-21	39	0	6	34	1	0.00	0.01	0.01	

1N	74	-890	186	39	0	6	19	1	0.01	0.01	0.00
1O	74	-890	-21	-57	0	-2	34	1	0.00	0.01	0.01
1P	74	-890	186	-57	0	-2	19	1	0.01	0.01	0.00
2	74	-1614	124	-13	0	3	40	1	0.01	0.01	0.01
3	74	-1474	112	-12	0	3	36	1	0.01	0.01	0.01
4	74	-1330	108	-12	0	3	32	1	0.01	0.01	0.00
5	74	-1340	100	-20	0	2	33	1	0.00	0.01	0.01
1A	148	-1282	-215	6	0	-1	-112	1	0.01	0.01	0.02
1B	148	-1282	379	6	0	-1	287	1	0.02	0.01	0.04
1C	148	-1282	-215	-24	0	19	-112	1	0.01	0.01	0.02
1D	148	-1282	379	-24	0	19	287	1	0.02	0.01	0.04
1E	148	-832	-215	6	0	-1	-112	1	0.01	0.01	0.02
1F	148	-832	379	6	0	-1	287	1	0.02	0.01	0.04
1G	148	-832	-215	-24	0	19	-112	1	0.01	0.01	0.02
1H	148	-832	379	-24	0	19	287	1	0.02	0.01	0.04
1I	148	-1249	-21	39	0	-22	18	1	0.00	0.01	0.01
1J	148	-1249	186	39	0	-22	157	1	0.01	0.01	0.02
1K	148	-1249	-21	-57	0	40	18	1	0.00	0.01	0.01
1L	148	-1249	186	-57	0	40	157	1	0.01	0.01	0.02
1M	148	-865	-21	39	0	-22	18	1	0.00	0.01	0.01
1N	148	-865	186	39	0	-22	157	1	0.01	0.01	0.02
1O	148	-865	-21	-57	0	40	18	1	0.00	0.01	0.01
1P	148	-865	186	-57	0	40	157	1	0.01	0.01	0.02
2	148	-1581	124	-13	0	12	132	1	0.01	0.01	0.02
3	148	-1441	112	-12	0	12	120	1	0.01	0.01	0.02
4	148	-1297	108	-12	0	11	112	1	0.01	0.01	0.02
5	148	-1307	100	-20	0	17	107	1	0.00	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-1332	8	206	1	0.8534	0.9944	0.9973	0.9999	0.9915	0.01	0.03	0.05	Snell. 'zx'= 41
1B	-1332	8	287	1	0.8534	0.9944	0.9953	0.9996	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1C	-1332	19	206	1	0.8534	0.9883	0.9973	0.9997	0.9915	0.01	0.03	0.05	Snell. 'zx'= 41
1D	-1332	19	287	1	0.8534	0.9883	0.9953	0.9996	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1E	-882	8	206	1	0.8534	0.9963	0.9982	0.9999	0.9915	0.01	0.03	0.04	Snell. 'zx'= 41
1F	-882	8	287	1	0.8534	0.9963	0.9969	0.9998	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1G	-882	19	206	1	0.8534	0.9923	0.9982	0.9998	0.9915	0.01	0.03	0.05	Snell. 'zx'= 41
1H	-882	19	287	1	0.8534	0.9923	0.9969	0.9998	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1I	-1299	35	50	1	0.8534	0.9902	1.0014	0.9998	0.9710	0.01	0.01	0.03	Snell. 'zx'= 41
1J	-1299	35	157	1	0.8534	0.9902	0.9964	0.9998	0.9932	0.01	0.02	0.05	Snell. 'zx'= 41
1K	-1299	-45	50	1	0.8534	0.9886	1.0014	0.9997	0.9710	0.01	0.01	0.03	Snell. 'zx'= 41
1L	-1299	-45	157	1	0.8534	0.9886	0.9964	0.9997	0.9932	0.01	0.02	0.05	Snell. 'zx'= 41
1M	-915	35	50	1	0.8534	0.9931	1.0010	0.9999	0.9710	0.01	0.01	0.03	Snell. 'zx'= 41
1N	-915	35	157	1	0.8534	0.9931	0.9974	0.9998	0.9932	0.01	0.02	0.04	Snell. 'zx'= 41
1O	-915	-45	50	1	0.8534	0.9920	1.0010	0.9998	0.9710	0.01	0.01	0.03	Snell. 'zx'= 41
1P	-915	-45	157	1	0.8534	0.9920	0.9974	0.9998	0.9932	0.01	0.02	0.05	Snell. 'zx'= 41
2	-1646	12	132	1	0.8534	0.9887	0.9975	0.9999	0.9893	0.02	0.02	0.04	Snell. 'zx'= 41
3	-1506	12	120	1	0.8534	0.9897	0.9977	0.9999	0.9893	0.02	0.02	0.04	Snell. 'zx'= 41
4	-1362	11	112	1	0.8534	0.9907	0.9978	0.9999	0.9898	0.01	0.02	0.03	Snell. 'zx'= 41
5	-1372	17	107	1	0.8534	0.9887	0.9979	0.9998	0.9892	0.01	0.02	0.04	Snell. 'zx'= 41

ASTA NUM. 18 NI 18 NF 25 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1887	-251	4	0	6	214	1	0.01	0.02	0.03	
1B	0	-1887	275	4	0	6	-225	1	0.01	0.02	0.03	
1C	0	-1887	-251	-27	0	-18	214	1	0.01	0.02	0.03	
1D	0	-1887	275	-27	0	-18	-225	1	0.01	0.02	0.03	
1E	0	-1309	-251	4	0	6	214	1	0.01	0.01	0.03	
1F	0	-1309	275	4	0	6	-225	1	0.01	0.01	0.03	
1G	0	-1309	-251	-27	0	-18	214	1	0.01	0.01	0.03	
1H	0	-1309	275	-27	0	-18	-225	1	0.01	0.01	0.03	
1I	0	-2404	-77	28	0	27	68	1	0.00	0.02	0.01	
1J	0	-2404	101	28	0	27	-79	1	0.00	0.02	0.01	
1K	0	-2404	-77	-50	0	-38	68	1	0.00	0.02	0.01	
1L	0	-2404	101	-50	0	-38	-79	1	0.00	0.02	0.01	
1M	0	-792	-77	28	0	27	68	1	0.00	0.01	0.01	
1N	0	-792	101	28	0	27	-79	1	0.00	0.01	0.01	
1O	0	-792	-77	-50	0	-38	68	1	0.00	0.01	0.01	
1P	0	-792	101	-50	0	-38	-79	1	0.00	0.01	0.01	
2	0	-2382	18	-15	0	-8	-8	1	0.00	0.02	0.00	
3	0	-2176	16	-15	0	-8	-7	1	0.00	0.02	0.00	
4	0	-1969	21	-14	0	-7	-11	1	0.00	0.02	0.00	
5	0	-2063	15	-21	0	-13	-6	1	0.00	0.02	0.00	
1A	74	-1862	-251	4	0	3	29	1	0.01	0.02	0.00	
1B	74	-1862	275	4	0	3	-21	1	0.01	0.02	0.00	
1C	74	-1862	-251	-27	0	2	29	1	0.01	0.02	0.00	
1D	74	-1862	275	-27	0	2	-21	1	0.01	0.02	0.00	
1E	74	-1284	-251	4	0	3	29	1	0.01	0.01	0.00	
1F	74	-1284	275	4	0	3	-21	1	0.01	0.01	0.00	
1G	74	-1284	-251	-27	0	2	29	1	0.01	0.01	0.00	
1H	74	-1284	275	-27	0	2	-21	1	0.01	0.01	0.00	
1I	74	-2379	-77	28	0	6	12	1	0.00	0.02	0.00	
1J	74	-2379	101	28	0	6	-4	1	0.00	0.02	0.00	
1K	74	-2379	-77	-50	0	-1	12	1	0.00	0.02	0.00	
1L	74	-2379	101	-50	0	-1	-4	1	0.00	0.02	0.00	
1M	74	-767	-77	28	0	6	12	1	0.00	0.01	0.00	
1N	74	-767	101	28	0	6	-4	1	0.00	0.01	0.00	
1O	74	-767	-77	-50	0	-1	12	1	0.00	0.01	0.00	
1P	74	-767	101	-50	0	-1	-4	1	0.00	0.01	0.00	
2	74	-2350	18	-15	0	4	6	1	0.00	0.02	0.00	
3	74	-2144	16	-15	0	4	5	1	0.00	0.02	0.00	
4	74	-1937	21	-14	0	3	4	1	0.00	0.02	0.00	
5	74	-2031	15	-21	0	3	5	1	0.00	0.02	0.00	
1A	148	-1837	-251	4	0	-0	-157	1	0.01	0.02	0.02	
1B	148	-1837	275	4	0	-0	183	1	0.01	0.02	0.03	
1C	148	-1837	-251	-27	0	22	-157	1	0.01	0.02	0.02	
1D	148	-1837	275	-27	0	22	183	1	0.01	0.02	0.03	
1E	148	-1259	-251	4	0	-0	-157	1	0.01	0.01	0.02	
1F	148	-1259	275	4	0	-0	183	1	0.01	0.01	0.03	
1G	148	-1259	-251	-27	0	22	-157	1	0.01	0.01	0.02	
1H	148	-1259	275	-27	0	22	183	1	0.01	0.01	0.03	
1I	148	-2354	-77	28	0	-14	-45	1	0.00	0.02	0.01	
1J	148	-2354	101	28	0	-14	70	1	0.00	0.02	0.01	
1K	148	-2354	-77	-50	0	37	-45	1	0.00	0.02	0.01	
1L	148	-2354	101	-50	0	37	70	1	0.00	0.02	0.01	
1M	148	-742	-77	28	0	-14	-45	1	0.00	0.01	0.01	

1N	148	-742	101	28	0	-14	70	1	0.00	0.01	0.01
1O	148	-742	-77	-50	0	37	-45	1	0.00	0.01	0.01
1P	148	-742	101	-50	0	37	70	1	0.00	0.01	0.01
2	148	-2317	18	-15	0	15	19	1	0.00	0.02	0.00
3	148	-2111	16	-15	0	15	17	1	0.00	0.02	0.00
4	148	-1904	21	-14	0	14	19	1	0.00	0.02	0.00
5	148	-1998	15	-21	0	19	15	1	0.00	0.02	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-1887	6	214	1	0.8534	0.9934	0.9949	0.9997	0.9931	0.02	0.03	0.05	Snell. 'zx'= 41
1B	-1887	6	-225	1	0.8534	0.9934	0.9943	0.9996	0.9929	0.02	0.03	0.06	Snell. 'zx'= 41
1C	-1887	22	214	1	0.8534	0.9838	0.9949	0.9996	0.9931	0.02	0.03	0.06	Snell. 'zx'= 41
1D	-1887	22	-225	1	0.8534	0.9838	0.9943	0.9996	0.9929	0.02	0.03	0.06	Snell. 'zx'= 41
1E	-1309	6	214	1	0.8534	0.9954	0.9964	0.9998	0.9931	0.01	0.03	0.05	Snell. 'zx'= 41
1F	-1309	6	-225	1	0.8534	0.9954	0.9961	0.9997	0.9929	0.01	0.03	0.05	Snell. 'zx'= 41
1G	-1309	22	214	1	0.8534	0.9888	0.9964	0.9997	0.9931	0.01	0.03	0.05	Snell. 'zx'= 41
1H	-1309	22	-225	1	0.8534	0.9888	0.9961	0.9997	0.9929	0.01	0.03	0.05	Snell. 'zx'= 41
1I	-2404	27	68	1	0.8534	0.9835	0.9941	0.9997	0.9925	0.02	0.01	0.04	Snell. 'zx'= 41
1J	-2404	27	-79	1	0.8534	0.9835	0.9921	0.9994	0.9924	0.02	0.01	0.04	Snell. 'zx'= 41
1K	-2404	-38	68	1	0.8534	0.9790	0.9941	0.9993	0.9925	0.02	0.01	0.05	Snell. 'zx'= 41
1L	-2404	-38	-79	1	0.8534	0.9790	0.9921	0.9993	0.9924	0.02	0.01	0.05	Snell. 'zx'= 41
1M	-792	27	68	1	0.8534	0.9946	0.9981	0.9999	0.9925	0.01	0.01	0.03	Snell. 'zx'= 41
1N	-792	27	-79	1	0.8534	0.9946	0.9974	0.9998	0.9924	0.01	0.01	0.03	Snell. 'zx'= 41
1O	-792	-38	68	1	0.8534	0.9931	0.9981	0.9998	0.9925	0.01	0.01	0.03	Snell. 'zx'= 41
1P	-792	-38	-79	1	0.8534	0.9931	0.9974	0.9998	0.9924	0.01	0.01	0.03	Snell. 'zx'= 41
2	-2382	15	19	1	0.8534	0.9839	0.9962	0.9999	0.9896	0.02	0.00	0.03	Snell. 'zx'= 41
3	-2176	15	17	1	0.8534	0.9854	0.9965	0.9999	0.9896	0.02	0.00	0.03	Snell. 'zx'= 41
4	-1969	14	19	1	0.8534	0.9868	0.9957	0.9998	0.9919	0.02	0.00	0.03	Snell. 'zx'= 41
5	-2063	19	15	1	0.8534	0.9841	0.9968	0.9997	0.9894	0.02	0.00	0.03	Snell. 'zx'= 41

ASTA NUM. 19 NI 17 NF 26 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1887	-275	4	0	6	225	1	0.01	0.02	0.03	
1B	0	-1887	251	4	0	6	-214	1	0.01	0.02	0.03	
1C	0	-1887	-275	-27	0	-18	225	1	0.01	0.02	0.03	
1D	0	-1887	251	-27	0	-18	-214	1	0.01	0.02	0.03	
1E	0	-1309	-275	4	0	6	225	1	0.01	0.01	0.03	
1F	0	-1309	251	4	0	6	-214	1	0.01	0.01	0.03	
1G	0	-1309	-275	-27	0	-18	225	1	0.01	0.01	0.03	
1H	0	-1309	251	-27	0	-18	-214	1	0.01	0.01	0.03	
1I	0	-2404	-101	28	0	27	79	1	0.00	0.02	0.01	
1J	0	-2404	77	28	0	27	-68	1	0.00	0.02	0.01	
1K	0	-2404	-101	-50	0	-38	79	1	0.00	0.02	0.01	
1L	0	-2404	77	-50	0	-38	-68	1	0.00	0.02	0.01	
1M	0	-792	-101	28	0	27	79	1	0.00	0.01	0.01	
1N	0	-792	77	28	0	27	-68	1	0.00	0.01	0.01	
1O	0	-792	-101	-50	0	-38	79	1	0.00	0.01	0.01	
1P	0	-792	77	-50	0	-38	-68	1	0.00	0.01	0.01	

2	0	-2382	-18	-15	0	-8	8	1	0.00	0.02	0.00
3	0	-2176	-16	-15	0	-8	7	1	0.00	0.02	0.00
4	0	-1971	-9	-15	0	-7	1	1	0.00	0.02	0.00
5	0	-2057	-13	-21	0	-12	4	1	0.00	0.02	0.00
1A	74	-1862	-275	4	0	3	21	1	0.01	0.02	0.00
1B	74	-1862	251	4	0	3	-29	1	0.01	0.02	0.00
1C	74	-1862	-275	-27	0	2	21	1	0.01	0.02	0.00
1D	74	-1862	251	-27	0	2	-29	1	0.01	0.02	0.00
1E	74	-1284	-275	4	0	3	21	1	0.01	0.01	0.00
1F	74	-1284	251	4	0	3	-29	1	0.01	0.01	0.00
1G	74	-1284	-275	-27	0	2	21	1	0.01	0.01	0.00
1H	74	-1284	251	-27	0	2	-29	1	0.01	0.01	0.00
1I	74	-2379	-101	28	0	6	4	1	0.00	0.02	0.00
1J	74	-2379	77	28	0	6	-12	1	0.00	0.02	0.00
1K	74	-2379	-101	-50	0	-1	4	1	0.00	0.02	0.00
1L	74	-2379	77	-50	0	-1	-12	1	0.00	0.02	0.00
1M	74	-767	-101	28	0	6	4	1	0.00	0.01	0.00
1N	74	-767	77	28	0	6	-12	1	0.00	0.01	0.00
1O	74	-767	-101	-50	0	-1	4	1	0.00	0.01	0.00
1P	74	-767	77	-50	0	-1	-12	1	0.00	0.01	0.00
2	74	-2350	-18	-15	0	4	-6	1	0.00	0.02	0.00
3	74	-2144	-16	-15	0	4	-5	1	0.00	0.02	0.00
4	74	-1939	-9	-15	0	3	-5	1	0.00	0.02	0.00
5	74	-2025	-13	-21	0	3	-5	1	0.00	0.02	0.00
1A	148	-1837	-275	4	0	-0	-183	1	0.01	0.02	0.03
1B	148	-1837	251	4	0	-0	157	1	0.01	0.02	0.02
1C	148	-1837	-275	-27	0	22	-183	1	0.01	0.02	0.03
1D	148	-1837	251	-27	0	22	157	1	0.01	0.02	0.02
1E	148	-1259	-275	4	0	-0	-183	1	0.01	0.01	0.03
1F	148	-1259	251	4	0	-0	157	1	0.01	0.01	0.02
1G	148	-1259	-275	-27	0	22	-183	1	0.01	0.01	0.03
1H	148	-1259	251	-27	0	22	157	1	0.01	0.01	0.02
1I	148	-2354	-101	28	0	-14	-70	1	0.00	0.02	0.01
1J	148	-2354	77	28	0	-14	45	1	0.00	0.02	0.01
1K	148	-2354	-101	-50	0	37	-70	1	0.00	0.02	0.01
1L	148	-2354	77	-50	0	37	45	1	0.00	0.02	0.01
1M	148	-742	-101	28	0	-14	-70	1	0.00	0.01	0.01
1N	148	-742	77	28	0	-14	45	1	0.00	0.01	0.01
1O	148	-742	-101	-50	0	37	-70	1	0.00	0.01	0.01
1P	148	-742	77	-50	0	37	45	1	0.00	0.01	0.01
2	148	-2317	-18	-15	0	15	-19	1	0.00	0.02	0.00
3	148	-2111	-16	-15	0	15	-17	1	0.00	0.02	0.00
4	148	-1906	-9	-15	0	14	-12	1	0.00	0.02	0.00
5	148	-1992	-13	-21	0	19	-14	1	0.00	0.02	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	-1887	6	225	1	0.8534	0.9934	0.9943	0.9996	0.9929	0.02	0.03	0.06	Snell. 'zx'= 41
1B	-1887	6	-214	1	0.8534	0.9934	0.9949	0.9997	0.9931	0.02	0.03	0.05	Snell. 'zx'= 41
1C	-1887	22	225	1	0.8534	0.9838	0.9943	0.9996	0.9929	0.02	0.03	0.06	Snell. 'zx'= 41
1D	-1887	22	-214	1	0.8534	0.9838	0.9949	0.9996	0.9931	0.02	0.03	0.06	Snell. 'zx'= 41
1E	-1309	6	225	1	0.8534	0.9954	0.9961	0.9997	0.9929	0.01	0.03	0.05	Snell. 'zx'= 41
1F	-1309	6	-214	1	0.8534	0.9954	0.9964	0.9998	0.9931	0.01	0.03	0.05	Snell. 'zx'= 41

1G	-1309	22	225	1	0.8534	0.9888	0.9961	0.9997	0.9929	0.01	0.03	0.05	Snell. 'zx'=	41
1H	-1309	22	-214	1	0.8534	0.9888	0.9964	0.9997	0.9931	0.01	0.03	0.05	Snell. 'zx'=	41
1I	-2404	27	79	1	0.8534	0.9835	0.9921	0.9994	0.9924	0.02	0.01	0.04	Snell. 'zx'=	41
1J	-2404	27	-68	1	0.8534	0.9835	0.9941	0.9997	0.9925	0.02	0.01	0.04	Snell. 'zx'=	41
1K	-2404	-38	79	1	0.8534	0.9790	0.9921	0.9993	0.9924	0.02	0.01	0.05	Snell. 'zx'=	41
1L	-2404	-38	-68	1	0.8534	0.9790	0.9941	0.9993	0.9925	0.02	0.01	0.05	Snell. 'zx'=	41
1M	-792	27	79	1	0.8534	0.9946	0.9974	0.9998	0.9924	0.01	0.01	0.03	Snell. 'zx'=	41
1N	-792	27	-68	1	0.8534	0.9946	0.9981	0.9999	0.9925	0.01	0.01	0.03	Snell. 'zx'=	41
1O	-792	-38	79	1	0.8534	0.9931	0.9974	0.9998	0.9924	0.01	0.01	0.03	Snell. 'zx'=	41
1P	-792	-38	-68	1	0.8534	0.9931	0.9981	0.9998	0.9925	0.01	0.01	0.03	Snell. 'zx'=	41
2	-2382	15	-19	1	0.8534	0.9839	0.9962	0.9999	0.9896	0.02	0.00	0.03	Snell. 'zx'=	41
3	-2176	15	-17	1	0.8534	0.9854	0.9965	0.9999	0.9896	0.02	0.00	0.03	Snell. 'zx'=	41
4	-1971	14	-12	1	0.8534	0.9868	0.9989	0.9999	0.9834	0.02	0.00	0.03	Snell. 'zx'=	41
5	-2057	19	-14	1	0.8534	0.9842	0.9974	0.9997	0.9879	0.02	0.00	0.03	Snell. 'zx'=	41

ASTA NUM. 20 NI 16 NF 27 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1323	-203	6	0	8	199	1	0.01	0.01	0.03	
1B	0	-1323	388	6	0	8	-279	1	0.02	0.01	0.04	
1C	0	-1323	-203	-24	0	-17	199	1	0.01	0.01	0.03	
1D	0	-1323	388	-24	0	-17	-279	1	0.02	0.01	0.04	
1E	0	-971	-203	6	0	8	199	1	0.01	0.01	0.03	
1F	0	-971	388	6	0	8	-279	1	0.02	0.01	0.04	
1G	0	-971	-203	-24	0	-17	199	1	0.01	0.01	0.03	
1H	0	-971	388	-24	0	-17	-279	1	0.02	0.01	0.04	
1I	0	-1321	-14	36	0	33	45	1	0.00	0.01	0.01	
1J	0	-1321	198	36	0	33	-126	1	0.01	0.01	0.02	
1K	0	-1321	-14	-55	0	-42	45	1	0.00	0.01	0.01	
1L	0	-1321	198	-55	0	-42	-126	1	0.01	0.01	0.02	
1M	0	-973	-14	36	0	33	45	1	0.00	0.01	0.01	
1N	0	-973	198	36	0	33	-126	1	0.01	0.01	0.02	
1O	0	-973	-14	-55	0	-42	45	1	0.00	0.01	0.01	
1P	0	-973	198	-55	0	-42	-126	1	0.01	0.01	0.02	
2	0	-1707	139	-13	0	-7	-60	1	0.01	0.01	0.01	
3	0	-1561	126	-12	0	-6	-55	1	0.01	0.01	0.01	
4	0	-1412	120	-12	0	-6	-54	1	0.01	0.01	0.01	
5	0	-1419	117	-19	0	-11	-52	1	0.01	0.01	0.01	
1A	74	-1298	-203	6	0	3	49	1	0.01	0.01	0.01	
1B	74	-1298	388	6	0	3	7	1	0.02	0.01	0.00	
1C	74	-1298	-203	-24	0	1	49	1	0.01	0.01	0.01	
1D	74	-1298	388	-24	0	1	7	1	0.02	0.01	0.00	
1E	74	-946	-203	6	0	3	49	1	0.01	0.01	0.01	
1F	74	-946	388	6	0	3	7	1	0.02	0.01	0.00	
1G	74	-946	-203	-24	0	1	49	1	0.01	0.01	0.01	
1H	74	-946	388	-24	0	1	7	1	0.02	0.01	0.00	
1I	74	-1296	-14	36	0	6	35	1	0.00	0.01	0.01	
1J	74	-1296	198	36	0	6	21	1	0.01	0.01	0.00	
1K	74	-1296	-14	-55	0	-2	35	1	0.00	0.01	0.01	
1L	74	-1296	198	-55	0	-2	21	1	0.01	0.01	0.00	
1M	74	-948	-14	36	0	6	35	1	0.00	0.01	0.01	

1N	74	-948	198	36	0	6	21	1	0.01	0.01	0.00
1O	74	-948	-14	-55	0	-2	35	1	0.00	0.01	0.01
1P	74	-948	198	-55	0	-2	21	1	0.01	0.01	0.00
2	74	-1675	139	-13	0	3	43	1	0.01	0.01	0.01
3	74	-1529	126	-12	0	3	39	1	0.01	0.01	0.01
4	74	-1380	120	-12	0	3	34	1	0.01	0.01	0.01
5	74	-1387	117	-19	0	2	35	1	0.01	0.01	0.01
1A	148	-1273	-203	6	0	-1	-101	1	0.01	0.01	0.02
1B	148	-1273	388	6	0	-1	294	1	0.02	0.01	0.04
1C	148	-1273	-203	-24	0	19	-101	1	0.01	0.01	0.02
1D	148	-1273	388	-24	0	19	294	1	0.02	0.01	0.04
1E	148	-921	-203	6	0	-1	-101	1	0.01	0.01	0.02
1F	148	-921	388	6	0	-1	294	1	0.02	0.01	0.04
1G	148	-921	-203	-24	0	19	-101	1	0.01	0.01	0.02
1H	148	-921	388	-24	0	19	294	1	0.02	0.01	0.04
1I	148	-1271	-14	36	0	-21	25	1	0.00	0.01	0.01
1J	148	-1271	198	36	0	-21	168	1	0.01	0.01	0.03
1K	148	-1271	-14	-55	0	38	25	1	0.00	0.01	0.01
1L	148	-1271	198	-55	0	38	168	1	0.01	0.01	0.03
1M	148	-923	-14	36	0	-21	25	1	0.00	0.01	0.01
1N	148	-923	198	36	0	-21	168	1	0.01	0.01	0.03
1O	148	-923	-14	-55	0	38	25	1	0.00	0.01	0.01
1P	148	-923	198	-55	0	38	168	1	0.01	0.01	0.03
2	148	-1642	139	-13	0	12	145	1	0.01	0.01	0.02
3	148	-1496	126	-12	0	12	132	1	0.01	0.01	0.02
4	148	-1347	120	-12	0	11	123	1	0.01	0.01	0.02
5	148	-1354	117	-19	0	16	121	1	0.01	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-1323	8	199	1	0.8534	0.9947	0.9974	0.9999	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41
1B	-1323	8	294	1	0.8534	0.9947	0.9954	0.9996	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1C	-1323	19	199	1	0.8534	0.9884	0.9974	0.9997	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41
1D	-1323	19	294	1	0.8534	0.9884	0.9954	0.9996	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1E	-971	8	199	1	0.8534	0.9961	0.9981	0.9999	0.9913	0.01	0.03	0.04	Snell. 'zx'= 41
1F	-971	8	294	1	0.8534	0.9961	0.9966	0.9997	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1G	-971	19	199	1	0.8534	0.9915	0.9981	0.9998	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41
1H	-971	19	294	1	0.8534	0.9915	0.9966	0.9997	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1I	-1321	33	45	1	0.8534	0.9902	1.0024	0.9999	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1J	-1321	33	168	1	0.8534	0.9902	0.9963	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1K	-1321	-42	45	1	0.8534	0.9884	1.0024	0.9997	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1L	-1321	-42	168	1	0.8534	0.9884	0.9963	0.9997	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1M	-973	33	45	1	0.8534	0.9928	1.0017	0.9999	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1N	-973	33	168	1	0.8534	0.9928	0.9973	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1O	-973	-42	45	1	0.8534	0.9915	1.0017	0.9998	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1P	-973	-42	168	1	0.8534	0.9915	0.9973	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
2	-1707	12	145	1	0.8534	0.9883	0.9972	0.9999	0.9897	0.02	0.02	0.04	Snell. 'zx'= 41
3	-1561	12	132	1	0.8534	0.9893	0.9975	0.9999	0.9897	0.02	0.02	0.04	Snell. 'zx'= 41
4	-1412	11	123	1	0.8534	0.9904	0.9976	0.9999	0.9902	0.01	0.02	0.04	Snell. 'zx'= 41
5	-1419	16	121	1	0.8534	0.9887	0.9976	0.9998	0.9899	0.01	0.02	0.04	Snell. 'zx'= 41

ASTA NUM. 21 NI 15 NF 28 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm		daN			daN*m						
1A	0	-1723	-263	6	0	8	220	1	0.01	0.02	0.03	
1B	0	-1723	282	6	0	8	-235	1	0.01	0.02	0.04	
1C	0	-1723	-263	-27	0	-19	220	1	0.01	0.02	0.03	
1D	0	-1723	282	-27	0	-19	-235	1	0.01	0.02	0.04	
1E	0	-1559	-263	6	0	8	220	1	0.01	0.01	0.03	
1F	0	-1559	282	6	0	8	-235	1	0.01	0.01	0.04	
1G	0	-1559	-263	-27	0	-19	220	1	0.01	0.01	0.03	
1H	0	-1559	282	-27	0	-19	-235	1	0.01	0.01	0.04	
1I	0	-1792	-80	43	0	39	68	1	0.00	0.02	0.01	
1J	0	-1792	100	43	0	39	-83	1	0.00	0.02	0.01	
1K	0	-1792	-80	-63	0	-49	68	1	0.00	0.02	0.02	
1L	0	-1792	100	-63	0	-49	-83	1	0.00	0.02	0.02	
1M	0	-1490	-80	43	0	39	68	1	0.00	0.01	0.01	
1N	0	-1490	100	43	0	39	-83	1	0.00	0.01	0.01	
1O	0	-1490	-80	-63	0	-49	68	1	0.00	0.01	0.02	
1P	0	-1490	100	-63	0	-49	-83	1	0.00	0.01	0.02	
2	0	-2449	15	-14	0	-7	-12	1	0.00	0.02	0.00	
3	0	-2236	13	-13	0	-7	-10	1	0.00	0.02	0.00	
4	0	-2023	18	-13	0	-7	-14	1	0.00	0.02	0.00	
5	0	-2028	14	-20	0	-12	-11	1	0.00	0.02	0.00	
1A	74	-1698	-263	6	0	4	26	1	0.01	0.01	0.00	
1B	74	-1698	282	6	0	4	-27	1	0.01	0.01	0.00	
1C	74	-1698	-263	-27	0	1	26	1	0.01	0.01	0.00	
1D	74	-1698	282	-27	0	1	-27	1	0.01	0.01	0.00	
1E	74	-1534	-263	6	0	4	26	1	0.01	0.01	0.00	
1F	74	-1534	282	6	0	4	-27	1	0.01	0.01	0.00	
1G	74	-1534	-263	-27	0	1	26	1	0.01	0.01	0.00	
1H	74	-1534	282	-27	0	1	-27	1	0.01	0.01	0.00	
1I	74	-1767	-80	43	0	7	8	1	0.00	0.02	0.00	
1J	74	-1767	100	43	0	7	-9	1	0.00	0.02	0.00	
1K	74	-1767	-80	-63	0	-2	8	1	0.00	0.02	0.00	
1L	74	-1767	100	-63	0	-2	-9	1	0.00	0.02	0.00	
1M	74	-1465	-80	43	0	7	8	1	0.00	0.01	0.00	
1N	74	-1465	100	43	0	7	-9	1	0.00	0.01	0.00	
1O	74	-1465	-80	-63	0	-2	8	1	0.00	0.01	0.00	
1P	74	-1465	100	-63	0	-2	-9	1	0.00	0.01	0.00	
2	74	-2417	15	-14	0	3	-1	1	0.00	0.02	0.00	
3	74	-2204	13	-13	0	3	-1	1	0.00	0.02	0.00	
4	74	-1991	18	-13	0	3	-1	1	0.00	0.02	0.00	
5	74	-1996	14	-20	0	3	-1	1	0.00	0.02	0.00	
1A	148	-1673	-263	6	0	-1	-169	1	0.01	0.01	0.03	
1B	148	-1673	282	6	0	-1	182	1	0.01	0.01	0.03	
1C	148	-1673	-263	-27	0	21	-169	1	0.01	0.01	0.03	
1D	148	-1673	282	-27	0	21	182	1	0.01	0.01	0.03	
1E	148	-1509	-263	6	0	-1	-169	1	0.01	0.01	0.03	
1F	148	-1509	282	6	0	-1	182	1	0.01	0.01	0.03	
1G	148	-1509	-263	-27	0	21	-169	1	0.01	0.01	0.03	
1H	148	-1509	282	-27	0	21	182	1	0.01	0.01	0.03	
1I	148	-1742	-80	43	0	-25	-51	1	0.00	0.02	0.01	
1J	148	-1742	100	43	0	-25	65	1	0.00	0.02	0.01	
1K	148	-1742	-80	-63	0	44	-51	1	0.00	0.02	0.01	
1L	148	-1742	100	-63	0	44	65	1	0.00	0.02	0.01	
1M	148	-1440	-80	43	0	-25	-51	1	0.00	0.01	0.01	

1N	148	-1440	100	43	0	-25	65	1	0.00	0.01	0.01
1O	148	-1440	-80	-63	0	44	-51	1	0.00	0.01	0.01
1P	148	-1440	100	-63	0	44	65	1	0.00	0.01	0.01
2	148	-2384	15	-14	0	14	10	1	0.00	0.02	0.00
3	148	-2171	13	-13	0	13	9	1	0.00	0.02	0.00
4	148	-1958	18	-13	0	13	12	1	0.00	0.02	0.00
5	148	-1963	14	-20	0	18	9	1	0.00	0.02	0.01

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-1723	8	220	1	0.8534	0.9931	0.9951	0.9997	0.9932	0.02	0.03	0.05	Snell. 'zx'= 41
1B	-1723	8	-235	1	0.8534	0.9931	0.9951	0.9997	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1C	-1723	21	220	1	0.8534	0.9849	0.9951	0.9996	0.9932	0.02	0.03	0.06	Snell. 'zx'= 41
1D	-1723	21	-235	1	0.8534	0.9849	0.9951	0.9996	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1E	-1559	8	220	1	0.8534	0.9937	0.9956	0.9997	0.9932	0.02	0.03	0.05	Snell. 'zx'= 41
1F	-1559	8	-235	1	0.8534	0.9937	0.9955	0.9997	0.9931	0.02	0.04	0.05	Snell. 'zx'= 41
1G	-1559	21	220	1	0.8534	0.9864	0.9956	0.9996	0.9932	0.02	0.03	0.06	Snell. 'zx'= 41
1H	-1559	21	-235	1	0.8534	0.9864	0.9955	0.9996	0.9931	0.02	0.04	0.06	Snell. 'zx'= 41
1I	-1792	39	68	1	0.8534	0.9865	0.9950	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1J	-1792	39	-83	1	0.8534	0.9865	0.9948	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
1K	-1792	-49	68	1	0.8534	0.9843	0.9950	0.9996	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1L	-1792	-49	-83	1	0.8534	0.9843	0.9948	0.9996	0.9931	0.02	0.01	0.05	Snell. 'zx'= 41
1M	-1490	39	68	1	0.8534	0.9888	0.9958	0.9997	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1N	-1490	39	-83	1	0.8534	0.9888	0.9957	0.9997	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
1O	-1490	-49	68	1	0.8534	0.9870	0.9958	0.9996	0.9932	0.02	0.01	0.04	Snell. 'zx'= 41
1P	-1490	-49	-83	1	0.8534	0.9870	0.9957	0.9996	0.9931	0.02	0.01	0.04	Snell. 'zx'= 41
2	-2449	14	-11	1	0.8534	0.9833	0.9920	0.9994	0.9924	0.02	0.00	0.03	Snell. 'zx'= 41
3	-2236	13	-10	1	0.8534	0.9848	0.9927	0.9995	0.9924	0.02	0.00	0.03	Snell. 'zx'= 41
4	-2023	13	-14	1	0.8534	0.9863	0.9937	0.9996	0.9927	0.02	0.00	0.03	Snell. 'zx'= 41
5	-2028	18	-11	1	0.8534	0.9840	0.9935	0.9995	0.9925	0.02	0.00	0.03	Snell. 'zx'= 41

ASTA NUM. 22 NI 98 NF 94 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
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	cm	daN			daN*m							
1A	0	-1406	-373	8	0	9	272	1	0.02	0.01	0.04	
1B	0	-1406	187	8	0	9	-179	1	0.01	0.01	0.03	
1C	0	-1406	-373	-26	0	-19	272	1	0.02	0.01	0.04	
1D	0	-1406	187	-26	0	-19	-179	1	0.01	0.01	0.03	
1E	0	-1064	-373	8	0	9	272	1	0.02	0.01	0.04	
1F	0	-1064	187	8	0	9	-179	1	0.01	0.01	0.03	
1G	0	-1064	-373	-26	0	-19	272	1	0.02	0.01	0.04	
1H	0	-1064	187	-26	0	-19	-179	1	0.01	0.01	0.03	
1I	0	-1373	-182	46	0	41	118	1	0.01	0.01	0.02	
1J	0	-1373	-5	46	0	41	-24	1	0.00	0.01	0.01	
1K	0	-1373	-182	-65	0	-51	118	1	0.01	0.01	0.02	
1L	0	-1373	-5	-65	0	-51	-24	1	0.00	0.01	0.02	
1M	0	-1097	-182	46	0	41	118	1	0.01	0.01	0.02	
1N	0	-1097	-5	46	0	41	-24	1	0.00	0.01	0.01	
1O	0	-1097	-182	-65	0	-51	118	1	0.01	0.01	0.02	
1P	0	-1097	-5	-65	0	-51	-24	1	0.00	0.01	0.02	

2	0	-1839	-140	-13	0	-7	71	1	0.01	0.02	0.01
3	0	-1682	-127	-12	0	-6	64	1	0.01	0.01	0.01
4	0	-1513	-110	-12	0	-6	53	1	0.01	0.01	0.01
5	0	-1531	-114	-22	0	-14	57	1	0.01	0.01	0.01
1A	74	-1381	-373	8	0	4	-4	1	0.02	0.01	0.00
1B	74	-1381	187	8	0	4	-40	1	0.01	0.01	0.01
1C	74	-1381	-373	-26	0	1	-4	1	0.02	0.01	0.00
1D	74	-1381	187	-26	0	1	-40	1	0.01	0.01	0.01
1E	74	-1039	-373	8	0	4	-4	1	0.02	0.01	0.00
1F	74	-1039	187	8	0	4	-40	1	0.01	0.01	0.01
1G	74	-1039	-373	-26	0	1	-4	1	0.02	0.01	0.00
1H	74	-1039	187	-26	0	1	-40	1	0.01	0.01	0.01
1I	74	-1348	-182	46	0	7	-17	1	0.01	0.01	0.00
1J	74	-1348	-5	46	0	7	-28	1	0.00	0.01	0.00
1K	74	-1348	-182	-65	0	-3	-17	1	0.01	0.01	0.00
1L	74	-1348	-5	-65	0	-3	-28	1	0.00	0.01	0.00
1M	74	-1072	-182	46	0	7	-17	1	0.01	0.01	0.00
1N	74	-1072	-5	46	0	7	-28	1	0.00	0.01	0.00
1O	74	-1072	-182	-65	0	-3	-17	1	0.01	0.01	0.00
1P	74	-1072	-5	-65	0	-3	-28	1	0.00	0.01	0.00
2	74	-1807	-140	-13	0	3	-33	1	0.01	0.02	0.01
3	74	-1650	-127	-12	0	3	-30	1	0.01	0.01	0.00
4	74	-1481	-110	-12	0	3	-28	1	0.01	0.01	0.00
5	74	-1499	-114	-22	0	2	-27	1	0.01	0.01	0.00
1A	148	-1356	-373	8	0	-2	-281	1	0.02	0.01	0.04
1B	148	-1356	187	8	0	-2	99	1	0.01	0.01	0.02
1C	148	-1356	-373	-26	0	20	-281	1	0.02	0.01	0.04
1D	148	-1356	187	-26	0	20	99	1	0.01	0.01	0.02
1E	148	-1014	-373	8	0	-2	-281	1	0.02	0.01	0.04
1F	148	-1014	187	8	0	-2	99	1	0.01	0.01	0.02
1G	148	-1014	-373	-26	0	20	-281	1	0.02	0.01	0.04
1H	148	-1014	187	-26	0	20	99	1	0.01	0.01	0.02
1I	148	-1323	-182	46	0	-27	-151	1	0.01	0.01	0.02
1J	148	-1323	-5	46	0	-27	-31	1	0.00	0.01	0.01
1K	148	-1323	-182	-65	0	45	-151	1	0.01	0.01	0.02
1L	148	-1323	-5	-65	0	45	-31	1	0.00	0.01	0.01
1M	148	-1047	-182	46	0	-27	-151	1	0.01	0.01	0.02
1N	148	-1047	-5	46	0	-27	-31	1	0.00	0.01	0.01
1O	148	-1047	-182	-65	0	45	-151	1	0.01	0.01	0.02
1P	148	-1047	-5	-65	0	45	-31	1	0.00	0.01	0.01
2	148	-1774	-140	-13	0	12	-137	1	0.01	0.02	0.02
3	148	-1617	-127	-12	0	12	-124	1	0.01	0.01	0.02
4	148	-1448	-110	-12	0	11	-109	1	0.01	0.01	0.02
5	148	-1466	-114	-22	0	18	-111	1	0.01	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	--------											
	daN	daN*m											
1A	-1406	9	-281	1	0.8534	0.9933	0.9950	0.9996	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1B	-1406	9	-179	1	0.8534	0.9933	0.9971	0.9999	0.9916	0.01	0.03	0.04	Snell. 'zx'= 41
1C	-1406	20	-281	1	0.8534	0.9877	0.9950	0.9996	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1D	-1406	20	-179	1	0.8534	0.9877	0.9971	0.9996	0.9916	0.01	0.03	0.05	Snell. 'zx'= 41
1E	-1064	9	-281	1	0.8534	0.9949	0.9962	0.9997	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1F	-1064	9	-179	1	0.8534	0.9949	0.9978	0.9999	0.9916	0.01	0.03	0.04	Snell. 'zx'= 41

1G	-1064	20	-281	1	0.8534	0.9907	0.9962	0.9997	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1H	-1064	20	-179	1	0.8534	0.9907	0.9978	0.9997	0.9916	0.01	0.03	0.04	Snell. 'zx'= 41
1I	-1373	41	-151	1	0.8534	0.9895	0.9960	0.9997	0.9931	0.01	0.02	0.05	Snell. 'zx'= 41
1J	-1373	41	-31	1	0.8534	0.9895	1.0035	0.9998	0.9599	0.01	0.00	0.03	Snell. 'zx'= 41
1K	-1373	-51	-151	1	0.8534	0.9880	0.9960	0.9997	0.9931	0.01	0.02	0.05	Snell. 'zx'= 41
1L	-1373	-51	-31	1	0.8534	0.9880	1.0035	0.9997	0.9599	0.01	0.00	0.03	Snell. 'zx'= 41
1M	-1097	41	-151	1	0.8534	0.9916	0.9968	0.9998	0.9931	0.01	0.02	0.05	Snell. 'zx'= 41
1N	-1097	41	-31	1	0.8534	0.9916	1.0028	0.9999	0.9599	0.01	0.00	0.03	Snell. 'zx'= 41
1O	-1097	-51	-151	1	0.8534	0.9904	0.9968	0.9997	0.9931	0.01	0.02	0.05	Snell. 'zx'= 41
1P	-1097	-51	-31	1	0.8534	0.9904	1.0028	0.9997	0.9599	0.01	0.00	0.03	Snell. 'zx'= 41
2	-1839	12	-137	1	0.8534	0.9874	0.9964	0.9999	0.9913	0.02	0.02	0.04	Snell. 'zx'= 41
3	-1682	12	-124	1	0.8534	0.9885	0.9967	0.9999	0.9913	0.02	0.02	0.04	Snell. 'zx'= 41
4	-1513	11	-109	1	0.8534	0.9897	0.9972	0.9999	0.9910	0.02	0.02	0.04	Snell. 'zx'= 41
5	-1531	18	-111	1	0.8534	0.9872	0.9970	0.9997	0.9913	0.02	0.02	0.04	Snell. 'zx'= 41

ASTA NUM. 23 NI 99 NF 93 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica — Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-2494	-445	21	0	16	303	1	0.02	0.02	0.05	
1B	0	-2494	114	21	0	16	-147	1	0.01	0.02	0.02	
1C	0	-2494	-445	-21	0	-16	303	1	0.02	0.02	0.05	
1D	0	-2494	114	-21	0	-16	-147	1	0.01	0.02	0.02	
1E	0	-2281	-445	21	0	16	303	1	0.02	0.02	0.05	
1F	0	-2281	114	21	0	16	-147	1	0.01	0.02	0.02	
1G	0	-2281	-445	-21	0	-16	303	1	0.02	0.02	0.05	
1H	0	-2281	114	-21	0	-16	-147	1	0.01	0.02	0.02	
1I	0	-2419	-249	69	0	53	146	1	0.01	0.02	0.02	
1J	0	-2419	-82	69	0	53	11	1	0.00	0.02	0.02	
1K	0	-2419	-249	-69	0	-53	146	1	0.01	0.02	0.02	
1L	0	-2419	-82	-69	0	-53	11	1	0.00	0.02	0.02	
1M	0	-2355	-249	69	0	53	146	1	0.01	0.02	0.02	
1N	0	-2355	-82	69	0	53	11	1	0.00	0.02	0.02	
1O	0	-2355	-249	-69	0	-53	146	1	0.01	0.02	0.02	
1P	0	-2355	-82	-69	0	-53	11	1	0.00	0.02	0.02	
2	0	-3569	-250	-0	0	-0	119	1	0.01	0.03	0.02	
3	0	-3254	-226	-0	0	-0	107	1	0.01	0.03	0.02	
4	0	-2913	-200	-0	0	-0	92	1	0.01	0.03	0.01	
5	0	-2927	-203	-9	0	-7	96	1	0.01	0.03	0.01	
1A	74	-2469	-445	21	0	0	-26	1	0.02	0.02	0.00	
1B	74	-2469	114	21	0	0	-62	1	0.01	0.02	0.01	
1C	74	-2469	-445	-21	0	-0	-26	1	0.02	0.02	0.00	
1D	74	-2469	114	-21	0	-0	-62	1	0.01	0.02	0.01	
1E	74	-2256	-445	21	0	0	-26	1	0.02	0.02	0.00	
1F	74	-2256	114	21	0	0	-62	1	0.01	0.02	0.01	
1G	74	-2256	-445	-21	0	-0	-26	1	0.02	0.02	0.00	
1H	74	-2256	114	-21	0	-0	-62	1	0.01	0.02	0.01	
1I	74	-2394	-249	69	0	2	-39	1	0.01	0.02	0.01	
1J	74	-2394	-82	69	0	2	-49	1	0.00	0.02	0.01	
1K	74	-2394	-249	-69	0	-2	-39	1	0.01	0.02	0.01	
1L	74	-2394	-82	-69	0	-2	-49	1	0.00	0.02	0.01	
1M	74	-2330	-249	69	0	2	-39	1	0.01	0.02	0.01	

1N	74	-2330	-82	69	0	2	-49	1	0.00	0.02	0.01
1O	74	-2330	-249	-69	0	-2	-39	1	0.01	0.02	0.01
1P	74	-2330	-82	-69	0	-2	-49	1	0.00	0.02	0.01
2	74	-3537	-250	-0	0	0	-66	1	0.01	0.03	0.01
3	74	-3222	-226	-0	0	0	-60	1	0.01	0.03	0.01
4	74	-2881	-200	-0	0	0	-55	1	0.01	0.03	0.01
5	74	-2895	-203	-9	0	-1	-54	1	0.01	0.03	0.01
1A	148	-2444	-445	21	0	-15	-356	1	0.02	0.02	0.05
1B	148	-2444	114	21	0	-15	23	1	0.01	0.02	0.00
1C	148	-2444	-445	-21	0	15	-356	1	0.02	0.02	0.05
1D	148	-2444	114	-21	0	15	23	1	0.01	0.02	0.00
1E	148	-2231	-445	21	0	-15	-356	1	0.02	0.02	0.05
1F	148	-2231	114	21	0	-15	23	1	0.01	0.02	0.00
1G	148	-2231	-445	-21	0	15	-356	1	0.02	0.02	0.05
1H	148	-2231	114	-21	0	15	23	1	0.01	0.02	0.00
1I	148	-2369	-249	69	0	-49	-223	1	0.01	0.02	0.03
1J	148	-2369	-82	69	0	-49	-110	1	0.00	0.02	0.02
1K	148	-2369	-249	-69	0	49	-223	1	0.01	0.02	0.03
1L	148	-2369	-82	-69	0	49	-110	1	0.00	0.02	0.02
1M	148	-2305	-249	69	0	-49	-223	1	0.01	0.02	0.03
1N	148	-2305	-82	69	0	-49	-110	1	0.00	0.02	0.02
1O	148	-2305	-249	-69	0	49	-223	1	0.01	0.02	0.03
1P	148	-2305	-82	-69	0	49	-110	1	0.00	0.02	0.02
2	148	-3504	-250	-0	0	0	-251	1	0.01	0.03	0.04
3	148	-3189	-226	-0	0	0	-228	1	0.01	0.03	0.03
4	148	-2848	-200	-0	0	0	-203	1	0.01	0.02	0.03
5	148	-2862	-203	-9	0	6	-204	1	0.01	0.02	0.03

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	--	----------											
	daN	daN*m											
1A	-2494	16	-356	1	0.8534	0.9782	0.9922	0.9993	0.9926	0.03	0.05	0.08	Snell. 'zx'= 41
1B	-2494	16	-147	1	0.8534	0.9782	0.9982	0.9993	0.9843	0.03	0.02	0.05	Snell. 'zx'= 41
1C	-2494	-16	-356	1	0.8534	0.9782	0.9922	0.9993	0.9926	0.03	0.05	0.08	Snell. 'zx'= 41
1D	-2494	-16	-147	1	0.8534	0.9782	0.9982	0.9993	0.9843	0.03	0.02	0.05	Snell. 'zx'= 41
1E	-2281	16	-356	1	0.8534	0.9800	0.9928	0.9994	0.9926	0.02	0.05	0.08	Snell. 'zx'= 41
1F	-2281	16	-147	1	0.8534	0.9800	0.9984	0.9994	0.9843	0.02	0.02	0.05	Snell. 'zx'= 41
1G	-2281	-16	-356	1	0.8534	0.9800	0.9928	0.9994	0.9926	0.02	0.05	0.08	Snell. 'zx'= 41
1H	-2281	-16	-147	1	0.8534	0.9800	0.9984	0.9994	0.9843	0.02	0.02	0.05	Snell. 'zx'= 41
1I	-2419	53	-223	1	0.8534	0.9788	0.9941	0.9994	0.9925	0.02	0.03	0.07	Snell. 'zx'= 41
1J	-2419	53	-110	1	0.8534	0.9788	0.9987	0.9994	0.9830	0.02	0.02	0.06	Snell. 'zx'= 41
1K	-2419	-53	-223	1	0.8534	0.9788	0.9941	0.9994	0.9925	0.02	0.03	0.07	Snell. 'zx'= 41
1L	-2419	-53	-110	1	0.8534	0.9788	0.9987	0.9994	0.9830	0.02	0.02	0.06	Snell. 'zx'= 41
1M	-2355	53	-223	1	0.8534	0.9794	0.9942	0.9994	0.9925	0.02	0.03	0.07	Snell. 'zx'= 41
1N	-2355	53	-110	1	0.8534	0.9794	0.9988	0.9994	0.9830	0.02	0.02	0.06	Snell. 'zx'= 41
1O	-2355	-53	-223	1	0.8534	0.9794	0.9942	0.9994	0.9925	0.02	0.03	0.07	Snell. 'zx'= 41
1P	-2355	-53	-110	1	0.8534	0.9794	0.9988	0.9994	0.9830	0.02	0.02	0.06	Snell. 'zx'= 41
2	-3569	0	-251	1	0.8534	1.0476	0.9935	0.9999	0.9907	0.04	0.04	0.07	Snell. 'zx'= 41
3	-3254	0	-228	1	0.8534	1.0434	0.9941	0.9999	0.9907	0.03	0.04	0.07	Snell. 'zx'= 41
4	-2913	0	-203	1	0.8534	1.0388	0.9949	0.9999	0.9904	0.03	0.03	0.06	Snell. 'zx'= 41
5	-2927	-7	-204	1	0.8534	0.9756	0.9947	0.9995	0.9907	0.03	0.03	0.06	Snell. 'zx'= 41

ASTA NUM. 24 NI 100 NF 92 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm		daN			daN*m						
1A	0	-1406	-373	26	0	19	272	1	0.02	0.01	0.04	
1B	0	-1406	187	26	0	19	-179	1	0.01	0.01	0.03	
1C	0	-1406	-373	-8	0	-9	272	1	0.02	0.01	0.04	
1D	0	-1406	187	-8	0	-9	-179	1	0.01	0.01	0.03	
1E	0	-1064	-373	26	0	19	272	1	0.02	0.01	0.04	
1F	0	-1064	187	26	0	19	-179	1	0.01	0.01	0.03	
1G	0	-1064	-373	-8	0	-9	272	1	0.02	0.01	0.04	
1H	0	-1064	187	-8	0	-9	-179	1	0.01	0.01	0.03	
1I	0	-1373	-182	65	0	51	118	1	0.01	0.01	0.02	
1J	0	-1373	-5	65	0	51	-24	1	0.00	0.01	0.02	
1K	0	-1373	-182	-46	0	-41	118	1	0.01	0.01	0.02	
1L	0	-1373	-5	-46	0	-41	-24	1	0.00	0.01	0.01	
1M	0	-1097	-182	65	0	51	118	1	0.01	0.01	0.02	
1N	0	-1097	-5	65	0	51	-24	1	0.00	0.01	0.02	
1O	0	-1097	-182	-46	0	-41	118	1	0.01	0.01	0.02	
1P	0	-1097	-5	-46	0	-41	-24	1	0.00	0.01	0.01	
2	0	-1839	-140	13	0	7	71	1	0.01	0.02	0.01	
3	0	-1682	-127	12	0	6	64	1	0.01	0.01	0.01	
4	0	-1513	-110	12	0	6	53	1	0.01	0.01	0.01	
5	0	-1530	-115	-137	0	-39	58	1	0.01	0.01	0.01	
1A	74	-1381	-373	26	0	-1	-4	1	0.02	0.01	0.00	
1B	74	-1381	187	26	0	-1	-40	1	0.01	0.01	0.01	
1C	74	-1381	-373	-8	0	-4	-4	1	0.02	0.01	0.00	
1D	74	-1381	187	-8	0	-4	-40	1	0.01	0.01	0.01	
1E	74	-1039	-373	26	0	-1	-4	1	0.02	0.01	0.00	
1F	74	-1039	187	26	0	-1	-40	1	0.01	0.01	0.01	
1G	74	-1039	-373	-8	0	-4	-4	1	0.02	0.01	0.00	
1H	74	-1039	187	-8	0	-4	-40	1	0.01	0.01	0.01	
1I	74	-1348	-182	65	0	3	-17	1	0.01	0.01	0.00	
1J	74	-1348	-5	65	0	3	-28	1	0.00	0.01	0.00	
1K	74	-1348	-182	-46	0	-7	-17	1	0.01	0.01	0.00	
1L	74	-1348	-5	-46	0	-7	-28	1	0.00	0.01	0.00	
1M	74	-1072	-182	65	0	3	-17	1	0.01	0.01	0.00	
1N	74	-1072	-5	65	0	3	-28	1	0.00	0.01	0.00	
1O	74	-1072	-182	-46	0	-7	-17	1	0.01	0.01	0.00	
1P	74	-1072	-5	-46	0	-7	-28	1	0.00	0.01	0.00	
2	74	-1807	-140	13	0	-3	-33	1	0.01	0.02	0.01	
3	74	-1650	-127	12	0	-3	-30	1	0.01	0.01	0.00	
4	74	-1481	-110	12	0	-3	-28	1	0.01	0.01	0.00	
5	74	-1498	-115	-10	0	15	-27	1	0.01	0.01	0.00	
1A	148	-1356	-373	26	0	-20	-281	1	0.02	0.01	0.04	
1B	148	-1356	187	26	0	-20	99	1	0.01	0.01	0.02	
1C	148	-1356	-373	-8	0	2	-281	1	0.02	0.01	0.04	
1D	148	-1356	187	-8	0	2	99	1	0.01	0.01	0.02	
1E	148	-1014	-373	26	0	-20	-281	1	0.02	0.01	0.04	
1F	148	-1014	187	26	0	-20	99	1	0.01	0.01	0.02	
1G	148	-1014	-373	-8	0	2	-281	1	0.02	0.01	0.04	
1H	148	-1014	187	-8	0	2	99	1	0.01	0.01	0.02	
1I	148	-1323	-182	65	0	-45	-151	1	0.01	0.01	0.02	
1J	148	-1323	-5	65	0	-45	-31	1	0.00	0.01	0.01	
1K	148	-1323	-182	-46	0	27	-151	1	0.01	0.01	0.02	
1L	148	-1323	-5	-46	0	27	-31	1	0.00	0.01	0.01	
1M	148	-1047	-182	65	0	-45	-151	1	0.01	0.01	0.02	

1N	148	-1047	-5	65	0	-45	-31	1	0.00	0.01	0.01
1O	148	-1047	-182	-46	0	27	-151	1	0.01	0.01	0.02
1P	148	-1047	-5	-46	0	27	-31	1	0.00	0.01	0.01
2	148	-1774	-140	13	0	-12	-137	1	0.01	0.02	0.02
3	148	-1617	-127	12	0	-12	-124	1	0.01	0.01	0.02
4	148	-1448	-110	12	0	-11	-109	1	0.01	0.01	0.02
5	148	-1465	-115	118	0	-25	-112	1	0.01	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	daN	daN*m											
1A	-1406	-20	-281	1	0.8534	1.0050	0.9950	0.9996	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1B	-1406	-20	-179	1	0.8534	1.0050	0.9971	0.9999	0.9916	0.01	0.03	0.05	Snell. 'zx'= 41
1C	-1406	-9	-281	1	0.8534	1.0289	0.9950	0.9996	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1D	-1406	-9	-179	1	0.8534	1.0289	0.9971	0.9999	0.9916	0.01	0.03	0.04	Snell. 'zx'= 41
1E	-1064	-20	-281	1	0.8534	1.0038	0.9962	0.9997	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1F	-1064	-20	-179	1	0.8534	1.0038	0.9978	0.9999	0.9916	0.01	0.03	0.04	Snell. 'zx'= 41
1G	-1064	-9	-281	1	0.8534	1.0219	0.9962	0.9997	0.9919	0.01	0.04	0.06	Snell. 'zx'= 41
1H	-1064	-9	-179	1	0.8534	1.0219	0.9978	0.9999	0.9916	0.01	0.03	0.04	Snell. 'zx'= 41
1I	-1373	51	-151	1	0.8534	0.9945	0.9960	0.9997	0.9931	0.01	0.02	0.05	Snell. 'zx'= 41
1J	-1373	51	-31	1	0.8534	0.9945	1.0035	1.0000	0.9599	0.01	0.00	0.03	Snell. 'zx'= 41
1K	-1373	-41	-151	1	0.8534	0.9980	0.9960	0.9997	0.9931	0.01	0.02	0.05	Snell. 'zx'= 41
1L	-1373	-41	-31	1	0.8534	0.9980	1.0035	1.0000	0.9599	0.01	0.00	0.03	Snell. 'zx'= 41
1M	-1097	51	-151	1	0.8534	0.9956	0.9968	0.9998	0.9931	0.01	0.02	0.05	Snell. 'zx'= 41
1N	-1097	51	-31	1	0.8534	0.9956	1.0028	1.0000	0.9599	0.01	0.00	0.03	Snell. 'zx'= 41
1O	-1097	-41	-151	1	0.8534	0.9984	0.9968	0.9998	0.9931	0.01	0.02	0.05	Snell. 'zx'= 41
1P	-1097	-41	-31	1	0.8534	0.9984	1.0028	1.0000	0.9599	0.01	0.00	0.03	Snell. 'zx'= 41
2	-1839	-12	-137	1	0.8534	1.0248	0.9964	0.9999	0.9913	0.02	0.02	0.04	Snell. 'zx'= 41
3	-1682	-12	-124	1	0.8534	1.0239	0.9967	0.9999	0.9913	0.02	0.02	0.04	Snell. 'zx'= 41
4	-1513	-11	-109	1	0.8534	1.0228	0.9972	0.9999	0.9910	0.02	0.02	0.04	Snell. 'zx'= 41
5	-1530	-39	-112	1	0.8534	1.0019	0.9970	0.9999	0.9913	0.02	0.02	0.04	Snell. 'zx'= 41

ASTA NUM. 25 NI 110 NF 106 Lungh. 148.0 cm SEZ. 1 Ps HEB 140

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	daN			daN*m							
1A	0	-1323	-388	24	0	17	279	1	0.02	0.01	0.04	
1B	0	-1323	203	24	0	17	-199	1	0.01	0.01	0.03	
1C	0	-1323	-388	-6	0	-8	279	1	0.02	0.01	0.04	
1D	0	-1323	203	-6	0	-8	-199	1	0.01	0.01	0.03	
1E	0	-971	-388	24	0	17	279	1	0.02	0.01	0.04	
1F	0	-971	203	24	0	17	-199	1	0.01	0.01	0.03	
1G	0	-971	-388	-6	0	-8	279	1	0.02	0.01	0.04	
1H	0	-971	203	-6	0	-8	-199	1	0.01	0.01	0.03	
1I	0	-1321	-198	55	0	42	126	1	0.01	0.01	0.02	
1J	0	-1321	14	55	0	42	-45	1	0.00	0.01	0.01	
1K	0	-1321	-198	-36	0	-33	126	1	0.01	0.01	0.02	
1L	0	-1321	14	-36	0	-33	-45	1	0.00	0.01	0.01	
1M	0	-973	-198	55	0	42	126	1	0.01	0.01	0.02	
1N	0	-973	14	55	0	42	-45	1	0.00	0.01	0.01	
1O	0	-973	-198	-36	0	-33	126	1	0.01	0.01	0.02	
1P	0	-973	14	-36	0	-33	-45	1	0.00	0.01	0.01	

2	0	-1707	-139	13	0	7	60	1	0.01	0.01	0.01
3	0	-1561	-126	12	0	6	55	1	0.01	0.01	0.01
4	0	-1420	-107	12	0	6	44	1	0.01	0.01	0.01
5	0	-1423	-112	-137	0	-38	48	1	0.01	0.01	0.01
1A	74	-1298	-388	24	0	-1	-7	1	0.02	0.01	0.00
1B	74	-1298	203	24	0	-1	-49	1	0.01	0.01	0.01
1C	74	-1298	-388	-6	0	-3	-7	1	0.02	0.01	0.00
1D	74	-1298	203	-6	0	-3	-49	1	0.01	0.01	0.01
1E	74	-946	-388	24	0	-1	-7	1	0.02	0.01	0.00
1F	74	-946	203	24	0	-1	-49	1	0.01	0.01	0.01
1G	74	-946	-388	-6	0	-3	-7	1	0.02	0.01	0.00
1H	74	-946	203	-6	0	-3	-49	1	0.01	0.01	0.01
1I	74	-1296	-198	55	0	2	-21	1	0.01	0.01	0.00
1J	74	-1296	14	55	0	2	-35	1	0.00	0.01	0.01
1K	74	-1296	-198	-36	0	-6	-21	1	0.01	0.01	0.00
1L	74	-1296	14	-36	0	-6	-35	1	0.00	0.01	0.01
1M	74	-948	-198	55	0	2	-21	1	0.01	0.01	0.00
1N	74	-948	14	55	0	2	-35	1	0.00	0.01	0.01
1O	74	-948	-198	-36	0	-6	-21	1	0.01	0.01	0.00
1P	74	-948	14	-36	0	-6	-35	1	0.00	0.01	0.01
2	74	-1675	-139	13	0	-3	-43	1	0.01	0.01	0.01
3	74	-1529	-126	12	0	-3	-39	1	0.01	0.01	0.01
4	74	-1388	-107	12	0	-3	-35	1	0.01	0.01	0.01
5	74	-1391	-112	-8	0	16	-35	1	0.01	0.01	0.01
1A	148	-1273	-388	24	0	-19	-294	1	0.02	0.01	0.04
1B	148	-1273	203	24	0	-19	101	1	0.01	0.01	0.02
1C	148	-1273	-388	-6	0	1	-294	1	0.02	0.01	0.04
1D	148	-1273	203	-6	0	1	101	1	0.01	0.01	0.02
1E	148	-921	-388	24	0	-19	-294	1	0.02	0.01	0.04
1F	148	-921	203	24	0	-19	101	1	0.01	0.01	0.02
1G	148	-921	-388	-6	0	1	-294	1	0.02	0.01	0.04
1H	148	-921	203	-6	0	1	101	1	0.01	0.01	0.02
1I	148	-1271	-198	55	0	-38	-168	1	0.01	0.01	0.03
1J	148	-1271	14	55	0	-38	-25	1	0.00	0.01	0.01
1K	148	-1271	-198	-36	0	21	-168	1	0.01	0.01	0.03
1L	148	-1271	14	-36	0	21	-25	1	0.00	0.01	0.01
1M	148	-923	-198	55	0	-38	-168	1	0.01	0.01	0.03
1N	148	-923	14	55	0	-38	-25	1	0.00	0.01	0.01
1O	148	-923	-198	-36	0	21	-168	1	0.01	0.01	0.03
1P	148	-923	14	-36	0	21	-25	1	0.00	0.01	0.01
2	148	-1642	-139	13	0	-12	-145	1	0.01	0.01	0.02
3	148	-1496	-126	12	0	-12	-132	1	0.01	0.01	0.02
4	148	-1355	-107	12	0	-11	-114	1	0.01	0.01	0.02
5	148	-1358	-112	121	0	-26	-118	1	0.01	0.01	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χmin.	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
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	daN	daN*m											
1A	-1323	-19	-294	1	0.8534	1.0066	0.9954	0.9996	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1B	-1323	-19	-199	1	0.8534	1.0066	0.9974	0.9999	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41
1C	-1323	-8	-294	1	0.8534	1.0353	0.9954	0.9996	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1D	-1323	-8	-199	1	0.8534	1.0353	0.9974	0.9999	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41
1E	-971	-19	-294	1	0.8534	1.0048	0.9966	0.9997	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1F	-971	-19	-199	1	0.8534	1.0048	0.9981	0.9999	0.9913	0.01	0.03	0.05	Snell. 'zx'= 41

1G	-971	-8	-294	1	0.8534	1.0259	0.9966	0.9997	0.9920	0.01	0.05	0.06	Snell. 'zx'= 41
1H	-971	-8	-199	1	0.8534	1.0259	0.9981	0.9999	0.9913	0.01	0.03	0.04	Snell. 'zx'= 41
1I	-1321	42	-168	1	0.8534	0.9960	0.9963	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1J	-1321	42	-45	1	0.8534	0.9960	1.0024	1.0000	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1K	-1321	-33	-168	1	0.8534	1.0005	0.9963	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1L	-1321	-33	-45	1	0.8534	1.0005	1.0024	1.0000	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1M	-973	42	-168	1	0.8534	0.9971	0.9973	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1N	-973	42	-45	1	0.8534	0.9971	1.0017	1.0000	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
1O	-973	-33	-168	1	0.8534	1.0004	0.9973	0.9998	0.9932	0.01	0.03	0.05	Snell. 'zx'= 41
1P	-973	-33	-45	1	0.8534	1.0004	1.0017	1.0000	0.9658	0.01	0.01	0.03	Snell. 'zx'= 41
2	-1707	-12	-145	1	0.8534	1.0240	0.9972	1.0000	0.9897	0.02	0.02	0.04	Snell. 'zx'= 41
3	-1561	-12	-132	1	0.8534	1.0231	0.9975	1.0000	0.9897	0.02	0.02	0.04	Snell. 'zx'= 41
4	-1420	-11	-114	1	0.8534	1.0222	0.9979	1.0000	0.9891	0.01	0.02	0.04	Snell. 'zx'= 41
5	-1423	-38	-118	1	0.8534	1.0019	0.9977	1.0000	0.9896	0.01	0.02	0.04	Snell. 'zx'= 41

9. GIUDIZIO MOTIVATO DI ACCETTABILITÀ DEI RISULTATI

I risultati delle elaborazioni sono stati sottoposti a controlli che ne comprovano l'attendibilità. Tale valutazione ha compreso il confronto con i risultati di semplici calcoli, eseguiti con metodi tradizionali e adottati, anche in fase di primo proporzionamento della struttura. Inoltre, sulla base di considerazioni riguardanti gli stati tensionali e deformativi determinati, si è valutata la validità delle scelte operate in sede di schematizzazione e di modellazione della struttura e delle azioni. Si allega al termine della presente relazione elenco sintetico dei controlli svolti (verifiche di equilibrio tra reazioni vincolari e carichi applicati, comparazioni tra i risultati delle analisi e quelli di valutazioni semplificate, etc.).

In base a quando detto, si può asserire che l'elaborazione è corretta ed idonea al caso specifico; pertanto, i risultati di calcolo sono da ritenersi validi ed accettabili.

10. CONCLUSIONI

La struttura in tutte le sue componenti è idonea a sostenere le sollecitazioni trasmesse dai carichi e dall'effetto sismico.

Sono state rispettate le "Norme Tecniche per le Costruzioni" di cui al D.M. Infrastrutture 17 gennaio 2018, nonché la Circolare 21 Gennaio 2019 n. 7 del Consiglio Superiore dei LL.PP. – Istruzioni per l'applicazione dell'"Aggiornamento delle "Norme Tecniche per le Costruzioni" di cui D.M. Infrastrutture 17 Gennaio 2018".

Lì, 22/03/2022

Il Tecnico

Dott. Ing. Pasquale IZZO

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