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TITLE: CALCOLI PRELIMINARI DI DIMENSIONAMENTO DELLE STRUTTURE

AVAILABLE LANGUAGE: IT

CALCOLI PRELIMINARI DI DIMENSIONAMENTO DELLE STRUTTURE

Progetto di un impianto agrivoltaico della potenza complessiva di 103.314,00 kW_p con sistema di accumulo di capacità pari a 20 MW e relative opere di connessione alla rete.

Da realizzarsi nei Comuni di Foggia, Manfredonia (FG)
e Zapponeta (FG)

File: FOM.ENG.REL.005.00_Calcoli preliminari di dimensionamento strutture

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UTILIZATION SCOPE *Basic Design*

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1.0 INDICAZIONI GENERALI

1.1 Struttura

Legge 5 novembre 1971 N. 1086 - Norme per la disciplina delle opere in conglomerato cementizio armato normale e precompresso ed a struttura metallica.

Decreto Ministeriale 17/01/2018 – Aggiornamento delle Norme tecniche per le Costruzioni.

Circolare Esplicativa 21/01/2019 – Istruzioni per l'applicazione dell'aggiornamento delle Norme tecniche per le Costruzioni D.M. 17/01/2018.

1.2 Norme di cui è consentita l'applicazione ai sensi del cap. 12 del D.M. 17/01/2018

UNI EN 1990: 2006 - Eurocodice 1 – Criteri generali di progettazione strutturale.

UNI ENV 1991-1-1: 2010; -1-2; 1-3; 1-4; 1.5; Azioni sulla struttura.

Eurocodice 2 - Progettazione delle strutture in calcestruzzo.

UNI ENV 1992-1-1 Parte 1-1: Regole generali e regole per gli edifici.

Eurocodice 3 – Progettazione delle strutture in acciaio.

UNI ENV 1993-1-1 - Parte 1-1: Regole generali e regole per gli edifici.

UNI EN 206:2016 - Calcestruzzo. Specificazioni, prestazioni, produzione e conformità.

Servizio Tecnico Centrale del Ministero dei Lavori Pubblici – “Linee Guida sul calcestruzzo strutturale”

Circ. MIN.LL.PP. N.11951 del 14 febbraio 1992 - Circolare illustrativa della legge N. 1086.

1.3 Carichi e sovraccarichi

Decreto Ministeriale 17/01/2018 – Aggiornamento delle Norme tecniche per le Costruzioni.

Circolare Esplicativa 21/01/2019 – Istruzioni per l'applicazione dell'aggiornamento delle Norme tecniche per le Costruzioni D.M. 17/01/2018.

1.4 Terreni e fondazione

Decreto Ministeriale 17/01/2018 – Aggiornamento delle Norme tecniche per le Costruzioni.

Circolare Esplicativa 21/01/2019 – Istruzioni per l'applicazione dell'aggiornamento delle Norme tecniche per le Costruzioni D.M. 17/01/2018.

D.M. 11 marzo 1988 – Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione ed il collaudo delle opere di sostegno delle terre e delle opere di fondazione.

Circ. MIN.LL.PP. N.30483 del 24 settembre 1988 - Istruzioni riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione ed il collaudo delle opere di sostegno delle terre.

1.5 Norme generali di riferimento

"Linee guida in materia di impianti agrivoltaici", Ministero della Transizione Ecologica - Dipartimento per l'energia.

LEGGE 29 luglio 2021, n. 108 *"Conversione in legge, con modificazioni, del decreto-legge 31 maggio 2021, n. 77, recante governance del Piano nazionale di ripresa e resilienza e prime misure di rafforzamento delle strutture amministrative e di accelerazione e snellimento delle procedure"*.

"Consultazione pubblica Misura PNRR Sviluppo Agrivoltaico: Piano di Ripresa e Resilienza, Missione 2 (Rivoluzione verde e Transizione ecologica), Componente 2 (Energia rinnovabile, idrogeno, rete e mobilità sostenibile), Investimento 1.1 (Sviluppo Agrovoltaico)".

"Piano Nazionale Integrato per l'Energia e il Clima 2030 (PNIEC)", Ministero dello Sviluppo Economico ([PNIEC finale 17012020.pdf \(mise.gov.it\)](#)).



D.Lgs. 8 novembre 2021, n. 199, di recepimento della direttiva UE 2018/2001 del Parlamento europeo e del Consiglio sulla promozione dell'uso dell'energia da fonti rinnovabili (*Direttiva RED II*).

2.0 DESCRIZIONE GENERALE DEL PROGETTO

2.1 Generalità

La presente relazione riguarda il dimensionamento e le verifiche preliminari lato struttura (STR) delle strutture previste per il progetto definitivo, proposto da Foggia Solar S.r.l., che prevede la realizzazione di un impianto agrivoltaico con sistema di accumulo denominato "Foggia-Manfredonia", localizzato nei Comuni di Foggia, Manfredonia e Zapponeta in Provincia di Foggia.

L'impianto, installato a terra, con potenza di picco pari a 103.314,00 kW_p ed integrato da un sistema di accumulo da 20 MW, è destinato ad essere collegato in antenna a 150 kV su un futuro ampliamento della Stazione Elettrica a 380/150 kV della RTN di Manfredonia come indicato nella Soluzione Tecnica Minima Generale (STMG) fornita dal distributore di rete.

Viene quindi prevista, ai fini della connessione sopra descritta, la realizzazione di una Sottostazione Elettrica di Utenza per l'innalzamento della potenza da MT ad AT, nei pressi della SE di Manfredonia.

L'agrivoltaico prevede l'integrazione della tecnologia fotovoltaica nell'attività agricola permettendo di produrre energia e al contempo di continuare la coltivazione delle colture agricole o l'allevamento di animali sui terreni interessati.

I criteri generali adottati per lo sviluppo del presente progetto sono in linea con le prescrizioni contenute nel quadro normativo di riferimento per tali interventi.

La presente relazione tecnica ha carattere di preliminare e per tale motivo si rimanda alle specifiche tecniche dei produttori/fornitori delle strutture porta moduli, delle componentistiche e delle strutture prefabbricate, scelti in fase successiva, per le caratteristiche delle stesse. Pertanto, il calcolo fornisce una prima indicazione per caratterizzare dimensioni, sezioni e caratteristiche dei materiali delle strutture oggetto di progettazione, le assunzioni ed ipotesi alla base della presente progettazione dovranno essere verificate nelle successive fasi di progettazione di concerto con i produttori/fornitori delle strutture.

In linea generale, si prevede l'infissione delle strutture porta-moduli nel terreno mediante battipalo, per una profondità non inferiore ai 2,5 m.

Tuttavia, le fondazioni delle strutture porta moduli fotovoltaici, ed in particolare la lunghezza di infissione dei pali, saranno definite nelle successive fasi di progettazione (ingegneria di dettaglio), a seguito dell'individuazione del fornitore della struttura porta-moduli, della definizione finale delle caratteristiche tecniche e geometriche della struttura e dell'esecuzione di specifiche prove di campo (pull-out test).

Nel presente documento si riportano le verifiche lato struttura dei tracker porta moduli, delle platee di fondazione in cemento armato delle componenti appartenenti all'impianto BESS, delle platee di fondazione in cemento armato della cabina di raccolta e della cabina scada, del locale interrato a servizio del locale utente, della platea di fondazione per il posizionamento dei trasformatori MT/BT e della platea di fondazione per il posizionamento del trasformatore MT/AT previsti per la realizzazione dell'impianto oggetto di progettazione.

Si rimanda all'elaborato FOM.ENG.REL.003_RELAZIONE TECNICA per i dettagli riguardanti il layout di impianto ed all'elaborato FOM.ENG.REL.0011_RELAZIONE GEOTECNICA per i dettagli riguardanti le verifiche ed il calcolo lato geotecnico (GEO) delle opere in progetto.

Si riportano in sintesi le caratteristiche generali inserite nel codice di calcolo:

Intestazione del lavoro	Foggia Manfredonia
Tipo di struttura	Nello Spazio
Tipo di analisi	Statica e Sismica
Tipo di soluzione	Lineare
Unita' di misura delle forze	daN – kg
Unita' di misura delle lunghezze	cm – m
Normativa	NTC 2018

2.2 Descrizione delle strutture tracker

Nel seguito si riporta una breve descrizione delle strutture tracker progettate.

2.2.1 Struttura 2x15

La struttura sarà caratterizzata dai seguenti elementi (Vedi Figura 1 e Figura 2):

- 1) Telaio Principale, composto da:
 - a. Montante – sezione HEA 240;
 - b. Trave principale – sezione 200x200x8;
- 2) Travi secondarie porta pannelli – sezione 150x100x8.

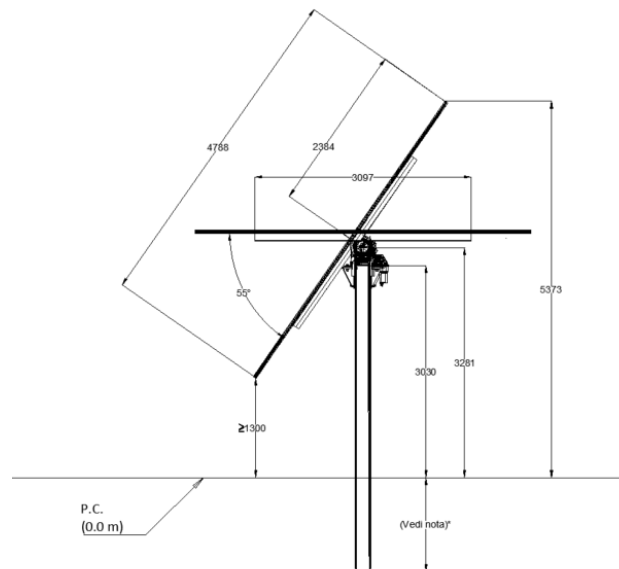


Figure 1: Telaio trasversale Tracker

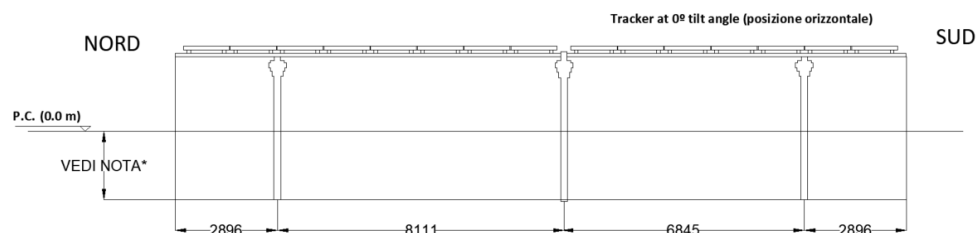


Figure 2: Vista Longitudinale Tracker

Note* Le dimensioni indicate saranno validate in una fase successiva del progetto (ingegneria di dettaglio) dopo aver definito in maniera definitiva le caratteristiche geometriche e meccaniche delle strutture porta moduli (scelta delle sezioni e del fornitore/produttore) ed eseguito le prove di campo (pull-out test ecc.).

MODELLI DI CALCOLO

Si è analizzato la struttura 2x15 nelle due configurazioni tipo:

- Configurazione a riposo: inclinazione pannelli 0°;
- Configurazione in esercizio: inclinazione pannelli a 55°.

Nei calcoli si è considerato che le strutture siano dotate di sensori tali che nella configurazione di esercizio una volta raggiunta la velocità limite del vento di 15 m/s la struttura tracker si posizionerà automaticamente in configurazione di riposo.

Tale valore della velocità del vento dovrà essere validato e confermato dal produttore/fornitore scelto per le strutture tracker nelle successive fasi.

Nel seguito si riportano le immagini dei due modelli di calcolo analizzati.

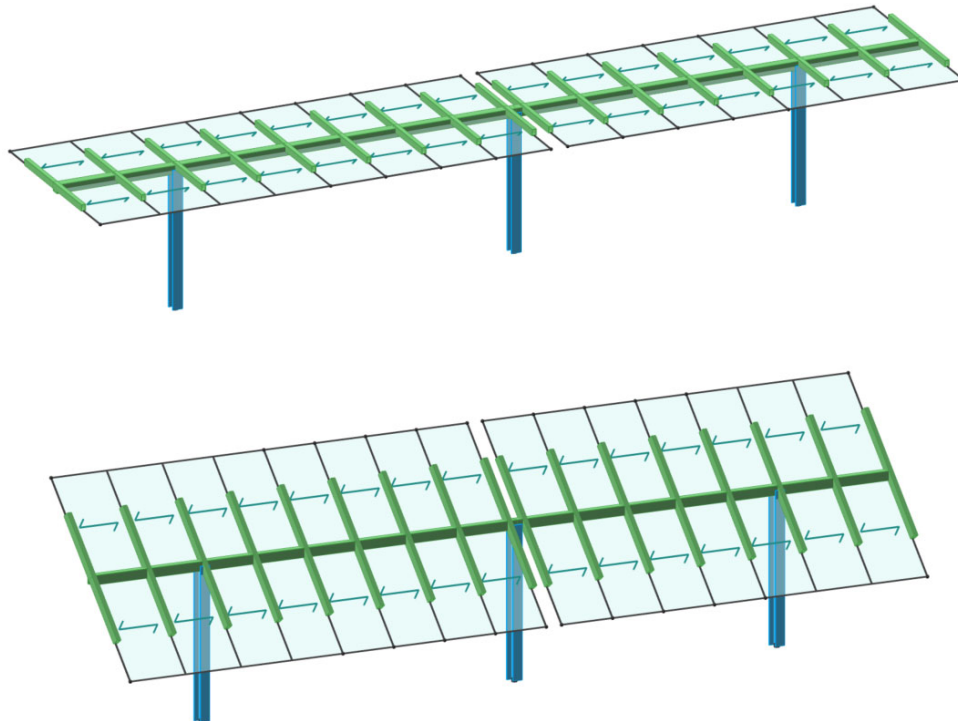


Figure 3: Vista modellazione strutturale: in alto configurazione di riposo, in basso configurazione di esercizio

Tutti gli elementi saranno realizzati con acciaio del tipo S355 (FE 510).

LISTA MATERIALI UTILIZZATI

Materiale acciaio:

Modulo elastico - $E = 2.100.000 \text{ daN/cm}^2$

Coefficiente di Poisson - $\nu = 0,30$

Peso specifico - $\gamma = 7.850 \text{ daN/m}^3$

2.2.2 Struttura 2x30

La struttura sarà caratterizzata dai seguenti elementi (Vedi Figura 4 e Figura 5):

- 1) Telaio Principale, composto da:
 - a. Montante – sezione HEA 240;
 - b. Trave principale – sezione 200x200x8;
- 2) Travi secondarie porta pannelli – sezione 150x100x8.

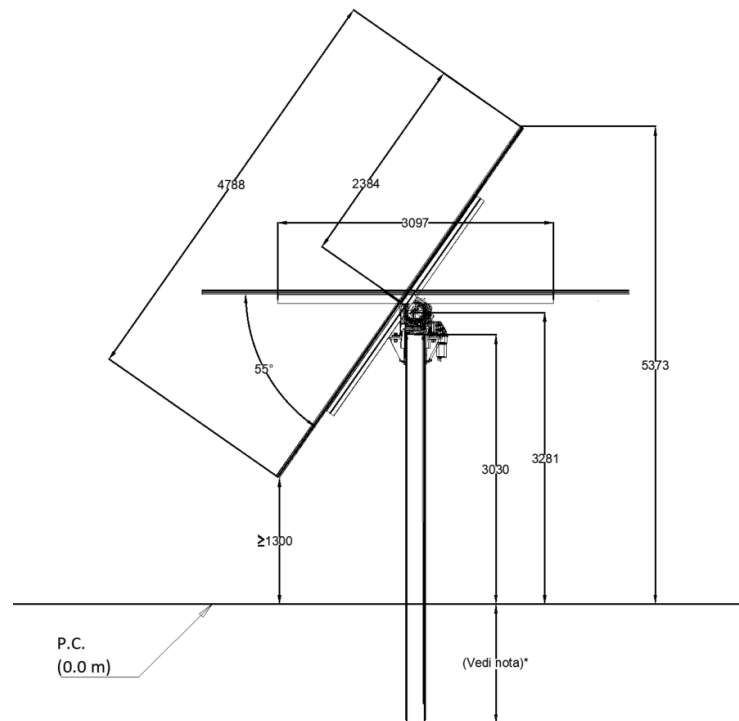


Figure 4: Telaio trasversale Tracker

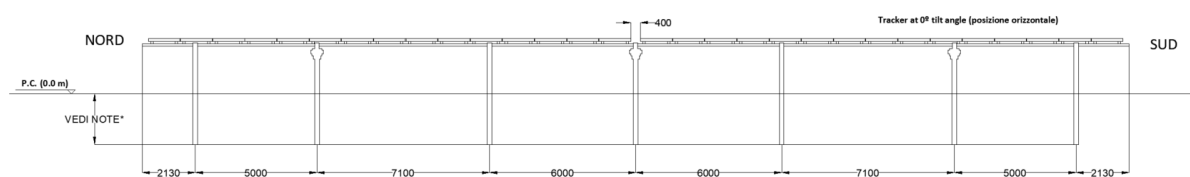


Figure 5: Vista Longitudinale Tracker

Note* Le dimensioni indicate saranno validate in una fase successiva del progetto (ingegneria di dettaglio) dopo aver definito in maniera definitiva le caratteristiche geometriche e meccaniche delle strutture porta moduli (scelta delle sezioni e del fornitore/produttore) ed eseguito le prove di campo (pull-out test ecc.).

MODELLI DI CALCOLO

Si è analizzato la struttura 2x30 nelle due configurazioni tipo:

- Configurazione a riposo: inclinazione pannelli 0°;
- Configurazione in esercizio: inclinazione pannelli a 55°.

Nei calcoli si è considerato che le strutture siano dotate di sensori tali che nella configurazione di esercizio una volta raggiunta la velocità limite di 15 m/s la struttura tracker si posizionerà automaticamente in configurazione di riposo.

Tale valore della velocità del vento dovrà essere validato e confermato dal produttore/fornitore scelto per le strutture tracker nelle successive fasi.

Nel seguito si riportano le immagini dei due modelli di calcolo analizzati.

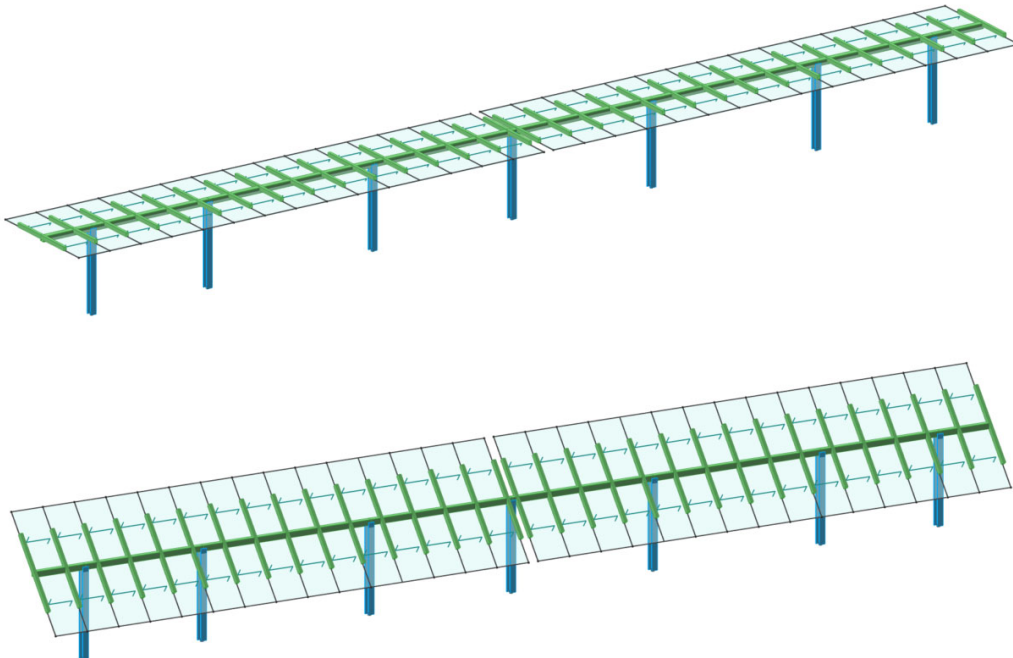


Figure 6: Vista modellazione strutturale: in alto configurazione di riposo, in basso configurazione di esercizio

Tutti gli elementi saranno realizzati con acciaio del tipo S355 (FE 510) o superiori.

LISTA MATERIALI UTILIZZATI

Materiale acciaio:

Modulo elastico - $E = 2.100.000 \text{ daN/cm}^2$

Coefficiente di Poisson - $\nu = 0,30$

Peso specifico - $\gamma = 7.850 \text{ daN/m}^3$

2.3 Descrizione delle fondazioni impianto BESS

L'impianto BESS è costituito da cabinati container prefabbricati contenenti le batterie al litio, cabinati prefabbricati contenenti gli inverter (PCS) e trasformatori BT/MT.

Si prevede la realizzazione di platee di fondazione dello spessore di 50 cm e di dimensioni pari a:

- 13x3,5 m per i container contenenti le batterie al litio;
- 6x4 per i cabinati PCS ed i trasformatori BT/MT con cordoli perimetrali per contenimento eventuali perdite olio di altezza 30 cm e spessore 15 cm.

Si riportano nel seguito i modelli di calcolo elaborati per le verifiche.

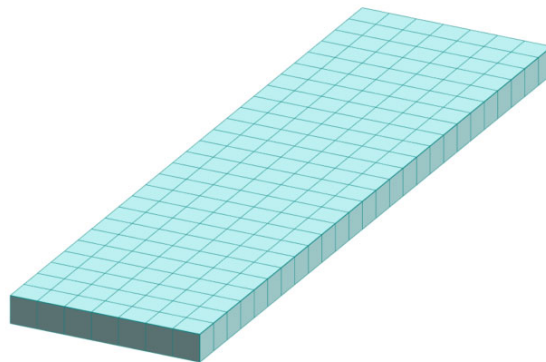


Figure 7: Platea container

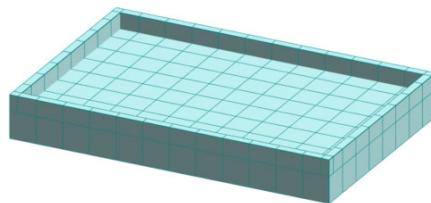


Figure 8: Platea PCS e trasformatori MT/BT

MATERIALI UTILIZZATI

Cemento armato:

Classe C32/40

Peso specifico – $\gamma = 2500 \text{ daN/m}^3$

2.4 Descrizione delle fondazioni cabine

Saranno installate due cabine prefabbricate, non oggetto della presente relazione di calcolo, di dimensioni pari a:

- 9x2,5 m circa per la cabina di raccolta;
- 5,3x2,5 m circa per la cabina scada.

Si prevede la realizzazione di platee di fondazione dello spessore di 50 cm e di dimensioni pari a:

- 10x3,5 m per la cabina di raccolta;
- 6,5x3,5 per la cabina SCADA.

Si riportano nel seguito i modelli di calcolo elaborati per le verifiche.

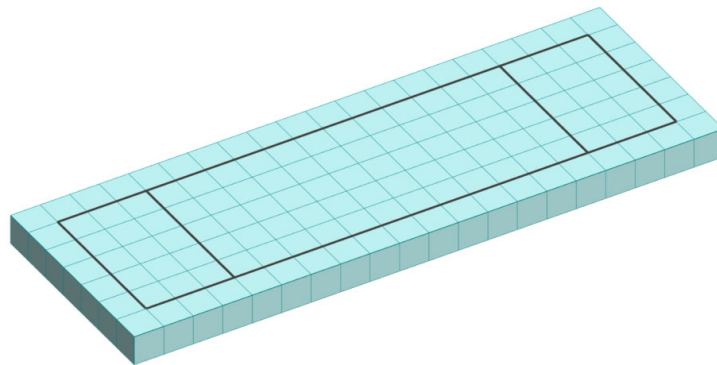


Figure 9: Platea cabina di raccolta

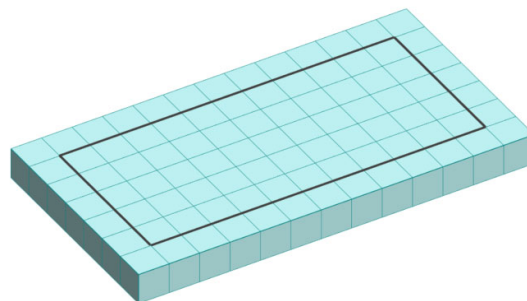


Figure 10: Platea cabina scada

MATERIALI UTILIZZATI

Cemento armato:

Classe C32/40

Peso specifico – $\gamma = 2500 \text{ daN/m}^3$

2.5 Descrizione dell'interrato per locale utenze

Sarà installato un locale utenze prefabbricato di dimensioni in pianta pari a circa 4,6x25,6 m ed altezza di circa 3,5 m. Per tale manufatto è prevista la realizzazione di un locale interrato in cemento armato gettato in opera di dimensioni in pianta pari a 4,6x25,6 m ed altezza di 2,7 m.

Tale manufatto sarà fondato su platea di fondazione dello spessore di 50 cm e di dimensioni in pianta pari a 5,6x26,6.

Il locale interrato avrà un solaio realizzato in soletta piana dello spessore di 30 cm sul quale sarà posizionata la struttura portante del locale utenze.

Si riporta il modello di calcolo elaborato per le verifiche.

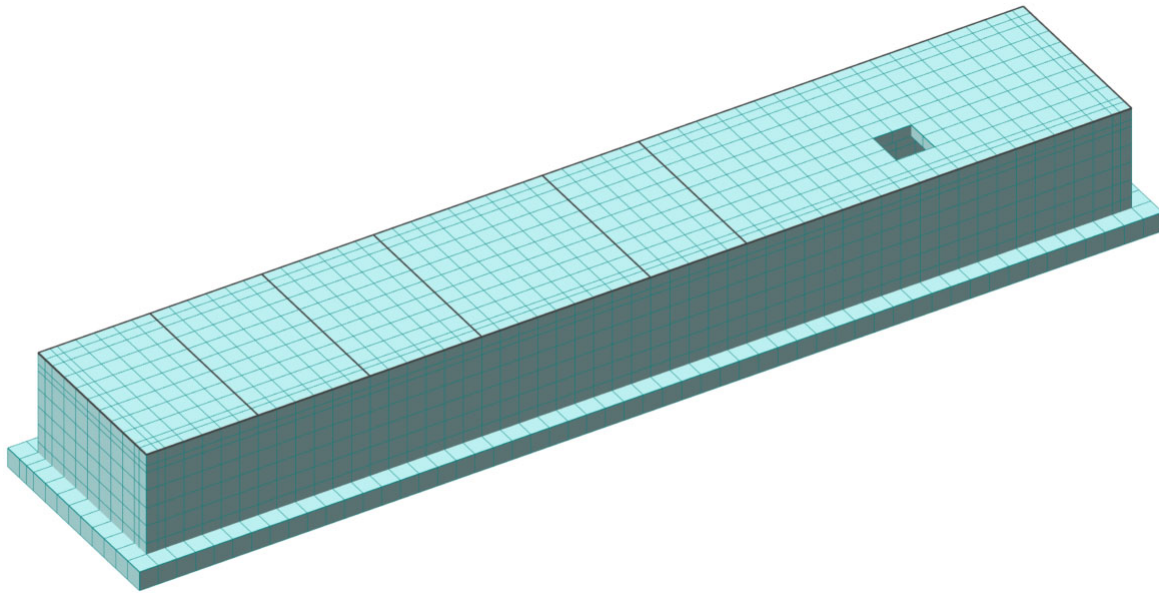


Figure 11: Locale interrato

MATERIALI UTILIZZATI

Cemento armato:

Classe C32/40

Peso specifico – $\gamma = 2500 \text{ daN/m}^3$

2.6 Descrizione della fondazione trasformatore MT/AT

Per l'installazione del trasformatore MT/AT si prevede la realizzazione di una platea di fondazione di dimensioni in pianta di 8x5 m circa e spessore di 50 cm; per evitare eventuali sversamenti di olio dovuto a rotture si prevede la realizzazione di cordoli di contenimento dello spessore di 30 cm e di altezza di 60 cm su tutto il perimetro, saranno inoltre realizzati due muretti centrali in cemento armato di spessore 60 cm ed altezza 60 cm per il posizionamento del trasformatore stesso.

All'interno delle vasche realizzate dai cordoli perimetrali ed i cordoli centrali sarà posizionato del materiale inerte per drenare eventuali perdite di olio a seguito di rotture.

Si riporta il modello di calcolo elaborato per le verifiche.

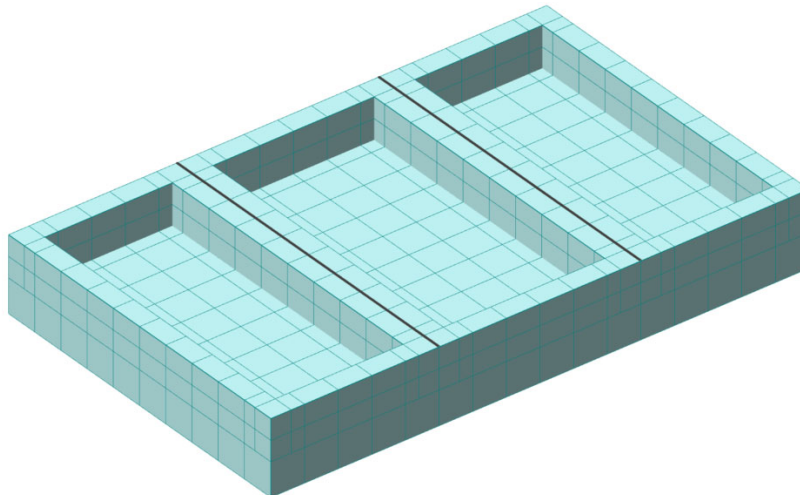


Figure 12: Platea Trasformatore MT/AT

MATERIALI UTILIZZATI

Cemento armato:

Classe C32/40

Peso specifico - $\gamma = 2500 \text{ daN/m}^3$

2.7 Descrizione della fondazione trasformatore MT/BT

Per l'installazione del trasformatore MT/BT si prevede la realizzazione di una platea di fondazione di dimensioni in pianta di 3,75x7 m circa e spessore di 50 cm; per la raccolta di eventuali spandimenti di olio dovuto a rotture si prevede il posizionamento di un pozzetto interrato prefabbricato di dimensioni in pianta 2,5x2,5 m e altezza 0,95 m, non oggetto della presente relazione di calcolo.

Si riporta il modello di calcolo elaborato per le verifiche.

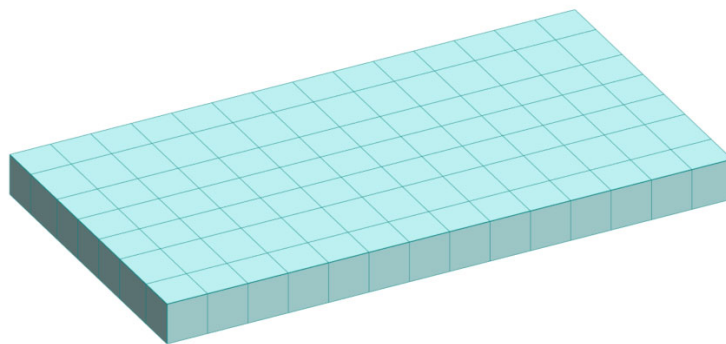


Figure 13: Platea cabina di raccolta

MATERIALI UTILIZZATI

Cemento armato:

Classe C32/40

Peso specifico - $\gamma = 2500 \text{ daN/m}^3$

3.0 CARICHI DI PROGETTO STRUTTURE TRACKER

3.1 Generalità

I carichi considerati per la progettazione delle strutture tracker sono:

Carichi permanenti (G):

- Peso Strutture (Carico Permanente Strutturale)
- Peso Moduli (Carico Permanente non Strutturale)

Carichi Variabili (Q):

- Neve
- Vento

3.2 Carichi permanenti strutturale

I pesi propri degli elementi strutturali, quali travi e pilastri, sono stati considerati in automatico dal programma di calcolo.

Si assume il seguente valore per il peso del materiale utilizzato:

- Peso Strutture in acciaio: 7850 daN/m³
- Peso Strutture in cemento armato: 2500 daN/m³

3.3 Carichi permanenti non strutturali

Nel seguito si riportano i valori dei carichi permanenti non strutturali assunti nel calcolo delle strutture oggetto della presente progettazione.

Per le strutture tracker i carichi permanenti non strutturali assumono i seguenti valori:

- Peso Moduli: 35 daN

3.4 Carichi da neve

Il carico provocato dalla presenza della neve agisce in direzione verticale ed è riferito alla proiezione orizzontale della superficie della copertura. Esso è valutato con la seguente espressione:

$$q_s = \mu_i \cdot q_{sk} \cdot C_E \cdot C_t$$

Provincia : Foggia

Zona : II Appenninica

Altitudine : 76 m s.l.m.

Valore caratteristico neve al suolo : $q_{sk} = 100 \text{ kg/m}^2$

Coefficiente di esposizione C_E : 0,9

Coefficiente termico C_t : 1

Tipo di copertura: ad una falda

Si assume che la neve non sia impedita di scivolare.

Se l'estremità più bassa della falda termina con un parapetto, una barriera od altre ostruzioni, allora il coefficiente di forma non potrà essere assunto inferiore a 0,8 indipendentemente dall'angolo α .

La struttura del tracker può essere assimilata ad una pensilina ad una falda, per tale motivo si può considerare la condizione di carico riportata nella figura, la quale deve essere utilizzata per entrambi i casi di carico, con o senza vento.

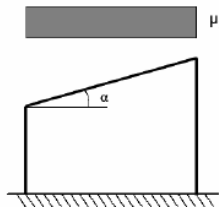


Figure 14: Carico neve per copertura ad una falda

Carico da neve :

Per $\alpha = 0^\circ$ configurazione di riposo

$$q_s(\mu_1=0,8) = 72 \text{ kg/m}^2$$

Si assume un carico pari a **75 kg/m²**.

Per $\alpha = 55^\circ$ configurazione di esercizio

$$q_s(\mu_1=0,133) = 12 \text{ kg/m}^2$$

Si assume un carico pari a **15 kg/m²**.

3.5 Carichi da vento

La pressione del vento è calcolata secondo l'espressione:

$$p = q_b \cdot c_e \cdot c_p \cdot c_d$$

Provincia: Foggia

Zona: 3

Altitudine: 76 m s.l.m

Tempo di ritorno Tr: 50 anni;

Distanza dalla costa: entro 30 km dalla costa

Classe di rugosità del terreno: D

Categoria di esposizione del sito: II

Coefficiente topografico ct: 1

Coefficiente dinamico cd: 1

Per la configurazione di riposo:

Velocità di riferimento $v_b(Tr)$: 27 m/s

Altezza della costruzione h : 3,3 m

Pressione cinetica di riferimento q_b : 45,6 Kg/m²

Coefficiente di esposizione $c_e(z)$: $c_e = 1,8$

Si assume il seguente valore della pressione del vento:

$$p = 82,2 \text{ daN/m}^2$$

Il riferimento è il p.to C3.3.8.2.1 della Circolare n. 7 del 21.01.2019 per cui risulta (vedi anche figura seguente):

$$\alpha = 0^\circ$$

$$\varphi = 0$$

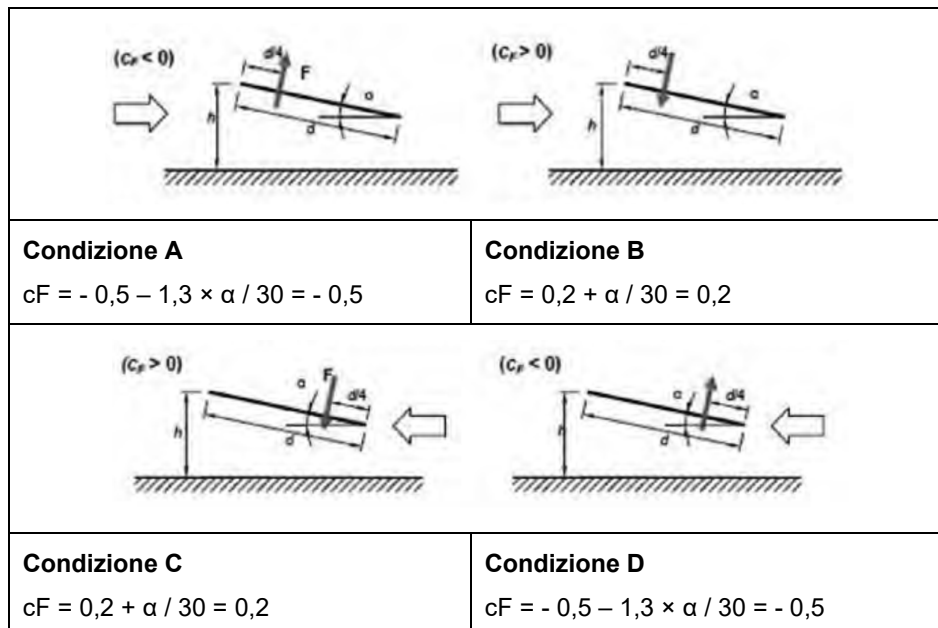


Figure 15: Casistiche carico vento per tettoia ad una falda – condizioni di riposo

Per la configurazione di esercizio:Velocità di riferimento $v_b(\text{Tr})$: 15 m/sAltezza della costruzione h : 5,4 mPressione cinetica di riferimento q_b : 14,1 Kg/m²Coefficiente di esposizione $c_e(z)$: $c_e = 1,97$ **Si assume il seguente valore della pressione del vento:** **$p = 27,8 \text{ daN/m}^2$**

Il riferimento è il p.to C3.3.8.2.1 della Circolare n. 7 del 21.01.2019 per cui risulta (vedi anche figura seguente):

$$\alpha = 55^\circ$$

$$\varphi = 0$$

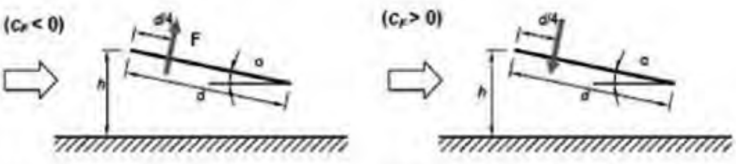
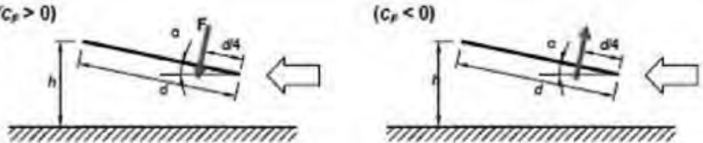
	
Condizione A $cF = -0,5 - 1,3 \times \alpha / 30 = -2,9$	Condizione B $cF = 0,2 + \alpha / 30 = 2,0$
	
Condizione C $cF = 0,2 + \alpha / 30 = 2,0$	Condizione D $cF = -0,5 - 1,3 \times \alpha / 30 = -2,9$

Figure 16: Casistiche carico vento per tettoia ad una falda – condizioni di esercizio

4.0 CARICHI DI PROGETTO STRUTTURE DI FONDAZIONE

4.1 Generalità

I carichi considerati per la progettazione delle strutture di fondazione e la struttura interrata sono:

Carichi permanenti (G):

- Peso Strutture (Carico Permanente Strutturale)
- Peso componenti e manufatti installati (Carico Permanente non Strutturale)

Carichi Variabili (Q):

- Accidentali

4.2 Carichi permanenti strutturale

I pesi propri degli elementi strutturali, quali travi e pilastri, sono stati considerati in automatico dal programma di calcolo.

Si assume il seguente valore per il peso del materiale utilizzato:

- Peso Strutture in acciaio: 7850 daN/m³
- Peso Strutture in cemento armato: 2500 daN/m³

4.3 Carichi permanenti non strutturali

Nel seguito si riportano i valori dei carichi permanenti non strutturali assunti nel calcolo delle strutture oggetto della presente progettazione.

Per le strutture di fondazione dell'impianto BESS i carichi permanenti non strutturali assumono i seguenti valori:

- Peso container: 82500 daN
- Peso PCS: 5700 daN
- Peso trasformatore: 2100 daN

Per le strutture di fondazione delle cabine i carichi permanenti non strutturali assumono i seguenti valori:

- Peso cabina di raccolta: 3000 daN/m
- Peso cabina scada: 2500 daN/m

Per le strutture dell'interrato a servizio del locale utente i carichi permanenti non strutturali assumono i seguenti valori:

- Peso pavimentazione: 200 daN/m²
- Peso cavi ed attrezzi: 150 daN/m²
- Spinta del terreno (andamento costante): 150 daN/m²
- Spinta del terreno (andamento triangolare): 3190 daN/m²

Per le strutture di fondazione dei trasformatori MT/BT i carichi permanenti non strutturali assumono i seguenti valori:

- Peso trasformatore: 25000 daN

Per le strutture di fondazione del trasformatore MT/AT i carichi permanenti non strutturali assumono i seguenti valori:

- Peso trasformatore: 62500 daN

4.4 Carichi accidentali

Nel seguito si riportano i valori dei carichi accidentali assunti nel calcolo delle strutture oggetto della presente progettazione.

Per le strutture dell'interrato a servizio del locale utente i carichi accidentali assumono i seguenti valori:

- Carico cat. E: 300 daN/m²

4.5 Combinazioni di carico

NORMATIVA: NORME TECNICHE PER LE COSTRUZIONI - 17/01/2018 (STATICO E SISMICO)

per le strutture di fondazione sono state considerate le seguenti combinazioni di carico:

CC	Commento	Tipo CCE	Sic.
1	G1 - permanenti strutturali	1 D.M. 18 Permanenti strutturali	a sfavore
2	G2 - permanenti non strutturali	2 D.M. 18 Permanenti non strutturali	a sfavore
3	Q - variabili cat. E	7 D.M. 18 Variabili Categoria E - Aree per immagazzinamento, uso	a sfavore

CC	Commento	TCC	An.	Bk	1	2	3
1	Amb. 1 (SLU)	SLU	L		1.30	1.50	1.50
2	Amb. 1 (SLE R)	SLE R	L		1.00	1.00	1.00
3	Amb. 1 (SLE F)	SLE F	L		1.00	1.00	0.90
4	Amb. 1 (SLE Q)	SLE Q	L		1.00	1.00	0.80

per la struttura interrata sono state considerate le seguenti combinazioni di carico:

CC	Commento	Tipo CCE	Sic.
1	G1 - permanenti strutturali	1 D.M. 18 Permanenti strutturali	a sfavore
2	G2 - permanenti non strutturali	2 D.M. 18 Permanenti non strutturali	a sfavore
3	Q - variabili cat. E	7 D.M. 18 Variabili Categoria E - Aree per immagazzinamento, uso	a sfavore

CC	Commento	TCC	An.	Bk	1	2	3	S X	S Y
1	Amb. 1 (SLU S) S +X+0.3Y	SND	L		1.00	1.00	0.80	1.00	0.30
2	Amb. 1 (SLE) S +X+0.3Y	SLD	L		1.00	1.00	0.80	1.00	0.30
3	Amb. 1 (SLU S) S +X-0.3Y	SND	L		1.00	1.00	0.80	1.00	-0.30
4	Amb. 1 (SLE) S +X-0.3Y	SLD	L		1.00	1.00	0.80	1.00	-0.30
5	Amb. 1 (SLU S) S -X+0.3Y	SND	L		1.00	1.00	0.80	-1.00	0.30
6	Amb. 1 (SLE) S -X+0.3Y	SLD	L		1.00	1.00	0.80	-1.00	0.30
7	Amb. 1 (SLU S) S -X-0.3Y	SND	L		1.00	1.00	0.80	-1.00	-0.30
8	Amb. 1 (SLE) S -X-0.3Y	SLD	L		1.00	1.00	0.80	-1.00	-0.30
9	Amb. 1 (SLU S) S +0.3X+Y	SND	L		1.00	1.00	0.80	0.30	1.00
10	Amb. 1 (SLE) S +0.3X+Y	SLD	L		1.00	1.00	0.80	0.30	1.00
11	Amb. 1 (SLU S) S -0.3X+Y	SND	L		1.00	1.00	0.80	-0.30	1.00
12	Amb. 1 (SLE) S -0.3X+Y	SLD	L		1.00	1.00	0.80	-0.30	1.00
13	Amb. 1 (SLU S) S +0.3X-Y	SND	L		1.00	1.00	0.80	0.30	-1.00
14	Amb. 1 (SLE) S +0.3X-Y	SLD	L		1.00	1.00	0.80	0.30	-1.00
15	Amb. 1 (SLU S) S -0.3X-Y	SND	L		1.00	1.00	0.80	-0.30	-1.00
16	Amb. 1 (SLE) S -0.3X-Y	SLD	L		1.00	1.00	0.80	-0.30	-1.00
17	Amb. 2 (SLU)	SLU	L		1.30	1.50	1.50	0.00	0.00
18	Amb. 2 (SLE R)	SLE R	L		1.00	1.00	1.00	0.00	0.00
19	Amb. 2 (SLE F)	SLE F	L		1.00	1.00	0.90	0.00	0.00
20	Amb. 2 (SLE Q)	SLE Q	L		1.00	1.00	0.80	0.00	0.00

5.0 CRITERI DI VERIFICA

5.1 DI OPERE IN ACCIAIO CON IL METODO DELLE NTC 2018 E DELL'EUROCODICE 3

Il tabulato riporta una legenda dei parametri di calcolo e di progetto richiamati nel tabulato stesso, le caratteristiche delle sezioni e dei materiali utilizzate e successivamente, in sequenza per ogni asta, le verifiche svolte nelle quali sono riportati:

- numero combinazione di carico;
- sollecitazioni di calcolo a seconda della verifica condotta;
- classe della sezione; non viene riportata se agisce la trazione;
- parametri di calcolo utilizzati nella verifica;
- Verifica svolta con indice di sfruttamento ottenuto come rapporto fra la sollecitazione esterna e la resistenza di progetto.

Se è abilitata la verifica di stabilità per aste consecutive (membrature) viene riportato un ulteriore tabulato riguardante la verifica globale delle aste che costituiscono la membratura; la sola differenza con il precedente riguarda l'indicazione, nel prospetto, della lunghezza totale che influisce sul valore di snellezza e quindi sul risultato finale della verifica.

5.2 DI OPERE IN CEMENTO ARMATO CON IL METODO DELLE NTC 2018

Il tabulato riporta una legenda dei parametri di calcolo e di progetto richiamati nel tabulato stesso, le caratteristiche delle sezioni e dei materiali utilizzate e successivamente, in sequenza per ogni elemento, le verifiche svolte nelle quali sono riportati:

- numero combinazione di carico;
- sollecitazioni di calcolo a seconda della verifica condotta;
- armatura presente;
- Verifica svolta con indice di sfruttamento ottenuto come rapporto fra la sollecitazione esterna e la resistenza di progetto.

6.0 RISULTATI STRUTTURE TRACKER

6.1 Tracker 2x15 – configurazione a riposo ($\alpha = 0^\circ$)

6.1.1 Diagrammi tassi di sfruttamento

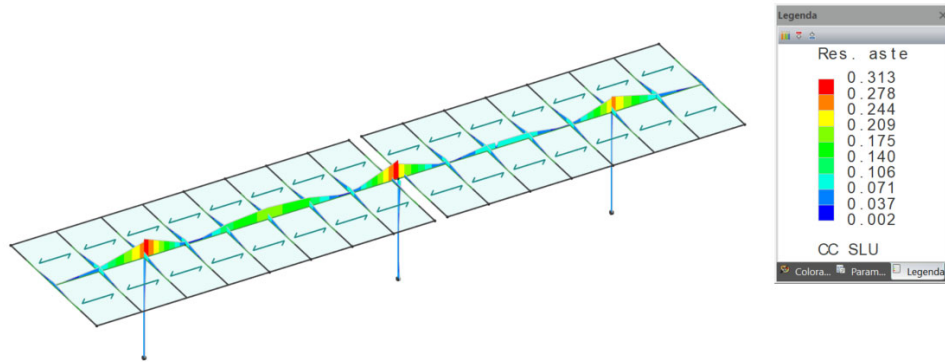


Diagramma tassi di sfruttamento resistenza aste combo SLU con valore massimo pari a 0,313

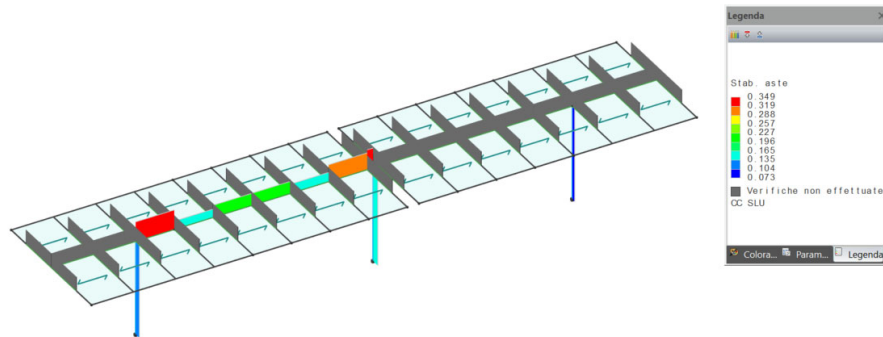


Diagramma tassi di sfruttamento stabilità aste combo SLU con valore massimo pari a 0,349

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

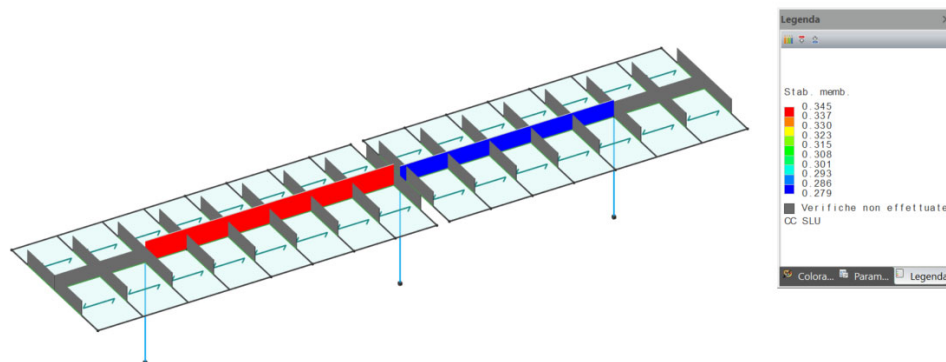


Diagramma tassi di sfruttamento stabilità membrature combo SLU con valore massimo pari a 0,345

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

Figure 17: Tassi di sfruttamento SLU (Stato limite ultimo)

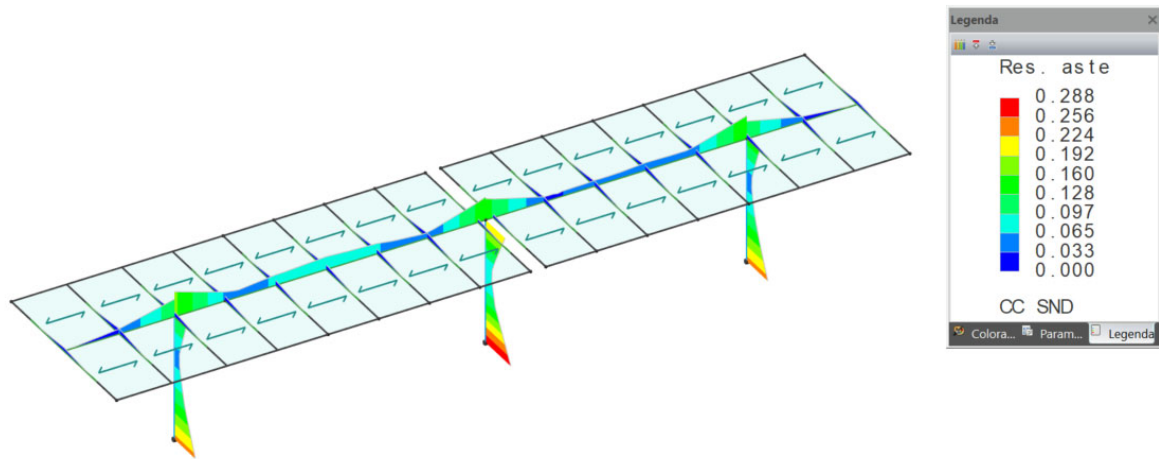


Diagramma tassi di sfruttamento resistenza aste combo SND con valore massimo pari a 0,288

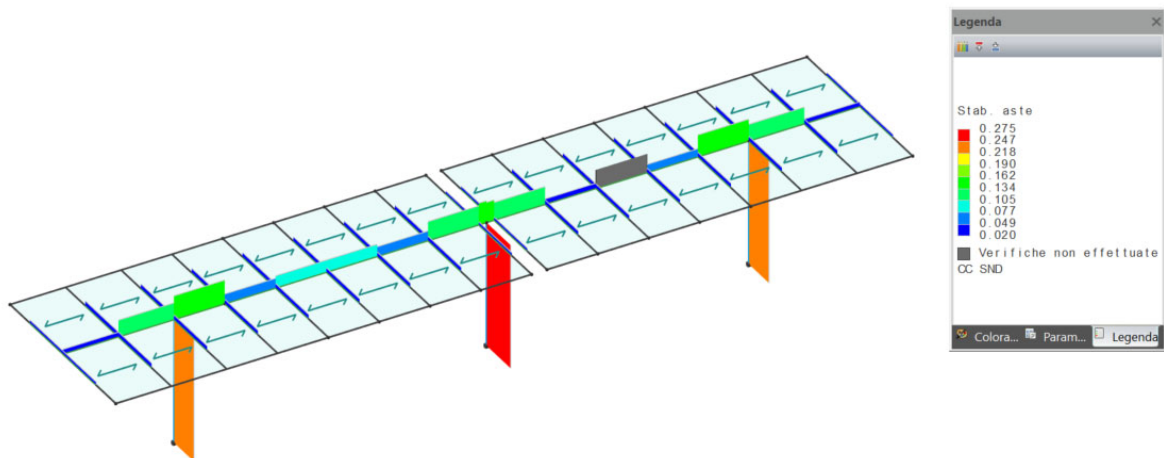


Diagramma tassi di sfruttamento stabilità aste combo SND con valore massimo pari a 0,275

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

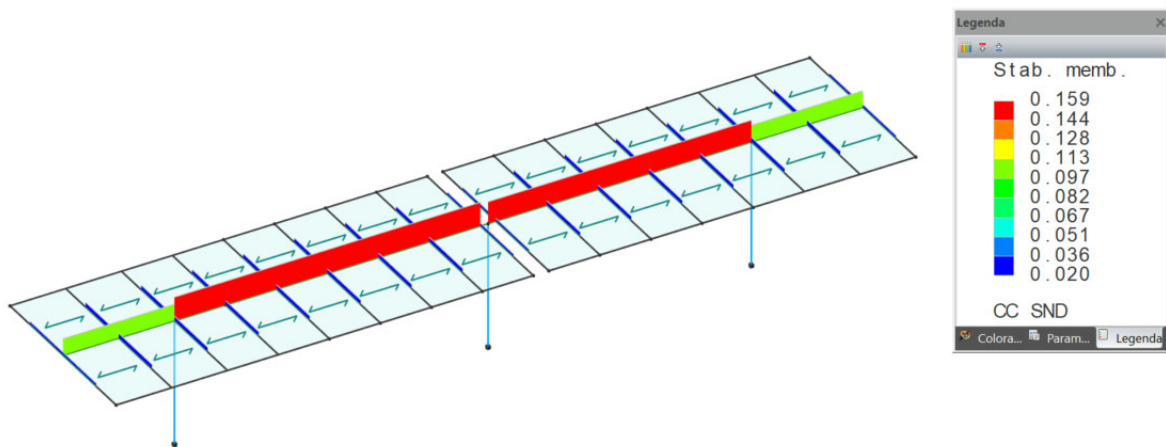
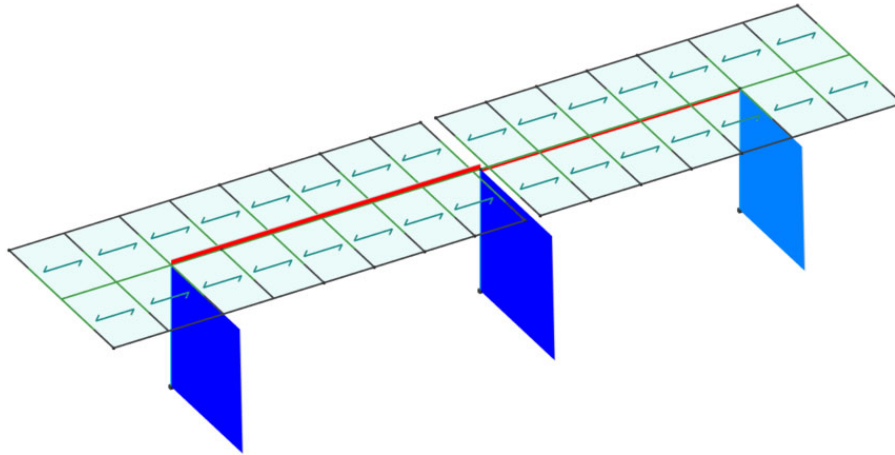


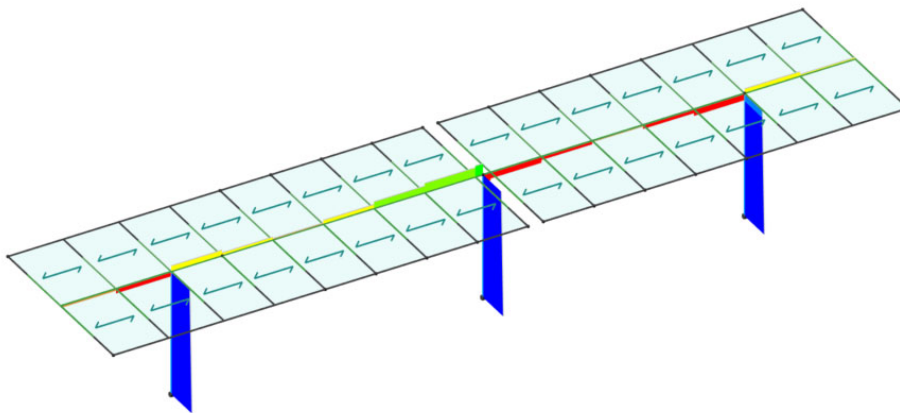
Diagramma tassi di sfruttamento stabilità membrature combo SND con valore massimo pari a 0,159

Figure 18: Tassi di sfruttamento SND (Stato limite di vita non dissipativo)

6.1.2 Sollecitazioni

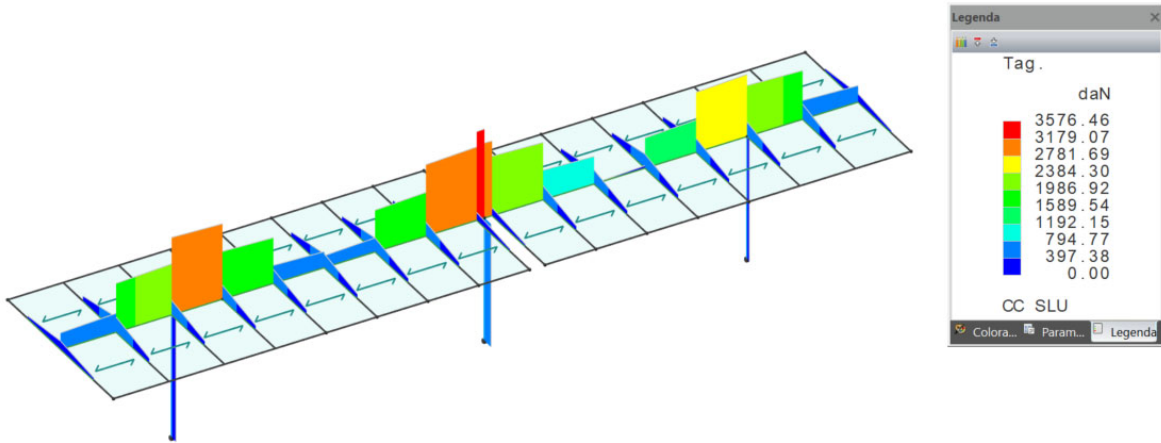


Inviluppo sforzo normale SLU $N_{max} = 6832,98$ daN (compressione)

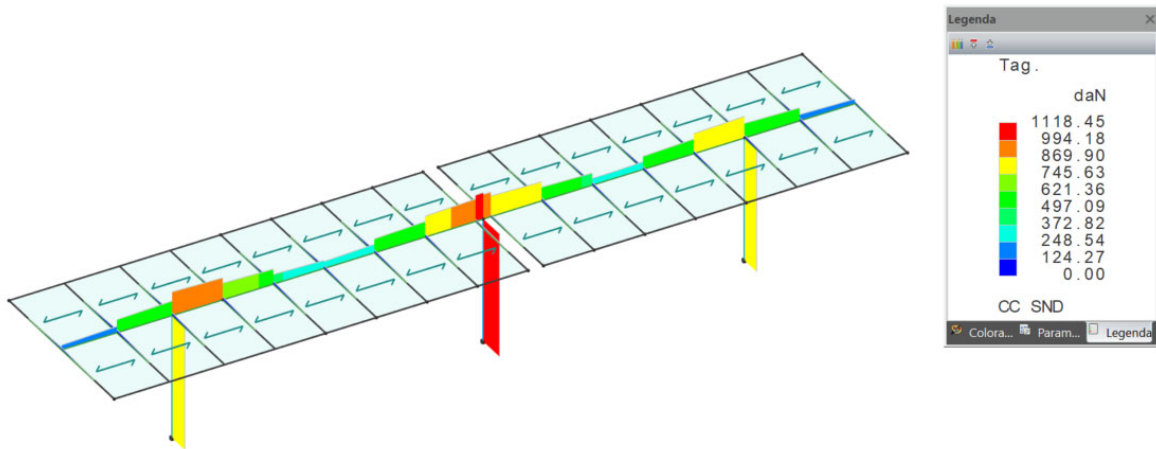


Inviluppo sforzo normale SND $N_{max} = 1876,44$ daN (compressione)

Figure 19: Sforzo Normale

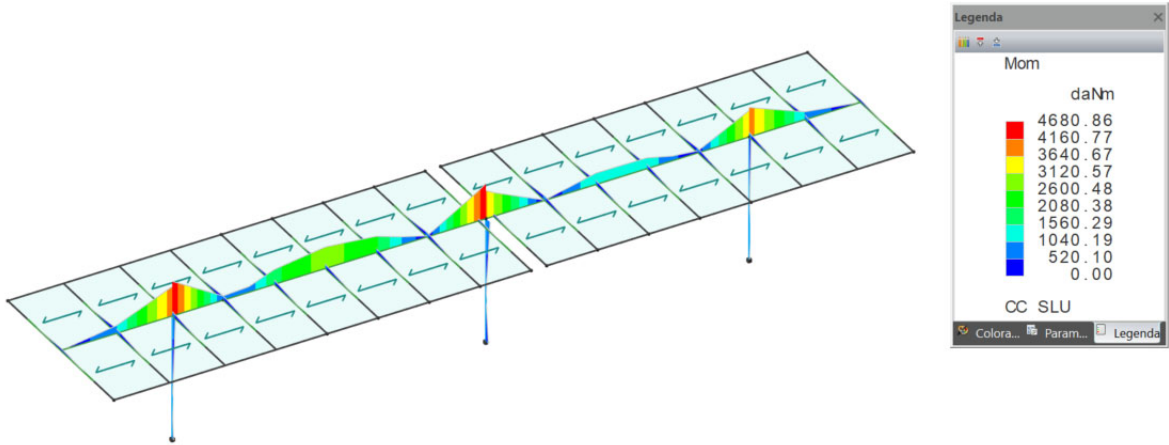


Inviluppo sforzo di taglio SLU $T_{max} = 3576,46$ daN

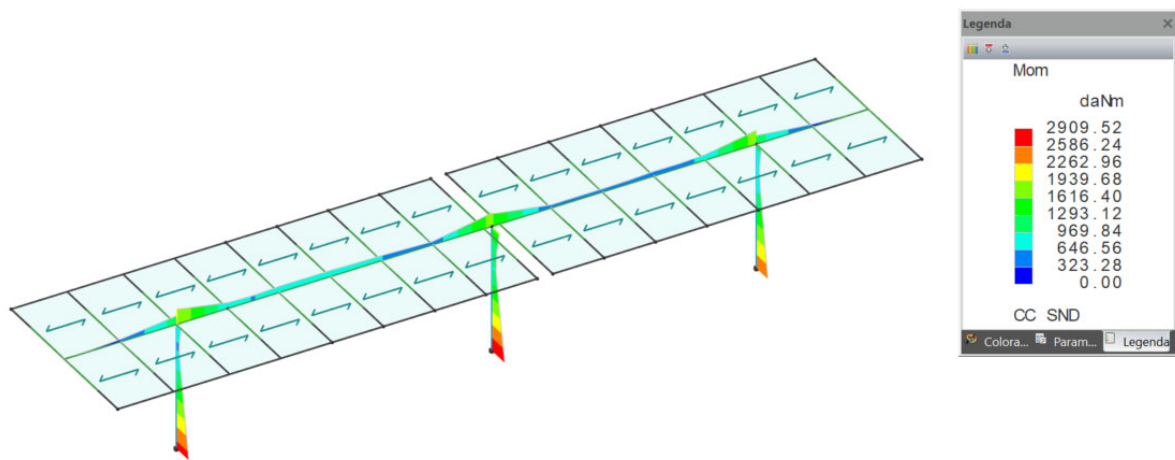


Inviluppo sforzo di taglio SND $T_{max} = 1118,45$ daN

Figure 20: Taglio



Inviluppo momento flettente SLU $M_{max} = 4680,86 \text{ daN}\times\text{m}$



Inviluppo momento flettente SND $M_{max} = 2909,52 \text{ daN}\times\text{m}$

Figure 21: Momento Flettente

6.1.3 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
 ModeSt ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
 Xfinest ver. 9.5.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18
 Tipo di calcolo: sismica statica
 Vincoli esterni: Considera sempre vincoli assegnati in modellazione
 Schematizzazione piani rigidi: nessun impalcato rigido
 Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Non sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

Dati struttura

- Sito di costruzione: CPHJ+52 Foggia FG, Italia LON. 15.73010 LAT. 41.42790
- Contenuto tra ID reticolo: 30559 30558 30337 30336

Simbologia

Ag = Accelerazione orizzontale massima al sito
 Cc = Coefficiente funzione della categoria del suolo
 Fo = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
 Ss = Coefficiente di amplificazione stratigrafica
 Tr = Periodo di ritorno <anni>
 TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SND = Stato limite di salvaguardia della vita (non dissipativo)
 Tc* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

TCC	Tr	Ag <g>	Fo	Tc*	Ss	Cc
SLD	50	0.0554	2.54	0.33	1.50	1.52
SLV	475	0.1323	2.61	0.43	1.49	1.38

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale Vn: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 3.30 <m>
- Altezza della struttura: 3.30 <m>
- Numero piani edificio: 0
- Coefficiente 0: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia strutturale: acciaio a mensola o a pendolo inverso

Periodo T1	0.20812
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00

Rapporto di sovrarresistenza (α_u/α_1)	1.00
Valore di riferimento del fattore di comportamento (q_0)	1.00
Fattore riduttivo (K_w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di comportamento dissipativo (q)	1.00
Fattore di comportamento non dissipativo (qND)	1.00
Fattore di comportamento per SLD (qD)	1.00

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica S_T : 1.00
- Accelerazione di picco del terreno $A_g S$: 0.1976 <g>
- Fattore di comportamento per sisma verticale (qv): 1.50
- Smorzamento spettro: 5.00%

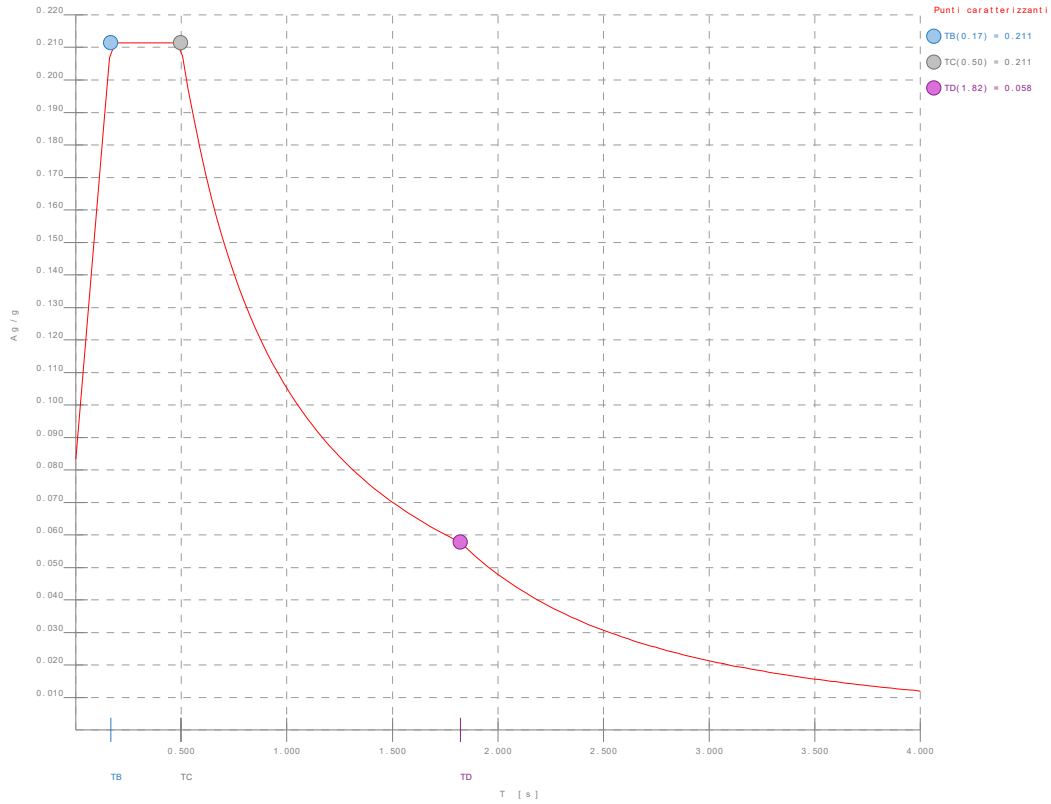


Figura numero 1: Spettro SLD

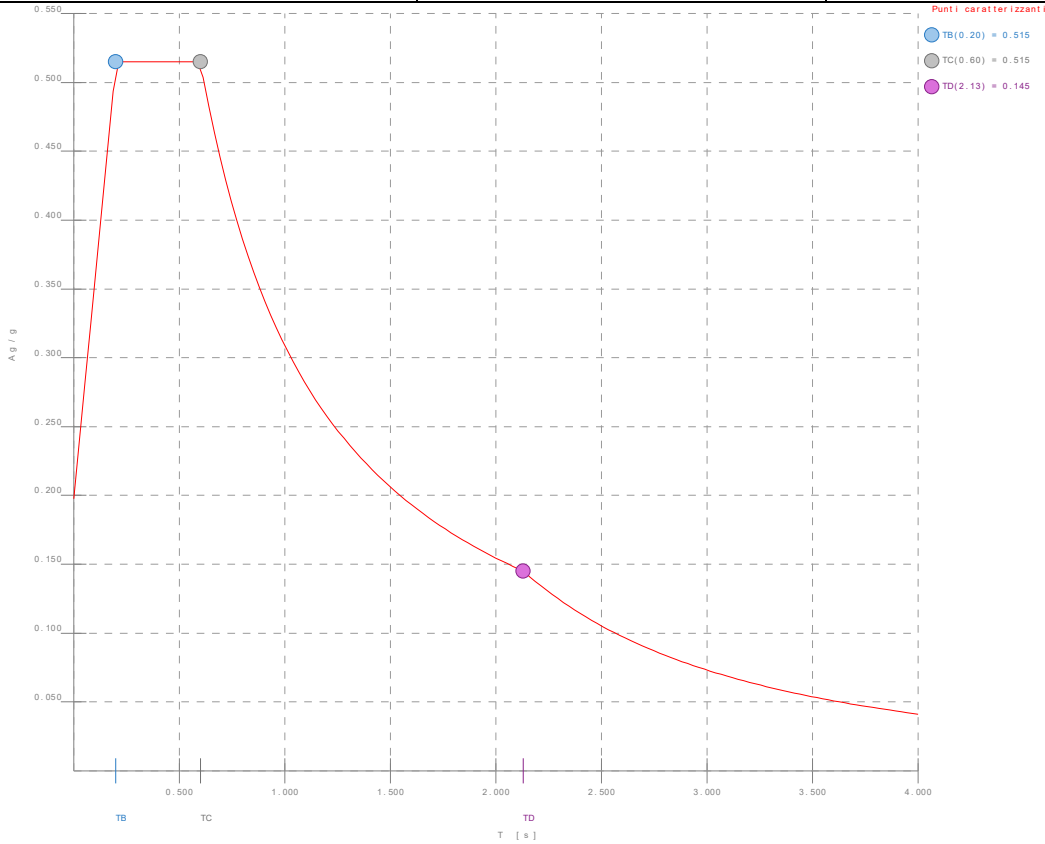


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>
- Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

- N = Numero
- Comm. = Commento
- 1 = G1 - Peso Proprio
- 2 = G2 - Permanenti non strutturali
- 3 = Q - Variabili neve
- 4 = Vento da retro - Cond. A
- 5 = Vento da retro - Cond. B
- 6 = Vento da fronte - Cond. C
- 7 = Vento da fronte - Cond. D
- F = azioni orizzontali convenzionali
- SLU = Stato limite ultimo
- SLR = Stato limite per combinazioni rare
- SLE F = Stato limite per combinazioni frequenti
- SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
- S = Si
- N = No

N/Comm.	1	2	3	4	5	6	7	S	SLU	SLR	SLE F	SLQ
1 Calcolo sismico	S	S	S	N	N	N	N	S	N	N	N	N
2 Calcolo statico	S	S	S	N	N	N	N	S	S	S	S	S
3 Vento da 270° - cond A	S	S	S	N	N	N	N	S	S	S	S	S
4 Vento da 270° - cond B	S	S	S	N	N	N	N	S	S	S	S	S
5 Vento da 90° - cond C	S	S	S	N	N	N	N	S	S	S	S	S
6 Vento da 90° - cond D	S	S	S	N	N	N	N	S	S	S	S	S

Elenco combinazioni di carico simboliche

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	1	2	3	4	5	6	7	S
1	Amb. 1 (Sisma)	SLU	S	1	ψ ₂	----	----	----	----	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	----	----	----	----	----
3	Amb. 2 (SLE R)	SLE R	1	1	1	----	----	----	----	----
4	Amb. 2 (SLE F)	SLE F	1	1	ψ ₁	----	----	----	----	----
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ ₂	----	----	----	----	----
6	Amb. 3 (SLU)	SLU	γ max	γ max	ψ ₀ *γ max	γ max	----	----	----	----



7	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	-----
8	Amb. 3 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
9	Amb. 3 (SLE R)	SLE R	1	1	1	ψ_0	-----	-----	-----	-----
10	Amb. 3 (SLE F)	SLE F	1	1	ψ_2	ψ_1	-----	-----	-----	-----
11	Amb. 3 (SLE F)	SLE F	1	1	ψ_1	ψ_2	-----	-----	-----	-----
12	Amb. 3 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	-----	-----	-----	-----
13	Amb. 4 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
14	Amb. 4 (SLU)	SLU	γ max	γ max	γ max	-----	$\psi_0 * \gamma$ max	-----	-----	-----
15	Amb. 4 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
16	Amb. 4 (SLE R)	SLE R	1	1	1	ψ_0	-----	-----	-----	-----
17	Amb. 4 (SLE F)	SLE F	1	1	ψ_2	-----	ψ_1	-----	-----	-----
18	Amb. 4 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_2	-----	-----	-----
19	Amb. 4 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	-----	-----	-----
20	Amb. 5 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
21	Amb. 5 (SLU)	SLU	γ max	γ max	γ max	-----	$\psi_0 * \gamma$ max	-----	-----	-----
22	Amb. 5 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
23	Amb. 5 (SLE R)	SLE R	1	1	1	ψ_0	-----	-----	-----	-----
24	Amb. 5 (SLE F)	SLE F	1	1	ψ_2	-----	ψ_1	-----	-----	-----
25	Amb. 5 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_2	-----	-----	-----
26	Amb. 5 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	-----	-----	-----
27	Amb. 6 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	γ max	-----
28	Amb. 6 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	$\psi_0 * \gamma$ max	-----
29	Amb. 6 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
30	Amb. 6 (SLE R)	SLE R	1	1	1	-----	-----	-----	ψ_0	-----
31	Amb. 6 (SLE F)	SLE F	1	1	ψ_2	-----	-----	-----	ψ_1	-----
32	Amb. 6 (SLE F)	SLE F	1	1	ψ_1	-----	-----	-----	ψ_2	-----
33	Amb. 6 (SLE Q)	SLE Q	1	1	ψ_2	-----	-----	-----	ψ_2	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: S1

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

An. = Tipo di analisi

L = Lineare

NL = Non lineare

Bk = Buckling

S = Si

N = No

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	S X	S Y
1	Amb. 1 (SLU S) S +X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
2	Amb. 1 (SLE) S +X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
3	Amb. 1 (SLU S) S +X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
4	Amb. 1 (SLE) S +X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
5	Amb. 1 (SLU S) S -X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
6	Amb. 1 (SLE) S -X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
7	Amb. 1 (SLU S) S -X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
8	Amb. 1 (SLE) S -X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
9	Amb. 1 (SLU S) S +0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
10	Amb. 1 (SLE) S +0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
11	Amb. 1 (SLU S) S -0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
12	Amb. 1 (SLE) S -0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
13	Amb. 1 (SLU S) S +0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
14	Amb. 1 (SLE) S +0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
15	Amb. 1 (SLU S) S -0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
16	Amb. 1 (SLE) S -0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
17	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.00	0.00	0.00
18	Amb. 2 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
19	Amb. 2 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
20	Amb. 2 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	0.75	1.50	0.00	0.00	0.00	0.00	0.00
22	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
23	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	0.50	1.00	0.00	0.00	0.00	0.00	0.00
24	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
25	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.20	0.00	0.00	0.00	0.00	0.00
26	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
27	Amb. 3 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	1.50	0.00	0.00	0.00	0.00
29	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
30	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	1.00	0.00	0.00	0.00	0.00
31	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
32	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.20	0.00	0.00	0.00	0.00
33	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
34	Amb. 4 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	1.50	0.00	0.00	0.00
36	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
37	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00
38	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00
39	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00
40	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
41	Amb. 5 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	0.00	1.50	0.00	0.00
43	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.90	0.00	0.00
44	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00
45	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00
46	Amb. 6 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.20	0.00	0.00



47	Amb. 6 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00
48	Amb. 6 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Elenco masse nodi

Simbologia
Mo = Massa orizzontale
Nodo = Numero del nodo

Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>
-80	68.95	-79	68.95	-78	66.90	-77	66.90	-76	71.00	-75	71.00	-74	71.00	-73	71.00	-72	69.01	-71	46.74	-70	46.74
-69	46.74	-68	46.74	-67	69.01	-66	67.01	-65	67.01	-64	67.01	-63	67.01	-62	67.01	-61	67.01	-60	67.01	-59	67.01
-58	44.74	-57	44.74	-56	44.69	-55	44.69	-54	66.90	-53	66.90	-52	66.90	-51	66.90	-50	66.90	-49	66.90	-48	66.90
-47	66.90	-45	251.98	-29	160.41	-26	160.41	-18	102.67	-15	150.92	-14	150.92	-13	150.92	-12	150.92	-11	102.85	-10	102.71
-9	150.66	-8	150.66	-7	150.66	-6	150.66	-3	102.67	201	150.66	202	106.28	203	252.12						

Totali masse nodi

Mo <kg>
4829.94

Elenco forze sismiche nodali allo SLD

Simbologia
Fx = Forza in dir. X
Fy = Forza in dir. Y
Nodo = Numero del nodo
cx = Coeff. c in dir. X
cy = Coeff. c in dir. Y

Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>
-80	0.01	0.01	14.29	14.29	-79	0.01	0.01	14.29	14.29	-78	0.01	0.01	13.87	13.87	-77	0.01	0.01	13.87	13.87	-76	0.01	0.01	14.72	14.72					
-75	0.01	0.01	14.72	14.72	-74	0.01	0.01	14.72	14.72	-73	0.01	0.01	14.72	14.72	-72	0.01	0.01	14.31	14.31	-71	0.01	0.01	9.69	9.69					
-70	0.01	0.01	9.69	9.69	-69	0.01	0.01	9.69	9.69	-68	0.01	0.01	9.69	9.69	-67	0.01	0.01	13.89	13.89	-66	0.01	0.01	13.89	13.89					
-65	0.01	0.01	13.89	13.89	-64	0.01	0.01	13.89	13.89	-63	0.01	0.01	13.89	13.89	-62	0.01	0.01	13.89	13.89	-61	0.01	0.01	13.89	13.89					
-60	0.01	0.01	13.89	13.89	-59	0.01	0.01	13.89	13.89	-58	0.01	0.01	9.28	9.28	-57	0.01	0.01	9.28	9.28	-56	0.01	0.01	9.26	9.26					
-55	0.01	0.01	9.26	9.26	-54	0.01	0.01	13.87	13.87	-53	0.01	0.01	13.87	13.87	-52	0.01	0.01	13.87	13.87	-51	0.01	0.01	13.87	13.87					
-50	0.01	0.01	13.87	13.87	-49	0.01	0.01	13.87	13.87	-48	0.01	0.01	13.87	13.87	-47	0.01	0.01	13.87	13.87	-45	0.05	0.05	52.24	52.24					
-29	0.03	0.03	33.26	33.26	-26	0.03	0.03	33.25	33.25	-18	0.02	0.02	21.29	21.29	-15	0.03	0.03	31.29	31.29	-14	0.03	0.03	31.29	31.29					
-13	0.03	0.03	31.29	31.29	-12	0.03	0.03	31.29	31.29	-11	0.02	0.02	21.32	21.32	-10	0.02	0.02	21.29	21.29	-9	0.03	0.03	31.23	31.23					
-8	0.03	0.03	31.23	31.23	-7	0.03	0.03	31.23	31.23	-6	0.03	0.03	31.23	31.23	-3	0.02	0.02	21.29	21.29	201	0.03	0.03	31.23	31.23					
202	0.02	0.02	22.03	22.03	203	0.05	0.05	52.27	52.27																				

Totali forze sismiche

Fx <daN>	Fy <daN>
1001.30	1001.30

Elenco forze sismiche nodali allo SND

Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>
-80	0.01	0.01	34.83	34.83	-79	0.01	0.01	34.83	34.83	-78	0.01	0.01	33.80	33.80	-77	0.01	0.01	33.80	33.80	-76	0.01	0.01	35.87	35.87					
-75	0.01	0.01	35.87	35.87	-74	0.01	0.01	35.87	35.87	-73	0.01	0.01	35.87	35.87	-72	0.01	0.01	34.86	34.86	-71	0.01	0.01	23.61	23.61					
-70	0.01	0.01	23.61	23.61	-69	0.01	0.01	23.61	23.61	-68	0.01	0.01	23.61	23.61	-67	0.01	0.01	34.86	34.86	-66	0.01	0.01	33.85	33.85					
-65	0.01	0.01	33.85	33.85	-64	0.01	0.01	33.85	33.85	-63	0.01	0.01	33.85	33.85	-62	0.01	0.01	33.85	33.85	-61	0.01	0.01	33.85	33.85					
-60	0.01	0.01	33.85	33.85	-59	0.01	0.01	33.85	33.85	-58	0.01	0.01	22.60	22.60	-57	0.01	0.01	22.60	22.60	-56	0.01	0.01	22.57	22.57					
-55	0.01	0.01	22.57	22.57	-54	0.01	0.01	33.80	33.80	-53	0.01	0.01	33.80	33.80	-52	0.01	0.01	33.80	33.80	-51	0.01	0.01	33.80	33.80					
-50	0.01	0.01	33.80	33.80	-49	0.01	0.01	33.80	33.80	-48	0.01	0.01	33.80	33.80	-47	0.01	0.01	33.80	33.80	-45	0.05	0.05	127.29	127.29					
-29	0.03	0.03	81.03	81.03	-26	0.03	0.03	81.03	81.03	-18	0.02	0.02	51.87	51.87	-15	0.03	0.03	76.24	76.24	-14	0.03	0.03	76.24	76.24					
-13	0.03	0.03	76.24	76.24	-12	0.03	0.03	76.24	76.24	-11	0.02	0.02	51.95	51.95	-10	0.02	0.02	51.89	51.89	-9	0.03	0.03	76.11	76.11					
-8	0.03	0.03	76.11	76.11	-7	0.03	0.03	76.11	76.11	-6	0.03	0.03	76.11	76.11	-3	0.02	0.02	51.87	51.87	201	0.03	0.03	76.11	76.11					
202	0.02	0.02	53.69	53.69	203	0.05	0.05	127.36	127.36																				

Totali forze sismiche

Fx <daN>	Fy <daN>
2439.92	2439.92

Domanda in duttilità di curvatura

Direzione X $\mu_{max}=1.20$
Direzione Y $\mu_{max}=1.20$

Reazioni vincolari

Simbologia
CC = Numero della combinazione delle condizioni di carico elementari
Fx = Reazione vincolare (forza) in dir. X
Fy = Reazione vincolare (forza) in dir. Y
Fz = Reazione vincolare (forza) in dir. Z
Mx = Reazione vincolare (momento) intorno all'asse X
My = Reazione vincolare (momento) intorno all'asse Y
Mz = Reazione vincolare (momento) intorno all'asse Z
Nodo = Numero del nodo
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SND = Stato limite di salvaguardia della vita (non dissipativo)

Nodo	CC	TCC	Fx <daN>	Fy <daN>	Fz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>											
2	Max	5	SND	877.85	13	SND	866.05	29	SLU	6832.98	9	SND	2833.68	5	SND	1651.42	9	SND	0.42
2	Min	1	SND	-1087.85	9	SND	-866.05	25	SLE F	1507.89	13	SND	-2833.68	15	SND	-1904.54	1	SND	-0.42
3	Max	5	SND	806.48	13	SND	751.62	29	SLU	5947.23	9	SND	2499.76	5	SND	1573.13	15	SND	0.26
3	Min	1	SND	-693.75	9	SND	-751.62	5	SND	1291.33	13	SND	-2499.77	9	SND	-1474.35	1	SND	-0.26
315	Max	5	SND	755.60	13	SND	822.25	29	SLU	6563.62	11	SND	2718.29	5	SND	1518.31	15	SND	0.42
315	Min	1	SND	-658.32	9	SND	-822.25	25	SLE F	1413.89	13	SND	-2718.29	9	SND	-1436.43	1	SND	-0.42



Sollecitazioni aste

Simbologia
Asta = Numero dell'asta
CC = Numero della combinazione delle condizioni di carico elementari
Mx = Momento torcente intorno all'asse X
My = Momento flettente intorno all'asse Y
Mz = Momento flettente intorno all'asse Z
N = Sforzo normale
N1 = Nodo1
N2 = Nodo2
Ty = Taglio in dir. Y
Tz = Taglio in dir. Z
X = Coordinata progressiva rispetto al nodo iniziale

Tipo di combinazione di carico: SND

Table with columns: Asta, N1, N2, X <cm>, N <daN>, CC, Ty <daN>, Mz <daNm>, Tz <daN>, My <daNm>, Mx <daNm>, CC. It contains a large grid of numerical data representing structural load combinations.



204	-26	-18	Min.	0.00	-99.09	5	-99.09	9	-143.48	13	227.34	1	-278.62	1	0.00	1
204	-26	-18	Min.	144.80	-99.09	5	-99.09	9	0.00	15	157.50	1	0.00	5	0.00	1
301	-45	-79	Max	0.00	34.83	13	34.83	5	52.25	1	110.49	1	-101.46	1	0.00	13
301	-45	-79	Max	150.00	34.83	13	34.83	5	0.00	1	24.80	1	0.00	1	0.00	13
301	-45	-79	Min.	0.00	-34.83	9	-34.83	1	-52.25	5	110.49	1	-101.46	1	0.00	9
301	-45	-79	Min.	150.00	-34.83	9	-34.83	1	0.00	5	24.80	1	0.00	1	0.00	9
301	-80	-45	Max	0.00	34.83	9	34.83	1	0.00	5	-24.80	1	0.00	9	0.00	1
301	-80	-45	Max	150.00	34.83	9	34.83	1	52.25	1	-110.49	1	-101.46	1	0.00	1
301	-80	-45	Min.	0.00	-34.83	13	-34.83	5	0.00	1	-24.80	1	0.00	13	0.00	1
301	-80	-45	Min.	150.00	-34.83	13	-34.83	5	-52.25	5	-110.49	1	-101.46	1	0.00	1
302	-3	-69	Max	0.00	23.61	13	23.61	5	35.41	1	78.75	1	-68.77	1	0.00	1
302	-3	-69	Max	150.00	23.61	13	23.61	5	0.00	1	12.95	1	0.00	1	0.00	1
302	-3	-69	Min.	0.00	-23.61	9	-23.61	1	-35.41	5	78.75	1	-68.77	1	0.00	1
302	-3	-69	Min.	150.00	-23.61	9	-23.61	1	0.00	5	12.95	1	0.00	1	0.00	1
302	-68	-3	Max	0.00	23.61	9	23.61	1	0.00	3	-12.95	1	0.00	1	0.00	1
302	-68	-3	Max	150.00	23.61	9	23.61	1	35.41	1	-78.75	1	-68.77	1	0.00	1
302	-68	-3	Min.	0.00	-23.61	13	-23.61	5	0.00	5	-12.95	1	0.00	7	0.00	1
302	-68	-3	Min.	150.00	-23.61	13	-23.61	5	-35.41	5	-78.75	1	-68.77	1	0.00	1
303	-29	-76	Max	0.00	35.87	13	35.87	5	53.80	1	113.42	1	-104.48	1	0.00	1
303	-29	-76	Max	150.00	35.87	13	35.87	5	0.00	1	25.89	1	0.00	1	0.00	1
303	-29	-76	Min.	0.00	-35.87	9	-35.87	1	-53.80	5	113.42	1	-104.48	1	0.00	1
303	-29	-76	Min.	150.00	-35.87	9	-35.87	1	0.00	5	25.89	1	0.00	1	0.00	1
303	-75	-29	Max	0.00	35.87	9	35.87	1	0.00	1	-25.89	1	0.00	9	0.00	1
303	-75	-29	Max	150.00	35.87	9	35.87	1	53.80	1	-113.42	1	-104.48	1	0.00	1
303	-75	-29	Min.	0.00	-35.87	13	-35.87	5	0.00	7	-25.89	1	0.00	13	0.00	1
303	-75	-29	Min.	150.00	-35.87	13	-35.87	5	-53.80	5	-113.42	1	-104.48	1	0.00	1
304	201	-77	Max	0.00	33.80	13	33.80	5	50.69	1	107.56	1	-98.45	1	0.00	1
304	201	-77	Max	150.00	33.80	13	33.80	5	0.00	5	23.70	1	0.00	1	0.00	1
304	201	-77	Min.	0.00	-33.80	9	-33.80	1	-50.69	5	107.56	1	-98.45	1	0.00	1
304	201	-77	Min.	150.00	-33.80	9	-33.80	1	0.00	1	23.70	1	0.00	1	0.00	1
304	-78	201	Max	0.00	33.80	9	33.80	1	0.00	3	-23.70	1	0.00	9	0.00	1
304	-78	201	Max	150.00	33.80	9	33.80	1	50.69	1	-107.56	1	-98.45	1	0.00	1
304	-78	201	Min.	0.00	-33.80	13	-33.80	5	0.00	5	-23.70	1	0.00	15	0.00	1
304	-78	201	Min.	150.00	-33.80	13	-33.80	5	-50.69	5	-107.56	1	-98.45	1	0.00	1
305	-6	-48	Max	0.00	33.80	13	33.80	5	50.69	1	107.56	1	-98.45	1	0.00	1
305	-6	-48	Max	150.00	33.80	13	33.80	5	0.00	5	23.70	1	0.00	1	0.00	1
305	-6	-48	Min.	0.00	-33.80	9	-33.80	1	-50.69	5	107.56	1	-98.45	1	0.00	1
305	-6	-48	Min.	150.00	-33.80	9	-33.80	1	0.00	1	23.70	1	0.00	1	0.00	1
305	-47	-6	Max	0.00	33.80	9	33.80	1	0.00	13	-23.70	1	0.00	9	0.00	1
305	-47	-6	Max	150.00	33.80	9	33.80	1	50.69	1	-107.56	1	-98.45	1	0.00	1
305	-47	-6	Min.	0.00	-33.80	13	-33.80	5	0.00	9	-23.70	1	0.00	13	0.00	1
305	-47	-6	Min.	150.00	-33.80	13	-33.80	5	-50.69	5	-107.56	1	-98.45	1	0.00	1
306	-7	-50	Max	0.00	33.80	13	33.80	5	50.69	1	107.56	1	-98.45	1	0.00	1
306	-7	-50	Max	150.00	33.80	13	33.80	5	0.00	5	23.70	1	0.00	1	0.00	1
306	-7	-50	Min.	0.00	-33.80	9	-33.80	1	-50.69	5	107.56	1	-98.45	1	0.00	1
306	-7	-50	Min.	150.00	-33.80	9	-33.80	1	0.00	1	23.70	1	0.00	1	0.00	1
306	-49	-7	Max	0.00	33.80	9	33.80	1	0.00	1	-23.70	1	0.00	5	0.00	1
306	-49	-7	Max	150.00	33.80	9	33.80	1	50.69	1	-107.56	1	-98.45	1	0.00	1
306	-49	-7	Min.	0.00	-33.80	13	-33.80	5	0.00	5	-23.70	1	0.00	1	0.00	1
306	-49	-7	Min.	150.00	-33.80	13	-33.80	5	-50.69	5	-107.56	1	-98.45	1	0.00	1
307	-8	-52	Max	0.00	33.80	13	33.80	5	50.69	1	107.56	1	-98.45	1	0.00	1
307	-8	-52	Max	150.00	33.80	13	33.80	5	0.00	5	23.70	1	0.00	1	0.00	1
307	-8	-52	Min.	0.00	-33.80	9	-33.80	1	-50.69	5	107.56	1	-98.45	1	0.00	1
307	-8	-52	Min.	150.00	-33.80	9	-33.80	1	0.00	1	23.70	1	0.00	1	0.00	1
307	-51	-8	Max	0.00	33.80	9	33.80	1	0.00	5	-23.70	1	0.00	1	0.00	1
307	-51	-8	Max	150.00	33.80	9	33.80	1	50.69	1	-107.56	1	-98.45	1	0.00	1
307	-51	-8	Min.	0.00	-33.80	13	-33.80	5	0.00	1	-23.70	1	0.00	1	0.00	1
307	-51	-8	Min.	150.00	-33.80	13	-33.80	5	-50.69	5	-107.56	1	-98.45	1	0.00	1
308	-9	-54	Max	0.00	33.80	13	33.80	5	50.69	1	107.56	1	-98.45	1	0.00	1
308	-9	-54	Max	150.00	33.80	13	33.80	5	0.00	5	23.70	1	0.00	1	0.00	1
308	-9	-54	Min.	0.00	-33.80	9	-33.80	1	-50.69	5	107.56	1	-98.45	1	0.00	1
308	-9	-54	Min.	150.00	-33.80	9	-33.80	1	0.00	1	23.70	1	0.00	1	0.00	1
308	-53	-9	Max	0.00	33.80	9	33.80	1	0.00	1	-23.70	1	0.00	1	0.00	1
308	-53	-9	Max	150.00	33.80	9	33.80	1	50.69	1	-107.56	1	-98.45	1	0.00	1
308	-53	-9	Min.	0.00	-33.80	13	-33.80	5	0.00	1	-23.70	1	0.00	1	0.00	1
308	-53	-9	Min.	150.00	-33.80	13	-33.80	5	-50.69	5	-107.56	1	-98.45	1	0.00	1
309	-10	-56	Max	0.00	22.57	13	22.57	5	33.86	1	75.82	1	-65.76	1	0.00	1
309	-10	-56	Max	150.00	22.57	13	22.57	5	0.00	1	11.85	1	0.00	1	0.00	1
309	-10	-56	Min.	0.00	-22.57	9	-22.57	1	-33.86	5	75.82	1	-65.76	1	0.00	1
309	-10	-56	Min.	150.00	-22.57	9	-22.57	1	0.00	5	11.85	1	0.00	1	0.00	1
309	-55	-10	Max	0.00	22.57	9	22.57	1	0.00	7	-11.85	1	0.00	13	0.00	1
309	-55	-10	Max	150.00	22.57	9	22.57	1	33.86	1	-75.82	1	-65.76	1	0.00	1
309	-55	-10	Min.	0.00	-22.57	13	-22.57	5	0.00	1	-11.85	1	0.00	9	0.00	1
309	-55	-10	Min.	150.00	-22.57	13	-22.57	5	-33.86	5	-75.82	1	-65.76	1	0.00	1
310	-11	-58	Max	0.00	22.60	13	22.60	5	33.90	1	75.90	1	-65.84	1	0.00	1
310	-11	-58	Max	150.00	22.60	13	22.60	5	0.00	5	11.88	1	0.00	9	0.00	1
310	-11	-58	Min.	0.00	-22.60	9	-22.60	1	-33.90	5	75.90	1	-65.84	1	0.00	1
310	-11	-58	Min.	150.00	-22.60	9	-22.60	1	0.00	1	11.88	1	0.00	13	0.00	1
310	-57	-11	Max	0.00	22.60	9	22.60	1	0.00	1	-11.88	1	0.00	1	0.00	1
310	-57	-11	Max	150.00	22.60	9	22.60	1	33.90	1	-75.90	1	-65.84	1	0.00	1
310	-57	-11	Min.	0.00	-22.60	13	-22.60	5	0.00	1	-11.88	1	0.00	1	0.00	1
310	-57	-11	Min.	150.00	-22.60	13	-22.60	5	-33.90	5	-75.90	1	-65.84	1	0.00	1
311	-12	-60	Max	0.00	33.85	13	33.85	5	50.78	1	107.72	1	-98.61	1	0.00	1
311	-12	-60	Max	150.00	33.85	13	33.85	5	0.00	1	23.76	1	0.00	1	0.00	1
311	-12	-60	Min.	0.00	-33.85	9	-33.85	1	-50.78	5	107.72	1	-98.61	1	0.00	1
311	-12	-60	Min.	150.00	-33.85	9	-33.85	1	0.00	5	23.76	1	0.00	13	0.00	1
311	-59	-12	Max	0.00	33.85	9	33.85	1	0.00	3	-23.76	1	0.00	13	0.00	1
311	-59	-12	Max	150.00	33.85	9	33.85	1	50.78	1	-107.72	1	-9			

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313	-14	-64	Min.	150.00	-33.85	9	-33.85	1	0.00	5	23.76	1	0.00	1	0.00	1	0.00	1
313	-63	-14	Max	0.00	33.85	9	33.85	1	0.00	7	-23.76	1	0.00	13	0.00	1	0.00	1
313	-63	-14	Max	150.00	33.85	9	33.85	1	50.78	1	-107.72	1	-98.61	1	0.00	1	0.00	1
313	-63	-14	Min.	0.00	-33.85	13	-33.85	5	0.00	1	-23.76	1	0.00	11	0.00	1	0.00	1
313	-63	-14	Min.	150.00	-33.85	13	-33.85	5	-50.78	5	-107.72	1	-98.61	1	0.00	1	0.00	1
314	-15	-66	Max	0.00	33.85	13	33.85	5	50.78	1	107.72	1	-98.61	1	0.00	1	0.00	1
314	-15	-66	Max	150.00	33.85	13	33.85	5	0.00	1	23.76	1	0.00	1	0.00	1	0.00	1
314	-15	-66	Min.	0.00	-33.85	9	-33.85	1	-50.78	5	107.72	1	-98.61	1	0.00	1	0.00	1
314	-15	-66	Min.	150.00	-33.85	9	-33.85	1	0.00	5	23.76	1	0.00	1	0.00	1	0.00	1
314	-65	-15	Max	0.00	33.85	9	33.85	1	0.00	1	-23.76	1	0.00	13	0.00	1	0.00	1
314	-65	-15	Max	150.00	33.85	9	33.85	1	50.78	1	-107.72	1	-98.61	1	0.00	1	0.00	1
314	-65	-15	Min.	0.00	-33.85	13	-33.85	5	0.00	7	-23.76	1	0.00	9	0.00	1	0.00	1
314	-65	-15	Min.	150.00	-33.85	13	-33.85	5	-50.78	5	-107.72	1	-98.61	1	0.00	1	0.00	1
315	203	-67	Max	0.00	34.86	13	34.86	5	52.29	1	110.57	1	-101.55	1	0.00	1	0.00	1
315	203	-67	Max	150.00	34.86	13	34.86	5	0.00	1	24.83	1	0.00	1	0.00	1	0.00	1
315	203	-67	Min.	0.00	-34.86	9	-34.86	1	-52.29	5	110.57	1	-101.55	1	0.00	1	0.00	1
315	203	-67	Min.	150.00	-34.86	9	-34.86	1	0.00	5	24.83	1	0.00	1	0.00	1	0.00	1
315	-72	203	Max	0.00	34.86	9	34.86	1	0.00	5	-24.83	1	0.00	13	0.00	1	0.00	1
315	-72	203	Max	150.00	34.86	9	34.86	1	52.29	1	-110.57	1	-101.55	1	0.00	1	0.00	1
315	-72	203	Min.	0.00	-34.86	13	-34.86	5	0.00	3	-24.83	1	0.00	11	0.00	1	0.00	1
315	-72	203	Min.	150.00	-34.86	13	-34.86	5	-52.29	5	-110.57	1	-101.55	1	0.00	1	0.00	1
316	-26	-74	Max	0.00	35.87	13	35.87	5	53.80	1	113.42	1	-104.48	1	0.00	1	0.00	1
316	-26	-74	Max	150.00	35.87	13	35.87	5	0.00	5	25.89	1	0.00	1	0.00	1	0.00	1
316	-26	-74	Min.	0.00	-35.87	9	-35.87	1	-53.80	5	113.42	1	-104.48	1	0.00	1	0.00	1
316	-26	-74	Min.	150.00	-35.87	9	-35.87	1	0.00	1	25.89	1	0.00	1	0.00	1	0.00	1
316	-73	-26	Max	0.00	35.87	9	35.87	1	0.00	5	-25.89	1	0.00	1	0.00	1	0.00	1
316	-73	-26	Max	150.00	35.87	9	35.87	1	53.80	1	-113.42	1	-104.48	1	0.00	1	0.00	1
316	-73	-26	Min.	0.00	-35.87	13	-35.87	5	0.00	1	-25.89	1	0.00	5	0.00	1	0.00	1
316	-73	-26	Min.	150.00	-35.87	13	-35.87	5	-53.80	5	-113.42	1	-104.48	1	0.00	1	0.00	1
317	-18	-71	Max	0.00	23.61	13	23.61	5	35.41	1	78.75	1	-68.77	1	0.00	1	0.00	1
317	-18	-71	Max	150.00	23.61	13	23.61	5	0.00	13	12.95	1	0.00	5	0.00	1	0.00	1
317	-18	-71	Min.	0.00	-23.61	9	-23.61	1	-35.41	5	78.75	1	-68.77	1	0.00	1	0.00	1
317	-18	-71	Min.	150.00	-23.61	9	-23.61	1	0.00	9	12.95	1	0.00	1	0.00	1	0.00	1
317	-70	-18	Max	0.00	23.61	9	23.61	1	0.00	3	-12.95	1	0.00	13	0.00	1	0.00	1
317	-70	-18	Max	150.00	23.61	9	23.61	1	35.41	1	-78.75	1	-68.77	1	0.00	1	0.00	1
317	-70	-18	Min.	0.00	-23.61	13	-23.61	5	0.00	5	-12.95	1	0.00	9	0.00	1	0.00	1
317	-70	-18	Min.	150.00	-23.61	13	-23.61	5	-35.41	5	-78.75	1	-68.77	1	0.00	1	0.00	1

Tipo di combinazione di carico: SLD

Asta	N1	N2	X	N	CC Ty	CC Mz	CC Tz	CC My	CC Mx	CC						
			<cm>	<daN>	<daN>	<daNm>	<daN>	<daNm>	<daNm>							
1	315	-45	Max	0.00	-1610.02	2	241.49	2	647.22	6	337.44	10	1115.53	14	0.17	10
1	315	-45	Max	330.00	-1420.79	2	241.49	2	231.56	2	337.44	10	1.99	16	0.17	10
1	315	-45	Min.	0.00	-1765.07	6	-338.76	6	-565.35	2	-337.44	14	-1115.53	10	-0.17	16
1	315	-45	Min.	330.00	-1575.83	6	-338.76	6	-470.68	6	-337.44	14	-1.99	10	-0.17	16
2	202	Max	0.00	-1763.72	2	508.34	2	603.09	6	355.41	10	1162.89	14	0.17	16	
2	202	Max	330.00	-1574.49	2	508.34	2	821.33	2	355.41	10	9.97	12	0.17	16	
2	202	Min.	0.00	-1816.40	6	-298.34	6	-856.21	2	-355.41	14	-1162.89	10	-0.17	10	
2	202	Min.	330.00	-1627.17	6	-298.34	6	-381.44	6	-355.41	14	-9.97	14	-0.17	10	
3	3	203	Max	0.00	-1440.55	6	251.47	2	674.70	6	308.45	10	1025.86	14	0.11	10
3	3	203	Max	330.00	-1251.32	6	251.47	2	253.92	2	308.45	10	7.98	16	0.11	10
3	3	203	Min.	0.00	-1648.28	2	-364.19	6	-575.92	2	-308.45	14	-1025.85	10	-0.11	16
3	3	203	Min.	330.00	-1459.04	2	-364.19	6	-527.14	6	-308.45	14	-7.98	10	-0.11	16
201	-3	-29	Max	0.00	40.66	6	40.66	10	0.00	6	-157.50	2	0.00	2	0.00	2
201	-3	-29	Max	144.80	40.66	6	40.66	10	58.88	12	-227.34	2	-278.62	2	0.00	2
201	-3	-29	Min.	0.00	-40.66	2	-40.66	14	0.00	2	-157.50	2	0.00	6	0.00	2
201	-3	-29	Min.	144.80	-40.66	2	-40.66	14	-58.88	14	-227.34	2	-278.62	2	0.00	2
201	-29	-45	Max	0.00	103.36	6	103.36	10	58.88	12	-454.17	2	-278.62	2	0.00	2
201	-29	-45	Max	144.80	103.36	6	103.36	10	208.54	10	-524.01	2	-986.83	2	0.00	2
201	-29	-45	Min.	0.00	-103.36	2	-103.36	14	-58.88	14	-454.17	2	-278.62	2	0.00	2
201	-29	-45	Min.	144.80	-103.36	2	-103.36	14	-208.54	14	-524.01	2	-986.83	2	0.00	2
202	-45	201	Max	0.00	57.30	2	153.25	14	208.72	12	830.85	6	-755.27	2	1.99	16
202	-45	201	Max	132.57	57.30	2	153.25	14	5.55	12	766.91	6	98.24	2	1.99	16
202	-45	201	Min.	0.00	-154.57	6	-153.25	10	-208.72	14	675.80	2	-1457.51	6	-1.99	10
202	-45	201	Min.	132.57	-154.57	6	-153.25	10	-5.55	14	611.87	2	-398.47	6	-1.99	10
202	201	-6	Max	0.00	-1.67	4	94.28	14	5.55	12	551.79	6	98.24	2	1.99	16
202	201	-6	Max	132.57	-1.67	4	94.28	14	119.43	16	487.85	6	581.82	2	1.99	16
202	201	-6	Min.	0.00	-95.60	6	-94.28	12	-5.55	14	396.75	2	-398.46	6	-1.99	10
202	201	-6	Min.	132.57	-95.60	6	-94.28	12	-119.43	10	332.81	2	290.64	6	-1.99	10
202	-6	-7	Max	0.00	-36.63	6	35.31	14	119.43	16	272.74	6	581.81	2	1.99	16
202	-6	-7	Max	132.57	-36.63	6	35.31	14	166.24	14	208.80	6	695.45	2	1.99	16
202	-6	-7	Min.	0.00	-60.64	2	-35.31	12	-119.43	10	117.70	2	290.63	6	-1.99	10
202	-6	-7	Min.	132.57	-60.64	2	-35.31	12	-166.24	10	53.76	2	609.81	6	-1.99	10
202	-7	-8	Max	0.00	22.34	6	23.66	10	166.24	16	-6.32	8	695.46	2	1.99	16
202	-7	-8	Max	132.57	22.34	6	23.66	10	134.87	14	-70.26	6	559.06	6	1.99	16
202	-7	-8	Min.	0.00	-119.61	2	-23.66	16	-166.24	10	-161.36	2	609.81	6	-1.99	10
202	-7	-8	Min.	132.57	-119.61	2	-23.66	16	-134.87	10	-225.30	2	439.17	2	-1.99	10
202	-8	-9	Max	0.00	81.31	6	82.63	10	134.87	16	-285.38	6	559.05	6	1.99	16
202	-8	-9	Max	132.57	81.31	6	82.63	10	25.33	14	-349.31	6	138.36	6	1.99	16
202	-8	-9	Min.	0.00	-178.59	2	-82.63	16	-134.87	10	-440.42	2	439.16	2	-1.99	10
202	-8	-9	Min.	132.57	-178.59	2	-82.63	16	-25.33	12	-504.35	2	-187.07	2	-1.99	10
202	-9	-10	Max	0.00	140.28	6	141.60	10	25.33	16	-564.43	6	138.38	6	1.99	16
202	-9	-10	Max	132.57	140.28	6	141.60	10	162.39	10	-628.37	6	-652.24	6	1.99	16
202	-9	-10	Min.	0.00	-237.56	2	-141.60	14	-25.33	10	-719.47	2	-187.03	2	-1.99	10
202	-9	-10	Min.	132.57	-237.56	2	-141.60</									

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203	-12	-13	Min.	132.90	2.74	6	-53.01	12	-51.28	12	124.71	2	316.16	6	-7.98	14
203	-13	-14	Max	0.00	61.81	6	6.07	10	51.28	14	116.99	6	363.28	2	7.98	12
203	-13	-14	Max	91.83					-45.71	12			352.99	12		
203	-13	-14	Max	132.90	61.81	6	6.07	10	43.22	14	52.89	6	429.05	6	7.98	12
203	-13	-14	Min.	0.00	50.91	2	-6.07	16	-51.28	12	-90.73	2	316.16	6	-7.98	14
203	-13	-14	Min.	91.83					-45.71	12			352.99	12		
203	-13	-14	Min.	132.90	50.91	2	-6.07	16	-43.22	12	-154.83	2	200.11	2	-7.98	14
203	-14	-15	Max	0.00	120.89	6	65.14	10	43.22	14	-162.54	6	429.05	6	7.98	12
203	-14	-15	Max	132.90	120.89	6	65.14	10	43.36	10	-226.64	6	170.43	6	7.98	12
203	-14	-15	Min.	0.00	-8.16	2	-65.14	16	-43.22	12	-370.26	2	200.11	2	-7.98	14
203	-14	-15	Min.	132.90	-8.16	2	-65.14	16	-43.36	16	-434.36	2	-334.56	2	-7.98	14
203	-15	203	Max	0.00	179.96	6	124.21	10	43.36	10	-442.08	6	170.43	6	7.98	12
203	-15	203	Max	132.90	179.96	6	124.21	10	208.43	10	-506.18	6	-459.68	6	7.98	12
203	-15	203	Min.	0.00	-67.23	2	-124.21	16	-43.36	16	-649.80	2	-334.56	2	-7.98	14
203	-15	203	Min.	132.90	-67.23	2	-124.21	16	-208.43	16	-713.90	2	-1240.74	2	-7.98	14
204	203	-26	Max	0.00	103.36	2	103.36	14	208.54	10	524.01	2	-986.83	2	0.00	2
204	203	-26	Max	144.80	103.36	2	103.36	14	58.88	10	454.17	2	-278.62	2	0.00	2
204	203	-26	Min.	0.00	-103.36	6	-103.36	10	-208.54	14	524.01	2	-986.83	2	0.00	2
204	203	-26	Min.	144.80	-103.36	6	-103.36	10	-58.88	16	454.17	2	-278.62	2	0.00	2
204	-26	-18	Max	0.00	40.66	2	40.66	14	58.88	10	227.34	2	-278.62	2	0.00	2
204	-26	-18	Max	144.80	40.66	2	40.66	14	0.00	10	157.50	2	0.00	2	0.00	2
204	-26	-18	Min.	0.00	-40.66	6	-40.66	10	-58.88	16	227.34	2	-278.62	2	0.00	2
204	-26	-18	Min.	144.80	-40.66	6	-40.66	10	0.00	16	157.50	2	0.00	2	0.00	2
301	-45	-79	Max	0.00	14.29	14	14.29	6	21.44	2	110.49	2	-101.46	2	0.00	14
301	-45	-79	Max	150.00	14.29	14	14.29	6	0.00	2	24.80	2	0.00	2	0.00	14
301	-45	-79	Min.	0.00	-14.29	10	-14.29	2	-21.44	6	110.49	2	-101.46	2	0.00	10
301	-45	-79	Min.	150.00	-14.29	10	-14.29	2	0.00	6	24.80	2	0.00	2	0.00	10
301	-80	-45	Max	0.00	14.29	10	14.29	2	0.00	6	-24.80	2	0.00	10	0.00	2
301	-80	-45	Max	150.00	14.29	10	14.29	2	21.44	2	-110.49	2	-101.46	2	0.00	2
301	-80	-45	Min.	0.00	-14.29	6	-14.29	2	0.00	2	-24.80	2	0.00	14	0.00	2
301	-80	-45	Min.	150.00	-14.29	14	-14.29	6	-21.44	6	-110.49	2	-101.46	2	0.00	2
302	-3	-69	Max	0.00	9.69	6	14.53	2	14.53	2	78.75	2	-68.77	2	0.00	2
302	-3	-69	Max	150.00	9.69	6	14.53	2	0.00	2	12.95	2	0.00	2	0.00	2
302	-3	-69	Min.	0.00	-9.69	10	-9.69	2	-14.53	6	78.75	2	-68.77	2	0.00	2
302	-3	-69	Min.	150.00	-9.69	10	-9.69	2	0.00	6	12.95	2	0.00	2	0.00	2
302	-68	-3	Max	0.00	9.69	10	9.69	2	0.00	4	-12.95	2	0.00	2	0.00	2
302	-68	-3	Max	150.00	9.69	10	9.69	2	14.53	2	-78.75	2	-68.77	2	0.00	2
302	-68	-3	Min.	0.00	-9.69	14	-9.69	6	0.00	6	-12.95	2	0.00	8	0.00	2
302	-68	-3	Min.	150.00	-9.69	14	-9.69	6	-14.53	6	-78.75	2	-68.77	2	0.00	2
303	-29	-76	Max	0.00	14.72	14	14.72	6	22.08	2	113.42	2	-104.48	2	0.00	2
303	-29	-76	Max	150.00	14.72	14	14.72	6	0.00	2	25.89	2	0.00	2	0.00	2
303	-29	-76	Min.	0.00	-14.72	10	-14.72	2	-22.08	6	113.42	2	-104.48	2	0.00	2
303	-29	-76	Min.	150.00	-14.72	10	-14.72	2	0.00	6	25.89	2	0.00	2	0.00	2
303	-75	-29	Max	0.00	14.72	10	14.72	2	0.00	2	-25.89	2	0.00	10	0.00	2
303	-75	-29	Max	150.00	14.72	10	14.72	2	22.08	2	-113.42	2	-104.48	2	0.00	2
303	-75	-29	Min.	0.00	-14.72	14	-14.72	6	0.00	8	-25.89	2	0.00	14	0.00	2
303	-75	-29	Min.	150.00	-14.72	14	-14.72	6	-22.08	6	-113.42	2	-104.48	2	0.00	2
304	201	-77	Max	0.00	13.87	14	13.87	6	20.80	2	107.56	2	-98.45	2	0.00	2
304	201	-77	Max	150.00	13.87	14	13.87	6	0.00	6	23.70	2	0.00	2	0.00	2
304	201	-77	Min.	0.00	-13.87	10	-13.87	2	-20.80	6	107.56	2	-98.45	2	0.00	2
304	201	-77	Min.	150.00	-13.87	10	-13.87	2	0.00	2	23.70	2	0.00	2	0.00	2
304	-78	201	Max	0.00	13.87	10	13.87	2	0.00	4	-23.70	2	0.00	10	0.00	2
304	-78	201	Max	150.00	13.87	10	13.87	2	20.80	2	-107.56	2	-98.45	2	0.00	2
304	-78	201	Min.	0.00	-13.87	14	-13.87	6	0.00	6	-23.70	2	0.00	16	0.00	2
304	-78	201	Min.	150.00	-13.87	14	-13.87	6	-20.80	6	-107.56	2	-98.45	2	0.00	2
305	-6	-48	Max	0.00	13.87	14	13.87	6	20.80	2	107.56	2	-98.45	2	0.00	2
305	-6	-48	Max	150.00	13.87	14	13.87	6	0.00	6	23.70	2	0.00	2	0.00	2
305	-6	-48	Min.	0.00	-13.87	10	-13.87	2	-20.80	6	107.56	2	-98.45	2	0.00	2
305	-6	-48	Min.	150.00	-13.87	10	-13.87	2	0.00	2	23.70	2	0.00	2	0.00	2
305	-47	-6	Max	0.00	13.87	10	13.87	2	0.00	14	-23.70	2	0.00	10	0.00	2
305	-47	-6	Max	150.00	13.87	10	13.87	2	20.80	2	-107.56	2	-98.45	2	0.00	2
305	-47	-6	Min.	0.00	-13.87	14	-13.87	6	0.00	10	-23.70	2	0.00	14	0.00	2
305	-47	-6	Min.	150.00	-13.87	14	-13.87	6	-20.80	6	-107.56	2	-98.45	2	0.00	2
306	-7	-50	Max	0.00	13.87	14	13.87	6	20.80	2	107.56	2	-98.45	2	0.00	2
306	-7	-50	Max	150.00	13.87	14	13.87	6	0.00	6	23.70	2	0.00	2	0.00	2
306	-7	-50	Min.	0.00	-13.87	10	-13.87	2	-20.80	6	107.56	2	-98.45	2	0.00	2
306	-7	-50	Min.	150.00	-13.87	10	-13.87	2	0.00	2	23.70	2	0.00	2	0.00	2
306	-49	-7	Max	0.00	13.87	10	13.87	2	0.00	2	-23.70	2	0.00	6	0.00	2
306	-49	-7	Max	150.00	13.87	10	13.87	2	20.80	2	-107.56	2	-98.45	2	0.00	2
306	-49	-7	Min.	0.00	-13.87	14	-13.87	6	0.00	6	-23.70	2	0.00	2	0.00	2
306	-49	-7	Min.	150.00	-13.87	14	-13.87	6	-20.80	6	-107.56	2	-98.45	2	0.00	2
307	-8	-52	Max	0.00	13.87	14	13.87	6	20.80	2	107.56	2	-98.45	2	0.00	2
307	-8	-52	Max	150.00	13.87	14	13.87	6	0.00	6	23.70	2	0.00	2	0.00	2
307	-8	-52	Min.	0.00	-13.87	10	-13.87	2	-20.80	6	107.56	2	-98.45	2	0.00	2
307	-8	-52	Min.	150.00	-13.87	10	-13.87	2	0.00	2	23.70	2	0.00	2	0.00	2
307	-51	-8	Max	0.00	13.87	10	13.87	2	0.00	6	-23.70	2	0.00	2	0.00	2
307	-51	-8	Max	150.00	13.87	10	13.87	2	20.80	2	-107.56	2	-98.45	2	0.00	2
307	-51	-8	Min.	0.00	-13.87	14	-13.87	6	0.00	2	-23.70	2	0.00	2	0.00	2
307	-51	-8	Min.	150.00	-13.87	14	-13.87	6	-20.80	6	-107.56	2	-98.45	2	0.00	2
308	-9	-54	Max	0.00	13.87	14	13.87	6	20.80	2	107.56	2	-98.45	2	0.00	2
308	-9	-54	Max	150.00	13.87	14	13.87	6	0.00	6	23.70	2	0.00	2	0.00	2
308	-9	-54	Min.	0.00	-13.87	10	-13.87	2	-20.80	6	107.56	2	-98.45	2	0.00	2
308	-9	-54	Min.	150.00	-13.87	10	-13.87	2	0.00	2	23.70	2	0.00	2	0.00	2
308	-53	-9	Max	0.00	13.87	10	13.87	2	0.00	2	-23.70	2	0.00	2	0.00	2
308	-53	-9	Max	150.00	13.87	10	13.87	2	20.80	2	-107.56	2	-98.45	2	0.00	2
308	-53	-9	Min.	0.00	-13.87	14	-13.87	6	0.00	2	-23.70	2	0.00	2	0.00	2
308	-53	-9	Min.	150.00	-13.87	14	-13.87	6	-20.80	6	-107.56	2	-98.45	2	0.00	2
309	-10	-56	Max	0.00	9.26	14</										



310	-57	-11	Min.	0.00	-9.28	14	-9.28	6	0.00	2	-11.88	2	0.00	2	0.00	2
310	-57	-11	Min.	150.00	-9.28	14	-9.28	6	-13.91	6	-75.90	2	-65.84	2	0.00	2
311	-12	-60	Max	0.00	13.89	14	13.89	6	20.84	2	107.72	2	-98.61	2	0.00	2
311	-12	-60	Max	150.00	13.89	14	13.89	6	0.00	2	23.76	2	0.00	2	0.00	2
311	-12	-60	Min.	0.00	-13.89	10	-13.89	2	-20.84	6	107.72	2	-98.61	2	0.00	2
311	-12	-60	Min.	150.00	-13.89	10	-13.89	2	0.00	6	23.76	2	0.00	2	0.00	2
311	-59	-12	Max	0.00	13.89	10	13.89	2	0.00	4	-23.76	2	0.00	2	14.00	2
311	-59	-12	Max	150.00	13.89	10	13.89	2	20.84	2	-107.72	2	-98.61	2	0.00	2
311	-59	-12	Min.	0.00	-13.89	14	-13.89	6	0.00	6	-23.76	2	0.00	2	10.00	2
311	-59	-12	Min.	150.00	-13.89	14	-13.89	6	-20.84	6	-107.72	2	-98.61	2	0.00	2
312	-13	-62	Max	0.00	13.89	14	13.89	6	20.84	2	107.72	2	-98.61	2	0.00	2
312	-13	-62	Max	150.00	13.89	14	13.89	6	0.00	2	23.76	2	0.00	2	0.00	2
312	-13	-62	Min.	0.00	-13.89	10	-13.89	2	-20.84	6	107.72	2	-98.61	2	0.00	2
312	-13	-62	Min.	150.00	-13.89	10	-13.89	2	0.00	6	23.76	2	0.00	2	0.00	2
312	-61	-13	Max	0.00	13.89	10	13.89	2	0.00	2	-23.76	2	0.00	2	0.00	2
312	-61	-13	Max	150.00	13.89	10	13.89	2	20.84	2	-107.72	2	-98.61	2	0.00	2
312	-61	-13	Min.	0.00	-13.89	14	-13.89	6	0.00	6	-23.76	2	0.00	2	0.00	2
312	-61	-13	Min.	150.00	-13.89	14	-13.89	6	-20.84	6	-107.72	2	-98.61	2	0.00	2
313	-14	-64	Max	0.00	13.89	14	13.89	6	20.84	2	107.72	2	-98.61	2	0.00	2
313	-14	-64	Max	150.00	13.89	14	13.89	6	0.00	2	23.76	2	0.00	2	0.00	2
313	-14	-64	Min.	0.00	-13.89	10	-13.89	2	-20.84	6	107.72	2	-98.61	2	0.00	2
313	-14	-64	Min.	150.00	-13.89	10	-13.89	2	0.00	6	23.76	2	0.00	2	0.00	2
313	-63	-14	Max	0.00	13.89	10	13.89	2	0.00	8	-23.76	2	0.00	2	14.00	2
313	-63	-14	Max	150.00	13.89	10	13.89	2	20.84	2	-107.72	2	-98.61	2	0.00	2
313	-63	-14	Min.	0.00	-13.89	14	-13.89	6	0.00	2	-23.76	2	0.00	2	12.00	2
313	-63	-14	Min.	150.00	-13.89	14	-13.89	6	-20.84	6	-107.72	2	-98.61	2	0.00	2
314	-15	-66	Max	0.00	13.89	14	13.89	6	20.84	2	107.72	2	-98.61	2	0.00	2
314	-15	-66	Max	150.00	13.89	14	13.89	6	0.00	2	23.76	2	0.00	2	0.00	2
314	-15	-66	Min.	0.00	-13.89	10	-13.89	2	-20.84	6	107.72	2	-98.61	2	0.00	2
314	-15	-66	Min.	150.00	-13.89	10	-13.89	2	0.00	6	23.76	2	0.00	2	0.00	2
314	-65	-15	Max	0.00	13.89	10	13.89	2	0.00	2	-23.76	2	0.00	2	14.00	2
314	-65	-15	Max	150.00	13.89	10	13.89	2	20.84	2	-107.72	2	-98.61	2	0.00	2
314	-65	-15	Min.	0.00	-13.89	14	-13.89	6	0.00	8	-23.76	2	0.00	2	10.00	2
314	-65	-15	Min.	150.00	-13.89	14	-13.89	6	-20.84	6	-107.72	2	-98.61	2	0.00	2
315	203	-67	Max	0.00	14.31	14	14.31	6	21.46	2	110.57	2	-101.55	2	0.00	2
315	203	-67	Max	150.00	14.31	14	14.31	6	0.00	2	24.83	2	0.00	2	0.00	2
315	203	-67	Min.	0.00	-14.31	10	-14.31	2	-21.46	6	110.57	2	-101.55	2	0.00	2
315	203	-67	Min.	150.00	-14.31	10	-14.31	2	0.00	6	24.83	2	0.00	2	0.00	2
315	-72	203	Max	0.00	14.31	10	14.31	2	0.00	6	-24.83	2	0.00	2	14.00	2
315	-72	203	Max	150.00	14.31	10	14.31	2	21.46	2	-110.57	2	-101.55	2	0.00	2
315	-72	203	Min.	0.00	-14.31	14	-14.31	6	0.00	4	-24.83	2	0.00	2	12.00	2
315	-72	203	Min.	150.00	-14.31	14	-14.31	6	-21.46	6	-110.57	2	-101.55	2	0.00	2
316	-26	-74	Max	0.00	14.72	14	14.72	6	22.08	2	113.42	2	-104.48	2	0.00	2
316	-26	-74	Max	150.00	14.72	14	14.72	6	0.00	6	25.89	2	0.00	2	0.00	2
316	-26	-74	Min.	0.00	-14.72	10	-14.72	2	-22.08	6	113.42	2	-104.48	2	0.00	2
316	-26	-74	Min.	150.00	-14.72	10	-14.72	2	0.00	2	25.89	2	0.00	2	0.00	2
316	-73	-26	Max	0.00	14.72	10	14.72	2	0.00	6	-25.89	2	0.00	2	0.00	2
316	-73	-26	Max	150.00	14.72	10	14.72	2	22.08	2	-113.42	2	-104.48	2	0.00	2
316	-73	-26	Min.	0.00	-14.72	14	-14.72	6	0.00	2	-25.89	2	0.00	2	6.00	2
316	-73	-26	Min.	150.00	-14.72	14	-14.72	6	-22.08	6	-113.42	2	-104.48	2	0.00	2
317	-18	-71	Max	0.00	9.69	14	9.69	6	14.53	2	78.75	2	-68.77	2	0.00	2
317	-18	-71	Max	150.00	9.69	14	9.69	6	0.00	14	12.95	2	0.00	2	0.00	2
317	-18	-71	Min.	0.00	-9.69	10	-9.69	2	-14.53	6	78.75	2	-68.77	2	0.00	2
317	-18	-71	Min.	150.00	-9.69	10	-9.69	2	0.00	10	12.95	2	0.00	2	0.00	2
317	-70	-18	Max	0.00	9.69	10	9.69	2	0.00	4	-12.95	2	0.00	2	14.00	2
317	-70	-18	Max	150.00	9.69	10	9.69	2	14.53	2	-78.75	2	-68.77	2	0.00	2
317	-70	-18	Min.	0.00	-9.69	14	-9.69	6	0.00	6	-12.95	2	0.00	2	10.00	2
317	-70	-18	Min.	150.00	-9.69	14	-9.69	6	-14.53	6	-78.75	2	-68.77	2	0.00	2

Tipo di combinazione di carico: SLU

Asta	N1	N2	X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC						
1	315	-45	Max	0.00	-2147.20	21	-60.81	21	261.84	29	0.00	29	0.00	29	0.00	28
1	315	-45	Max	330.00	-1901.20	21	-60.81	21	-149.69	21	0.00	29	0.00	29	0.00	28
1	315	-45	Min.	0.00	-6563.62	29	-289.62	29	51.00	21	0.00	21	0.00	21	0.00	21
1	315	-45	Min.	330.00	-6317.61	29	-289.62	29	-693.90	29	0.00	21	0.00	21	0.00	21
2	2	202	Max	0.00	-2279.03	21	450.59	29	-160.47	21	0.00	21	0.00	29	0.00	22
2	2	202	Max	330.00	-2033.02	21	450.59	29	942.17	29	0.00	21	0.00	29	0.00	22
2	2	202	Min.	0.00	-6832.98	29	133.15	21	-544.78	29	0.00	28	0.00	28	0.00	28
2	2	202	Min.	330.00	-6586.97	29	133.15	21	278.93	21	0.00	28	0.00	28	0.00	28
3	3	203	Max	0.00	-1965.72	21	-72.34	21	122.35	29	0.00	28	0.00	29	0.00	22
3	3	203	Max	330.00	-1719.71	21	-72.34	21	-175.13	21	0.00	28	0.00	29	0.00	22
3	3	203	Min.	0.00	-5947.23	29	-160.97	29	63.59	21	0.00	21	0.00	21	0.00	28
3	3	203	Min.	330.00	-5701.22	29	-160.97	29	-408.86	29	0.00	21	0.00	21	0.00	28
201	-3	-29	Max	0.00	0.00	17	0.00	17	0.00	28	-199.90	21	0.00	21	0.00	21
201	-3	-29	Max	144.80	0.00	17	0.00	17	0.00	28	-290.69	21	-355.19	21	0.00	21
201	-3	-29	Min.	0.00	0.00	17	0.00	17	0.00	22	-659.77	29	0.00	17	0.00	29
201	-3	-29	Min.	144.80	0.00	17	0.00	17	0.00	22	-750.56	29	-1021.08	29	0.00	29
201	-29	-45	Max	0.00	0.00	17	0.00	17	0.00	17	-575.86	21	-355.19	21	0.00	21
201	-29	-45	Max	144.80	0.00	17	0.00	17	0.00	17	-666.65	21	-1254.77	21	0.00	21
201	-29	-45	Min.	0.00	0.00	17	0.00	17	0.00	17	-1955.47	29	-1021.07	29	0.00	29
201	-29	-45	Min.	144.80	0.00	17	0.00	17	0.00	17	-2046.26	29	-3918.33	29	0.00	29
202	-45	201	Max	0.00	-60.81	21	0.00	22	0.00	28	3112.50	29	-1404.46	21	0.00	29
202	-45	201	Max	132.57	-60.81	21	0.00	22	0.00	28	3029.38	29	-191.46	21	0.00	29
202	-45	201	Min.	0.00	-289.62	29	0.00	28	0.00	21	956.57	21	-4612.23	29	0.00	21
202	-45	201	Min.	132.57	-289.62	29	0.00	28	0.00	28	873.45	21	-541.19	29	0.00	21
202	01	-6	Max	0.00	-60.81	21	0.00	22	0.00	22	1916.58	29	-191.45	21	0.00	29
202	01	-6	Max	132.57	-60.81	21	0.00	22	0.00	22	1833.46	29	1944.48	29	0.00	29
202	01	-6	Min.	0.00	-289.62	29	0.00	28								

Foggia Solar S.r.l.



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202	-8	-9	Min.	0.00	-289.62	29	0.00	28	-1671.17	29	632.73	21	0.00	29
202	-8	-9	Min.	132.57	-289.62	29	0.00	28	-1754.29	29	-110.94	29	0.00	29
202	-9	-10	Max	0.00	-60.81	21	0.00	22	-812.86	21	-30.78	21	0.00	28
202	-9	-10	Max	132.57	-60.81	21	0.00	22	-895.97	21	-1163.45	21	0.00	28
202	-9	-10	Min.	0.00	-289.62	29	0.00	28	-2867.09	29	-110.83	29	-0.00	22
202	-9	-10	Min.	132.57	-289.62	29	0.00	28	-2950.20	29	-3966.71	29	-0.00	22
202	-10	202	Max	0.00	-60.81	21	0.00	22	-1088.67	21	-1163.48	21	-0.00	28
202	-10	202	Max	20.00	-60.81	21	0.00	22	-1101.21	21	-1382.47	21	-0.00	28
202	-10	202	Min.	0.00	-289.62	29	0.00	28	-3563.92	29	-3966.82	29	-0.00	22
202	-10	202	Min.	20.00	-289.62	29	0.00	28	-3576.46	29	-4680.86	29	-0.00	22
203	202	-11	Max	0.00	160.97	29	0.00	28	3010.51	29	-1103.53	21	0.00	29
203	202	-11	Max	20.00	160.97	29	0.00	28	2997.97	29	-918.42	21	0.00	29
203	202	-11	Min.	0.00	72.34	21	-0.00	22	931.81	21	-3738.68	29	0.00	21
203	202	-11	Min.	20.00	72.34	21	-0.00	22	919.27	21	-3137.82	29	0.00	21
203	-11	-12	Max	0.00	160.97	29	0.00	28	22383.01	29	-918.43	21	0.00	29
203	-11	-12	Max	132.90	160.97	29	0.00	28	22299.68	29	-8.44	21	0.00	29
203	-11	-12	Min.	0.00	72.34	21	-0.00	22	726.38	21	-3137.83	29	0.00	21
203	-11	-12	Min.	132.90	72.34	21	-0.00	22	643.05	21	-26.19	29	0.00	21
203	-12	-13	Max	0.00	160.97	29	0.00	28	1184.37	29	-8.44	21	0.00	29
203	-12	-13	Max	132.90	160.97	29	0.00	28	1101.05	29	1492.48	29	0.00	29
203	-12	-13	Min.	0.00	72.34	21	-0.00	22	371.89	21	-26.18	29	0.00	21
203	-12	-13	Min.	132.90	72.34	21	-0.00	22	288.56	21	430.43	21	0.00	21
203	-13	-14	Max	0.00	160.97	29	0.00	28	17.40	21	1492.48	29	0.00	28
203	-13	-14	Max	27.76							432.84	21		
203	-13	-14	Max	132.90	160.97	29	0.00	28	-65.92	21	1418.15	29	0.00	28
203	-13	-14	Min.	0.00	72.34	21	-0.00	22	-14.26	29	430.43	21	0.00	22
203	-13	-14	Min.	27.76							432.84	21		
203	-13	-14	Min.	132.90	72.34	21	-0.00	22	-97.59	29	398.19	21	0.00	22
203	-14	-15	Max	0.00	160.97	29	0.00	28	-337.08	21	1418.15	29	0.00	21
203	-14	-15	Max	132.90	160.97	29	0.00	28	-420.41	21	-105.17	21	0.00	21
203	-14	-15	Min.	0.00	72.34	21	-0.00	22	-1212.90	29	398.19	21	0.00	29
203	-14	-15	Min.	132.90	72.34	21	-0.00	22	-1296.23	29	-249.16	29	0.00	29
203	-15	203	Max	0.00	160.97	29	0.00	28	-691.57	21	-105.17	21	0.00	21
203	-15	203	Max	132.90	160.97	29	0.00	28	-774.90	21	-1079.63	21	0.00	21
203	-15	203	Min.	0.00	72.34	21	-0.00	22	-2411.53	29	-249.16	29	-0.00	29
203	-15	203	Min.	132.90	72.34	21	-0.00	22	-2494.86	29	-3509.46	29	-0.00	29
204	203	-26	Max	0.00	0.00	21	0.00	17	2046.25	29	-1254.77	21	0.00	28
204	203	-26	Max	144.80	0.00	21	0.00	17	1955.47	29	-355.19	21	0.00	28
204	203	-26	Min.	0.00	0.00	17	0.00	17	666.65	21	-3918.32	29	0.00	21
204	203	-26	Min.	144.80	0.00	17	0.00	17	575.86	21	-1021.07	29	0.00	21
204	-26	-18	Max	0.00	0.00	17	0.00	17	1750.55	29	-355.19	21	0.00	28
204	-26	-18	Max	144.80	0.00	17	0.00	17	1659.77	29	0.00	22	0.00	28
204	-26	-18	Min.	0.00	0.00	17	0.00	17	290.69	21	-1021.07	29	0.00	21
204	-26	-18	Min.	144.80	0.00	17	0.00	17	199.90	21	0.00	28	0.00	21
301	-45	-79	Max	0.00	0.00	17	0.00	17	579.43	29	-127.11	21	0.00	17
301	-45	-79	Max	150.00	0.00	17	0.00	17	194.98	29	0.00	29	0.00	17
301	-45	-79	Min.	0.00	0.00	17	0.00	17	138.99	21	-580.80	29	0.00	17
301	-45	-79	Min.	150.00	0.00	17	0.00	17	30.50	21	0.00	21	0.00	17
301	-80	-45	Max	0.00	0.00	17	0.00	17	-30.50	21	0.00	21	0.00	17
301	-80	-45	Max	150.00	0.00	17	0.00	17	-138.99	21	-127.11	21	0.00	17
301	-80	-45	Min.	0.00	0.00	17	0.00	17	-194.98	29	0.00	29	0.00	17
301	-80	-45	Min.	150.00	0.00	17	0.00	17	-579.43	29	-580.80	29	0.00	17
302	-3	-69	Max	0.00	0.00	17	0.00	17	329.88	29	-86.90	21	0.00	17
302	-3	-69	Max	150.00	0.00	17	0.00	17	101.79	29	0.00	21	0.00	17
302	-3	-69	Min.	0.00	0.00	17	0.00	17	99.95	21	-323.75	29	0.00	17
302	-3	-69	Min.	150.00	0.00	17	0.00	17	15.92	21	0.00	28	0.00	17
302	-68	-3	Max	0.00	0.00	17	0.00	17	-15.92	21	0.00	29	0.00	17
302	-68	-3	Max	150.00	0.00	17	0.00	17	-99.95	21	-86.90	21	0.00	17
302	-68	-3	Min.	0.00	0.00	17	0.00	17	-101.79	29	0.00	21	0.00	17
302	-68	-3	Min.	150.00	0.00	17	0.00	17	-329.88	29	-323.75	29	0.00	17
303	-29	-76	Max	0.00	0.00	17	0.00	17	602.46	29	-130.82	21	0.00	17
303	-29	-76	Max	150.00	0.00	17	0.00	17	203.57	29	0.00	17	0.00	17
303	-29	-76	Min.	0.00	0.00	17	0.00	17	142.59	21	-604.52	29	0.00	17
303	-29	-76	Min.	150.00	0.00	17	0.00	17	31.85	21	0.00	28	0.00	17
303	-75	-29	Max	0.00	0.00	17	0.00	17	-31.85	21	0.00	22	0.00	17
303	-75	-29	Max	150.00	0.00	17	0.00	17	-142.59	21	-130.82	21	0.00	17
303	-75	-29	Min.	0.00	0.00	17	0.00	17	-203.58	29	0.00	28	0.00	17
303	-75	-29	Min.	150.00	0.00	17	0.00	17	-602.46	29	-604.52	29	0.00	17
304	201	-77	Max	0.00	0.00	17	0.00	17	556.40	29	-123.40	21	0.00	17
304	201	-77	Max	150.00	0.00	17	0.00	17	186.38	29	0.00	28	0.00	17
304	201	-77	Min.	0.00	0.00	17	0.00	17	135.38	21	-557.08	29	0.00	17
304	201	-77	Min.	150.00	0.00	17	0.00	17	29.16	21	0.00	17	0.00	17
304	-78	201	Max	0.00	0.00	17	0.00	17	-29.15	21	0.00	21	0.00	17
304	-78	201	Max	150.00	0.00	17	0.00	17	-135.38	21	-123.40	21	0.00	17
304	-78	201	Min.	0.00	0.00	17	0.00	17	-186.38	29	0.00	29	0.00	17
304	-78	201	Min.	150.00	0.00	17	0.00	17	-556.40	29	-557.08	29	0.00	17
305	-6	-48	Max	0.00	0.00	17	0.00	17	556.40	29	-123.40	21	0.00	17
305	-6	-48	Max	150.00	0.00	17	0.00	17	186.38	29	0.00	28	0.00	17
305	-6	-48	Min.	0.00	0.00	17	0.00	17	135.38	21	-557.08	29	0.00	17
305	-6	-48	Min.	150.00	0.00	17	0.00	17	29.16	21	0.00	17	0.00	17
305	-47	-6	Max	0.00	0.00	17	0.00	17	-29.15	21	0.00	28	0.00	17
305	-47	-6	Max	150.00	0.00	17	0.00	17	-135.38	21	-123.40	21	0.00	17
305	-47	-6	Min.	0.00	0.00	17	0.00	17	-186.38	29	0.00	22	0.00	17
305	-47	-6	Min.	150.00	0.00	17	0.00	17	-556.40	29	-557.08	29	0.00	17
306	-7	-50	Max	0.00	0.00	17	0.00	17	556.40	29	-123.40	21	0.00	17
306	-7	-50	Max	150.00	0.00	17	0.00	17	186.38	29	0.00	28	0.00	17
306	-7	-50	Min.	0.00	0.00	17	0.00	17	135.38	21	-557.08	29	0.00	17
306	-7	-50	Min.	150.00	0.00	17	0.00	17	29.16	21	0.00	17	0.00	17
306	-49	-7	Max	0.00	0.00	17	0.00	17	-29.15	21	0.00	21	0.00	17
306	-49	-7	Max	150.00	0.00	17	0.00	17	-135.38	21	-123.40	21	0.00	17
306	-49	-7	Min.	0.00	0.00	17	0.00	17	-186.38	29	0.00	28	0.00	17
306	-49	-7	Min.	150.00	0.00	17	0.00	17	-556.40	29	-557.08	29	0.00	17
307	-8	-52	Max	0.00	0.00	17	0.00	17	556.40	29	-123.40	21	0.00	17
307	-8	-52	Max	150.00	0.00	17	0.00	17	186.38	29	0.00	28	0.00	17
307	-8	-52	Min.	0.00	0.00	17	0.00	17	135.38	21	-557.08	29	0.00	17
307	-8	-52	Min.	150.00	0.00	17	0.00	17	29.16	21	0.00	17	0.00	17
307	-51	-8	Max	0.00	0.00	17	0.00	17	-29.15	21	0.00	21		



308	-9	-54	Max	150.00	0.00	17	0.00	17	0.00	17	186.38	29	0.00	28	0.00	17
308	-9	-54	Min.	0.00	0.00	17	0.00	17	0.00	17	135.38	21	-557.08	29	0.00	17
308	-9	-54	Max	150.00	0.00	17	0.00	17	0.00	17	29.16	21	0.00	21	0.00	17
308	-53	-9	Max	0.00	0.00	17	0.00	17	0.00	17	-29.15	21	0.00	28	0.00	17
308	-53	-9	Max	150.00	0.00	17	0.00	17	0.00	17	-135.38	21	-123.40	21	0.00	17
308	-53	-9	Min.	0.00	0.00	17	0.00	17	0.00	17	-186.38	29	0.00	22	0.00	17
308	-53	-9	Min.	150.00	0.00	17	0.00	17	0.00	17	-556.40	29	-557.08	29	0.00	17
309	-10	-56	Max	0.00	0.00	17	0.00	17	0.00	17	306.86	29	-83.19	21	0.00	17
309	-10	-56	Max	150.00	0.00	17	0.00	17	0.00	17	93.19	29	0.00	28	0.00	17
309	-10	-56	Min.	0.00	0.00	17	0.00	17	0.00	17	96.35	21	-300.03	29	0.00	17
309	-10	-56	Min.	150.00	0.00	17	0.00	17	0.00	17	14.58	21	0.00	17	0.00	17
309	-55	-10	Max	0.00	0.00	17	0.00	17	0.00	17	-14.58	21	0.00	21	0.00	17
309	-55	-10	Max	150.00	0.00	17	0.00	17	0.00	17	-96.35	21	-83.19	21	0.00	17
309	-55	-10	Min.	0.00	0.00	17	0.00	17	0.00	17	-93.19	29	0.00	17	0.00	17
309	-55	-10	Min.	150.00	0.00	17	0.00	17	0.00	17	-306.86	29	-300.03	29	0.00	17
310	-11	-58	Max	0.00	0.00	17	0.00	17	0.00	17	307.48	29	-83.29	21	0.00	17
310	-11	-58	Max	150.00	0.00	17	0.00	17	0.00	17	93.42	29	0.00	22	0.00	17
310	-11	-58	Min.	0.00	0.00	17	0.00	17	0.00	17	96.45	21	-300.68	29	0.00	17
310	-11	-58	Min.	150.00	0.00	17	0.00	17	0.00	17	14.61	21	0.00	28	0.00	17
310	-57	-11	Max	0.00	0.00	17	0.00	17	0.00	17	-14.61	21	0.00	22	0.00	17
310	-57	-11	Max	150.00	0.00	17	0.00	17	0.00	17	-96.45	21	-83.29	21	0.00	17
310	-57	-11	Min.	0.00	0.00	17	0.00	17	0.00	17	-93.42	29	0.00	28	0.00	17
310	-57	-11	Min.	150.00	0.00	17	0.00	17	0.00	17	-307.48	29	-300.68	29	0.00	17
311	-12	-60	Max	0.00	0.00	17	0.00	17	0.00	17	557.65	29	-123.61	21	0.00	17
311	-12	-60	Max	150.00	0.00	17	0.00	17	0.00	17	186.84	29	0.00	21	0.00	17
311	-12	-60	Min.	0.00	0.00	17	0.00	17	0.00	17	135.58	21	-558.38	29	0.00	17
311	-12	-60	Min.	150.00	0.00	17	0.00	17	0.00	17	29.23	21	0.00	17	0.00	17
311	-59	-12	Max	0.00	0.00	17	0.00	17	0.00	17	-29.23	21	0.00	17	0.00	17
311	-59	-12	Max	150.00	0.00	17	0.00	17	0.00	17	-135.58	21	-123.61	21	0.00	17
311	-59	-12	Min.	0.00	0.00	17	0.00	17	0.00	17	-186.84	29	0.00	21	0.00	17
311	-59	-12	Min.	150.00	0.00	17	0.00	17	0.00	17	-557.65	29	-558.38	29	0.00	17
312	-13	-62	Max	0.00	0.00	17	0.00	17	0.00	17	557.65	29	-123.61	21	0.00	17
312	-13	-62	Max	150.00	0.00	17	0.00	17	0.00	17	186.84	29	0.00	21	0.00	17
312	-13	-62	Min.	0.00	0.00	17	0.00	17	0.00	17	135.58	21	-558.38	29	0.00	17
312	-13	-62	Min.	150.00	0.00	17	0.00	17	0.00	17	29.23	21	0.00	17	0.00	17
312	-61	-13	Max	0.00	0.00	17	0.00	17	0.00	17	-29.23	21	0.00	28	0.00	17
312	-61	-13	Max	150.00	0.00	17	0.00	17	0.00	17	-135.58	21	-123.61	21	0.00	17
312	-61	-13	Min.	0.00	0.00	17	0.00	17	0.00	17	-186.84	29	0.00	22	0.00	17
312	-61	-13	Min.	150.00	0.00	17	0.00	17	0.00	17	-557.65	29	-558.38	29	0.00	17
313	-14	-64	Max	0.00	0.00	17	0.00	17	0.00	17	557.65	29	-123.61	21	0.00	17
313	-14	-64	Max	150.00	0.00	17	0.00	17	0.00	17	186.84	29	0.00	21	0.00	17
313	-14	-64	Min.	0.00	0.00	17	0.00	17	0.00	17	135.58	21	-558.38	29	0.00	17
313	-14	-64	Min.	150.00	0.00	17	0.00	17	0.00	17	29.23	21	0.00	17	0.00	17
313	-63	-14	Max	0.00	0.00	17	0.00	17	0.00	17	-29.23	21	0.00	28	0.00	17
313	-63	-14	Max	150.00	0.00	17	0.00	17	0.00	17	-135.58	21	-123.61	21	0.00	17
313	-63	-14	Min.	0.00	0.00	17	0.00	17	0.00	17	-186.84	29	0.00	22	0.00	17
313	-63	-14	Min.	150.00	0.00	17	0.00	17	0.00	17	-557.65	29	-558.38	29	0.00	17
314	-15	-66	Max	0.00	0.00	17	0.00	17	0.00	17	557.65	29	-123.61	21	0.00	17
314	-15	-66	Max	150.00	0.00	17	0.00	17	0.00	17	186.84	29	0.00	21	0.00	17
314	-15	-66	Min.	0.00	0.00	17	0.00	17	0.00	17	135.58	21	-558.38	29	0.00	17
314	-15	-66	Min.	150.00	0.00	17	0.00	17	0.00	17	29.23	21	0.00	17	0.00	17
314	-65	-15	Max	0.00	0.00	17	0.00	17	0.00	17	-29.23	21	0.00	28	0.00	17
314	-65	-15	Max	150.00	0.00	17	0.00	17	0.00	17	-135.58	21	-123.61	21	0.00	17
314	-65	-15	Min.	0.00	0.00	17	0.00	17	0.00	17	-186.84	29	0.00	22	0.00	17
314	-65	-15	Min.	150.00	0.00	17	0.00	17	0.00	17	-557.65	29	-558.38	29	0.00	17
315	203	-67	Max	0.00	0.00	17	0.00	17	0.00	17	580.05	29	-127.22	21	0.00	17
315	203	-67	Max	150.00	0.00	17	0.00	17	0.00	17	195.21	29	0.00	28	0.00	17
315	203	-67	Min.	0.00	0.00	17	0.00	17	0.00	17	139.08	21	-581.45	29	0.00	17
315	203	-67	Min.	150.00	0.00	17	0.00	17	0.00	17	30.54	21	0.00	22	0.00	17
315	-72	203	Max	0.00	0.00	17	0.00	17	0.00	17	-30.54	21	0.00	21	0.00	17
315	-72	203	Max	150.00	0.00	17	0.00	17	0.00	17	-139.08	21	-127.22	21	0.00	17
315	-72	203	Min.	0.00	0.00	17	0.00	17	0.00	17	-195.21	29	0.00	17	0.00	17
315	-72	203	Min.	150.00	0.00	17	0.00	17	0.00	17	-580.05	29	-581.45	29	0.00	17
316	-26	-74	Max	0.00	0.00	17	0.00	17	0.00	17	602.46	29	-130.82	21	0.00	17
316	-26	-74	Max	150.00	0.00	17	0.00	17	0.00	17	203.57	29	0.00	28	0.00	17
316	-26	-74	Min.	0.00	0.00	17	0.00	17	0.00	17	142.59	21	-604.52	29	0.00	17
316	-26	-74	Min.	150.00	0.00	17	0.00	17	0.00	17	31.84	21	0.00	21	0.00	17
316	-73	-26	Max	0.00	0.00	17	0.00	17	0.00	17	-31.85	21	0.00	21	0.00	17
316	-73	-26	Max	150.00	0.00	17	0.00	17	0.00	17	-142.59	21	-130.82	21	0.00	17
316	-73	-26	Min.	0.00	0.00	17	0.00	17	0.00	17	-203.57	29	0.00	29	0.00	17
316	-73	-26	Min.	150.00	0.00	17	0.00	17	0.00	17	-602.46	29	-604.52	29	0.00	17
317	-18	-71	Max	0.00	0.00	17	0.00	17	0.00	17	329.88	29	-86.90	21	0.00	17
317	-18	-71	Max	150.00	0.00	17	0.00	17	0.00	17	101.79	29	0.00	28	0.00	17
317	-18	-71	Min.	0.00	0.00	17	0.00	17	0.00	17	99.95	21	-323.75	29	0.00	17
317	-18	-71	Min.	150.00	0.00	17	0.00	17	0.00	17	15.92	21	0.00	22	0.00	17
317	-70	-18	Max	0.00	0.00	17	0.00	17	0.00	17	-15.92	21	0.00	28	0.00	17
317	-70	-18	Max	150.00	0.00	17	0.00	17	0.00	17	-99.95	21	-86.90	21	0.00	17
317	-70	-18	Min.	0.00	0.00	17	0.00	17	0.00	17	-101.79	29	0.00	22	0.00	17
317	-70	-18	Min.	150.00	0.00	17	0.00	17	0.00	17	-329.88	29	-323.75	29	0.00	17

Tipo di combinazione di carico: SLE R

Asta	N1	N2	X	N	CC Ty	CC Mz	CC Tz	CC My	CC Mx	CC						
			<cm>	<daN>	<daN>	<daNm>	<daN>	<daNm>	<daNm>							
1	315	-45	Max	0.00	-1567.70	23	-42.43	23	175.78	31	0.00	31	0.00	31	0.00	30
1	315	-45	Max	330.00	-1378.46	23	-42.43	23	-104.80	23	0.00	31	0.00	31	0.00	30
1	315	-45	Min.	0.00	-4511.98	31	-194.97	31	35.22	23	0.00	23	0.00	23	0.00	23
1	315	-45	Min.	330.00	-4322.74	31	-194.97	31	-467.61	31	0.00	23	0.00	23	0.00	23
2	2	202	Max	0.00	-16											



305	-47	-6	Max	0.00	0.00	18	0.00	18	0.00	18	-19.44	23	0.00	30	0.00	18
305	-47	-6	Max	150.00	0.00	18	0.00	18	0.00	18	-96.13	23	-86.68	23	0.00	18
305	-47	-6	Min.	0.00	0.00	18	0.00	18	0.00	18	-124.25	31	0.00	24	0.00	18
305	-47	-6	Min.	150.00	0.00	18	0.00	18	0.00	18	-376.81	31	-375.80	31	0.00	18
306	-7	-50	Max	0.00	0.00	18	0.00	18	0.00	18	376.81	31	-86.68	23	0.00	18
306	-7	-50	Max	150.00	0.00	18	0.00	18	0.00	18	124.25	31	0.00	30	0.00	18
306	-7	-50	Min.	0.00	0.00	18	0.00	18	0.00	18	96.13	23	-375.80	31	0.00	18
306	-7	-50	Min.	150.00	0.00	18	0.00	18	0.00	18	19.44	23	0.00	18	0.00	18
306	-49	-7	Max	0.00	0.00	18	0.00	18	0.00	18	-19.44	23	0.00	23	0.00	18
306	-49	-7	Max	150.00	0.00	18	0.00	18	0.00	18	-96.13	23	-86.68	23	0.00	18
306	-49	-7	Min.	0.00	0.00	18	0.00	18	0.00	18	-124.25	31	0.00	30	0.00	18
306	-49	-7	Min.	150.00	0.00	18	0.00	18	0.00	18	-376.81	31	-375.80	31	0.00	18
307	-8	-52	Max	0.00	0.00	18	0.00	18	0.00	18	376.81	31	-86.68	23	0.00	18
307	-8	-52	Max	150.00	0.00	18	0.00	18	0.00	18	124.25	31	0.00	30	0.00	18
307	-8	-52	Min.	0.00	0.00	18	0.00	18	0.00	18	96.13	23	-375.80	31	0.00	18
307	-8	-52	Min.	150.00	0.00	18	0.00	18	0.00	18	19.44	23	0.00	18	0.00	18
307	-51	-8	Max	0.00	0.00	18	0.00	18	0.00	18	-19.44	23	0.00	18	0.00	18
307	-51	-8	Max	150.00	0.00	18	0.00	18	0.00	18	-96.13	23	-86.68	23	0.00	18
307	-51	-8	Min.	0.00	0.00	18	0.00	18	0.00	18	-124.25	31	0.00	23	0.00	18
307	-51	-8	Min.	150.00	0.00	18	0.00	18	0.00	18	-376.81	31	-375.80	31	0.00	18
308	-9	-54	Max	0.00	0.00	18	0.00	18	0.00	18	376.81	31	-86.68	23	0.00	18
308	-9	-54	Max	150.00	0.00	18	0.00	18	0.00	18	124.25	31	0.00	30	0.00	18
308	-9	-54	Min.	0.00	0.00	18	0.00	18	0.00	18	96.13	23	-375.80	31	0.00	18
308	-9	-54	Min.	150.00	0.00	18	0.00	18	0.00	18	19.44	23	0.00	23	0.00	18
308	-53	-9	Max	0.00	0.00	18	0.00	18	0.00	18	-19.44	23	0.00	30	0.00	18
308	-53	-9	Max	150.00	0.00	18	0.00	18	0.00	18	-96.13	23	-86.68	23	0.00	18
308	-53	-9	Min.	0.00	0.00	18	0.00	18	0.00	18	-124.25	31	0.00	24	0.00	18
308	-53	-9	Min.	150.00	0.00	18	0.00	18	0.00	18	-376.81	31	-375.80	31	0.00	18
309	-10	-56	Max	0.00	0.00	18	0.00	18	0.00	18	210.45	31	-59.87	23	0.00	18
309	-10	-56	Max	150.00	0.00	18	0.00	18	0.00	18	62.13	31	0.00	30	0.00	18
309	-10	-56	Min.	0.00	0.00	18	0.00	18	0.00	18	70.11	23	-204.43	31	0.00	18
309	-10	-56	Min.	150.00	0.00	18	0.00	18	0.00	18	89.72	23	0.00	18	0.00	18
309	-55	-10	Max	0.00	0.00	18	0.00	18	0.00	18	-9.72	23	0.00	23	0.00	18
309	-55	-10	Max	150.00	0.00	18	0.00	18	0.00	18	-70.11	23	-59.87	23	0.00	18
309	-55	-10	Min.	0.00	0.00	18	0.00	18	0.00	18	-62.13	31	0.00	18	0.00	18
309	-55	-10	Min.	150.00	0.00	18	0.00	18	0.00	18	-210.45	31	-204.43	31	0.00	18
310	-11	-58	Max	0.00	0.00	18	0.00	18	0.00	18	210.87	31	-59.94	23	0.00	18
310	-11	-58	Max	150.00	0.00	18	0.00	18	0.00	18	62.28	31	0.00	24	0.00	18
310	-11	-58	Min.	0.00	0.00	18	0.00	18	0.00	18	70.17	23	-204.86	31	0.00	18
310	-11	-58	Min.	150.00	0.00	18	0.00	18	0.00	18	89.74	23	0.00	30	0.00	18
310	-57	-11	Max	0.00	0.00	18	0.00	18	0.00	18	-9.74	23	0.00	24	0.00	18
310	-57	-11	Max	150.00	0.00	18	0.00	18	0.00	18	-70.17	23	-59.94	23	0.00	18
310	-57	-11	Min.	0.00	0.00	18	0.00	18	0.00	18	-62.28	31	0.00	30	0.00	18
310	-57	-11	Min.	150.00	0.00	18	0.00	18	0.00	18	-210.87	31	-204.86	31	0.00	18
311	-12	-60	Max	0.00	0.00	18	0.00	18	0.00	18	377.65	31	-86.81	23	0.00	18
311	-12	-60	Max	150.00	0.00	18	0.00	18	0.00	18	124.56	31	0.00	23	0.00	18
311	-12	-60	Min.	0.00	0.00	18	0.00	18	0.00	18	96.26	23	-376.66	31	0.00	18
311	-12	-60	Min.	150.00	0.00	18	0.00	18	0.00	18	19.49	23	0.00	18	0.00	18
311	-59	-12	Max	0.00	0.00	18	0.00	18	0.00	18	-19.49	23	0.00	18	0.00	18
311	-59	-12	Max	150.00	0.00	18	0.00	18	0.00	18	-96.26	23	-86.81	23	0.00	18
311	-59	-12	Min.	0.00	0.00	18	0.00	18	0.00	18	-124.56	31	0.00	23	0.00	18
311	-59	-12	Min.	150.00	0.00	18	0.00	18	0.00	18	-377.65	31	-376.66	31	0.00	18
312	-13	-62	Max	0.00	0.00	18	0.00	18	0.00	18	377.65	31	-86.81	23	0.00	18
312	-13	-62	Max	150.00	0.00	18	0.00	18	0.00	18	124.56	31	0.00	23	0.00	18
312	-13	-62	Min.	0.00	0.00	18	0.00	18	0.00	18	96.26	23	-376.66	31	0.00	18
312	-13	-62	Min.	150.00	0.00	18	0.00	18	0.00	18	19.49	23	0.00	18	0.00	18
312	-61	-13	Max	0.00	0.00	18	0.00	18	0.00	18	-19.49	23	0.00	30	0.00	18
312	-61	-13	Max	150.00	0.00	18	0.00	18	0.00	18	-96.26	23	-86.81	23	0.00	18
312	-61	-13	Min.	0.00	0.00	18	0.00	18	0.00	18	-124.56	31	0.00	24	0.00	18
312	-61	-13	Min.	150.00	0.00	18	0.00	18	0.00	18	-377.65	31	-376.66	31	0.00	18
313	-14	-64	Max	0.00	0.00	18	0.00	18	0.00	18	377.65	31	-86.81	23	0.00	18
313	-14	-64	Max	150.00	0.00	18	0.00	18	0.00	18	124.56	31	0.00	23	0.00	18
313	-14	-64	Min.	0.00	0.00	18	0.00	18	0.00	18	96.26	23	-376.66	31	0.00	18
313	-14	-64	Min.	150.00	0.00	18	0.00	18	0.00	18	19.49	23	0.00	18	0.00	18
313	-63	-14	Max	0.00	0.00	18	0.00	18	0.00	18	-19.49	23	0.00	30	0.00	18
313	-63	-14	Max	150.00	0.00	18	0.00	18	0.00	18	-96.26	23	-86.81	23	0.00	18
313	-63	-14	Min.	0.00	0.00	18	0.00	18	0.00	18	-124.56	31	0.00	24	0.00	18
313	-63	-14	Min.	150.00	0.00	18	0.00	18	0.00	18	-377.65	31	-376.66	31	0.00	18
314	-15	-66	Max	0.00	0.00	18	0.00	18	0.00	18	377.65	31	-86.81	23	0.00	18
314	-15	-66	Max	150.00	0.00	18	0.00	18	0.00	18	124.56	31	0.00	23	0.00	18
314	-15	-66	Min.	0.00	0.00	18	0.00	18	0.00	18	96.26	23	-376.66	31	0.00	18
314	-15	-66	Min.	150.00	0.00	18	0.00	18	0.00	18	19.49	23	0.00	18	0.00	18
314	-65	-15	Max	0.00	0.00	18	0.00	18	0.00	18	-19.49	23	0.00	30	0.00	18
314	-65	-15	Max	150.00	0.00	18	0.00	18	0.00	18	-96.26	23	-86.81	23	0.00	18
314	-65	-15	Min.	0.00	0.00	18	0.00	18	0.00	18	-124.56	31	0.00	24	0.00	18
314	-65	-15	Min.	150.00	0.00	18	0.00	18	0.00	18	-377.65	31	-376.66	31	0.00	18
315	203	-67	Max	0.00	0.00	18	0.00	18	0.00	18	392.58	31	-89.22	23	0.00	18
315	203	-67	Max	150.00	0.00	18	0.00	18	0.00	18	130.14	31	0.00	30	0.00	18
315	203	-67	Min.	0.00	0.00	18	0.00	18	0.00	18	98.60	23	-392.04	31	0.00	18
315	203	-67	Min.	150.00	0.00	18	0.00	18	0.00	18	20.36	23	0.00	24	0.00	18
315	-72	203	Max	0.00	0.00	18	0.00	18	0.00	18	-20.36	23	0.00	23	0.00	18
315	-72	203	Max	150.00	0.00	18	0.00	18	0.00	18	-98.60	23	-89.22	23	0.00	18
315	-72	203	Min.	0.00	0.00	18	0.00	18	0.00	18	-130.14	31	0.00	18	0.00	18
315	-72	203	Min.	150.00	0.00	18	0.00	18	0.00	18	-392.58	31	-392.04	31	0.00	18
316	-26	-74	Max	0.00	0.00	18	0.00	18	0.00	18	407.51	31	-91.62	23	0.00	18
316	-26	-74	Max	150.00	0.00	18	0.00	18	0.00	18	135.72	31				

Foggia Solar S.r.l.



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204	203	-26	Min.	0.00	0.00	20	0.00	20	0.00	20	524.01	20	-986.83	20	0.00	20
204	203	-26	Min.	144.80	0.00	20	0.00	20	0.00	20	454.17	20	-278.62	20	0.00	20
204	-26	-18	Max	0.00	0.00	20	0.00	20	0.00	20	227.34	20	-278.62	20	0.00	20
204	-26	-18	Max	144.80	0.00	20	0.00	20	0.00	20	157.50	20	0.00	20	0.00	20
204	-26	-18	Min.	0.00	0.00	20	0.00	20	0.00	20	227.34	20	-278.62	20	0.00	20
204	-26	-18	Min.	144.80	0.00	20	0.00	20	0.00	20	157.50	20	0.00	20	0.00	20
301	-45	-79	Max	0.00	0.00	20	0.00	20	0.00	20	110.49	20	-101.46	20	0.00	20
301	-45	-79	Max	150.00	0.00	20	0.00	20	0.00	20	24.80	20	0.00	20	0.00	20
301	-45	-79	Min.	0.00	0.00	20	0.00	20	0.00	20	110.49	20	-101.46	20	0.00	20
301	-45	-79	Min.	150.00	0.00	20	0.00	20	0.00	20	24.80	20	0.00	20	0.00	20
301	-80	-45	Max	0.00	0.00	20	0.00	20	0.00	20	-24.80	20	0.00	20	0.00	20
301	-80	-45	Max	150.00	0.00	20	0.00	20	0.00	20	-110.49	20	-101.46	20	0.00	20
301	-80	-45	Min.	0.00	0.00	20	0.00	20	0.00	20	-24.80	20	0.00	20	0.00	20
301	-80	-45	Min.	150.00	0.00	20	0.00	20	0.00	20	-110.49	20	-101.46	20	0.00	20
302	-3	-69	Max	0.00	0.00	20	0.00	20	0.00	20	78.75	20	-68.77	20	0.00	20
302	-3	-69	Max	150.00	0.00	20	0.00	20	0.00	20	12.95	20	0.00	20	0.00	20
302	-3	-69	Min.	0.00	0.00	20	0.00	20	0.00	20	78.75	20	-68.77	20	0.00	20
302	-3	-69	Min.	150.00	0.00	20	0.00	20	0.00	20	12.95	20	0.00	20	0.00	20
302	-68	-3	Max	0.00	0.00	20	0.00	20	0.00	20	-12.95	20	0.00	20	0.00	20
302	-68	-3	Max	150.00	0.00	20	0.00	20	0.00	20	-78.75	20	-68.77	20	0.00	20
302	-68	-3	Min.	0.00	0.00	20	0.00	20	0.00	20	-12.95	20	0.00	20	0.00	20
302	-68	-3	Min.	150.00	0.00	20	0.00	20	0.00	20	-78.75	20	-68.77	20	0.00	20
303	-29	-76	Max	0.00	0.00	20	0.00	20	0.00	20	113.42	20	-104.48	20	0.00	20
303	-29	-76	Max	150.00	0.00	20	0.00	20	0.00	20	25.89	20	0.00	20	0.00	20
303	-29	-76	Min.	0.00	0.00	20	0.00	20	0.00	20	113.42	20	-104.48	20	0.00	20
303	-29	-76	Min.	150.00	0.00	20	0.00	20	0.00	20	25.89	20	0.00	20	0.00	20
303	-75	-29	Max	0.00	0.00	20	0.00	20	0.00	20	-25.89	20	0.00	20	0.00	20
303	-75	-29	Max	150.00	0.00	20	0.00	20	0.00	20	-113.42	20	-104.48	20	0.00	20
303	-75	-29	Min.	0.00	0.00	20	0.00	20	0.00	20	-25.89	20	0.00	20	0.00	20
303	-75	-29	Min.	150.00	0.00	20	0.00	20	0.00	20	-113.42	20	-104.48	20	0.00	20
304	201	-77	Max	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
304	201	-77	Max	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
304	201	-77	Min.	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
304	201	-77	Min.	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
304	-78	201	Max	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
304	-78	201	Max	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
304	-78	201	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
304	-78	201	Min.	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
305	-6	-48	Max	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
305	-6	-48	Max	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
305	-6	-48	Min.	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
305	-6	-48	Min.	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
305	-47	-6	Max	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
305	-47	-6	Max	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
305	-47	-6	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
305	-47	-6	Min.	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
306	-7	-50	Max	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
306	-7	-50	Max	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
306	-7	-50	Min.	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
306	-7	-50	Min.	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
306	-49	-7	Max	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
306	-49	-7	Max	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
306	-49	-7	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
306	-49	-7	Min.	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
307	-8	-52	Max	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
307	-8	-52	Max	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
307	-8	-52	Min.	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
307	-8	-52	Min.	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
307	-51	-8	Max	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
307	-51	-8	Max	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
307	-51	-8	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
307	-51	-8	Min.	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
308	-9	-54	Max	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
308	-9	-54	Max	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
308	-9	-54	Min.	0.00	0.00	20	0.00	20	0.00	20	107.56	20	-98.45	20	0.00	20
308	-9	-54	Min.	150.00	0.00	20	0.00	20	0.00	20	23.70	20	0.00	20	0.00	20
308	-53	-9	Max	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
308	-53	-9	Max	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
308	-53	-9	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.70	20	0.00	20	0.00	20
308	-53	-9	Min.	150.00	0.00	20	0.00	20	0.00	20	-107.56	20	-98.45	20	0.00	20
309	-10	-56	Max	0.00	0.00	20	0.00	20	0.00	20	75.82	20	-65.76	20	0.00	20
309	-10	-56	Max	150.00	0.00	20	0.00	20	0.00	20	11.85	20	0.00	20	0.00	20
309	-10	-56	Min.	0.00	0.00	20	0.00	20	0.00	20	75.82	20	-65.76	20	0.00	20
309	-10	-56	Min.	150.00	0.00	20	0.00	20	0.00	20	11.85	20	0.00	20	0.00	20
309	-55	-10	Max	0.00	0.00	20	0.00	20	0.00	20	-11.85	20	0.00	20	0.00	20
309	-55	-10	Max	150.00	0.00	20	0.00	20	0.00	20	-75.82	20	-65.76	20	0.00	20
309	-55	-10	Min.	0.00	0.00	20	0.00	20	0.00	20	-11.85	20	0.00	20	0.00	20
309	-55	-10	Min.	150.00	0.00	20	0.00	20	0.00	20	-75.82	20	-65.76	20	0.00	20
310	-11	-58	Max	0.00	0.00	20	0.00	20	0.00	20	75.90	20	-65.84	20	0.00	20
310	-11	-58	Max	150.00	0.00	20	0.00	20	0.00	20	11.88	20	0.00	20	0.00	20
310	-11	-58	Min.	0.00	0.00	20	0.00	20	0.00	20	75.90	20	-65.84	20	0.00	20
310	-11	-58	Min.	150.00	0.00	20	0.00	20	0.00	20	11.88	20	0.00	20	0.00	20
310	-57	-11	Max	0.00	0.00	20	0.00	20	0.00	20	-11.88	20	0.00	20	0.00	20
310	-57	-11	Max	150.00	0.00	20	0.00	20	0.00	20	-75.90	20	-65.84	20	0.00	20
310	-57	-11	Min.	0.00	0.00	20	0.00	20	0.00	20	-11.88	20	0.00	20	0.00	20
310	-57	-11	Min.	150.00	0.00	20	0.00	20	0.00	20	-75.90	20	-65.84	20	0.00	20
311	-12	-60	Max	0.00	0.00	20	0.00	20	0.00	20	107.72	20	-98.61</			



312	-61	-13	Min.	150.00	0.00	20	0.00	20	0.00	20	-107.72	20	-98.61	20	0.00	20
313	-14	-64	Max	0.00	0.00	20	0.00	20	0.00	20	107.72	20	-98.61	20	0.00	20
313	-14	-64	Max	150.00	0.00	20	0.00	20	0.00	20	23.76	20	0.00	20	0.00	20
313	-14	-64	Min.	0.00	0.00	20	0.00	20	0.00	20	107.72	20	-98.61	20	0.00	20
313	-14	-64	Min.	150.00	0.00	20	0.00	20	0.00	20	23.76	20	0.00	20	0.00	20
313	-63	-14	Max	0.00	0.00	20	0.00	20	0.00	20	-23.76	20	0.00	20	0.00	20
313	-63	-14	Max	150.00	0.00	20	0.00	20	0.00	20	-107.72	20	-98.61	20	0.00	20
313	-63	-14	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.76	20	0.00	20	0.00	20
313	-63	-14	Min.	150.00	0.00	20	0.00	20	0.00	20	-107.72	20	-98.61	20	0.00	20
314	-15	-66	Max	0.00	0.00	20	0.00	20	0.00	20	107.72	20	-98.61	20	0.00	20
314	-15	-66	Max	150.00	0.00	20	0.00	20	0.00	20	23.76	20	0.00	20	0.00	20
314	-15	-66	Min.	0.00	0.00	20	0.00	20	0.00	20	107.72	20	-98.61	20	0.00	20
314	-15	-66	Min.	150.00	0.00	20	0.00	20	0.00	20	23.76	20	0.00	20	0.00	20
314	-65	-15	Max	0.00	0.00	20	0.00	20	0.00	20	-23.76	20	0.00	20	0.00	20
314	-65	-15	Max	150.00	0.00	20	0.00	20	0.00	20	-107.72	20	-98.61	20	0.00	20
314	-65	-15	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.76	20	0.00	20	0.00	20
314	-65	-15	Min.	150.00	0.00	20	0.00	20	0.00	20	-107.72	20	-98.61	20	0.00	20
315	203	-67	Max	0.00	0.00	20	0.00	20	0.00	20	110.57	20	-101.55	20	0.00	20
315	203	-67	Max	150.00	0.00	20	0.00	20	0.00	20	24.83	20	0.00	20	0.00	20
315	203	-67	Min.	0.00	0.00	20	0.00	20	0.00	20	110.57	20	-101.55	20	0.00	20
315	203	-67	Min.	150.00	0.00	20	0.00	20	0.00	20	24.83	20	0.00	20	0.00	20
315	-72	203	Max	0.00	0.00	20	0.00	20	0.00	20	-24.83	20	0.00	20	0.00	20
315	-72	203	Max	150.00	0.00	20	0.00	20	0.00	20	-110.57	20	-101.55	20	0.00	20
315	-72	203	Min.	0.00	0.00	20	0.00	20	0.00	20	-24.83	20	0.00	20	0.00	20
315	-72	203	Min.	150.00	0.00	20	0.00	20	0.00	20	-110.57	20	-101.55	20	0.00	20
316	-26	-74	Max	0.00	0.00	20	0.00	20	0.00	20	113.42	20	-104.48	20	0.00	20
316	-26	-74	Max	150.00	0.00	20	0.00	20	0.00	20	25.89	20	0.00	20	0.00	20
316	-26	-74	Min.	0.00	0.00	20	0.00	20	0.00	20	113.42	20	-104.48	20	0.00	20
316	-26	-74	Min.	150.00	0.00	20	0.00	20	0.00	20	25.89	20	0.00	20	0.00	20
316	-73	-26	Max	0.00	0.00	20	0.00	20	0.00	20	-25.89	20	0.00	20	0.00	20
316	-73	-26	Max	150.00	0.00	20	0.00	20	0.00	20	-113.42	20	-104.48	20	0.00	20
316	-73	-26	Min.	0.00	0.00	20	0.00	20	0.00	20	-25.89	20	0.00	20	0.00	20
316	-73	-26	Min.	150.00	0.00	20	0.00	20	0.00	20	-113.42	20	-104.48	20	0.00	20
317	-18	-71	Max	0.00	0.00	20	0.00	20	0.00	20	78.75	20	-68.77	20	0.00	20
317	-18	-71	Max	150.00	0.00	20	0.00	20	0.00	20	12.95	20	0.00	20	0.00	20
317	-18	-71	Min.	0.00	0.00	20	0.00	20	0.00	20	78.75	20	-68.77	20	0.00	20
317	-18	-71	Min.	150.00	0.00	20	0.00	20	0.00	20	12.95	20	0.00	20	0.00	20
317	-70	-18	Max	0.00	0.00	20	0.00	20	0.00	20	-12.95	20	0.00	20	0.00	20
317	-70	-18	Max	150.00	0.00	20	0.00	20	0.00	20	-78.75	20	-68.77	20	0.00	20
317	-70	-18	Min.	0.00	0.00	20	0.00	20	0.00	20	-12.95	20	0.00	20	0.00	20
317	-70	-18	Min.	150.00	0.00	20	0.00	20	0.00	20	-78.75	20	-68.77	20	0.00	20

Verifiche aste in acciaio

Simbologia

Φ_{LT}	=	Coefficiente Φ per stabilità laterale membrature inflesse
Φ_y	=	Coefficiente Φ per inflessione intorno all'asse y(c)
Φ_z	=	Coefficiente Φ per inflessione intorno all'asse z(e)
α_{imp}	=	Coefficiente di imperfezione
$\alpha_{my}, \alpha_{mz}, \alpha_{LT}$	=	Coefficienti correttivi per il momento flettente
β_{LT}	=	Coefficiente per calcolo Φ_{LT}
χ_{LT}	=	Coefficiente di riduzione per stabilità laterale membrature inflesse
χ_y	=	Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
χ_z	=	Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
δ	<cm>	=Spostamento relativo asta
λ_y^*	=	Snellezza adimensionale per inflessione intorno all'asse y(c)
λ_z^*	=	Snellezza adimensionale per inflessione intorno all'asse z(e)
λ_{LT}	=	Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$	=	Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
λ_y	=	Snellezza per inflessione intorno all'asse y(c)
λ_z	=	Snellezza per inflessione intorno all'asse z(e)
$\sigma_{D,max}$	<daN/cm²>	=Tensione ideale massima
σ_N	<daN/cm²>	=Tensione normale per momento flettente
σ_N	<daN/cm²>	=Tensione normale per sforzo normale
τ	<daN/cm²>	=Tensione tangenziale per taglio e/o torsione
ψ	=	Coeff. di correzione momento critico per stabilità laterale membrature inflesse
A_{eff}	<cm²>	=Area effettiva per trazione
A_{net}	<cm²>	=Area netta per compressione
A_{area}	<cm²>	=Area
$A_{tag,y}$	<cm²>	=Area resistente a taglio in dir. Y
$A_{tag,z}$	<cm²>	=Area resistente a taglio in dir. Z
CC	=	Numero della combinazione delle condizioni di carico elementari
Cod.	=	Codice
Curva	=	Curva di instabilità adottata
D	<cm>	=Distanza
F_{yk}	<daN/cm²>	=Tensione caratteristica di snervamento dell'acciaio
F_{yt}	<daN/cm²>	=Tensione caratteristica di rottura
I_y	<cm⁴>	=Raggio giratorio d'inerzia rispetto all'asse Y
I_z	<cm⁴>	=Raggio giratorio d'inerzia rispetto all'asse Z
$J\theta$	<cm⁶>	=Costante di ingobbamento
J_y	<cm⁴>	=Momento d'inerzia rispetto all'asse Y
J_z	<cm⁴>	=Momento d'inerzia rispetto all'asse Z
$K_{yy}, K_{yz}, K_{zy}, K_{zz}$	=	Coefficienti di interazione
L	<m>	=Lunghezza dell'asta
L_{cr}	<m>	=Lunghezza di libera inflessione laterale fra ritegni torsionali
M, cr	<daNm>	=Momento critico per instabilità flesso torsionale
M_{Ny}, c, R_d	<daNm>	=Resistenza di calcolo a pressoflessione intorno all'asse Y
M_{Nz}, c, R_d	<daNm>	=Resistenza di calcolo a pressoflessione intorno all'asse Z
M_x	<daNm>	=Momento torcente intorno all'asse X
M_y	<daNm>	=Momento flettente intorno all'asse Y
M_y, Ed	<daNm>	=Momento flettente di calcolo intorno all'asse Y
M_y, V, c, R_d	<daNm>	=Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y
M_z	<daNm>	=Momento flettente intorno all'asse Z
M_z, Ed	<daNm>	=Momento flettente di calcolo intorno all'asse Z
M_z, V, c, R_d	<daNm>	=Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Z
N	<daN>	=Sforzo normale
N, Ed	<daN>	=Forza assiale di calcolo
Nc, Rd	<daN>	=Resistenza a compressione
Ncr, y	<daN>	=Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
Ncr, z	<daN>	=Sforzo normale critico euleriano per inflessione intorno all'asse z(e)



Sez. = Numero della sezione
 Tipo = Tipologia
 Rc = Rettangolare cava
 Is = I stondata
 Tp = Tipo di acciaio
 Ty <daN> = Taglio in dir. Y
 Tz <daN> = Taglio in dir. Z
 V,Ed <daN> = Forza di taglio di calcolo
 Vc,Rd <daN> = Resistenza a taglio
 Wy,plac <cmc> = Modulo di resistenza plastico intorno all'asse Y
 Wymn <cmc> = Modulo di resistenza minimo rispetto all'asse Y
 Wz,plac <cmc> = Modulo di resistenza plastico intorno all'asse Z
 Wzmn <cmc> = Modulo di resistenza minimo rispetto all'asse Z
 X1 <cm> = Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
 f = Fattore di modifica per il coefficiente di riduzione
 fz,g <cm> = Freccia in direzione Z globale
 fz,l <cm> = Freccia in direzione Z locale
 kc = Coeff. di correzione momento flettente per stabilit  laterale membrature inflesse

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D	Area	Anet	Aeff	Jy	Jz	Iy	Iz	Wymn	Wzmn	Tp	Fyk	Fyt
				<cm>	<cmq>	<cmq>	<cm4>	<cm4>	<cm>	<cm>	<cm>	<cm>		<daN/cm>	<daN/cm>
1	TRV SEC RHS150x100x8	Rc	--	37.44	37.44	37.44	1128.23	588.15	5.49	3.96	150.43	117.63	S355H UNI EN 10210-1	3550.00	5100.00
2	COL HEA240	Is	--	76.84	76.84	76.84	7763.40	2768.81	10.05	6.00	675.08	230.73	S355 UNI EN 10025-2	3550.00	5100.00
3	TRV PRINC SHS200x200x8	Rc	--	61.44	61.44	61.44	3781.43	3781.43	7.85	7.85	378.14	378.14	S355H UNI EN 10210-1	3550.00	5100.00

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy,plac	Wz,plac	Atag,y	Atag,z	Jw
		<cmc>	<cmc>	<cmq>	<cmq>	<cm6>
1	TRV SEC RHS150x100x8	185.42	138.62	14.98	22.46	
2	COL HEA240	747.99	352.10	64.54	25.18	328486.00
3	TRV PRINC SHS200x200x8	442.62	442.62	30.72	30.72	

Asta n. 1 (315 -45) - Sez. 2 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-1876.44 Tz=-246.68 My=-815.49 Ty=-755.60 Mz=1518.31
 Tensioni: $\sigma_N=-24.42$ $\sigma_{m,d}=-778.83$ $\tau=0.00$ $\sigma_{max}=-803.25$ (sfrut=0.24)
 Tensioni: $\sigma_N=-24.42$ $\sigma_{m,d}=243.91$ $\tau=18.92$ $\tau_{max}=18.92$ (sfrut=0.01)
 Tensioni: $\sigma_N=-24.42$ $\sigma_{m,d}=-778.83$ $\tau=0.00$ $\sigma_{ID,max}=803.25$ (sfrut=0.24)

- Verifica a taglio Dir. Y [4.2.16] - CC 29 SLU X1=0.00 - Classe 2
 Sollecitazioni: Ty=-289.62
 V,Ed=-289.62 Vc,Rd=125981.00 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU X1=3.30 - Classe 2
 Sollecitazioni: N=-6317.61 Ty=-289.62 Mz=-693.90
 Mz,Ed=-693.90 Mz,V,c,Rd=11904.20
 N,Ed=-6317.61 Nc,Rd=-259785.00 ZZ n=N,Ed/Nc,Rd=0.02 MNz,c,Rd=11904.20 Mz,Ed/MNz,c,Rd=0.06

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3
 Sollecitazioni: N,Ed=-1876.44 My,Ed=-815.49 Mz,Ed=1518.31 L=3.30
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 Lcr=3.30 Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.75$ M,cr=122159.00 $\lambda_{LT}=0.44$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.58$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.03+0.19=0.23
 Verifica ZZ: 0.01+0.03+0.19=0.22

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.05$ (L/6377)

Asta n. 2 (2 202) - Sez. 2 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 3 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-1725.88 Tz=-259.81 My=-850.11 Ty=1087.85 Mz=-1904.54
 Tensioni: $\sigma_N=-22.46$ $\sigma_{m,d}=-951.35$ $\tau=0.00$ $\sigma_{max}=-973.81$ (sfrut=0.29)
 Tensioni: $\sigma_N=-22.46$ $\sigma_{m,d}=-57.46$ $\tau=27.17$ $\tau_{max}=27.17$ (sfrut=0.01)
 Tensioni: $\sigma_N=-22.46$ $\sigma_{m,d}=-951.35$ $\tau=0.00$ $\sigma_{ID,max}=973.81$ (sfrut=0.29)

- Verifica a taglio Dir. Y [4.2.16] - CC 29 SLU X1=0.00 - Classe 2
 Sollecitazioni: Ty=450.59
 V,Ed=450.59 Vc,Rd=125981.00 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU X1=3.30 - Classe 2
 Sollecitazioni: N=-6586.97 Ty=450.59 Mz=942.17
 Mz,Ed=942.17 Mz,V,c,Rd=11904.20
 N,Ed=-6586.97 Nc,Rd=-259785.00 ZZ n=N,Ed/Nc,Rd=0.03 MNz,c,Rd=11904.20 Mz,Ed/MNz,c,Rd=0.08

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-1725.88 My,Ed=-850.11 Mz,Ed=-1904.54 L=3.30
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 Lcr=3.30 Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.76$ M,cr=122920.00 $\lambda_{LT}=0.44$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.58$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.01+0.04+0.23=0.27
 Verifica ZZ: 0.01+0.03+0.23=0.27

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.06$ (L/5166)

Asta n. 3 (3 203) - Sez. 2 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-1291.33 Tz=-225.48 My=-749.93 Ty=-806.48 Mz=1573.13
 Tensioni: $\sigma_N=-16.81$ $\sigma_{m,d}=-792.88$ $\tau=0.00$ $\sigma_{max}=-809.68$ (sfrut=0.24)
 Tensioni: $\sigma_N=-16.81$ $\sigma_{m,d}=240.12$ $\tau=20.16$ $\tau_{max}=20.16$ (sfrut=0.01)

Tensioni: $\sigma_N=-16.81$ $\sigma_{m,d}=-792.88$ $\tau=0.00$ $\sigma_{ID,max}=809.68$ (sfrut=0.24)

- Verifica a taglio Dir. Y [4.2.16] - CC 11 SND X1=1.80 - Classe 2
Sollecitazioni: $T_y=-281.40$
 $V,Ed=-281.40$ $V_c,Rd=125981.00$ $V,Ed/V_c,Rd=0.00$
- Verifica a taglio Dir. Z [4.2.16] - CC 11 SND X1=1.80 - Classe 2
Sollecitazioni: $T_z=751.62$
 $V,Ed=751.62$ $V_c,Rd=49148.50$ $V,Ed/V_c,Rd=0.02$
- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU X1=3.30 - Classe 2
Sollecitazioni: $N=-5701.22$ $T_y=-160.97$ $M_z=-408.86$
 $M_z,Ed=-408.86$ $M_z,V,c,Rd=11904.20$
 $N,Ed=-5701.22$ $N_c,Rd=-259785.00$ ZZ $n=N,Ed/N_c,Rd=0.02$ MNz,c,Rd=11904.20 $M_z,Ed/MNz,c,Rd=0.03$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3
Sollecitazioni: $N,Ed=-1291.33$ $M_y,Ed=-749.93$ $M_z,Ed=1573.13$ $L=3.30$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $L_{cr}=3.30$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.74$ $M,cr=121721.00$ $\lambda_{LT}=0.44$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.58$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.19=0.23
Verifica ZZ: 0.00+0.03+0.19=0.22
- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.04$ (L/8176)

Asta n. 201 (-3 -29) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND X1=1.45 - Classe 3
Sollecitazioni: $N=-29.73$ $T_x=-227.34$ $M_y=278.62$ $T_y=99.09$ $M_z=143.48$
Tensioni: $\sigma_N=-0.48$ $\sigma_{m,d}=-111.62$ $\tau=0.00$ $\sigma_{max}=-112.11$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.48$ $\sigma_{m,d}=34.91$ $\tau=8.32$ $\tau_{max}=8.32$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.48$ $\sigma_{m,d}=-111.62$ $\tau=0.00$ $\sigma_{ID,max}=112.11$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.45 - Classe 1
Sollecitazioni: $T_z=-750.56$
 $V,Ed=-750.56$ $V_c,Rd=59967.00$ $V,Ed/V_c,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.45 - Classe 1
Sollecitazioni: $T_x=-750.56$ $M_y=1021.08$
 $M_y,Ed=1021.08$ $M_y,V,c,Rd=14964.90$ $M_y,Ed/M_y,V,c,Rd=0.07$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: $N,Ed=-29.73$ $M_y,Ed=278.62$ $M_z,Ed=143.48$ $L=1.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=18.46$ Ncr,y=3737980.00 $\lambda'_y=0.24$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=18.46$ Ncr,z=3737980.00 $\lambda'_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 201 (-29 -45) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND X1=1.45 - Classe 3
Sollecitazioni: $N=75.56$ $T_x=-524.01$ $M_y=986.83$ $T_y=251.86$ $M_z=508.17$
Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=395.35$ $\tau=0.00$ $\sigma_{max}=396.58$ (sfrut=0.12)
Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=123.63$ $\tau=19.17$ $\tau_{max}=19.17$ (sfrut=0.01)
Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=395.35$ $\tau=0.00$ $\sigma_{ID,max}=396.58$ (sfrut=0.12)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.45 - Classe 1
Sollecitazioni: $T_z=-2046.26$
 $V,Ed=-2046.26$ $V_c,Rd=59967.00$ $V,Ed/V_c,Rd=0.03$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.45 - Classe 1
Sollecitazioni: $T_x=-2046.26$ $M_y=3918.33$
 $M_y,Ed=3918.33$ $M_y,V,c,Rd=14964.90$ $M_y,Ed/M_y,V,c,Rd=0.26$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: $N,Ed=-75.56$ $M_y,Ed=986.83$ $M_z,Ed=-508.17$ $L=1.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=18.46$ Ncr,y=3737980.00 $\lambda'_y=0.24$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=18.46$ Ncr,z=3737980.00 $\lambda'_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.07+0.04=0.11
Verifica ZZ: 0.00+0.06+0.04=0.10

Asta n. 202 (-45 201) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND X1=0.00 - Classe 3
Sollecitazioni: $N=-306.78$ $T_x=942.22$ $M_y=1961.99$ $T_y=-112.03$ $M_z=152.58$ $M_x=-1.45$
Tensioni: $\sigma_N=-4.99$ $\sigma_{m,d}=-559.20$ $\tau=0.25$ $\sigma_{max}=-564.19$ (sfrut=0.17)
Tensioni: $\sigma_N=-4.99$ $\sigma_{m,d}=-37.12$ $\tau=34.71$ $\tau_{max}=34.71$ (sfrut=0.02)
Tensioni: $\sigma_N=-4.99$ $\sigma_{m,d}=-559.20$ $\tau=0.25$ $\sigma_{ID,max}=564.19$ (sfrut=0.17)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_z=3112.50$
 $V,Ed=3112.50$ $V_c,Rd=59967.00$ $V,Ed/V_c,Rd=0.05$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $N=-289.62$ $T_x=3112.50$ $M_y=4612.23$
 $M_y,Ed=4612.23$ $M_y,V,c,Rd=14964.90$
 $N,Ed=-289.62$ $N_c,Rd=-207726.00$ YY $n=N,Ed/N_c,Rd=0.00$ MNy,c,Rd=14964.90 $M_y,Ed/MNy,c,Rd=0.31$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $N,Ed=-289.62$ $M_y,Ed=4612.23$ $M_z,Ed=0.00$ $L=1.33$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.34=0.34
 Verifica ZZ: 0.00+0.27=0.28

Asta n. 202 (201 -6) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.33 - Classe 3
 Sollecitazioni: N=65.81 T_z=221.43 M_y=-790.99 T_y=-68.92 M_z=-87.31 M_x=-1.45
 Tensioni: $\sigma_N=1.07$ $\sigma_{m,d}=232.27$ $\tau=0.25$ $\sigma_{max}=233.34$ (sfrut=0.07)
 Tensioni: $\sigma_N=1.07$ $\sigma_{m,d}=21.24$ $\tau=8.35$ $\tau_{max}=8.35$ (sfrut=0.00)
 Tensioni: $\sigma_N=1.07$ $\sigma_{m,d}=232.27$ $\tau=0.25$ $\sigma_{TD,max}=233.34$ (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=1916.58
 V,Ed=1916.58 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.33 - Classe 1
 Sollecitazioni: N=-289.62 T_z=1833.46 M_y=-1944.48
 My,Ed=-1944.48 My,V,c,Rd=14964.90
 N,Ed=-289.62 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.13

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-289.62 My,Ed=-1944.48 Mz,Ed=0.00 L=1.33
 α_{my} , α_{mz} , $\alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.14=0.15
 Verifica ZZ: 0.00+0.12=0.12

Asta n. 202 (-6 -7) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.33 - Classe 3
 Sollecitazioni: N=-57.41 T_z=74.61 M_y=-683.93 T_y=-86.04 M_z=-405.08 M_x=-4.85
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-287.99$ $\tau=0.82$ $\sigma_{max}=-288.92$ (sfrut=0.09)
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=166.40$ $\tau=3.97$ $\tau_{max}=3.97$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.93$ $\sigma_{m,d}=-287.99$ $\tau=0.82$ $\sigma_{TD,max}=288.93$ (sfrut=0.09)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=720.67
 V,Ed=720.67 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.33 - Classe 1
 Sollecitazioni: N=-289.62 T_z=637.55 M_y=-2844.69
 My,Ed=-2844.69 My,V,c,Rd=14964.90
 N,Ed=-289.62 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.19

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-289.62 My,Ed=-2844.69 Mz,Ed=0.00 L=1.33
 α_{my} , α_{mz} , $\alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.21=0.21
 Verifica ZZ: 0.00+0.17=0.17

Asta n. 202 (-7 -8) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-100.52 T_z=-140.51 M_y=-683.94 T_y=57.66 M_z=-405.08 M_x=-4.85
 Tensioni: $\sigma_N=-1.64$ $\sigma_{m,d}=-287.99$ $\tau=0.82$ $\sigma_{max}=-289.63$ (sfrut=0.09)
 Tensioni: $\sigma_N=-1.64$ $\sigma_{m,d}=-98.55$ $\tau=5.96$ $\tau_{max}=5.96$ (sfrut=0.00)
 Tensioni: $\sigma_N=-1.64$ $\sigma_{m,d}=-287.99$ $\tau=0.82$ $\sigma_{TD,max}=289.63$ (sfrut=0.09)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.33 - Classe 1
 Sollecitazioni: T_z=-558.37
 V,Ed=-558.37 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-289.62 T_z=-475.25 M_y=-2844.71
 My,Ed=-2844.71 My,V,c,Rd=14964.90
 N,Ed=-289.62 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.19

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-289.62 My,Ed=-2844.71 Mz,Ed=0.00 L=1.33
 α_{my} , α_{mz} , $\alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.21=0.21
 Verifica ZZ: 0.00+0.17=0.17

Asta n. 202 (-8 -9) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=46.36 T_z=-306.23 M_y=-542.93 T_y=201.36 M_z=-328.64 M_x=-4.85
 Tensioni: $\sigma_N=0.75$ $\sigma_{m,d}=230.49$ $\tau=0.82$ $\sigma_{max}=231.24$ (sfrut=0.07)
 Tensioni: $\sigma_N=0.75$ $\sigma_{m,d}=-79.96$ $\tau=12.03$ $\tau_{max}=12.03$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.75$ $\sigma_{m,d}=230.49$ $\tau=0.82$ $\sigma_{TD,max}=231.25$ (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.33 - Classe 1
 Sollecitazioni: T_z=-1754.29
 V,Ed=-1754.29 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-289.62 T_z=-1671.17 M_y=-2159.57
 My,Ed=-2159.57 My,V,c,Rd=14964.90
 N,Ed=-289.62 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.14

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-289.62 My,Ed=-2159.57 Mz,Ed=0.00 L=1.33

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$

$\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.16=0.16

Verifica ZZ: 0.00+0.13=0.13

Asta n. 202 (-9 -10) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.33 - Classe 3
Sollecitazioni: N=-508.99 T_z=-894.78 M_y=1564.61 T_y=103.52 M_z=118.71 M_x=-1.46
Tensioni: $\sigma_{N}=-8.28$ $\sigma_{m,d}=-445.16$ $\tau=0.25$ $\sigma_{max}=-453.44$ (sfrut=0.13)
Tensioni: $\sigma_{N}=-8.28$ $\sigma_{m,d}=28.88$ $\tau=32.98$ $\tau_{max}=32.98$ (sfrut=0.02)
Tensioni: $\sigma_{N}=-8.28$ $\sigma_{m,d}=-445.16$ $\tau=0.25$ $\sigma_{TD,max}=453.44$ (sfrut=0.13)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_z=-2950.20
V,Ed=-2950.20 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.05

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.33 - Classe 1
Sollecitazioni: N=-289.62 T_z=-2950.20 M_y=3966.71
My,Ed=3966.71 My,V,c,Rd=14964.90
N,Ed=-289.62 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.27

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-289.62 My,Ed=3966.71 Mz,Ed=0.00 L=1.33

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$

$\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.29=0.30

Verifica ZZ: 0.00+0.24=0.24

Asta n. 202 (-10 202) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.20 - Classe 3
Sollecitazioni: N=-606.02 T_z=-1056.08 M_y=1774.90 T_y=132.63 M_z=145.24 M_x=-1.46
Tensioni: $\sigma_{N}=-9.86$ $\sigma_{m,d}=-507.78$ $\tau=0.25$ $\sigma_{max}=-517.64$ (sfrut=0.15)
Tensioni: $\sigma_{N}=-9.86$ $\sigma_{m,d}=35.34$ $\tau=38.88$ $\tau_{max}=38.88$ (sfrut=0.02)
Tensioni: $\sigma_{N}=-9.86$ $\sigma_{m,d}=-507.78$ $\tau=0.25$ $\sigma_{TD,max}=517.65$ (sfrut=0.15)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.20 - Classe 1
Sollecitazioni: T_z=-3576.46
V,Ed=-3576.46 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.06

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.20 - Classe 1
Sollecitazioni: N=-289.62 T_z=-3576.46 M_y=4680.86
My,Ed=4680.86 My,V,c,Rd=14964.90
N,Ed=-289.62 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.31

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-289.62 My,Ed=4680.86 Mz,Ed=0.00 L=0.20

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=2.55$ Ncr,y=195931000.00 $\lambda'_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=2.55$ Ncr,z=195931000.00 $\lambda'_z=0.03$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.35=0.35

Verifica ZZ: 0.00+0.28=0.28

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.00$ (L/19973)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.00$ (L/13315)

Asta n. 203 (202 -11) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-315.41 T_z=986.73 M_y=1651.00 T_y=-111.08 M_z=145.12 M_x=5.83
Tensioni: $\sigma_{N}=-5.13$ $\sigma_{m,d}=-474.98$ $\tau=0.99$ $\sigma_{max}=-480.12$ (sfrut=0.14)
Tensioni: $\sigma_{N}=-5.13$ $\sigma_{m,d}=35.31$ $\tau=37.08$ $\tau_{max}=37.08$ (sfrut=0.02)
Tensioni: $\sigma_{N}=-5.13$ $\sigma_{m,d}=-474.98$ $\tau=0.99$ $\sigma_{TD,max}=480.12$ (sfrut=0.14)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=3010.51
V,Ed=3010.51 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.05

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=160.97 T_z=3010.51 M_y=3738.68
My,Ed=3738.68 My,V,c,Rd=14964.90
N,Ed=160.97 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.25

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: My,Ed=3738.68 Mz,Ed=0.00 L=0.20

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=2.55$ Ncr,y=195931000.00 $\lambda'_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$

$\lambda_z=2.55$ Ncr,z=195931000.00 $\lambda'_z=0.03$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.28=0.28

Verifica ZZ: 0.00+0.22=0.22

Asta n. 203 (-11 -12) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-218.25 T_z=825.28 M_y=1454.62 T_y=-81.93 M_z=122.90 M_x=5.83
Tensioni: $\sigma_{N}=-3.55$ $\sigma_{m,d}=-417.18$ $\tau=0.99$ $\sigma_{max}=-420.73$ (sfrut=0.12)
Tensioni: $\sigma_{N}=-3.55$ $\sigma_{m,d}=29.90$ $\tau=31.18$ $\tau_{max}=31.18$ (sfrut=0.02)
Tensioni: $\sigma_{N}=-3.55$ $\sigma_{m,d}=-417.18$ $\tau=0.99$ $\sigma_{TD,max}=420.73$ (sfrut=0.12)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=2383.01

V,Ed=2383.01 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.04

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=160.97 T_z=2383.01 M_y=3137.83
My,Ed=3137.83 My,V,c,Rd=14964.90
N,Ed=160.97 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.21

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: My,Ed=3137.83 Mz,Ed=0.00 L=1.33
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=16.94 Ncr,y=4437370.00 λ'_y=0.22 Curva a: Φ_y=0.53 χ_y=1.00
λ_z=16.94 Ncr,z=4437370.00 λ'_z=0.22 Curva a: Φ_z=0.53 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.23=0.23
Verifica ZZ: 0.00+0.19=0.19

Asta n. 203 (-12 -13) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.33 - Classe 3
Sollecitazioni: N=95.56 T_z=152.64 M_y=-356.95 T_y=-129.16 M_z=-124.95 M_x=19.44
Tensioni: σ_N=1.56 σ_{m,d}=127.44 τ=3.30 σ_{max}=128.99 (sfrut=0.04)
Tensioni: σ_N=1.56 σ_{m,d}=-30.40 τ=8.88 τ_{max}=8.88 (sfrut=0.00)
Tensioni: σ_N=1.56 σ_{m,d}=127.44 τ=3.30 σ_{TD,max}=129.12 (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=1184.37
V,Ed=1184.37 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.33 - Classe 1
Sollecitazioni: N=160.97 T_z=1101.05 M_y=-1492.48
My,Ed=-1492.48 My,V,c,Rd=14964.90
N,Ed=160.97 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: My,Ed=-1492.48 Mz,Ed=0.00 L=1.33
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=16.94 Ncr,y=4437360.00 λ'_y=0.22 Curva a: Φ_y=0.53 χ_y=1.00
λ_z=16.94 Ncr,z=4437360.00 λ'_z=0.22 Curva a: Φ_z=0.53 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.11=0.11
Verifica ZZ: 0.00+0.09=0.09

Asta n. 203 (-13 -14) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.33 - Classe 3
Sollecitazioni: N=69.64 T_z=202.12 M_y=-593.51 T_y=4.44 M_z=-31.59 M_x=5.83
Tensioni: σ_N=1.13 σ_{m,d}=165.31 τ=0.99 σ_{max}=166.44 (sfrut=0.05)
Tensioni: σ_N=1.13 σ_{m,d}=-7.69 τ=8.38 τ_{max}=8.38 (sfrut=0.00)
Tensioni: σ_N=1.13 σ_{m,d}=165.31 τ=0.99 σ_{TD,max}=166.45 (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_z=-97.59
V,Ed=-97.59 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=160.97 T_z=-14.26 M_y=-1492.48
My,Ed=-1492.48 My,V,c,Rd=14964.90
N,Ed=160.97 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.10

Asta n. 203 (-14 -15) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.33 - Classe 3
Sollecitazioni: N=-100.86 T_z=-583.59 M_y=697.35 T_y=47.62 M_z=31.69 M_x=5.83
Tensioni: σ_N=-1.64 σ_{m,d}=-192.79 τ=0.99 σ_{max}=-194.44 (sfrut=0.06)
Tensioni: σ_N=-1.64 σ_{m,d}=-7.71 τ=22.34 τ_{max}=22.34 (sfrut=0.01)
Tensioni: σ_N=-1.64 σ_{m,d}=-192.79 τ=0.99 σ_{TD,max}=194.44 (sfrut=0.06)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_z=-1296.23
V,Ed=-1296.23 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=160.97 T_z=-1212.90 M_y=-1418.15
My,Ed=-1418.15 My,V,c,Rd=14964.90
N,Ed=160.97 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: My,Ed=-1418.15 Mz,Ed=0.00 L=1.33
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=16.94 Ncr,y=4437360.00 λ'_y=0.22 Curva a: Φ_y=0.53 χ_y=1.00
λ_z=16.94 Ncr,z=4437360.00 λ'_z=0.22 Curva a: Φ_z=0.53 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.11=0.11
Verifica ZZ: 0.00+0.08=0.08

Asta n. 203 (-15 203) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.33 - Classe 3
Sollecitazioni: N=-244.81 T_z=-863.12 M_y=1801.84 T_y=90.80 M_z=152.37 M_x=5.83
Tensioni: σ_N=-3.98 σ_{m,d}=-516.79 τ=0.99 σ_{max}=-520.78 (sfrut=0.15)
Tensioni: σ_N=-3.98 σ_{m,d}=-37.07 τ=32.56 τ_{max}=32.56 (sfrut=0.02)
Tensioni: σ_N=-3.98 σ_{m,d}=-516.79 τ=0.99 σ_{TD,max}=520.78 (sfrut=0.15)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_z=-2494.86
V,Ed=-2494.86 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.04

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.33 - Classe 1
Sollecitazioni: N=160.97 T_z=-2494.86 M_y=3509.46
My,Ed=3509.46 My,V,c,Rd=14964.90
N,Ed=160.97 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.23

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $M_y, Ed=3509.46$ $M_z, Ed=0.00$ $L=1.33$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.94$ Ncr, $y=4437370.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.94$ Ncr, $z=4437370.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.26=0.26$
 Verifica ZZ: $0.00+0.21=0.21$

Asta n. 204 (203 -26) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=75.56$ $T_x=524.01$ $M_y=986.83$ $T_y=-251.86$ $M_z=508.17$
 Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=395.35$ $\tau=0.00$ $\sigma_{max}=396.58$ (sfrut=0.12)
 Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=123.63$ $\tau=19.17$ $\tau_{max}=19.17$ (sfrut=0.01)
 Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=395.35$ $\tau=0.00$ $\sigma_{ID,max}=396.58$ (sfrut=0.12)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=2046.25$
 $V, Ed=2046.25$ $V_c, Rd=59967.00$ $V, Ed/V_c, Rd=0.03$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=2046.25$ $M_y=3918.32$
 $M_y, Ed=3918.32$ $M_y, V, c, Rd=14964.90$ $M_y, Ed/M_y, V, c, Rd=0.26$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
 Sollecitazioni: $N, Ed=-75.56$ $M_y, Ed=986.83$ $M_z, Ed=508.17$ $L=1.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=18.46$ Ncr, $y=3737990.00$ $\lambda'_y=0.24$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=18.46$ Ncr, $z=3737990.00$ $\lambda'_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.07+0.04=0.11$
 Verifica ZZ: $0.00+0.06+0.04=0.10$

Asta n. 204 (-26 -18) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=29.73$ $T_x=227.34$ $M_y=278.62$ $T_y=-99.09$ $M_z=143.48$
 Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=111.62$ $\tau=0.00$ $\sigma_{max}=112.11$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=34.91$ $\tau=8.32$ $\tau_{max}=8.32$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=111.62$ $\tau=0.00$ $\sigma_{ID,max}=112.11$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=750.55$
 $V, Ed=750.55$ $V_c, Rd=59967.00$ $V, Ed/V_c, Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=750.55$ $M_y=1021.07$
 $M_y, Ed=1021.07$ $M_y, V, c, Rd=14964.90$ $M_y, Ed/M_y, V, c, Rd=0.07$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
 Sollecitazioni: $N, Ed=-29.73$ $M_y, Ed=278.62$ $M_z, Ed=143.48$ $L=1.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=18.46$ Ncr, $y=3737990.00$ $\lambda'_y=0.24$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=18.46$ Ncr, $z=3737990.00$ $\lambda'_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.02+0.01=0.03$

Asta n. 301 (-45 -79) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-10.45$ $T_x=110.49$ $M_y=101.46$ $T_y=-34.83$ $M_z=52.25$
 Tensioni: $\sigma_N=-0.28$ $\sigma_{m,d}=-111.87$ $\tau=0.00$ $\sigma_{max}=-112.15$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.28$ $\sigma_{m,d}=37.31$ $\tau=5.68$ $\tau_{max}=5.68$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.28$ $\sigma_{m,d}=-111.87$ $\tau=0.00$ $\sigma_{ID,max}=112.15$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=579.43$
 $V, Ed=579.43$ $V_c, Rd=43850.90$ $V, Ed/V_c, Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=579.43$ $M_y=580.80$
 $M_y, Ed=580.80$ $M_y, V, c, Rd=6269.10$ $M_y, Ed/M_y, V, c, Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed=-10.45$ $M_y, Ed=101.46$ $M_z, Ed=52.25$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.02+0.01=0.03$

Asta n. 301 (-80 -45) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
 Sollecitazioni: $N=10.45$ $T_x=-110.49$ $M_y=101.46$ $T_y=34.83$ $M_z=52.25$
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=111.87$ $\tau=0.00$ $\sigma_{max}=112.15$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=37.31$ $\tau=5.68$ $\tau_{max}=5.68$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=111.87$ $\tau=0.00$ $\sigma_{ID,max}=112.15$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-579.43$
 $V, Ed=-579.43$ $V_c, Rd=43850.90$ $V, Ed/V_c, Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-579.43$ $M_y=580.80$
 $M_y, Ed=580.80$ $M_y, V, c, Rd=6269.10$ $M_y, Ed/M_y, V, c, Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.45 My,Ed=101.46 Mz,Ed=52.25 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 302 (-3 -69) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-7.08 T_x=78.75 M_y=68.77 T_y=-23.61 M_z=35.41
 Tensioni: $\sigma_N=-0.19$ $\sigma_{m,d}=-75.82$ $\tau=0.00$ $\sigma_{max}=-76.01$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.19$ $\sigma_{m,d}=25.29$ $\tau=4.05$ $\tau_{max}=4.05$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.19$ $\sigma_{m,d}=-75.82$ $\tau=0.00$ $\sigma_{ID,max}=76.01$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=329.88
 V,Ed=329.88 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=329.88 M_y=323.75
 My,Ed=323.75 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-7.08 My,Ed=68.77 Mz,Ed=35.41 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 302 (-68 -3) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=7.08 T_x=-78.75 M_y=68.77 T_y=23.61 M_z=35.41
 Tensioni: $\sigma_N=0.19$ $\sigma_{m,d}=75.82$ $\tau=0.00$ $\sigma_{max}=76.01$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.19$ $\sigma_{m,d}=25.29$ $\tau=4.05$ $\tau_{max}=4.05$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.19$ $\sigma_{m,d}=75.82$ $\tau=0.00$ $\sigma_{ID,max}=76.01$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-329.88
 V,Ed=-329.88 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-329.88 M_y=323.75
 My,Ed=323.75 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-7.08 My,Ed=68.77 Mz,Ed=35.41 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 303 (-29 -76) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-10.76 T_x=113.42 M_y=104.48 T_y=-35.87 M_z=53.80
 Tensioni: $\sigma_N=-0.29$ $\sigma_{m,d}=-115.19$ $\tau=0.00$ $\sigma_{max}=-115.48$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.29$ $\sigma_{m,d}=38.42$ $\tau=5.83$ $\tau_{max}=5.83$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.29$ $\sigma_{m,d}=-115.19$ $\tau=0.00$ $\sigma_{ID,max}=115.48$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=602.46
 V,Ed=602.46 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=602.46 M_y=604.52
 My,Ed=604.52 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.76 My,Ed=104.48 Mz,Ed=53.80 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 303 (-75 -29) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=10.76 T_x=-113.42 M_y=104.48 T_y=35.87 M_z=53.80
 Tensioni: $\sigma_N=0.29$ $\sigma_{m,d}=115.19$ $\tau=0.00$ $\sigma_{max}=115.48$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.29$ $\sigma_{m,d}=38.42$ $\tau=5.83$ $\tau_{max}=5.83$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.29$ $\sigma_{m,d}=115.19$ $\tau=0.00$ $\sigma_{ID,max}=115.48$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-602.46
 V,Ed=-602.46 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-602.46 M_y=604.52
 My,Ed=604.52 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.76 My,Ed=104.48 Mz,Ed=53.80 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 304 (201 -77) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-10.14 T_z=107.56 M_y=98.45 T_y=-33.80 M_z=50.69
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{max}=-108.81$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{ID,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=556.40
 V,Ed=556.40 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=556.40 M_y=557.08
 My,Ed=557.08 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 304 (-78 201) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=10.14 T_z=-107.56 M_y=98.45 T_y=33.80 M_z=50.69
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{max}=108.81$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{ID,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-556.40
 V,Ed=-556.40 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-556.40 M_y=557.08
 My,Ed=557.08 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 305 (-6 -48) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-10.14 T_z=107.56 M_y=98.45 T_y=-33.80 M_z=50.69
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{max}=-108.81$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{ID,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=556.40
 V,Ed=556.40 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=556.40 M_y=557.08
 My,Ed=557.08 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 305 (-47 -6) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=10.14 T_z=-107.56 M_y=98.45 T_y=33.80 M_z=50.69
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{max}=108.81$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{ID,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-556.40
 V,Ed=-556.40 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_z=-556.40 M_y=557.08
 My,Ed=557.08 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.00+0.02+0.01=0.03$

Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 306 (-7 -50) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-10.14 $T_x=107.56$ $M_y=98.45$ $T_y=-33.80$ $M_z=50.69$

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{max}=-108.81$ (sfrut=0.03)

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{TD,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: $T_z=556.40$

$V_{Ed}=556.40$ $V_{c,Rd}=43850.90$ $V_{Ed}/V_{c,Rd}=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: $T_z=556.40$ $M_y=557.08$

$M_{y,Ed}=557.08$ $M_{y,V,c,Rd}=6269.10$ $M_{y,Ed}/M_{y,V,c,Rd}=0.09$

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.14 $M_y,Ed=98.45$ $M_z,Ed=50.69$ L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.00+0.02+0.01=0.03$

Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 306 (-49 -7) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=10.14 $T_x=-107.56$ $M_y=98.45$ $T_y=33.80$ $M_z=50.69$

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{max}=108.81$ (sfrut=0.03)

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{TD,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: $T_z=-556.40$

$V_{Ed}=-556.40$ $V_{c,Rd}=43850.90$ $V_{Ed}/V_{c,Rd}=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: $T_z=-556.40$ $M_y=557.08$

$M_{y,Ed}=557.08$ $M_{y,V,c,Rd}=6269.10$ $M_{y,Ed}/M_{y,V,c,Rd}=0.09$

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.14 $M_y,Ed=98.45$ $M_z,Ed=50.69$ L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.00+0.02+0.01=0.03$

Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 307 (-8 -52) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-10.14 $T_x=107.56$ $M_y=98.45$ $T_y=-33.80$ $M_z=50.69$

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{max}=-108.81$ (sfrut=0.03)

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{TD,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: $T_z=556.40$

$V_{Ed}=556.40$ $V_{c,Rd}=43850.90$ $V_{Ed}/V_{c,Rd}=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: $T_z=556.40$ $M_y=557.08$

$M_{y,Ed}=557.08$ $M_{y,V,c,Rd}=6269.10$ $M_{y,Ed}/M_{y,V,c,Rd}=0.09$

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.14 $M_y,Ed=98.45$ $M_z,Ed=50.69$ L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.00+0.02+0.01=0.03$

Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 307 (-51 -8) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=10.14 $T_x=-107.56$ $M_y=98.45$ $T_y=33.80$ $M_z=50.69$

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{max}=108.81$ (sfrut=0.03)

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{TD,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: $T_z=-556.40$

$V_{Ed}=-556.40$ $V_{c,Rd}=43850.90$ $V_{Ed}/V_{c,Rd}=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: $T_z=-556.40$ $M_y=557.08$

$M_{y,Ed}=557.08$ $M_{y,V,c,Rd}=6269.10$ $M_{y,Ed}/M_{y,V,c,Rd}=0.09$

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.14 $M_y,Ed=98.45$ $M_z,Ed=50.69$ L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 308 (-9 -54) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-10.14$ $T_x=107.56$ $M_y=98.45$ $T_y=-33.80$ $M_z=50.69$
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{max}=-108.81$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.54$ $\tau=0.00$ $\sigma_{TD,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_x=556.40$
 $V,Ed=556.40$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_x=556.40$ $M_y=557.08$
 $My,Ed=557.08$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.14$ $My,Ed=98.45$ $Mz,Ed=50.69$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 308 (-53 -9) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: $N=10.14$ $T_x=-107.56$ $M_y=98.45$ $T_y=33.80$ $M_z=50.69$
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{max}=108.81$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.20$ $\tau=5.53$ $\tau_{max}=5.53$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.54$ $\tau=0.00$ $\sigma_{TD,max}=108.81$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_x=-556.40$
 $V,Ed=-556.40$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_x=-556.40$ $M_y=557.08$
 $My,Ed=557.08$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.14$ $My,Ed=98.45$ $Mz,Ed=50.69$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 309 (-10 -56) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-6.77$ $T_x=75.82$ $M_y=65.76$ $T_y=-22.57$ $M_z=33.86$
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.50$ $\tau=0.00$ $\sigma_{max}=-72.68$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=24.18$ $\tau=3.90$ $\tau_{max}=3.90$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.50$ $\tau=0.00$ $\sigma_{TD,max}=72.68$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_x=306.86$
 $V,Ed=306.86$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_x=306.86$ $M_y=300.03$
 $My,Ed=300.03$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-6.77$ $My,Ed=65.76$ $Mz,Ed=33.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.01+0.01=0.02$
 Verifica ZZ: $0.00+0.01+0.01=0.02$

Asta n. 309 (-55 -10) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: $N=6.77$ $T_x=-75.82$ $M_y=65.76$ $T_y=22.57$ $M_z=33.86$
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.50$ $\tau=0.00$ $\sigma_{max}=72.68$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=24.18$ $\tau=3.90$ $\tau_{max}=3.90$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.50$ $\tau=0.00$ $\sigma_{TD,max}=72.68$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_x=-306.86$
 $V,Ed=-306.86$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: $T_x=-306.86$ $M_y=300.03$
 $My,Ed=300.03$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-6.77$ $My,Ed=65.76$ $Mz,Ed=33.86$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 310 (-11 -58) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-6.78 T_z=75.90 M_y=65.84 T_y=-22.60 M_z=33.90
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.59$ $\tau=0.00$ $\sigma_{max}=-72.77$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=24.21$ $\tau=3.90$ $\tau_{max}=3.90$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.59$ $\tau=0.00$ $\sigma_{ID,max}=72.77$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=307.48
 V,Ed=307.48 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=307.48 M_y=300.68
 My,Ed=300.68 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-6.78 My,Ed=65.84 Mz,Ed=33.90 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr, y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 310 (-57 -11) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=6.78 T_z=-75.90 M_y=65.84 T_y=22.60 M_z=33.90
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.59$ $\tau=0.00$ $\sigma_{max}=72.77$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=24.21$ $\tau=3.90$ $\tau_{max}=3.90$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.59$ $\tau=0.00$ $\sigma_{ID,max}=72.77$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-307.48
 V,Ed=-307.48 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-307.48 M_y=300.68
 My,Ed=300.68 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-6.78 My,Ed=65.84 Mz,Ed=33.90 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr, y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 311 (-12 -60) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-10.16 T_z=107.72 M_y=98.61 T_y=-33.85 M_z=50.78
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.72$ $\tau=0.00$ $\sigma_{max}=-108.99$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.26$ $\tau=5.54$ $\tau_{max}=5.54$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.72$ $\tau=0.00$ $\sigma_{ID,max}=108.99$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=557.65
 V,Ed=557.65 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=557.65 M_y=558.38
 My,Ed=558.38 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr, y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 311 (-59 -12) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=10.16 T_z=-107.72 M_y=98.61 T_y=33.85 M_z=50.78
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.72$ $\tau=0.00$ $\sigma_{max}=108.99$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.26$ $\tau=5.54$ $\tau_{max}=5.54$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.72$ $\tau=0.00$ $\sigma_{ID,max}=108.99$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-557.65
 V,Ed=-557.65 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-557.65 M_y=558.38
 My,Ed=558.38 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr, y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 312 (-13 -62) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-10.16 T_x=107.72 M_y=98.61 T_y=-33.85 M_z=50.78
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =-108.72 τ =0.00 σ_{max} =-108.99 (sfrut=0.03)
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =36.26 τ =5.54 τ_{max} =5.54 (sfrut=0.00)
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =-108.72 τ =0.00 $\sigma_{ID,max}$ =108.99 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_x=557.65
 V,Ed=557.65 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_x=557.65 M_y=558.38
 My,Ed=558.38 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96
 λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 312 (-61 -13) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=10.16 T_x=-107.72 M_y=98.61 T_y=33.85 M_z=50.78
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =108.72 τ =0.00 σ_{max} =108.99 (sfrut=0.03)
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =36.26 τ =5.54 τ_{max} =5.54 (sfrut=0.00)
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =108.72 τ =0.00 $\sigma_{ID,max}$ =108.99 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_x=-557.65
 V,Ed=-557.65 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_x=-557.65 M_y=558.38
 My,Ed=558.38 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96
 λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 313 (-14 -64) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-10.16 T_x=107.72 M_y=98.61 T_y=-33.85 M_z=50.78
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =-108.72 τ =0.00 σ_{max} =-108.99 (sfrut=0.03)
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =36.26 τ =5.54 τ_{max} =5.54 (sfrut=0.00)
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =-108.72 τ =0.00 $\sigma_{ID,max}$ =108.99 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_x=557.65
 V,Ed=557.65 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_x=557.65 M_y=558.38
 My,Ed=558.38 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96
 λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 313 (-63 -14) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=10.16 T_x=-107.72 M_y=98.61 T_y=33.85 M_z=50.78
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =108.72 τ =0.00 σ_{max} =108.99 (sfrut=0.03)
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =36.26 τ =5.54 τ_{max} =5.54 (sfrut=0.00)
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =108.72 τ =0.00 $\sigma_{ID,max}$ =108.99 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_x=-557.65
 V,Ed=-557.65 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_x=-557.65 M_y=558.38
 My,Ed=558.38 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96
 λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 314 (-15 -66) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-10.16 T_x=107.72 M_y=98.61 T_y=-33.85 M_z=50.78
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.72$ $\tau=0.00$ $\sigma_{max}=-108.99$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.26$ $\tau=5.54$ $\tau_{max}=5.54$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-108.72$ $\tau=0.00$ $\sigma_{ID,max}=108.99$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=557.65
V,Ed=557.65 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=557.65 M_y=558.38
My,Ed=558.38 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 314 (-65 -15) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=10.16 T_x=-107.72 M_y=98.61 T_y=33.85 M_z=50.78
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.72$ $\tau=0.00$ $\sigma_{max}=108.99$ (sfrut=0.03)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.26$ $\tau=5.54$ $\tau_{max}=5.54$ (sfrut=0.00)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=108.72$ $\tau=0.00$ $\sigma_{ID,max}=108.99$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-557.65
V,Ed=-557.65 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-557.65 M_y=558.38
My,Ed=558.38 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 315 (203 -67) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-10.46 T_x=110.57 M_y=101.55 T_y=-34.86 M_z=52.29
Tensioni: $\sigma_N=-0.28$ $\sigma_{m,d}=-111.96$ $\tau=0.00$ $\sigma_{max}=-112.24$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.28$ $\sigma_{m,d}=37.34$ $\tau=5.68$ $\tau_{max}=5.68$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.28$ $\sigma_{m,d}=-111.96$ $\tau=0.00$ $\sigma_{ID,max}=112.24$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=580.05
V,Ed=580.05 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=580.05 M_y=581.45
My,Ed=581.45 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.46 My,Ed=101.55 Mz,Ed=52.29 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 315 (-72 203) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=10.46 T_x=-110.57 M_y=101.55 T_y=34.86 M_z=52.29
Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=111.96$ $\tau=0.00$ $\sigma_{max}=112.24$ (sfrut=0.03)
Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=37.34$ $\tau=5.68$ $\tau_{max}=5.68$ (sfrut=0.00)
Tensioni: $\sigma_N=0.28$ $\sigma_{m,d}=111.96$ $\tau=0.00$ $\sigma_{ID,max}=112.24$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-580.05
V,Ed=-580.05 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-580.05 M_y=581.45
My,Ed=581.45 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-10.46 My,Ed=101.55 Mz,Ed=52.29 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 316 (-26 -74) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-10.76 T_z=113.42 M_y=104.48 T_y=-35.87 M_z=53.80

Tensioni: σ_N =-0.29 $\sigma_{m,d}$ =-115.19 τ =0.00 σ_{max} =-115.48 (sfrut=0.03)

Tensioni: σ_N =-0.29 $\sigma_{m,d}$ =38.42 τ =5.83 τ_{max} =5.83 (sfrut=0.00)

Tensioni: σ_N =-0.29 $\sigma_{m,d}$ =-115.19 τ =0.00 $\sigma_{ID,max}$ =115.48 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=602.46

V,Ed=602.46 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=602.46 M_y=604.52

My,Ed=604.52 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.10

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.76 My,Ed=104.48 Mz,Ed=53.80 L=1.50

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96

λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 316 (-73 -26) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=10.76 T_z=-113.42 M_y=104.48 T_y=35.87 M_z=53.80

Tensioni: σ_N =0.29 $\sigma_{m,d}$ =115.19 τ =0.00 σ_{max} =115.48 (sfrut=0.03)

Tensioni: σ_N =0.29 $\sigma_{m,d}$ =38.42 τ =5.83 τ_{max} =5.83 (sfrut=0.00)

Tensioni: σ_N =0.29 $\sigma_{m,d}$ =115.19 τ =0.00 $\sigma_{ID,max}$ =115.48 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: T_z=-602.46

V,Ed=-602.46 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: T_z=-602.46 M_y=604.52

My,Ed=604.52 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.10

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.76 My,Ed=104.48 Mz,Ed=53.80 L=1.50

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96

λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.02+0.01=0.03

Asta n. 317 (-18 -71) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-7.08 T_z=78.75 M_y=68.77 T_y=-23.61 M_z=35.41

Tensioni: σ_N =-0.19 $\sigma_{m,d}$ =-75.82 τ =0.00 σ_{max} =-76.01 (sfrut=0.02)

Tensioni: σ_N =-0.19 $\sigma_{m,d}$ =25.29 τ =4.05 τ_{max} =4.05 (sfrut=0.00)

Tensioni: σ_N =-0.19 $\sigma_{m,d}$ =-75.82 τ =0.00 $\sigma_{ID,max}$ =76.01 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=329.88

V,Ed=329.88 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=329.88 M_y=323.75

My,Ed=323.75 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-7.08 My,Ed=68.77 Mz,Ed=35.41 L=1.50

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96

λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.01+0.01=0.02

Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 317 (-70 -18) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=7.08 T_z=-78.75 M_y=68.77 T_y=23.61 M_z=35.41

Tensioni: σ_N =0.19 $\sigma_{m,d}$ =75.82 τ =0.00 σ_{max} =76.01 (sfrut=0.02)

Tensioni: σ_N =0.19 $\sigma_{m,d}$ =25.29 τ =4.05 τ_{max} =4.05 (sfrut=0.00)

Tensioni: σ_N =0.19 $\sigma_{m,d}$ =75.82 τ =0.00 $\sigma_{ID,max}$ =76.01 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: T_z=-329.88

V,Ed=-329.88 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: T_z=-329.88 M_y=323.75

My,Ed=323.75 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-7.08 My,Ed=68.77 Mz,Ed=35.41 L=1.50

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96

λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.01+0.01=0.02

Verifica ZZ: 0.00+0.01+0.01=0.02

Membratura

Asta n. 201 (-3 -29 -45) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-75.56 My,Ed=986.83 Mz,Ed=508.17 L=2.90

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=36.91$ Ncr,y=934494.00 $\lambda'_y=0.48$ Curva a: $\Phi_y=0.65$ $\chi_y=0.93$

$\lambda_z=36.91$ Ncr,z=934494.00 $\lambda'_z=0.48$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.07+0.04=0.11

Verifica ZZ: 0.00+0.06+0.04=0.10

- Verifica freccia massima per soli carichi accidentali - CC 31

$f_{z,1}=0.23$ (L/1244) $f_{z,6}=0.08$ (L/3727)

- Verifica freccia massima carichi totali - CC 31

$f_{z,1}=0.39$ (L/743) $f_{z,6}=0.12$ (L/2329)

Membratura

Asta n. 202 (-45 201 -6 -7 -8 -9 -10) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-289.62 My,Ed=4612.23 Mz,Ed=0.00 L=7.95

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=101.39$ Ncr,y=123881.00 $\lambda'_y=1.33$ Curva a: $\Phi_y=1.50$ $\chi_y=0.46$

$\lambda_z=101.39$ Ncr,z=123881.00 $\lambda'_z=1.33$ Curva a: $\Phi_z=1.50$ $\chi_z=0.46$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.34=0.34

Verifica ZZ: 0.00+0.27=0.28

- Verifica freccia massima per soli carichi accidentali - CC 31

$f_{z,1}=0.71$ (L/1123) $f_{z,6}=0.71$ (L/1127)

- Verifica freccia massima carichi totali - CC 31

$f_{z,1}=1.07$ (L/746) $f_{z,6}=1.06$ (L/748)

Membratura

Asta n. 203 (202 -11 -12 -13 -14 -15 203) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=160.97 My,Ed=3738.68 Mz,Ed=0.00 L=6.84

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.28=0.28

Verifica ZZ: 0.00+0.22=0.22

- Verifica freccia massima per soli carichi accidentali - CC 31

$f_{z,6}=0.23$ (L/2983)

- Verifica freccia massima carichi totali - CC 31

$f_{z,6}=0.34$ (L/2007)

Membratura

Asta n. 204 (203 -26 -18) - Sez. 3 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
Sollecitazioni: N,Ed=-75.56 My,Ed=986.83 Mz,Ed=508.17 L=2.90

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=36.91$ Ncr,y=934497.00 $\lambda'_y=0.48$ Curva a: $\Phi_y=0.65$ $\chi_y=0.93$

$\lambda_z=36.91$ Ncr,z=934497.00 $\lambda'_z=0.48$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.07+0.04=0.11

Verifica ZZ: 0.00+0.06+0.04=0.10

- Verifica freccia massima per soli carichi accidentali - CC 31

$f_{z,1}=0.29$ (L/988) $f_{z,6}=0.08$ (L/3677)

- Verifica freccia massima carichi totali - CC 31

$f_{z,1}=0.47$ (L/611) $f_{z,6}=0.13$ (L/2300)

Membratura

Asta n. 301 (-79 -45 -80) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.45 My,Ed=101.46 Mz,Ed=52.25 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.02+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31

$f_{z,1}=0.08$ (L/3618)

- Verifica freccia massima carichi totali - CC 31

$f_{z,1}=0.11$ (L/2716)

Membratura

Asta n. 302 (-69 -3 -68) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-7.08 My,Ed=68.77 Mz,Ed=35.41 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.01+0.01=0.02

Verifica ZZ: 0.00+0.01+0.01=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31

$f_{z,1}=0.04$ (L/6936)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.06$ (L/4880)

Membratura

Asta n. 303 (-76 -29 -75) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.76 My,Ed=104.48 Mz,Ed=53.80 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.02+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.09$ (L/3466)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2609)

Membratura

Asta n. 304 (-77 201 -78) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2832)

Membratura

Asta n. 305 (-48 -6 -47) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2832)

Membratura

Asta n. 306 (-50 -7 -49) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2832)

Membratura

Asta n. 307 (-52 -8 -51) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2832)

Membratura

Asta n. 308 (-54 -9 -53) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.14 My,Ed=98.45 Mz,Ed=50.69 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3786)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2832)

Membratura

Asta n. 309 (-56 -10 -55) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-6.77 My,Ed=65.76 Mz,Ed=33.86 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.04$ (L/7570)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.06$ (L/5264)

Membratura

Asta n. 310 (-58 -11 -57) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-6.78 My,Ed=65.84 Mz,Ed=33.90 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.04$ (L/7552)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.06$ (L/5253)

Membratura

Asta n. 311 (-60 -12 -59) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3776)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2824)

Membratura

Asta n. 312 (-62 -13 -61) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3777)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2825)

Membratura

Asta n. 313 (-64 -14 -63) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3777)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2826)

Membratura

Asta n. 314 (-66 -15 -65) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.16 My,Ed=98.61 Mz,Ed=50.78 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3777)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2825)

Membratura

Asta n. 315 (-67 203 -72) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.46 My,Ed=101.55 Mz,Ed=52.29 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.02+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3614)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2713)

Membratura

Asta n. 316 (-74 -26 -73) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.76 My,Ed=104.48 Mz,Ed=53.80 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.02+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.09$ (L/3467)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2610)

Membratura

Asta n. 317 (-71 -18 -70) - Sez. 1 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-7.08 My,Ed=68.77 Mz,Ed=35.41 L=3.00
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 K_{yy} , K_{yz} , K_{zy} , K_{zz} =0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.04$ (L/6928)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.06$ (L/4877)

6.2 Tracker 2x15 – configurazione in esercizio ($\alpha = 55^\circ$)

6.2.1 Diagrammi tassi di sfruttamento

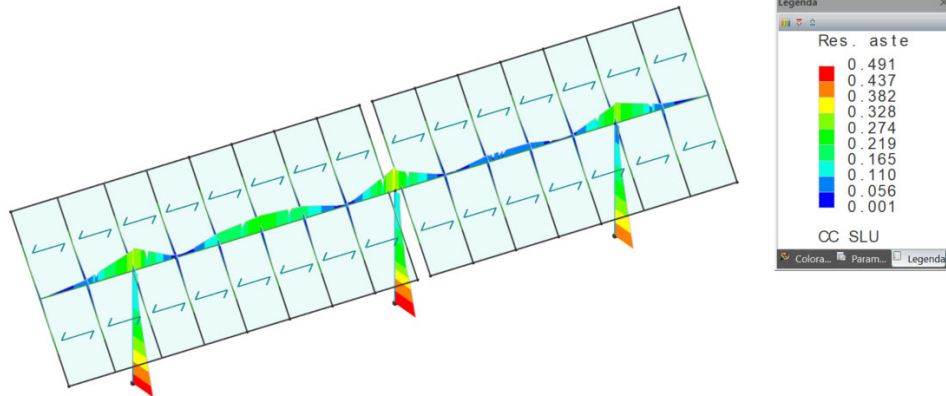


Diagramma tassi di sfruttamento resistenza aste combo SLU con valore massimo pari a 0,491

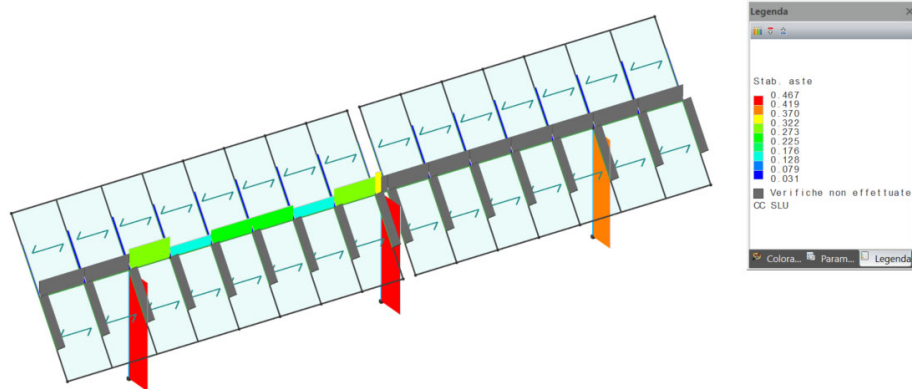


Diagramma tassi di sfruttamento stabilità aste combo SLU con valore massimo pari a 0,467

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

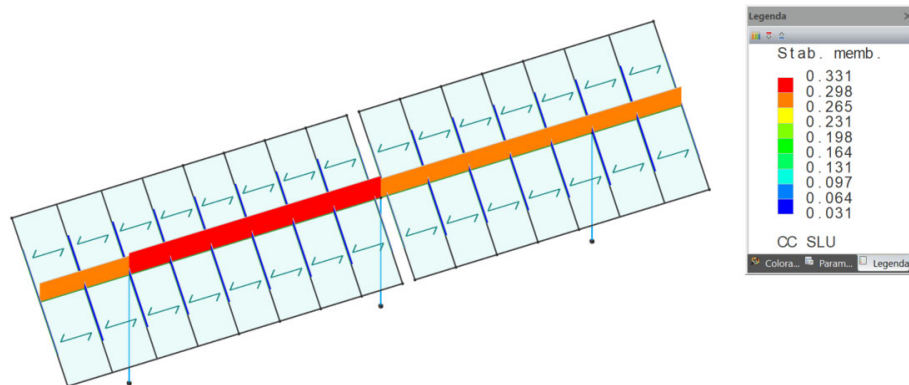


Diagramma tassi di sfruttamento stabilità membrature combo SLU con valore massimo pari a 0,331

Figure 22: Tassi di sfruttamento SLU (Stato limite ultimo)

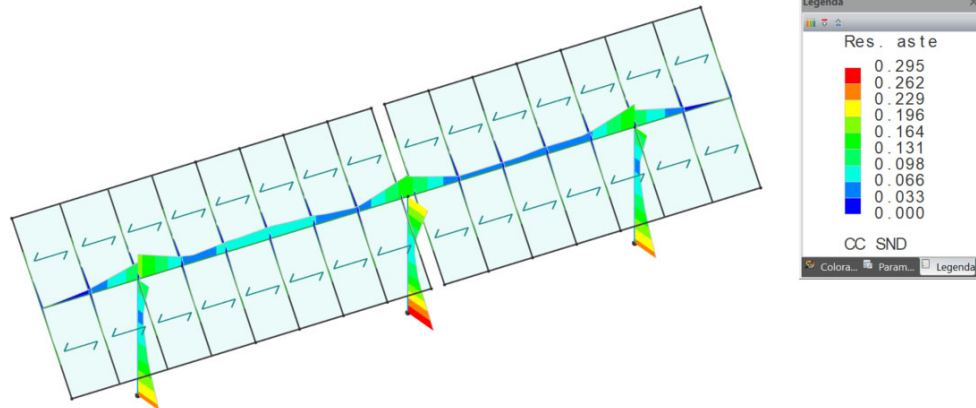


Diagramma tassi di sfruttamento resistenza aste combo SND con valore massimo pari a 0,295

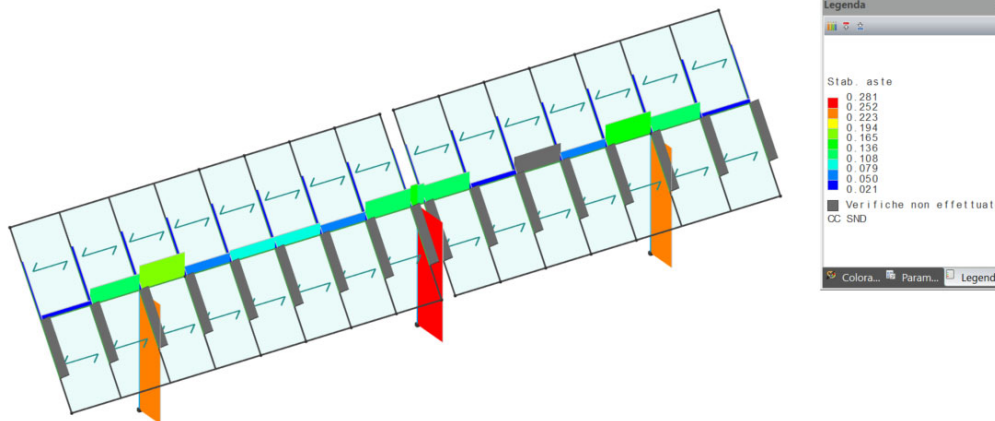


Diagramma tassi di sfruttamento stabilità aste combo SND con valore massimo pari a 0,281

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

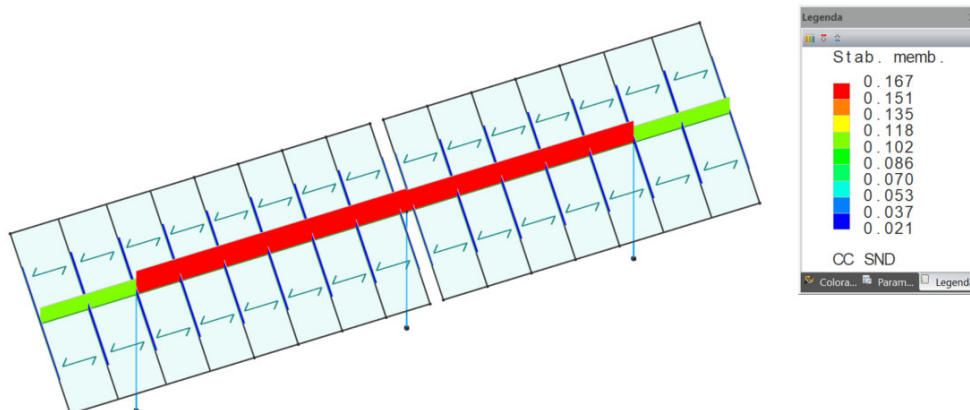
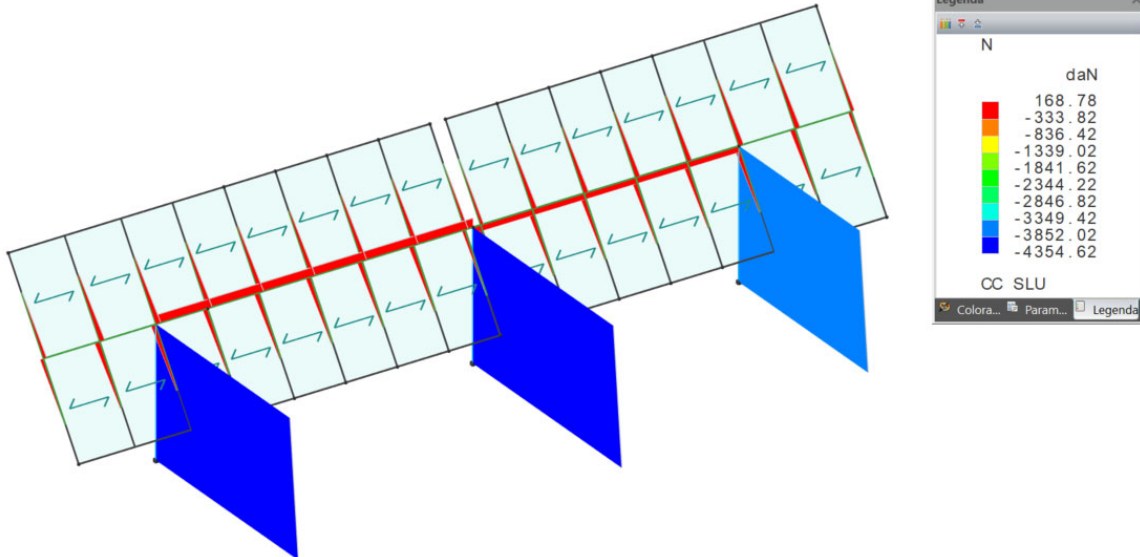


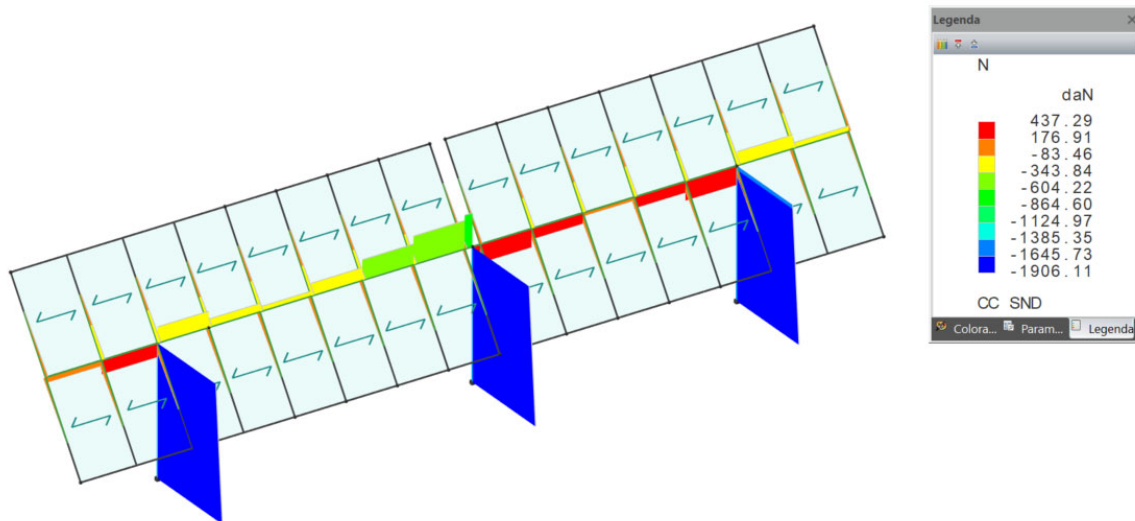
Diagramma tassi di sfruttamento stabilità membrature combo SND con valore massimo pari a 0,167

Figure 23: Tassi di sfruttamento SND (Stato limite di vita non dissipativo)

6.2.2 Sollecitazioni

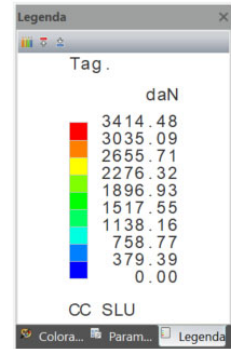
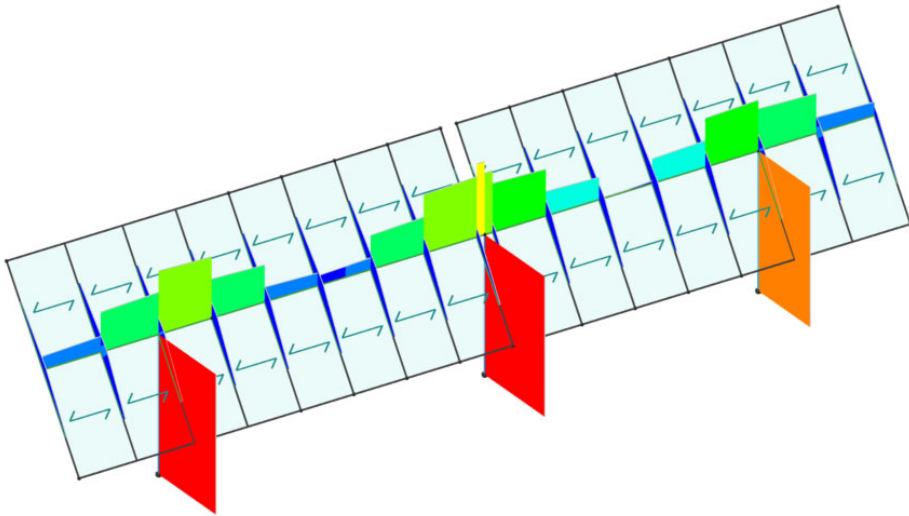


Inviluppo sforzo normale SLU $N_{max} = 4354,62$ daN (compressione)

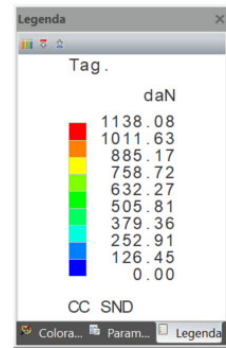
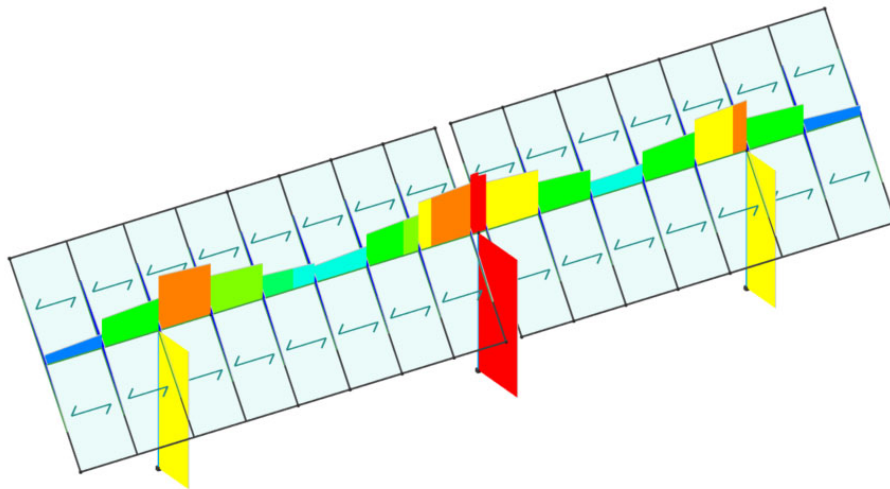


Inviluppo sforzo normale SND $N_{max} = 1906,11$ daN (compressione)

Figure 24: Sforzo Normale

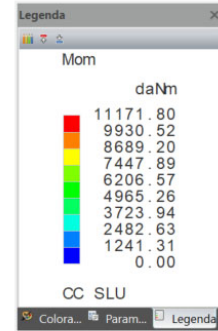
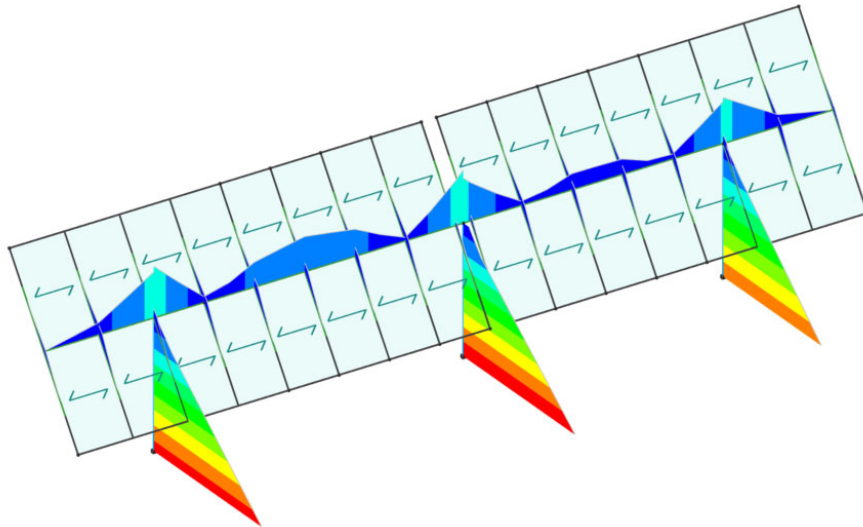


Inviluppo sforzo di taglio SLU $T_{max} = 3414,48$ daN

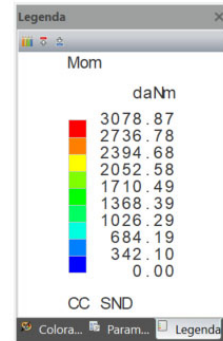
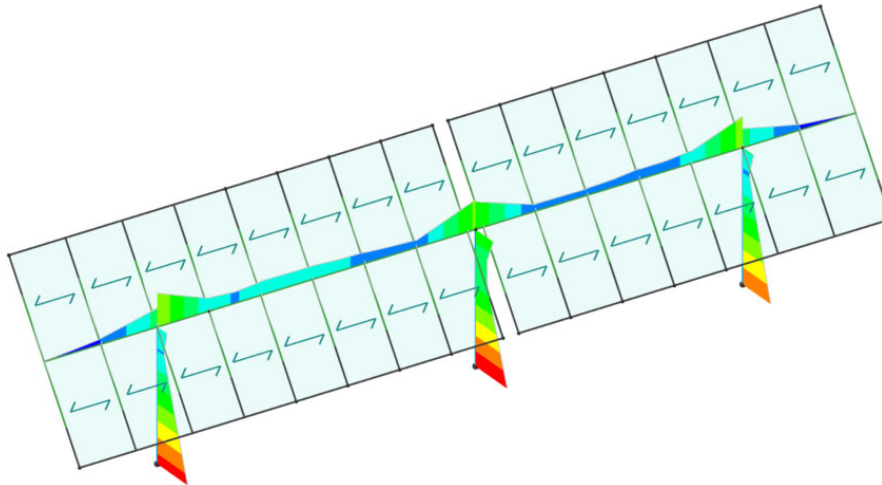


Inviluppo sforzo di taglio SND $T_{max} = 1138,08$ daN

Figure 25: Taglio



Inviluppo momento flettente SLU $M_{max} = 11171,80 \text{ daN}\times\text{m}$



Inviluppo momento flettente SND $M_{max} = 3078,87 \text{ daN}\times\text{m}$

Figure 26: Momento Flettente

6.2.3 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
 ModeSt ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
 Xfinest ver. 9.5.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18
 Tipo di calcolo: sismica statica
 Vincoli esterni: Considera sempre vincoli assegnati in modellazione
 Schematizzazione piani rigidi: nessun impalcato rigido
 Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Non sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

Dati struttura

- Sito di costruzione: CPHJ+52 Foggia FG, Italia LON. 15.73010 LAT. 41.42790
 Contenuto tra ID reticolo: 30559 30558 30337 30336

Simbologia

Ag = Accelerazione orizzontale massima al sito
 Cc = Coefficiente funzione della categoria del suolo
 Fo = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
 Ss = Coefficiente di amplificazione stratigrafica
 Tr = Periodo di ritorno <anni>
 TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SND = Stato limite di salvaguardia della vita (non dissipativo)
 Tc* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

TCC	Tr	Ag <g>	Fo	Tc*	Ss	Cc
SLD	50	0.0554	2.54	0.33	1.50	1.52
SLV	475	0.1323	2.61	0.43	1.49	1.38

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale Vn: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 5.26 <m>
- Altezza della struttura: 5.26 <m>
- Numero piani edificio: 0
- Coefficiente 0: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia strutturale: acciaio a mensola o a pendolo inverso

Periodo T1	0.29527
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00

Rapporto di sovrarresistenza (α_u/α_1)	1.00
Valore di riferimento del fattore di comportamento (q_0)	1.00
Fattore riduttivo (K_w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di comportamento dissipativo (q)	1.00
Fattore di comportamento non dissipativo (qND)	1.00
Fattore di comportamento per SLD (qD)	1.00

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica S_T : 1.00
- Accelerazione di picco del terreno A_gS : 0.1976 <g>
- Fattore di comportamento per sisma verticale (qv): 1.50
- Smorzamento spettro: 5.00%

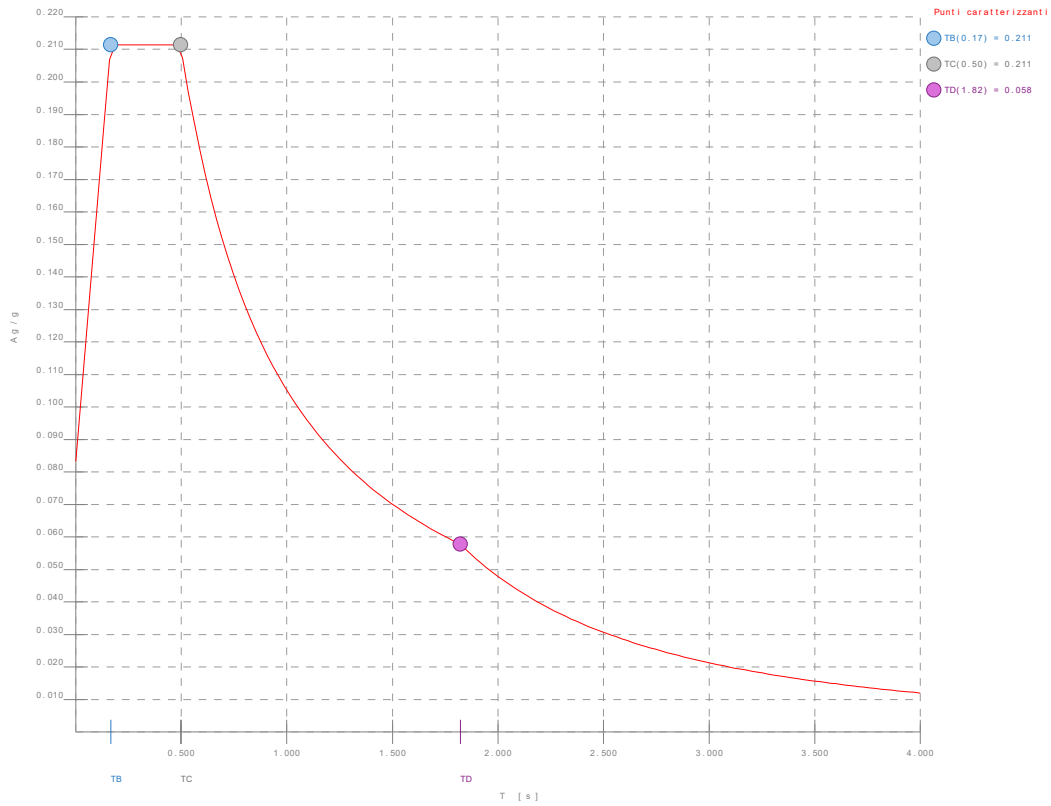


Figura numero 1: Spettro SLD

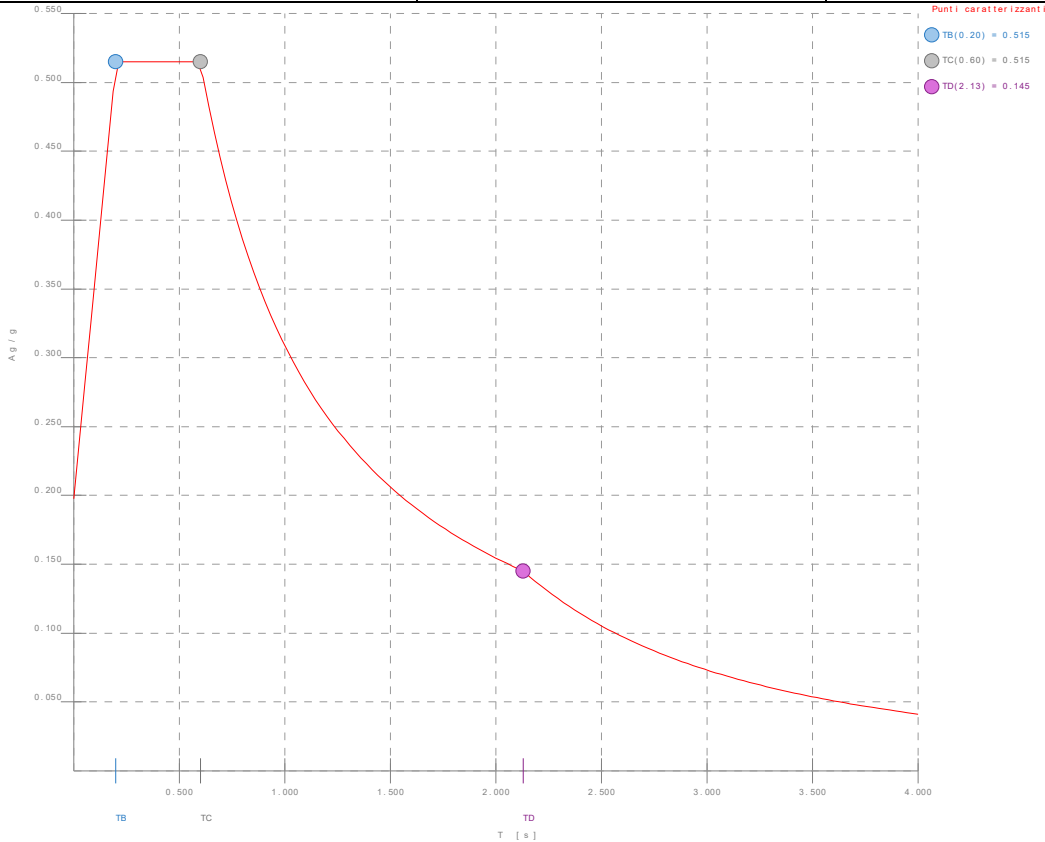


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>
- Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

- N = Numero
- Comm. = Commento
- 1 = G1 - Peso Proprio
- 2 = G2 - Permanenti non strutturali
- 3 = Q - Variabili neve
- 4 = Vento da retro - Cond. A
- 5 = Vento da retro - Cond. B
- 6 = Vento da fronte - Cond. C
- 7 = Vento da fronte - Cond. D
- F = azioni orizzontali convenzionali
- SLU = Stato limite ultimo
- SLR = Stato limite per combinazioni rare
- SLE F = Stato limite per combinazioni frequenti
- SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
- S = Si
- N = No

N/Comm.	1	2	3	4	5	6	7	S	SLU	SLR	SLE F	SLQ
1 Calcolo sismico	S	S	S	N	N	N	N	S	N	N	N	N
2 Calcolo statico	S	S	S	N	N	N	N	S	S	S	S	S
3 Vento da 270° - cond A	S	S	S	N	N	N	N	S	S	S	S	S
4 Vento da 270° - cond B	S	S	S	N	N	N	N	S	S	S	S	S
5 Vento da 90° - cond C	S	S	S	N	N	N	N	S	S	S	S	S
6 Vento da 90° - cond D	S	S	S	N	N	N	N	S	S	S	S	S

Elenco combinazioni di carico simboliche

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	1	2	3	4	5	6	7	S
1	Amb. 1 (Sisma)	SLU	S	1	ψ_2	----	----	----	----	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	----	----	----	----	----
3	Amb. 2 (SLE R)	SLE R	1	1	1	----	----	----	----	----
4	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	----	----	----	----	----
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	----	----	----	----	----
6	Amb. 3 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	γ max	----	----	----	----



7	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	-----
8	Amb. 3 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
9	Amb. 3 (SLE R)	SLE R	1	1	1	1	-----	-----	-----	-----
10	Amb. 3 (SLE F)	SLE F	1	1	ψ_2	ψ_1	-----	-----	-----	-----
11	Amb. 3 (SLE F)	SLE F	1	1	ψ_1	ψ_2	-----	-----	-----	-----
12	Amb. 3 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	-----	-----	-----	-----
13	Amb. 4 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
14	Amb. 4 (SLU)	SLU	γ max	γ max	γ max	-----	$\psi_0 * \gamma$ max	-----	-----	-----
15	Amb. 4 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
16	Amb. 4 (SLE R)	SLE R	1	1	1	1	-----	-----	-----	-----
17	Amb. 4 (SLE F)	SLE F	1	1	ψ_2	-----	ψ_1	-----	-----	-----
18	Amb. 4 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_2	-----	-----	-----
19	Amb. 4 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	-----	-----	-----
20	Amb. 5 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
21	Amb. 5 (SLU)	SLU	γ max	γ max	γ max	-----	$\psi_0 * \gamma$ max	-----	-----	-----
22	Amb. 5 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
23	Amb. 5 (SLE R)	SLE R	1	1	1	1	-----	-----	-----	-----
24	Amb. 5 (SLE F)	SLE F	1	1	ψ_2	-----	ψ_1	-----	-----	-----
25	Amb. 5 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_2	-----	-----	-----
26	Amb. 5 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	-----	-----	-----
27	Amb. 6 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	γ max	-----
28	Amb. 6 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	$\psi_0 * \gamma$ max	-----
29	Amb. 6 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
30	Amb. 6 (SLE R)	SLE R	1	1	1	1	-----	-----	ψ_0	-----
31	Amb. 6 (SLE F)	SLE F	1	1	ψ_2	-----	-----	-----	ψ_1	-----
32	Amb. 6 (SLE F)	SLE F	1	1	ψ_1	-----	-----	-----	ψ_2	-----
33	Amb. 6 (SLE Q)	SLE Q	1	1	ψ_2	-----	-----	-----	ψ_2	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: S1

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

An. = Tipo di analisi
 L = Lineare
 NL = Non lineare

Bk = Buckling
 S = Si
 N = No

CC = Numero della combinazione delle condizioni di carico elementari
 Comm. = Commento

TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	S X	S Y
1	Amb. 1 (SLU S) S +X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
2	Amb. 1 (SLE) S +X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
3	Amb. 1 (SLU S) S +X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
4	Amb. 1 (SLE) S +X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
5	Amb. 1 (SLU S) S -X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
6	Amb. 1 (SLE) S -X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
7	Amb. 1 (SLU S) S -X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
8	Amb. 1 (SLE) S -X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
9	Amb. 1 (SLU S) S +0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
10	Amb. 1 (SLE) S +0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
11	Amb. 1 (SLU S) S -0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
12	Amb. 1 (SLE) S -0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
13	Amb. 1 (SLU S) S +0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
14	Amb. 1 (SLE) S +0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
15	Amb. 1 (SLU S) S -0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
16	Amb. 1 (SLE) S -0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
17	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.00	0.00	0.00
18	Amb. 2 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
19	Amb. 2 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
20	Amb. 2 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	0.75	1.50	0.00	0.00	0.00	0.00	0.00
22	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
23	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	0.50	1.00	0.00	0.00	0.00	0.00	0.00
24	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
25	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.20	0.00	0.00	0.00	0.00	0.00
26	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
27	Amb. 3 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	1.50	0.00	0.00	0.00	0.00
29	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
30	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	1.00	0.00	0.00	0.00	0.00
31	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
32	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.20	0.00	0.00	0.00	0.00
33	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
34	Amb. 4 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	1.50	0.00	0.00	0.00
36	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
37	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00
38	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00
39	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00
40	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
41	Amb. 5 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	0.00	1.50	0.00	0.00
43	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.90	0.00	0.00
44	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00
45	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00
46	Amb. 6 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.20	0.00	0.00



47	Amb. 6 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
48	Amb. 6 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Elenco masse nodi

Simbologia
Mo = Massa orizzontale
Nodo = Numero del nodo

Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>		
-80	68.95	-79	68.95	-78	66.90	-77	66.90	-76	71.00	-75	71.00	-74	71.00	-73	71.00	-72	69.01	-71	46.74	-70	46.74
-69	46.74	-68	46.74	-67	69.01	-66	67.01	-65	67.01	-64	67.01	-63	67.01	-62	67.01	-61	67.01	-60	67.01	-59	67.01
-58	44.74	-57	44.74	-56	44.69	-55	44.69	-54	66.90	-53	66.90	-52	66.90	-51	66.90	-50	66.90	-49	66.90	-48	66.90
-47	66.90	-45	251.98	-29	160.41	-26	160.41	-18	102.67	-15	150.92	-14	150.92	-13	150.92	-12	150.92	-11	102.85	-10	102.71
-9	150.66	-8	150.66	-7	150.66	-6	150.66	-3	102.67	201	150.66	202	106.28	203	252.12						

Totali masse nodi

Mo <kg>	4829.94
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Elenco forze sismiche nodali allo SLD

Simbologia
Fx = Forza in dir. X
Fy = Forza in dir. Y
Nodo = Numero del nodo
cx = Coeff. c in dir. X
cy = Coeff. c in dir. Y

Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>
-80	0.02	0.02	19.62	19.62	-79	0.01	0.01	8.97	8.97	-78	0.02	0.02	19.03	19.03	-77	0.01	0.01	8.71	8.71	-76	0.01	0.01	9.24	9.24
-75	0.02	0.02	20.20	20.20	-74	0.01	0.01	9.24	9.24	-73	0.02	0.02	20.20	20.20	-72	0.02	0.02	19.63	19.63	-71	0.01	0.01	6.08	6.08
-70	0.01	0.01	13.30	13.30	-69	0.01	0.01	6.08	6.08	-68	0.01	0.01	13.30	13.30	-67	0.01	0.01	8.98	8.98	-66	0.01	0.01	8.72	8.72
-65	0.02	0.02	19.07	19.07	-64	0.01	0.01	8.72	8.72	-63	0.02	0.02	19.07	19.07	-62	0.01	0.01	8.72	8.72	-61	0.02	0.02	19.07	19.07
-60	0.01	0.01	8.72	8.72	-59	0.02	0.02	19.07	19.07	-58	0.01	0.01	5.82	5.82	-57	0.01	0.01	12.73	12.73	-56	0.01	0.01	5.81	5.81
-55	0.01	0.01	12.71	12.71	-54	0.01	0.01	8.71	8.71	-53	0.02	0.02	19.03	19.03	-52	0.01	0.01	8.71	8.71	-51	0.02	0.02	19.03	19.03
-50	0.01	0.01	8.71	8.71	-49	0.02	0.02	19.03	19.03	-48	0.01	0.01	8.71	8.71	-47	0.02	0.02	19.03	19.03	-45	0.05	0.05	52.24	52.24
-29	0.03	0.03	33.26	33.26	-26	0.03	0.03	33.25	33.25	-18	0.02	0.02	21.29	21.29	-15	0.03	0.03	31.29	31.29	-14	0.03	0.03	31.29	31.29
-13	0.03	0.03	31.29	31.29	-12	0.03	0.03	31.29	31.29	-11	0.02	0.02	21.32	21.32	-10	0.02	0.02	21.29	21.29	-9	0.03	0.03	31.23	31.23
-8	0.03	0.03	31.23	31.23	-7	0.03	0.03	31.23	31.23	-6	0.03	0.03	31.23	31.23	-3	0.02	0.02	21.29	21.29	201	0.03	0.03	31.23	31.23
202	0.02	0.02	22.03	22.03	203	0.05	0.05	52.27	52.27															

Totali forze sismiche

Fx <daN>	1001.30
Fy <daN>	1001.30

Elenco forze sismiche nodali allo SND

Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>
-80	0.02	0.02	47.80	47.80	-79	0.01	0.01	21.86	21.86	-78	0.02	0.02	46.38	46.38	-77	0.01	0.01	21.21	21.21	-76	0.01	0.01	22.51	22.51
-75	0.02	0.02	49.22	49.22	-74	0.01	0.01	22.51	22.51	-73	0.02	0.02	49.22	49.22	-72	0.02	0.02	47.84	47.84	-71	0.01	0.01	14.82	14.82
-70	0.01	0.01	32.40	32.40	-69	0.01	0.01	14.82	14.82	-68	0.01	0.01	32.40	32.40	-67	0.01	0.01	21.88	21.88	-66	0.01	0.01	21.25	21.25
-65	0.02	0.02	46.46	46.46	-64	0.01	0.01	21.25	21.25	-63	0.02	0.02	46.46	46.46	-62	0.01	0.01	21.25	21.25	-61	0.02	0.02	46.46	46.46
-60	0.01	0.01	21.25	21.25	-59	0.02	0.02	46.46	46.46	-58	0.01	0.01	14.19	14.19	-57	0.01	0.01	31.02	31.02	-56	0.01	0.01	14.17	14.17
-55	0.01	0.01	30.98	30.98	-54	0.01	0.01	21.21	21.21	-53	0.02	0.02	46.38	46.38	-52	0.01	0.01	21.21	21.21	-51	0.02	0.02	46.38	46.38
-50	0.01	0.01	21.21	21.21	-49	0.02	0.02	46.38	46.38	-48	0.01	0.01	21.21	21.21	-47	0.02	0.02	46.38	46.38	-45	0.05	0.05	127.29	127.29
-29	0.03	0.03	81.03	81.03	-26	0.03	0.03	81.03	81.03	-18	0.02	0.02	51.87	51.87	-15	0.03	0.03	76.24	76.24	-14	0.03	0.03	76.24	76.24
-13	0.03	0.03	76.24	76.24	-12	0.03	0.03	76.24	76.24	-11	0.02	0.02	51.95	51.95	-10	0.02	0.02	51.89	51.89	-9	0.03	0.03	76.11	76.11
-8	0.03	0.03	76.11	76.11	-7	0.03	0.03	76.11	76.11	-6	0.03	0.03	76.11	76.11	-3	0.02	0.02	51.87	51.87	201	0.03	0.03	76.11	76.11
202	0.02	0.02	53.69	53.69	203	0.05	0.05	127.36	127.36															

Totali forze sismiche

Fx <daN>	2439.92
Fy <daN>	2439.92

Domanda in duttilità di curvatura

Direzione X $\mu_{max}=1.20$
Direzione Y $\mu_{max}=1.20$

Reazioni vincolari

Simbologia
CC = Numero della combinazione delle condizioni di carico elementari
Fx = Reazione vincolare (forza) in dir. X
Fy = Reazione vincolare (forza) in dir. Y
Fz = Reazione vincolare (forza) in dir. Z
Mx = Reazione vincolare (momento) intorno all'asse X
My = Reazione vincolare (momento) intorno all'asse Y
Mz = Reazione vincolare (momento) intorno all'asse Z
Nodo = Numero del nodo
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SND = Stato limite di salvaguardia della vita (non dissipativo)

Nodo	CC	TCC	Fx <daN>	Fy <daN>	Fz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>											
2	Max	5	SND	897.96	21	SLU	3414.48	28	SLU	4354.62	28	SLU	7870.44	5	SND	1684.59	28	SLU	1.27
2	Min	1	SND	-1107.96	28	SLU	-2405.46	21	SLU	317.23	21	SLU	-11171.80	21	SND	-1937.71	1	SND	-1.80
3	Max	5	SND	797.32	21	SLU	2945.98	28	SLU	3780.41	28	SLU	6905.20	5	SND	1574.37	21	SLU	0.72
3	Min	1	SND	-684.59	28	SLU	-2075.41	21	SLU	250.53	21	SLU	-9801.71	28	SLU	-1475.60	1	SND	-0.51
315	Max	5	SND	744.64	21	SLU	3260.61	28	SLU	4160.11	28	SLU	7591.57	5	SND	1517.62	21	SLU	2.34
315	Min	1	SND	-647.37	28	SLU	-2297.06	21	SLU	244.65	21	SLU	-10776.00	28	SLU	-1435.74	1	SND	-1.65



Table with columns for load combination ID, type (Min./Max), and values for various parameters (e.g., 150.00, -99.17, 14.8.72, etc.).

Tipo di combinazione di carico: SLU

Table with columns for Asta, N1, N2, X, N, CC/Ty, CC/Mz, CC/Tz, CC/My, CC/Mx, and CC. It lists structural member details and associated values.



311	-59	-12	Max	150.00	-88.24	20	0.00	20	0.00	20	-61.78	20	-56.56	20	0.00	20
311	-59	-12	Min.	0.00	-19.47	20	0.00	20	0.00	20	-13.63	20	0.00	20	0.00	20
311	-59	-12	Min.	150.00	-88.24	20	0.00	20	0.00	20	-61.78	20	-56.56	20	0.00	20
312	-13	-62	Max	0.00	88.24	20	0.00	20	0.00	20	61.78	20	-56.56	20	0.00	20
312	-13	-62	Max	150.00	19.47	20	0.00	20	0.00	20	13.63	20	0.00	20	0.00	20
312	-13	-62	Min.	0.00	88.24	20	0.00	20	0.00	20	61.78	20	-56.56	20	0.00	20
312	-13	-62	Min.	150.00	19.47	20	0.00	20	0.00	20	13.63	20	0.00	20	0.00	20
312	-61	-13	Max	0.00	-19.47	20	0.00	20	0.00	20	-13.63	20	0.00	20	0.00	20
312	-61	-13	Max	150.00	-88.24	20	0.00	20	0.00	20	-61.78	20	-56.56	20	0.00	20
312	-61	-13	Min.	0.00	-19.47	20	0.00	20	0.00	20	-13.63	20	0.00	20	0.00	20
312	-61	-13	Min.	150.00	-88.24	20	0.00	20	0.00	20	-61.78	20	-56.56	20	0.00	20
313	-14	-64	Max	0.00	88.24	20	0.00	20	0.00	20	61.78	20	-56.56	20	0.00	20
313	-14	-64	Max	150.00	19.47	20	0.00	20	0.00	20	13.63	20	0.00	20	0.00	20
313	-14	-64	Min.	0.00	88.24	20	0.00	20	0.00	20	61.78	20	-56.56	20	0.00	20
313	-14	-64	Min.	150.00	19.47	20	0.00	20	0.00	20	13.63	20	0.00	20	0.00	20
313	-63	-14	Max	0.00	-19.47	20	0.00	20	0.00	20	-13.63	20	0.00	20	0.00	20
313	-63	-14	Max	150.00	-88.24	20	0.00	20	0.00	20	-61.78	20	-56.56	20	0.00	20
313	-63	-14	Min.	0.00	-19.47	20	0.00	20	0.00	20	-13.63	20	0.00	20	0.00	20
313	-63	-14	Min.	150.00	-88.24	20	0.00	20	0.00	20	-61.78	20	-56.56	20	0.00	20
314	-15	-66	Max	0.00	88.24	20	0.00	20	0.00	20	61.78	20	-56.56	20	0.00	20
314	-15	-66	Max	150.00	19.47	20	0.00	20	0.00	20	13.63	20	0.00	20	0.00	20
314	-15	-66	Min.	0.00	88.24	20	0.00	20	0.00	20	61.78	20	-56.56	20	0.00	20
314	-15	-66	Min.	150.00	19.47	20	0.00	20	0.00	20	13.63	20	0.00	20	0.00	20
314	-65	-15	Max	0.00	-19.47	20	0.00	20	0.00	20	-13.63	20	0.00	20	0.00	20
314	-65	-15	Max	150.00	-88.24	20	0.00	20	0.00	20	-61.78	20	-56.56	20	0.00	20
314	-65	-15	Min.	0.00	-19.47	20	0.00	20	0.00	20	-13.63	20	0.00	20	0.00	20
314	-65	-15	Min.	150.00	-88.24	20	0.00	20	0.00	20	-61.78	20	-56.56	20	0.00	20
315	203	-67	Max	0.00	90.57	20	0.00	20	0.00	20	63.42	20	-58.24	20	0.00	20
315	203	-67	Max	150.00	20.34	20	0.00	20	0.00	20	14.24	20	0.00	20	0.00	20
315	203	-67	Min.	0.00	90.57	20	0.00	20	0.00	20	63.42	20	-58.24	20	0.00	20
315	203	-67	Min.	150.00	20.34	20	0.00	20	0.00	20	14.24	20	0.00	20	0.00	20
315	-72	203	Max	0.00	-20.34	20	0.00	20	0.00	20	-14.24	20	0.00	20	0.00	20
315	-72	203	Max	150.00	-90.57	20	0.00	20	0.00	20	-63.42	20	-58.24	20	0.00	20
315	-72	203	Min.	0.00	-20.34	20	0.00	20	0.00	20	-14.24	20	0.00	20	0.00	20
315	-72	203	Min.	150.00	-90.57	20	0.00	20	0.00	20	-63.42	20	-58.24	20	0.00	20
316	-26	-74	Max	0.00	92.90	20	0.00	20	0.00	20	65.05	20	-59.93	20	0.00	20
316	-26	-74	Max	150.00	21.21	20	0.00	20	0.00	20	14.85	20	0.00	20	0.00	20
316	-26	-74	Min.	0.00	92.90	20	0.00	20	0.00	20	65.05	20	-59.93	20	0.00	20
316	-26	-74	Min.	150.00	21.21	20	0.00	20	0.00	20	14.85	20	0.00	20	0.00	20
316	-73	-26	Max	0.00	-21.21	20	0.00	20	0.00	20	-14.85	20	0.00	20	0.00	20
316	-73	-26	Max	150.00	-92.90	20	0.00	20	0.00	20	-65.05	20	-59.93	20	0.00	20
316	-73	-26	Min.	0.00	-21.21	20	0.00	20	0.00	20	-14.85	20	0.00	20	0.00	20
316	-73	-26	Min.	150.00	-92.90	20	0.00	20	0.00	20	-65.05	20	-59.93	20	0.00	20
317	-18	-71	Max	0.00	64.51	20	0.00	20	0.00	20	45.17	20	-39.45	20	0.00	20
317	-18	-71	Max	150.00	10.60	20	0.00	20	0.00	20	7.42	20	0.00	20	0.00	20
317	-18	-71	Min.	0.00	64.51	20	0.00	20	0.00	20	45.17	20	-39.45	20	0.00	20
317	-18	-71	Min.	150.00	10.60	20	0.00	20	0.00	20	7.42	20	0.00	20	0.00	20
317	-70	-18	Max	0.00	-10.60	20	0.00	20	0.00	20	-7.43	20	0.00	20	0.00	20
317	-70	-18	Max	150.00	-64.51	20	0.00	20	0.00	20	-45.17	20	-39.45	20	0.00	20
317	-70	-18	Min.	0.00	-10.60	20	0.00	20	0.00	20	-7.43	20	0.00	20	0.00	20
317	-70	-18	Min.	150.00	-64.51	20	0.00	20	0.00	20	-45.17	20	-39.45	20	0.00	20

Verifiche aste in acciaio

Simbologia

Φ_{LT}	=	Coefficiente Φ per stabilità laterale membrature inflesse
Φ_y	=	Coefficiente Φ per inflessione intorno all'asse y(c)
Φ_z	=	Coefficiente Φ per inflessione intorno all'asse z(e)
α_{imp}	=	Coefficiente di imperfezione
$\alpha_{my}, \alpha_{mz}, \alpha_{LT}$	=	Coefficienti correttivi per il momento flettente
β_{LT}	=	Coefficiente per calcolo Φ_{LT}
χ_{LT}	=	Coefficiente di riduzione per stabilità laterale membrature inflesse
χ_y	=	Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
χ_z	=	Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
δ	<cm>	=Spostamento relativo asta
λ_y	=	Snellezza adimensionale per inflessione intorno all'asse y(c)
λ_z	=	Snellezza adimensionale per inflessione intorno all'asse z(e)
λ_{LT}	=	Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$	=	Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
λ_y	=	Snellezza per inflessione intorno all'asse y(c)
λ_z	=	Snellezza per inflessione intorno all'asse z(e)
$\sigma_{D,max}$	<daN/cm²>	=Tensione ideale massima
σ_M	<daN/cm²>	=Tensione normale per momento flettente
σ_N	<daN/cm²>	=Tensione normale per sforzo normale
τ	<daN/cm²>	=Tensione tangenziale per taglio e/o torsione
ψ	=	Coeff. di correzione momento critico per stabilità laterale membrature inflesse
A_{eff}	<cm²>	=Area effettiva per trazione
A_{net}	<cm²>	=Area netta per compressione
Area	=	Area
$A_{tag,y}$	<cm²>	=Area resistente a taglio in dir. Y
$A_{tag,z}$	<cm²>	=Area resistente a taglio in dir. Z
CC	=	Numero della combinazione delle condizioni di carico elementari
Cod.	=	Codice
Curva	=	Curva di instabilità adottata
D	<cm>	=Distanza
F_{yk}	<daN/cm²>	=Tensione caratteristica di snervamento dell'acciaio
F_{yt}	<daN/cm²>	=Tensione caratteristica di rottura
I_y	<cm⁴>	=Raggio giratorio d'inerzia rispetto all'asse Y
I_z	<cm⁴>	=Raggio giratorio d'inerzia rispetto all'asse Z
J_0	<cm⁶>	=Costante di ingobbamento
J_y	<cm⁴>	=Momento d'inerzia rispetto all'asse Y
J_z	<cm⁴>	=Momento d'inerzia rispetto all'asse Z
$K_{yy}, K_{yz}, K_{zy}, K_{zz}$	=	Coefficienti di interazione
L	<cm>	=Lunghezza dell'asta
L_{cr}	<cm>	=Lunghezza di libera inflessione laterale fra ritegni torsionali
M_{cr}	<daNm>	=Momento critico per instabilità flesso torsionale
M_{Ny}, c, Rd	<daNm>	=Resistenza di calcolo a pressoflessione intorno all'asse Y
M_x	<daNm>	=Momento torcente intorno all'asse X
M_y	<daNm>	=Momento flettente intorno all'asse Y
M_y, Ed	<daNm>	=Momento flettente di calcolo intorno all'asse Y



My,V,c,Rd	<daNm>	= Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y
Mz	<daNm>	= Momento flettente intorno all'asse Z
Mz,Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Z
N	<daN>	= Sforzo normale
N,Ed	<daN>	= Forza assiale di calcolo
Nc,Rd	<daN>	= Resistenza a compressione
Ncr,y	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
Ncr,z	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
Sez.		= Numero della sezione
Tipo		= Tipologia
		Rc = Rettangolare cava
		Is = I stondata
Tp		= Tipo di acciaio
Ty	<daN>	= Taglio in dir. Y
Tz	<daN>	= Taglio in dir. Z
V,Ed	<daN>	= Forza di taglio di calcolo
Vc,Rd	<daN>	= Resistenza a taglio
Vc,Rd,Red	<daN>	= Resistenza a taglio ridotta
Wy,plac	<cmc>	= Modulo di resistenza plastico intorno all'asse Y
Wymin	<cmc>	= Modulo di resistenza minimo rispetto all'asse Y
Wz,plac	<cmc>	= Modulo di resistenza plastico intorno all'asse Z
Wzmin	<cmc>	= Modulo di resistenza minimo rispetto all'asse Z
Xl	<m>	= Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
f		= Fattore di modifica per il coefficiente di riduzione
fz,g	<cm>	= Freccia in direzione Z globale
fz,l	<cm>	= Freccia in direzione Z locale
kc		= Coeff. di correzione momento flettente per stabilità laterale membrature inflesse

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D	Area	Anet	Aeff	Jy	Jz	Iy	Iz	Wymin	Wzmin	TP	Fyk	Fyt
			<cm>	<cmq>	<cmq>	<cmq>	<cm4>	<cm4>	<cm>	<cm>	<cmc>	<cmc>		<daN/cmq>	<daN/cmq>
1	COL HEA240	Is	--	76.84	76.84	76.84	7763.40	2768.81	10.05	6.00	675.08	230.73	S355 UNI EN 10025-2	3550.00	5100.00
2	TRV PRINC SHS200x200x8	Rc	--	61.44	61.44	61.44	3781.43	3781.43	7.85	7.85	378.14	378.14	S355H UNI EN 10210-1	3550.00	5100.00
3	TRV SEC RHS150x100x8	Rc	--	37.44	37.44	37.44	1128.23	588.15	5.49	3.96	150.43	117.63	S355H UNI EN 10210-1	3550.00	5100.00

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy,plac	Wz,plac	Atag,y	Atag,z	J0
		<cmc>	<cmc>	<cmq>	<cmq>	<cm6>
1	COL HEA240	747.99	352.10	64.54	25.18	328486.00
2	TRV PRINC SHS200x200x8	442.62	442.62	30.72	30.72	
3	TRV SEC RHS150x100x8	185.42	138.62	14.98	22.46	

Asta n. 1 (315 -45) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1906.11 T_s=-269.52 M_y=-937.05 T_y=-744.64 M_z=1517.62
Tensioni: σ_N=-24.81 σ_{m,d}=-796.54 τ=0.00 σ_{max}=821.35 (sfrut=0.24)
Tensioni: σ_N=-24.81 σ_{m,d}=259.98 τ=18.67 τ_{max}=18.67 (sfrut=0.01)
Tensioni: σ_N=-24.81 σ_{m,d}=-796.54 τ=0.00 σ_{ID,max}=821.35 (sfrut=0.24)
- Verifica a taglio Dir. Y [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
Sollecitazioni: T_y=-92.39
V,Ed=-92.39 Vc,Rd=125981.00 V,Ed/Vc,Rd=0.00
- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=-244.65 T_s=-3260.61 M_y=-10776.00 T_y=37.75 M_z=-39.83 M_x=-2.34
Tensioni: σ_N=-3.18 σ_{m,d}=-1613.52 τ=7.52 σ_{max}=1616.70 (sfrut=0.48)
Tensioni: σ_N=-3.18 σ_{m,d}=-0.54 τ=221.91 τ_{max}=221.91 (sfrut=0.11)
Tensioni: σ_N=-3.18 σ_{m,d}=-1613.52 τ=7.52 σ_{ID,max}=1616.76 (sfrut=0.48)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
Sollecitazioni: N,Ed=-244.65 My,Ed=-10776.00 Mz,Ed=84.75 L=3.30
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
L_{cr}=3.30 Curva b: α_{lmp}=0.34 k_c=0.94 ψ=1.75 M,cr=122181.00 λ_{LT}=0.44
λ_{LT,0}=0.40 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=32.83 Ncr,y=1477550.00 λ_y'=0.43 Curva b: Φ_y=0.63 χ_y=0.91
λ_z=54.97 Ncr,z=526968.00 λ_z'=0.72 Curva c: Φ_z=0.89 χ_z=0.71
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.45+0.01=0.46
Verifica ZZ: 0.00+0.36+0.01=0.37
- Verifica Spostamento relativo massimo per singola asta - CC 23
δ=1.65 (L/199)

Asta n. 2 (2 202) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1723.86 T_s=260.09 M_y=902.12 T_y=1107.96 M_z=-1937.71
Tensioni: σ_N=-22.43 σ_{m,d}=-973.43 τ=0.00 σ_{max}=995.87 (sfrut=0.29)
Tensioni: σ_N=-22.43 σ_{m,d}=-292.90 τ=27.67 τ_{max}=27.67 (sfrut=0.01)
Tensioni: σ_N=-22.43 σ_{m,d}=-973.43 τ=0.00 σ_{ID,max}=995.87 (sfrut=0.29)
- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 21 SLU Xl=1.20 - Classe 2
Sollecitazioni: T_y=-3.60 M_x=1.80
V,Ed=-3.60 Vc,Rd,Red=125831.00 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 21 SLU Xl=1.20 - Classe 2
Sollecitazioni: T_z=-3414.48 M_x=1.80
V,Ed=-3414.48 Vc,Rd,Red=49090.00 V,Ed/Vc,Rd,Red=0.07
- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=-317.23 T_s=-3414.48 M_y=-11171.80 T_y=-3.60 M_z=5.08 M_x=1.80
Tensioni: σ_N=-4.13 σ_{m,d}=-1657.10 τ=5.80 σ_{max}=1661.23 (sfrut=0.49)
Tensioni: σ_N=-4.13 σ_{m,d}=0.07 τ=232.32 τ_{max}=232.32 (sfrut=0.12)
Tensioni: σ_N=-4.13 σ_{m,d}=-1657.10 τ=5.80 σ_{ID,max}=1661.26 (sfrut=0.49)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
Sollecitazioni: N,Ed=-317.23 My,Ed=-11171.80 Mz,Ed=-6.79 L=3.30
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
L_{cr}=3.30 Curva b: α_{lmp}=0.34 k_c=0.94 ψ=1.76 M,cr=122921.00 λ_{LT}=0.44
λ_{LT,0}=0.40 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00

$\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.47+0.00=0.47
 Verifica ZZ: 0.00+0.37+0.00=0.37

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=1.71$ (L/193)

Asta n. 3 (3 203) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-1259.65 $T_x=248.76$ $M_y=868.16$ $T_y=-797.32$ $M_z=1574.37$
 Tensioni: $\sigma_N=-16.39$ $\sigma_{m,d}=-810.93$ $\tau=0.00$ $\sigma_{max}=-827.33$ (sfrut=0.24)
 Tensioni: $\sigma_N=-16.39$ $\sigma_{m,d}=25.55$ $\tau=19.96$ $\tau_{max}=19.96$ (sfrut=0.01)
 Tensioni: $\sigma_N=-16.39$ $\sigma_{m,d}=-810.93$ $\tau=0.00$ $\sigma_{ID,max}=827.33$ (sfrut=0.24)

- Verifica a taglio Dir. Y [4.2.16] - CC 17 SLU Xl=0.00 - Classe 2
 Sollecitazioni: $T_y=-84.57$
 $V_{Ed}=-84.57$ $V_{c,Rd}=125981.00$ $V_{Ed/V_{c,Rd}}=0.00$

- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-250.53 $T_x=-2945.98$ $M_y=-9801.71$ $T_y=-34.16$ $M_z=38.27$
 Tensioni: $\sigma_N=-3.26$ $\sigma_{m,d}=-1468.52$ $\tau=0.00$ $\sigma_{max}=-1471.78$ (sfrut=0.44)
 Tensioni: $\sigma_N=-3.26$ $\sigma_{m,d}=0.52$ $\tau=200.38$ $\tau_{max}=200.38$ (sfrut=0.10)
 Tensioni: $\sigma_N=-3.26$ $\sigma_{m,d}=-1468.52$ $\tau=0.00$ $\sigma_{ID,max}=1471.78$ (sfrut=0.44)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3
 Sollecitazioni: N,Ed=-250.53 $M_y,Ed=-9801.71$ $M_z,Ed=-74.45$ L=3.30
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $L_{cr}=3.30$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.74$ $M_{cr}=121692.00$ $\lambda_{LT}=0.44$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.58$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.41+0.01=0.42
 Verifica ZZ: 0.00+0.33+0.01=0.34

- Verifica Spostamento relativo massimo per singola asta - CC 23
 $\delta=1.51$ (L/218)

Asta n. 201 (-3 -29) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=1.45 - Classe 3
 Sollecitazioni: N=29.73 $T_x=-227.34$ $M_y=285.11$ $T_y=-99.09$ $M_z=-148.02$ $M_x=-21.60$
 Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=114.54$ $\tau=3.66$ $\sigma_{max}=115.02$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=-36.01$ $\tau=11.98$ $\tau_{max}=11.98$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=114.54$ $\tau=3.66$ $\sigma_{ID,max}=115.02$ (sfrut=0.03)

- Verifica a taglio Dir. Y [4.2.16] - CC 28 SLU Xl=0.00
 Sollecitazioni: $T_y=240.66$
 $V_{Ed}=240.66$ $V_{c,Rd}=59967.00$ $V_{Ed/V_{c,Rd}}=0.00$

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00
 Sollecitazioni: $T_z=-409.50$
 $V_{Ed}=-409.50$ $V_{c,Rd}=59967.00$ $V_{Ed/V_{c,Rd}}=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.45 - Classe 3
 Sollecitazioni: $T_x=-500.29$ $M_y=658.68$ $T_y=240.66$ $M_z=348.47$
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-266.34$ $\tau=0.00$ $\sigma_{max}=-266.34$ (sfrut=0.08)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=84.78$ $\tau=18.31$ $\tau_{max}=18.31$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-266.34$ $\tau=0.00$ $\sigma_{ID,max}=266.34$ (sfrut=0.08)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $M_y,Ed=658.68$ $M_z,Ed=348.47$ L=1.45
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=18.46$ Ncr,y=3737980.00 $\lambda'_y=0.24$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=18.46$ Ncr,z=3737980.00 $\lambda'_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.05+0.03=0.07
 Verifica ZZ: 0.00+0.04+0.03=0.07

Asta n. 201 (-29 -45) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=1.45 - Classe 3
 Sollecitazioni: N=75.56 $T_x=-524.01$ $M_y=1003.16$ $T_y=-251.86$ $M_z=-519.60$ $M_x=-54.42$
 Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=402.69$ $\tau=9.23$ $\sigma_{max}=403.92$ (sfrut=0.12)
 Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=-126.42$ $\tau=28.40$ $\tau_{max}=28.40$ (sfrut=0.01)
 Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=402.69$ $\tau=9.23$ $\sigma_{ID,max}=404.24$ (sfrut=0.12)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.45 - Classe 1
 Sollecitazioni: $T_z=-857.02$
 $V_{Ed}=-857.02$ $V_{c,Rd}=59967.00$ $V_{Ed/V_{c,Rd}}=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.45 - Classe 3
 Sollecitazioni: $T_x=-1295.45$ $M_y=2468.76$ $T_y=721.97$ $M_z=1393.89$
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-1021.48$ $\tau=0.00$ $\sigma_{max}=-1021.48$ (sfrut=0.30)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=339.12$ $\tau=47.41$ $\tau_{max}=47.41$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-1021.48$ $\tau=0.00$ $\sigma_{ID,max}=1021.48$ (sfrut=0.30)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $M_y,Ed=2468.76$ $M_z,Ed=1393.89$ L=1.45
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=18.46$ Ncr,y=3737980.00 $\lambda'_y=0.24$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=18.46$ Ncr,z=3737980.00 $\lambda'_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.18+0.10=0.29
 Verifica ZZ: 0.00+0.15+0.10=0.25

Asta n. 202 (-45 201) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-295.83 T_x=971.89 M_y=2012.83 T_y=134.88 M_z=-212.83 M_x=21.74
Tensioni: $\sigma_N=-4.81$ $\sigma_{m,d}=-588.58$ $\tau=3.69$ $\sigma_{max}=-593.39$ (sfrut=0.18)
Tensioni: $\sigma_N=-4.81$ $\sigma_{m,d}=-51.78$ $\tau=39.24$ $\tau_{max}=39.24$ (sfrut=0.02)
Tensioni: $\sigma_N=-4.81$ $\sigma_{m,d}=-588.58$ $\tau=3.69$ $\sigma_{TD,max}=593.43$ (sfrut=0.18)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=1254.06
V,Ed=1254.06 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=-165.10 T_x=1939.20 M_y=2866.49 T_y=-1114.11 M_z=1395.53 M_x=-11.25
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-1127.09$ $\tau=1.91$ $\sigma_{max}=-1129.78$ (sfrut=0.33)
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-339.52$ $\tau=72.88$ $\tau_{max}=72.88$ (sfrut=0.04)
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-1127.09$ $\tau=1.91$ $\sigma_{TD,max}=1129.78$ (sfrut=0.33)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: N,Ed=-165.10 M_y,Ed=2866.49 M_z,Ed=1395.53 L=1.33
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.21+0.10=0.32
Verifica ZZ: 0.00+0.17+0.10=0.27
- Asta n. 202 (201 -6) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.33 - Classe 3
Sollecitazioni: N=54.85 T_x=191.77 M_y=-794.11 T_y=46.20 M_z=108.97 M_x=20.07
Tensioni: $\sigma_N=0.89$ $\sigma_{m,d}=238.82$ $\tau=3.40$ $\sigma_{max}=239.71$ (sfrut=0.07)
Tensioni: $\sigma_N=0.89$ $\sigma_{m,d}=26.51$ $\tau=10.42$ $\tau_{max}=10.42$ (sfrut=0.01)
Tensioni: $\sigma_N=0.89$ $\sigma_{m,d}=238.82$ $\tau=3.40$ $\sigma_{TD,max}=239.79$ (sfrut=0.07)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=783.99
V,Ed=783.99 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.33 - Classe 3
Sollecitazioni: N=-165.10 T_x=1118.41 M_y=-1186.89 T_y=-673.46 M_z=-974.20 M_x=-11.25
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-571.50$ $\tau=1.91$ $\sigma_{max}=-574.19$ (sfrut=0.17)
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=237.02$ $\tau=42.84$ $\tau_{max}=42.84$ (sfrut=0.02)
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-571.50$ $\tau=1.91$ $\sigma_{TD,max}=574.20$ (sfrut=0.17)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: N,Ed=-165.10 M_y,Ed=-1186.89 M_z,Ed=-974.20 L=1.33
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.09+0.07=0.16
Verifica ZZ: 0.00+0.07+0.07=0.14
- Asta n. 202 (-6 -7) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.33 - Classe 3
Sollecitazioni: N=-60.70 T_x=65.71 M_y=-682.35 T_y=79.41 M_z=409.79 M_x=24.43
Tensioni: $\sigma_N=-0.99$ $\sigma_{m,d}=-288.82$ $\tau=4.14$ $\sigma_{max}=-289.81$ (sfrut=0.09)
Tensioni: $\sigma_N=-0.99$ $\sigma_{m,d}=166.01$ $\tau=7.05$ $\tau_{max}=7.05$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.99$ $\sigma_{m,d}=-288.82$ $\tau=4.14$ $\sigma_{TD,max}=289.89$ (sfrut=0.09)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=313.91
V,Ed=313.91 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.33 - Classe 3
Sollecitazioni: N=-165.10 T_x=380.75 M_y=-1746.69 T_y=-232.81 M_z=-1282.81 M_x=-11.25
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-801.15$ $\tau=1.91$ $\sigma_{max}=-803.84$ (sfrut=0.24)
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=312.10$ $\tau=15.84$ $\tau_{max}=15.84$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-801.15$ $\tau=1.91$ $\sigma_{TD,max}=803.85$ (sfrut=0.24)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: N,Ed=-165.10 M_y,Ed=-1746.69 M_z,Ed=-1282.81 L=1.33
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.13+0.10=0.23
Verifica ZZ: 0.00+0.10+0.10=0.20
- Asta n. 202 (-7 -8) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-103.81 T_x=-149.41 M_y=-691.63 T_y=-64.28 M_z=416.29 M_x=-6.50
Tensioni: $\sigma_N=-1.69$ $\sigma_{m,d}=-292.99$ $\tau=1.10$ $\sigma_{max}=-294.68$ (sfrut=0.09)
Tensioni: $\sigma_N=-1.69$ $\sigma_{m,d}=101.28$ $\tau=6.57$ $\tau_{max}=6.57$ (sfrut=0.00)
Tensioni: $\sigma_N=-1.69$ $\sigma_{m,d}=-292.99$ $\tau=1.10$ $\sigma_{TD,max}=294.69$ (sfrut=0.09)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_z=-239.28
V,Ed=-239.28 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=-165.10 T_x=-273.80 M_y=-1746.70 T_y=207.84 M_z=-1282.82 M_x=-11.25
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-801.16$ $\tau=1.91$ $\sigma_{max}=-803.84$ (sfrut=0.24)
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-312.10$ $\tau=11.93$ $\tau_{max}=11.93$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-801.16$ $\tau=1.91$ $\sigma_{TD,max}=803.85$ (sfrut=0.24)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: N,Ed=-165.10 M_y,Ed=-1746.70 M_z,Ed=-1282.82 L=1.33

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.13+0.10=0.23
 Verifica ZZ: 0.00+0.10+0.10=0.20

Asta n. 202 (-8 -9) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=49.64 T_z=-297.33 M_y=-537.76 T_y=207.99 M_z=-337.56 M_x=37.42
 Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=231.48$ $\tau=6.34$ $\sigma_{max}=232.29$ (sfrut=0.07)
 Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=82.13$ $\tau=17.23$ $\tau_{max}=17.23$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=231.48$ $\tau=6.34$ $\sigma_{ID,max}=232.55$ (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.33 - Classe 1
 Sollecitazioni: T_z=-709.36
 V,Ed=-709.36 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
 Sollecitazioni: N=-165.10 T_z=-1011.47 M_y=-1328.63 T_y=648.49 M_z=-1007.29 M_x=-11.24
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-617.73$ $\tau=1.91$ $\sigma_{max}=-620.42$ (sfrut=0.18)
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-245.07$ $\tau=38.93$ $\tau_{max}=38.93$ (sfrut=0.02)
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-617.73$ $\tau=1.91$ $\sigma_{ID,max}=620.43$ (sfrut=0.18)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-165.10 My,Ed=-1328.63 Mz,Ed=-1007.29 L=1.33
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.10+0.07=0.17
 Verifica ZZ: 0.00+0.08+0.07=0.15

Asta n. 202 (-9 -10) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.33 - Classe 3
 Sollecitazioni: N=-519.94 T_z=-924.45 M_y=1595.09 T_y=-126.24 M_z=-130.91 M_x=-17.04
 Tensioni: $\sigma_N=-8.46$ $\sigma_{m,d}=-456.44$ $\tau=2.89$ $\sigma_{max}=-464.91$ (sfrut=0.14)
 Tensioni: $\sigma_N=-8.46$ $\sigma_{m,d}=-31.85$ $\tau=36.71$ $\tau_{max}=36.71$ (sfrut=0.02)
 Tensioni: $\sigma_N=-8.46$ $\sigma_{m,d}=-456.44$ $\tau=2.89$ $\sigma_{ID,max}=464.93$ (sfrut=0.14)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.33 - Classe 1
 Sollecitazioni: T_z=-1179.43
 V,Ed=-1179.43 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.33 - Classe 3
 Sollecitazioni: N=-165.10 T_z=-1832.25 M_y=2441.11 T_y=1089.13 M_z=1296.17 M_x=-11.24
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-988.33$ $\tau=1.91$ $\sigma_{max}=-991.01$ (sfrut=0.29)
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=315.35$ $\tau=68.96$ $\tau_{max}=68.96$ (sfrut=0.04)
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-988.33$ $\tau=1.91$ $\sigma_{ID,max}=991.02$ (sfrut=0.29)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-165.10 My,Ed=2441.11 Mz,Ed=1296.17 L=1.33
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.90$ Ncr,y=4459710.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.90$ Ncr,z=4459710.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.18+0.10=0.28
 Verifica ZZ: 0.00+0.15+0.10=0.24

Asta n. 202 (-10 202) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.20 - Classe 3
 Sollecitazioni: N=-616.98 T_z=-1085.74 M_y=1790.66 T_y=-155.35 M_z=-147.53 M_x=-23.24
 Tensioni: $\sigma_N=-10.04$ $\sigma_{m,d}=-512.55$ $\tau=3.94$ $\sigma_{max}=-522.60$ (sfrut=0.15)
 Tensioni: $\sigma_N=-10.04$ $\sigma_{m,d}=-35.89$ $\tau=43.66$ $\tau_{max}=43.66$ (sfrut=0.02)
 Tensioni: $\sigma_N=-10.04$ $\sigma_{m,d}=-512.55$ $\tau=3.94$ $\sigma_{ID,max}=522.64$ (sfrut=0.15)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.20 - Classe 1
 Sollecitazioni: T_z=-1442.76
 V,Ed=-1442.76 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.20 - Classe 3
 Sollecitazioni: N=-165.10 T_z=-2229.37 M_y=2885.80 T_y=1309.46 M_z=1558.10 M_x=-11.24
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-1175.19$ $\tau=1.91$ $\sigma_{max}=-1177.88$ (sfrut=0.35)
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=379.08$ $\tau=83.50$ $\tau_{max}=83.50$ (sfrut=0.04)
 Tensioni: $\sigma_N=-2.69$ $\sigma_{m,d}=-1175.19$ $\tau=1.91$ $\sigma_{ID,max}=1177.88$ (sfrut=0.35)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: N,Ed=-165.10 My,Ed=2885.80 Mz,Ed=1558.10 L=0.20
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=2.55$ Ncr,y=195931000.00 $\lambda'_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=2.55$ Ncr,z=195931000.00 $\lambda'_z=0.03$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.21+0.12=0.33
 Verifica ZZ: 0.00+0.17+0.12=0.29

Asta n. 203 (202 -11) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-324.56 T_z=1018.42 M_y=1668.44 T_y=-87.81 M_z=147.35 M_x=-22.01
 Tensioni: $\sigma_N=-5.28$ $\sigma_{m,d}=-480.19$ $\tau=3.73$ $\sigma_{max}=-485.47$ (sfrut=0.14)
 Tensioni: $\sigma_N=-5.28$ $\sigma_{m,d}=-35.85$ $\tau=40.99$ $\tau_{max}=40.99$ (sfrut=0.02)
 Tensioni: $\sigma_N=-5.28$ $\sigma_{m,d}=-480.19$ $\tau=3.73$ $\sigma_{ID,max}=485.51$ (sfrut=0.14)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=1218.65
 V,Ed=1218.65 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=112.74 T_x=1879.24 M_y=2304.58 T_y=-1096.00 M_z=1556.83 M_x=56.34
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=1021.15$ $\tau=9.55$ $\sigma_{max}=1022.98$ (sfrut=0.30)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=378.77$ $\tau=78.32$ $\tau_{max}=78.32$ (sfrut=0.04)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=1021.15$ $\tau=9.55$ $\sigma_{TD,max}=1023.12$ (sfrut=0.30)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: My,Ed=2304.58 Mz,Ed=1556.83 L=0.20
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=2.55$ Ncr,y=195931000.00 $\lambda'_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=2.55$ Ncr,z=195931000.00 $\lambda'_z=0.03$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.17+0.12=0.29
Verifica ZZ: 0.00+0.14+0.12=0.25

Asta n. 203 (-11 -12) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-227.41 T_x=856.97 M_y=1486.40 T_y=105.05 M_z=-129.50 M_x=6.77
Tensioni: $\sigma_N=-3.70$ $\sigma_{m,d}=-427.33$ $\tau=1.15$ $\sigma_{max}=-431.03$ (sfrut=0.13)
Tensioni: $\sigma_N=-3.70$ $\sigma_{m,d}=-31.51$ $\tau=32.50$ $\tau_{max}=32.50$ (sfrut=0.02)
Tensioni: $\sigma_N=-3.70$ $\sigma_{m,d}=-427.33$ $\tau=1.15$ $\sigma_{TD,max}=431.03$ (sfrut=0.13)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_y=1242.21 M_x=-79.98
V,Ed=1242.21 Vc,Rd,Red=59550.40 V,Ed/Vc,Rd,Red=0.02

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_z=-70.61 M_x=-79.98
V,Ed=-70.61 Vc,Rd,Red=59550.40 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=112.74 T_x=1481.43 M_y=1929.98 T_y=-875.12 M_z=1337.63 M_x=56.34
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=864.12$ $\tau=9.55$ $\sigma_{max}=865.96$ (sfrut=0.26)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=325.44$ $\tau=63.77$ $\tau_{max}=63.77$ (sfrut=0.03)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=864.12$ $\tau=9.55$ $\sigma_{TD,max}=866.11$ (sfrut=0.26)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: My,Ed=1929.98 Mz,Ed=1337.63 L=1.33
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=16.94$ Ncr,y=4437370.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.94$ Ncr,z=4437370.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.14+0.10=0.24
Verifica ZZ: 0.00+0.11+0.10=0.21

Asta n. 203 (-12 -13) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.33 - Classe 3
Sollecitazioni: N=98.31 T_x=143.14 M_y=-350.51 T_y=-135.87 M_z=-135.80 M_x=-5.30
Tensioni: $\sigma_N=1.60$ $\sigma_{m,d}=128.60$ $\tau=0.90$ $\sigma_{max}=130.21$ (sfrut=0.04)
Tensioni: $\sigma_N=1.60$ $\sigma_{m,d}=33.04$ $\tau=6.14$ $\tau_{max}=6.14$ (sfrut=0.00)
Tensioni: $\sigma_N=1.60$ $\sigma_{m,d}=128.60$ $\tau=0.90$ $\sigma_{TD,max}=130.21$ (sfrut=0.04)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=615.15 M_x=-79.98
V,Ed=615.15 Vc,Rd,Red=59550.40 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=21.88 M_x=-79.98
V,Ed=21.88 Vc,Rd,Red=59550.40 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.33 - Classe 3
Sollecitazioni: N=112.74 T_x=658.88 M_y=-914.49 T_y=-433.37 M_z=-401.36 M_x=56.35
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=347.98$ $\tau=9.55$ $\sigma_{max}=349.81$ (sfrut=0.10)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=-97.65$ $\tau=33.67$ $\tau_{max}=33.67$ (sfrut=0.02)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=347.98$ $\tau=9.55$ $\sigma_{TD,max}=350.20$ (sfrut=0.10)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: My,Ed=-914.49 Mz,Ed=-401.36 L=1.33
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=16.94$ Ncr,y=4437360.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.94$ Ncr,z=4437360.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.07+0.03=0.10
Verifica ZZ: 0.00+0.05+0.03=0.08

Asta n. 203 (-13 -14) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=1.33 - Classe 3
Sollecitazioni: N=60.49 T_x=233.80 M_y=-626.10 T_y=18.69 M_z=73.80 M_x=-11.81
Tensioni: $\sigma_N=0.98$ $\sigma_{m,d}=185.09$ $\tau=2.00$ $\sigma_{max}=186.07$ (sfrut=0.06)
Tensioni: $\sigma_N=0.98$ $\sigma_{m,d}=-17.95$ $\tau=10.55$ $\tau_{max}=10.55$ (sfrut=0.01)
Tensioni: $\sigma_N=0.98$ $\sigma_{m,d}=185.09$ $\tau=2.00$ $\sigma_{TD,max}=186.10$ (sfrut=0.06)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 3 SND Xl=0.97 - Classe 1
Sollecitazioni: T_y=-27.71 M_x=-2.78
V,Ed=-27.71 Vc,Rd,Red=59952.50 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 3 SND Xl=0.97 - Classe 1
Sollecitazioni: T_z=-318.26 M_x=-2.78
V,Ed=-318.26 Vc,Rd,Red=59952.50 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=112.74 T_x=2.97 M_y=-914.49 T_y=8.39 M_z=-401.36 M_x=56.35
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=347.98$ $\tau=9.55$ $\sigma_{max}=349.81$ (sfrut=0.10)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=222.49$ $\tau=9.86$ $\tau_{max}=9.86$ (sfrut=0.01)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=347.98$ $\tau=9.55$ $\sigma_{TD,max}=350.20$ (sfrut=0.10)

Asta n. 203 (-14 -15) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.33 - Classe 3
Sollecitazioni: N=-91.70 T_x=-615.27 M_y=741.07 T_y=-70.89 M_z=-82.75 M_x=-12.07
Tensioni: $\sigma_N=-1.49$ $\sigma_{m,d}=-217.86$ $\tau=2.05$ $\sigma_{max}=-219.35$ (sfrut=0.06)
Tensioni: $\sigma_N=-1.49$ $\sigma_{m,d}=-20.13$ $\tau=24.55$ $\tau_{max}=24.55$ (sfrut=0.01)
Tensioni: $\sigma_N=-1.49$ $\sigma_{m,d}=-217.86$ $\tau=2.05$ $\sigma_{TD,max}=219.38$ (sfrut=0.06)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_x=-541.26
V,Ed=-541.26 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
Sollecitazioni: N=112.74 T_x=-736.26 M_y=-863.06 T_y=450.15 M_z=-390.21 M_x=56.35
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=331.43$ $\tau=9.55$ $\sigma_{max}=333.26$ (sfrut=0.10)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=94.94$ $\tau=36.50$ $\tau_{max}=36.50$ (sfrut=0.02)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=331.43$ $\tau=9.55$ $\sigma_{TD,max}=333.67$ (sfrut=0.10)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: My,Ed=-863.06 Mz,Ed=-390.21 L=1.33
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.94$ Ncr,y=4437360.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.94$ Ncr,z=4437360.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.06+0.03=0.09
Verifica ZZ: 0.00+0.05+0.03=0.08
- Asta n. 203 (-15 203) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.33 - Classe 3
Sollecitazioni: N=-235.65 T_x=-894.81 M_y=1856.70 T_y=-114.07 M_z=-212.66 M_x=-21.36
Tensioni: $\sigma_N=-3.84$ $\sigma_{m,d}=-547.24$ $\tau=3.62$ $\sigma_{max}=-551.08$ (sfrut=0.16)
Tensioni: $\sigma_N=-3.84$ $\sigma_{m,d}=-51.74$ $\tau=36.35$ $\tau_{max}=36.35$ (sfrut=0.02)
Tensioni: $\sigma_N=-3.84$ $\sigma_{m,d}=-547.24$ $\tau=3.62$ $\sigma_{TD,max}=551.11$ (sfrut=0.16)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.33 - Classe 1
Sollecitazioni: T_x=-1012.23
V,Ed=-1012.23 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.33 - Classe 3
Sollecitazioni: N=112.74 T_x=-1558.82 M_y=2187.09 T_y=891.90 M_z=1393.37 M_x=56.35
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=946.86$ $\tau=9.55$ $\sigma_{max}=948.69$ (sfrut=0.28)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=-339.00$ $\tau=66.60$ $\tau_{max}=66.60$ (sfrut=0.03)
Tensioni: $\sigma_N=1.83$ $\sigma_{m,d}=946.86$ $\tau=9.55$ $\sigma_{TD,max}=948.84$ (sfrut=0.28)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: My,Ed=2187.09 Mz,Ed=1393.37 L=1.33
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=16.94$ Ncr,y=4437370.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=1.00$
 $\lambda_z=16.94$ Ncr,z=4437370.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.16+0.10=0.27
Verifica ZZ: 0.00+0.13+0.10=0.23
- Asta n. 204 (203 -26) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=75.56 T_x=524.01 M_y=1003.15 T_y=251.86 M_z=-519.60 M_x=54.42
Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=402.69$ $\tau=9.23$ $\sigma_{max}=403.92$ (sfrut=0.12)
Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=-126.42$ $\tau=28.40$ $\tau_{max}=28.40$ (sfrut=0.01)
Tensioni: $\sigma_N=1.23$ $\sigma_{m,d}=402.69$ $\tau=9.23$ $\sigma_{TD,max}=404.24$ (sfrut=0.12)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=857.02
V,Ed=857.02 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
Sollecitazioni: T_x=1295.44 M_y=2468.75 T_y=-721.97 M_z=1393.88
Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-1021.48$ $\tau=0.00$ $\sigma_{max}=-1021.48$ (sfrut=0.30)
Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=339.12$ $\tau=47.41$ $\tau_{max}=47.41$ (sfrut=0.02)
Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-1021.48$ $\tau=0.00$ $\sigma_{TD,max}=1021.48$ (sfrut=0.30)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: My,Ed=2468.75 Mz,Ed=1393.88 L=1.45
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=18.46$ Ncr,y=3737990.00 $\lambda'_y=0.24$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=18.46$ Ncr,z=3737990.00 $\lambda'_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.18+0.10=0.29
Verifica ZZ: 0.00+0.15+0.10=0.25
- Asta n. 204 (-26 -18) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=29.73 T_x=227.34 M_y=285.11 T_y=99.09 M_z=-148.02 M_x=21.60
Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=114.54$ $\tau=3.66$ $\sigma_{max}=115.02$ (sfrut=0.03)
Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=-36.01$ $\tau=11.98$ $\tau_{max}=11.98$ (sfrut=0.01)
Tensioni: $\sigma_N=0.48$ $\sigma_{m,d}=114.54$ $\tau=3.66$ $\sigma_{TD,max}=115.20$ (sfrut=0.03)
- Verifica a taglio Dir. Y [4.2.16] - CC 28 SLU Xl=1.45
Sollecitazioni: T_y=-240.66
V,Ed=-240.66 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.45
Sollecitazioni: T_x=409.50
V,Ed=409.50 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3
Sollecitazioni: T_x=500.29 M_y=658.68 T_y=-240.66 M_z=348.47
Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-266.34$ $\tau=0.00$ $\sigma_{max}=-266.34$ (sfrut=0.08)
Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=84.78$ $\tau=18.31$ $\tau_{max}=18.31$ (sfrut=0.01)

Tensioni: $\sigma_N=0.00$ $\sigma_{m,d}=-266.34$ $\tau=0.00$ $\sigma_{TD,max}=266.34$ (sfrut=0.08)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
Sollecitazioni: $M_y, Ed=658.68$ $M_z, Ed=348.47$ $L=1.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=18.46$ Ncr, $y=3737990.00$ $\lambda'_y=0.24$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=18.46$ Ncr, $z=3737990.00$ $\lambda'_z=0.24$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: $0.00+0.05+0.03=0.07$
Verifica ZZ: $0.00+0.04+0.03=0.07$

Asta n. 301 (-45 -79) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=86.74$ $T_x=68.75$ $M_y=66.26$ $T_y=-21.86$ $M_z=32.79$
Tensioni: $\sigma_N=2.32$ $\sigma_{m,d}=71.92$ $\tau=0.00$ $\sigma_{max}=74.24$ (sfrut=0.02)
Tensioni: $\sigma_N=2.32$ $\sigma_{m,d}=23.42$ $\tau=3.53$ $\tau_{max}=3.53$ (sfrut=0.00)
Tensioni: $\sigma_N=2.32$ $\sigma_{m,d}=71.92$ $\tau=0.00$ $\sigma_{TD,max}=74.24$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=383.67$
 $V, Ed=383.67$ $V_c, Rd=43850.90$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $N=146.09$ $T_x=383.67$ $M_y=386.00$
 $M_y, Ed=386.00$ $M_y, V, c, Rd=6269.10$
 $N, Ed=146.09$ $N_c, Rd=126583.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=6269.10$ $M_y, Ed/MNy, c, Rd=0.06$

Asta n. 301 (-80 -45) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: $N=-82.28$ $T_x=-75.12$ $M_y=75.82$ $T_y=47.80$ $M_z=71.70$
Tensioni: $\sigma_N=-2.20$ $\sigma_{m,d}=-111.36$ $\tau=0.00$ $\sigma_{max}=-113.56$ (sfrut=0.03)
Tensioni: $\sigma_N=-2.20$ $\sigma_{m,d}=51.20$ $\tau=3.87$ $\tau_{max}=3.87$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.20$ $\sigma_{m,d}=-111.36$ $\tau=0.00$ $\sigma_{TD,max}=113.56$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-383.67$
 $V, Ed=-383.67$ $V_c, Rd=43850.90$ $V, Ed/V_c, Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1
Sollecitazioni: $N=-146.09$ $T_x=-383.67$ $M_y=386.00$
 $M_y, Ed=386.00$ $M_y, V, c, Rd=6269.10$
 $N, Ed=-146.09$ $N_c, Rd=126583.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=6269.10$ $M_y, Ed/MNy, c, Rd=0.06$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N, Ed=-146.09$ $M_y, Ed=386.00$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: $0.00+0.06=0.06$
Verifica ZZ: $0.00=0.00$

Asta n. 302 (-3 -69) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=61.96$ $T_x=48.81$ $M_y=44.91$ $T_y=-14.82$ $M_z=22.23$
Tensioni: $\sigma_N=1.65$ $\sigma_{m,d}=48.75$ $\tau=0.00$ $\sigma_{max}=50.40$ (sfrut=0.01)
Tensioni: $\sigma_N=1.65$ $\sigma_{m,d}=15.87$ $\tau=2.51$ $\tau_{max}=2.51$ (sfrut=0.00)
Tensioni: $\sigma_N=1.65$ $\sigma_{m,d}=48.75$ $\tau=0.00$ $\sigma_{TD,max}=50.40$ (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=216.01$
 $V, Ed=216.01$ $V_c, Rd=43850.90$ $V, Ed/V_c, Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $N=98.70$ $T_x=216.01$ $M_y=213.30$
 $M_y, Ed=213.30$ $M_y, V, c, Rd=6269.10$
 $N, Ed=98.70$ $N_c, Rd=126583.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=6269.10$ $M_y, Ed/MNy, c, Rd=0.03$

Asta n. 302 (-68 -3) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: $N=-58.93$ $T_x=-53.13$ $M_y=51.39$ $T_y=32.40$ $M_z=48.60$
Tensioni: $\sigma_N=-1.57$ $\sigma_{m,d}=-75.48$ $\tau=0.00$ $\sigma_{max}=-77.05$ (sfrut=0.02)
Tensioni: $\sigma_N=-1.57$ $\sigma_{m,d}=34.71$ $\tau=2.74$ $\tau_{max}=2.74$ (sfrut=0.00)
Tensioni: $\sigma_N=-1.57$ $\sigma_{m,d}=-75.48$ $\tau=0.00$ $\sigma_{TD,max}=77.05$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-216.01$
 $V, Ed=-216.01$ $V_c, Rd=43850.90$ $V, Ed/V_c, Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1
Sollecitazioni: $N=-98.70$ $T_x=-216.01$ $M_y=213.30$
 $M_y, Ed=213.30$ $M_y, V, c, Rd=6269.10$
 $N, Ed=-98.70$ $N_c, Rd=126583.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=6269.10$ $M_y, Ed/MNy, c, Rd=0.03$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N, Ed=-98.70$ $M_y, Ed=213.30$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: $0.00+0.03=0.03$
Verifica ZZ: $0.00=0.00$

Asta n. 303 (-29 -76) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=89.03$ $T_x=70.59$ $M_y=68.23$ $T_y=-22.51$ $M_z=33.77$

Tensioni: $\sigma_N=2.38$ $\sigma_{m,d}=74.06$ $\tau=0.00$ $\sigma_{max}=76.44$ (sfrut=0.02)
Tensioni: $\sigma_N=2.38$ $\sigma_{m,d}=24.11$ $\tau=3.63$ $\tau_{max}=3.63$ (sfrut=0.00)
Tensioni: $\sigma_N=2.38$ $\sigma_{m,d}=74.06$ $\tau=0.00$ $\sigma_{TD,max}=76.44$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=399.14$
 $V,Ed=399.14$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $N=150.46$ $T_x=399.14$ $M_y=401.94$
 $My,Ed=401.94$ $My,V,c,Rd=6269.10$
 $N,Ed=150.46$ $Nc,Rd=126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $My,Ed/MNy,c,Rd=0.06$

Asta n. 303 (-75 -29) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: $N=-84.43$ $T_x=-77.15$ $M_y=78.07$ $T_y=49.22$ $M_z=73.83$
Tensioni: $\sigma_N=-2.26$ $\sigma_{m,d}=-114.67$ $\tau=0.00$ $\sigma_{max}=-116.92$ (sfrut=0.03)
Tensioni: $\sigma_N=-2.26$ $\sigma_{m,d}=52.73$ $\tau=3.97$ $\tau_{max}=3.97$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.26$ $\sigma_{m,d}=-114.67$ $\tau=0.00$ $\sigma_{TD,max}=116.92$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-399.14$
 $V,Ed=-399.14$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1
Sollecitazioni: $N=-150.46$ $T_x=-399.14$ $M_y=401.94$
 $My,Ed=401.94$ $My,V,c,Rd=6269.10$
 $N,Ed=-150.46$ $Nc,Rd=-126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $My,Ed/MNy,c,Rd=0.06$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N,Ed=-150.46$ $My,Ed=401.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ $Ncr,y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr,z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
Verifica YY: $0.00+0.06=0.06$
Verifica ZZ: $0.00=0.00$

Asta n. 304 (201 -77) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=84.46$ $T_x=66.91$ $M_y=64.29$ $T_y=-21.21$ $M_z=31.82$
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{max}=72.04$ (sfrut=0.02)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=22.72$ $\tau=3.44$ $\tau_{max}=3.44$ (sfrut=0.00)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{TD,max}=72.04$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=368.19$
 $V,Ed=368.19$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $N=141.71$ $T_x=368.19$ $M_y=370.06$
 $My,Ed=370.06$ $My,V,c,Rd=6269.10$
 $N,Ed=141.71$ $Nc,Rd=126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $My,Ed/MNy,c,Rd=0.06$

Asta n. 304 (-78 201) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: $N=-80.13$ $T_x=-73.09$ $M_y=73.56$ $T_y=46.38$ $M_z=69.57$
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{max}=-110.19$ (sfrut=0.03)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=49.68$ $\tau=3.77$ $\tau_{max}=3.77$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{TD,max}=110.19$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-368.19$
 $V,Ed=-368.19$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1
Sollecitazioni: $N=-141.71$ $T_x=-368.19$ $M_y=370.06$
 $My,Ed=370.06$ $My,V,c,Rd=6269.10$
 $N,Ed=-141.71$ $Nc,Rd=-126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $My,Ed/MNy,c,Rd=0.06$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N,Ed=-141.71$ $My,Ed=370.06$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ $Ncr,y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr,z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
Verifica YY: $0.00+0.06=0.06$
Verifica ZZ: $0.00=0.00$

Asta n. 305 (-6 -48) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=84.46$ $T_x=66.91$ $M_y=64.29$ $T_y=-21.21$ $M_z=31.82$
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{max}=72.04$ (sfrut=0.02)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=22.72$ $\tau=3.44$ $\tau_{max}=3.44$ (sfrut=0.00)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{TD,max}=72.04$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=368.19$
 $V,Ed=368.19$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1
Sollecitazioni: $N=141.71$ $T_x=368.19$ $M_y=370.06$
 $My,Ed=370.06$ $My,V,c,Rd=6269.10$
 $N,Ed=141.71$ $Nc,Rd=126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $My,Ed/MNy,c,Rd=0.06$

Asta n. 305 (-47 -6) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-80.13 T_x=-73.09 M_y=73.56 T_y=46.38 M_z=69.57
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{max}=-110.19$ (sfrut=0.03)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=49.68$ $\tau=3.77$ $\tau_{max}=3.77$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{ID,max}=110.19$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-368.19
V,Ed=-368.19 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-141.71 T_x=-368.19 M_y=370.06
My,Ed=370.06 My,V,c,Rd=6269.10
N,Ed=-141.71 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

Asta n. 306 (-7 -50) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=84.46 T_x=66.91 M_y=64.29 T_y=-21.21 M_z=31.82
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{max}=72.04$ (sfrut=0.02)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=22.72$ $\tau=3.44$ $\tau_{max}=3.44$ (sfrut=0.00)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{ID,max}=72.04$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=368.19
V,Ed=368.19 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=141.71 T_x=368.19 M_y=370.06
My,Ed=370.06 My,V,c,Rd=6269.10
N,Ed=141.71 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 306 (-49 -7) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-80.13 T_x=-73.09 M_y=73.56 T_y=46.38 M_z=69.57
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{max}=-110.19$ (sfrut=0.03)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=49.68$ $\tau=3.77$ $\tau_{max}=3.77$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{ID,max}=110.19$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-368.19
V,Ed=-368.19 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-141.71 T_x=-368.19 M_y=370.06
My,Ed=370.06 My,V,c,Rd=6269.10
N,Ed=-141.71 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

Asta n. 307 (-8 -52) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=84.46 T_x=66.91 M_y=64.29 T_y=-21.21 M_z=31.82
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{max}=72.04$ (sfrut=0.02)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=22.72$ $\tau=3.44$ $\tau_{max}=3.44$ (sfrut=0.00)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{ID,max}=72.04$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=368.19
V,Ed=368.19 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=141.71 T_x=368.19 M_y=370.06
My,Ed=370.06 My,V,c,Rd=6269.10
N,Ed=141.71 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 307 (-51 -8) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-80.13 T_x=-73.09 M_y=73.56 T_y=46.38 M_z=69.57
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{max}=-110.19$ (sfrut=0.03)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=49.68$ $\tau=3.77$ $\tau_{max}=3.77$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{ID,max}=110.19$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-368.19
V,Ed=-368.19 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-141.71 T_x=-368.19 M_y=370.06
My,Ed=370.06 My,V,c,Rd=6269.10
N,Ed=-141.71 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

Asta n. 308 (-9 -54) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=84.46 T_x=66.91 M_y=64.29 T_y=-21.21 M_z=31.82
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{max}=72.04$ (sfrut=0.02)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=22.72$ $\tau=3.44$ $\tau_{max}=3.44$ (sfrut=0.00)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.78$ $\tau=0.00$ $\sigma_{TD,max}=72.04$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=368.19
V,Ed=368.19 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=141.71 T_x=368.19 M_y=370.06
My,Ed=370.06 My,V,c,Rd=6269.10
N,Ed=141.71 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 308 (-53 -9) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-80.13 T_x=-73.09 M_y=73.56 T_y=46.38 M_z=69.57
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{max}=-110.19$ (sfrut=0.03)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=49.68$ $\tau=3.77$ $\tau_{max}=3.77$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.05$ $\tau=0.00$ $\sigma_{TD,max}=110.19$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-368.19
V,Ed=-368.19 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-141.71 T_x=-368.19 M_y=370.06
My,Ed=370.06 My,V,c,Rd=6269.10
N,Ed=-141.71 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

Asta n. 309 (-10 -56) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=59.67 T_x=46.97 M_y=42.94 T_y=-14.17 M_z=21.25
Tensioni: $\sigma_N=1.59$ $\sigma_{m,d}=46.61$ $\tau=0.00$ $\sigma_{max}=48.21$ (sfrut=0.01)
Tensioni: $\sigma_N=1.59$ $\sigma_{m,d}=15.18$ $\tau=2.41$ $\tau_{max}=2.41$ (sfrut=0.00)
Tensioni: $\sigma_N=1.59$ $\sigma_{m,d}=46.61$ $\tau=0.00$ $\sigma_{TD,max}=48.21$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=200.53
V,Ed=200.53 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=94.33 T_x=200.53 M_y=197.36
My,Ed=197.36 My,V,c,Rd=6269.10
N,Ed=94.33 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.03

Asta n. 309 (-55 -10) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-56.78 T_x=-51.10 M_y=49.14 T_y=30.98 M_z=46.47
Tensioni: $\sigma_N=-1.52$ $\sigma_{m,d}=-72.17$ $\tau=0.00$ $\sigma_{max}=-73.68$ (sfrut=0.02)
Tensioni: $\sigma_N=-1.52$ $\sigma_{m,d}=33.18$ $\tau=2.63$ $\tau_{max}=2.63$ (sfrut=0.00)
Tensioni: $\sigma_N=-1.52$ $\sigma_{m,d}=-72.17$ $\tau=0.00$ $\sigma_{TD,max}=73.68$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-200.53
V,Ed=-200.53 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-94.33 T_x=-200.53 M_y=197.36
My,Ed=197.36 My,V,c,Rd=6269.10
N,Ed=-94.33 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-94.33 My,Ed=197.36 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

Asta n. 310 (-11 -58) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=59.73 T_x=47.02 M_y=42.99 T_y=-14.19 M_z=21.28
Tensioni: $\sigma_N=1.60$ $\sigma_{m,d}=46.67$ $\tau=0.00$ $\sigma_{max}=48.27$ (sfrut=0.01)
Tensioni: $\sigma_N=1.60$ $\sigma_{m,d}=15.20$ $\tau=2.42$ $\tau_{max}=2.42$ (sfrut=0.00)

Tensioni: $\sigma_N=1.60$ $\sigma_{m,d}=46.67$ $\tau=0.00$ $\sigma_{TD,max}=48.27$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=0.00$ - Classe 1
Sollecitazioni: $T_2=200.96$
 $V,Ed=200.96$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=0.00$ - Classe 1
Sollecitazioni: $N=94.45$ $T_2=200.96$ $M_y=197.79$
 $M_y,Ed=197.79$ $M_y,V,c,Rd=6269.10$
 $N,Ed=94.45$ $Nc,Rd=126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $M_y,Ed/MNy,c,Rd=0.03$

Asta n. 310 (-57 -11) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
Sollecitazioni: $N=-56.84$ $T_2=-51.16$ $M_y=49.20$ $T_y=31.02$ $M_z=46.53$
Tensioni: $\sigma_N=-1.52$ $\sigma_{m,d}=-72.26$ $\tau=0.00$ $\sigma_{max}=-73.78$ (sfrut=0.02)
Tensioni: $\sigma_N=-1.52$ $\sigma_{m,d}=33.22$ $\tau=2.63$ $\tau_{max}=2.63$ (sfrut=0.00)
Tensioni: $\sigma_N=-1.52$ $\sigma_{m,d}=-72.26$ $\tau=0.00$ $\sigma_{TD,max}=73.78$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=1.50$ - Classe 1
Sollecitazioni: $T_2=200.96$
 $V,Ed=-200.96$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=1.50$ - Classe 1
Sollecitazioni: $N=-94.45$ $T_2=200.96$ $M_y=197.79$
 $M_y,Ed=197.79$ $M_y,V,c,Rd=6269.10$
 $N,Ed=-94.45$ $Nc,Rd=126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $M_y,Ed/MNy,c,Rd=0.03$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N,Ed=-94.45$ $M_y,Ed=197.79$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.33$ $Ncr,y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr,z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.57 , 0.00 , 0.95
Verifica YY: $0.00+0.03=0.03$
Verifica ZZ: $0.00=0.00$

Asta n. 311 (-12 -60) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=84.58$ $T_2=67.01$ $M_y=64.39$ $T_y=-21.25$ $M_z=31.87$
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.90$ $\tau=0.00$ $\sigma_{max}=72.16$ (sfrut=0.02)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=22.76$ $\tau=3.44$ $\tau_{max}=3.44$ (sfrut=0.00)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.90$ $\tau=0.00$ $\sigma_{TD,max}=72.16$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=0.00$ - Classe 1
Sollecitazioni: $T_2=369.04$
 $V,Ed=369.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=0.00$ - Classe 1
Sollecitazioni: $N=141.95$ $T_2=369.04$ $M_y=370.93$
 $M_y,Ed=370.93$ $M_y,V,c,Rd=6269.10$
 $N,Ed=141.95$ $Nc,Rd=126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $M_y,Ed/MNy,c,Rd=0.06$

Asta n. 311 (-59 -12) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
Sollecitazioni: $N=-80.24$ $T_2=-73.20$ $M_y=73.69$ $T_y=46.46$ $M_z=69.69$
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.23$ $\tau=0.00$ $\sigma_{max}=-110.37$ (sfrut=0.03)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=49.76$ $\tau=3.77$ $\tau_{max}=3.77$ (sfrut=0.00)
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.23$ $\tau=0.00$ $\sigma_{TD,max}=110.37$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=1.50$ - Classe 1
Sollecitazioni: $T_2=-369.04$
 $V,Ed=-369.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=1.50$ - Classe 1
Sollecitazioni: $N=-141.95$ $T_2=-369.04$ $M_y=370.93$
 $M_y,Ed=370.93$ $M_y,V,c,Rd=6269.10$
 $N,Ed=-141.95$ $Nc,Rd=126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $M_y,Ed/MNy,c,Rd=0.06$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: $N,Ed=-141.95$ $M_y,Ed=370.93$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.33$ $Ncr,y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr,z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.57 , 0.00 , 0.95
Verifica YY: $0.00+0.06=0.06$
Verifica ZZ: $0.00=0.00$

Asta n. 312 (-13 -62) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
Sollecitazioni: $N=84.58$ $T_2=67.01$ $M_y=64.39$ $T_y=-21.25$ $M_z=31.87$
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.90$ $\tau=0.00$ $\sigma_{max}=72.16$ (sfrut=0.02)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=22.76$ $\tau=3.44$ $\tau_{max}=3.44$ (sfrut=0.00)
Tensioni: $\sigma_N=2.26$ $\sigma_{m,d}=69.90$ $\tau=0.00$ $\sigma_{TD,max}=72.16$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=0.00$ - Classe 1
Sollecitazioni: $T_2=369.04$
 $V,Ed=369.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=0.00$ - Classe 1
Sollecitazioni: $N=141.95$ $T_2=369.04$ $M_y=370.93$
 $M_y,Ed=370.93$ $M_y,V,c,Rd=6269.10$
 $N,Ed=141.95$ $Nc,Rd=126583.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=6269.10$ $M_y,Ed/MNy,c,Rd=0.06$

Asta n. 312 (-61 -13) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
Sollecitazioni: $N=-80.24$ $T_2=-73.20$ $M_y=73.69$ $T_y=46.46$ $M_z=69.69$
Tensioni: $\sigma_N=-2.14$ $\sigma_{m,d}=-108.23$ $\tau=0.00$ $\sigma_{max}=-110.37$ (sfrut=0.03)

Tensioni: $\sigma_N = -2.14$ $\sigma_{m,d} = 49.76$ $\tau = 3.77$ $\tau_{max} = 3.77$ (sfrut=0.00)
 Tensioni: $\sigma_N = -2.14$ $\sigma_{m,d} = -108.23$ $\tau = 0.00$ $\sigma_{TD,max} = 110.37$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_z = -369.04$
 $V, Ed = -369.04$ $Vc, Rd = 43850.90$ $V, Ed/Vc, Rd = 0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $N = -141.95$ $T_z = -369.04$ $M_y = 370.93$
 $My, Ed = 370.93$ $My, V, c, Rd = 6269.10$
 $N, Ed = -141.95$ $Nc, Rd = 126583.00$ YY $n = N, Ed/Nc, Rd = 0.00$ $MNy, c, Rd = 6269.10$ $My, Ed/MNy, c, Rd = 0.06$
- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N, Ed = -141.95$ $My, Ed = 370.93$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.33$ $Ncr, y = 1039280.00$ $\lambda'_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 37.85$ $Ncr, z = 541779.00$ $\lambda'_z = 0.50$ Curva a: $\Phi_z = 0.65$ $\chi_z = 0.93$
 $Kyy, Kyz, Kzy, Kzz = 0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00 + 0.06 = 0.06$
 Verifica ZZ: $0.00 = 0.00$

Asta n. 313 (-14 -64) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N = 84.58$ $T_z = 67.01$ $M_y = 64.39$ $T_y = -21.25$ $M_z = 31.87$
 Tensioni: $\sigma_N = 2.26$ $\sigma_{m,d} = 69.90$ $\tau = 0.00$ $\sigma_{max} = 72.16$ (sfrut=0.02)
 Tensioni: $\sigma_N = 2.26$ $\sigma_{m,d} = 22.76$ $\tau = 3.44$ $\tau_{max} = 3.44$ (sfrut=0.00)
 Tensioni: $\sigma_N = 2.26$ $\sigma_{m,d} = 69.90$ $\tau = 0.00$ $\sigma_{TD,max} = 72.16$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_z = 369.04$
 $V, Ed = 369.04$ $Vc, Rd = 43850.90$ $V, Ed/Vc, Rd = 0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $N = 141.95$ $T_z = 369.04$ $M_y = 370.93$
 $My, Ed = 370.93$ $My, V, c, Rd = 6269.10$
 $N, Ed = 141.95$ $Nc, Rd = 126583.00$ YY $n = N, Ed/Nc, Rd = 0.00$ $MNy, c, Rd = 6269.10$ $My, Ed/MNy, c, Rd = 0.06$

Asta n. 313 (-63 -14) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
 Sollecitazioni: $N = -80.24$ $T_z = -73.20$ $M_y = 73.69$ $T_y = 46.46$ $M_z = 69.69$
 Tensioni: $\sigma_N = -2.14$ $\sigma_{m,d} = -108.23$ $\tau = 0.00$ $\sigma_{max} = -110.37$ (sfrut=0.03)
 Tensioni: $\sigma_N = -2.14$ $\sigma_{m,d} = 49.76$ $\tau = 3.77$ $\tau_{max} = 3.77$ (sfrut=0.00)
 Tensioni: $\sigma_N = -2.14$ $\sigma_{m,d} = -108.23$ $\tau = 0.00$ $\sigma_{TD,max} = 110.37$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_z = -369.04$
 $V, Ed = -369.04$ $Vc, Rd = 43850.90$ $V, Ed/Vc, Rd = 0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $N = -141.95$ $T_z = -369.04$ $M_y = 370.93$
 $My, Ed = 370.93$ $My, V, c, Rd = 6269.10$
 $N, Ed = -141.95$ $Nc, Rd = 126583.00$ YY $n = N, Ed/Nc, Rd = 0.00$ $MNy, c, Rd = 6269.10$ $My, Ed/MNy, c, Rd = 0.06$
- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N, Ed = -141.95$ $My, Ed = 370.93$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $\lambda_y = 27.33$ $Ncr, y = 1039280.00$ $\lambda'_y = 0.36$ Curva a: $\Phi_y = 0.58$ $\chi_y = 0.96$
 $\lambda_z = 37.85$ $Ncr, z = 541779.00$ $\lambda'_z = 0.50$ Curva a: $\Phi_z = 0.65$ $\chi_z = 0.93$
 $Kyy, Kyz, Kzy, Kzz = 0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00 + 0.06 = 0.06$
 Verifica ZZ: $0.00 = 0.00$

Asta n. 314 (-15 -66) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N = 84.58$ $T_z = 67.01$ $M_y = 64.39$ $T_y = -21.25$ $M_z = 31.87$
 Tensioni: $\sigma_N = 2.26$ $\sigma_{m,d} = 69.90$ $\tau = 0.00$ $\sigma_{max} = 72.16$ (sfrut=0.02)
 Tensioni: $\sigma_N = 2.26$ $\sigma_{m,d} = 22.76$ $\tau = 3.44$ $\tau_{max} = 3.44$ (sfrut=0.00)
 Tensioni: $\sigma_N = 2.26$ $\sigma_{m,d} = 69.90$ $\tau = 0.00$ $\sigma_{TD,max} = 72.16$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_z = 369.04$
 $V, Ed = 369.04$ $Vc, Rd = 43850.90$ $V, Ed/Vc, Rd = 0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $N = 141.95$ $T_z = 369.04$ $M_y = 370.93$
 $My, Ed = 370.93$ $My, V, c, Rd = 6269.10$
 $N, Ed = 141.95$ $Nc, Rd = 126583.00$ YY $n = N, Ed/Nc, Rd = 0.00$ $MNy, c, Rd = 6269.10$ $My, Ed/MNy, c, Rd = 0.06$

Asta n. 314 (-65 -15) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
 Sollecitazioni: $N = -80.24$ $T_z = -73.20$ $M_y = 73.69$ $T_y = 46.46$ $M_z = 69.69$
 Tensioni: $\sigma_N = -2.14$ $\sigma_{m,d} = -108.23$ $\tau = 0.00$ $\sigma_{max} = -110.37$ (sfrut=0.03)
 Tensioni: $\sigma_N = -2.14$ $\sigma_{m,d} = 49.76$ $\tau = 3.77$ $\tau_{max} = 3.77$ (sfrut=0.00)
 Tensioni: $\sigma_N = -2.14$ $\sigma_{m,d} = -108.23$ $\tau = 0.00$ $\sigma_{TD,max} = 110.37$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_z = -369.04$
 $V, Ed = -369.04$ $Vc, Rd = 43850.90$ $V, Ed/Vc, Rd = 0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $N = -141.95$ $T_z = -369.04$ $M_y = 370.93$
 $My, Ed = 370.93$ $My, V, c, Rd = 6269.10$
 $N, Ed = -141.95$ $Nc, Rd = 126583.00$ YY $n = N, Ed/Nc, Rd = 0.00$ $MNy, c, Rd = 6269.10$ $My, Ed/MNy, c, Rd = 0.06$
- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: $N, Ed = -141.95$ $My, Ed = 370.93$ $L = 1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
 Verifica YY: 0.00+0.06=0.06
 Verifica ZZ: 0.00=0.00

Asta n. 315 (203 -67) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=86.81 T_x=68.80 M_y=66.31 T_y=-21.88 M_z=32.82

Tensioni: $\sigma_N=2.32$ $\sigma_{m,d}=71.98$ $\tau=0.00$ $\sigma_{max}=74.30$ (sfrut=0.02)

Tensioni: $\sigma_N=2.32$ $\sigma_{m,d}=23.44$ $\tau=3.54$ $\tau_{max}=3.54$ (sfrut=0.00)

Tensioni: $\sigma_N=2.32$ $\sigma_{m,d}=71.98$ $\tau=0.00$ $\sigma_{TD,max}=74.30$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: T_x=384.09

V,Ed=384.09 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: N=146.21 T_x=384.09 M_y=386.43

My,Ed=386.43 My,V,c,Rd=6269.10

N,Ed=146.21 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 315 (-72 203) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3

Sollecitazioni: N=-82.34 T_x=-75.18 M_y=75.88 T_y=47.84 M_z=71.76

Tensioni: $\sigma_N=-2.20$ $\sigma_{m,d}=-111.45$ $\tau=0.00$ $\sigma_{max}=-113.65$ (sfrut=0.03)

Tensioni: $\sigma_N=-2.20$ $\sigma_{m,d}=51.24$ $\tau=3.87$ $\tau_{max}=3.87$ (sfrut=0.00)

Tensioni: $\sigma_N=-2.20$ $\sigma_{m,d}=-111.45$ $\tau=0.00$ $\sigma_{TD,max}=113.65$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1

Sollecitazioni: T_x=-384.09

V,Ed=-384.09 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1

Sollecitazioni: N=-146.20 T_x=-384.09 M_y=386.43

My,Ed=386.43 My,V,c,Rd=6269.10

N,Ed=-146.20 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-146.20 My,Ed=386.43 L=1.50

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

Asta n. 316 (-26 -74) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=89.03 T_x=70.59 M_y=68.23 T_y=-22.51 M_z=33.77

Tensioni: $\sigma_N=2.38$ $\sigma_{m,d}=74.06$ $\tau=0.00$ $\sigma_{max}=76.44$ (sfrut=0.02)

Tensioni: $\sigma_N=2.38$ $\sigma_{m,d}=24.11$ $\tau=3.63$ $\tau_{max}=3.63$ (sfrut=0.00)

Tensioni: $\sigma_N=2.38$ $\sigma_{m,d}=74.06$ $\tau=0.00$ $\sigma_{TD,max}=76.44$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: T_x=399.14

V,Ed=399.14 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: N=150.46 T_x=399.14 M_y=401.94

My,Ed=401.94 My,V,c,Rd=6269.10

N,Ed=150.46 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 316 (-73 -26) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3

Sollecitazioni: N=-84.43 T_x=-77.15 M_y=78.07 T_y=49.22 M_z=73.83

Tensioni: $\sigma_N=-2.26$ $\sigma_{m,d}=-114.67$ $\tau=0.00$ $\sigma_{max}=-116.92$ (sfrut=0.03)

Tensioni: $\sigma_N=-2.26$ $\sigma_{m,d}=52.73$ $\tau=3.97$ $\tau_{max}=3.97$ (sfrut=0.00)

Tensioni: $\sigma_N=-2.26$ $\sigma_{m,d}=-114.67$ $\tau=0.00$ $\sigma_{TD,max}=116.92$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1

Sollecitazioni: T_x=-399.14

V,Ed=-399.14 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1

Sollecitazioni: N=-150.46 T_x=-399.14 M_y=401.94

My,Ed=401.94 My,V,c,Rd=6269.10

N,Ed=-150.46 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-150.46 My,Ed=401.94 L=1.50

α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

Asta n. 317 (-18 -71) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=61.96 T_x=48.81 M_y=44.91 T_y=-14.82 M_z=22.23

Tensioni: $\sigma_N=1.65$ $\sigma_{m,d}=48.75$ $\tau=0.00$ $\sigma_{max}=50.40$ (sfrut=0.01)

Tensioni: $\sigma_N=1.65$ $\sigma_{m,d}=15.87$ $\tau=2.51$ $\tau_{max}=2.51$ (sfrut=0.00)

Tensioni: $\sigma_N=1.65$ $\sigma_{m,d}=48.75$ $\tau=0.00$ $\sigma_{TD,max}=50.40$ (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: $T_z=216.01$
 $V,Ed=216.01$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.00$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $N=98.70$ $T_z=216.01$ $M_y=213.30$
 $M_y,Ed=213.30$ $M_y,V,c,Rd=6269.10$
 $N,Ed=98.70$ $N_c,Rd=126583.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=6269.10$ $M_y,Ed/MNy,c,Rd=0.03$

Asta n. 317 (-70 -18) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
 Sollecitazioni: $N=-58.93$ $T_z=-53.13$ $M_y=51.39$ $T_y=32.40$ $M_z=48.60$
 Tensioni: $\sigma_{m,d}=-1.57$ $\sigma_{m,d}=-75.48$ $\tau=0.00$ $\sigma_{max}=-77.05$ (sfrut=0.02)
 Tensioni: $\sigma_{m,d}=-1.57$ $\sigma_{m,d}=34.71$ $\tau=2.74$ $\tau_{max}=2.74$ (sfrut=0.00)
 Tensioni: $\sigma_{m,d}=-1.57$ $\sigma_{m,d}=-75.48$ $\tau=0.00$ $\sigma_{ID,max}=77.05$ (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_z=-216.01$
 $V,Ed=-216.01$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $N=-98.70$ $T_z=-216.01$ $M_y=213.30$
 $M_y,Ed=213.30$ $M_y,V,c,Rd=6269.10$
 $N,Ed=-98.70$ $N_c,Rd=126583.00$ YY $n=N,Ed/N_c,Rd=0.00$ $MNy,c,Rd=6269.10$ $M_y,Ed/MNy,c,Rd=0.03$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: $N,Ed=-98.70$ $M_y,Ed=213.30$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.33$ $Ncr,y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr,z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.57 , 0.00 , 0.95
 Verifica YY: $0.00+0.03=0.03$
 Verifica ZZ: $0.00=0.00$

Membratura

Asta n. 201 (-3 -29 -45) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $M_y,Ed=2468.76$ $M_z,Ed=1393.89$ $L=2.90$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.00+0.18+0.10=0.29$
 Verifica ZZ: $0.00+0.15+0.10=0.25$
- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=0.11$ (L/2532) $f_{z,g}=0.04$ (L/7577)
- Verifica freccia massima carichi totali - CC 30
 $f_{z,1}=0.26$ (L/1123) $f_{z,g}=0.08$ (L/3608)

Membratura

Asta n. 202 (-45 201 -6 -7 -8 -9 -10 202) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=-165.10$ $M_y,Ed=2885.80$ $M_z,Ed=1558.10$ $L=8.15$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=103.94$ $Ncr,y=117878.00$ $\lambda'_y=1.36$ Curva a: $\Phi_y=1.55$ $\chi_y=0.44$
 $\lambda_z=103.94$ $Ncr,z=117878.00$ $\lambda'_z=1.36$ Curva a: $\Phi_z=1.55$ $\chi_z=0.44$
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.00+0.21+0.12=0.33$
 Verifica ZZ: $0.00+0.17+0.12=0.29$
- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=0.35$ (L/2324)
- Verifica freccia massima carichi totali - CC 30
 $f_{z,1}=0.67$ (L/1216)

Membratura

Asta n. 203 (202 -11 -12 -13 -14 -15 203) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $N,Ed=112.74$ $M_y,Ed=2304.58$ $M_z,Ed=1556.83$ $L=6.84$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.00+0.17+0.12=0.29$
 Verifica ZZ: $0.00+0.14+0.12=0.25$
- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,g}=0.11$ (L/6071)
- Verifica freccia massima carichi totali - CC 30
 $f_{z,g}=0.21$ (L/3246)

Membratura

Asta n. 204 (203 -26 -18) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3
 Sollecitazioni: $M_y,Ed=2468.75$ $M_z,Ed=1393.88$ $L=2.90$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 K_{yy} , K_{yz} , K_{zy} , $K_{zz}=0.95$, 0.95 , 0.76 , 0.95
 Verifica YY: $0.00+0.18+0.10=0.29$
 Verifica ZZ: $0.00+0.15+0.10=0.25$
- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=0.14$ (L/2011) $f_{z,g}=0.04$ (L/7479)
- Verifica freccia massima carichi totali - CC 30
 $f_{z,1}=0.31$ (L/941) $f_{z,g}=0.08$ (L/3564)

Membratura

Asta n. 301 (-79 -45 -80) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-146.09 My,Ed=386.00 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.17$ (L/256) $f_{z,e}=0.08$ (L/3949)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.15$ (L/260) $f_{z,e}=0.06$ (L/4984)

Membratura

Asta n. 302 (-69 -3 -68) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-98.70 My,Ed=213.30 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.03=0.03
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.13$ (L/265) $f_{z,e}=0.04$ (L/7561)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.12$ (L/267) $f_{z,e}=0.03$ (L/10267)

Membratura

Asta n. 303 (-76 -29 -75) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-150.46 My,Ed=401.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.17$ (L/256) $f_{z,e}=0.08$ (L/3783)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.16$ (L/259) $f_{z,e}=0.06$ (L/4759)

Membratura

Asta n. 304 (-77 201 -78) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.17$ (L/256) $f_{z,e}=0.07$ (L/4132)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.15$ (L/260) $f_{z,e}=0.06$ (L/5234)

Membratura

Asta n. 305 (-48 -6 -47) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.17$ (L/255) $f_{z,e}=0.07$ (L/4131)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.16$ (L/258) $f_{z,e}=0.06$ (L/5235)

Membratura

Asta n. 306 (-50 -7 -49) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.06=0.06
Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.18$ (L/254) $f_{z,e}=0.07$ (L/4131)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.16$ (L/257) $f_{z,6}=0.06$ (L/5233)

Membratura

Asta n. 307 (-52 -8 -51) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.06=0.06$
 Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.18$ (L/253) $f_{z,6}=0.07$ (L/4130)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.17$ (L/256) $f_{z,6}=0.06$ (L/5233)

Membratura

Asta n. 308 (-54 -9 -53) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-141.71 My,Ed=370.06 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.06=0.06$
 Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.19$ (L/252) $f_{z,6}=0.07$ (L/4130)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.17$ (L/255) $f_{z,6}=0.06$ (L/5235)

Membratura

Asta n. 309 (-56 -10 -55) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-94.33 My,Ed=197.36 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.03=0.03$
 Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.16$ (L/259) $f_{z,6}=0.04$ (L/8261)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.15$ (L/261) $f_{z,6}=0.03$ (L/11382)

Membratura

Asta n. 310 (-58 -11 -57) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-94.45 My,Ed=197.79 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.03=0.03$
 Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.15$ (L/260) $f_{z,6}=0.04$ (L/8242)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.14$ (L/262) $f_{z,6}=0.03$ (L/11341)

Membratura

Asta n. 311 (-60 -12 -59) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-141.95 My,Ed=370.93 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$
 Verifica YY: $0.00+0.06=0.06$
 Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.17$ (L/257) $f_{z,6}=0.07$ (L/4120)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.15$ (L/260) $f_{z,6}=0.06$ (L/5222)

Membratura

Asta n. 312 (-62 -13 -61) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-141.95 My,Ed=370.93 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$

Verifica YY: $0.00+0.06=0.06$
 Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.14$ (L/262) $f_{z,6}=0.07$ (L/4122)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.13$ (L/265) $f_{z,6}=0.06$ (L/5222)

Membratura

Asta n. 313 (-64 -14 -63) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-141.95 My,Ed=370.93 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: $0.00+0.06=0.06$

Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.12$ (L/267) $f_{z,6}=0.07$ (L/4120)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.10$ (L/271) $f_{z,6}=0.06$ (L/5218)

Membratura

Asta n. 314 (-66 -15 -65) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-141.95 My,Ed=370.93 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: $0.00+0.06=0.06$

Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.10$ (L/273) $f_{z,6}=0.07$ (L/4120)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.08$ (L/277) $f_{z,6}=0.06$ (L/5220)

Membratura

Asta n. 315 (-67 203 -72) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-146.20 My,Ed=386.43 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: $0.00+0.06=0.06$

Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.08$ (L/278) $f_{z,6}=0.08$ (L/3944)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.06$ (L/282) $f_{z,6}=0.06$ (L/4980)

Membratura

Asta n. 316 (-74 -26 -73) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-150.46 My,Ed=401.94 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: $0.00+0.06=0.06$

Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.08$ (L/277) $f_{z,6}=0.08$ (L/3782)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.06$ (L/282) $f_{z,6}=0.06$ (L/4762)

Membratura

Asta n. 317 (-71 -18 -70) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
 Sollecitazioni: N,Ed=-98.70 My,Ed=213.30 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$

$\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: $0.00+0.03=0.03$

Verifica ZZ: $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23
 $f_{z,1}=1.04$ (L/288) $f_{z,6}=0.04$ (L/7561)

- Verifica freccia massima carichi totali - CC 23
 $f_{z,1}=1.03$ (L/291) $f_{z,6}=0.03$ (L/10263)

6.3 Tracker 2x30 – configurazione a riposo ($\alpha = 0^\circ$)

6.3.1 Diagrammi tassi di sfruttamento

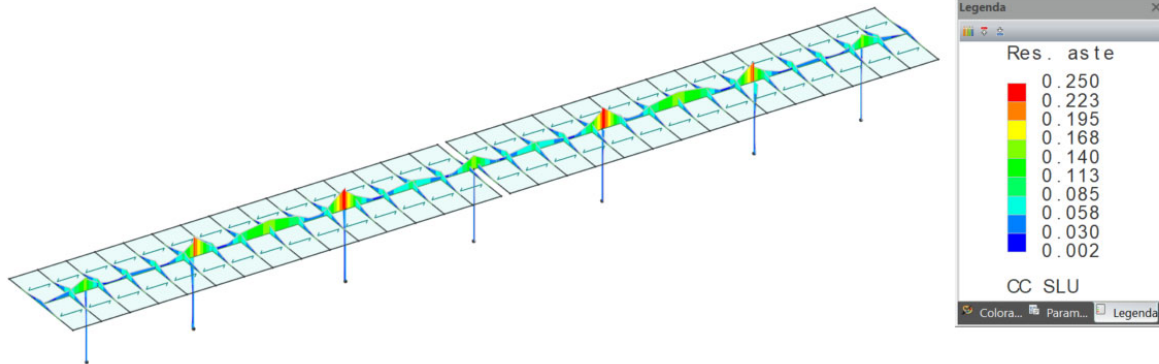


Diagramma tassi di sfruttamento resistenza aste combo SLU con valore massimo pari a 0,250

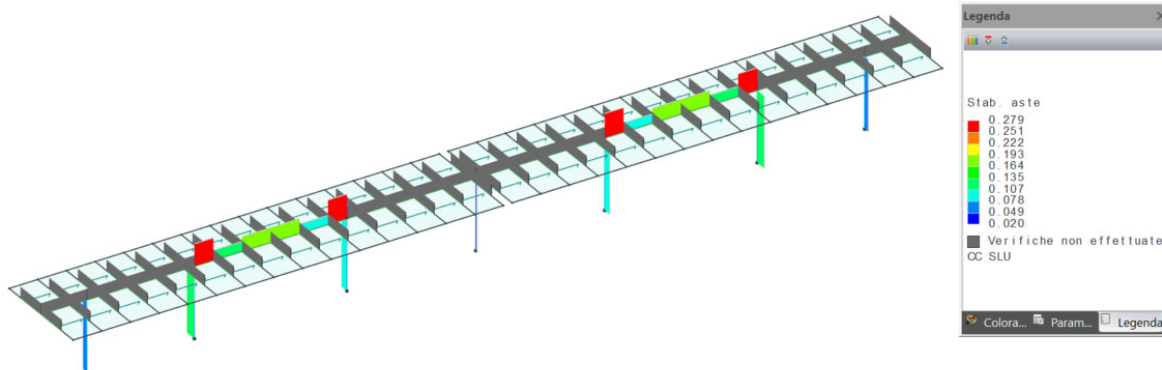


Diagramma tassi di sfruttamento stabilità aste combo SLU con valore massimo pari a 0,279

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

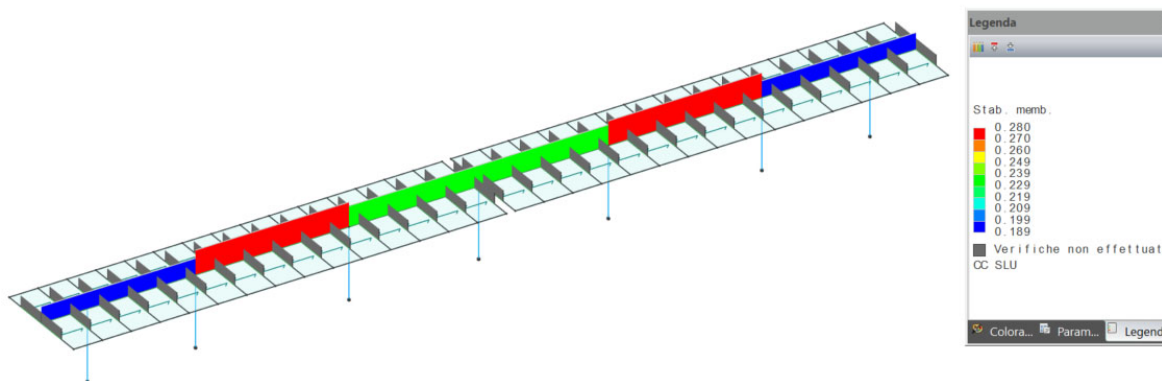


Diagramma tassi di sfruttamento stabilità membrature combo SLU con valore massimo pari a 0,280

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

Figure 27: Tassi di sfruttamento SLU (Stato limite ultimo)

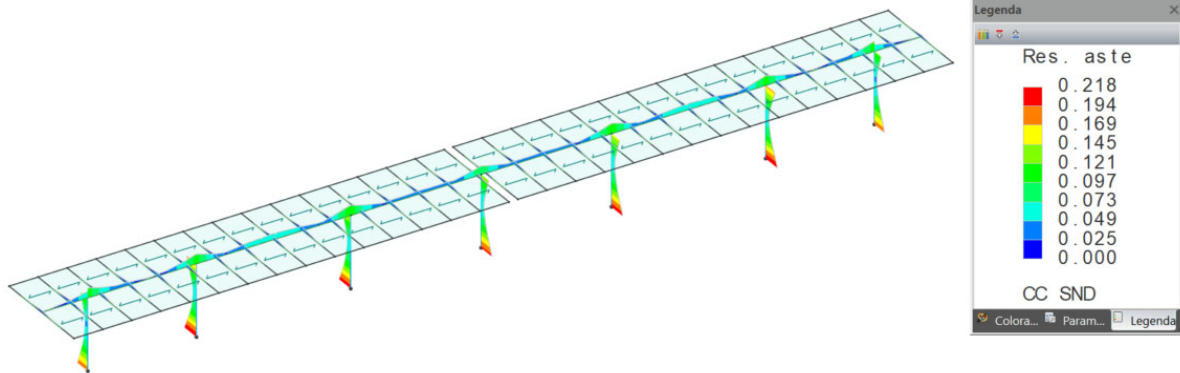


Diagramma tassi di sfruttamento resistenza aste combo SND con valore massimo pari a 0,218

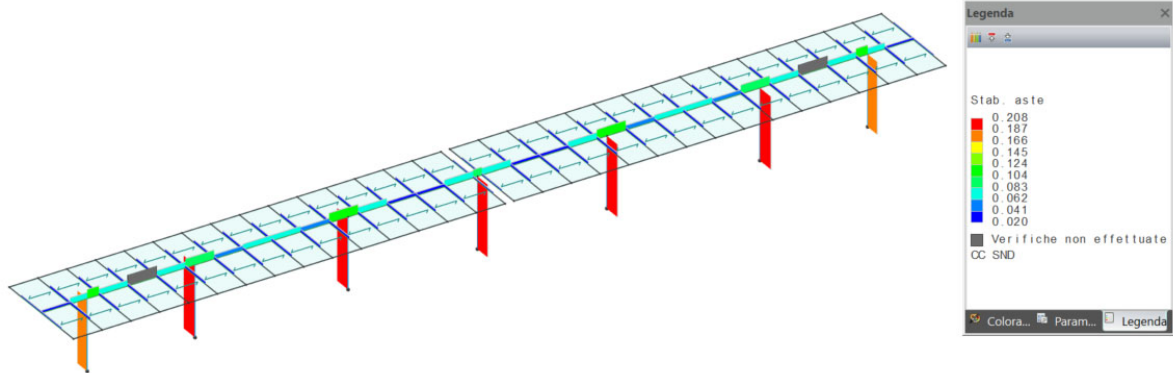


Diagramma tassi di sfruttamento stabilità aste combo SND con valore massimo pari a 0,208

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

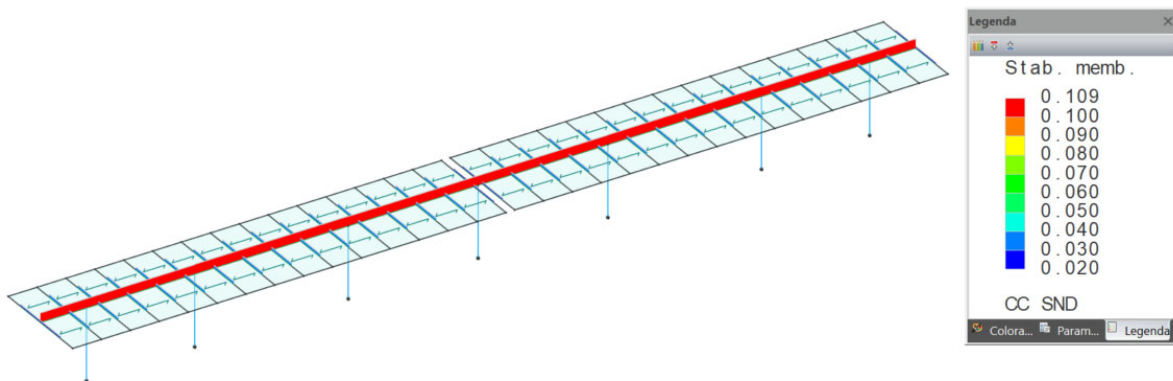
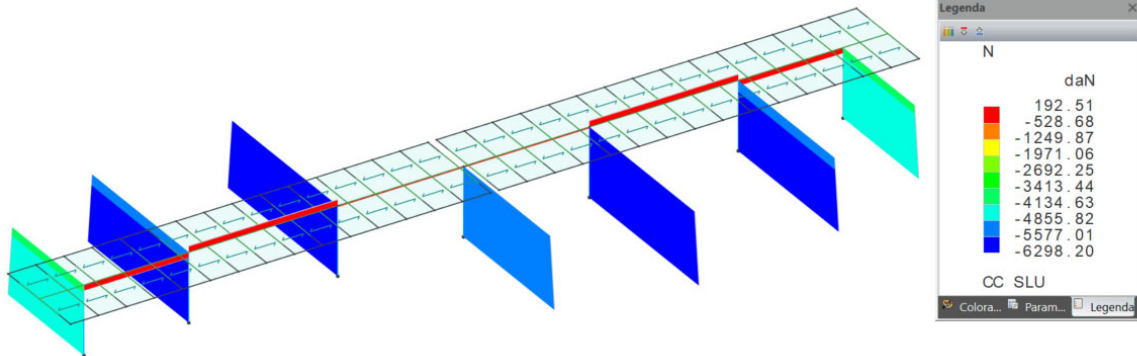


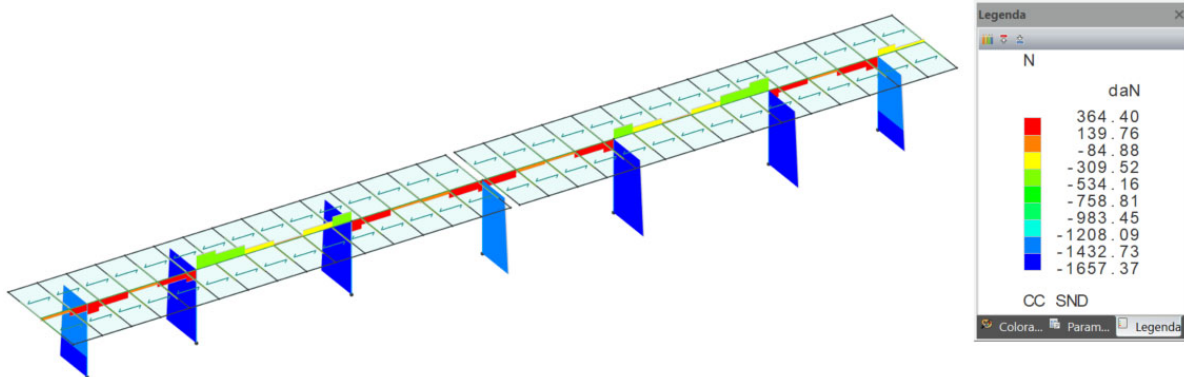
Diagramma tassi di sfruttamento stabilità membrature combo SND con valore massimo pari a 0,109

Figure 28: Tassi di sfruttamento SND (Stato limite di vita non dissipativo)

6.3.2 Sollecitazioni

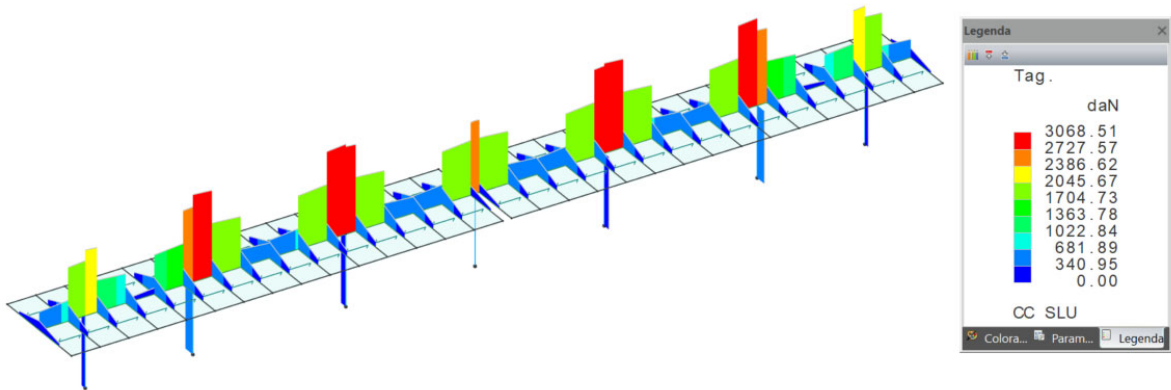


Inviluppo sforzo normale SLU $N_{max} = 6298,20$ daN (compressione)

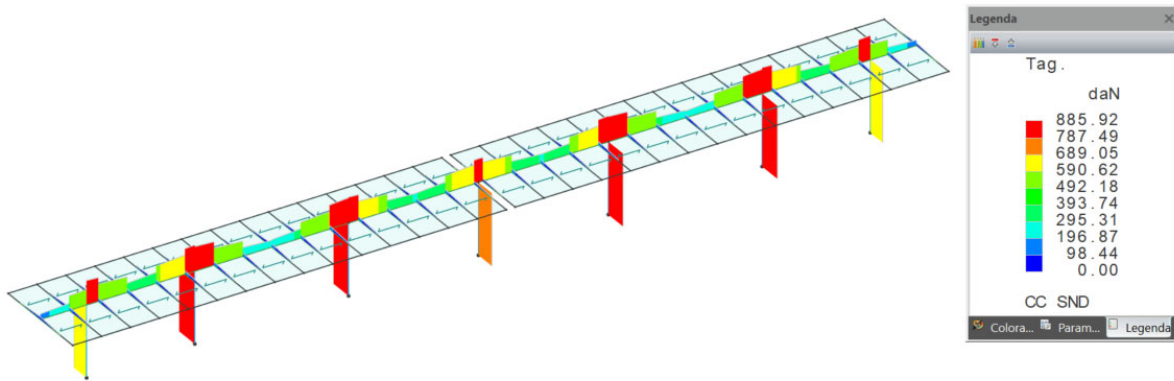


Inviluppo sforzo normale SND $N_{max} = -1657,37$ daN (compressione)

Figure 29: Sforzo Normale

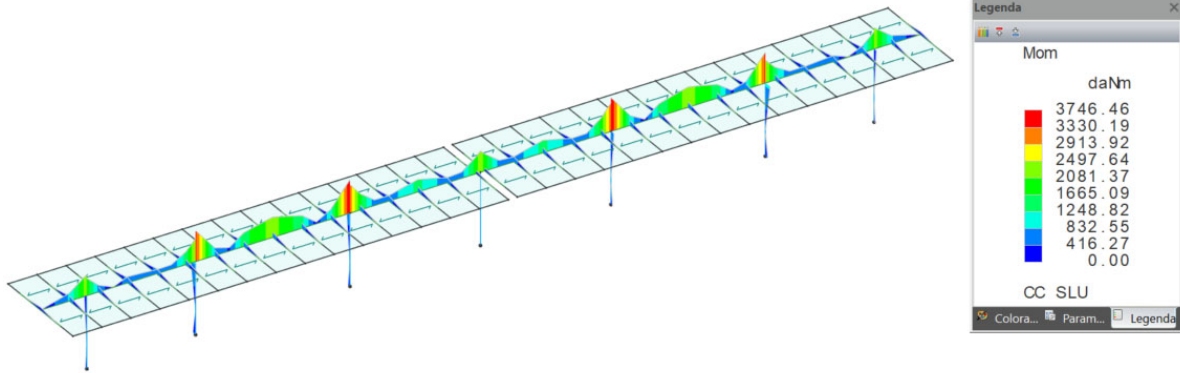


Inviluppo sforzo di taglio SLU Tmax = 3068,51 daN

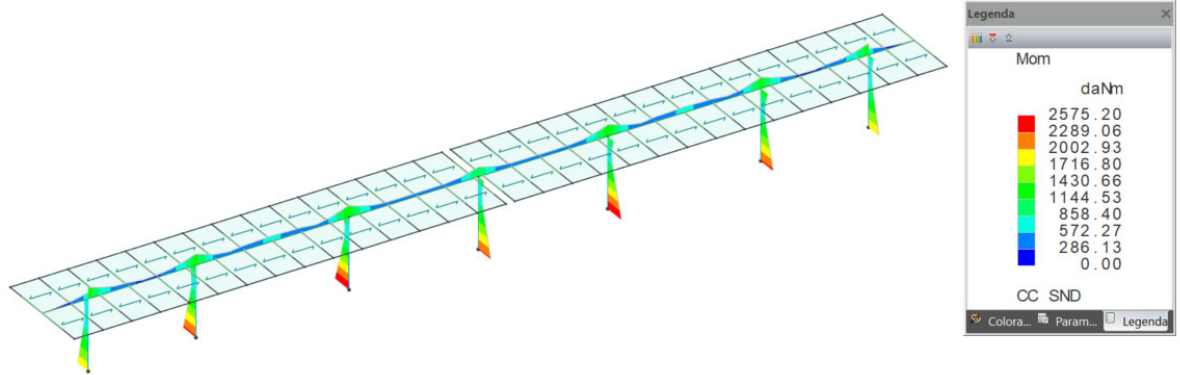


Inviluppo sforzo di taglio SND Tmax = 885,92 daN

Figure 30: Taglio



Inviluppo momento flettente SLU $M_{max} = 3746,46 \text{ daN}\times\text{m}$



Inviluppo momento flettente SND $M_{max} = 2575,20 \text{ daN}\times\text{m}$

Figure 31: Momento Flettente

6.3.3 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
 ModeSt ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
 Xfinest ver. 9.5.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18
 Tipo di calcolo: sismica statica
 Vincoli esterni: Considera sempre vincoli assegnati in modellazione
 Schematizzazione piani rigidi: nessun impalcato rigido
 Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Non sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
 - Calcolo sforzo nei nodi: No
 - Trascura deformabilità a taglio delle aste: No
 - Analisi dinamica con metodo di Lanczos: Sì
 - Check sequenza di Sturm: Sì
 - Analisi non lineare con Newton modificato: No
 - Usa formulazione secante per buckling: No
 - Trascura buckling torsionale: No
 - Opzioni aggiuntive per analisi non lineari in presenza di elementi bidimensionali con comportamento Drucker-Prager:
- OPTION PARAM CONV=E
 OPTION PARAM RESENNORM=1.E-8
 OPTION PARAM AUTO_INCREMENT=YES
 OPTION PARAM LINE_SEARCHES=YES
 OPTION PARAM BGINCRS=1.0
 OPTION PARAM AVINCRS=1.0

Dati struttura

- Sito di costruzione: CPHJ+42 Foggia FG, Italia LON. 15.73010 LAT. 41.42780
 Contenuto tra ID reticolo: 30559 30558 30337 30336

Simbologia

Ag =Accelerazione orizzontale massima al sito
 Cc =Coefficiente funzione della categoria del suolo
 Fo =Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
 Ss =Coefficiente di amplificazione stratigrafica
 Tr =Periodo di ritorno <anni>
 TCC=Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SND = Stato limite di salvaguardia della vita (non dissipativo)
 Tc* =Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

TCC	Tr	Ag <g>	Fo	Tc*	Ss	Cc
SLD	50	0.0554	2.54	0.33	1.50	1.52
SLV	475	0.1323	2.61	0.43	1.49	1.38

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale Vn: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 3.30 <m>
- Altezza della struttura: 3.30 <m>
- Numero piani edificio: 0
- Coefficiente 0: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia strutturale: acciaio a mensola o a pendolo inverso

Periodo T_1	0.20812
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovrarresistenza (α_u/α_i)	1.00
Valore di riferimento del fattore di comportamento (q_0)	1.00
Fattore riduttivo (K_w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di comportamento dissipativo (q)	1.00
Fattore di comportamento non dissipativo (qND)	1.00
Fattore di comportamento per SLD (qD)	1.00

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
- Coeff. amplificazione topografica S_T : 1.00
- Accelerazione di picco del terreno A_gS : 0.1976 <g>
- Fattore di comportamento per sisma verticale (qv): 1.50
- Smorzamento spettro: 5.00%

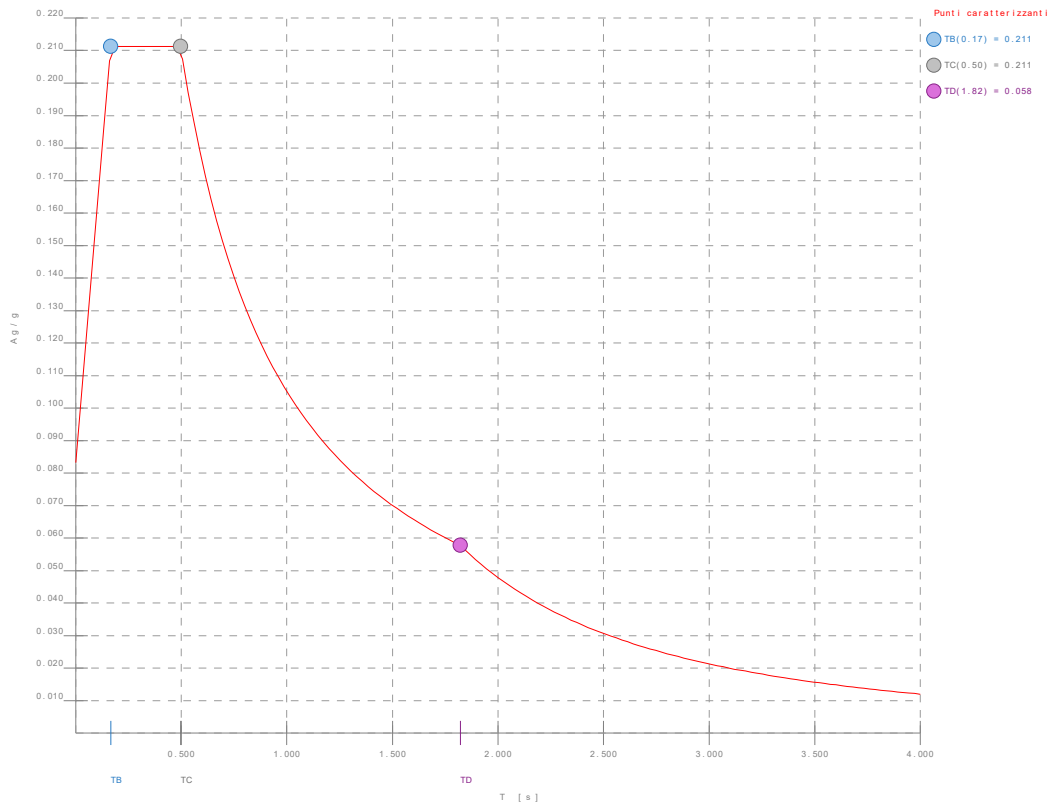


Figura numero 1: Spettro SLD

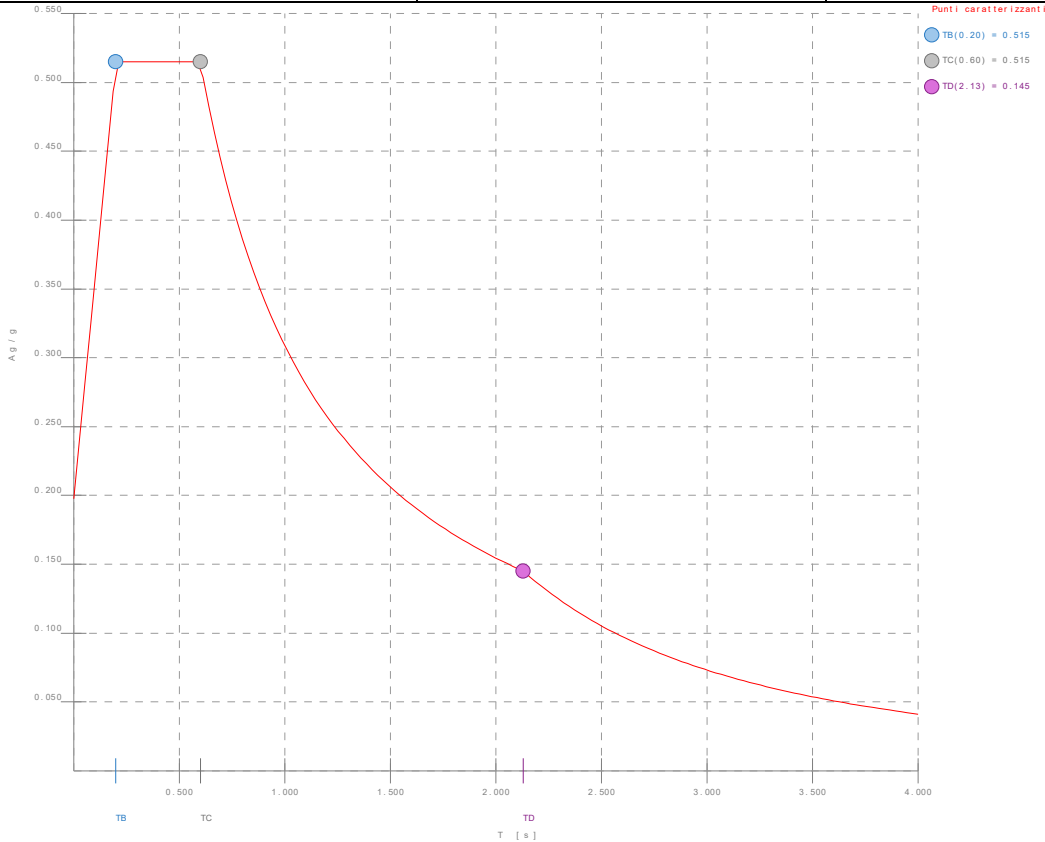


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>
 - Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

- N = Numero
- Comm. = Commento
- 1 = G1 - Peso Proprio
- 2 = G2 - Permanenti non strutturali
- 3 = Q - Variabili neve
- 4 = Q - Vento retro Cond.A
- 5 = Q - Vento retro Cond.B
- 6 = Q - Vento fronte Cond.C
- 7 = Q - Vento fronte Cond.D
- F = azioni orizzontali convenzionali
- SLU = Stato limite ultimo
- SLR = Stato limite per combinazioni rare
- SLE F = Stato limite per combinazioni frequenti
- SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
- S = Si
- N = No

NComm.	1	2	3	4	5	6	7	S	SLU	SLR	SLE F	SLQ
1 Calcolo sismico	S	S	S	N	N	N	N	N	S	N	N	N
2 Calcolo statico	S	S	S	N	N	N	N	S	S	S	S	S
3 Vento cond A	S	S	S	N	N	N	N	S	S	S	S	S
4 Vento cond B	S	S	S	N	N	N	N	S	S	S	S	S
5 Vento cond C	S	S	S	N	N	N	N	S	S	S	S	S
6 Vento cond D	S	S	S	N	N	N	N	S	S	S	S	S

Elenco combinazioni di carico simboliche

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	1	2	3	4	5	6	7	S	
1	Amb. 1 (Sisma)	SLU	S	1	1	ψ ₂	-----	-----	-----	-----	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	-----	-----	
3	Amb. 2 (SLE R)	SLE R	1	1	1	-----	-----	-----	-----	-----	
4	Amb. 2 (SLE F)	SLE F	1	1	ψ ₁	-----	-----	-----	-----	-----	
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ ₂	-----	-----	-----	-----	-----	
6	Amb. 3 (SLU)	SLU	γ max	γ max	ψ ₀ *γ max	γ max	-----	-----	-----	-----	



7	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	-----
8	Amb. 3 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
9	Amb. 3 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
10	Amb. 3 (SLE F)	SLE F	1	1	ψ_2	ψ_1	-----	-----	-----	-----
11	Amb. 3 (SLE F)	SLE F	1	1	ψ_1	ψ_2	-----	-----	-----	-----
12	Amb. 3 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	-----	-----	-----	-----
13	Amb. 4 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
14	Amb. 4 (SLU)	SLU	γ max	γ max	γ max	-----	$\psi_0 * \gamma$ max	-----	-----	-----
15	Amb. 4 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
16	Amb. 4 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
17	Amb. 4 (SLE F)	SLE F	1	1	ψ_2	-----	ψ_1	-----	-----	-----
18	Amb. 4 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_2	-----	-----	-----
19	Amb. 4 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	-----	-----	-----
20	Amb. 5 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	γ max	-----	-----	-----
21	Amb. 5 (SLU)	SLU	γ max	γ max	γ max	-----	$\psi_0 * \gamma$ max	-----	-----	-----
22	Amb. 5 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
23	Amb. 5 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
24	Amb. 5 (SLE F)	SLE F	1	1	ψ_2	-----	ψ_1	-----	-----	-----
25	Amb. 5 (SLE F)	SLE F	1	1	ψ_1	-----	ψ_2	-----	-----	-----
26	Amb. 5 (SLE Q)	SLE Q	1	1	ψ_2	-----	ψ_2	-----	-----	-----
27	Amb. 6 (SLU)	SLU	γ max	γ max	$\psi_0 * \gamma$ max	-----	-----	-----	γ max	-----
28	Amb. 6 (SLU)	SLU	γ max	γ max	γ max	-----	-----	-----	$\psi_0 * \gamma$ max	-----
29	Amb. 6 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	-----	-----
30	Amb. 6 (SLE R)	SLE R	1	1	ψ_0	1	-----	-----	ψ_0	-----
31	Amb. 6 (SLE F)	SLE F	1	1	ψ_2	-----	-----	-----	ψ_1	-----
32	Amb. 6 (SLE F)	SLE F	1	1	ψ_1	-----	-----	-----	ψ_2	-----
33	Amb. 6 (SLE Q)	SLE Q	1	1	ψ_2	-----	-----	-----	ψ_2	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: S1

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

An. = Tipo di analisi

L = Lineare

NL = Non lineare

Bk = Buckling

S = Si

N = No

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	S X	S Y
1	Amb. 1 (SLU S) S +X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
2	Amb. 1 (SLE) S +X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30
3	Amb. 1 (SLU S) S +X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
4	Amb. 1 (SLE) S +X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30
5	Amb. 1 (SLU S) S -X+0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
6	Amb. 1 (SLE) S -X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30
7	Amb. 1 (SLU S) S -X-0.3Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
8	Amb. 1 (SLE) S -X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30
9	Amb. 1 (SLU S) S +0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
10	Amb. 1 (SLE) S +0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	1.00
11	Amb. 1 (SLU S) S -0.3X+Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
12	Amb. 1 (SLE) S -0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	1.00
13	Amb. 1 (SLU S) S +0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
14	Amb. 1 (SLE) S +0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.30	-1.00
15	Amb. 1 (SLU S) S -0.3X-Y	SND	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
16	Amb. 1 (SLE) S -0.3X-Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	-0.30	-1.00
17	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.00	0.00	0.00	0.00	0.00
18	Amb. 2 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
19	Amb. 2 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
20	Amb. 2 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	0.75	1.50	0.00	0.00	0.00	0.00	0.00
22	Amb. 3 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
23	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	0.50	1.00	0.00	0.00	0.00	0.00	0.00
24	Amb. 3 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
25	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.20	0.00	0.00	0.00	0.00	0.00
26	Amb. 3 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
27	Amb. 3 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	1.50	0.00	0.00	0.00	0.00
29	Amb. 4 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
30	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	1.00	0.00	0.00	0.00	0.00
31	Amb. 4 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00
32	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.20	0.00	0.00	0.00	0.00
33	Amb. 4 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
34	Amb. 4 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
35	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	1.50	0.00	0.00	0.00
36	Amb. 5 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.00	0.00	0.00
37	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00
38	Amb. 5 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00
39	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00
40	Amb. 5 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
41	Amb. 5 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
42	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	0.75	0.00	0.00	0.00	1.50	0.00	0.00
43	Amb. 6 (SLU)	SLU	L	N	1.30	1.50	1.50	0.90	0.00	0.00	0.90	0.00	0.00
44	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00
45	Amb. 6 (SLE R)	SLE R	L	N	1.00	1.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00
46	Amb. 6 (SLE F)	SLE F	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.20	0.00	0.00



47	Amb. 6 (SLE F)	SLE F	L	N	1.00	1.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00
48	Amb. 6 (SLE Q)	SLE Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Elenco masse nodi

Simbologia
Mo = Massa orizzontale
Nodo = Numero del nodo

Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>	Nodo	Mo <kg>
-104	67.23	-103	67.23	-102	67.23	-101	67.23	-100	44.85	-99	44.85	-98	67.23	-97	67.23	-96	67.23	-95	67.23	-94	67.23
-93	67.23	-92	67.23	-91	67.23	-90	67.23	-89	67.23	-88	67.23	-87	67.23	-86	67.23	-85	67.23	-84	67.23	-83	67.23
-82	67.23	-81	67.23	-80	67.23	-79	67.23	-78	67.23	-77	67.23	-76	67.23	-75	67.23	-74	67.23	-73	67.23	-72	67.23
-71	67.23	-70	67.23	-69	67.23	-68	67.23	-67	67.23	-66	67.23	-65	44.85	-64	67.23	-63	44.85	-62	67.23	-61	67.23
-60	44.85	-59	44.85	-58	67.23	-57	67.23	-56	67.23	-55	67.23	-54	67.23	-53	67.23	-52	67.23	-51	44.85	-50	44.85
-49	67.23	-48	67.23	-47	67.23	-46	67.23	-45	67.23	-44	67.23	-43	67.23	-42	67.23	-41	67.23	-38	98.18	-37	138.14
-36	129.28	-35	131.89	-34	151.43	-33	151.43	-32	129.75	-31	129.28	-30	140.28	-29	151.43	-28	151.43	-27	151.43	-26	140.15
-25	129.88	-24	151.43	-23	151.43	-22	151.43	-21	103.10	-20	103.10	-19	151.43	-18	151.43	-17	151.43	-16	129.88	-15	140.15
-14	151.43	-13	151.43	-12	151.43	-11	140.28	-10	129.28	-9	129.75	-8	151.43	-7	151.43	-6	131.89	-5	129.28	-4	138.14
-3	98.18	203	129.28	204	106.28	205	129.28														

Totali masse nodi

Mo	
<kg>	9450.93

Elenco forze sismiche nodali allo SLD

Simbologia
Fx = Forza in dir. X
Fy = Forza in dir. Y
Nodo = Numero del nodo
cx = Coeff. c in dir. X
cy = Coeff. c in dir. Y

Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>
-104	0.01	0.01	13.94	13.94	-103	0.01	0.01	13.94	13.94	-102	0.01	0.01	13.94	13.94	-101	0.01	0.01	13.94	13.94	-100	0.00	0.00	9.30	9.30										
-99	0.00	0.00	9.30	9.30	-98	0.01	0.01	13.94	13.94	-97	0.01	0.01	13.94	13.94	-96	0.01	0.01	13.94	13.94	-95	0.01	0.01	13.94	13.94										
-94	0.01	0.01	13.94	13.94	-93	0.01	0.01	13.94	13.94	-92	0.01	0.01	13.94	13.94	-91	0.01	0.01	13.94	13.94	-90	0.01	0.01	13.94	13.94										
-89	0.01	0.01	13.94	13.94	-88	0.01	0.01	13.94	13.94	-87	0.01	0.01	13.94	13.94	-86	0.01	0.01	13.94	13.94	-85	0.01	0.01	13.94	13.94										
-84	0.01	0.01	13.94	13.94	-83	0.01	0.01	13.94	13.94	-82	0.01	0.01	13.94	13.94	-81	0.01	0.01	13.94	13.94	-80	0.01	0.01	13.94	13.94										
-79	0.01	0.01	13.94	13.94	-78	0.01	0.01	13.94	13.94	-77	0.01	0.01	13.94	13.94	-76	0.01	0.01	13.94	13.94	-75	0.01	0.01	13.94	13.94										
-74	0.01	0.01	13.94	13.94	-73	0.01	0.01	13.94	13.94	-72	0.01	0.01	13.94	13.94	-71	0.01	0.01	13.94	13.94	-70	0.01	0.01	13.94	13.94										
-69	0.01	0.01	13.94	13.94	-68	0.01	0.01	13.94	13.94	-67	0.01	0.01	13.94	13.94	-66	0.01	0.01	13.94	13.94	-65	0.00	0.00	9.30	9.30										
-64	0.01	0.01	13.94	13.94	-63	0.00	0.00	9.30	9.30	-62	0.01	0.01	13.94	13.94	-61	0.01	0.01	13.94	13.94	-60	0.00	0.00	9.30	9.30										
-59	0.00	0.00	9.30	9.30	-58	0.01	0.01	13.94	13.94	-57	0.01	0.01	13.94	13.94	-56	0.01	0.01	13.94	13.94	-55	0.01	0.01	13.94	13.94										
-54	0.01	0.01	13.94	13.94	-53	0.01	0.01	13.94	13.94	-52	0.01	0.01	13.94	13.94	-51	0.00	0.00	9.30	9.30	-50	0.00	0.00	9.30	9.30										
-49	0.01	0.01	13.94	13.94	-48	0.01	0.01	13.94	13.94	-47	0.01	0.01	13.94	13.94	-46	0.01	0.01	13.94	13.94	-45	0.01	0.01	13.94	13.94										
-44	0.01	0.01	13.94	13.94	-43	0.01	0.01	13.94	13.94	-42	0.01	0.01	13.94	13.94	-41	0.01	0.01	13.94	13.94	-38	0.01	0.01	20.35	20.35										
-37	0.01	0.01	28.64	28.64	-36	0.01	0.01	26.80	26.80	-35	0.01	0.01	27.34	27.34	-34	0.02	0.02	31.39	31.39	-33	0.02	0.02	31.39	31.39										
-32	0.01	0.01	26.90	26.90	-31	0.01	0.01	26.80	26.80	-30	0.01	0.01	29.08	29.08	-29	0.02	0.02	31.39	31.39	-28	0.02	0.02	31.39	31.39										
-27	0.02	0.02	31.39	31.39	-26	0.01	0.01	29.05	29.05	-25	0.01	0.01	26.92	26.92	-24	0.02	0.02	31.39	31.39	-23	0.02	0.02	31.39	31.39										
-22	0.02	0.02	31.39	31.39	-21	0.01	0.01	21.37	21.37	-20	0.01	0.01	21.37	21.37	-19	0.02	0.02	31.39	31.39	-18	0.02	0.02	31.39	31.39										
-17	0.02	0.02	31.39	31.39	-16	0.01	0.01	26.92	26.92	-15	0.01	0.01	29.05	29.05	-14	0.02	0.02	31.39	31.39	-13	0.02	0.02	31.39	31.39										
-12	0.02	0.02	31.39	31.39	-11	0.01	0.01	29.08	29.08	-10	0.01	0.01	26.80	26.80	-9	0.01	0.01	26.90	26.90	-8	0.02	0.02	31.39	31.39										
-7	0.02	0.02	31.39	31.39	-6	0.01	0.01	27.34	27.34	-5	0.01	0.01	26.80	26.80	-4	0.01	0.01	28.64	28.64	-3	0.01	0.01	20.35	20.35										
203	0.01	0.01	26.80	26.80	204	0.01	0.01	22.03	22.03	205	0.01	0.01	26.80	26.80																				

Totali forze sismiche

Fx <daN>	1959.23	Fy <daN>	1959.23
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Elenco forze sismiche nodali allo SND

Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>	Nodo	cx	cy	Fx <daN>	Fy <daN>
-104	0.01	0.01	33.96	33.96	-103	0.01	0.01	33.96	33.96	-102	0.01	0.01	33.96	33.96	-101	0.01	0.01	33.96	33.96	-100	0.00	0.00	22.66	22.66										
-99	0.00	0.00	22.66	22.66	-98	0.01	0.01	33.96	33.96	-97	0.01	0.01	33.96	33.96	-96	0.01	0.01	33.96	33.96	-95	0.01	0.01	33.96	33.96										
-94	0.01	0.01	33.96	33.96	-93	0.01	0.01	33.96	33.96	-92	0.01	0.01	33.96	33.96	-91	0.01	0.01	33.96	33.96	-90	0.01	0.01	33.96	33.96										
-89	0.01	0.01	33.96	33.96	-88	0.01	0.01	33.96	33.96	-87	0.01	0.01	33.96	33.96	-86	0.01	0.01	33.96	33.96	-85	0.01	0.01	33.96	33.96										
-84	0.01	0.01	33.96	33.96	-83	0.01	0.01	33.96	33.96	-82	0.01	0.01	33.96	33.96	-81	0.01	0.01	33.96	33.96	-80	0.01	0.01	33.96	33.96										
-79	0.01	0.01	33.96	33.96	-78	0.01	0.01	33.96	33.96	-77	0.01	0.01	33.96	33.96	-76	0.01	0.01	33.96	33.96	-75	0.01	0.01	33.96	33.96										
-74	0.01	0.01	33.96	33.96	-73	0.01	0.01	33.96	33.96	-72	0.01	0.01	33.96	33.96	-71	0.01	0.01	33.96	33.96	-70	0.01	0.01	33.96	33.96										
-69	0.01	0.01	33.96	33.96	-68	0.01	0.01	33.96	33.96	-67	0.01	0.01	33.96	33.96	-66	0.01	0.01	33.96	33.96	-65	0.00	0.00	22.66	22.66										
-64	0.01	0.01	33.96	33.96	-63	0.00	0.00	22.66	22.66	-62	0.01	0.01	33.96	33.96	-61	0.01	0.01	33.96	33.96	-60	0.00	0.00	22.66	22.66										
-59	0.00	0.00	22.66	22.66	-58	0.01	0.01	33.96	33.96	-57	0.01	0.01	33.96	33.96	-56	0.01	0.01	33.96	33.96	-55	0.01	0.01	33.96	33.96										
-54	0.01	0.01	33.96	33.96	-53	0.01	0.01	33.96	33.96	-52	0.01	0.01	33.96	33.96	-51	0.00	0.00	22.66	22.66	-50	0.00	0.00	22.66	22.66										
-49	0.01	0.01	33.96	33.96	-48	0.01	0.01	33.96	33.96	-47	0.01	0.01	33.96	33.96	-46	0.01	0.01	33.96	33.96	-45	0.01	0.01	33.96	33.96										
-44	0.01	0.01	33.96	33.96	-43	0.01	0.01	33.96	33.96	-42	0.01	0.01	33.96	33.96	-41	0.01	0.01	33.96	33.96	-38	0.01	0.01	49.60	49.60										
-37	0.01	0.01	69.78	69.78	-36	0.01	0.01	65.31	65.31	-35	0.01	0.01	66.63	66.63	-34	0.02	0.02	76.49	76.49	-33	0.02	0.02	76.49	76.49										
-32	0.01	0.01	65.54	65.54	-31	0.01	0.01	65.31	65.31	-30	0.01	0.01	70.86	70.86	-29	0.02	0.02	76.49	76.49	-28	0.02	0.02	76.49	76.49										
-27	0.02	0.02	76.49	76.49	-26	0.01	0.01	70.80	70.80	-25																								



Simbologia
 CC = Numero della combinazione delle condizioni di carico elementari
 Fx = Reazione vincolare (forza) in dir. X
 Fy = Reazione vincolare (forza) in dir. Y
 Fz = Reazione vincolare (forza) in dir. Z
 Mx = Reazione vincolare (momento) intorno all'asse X
 My = Reazione vincolare (momento) intorno all'asse Y
 Mz = Reazione vincolare (momento) intorno all'asse Z
 Nodo = Numero del nodo
 TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SND = Stato limite di salvaguardia della vita (non dissipativo)

Nodo	CC	TCC	Fx <daN>	Fy <daN>	Fz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>
1	Max	5	SND 542.86	13 SND 565.98	29 SLU 4350.84	11 SND 1899.64	5 SND 1107.10	11 SND 0.11
1	Min	1	SND -662.32	9 SND -565.98	1 SND 883.76	13 SND -1899.64	13 SND -1237.31	1 SND -0.11
2	Max	5	SND 832.33	13 SND 701.25	29 SLU 5782.99	9 SND 2296.89	5 SND 1423.19	13 SND 0.45
2	Min	1	SND -637.90	9 SND -701.25	25 SLE F 1228.65	13 SND -2296.89	9 SND -1211.01	1 SND -0.45
3	Max	5	SND 630.73	13 SND 777.34	29 SLU 6298.20	9 SND 2536.13	5 SND 1203.56	11 SND 0.24
3	Min	1	SND -751.74	9 SND -777.34	25 SLE F 1336.18	13 SND -2536.13	13 SND -1335.51	1 SND -0.24
4	Max	5	SND 716.36	13 SND 685.09	29 SLU 5226.35	9 SND 2289.61	5 SND 1296.97	11 SND 0.00
4	Min	1	SND -716.36	9 SND -685.09	25 SLE F 1212.17	13 SND -2289.61	13 SND -1296.97	1 SND 0.00
5	Max	5	SND 751.74	13 SND 777.34	29 SLU 6298.20	9 SND 2536.13	5 SND 1335.51	13 SND 0.24
5	Min	1	SND -630.73	9 SND -777.34	25 SLE F 1336.18	13 SND -2536.13	9 SND -1203.56	1 SND -0.24
6	Max	5	SND 637.90	13 SND 701.25	29 SLU 5782.99	9 SND 2296.89	5 SND 1211.01	9 SND 0.45
6	Min	1	SND -832.33	9 SND -701.25	25 SLE F 1228.65	13 SND -2296.89	13 SND -1423.19	1 SND -0.45
7	Max	5	SND 662.32	13 SND 565.98	29 SLU 4350.85	9 SND 1899.65	5 SND 1237.31	15 SND 0.11
7	Min	1	SND -542.86	9 SND -565.98	5 SND 883.76	13 SND -1899.65	9 SND -1107.10	1 SND -0.11

Sollecitazioni aste

Simbologia
 Asta = Numero dell'asta
 CC = Numero della combinazione delle condizioni di carico elementari
 Mx = Momento torcente intorno all'asse X
 My = Momento flettente intorno all'asse Y
 Mz = Momento flettente intorno all'asse Z
 N = Sforzo normale
 N1 = Nodo1
 N2 = Nodo2
 Ty = Taglio in dir. Y
 Tz = Taglio in dir. Z
 X = Coordinata progressiva rispetto al nodo iniziale

Tipo di combinazione di carico: SND

Asta	N1	N2	X <cm>	N <daN>	CC	Ty <daN>	Mz <daNm>	Tz <daN>	My <daNm>	Mx <daNm>	CC	
1	1	-5	Max	0.00	-883.76	1	542.86	5	1237.31	1	565.98	13
1	1	-5	Max	330.00	-694.52	1	542.86	5	684.33	5	565.98	13
1	1	-5	Min.	0.00	-1483.62	5	-662.32	1	-1107.10	5	-565.98	9
1	1	-5	Min.	330.00	-1294.38	5	-662.32	1	-948.33	1	-565.98	9
2	2	-10	Max	0.00	-1295.40	5	832.33	5	1211.01	1	701.25	13
2	2	-10	Max	330.00	-1106.16	5	832.33	5	1323.50	5	701.25	13
2	2	-10	Min.	0.00	-1646.69	1	-637.90	1	-1423.19	5	-701.25	9
2	2	-10	Min.	330.00	-1457.45	1	-637.90	1	-894.05	1	-701.25	9
3	3	203	Max	0.00	-1543.26	1	630.73	5	1335.51	1	777.34	13
3	3	203	Max	330.00	-1354.02	1	630.73	5	877.85	5	777.34	13
3	3	203	Min.	0.00	-1657.37	5	-751.74	1	-1203.56	5	-777.34	9
3	3	203	Min.	330.00	-1468.14	5	-751.74	1	-1145.22	1	-777.34	9
4	4	204	Max	0.00	-1423.57	1	716.36	1	1296.97	5	685.09	9
4	4	204	Max	330.00	-1234.34	1	716.36	1	1067.00	1	685.09	9
4	4	204	Min.	0.00	-1423.57	1	-716.36	5	-1296.97	1	-685.09	13
4	4	204	Min.	330.00	-1234.34	1	-716.36	5	-1067.00	5	-685.09	13
5	5	205	Max	0.00	-1543.26	5	630.73	1	1335.51	5	777.34	9
5	5	205	Max	330.00	-1354.02	5	630.73	1	877.85	1	777.34	9
5	5	205	Min.	0.00	-1657.37	1	-751.74	5	-1203.56	1	-777.34	13
5	5	205	Min.	330.00	-1468.14	1	-751.74	5	-1145.22	5	-777.34	13
6	6	-31	Max	0.00	-1295.40	1	832.33	1	1211.01	5	701.25	9
6	6	-31	Max	330.00	-1106.16	1	832.33	1	1323.50	1	701.25	9
6	6	-31	Min.	0.00	-1646.69	5	-637.90	5	-1423.19	1	-701.25	13
6	6	-31	Min.	330.00	-1457.45	5	-637.90	5	-894.05	5	-701.25	13
7	7	-36	Max	0.00	-883.76	5	542.86	1	1237.31	5	565.98	9
7	7	-36	Max	330.00	-694.52	5	542.86	1	684.33	1	565.98	9
7	7	-36	Min.	0.00	-1483.62	1	-662.32	5	-1107.10	1	-565.98	13
7	7	-36	Min.	330.00	-1294.39	1	-662.32	5	-948.33	5	-565.98	13
201	-4	-3	Max	0.00	94.91	5	94.91	9	126.73	13	216.51	1
201	-4	-3	Max	133.53	94.91	5	94.91	9	0.00	9	152.11	1
201	-4	-3	Min.	0.00	-94.91	1	-94.91	13	-126.73	11	216.51	1
201	-4	-3	Min.	133.53	-94.91	1	-94.91	13	0.00	15	152.11	1
201	-5	-4	Max	0.00	232.61	5	232.61	9	311.58	13	470.88	1
201	-5	-4	Max	79.47	232.61	5	232.61	9	126.73	13	432.55	1
201	-5	-4	Min.	0.00	-232.61	1	-232.61	13	-311.58	11	470.88	1
201	-5	-4	Min.	79.47	-232.61	1	-232.61	13	-126.73	11	432.55	1
201	-6	-5	Max	0.00	364.40	1	268.06	13	166.53	13	-197.57	1
201	-6	-5	Max	54.07	364.40	1	268.06	13	311.47	13	-223.65	1
201	-6	-5	Min.	0.00	-244.94	5	-268.06	9	-166.53	11	-797.43	5
201	-6	-5	Min.	54.07	-244.94	5	-268.06	9	-311.47	11	-823.50	5
201	-7	-6	Max	0.00	229.85	1	133.52	13	11.76	9	82.88	1
201	-7	-6	Max	133.53	229.85	1	133.52	13	166.53	13	18.47	1
201	-7	-6	Min.	0.00	-110.40	7	-133.52	11	-11.76	15	-516.98	5
201	-7	-6	Min.	133.53	-110.40	7	-133.52	11	-166.53	11	-581.38	5
201	-8	-7	Max	0.00	85.44	1	10.90	9	2.79	13	363.32	1
201	-8	-7	Max	133.53	85.44	1	10.90	9	11.76	9	298.92	1
201	-8	-7	Min.	0.00	34.02	7	-10.90	15	-2.79	11	-236.54	5
201	-8	-7	Min.	133.53	34.02	7	-10.90	15	-11.76	15	-300.94	5
201	-9	-8	Max	0.00	178.43	5	155.31	9	210.18	13	643.77	1
201	-9	-8	Max	0.00	178.43	5	155.31	9	210.18	13	643.77	1



205	-28	-29	Max	133.53	96.96	5	63.97	9	242.92	13	-36.75	5	499.58	5	14.68	9
205	-28	-29	Min.	0.00	-171.93	3	-63.97	15	-328.35	9	-220.91	1	505.65	5	-14.68	15
205	-28	-29	Min.	57.34					-87.50	5			513.58	5		
205	-28	-29	Min.	133.53	-171.93	3	-63.97	15	-242.92	11	-285.32	1	199.86	1	-14.68	15
205	-29	-30	Max	0.00	241.37	5	208.39	9	242.92	15	-252.79	5	499.58	5	14.68	9
205	-29	-30	Max	133.53	241.37	5	208.39	9	35.35	9	-317.20	5	119.02	5	14.68	9
205	-29	-30	Min.	0.00	-316.35	1	-208.39	13	-242.92	9	-501.36	1	199.84	1	-14.68	15
205	-29	-30	Min.	133.53	-316.35	1	-208.39	13	-35.35	13	-565.77	1	-512.64	1	-14.68	15
205	-30	-31	Max	0.00	380.16	5	347.17	9	35.34	11	-533.24	5	119.03	5	14.68	9
205	-30	-31	Max	88.20	380.16	5	347.17	9	341.55	9	-575.78	5	-370.05	5	14.68	9
205	-30	-31	Min.	0.00	-455.13	1	-347.17	13	-35.34	13	-781.81	1	-512.62	1	-14.68	15
205	-30	-31	Min.	88.20	-455.13	1	-347.17	13	-341.55	13	-824.35	1	-1220.94	1	-14.68	15
206	-31	-32	Max	0.00	311.89	1	288.77	13	341.10	9	881.68	5	102.56	1	31.92	11
206	-31	-32	Max	45.33	311.89	1	288.77	13	210.19	11	859.81	5	225.36	1	31.92	11
206	-31	-32	Min.	0.00	-192.43	5	-288.77	9	-341.10	13	281.82	1	-1264.09	5	-31.92	13
206	-31	-32	Min.	45.33	-192.43	5	-288.77	9	-210.19	13	259.95	1	-869.35	5	-31.92	13
206	-32	-33	Max	0.00	178.43	1	155.31	13	210.19	9	643.77	5	225.35	1	31.92	11
206	-32	-33	Max	91.04					20.64	1			245.34	1		
206	-32	-33	Max	133.53	178.43	1	155.31	13	2.80	9	579.37	5	240.99	1	31.92	11
206	-32	-33	Min.	0.00	-58.97	7	-155.31	9	-210.19	15	43.91	1	-869.38	5	-31.92	13
206	-32	-33	Min.	91.04					20.64	1			245.34	1		
206	-32	-33	Min.	133.53	-58.97	7	-155.31	9	-2.80	15	-20.49	1	-52.73	5	-31.92	13
206	-33	-34	Max	0.00	85.44	5	10.90	13	2.79	9	363.32	5	240.99	1	31.92	11
206	-33	-34	Max	133.53	85.44	5	10.90	13	11.75	13	298.92	5	389.46	5	31.92	11
206	-33	-34	Min.	0.00	34.02	3	-10.90	11	-2.79	15	-236.54	1	-52.69	5	-31.92	13
206	-33	-34	Min.	133.53	34.02	3	-10.90	11	-11.75	11	-300.94	1	-117.87	1	-31.92	13
206	-34	-35	Max	0.00	229.86	5	133.52	9	11.75	15	82.88	5	389.45	5	31.92	11
206	-34	-35	Max	133.53	229.86	5	133.52	9	166.54	9	18.47	5	457.12	5	31.92	11
206	-34	-35	Min.	0.00	-110.39	3	-133.52	13	-11.75	9	-516.98	1	-117.86	1	-31.92	13
206	-34	-35	Min.	133.53	-110.39	3	-133.52	13	-166.54	13	-581.39	1	-851.21	1	-31.92	13
206	-35	-36	Max	0.00	364.40	5	268.06	9	166.53	9	-197.57	5	457.12	5	31.92	11
206	-35	-36	Max	54.07	364.40	5	268.06	9	311.47	9	-223.64	5	343.26	5	31.92	11
206	-35	-36	Min.	0.00	-244.94	1	-268.06	13	-166.53	15	-797.43	1	-851.19	1	-31.92	13
206	-35	-36	Min.	54.07	-244.94	1	-268.06	13	-311.47	15	-823.50	1	-1289.38	1	-31.92	13
206	-36	-37	Max	0.00	232.61	1	232.61	13	311.59	9	470.88	1	-605.09	1	0.00	1
206	-36	-37	Max	79.47	232.61	1	232.61	13	126.74	9	432.55	1	-246.12	1	0.00	1
206	-36	-37	Min.	0.00	-232.61	5	-232.61	9	-311.59	15	470.88	1	-605.09	1	0.00	1
206	-36	-37	Min.	79.47	-232.61	5	-232.61	9	-126.74	15	432.55	1	-246.12	1	0.00	1
206	-37	-38	Max	0.00	94.91	1	94.91	13	126.73	9	216.51	1	-246.11	1	0.00	1
206	-37	-38	Max	133.53	94.91	1	94.91	13	0.00	13	152.10	1	0.00	1	0.00	1
206	-37	-38	Min.	0.00	-94.91	5	-94.91	9	-126.73	15	216.51	1	-246.11	1	0.00	1
206	-37	-38	Min.	133.53	-94.91	5	-94.91	9	-0.00	11	152.10	1	0.00	1	0.00	1
301	-3	-60	Max	0.00	22.66	13	22.66	5	33.98	1	76.05	1	-65.99	1	0.00	1
301	-3	-60	Max	150.00	22.66	13	22.66	5	0.00	1	11.94	1	0.00	1	0.00	1
301	-3	-60	Min.	0.00	-22.66	9	-22.66	1	-33.98	5	76.05	1	-65.99	1	0.00	1
301	-3	-60	Min.	150.00	-22.66	9	-22.66	1	0.00	5	11.94	1	0.00	1	0.00	1
301	-59	-3	Max	0.00	22.66	9	22.66	1	0.00	7	-11.94	1	0.00	7	0.00	1
301	-59	-3	Max	150.00	22.66	9	22.66	1	33.98	1	-76.05	1	-65.99	1	0.00	1
301	-59	-3	Min.	0.00	-22.66	13	-22.66	5	0.00	1	-11.94	1	0.00	1	0.00	1
301	-59	-3	Min.	150.00	-22.66	13	-22.66	5	-33.98	5	-76.05	1	-65.99	1	0.00	1
302	-4	-47	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
302	-4	-47	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
302	-4	-47	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
302	-4	-47	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
302	-46	-4	Max	0.00	33.96	9	33.96	1	0.00	3	-23.88	1	0.00	15	0.00	1
302	-46	-4	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
302	-46	-4	Min.	0.00	-33.96	13	-33.96	5	0.00	5	-23.88	1	0.00	9	0.00	1
302	-46	-4	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
303	-6	-48	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
303	-6	-48	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
303	-6	-48	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
303	-6	-48	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
303	-49	-6	Max	0.00	33.96	9	33.96	1	0.00	1	-23.88	1	0.00	9	0.00	1
303	-49	-6	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
303	-49	-6	Min.	0.00	-33.96	13	-33.96	5	0.00	5	-23.88	1	0.00	15	0.00	1
303	-49	-6	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
304	-7	-96	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
304	-7	-96	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
304	-7	-96	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
304	-7	-96	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
304	-95	-7	Max	0.00	33.96	9	33.96	1	0.00	1	-23.88	1	0.00	13	0.00	1
304	-95	-7	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
304	-95	-7	Min.	0.00	-33.96	13	-33.96	5	0.00	5	-23.88	1	0.00	11	0.00	1
304	-95	-7	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
305	-8	-66	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
305	-8	-66	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
305	-8	-66	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
305	-8	-66	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
305	-67	-8	Max	0.00	33.96	9	33.96	1	0.00	3	-23.88	1	0.00	9	0.00	1
305	-67	-8	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
305	-67	-8	Min.	0.00	-33.96	13	-33.96	5	0.00	5	-23.88	1	0.00	13	0.00	1
305	-67	-8	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
306	-9	-69	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
306	-9	-69	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
306	-9	-69	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
306	-9	-69	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
306	-68	-9	Max	0.00	33.96	9	33.96	1	0.00	5	-23.88	1	0.00			



308	-12	-72	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
308	-73	-12	Max	0.00	33.96	9	33.96	1	0.00	3	-23.88	1	0.00	13	0.00	1
308	-73	-12	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
308	-73	-12	Min.	0.00	-33.96	13	-33.96	5	0.00	5	-23.88	1	0.00	9	0.00	1
308	-73	-12	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
309	-13	-74	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
309	-13	-74	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
309	-13	-74	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
309	-13	-74	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
309	-75	-13	Max	0.00	33.96	9	33.96	1	0.00	5	-23.88	1	0.00	9	0.00	1
309	-75	-13	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
309	-75	-13	Min.	0.00	-33.96	13	-33.96	5	0.00	3	-23.88	1	0.00	13	0.00	1
309	-75	-13	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
310	-14	-90	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
310	-14	-90	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
310	-14	-90	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
310	-14	-90	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
310	-91	-14	Max	0.00	33.96	9	33.96	1	0.00	1	-23.88	1	0.00	1	0.00	1
310	-91	-14	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
310	-91	-14	Min.	0.00	-33.96	13	-33.96	5	0.00	1	-23.88	1	0.00	1	0.00	1
310	-91	-14	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
311	-15	-92	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
311	-15	-92	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
311	-15	-92	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
311	-15	-92	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
311	-93	-15	Max	0.00	33.96	9	33.96	1	0.00	1	-23.88	1	0.00	1	0.00	1
311	-93	-15	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
311	-93	-15	Min.	0.00	-33.96	13	-33.96	5	0.00	5	-23.88	1	0.00	5	0.00	1
311	-93	-15	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
312	-16	-98	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
312	-16	-98	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
312	-16	-98	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
312	-16	-98	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
312	-94	-16	Max	0.00	33.96	9	33.96	1	0.00	7	-23.88	1	0.00	13	0.00	1
312	-94	-16	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
312	-94	-16	Min.	0.00	-33.96	13	-33.96	5	0.00	1	-23.88	1	0.00	9	0.00	1
312	-94	-16	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
313	-17	-97	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
313	-17	-97	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
313	-17	-97	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
313	-17	-97	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
313	-42	-17	Max	0.00	33.96	9	33.96	1	0.00	9	-23.88	1	0.00	9	0.00	1
313	-42	-17	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
313	-42	-17	Min.	0.00	-33.96	13	-33.96	5	0.00	13	-23.88	1	0.00	13	0.00	1
313	-42	-17	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
314	-18	-43	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
314	-18	-43	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
314	-18	-43	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
314	-18	-43	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
314	-44	-18	Max	0.00	33.96	9	33.96	1	0.00	5	-23.88	1	0.00	5	0.00	1
314	-44	-18	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
314	-44	-18	Min.	0.00	-33.96	13	-33.96	5	0.00	1	-23.88	1	0.00	1	0.00	1
314	-44	-18	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
315	-19	-45	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
315	-19	-45	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
315	-19	-45	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
315	-19	-45	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
315	-58	-19	Max	0.00	33.96	9	33.96	1	0.00	3	-23.88	1	0.00	13	0.00	1
315	-58	-19	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
315	-58	-19	Min.	0.00	-33.96	13	-33.96	5	0.00	5	-23.88	1	0.00	11	0.00	1
315	-58	-19	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
316	-20	-63	Max	0.00	22.66	13	22.66	5	33.98	1	76.05	1	-65.99	1	0.00	1
316	-20	-63	Max	150.00	22.66	13	22.66	5	0.00	1	11.94	1	0.00	1	0.00	1
316	-20	-63	Min.	0.00	-22.66	9	-22.66	1	-33.98	5	76.05	1	-65.99	1	0.00	1
316	-20	-63	Min.	150.00	-22.66	9	-22.66	1	0.00	5	11.94	1	0.00	1	0.00	1
316	-65	-20	Max	0.00	22.66	9	22.66	1	0.00	1	-11.94	1	0.00	1	0.00	1
316	-65	-20	Max	150.00	22.66	9	22.66	1	33.98	1	-76.05	1	-65.99	1	0.00	1
316	-65	-20	Min.	0.00	-22.66	13	-22.66	5	0.00	1	-11.94	1	0.00	1	0.00	1
316	-65	-20	Min.	150.00	-22.66	13	-22.66	5	-33.98	5	-76.05	1	-65.99	1	0.00	1
317	-21	-51	Max	0.00	22.66	13	22.66	5	33.98	1	76.05	1	-65.99	1	0.00	1
317	-21	-51	Max	150.00	22.66	13	22.66	5	0.00	1	11.94	1	0.00	1	0.00	1
317	-21	-51	Min.	0.00	-22.66	9	-22.66	1	-33.98	5	76.05	1	-65.99	1	0.00	1
317	-21	-51	Min.	150.00	-22.66	9	-22.66	1	0.00	5	11.94	1	0.00	1	0.00	1
317	-50	-21	Max	0.00	22.66	9	22.66	1	0.00	1	-11.94	1	0.00	13	0.00	1
317	-50	-21	Max	150.00	22.66	9	22.66	1	33.98	1	-76.05	1	-65.99	1	0.00	1
317	-50	-21	Min.	0.00	-22.66	13	-22.66	5	0.00	7	-11.94	1	0.00	9	0.00	1
317	-50	-21	Min.	150.00	-22.66	13	-22.66	5	-33.98	5	-76.05	1	-65.99	1	0.00	1
318	-22	-53	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
318	-22	-53	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
318	-22	-53	Min.	0.00	-33.96	9	-33.96	1	-50.94	5	108.02	1	-98.92	1	0.00	1
318	-22	-53	Min.	150.00	-33.96	9	-33.96	1	0.00	1	23.88	1	0.00	1	0.00	1
318	-52	-22	Max	0.00	33.96	9	33.96	1	0.00	3	-23.88	1	0.00	11	0.00	1
318	-52	-22	Max	150.00	33.96	9	33.96	1	50.94	1	-108.02	1	-98.92	1	0.00	1
318	-52	-22	Min.	0.00	-33.96	13	-33.96	5	0.00	5	-23.88	1	0.00	13	0.00	1
318	-52	-22	Min.	150.00	-33.96	13	-33.96	5	-50.94	5	-108.02	1	-98.92	1	0.00	1
319	-23	-55	Max	0.00	33.96	13	33.96	5	50.94	1	108.02	1	-98.92	1	0.00	1
319	-23	-55	Max	150.00	33.96	13	33.96	5	0.00	5	23.88	1	0.00	1	0.00	1
319	-23	-55	Min.	0.00	-33.96	9	-33.96	1	-50.94</							



1	1	-5	Max	0.00	-1060.61	2	187.56	6	546.15	2	232.26	14	779.57	10	0.05	14
1	1	-5	Max	330.00	-871.37	2	187.56	6	203.00	6	232.26	14	13.10	12	0.05	14
1	1	-5	Min.	0.00	-1306.77	6	-307.02	2	-415.94	6	-232.26	10	-779.57	14	-0.05	12
1	1	-5	Min.	330.00	-1117.54	6	-307.02	2	-467.00	2	-232.26	10	-13.10	14	-0.05	12
2	2	-10	Max	0.00	-1398.96	6	398.89	6	434.42	2	287.78	14	942.59	10	0.19	10
2	2	-10	Max	330.00	-1209.73	6	398.89	6	669.74	6	287.78	14	7.07	16	0.19	10
2	2	-10	Min.	0.00	-1543.13	2	-204.46	2	-646.60	6	-287.78	10	-942.59	14	-0.19	14
2	2	-10	Min.	330.00	-1353.89	2	-204.46	2	-240.29	2	-287.78	10	-7.07	10	-0.19	14
3	3	203	Max	0.00	-1576.90	2	223.16	6	586.96	2	319.00	14	1040.77	10	0.10	14
3	3	203	Max	330.00	-1387.66	2	223.16	6	281.43	6	319.00	14	11.94	16	0.10	14
3	3	203	Min.	0.00	-1623.73	6	-344.17	2	-455.01	6	-319.00	10	-1040.77	14	-0.10	12
3	3	203	Min.	330.00	-1434.50	6	-344.17	2	-548.79	2	-319.00	10	-11.94	10	-0.10	12
4	4	204	Max	0.00	-1423.57	2	293.98	2	532.25	6	281.14	10	939.60	14	0.00	14
4	4	204	Max	330.00	-1234.34	2	293.98	2	437.87	2	281.14	10	11.83	16	0.00	14
4	4	204	Min.	0.00	-1423.57	2	-293.98	6	-532.25	2	-281.14	14	-939.60	12	0.00	12
4	4	204	Min.	330.00	-1234.34	2	-293.98	6	-437.87	6	-281.14	14	-11.83	10	0.00	12
5	5	205	Max	0.00	-1576.90	6	223.16	2	586.96	6	319.00	10	1040.77	14	0.10	10
5	5	205	Max	330.00	-1387.66	6	223.16	2	281.43	2	319.00	10	11.94	12	0.10	10
5	5	205	Min.	0.00	-1623.73	2	-344.17	6	-455.01	2	-319.00	14	-1040.77	10	-0.10	14
5	5	205	Min.	330.00	-1434.50	2	-344.17	6	-548.79	6	-319.00	14	-11.94	14	-0.10	14
6	6	-31	Max	0.00	-1398.96	2	398.89	2	434.42	6	287.78	10	942.59	14	0.19	14
6	6	-31	Max	330.00	-1209.73	2	398.89	2	669.74	2	287.78	10	7.07	12	0.19	14
6	6	-31	Min.	0.00	-1543.13	6	-204.46	6	-646.60	2	-287.78	14	-942.59	10	-0.19	10
6	6	-31	Min.	330.00	-1353.89	6	-204.46	6	-240.29	6	-287.78	14	-7.07	14	-0.19	10
7	7	-36	Max	0.00	-1060.61	6	187.56	2	546.15	6	232.26	10	779.57	14	0.05	10
7	7	-36	Max	330.00	-871.37	6	187.56	2	203.00	2	232.26	10	13.10	16	0.05	10
7	7	-36	Min.	0.00	-1306.78	2	-307.02	6	-415.94	2	-232.26	14	-779.57	10	-0.05	16
7	7	-36	Min.	330.00	-1117.54	2	-307.02	6	-467.01	6	-232.26	14	-13.10	10	-0.05	16
201	-4	-3	Max	0.00	38.95	6	38.95	10	52.01	14	216.51	2	-246.11	2	0.00	2
201	-4	-3	Max	133.53	38.95	6	38.95	10	0.00	10	152.11	2	0.00	2	0.00	2
201	-4	-3	Min.	0.00	-38.95	2	-38.95	14	-52.01	12	216.51	2	-246.11	2	0.00	2
201	-4	-3	Min.	133.53	-38.95	2	-38.95	14	0.00	16	152.11	2	0.00	2	0.00	2
201	-5	-4	Max	0.00	95.46	6	95.46	10	127.86	14	470.88	2	-605.07	2	0.00	2
201	-5	-4	Max	79.47	95.46	6	95.46	10	52.01	14	432.55	2	-246.11	2	0.00	2
201	-5	-4	Min.	0.00	-95.46	2	-95.46	14	-127.86	12	470.88	2	-605.07	2	0.00	2
201	-5	-4	Min.	79.47	-95.46	2	-95.46	14	-52.01	12	432.55	2	-246.11	2	0.00	2
201	-6	-5	Max	0.00	184.76	2	110.01	14	68.34	14	-374.41	2	71.41	2	13.10	16
201	-6	-5	Max	54.07	184.76	2	110.01	14	127.82	14	-400.49	2	-138.07	2	13.10	16
201	-6	-5	Min.	0.00	-65.30	6	-110.01	12	-68.34	12	-620.58	6	-465.49	6	-13.10	10
201	-6	-5	Min.	54.07	-65.30	6	-110.01	12	-127.82	12	-646.66	6	-808.07	6	-13.10	10
201	-7	-6	Max	0.00	129.54	2	54.79	14	4.82	10	-93.97	2	239.89	2	13.10	16
201	-7	-6	Max	133.53	129.54	2	54.79	14	68.34	14	-158.37	2	71.41	2	13.10	16
201	-7	-6	Min.	0.00	-10.09	8	-54.79	12	-4.82	16	-340.14	6	31.70	6	-13.10	10
201	-7	-6	Min.	133.53	-10.09	8	-54.79	12	-68.34	12	-404.54	6	-465.49	6	-13.10	10
201	-8	-7	Max	0.00	70.28	2	4.47	10	1.15	14	186.48	2	154.41	6	13.10	16
201	-8	-7	Max	54.88	70.28	2	4.47	10	1.31	12	1.31	12	119.49	12	13.10	16
201	-8	-7	Min.	0.00	49.18	8	-4.47	16	-1.15	12	-59.69	6	33.88	2	-13.10	10
201	-8	-7	Min.	54.88	49.18	8	-4.47	16	-1.31	12	1.31	12	119.49	12	-13.10	10
201	-8	-7	Min.	133.53	49.18	8	-4.47	16	-4.82	16	-124.09	6	31.70	6	-13.10	10
201	-9	-8	Max	0.00	108.44	6	63.74	10	86.25	16	466.93	2	-97.37	6	13.10	16
201	-9	-8	Max	133.53	108.44	6	63.74	10	1.15	14	402.52	2	154.41	6	13.10	16
201	-9	-8	Min.	0.00	11.02	4	-63.74	16	-86.25	10	220.76	6	-546.62	2	-13.10	10
201	-9	-8	Min.	133.53	11.02	4	-63.74	16	-1.15	12	156.35	6	33.88	2	-13.10	10
201	-10	-9	Max	0.00	163.21	6	118.50	10	139.98	14	704.83	2	-300.35	6	13.10	16
201	-10	-9	Max	45.33	163.21	6	118.50	10	86.26	14	682.97	2	-97.38	6	13.10	16
201	-10	-9	Min.	0.00	-43.75	4	-118.50	16	-139.98	10	458.66	6	-861.19	2	-13.10	10
201	-10	-9	Min.	45.33	-43.75	4	-118.50	16	-86.26	12	436.80	6	-546.62	2	-13.10	10
202	-11	-10	Max	0.00	133.91	2	142.47	14	14.50	16	-606.52	2	-67.19	2	6.03	16
202	-11	-10	Max	88.20	133.91	2	142.47	14	140.16	14	-649.06	2	-620.90	2	6.03	16
202	-11	-10	Min.	0.00	-208.88	6	-142.47	10	-14.50	20	-708.52	6	-326.41	6	-6.03	10
202	-11	-10	Min.	88.20	-208.88	6	-142.47	10	-140.16	10	-751.06	6	-970.09	6	-6.03	10
202	-12	-11	Max	0.00	76.95	2	85.52	14	99.69	12	-326.07	2	411.22	2	6.03	14
202	-12	-11	Max	133.53	76.95	2	85.52	14	14.50	14	-390.48	2	-67.19	2	6.03	14
202	-12	-11	Min.	0.00	-151.92	6	-85.52	10	-99.69	14	-428.08	6	288.22	6	-6.03	10
202	-12	-11	Min.	133.53	-151.92	6	-85.52	10	-14.50	12	-492.48	6	-326.41	6	-6.03	10
202	-13	-12	Max	0.00	17.69	2	26.25	14	134.75	10	-45.63	2	528.36	6	6.03	16
202	-13	-12	Max	133.53	17.69	2	26.25	14	99.69	10	-110.03	2	411.22	2	6.03	16
202	-13	-12	Min.	0.00	-92.66	8	-26.25	12	-134.75	14	-147.63	6	515.15	2	-6.03	10
202	-13	-12	Min.	133.53	-92.66	8	-26.25	12	-99.69	16	-212.04	6	288.22	6	-6.03	10
202	-14	-13	Max	0.00	-33.40	6	33.01	10	90.67	12	234.82	2	394.01	6	6.03	14
202	-14	-13	Max	133.53	-33.40	6	33.01	10	134.75	10	170.42	2	528.36	6	6.03	14
202	-14	-13	Min.	0.00	-41.58	4	-33.01	16	-90.67	14	132.81	6	244.58	2	-6.03	10
202	-14	-13	Min.	133.53	-41.58	4	-33.01	16	-134.75	14	68.41	6	515.15	2	-6.03	10
202	-15	-14	Max	0.00	25.87	6	92.28	10	32.55	16	515.27	2	-114.83	6	6.03	14
202	-15	-14	Max	133.53	25.87	6	92.28	10	90.67	10	450.86	2	394.01	6	6.03	14
202	-15	-14	Min.	0.00	-100.84	4	-92.28	14	-32.55	10	413.26	6	-400.47	2	-6.03	10
202	-15	-14	Min.	133.53	-100.84	4	-92.28	14	-90.67	16	348.86	6	244.59	2	-6.03	10
202	203	-15	Max	0.00	82.80	6	149.20	10	163.35	14	773.59	2	-685.05	6	6.03	14
202	203	-15	Max	87.67	82.80	6	149.20	10	32.55	14	731.31	2	-114.83	6	6.03	14
202	203	-15	Min.	0.00	-157.77	2	-149.20	14	-163.35	10	671.59	6	-1060.12	2	-6.03	10
202	203	-15	Min.	87.67	-157.77	2	-149.20	14	-32.55	10	629.30	6	-400.47	2	-6.03	10
203	-16	203	Max	0.00	159.60	2	143.00	14	97.66	16	-591.95	2	-234.73	2	5.91	12
203	-16	203	Max	45.87	159.60	2	143.00	14	163.25	14	-614.07	2	-511.31	2	5.91	12
203	-16	203	Min.	0.00	-113.57	8	-143.00	10	-97.66	10	-740.79	6	-621.61	6	-5.91	14
203	-16	203	Min.	45.87	-113.57	8	-143.00	10	-163.25	10	-762.91	6	-966.46	6	-5.91	14



203	-20	-19	Min.	133.53	-72.99	4	-89.59	16	-18.27	16	316.59	6	18.68	2	-5.91	14
203	204	-20	Max	0.00	158.99	6	129.56	10	127.27	14	691.59	2	-345.30	6	5.91	12
203	204	-20	Max	20.00	158.99	6	129.56	10	101.36	14	681.94	2	-237.72	6	5.91	12
203	204	-20	Min.	0.00	-112.95	4	-129.56	14	-127.27	12	542.75	6	-783.17	2	-5.91	14
203	204	-20	Min.	20.00	-112.95	4	-129.56	14	-101.36	12	533.10	6	-645.82	2	-5.91	14
204	204	-21	Max	0.00	158.99	2	129.56	14	127.27	12	691.59	6	-345.30	2	5.91	16
204	204	-21	Max	20.00	158.99	2	129.56	14	101.36	12	681.94	6	-237.72	2	5.91	16
204	204	-21	Min.	0.00	-112.95	8	-129.56	10	-127.27	14	542.75	2	-783.17	6	-5.91	10
204	204	-21	Min.	20.00	-112.95	8	-129.56	10	-101.36	14	533.10	2	-645.82	6	-5.91	10
204	-21	-22	Max	0.00	119.02	2	89.59	14	101.36	12	529.83	6	-237.72	2	5.91	16
204	-21	-22	Max	133.53	119.02	2	89.59	14	18.27	14	465.43	6	228.04	2	5.91	16
204	-21	-22	Min.	0.00	-72.99	8	-89.59	12	-101.36	14	381.00	2	-645.82	6	-5.91	10
204	-21	-22	Min.	133.53	-72.99	8	-89.59	12	-18.27	12	316.59	2	18.68	6	-5.91	10
204	-22	-23	Max	0.00	59.76	2	30.32	14	18.27	16	249.39	6	228.03	2	5.91	16
204	-22	-23	Max	133.53	59.76	2	30.32	14	58.76	14	184.99	6	319.30	2	5.91	16
204	-22	-23	Min.	0.00	-13.72	8	-30.32	12	-18.27	10	100.55	2	18.67	6	-5.91	10
204	-22	-23	Min.	133.53	-13.72	8	-30.32	12	-58.76	10	36.15	2	308.69	6	-5.91	10
204	-23	-24	Max	0.00	45.54	6	28.94	10	58.76	16	-31.06	6	319.30	2	5.91	16
204	-23	-24	Max	133.53	45.54	6	28.94	10	20.12	14	-95.46	6	224.22	6	5.91	16
204	-23	-24	Min.	0.00	0.49	4	-28.94	16	-58.76	10	-179.90	2	308.70	6	-5.91	10
204	-23	-24	Min.	133.53	0.49	4	-28.94	16	-20.12	12	-244.30	2	36.08	2	-5.91	10
204	-24	-25	Max	0.00	104.81	6	88.20	10	20.12	16	-311.50	6	224.22	6	5.91	16
204	-24	-25	Max	133.53	104.81	6	88.20	10	97.66	10	-375.91	6	-234.74	6	5.91	16
204	-24	-25	Min.	0.00	-58.77	4	-88.20	16	-20.12	10	-460.34	2	36.08	2	-5.91	10
204	-24	-25	Min.	133.53	-58.77	4	-88.20	16	-97.66	16	-524.75	2	-621.63	2	-5.91	10
204	-25	205	Max	0.00	159.60	6	143.00	10	97.66	12	-591.95	6	-234.73	6	5.91	16
204	-25	205	Max	45.87	159.60	6	143.00	10	163.25	10	-614.07	6	-511.31	6	5.91	16
204	-25	205	Min.	0.00	-113.57	4	-143.00	14	-97.66	14	-740.79	2	-621.61	2	-5.91	10
204	-25	205	Min.	45.87	-113.57	4	-143.00	14	-163.25	14	-762.91	2	-966.46	2	-5.91	10
205	205	-26	Max	0.00	82.80	2	149.20	14	163.35	10	773.59	6	-685.06	2	6.03	10
205	205	-26	Max	87.67	82.80	2	149.20	14	32.55	10	731.31	6	-114.83	2	6.03	10
205	205	-26	Min.	0.00	-157.77	6	-149.20	10	-163.35	14	671.58	2	-1060.12	6	-6.03	16
205	205	-26	Min.	87.67	-157.77	6	-149.20	10	-32.55	14	629.30	2	-400.48	6	-6.03	16
205	-26	-27	Max	0.00	25.87	2	92.28	14	32.55	12	515.26	6	-114.81	2	6.03	10
205	-26	-27	Max	133.53	25.87	2	92.28	14	90.67	16	450.86	6	394.02	2	6.03	10
205	-26	-27	Min.	0.00	-100.84	8	-92.28	10	-32.55	14	413.26	2	-400.45	6	-6.03	16
205	-26	-27	Min.	133.53	-100.84	8	-92.28	10	-90.67	10	348.85	2	244.60	6	-6.03	16
205	-27	-28	Max	0.00	-33.40	2	33.01	14	90.67	14	234.82	6	394.01	2	6.03	10
205	-27	-28	Max	133.53	-33.40	2	33.01	14	134.75	14	170.42	6	528.36	2	6.03	10
205	-27	-28	Min.	0.00	-41.58	8	-33.01	10	-90.67	12	132.81	2	244.59	6	-6.03	16
205	-27	-28	Min.	133.53	-41.58	8	-33.01	10	-134.75	12	68.41	2	515.15	6	-6.03	16
205	-28	-29	Max	0.00	17.69	6	26.25	10	134.75	14	-45.62	6	528.36	2	6.03	10
205	-28	-29	Max	133.53	17.69	6	26.25	10	99.69	14	-110.03	6	411.22	6	6.03	10
205	-28	-29	Min.	0.00	-92.66	4	-26.25	16	-134.75	10	-147.63	2	515.14	6	-6.03	16
205	-28	-29	Min.	133.53	-92.66	4	-26.25	16	-99.69	12	-212.03	2	288.22	2	-6.03	16
205	-29	-30	Max	0.00	76.95	6	85.52	10	99.69	16	-326.07	6	411.21	6	6.03	10
205	-29	-30	Max	133.53	76.95	6	85.52	10	14.51	10	-390.48	6	-67.20	6	6.03	10
205	-29	-30	Min.	0.00	-151.92	2	-85.52	14	-99.69	10	-428.08	2	288.21	2	-6.03	16
205	-29	-30	Min.	133.53	-151.92	2	-85.52	14	-14.51	14	-492.48	2	-326.42	2	-6.03	16
205	-30	-31	Max	0.00	133.91	6	142.47	10	14.50	12	-606.52	6	-67.19	6	6.03	10
205	-30	-31	Max	88.20	133.91	6	142.47	10	140.16	10	-649.06	6	-620.90	6	6.03	10
205	-30	-31	Min.	0.00	-208.88	2	-142.47	14	-14.50	14	-708.53	2	-326.41	2	-6.03	16
205	-30	-31	Min.	88.20	-208.88	2	-142.47	14	-140.16	14	-751.07	2	-970.09	2	-6.03	16
206	-31	-32	Max	0.00	163.21	2	118.50	14	139.98	10	704.83	6	-300.34	2	13.10	12
206	-31	-32	Max	45.33	163.21	2	118.50	14	86.25	12	682.97	6	-97.37	2	13.10	12
206	-31	-32	Min.	0.00	-43.75	8	-118.50	10	-139.98	14	458.66	2	-861.19	6	-13.10	14
206	-31	-32	Min.	45.33	-43.75	8	-118.50	10	-86.25	14	436.80	2	-546.62	6	-13.10	14
206	-32	-33	Max	0.00	108.44	2	63.74	14	86.26	10	466.93	6	-97.39	2	13.10	12
206	-32	-33	Max	133.53	108.44	2	63.74	14	1.15	10	402.52	6	154.40	2	13.10	12
206	-32	-33	Min.	0.00	11.02	8	-63.74	12	-86.26	16	220.76	2	-546.64	6	-13.10	14
206	-32	-33	Min.	133.53	11.02	8	-63.74	12	-1.15	16	156.35	2	33.86	6	-13.10	14
206	-33	-34	Max	0.00	70.28	6	4.47	14	1.15	10	186.48	6	154.41	2	13.10	12
206	-33	-34	Max	54.88	70.28	6	4.47	14	-1.31	10	-119.49	10				
206	-33	-34	Min.	133.53	70.28	6	4.47	14	4.82	14	122.07	6	239.90	6	13.10	12
206	-33	-34	Min.	0.00	49.18	4	-4.47	12	-1.15	16	-59.69	2	33.89	6	-13.10	14
206	-33	-34	Min.	54.88	49.18	4	-4.47	12	-1.31	10	-119.49	10				
206	-33	-34	Min.	133.53	49.18	4	-4.47	12	-4.82	12	-124.10	2	31.70	2	-13.10	14
206	-34	-35	Max	0.00	129.55	6	54.79	10	4.82	16	-93.97	6	239.89	6	13.10	12
206	-34	-35	Max	133.53	129.55	6	54.79	10	68.34	10	-158.37	6	71.41	6	13.10	12
206	-34	-35	Min.	0.00	-10.08	4	-54.79	16	-4.82	10	-340.14	2	31.70	2	-13.10	14
206	-34	-35	Min.	133.53	-10.08	4	-54.79	16	-68.34	14	-404.54	2	-465.50	2	-13.10	14
206	-35	-36	Max	0.00	184.76	6	110.01	10	68.34	10	-374.41	6	71.42	6	13.10	12
206	-35	-36	Max	54.07	184.76	6	110.01	10	127.82	10	-400.49	6	-138.06	6	13.10	12
206	-35	-36	Min.	0.00	-65.30	2	-110.01	14	-68.34	16	-620.58	2	-465.48	2	-13.10	14
206	-35	-36	Min.	54.07	-65.30	2	-110.01	14	-127.82	16	-646.66	2	-808.06	2	-13.10	14
206	-36	-37	Max	0.00	95.46	2	95.46	14	127.87	10	470.88	2	-605.09	2	0.00	2
206	-36	-37	Max	79.47	95.46	2	95.46	14	52.01	10	432.55	2	-246.12	2	0.00	2
206	-36	-37	Min.	0.00	-95.46	6	-95.46	10	-127.87	16	470.88	2	-605.09	2	0.00	2
206	-36	-37	Min.	79.47	-95.46	6	-95.46	10	-52.01	16	432.55	2	-246.12	2	0.00	2
206	-37	-38	Max	0.00	38.95	2	38.95	14	52.01	10	216.51	2	-246.11	2	0.00	2
206	-37	-38	Max	133.53	38.95	2	38.95	14	0.00	14	152.10	2	0.00	2	0.00	2
206	-37	-38	Min.	0.00	-38.95	6	-38.95	10	-52.01	16	216.51	2	-246.11	2	0.00	2
206	-37	-38	Min.	133.53	-38.95	6	-38.95	10	-0.00	12	152.10	2	0.00	2	0.00	2
301	-3	-60	Max	0.00	9.30	14	9.30	6	13.95	2	76.05	2	-65.99	2	0.00	2
301	-3	-60	Max	150.00	9.30	14	9									



315	-58	-19	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
316	-20	-63	Max	0.00	9.30	14	9.30	6	13.95	2	76.05	2	-65.99	2	0.00	2
316	-20	-63	Max	150.00	9.30	14	9.30	6	0.00	2	11.94	2	0.00	2	0.00	2
316	-20	-63	Min.	0.00	-9.30	10	-9.30	2	-13.95	6	76.05	2	-65.99	2	0.00	2
316	-20	-63	Min.	150.00	-9.30	10	-9.30	2	0.00	6	11.94	2	0.00	2	0.00	2
316	-65	-20	Max	0.00	9.30	10	9.30	2	0.00	2	-11.94	2	0.00	2	0.00	2
316	-65	-20	Max	150.00	9.30	10	9.30	2	13.95	2	-76.05	2	-65.99	2	0.00	2
316	-65	-20	Min.	0.00	-9.30	14	-9.30	6	0.00	2	-11.94	2	0.00	2	0.00	2
316	-65	-20	Min.	150.00	-9.30	14	-9.30	6	-13.95	6	-76.05	2	-65.99	2	0.00	2
317	-21	-51	Max	0.00	9.30	14	9.30	6	13.95	2	76.05	2	-65.99	2	0.00	2
317	-21	-51	Max	150.00	9.30	14	9.30	6	0.00	2	11.94	2	0.00	2	0.00	2
317	-21	-51	Min.	0.00	-9.30	10	-9.30	2	-13.95	6	76.05	2	-65.99	2	0.00	2
317	-21	-51	Min.	150.00	-9.30	10	-9.30	2	0.00	6	11.94	2	0.00	2	0.00	2
317	-50	-21	Max	0.00	9.30	10	9.30	2	0.00	2	-11.94	2	0.00	14	0.00	2
317	-50	-21	Max	150.00	9.30	10	9.30	2	13.95	2	-76.05	2	-65.99	2	0.00	2
317	-50	-21	Min.	0.00	-9.30	14	-9.30	6	0.00	8	-11.94	2	0.00	10	0.00	2
317	-50	-21	Min.	150.00	-9.30	14	-9.30	6	-13.95	6	-76.05	2	-65.99	2	0.00	2
318	-22	-53	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
318	-22	-53	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
318	-22	-53	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
318	-22	-53	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
318	-52	-22	Max	0.00	13.94	10	13.94	2	0.00	4	-23.88	2	0.00	12	0.00	2
318	-52	-22	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
318	-52	-22	Min.	0.00	-13.94	14	-13.94	6	0.00	6	-23.88	2	0.00	14	0.00	2
318	-52	-22	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
319	-23	-55	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
319	-23	-55	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
319	-23	-55	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
319	-23	-55	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
319	-54	-23	Max	0.00	13.94	10	13.94	2	0.00	8	-23.88	2	0.00	10	0.00	2
319	-54	-23	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
319	-54	-23	Min.	0.00	-13.94	14	-13.94	6	0.00	2	-23.88	2	0.00	14	0.00	2
319	-54	-23	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
320	-24	-57	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
320	-24	-57	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
320	-24	-57	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
320	-24	-57	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
320	-56	-24	Max	0.00	13.94	10	13.94	2	0.00	6	-23.88	2	0.00	2	0.00	2
320	-56	-24	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
320	-56	-24	Min.	0.00	-13.94	14	-13.94	6	0.00	2	-23.88	2	0.00	2	0.00	2
320	-56	-24	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
322	-25	-41	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
322	-25	-41	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
322	-25	-41	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
322	-25	-41	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
322	-64	-25	Max	0.00	13.94	10	13.94	2	0.00	8	-23.88	2	0.00	10	0.00	2
322	-64	-25	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
322	-64	-25	Min.	0.00	-13.94	14	-13.94	6	0.00	2	-23.88	2	0.00	16	0.00	2
322	-64	-25	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
323	-26	-77	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
323	-26	-77	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
323	-26	-77	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
323	-26	-77	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
323	-76	-26	Max	0.00	13.94	10	13.94	2	0.00	4	-23.88	2	0.00	10	0.00	2
323	-76	-26	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
323	-76	-26	Min.	0.00	-13.94	14	-13.94	6	0.00	6	-23.88	2	0.00	14	0.00	2
323	-76	-26	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
324	-27	-79	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
324	-27	-79	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
324	-27	-79	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
324	-27	-79	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
324	-78	-27	Max	0.00	13.94	10	13.94	2	0.00	4	-23.88	2	0.00	10	0.00	2
324	-78	-27	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
324	-78	-27	Min.	0.00	-13.94	14	-13.94	6	0.00	6	-23.88	2	0.00	14	0.00	2
324	-78	-27	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
325	-28	-81	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
325	-28	-81	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
325	-28	-81	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
325	-28	-81	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
325	-80	-28	Max	0.00	13.94	10	13.94	2	0.00	6	-23.88	2	0.00	10	0.00	2
325	-80	-28	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
325	-80	-28	Min.	0.00	-13.94	14	-13.94	6	0.00	4	-23.88	2	0.00	14	0.00	2
325	-80	-28	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
326	-29	-83	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
326	-29	-83	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
326	-29	-83	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
326	-29	-83	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
326	-82	-29	Max	0.00	13.94	10	13.94	2	0.00	10	-23.88	2	0.00	14	0.00	2
326	-82	-29	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
326	-82	-29	Min.	0.00	-13.94	14	-13.94	6	0.00	14	-23.88	2	0.00	10	0.00	2
326	-82	-29	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
327	-30	-85	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
327	-30	-85	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
327	-30	-85	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
327	-30	-85	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
327	-84	-30	Max	0.00	13.94	10	13.94	2	0.00	6	-23.88	2	0.00	10	0.00	2
327	-84	-30	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
327	-84	-30	Min.	0.00	-13.94	14										



330	-88	-33	Max	0.00	13.94	10	13.94	2	0.00	8	-23.88	2	0.00	14	0.00	2
330	-88	-33	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
330	-88	-33	Min.	0.00	-13.94	14	-13.94	6	0.00	2	-23.88	2	0.00	12	0.00	2
330	-88	-33	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
331	-34	-61	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
331	-34	-61	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
331	-34	-61	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
331	-34	-61	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
331	-62	-34	Max	0.00	13.94	10	13.94	2	0.00	2	-23.88	2	0.00	10	0.00	2
331	-62	-34	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
331	-62	-34	Min.	0.00	-13.94	14	-13.94	6	0.00	8	-23.88	2	0.00	14	0.00	2
331	-62	-34	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
332	-35	-102	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
332	-35	-102	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
332	-35	-102	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
332	-35	-102	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
332	-101	-35	Max	0.00	13.94	10	13.94	2	0.00	4	-23.88	2	0.00	14	0.00	2
332	-101	-35	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
332	-101	-35	Min.	0.00	-13.94	14	-13.94	6	0.00	6	-23.88	2	0.00	10	0.00	2
332	-101	-35	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
333	-37	-103	Max	0.00	13.94	14	13.94	6	20.90	2	108.02	2	-98.92	2	0.00	2
333	-37	-103	Max	150.00	13.94	14	13.94	6	0.00	6	23.88	2	0.00	2	0.00	2
333	-37	-103	Min.	0.00	-13.94	10	-13.94	2	-20.90	6	108.02	2	-98.92	2	0.00	2
333	-37	-103	Min.	150.00	-13.94	10	-13.94	2	0.00	2	23.88	2	0.00	2	0.00	2
333	-104	-37	Max	0.00	13.94	10	13.94	2	0.00	2	-23.88	2	0.00	6	0.00	2
333	-104	-37	Max	150.00	13.94	10	13.94	2	20.90	2	-108.02	2	-98.92	2	0.00	2
333	-104	-37	Min.	0.00	-13.94	14	-13.94	6	0.00	8	-23.88	2	0.00	14	0.00	2
333	-104	-37	Min.	150.00	-13.94	14	-13.94	6	-20.90	6	-108.02	2	-98.92	2	0.00	2
334	-38	-99	Max	0.00	9.30	14	9.30	6	13.95	2	76.05	2	-65.99	2	0.00	2
334	-38	-99	Max	150.00	9.30	14	9.30	6	0.00	2	11.94	2	0.00	2	0.00	2
334	-38	-99	Min.	0.00	-9.30	10	-9.30	2	-13.95	6	76.05	2	-65.99	2	0.00	2
334	-38	-99	Min.	150.00	-9.30	10	-9.30	2	0.00	6	11.94	2	0.00	2	0.00	2
334	-100	-38	Max	0.00	9.30	10	9.30	2	0.00	6	-11.94	2	0.00	2	0.00	2
334	-100	-38	Max	150.00	9.30	10	9.30	2	13.95	2	-76.05	2	-65.99	2	0.00	2
334	-100	-38	Min.	0.00	-9.30	14	-9.30	6	0.00	4	-11.94	2	0.00	8	0.00	2
334	-100	-38	Min.	150.00	-9.30	14	-9.30	6	-13.95	6	-76.05	2	-65.99	2	0.00	2

Tipo di combinazione di carico: SLU

Asta	N1	N2		X	N	CC	Ty	CC	Mz	CC	Tz	CC	My	CC	Mx	CC
				<cm>	<daN>		<daN>		<daNm>		<daN>		<daNm>		<daNm>	
1	1	-5	Max	0.00	-1508.80	21	-76.42	21	210.50	29	0.00	21	0.00	21	0.00	21
1	1	-5	Max	330.00	-1262.80	21	-76.42	21	-168.90	21	0.00	21	0.00	21	0.00	21
1	1	-5	Min.	0.00	-4350.84	29	-192.50	29	83.29	21	0.00	29	-0.00	29	0.00	29
1	1	-5	Min.	330.00	-4104.84	29	-192.50	29	-424.76	29	0.00	29	-0.00	29	0.00	29
2	2	-10	Max	0.00	-1871.07	21	404.76	29	-134.68	21	0.00	29	0.00	21	0.00	21
2	2	-10	Max	330.00	-1625.07	21	404.76	29	894.58	29	0.00	29	0.00	21	0.00	21
2	2	-10	Min.	0.00	-5782.99	29	123.41	21	-441.12	29	0.00	21	-0.00	29	0.00	29
2	2	-10	Min.	330.00	-5536.98	29	123.41	21	272.58	21	0.00	21	-0.00	29	0.00	29
3	3	203	Max	0.00	-2035.42	21	-76.73	21	282.49	29	0.00	21	0.00	21	0.00	29
3	3	203	Max	330.00	-1789.42	21	-76.73	21	-169.54	21	0.00	21	0.00	21	0.00	29
3	3	203	Min.	0.00	-6298.20	29	-258.82	29	83.67	21	-0.00	29	-0.00	29	0.00	21
3	3	203	Min.	330.00	-6052.19	29	-258.82	29	-571.61	29	-0.00	29	-0.00	29	0.00	21
4	4	204	Max	0.00	-1814.64	21	0.00	29	0.00	21	0.00	21	0.00	21	0.00	29
4	4	204	Max	330.00	-1568.63	21	0.00	29	0.00	29	0.00	21	0.00	21	0.00	29
4	4	204	Min.	0.00	-5226.35	29	0.00	21	-0.00	29	-0.00	29	0.00	21	0.00	21
4	4	204	Min.	330.00	-4980.34	29	0.00	21	0.00	21	-0.00	29	0.00	21	0.00	21
5	5	205	Max	0.00	-2035.43	21	-76.73	21	282.49	29	0.00	29	0.00	29	0.00	21
5	5	205	Max	330.00	-1789.42	21	-76.73	21	-169.54	21	0.00	29	0.00	29	0.00	21
5	5	205	Min.	0.00	-6298.20	29	-258.82	29	83.67	21	0.00	21	0.00	21	0.00	29
5	5	205	Min.	330.00	-6052.19	29	-258.82	29	-571.61	29	0.00	21	0.00	21	0.00	29
6	6	-31	Max	0.00	-1871.07	21	404.76	29	-134.68	21	0.00	21	0.00	29	0.00	29
6	6	-31	Max	330.00	-1625.07	21	404.76	29	894.59	29	0.00	21	0.00	29	0.00	29
6	6	-31	Min.	0.00	-5782.99	29	123.41	21	-441.13	29	-0.00	29	0.00	21	0.00	21
6	6	-31	Min.	330.00	-5536.98	29	123.41	21	272.58	21	-0.00	29	0.00	21	0.00	21
7	7	-36	Max	0.00	-1508.81	21	-76.43	21	210.51	29	0.00	29	0.00	29	0.00	29
7	7	-36	Max	330.00	-1262.80	21	-76.43	21	-168.91	21	0.00	29	0.00	29	0.00	29
7	7	-36	Min.	0.00	-4350.85	29	-192.51	29	83.30	21	0.00	21	0.00	21	0.00	21
7	7	-36	Min.	330.00	-4104.84	29	-192.51	29	-424.77	29	0.00	21	0.00	21	0.00	21
201	-4	-3	Max	0.00	0.00	17	0.00	17	0.00	17	701.07	29	-313.97	21	0.00	21
201	-4	-3	Max	133.53	0.00	17	0.00	17	0.00	17	617.35	29	0.00	29	0.00	21
201	-4	-3	Min.	0.00	0.00	17	0.00	17	0.00	17	276.99	21	-880.26	29	0.00	29
201	-4	-3	Min.	133.53	0.00	17	0.00	17	0.00	17	193.26	21	0.00	21	0.00	29
201	-5	-4	Max	0.00	0.00	17	0.00	17	0.00	17	1870.98	29	-769.95	21	0.00	21
201	-5	-4	Max	79.47	0.00	17	0.00	17	0.00	17	1821.15	29	-313.97	21	0.00	21
201	-5	-4	Min.	0.00	0.00	17	0.00	17	0.00	17	598.72	21	-2347.26	29	0.00	29
201	-5	-4	Min.	79.47	0.00	17	0.00	17	0.00	17	548.89	21	-880.26	29	0.00	29
201	-6	-5	Max	0.00	192.50	29	0.00	29	0.00	21	-630.18	21	-251.16	21	0.00	29
201	-6	-5	Max	54.07	192.50	29	0.00	29	0.00	29	-664.08	21	-601.05	21	0.00	29
201	-6	-5	Min.	0.00	76.42	21	0.00	21	0.00	29	-2199.96	29	-723.88	29	0.00	21
201	-6	-5	Min.	54.07	76.42	21	0.00	21	0.00	21	-2233.86	29	-1922.50	29	0.00	21
201	-7	-6	Max	0.00	192.50	29	0.00	29	0.00	21	-274.55	21	662.22	29	0.00	29
201	-7	-6	Max	133.53	192.50	29	0.00	29	0.00	21	-358.28	21	-251.16	21	0.00	29
201	-7	-6	Min.	0.00	76.42	21	0.00	21	0.00	29	-996.16	29	171.36	21	0.00	21
201	-7	-6	Min.	133.53	76.42	21	0.00	21	0.00	29	-1079.88	29	-723.88	29	0.00	21
201	-8	-7	Max	0.00	192.50	29	0.00	29	0.00	21	207.64	29	440.85	29	0.00	29
201	-8	-7	Max	129.31								171.41	21			
201	-8	-7	Max	133.53	192.50	29	0.00	29	0.00	21	123.92	29	662.22	29	0.00	29
201	-8	-7	Min.	0.00	76.42	21	0.00	21	0.00	29	81.08	21	118.99	21	0.00	21
201	-8	-7	Min.	129.31												



202	-11	-10	Min.	0.00	-212.25	29	0.00	21	0.00	29	-2921.74	29	-835.29	29	0.00	21
202	-11	-10	Min.	88.20	-212.25	29	0.00	21	0.00	29	-2977.04	29	-3436.65	29	0.00	21
202	-12	-11	Max	0.00	-46.99	21	0.00	29	0.00	21	-477.10	21	1514.62	29	0.00	29
202	-12	-11	Max	133.53	-46.99	21	0.00	29	0.00	21	-560.83	21	-249.66	21	0.00	29
202	-12	-11	Min.	0.00	-212.25	29	0.00	21	0.00	29	-1717.94	29	443.33	21	0.00	21
202	-12	-11	Min.	133.53	-212.25	29	0.00	21	0.00	29	-1801.66	29	-835.29	29	0.00	21
202	-13	-12	Max	0.00	-46.99	21	0.00	29	0.00	21	-121.47	21	2257.07	29	0.00	29
202	-13	-12	Max	133.53	-46.99	21	0.00	29	0.00	21	-205.20	21	1514.63	29	0.00	29
202	-13	-12	Min.	0.00	-212.25	29	0.00	21	0.00	29	-514.13	29	661.44	21	0.00	21
202	-13	-12	Min.	133.53	-212.25	29	0.00	21	0.00	29	-597.86	29	443.33	21	0.00	21
202	-14	-13	Max	0.00	-46.99	21	0.00	29	0.00	21	689.67	29	1392.03	29	0.00	21
202	-14	-13	Max	133.53	-46.99	21	0.00	29	0.00	21	605.94	29	2257.07	29	0.00	21
202	-14	-13	Min.	0.00	-212.25	29	0.00	21	0.00	29	234.16	21	404.67	21	0.00	29
202	-14	-13	Min.	133.53	-212.25	29	0.00	21	0.00	29	150.43	21	661.44	21	0.00	29
202	-15	-14	Max	0.00	-46.99	21	0.00	29	0.00	21	1893.47	29	-326.99	21	0.00	21
202	-15	-14	Max	133.53	-46.99	21	0.00	29	0.00	21	1809.74	29	1392.04	29	0.00	21
202	-15	-14	Min.	0.00	-212.25	29	0.00	21	0.00	29	589.78	21	-1080.47	29	0.00	29
202	-15	-14	Min.	133.53	-212.25	29	0.00	21	0.00	29	506.06	21	404.67	21	0.00	29
202	203	-15	Max	0.00	-46.99	21	0.00	29	0.00	21	3068.51	29	-1106.50	21	0.00	21
202	203	-15	Max	87.67	-46.99	21	0.00	29	0.00	21	3013.55	29	-327.00	21	0.00	21
202	203	-15	Min.	0.00	-212.25	29	0.00	21	0.00	29	916.65	21	-3746.45	29	-0.00	29
202	203	-15	Min.	87.67	-212.25	29	0.00	21	0.00	29	861.69	21	-1080.48	29	-0.00	29
203	-16	203	Max	0.00	46.56	29	0.00	21	0.00	21	-844.00	21	-543.22	21	0.00	29
203	-16	203	Max	45.87	46.56	29	0.00	21	0.00	21	-872.76	21	-936.93	21	0.00	29
203	-16	203	Min.	0.00	29.74	21	-0.00	29	0.00	29	-2954.92	29	-1812.82	29	0.00	21
203	-16	203	Min.	45.87	29.74	21	-0.00	29	0.00	29	-2983.68	29	-3174.75	29	0.00	21
203	-17	-16	Max	0.00	46.56	29	0.00	21	0.00	21	-488.38	21	581.35	29	0.00	29
203	-17	-16	Max	133.53	46.56	29	0.00	21	0.00	21	-572.10	21	-543.24	21	0.00	29
203	-17	-16	Min.	0.00	29.74	21	-0.00	29	0.00	29	-1751.12	29	164.81	21	0.00	21
203	-17	-16	Min.	133.53	29.74	21	-0.00	29	0.00	29	-1834.85	29	-1812.88	29	0.00	21
203	-18	-17	Max	0.00	46.56	29	0.00	21	0.00	21	-132.75	21	1368.08	29	0.00	29
203	-18	-17	Max	133.53	46.56	29	0.00	21	0.00	21	-216.47	21	581.32	29	0.00	29
203	-18	-17	Min.	0.00	29.74	21	-0.00	29	0.00	21	-547.32	29	397.96	21	0.00	21
203	-18	-17	Min.	133.53	29.74	21	-0.00	29	0.00	29	-631.05	29	164.80	21	0.00	21
203	-19	-18	Max	0.00	46.56	29	0.00	21	0.00	29	656.48	29	547.32	29	0.00	21
203	-19	-18	Max	133.53	46.56	29	0.00	21	0.00	29	572.76	29	1368.04	29	0.00	21
203	-19	-18	Min.	0.00	29.74	21	-0.00	29	0.00	21	222.88	21	156.23	21	0.00	29
203	-19	-18	Min.	133.53	29.74	21	-0.00	29	0.00	21	139.16	21	397.95	21	0.00	29
203	-20	-19	Max	0.00	46.56	29	0.00	21	0.00	29	1860.28	29	-560.36	21	0.00	21
203	-20	-19	Max	133.53	46.56	29	0.00	21	0.00	29	1776.56	29	547.38	29	0.00	21
203	-20	-19	Min.	0.00	29.74	21	-0.00	29	0.00	21	578.51	21	-1880.82	29	0.00	29
203	-20	-19	Min.	133.53	29.74	21	-0.00	29	0.00	21	494.79	21	156.24	21	0.00	29
203	204	-20	Max	0.00	46.56	29	0.00	21	0.00	29	2490.17	29	-715.97	21	0.00	21
203	204	-20	Max	20.00	46.56	29	0.00	21	0.00	29	2477.63	29	-560.36	21	0.00	29
203	204	-20	Min.	0.00	29.74	21	-0.00	29	0.00	21	784.32	21	-2377.60	29	-0.00	29
203	204	-20	Min.	20.00	29.74	21	-0.00	29	0.00	21	771.78	21	-1880.82	29	-0.00	29
204	204	-21	Max	0.00	46.56	29	0.00	21	0.00	21	2490.17	29	-715.97	21	0.00	29
204	204	-21	Max	20.00	46.56	29	0.00	21	0.00	21	2477.63	29	-560.36	21	0.00	29
204	204	-21	Min.	0.00	29.74	21	0.00	21	0.00	29	784.32	21	-2377.60	29	0.00	21
204	204	-21	Min.	20.00	29.74	21	0.00	21	0.00	29	771.77	21	-1880.82	29	0.00	21
204	-21	-22	Max	0.00	46.56	29	0.00	21	0.00	21	1860.28	29	-560.36	21	0.00	29
204	-21	-22	Max	133.53	46.56	29	0.00	21	0.00	21	1776.56	29	547.38	29	0.00	29
204	-21	-22	Min.	0.00	29.74	21	0.00	21	0.00	21	578.51	21	-1880.82	29	0.00	21
204	-21	-22	Min.	133.53	29.74	21	0.00	21	0.00	29	494.79	21	156.24	21	0.00	21
204	-22	-23	Max	0.00	46.56	29	0.00	21	0.00	21	656.48	29	547.32	29	0.00	29
204	-22	-23	Max	133.53	46.56	29	0.00	21	0.00	21	572.76	29	1368.04	29	0.00	29
204	-22	-23	Min.	0.00	29.74	21	0.00	21	0.00	29	222.88	21	156.23	21	0.00	21
204	-22	-23	Min.	133.53	29.74	21	0.00	21	0.00	29	139.16	21	397.95	21	0.00	21
204	-23	-24	Max	0.00	46.56	29	0.00	21	0.00	21	-132.75	21	1368.08	29	0.00	21
204	-23	-24	Max	133.53	46.56	29	0.00	21	0.00	21	-216.47	21	581.32	29	0.00	21
204	-23	-24	Min.	0.00	29.74	21	0.00	21	0.00	29	-547.32	29	397.96	21	0.00	29
204	-23	-24	Min.	133.53	29.74	21	0.00	21	0.00	29	-631.05	29	164.80	21	0.00	29
204	-24	-25	Max	0.00	46.56	29	0.00	21	0.00	21	-488.38	21	581.34	29	0.00	21
204	-24	-25	Max	133.53	46.56	29	0.00	21	0.00	29	-572.10	21	-543.24	21	0.00	21
204	-24	-25	Min.	0.00	29.74	21	0.00	21	0.00	21	-1751.12	29	164.81	21	0.00	29
204	-24	-25	Min.	133.53	29.74	21	0.00	21	0.00	21	-1834.85	29	-1812.89	29	0.00	29
204	-25	205	Max	0.00	46.56	29	0.00	21	0.00	29	-844.00	21	-543.22	21	0.00	21
204	-25	205	Max	45.87	46.56	29	0.00	21	0.00	29	-872.76	21	-936.93	21	0.00	21
204	-25	205	Min.	0.00	29.74	21	0.00	21	0.00	21	-2954.92	29	-1812.83	29	-0.00	29
204	-25	205	Min.	45.87	29.74	21	0.00	21	0.00	21	-2983.68	29	-3174.75	29	-0.00	29
205	205	-26	Max	0.00	-46.99	21	0.00	21	0.00	29	3068.51	29	-1106.51	21	0.00	29
205	205	-26	Max	87.67	-46.99	21	0.00	21	0.00	29	3013.54	29	-327.00	21	0.00	29
205	205	-26	Min.	0.00	-212.25	29	0.00	21	0.00	29	916.65	21	-3746.46	29	0.00	21
205	205	-26	Min.	87.67	-212.25	29	0.00	21	0.00	29	861.69	21	-1080.50	29	0.00	21
205	-26	-27	Max	0.00	-46.99	21	0.00	21	0.00	29	1893.47	29	-326.99	21	0.00	29
205	-26	-27	Max	133.53	-46.99	21	0.00	21	0.00	29	1809.74	29	1392.11	29	0.00	29
205	-26	-27	Min.	0.00	-212.25	29	0.00	21	0.00	29	589.78	21	-1080.40	29	0.00	21
205	-26	-27	Min.	133.53	-212.25	29	0.00	21	0.00	29	506.06	21	404.69	21	0.00	21
205	-27	-28	Max	0.00	-46.99	21	0.00	21	0.00	29	689.67	29	1392.05	29	0.00	29
205	-27	-28	Max	133.53	-46.99	21	0.00	21	0.00	29	605.94	29	2257.09	29	0.00	29
205	-27	-28	Min.	0.00	-212.25	29	0.00	21	0.00	29	234.16	21	404.67	21	0.00	21
205	-27	-28	Min.	133.53	-212.25	29	0.00	21	0.00	29	150.43	21	661.44	21	0.00	21
205	-28	-29	Max	0.00	-46.99	21	0.00	21	0.00	29	-121.47	21	2257.06	29	0.00	21
205	-28	-29	Max	133.53	-4											



206	-32	-33	Min.	133.53	76.43	21	0.00	29	0.00	21	352.98	21	118.97	21	0.00	21
206	-33	-34	Max	0.00	192.51	29	0.00	21	0.00	29	207.64	29	440.86	29	0.00	21
206	-33	-34	Max	129.31									171.41	21		
206	-33	-34	Max	133.53	192.51	29	0.00	21	0.00	29	123.91	29	662.23	29	0.00	21
206	-33	-34	Min.	0.00	76.43	21	0.00	29	0.00	21	81.07	21	119.00	21	0.00	29
206	-33	-34	Min.	129.31									171.41	21		
206	-33	-34	Min.	133.53	76.43	21	0.00	29	0.00	21	-2.65	21	171.36	21	0.00	29
206	-34	-35	Max	0.00	192.51	29	0.00	21	0.00	29	-274.55	21	662.22	29	0.00	21
206	-34	-35	Max	133.53	192.51	29	0.00	21	0.00	29	-358.28	21	-251.16	21	0.00	21
206	-34	-35	Min.	0.00	76.43	21	0.00	29	0.00	21	-996.16	29	171.36	21	0.00	29
206	-34	-35	Min.	133.53	76.43	21	0.00	29	0.00	21	-1079.89	29	-723.89	29	0.00	29
206	-35	-36	Max	0.00	192.51	29	0.00	21	0.00	29	-630.18	21	-251.15	21	0.00	21
206	-35	-36	Max	54.07	192.51	29	0.00	21	0.00	21	-664.08	21	-601.04	21	0.00	21
206	-35	-36	Min.	0.00	76.43	21	0.00	29	0.00	21	-2199.96	29	-723.85	29	-0.00	29
206	-35	-36	Min.	54.07	76.43	21	0.00	29	0.00	29	-2233.86	29	-1922.46	29	-0.00	29
206	-36	-37	Max	0.00	0.00	17	0.00	17	0.00	17	1870.97	29	-769.97	21	0.00	29
206	-36	-37	Max	79.47	0.00	17	0.00	17	0.00	17	1821.15	29	-313.98	21	0.00	29
206	-36	-37	Min.	0.00	0.00	17	0.00	17	0.00	17	598.72	21	-2347.31	29	0.00	21
206	-36	-37	Min.	79.47	0.00	17	0.00	17	0.00	17	548.89	21	-880.30	29	0.00	21
206	-37	-38	Max	0.00	0.00	17	0.00	17	0.00	17	701.07	29	-313.96	21	0.00	29
206	-37	-38	Max	133.53	0.00	17	0.00	17	0.00	17	617.35	29	0.02	29	0.00	29
206	-37	-38	Min.	0.00	0.00	17	0.00	17	0.00	17	276.99	21	-880.24	29	0.00	21
206	-37	-38	Min.	133.53	0.00	17	0.00	17	0.00	17	193.26	21	0.01	21	0.00	21
301	-3	-60	Max	0.00	0.00	17	0.00	17	0.00	17	308.68	29	-83.49	21	0.00	17
301	-3	-60	Max	150.00	0.00	17	0.00	17	0.00	17	93.87	29	0.00	21	0.00	17
301	-3	-60	Min.	0.00	0.00	17	0.00	17	0.00	17	96.63	21	-301.91	29	0.00	17
301	-3	-60	Min.	150.00	0.00	17	0.00	17	0.00	17	14.68	21	0.00	28	0.00	17
301	-59	-3	Max	0.00	0.00	17	0.00	17	0.00	17	-14.68	21	0.00	21	0.00	17
301	-59	-3	Max	150.00	0.00	17	0.00	17	0.00	17	-96.63	21	-83.49	21	0.00	17
301	-59	-3	Min.	0.00	0.00	17	0.00	17	0.00	17	-93.87	29	0.00	29	0.00	17
301	-59	-3	Min.	150.00	0.00	17	0.00	17	0.00	17	-308.68	29	-301.91	29	0.00	17
302	-4	-47	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
302	-4	-47	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
302	-4	-47	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
302	-4	-47	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	21	0.00	17
302	-46	-4	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	29	0.00	17
302	-46	-4	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
302	-46	-4	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	21	0.00	17
302	-46	-4	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
303	-6	-48	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
303	-6	-48	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
303	-6	-48	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
303	-6	-48	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	21	0.00	17
303	-49	-6	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	28	0.00	17
303	-49	-6	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
303	-49	-6	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	17	0.00	17
303	-49	-6	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
304	-7	-96	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
304	-7	-96	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
304	-7	-96	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
304	-7	-96	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
304	-95	-7	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	22	0.00	17
304	-95	-7	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
304	-95	-7	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	28	0.00	17
304	-95	-7	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
305	-8	-66	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
305	-8	-66	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
305	-8	-66	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
305	-8	-66	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	29	0.00	17
305	-67	-8	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	29	0.00	17
305	-67	-8	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
305	-67	-8	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	21	0.00	17
305	-67	-8	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
306	-9	-69	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
306	-9	-69	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
306	-9	-69	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
306	-9	-69	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	29	0.00	17
306	-68	-9	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	21	0.00	17
306	-68	-9	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
306	-68	-9	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	29	0.00	17
306	-68	-9	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
307	-11	-70	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
307	-11	-70	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
307	-11	-70	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
307	-11	-70	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	29	0.00	17
307	-71	-11	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	21	0.00	17
307	-71	-11	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
307	-71	-11	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	28	0.00	17
307	-71	-11	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
308	-12	-72	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
308	-12	-72	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
308	-12	-72	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
308	-12	-72	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	29	0.00	17
308	-73	-12	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	28	0.00	17
308	-73	-12	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
308	-73	-12	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	22	0.00	



324	-27	-79	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
324	-78	-27	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	21	0.00	17
324	-78	-27	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
324	-78	-27	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	17	0.00	17
324	-78	-27	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
325	-28	-81	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
325	-28	-81	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
325	-28	-81	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
325	-28	-81	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
325	-80	-28	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	28	0.00	17
325	-80	-28	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
325	-80	-28	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	22	0.00	17
325	-80	-28	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
326	-29	-83	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
326	-29	-83	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
326	-29	-83	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
326	-29	-83	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	21	0.00	17
326	-82	-29	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	28	0.00	17
326	-82	-29	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
326	-82	-29	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	22	0.00	17
326	-82	-29	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
327	-30	-85	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
327	-30	-85	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
327	-30	-85	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
327	-30	-85	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
327	-84	-30	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	17	0.00	17
327	-84	-30	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
327	-84	-30	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	28	0.00	17
327	-84	-30	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
329	-32	-86	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
329	-32	-86	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
329	-32	-86	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
329	-32	-86	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
329	-87	-32	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	22	0.00	17
329	-87	-32	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
329	-87	-32	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	28	0.00	17
329	-87	-32	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
330	-33	-89	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
330	-33	-89	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	22	0.00	17
330	-33	-89	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
330	-33	-89	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
330	-88	-33	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	21	0.00	17
330	-88	-33	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
330	-88	-33	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	29	0.00	17
330	-88	-33	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
331	-34	-61	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
331	-34	-61	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	22	0.00	17
331	-34	-61	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
331	-34	-61	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
331	-62	-34	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	21	0.00	17
331	-62	-34	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
331	-62	-34	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	17	0.00	17
331	-62	-34	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
332	-35	-102	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
332	-35	-102	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	17	0.00	17
332	-35	-102	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
332	-35	-102	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
332	-101	-35	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	28	0.00	17
332	-101	-35	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
332	-101	-35	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	17	0.00	17
332	-101	-35	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
333	-37	-103	Max	0.00	0.00	17	0.00	17	0.00	17	560.04	29	-123.99	21	0.00	17
333	-37	-103	Max	150.00	0.00	17	0.00	17	0.00	17	187.74	29	0.00	22	0.00	17
333	-37	-103	Min.	0.00	0.00	17	0.00	17	0.00	17	135.95	21	-560.83	29	0.00	17
333	-37	-103	Min.	150.00	0.00	17	0.00	17	0.00	17	29.37	21	0.00	28	0.00	17
333	-104	-37	Max	0.00	0.00	17	0.00	17	0.00	17	-29.37	21	0.00	22	0.00	17
333	-104	-37	Max	150.00	0.00	17	0.00	17	0.00	17	-135.95	21	-123.99	21	0.00	17
333	-104	-37	Min.	0.00	0.00	17	0.00	17	0.00	17	-187.74	29	0.00	28	0.00	17
333	-104	-37	Min.	150.00	0.00	17	0.00	17	0.00	17	-560.04	29	-560.83	29	0.00	17
334	-38	-99	Max	0.00	0.00	17	0.00	17	0.00	17	308.67	29	-83.49	21	0.00	17
334	-38	-99	Max	150.00	0.00	17	0.00	17	0.00	17	93.87	29	0.00	21	0.00	17
334	-38	-99	Min.	0.00	0.00	17	0.00	17	0.00	17	96.63	21	-301.91	29	0.00	17
334	-38	-99	Min.	150.00	0.00	17	0.00	17	0.00	17	14.68	21	0.00	29	0.00	17
334	-100	-38	Max	0.00	0.00	17	0.00	17	0.00	17	-14.68	21	0.00	29	0.00	17
334	-100	-38	Max	150.00	0.00	17	0.00	17	0.00	17	-96.63	21	-83.49	21	0.00	17
334	-100	-38	Min.	0.00	0.00	17	0.00	17	0.00	17	-93.87	29	0.00	21	0.00	17
334	-100	-38	Min.	150.00	0.00	17	0.00	17	0.00	17	-308.68	29	-301.91	29	0.00	17

Tipo di combinazione di carico: SLE R

Asta	N1	N2	X	N	CC Ty	CC Mz	CC Tz	CC My	CC Mx	CC						
			<cm>	<daN>	<daN>	<daNm>	<daN>	<daNm>	<daNm>							
1	1	-5	Max	-1106.57	23	-56.58	23	146.46	31	0.00	23	0.00	23	0.00	23	
1	1	-5	Max	330.00	-917.33	23	-56.58	23	-125.06	23	0.00	23	0.00	23	0.00	23
1	1	-5	Min.	0.00	-3001.26	31	-133.97	31	61.65	23	0.00	31	-0.00	31	0.00	31
1	1	-5	Min.	330.00	-2812.02	31	-133.97	31	-295.63	31	0.00	31	-0.00	31	0.00	31
2	2	-10	Max	0.00	-1364.89	23	277.14	31	-97.77	23	0.00	31	0.00	23	0.00	23
2	2	-10	Max	330.00	-1175.65	23	277.14	31	612.51	31	0.00	31	0.00	23	0.00	23
2	2	-10	Min.	0.0												



5	5	205	Min.	330.00	-4137.25	31	-176.95	31	-390.82	31	0.00	23	0.00	23	0.00	31
6	6	-31	Max	0.00	-1364.89	23	277.15	31	-97.77	23	0.00	23	0.00	31	0.00	31
6	6	-31	Max	330.00	-1175.65	23	277.15	31	612.52	31	0.00	23	0.00	31	0.00	31
6	6	-31	Min.	0.00	-3972.83	31	89.58	23	-302.07	31	-0.00	31	0.00	23	0.00	23
6	6	-31	Min.	330.00	-3783.59	31	89.58	23	197.85	23	-0.00	31	0.00	23	0.00	23
7	7	-36	Max	0.00	-1106.57	23	-56.58	23	146.46	31	0.00	31	0.00	31	0.00	31
7	7	-36	Max	330.00	-917.33	23	-56.58	23	-125.06	23	0.00	31	0.00	31	0.00	31
7	7	-36	Min.	0.00	-3001.26	31	-133.97	31	61.65	23	0.00	23	0.00	23	0.00	23
7	7	-36	Min.	330.00	-2812.02	31	-133.97	31	-295.64	31	0.00	23	0.00	23	0.00	23
201	-4	-3	Max	0.00	0.00	18	0.00	18	0.00	18	487.73	31	-230.75	23	0.00	23
201	-4	-3	Max	133.53	0.00	18	0.00	18	0.00	18	423.32	31	0.00	31	0.00	23
201	-4	-3	Min.	0.00	0.00	18	0.00	18	0.00	18	205.00	23	-608.27	31	0.00	31
201	-4	-3	Min.	133.53	0.00	18	0.00	18	0.00	18	140.60	23	0.00	23	0.00	31
201	-5	-4	Max	0.00	0.00	18	0.00	18	0.00	18	1284.53	31	-562.27	23	0.00	23
201	-5	-4	Max	79.47	0.00	18	0.00	18	0.00	18	1246.20	31	-230.74	23	0.00	23
201	-5	-4	Min.	0.00	0.00	18	0.00	18	0.00	18	436.35	23	-1613.81	31	0.00	31
201	-5	-4	Min.	79.47	0.00	18	0.00	18	0.00	18	398.03	23	-608.27	31	0.00	31
201	-6	-5	Max	0.00	133.97	31	0.00	31	0.00	23	-454.90	23	-184.21	23	0.00	31
201	-6	-5	Max	54.07	133.97	31	0.00	31	0.00	31	-480.98	23	-437.21	23	0.00	31
201	-6	-5	Min.	0.00	56.58	23	0.00	23	0.00	31	-1501.42	31	-499.36	31	0.00	23
201	-6	-5	Min.	54.07	56.58	23	0.00	23	0.00	23	-1527.50	31	-1318.18	31	0.00	23
201	-7	-6	Max	0.00	133.97	31	0.00	31	0.00	23	-197.47	23	449.72	31	0.00	31
201	-7	-6	Max	133.53	133.97	31	0.00	31	0.00	23	-261.87	23	-184.21	23	0.00	31
201	-7	-6	Min.	0.00	56.58	23	0.00	23	0.00	31	-678.54	31	122.48	23	0.00	23
201	-7	-6	Min.	133.53	56.58	23	0.00	23	0.00	31	-742.94	31	-499.36	31	0.00	23
201	-8	-7	Max	0.00	133.97	31	0.00	31	0.00	23	144.34	31	299.98	31	0.00	31
201	-8	-7	Max	124.32	124.32								122.68	23		
201	-8	-7	Max	133.53	133.97	31	0.00	31	0.00	23	79.93	31	449.72	31	0.00	31
201	-8	-7	Min.	0.00	56.58	23	0.00	23	0.00	31	59.96	23	85.41	23	0.00	23
201	-8	-7	Min.	124.32	124.32								122.68	23		
201	-8	-7	Min.	133.53	56.58	23	0.00	23	0.00	31	-4.44	23	122.48	23	0.00	23
201	-9	-8	Max	0.00	133.97	31	0.00	31	0.00	23	967.21	31	-295.41	23	0.00	23
201	-9	-8	Max	133.53	133.97	31	0.00	31	0.00	23	902.81	31	299.99	31	0.00	23
201	-9	-8	Min.	0.00	56.58	23	0.00	23	0.00	31	317.39	23	-948.57	31	0.00	31
201	-9	-8	Min.	133.53	56.58	23	0.00	23	0.00	31	252.99	23	85.41	23	0.00	31
201	-10	-9	Max	0.00	133.97	31	0.00	31	0.00	23	1747.55	31	-531.76	23	0.00	23
201	-10	-9	Max	45.33	133.97	31	0.00	31	0.00	23	1725.69	31	-295.41	23	0.00	23
201	-10	-9	Min.	0.00	56.58	23	0.00	23	0.00	31	532.28	23	-1735.85	31	0.00	31
201	-10	-9	Min.	45.33	56.58	23	0.00	23	0.00	31	510.42	23	-948.58	31	0.00	31
202	-11	-10	Max	0.00	-33.00	23	0.00	31	0.00	23	-600.83	23	-180.91	23	0.00	31
202	-11	-10	Max	88.20	-33.00	23	0.00	31	0.00	23	-643.37	23	-729.60	23	0.00	31
202	-11	-10	Min.	0.00	-143.18	31	0.00	23	0.00	31	-1993.50	31	-571.33	31	0.00	23
202	-11	-10	Min.	88.20	-143.18	31	0.00	23	0.00	31	-2036.04	31	-2348.35	31	0.00	23
202	-12	-11	Max	0.00	-33.00	23	0.00	31	0.00	23	-343.40	23	1034.84	31	0.00	31
202	-12	-11	Max	133.53	-33.00	23	0.00	31	0.00	23	-407.81	23	-180.91	23	0.00	31
202	-12	-11	Min.	0.00	-143.18	31	0.00	23	0.00	31	-1170.62	31	320.65	23	0.00	23
202	-12	-11	Min.	133.53	-143.18	31	0.00	23	0.00	31	-1235.03	31	-571.33	31	0.00	23
202	-13	-12	Max	0.00	-33.00	23	0.00	31	0.00	23	-85.97	23	1542.20	31	0.00	31
202	-13	-12	Max	133.53	-33.00	23	0.00	31	0.00	23	-150.38	23	1034.85	31	0.00	31
202	-13	-12	Min.	0.00	-143.18	31	0.00	23	0.00	31	-347.75	31	478.45	23	0.00	23
202	-13	-12	Min.	133.53	-143.18	31	0.00	23	0.00	31	-412.15	31	320.65	23	0.00	23
202	-14	-13	Max	0.00	-33.00	23	0.00	31	0.00	23	475.13	31	950.75	31	0.00	23
202	-14	-13	Max	133.53	-33.00	23	0.00	31	0.00	23	410.73	31	1542.21	31	0.00	23
202	-14	-13	Min.	0.00	-143.18	31	0.00	23	0.00	31	171.46	23	292.50	23	0.00	31
202	-14	-13	Min.	133.53	-143.18	31	0.00	23	0.00	31	107.05	23	478.45	23	0.00	31
202	-15	-14	Max	0.00	-33.00	23	0.00	31	0.00	23	1298.01	31	-237.20	23	0.00	23
202	-15	-14	Max	133.53	-33.00	23	0.00	31	0.00	23	1233.60	31	950.75	31	0.00	23
202	-15	-14	Min.	0.00	-143.18	31	0.00	23	0.00	31	428.88	23	-739.52	31	0.00	31
202	-15	-14	Min.	133.53	-143.18	31	0.00	23	0.00	31	364.48	23	292.50	23	0.00	31
202	203	-15	Max	0.00	-33.00	23	0.00	31	0.00	23	2098.76	31	-800.95	23	0.00	23
202	203	-15	Max	87.67	-33.00	23	0.00	31	0.00	23	2056.48	31	-237.20	23	0.00	23
202	203	-15	Min.	0.00	-143.18	31	0.00	23	0.00	31	664.19	23	-2560.91	31	0.00	31
202	203	-15	Min.	87.67	-143.18	31	0.00	23	0.00	31	621.91	23	-739.53	31	0.00	31
203	-16	203	Max	0.00	33.77	31	0.00	23	0.00	23	-609.09	23	-393.71	23	0.00	31
203	-16	203	Max	45.87	33.77	31	0.00	23	0.00	23	-631.21	23	-678.15	23	0.00	31
203	-16	203	Min.	0.00	22.56	23	0.00	31	0.00	31	-2016.36	31	-1240.12	31	0.00	23
203	-16	203	Min.	45.87	22.56	23	0.00	31	0.00	31	-2038.49	31	-2170.03	31	0.00	23
203	-17	-16	Max	0.00	33.77	31	0.00	23	0.00	23	-351.66	23	396.55	31	0.00	31
203	-17	-16	Max	133.53	33.77	31	0.00	23	0.00	23	-416.06	23	-393.73	23	0.00	31
203	-17	-16	Min.	0.00	22.56	23	0.00	31	0.00	31	-1193.49	31	118.85	23	0.00	23
203	-17	-16	Min.	133.53	22.56	23	0.00	31	0.00	31	-1257.89	31	-1240.16	31	0.00	23
203	-18	-17	Max	0.00	33.77	31	0.00	23	0.00	31	-94.23	23	934.42	31	0.00	31
203	-18	-17	Max	133.53	33.77	31	0.00	23	0.00	23	-158.63	23	396.53	31	0.00	31
203	-18	-17	Min.	0.00	22.56	23	0.00	31	0.00	23	-370.61	31	287.67	23	0.00	23
203	-18	-17	Min.	133.53	22.56	23	0.00	31	0.00	31	-435.01	31	118.85	23	0.00	23
203	-19	-18	Max	0.00	33.77	31	0.00	23	0.00	31	452.27	31	373.46	31	0.00	23
203	-19	-18	Max	133.53	33.77	31	0.00	23	0.00	31	387.87	31	934.39	31	0.00	23
203	-19	-18	Min.	0.00	22.56	23	0.00	31	0.00	23	163.20	23	112.74	23	0.00	31
203	-19	-18	Min.	133.53	22.56	23	0.00	31	0.00	23	298.80	23	287.67	23	0.00	31
203	-20	-19	Max	0.00	33.77	31	0.00	23	0.00	31	1275.15	31	-405.94	23	0.00	23
203	-20	-19	Max	133.53	33.77	31	0.00	23	0.00	31	1210.74	31	373.51	31	0.00	23
203	-20	-19	Min.	0.00	22.56	23	0.00	31	0.00	23	420.63	23	-1286.24	31	0.00	31
203	-20	-19	Min.	133.53	22.56	23	0.00	31	0.00	23	356.23	23	112.75	23	0.00	31
203	204	-20	Max	0.00	33.77	31	0.00	23	0.00	31	1708.11	31	-519.15	23	0.00	23
203	204	-20	Max	20.00	33.77	31	0.00	23	0.00	31	1698.47					



204	-23	-24	Min.	0.00	22.56	23	0.00	23	0.00	31	-370.61	31	287.67	23	0.00	31
204	-23	-24	Min.	133.53	22.56	23	0.00	23	0.00	23	-435.02	31	118.84	23	0.00	31
204	-24	-25	Max	0.00	33.77	31	0.00	31	0.00	31	-351.66	23	396.54	31	0.00	23
204	-24	-25	Max	133.53	33.77	31	0.00	31	0.00	31	-416.06	23	-393.73	23	0.00	23
204	-24	-25	Min.	0.00	22.56	23	0.00	23	0.00	23	-1193.49	31	118.85	23	0.00	31
204	-24	-25	Min.	133.53	22.56	23	0.00	23	0.00	23	-1257.89	31	-1240.16	31	0.00	31
204	-25	205	Max	0.00	33.77	31	0.00	31	0.00	31	-609.09	23	-393.71	23	0.00	23
204	-25	205	Max	45.87	33.77	31	0.00	31	0.00	31	-631.21	23	-678.16	23	0.00	23
204	-25	205	Min.	0.00	22.56	23	0.00	23	0.00	23	-2016.37	31	-1240.12	31	0.00	31
204	-25	205	Min.	45.87	22.56	23	0.00	23	0.00	23	-2038.49	31	-2170.04	31	0.00	31
205	205	-26	Max	0.00	-33.00	23	0.00	23	0.00	31	2098.76	31	-800.95	23	0.00	31
205	205	-26	Max	87.67	-33.00	23	0.00	23	0.00	31	2056.48	31	-237.21	23	0.00	31
205	205	-26	Min.	0.00	-143.18	31	0.00	31	0.00	23	664.19	23	-2560.92	31	0.00	23
205	205	-26	Min.	87.67	-143.18	31	0.00	31	0.00	23	621.91	23	-739.54	31	0.00	23
205	-26	-27	Max	0.00	-33.00	23	0.00	23	0.00	31	1298.01	31	-237.19	23	0.00	31
205	-26	-27	Max	133.53	-33.00	23	0.00	23	0.00	31	1233.60	31	950.80	31	0.00	31
205	-26	-27	Min.	0.00	-143.18	31	0.00	31	0.00	23	428.88	23	-739.47	31	0.00	23
205	-26	-27	Min.	133.53	-143.18	31	0.00	31	0.00	23	364.48	23	292.52	23	0.00	23
205	-27	-28	Max	0.00	-33.00	23	0.00	23	0.00	31	475.13	31	950.76	31	0.00	31
205	-27	-28	Max	133.53	-33.00	23	0.00	23	0.00	31	410.73	31	1542.22	31	0.00	31
205	-27	-28	Min.	0.00	-143.18	31	0.00	31	0.00	23	171.46	23	292.50	23	0.00	23
205	-27	-28	Min.	133.53	-143.18	31	0.00	31	0.00	23	107.05	23	478.46	23	0.00	23
205	-28	-29	Max	0.00	-33.00	23	0.00	23	0.00	31	-85.97	23	1542.20	31	0.00	23
205	-28	-29	Max	133.53	-33.00	23	0.00	23	0.00	31	-150.38	23	1034.84	31	0.00	23
205	-28	-29	Min.	0.00	-143.18	31	0.00	31	0.00	23	-347.75	31	478.45	23	0.00	31
205	-28	-29	Min.	133.53	-143.18	31	0.00	31	0.00	23	-412.15	31	320.65	23	0.00	31
205	-29	-30	Max	0.00	-33.00	23	0.00	23	0.00	31	-343.40	23	1034.82	31	0.00	23
205	-29	-30	Max	133.53	-33.00	23	0.00	23	0.00	31	-407.81	23	-180.92	23	0.00	23
205	-29	-30	Min.	0.00	-143.18	31	0.00	31	0.00	23	-1170.63	31	320.64	23	0.00	31
205	-29	-30	Min.	133.53	-143.18	31	0.00	31	0.00	23	-1235.03	31	-571.36	31	0.00	31
205	-30	-31	Max	0.00	-33.00	23	0.00	23	0.00	31	-600.83	23	-180.91	23	0.00	23
205	-30	-31	Max	88.20	-33.00	23	0.00	23	0.00	31	-643.37	23	-729.60	23	0.00	23
205	-30	-31	Min.	0.00	-143.18	31	0.00	31	0.00	23	-1993.50	31	-571.32	31	0.00	31
205	-30	-31	Min.	88.20	-143.18	31	0.00	31	0.00	23	-2036.04	31	-2348.35	31	0.00	31
206	-31	-32	Max	0.00	133.97	31	0.00	23	0.00	31	1747.55	31	-531.75	23	0.00	31
206	-31	-32	Max	45.33	133.97	31	0.00	23	0.00	31	1725.69	31	-295.41	23	0.00	31
206	-31	-32	Min.	0.00	56.58	23	0.00	31	0.00	23	532.28	23	-1735.83	31	0.00	23
206	-31	-32	Min.	45.33	56.58	23	0.00	31	0.00	23	510.41	23	-948.56	31	0.00	23
206	-32	-33	Max	0.00	133.97	31	0.00	23	0.00	31	967.21	31	-295.43	23	0.00	31
206	-32	-33	Max	133.53	133.97	31	0.00	23	0.00	31	902.81	31	299.93	31	0.00	31
206	-32	-33	Min.	0.00	56.58	23	0.00	31	0.00	23	317.39	23	-948.62	31	0.00	23
206	-32	-33	Min.	133.53	56.58	23	0.00	31	0.00	23	252.99	23	85.40	23	0.00	23
206	-33	-34	Max	0.00	133.97	31	0.00	23	0.00	31	144.33	31	299.99	31	0.00	23
206	-33	-34	Max	124.31								122.68	23			
206	-33	-34	Max	133.53	133.97	31	0.00	23	0.00	31	79.93	31	449.72	31	0.00	23
206	-33	-34	Min.	0.00	56.58	23	0.00	31	0.00	23	59.96	23	85.41	23	0.00	31
206	-33	-34	Min.	124.31								122.68	23			
206	-33	-34	Min.	133.53	56.58	23	0.00	31	0.00	23	-4.45	23	122.48	23	0.00	31
206	-34	-35	Max	0.00	133.97	31	0.00	23	0.00	31	-197.47	23	449.72	31	0.00	23
206	-34	-35	Max	133.53	133.97	31	0.00	23	0.00	31	-261.87	23	-184.21	23	0.00	23
206	-34	-35	Min.	0.00	56.58	23	0.00	31	0.00	23	-678.54	31	122.48	23	0.00	31
206	-34	-35	Min.	133.53	56.58	23	0.00	31	0.00	23	-742.95	31	-499.36	31	0.00	31
206	-35	-36	Max	0.00	133.97	31	0.00	23	0.00	31	-454.90	23	-184.20	23	0.00	23
206	-35	-36	Max	54.07	133.97	31	0.00	23	0.00	23	-480.98	23	-437.20	23	0.00	23
206	-35	-36	Min.	0.00	56.58	23	0.00	31	0.00	23	-1501.42	31	-499.33	31	0.00	31
206	-35	-36	Min.	54.07	56.58	23	0.00	31	0.00	31	-1527.50	31	-1318.15	31	0.00	31
206	-36	-37	Max	0.00	0.00	18	0.00	18	0.00	18	1284.53	31	-562.28	23	0.00	31
206	-36	-37	Max	79.47	0.00	18	0.00	18	0.00	18	1246.20	31	-230.75	23	0.00	31
206	-36	-37	Min.	0.00	0.00	18	0.00	18	0.00	18	436.36	23	-1613.84	31	0.00	23
206	-36	-37	Min.	79.47	0.00	18	0.00	18	0.00	18	398.03	23	-608.30	31	0.00	23
206	-37	-38	Max	0.00	0.00	18	0.00	18	0.00	18	487.72	31	-230.74	23	0.00	31
206	-37	-38	Max	133.53	0.00	18	0.00	18	0.00	18	423.32	31	0.01	31	0.00	31
206	-37	-38	Min.	0.00	0.00	18	0.00	18	0.00	18	205.00	23	-608.26	31	0.00	23
206	-37	-38	Min.	133.53	0.00	18	0.00	18	0.00	18	140.60	23	0.00	23	0.00	23
301	-3	-60	Max	0.00	0.00	18	0.00	18	0.00	18	211.66	31	-60.07	23	0.00	18
301	-3	-60	Max	150.00	0.00	18	0.00	18	0.00	18	62.58	31	0.00	23	0.00	18
301	-3	-60	Min.	0.00	0.00	18	0.00	18	0.00	18	70.30	23	-205.68	31	0.00	18
301	-3	-60	Min.	150.00	0.00	18	0.00	18	0.00	18	9.79	23	0.00	30	0.00	18
301	-59	-3	Max	0.00	0.00	18	0.00	18	0.00	18	-9.79	23	0.00	23	0.00	18
301	-59	-3	Max	150.00	0.00	18	0.00	18	0.00	18	-70.30	23	-60.07	23	0.00	18
301	-59	-3	Min.	0.00	0.00	18	0.00	18	0.00	18	-62.58	31	0.00	31	0.00	18
301	-59	-3	Min.	150.00	0.00	18	0.00	18	0.00	18	-211.66	31	-205.68	31	0.00	18
302	-4	-47	Max	0.00	0.00	18	0.00	18	0.00	18	379.24	31	-87.07	23	0.00	18
302	-4	-47	Max	150.00	0.00	18	0.00	18	0.00	18	125.16	31	0.00	18	0.00	18
302	-4	-47	Min.	0.00	0.00	18	0.00	18	0.00	18	96.51	23	-378.30	31	0.00	18
302	-4	-47	Min.	150.00	0.00	18	0.00	18	0.00	18	19.58	23	0.00	23	0.00	18
302	-46	-4	Max	0.00	0.00	18	0.00	18	0.00	18	-19.58	23	0.00	31	0.00	18
302	-46	-4	Max	150.00	0.00	18	0.00	18	0.00	18	-96.51	23	-87.07	23	0.00	18
302	-46	-4	Min.	0.00	0.00	18	0.00	18	0.00	18	-125.16	31	0.00	23	0.00	18
302	-46	-4	Min.	150.00	0.00	18	0.00	18	0.00	18	-379.24	31	-378.30	31	0.00	18
303	-6	-48	Max	0.00	0.00	18	0.00	18	0.00	18	379.24	31	-87.07	23	0.00	18
303	-6	-48	Max	150.00	0.00	18	0.00	18	0.00	18	125.16	31	0.00	18	0.00	18
303	-6	-48	Min.	0.00	0.00	18	0.00	18	0.00	18	96.51	23	-378.30	31	0.00	18
303	-6	-48	Min.	150.00	0.00	18	0.00	18	0.00	18	19.58	23	0.00	23	0.00	18
303	-49	-6	Max	0.00	0.00	18	0.00	18	0.00	18	-19.58	23	0.00	30	0.00	



332	-101	-35	Min.	150.00	0.00	18	0.00	18	0.00	18	-379.24	31	-378.30	31	0.00	18
333	-37	-103	Max	0.00	0.00	18	0.00	18	0.00	18	379.24	31	-87.07	23	0.00	18
333	-37	-103	Max	150.00	0.00	18	0.00	18	0.00	18	125.16	31	0.00	24	0.00	18
333	-37	-103	Min.	0.00	0.00	18	0.00	18	0.00	18	96.51	23	-378.30	31	0.00	18
333	-37	-103	Min.	150.00	0.00	18	0.00	18	0.00	18	19.58	23	0.00	30	0.00	18
333	-104	-37	Max	0.00	0.00	18	0.00	18	0.00	18	-19.58	23	0.00	24	0.00	18
333	-104	-37	Max	150.00	0.00	18	0.00	18	0.00	18	-96.51	23	-87.07	23	0.00	18
333	-104	-37	Min.	0.00	0.00	18	0.00	18	0.00	18	-125.16	31	0.00	30	0.00	18
333	-104	-37	Min.	150.00	0.00	18	0.00	18	0.00	18	-379.24	31	-378.30	31	0.00	18
334	-38	-99	Max	0.00	0.00	18	0.00	18	0.00	18	211.66	31	-60.07	23	0.00	18
334	-38	-99	Max	150.00	0.00	18	0.00	18	0.00	18	62.58	31	0.00	23	0.00	18
334	-38	-99	Min.	0.00	0.00	18	0.00	18	0.00	18	70.30	23	-205.68	31	0.00	18
334	-38	-99	Min.	150.00	0.00	18	0.00	18	0.00	18	9.79	23	0.00	31	0.00	18
334	-100	-38	Max	0.00	0.00	18	0.00	18	0.00	18	-9.79	23	0.00	31	0.00	18
334	-100	-38	Max	150.00	0.00	18	0.00	18	0.00	18	-70.30	23	-60.07	23	0.00	18
334	-100	-38	Min.	0.00	0.00	18	0.00	18	0.00	18	-62.58	31	0.00	23	0.00	18
334	-100	-38	Min.	150.00	0.00	18	0.00	18	0.00	18	-211.66	31	-205.68	31	0.00	18

Tipo di combinazione di carico: SLE F

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC	
1	1	-5	Max	0.00	-1007.59	25	-52.54	19	0.00	25	0.00	25
1	1	-5	Max	330.00	-818.35	25	-52.54	25	0.00	25	0.00	25
1	1	-5	Min.	0.00	-1505.04	19	-72.85	19	0.00	19	0.00	19
1	1	-5	Min.	330.00	-1315.81	19	-72.85	19	0.00	19	0.00	19
2	2	-10	Max	0.00	-1228.65	25	129.03	19	-87.10	25	0.00	25
2	2	-10	Max	330.00	-1039.42	25	129.03	19	285.05	19	0.00	25
2	2	-10	Min.	0.00	-1913.37	19	79.78	25	-140.74	19	0.00	19
2	2	-10	Min.	330.00	-1724.13	19	79.78	25	176.18	25	0.00	19
3	3	203	Max	0.00	-1336.18	25	-49.22	25	88.46	19	0.00	25
3	3	203	Max	330.00	-1146.95	25	-49.22	25	-108.77	25	0.00	25
3	3	203	Min.	0.00	-2082.31	19	-81.09	19	53.66	25	0.00	25
3	3	203	Min.	330.00	-1893.08	19	-81.09	19	-179.14	19	0.00	25
4	4	204	Max	0.00	-1212.17	25	0.00	19	0.00	25	0.00	19
4	4	204	Max	330.00	-1022.94	25	0.00	19	0.00	25	0.00	19
4	4	204	Min.	0.00	-1809.34	19	0.00	25	0.00	19	0.00	25
4	4	204	Min.	330.00	-1620.10	19	0.00	25	0.00	19	0.00	25
5	5	205	Max	0.00	-1336.18	25	-49.22	25	88.46	19	0.00	25
5	5	205	Max	330.00	-1146.95	25	-49.22	25	-108.77	25	0.00	25
5	5	205	Min.	0.00	-2082.31	19	-81.09	19	53.66	25	0.00	25
5	5	205	Min.	330.00	-1893.08	19	-81.09	19	-179.15	19	0.00	25
6	6	-31	Max	0.00	-1228.65	25	129.03	19	-87.10	25	0.00	19
6	6	-31	Max	330.00	-1039.41	25	129.03	19	285.06	19	0.00	19
6	6	-31	Min.	0.00	-1913.37	19	79.78	25	-140.74	19	0.00	25
6	6	-31	Min.	330.00	-1724.13	19	79.78	25	176.19	25	0.00	25
7	7	-36	Max	0.00	-1007.59	25	-52.54	25	79.49	19	0.00	19
7	7	-36	Max	330.00	-818.36	25	-52.54	25	-116.15	25	0.00	19
7	7	-36	Min.	0.00	-1505.04	19	-72.86	19	57.22	25	0.00	25
7	7	-36	Min.	330.00	-1315.81	19	-72.86	19	-160.94	19	0.00	25
201	-4	-3	Max	0.00	0.00	19	0.00	19	0.00	19	264.46	19
201	-4	-3	Max	133.53	0.00	19	0.00	19	0.00	19	200.06	19
201	-4	-3	Min.	0.00	0.00	19	0.00	19	0.00	19	190.23	25
201	-4	-3	Min.	133.53	0.00	19	0.00	19	0.00	19	125.83	25
201	-5	-4	Max	0.00	0.00	19	0.00	19	0.00	19	614.74	19
201	-5	-4	Max	79.47	0.00	19	0.00	19	0.00	19	576.41	19
201	-5	-4	Min.	0.00	0.00	19	0.00	19	0.00	19	392.05	25
201	-5	-4	Min.	79.47	0.00	19	0.00	19	0.00	19	353.72	25
201	-6	-5	Max	0.00	72.85	19	0.00	19	0.00	25	-400.23	25
201	-6	-5	Max	54.07	72.85	19	0.00	19	0.00	19	-426.31	25
201	-6	-5	Min.	0.00	52.54	25	0.00	25	0.00	19	-675.00	19
201	-6	-5	Min.	54.07	52.54	25	0.00	25	0.00	25	-701.07	19
201	-7	-6	Max	0.00	72.85	19	0.00	19	0.00	25	-172.34	25
201	-7	-6	Max	133.53	72.85	19	0.00	19	0.00	25	-236.74	25
201	-7	-6	Min.	0.00	52.54	25	0.00	25	0.00	19	-298.64	19
201	-7	-6	Min.	133.53	52.54	25	0.00	25	0.00	19	-363.05	19
201	-8	-7	Max	0.00	72.85	19	0.00	19	0.00	25	77.71	19
201	-8	-7	Max	115.18							106.19	25
201	-8	-7	Min.	133.53	72.85	19	0.00	19	0.00	25	13.30	19
201	-8	-7	Min.	0.00	52.54	25	0.00	25	0.00	19	55.55	25
201	-8	-7	Min.	115.18							106.19	25
201	-8	-7	Min.	133.53	52.54	25	0.00	25	0.00	19	-8.85	25
201	-9	-8	Max	0.00	72.85	19	0.00	19	0.00	25	454.06	19
201	-9	-8	Max	133.53	72.85	19	0.00	19	0.00	25	389.65	19
201	-9	-8	Min.	0.00	52.54	25	0.00	25	0.00	19	283.44	25
201	-9	-8	Min.	133.53	52.54	25	0.00	25	0.00	19	219.04	25
201	-10	-9	Max	0.00	72.85	19	0.00	19	0.00	25	787.87	19
201	-10	-9	Max	45.33	72.85	19	0.00	19	0.00	25	766.00	19
201	-10	-9	Min.	0.00	52.54	25	0.00	25	0.00	19	468.80	25
201	-10	-9	Min.	45.33	52.54	25	0.00	25	0.00	19	446.93	25
202	-11	-10	Max	0.00	-27.25	25	0.00	19	0.00	25	-528.08	25
202	-11	-10	Max	88.20	-27.25	25	0.00	19	0.00	25	-570.62	25
202	-11	-10	Min.	0.00	-56.17	19	0.00	25	0.00	19	-893.73	19
202	-11	-10	Min.	88.20	-56.17	19	0.00	25	0.00	19	-936.27	19
202	-12	-11	Max	0.00	-27.25	25	0.00	19	0.00	25	-300.19	25
202	-12	-11	Max	133.53	-27.25	25	0.00	19	0.00	25	-364.59	25
202	-12	-11	Min.	0.00	-56.17	19	0.00	25	0.00	19	-517.38	19
202	-12	-11	Min.	133.53	-56.17	19	0.00	25	0.00	19	-581.78	19
202	-13	-12	Max	0.00	-27.25	25	0.00	19	0.00	25	-72.30	25
202	-13	-12	Max	133.53	-27.25	25	0.00	19	0.00	25	-136.70	25
202	-13	-12	Min.	0.00	-56.17	19	0.00	25	0.00	19	-141.03	19
202	-13	-12	Min.	133.53	-56.17	19	0.00	25	0.00	19	-205.43	19
202	-14	-13	Max	0.00	-27.25	25	0.00	19	0.00	25	235.32	19
202	-14	-13	Max	133.53	-27.25	25	0.00	19	0.00	25	170.92	19
202	-14	-13	Min.	0.00	-56.17	19	0.00	25	0.00	19	155.59	25
202	-14	-13	Min.	133.53	-56.17	19	0.00	25	0.00	19	91.19	25
202	-15	-14	Max	0.00	-27.25	25	0.00	19	0.00	25	611.67	19
202	-15	-14	Max	133.53	-27.25	25	0.00	19	0.00	25	547.27	19
202	-15	-14	Min.	0.00	-56.17	19	0.00	25	0.00	19	383.48	25
202	-15	-14	Min.	133.53	-56.17	19	0.00	25	0.00	19	319.08	25
202	203	-15	Max	0.00	-27.25	25	0.00	19	0.00	25	965.90	19



202	203	-15	Max	87.67	-27.25	25	0.00	19	0.00	25	923.62	19	-210.96	25	0.00	25
202	203	-15	Min.	0.00	-56.17	19	0.00	25	0.00	19	589.25	25	-1171.09	19	0.00	19
202	203	-15	Max	87.67	-56.17	19	0.00	25	0.00	19	546.97	25	-342.85	19	0.00	19
203	-16	203	Max	0.00	24.92	19	0.00	25	0.00	25	-535.57	25	-349.50	25	0.00	19
203	-16	203	Max	45.87	24.92	19	0.00	25	0.00	25	-557.69	25	-600.22	25	0.00	19
203	-16	203	Min.	0.00	21.97	25	0.00	19	0.00	19	-905.05	19	-571.72	19	0.00	25
203	-16	203	Min.	45.87	21.97	25	0.00	19	0.00	19	-927.17	19	-991.91	19	0.00	25
203	-17	-16	Max	0.00	24.92	19	0.00	25	0.00	25	-307.68	25	177.25	19	0.00	19
203	-17	-16	Max	133.53	24.92	19	0.00	25	0.00	25	-372.08	25	-349.51	25	0.00	19
203	-17	-16	Min.	0.00	21.97	25	0.00	19	0.00	19	-528.70	19	104.34	25	0.00	25
203	-17	-16	Min.	133.53	21.97	25	0.00	19	0.00	19	-593.11	19	-571.74	19	0.00	25
203	-18	-17	Max	0.00	24.92	19	0.00	25	0.00	25	-79.79	25	423.69	19	0.00	19
203	-18	-17	Max	133.53	24.92	19	0.00	25	0.00	25	-144.19	25	177.25	19	0.00	19
203	-18	-17	Min.	0.00	21.97	25	0.00	19	0.00	25	-152.36	19	253.89	25	0.00	25
203	-18	-17	Min.	133.53	21.97	25	0.00	19	0.00	19	-216.76	19	104.34	25	0.00	25
203	-19	-18	Max	0.00	24.92	19	0.00	25	0.00	19	224.00	19	167.57	19	0.00	25
203	-19	-18	Max	133.53	24.92	19	0.00	25	0.00	19	159.59	19	423.68	19	0.00	25
203	-19	-18	Min.	0.00	21.97	25	0.00	19	0.00	25	148.10	25	99.12	25	0.00	19
203	-19	-18	Min.	133.53	21.97	25	0.00	19	0.00	25	83.70	25	253.88	25	0.00	19
203	-20	-19	Max	0.00	24.92	19	0.00	25	0.00	19	600.35	19	-359.95	25	0.00	25
203	-20	-19	Max	133.53	24.92	19	0.00	25	0.00	19	535.94	19	167.59	19	0.00	25
203	-20	-19	Min.	0.00	21.97	25	0.00	19	0.00	25	375.99	25	-591.07	19	0.00	19
203	-20	-19	Min.	133.53	21.97	25	0.00	19	0.00	25	311.59	25	99.13	25	0.00	19
203	204	-20	Max	0.00	24.92	19	0.00	25	0.00	19	810.05	19	-461.28	25	0.00	25
203	204	-20	Max	20.00	24.92	19	0.00	25	0.00	19	800.40	19	-359.95	25	0.00	25
203	204	-20	Min.	0.00	21.97	25	0.00	19	0.00	25	511.47	25	-752.12	19	0.00	19
203	204	-20	Min.	20.00	21.97	25	0.00	19	0.00	25	501.82	25	-591.07	19	0.00	19
204	204	-21	Max	0.00	24.92	19	0.00	19	0.00	25	810.05	19	-461.28	25	0.00	19
204	204	-21	Max	20.00	24.92	19	0.00	19	0.00	25	800.40	19	-359.95	25	0.00	19
204	204	-21	Min.	0.00	21.97	25	0.00	25	0.00	19	511.47	25	-752.12	19	0.00	25
204	204	-21	Min.	20.00	21.97	25	0.00	25	0.00	19	501.82	25	-591.07	19	0.00	25
204	-21	-22	Max	0.00	24.92	19	0.00	19	0.00	25	600.35	19	-359.95	25	0.00	19
204	-21	-22	Max	133.53	24.92	19	0.00	19	0.00	25	535.94	19	167.59	19	0.00	19
204	-21	-22	Min.	0.00	21.97	25	0.00	25	0.00	19	375.99	25	-591.07	19	0.00	25
204	-21	-22	Min.	133.53	21.97	25	0.00	25	0.00	19	311.59	25	99.13	25	0.00	25
204	-22	-23	Max	0.00	24.92	19	0.00	19	0.00	25	224.00	19	167.57	19	0.00	19
204	-22	-23	Max	133.53	24.92	19	0.00	19	0.00	25	159.59	19	423.68	19	0.00	19
204	-22	-23	Min.	0.00	21.97	25	0.00	25	0.00	19	148.10	25	99.12	25	0.00	25
204	-22	-23	Min.	133.53	21.97	25	0.00	25	0.00	19	83.70	25	253.88	25	0.00	25
204	-23	-24	Max	0.00	24.92	19	0.00	19	0.00	25	-79.79	25	423.69	19	0.00	25
204	-23	-24	Max	133.53	24.92	19	0.00	19	0.00	25	-144.19	25	177.25	19	0.00	25
204	-23	-24	Min.	0.00	21.97	25	0.00	25	0.00	19	-152.36	19	253.89	25	0.00	19
204	-23	-24	Min.	133.53	21.97	25	0.00	25	0.00	19	-216.76	19	104.34	25	0.00	19
204	-24	-25	Max	0.00	24.92	19	0.00	19	0.00	25	-307.68	25	177.25	19	0.00	25
204	-24	-25	Max	133.53	24.92	19	0.00	19	0.00	25	-372.08	25	-349.51	25	0.00	25
204	-24	-25	Min.	0.00	21.97	25	0.00	25	0.00	19	-528.71	19	104.34	25	0.00	19
204	-24	-25	Min.	133.53	21.97	25	0.00	25	0.00	19	-593.11	19	-571.74	19	0.00	19
204	-25	205	Max	0.00	24.92	19	0.00	19	0.00	25	-535.57	25	-349.50	25	0.00	25
204	-25	205	Max	45.87	24.92	19	0.00	19	0.00	25	-557.69	25	-600.22	25	0.00	25
204	-25	205	Min.	0.00	21.97	25	0.00	25	0.00	19	-905.05	19	-571.73	19	0.00	19
204	-25	205	Min.	45.87	21.97	25	0.00	25	0.00	19	-927.17	19	-991.92	19	0.00	19
205	205	-26	Max	0.00	-27.25	25	0.00	25	0.00	19	965.90	19	-709.01	25	0.00	19
205	205	-26	Max	87.67	-27.25	25	0.00	25	0.00	19	923.62	19	-210.97	25	0.00	19
205	205	-26	Min.	0.00	-56.17	19	0.00	19	0.00	25	589.25	25	-1171.09	19	0.00	25
205	205	-26	Min.	87.67	-56.17	19	0.00	19	0.00	25	546.97	25	-342.85	19	0.00	25
205	-26	-27	Max	0.00	-27.25	25	0.00	25	0.00	19	611.67	19	-210.95	25	0.00	19
205	-26	-27	Max	133.53	-27.25	25	0.00	25	0.00	19	547.27	19	430.96	19	0.00	19
205	-26	-27	Min.	0.00	-56.17	19	0.00	19	0.00	25	383.48	25	-342.82	19	0.00	25
205	-26	-27	Min.	133.53	-56.17	19	0.00	19	0.00	25	319.08	25	258.13	25	0.00	25
205	-27	-28	Max	0.00	-27.25	25	0.00	25	0.00	19	235.32	19	430.94	19	0.00	19
205	-27	-28	Max	133.53	-27.25	25	0.00	25	0.00	19	170.92	19	702.18	19	0.00	19
205	-27	-28	Min.	0.00	-56.17	19	0.00	19	0.00	25	155.59	25	258.12	25	0.00	25
205	-27	-28	Min.	133.53	-56.17	19	0.00	19	0.00	25	91.19	25	422.89	25	0.00	25
205	-28	-29	Max	0.00	-27.25	25	0.00	25	0.00	19	-72.30	25	702.17	19	0.00	25
205	-28	-29	Max	133.53	-27.25	25	0.00	25	0.00	19	-136.70	25	470.85	19	0.00	25
205	-28	-29	Min.	0.00	-56.17	19	0.00	19	0.00	25	-141.03	19	422.88	25	0.00	19
205	-28	-29	Min.	133.53	-56.17	19	0.00	19	0.00	25	-205.43	19	283.34	25	0.00	19
205	-29	-30	Max	0.00	-27.25	25	0.00	25	0.00	19	-300.19	25	470.84	19	0.00	25
205	-29	-30	Max	133.53	-27.25	25	0.00	25	0.00	19	-364.60	25	-160.52	25	0.00	25
205	-29	-30	Min.	0.00	-56.17	19	0.00	19	0.00	25	-517.38	19	283.33	25	0.00	19
205	-29	-30	Min.	133.53	-56.17	19	0.00	19	0.00	25	-581.78	19	-263.03	19	0.00	19
205	-30	-31	Max	0.00	-27.25	25	0.00	25	0.00	19	-528.08	25	-160.51	25	0.00	25
205	-30	-31	Max	88.20	-27.25	25	0.00	25	0.00	19	-570.62	25	-645.04	25	0.00	25
205	-30	-31	Min.	0.00	-56.17	19	0.00	19	0.00	25	-893.73	19	-263.01	19	0.00	19
205	-30	-31	Min.	88.20	-56.17	19	0.00	19	0.00	25	-936.27	19	-1070.04	19	0.00	19
206	-31	-32	Max	0.00	72.86	19	0.00	25	0.00	19	787.87	19	-468.85	25	0.00	19
206	-31	-32	Max	45.33	72.86	19	0.00	25	0.00	19	766.00	19	-261.29	25	0.00	19
206	-31	-32	Min.	0.00	52.54	25	0.00	19	0.00	25	468.79	25	-784.98	19	0.00	25
206	-31	-32	Min.	45.33	52.54	25	0.00	19	0.00	25	446.93	25	-432.77	19	0.00	25
206	-32	-33	Max	0.00	72.86	19	0.00	25	0.00	19	454.06	19	-261.30	25	0.00	19
206	-32	-33	Max	133.53	72.86	19	0.00	25	0.00	19	389.65	19	130.52	19	0.00	19
206	-32	-33	Min.	0.00	52.54	25	0.00	19	0.00	25	283.44	25	-432.80	19	0.00	25
206	-32	-33	Min.	133.53	52.54	25	0.00	19	0.00	25	219.04	25	74.19	25	0.00	25
206	-33	-34	Max	0.00	72.86	19	0.00	25	0.00	19	77.70	19	130.54	19	0.00	2



206	-37	-38	Max	0.00	0.00	19	0.00	19	0.00	19	264.46	19	-211.02	25	0.00	19
206	-37	-38	Max	133.53	0.00	19	0.00	19	0.00	19	200.06	19	0.01	19	0.00	19
206	-37	-38	Min.	0.00	0.00	19	0.00	19	0.00	19	190.23	25	-310.14	19	0.00	25
206	-37	-38	Min.	133.53	0.00	19	0.00	19	0.00	19	125.83	25	0.00	25	0.00	25
301	-3	-60	Max	0.00	0.00	19	0.00	19	0.00	19	100.03	19	-52.46	25	0.00	19
301	-3	-60	Max	150.00	0.00	19	0.00	19	0.00	19	20.89	19	0.00	25	0.00	19
301	-3	-60	Min.	0.00	0.00	19	0.00	19	0.00	19	62.91	25	-90.69	19	0.00	19
301	-3	-60	Min.	150.00	0.00	19	0.00	19	0.00	19	7.03	25	0.00	32	0.00	19
301	-59	-3	Max	0.00	0.00	19	0.00	19	0.00	19	-7.03	25	0.00	25	0.00	19
301	-59	-3	Max	150.00	0.00	19	0.00	19	0.00	19	-62.91	25	-52.46	25	0.00	19
301	-59	-3	Min.	0.00	0.00	19	0.00	19	0.00	19	-20.89	19	0.00	19	0.00	19
301	-59	-3	Min.	150.00	0.00	19	0.00	19	0.00	19	-100.03	19	-90.69	19	0.00	19
302	-4	-47	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
302	-4	-47	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
302	-4	-47	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
302	-4	-47	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	25	0.00	19
302	-46	-4	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	19	0.00	19
302	-46	-4	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
302	-46	-4	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	25	0.00	19
302	-46	-4	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
303	-6	-48	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
303	-6	-48	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
303	-6	-48	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
303	-6	-48	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	25	0.00	19
303	-49	-6	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	32	0.00	19
303	-49	-6	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
303	-49	-6	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	19	0.00	19
303	-49	-6	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
304	-7	-96	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
304	-7	-96	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
304	-7	-96	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
304	-7	-96	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	32	0.00	19
304	-95	-7	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	19	0.00	19
304	-95	-7	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
304	-95	-7	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	32	0.00	19
304	-95	-7	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
305	-8	-66	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
305	-8	-66	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	25	0.00	19
305	-8	-66	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
305	-8	-66	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	19	0.00	19
305	-67	-8	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	19	0.00	19
305	-67	-8	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
305	-67	-8	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	25	0.00	19
305	-67	-8	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
306	-9	-69	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
306	-9	-69	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	25	0.00	19
306	-9	-69	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
306	-9	-69	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	19	0.00	19
306	-68	-9	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	25	0.00	19
306	-68	-9	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
306	-68	-9	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	19	0.00	19
306	-68	-9	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
307	-11	-70	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
307	-11	-70	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	25	0.00	19
307	-11	-70	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
307	-11	-70	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	19	0.00	19
307	-71	-11	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	25	0.00	19
307	-71	-11	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
307	-71	-11	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	32	0.00	19
307	-71	-11	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
308	-12	-72	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
308	-12	-72	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	25	0.00	19
308	-12	-72	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
308	-12	-72	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	19	0.00	19
308	-73	-12	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	32	0.00	19
308	-73	-12	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
308	-73	-12	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	19	0.00	19
308	-73	-12	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
309	-13	-74	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
309	-13	-74	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	25	0.00	19
309	-13	-74	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
309	-13	-74	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	19	0.00	19
309	-75	-13	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	19	0.00	19
309	-75	-13	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
309	-75	-13	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	25	0.00	19
309	-75	-13	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
310	-14	-90	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
310	-14	-90	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	25	0.00	19
310	-14	-90	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
310	-14	-90	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	19	0.00	19
310	-91	-14	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	32	0.00	19
310	-91	-14	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
310	-91	-14	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	19	0.00	19
310	-91	-14	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
311	-15	-92	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
311	-15	-92	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	25	0.00	19
311																



326	-82	-29	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	19	0.00	19
326	-82	-29	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
327	-30	-85	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	19	25	0.00
327	-30	-85	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
327	-30	-85	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
327	-30	-85	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	32	0.00	19
327	-84	-30	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	19	0.00	19
327	-84	-30	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
327	-84	-30	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	32	0.00	19
327	-84	-30	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
329	-32	-86	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
329	-32	-86	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
329	-32	-86	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
329	-32	-86	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	32	0.00	19
329	-87	-32	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	19	0.00	19
329	-87	-32	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
329	-87	-32	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	32	0.00	19
329	-87	-32	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
330	-33	-89	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
330	-33	-89	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
330	-33	-89	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
330	-33	-89	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	32	0.00	19
330	-88	-33	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	25	0.00	19
330	-88	-33	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
330	-88	-33	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	19	0.00	19
330	-88	-33	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
331	-34	-61	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
331	-34	-61	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
331	-34	-61	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
331	-34	-61	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	32	0.00	19
331	-62	-34	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	25	0.00	19
331	-62	-34	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
331	-62	-34	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	19	0.00	19
331	-62	-34	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
332	-35	-102	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
332	-35	-102	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
332	-35	-102	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
332	-35	-102	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	32	0.00	19
332	-101	-35	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	32	0.00	19
332	-101	-35	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
332	-101	-35	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	19	0.00	19
332	-101	-35	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
333	-37	-103	Max	0.00	0.00	19	0.00	19	0.00	19	155.97	19	-71.86	25	0.00	19
333	-37	-103	Max	150.00	0.00	19	0.00	19	0.00	19	41.78	19	0.00	19	0.00	19
333	-37	-103	Min.	0.00	0.00	19	0.00	19	0.00	19	81.74	25	-148.32	19	0.00	19
333	-37	-103	Min.	150.00	0.00	19	0.00	19	0.00	19	14.06	25	0.00	32	0.00	19
333	-104	-37	Max	0.00	0.00	19	0.00	19	0.00	19	-14.06	25	0.00	19	0.00	19
333	-104	-37	Max	150.00	0.00	19	0.00	19	0.00	19	-81.74	25	-71.86	25	0.00	19
333	-104	-37	Min.	0.00	0.00	19	0.00	19	0.00	19	-41.78	19	0.00	32	0.00	19
333	-104	-37	Min.	150.00	0.00	19	0.00	19	0.00	19	-155.97	19	-148.32	19	0.00	19
334	-38	-99	Max	0.00	0.00	19	0.00	19	0.00	19	100.03	19	-52.46	25	0.00	19
334	-38	-99	Max	150.00	0.00	19	0.00	19	0.00	19	20.89	19	0.00	25	0.00	19
334	-38	-99	Min.	0.00	0.00	19	0.00	19	0.00	19	62.91	25	-90.69	19	0.00	19
334	-38	-99	Min.	150.00	0.00	19	0.00	19	0.00	19	7.03	25	0.00	19	0.00	19
334	-100	-38	Max	0.00	0.00	19	0.00	19	0.00	19	-7.03	25	0.00	19	0.00	19
334	-100	-38	Max	150.00	0.00	19	0.00	19	0.00	19	-62.91	25	-52.46	25	0.00	19
334	-100	-38	Min.	0.00	0.00	19	0.00	19	0.00	19	-20.89	19	0.00	25	0.00	19
334	-100	-38	Min.	150.00	0.00	19	0.00	19	0.00	19	-100.03	19	-90.69	19	0.00	19

Tipi di combinazione di carico: SLE Q

Asta	N1	N2		X <cm>	N <daN>	CC Ty <daN>	CC Mz <daNm>	CC Tz <daN>	CC My <daNm>	CC Mx <daNm>	CC					
1	1	-5	Max	0.00	-1183.69	20	-59.73	20	65.10	20	0.00	20	0.00	20	0.00	20
1	1	-5	Max	330.00	-994.46	20	-59.73	20	-132.00	20	0.00	20	0.00	20	0.00	20
1	1	-5	Min.	0.00	-1183.69	20	-59.73	20	65.10	20	0.00	20	0.00	20	0.00	20
1	1	-5	Min.	330.00	-994.46	20	-59.73	20	-132.00	20	0.00	20	0.00	20	0.00	20
2	2	-10	Max	0.00	-1471.04	20	97.22	20	-106.09	20	0.00	20	0.00	20	0.00	20
2	2	-10	Max	330.00	-1281.81	20	97.22	20	214.72	20	0.00	20	0.00	20	0.00	20
2	2	-10	Min.	0.00	-1471.04	20	97.22	20	-106.09	20	0.00	20	0.00	20	0.00	20
2	2	-10	Min.	330.00	-1281.81	20	97.22	20	214.72	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	0.00	-1600.32	20	-60.50	20	65.98	20	0.00	20	0.00	20	0.00	20
3	3	203	Max	330.00	-1411.08	20	-60.50	20	-133.68	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	0.00	-1600.32	20	-60.50	20	65.98	20	0.00	20	0.00	20	0.00	20
3	3	203	Min.	330.00	-1411.08	20	-60.50	20	-133.68	20	0.00	20	0.00	20	0.00	20
4	4	204	Max	0.00	-1423.57	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Max	330.00	-1234.34	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Min.	0.00	-1423.57	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
4	4	204	Min.	330.00	-1234.34	20	0.00	20	0.00	20	0.00	20	0.00	20	0.00	20
5	5	205	Max	0.00	-1600.32	20	-60.50	20	65.98	20	0.00	20	0.00	20	0.00	20
5	5	205	Max	330.00	-1411.08	20	-60.50	20	-133.68	20	0.00	20	0.00	20	0.00	20
5	5	205	Min.	0.00	-1600.32	20	-60.50	20	65.98	20	0.00	20	0.00	20	0.00	20
5	5	205	Min.	330.00	-1411.08	20	-60.50	20	-133.68	20	0.00	20	0.00	20	0.00	20
6	6	-31	Max	0.00	-1471.04	20	97.22	20	-106.09	20	0.00	20	0.00	20	0.00	20
6	6	-31	Max	330.00	-1281.81	20	97.22	20	214.73	20	0.00	20	0.00	20	0.00	20
6	6	-31	Min.	0.00	-1471.04	20	97.22	20	-106.09	20	0.00	20	0.00	20	0.00	20
6	6	-31	Min.	330.00	-1281.81	20	97.22	20	214.73	20	0.00	20	0.00	20	0.00	20
7	7	-36	Max	0.00	-1183.69	20	-59.73	20	65.11	20	0.00	20	0.00	20	0.00	20
7	7	-36	Max	330.00	-994.46	20	-59.73	20	-132.01	20	0.00	20	0.			

Foggia Solar S.r.l.



CODE

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201	-6	-5	Min.	0.00	59.73	20	0.00	20	0.00	20	-497.50	20	-197.04	20	0.00	20
201	-6	-5	Min.	54.07	59.73	20	0.00	20	0.00	20	-523.58	20	-473.07	20	0.00	20
201	-7	-6	Max	0.00	59.73	20	0.00	20	0.00	20	-217.05	20	135.80	20	0.00	20
201	-7	-6	Max	133.53	59.73	20	0.00	20	0.00	20	-281.45	20	-197.04	20	0.00	20
201	-7	-6	Min.	0.00	59.73	20	0.00	20	0.00	20	-217.05	20	135.80	20	0.00	20
201	-7	-6	Min.	133.53	59.73	20	0.00	20	0.00	20	-281.45	20	-197.04	20	0.00	20
201	-8	-7	Max	0.00	59.73	20	0.00	20	0.00	20	63.39	20	94.14	20	0.00	20
201	-8	-7	Max	131.44								135.81	20			
201	-8	-7	Max	133.53	59.73	20	0.00	20	0.00	20	-1.01	20	135.80	20	0.00	20
201	-8	-7	Min.	0.00	59.73	20	0.00	20	0.00	20	63.39	20	94.14	20	0.00	20
201	-8	-7	Min.	131.44								135.81	20			
201	-8	-7	Min.	133.53	59.73	20	0.00	20	0.00	20	-1.01	20	135.80	20	0.00	20
201	-9	-8	Max	0.00	59.73	20	0.00	20	0.00	20	343.84	20	-322.00	20	0.00	20
201	-9	-8	Max	133.53	59.73	20	0.00	20	0.00	20	279.44	20	94.15	20	0.00	20
201	-9	-8	Min.	0.00	59.73	20	0.00	20	0.00	20	343.84	20	-322.00	20	0.00	20
201	-9	-8	Min.	133.53	59.73	20	0.00	20	0.00	20	279.44	20	94.15	20	0.00	20
201	-10	-9	Max	0.00	59.73	20	0.00	20	0.00	20	581.75	20	-580.77	20	0.00	20
201	-10	-9	Max	45.33	59.73	20	0.00	20	0.00	20	559.88	20	-322.00	20	0.00	20
201	-10	-9	Min.	0.00	59.73	20	0.00	20	0.00	20	581.75	20	-580.77	20	0.00	20
201	-10	-9	Min.	45.33	59.73	20	0.00	20	0.00	20	559.88	20	-322.00	20	0.00	20
202	-11	-10	Max	0.00	-37.49	20	0.00	20	0.00	20	-657.52	20	-196.80	20	0.00	20
202	-11	-10	Max	88.20	-37.49	20	0.00	20	0.00	20	-700.06	20	-795.49	20	0.00	20
202	-11	-10	Min.	0.00	-37.49	20	0.00	20	0.00	20	-657.52	20	-196.80	20	0.00	20
202	-11	-10	Min.	88.20	-37.49	20	0.00	20	0.00	20	-700.06	20	-795.49	20	0.00	20
202	-12	-11	Max	0.00	-37.49	20	0.00	20	0.00	20	-377.07	20	349.72	20	0.00	20
202	-12	-11	Max	133.53	-37.49	20	0.00	20	0.00	20	-441.48	20	-196.80	20	0.00	20
202	-12	-11	Min.	0.00	-37.49	20	0.00	20	0.00	20	-377.07	20	349.72	20	0.00	20
202	-12	-11	Min.	133.53	-37.49	20	0.00	20	0.00	20	-441.48	20	-196.80	20	0.00	20
202	-13	-12	Max	0.00	-37.49	20	0.00	20	0.00	20	-96.63	20	521.75	20	0.00	20
202	-13	-12	Max	133.53	-37.49	20	0.00	20	0.00	20	-161.03	20	349.72	20	0.00	20
202	-13	-12	Min.	0.00	-37.49	20	0.00	20	0.00	20	-96.63	20	521.75	20	0.00	20
202	-13	-12	Min.	133.53	-37.49	20	0.00	20	0.00	20	-161.03	20	349.72	20	0.00	20
202	-14	-13	Max	0.00	-37.49	20	0.00	20	0.00	20	183.82	20	319.30	20	0.00	20
202	-14	-13	Max	133.53	-37.49	20	0.00	20	0.00	20	119.41	20	521.75	20	0.00	20
202	-14	-13	Min.	0.00	-37.49	20	0.00	20	0.00	20	183.82	20	319.30	20	0.00	20
202	-14	-13	Min.	133.53	-37.49	20	0.00	20	0.00	20	119.41	20	521.75	20	0.00	20
202	-15	-14	Max	0.00	-37.49	20	0.00	20	0.00	20	464.26	20	-257.65	20	0.00	20
202	-15	-14	Max	133.53	-37.49	20	0.00	20	0.00	20	399.86	20	319.30	20	0.00	20
202	-15	-14	Min.	0.00	-37.49	20	0.00	20	0.00	20	464.26	20	-257.65	20	0.00	20
202	-15	-14	Min.	133.53	-37.49	20	0.00	20	0.00	20	399.86	20	319.30	20	0.00	20
202	203	-15	Max	0.00	-37.49	20	0.00	20	0.00	20	722.59	20	-872.59	20	0.00	20
202	203	-15	Max	87.67	-37.49	20	0.00	20	0.00	20	680.31	20	-257.65	20	0.00	20
202	203	-15	Min.	0.00	-37.49	20	0.00	20	0.00	20	722.59	20	-872.59	20	0.00	20
202	203	-15	Min.	87.67	-37.49	20	0.00	20	0.00	20	680.31	20	-257.65	20	0.00	20
203	-16	203	Max	0.00	23.02	20	0.00	20	0.00	20	-666.37	20	-428.17	20	0.00	20
203	-16	203	Max	45.87	23.02	20	0.00	20	0.00	20	-688.49	20	-738.88	20	0.00	20
203	-16	203	Min.	0.00	23.02	20	0.00	20	0.00	20	-666.37	20	-428.17	20	0.00	20
203	-16	203	Min.	45.87	23.02	20	0.00	20	0.00	20	-688.49	20	-738.88	20	0.00	20
203	-17	-16	Max	0.00	23.02	20	0.00	20	0.00	20	-385.92	20	130.16	20	0.00	20
203	-17	-16	Max	133.53	23.02	20	0.00	20	0.00	20	-450.33	20	-428.18	20	0.00	20
203	-17	-16	Min.	0.00	23.02	20	0.00	20	0.00	20	-385.92	20	130.16	20	0.00	20
203	-17	-16	Min.	133.53	23.02	20	0.00	20	0.00	20	-450.33	20	-428.18	20	0.00	20
203	-18	-17	Max	0.00	23.02	20	0.00	20	0.00	20	-105.48	20	314.00	20	0.00	20
203	-18	-17	Max	133.53	23.02	20	0.00	20	0.00	20	-169.88	20	130.15	20	0.00	20
203	-18	-17	Min.	0.00	23.02	20	0.00	20	0.00	20	-105.48	20	314.00	20	0.00	20
203	-18	-17	Min.	133.53	23.02	20	0.00	20	0.00	20	-169.88	20	130.15	20	0.00	20
203	-19	-18	Max	0.00	23.02	20	0.00	20	0.00	20	174.97	20	123.35	20	0.00	20
203	-19	-18	Max	133.53	23.02	20	0.00	20	0.00	20	110.57	20	313.99	20	0.00	20
203	-19	-18	Min.	0.00	23.02	20	0.00	20	0.00	20	174.97	20	123.35	20	0.00	20
203	-19	-18	Min.	133.53	23.02	20	0.00	20	0.00	20	110.57	20	313.99	20	0.00	20
203	-20	-19	Max	0.00	23.02	20	0.00	20	0.00	20	455.42	20	-441.77	20	0.00	20
203	-20	-19	Max	133.53	23.02	20	0.00	20	0.00	20	391.01	20	123.36	20	0.00	20
203	-20	-19	Min.	0.00	23.02	20	0.00	20	0.00	20	455.42	20	-441.77	20	0.00	20
203	-20	-19	Min.	133.53	23.02	20	0.00	20	0.00	20	391.01	20	123.36	20	0.00	20
203	204	-20	Max	0.00	23.02	20	0.00	20	0.00	20	617.17	20	-564.24	20	0.00	20
203	204	-20	Max	20.00	23.02	20	0.00	20	0.00	20	607.52	20	-441.77	20	0.00	20
203	204	-20	Min.	0.00	23.02	20	0.00	20	0.00	20	617.17	20	-564.24	20	0.00	20
203	204	-20	Min.	20.00	23.02	20	0.00	20	0.00	20	607.52	20	-441.77	20	0.00	20
204	204	-21	Max	0.00	23.02	20	0.00	20	0.00	20	617.17	20	-564.24	20	0.00	20
204	204	-21	Max	20.00	23.02	20	0.00	20	0.00	20	607.52	20	-441.77	20	0.00	20
204	204	-21	Min.	0.00	23.02	20	0.00	20	0.00	20	617.17	20	-564.24	20	0.00	20
204	204	-21	Min.	20.00	23.02	20	0.00	20	0.00	20	607.52	20	-441.77	20	0.00	20
204	-21	-22	Max	0.00	23.02	20	0.00	20	0.00	20	455.41	20	-441.77	20	0.00	20
204	-21	-22	Max	133.53	23.02	20	0.00	20	0.00	20	391.01	20	123.36	20	0.00	20
204	-21	-22	Min.	0.00	23.02	20	0.00	20	0.00	20	455.41	20	-441.77	20	0.00	20
204	-21	-22	Min.	133.53	23.02	20	0.00	20	0.00	20	391.01	20	123.36	20	0.00	20
204	-22	-23	Max	0.00	23.02	20	0.00	20	0.00	20	174.97	20	123.35	20	0.00	20
204	-22	-23	Max	133.53	23.02	20	0.00	20	0.00	20	110.57	20	313.99	20	0.00	20
204	-22	-23	Min.	0.00	23.02	20	0.00	20	0.00	20	174.97	20	123.35	20	0.00	20
204	-22	-23	Min.	133.53	23.02	20	0.00	20	0.00	20	110.57	20	313.99	20	0.00	20
204	-23	-24	Max	0.00	23.02	20	0.00	20	0.00	20	-105.48	20	314.00	20	0.00	20
204	-23	-24	Max	133.53	23.02	20	0.00	20	0.00	20	-169.88	20	130.15	20	0.00	20
204	-23	-24	Min.	0.00	23.02	20	0.00	20	0.00	20	-105.48	20	314.00	20	0.00	20
204	-23	-24	Min.	133.53	23.02	20	0.00	20	0.00	20	-169.88	20	130.15	20	0.00	20
204	-24	-25	Max	0.00	23.02	20	0.00	20	0.00	20	-385.92	20	130.15	20	0.00	20
204	-24	-25	Max	133.53	23.02	20	0.00	20	0.00	20	-450.33					



205	-27	-28	Max	133.53	-37.49	20	0.00	20	0.00	20	119.41	20	521.76	20	0.00	20
205	-27	-28	Min.	0.00	-37.49	20	0.00	20	0.00	20	183.82	20	319.30	20	0.00	20
205	-27	-28	Max	133.53	-37.49	20	0.00	20	0.00	20	119.41	20	521.76	20	0.00	20
205	-28	-29	Max	0.00	-37.49	20	0.00	20	0.00	20	-96.63	20	521.75	20	0.00	20
205	-28	-29	Max	133.53	-37.49	20	0.00	20	0.00	20	-161.03	20	349.72	20	0.00	20
205	-28	-29	Min.	0.00	-37.49	20	0.00	20	0.00	20	-96.63	20	521.75	20	0.00	20
205	-28	-29	Min.	133.53	-37.49	20	0.00	20	0.00	20	-161.03	20	349.72	20	0.00	20
205	-29	-30	Max	0.00	-37.49	20	0.00	20	0.00	20	-377.08	20	349.71	20	0.00	20
205	-29	-30	Max	133.53	-37.49	20	0.00	20	0.00	20	-441.48	20	-196.81	20	0.00	20
205	-29	-30	Min.	0.00	-37.49	20	0.00	20	0.00	20	-377.08	20	349.71	20	0.00	20
205	-29	-30	Min.	133.53	-37.49	20	0.00	20	0.00	20	-441.48	20	-196.81	20	0.00	20
205	-30	-31	Max	0.00	-37.49	20	0.00	20	0.00	20	-657.52	20	-196.80	20	0.00	20
205	-30	-31	Max	88.20	-37.49	20	0.00	20	0.00	20	-700.06	20	-795.49	20	0.00	20
205	-30	-31	Min.	0.00	-37.49	20	0.00	20	0.00	20	-657.52	20	-196.80	20	0.00	20
205	-30	-31	Min.	88.20	-37.49	20	0.00	20	0.00	20	-700.06	20	-795.49	20	0.00	20
206	-31	-32	Max	0.00	59.73	20	0.00	20	0.00	20	581.75	20	-580.76	20	0.00	20
206	-31	-32	Max	45.33	59.73	20	0.00	20	0.00	20	559.88	20	-321.99	20	0.00	20
206	-31	-32	Min.	0.00	59.73	20	0.00	20	0.00	20	581.75	20	-580.76	20	0.00	20
206	-31	-32	Min.	45.33	59.73	20	0.00	20	0.00	20	559.88	20	-321.99	20	0.00	20
206	-32	-33	Max	0.00	59.73	20	0.00	20	0.00	20	343.84	20	-322.01	20	0.00	20
206	-32	-33	Max	133.53	59.73	20	0.00	20	0.00	20	279.44	20	94.13	20	0.00	20
206	-32	-33	Min.	0.00	59.73	20	0.00	20	0.00	20	343.84	20	-322.01	20	0.00	20
206	-32	-33	Min.	133.53	59.73	20	0.00	20	0.00	20	279.44	20	94.13	20	0.00	20
206	-33	-34	Max	0.00	59.73	20	0.00	20	0.00	20	63.39	20	94.15	20	0.00	20
206	-33	-34	Max	131.44									135.81	20		
206	-33	-34	Min.	133.53	59.73	20	0.00	20	0.00	20	-1.01	20	135.80	20	0.00	20
206	-33	-34	Min.	0.00	59.73	20	0.00	20	0.00	20	63.39	20	94.15	20	0.00	20
206	-33	-34	Min.	131.44									135.81	20		
206	-33	-34	Min.	133.53	59.73	20	0.00	20	0.00	20	-1.01	20	135.80	20	0.00	20
206	-34	-35	Max	0.00	59.73	20	0.00	20	0.00	20	-217.05	20	135.80	20	0.00	20
206	-34	-35	Max	133.53	59.73	20	0.00	20	0.00	20	-281.46	20	-197.04	20	0.00	20
206	-34	-35	Min.	0.00	59.73	20	0.00	20	0.00	20	-217.05	20	135.80	20	0.00	20
206	-34	-35	Min.	133.53	59.73	20	0.00	20	0.00	20	-281.46	20	-197.04	20	0.00	20
206	-35	-36	Max	0.00	59.73	20	0.00	20	0.00	20	-497.50	20	-197.03	20	0.00	20
206	-35	-36	Max	54.07	59.73	20	0.00	20	0.00	20	-523.57	20	-473.06	20	0.00	20
206	-35	-36	Min.	0.00	59.73	20	0.00	20	0.00	20	-497.50	20	-197.03	20	0.00	20
206	-35	-36	Min.	54.07	59.73	20	0.00	20	0.00	20	-523.57	20	-473.06	20	0.00	20
206	-36	-37	Max	0.00	0.00	20	0.00	20	0.00	20	470.88	20	-605.09	20	0.00	20
206	-36	-37	Max	79.47	0.00	20	0.00	20	0.00	20	432.55	20	-246.12	20	0.00	20
206	-36	-37	Min.	0.00	0.00	20	0.00	20	0.00	20	470.88	20	-605.09	20	0.00	20
206	-36	-37	Min.	79.47	0.00	20	0.00	20	0.00	20	432.55	20	-246.12	20	0.00	20
206	-37	-38	Max	0.00	0.00	20	0.00	20	0.00	20	216.51	20	-246.11	20	0.00	20
206	-37	-38	Max	133.53	0.00	20	0.00	20	0.00	20	152.10	20	0.00	20	0.00	20
206	-37	-38	Min.	0.00	0.00	20	0.00	20	0.00	20	216.51	20	-246.11	20	0.00	20
206	-37	-38	Min.	133.53	0.00	20	0.00	20	0.00	20	152.10	20	0.00	20	0.00	20
301	-3	-60	Max	0.00	0.00	20	0.00	20	0.00	20	76.05	20	-65.99	20	0.00	20
301	-3	-60	Max	150.00	0.00	20	0.00	20	0.00	20	11.94	20	0.00	20	0.00	20
301	-3	-60	Min.	0.00	0.00	20	0.00	20	0.00	20	76.05	20	-65.99	20	0.00	20
301	-3	-60	Min.	150.00	0.00	20	0.00	20	0.00	20	11.94	20	0.00	20	0.00	20
301	-59	-3	Max	0.00	0.00	20	0.00	20	0.00	20	-11.94	20	0.00	20	0.00	20
301	-59	-3	Max	150.00	0.00	20	0.00	20	0.00	20	-76.05	20	-65.99	20	0.00	20
301	-59	-3	Min.	0.00	0.00	20	0.00	20	0.00	20	-11.94	20	0.00	20	0.00	20
301	-59	-3	Min.	150.00	0.00	20	0.00	20	0.00	20	-76.05	20	-65.99	20	0.00	20
302	-4	-47	Max	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.00	20
302	-4	-47	Max	150.00	0.00	20	0.00	20	0.00	20	23.88	20	0.00	20	0.00	20
302	-4	-47	Min.	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.00	20
302	-4	-47	Min.	150.00	0.00	20	0.00	20	0.00	20	23.88	20	0.00	20	0.00	20
302	-46	-4	Max	0.00	0.00	20	0.00	20	0.00	20	-23.88	20	0.00	20	0.00	20
302	-46	-4	Max	150.00	0.00	20	0.00	20	0.00	20	-108.02	20	-98.92	20	0.00	20
302	-46	-4	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.88	20	0.00	20	0.00	20
302	-46	-4	Min.	150.00	0.00	20	0.00	20	0.00	20	-108.02	20	-98.92	20	0.00	20
303	-6	-48	Max	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.00	20
303	-6	-48	Max	150.00	0.00	20	0.00	20	0.00	20	23.88	20	0.00	20	0.00	20
303	-6	-48	Min.	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.00	20
303	-6	-48	Min.	150.00	0.00	20	0.00	20	0.00	20	23.88	20	0.00	20	0.00	20
303	-49	-6	Max	0.00	0.00	20	0.00	20	0.00	20	-23.88	20	0.00	20	0.00	20
303	-49	-6	Max	150.00	0.00	20	0.00	20	0.00	20	-108.02	20	-98.92	20	0.00	20
303	-49	-6	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.88	20	0.00	20	0.00	20
303	-49	-6	Min.	150.00	0.00	20	0.00	20	0.00	20	-108.02	20	-98.92	20	0.00	20
304	-7	-96	Max	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.00	20
304	-7	-96	Max	150.00	0.00	20	0.00	20	0.00	20	23.88	20	0.00	20	0.00	20
304	-7	-96	Min.	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.00	20
304	-7	-96	Min.	150.00	0.00	20	0.00	20	0.00	20	23.88	20	0.00	20	0.00	20
304	-95	-7	Max	0.00	0.00	20	0.00	20	0.00	20	-23.88	20	0.00	20	0.00	20
304	-95	-7	Max	150.00	0.00	20	0.00	20	0.00	20	-108.02	20	-98.92	20	0.00	20
304	-95	-7	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.88	20	0.00	20	0.00	20
304	-95	-7	Min.	150.00	0.00	20	0.00	20	0.00	20	-108.02	20	-98.92	20	0.00	20
305	-8	-66	Max	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.00	20
305	-8	-66	Max	150.00	0.00	20	0.00	20	0.00	20	23.88	20	0.00	20	0.00	20
305	-8	-66	Min.	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.00	20
305	-8	-66	Min.	150.00	0.00	20	0.00	20	0.00	20	23.88	20	0.00	20	0.00	20
305	-67	-8	Max	0.00	0.00	20	0.00	20	0.00	20	-23.88	20	0.00	20	0.00	20
305	-67	-8	Max	150.00	0.00	20	0.00	20	0.00	20	-108.02	20	-98.92	20	0.00	20
305	-67	-8	Min.	0.00	0.00	20	0.00	20	0.00	20	-23.88	20	0.00	20	0.00	20
305	-67	-8	Min.	150.00	0.00	20	0.00	20	0.00	20	-108.02	20	-98.92	20	0.00	20
306	-9	-69	Max	0.00	0.00	20	0.00	20	0.00	20	108.02	20	-98.92	20	0.0	



Simbologia

Φ_{LT}	=	Coefficiente Φ per stabilità laterale membrature inflesse
Φ_y	=	Coefficiente Φ per inflessione intorno all'asse y(c)
Φ_z	=	Coefficiente Φ per inflessione intorno all'asse z(e)
α_{imp}	=	Coefficiente di imperfezione
$\alpha_{my}, \alpha_{mz}, \alpha_{LT}$	=	Coefficienti correttivi per il momento flettente
β_{LT}	=	Coefficiente per calcolo Φ_{LT}
χ_{LT}	=	Coefficiente di riduzione per stabilità laterale membrature inflesse
χ_y	=	Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
χ_z	=	Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
δ	<cm>	=Spostamento relativo asta
λ'_y	=	Snellezza adimensionale per inflessione intorno all'asse y(c)
λ'_z	=	Snellezza adimensionale per inflessione intorno all'asse z(e)
λ_{LT}	=	Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$	=	Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
λ_y	=	Snellezza per inflessione intorno all'asse y(c)
λ_z	=	Snellezza per inflessione intorno all'asse z(e)
$\sigma_{ID,max}$	<daN/cm²>	= Tensione ideale massima
σ_M	<daN/cm²>	= Tensione normale per momento flettente
σ_N	<daN/cm²>	= Tensione normale per sforzo normale
τ	<daN/cm²>	= Tensione tangenziale per taglio e/o torsione
ψ	=	Coeff. di correzione momento critico per stabilità laterale membrature inflesse
A_{eff}	<cm²>	= Area effettiva per trazione
A_{net}	<cm²>	= Area netta per compressione
A_{area}	<cm²>	= Area
$A_{tag,y}$	<cm²>	= Area resistente a taglio in dir. Y
$A_{tag,z}$	<cm²>	= Area resistente a taglio in dir. Z
CC	=	Numero della combinazione delle condizioni di carico elementari
$Cod.$	=	Codice
$Curva$	=	Curva di instabilità adottata
D	<cm>	= Distanza
F_{yk}	<daN/cm²>	= Tensione caratteristica di snervamento dell'acciaio
F_{yt}	<daN/cm²>	= Tensione caratteristica di rottura
I_y	<cm⁴>	= Raggio giratorio d'inerzia rispetto all'asse Y
I_z	<cm⁴>	= Raggio giratorio d'inerzia rispetto all'asse Z
J_0	<cm⁶>	= Costante di ingobbamento
J_y	<cm⁴>	= Momento d'inerzia rispetto all'asse Y
J_z	<cm⁴>	= Momento d'inerzia rispetto all'asse Z
$K_{yy}, K_{yz}, K_{zy}, K_{zz}$	=	Coefficienti di interazione
L	<m>	= Lunghezza dell'asta
L_{cr}	<m>	= Lunghezza di libera inflessione laterale fra ritegni torsionali
M_{cr}	<daNm>	= Momento critico per instabilità flessio torsionale
$M_{Ny,c,Rd}$	<daNm>	= Resistenza di calcolo a pressoflessione intorno all'asse Y
$M_{Nz,c,Rd}$	<daNm>	= Resistenza di calcolo a pressoflessione intorno all'asse Z
M_x	<daNm>	= Momento torcente intorno all'asse X
M_y	<daNm>	= Momento flettente intorno all'asse Y
M_y,Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Y
M_y,V,c,Rd	<daNm>	= Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y
M_z	<daNm>	= Momento flettente intorno all'asse Z
M_z,Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Z
M_z,V,c,Rd	<daNm>	= Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Z
N	<daN>	= Sforzo normale
N,Ed	<daN>	= Forza assiale di calcolo
N_c,Rd	<daN>	= Resistenza a compressione
$N_{cr,y}$	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
$N_{cr,z}$	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
$Sez.$	=	Numero della sezione
$Tipo$	=	Tipologia
		Rc = Rettangolare cava
		Is = I stondata
Tp	=	Tipo di acciaio
T_y	<daN>	= Taglio in dir. Y
T_z	<daN>	= Taglio in dir. Z
V_y,Ed	<daN>	= Forza di taglio di calcolo
V_c,Rd	<daN>	= Resistenza a taglio
V_c,Rd,Red	<daN>	= Resistenza a taglio ridotta
$W_y,plac$	<cm³>	= Modulo di resistenza plastico intorno all'asse Y
W_{ymin}	<cm³>	= Modulo di resistenza minimo rispetto all'asse Y
$W_z,plac$	<cm³>	= Modulo di resistenza plastico intorno all'asse Z
W_{zmin}	<cm³>	= Modulo di resistenza minimo rispetto all'asse Z
X_1	<m>	= Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
f	=	Fattore di modifica per il coefficiente di riduzione
$f_{z,g}$	<cm>	= Freccia in direzione Z globale
$f_{z,l}$	<cm>	= Freccia in direzione Z locale
k_c	=	Coeff. di correzione momento flettente per stabilità laterale membrature inflesse

Caratteristiche profilati utilizzati

Sez. Cod.	Tipo	D	Area	Anet	Aeff	Jy	Jz	Iy	Iz	Wymin	Wzmin	Tp	Fyk	Fyt	
		<cm>	<cm²>	<cm²>	<cm²>	<cm⁴>	<cm⁴>	<cm⁴>	<cm⁴>	<cm³>	<cm³>		<daN/cm²>	<daN/cm²>	
1	COL HEA240	Is	--	76.84	76.84	76.84	7763.40	2768.81	10.05	6.00	675.08	230.73	S355 UNI EN 10025-2	3550.00	5100.00
2	TRV PRINC SHS200x200x8	Rc	--	61.44	61.44	61.44	3781.43	3781.43	7.85	7.85	378.14	378.14	S355H UNI EN 10210-1	3550.00	5100.00
3	TRV SEC RHS150x100x8	Rc	--	37.44	37.44	37.44	1128.23	588.15	5.49	3.96	150.43	117.63	S355H UNI EN 10210-1	3550.00	5100.00

Caratteristiche profilati utilizzati

Sez. Cod.	Wy,plac	Wz,plac	Atag,y	Atag,z	J0	
	<cm³>	<cm³>	<cm²>	<cm²>	<cm⁶>	
1	COL HEA240	747.99	352.10	64.54	25.18	328486.00
2	TRV PRINC SHS200x200x8	442.62	442.62	30.72	30.72	
3	TRV SEC RHS150x100x8	185.42	138.62	14.98	22.46	

Asta n. 1 (1 -5) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 3 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-883.76 T_y=169.79 M_y=569.89 T_y=-662.32 M_z=1237.31
 Tensioni: σ_N =-11.50 $\sigma_{m,d}$ =-620.67 τ =0.00 σ_{max} =-632.17 (sfrut=0.19)
 Tensioni: σ_N =-11.50 $\sigma_{m,d}$ =34.99 τ =16.55 τ_{max} =16.55 (sfrut=0.01)
 Tensioni: σ_N =-11.50 $\sigma_{m,d}$ =-620.67 τ =0.00 $\sigma_{ID,max}$ =632.17 (sfrut=0.19)

- Verifica a taglio Dir. Y [4.2.16] - CC 29 SLU X1=0.00 - Classe 2

Sollecitazioni: $T_y = -192.50$
 $V, Ed = -192.50$ $V_c, Rd = 125981.00$ $V, Ed/V_c, Rd = 0.00$

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU $X1 = 3.30$ - Classe 2
 Sollecitazioni: $N = -4104.84$ $T_y = -192.50$ $M_z = -424.76$
 $M_z, Ed = -424.76$ $M_z, V, c, Rd = 11904.20$
 $N, Ed = -4104.84$ $N_c, Rd = -259785.00$ ZZ $n = N, Ed/N_c, Rd = 0.02$ $MNz, c, Rd = 11904.20$ $Mz, Ed/MNz, c, Rd = 0.04$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N, Ed = -883.76$ $M_y, Ed = 569.89$ $M_z, Ed = 1237.31$ $L = 3.30$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $L_{cr} = 3.30$ Curva b: $\alpha_{imp} = 0.34$ $k_c = 0.94$ $\psi = 1.73$ $M, cr = 121063.00$ $\lambda_{LT} = 0.44$
 $\lambda_{LT, 0} = 0.40$ $\Phi_{LT} = 0.58$ $\beta_{LT} = 0.75$ $f = 0.98$ $\chi_{LT} = 1.00$
 $\lambda_y = 32.83$ $Ncr, y = 1477550.00$ $\lambda'_y = 0.43$ Curva b: $\Phi_y = 0.63$ $\chi_y = 0.91$
 $\lambda_z = 54.97$ $Ncr, z = 526968.00$ $\lambda'_z = 0.72$ Curva c: $\Phi_z = 0.89$ $\chi_z = 0.71$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.02 + 0.15 = 0.18$
 Verifica ZZ: $0.00 + 0.02 + 0.15 = 0.17$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta = 0.02$ (L/16009)

Asta n. 2 (2 -10) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = -1295.40$ $T_x = 210.38$ $M_y = 689.07$ $T_y = 832.33$ $M_z = -1423.19$
 Tensioni: $\sigma_N = -16.86$ $\sigma_{m, d} = -718.88$ $\tau = 0.00$ $\sigma_{max} = -735.74$ (sfrut=0.22)
 Tensioni: $\sigma_N = -16.86$ $\sigma_{m, d} = -218.64$ $\tau = 20.79$ $\tau_{max} = 20.79$ (sfrut=0.01)
 Tensioni: $\sigma_N = -16.86$ $\sigma_{m, d} = -718.88$ $\tau = 0.00$ $\sigma_{ID, max} = 735.74$ (sfrut=0.22)

- Verifica a taglio Dir. Y [4.2.16] - CC 29 SLU $X1 = 0.00$ - Classe 2
 Sollecitazioni: $T_y = 404.76$
 $V, Ed = 404.76$ $V_c, Rd = 125981.00$ $V, Ed/V_c, Rd = 0.00$

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU $X1 = 3.30$ - Classe 2
 Sollecitazioni: $N = -5536.98$ $T_y = 404.76$ $M_z = 894.58$
 $M_z, Ed = 894.58$ $M_z, V, c, Rd = 11904.20$
 $N, Ed = -5536.98$ $N_c, Rd = -259785.00$ ZZ $n = N, Ed/N_c, Rd = 0.02$ $MNz, c, Rd = 11904.20$ $Mz, Ed/MNz, c, Rd = 0.08$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3
 Sollecitazioni: $N, Ed = -1295.40$ $M_y, Ed = 689.07$ $M_z, Ed = -1423.19$ $L = 3.30$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $L_{cr} = 3.30$ Curva b: $\alpha_{imp} = 0.34$ $k_c = 0.94$ $\psi = 1.76$ $M, cr = 122841.00$ $\lambda_{LT} = 0.44$
 $\lambda_{LT, 0} = 0.40$ $\Phi_{LT} = 0.58$ $\beta_{LT} = 0.75$ $f = 0.98$ $\chi_{LT} = 1.00$
 $\lambda_y = 32.83$ $Ncr, y = 1477550.00$ $\lambda'_y = 0.43$ Curva b: $\Phi_y = 0.63$ $\chi_y = 0.91$
 $\lambda_z = 54.97$ $Ncr, z = 526968.00$ $\lambda'_z = 0.72$ Curva c: $\Phi_z = 0.89$ $\chi_z = 0.71$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00 + 0.03 + 0.17 = 0.21$
 Verifica ZZ: $0.00 + 0.02 + 0.17 = 0.20$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta = 0.04$ (L/7697)

Asta n. 3 (3 203) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 3 SND $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = -1543.26$ $T_x = 233.20$ $M_y = 760.84$ $T_y = -751.74$ $M_z = 1335.51$
 Tensioni: $\sigma_N = -20.08$ $\sigma_{m, d} = -691.51$ $\tau = 0.00$ $\sigma_{max} = -711.60$ (sfrut=0.21)
 Tensioni: $\sigma_N = -20.08$ $\sigma_{m, d} = 18.44$ $\tau = 18.81$ $\tau_{max} = 18.81$ (sfrut=0.01)
 Tensioni: $\sigma_N = -20.08$ $\sigma_{m, d} = -691.51$ $\tau = 0.00$ $\sigma_{ID, max} = 711.60$ (sfrut=0.21)

- Verifica a taglio Dir. Y [4.2.16] - CC 29 SLU $X1 = 0.00$ - Classe 2
 Sollecitazioni: $T_y = -258.82$
 $V, Ed = -258.82$ $V_c, Rd = 125981.00$ $V, Ed/V_c, Rd = 0.00$

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU $X1 = 3.30$ - Classe 2
 Sollecitazioni: $N = -6052.19$ $T_y = -258.82$ $M_z = -571.61$
 $M_z, Ed = -571.61$ $M_z, V, c, Rd = 11904.20$
 $N, Ed = -6052.19$ $N_c, Rd = -259785.00$ ZZ $n = N, Ed/N_c, Rd = 0.02$ $MNz, c, Rd = 11904.20$ $Mz, Ed/MNz, c, Rd = 0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N, Ed = -1543.26$ $M_y, Ed = 760.84$ $M_z, Ed = 1335.51$ $L = 3.30$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$
 $L_{cr} = 3.30$ Curva b: $\alpha_{imp} = 0.34$ $k_c = 0.94$ $\psi = 1.76$ $M, cr = 123134.00$ $\lambda_{LT} = 0.44$
 $\lambda_{LT, 0} = 0.40$ $\Phi_{LT} = 0.58$ $\beta_{LT} = 0.75$ $f = 0.98$ $\chi_{LT} = 1.00$
 $\lambda_y = 32.83$ $Ncr, y = 1477550.00$ $\lambda'_y = 0.43$ Curva b: $\Phi_y = 0.63$ $\chi_y = 0.91$
 $\lambda_z = 54.97$ $Ncr, z = 526968.00$ $\lambda'_z = 0.72$ Curva c: $\Phi_z = 0.89$ $\chi_z = 0.71$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz} = 0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01 + 0.03 + 0.16 = 0.20$
 Verifica ZZ: $0.01 + 0.03 + 0.16 = 0.19$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta = 0.03$ (L/12123)

Asta n. 4 (4 204) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 3 SND $X1 = 0.00$ - Classe 3
 Sollecitazioni: $N = -1423.57$ $T_x = -205.53$ $M_y = -686.88$ $T_y = 716.36$ $M_z = -1296.97$
 Tensioni: $\sigma_N = -18.53$ $\sigma_{m, d} = -663.86$ $\tau = 0.00$ $\sigma_{max} = -682.38$ (sfrut=0.20)
 Tensioni: $\sigma_N = -18.53$ $\sigma_{m, d} = -24.80$ $\tau = 17.91$ $\tau_{max} = 17.91$ (sfrut=0.01)
 Tensioni: $\sigma_N = -18.53$ $\sigma_{m, d} = -663.86$ $\tau = 0.00$ $\sigma_{ID, max} = 682.38$ (sfrut=0.20)

- Verifica a compressione (4.2.4.1.2.2) - CC 29 SLU $X1 = 0.00$ - Classe 2
 Sollecitazioni: $N = -5226.35$
 Verifica a compressione [4.2.9]
 $N, Ed = -5226.35$ $N_c, Rd = -259785.00$ $N, Ed/N_c, Rd = 0.02$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N, Ed = -1423.57$ $M_y, Ed = -686.88$ $M_z, Ed = -1296.97$ $L = 3.30$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT} = 0.95, 0.95, 0.95$

$L_{cr}=3.30$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.74$ $M,cr=121369.00$ $\lambda_{LT}=0.44$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.58$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.03+0.16=0.19$
 Verifica ZZ: $0.01+0.02+0.16=0.19$

Asta n. 5 (5 205) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-1543.26$ $T_x=-233.20$ $M_y=-760.84$ $T_y=-751.74$ $M_z=1335.51$
 Tensioni: $\sigma_{N}=-20.08$ $\sigma_{M,d}=-691.51$ $\tau=0.00$ $\sigma_{max}=-711.60$ (sfrut=0.21)
 Tensioni: $\sigma_{N}=-20.08$ $\sigma_{M,d}=220.32$ $\tau=18.81$ $\tau_{max}=18.81$ (sfrut=0.01)
 Tensioni: $\sigma_{N}=-20.08$ $\sigma_{M,d}=-691.51$ $\tau=0.00$ $\sigma_{ID,max}=711.60$ (sfrut=0.21)

- Verifica a taglio Dir. Y [4.2.16] - CC 29 SLU $X1=0.00$ - Classe 2
 Sollecitazioni: $T_y=-258.82$
 $V,Ed=-258.82$ $V_c,Rd=125981.00$ $V,Ed/V_c,Rd=0.00$

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU $X1=3.30$ - Classe 2
 Sollecitazioni: $N=-6052.19$ $T_y=-258.82$ $M_z=571.61$
 $M_z,Ed=-571.61$ $M_z,V,c,Rd=11904.20$
 $N,Ed=-6052.19$ $N_c,Rd=259785.00$ ZZ $n=N,Ed/N_c,Rd=0.02$ $MNz,c,Rd=11904.20$ $Mz,Ed/MNz,c,Rd=0.05$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3
 Sollecitazioni: $N,Ed=-1543.26$ $M_y,Ed=-760.84$ $M_z,Ed=1335.51$ $L=3.30$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$L_{cr}=3.30$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.76$ $M,cr=123134.00$ $\lambda_{LT}=0.44$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.58$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.01+0.03+0.16=0.20$
 Verifica ZZ: $0.01+0.03+0.16=0.19$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.03$ (L/12142)

Asta n. 6 (6 -31) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 3 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-1295.40$ $T_x=-210.38$ $M_y=-689.07$ $T_y=832.33$ $M_z=-1423.19$
 Tensioni: $\sigma_{N}=-16.86$ $\sigma_{M,d}=-718.88$ $\tau=0.00$ $\sigma_{max}=-735.74$ (sfrut=0.22)
 Tensioni: $\sigma_{N}=-16.86$ $\sigma_{M,d}=-35.80$ $\tau=20.79$ $\tau_{max}=20.79$ (sfrut=0.01)
 Tensioni: $\sigma_{N}=-16.86$ $\sigma_{M,d}=-718.88$ $\tau=0.00$ $\sigma_{ID,max}=735.74$ (sfrut=0.22)

- Verifica a taglio Dir. Y [4.2.16] - CC 29 SLU $X1=0.00$ - Classe 2
 Sollecitazioni: $T_y=404.76$
 $V,Ed=404.76$ $V_c,Rd=125981.00$ $V,Ed/V_c,Rd=0.00$

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU $X1=3.30$ - Classe 2
 Sollecitazioni: $N=-5536.98$ $T_y=404.76$ $M_z=894.59$
 $M_z,Ed=894.59$ $M_z,V,c,Rd=11904.20$
 $N,Ed=-5536.98$ $N_c,Rd=259785.00$ ZZ $n=N,Ed/N_c,Rd=0.02$ $MNz,c,Rd=11904.20$ $Mz,Ed/MNz,c,Rd=0.08$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-1295.40$ $M_y,Ed=-689.07$ $M_z,Ed=-1423.19$ $L=3.30$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$L_{cr}=3.30$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.76$ $M,cr=122841.00$ $\lambda_{LT}=0.44$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.58$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.03+0.17=0.21$
 Verifica ZZ: $0.00+0.02+0.17=0.20$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.04$ (L/7693)

Asta n. 7 (7 -36) - Sez. 1 (COL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-883.76$ $T_x=-169.79$ $M_y=-569.89$ $T_y=-662.32$ $M_z=1237.31$
 Tensioni: $\sigma_{N}=-11.50$ $\sigma_{M,d}=-620.67$ $\tau=0.00$ $\sigma_{max}=632.17$ (sfrut=0.19)
 Tensioni: $\sigma_{N}=-11.50$ $\sigma_{M,d}=186.21$ $\tau=16.55$ $\tau_{max}=16.55$ (sfrut=0.01)
 Tensioni: $\sigma_{N}=-11.50$ $\sigma_{M,d}=-620.67$ $\tau=0.00$ $\sigma_{ID,max}=632.17$ (sfrut=0.19)

- Verifica a taglio Dir. Y [4.2.16] - CC 29 SLU $X1=0.00$ - Classe 2
 Sollecitazioni: $T_y=-192.51$
 $V,Ed=-192.51$ $V_c,Rd=125981.00$ $V,Ed/V_c,Rd=0.00$

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 29 SLU $X1=3.30$ - Classe 2
 Sollecitazioni: $N=-4104.84$ $T_y=-192.51$ $M_z=-424.77$
 $M_z,Ed=-424.77$ $M_z,V,c,Rd=11904.20$
 $N,Ed=-4104.84$ $N_c,Rd=259785.00$ ZZ $n=N,Ed/N_c,Rd=0.02$ $MNz,c,Rd=11904.20$ $Mz,Ed/MNz,c,Rd=0.04$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3
 Sollecitazioni: $N,Ed=-883.76$ $M_y,Ed=-569.89$ $M_z,Ed=1237.31$ $L=3.30$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$L_{cr}=3.30$ Curva b: $\alpha_{imp}=0.34$ $k_c=0.94$ $\psi=1.73$ $M,cr=121063.00$ $\lambda_{LT}=0.44$
 $\lambda_{LT,0}=0.40$ $\Phi_{LT}=0.58$ $\beta_{LT}=0.75$ $f=0.98$ $\chi_{LT}=1.00$
 $\lambda_y=32.83$ Ncr,y=1477550.00 $\lambda'_y=0.43$ Curva b: $\Phi_y=0.63$ $\chi_y=0.91$
 $\lambda_z=54.97$ Ncr,z=526968.00 $\lambda'_z=0.72$ Curva c: $\Phi_z=0.89$ $\chi_z=0.71$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.15=0.18$
 Verifica ZZ: $0.00+0.02+0.15=0.17$

- Verifica Spostamento relativo massimo per singola asta - CC 31
 $\delta=0.02$ (L/15879)

Asta n. 201 (-4 -3) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=28.47 T_x=216.51 M_y=246.11 T_y=94.91 M_z=-126.73
 Tensioni: $\sigma_N=0.46$ $\sigma_{m,d}=98.60$ $\tau=0.00$ $\sigma_{max}=99.06$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.46$ $\sigma_{m,d}=-30.83$ $\tau=7.92$ $\tau_{max}=7.92$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.46$ $\sigma_{m,d}=98.60$ $\tau=0.00$ $\sigma_{TD,max}=99.06$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=701.07
 V,Ed=701.07 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=701.07 M_y=880.26
 My,Ed=880.26 My,V,c,Rd=14964.90 My,Ed/My,V,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
 Sollecitazioni: N,Ed=-28.47 My,Ed=246.11 Mz,Ed=-126.73 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=17.02$ Ncr,y=4395380.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395380.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 201 (-5 -4) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-69.78 T_x=470.88 M_y=605.07 T_y=232.61 M_z=-311.58
 Tensioni: $\sigma_N=-1.14$ $\sigma_{m,d}=-242.41$ $\tau=0.00$ $\sigma_{max}=-243.54$ (sfrut=0.07)
 Tensioni: $\sigma_N=-1.14$ $\sigma_{m,d}=-75.81$ $\tau=17.23$ $\tau_{max}=17.23$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.14$ $\sigma_{m,d}=-242.41$ $\tau=0.00$ $\sigma_{TD,max}=243.54$ (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=1870.98
 V,Ed=1870.98 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=1870.98 M_y=2347.26
 My,Ed=2347.26 My,V,c,Rd=14964.90 My,Ed/My,V,c,Rd=0.16

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
 Sollecitazioni: N,Ed=-69.78 My,Ed=605.07 Mz,Ed=311.58 L=0.79
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=10.13$ Ncr,y=12411000.00 $\lambda'_y=0.13$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=10.13$ Ncr,z=12411000.00 $\lambda'_z=0.13$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.04+0.02=0.07
 Verifica ZZ: 0.00+0.04+0.02=0.06

Asta n. 201 (-6 -5) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.54 - Classe 3
 Sollecitazioni: N=-244.94 T_x=-823.50 M_y=1289.40 T_y=-80.42 M_z=-93.44 M_x=-9.57
 Tensioni: $\sigma_N=-3.99$ $\sigma_{m,d}=-365.69$ $\tau=1.62$ $\sigma_{max}=-369.68$ (sfrut=0.11)
 Tensioni: $\sigma_N=-3.99$ $\sigma_{m,d}=-22.73$ $\tau=31.75$ $\tau_{max}=31.75$ (sfrut=0.02)
 Tensioni: $\sigma_N=-3.99$ $\sigma_{m,d}=-365.69$ $\tau=1.62$ $\sigma_{TD,max}=369.69$ (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.54 - Classe 1
 Sollecitazioni: T_x=-2233.86
 V,Ed=-2233.86 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.04

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.54 - Classe 1
 Sollecitazioni: N=192.50 T_x=-2233.86 M_y=1922.50
 My,Ed=1922.50 My,V,c,Rd=14964.90
 N,Ed=192.50 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.13

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
 Sollecitazioni: N,Ed=-244.94 My,Ed=1289.40 Mz,Ed=-93.44 L=0.54
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=6.89$ Ncr,y=26811000.00 $\lambda'_y=0.09$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=6.89$ Ncr,z=26811000.00 $\lambda'_z=0.09$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.10+0.01=0.10
 Verifica ZZ: 0.00+0.08+0.01=0.08

Asta n. 201 (-7 -6) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-110.40 T_x=-581.38 M_y=851.20 T_y=-40.06 M_z=-49.96 M_x=-9.57
 Tensioni: $\sigma_N=-1.80$ $\sigma_{m,d}=-238.31$ $\tau=1.62$ $\sigma_{max}=-240.11$ (sfrut=0.07)
 Tensioni: $\sigma_N=-1.80$ $\sigma_{m,d}=-12.16$ $\tau=22.89$ $\tau_{max}=22.89$ (sfrut=0.01)
 Tensioni: $\sigma_N=-1.80$ $\sigma_{m,d}=-238.31$ $\tau=1.62$ $\sigma_{TD,max}=240.13$ (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 1
 Sollecitazioni: T_x=-1079.88
 V,Ed=-1079.88 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 1
 Sollecitazioni: N=192.50 T_x=-1079.88 M_y=723.88
 My,Ed=723.88 My,V,c,Rd=14964.90
 N,Ed=192.50 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
 Sollecitazioni: N,Ed=-110.40 My,Ed=851.20 Mz,Ed=-49.96 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=17.02$ Ncr,y=4395380.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395380.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.06+0.00=0.07

Verifica ZZ: 0.00+0.05+0.00=0.05

Asta n. 201 (-8 -7) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=85.44 T_s=298.92 M_y=-389.45 T_y=3.27 M_z=3.53 M_x=-9.58
 Tensioni: σ_N=1.39 σ_{m,d}=103.92 τ=1.62 σ_{max}=105.31 (sfrut=0.03)
 Tensioni: σ_N=1.39 σ_{m,d}=-0.86 τ=12.56 τ_{max}=12.56 (sfrut=0.01)
 Tensioni: σ_N=1.39 σ_{m,d}=103.92 τ=1.62 σ_{TD,max}=105.35 (sfrut=0.03)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 1 SND Xl=0.00 - Classe 1
 Sollecitazioni: T_y=3.27 M_x=-9.58
 V,Ed=3.27 Vc,Rd,Red=59917.10 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 1 SND Xl=0.00 - Classe 1
 Sollecitazioni: T_z=363.32 M_x=-9.58
 V,Ed=363.32 Vc,Rd,Red=59917.10 V,Ed/Vc,Rd,Red=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 1
 Sollecitazioni: N=192.50 T_s=123.92 M_y=-662.22
 My,Ed=-662.22 My,V,c,Rd=14964.90
 N,Ed=192.50 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.04

Asta n. 201 (-9 -8) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-58.97 T_s=643.77 M_y=869.35 T_y=46.59 M_z=-63.06 M_x=-9.58
 Tensioni: σ_N=-0.96 σ_{m,d}=-246.58 τ=1.62 σ_{max}=-247.53 (sfrut=0.07)
 Tensioni: σ_N=-0.96 σ_{m,d}=15.34 τ=25.17 τ_{max}=25.17 (sfrut=0.01)
 Tensioni: σ_N=-0.96 σ_{m,d}=-246.58 τ=1.62 σ_{TD,max}=247.55 (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=1411.44
 V,Ed=1411.44 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=192.50 T_s=1411.44 M_y=1387.99
 My,Ed=1387.99 My,V,c,Rd=14964.90
 N,Ed=192.50 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: My,Ed=1387.99 Mz,Ed=-0.00 L=1.34
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=17.02 Ncr,y=4395370.00 λ'_y=0.22 Curva a: Φ_y=0.53 χ_y=0.99
 λ_z=17.02 Ncr,z=4395370.00 λ'_z=0.22 Curva a: Φ_z=0.53 χ_z=0.99
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.10=0.10
 Verifica ZZ: 0.00+0.08=0.08

Asta n. 201 (-10 -9) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-192.43 T_s=881.68 M_y=1264.10 T_y=86.63 M_z=-102.33 M_x=-9.58
 Tensioni: σ_N=-3.13 σ_{m,d}=-361.35 τ=1.62 σ_{max}=-364.48 (sfrut=0.11)
 Tensioni: σ_N=-3.13 σ_{m,d}=24.90 τ=33.87 τ_{max}=33.87 (sfrut=0.02)
 Tensioni: σ_N=-3.13 σ_{m,d}=-361.35 τ=1.62 σ_{TD,max}=364.50 (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_z=2559.94
 V,Ed=2559.94 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.04

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=192.50 T_s=2559.94 M_y=2542.07
 My,Ed=2542.07 My,V,c,Rd=14964.90
 N,Ed=192.50 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.17

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: My,Ed=2542.07 Mz,Ed=-0.00 L=0.45
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=5.78 Ncr,y=38136200.00 λ'_y=0.08 Curva a: Φ_y=0.00 χ_y=1.00
 λ_z=5.78 Ncr,z=38136200.00 λ'_z=0.08 Curva a: Φ_z=0.00 χ_z=1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.19=0.19
 Verifica ZZ: 0.00+0.15=0.15

Asta n. 202 (-11 -10) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

 - Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.88 - Classe 3
 Sollecitazioni: N=-455.13 T_s=-824.35 M_y=1220.94 T_y=-104.15 M_z=-102.46 M_x=-4.40
 Tensioni: σ_N=-7.41 σ_{m,d}=-349.97 τ=0.75 σ_{max}=-357.38 (sfrut=0.11)
 Tensioni: σ_N=-7.41 σ_{m,d}=-24.93 τ=30.90 τ_{max}=30.90 (sfrut=0.02)
 Tensioni: σ_N=-7.41 σ_{m,d}=-349.97 τ=0.75 σ_{TD,max}=357.38 (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.88 - Classe 1
 Sollecitazioni: T_z=-2977.04
 V,Ed=-2977.04 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.05

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.88 - Classe 1
 Sollecitazioni: N=-212.25 T_s=-2977.04 M_y=3436.65
 My,Ed=3436.65 My,V,c,Rd=14964.90
 N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.23

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-212.25 My,Ed=3436.65 Mz,Ed=-0.00 L=0.88
 α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
 λ_y=11.24 Ncr,y=10074900.00 λ'_y=0.15 Curva a: Φ_y=0.00 χ_y=1.00
 λ_z=11.24 Ncr,z=10074900.00 λ'_z=0.15 Curva a: Φ_z=0.00 χ_z=1.00
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.26=0.26
 Verifica ZZ: 0.00+0.20=0.21

Asta n. 202 (-12 -11) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=46.17 T_s=-339.79 M_y=-394.68 T_y=208.39 M_z=-242.92 M_x=14.68
 Tensioni: $\sigma_N=0.75$ $\sigma_{m,d}=168.61$ $\tau=2.49$ $\sigma_{max}=169.37$ (sfrut=0.05)
 Tensioni: $\sigma_N=0.75$ $\sigma_{m,d}=59.10$ $\tau=14.92$ $\tau_{max}=14.92$ (sfrut=0.01)
 Tensioni: $\sigma_N=0.75$ $\sigma_{m,d}=168.61$ $\tau=2.49$ $\sigma_{TD,max}=169.42$ (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 1
 Sollecitazioni: T_s=-1801.66
 V,Ed=-1801.66 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-212.25 T_s=-1717.94 M_y=-1514.62
 My,Ed=-1514.62 My,V,c,Rd=14964.90
 N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-212.25 My,Ed=-1514.62 Mz,Ed=-0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=17.02$ Ncr,y=4395370.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395370.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.11=0.11
 Verifica ZZ: 0.00+0.09=0.09

Asta n. 202 (-13 -12) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-77.82 T_s=-133.91 M_y=-526.58 T_y=-63.97 M_z=328.35 M_x=-14.68
 Tensioni: $\sigma_N=-1.27$ $\sigma_{m,d}=-226.09$ $\tau=2.49$ $\sigma_{max}=-227.35$ (sfrut=0.07)
 Tensioni: $\sigma_N=-1.27$ $\sigma_{m,d}=79.89$ $\tau=7.39$ $\tau_{max}=7.39$ (sfrut=0.00)
 Tensioni: $\sigma_N=-1.27$ $\sigma_{m,d}=-226.09$ $\tau=2.49$ $\sigma_{TD,max}=227.40$ (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 1
 Sollecitazioni: T_s=-597.86
 V,Ed=-597.86 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: N=-212.25 T_s=-514.13 M_y=-2257.07
 My,Ed=-2257.07 My,V,c,Rd=14964.90
 N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.15

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-212.25 My,Ed=-2257.07 Mz,Ed=-0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=17.02$ Ncr,y=4395370.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395370.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.17=0.17
 Verifica ZZ: 0.00+0.13=0.14

Asta n. 202 (-14 -13) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=1.34 - Classe 3
 Sollecitazioni: N=-34.50 T_s=82.13 M_y=-526.58 T_y=80.44 M_z=328.35 M_x=-14.68
 Tensioni: $\sigma_N=-0.56$ $\sigma_{m,d}=-226.09$ $\tau=2.49$ $\sigma_{max}=-226.65$ (sfrut=0.07)
 Tensioni: $\sigma_N=-0.56$ $\sigma_{m,d}=-79.89$ $\tau=5.50$ $\tau_{max}=5.50$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.56$ $\sigma_{m,d}=-226.09$ $\tau=2.49$ $\sigma_{TD,max}=226.69$ (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_s=689.67
 V,Ed=689.67 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 1
 Sollecitazioni: N=-212.25 T_s=605.94 M_y=-2257.07
 My,Ed=-2257.07 My,V,c,Rd=14964.90
 N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.15

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-212.25 My,Ed=-2257.07 Mz,Ed=-0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=17.02$ Ncr,y=4395370.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395370.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.17=0.17
 Verifica ZZ: 0.00+0.13=0.14

Asta n. 202 (-15 -14) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-191.87 T_s=588.55 M_y=605.67 T_y=67.46 M_z=-23.80 M_x=-4.40
 Tensioni: $\sigma_N=-3.12$ $\sigma_{m,d}=-166.46$ $\tau=0.75$ $\sigma_{max}=-169.59$ (sfrut=0.05)
 Tensioni: $\sigma_N=-3.12$ $\sigma_{m,d}=5.79$ $\tau=22.28$ $\tau_{max}=22.28$ (sfrut=0.01)
 Tensioni: $\sigma_N=-3.12$ $\sigma_{m,d}=-166.46$ $\tau=0.75$ $\sigma_{TD,max}=169.59$ (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_s=1893.47
 V,Ed=1893.47 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 1
 Sollecitazioni: N=-212.25 T_s=1809.74 M_y=-1392.04
 My,Ed=-1392.04 My,V,c,Rd=14964.90
 N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-212.25 My,Ed=-1392.04 Mz,Ed=-0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=17.02$ Ncr,y=4395370.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395370.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.10=0.10
Verifica ZZ: 0.00+0.08=0.08

Asta n. 202 (203 -15) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-330.59 T_s=846.87 M_y=1329.56 T_y=109.07 M_z=-119.42 M_x=-4.41
Tensioni: $\sigma_N=-5.38$ $\sigma_{m,d}=-383.18$ $\tau=0.75$ $\sigma_{max}=-388.56$ (sfrut=0.11)
Tensioni: $\sigma_N=-5.38$ $\sigma_{m,d}=29.05$ $\tau=31.73$ $\tau_{max}=31.73$ (sfrut=0.02)
Tensioni: $\sigma_N=-5.38$ $\sigma_{m,d}=-383.18$ $\tau=0.75$ $\sigma_{ID,max}=388.57$ (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_s=3068.51
V,Ed=3068.51 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.05

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-212.25 T_s=3068.51 M_y=3746.45
My,Ed=3746.45 My,V,c,Rd=14964.90
N,Ed=-212.25 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.25

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-212.25 My,Ed=3746.45 Mz,Ed=-0.00 L=0.88
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=11.17$ Ncr,y=10197800.00 $\lambda'_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.17$ Ncr,z=10197800.00 $\lambda'_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.28=0.28
Verifica ZZ: 0.00+0.22=0.22

Asta n. 203 (-16 203) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.46 - Classe 3
Sollecitazioni: N=-309.81 T_s=-869.83 M_y=1293.43 T_y=-104.54 M_z=-119.34 M_x=4.32
Tensioni: $\sigma_N=-5.04$ $\sigma_{m,d}=-373.61$ $\tau=0.73$ $\sigma_{max}=-378.65$ (sfrut=0.11)
Tensioni: $\sigma_N=-5.04$ $\sigma_{m,d}=29.04$ $\tau=32.55$ $\tau_{max}=32.55$ (sfrut=0.02)
Tensioni: $\sigma_N=-5.04$ $\sigma_{m,d}=-373.61$ $\tau=0.73$ $\sigma_{ID,max}=378.65$ (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.46 - Classe 1
Sollecitazioni: T_s=-2983.68
V,Ed=-2983.68 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.05

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.46 - Classe 1
Sollecitazioni: N=46.56 T_s=-2983.68 M_y=3174.75
My,Ed=3174.75 My,V,c,Rd=14964.90
N,Ed=46.56 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.21

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: My,Ed=3174.75 Mz,Ed=-0.00 L=0.46
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=5.85$ Ncr,y=37254500.00 $\lambda'_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.85$ Ncr,z=37254500.00 $\lambda'_z=0.08$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.24=0.24
Verifica ZZ: 0.00+0.19=0.19

Asta n. 203 (-17 -16) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.34 - Classe 3
Sollecitazioni: N=-176.28 T_s=-631.67 M_y=899.56 T_y=-64.48 M_z=-71.39 M_x=4.32
Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-256.77$ $\tau=0.73$ $\sigma_{max}=-259.64$ (sfrut=0.08)
Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=17.37$ $\tau=23.84$ $\tau_{max}=23.84$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-256.77$ $\tau=0.73$ $\sigma_{ID,max}=259.64$ (sfrut=0.08)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 1
Sollecitazioni: T_s=-1834.85
V,Ed=-1834.85 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 1
Sollecitazioni: N=46.56 T_s=-1834.85 M_y=1812.88
My,Ed=1812.88 My,V,c,Rd=14964.90
N,Ed=46.56 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.12

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: My,Ed=1812.88 Mz,Ed=-0.00 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=17.02$ Ncr,y=4395380.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395380.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.13=0.13
Verifica ZZ: 0.00+0.11=0.11

Asta n. 203 (-18 -17) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3
Sollecitazioni: N=6.55 T_s=-159.88 M_y=-317.88 T_y=-70.52 M_z=143.20 M_x=14.41
Tensioni: $\sigma_N=0.11$ $\sigma_{m,d}=121.93$ $\tau=2.44$ $\sigma_{max}=122.04$ (sfrut=0.04)
Tensioni: $\sigma_N=0.11$ $\sigma_{m,d}=-34.84$ $\tau=8.29$ $\tau_{max}=8.29$ (sfrut=0.00)
Tensioni: $\sigma_N=0.11$ $\sigma_{m,d}=121.93$ $\tau=2.44$ $\sigma_{ID,max}=122.11$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.34 - Classe 1
Sollecitazioni: T_s=-631.05
V,Ed=-631.05 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=46.56 T_s=-547.32 M_y=-1368.08
My,Ed=-1368.08 My,V,c,Rd=14964.90
N,Ed=46.56 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
Sollecitazioni: My,Ed=-317.88 Mz,Ed=143.20 L=1.34
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=17.02$ Ncr, $y=4395370.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr, $z=4395370.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.02+0.01=0.03$

Asta n. 203 (-19 -18) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=1.34 - Classe 3
 Sollecitazioni: $N=49.87$ $T_x=56.16$ $M_y=-317.87$ $T_y=73.89$ $M_z=143.19$ $M_x=14.41$
 Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=121.93$ $\tau=2.44$ $\sigma_{max}=122.74$ (sfrut=0.04)
 Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=77.34$ $\tau=5.15$ $\tau_{max}=5.15$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=121.93$ $\tau=2.44$ $\sigma_{ID,max}=122.81$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_x=656.48$
 $V,Ed=656.48$ $V_c,Rd=59967.00$ $V,Ed/V_c,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 1
 Sollecitazioni: $N=46.56$ $T_x=572.76$ $M_y=-1368.04$
 $My,Ed=-1368.04$ $My,V,c,Rd=14964.90$
 $N,Ed=46.56$ $Nc,Rd=207726.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=14964.90$ $My,Ed/MNy,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $My,Ed=-1368.04$ $Mz,Ed=0.00$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ Ncr, $y=4395380.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr, $z=4395380.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.10=0.10$
 Verifica ZZ: $0.00+0.08=0.08$

Asta n. 203 (-20 -19) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-210.93$ $T_x=636.76$ $M_y=939.00$ $T_y=65.49$ $M_z=-74.10$ $M_x=4.32$
 Tensioni: $\sigma_N=-3.43$ $\sigma_{m,d}=-267.91$ $\tau=0.73$ $\sigma_{max}=-271.35$ (sfrut=0.08)
 Tensioni: $\sigma_N=-3.43$ $\sigma_{m,d}=-18.03$ $\tau=24.03$ $\tau_{max}=24.03$ (sfrut=0.01)
 Tensioni: $\sigma_N=-3.43$ $\sigma_{m,d}=-267.91$ $\tau=0.73$ $\sigma_{ID,max}=271.35$ (sfrut=0.08)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_x=1860.28$
 $V,Ed=1860.28$ $V_c,Rd=59967.00$ $V,Ed/V_c,Rd=0.03$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $N=46.56$ $T_x=1860.28$ $M_y=1880.82$
 $My,Ed=1880.82$ $My,V,c,Rd=14964.90$
 $N,Ed=46.56$ $Nc,Rd=207726.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=14964.90$ $My,Ed/MNy,c,Rd=0.13$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $My,Ed=1880.82$ $Mz,Ed=0.00$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ Ncr, $y=4395370.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr, $z=4395370.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.14=0.14$
 Verifica ZZ: $0.00+0.11=0.11$

Asta n. 203 (204 -20) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-308.32$ $T_x=798.51$ $M_y=1097.74$ $T_y=94.71$ $M_z=-93.04$ $M_x=4.32$
 Tensioni: $\sigma_N=-5.02$ $\sigma_{m,d}=-314.90$ $\tau=0.73$ $\sigma_{max}=-319.92$ (sfrut=0.09)
 Tensioni: $\sigma_N=-5.02$ $\sigma_{m,d}=-22.64$ $\tau=29.94$ $\tau_{max}=29.94$ (sfrut=0.02)
 Tensioni: $\sigma_N=-5.02$ $\sigma_{m,d}=-314.90$ $\tau=0.73$ $\sigma_{ID,max}=319.92$ (sfrut=0.09)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_x=2490.17$
 $V,Ed=2490.17$ $V_c,Rd=59967.00$ $V,Ed/V_c,Rd=0.04$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $N=46.56$ $T_x=2490.17$ $M_y=2377.60$
 $My,Ed=2377.60$ $My,V,c,Rd=14964.90$
 $N,Ed=46.56$ $Nc,Rd=207726.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=14964.90$ $My,Ed/MNy,c,Rd=0.16$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: $My,Ed=2377.60$ $Mz,Ed=0.00$ $L=0.20$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=2.55$ Ncr, $y=195939000.00$ $\lambda'_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=2.55$ Ncr, $z=195939000.00$ $\lambda'_z=0.03$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.18=0.18$
 Verifica ZZ: $0.00+0.14=0.14$

Asta n. 204 (204 -21) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
 Sollecitazioni: $N=-308.32$ $T_x=798.51$ $M_y=1097.74$ $T_y=94.71$ $M_z=93.04$ $M_x=-4.32$
 Tensioni: $\sigma_N=-5.02$ $\sigma_{m,d}=-314.90$ $\tau=0.73$ $\sigma_{max}=-319.92$ (sfrut=0.09)
 Tensioni: $\sigma_N=-5.02$ $\sigma_{m,d}=-22.64$ $\tau=29.94$ $\tau_{max}=29.94$ (sfrut=0.02)
 Tensioni: $\sigma_N=-5.02$ $\sigma_{m,d}=-314.90$ $\tau=0.73$ $\sigma_{ID,max}=319.92$ (sfrut=0.09)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $T_x=2490.17$
 $V,Ed=2490.17$ $V_c,Rd=59967.00$ $V,Ed/V_c,Rd=0.04$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: $N=46.56$ $T_x=2490.17$ $M_y=2377.60$
 $My,Ed=2377.60$ $My,V,c,Rd=14964.90$
 $N,Ed=46.56$ $Nc,Rd=207726.00$ YY $n=N,Ed/Nc,Rd=0.00$ $MNy,c,Rd=14964.90$ $My,Ed/MNy,c,Rd=0.16$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $M_y, Ed=2377.60$ $M_z, Ed=-0.00$ $L=0.20$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=2.55$ Ncr, $y=195939000.00$ $\lambda'_y=0.03$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=2.55$ Ncr, $z=195939000.00$ $\lambda'_z=0.03$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.18=0.18$
Verifica ZZ: $0.00+0.14=0.14$

Asta n. 204 (-21 -22) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND $Xl=0.00$ - Classe 3
Sollecitazioni: $N=-210.93$ $T_x=636.76$ $M_y=939.00$ $T_y=-65.49$ $M_z=74.10$ $M_x=-4.32$
Tensioni: $\sigma_N=-3.43$ $\sigma_{m,d}=-267.91$ $\tau=0.73$ $\sigma_{max}=-271.35$ (sfrut=0.08)
Tensioni: $\sigma_N=-3.43$ $\sigma_{m,d}=-18.03$ $\tau=24.03$ $\tau_{max}=24.03$ (sfrut=0.01)
Tensioni: $\sigma_N=-3.43$ $\sigma_{m,d}=-267.91$ $\tau=0.73$ $\sigma_{ID,max}=271.35$ (sfrut=0.08)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=0.00$ - Classe 1
Sollecitazioni: $T_x=1860.28$
 $V, Ed=1860.28$ $V_c, Rd=59967.00$ $V, Ed/V_c, Rd=0.03$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $Xl=0.00$ - Classe 1
Sollecitazioni: $N=46.56$ $T_x=1860.28$ $M_y=1880.82$
 $M_y, Ed=1880.82$ $M_y, V, c, Rd=14964.90$
 $N, Ed=46.56$ $N_c, Rd=207726.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=14964.90$ $M_y, Ed/MNy, c, Rd=0.13$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $M_y, Ed=1880.82$ $M_z, Ed=-0.00$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ Ncr, $y=4395380.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr, $z=4395380.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.14=0.14$
Verifica ZZ: $0.00+0.11=0.11$

Asta n. 204 (-22 -23) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND $Xl=1.34$ - Classe 3
Sollecitazioni: $N=49.87$ $T_x=56.16$ $M_y=-317.87$ $T_y=73.89$ $M_z=143.19$ $M_x=14.41$
Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=121.93$ $\tau=2.44$ $\sigma_{max}=122.74$ (sfrut=0.04)
Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=77.34$ $\tau=5.15$ $\tau_{max}=5.15$ (sfrut=0.00)
Tensioni: $\sigma_N=0.81$ $\sigma_{m,d}=121.93$ $\tau=2.44$ $\sigma_{ID,max}=122.81$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=0.00$ - Classe 1
Sollecitazioni: $T_x=656.48$
 $V, Ed=656.48$ $V_c, Rd=59967.00$ $V, Ed/V_c, Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $Xl=1.34$ - Classe 1
Sollecitazioni: $N=46.56$ $T_x=572.76$ $M_y=-1368.04$
 $M_y, Ed=-1368.04$ $M_y, V, c, Rd=14964.90$
 $N, Ed=46.56$ $N_c, Rd=207726.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=14964.90$ $M_y, Ed/MNy, c, Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $M_y, Ed=-1368.04$ $M_z, Ed=-0.00$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ Ncr, $y=4395360.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr, $z=4395360.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.10=0.10$
Verifica ZZ: $0.00+0.08=0.08$

Asta n. 204 (-23 -24) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND $Xl=0.00$ - Classe 3
Sollecitazioni: $N=6.55$ $T_x=-159.88$ $M_y=-317.88$ $T_y=70.52$ $M_z=-143.19$ $M_x=-14.41$
Tensioni: $\sigma_N=0.11$ $\sigma_{m,d}=121.93$ $\tau=2.44$ $\sigma_{max}=122.04$ (sfrut=0.04)
Tensioni: $\sigma_N=0.11$ $\sigma_{m,d}=-34.84$ $\tau=8.29$ $\tau_{max}=8.29$ (sfrut=0.00)
Tensioni: $\sigma_N=0.11$ $\sigma_{m,d}=121.93$ $\tau=2.44$ $\sigma_{ID,max}=122.11$ (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=1.34$ - Classe 1
Sollecitazioni: $T_x=-631.05$
 $V, Ed=-631.05$ $V_c, Rd=59967.00$ $V, Ed/V_c, Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $Xl=0.00$ - Classe 1
Sollecitazioni: $N=46.56$ $T_x=-547.32$ $M_y=-1368.08$
 $M_y, Ed=-1368.08$ $M_y, V, c, Rd=14964.90$
 $N, Ed=46.56$ $N_c, Rd=207726.00$ YY $n=N, Ed/N_c, Rd=0.00$ $MNy, c, Rd=14964.90$ $M_y, Ed/MNy, c, Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: $M_y, Ed=-317.88$ $M_z, Ed=-143.19$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ Ncr, $y=4395380.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr, $z=4395380.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.02+0.01=0.03$

Asta n. 204 (-24 -25) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND $Xl=1.34$ - Classe 3
Sollecitazioni: $N=-176.28$ $T_x=-631.67$ $M_y=899.56$ $T_y=64.48$ $M_z=71.39$ $M_x=-4.32$
Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-256.77$ $\tau=0.73$ $\sigma_{max}=-259.64$ (sfrut=0.08)
Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=17.37$ $\tau=23.84$ $\tau_{max}=23.84$ (sfrut=0.01)
Tensioni: $\sigma_N=-2.87$ $\sigma_{m,d}=-256.77$ $\tau=0.73$ $\sigma_{ID,max}=259.64$ (sfrut=0.08)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $Xl=1.34$ - Classe 1
Sollecitazioni: $T_x=-1834.85$
 $V, Ed=-1834.85$ $V_c, Rd=59967.00$ $V, Ed/V_c, Rd=0.03$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU $Xl=1.34$ - Classe 1
Sollecitazioni: $N=46.56$ $T_x=-1834.85$ $M_y=1812.89$

My,Ed=1812.89 My,V,c,Rd=14964.90
N,Ed=46.56 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.12

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: My,Ed=1812.89 Mz,Ed=0.00 L=1.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ Ncr,y=4395380.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395380.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.13=0.13
Verifica ZZ: 0.00+0.11=0.11

Asta n. 204 (-25 205) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.46 - Classe 3
Sollecitazioni: N=-309.81 T_x=-869.83 M_y=1293.44 T_y=-104.54 M_z=-119.34 M_x=4.32
Tensioni: $\sigma_{N}=-5.04$ $\sigma_{m,d}=-373.61$ $\tau=0.73$ $\sigma_{max}=-378.65$ (sfrut=0.11)
Tensioni: $\sigma_{N}=-5.04$ $\sigma_{m,d}=29.04$ $\tau=32.55$ $\tau_{max}=32.55$ (sfrut=0.02)
Tensioni: $\sigma_{N}=-5.04$ $\sigma_{m,d}=-373.61$ $\tau=0.73$ $\sigma_{TD,max}=378.65$ (sfrut=0.11)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.46 - Classe 1
Sollecitazioni: T_x=-2983.68
V,Ed=-2983.68 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.05
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.46 - Classe 1
Sollecitazioni: N=46.56 T_x=-2983.68 M_y=3174.75
My,Ed=3174.75 My,V,c,Rd=14964.90
N,Ed=46.56 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.21
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: My,Ed=3174.75 Mz,Ed=0.00 L=0.46
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.85$ Ncr,y=37254500.00 $\lambda'_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.85$ Ncr,z=37254500.00 $\lambda'_z=0.08$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.24=0.24
Verifica ZZ: 0.00+0.19=0.19

Asta n. 205 (205 -26) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-330.59 T_x=846.87 M_y=1329.57 T_y=-109.07 M_z=119.42 M_x=4.41
Tensioni: $\sigma_{N}=-5.38$ $\sigma_{m,d}=-383.18$ $\tau=0.75$ $\sigma_{max}=-388.56$ (sfrut=0.11)
Tensioni: $\sigma_{N}=-5.38$ $\sigma_{m,d}=29.05$ $\tau=31.73$ $\tau_{max}=31.73$ (sfrut=0.02)
Tensioni: $\sigma_{N}=-5.38$ $\sigma_{m,d}=-383.18$ $\tau=0.75$ $\sigma_{TD,max}=388.57$ (sfrut=0.11)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=3068.51
V,Ed=3068.51 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.05
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-212.25 T_x=3068.51 M_y=3746.46
My,Ed=3746.46 My,V,c,Rd=14964.90
N,Ed=-212.25 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.25
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-212.25 My,Ed=3746.46 Mz,Ed=0.00 L=0.88
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=11.17$ Ncr,y=10197800.00 $\lambda'_y=0.15$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=11.17$ Ncr,z=10197800.00 $\lambda'_z=0.15$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.28=0.28
Verifica ZZ: 0.00+0.22=0.22

Asta n. 205 (-26 -27) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-191.87 T_x=588.55 M_y=605.65 T_y=-67.46 M_z=23.79 M_x=4.40
Tensioni: $\sigma_{N}=-3.12$ $\sigma_{m,d}=-166.46$ $\tau=0.75$ $\sigma_{max}=-169.58$ (sfrut=0.05)
Tensioni: $\sigma_{N}=-3.12$ $\sigma_{m,d}=5.79$ $\tau=22.28$ $\tau_{max}=22.28$ (sfrut=0.01)
Tensioni: $\sigma_{N}=-3.12$ $\sigma_{m,d}=-166.46$ $\tau=0.75$ $\sigma_{TD,max}=169.58$ (sfrut=0.05)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=1893.47
V,Ed=1893.47 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU Xl=1.34 - Classe 1
Sollecitazioni: N=-212.25 T_x=1809.74 M_y=-1392.11
My,Ed=-1392.11 My,V,c,Rd=14964.90
N,Ed=-212.25 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.09
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-212.25 My,Ed=-1392.11 Mz,Ed=0.00 L=1.34
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ Ncr,y=4395360.00 $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ Ncr,z=4395360.00 $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.10=0.10
Verifica ZZ: 0.00+0.08=0.08

Asta n. 205 (-27 -28) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.34 - Classe 3
Sollecitazioni: N=-34.50 T_x=82.13 M_y=-526.59 T_y=80.44 M_z=328.35 M_x=-14.68
Tensioni: $\sigma_{N}=-0.56$ $\sigma_{m,d}=-226.09$ $\tau=2.49$ $\sigma_{max}=-226.65$ (sfrut=0.07)
Tensioni: $\sigma_{N}=-0.56$ $\sigma_{m,d}=-79.89$ $\tau=5.50$ $\tau_{max}=5.50$ (sfrut=0.00)
Tensioni: $\sigma_{N}=-0.56$ $\sigma_{m,d}=-226.09$ $\tau=2.49$ $\sigma_{TD,max}=226.69$ (sfrut=0.07)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=689.67
V,Ed=689.67 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=1.34 - Classe 1
Sollecitazioni: N=-212.25 T_x=605.94 M_y=-2257.09
My,Ed=-2257.09 My,V,c,Rd=14964.90
N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.15
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-212.25 My,Ed=-2257.09 Mz,Ed=0.00 L=1.34
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=17.02 Ncr,y=4395360.00 λ'_y=0.22 Curva a: Φ_y=0.53 χ_y=0.99
λ_z=17.02 Ncr,z=4395360.00 λ'_z=0.22 Curva a: Φ_z=0.53 χ_z=0.99
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.17=0.17
Verifica ZZ: 0.00+0.13=0.14
- Asta n. 205 (-28 -29) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 9 SND X1=0.00 - Classe 3
Sollecitazioni: N=-77.82 T_x=-133.91 M_y=-526.58 T_y=63.97 M_z=-328.35 M_x=14.68
Tensioni: σ_N=-1.27 σ_{m,d}=-226.09 τ=2.49 σ_{max}=-227.35 (sfrut=0.07)
Tensioni: σ_N=-1.27 σ_{m,d}=79.89 τ=7.39 τ_{max}=7.39 (sfrut=0.00)
Tensioni: σ_N=-1.27 σ_{m,d}=-226.09 τ=2.49 σ_{TD,max}=227.40 (sfrut=0.07)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.34 - Classe 1
Sollecitazioni: T_z=-597.86
V,Ed=-597.86 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: N=-212.25 T_x=-514.13 M_y=-2257.06
My,Ed=-2257.06 My,V,c,Rd=14964.90
N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.15
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-212.25 My,Ed=-2257.06 Mz,Ed=0.00 L=1.34
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=17.02 Ncr,y=4395380.00 λ'_y=0.22 Curva a: Φ_y=0.53 χ_y=0.99
λ_z=17.02 Ncr,z=4395380.00 λ'_z=0.22 Curva a: Φ_z=0.53 χ_z=0.99
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.17=0.17
Verifica ZZ: 0.00+0.13=0.14
- Asta n. 205 (-29 -30) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 15 SND X1=0.00 - Classe 3
Sollecitazioni: N=46.17 T_x=-339.79 M_y=-394.67 T_y=-208.39 M_z=242.92 M_x=-14.68
Tensioni: σ_N=0.75 σ_{m,d}=168.61 τ=2.49 σ_{max}=169.36 (sfrut=0.05)
Tensioni: σ_N=0.75 σ_{m,d}=59.10 τ=14.92 τ_{max}=14.92 (sfrut=0.01)
Tensioni: σ_N=0.75 σ_{m,d}=168.61 τ=2.49 σ_{TD,max}=169.42 (sfrut=0.05)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.34 - Classe 1
Sollecitazioni: T_z=-1801.66
V,Ed=-1801.66 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: N=-212.25 T_x=-1717.94 M_y=-1514.58
My,Ed=-1514.58 My,V,c,Rd=14964.90
N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.10
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-212.25 My,Ed=-1514.58 Mz,Ed=0.00 L=1.34
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=17.02 Ncr,y=4395380.00 λ'_y=0.22 Curva a: Φ_y=0.53 χ_y=0.99
λ_z=17.02 Ncr,z=4395380.00 λ'_z=0.22 Curva a: Φ_z=0.53 χ_z=0.99
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.11=0.11
Verifica ZZ: 0.00+0.09=0.09
- Asta n. 205 (-30 -31) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.88 - Classe 3
Sollecitazioni: N=-455.13 T_x=-824.35 M_y=1220.94 T_y=104.15 M_z=102.46 M_x=4.40
Tensioni: σ_N=-7.41 σ_{m,d}=-349.97 τ=0.75 σ_{max}=-357.38 (sfrut=0.11)
Tensioni: σ_N=-7.41 σ_{m,d}=-24.93 τ=30.90 τ_{max}=30.90 (sfrut=0.02)
Tensioni: σ_N=-7.41 σ_{m,d}=-349.97 τ=0.75 σ_{TD,max}=357.38 (sfrut=0.11)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.88 - Classe 1
Sollecitazioni: T_z=-2977.04
V,Ed=-2977.04 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.05
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=0.88 - Classe 1
Sollecitazioni: N=-212.25 T_x=-2977.04 M_y=3436.64
My,Ed=3436.64 My,V,c,Rd=14964.90
N,Ed=-212.25 Nc,Rd=-207726.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=14964.90 My,Ed/MNy,c,Rd=0.23
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: N,Ed=-212.25 My,Ed=3436.64 Mz,Ed=0.00 L=0.88
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=11.24 Ncr,y=10074800.00 λ'_y=0.15 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=11.24 Ncr,z=10074800.00 λ'_z=0.15 Curva a: Φ_z=0.00 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.26=0.26
Verifica ZZ: 0.00+0.20=0.21
- Asta n. 206 (-31 -32) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 5 SND X1=0.00 - Classe 3
Sollecitazioni: N=-192.43 T_x=881.68 M_y=1264.09 T_y=-86.63 M_z=102.33 M_x=9.58
Tensioni: σ_N=-3.13 σ_{m,d}=-361.35 τ=1.62 σ_{max}=-364.48 (sfrut=0.11)
Tensioni: σ_N=-3.13 σ_{m,d}=24.90 τ=33.87 τ_{max}=33.87 (sfrut=0.02)
Tensioni: σ_N=-3.13 σ_{m,d}=-361.35 τ=1.62 σ_{TD,max}=364.49 (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=2559.94$
 $V, Ed=2559.94$ $Vc, Rd=59967.00$ $V, Ed/Vc, Rd=0.04$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $N=192.51$ $T_x=2559.94$ $M_y=2542.05$
 $M_y, Ed=2542.05$ $M_y, V, c, Rd=14964.90$
 $N, Ed=192.51$ $Nc, Rd=207726.00$ YY $n=N, Ed/Nc, Rd=0.00$ $MNy, c, Rd=14964.90$ $M_y, Ed/MNy, c, Rd=0.17$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $M_y, Ed=2542.05$ $M_z, Ed=0.00$ $L=0.45$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=5.78$ $Ncr, y=38136200.00$ $\lambda'_y=0.08$ Curva a: $\Phi_y=0.00$ $\chi_y=1.00$
 $\lambda_z=5.78$ $Ncr, z=38136200.00$ $\lambda'_z=0.08$ Curva a: $\Phi_z=0.00$ $\chi_z=1.00$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.19=0.19$
Verifica ZZ: $0.00+0.15=0.15$
- Asta n. 206 (-32 -33) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 7 SND X1=0.00 - Classe 3
Sollecitazioni: $N=-58.97$ $T_x=643.77$ $M_y=869.38$ $T_y=46.59$ $M_z=-63.06$ $M_x=-9.57$
Tensioni: $\sigma_N=-0.96$ $\sigma_{m,d}=-246.58$ $\tau=1.62$ $\sigma_{max}=-247.54$ (sfrut=0.07)
Tensioni: $\sigma_N=-0.96$ $\sigma_{m,d}=15.34$ $\tau=25.17$ $\tau_{max}=25.17$ (sfrut=0.01)
Tensioni: $\sigma_N=-0.96$ $\sigma_{m,d}=-246.58$ $\tau=1.62$ $\sigma_{TD, max}=247.56$ (sfrut=0.07)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=1411.44$
 $V, Ed=1411.44$ $Vc, Rd=59967.00$ $V, Ed/Vc, Rd=0.02$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $N=192.51$ $T_x=1411.44$ $M_y=1388.07$
 $M_y, Ed=1388.07$ $M_y, V, c, Rd=14964.90$
 $N, Ed=192.51$ $Nc, Rd=207726.00$ YY $n=N, Ed/Nc, Rd=0.00$ $MNy, c, Rd=14964.90$ $M_y, Ed/MNy, c, Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
Sollecitazioni: $M_y, Ed=1388.07$ $M_z, Ed=0.00$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ $Ncr, y=4395360.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ $Ncr, z=4395360.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.10=0.10$
Verifica ZZ: $0.00+0.08=0.08$
- Asta n. 206 (-33 -34) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 5 SND X1=1.34 - Classe 3
Sollecitazioni: $N=85.44$ $T_x=298.92$ $M_y=-389.46$ $T_y=-3.27$ $M_z=-3.53$ $M_x=9.57$
Tensioni: $\sigma_N=1.39$ $\sigma_{m,d}=103.93$ $\tau=1.62$ $\sigma_{max}=105.32$ (sfrut=0.03)
Tensioni: $\sigma_N=1.39$ $\sigma_{m,d}=-0.86$ $\tau=12.56$ $\tau_{max}=12.56$ (sfrut=0.01)
Tensioni: $\sigma_N=1.39$ $\sigma_{m,d}=103.93$ $\tau=1.62$ $\sigma_{TD, max}=105.36$ (sfrut=0.03)
- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 5 SND X1=0.00 - Classe 1
Sollecitazioni: $T_y=-3.27$ $M_x=9.57$
 $V, Ed=-3.27$ $Vc, Rd, Red=59917.10$ $V, Ed/Vc, Rd, Red=0.00$
- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 5 SND X1=0.00 - Classe 1
Sollecitazioni: $T_x=363.32$ $M_x=9.57$
 $V, Ed=363.32$ $Vc, Rd, Red=59917.10$ $V, Ed/Vc, Rd, Red=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=1.34 - Classe 1
Sollecitazioni: $N=192.51$ $T_x=123.91$ $M_y=-662.23$
 $M_y, Ed=-662.23$ $M_y, V, c, Rd=14964.90$
 $N, Ed=192.51$ $Nc, Rd=207726.00$ YY $n=N, Ed/Nc, Rd=0.00$ $MNy, c, Rd=14964.90$ $M_y, Ed/MNy, c, Rd=0.04$
- Asta n. 206 (-34 -35) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.34 - Classe 3
Sollecitazioni: $N=-110.39$ $T_x=-581.39$ $M_y=851.21$ $T_y=40.06$ $M_z=49.96$ $M_x=9.57$
Tensioni: $\sigma_N=-1.80$ $\sigma_{m,d}=-238.31$ $\tau=1.62$ $\sigma_{max}=-240.11$ (sfrut=0.07)
Tensioni: $\sigma_N=-1.80$ $\sigma_{m,d}=-12.16$ $\tau=22.89$ $\tau_{max}=22.89$ (sfrut=0.01)
Tensioni: $\sigma_N=-1.80$ $\sigma_{m,d}=-238.31$ $\tau=1.62$ $\sigma_{TD, max}=240.13$ (sfrut=0.07)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.34 - Classe 1
Sollecitazioni: $T_x=-1079.89$
 $V, Ed=-1079.89$ $Vc, Rd=59967.00$ $V, Ed/Vc, Rd=0.02$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=1.34 - Classe 1
Sollecitazioni: $N=192.51$ $T_x=-1079.89$ $M_y=723.89$
 $M_y, Ed=723.89$ $M_y, V, c, Rd=14964.90$
 $N, Ed=192.51$ $Nc, Rd=207726.00$ YY $n=N, Ed/Nc, Rd=0.00$ $MNy, c, Rd=14964.90$ $M_y, Ed/MNy, c, Rd=0.05$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N, Ed=-110.39$ $M_y, Ed=851.21$ $M_z, Ed=49.96$ $L=1.34$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=17.02$ $Ncr, y=4395360.00$ $\lambda'_y=0.22$ Curva a: $\Phi_y=0.53$ $\chi_y=0.99$
 $\lambda_z=17.02$ $Ncr, z=4395360.00$ $\lambda'_z=0.22$ Curva a: $\Phi_z=0.53$ $\chi_z=0.99$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.06+0.00=0.07$
Verifica ZZ: $0.00+0.05+0.00=0.05$
- Asta n. 206 (-35 -36) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.54 - Classe 3
Sollecitazioni: $N=-244.94$ $T_x=-823.50$ $M_y=1289.38$ $T_y=80.42$ $M_z=93.44$ $M_x=9.57$
Tensioni: $\sigma_N=-3.99$ $\sigma_{m,d}=-365.69$ $\tau=1.62$ $\sigma_{max}=-369.67$ (sfrut=0.11)
Tensioni: $\sigma_N=-3.99$ $\sigma_{m,d}=-22.73$ $\tau=31.75$ $\tau_{max}=31.75$ (sfrut=0.02)
Tensioni: $\sigma_N=-3.99$ $\sigma_{m,d}=-365.69$ $\tau=1.62$ $\sigma_{TD, max}=369.69$ (sfrut=0.11)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.54 - Classe 1
Sollecitazioni: $T_x=-2233.86$

V,Ed=-2233.86 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.04

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 29 SLU X1=0.54 - Classe 1
Sollecitazioni: N=192.51 T_z=-2233.86 M_y=1922.46
M_y,Ed=1922.46 M_y,V,c,Rd=14964.90
N,Ed=192.51 Nc,Rd=207726.00 YY n=N,Ed/Nc,Rd=0.00 MN_y,c,Rd=14964.90 M_y,Ed/MN_y,c,Rd=0.13

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-244.94 M_y,Ed=1289.38 M_z,Ed=93.44 L=0.54
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=6.89 Ncr,y=26811000.00 λ'_y=0.09 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=6.89 Ncr,z=26811000.00 λ'_z=0.09 Curva a: Φ_z=0.00 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.10+0.01=0.10
Verifica ZZ: 0.00+0.08+0.01=0.08

Asta n. 206 (-36 -37) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND X1=0.00 - Classe 3
Sollecitazioni: N=69.78 T_z=470.88 M_y=605.09 T_y=-232.61 M_z=311.59
Tensioni: σ_N=1.14 σ_{m,d}=242.41 τ=0.00 σ_{max}=243.55 (sfrut=0.07)
Tensioni: σ_N=1.14 σ_{m,d}=75.81 τ=17.23 τ_{max}=17.23 (sfrut=0.01)
Tensioni: σ_N=1.14 σ_{m,d}=242.41 τ=0.00 σ_{ID,max}=243.55 (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: T_z=1870.97
V,Ed=1870.97 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.03

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: T_z=1870.97 M_y=2347.31
M_y,Ed=2347.31 M_y,V,c,Rd=14964.90 M_y,Ed/M_y,V,c,Rd=0.16

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 15 SND - Classe 3
Sollecitazioni: N,Ed=-69.78 M_y,Ed=605.09 M_z,Ed=-311.59 L=0.79
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=10.13 Ncr,y=12411000.00 λ'_y=0.13 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=10.13 Ncr,z=12411000.00 λ'_z=0.13 Curva a: Φ_z=0.00 χ_z=1.00
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.02=0.07
Verifica ZZ: 0.00+0.04+0.02=0.06

Asta n. 206 (-37 -38) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND X1=0.00 - Classe 3
Sollecitazioni: N=28.47 T_z=216.51 M_y=246.11 T_y=-94.91 M_z=126.73
Tensioni: σ_N=0.46 σ_{m,d}=98.60 τ=0.00 σ_{max}=99.06 (sfrut=0.03)
Tensioni: σ_N=0.46 σ_{m,d}=30.83 τ=7.92 τ_{max}=7.92 (sfrut=0.00)
Tensioni: σ_N=0.46 σ_{m,d}=98.60 τ=0.00 σ_{ID,max}=99.06 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: T_z=701.07
V,Ed=701.07 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: T_z=701.07 M_y=880.24
M_y,Ed=880.24 M_y,V,c,Rd=14964.90 M_y,Ed/M_y,V,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 11 SND - Classe 3
Sollecitazioni: N,Ed=-28.47 M_y,Ed=246.11 M_z,Ed=126.73 L=1.34
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=17.02 Ncr,y=4395390.00 λ'_y=0.22 Curva a: Φ_y=0.53 χ_y=0.99
λ_z=17.02 Ncr,z=4395390.00 λ'_z=0.22 Curva a: Φ_z=0.53 χ_z=0.99
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 301 (-3 -60) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: N=-6.80 T_z=76.05 M_y=65.99 T_y=-22.66 M_z=33.98
Tensioni: σ_N=-0.18 σ_{m,d}=-72.76 τ=0.00 σ_{max}=-72.94 (sfrut=0.02)
Tensioni: σ_N=-0.18 σ_{m,d}=24.27 τ=3.91 τ_{max}=3.91 (sfrut=0.00)
Tensioni: σ_N=-0.18 σ_{m,d}=-72.76 τ=0.00 σ_{ID,max}=72.94 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: T_z=308.68
V,Ed=308.68 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: T_z=308.68 M_y=301.91
M_y,Ed=301.91 M_y,V,c,Rd=6269.10 M_y,Ed/M_y,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-6.80 M_y,Ed=65.99 M_z,Ed=33.98 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.33 Ncr,y=1039280.00 λ'_y=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=37.85 Ncr,z=541779.00 λ'_z=0.50 Curva a: Φ_z=0.65 χ_z=0.93
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.01=0.02
Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 301 (-59 -3) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: N=6.80 T_z=-76.05 M_y=65.99 T_y=22.66 M_z=33.98
Tensioni: σ_N=0.18 σ_{m,d}=72.76 τ=0.00 σ_{max}=72.94 (sfrut=0.02)
Tensioni: σ_N=0.18 σ_{m,d}=24.27 τ=3.91 τ_{max}=3.91 (sfrut=0.00)
Tensioni: σ_N=0.18 σ_{m,d}=72.76 τ=0.00 σ_{ID,max}=72.94 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: T_z=-308.68

V,Ed=-308.68 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_z=-308.68 M_y=301.91
My,Ed=301.91 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.33 Ncr,y=1039280.00 λ'_y=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=37.85 Ncr,z=541779.00 λ'_z=0.50 Curva a: Φ_z=0.65 χ_z=0.93
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.01=0.02
Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 302 (-4 -47) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-10.19 T_z=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
Tensioni: σ_N=-0.27 σ_{m,d}=-109.06 τ=0.00 σ_{max}=-109.34 (sfrut=0.03)
Tensioni: σ_N=-0.27 σ_{m,d}=36.38 τ=5.55 τ_{max}=5.55 (sfrut=0.00)
Tensioni: σ_N=-0.27 σ_{m,d}=-109.06 τ=0.00 σ_{TD,max}=109.34 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=560.04
V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.33 Ncr,y=1039280.00 λ'_y=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=37.85 Ncr,z=541779.00 λ'_z=0.50 Curva a: Φ_z=0.65 χ_z=0.93
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 302 (-46 -4) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=10.19 T_z=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
Tensioni: σ_N=0.27 σ_{m,d}=109.06 τ=0.00 σ_{max}=109.34 (sfrut=0.03)
Tensioni: σ_N=0.27 σ_{m,d}=36.38 τ=5.55 τ_{max}=5.55 (sfrut=0.00)
Tensioni: σ_N=0.27 σ_{m,d}=109.06 τ=0.00 σ_{TD,max}=109.34 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_z=-560.04
V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_z=-560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.33 Ncr,y=1039280.00 λ'_y=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=37.85 Ncr,z=541779.00 λ'_z=0.50 Curva a: Φ_z=0.65 χ_z=0.93
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 303 (-6 -48) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-10.19 T_z=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
Tensioni: σ_N=-0.27 σ_{m,d}=-109.06 τ=0.00 σ_{max}=-109.34 (sfrut=0.03)
Tensioni: σ_N=-0.27 σ_{m,d}=36.38 τ=5.55 τ_{max}=5.55 (sfrut=0.00)
Tensioni: σ_N=-0.27 σ_{m,d}=-109.06 τ=0.00 σ_{TD,max}=109.34 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=560.04
V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
α_{my}, α_{mz}, α_{LT}=0.95, 0.95, 0.95
λ_y=27.33 Ncr,y=1039280.00 λ'_y=0.36 Curva a: Φ_y=0.58 χ_y=0.96
λ_z=37.85 Ncr,z=541779.00 λ'_z=0.50 Curva a: Φ_z=0.65 χ_z=0.93
K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 303 (-49 -6) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=10.19 T_z=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
Tensioni: σ_N=0.27 σ_{m,d}=109.06 τ=0.00 σ_{max}=109.34 (sfrut=0.03)
Tensioni: σ_N=0.27 σ_{m,d}=36.38 τ=5.55 τ_{max}=5.55 (sfrut=0.00)
Tensioni: σ_N=0.27 σ_{m,d}=109.06 τ=0.00 σ_{TD,max}=109.34 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_z=-560.04
V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $M_y,Ed=560.83$ $M_y,V,c,Rd=6269.10$ $M_y,Ed/My,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: $N,Ed=-10.19$ $M_y,Ed=98.92$ $M_z,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.01+0.01=0.03$
- Asta n. 304 (-7 -96) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=560.04$
 $V,Ed=560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $M_y,Ed=560.83$ $M_y,V,c,Rd=6269.10$ $M_y,Ed/My,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N,Ed=-10.19$ $M_y,Ed=98.92$ $M_z,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.01+0.01=0.03$
- Asta n. 304 (-95 -7) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-560.04$
 $V,Ed=-560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $M_y,Ed=560.83$ $M_y,V,c,Rd=6269.10$ $M_y,Ed/My,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: $N,Ed=-10.19$ $M_y,Ed=98.92$ $M_z,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.01+0.01=0.03$
- Asta n. 305 (-8 -66) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=560.04$
 $V,Ed=560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $M_y,Ed=560.83$ $M_y,V,c,Rd=6269.10$ $M_y,Ed/My,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N,Ed=-10.19$ $M_y,Ed=98.92$ $M_z,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.01+0.01=0.03$
- Asta n. 305 (-67 -8) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-560.04$
 $V,Ed=-560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.01+0.01=0.03$
- Asta n. 306 (-9 -69) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=560.04$
 $V,Ed=560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.01+0.01=0.03$
- Asta n. 306 (-68 -9) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-560.04$
 $V,Ed=-560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.01+0.01=0.03$
- Asta n. 307 (-11 -70) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=560.04$
 $V,Ed=560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
Verifica YY: $0.00+0.02+0.01=0.03$
Verifica ZZ: $0.00+0.01+0.01=0.03$
- Asta n. 307 (-71 -11) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
Sollecitazioni: $T_x=-560.04$
 $V,Ed=-560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $M_y, Ed=560.83$ $M_y, V, c, Rd=6269.10$ $M_y, Ed/My, V, c, Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N, Ed=-10.19$ $M_y, Ed=98.92$ $M_z, Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ $Ncr, y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr, z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 308 (-12 -72) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m, d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m, d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m, d}=-109.06$ $\tau=0.00$ $\sigma_{ID, max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=560.04$
 $V, Ed=560.04$ $Vc, Rd=43850.90$ $V, Ed/Vc, Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $M_y, Ed=560.83$ $M_y, V, c, Rd=6269.10$ $M_y, Ed/My, V, c, Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed=-10.19$ $M_y, Ed=98.92$ $M_z, Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ $Ncr, y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr, z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 308 (-73 -12) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
 Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=0.27$ $\sigma_{m, d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m, d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m, d}=109.06$ $\tau=0.00$ $\sigma_{ID, max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-560.04$
 $V, Ed=-560.04$ $Vc, Rd=43850.90$ $V, Ed/Vc, Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $M_y, Ed=560.83$ $M_y, V, c, Rd=6269.10$ $M_y, Ed/My, V, c, Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N, Ed=-10.19$ $M_y, Ed=98.92$ $M_z, Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ $Ncr, y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr, z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 309 (-13 -74) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=0.00$ - Classe 3
 Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m, d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m, d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m, d}=-109.06$ $\tau=0.00$ $\sigma_{ID, max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=560.04$
 $V, Ed=560.04$ $Vc, Rd=43850.90$ $V, Ed/Vc, Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X1=0.00$ - Classe 1
 Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $M_y, Ed=560.83$ $M_y, V, c, Rd=6269.10$ $M_y, Ed/My, V, c, Rd=0.09$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N, Ed=-10.19$ $M_y, Ed=98.92$ $M_z, Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ $Ncr, y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ $Ncr, z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 309 (-75 -13) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X1=1.50$ - Classe 3
 Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=0.27$ $\sigma_{m, d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m, d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m, d}=109.06$ $\tau=0.00$ $\sigma_{ID, max}=109.34$ (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-560.04$
 $V, Ed=-560.04$ $Vc, Rd=43850.90$ $V, Ed/Vc, Rd=0.01$
- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-560.04$ $M_y=560.83$

My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 310 (-14 -90) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-10.19 T_z=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=560.04
 V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 310 (-91 -14) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=10.19 T_z=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-560.04
 V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 311 (-15 -92) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-10.19 T_z=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=560.04
 V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 311 (-93 -15) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=10.19 T_z=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-560.04
 V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 312 (-16 -98) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=560.04
 V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 312 (-94 -16) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04
 V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 313 (-17 -97) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=560.04
 V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 313 (-42 -17) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04
 V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 314 (-18 -43) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=560.04
 V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 314 (-44 -18) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04
 V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 315 (-19 -45) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
 Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=560.04
 V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
 Sollecitazioni: T_x=560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 315 (-58 -19) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
 Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04
 V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 316 (-20 -63) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-6.80 T_z=76.05 M_y=65.99 T_y=-22.66 M_z=33.98
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.76$ $\tau=0.00$ $\sigma_{max}=-72.94$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=24.27$ $\tau=3.91$ $\tau_{max}=3.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.76$ $\tau=0.00$ $\sigma_{ID,max}=72.94$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=308.68
 V,Ed=308.68 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=308.68 M_y=301.91
 My,Ed=301.91 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 316 (-65 -20) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=6.80 T_z=-76.05 M_y=65.99 T_y=22.66 M_z=33.98
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.76$ $\tau=0.00$ $\sigma_{max}=72.94$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=24.27$ $\tau=3.91$ $\tau_{max}=3.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.76$ $\tau=0.00$ $\sigma_{ID,max}=72.94$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: T_z=-308.68
 V,Ed=-308.68 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: T_z=-308.68 M_y=301.91
 My,Ed=301.91 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 317 (-21 -51) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-6.80 T_z=76.05 M_y=65.99 T_y=-22.66 M_z=33.98
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.76$ $\tau=0.00$ $\sigma_{max}=-72.94$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=24.27$ $\tau=3.91$ $\tau_{max}=3.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.76$ $\tau=0.00$ $\sigma_{ID,max}=72.94$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=308.68
 V,Ed=308.68 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=308.68 M_y=301.91
 My,Ed=301.91 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=1.50
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

Asta n. 317 (-50 -21) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=6.80 T_z=-76.05 M_y=65.99 T_y=22.66 M_z=33.98
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.76$ $\tau=0.00$ $\sigma_{max}=72.94$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=24.27$ $\tau=3.91$ $\tau_{max}=3.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.76$ $\tau=0.00$ $\sigma_{ID,max}=72.94$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: T_z=-308.68
 V,Ed=-308.68 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1

Sollecitazioni: T_z=-308.68 M_y=301.91
 My,Ed=301.91 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.00+0.01+0.01=0.02$

Verifica ZZ: $0.00+0.01+0.01=0.02$

Asta n. 318 (-22 -53) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=-10.19 $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1

Sollecitazioni: $T_z=560.04$

$V_{Ed}=560.04$ $V_{c,Rd}=43850.90$ $V_{Ed}/V_{c,Rd}=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1

Sollecitazioni: $T_x=560.04$ $M_y=560.83$

$M_y,Ed=560.83$ $M_y,V,c,Rd=6269.10$ $M_y,Ed/M_y,V,c,Rd=0.09$

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 $M_y,Ed=98.92$ $M_z,Ed=50.94$ L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.00+0.02+0.01=0.03$

Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 318 (-52 -22) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3

Sollecitazioni: N=10.19 $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: $T_z=-560.04$

$V_{Ed}=-560.04$ $V_{c,Rd}=43850.90$ $V_{Ed}/V_{c,Rd}=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: $T_x=-560.04$ $M_y=560.83$

$M_y,Ed=560.83$ $M_y,V,c,Rd=6269.10$ $M_y,Ed/M_y,V,c,Rd=0.09$

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 $M_y,Ed=98.92$ $M_z,Ed=50.94$ L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.00+0.02+0.01=0.03$

Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 319 (-23 -55) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=-10.19 $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)

Tensioni: $\sigma_{N}=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1

Sollecitazioni: $T_z=560.04$

$V_{Ed}=560.04$ $V_{c,Rd}=43850.90$ $V_{Ed}/V_{c,Rd}=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1

Sollecitazioni: $T_x=560.04$ $M_y=560.83$

$M_y,Ed=560.83$ $M_y,V,c,Rd=6269.10$ $M_y,Ed/M_y,V,c,Rd=0.09$

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 $M_y,Ed=98.92$ $M_z,Ed=50.94$ L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: $0.00+0.02+0.01=0.03$

Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 319 (-54 -23) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3

Sollecitazioni: N=10.19 $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)

Tensioni: $\sigma_{N}=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: $T_z=-560.04$

$V_{Ed}=-560.04$ $V_{c,Rd}=43850.90$ $V_{Ed}/V_{c,Rd}=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: $T_x=-560.04$ $M_y=560.83$

$M_y,Ed=560.83$ $M_y,V,c,Rd=6269.10$ $M_y,Ed/M_y,V,c,Rd=0.09$

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 $M_y,Ed=98.92$ $M_z,Ed=50.94$ L=1.50

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 320 (-24 -57) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: $T_x=560.04$
 $V,Ed=560.04$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 320 (-56 -24) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: $T_x=-560.04$
 $V,Ed=-560.04$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 322 (-25 -41) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: $T_x=560.04$
 $V,Ed=560.04$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 322 (-64 -25) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{TD,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: $T_x=-560.04$
 $V,Ed=-560.04$ $V_c,Rd=43850.90$ $V,Ed/V_c,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 323 (-26 -77) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $T_x=560.04$
 $V,Ed=560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 323 (-76 -26) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=1.50$ - Classe 3
 Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-560.04$
 $V,Ed=-560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 324 (-27 -79) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=0.00$ - Classe 3
 Sollecitazioni: $N=-10.19$ $T_x=108.02$ $M_y=98.92$ $T_y=-33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $T_x=560.04$
 $V,Ed=560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_1=0.00$ - Classe 1
 Sollecitazioni: $T_x=560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: $0.00+0.02+0.01=0.03$
 Verifica ZZ: $0.00+0.01+0.01=0.03$

Asta n. 324 (-78 -27) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND $X_1=1.50$ - Classe 3
 Sollecitazioni: $N=10.19$ $T_x=-108.02$ $M_y=98.92$ $T_y=33.96$ $M_z=50.94$
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU $X_1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-560.04$
 $V,Ed=-560.04$ $Vc,Rd=43850.90$ $V,Ed/Vc,Rd=0.01$

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU $X_1=1.50$ - Classe 1
 Sollecitazioni: $T_x=-560.04$ $M_y=560.83$
 $My,Ed=560.83$ $My,V,c,Rd=6269.10$ $My,Ed/My,V,c,Rd=0.09$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: $N,Ed=-10.19$ $My,Ed=98.92$ $Mz,Ed=50.94$ $L=1.50$
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95 , 0.95
 $\lambda_y=27.33$ Ncr, $y=1039280.00$ $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr, $z=541779.00$ $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 325 (-28 -81) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =-109.06 τ =0.00 σ_{max} =-109.34 (sfrut=0.03)
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =36.38 τ =5.55 τ_{max} =5.55 (sfrut=0.00)
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =-109.06 τ =0.00 $\sigma_{ID,max}$ =109.34 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_x=560.04
 V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_x=560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96
 λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 325 (-80 -28) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =109.06 τ =0.00 σ_{max} =109.34 (sfrut=0.03)
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =36.38 τ =5.55 τ_{max} =5.55 (sfrut=0.00)
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =109.06 τ =0.00 $\sigma_{ID,max}$ =109.34 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04
 V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96
 λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 326 (-29 -83) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =-109.06 τ =0.00 σ_{max} =-109.34 (sfrut=0.03)
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =36.38 τ =5.55 τ_{max} =5.55 (sfrut=0.00)
 Tensioni: σ_N =-0.27 $\sigma_{m,d}$ =-109.06 τ =0.00 $\sigma_{ID,max}$ =109.34 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_x=560.04
 V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_x=560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96
 λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 326 (-82 -29) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =109.06 τ =0.00 σ_{max} =109.34 (sfrut=0.03)
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =36.38 τ =5.55 τ_{max} =5.55 (sfrut=0.00)
 Tensioni: σ_N =0.27 $\sigma_{m,d}$ =109.06 τ =0.00 $\sigma_{ID,max}$ =109.34 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04
 V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_x=-560.04 M_y=560.83
 My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , α_{LT} =0.95, 0.95, 0.95
 λ_y =27.33 Ncr,y=1039280.00 λ'_y =0.36 Curva a: Φ_y =0.58 χ_y =0.96
 λ_z =37.85 Ncr,z=541779.00 λ'_z =0.50 Curva a: Φ_z =0.65 χ_z =0.93
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 327 (-30 -85) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=560.04
V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 327 (-84 -30) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-560.04
V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 329 (-32 -86) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=560.04
V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 329 (-87 -32) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-560.04
V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 330 (-33 -89) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=-10.19 T_z=108.02 M_y=98.92 T_y=-33.96 M_z=50.94

Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)

Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)

Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1

Sollecitazioni: T_z=560.04

V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1

Sollecitazioni: T_z=560.04 M_y=560.83

My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 330 (-88 -33) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3

Sollecitazioni: N=10.19 T_z=-108.02 M_y=98.92 T_y=33.96 M_z=50.94

Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)

Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)

Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: T_z=-560.04

V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: T_z=-560.04 M_y=560.83

My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 331 (-34 -61) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=-10.19 T_z=108.02 M_y=98.92 T_y=-33.96 M_z=50.94

Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)

Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)

Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1

Sollecitazioni: T_z=560.04

V,Ed=560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1

Sollecitazioni: T_z=560.04 M_y=560.83

My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 331 (-62 -34) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3

Sollecitazioni: N=10.19 T_z=-108.02 M_y=98.92 T_y=33.96 M_z=50.94

Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)

Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)

Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: T_z=-560.04

V,Ed=-560.04 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1

Sollecitazioni: T_z=-560.04 M_y=560.83

My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3

Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50

α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95

$\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$

$\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.02+0.01=0.03

Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 332 (-35 -102) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=560.04
V_{Ed}=560.04 V_c,Rd=43850.90 V_{Ed}/V_c,Rd=0.01
 - Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 332 (-101 -35) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-560.04
V_{Ed}=-560.04 V_c,Rd=43850.90 V_{Ed}/V_c,Rd=0.01
 - Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 333 (-37 -103) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-10.19 T_x=108.02 M_y=98.92 T_y=-33.96 M_z=50.94
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{max}=-109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=-0.27$ $\sigma_{m,d}=-109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=560.04
V_{Ed}=560.04 V_c,Rd=43850.90 V_{Ed}/V_c,Rd=0.01
 - Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_x=560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 333 (-104 -37) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3
Sollecitazioni: N=10.19 T_x=-108.02 M_y=98.92 T_y=33.96 M_z=50.94
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{max}=109.34$ (sfrut=0.03)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=36.38$ $\tau=5.55$ $\tau_{max}=5.55$ (sfrut=0.00)
Tensioni: $\sigma_N=0.27$ $\sigma_{m,d}=109.06$ $\tau=0.00$ $\sigma_{ID,max}=109.34$ (sfrut=0.03)
 - Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-560.04
V_{Ed}=-560.04 V_c,Rd=43850.90 V_{Ed}/V_c,Rd=0.01
 - Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU Xl=1.50 - Classe 1
Sollecitazioni: T_x=-560.04 M_y=560.83
My,Ed=560.83 My,V,c,Rd=6269.10 My,Ed/My,V,c,Rd=0.09
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

Asta n. 334 (-38 -99) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3
 Sollecitazioni: N=-6.80 T_x=76.05 M_y=65.99 T_y=-22.66 M_z=33.98
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.76$ $\tau=0.00$ $\sigma_{max}=-72.94$ (sfrut=0.02)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=24.27$ $\tau=3.91$ $\tau_{max}=3.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=-0.18$ $\sigma_{m,d}=-72.76$ $\tau=0.00$ $\sigma_{TD,max}=72.94$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=308.67
 V_{Ed}=308.67 V_c,R_d=43850.90 V_{Ed}/V_c,R_d=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=0.00 - Classe 1
 Sollecitazioni: T_z=308.67 M_y=301.91
 M_y,Ed=301.91 M_y,V,c,R_d=6269.10 M_y,Ed/M_y,V,c,R_d=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-6.80 M_y,Ed=65.99 M_z,Ed=33.98 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy}, K_{yz}, K_{zy}, K<sub>zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02</sub>

Asta n. 334 (-100 -38) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3
 Sollecitazioni: N=6.80 T_x=-76.05 M_y=65.99 T_y=22.66 M_z=33.98
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.76$ $\tau=0.00$ $\sigma_{max}=72.94$ (sfrut=0.02)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=24.27$ $\tau=3.91$ $\tau_{max}=3.91$ (sfrut=0.00)
 Tensioni: $\sigma_N=0.18$ $\sigma_{m,d}=72.76$ $\tau=0.00$ $\sigma_{TD,max}=72.94$ (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-308.68
 V_{Ed}=-308.68 V_c,R_d=43850.90 V_{Ed}/V_c,R_d=0.01

- Verifica a flessione e taglio YY[4.2.32] - CC 29 SLU X1=1.50 - Classe 1
 Sollecitazioni: T_z=-308.68 M_y=301.91
 M_y,Ed=301.91 M_y,V,c,R_d=6269.10 M_y,Ed/M_y,V,c,R_d=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3
 Sollecitazioni: N,Ed=-6.80 M_y,Ed=65.99 M_z,Ed=33.98 L=1.50
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=27.33$ Ncr,y=1039280.00 $\lambda'_y=0.36$ Curva a: $\Phi_y=0.58$ $\chi_y=0.96$
 $\lambda_z=37.85$ Ncr,z=541779.00 $\lambda'_z=0.50$ Curva a: $\Phi_z=0.65$ $\chi_z=0.93$
 K_{yy}, K_{yz}, K_{zy}, K<sub>zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02</sub>

Membratura

Asta n. 201 (-3 -4 -5 -6 -7 -8 -9 -10) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: M_y,Ed=2542.07 M_z,Ed=0.00 L=7.13
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 K_{yy}, K_{yz}, K_{zy}, K<sub>zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.19=0.19
 Verifica ZZ: 0.00+0.15=0.15</sub>

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,c}=0.14$ (L/4969)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,t}=0.24$ (L/2982)

Membratura

Asta n. 202 (-10 -11 -12 -13 -14 -15 203) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-212.25 M_y,Ed=3746.45 M_z,Ed=0.00 L=7.10
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=90.50$ Ncr,y=155474.00 $\lambda'_y=1.18$ Curva a: $\Phi_y=1.30$ $\chi_y=0.54$
 $\lambda_z=90.50$ Ncr,z=155474.00 $\lambda'_z=1.18$ Curva a: $\Phi_z=1.30$ $\chi_z=0.54$
 K_{yy}, K_{yz}, K_{zy}, K<sub>zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.28=0.28
 Verifica ZZ: 0.00+0.22=0.22</sub>

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,c}=0.43$ (L/1635)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,t}=0.66$ (L/1076)

Membratura

Asta n. 203 (203 -16 -17 -18 -19 -20 204) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=46.56 M_y,Ed=3174.75 M_z,Ed=0.00 L=6.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 K_{yy}, K_{yz}, K_{zy}, K<sub>zz}=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.24=0.24
 Verifica ZZ: 0.00+0.19=0.19</sub>

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,c}=0.15$ (L/3959)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,t}=0.23$ (L/2608)

Membratura

Asta n. 204 (204 -21 -22 -23 -24 -25 205) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=46.56 My,Ed=3174.75 Mz,Ed=0.00 L=6.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.24=0.24
 Verifica ZZ: 0.00+0.19=0.19

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.15$ (L/3959)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.23$ (L/2608)

Membratura

Asta n. 205 (205 -26 -27 -28 -29 -30 -31) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: N,Ed=-212.25 My,Ed=3746.46 Mz,Ed=0.00 L=7.10
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=90.50$ Ncr,y=155474.00 $\lambda'_y=1.18$ Curva a: $\Phi_y=1.30$ $\chi_y=0.54$
 $\lambda_z=90.50$ Ncr,z=155474.00 $\lambda'_z=1.18$ Curva a: $\Phi_z=1.30$ $\chi_z=0.54$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.28=0.28
 Verifica ZZ: 0.00+0.22=0.22

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.43$ (L/1635)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.66$ (L/1076)

Membratura

Asta n. 206 (-31 -32 -33 -34 -35 -36 -37 -38) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 29 SLU - Classe 3
 Sollecitazioni: My,Ed=2542.05 Mz,Ed=0.00 L=7.13
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.19=0.19
 Verifica ZZ: 0.00+0.15=0.15

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.14$ (L/4967)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.24$ (L/2982)

Membratura

Asta n. 301 (-60 -3 -59) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.01+0.01=0.02
 Verifica ZZ: 0.00+0.01+0.01=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.04$ (L/7516)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.06$ (L/5231)

Membratura

Asta n. 302 (-47 -4 -46) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 303 (-48 -6 -49) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_y=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 304 (-96 -7 -95) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 305 (-66 -8 -67) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 306 (-69 -9 -68) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 307 (-70 -11 -71) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2812)

Membratura

Asta n. 308 (-72 -12 -73) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 309 (-74 -13 -75) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 310 (-90 -14 -91) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 311 (-92 -15 -93) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 312 (-98 -16 -94) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 313 (-97 -17 -42) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 314 (-43 -18 -44) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2812)

Membratura

Asta n. 315 (-45 -19 -58) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$



$\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 316 (-63 -20 -65) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.01=0.02
Verifica ZZ: 0.00+0.01+0.01=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.04$ (L/7516)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.06$ (L/5231)

Membratura

Asta n. 317 (-51 -21 -50) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.01=0.02
Verifica ZZ: 0.00+0.01+0.01=0.02

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.04$ (L/7516)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.06$ (L/5231)

Membratura

Asta n. 318 (-53 -22 -52) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 319 (-55 -23 -54) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2812)

Membratura

Asta n. 320 (-57 -24 -56) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 α_{my} , α_{mz} , $\alpha_{LT}=0.95$, 0.95, 0.95
 $\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2812)

Membratura

Asta n. 322 (-41 -25 -64) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 323 (-77 -26 -76) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2812)

Membratura

Asta n. 324 (-79 -27 -78) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 325 (-81 -28 -80) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 326 (-83 -29 -82) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03
- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)
- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 327 (-85 -30 -84) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03
Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2812)

Membratura

Asta n. 329 (-86 -32 -87) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 330 (-89 -33 -88) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 331 (-61 -34 -62) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3758)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 332 (-102 -35 -101) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 333 (-103 -37 -104) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-10.19 My,Ed=98.92 Mz,Ed=50.94 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$
 $\lambda_1=54.65$ Ncr,y=259820.00 $\lambda'_1=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_2=75.69$ Ncr,z=135445.00 $\lambda'_2=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
 Verifica YY: 0.00+0.02+0.01=0.03
 Verifica ZZ: 0.00+0.01+0.01=0.03

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.08$ (L/3759)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.11$ (L/2813)

Membratura

Asta n. 334 (-99 -38 -100) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
 Sollecitazioni: N,Ed=-6.80 My,Ed=65.99 Mz,Ed=33.98 L=3.00
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

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CODE

FOM.ENG.REL.005.00

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$\lambda_y=54.65$ Ncr, $y=259820.00$ $\lambda'_y=0.72$ Curva a: $\Phi_y=0.81$ $\chi_y=0.84$
 $\lambda_z=75.69$ Ncr, $z=135445.00$ $\lambda'_z=0.99$ Curva a: $\Phi_z=1.07$ $\chi_z=0.67$
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: $0.00+0.01+0.01=0.02$
Verifica ZZ: $0.00+0.01+0.01=0.02$

- Verifica freccia massima per soli carichi accidentali - CC 31
 $f_{z,1}=0.04$ (L/7516)

- Verifica freccia massima carichi totali - CC 31
 $f_{z,1}=0.06$ (L/5231)

6.4 Tracker 2x30 - configurazione in esercizio ($\alpha = 55^\circ$)

6.4.1 Diagrammi tassi di sfruttamento

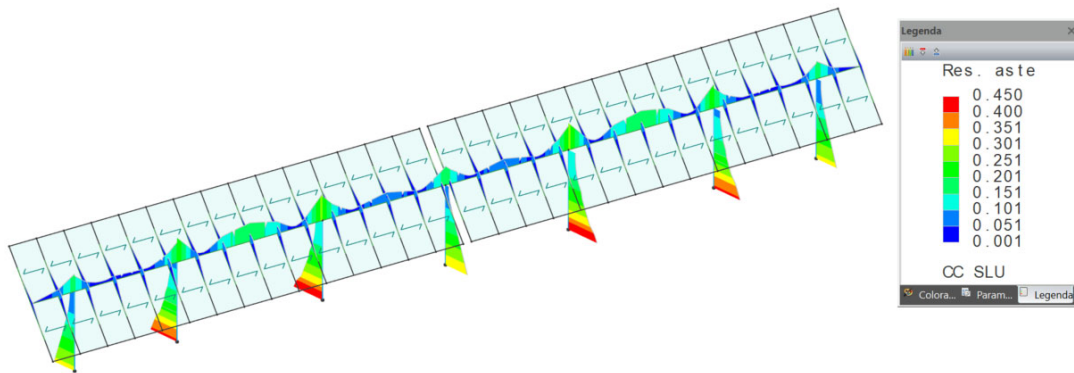


Diagramma tassi di sfruttamento resistenza aste combo SLU con valore massimo pari a 0,450

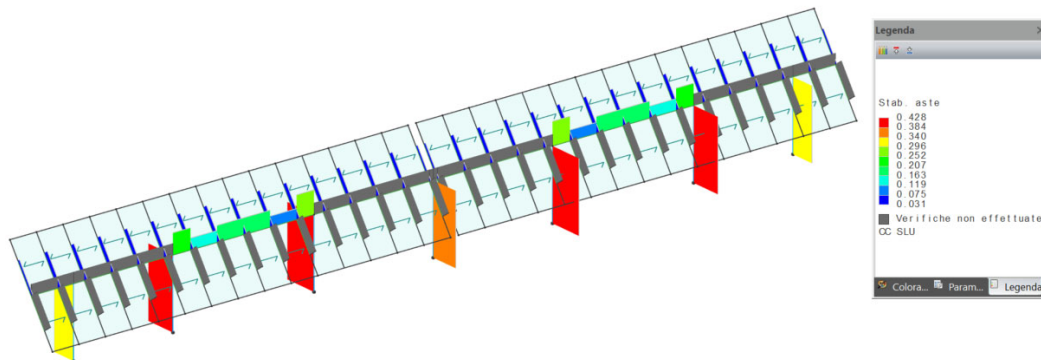


Diagramma tassi di sfruttamento stabilità aste combo SLU con valore massimo pari a 0,428

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

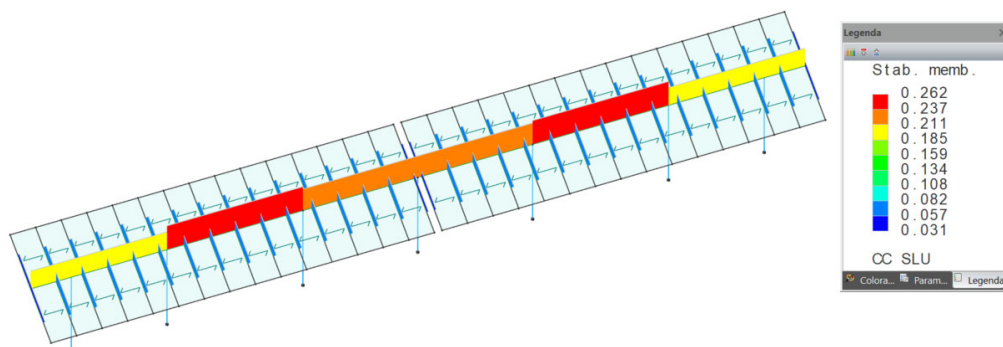


Diagramma tassi di sfruttamento stabilità membrature combo SLU con valore massimo pari a 0,262

Figure 32: Tassi di sfruttamento SLU (Stato limite ultimo)

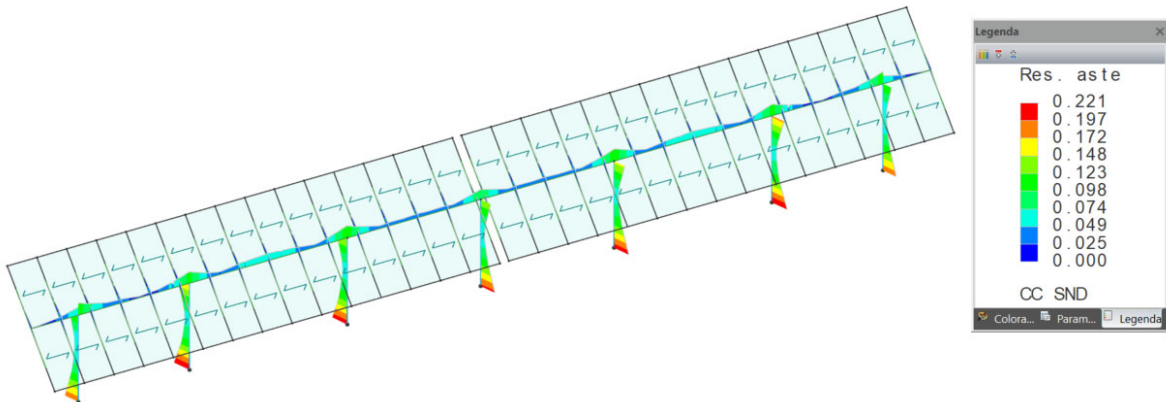


Diagramma tassi di sfruttamento resistenza aste combo SND con valore massimo pari a 0,221

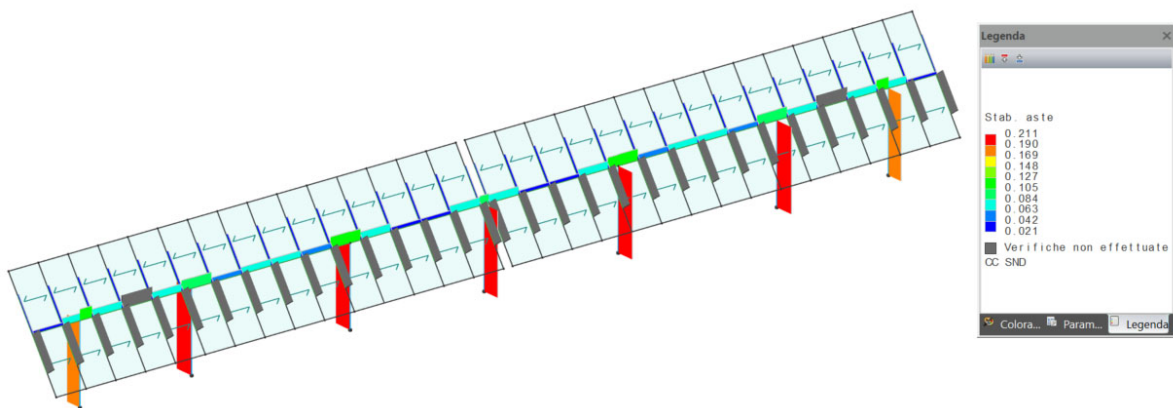


Diagramma tassi di sfruttamento stabilità aste combo SND con valore massimo pari a 0,211

(nota: la dicitura verifiche non effettuate si riferisce ad elementi non sollecitati per i quali non sono necessarie verifiche di stabilità)

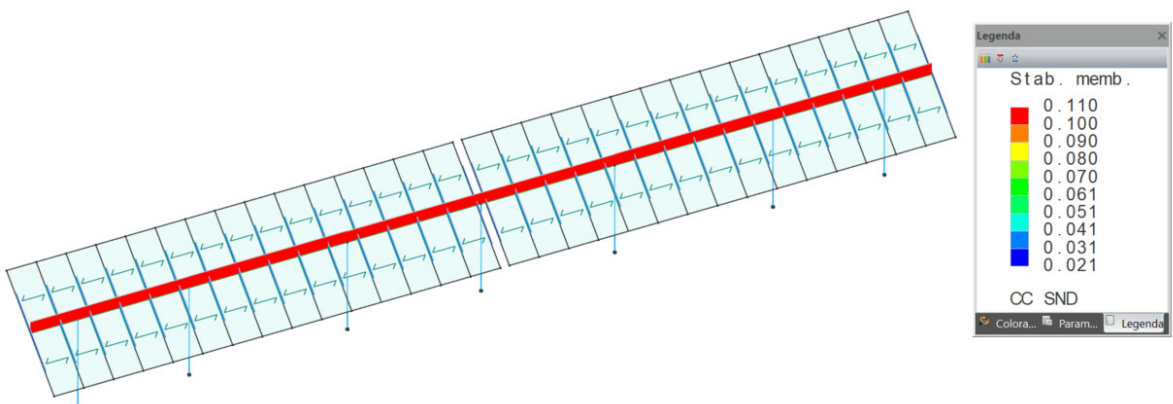
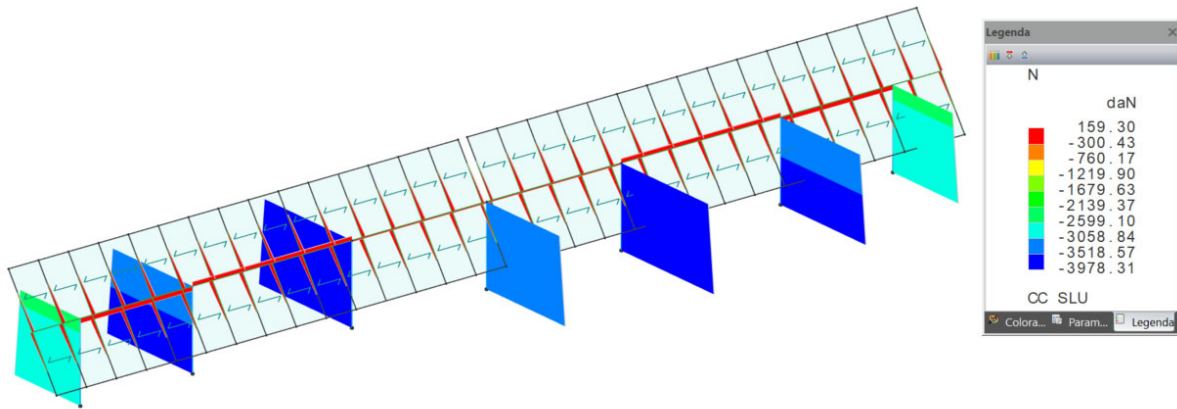


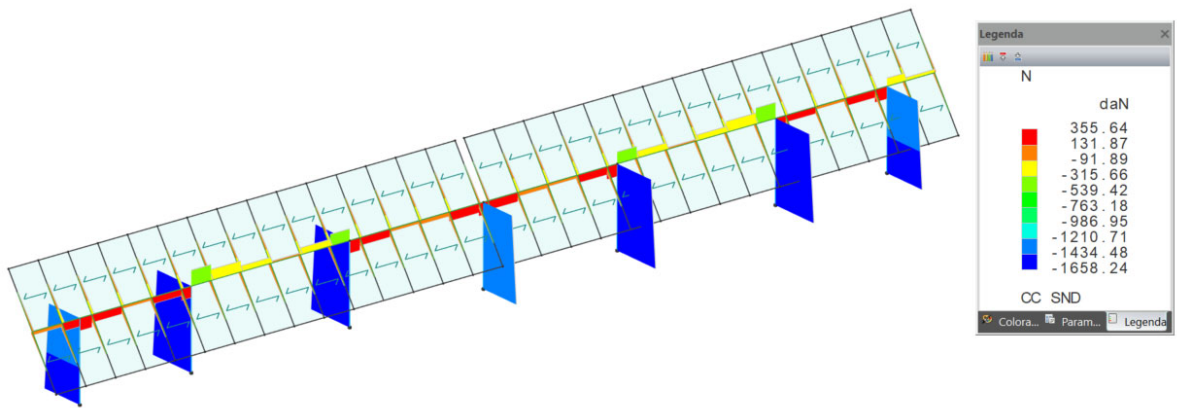
Diagramma tassi di sfruttamento stabilità membrature combo SND con valore massimo pari a 0,110

Figure 33: Tassi di sfruttamento SND (Stato limite di vita non dissipativo)

6.4.2 Sollecitazioni

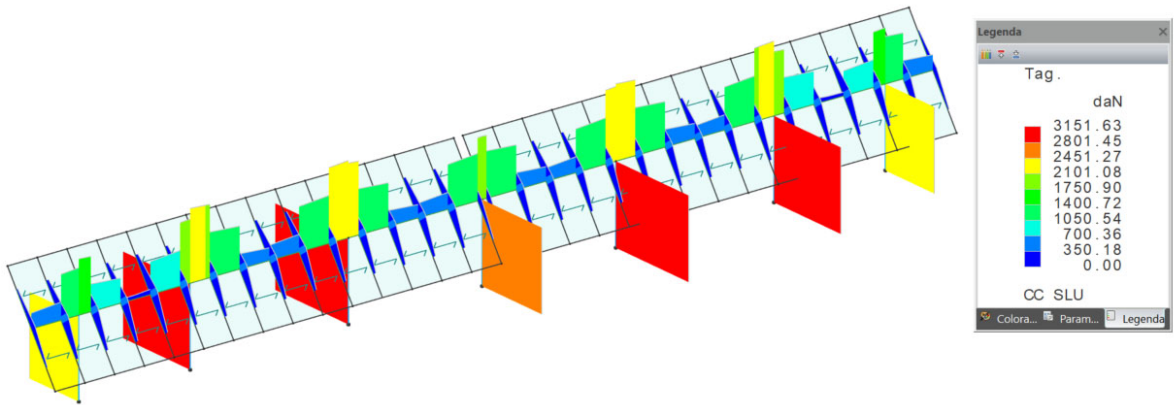


Involuppo sforzo normale SLU $N_{max} = 3978,31$ daN (compressione)

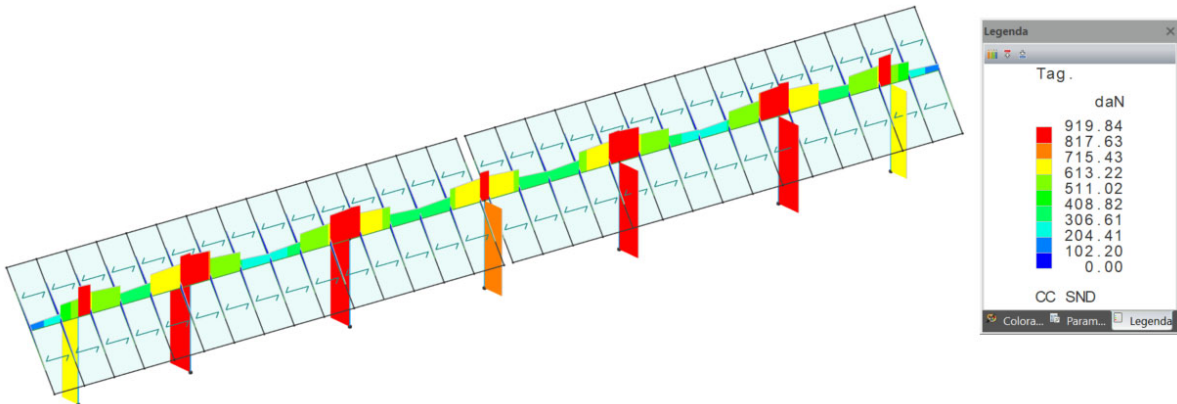


Involuppo sforzo normale SND $N_{max} = 1658,24$ daN (compressione)

Figure 34: Sforzo Normale

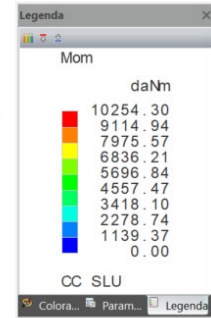
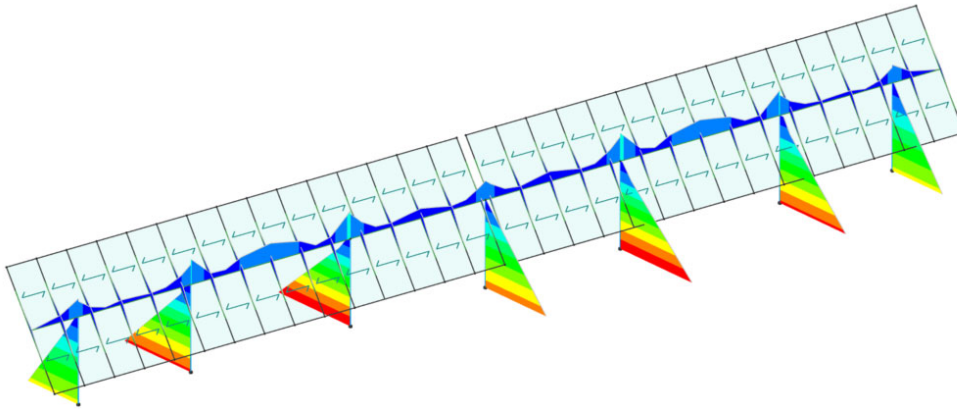


Involuppo sforzo di taglio SLU $T_{max} = 3151,63$ daN

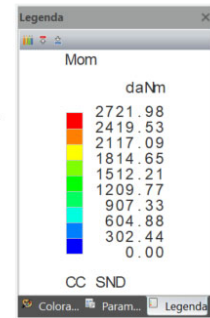
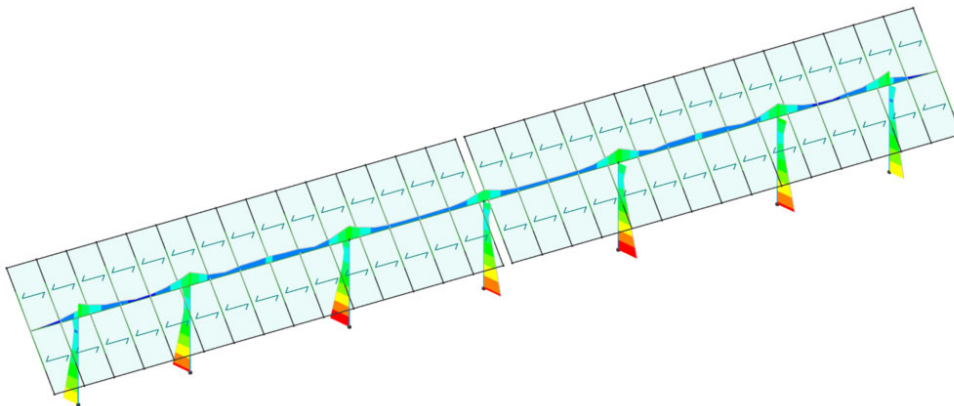


Involuppo sforzo di taglio SND $T_{max} = 919,84$ daN

Figure 35: Taglio



Inviluppo momento flettente SLU $M_{max} = 10254,30 \text{ daN}\times\text{m}$



Inviluppo momento flettente SND $M_{max} = 2721,98 \text{ daN}\times\text{m}$

Figure 36: Momento Flettente

6.4.3 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
 ModeSt ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
 Xfinest ver. 9.5.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18
 Tipo di calcolo: sismica statica
 Vincoli esterni: Considera sempre vincoli assegnati in modellazione
 Schematizzazione piani rigidi: nessun impalcato rigido
 Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Non sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
 - Calcolo sforzo nei nodi: No
 - Trascura deformabilità a taglio delle aste: No
 - Analisi dinamica con metodo di Lanczos: Sì
 - Check sequenza di Sturm: Sì
 - Analisi non lineare con Newton modificato: No
 - Usa formulazione secante per buckling: No
 - Trascura buckling torsionale: No
 - Opzioni aggiuntive per analisi non lineari in presenza di elementi bidimensionali con comportamento Drucker-Prager:
- ```
OPTION PARAM CONV=E
OPTION PARAM RESENNORM=1.E-8
OPTION PARAM AUTO_INCREMENT=YES
OPTION PARAM LINE_SEARCHES=YES
OPTION PARAM BGINCRS=1.0
OPTION PARAM AVINCRS=1.0
```

##### Dati struttura

- Sito di costruzione: CPHJ+42 Foggia FG, Italia LON. 15.73010 LAT. 41.42780  
 Contenuto tra ID reticolo: 30559 30558 30337 30336

##### Simbologia

Ag =Accelerazione orizzontale massima al sito  
 Cc =Coefficiente funzione della categoria del suolo  
 Fo =Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale  
 Ss =Coefficiente di amplificazione stratigrafica  
 Tr =Periodo di ritorno <anni>  
 TCC=Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
 SLD = Stato limite di danno  
 SND = Stato limite di salvaguardia della vita (non dissipativo)  
 Tc\*=Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

| TCC | Tr  | Ag<br><g> | Fo   | Tc*  | Ss   | Cc   |
|-----|-----|-----------|------|------|------|------|
| SLD | 50  | 0.0554    | 2.54 | 0.33 | 1.50 | 1.52 |
| SLV | 475 | 0.1323    | 2.61 | 0.43 | 1.49 | 1.38 |

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale V<sub>n</sub>: 50.00
- Classe d'uso: Classe II
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 5.26 <m>
- Altezza della struttura: 5.26 <m>
- Numero piani edificio: 0
- Coefficiente θ: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

##### Dati di calcolo

- Categoria del suolo di fondazione: C

- Tipologia strutturale: acciaio a mensola o a pendolo inverso

|                                                              |         |
|--------------------------------------------------------------|---------|
| Periodo $T_1$                                                | 0.29527 |
| Coeff. $\lambda$ SLD                                         | 1.00    |
| Coeff. $\lambda$ SLV                                         | 1.00    |
| Rapporto di sovrarresistenza ( $\alpha_w/\alpha_i$ )         | 1.00    |
| Valore di riferimento del fattore di comportamento ( $q_0$ ) | 1.00    |
| Fattore riduttivo ( $K_w$ )                                  | 1.00    |
| Fattore riduttivo regolarità in altezza (KR)                 | 1.00    |
| Fattore di comportamento dissipativo (q)                     | 1.00    |
| Fattore di comportamento non dissipativo (qND)               | 1.00    |
| Fattore di comportamento per SLD (qD)                        | 1.00    |

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media  $i \leq 15^\circ$
- Coeff. amplificazione topografica  $S_T$ : 1.00
- Accelerazione di picco del terreno  $A_g S$ : 0.1976 <g>
- Fattore di comportamento per sisma verticale (qv): 1.50
- Smorzamento spettro: 5.00%

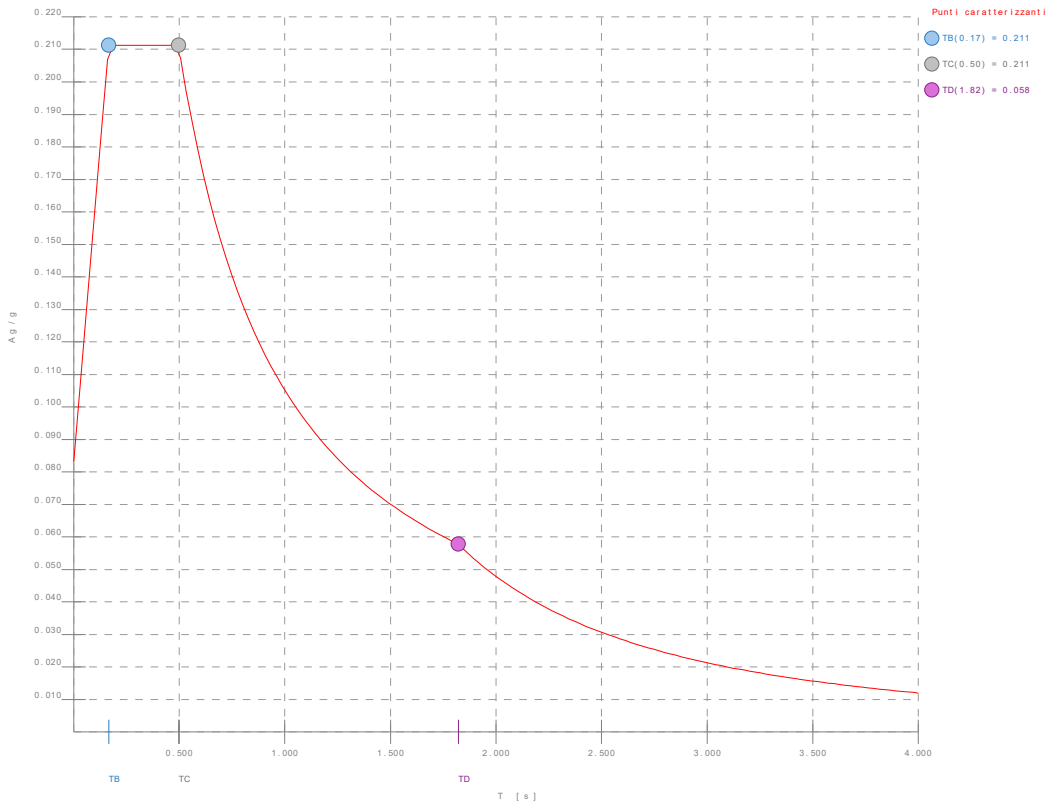


Figura numero 1: Spettro SLD

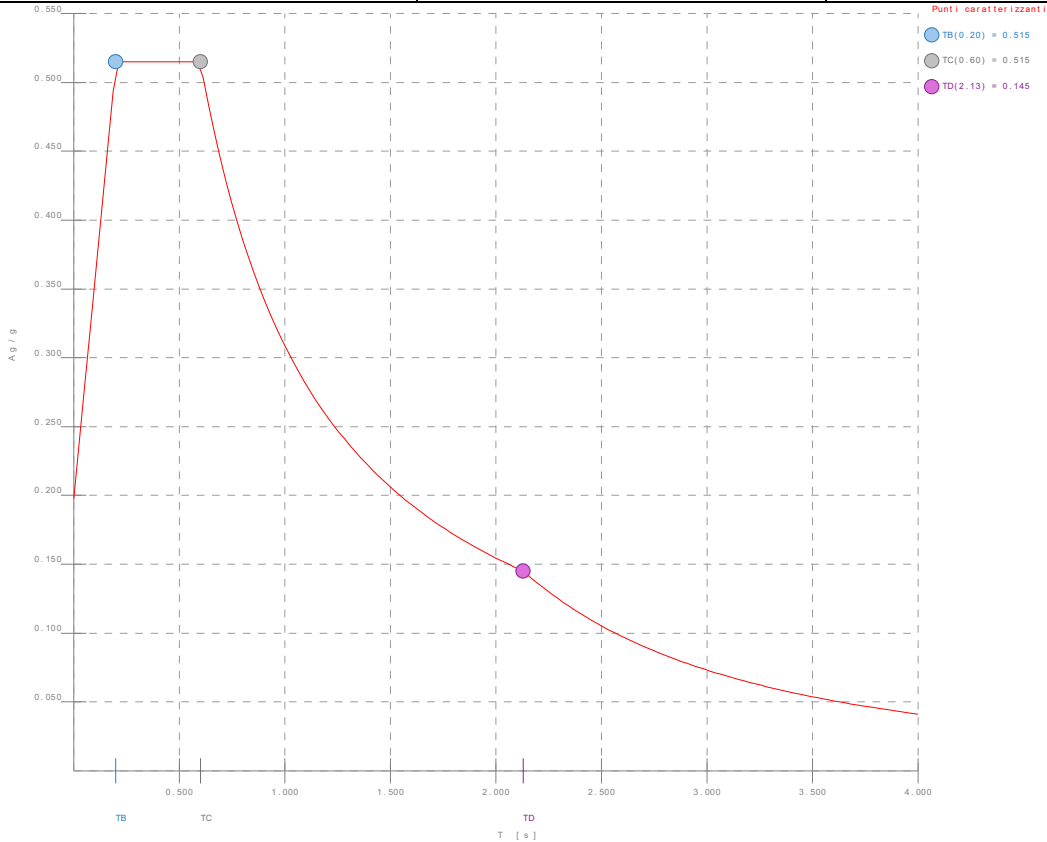


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>  
 - Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

- N = Numero
- Comm. = Commento
- 1 = G1 - Peso Proprio
- 2 = G2 - Permanenti non strutturali
- 3 = Q - Variabili neve
- 4 = Q - Vento retro Cond.A
- 5 = Q - Vento retro Cond.B
- 6 = Q - Vento fronte Cond.C
- 7 = Q - Vento fronte Cond.D
- F = azioni orizzontali convenzionali
- SLU = Stato limite ultimo
- SLR = Stato limite per combinazioni rare
- SLE F = Stato limite per combinazioni frequenti
- SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
- S = Si
- N = No

| NComm.            | 1 | 2 | 3 | 4 | 5 | 6 | 7 | S | SLU | SLR | SLE F | SLQ |
|-------------------|---|---|---|---|---|---|---|---|-----|-----|-------|-----|
| 1 Calcolo sismico | S | S | S | N | N | N | N | N | S   | N   | N     | N   |
| 2 Calcolo statico | S | S | S | N | N | N | N | S | S   | S   | S     | S   |
| 3 Vento cond A    | S | S | S | N | N | N | N | S | S   | S   | S     | S   |
| 4 Vento cond B    | S | S | S | N | N | N | N | S | S   | S   | S     | S   |
| 5 Vento cond C    | S | S | S | N | N | N | N | S | S   | S   | S     | S   |
| 6 Vento cond D    | S | S | S | N | N | N | N | S | S   | S   | S     | S   |

Elenco combinazioni di carico simboliche

Simbologia

- CC = Numero della combinazione delle condizioni di carico elementari
- Comm. = Commento
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

| CC | Comm.          | TCC   | 1     | 2     | 3                     | 4              | 5     | 6     | 7     | S     |
|----|----------------|-------|-------|-------|-----------------------|----------------|-------|-------|-------|-------|
| 1  | Amb. 1 (Sisma) | SLU   | S     | 1     | 1                     | ψ <sub>2</sub> | ----- | ----- | ----- | 1     |
| 2  | Amb. 2 (SLU)   | SLU   | γ max | γ max | γ max                 | -----          | ----- | ----- | ----- | ----- |
| 3  | Amb. 2 (SLE R) | SLE R | 1     | 1     | 1                     | -----          | ----- | ----- | ----- | ----- |
| 4  | Amb. 2 (SLE F) | SLE F | 1     | 1     | ψ <sub>1</sub>        | -----          | ----- | ----- | ----- | ----- |
| 5  | Amb. 2 (SLE Q) | SLE Q | 1     | 1     | ψ <sub>2</sub>        | -----          | ----- | ----- | ----- | ----- |
| 6  | Amb. 3 (SLU)   | SLU   | γ max | γ max | ψ <sub>0</sub> *γ max | γ max          | ----- | ----- | ----- | ----- |





|    |                |       |              |              |                       |                       |                       |       |                       |       |
|----|----------------|-------|--------------|--------------|-----------------------|-----------------------|-----------------------|-------|-----------------------|-------|
| 7  | Amb. 3 (SLU)   | SLU   | $\gamma$ max | $\gamma$ max | $\gamma$ max          | $\psi_0 * \gamma$ max | -----                 | ----- | -----                 | ----- |
| 8  | Amb. 3 (SLE R) | SLE R | 1            | 1            | $\psi_0$              | 1                     | -----                 | ----- | -----                 | ----- |
| 9  | Amb. 3 (SLE R) | SLE R | 1            | 1            | $\psi_0$              | 1                     | -----                 | ----- | -----                 | ----- |
| 10 | Amb. 3 (SLE F) | SLE F | 1            | 1            | $\psi_2$              | $\psi_1$              | -----                 | ----- | -----                 | ----- |
| 11 | Amb. 3 (SLE F) | SLE F | 1            | 1            | $\psi_1$              | $\psi_2$              | -----                 | ----- | -----                 | ----- |
| 12 | Amb. 3 (SLE Q) | SLE Q | 1            | 1            | $\psi_2$              | $\psi_2$              | -----                 | ----- | -----                 | ----- |
| 13 | Amb. 4 (SLU)   | SLU   | $\gamma$ max | $\gamma$ max | $\psi_0 * \gamma$ max | -----                 | $\gamma$ max          | ----- | -----                 | ----- |
| 14 | Amb. 4 (SLU)   | SLU   | $\gamma$ max | $\gamma$ max | $\gamma$ max          | -----                 | $\psi_0 * \gamma$ max | ----- | -----                 | ----- |
| 15 | Amb. 4 (SLE R) | SLE R | 1            | 1            | $\psi_0$              | 1                     | -----                 | ----- | -----                 | ----- |
| 16 | Amb. 4 (SLE R) | SLE R | 1            | 1            | $\psi_0$              | 1                     | -----                 | ----- | -----                 | ----- |
| 17 | Amb. 4 (SLE F) | SLE F | 1            | 1            | $\psi_2$              | -----                 | $\psi_1$              | ----- | -----                 | ----- |
| 18 | Amb. 4 (SLE F) | SLE F | 1            | 1            | $\psi_1$              | -----                 | $\psi_2$              | ----- | -----                 | ----- |
| 19 | Amb. 4 (SLE Q) | SLE Q | 1            | 1            | $\psi_2$              | -----                 | $\psi_2$              | ----- | -----                 | ----- |
| 20 | Amb. 5 (SLU)   | SLU   | $\gamma$ max | $\gamma$ max | $\psi_0 * \gamma$ max | -----                 | $\gamma$ max          | ----- | -----                 | ----- |
| 21 | Amb. 5 (SLU)   | SLU   | $\gamma$ max | $\gamma$ max | $\gamma$ max          | -----                 | $\psi_0 * \gamma$ max | ----- | -----                 | ----- |
| 22 | Amb. 5 (SLE R) | SLE R | 1            | 1            | $\psi_0$              | 1                     | -----                 | ----- | -----                 | ----- |
| 23 | Amb. 5 (SLE R) | SLE R | 1            | 1            | $\psi_0$              | 1                     | -----                 | ----- | -----                 | ----- |
| 24 | Amb. 5 (SLE F) | SLE F | 1            | 1            | $\psi_2$              | -----                 | $\psi_1$              | ----- | -----                 | ----- |
| 25 | Amb. 5 (SLE F) | SLE F | 1            | 1            | $\psi_1$              | -----                 | $\psi_2$              | ----- | -----                 | ----- |
| 26 | Amb. 5 (SLE Q) | SLE Q | 1            | 1            | $\psi_2$              | -----                 | $\psi_2$              | ----- | -----                 | ----- |
| 27 | Amb. 6 (SLU)   | SLU   | $\gamma$ max | $\gamma$ max | $\psi_0 * \gamma$ max | -----                 | -----                 | ----- | $\gamma$ max          | ----- |
| 28 | Amb. 6 (SLU)   | SLU   | $\gamma$ max | $\gamma$ max | $\gamma$ max          | -----                 | -----                 | ----- | $\psi_0 * \gamma$ max | ----- |
| 29 | Amb. 6 (SLE R) | SLE R | 1            | 1            | $\psi_0$              | 1                     | -----                 | ----- | -----                 | ----- |
| 30 | Amb. 6 (SLE R) | SLE R | 1            | 1            | $\psi_0$              | 1                     | -----                 | ----- | $\psi_0$              | ----- |
| 31 | Amb. 6 (SLE F) | SLE F | 1            | 1            | $\psi_2$              | -----                 | -----                 | ----- | $\psi_1$              | ----- |
| 32 | Amb. 6 (SLE F) | SLE F | 1            | 1            | $\psi_1$              | -----                 | -----                 | ----- | $\psi_2$              | ----- |
| 33 | Amb. 6 (SLE Q) | SLE Q | 1            | 1            | $\psi_2$              | -----                 | -----                 | ----- | $\psi_2$              | ----- |

Genera le combinazioni con un solo carico di tipo variabile come di base: S1

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

An. = Tipo di analisi

L = Lineare

NL = Non lineare

Bk = Buckling

S = Si

N = No

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

| CC | Comm.                    | TCC   | An. | Bk | 1    | 2    | 3    | 4    | 5    | 6    | 7    | S X   | S Y   |
|----|--------------------------|-------|-----|----|------|------|------|------|------|------|------|-------|-------|
| 1  | Amb. 1 (SLU S) S +X+0.3Y | SND   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00  | 0.30  |
| 2  | Amb. 1 (SLE) S +X+0.3Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00  | 0.30  |
| 3  | Amb. 1 (SLU S) S +X-0.3Y | SND   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00  | -0.30 |
| 4  | Amb. 1 (SLE) S +X-0.3Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00  | -0.30 |
| 5  | Amb. 1 (SLU S) S -X+0.3Y | SND   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -1.00 | 0.30  |
| 6  | Amb. 1 (SLE) S -X+0.3Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -1.00 | 0.30  |
| 7  | Amb. 1 (SLU S) S -X-0.3Y | SND   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -1.00 | -0.30 |
| 8  | Amb. 1 (SLE) S -X-0.3Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -1.00 | -0.30 |
| 9  | Amb. 1 (SLU S) S +0.3X+Y | SND   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.30  | 1.00  |
| 10 | Amb. 1 (SLE) S +0.3X+Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.30  | 1.00  |
| 11 | Amb. 1 (SLU S) S -0.3X+Y | SND   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.30 | 1.00  |
| 12 | Amb. 1 (SLE) S -0.3X+Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.30 | 1.00  |
| 13 | Amb. 1 (SLU S) S +0.3X-Y | SND   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.30  | -1.00 |
| 14 | Amb. 1 (SLE) S +0.3X-Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.30  | -1.00 |
| 15 | Amb. 1 (SLU S) S -0.3X-Y | SND   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.30 | -1.00 |
| 16 | Amb. 1 (SLE) S -0.3X-Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.30 | -1.00 |
| 17 | Amb. 2 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 1.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 18 | Amb. 2 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 19 | Amb. 2 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 20 | Amb. 2 (SLE Q)           | SLE Q | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 21 | Amb. 3 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 0.75 | 1.50 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 22 | Amb. 3 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 1.50 | 0.90 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 23 | Amb. 3 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 0.50 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 24 | Amb. 3 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 1.00 | 0.60 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 25 | Amb. 3 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.00 | 0.20 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 26 | Amb. 3 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 27 | Amb. 3 (SLE Q)           | SLE Q | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 28 | Amb. 4 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 0.75 | 0.00 | 1.50 | 0.00 | 0.00 | 0.00  | 0.00  |
| 29 | Amb. 4 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 1.50 | 0.90 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 30 | Amb. 4 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 0.50 | 0.00 | 1.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 31 | Amb. 4 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 1.00 | 0.60 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 32 | Amb. 4 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.20 | 0.00 | 0.00 | 0.00  | 0.00  |
| 33 | Amb. 4 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 34 | Amb. 4 (SLE Q)           | SLE Q | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 35 | Amb. 5 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 0.75 | 0.00 | 0.00 | 1.50 | 0.00 | 0.00  | 0.00  |
| 36 | Amb. 5 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 1.50 | 0.90 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 37 | Amb. 5 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 0.50 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00  | 0.00  |
| 38 | Amb. 5 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.60 | 0.00 | 0.00  | 0.00  |
| 39 | Amb. 5 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.20 | 0.00 | 0.00  | 0.00  |
| 40 | Amb. 5 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 41 | Amb. 5 (SLE Q)           | SLE Q | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  |
| 42 | Amb. 6 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 0.75 | 0.00 | 0.00 | 0.00 | 1.50 | 0.00  | 0.00  |
| 43 | Amb. 6 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 1.50 | 0.90 | 0.00 | 0.00 | 0.90 | 0.00  | 0.00  |
| 44 | Amb. 6 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 0.50 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00  | 0.00  |
| 45 | Amb. 6 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.60 | 0.00  | 0.00  |
| 46 | Amb. 6 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.20 | 0.00  | 0.00  |



|    |                |       |   |   |      |      |      |      |      |      |      |      |      |      |
|----|----------------|-------|---|---|------|------|------|------|------|------|------|------|------|------|
| 47 | Amb. 6 (SLE F) | SLE F | L | N | 1.00 | 1.00 | 0.20 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 48 | Amb. 6 (SLE Q) | SLE Q | L | N | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

Elenco masse nodi

Simbologia  
Mo = Massa orizzontale  
Nodo = Numero del nodo

| Nodo | Mo <kg> | Nodo | Mo <kg> | Nodo | Mo <kg> | Nodo | Mo <kg> | Nodo | Mo <kg> | Nodo | Mo <kg> | Nodo | Mo <kg> | Nodo | Mo <kg> | Nodo | Mo <kg> | Nodo | Mo <kg> |
|------|---------|------|---------|------|---------|------|---------|------|---------|------|---------|------|---------|------|---------|------|---------|------|---------|
| -104 | 67.23   | -103 | 67.23   | -102 | 67.23   | -101 | 67.23   | -100 | 44.85   | -99  | 44.85   | -98  | 67.23   | -97  | 67.23   | -96  | 67.23   | -95  | 67.23   |
| -93  | 67.23   | -92  | 67.23   | -91  | 67.23   | -90  | 67.23   | -89  | 67.23   | -88  | 67.23   | -87  | 67.23   | -86  | 67.23   | -85  | 67.23   | -84  | 67.23   |
| -82  | 67.23   | -81  | 67.23   | -80  | 67.23   | -79  | 67.23   | -78  | 67.23   | -77  | 67.23   | -76  | 67.23   | -75  | 67.23   | -74  | 67.23   | -73  | 67.23   |
| -71  | 67.23   | -70  | 67.23   | -69  | 67.23   | -68  | 67.23   | -67  | 67.23   | -66  | 67.23   | -65  | 44.85   | -64  | 67.23   | -63  | 44.85   | -62  | 67.23   |
| -60  | 44.85   | -59  | 44.85   | -58  | 67.23   | -57  | 67.23   | -56  | 67.23   | -55  | 67.23   | -54  | 67.23   | -53  | 67.23   | -52  | 67.23   | -51  | 44.85   |
| -49  | 67.23   | -48  | 67.23   | -47  | 67.23   | -46  | 67.23   | -45  | 67.23   | -44  | 67.23   | -43  | 67.23   | -42  | 67.23   | -41  | 67.23   | -38  | 98.18   |
| -36  | 129.28  | -35  | 131.89  | -34  | 151.43  | -33  | 151.43  | -32  | 129.75  | -31  | 129.28  | -30  | 140.28  | -29  | 151.43  | -28  | 151.43  | -27  | 151.43  |
| -25  | 129.88  | -24  | 151.43  | -23  | 151.43  | -22  | 151.43  | -21  | 103.10  | -20  | 103.10  | -19  | 151.43  | -18  | 151.43  | -17  | 151.43  | -16  | 129.88  |
| -14  | 151.43  | -13  | 151.43  | -12  | 151.43  | -11  | 140.28  | -10  | 129.28  | -9   | 129.75  | -8   | 151.43  | -7   | 151.43  | -6   | 131.89  | -5   | 129.28  |
| -3   | 98.18   | 203  | 129.28  | 204  | 106.28  | 205  | 129.28  |      |         |      |         |      |         |      |         |      |         |      |         |

Totali masse nodi

|      |         |
|------|---------|
| Mo   |         |
| <kg> | 9450.93 |

Elenco forze sismiche nodali allo SLD

Simbologia  
Fx = Forza in dir. X  
Fy = Forza in dir. Y  
Nodo = Numero del nodo  
cx = Coeff. c in dir. X  
cy = Coeff. c in dir. Y

| Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx | cy | Fx <daN> | Fy <daN> | Nodo | cx | cy | Fx <daN> | Fy <daN> |
|------|------|------|----------|----------|------|------|------|----------|----------|------|------|------|----------|----------|------|------|------|----------|----------|------|------|------|----------|----------|------|----|----|----------|----------|------|----|----|----------|----------|
| -104 | 0.01 | 0.01 | 19.13    | 19.13    | -103 | 0.00 | 0.00 | 8.75     | 8.75     | -102 | 0.00 | 0.00 | 8.75     | 8.75     | -101 | 0.01 | 0.01 | 19.13    | 19.13    | -100 | 0.01 | 0.01 | 12.76    | 12.76    |      |    |    |          |          |      |    |    |          |          |
| -99  | 0.00 | 0.00 | 5.84     | 5.84     | -98  | 0.00 | 0.00 | 8.75     | 8.75     | -97  | 0.00 | 0.00 | 8.75     | 8.75     | -96  | 0.00 | 0.00 | 8.75     | 8.75     | -95  | 0.01 | 0.01 | 19.13    | 19.13    |      |    |    |          |          |      |    |    |          |          |
| -94  | 0.01 | 0.01 | 19.13    | 19.13    | -93  | 0.01 | 0.01 | 19.13    | 19.13    | -92  | 0.00 | 0.00 | 8.75     | 8.75     | -91  | 0.01 | 0.01 | 19.13    | 19.13    | -90  | 0.00 | 0.00 | 8.75     | 8.75     |      |    |    |          |          |      |    |    |          |          |
| -89  | 0.00 | 0.00 | 8.75     | 8.75     | -88  | 0.01 | 0.01 | 19.13    | 19.13    | -87  | 0.01 | 0.01 | 19.13    | 19.13    | -86  | 0.00 | 0.00 | 8.75     | 8.75     | -85  | 0.00 | 0.00 | 8.75     | 8.75     |      |    |    |          |          |      |    |    |          |          |
| -84  | 0.01 | 0.01 | 19.13    | 19.13    | -83  | 0.00 | 0.00 | 8.75     | 8.75     | -82  | 0.01 | 0.01 | 19.13    | 19.13    | -81  | 0.00 | 0.00 | 8.75     | 8.75     | -80  | 0.01 | 0.01 | 19.13    | 19.13    |      |    |    |          |          |      |    |    |          |          |
| -79  | 0.00 | 0.00 | 8.75     | 8.75     | -78  | 0.01 | 0.01 | 19.13    | 19.13    | -77  | 0.00 | 0.00 | 8.75     | 8.75     | -76  | 0.01 | 0.01 | 19.13    | 19.13    | -75  | 0.01 | 0.01 | 19.13    | 19.13    |      |    |    |          |          |      |    |    |          |          |
| -74  | 0.00 | 0.00 | 8.75     | 8.75     | -73  | 0.01 | 0.01 | 19.13    | 19.13    | -72  | 0.00 | 0.00 | 8.75     | 8.75     | -71  | 0.01 | 0.01 | 19.13    | 19.13    | -70  | 0.00 | 0.00 | 8.75     | 8.75     |      |    |    |          |          |      |    |    |          |          |
| -69  | 0.00 | 0.00 | 8.75     | 8.75     | -68  | 0.01 | 0.01 | 19.13    | 19.13    | -67  | 0.01 | 0.01 | 19.13    | 19.13    | -66  | 0.00 | 0.00 | 8.75     | 8.75     | -65  | 0.01 | 0.01 | 12.76    | 12.76    |      |    |    |          |          |      |    |    |          |          |
| -64  | 0.01 | 0.01 | 19.13    | 19.13    | -63  | 0.00 | 0.00 | 5.84     | 5.84     | -62  | 0.01 | 0.01 | 19.13    | 19.13    | -61  | 0.00 | 0.00 | 8.75     | 8.75     | -60  | 0.00 | 0.00 | 5.84     | 5.84     |      |    |    |          |          |      |    |    |          |          |
| -59  | 0.01 | 0.01 | 12.76    | 12.76    | -58  | 0.01 | 0.01 | 19.13    | 19.13    | -57  | 0.00 | 0.00 | 8.75     | 8.75     | -56  | 0.01 | 0.01 | 19.13    | 19.13    | -55  | 0.00 | 0.00 | 8.75     | 8.75     |      |    |    |          |          |      |    |    |          |          |
| -54  | 0.01 | 0.01 | 19.13    | 19.13    | -53  | 0.00 | 0.00 | 8.75     | 8.75     | -52  | 0.01 | 0.01 | 19.13    | 19.13    | -51  | 0.00 | 0.00 | 5.84     | 5.84     | -50  | 0.01 | 0.01 | 12.76    | 12.76    |      |    |    |          |          |      |    |    |          |          |
| -49  | 0.01 | 0.01 | 19.13    | 19.13    | -48  | 0.00 | 0.00 | 8.75     | 8.75     | -47  | 0.00 | 0.00 | 8.75     | 8.75     | -46  | 0.01 | 0.01 | 19.13    | 19.13    | -45  | 0.00 | 0.00 | 8.75     | 8.75     |      |    |    |          |          |      |    |    |          |          |
| -44  | 0.01 | 0.01 | 19.13    | 19.13    | -43  | 0.00 | 0.00 | 8.75     | 8.75     | -42  | 0.01 | 0.01 | 19.13    | 19.13    | -41  | 0.00 | 0.00 | 8.75     | 8.75     | -38  | 0.01 | 0.01 | 20.35    | 20.35    |      |    |    |          |          |      |    |    |          |          |
| -37  | 0.01 | 0.01 | 28.64    | 28.64    | -36  | 0.01 | 0.01 | 26.80    | 26.80    | -35  | 0.01 | 0.01 | 27.34    | 27.34    | -34  | 0.02 | 0.02 | 31.39    | 31.39    | -33  | 0.02 | 0.02 | 31.39    | 31.39    |      |    |    |          |          |      |    |    |          |          |
| -32  | 0.01 | 0.01 | 26.90    | 26.90    | -31  | 0.01 | 0.01 | 26.80    | 26.80    | -30  | 0.01 | 0.01 | 29.08    | 29.08    | -29  | 0.02 | 0.02 | 31.39    | 31.39    | -28  | 0.02 | 0.02 | 31.39    | 31.39    |      |    |    |          |          |      |    |    |          |          |
| -27  | 0.02 | 0.02 | 31.39    | 31.39    | -26  | 0.01 | 0.01 | 29.05    | 29.05    | -25  | 0.01 | 0.01 | 26.92    | 26.92    | -24  | 0.02 | 0.02 | 31.39    | 31.39    | -23  | 0.02 | 0.02 | 31.39    | 31.39    |      |    |    |          |          |      |    |    |          |          |
| -22  | 0.02 | 0.02 | 31.39    | 31.39    | -21  | 0.01 | 0.01 | 21.37    | 21.37    | -20  | 0.01 | 0.01 | 21.37    | 21.37    | -19  | 0.02 | 0.02 | 31.39    | 31.39    | -18  | 0.02 | 0.02 | 31.39    | 31.39    |      |    |    |          |          |      |    |    |          |          |
| -17  | 0.02 | 0.02 | 31.39    | 31.39    | -16  | 0.01 | 0.01 | 26.92    | 26.92    | -15  | 0.01 | 0.01 | 29.05    | 29.05    | -14  | 0.02 | 0.02 | 31.39    | 31.39    | -13  | 0.02 | 0.02 | 31.39    | 31.39    |      |    |    |          |          |      |    |    |          |          |
| -12  | 0.02 | 0.02 | 31.39    | 31.39    | -11  | 0.01 | 0.01 | 29.08    | 29.08    | -10  | 0.01 | 0.01 | 26.80    | 26.80    | -9   | 0.01 | 0.01 | 26.90    | 26.90    | -8   | 0.02 | 0.02 | 31.39    | 31.39    |      |    |    |          |          |      |    |    |          |          |
| -7   | 0.02 | 0.02 | 31.39    | 31.39    | -6   | 0.01 | 0.01 | 27.34    | 27.34    | -5   | 0.01 | 0.01 | 26.80    | 26.80    | -4   | 0.01 | 0.01 | 28.64    | 28.64    | -3   | 0.01 | 0.01 | 20.35    | 20.35    |      |    |    |          |          |      |    |    |          |          |
| 203  | 0.01 | 0.01 | 26.80    | 26.80    | 204  | 0.01 | 0.01 | 22.03    | 22.03    | 205  | 0.01 | 0.01 | 26.80    | 26.80    |      |      |      |          |          |      |      |      |          |          |      |    |    |          |          |      |    |    |          |          |

Totali forze sismiche

|          |          |
|----------|----------|
| Fx <daN> | Fy <daN> |
| 1959.23  | 1959.23  |

Elenco forze sismiche nodali allo SND

| Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx   | cy   | Fx <daN> | Fy <daN> | Nodo | cx | cy | Fx <daN> | Fy <daN> | Nodo | cx | cy | Fx <daN> | Fy <daN> |
|------|------|------|----------|----------|------|------|------|----------|----------|------|------|------|----------|----------|------|------|------|----------|----------|------|------|------|----------|----------|------|----|----|----------|----------|------|----|----|----------|----------|
| -104 | 0.01 | 0.01 | 46.60    | 46.60    | -103 | 0.00 | 0.00 | 21.32    | 21.32    | -102 | 0.00 | 0.00 | 21.32    | 21.32    | -101 | 0.01 | 0.01 | 46.60    | 46.60    | -100 | 0.01 | 0.01 | 31.09    | 31.09    |      |    |    |          |          |      |    |    |          |          |
| -99  | 0.00 | 0.00 | 14.22    | 14.22    | -98  | 0.00 | 0.00 | 21.32    | 21.32    | -97  | 0.00 | 0.00 | 21.32    | 21.32    | -96  | 0.00 | 0.00 | 21.32    | 21.32    | -95  | 0.01 | 0.01 | 46.60    | 46.60    |      |    |    |          |          |      |    |    |          |          |
| -94  | 0.01 | 0.01 | 46.60    | 46.60    | -93  | 0.01 | 0.01 | 46.60    | 46.60    | -92  | 0.00 | 0.00 | 21.32    | 21.32    | -91  | 0.01 | 0.01 | 46.60    | 46.60    | -90  | 0.00 | 0.00 | 21.32    | 21.32    |      |    |    |          |          |      |    |    |          |          |
| -89  | 0.00 | 0.00 | 21.32    | 21.32    | -88  | 0.01 | 0.01 | 46.60    | 46.60    | -87  | 0.01 | 0.01 | 46.60    | 46.60    | -86  | 0.00 | 0.00 | 21.32    | 21.32    | -85  | 0.00 | 0.00 | 21.32    | 21.32    |      |    |    |          |          |      |    |    |          |          |
| -84  | 0.01 | 0.01 | 46.60    | 46.60    | -83  | 0.00 | 0.00 | 21.32    | 21.32    | -82  | 0.01 | 0.01 | 46.60    | 46.60    | -81  | 0.00 | 0.00 | 21.32    | 21.32    | -80  | 0.01 | 0.01 | 46.60    | 46.60    |      |    |    |          |          |      |    |    |          |          |
| -79  | 0.00 | 0.00 | 21.32    | 21.32    | -78  | 0.01 | 0.01 | 46.60    | 46.60    | -77  | 0.00 | 0.00 | 21.32    | 21.32    | -76  | 0.01 | 0.01 | 46.60    | 46.60    | -75  | 0.01 | 0.01 | 46.60    | 46.60    |      |    |    |          |          |      |    |    |          |          |
| -74  | 0.00 | 0.00 | 21.32    | 21.32    | -73  | 0.01 | 0.01 | 46.60    | 46.60    | -72  | 0.00 | 0.00 | 21.32    | 21.32    | -71  | 0.01 | 0.01 | 46.60    | 46.60    | -70  | 0.00 | 0.00 | 21.32    | 21.32    |      |    |    |          |          |      |    |    |          |          |
| -69  | 0.00 | 0.00 | 21.32    | 21.32    | -68  | 0.01 | 0.01 | 46.60    | 46.60    | -67  | 0.01 | 0.01 | 46.60    | 46.60    | -66  | 0.00 | 0.00 | 21.32    | 21.32    | -65  | 0.01 | 0.01 | 31.09    | 31.09    |      |    |    |          |          |      |    |    |          |          |
| -64  | 0.01 | 0.01 | 46.60    | 46.60    | -63  | 0.00 | 0.00 | 14.22    | 14.22    | -62  | 0.01 | 0.01 | 46.60    | 46.60    | -61  | 0.00 | 0.00 | 21.32    | 21.32    | -60  | 0.00 | 0.00 | 14.22    | 14.22    |      |    |    |          |          |      |    |    |          |          |
| -59  | 0.01 | 0.01 | 31.09    | 31.09    | -58  | 0.01 | 0.01 | 46.60    | 46.60    | -57  | 0.00 | 0.00 | 21.32    | 21.32    | -56  | 0.01 | 0.01 | 46.60    | 46.60    | -55  | 0.00 | 0.00 | 21.32    | 21.32    |      |    |    |          |          |      |    |    |          |          |
| -54  | 0.01 | 0.01 | 46.60    | 46.60    | -53  | 0.00 | 0.00 | 21.32    | 21.32    | -52  | 0.01 | 0.01 | 46.60    | 46.60    | -51  | 0.00 | 0.00 | 14.22    | 14.22    | -50  | 0.01 | 0.01 | 31.09    | 31.09    |      |    |    |          |          |      |    |    |          |          |
| -49  | 0.01 | 0.01 | 46.60    | 46.60    | -48  | 0.00 | 0.00 | 21.32    | 21.32    | -47  | 0.00 | 0.00 | 21.32    | 21.32    | -46  | 0.01 | 0.01 | 46.60    | 46.60    | -45  | 0.00 | 0.00 | 21.32    | 21.32    |      |    |    |          |          |      |    |    |          |          |
| -44  | 0.01 | 0.01 | 46.60    | 46.60    | -43  | 0.00 | 0.00 | 21.32    | 21.32    | -42  | 0.01 | 0.01 | 46.60    | 46.60    | -41  | 0.00 | 0.00 | 21.32    | 21.32    | -38  | 0.01 | 0.01 | 49.60    | 49.60    |      |    |    |          |          |      |    |    |          |          |
| -37  | 0.01 | 0.01 | 69.78    | 69.78    | -36  | 0.01 | 0.01 | 65.31    | 65.31    | -35  | 0.01 | 0.01 | 66.63    | 66.63    | -34  | 0.02 | 0.02 | 76.49    | 76.49    | -33  | 0.02 | 0.02 | 76.49    | 76.49    |      |    |    |          |          |      |    |    |          |          |
| -32  | 0.01 | 0.01 | 65.54    | 65.54    | -31  | 0.01 | 0.01 | 65.31    | 65.31    | -30  | 0.01 | 0.01 | 70.87    | 70.87    | -29  | 0.02 | 0.02 | 76.49    | 76.49    | -28  | 0.02 | 0.02 | 76.49    | 76.49    |      |    |    |          |          |      |    |    |          |          |
| -27  | 0.02 | 0.02 | 76.49    | 76.49    | -26  | 0.01 | 0.01 | 70.80    | 70.80    | -25  | 0.01 | 0.01 | 65.61    | 65.61    | -24  | 0.02 | 0.02 | 76.49    | 76.49    | -23  | 0.02 | 0.02 | 76.49    | 76.49    |      |    |    |          |          |      |    |    |          |          |
| -22  | 0.02 | 0.02 | 76.49    | 76.49    | -21  | 0.01 | 0.01 | 52.08    | 52.08    | -20  |      |      |          |          |      |      |      |          |          |      |      |      |          |          |      |    |    |          |          |      |    |    |          |          |



Simbologia

CC = Numero della combinazione delle condizioni di carico elementari  
 Fx = Reazione vincolare (forza) in dir. X  
 Fy = Reazione vincolare (forza) in dir. Y  
 Fz = Reazione vincolare (forza) in dir. Z  
 Mx = Reazione vincolare (momento) intorno all'asse X  
 My = Reazione vincolare (momento) intorno all'asse Y  
 Mz = Reazione vincolare (momento) intorno all'asse Z  
 Nodo = Numero del nodo  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
 SLD = Stato limite di danno  
 SND = Stato limite di salvaguardia della vita (non dissipativo)

| Nodo | CC  | TCC | Fx          | Fy              | Fz             | Mx               | My              | Mz          |
|------|-----|-----|-------------|-----------------|----------------|------------------|-----------------|-------------|
|      |     |     | <daN>       | <daN>           | <daN>          | <daNm>           | <daNm>          | <daNm>      |
| 1    | Max | 5   | SND 532.37  | 21 SLU 2116.46  | 28 SLU 2804.14 | 28 SLU 5046.51   | 5 SND 1098.19   | 1 SND 0.14  |
| 1    | Min | 1   | SND -651.83 | 28 SLU -1491.03 | 21 SLU 284.49  | 21 SLU -7163.35  | 7 SND -1228.40  | 1 SND -0.14 |
| 2    | Max | 5   | SND 838.48  | 21 SLU 2893.27  | 28 SLU 3654.04 | 28 SLU 6637.20   | 5 SND 1432.41   | 21 SLU 1.97 |
| 2    | Min | 1   | SND -644.05 | 28 SLU -2038.28 | 21 SLU 185.86  | 21 SLU -9421.30  | 28 SLU -1220.23 | 1 SND -1.39 |
| 3    | Max | 5   | SND 633.78  | 21 SLU 3151.63  | 28 SLU 3978.31 | 28 SLU 7224.05   | 5 SND 1209.36   | 28 SLU 0.85 |
| 3    | Min | 1   | SND -754.78 | 28 SLU -2220.28 | 21 SLU 199.06  | 21 SLU -10254.30 | 21 SLU -1341.31 | 1 SND -1.21 |
| 4    | Max | 5   | SND 718.93  | 21 SLU 2578.76  | 28 SLU 3369.62 | 28 SLU 6126.94   | 5 SND 1302.25   | 1 SND 0.00  |
| 4    | Min | 1   | SND -718.93 | 28 SLU -1816.71 | 21 SLU 344.91  | 21 SLU -8696.99  | 7 SND -1302.25  | 1 SND -0.00 |
| 5    | Max | 5   | SND 754.78  | 21 SLU 3151.63  | 28 SLU 3978.30 | 28 SLU 7224.05   | 5 SND 1341.31   | 21 SLU 1.21 |
| 5    | Min | 1   | SND -633.78 | 28 SLU -2220.29 | 21 SLU 199.06  | 21 SLU -10254.30 | 28 SLU -1209.36 | 1 SND -0.85 |
| 6    | Max | 5   | SND 644.05  | 21 SLU 2893.27  | 28 SLU 3654.04 | 28 SLU 6637.20   | 5 SND 1220.23   | 28 SLU 1.39 |
| 6    | Min | 1   | SND -838.48 | 28 SLU -2038.27 | 21 SLU 185.86  | 21 SLU -9421.29  | 21 SLU -1432.41 | 1 SND -1.97 |
| 7    | Max | 5   | SND 651.83  | 21 SLU 2116.47  | 28 SLU 2804.15 | 28 SLU 5046.51   | 5 SND 1228.40   | 3 SND 0.14  |
| 7    | Min | 1   | SND -532.37 | 28 SLU -1491.03 | 21 SLU 284.48  | 21 SLU -7163.36  | 5 SND -1098.19  | 1 SND -0.14 |

Sollecitazioni aste

Simbologia

Asta = Numero dell'asta  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Mx = Momento torcente intorno all'asse X  
 My = Momento flettente intorno all'asse Y  
 Mz = Momento flettente intorno all'asse Z  
 N = Sforzo normale  
 N1 = Nodo1  
 N2 = Nodo2  
 Ty = Taglio in dir. Y  
 Tz = Taglio in dir. Z  
 X = Coordinata progressiva rispetto al nodo iniziale

Tipo di combinazione di carico: SND

| Asta | N1 | N2  | X           | N        | Ty        | Mz         | Tz         | My          | Mx       | CC |
|------|----|-----|-------------|----------|-----------|------------|------------|-------------|----------|----|
|      |    |     | <cm>        | <daN>    | <daN>     | <daNm>     | <daN>      | <daNm>      | <daNm>   |    |
| 1    | 1  | -5  | Max 0.00    | -852.25  | 1 532.37  | 5 1228.40  | 1 573.40   | 15 2038.77  | 9 0.14   | 7  |
| 1    | 1  | -5  | Max 330.00  | -663.01  | 1 532.37  | 5 658.64   | 5 573.40   | 15 150.66   | 11 0.14  | 7  |
| 1    | 1  | -5  | Min. 0.00   | -1515.13 | 5 -651.83 | 1 -1098.19 | 5 -573.40  | 9 -2038.76  | 15 -0.14 | 1  |
| 1    | 1  | -5  | Min. 330.00 | -1325.90 | 5 -651.83 | 1 -922.64  | 1 -573.40  | 9 -150.66   | 13 -0.14 | 1  |
| 2    | 2  | -10 | Max 0.00    | -1287.17 | 5 838.48  | 5 1220.23  | 1 703.18   | 13 2439.50  | 11 0.46  | 9  |
| 2    | 2  | -10 | Max 330.00  | -1097.94 | 5 838.48  | 5 1334.58  | 5 703.18   | 13 123.43   | 9 0.46   | 9  |
| 2    | 2  | -10 | Min. 0.00   | -1654.92 | 1 -644.05 | 1 -1432.41 | 5 -703.18  | 11 -2439.49 | 13 -0.46 | 15 |
| 2    | 2  | -10 | Min. 330.00 | -1465.68 | 1 -644.05 | 1 -905.13  | 1 -703.18  | 11 -123.42  | 15 -0.46 | 15 |
| 3    | 3  | 203 | Max 0.00    | -1542.39 | 1 633.78  | 5 1341.31  | 1 776.99   | 13 2684.76  | 11 0.24  | 13 |
| 3    | 3  | 203 | Max 330.00  | -1353.16 | 1 633.78  | 5 882.11   | 5 776.99   | 13 120.70   | 11 0.24  | 13 |
| 3    | 3  | 203 | Min. 0.00   | -1658.24 | 5 -754.78 | 1 -1209.36 | 5 -776.99  | 11 -2684.76 | 13 -0.24 | 11 |
| 3    | 3  | 203 | Min. 330.00 | -1469.01 | 5 -754.78 | 1 -1149.47 | 1 -776.99  | 11 -120.70  | 13 -0.24 | 11 |
| 4    | 4  | 204 | Max 0.00    | -1423.57 | 1 718.93  | 1 1302.25  | 5 685.95   | 9 2435.81   | 13 0.00  | 7  |
| 4    | 4  | 204 | Max 330.00  | -1234.34 | 1 718.93  | 1 1070.22  | 1 685.95   | 9 172.18    | 15 0.00  | 7  |
| 4    | 4  | 204 | Min. 0.00   | -1423.57 | 1 -718.93 | 5 -1302.25 | 1 -685.95  | 13 -2435.81 | 9 -0.00  | 1  |
| 4    | 4  | 204 | Min. 330.00 | -1234.34 | 1 -718.93 | 5 -1070.22 | 5 -685.95  | 13 -172.18  | 9 -0.00  | 1  |
| 5    | 5  | 205 | Max 0.00    | -1542.39 | 5 633.78  | 1 1341.31  | 5 776.99   | 9 2684.76   | 15 0.24  | 9  |
| 5    | 5  | 205 | Max 330.00  | -1353.16 | 5 633.78  | 1 882.11   | 1 776.99   | 9 120.70    | 15 0.24  | 9  |
| 5    | 5  | 205 | Min. 0.00   | -1658.24 | 1 -754.78 | 5 -1209.36 | 1 -776.99  | 15 -2684.76 | 9 -0.24  | 15 |
| 5    | 5  | 205 | Min. 330.00 | -1469.01 | 1 -754.78 | 5 -1149.47 | 5 -776.99  | 15 -120.70  | 9 -0.24  | 15 |
| 6    | 6  | -31 | Max 0.00    | -1287.17 | 1 838.48  | 1 1220.23  | 5 703.18   | 9 2439.49   | 15 0.46  | 13 |
| 6    | 6  | -31 | Max 330.00  | -1097.94 | 1 838.48  | 1 1334.58  | 1 703.18   | 9 123.43    | 13 0.46  | 13 |
| 6    | 6  | -31 | Min. 0.00   | -1654.92 | 5 -644.05 | 5 -1432.41 | 1 -703.18  | 15 -2439.49 | 9 -0.46  | 11 |
| 6    | 6  | -31 | Min. 330.00 | -1465.68 | 5 -644.05 | 5 -905.13  | 5 -703.18  | 15 -123.43  | 11 -0.46 | 11 |
| 7    | 7  | -36 | Max 0.00    | -852.25  | 5 532.37  | 1 1228.40  | 5 573.40   | 11 2038.77  | 13 0.14  | 5  |
| 7    | 7  | -36 | Max 330.00  | -663.01  | 5 532.37  | 1 658.63   | 1 573.40   | 11 150.66   | 15 0.14  | 5  |
| 7    | 7  | -36 | Min. 0.00   | -1515.13 | 1 -651.83 | 5 -1098.19 | 1 -573.40  | 13 -2038.77 | 11 -0.14 | 3  |
| 7    | 7  | -36 | Min. 330.00 | -1325.90 | 1 -651.83 | 5 -922.65  | 5 -573.40  | 13 -150.66  | 9 -0.14  | 3  |
| 201  | -4 | -3  | Max 0.00    | 94.91    | 5 94.91   | 9 131.09   | 15 216.51  | 1 -225.38   | 1 20.73  | 9  |
| 201  | -4 | -3  | Max 133.53  | 94.91    | 5 94.91   | 9 14.52    | 5 152.11   | 1 20.73     | 1 20.73  | 9  |
| 201  | -4 | -3  | Min. 0.00   | -94.91   | 1 -94.91  | 13 -131.09 | 9 216.51   | 1 -266.84   | 5 -20.73 | 13 |
| 201  | -4 | -3  | Min. 133.53 | -94.91   | 1 -94.91  | 13 -14.52  | 3 152.11   | 1 -20.73    | 5 -20.73 | 13 |
| 201  | -5 | -4  | Max 0.00    | 232.61   | 5 232.61  | 9 322.46   | 15 470.88  | 1 -553.27   | 1 51.80  | 9  |
| 201  | -5 | -4  | Max 79.47   | 232.61   | 5 232.61  | 9 137.62   | 15 432.55  | 1 -194.31   | 1 51.80  | 9  |
| 201  | -5 | -4  | Min. 0.00   | -232.61  | 1 -232.61 | 13 -322.46 | 9 470.88   | 1 -656.88   | 5 -51.80 | 13 |
| 201  | -5 | -4  | Min. 79.47  | -232.61  | 1 -232.61 | 13 -137.62 | 9 432.55   | 1 -297.92   | 5 -51.80 | 13 |
| 201  | -6 | -5  | Max 0.00    | 353.92   | 1 275.48  | 15 173.39  | 15 -166.06 | 1 466.20    | 1 98.85  | 13 |
| 201  | -6 | -5  | Max 54.07   | 353.92   | 1 275.48  | 15 322.33  | 15 -192.13 | 1 369.37    | 1 98.85  | 13 |
| 201  | -6 | -5  | Min. 0.00   | -234.46  | 5 -275.48 | 9 -173.39  | 9 -828.94  | 5 -860.28   | 5 -98.85 | 11 |
| 201  | -6 | -5  | Min. 54.07  | -234.46  | 5 -275.48 | 9 -322.33  | 9 -855.02  | 5 -1315.51  | 5 -98.85 | 11 |
| 201  | -7 | -6  | Max 0.00    | 219.37   | 1 140.94  | 15 16.89   | 5 114.39   | 1 387.53    | 1 67.78  | 13 |
| 201  | -7 | -6  | Max 133.53  | 219.37   | 1 140.94  | 15 179.91  | 15 49.98   | 1 497.28    | 1 67.78  | 13 |
| 201  | -7 | -6  | Min. 0.00   | -99.91   | 7 -140.94 | 9 -16.89   | 3 -548.49  | 5 -115.93   | 5 -67.78 | 11 |
| 201  | -7 | -6  | Min. 133.53 | -99.91   | 7 -140.94 | 9 -179.91  | 9 -612.90  | 5 -891.36   | 5 -67.78 | 11 |
| 201  | -8 | -7  | Max 0.00    | 74.96    | 1 27.02   | 5 3.74     | 7 394.83   | 1 253.92    | 5 36.71  | 13 |
| 201  | -8 | -7  | Max 133.53  | 74.96    | 1 27.02   | 5 38.65    | 5 330.43   | 1 418.60    | 1 36.71  | 13 |
| 201  | -8 | -7  | Min. 0.00   | 44.50    | 7 -27.02  | 3 -3.74    | 1 -268.05  | 5 -65.63    | 1 -36.71 | 11 |
| 201  | -8 | -7  | Min. 133.53 | 44.50    | 7 -27.02  | 3 -38.65   | 3 -332.45  | 5 -147.01   | 5 -36.71 | 11 |
| 201  | -9 | -8  | Max 0.00    | 188.92   | 5 162.19  | 11 211.05  | 13 675.28  | 1 249.29    | 5 7.91   | 3  |





|     |     |     |      |        |         |    |         |    |         |    |         |    |          |    |        |    |
|-----|-----|-----|------|--------|---------|----|---------|----|---------|----|---------|----|----------|----|--------|----|
| 205 | -28 | -29 | Max  | 133.53 | 92.63   | 5  | 68.90   | 11 | 247.53  | 15 | -13.46  | 5  | 514.05   | 5  | 31.74  | 11 |
| 205 | -28 | -29 | Min. | 0.00   | -167.60 | 3  | -68.90  | 13 | -332.91 | 11 | -244.19 | 1  | 489.03   | 5  | -31.74 | 13 |
| 205 | -28 | -29 | Min. | 105.62 |         |    |         |    | -72.16  | 5  |         |    | 515.93   | 5  |        |    |
| 205 | -28 | -29 | Min. | 133.53 | -167.60 | 3  | -68.90  | 13 | -247.53 | 9  | -308.60 | 1  | 185.40   | 1  | -31.74 | 13 |
| 205 | -29 | -30 | Max  | 0.00   | 237.04  | 5  | 213.31  | 11 | 247.42  | 13 | -229.51 | 5  | 482.97   | 5  | 62.81  | 11 |
| 205 | -29 | -30 | Max  | 133.53 | 237.04  | 5  | 213.31  | 11 | 37.42   | 11 | -293.91 | 5  | 133.50   | 5  | 62.81  | 11 |
| 205 | -29 | -30 | Min. | 0.00   | -312.01 | 1  | -213.31 | 13 | -247.42 | 11 | -524.64 | 1  | 216.45   | 1  | -62.81 | 13 |
| 205 | -29 | -30 | Min. | 133.53 | -312.01 | 1  | -213.31 | 13 | -37.42  | 13 | -589.05 | 1  | -527.12  | 1  | -62.81 | 13 |
| 205 | -30 | -31 | Max  | 0.00   | 375.83  | 5  | 352.10  | 11 | 37.17   | 9  | -509.95 | 5  | 102.44   | 5  | 93.89  | 11 |
| 205 | -30 | -31 | Max  | 88.20  | 375.83  | 5  | 352.10  | 11 | 341.44  | 11 | -552.50 | 5  | -366.10  | 5  | 93.89  | 11 |
| 205 | -30 | -31 | Min. | 0.00   | -450.80 | 1  | -352.10 | 13 | -37.17  | 15 | -805.09 | 1  | -496.03  | 1  | -93.88 | 13 |
| 205 | -30 | -31 | Min. | 88.20  | -450.80 | 1  | -352.10 | 13 | -341.44 | 13 | -847.63 | 1  | -1224.88 | 1  | -93.88 | 13 |
| 206 | -31 | -32 | Max  | 0.00   | 322.38  | 1  | 295.65  | 15 | 340.97  | 11 | 913.19  | 5  | 109.70   | 1  | 29.54  | 13 |
| 206 | -31 | -32 | Max  | 45.33  | 322.38  | 1  | 295.65  | 15 | 213.43  | 11 | 891.33  | 5  | 218.22   | 1  | 29.54  | 13 |
| 206 | -31 | -32 | Min. | 0.00   | -202.92 | 5  | -295.65 | 9  | -340.97 | 13 | 250.31  | 1  | -1271.23 | 5  | -29.54 | 11 |
| 206 | -31 | -32 | Min. | 45.33  | -202.92 | 5  | -295.65 | 9  | -213.43 | 13 | 228.44  | 1  | -862.21  | 5  | -29.54 | 11 |
| 206 | -32 | -33 | Max  | 0.00   | 188.92  | 1  | 162.19  | 15 | 211.06  | 9  | 675.28  | 5  | 249.29   | 1  | 7.91   | 1  |
| 206 | -32 | -33 | Max  | 25.71  |         |    |         |    | 51.52   | 1  |         |    | 250.88   | 1  |        |    |
| 206 | -32 | -33 | Max  | 133.53 | 188.92  | 1  | 162.19  | 15 | 25.50   | 5  | 610.88  | 5  | 222.84   | 1  | 7.91   | 1  |
| 206 | -32 | -33 | Min. | 0.00   | -69.46  | 7  | -162.19 | 9  | -211.06 | 15 | 12.40   | 1  | -893.31  | 5  | -7.91  | 7  |
| 206 | -32 | -33 | Min. | 25.71  |         |    |         |    | 51.52   | 1  |         |    | 250.88   | 1  |        |    |
| 206 | -32 | -33 | Min. | 133.53 | -69.46  | 7  | -162.19 | 9  | -25.50  | 3  | -52.00  | 1  | -34.59   | 5  | -7.91  | 7  |
| 206 | -33 | -34 | Max  | 0.00   | 74.96   | 5  | 27.02   | 7  | 3.74    | 5  | 394.83  | 5  | 253.91   | 1  | 36.71  | 9  |
| 206 | -33 | -34 | Max  | 133.53 | 74.96   | 5  | 27.02   | 7  | 38.65   | 7  | 330.43  | 5  | 418.62   | 5  | 36.71  | 9  |
| 206 | -33 | -34 | Min. | 0.00   | 44.50   | 3  | -27.02  | 1  | -3.74   | 3  | -268.05 | 1  | -65.62   | 5  | -36.71 | 15 |
| 206 | -33 | -34 | Min. | 133.53 | 44.50   | 3  | -27.02  | 1  | -38.65  | 1  | -332.45 | 1  | -147.02  | 1  | -36.71 | 15 |
| 206 | -34 | -35 | Max  | 0.00   | 219.37  | 5  | 140.94  | 11 | 16.89   | 7  | 114.39  | 5  | 387.53   | 5  | 67.78  | 9  |
| 206 | -34 | -35 | Max  | 133.53 | 219.37  | 5  | 140.94  | 11 | 179.92  | 11 | 49.98   | 5  | 497.28   | 5  | 67.78  | 9  |
| 206 | -34 | -35 | Min. | 0.00   | -99.91  | 3  | -140.94 | 13 | -16.89  | 1  | -548.50 | 1  | -115.94  | 1  | -67.78 | 15 |
| 206 | -34 | -35 | Min. | 133.53 | -99.91  | 3  | -140.94 | 13 | -179.92 | 13 | -612.90 | 1  | -891.36  | 1  | -67.78 | 15 |
| 206 | -35 | -36 | Max  | 0.00   | 353.92  | 5  | 275.48  | 11 | 173.38  | 11 | -166.06 | 5  | 466.20   | 5  | 98.85  | 9  |
| 206 | -35 | -36 | Max  | 54.07  | 353.92  | 5  | 275.48  | 11 | 322.33  | 11 | -192.13 | 5  | 369.37   | 5  | 98.85  | 9  |
| 206 | -35 | -36 | Min. | 0.00   | -234.46 | 1  | -275.48 | 13 | -173.38 | 13 | -828.94 | 1  | -860.26  | 1  | -98.85 | 15 |
| 206 | -35 | -36 | Min. | 54.07  | -234.46 | 1  | -275.48 | 13 | -322.33 | 13 | -855.02 | 1  | -1315.50 | 1  | -98.85 | 15 |
| 206 | -36 | -37 | Max  | 0.00   | 232.61  | 1  | 232.61  | 13 | 322.47  | 11 | 470.88  | 1  | -553.28  | 5  | 51.80  | 13 |
| 206 | -36 | -37 | Max  | 79.47  | 232.61  | 1  | 232.61  | 13 | 137.62  | 11 | 432.55  | 1  | -194.32  | 5  | 51.80  | 13 |
| 206 | -36 | -37 | Min. | 0.00   | -232.61 | 5  | -232.61 | 9  | -322.47 | 13 | 470.88  | 1  | -656.89  | 1  | -51.80 | 9  |
| 206 | -36 | -37 | Min. | 79.47  | -232.61 | 5  | -232.61 | 9  | -137.62 | 13 | 432.55  | 1  | -297.93  | 1  | -51.80 | 9  |
| 206 | -37 | -38 | Max  | 0.00   | 94.91   | 1  | 94.91   | 13 | 131.09  | 11 | 216.51  | 1  | -225.38  | 5  | 20.73  | 13 |
| 206 | -37 | -38 | Max  | 133.53 | 94.91   | 1  | 94.91   | 13 | 14.52   | 7  | 152.11  | 1  | 20.73    | 5  | 20.73  | 13 |
| 206 | -37 | -38 | Min. | 0.00   | -94.91  | 5  | -94.91  | 9  | -131.09 | 13 | 216.51  | 1  | -266.84  | 1  | -20.73 | 9  |
| 206 | -37 | -38 | Min. | 133.53 | -94.91  | 5  | -94.91  | 9  | -14.52  | 1  | 152.11  | 1  | -20.73   | 1  | -20.73 | 9  |
| 301 | -3  | -60 | Max  | 0.00   | 70.46   | 13 | 14.22   | 5  | 21.33   | 1  | 55.27   | 9  | -20.38   | 13 | 0.00   | 1  |
| 301 | -3  | -60 | Max  | 130.42 |         |    |         |    | 0.84    | 13 |         |    | 0.47     | 13 |        |    |
| 301 | -3  | -60 | Max  | 150.00 | 17.94   | 13 | 14.22   | 5  | 0.00    | 1  | 18.50   | 9  | 0.00     | 13 | 0.00   | 1  |
| 301 | -3  | -60 | Min. | 0.00   | 54.14   | 9  | -14.22  | 1  | -21.33  | 5  | 31.97   | 13 | -55.32   | 9  | 0.00   | 1  |
| 301 | -3  | -60 | Min. | 130.42 |         |    |         |    | 0.84    | 13 |         |    | 0.47     | 13 |        |    |
| 301 | -3  | -60 | Min. | 150.00 | 1.62    | 9  | -14.22  | 1  | 0.00    | 5  | -4.80   | 13 | 0.00     | 9  | 0.00   | 1  |
| 301 | -59 | -3  | Max  | 0.00   | 8.05    | 9  | 31.09   | 1  | 0.00    | 1  | 18.62   | 13 | 0.00     | 1  | 0.00   | 1  |
| 301 | -59 | -3  | Max  | 75.95  |         |    |         |    | 7.08    | 13 |         |    | 7.07     | 13 |        |    |
| 301 | -59 | -3  | Max  | 150.00 | -44.47  | 9  | 31.09   | 1  | 46.64   | 1  | -18.15  | 13 | 0.35     | 13 | 0.00   | 1  |
| 301 | -59 | -3  | Min. | 0.00   | -27.61  | 13 | -31.09  | 5  | 0.00    | 5  | -32.32  | 9  | 0.00     | 1  | 0.00   | 5  |
| 301 | -59 | -3  | Min. | 3.38   |         |    |         |    | 1.05    | 3  |         |    | 0.01     | 3  |        |    |
| 301 | -59 | -3  | Min. | 150.00 | -80.13  | 13 | -31.09  | 5  | -46.64  | 5  | -69.09  | 9  | -76.05   | 9  | 0.00   | 5  |
| 302 | -4  | -47 | Max  | 0.00   | 100.71  | 13 | 21.32   | 5  | 31.97   | 1  | 79.42   | 9  | -30.55   | 13 | 0.00   | 1  |
| 302 | -4  | -47 | Max  | 138.30 |         |    |         |    | 0.75    | 13 |         |    | 0.22     | 13 |        |    |
| 302 | -4  | -47 | Max  | 150.00 | 31.78   | 13 | 21.32   | 5  | 0.00    | 1  | 31.15   | 9  | 0.00     | 13 | 0.00   | 1  |
| 302 | -4  | -47 | Min. | 0.00   | 76.26   | 9  | -21.32  | 1  | -31.97  | 5  | 44.50   | 13 | -82.93   | 9  | 0.00   | 1  |
| 302 | -4  | -47 | Min. | 138.30 |         |    |         |    | 0.75    | 13 |         |    | 0.22     | 13 |        |    |
| 302 | -4  | -47 | Min. | 150.00 | 7.33    | 9  | -21.32  | 1  | 0.00    | 5  | -3.77   | 13 | 0.00     | 9  | 0.00   | 1  |
| 302 | -46 | -4  | Max  | 0.00   | 7.17    | 9  | 46.60   | 1  | 0.00    | 5  | 24.48   | 13 | 0.00     | 5  | 0.00   | 5  |
| 302 | -46 | -4  | Max  | 76.09  |         |    |         |    | 10.64   | 13 |         |    | 9.31     | 13 |        |    |
| 302 | -46 | -4  | Max  | 150.00 | -61.75  | 9  | 46.60   | 1  | 69.91   | 1  | -23.78  | 13 | 0.52     | 13 | 0.00   | 5  |
| 302 | -46 | -4  | Min. | 0.00   | -46.29  | 13 | -46.60  | 5  | 0.00    | 1  | -51.87  | 9  | 0.00     | 1  | 0.00   | 1  |
| 302 | -46 | -4  | Min. | 76.09  |         |    |         |    | 10.64   | 13 |         |    | 9.31     | 13 |        |    |
| 302 | -46 | -4  | Min. | 150.00 | -115.22 | 13 | -46.60  | 5  | -69.91  | 5  | -100.14 | 9  | -114.00  | 9  | 0.00   | 1  |
| 303 | -6  | -48 | Max  | 0.00   | 100.71  | 13 | 21.32   | 5  | 31.97   | 1  | 79.42   | 9  | -30.55   | 13 | 0.00   | 1  |
| 303 | -6  | -48 | Max  | 138.30 |         |    |         |    | 0.75    | 13 |         |    | 0.22     | 13 |        |    |
| 303 | -6  | -48 | Max  | 150.00 | 31.78   | 13 | 21.32   | 5  | 0.00    | 1  | 31.15   | 9  | 0.00     | 13 | 0.00   | 1  |
| 303 | -6  | -48 | Min. | 0.00   | 76.26   | 9  | -21.32  | 1  | -31.97  | 5  | 44.50   | 13 | -82.93   | 9  | 0.00   | 1  |
| 303 | -6  | -48 | Min. | 138.30 |         |    |         |    | 0.75    | 13 |         |    | 0.22     | 13 |        |    |
| 303 | -6  | -48 | Min. | 150.00 | 7.33    | 9  | -21.32  | 1  | 0.00    | 5  | -3.77   | 13 | 0.00     | 9  | 0.00   | 1  |
| 303 | -49 | -6  | Max  | 0.00   | 7.17    | 9  | 46.60   | 1  | 0.00    | 7  | 24.48   | 13 | 0.00     | 9  | 0.00   | 3  |
| 303 | -49 | -6  | Max  | 76.09  |         |    |         |    | 10.64   | 13 |         |    | 9.31     | 13 |        |    |
| 303 | -49 | -6  | Max  | 150.00 | -61.75  | 9  | 46.60   | 1  | 69.91   | 1  | -23.78  | 13 | 0.52     | 13 | 0.00   | 3  |
| 303 | -49 | -6  | Min. | 0.00   | -46.29  | 13 | -46.60  | 5  | 0.00    | 1  | -51.87  | 9  | 0.00     | 13 | 0.00   | 5  |
| 303 | -49 | -6  | Min. | 76.09  |         |    |         |    | 10.64   | 13 |         |    | 9.31     | 13 |        |    |
| 303 | -49 | -6  | Min. | 150.00 | -115.22 | 13 | -46.60  | 5  | -69.91  | 5  | -100.14 | 9  | -114.00  | 9  | 0.00   | 5  |
| 304 | -7  | -96 | Max  | 0.00   | 100.71  | 13 | 21.32   | 5  | 31.97   | 1  | 79.42   | 9  | -30.55   | 13 | 0.00   | 1  |
| 304 | -7  | -96 | Max  | 138.30 |         |    |         |    | 0.75    | 13 |         |    | 0.22     | 13 |        |    |
| 304 | -7  | -96 | Max  | 150.00 | 31.78   | 13 | 21.32   | 5  | 0.00    | 1  | 31.15   | 9  | 0.00     | 13 | 0.00   | 1  |
| 304 | -7  | -96 | Min. | 0.00   | 76.26   | 9  | -21.32  | 1  | -31.97  | 5  | 44.50   | 13 | -82.93   | 9  | 0.00   | 1  |
| 304 | -7  | -96 | Min. | 138.30 |         |    |         |    | 0.75    | 13 |         |    | 0.22     | 13 |        |    |
| 304 | -7  | -96 | Min. | 150.00 | 7.33    | 9  | -21.32  | 1  | 0.00    | 5  | -3.77   | 13 | 0.00     | 9  | 0.00   | 1  |
| 304 | -95 | -7  | Max  | 0.00   | 7.17    | 9  | 46.60   | 1  | 0.00    | 5  | 24.48   | 13 | 0.00     | 1  | 0.00   | 1  |
| 304 | -95 | -7  | Max  | 76.09  |         |    |         |    | 10.64   | 13 |         |    | 9.31     | 13 |        |    |
| 304 | -95 | -7  | Max  | 150.00 | -61.75  | 9  | 46.60   | 1  | 69.91   | 1  | -23.78  | 13 | 0.52     | 13 | 0.00   | 1  |
| 304 | -95 | -7  | Min. | 0.00   | -46.29  | 13 | -46.60  | 5  | 0.00    | 1  | -51.87  | 9  | 0.00     | 1  | 0.00   | 5  |
| 304 | -95 | -7  | Min. | 76.09  |         |    |         |    | 10.64   | 13 |         |    | 9.31     | 13 |        |    |
| 304 | -95 | -7  | Min. | 150.00 | -115.22 | 13 | -46.60  | 5  | -69.91  | 5  | -100.14 | 9  | -114.00  | 9  | 0.00   | 5  |
| 305 | -8  | -66 |      |        |         |    |         |    |         |    |         |    |          |    |        |    |



|     |     |     |      |        |         |    |        |   |        |    |         |    |         |    |      |    |
|-----|-----|-----|------|--------|---------|----|--------|---|--------|----|---------|----|---------|----|------|----|
| 305 | -67 | -8  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 5  |
| 306 | -9  | -69 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1  |
| 306 | -9  | -69 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 306 | -9  | -69 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1  |
| 306 | -9  | -69 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1  |
| 306 | -9  | -69 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 306 | -9  | -69 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1  |
| 306 | -68 | -9  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 13 | 24.48   | 13 | 0.00    | 13 | 0.00 | 9  |
| 306 | -68 | -9  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 306 | -68 | -9  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 9  |
| 306 | -68 | -9  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 9  | -51.87  | 9  | 0.00    | 9  | 0.00 | 13 |
| 306 | -68 | -9  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 306 | -68 | -9  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 13 |
| 307 | -11 | -70 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1  |
| 307 | -11 | -70 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 307 | -11 | -70 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1  |
| 307 | -11 | -70 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1  |
| 307 | -11 | -70 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 307 | -11 | -70 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1  |
| 307 | -71 | -11 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 7  | 24.48   | 13 | 0.00    | 13 | 0.00 | 5  |
| 307 | -71 | -11 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 307 | -71 | -11 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5  |
| 307 | -71 | -11 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 11 | 0.00 | 3  |
| 307 | -71 | -11 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 307 | -71 | -11 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 3  |
| 308 | -12 | -72 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1  |
| 308 | -12 | -72 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 308 | -12 | -72 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1  |
| 308 | -12 | -72 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1  |
| 308 | -12 | -72 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 308 | -12 | -72 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1  |
| 308 | -73 | -12 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 13 | 24.48   | 13 | 0.00    | 13 | 0.00 | 1  |
| 308 | -73 | -12 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 308 | -73 | -12 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 1  |
| 308 | -73 | -12 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 9  | -51.87  | 9  | 0.00    | 9  | 0.00 | 1  |
| 308 | -73 | -12 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 308 | -73 | -12 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 1  |
| 309 | -13 | -74 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1  |
| 309 | -13 | -74 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 309 | -13 | -74 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1  |
| 309 | -13 | -74 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1  |
| 309 | -13 | -74 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 309 | -13 | -74 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1  |
| 309 | -75 | -13 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 3  | 24.48   | 13 | 0.00    | 15 | 0.00 | 5  |
| 309 | -75 | -13 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 309 | -75 | -13 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5  |
| 309 | -75 | -13 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 5  | -51.87  | 9  | 0.00    | 9  | 0.00 | 1  |
| 309 | -75 | -13 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 309 | -75 | -13 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 1  |
| 310 | -14 | -90 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1  |
| 310 | -14 | -90 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 310 | -14 | -90 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1  |
| 310 | -14 | -90 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1  |
| 310 | -14 | -90 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 310 | -14 | -90 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1  |
| 310 | -91 | -14 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 5  | 24.48   | 13 | 0.00    | 1  | 0.00 | 5  |
| 310 | -91 | -14 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 310 | -91 | -14 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5  |
| 310 | -91 | -14 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 5  | 0.00 | 1  |
| 310 | -91 | -14 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 310 | -91 | -14 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 1  |
| 311 | -15 | -92 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1  |
| 311 | -15 | -92 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 311 | -15 | -92 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1  |
| 311 | -15 | -92 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1  |
| 311 | -15 | -92 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 311 | -15 | -92 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1  |
| 311 | -93 | -15 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 1  | 24.48   | 13 | 0.00    | 5  | 0.00 | 1  |
| 311 | -93 | -15 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 311 | -93 | -15 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 1  |
| 311 | -93 | -15 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 5  | -51.87  | 9  | 0.00    | 1  | 0.00 | 5  |
| 311 | -93 | -15 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 311 | -93 | -15 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 5  |
| 312 | -16 | -98 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1  |
| 312 | -16 | -98 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 312 | -16 | -98 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1  |
| 312 | -16 | -98 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1  |
| 312 | -16 | -98 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 312 | -16 | -98 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1  |
| 312 | -94 | -16 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 9  | 24.48   | 13 | 0.00    | 9  | 0.00 | 5  |
| 312 | -94 | -16 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 312 | -94 | -16 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5  |
| 312 | -94 | -16 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 13 | -51.87  | 9  | 0.00    | 13 | 0.00 | 3  |
| 312 | -94 | -16 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 312 | -94 | -16 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 3  |
| 313 | -17 | -97 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1  |
| 313 | -17 | -97 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 313 | -17 | -97 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1  |
| 313 | -17 | -97 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1  |
| 313 | -17 | -97 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |    |
| 313 | -17 | -97 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1  |
| 313 | -42 | -17 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 5  | 24.48   | 13 | 0.00    | 11 | 0.00 | 5  |
| 313 | -42 | -17 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |    |
| 313 | -42 | -17 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5  |
| 313 | -42 | -1  |      |        |         |    |        |   |        |    |         |    |         |    |      |    |



|     |     |     |      |        |         |    |        |   |        |    |         |    |         |    |      |   |  |
|-----|-----|-----|------|--------|---------|----|--------|---|--------|----|---------|----|---------|----|------|---|--|
| 314 | -18 | -43 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 314 | -18 | -43 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 314 | -44 | -18 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 13 | 24.48   | 13 | 0.00    | 13 | 0.00 | 5 |  |
| 314 | -44 | -18 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 314 | -44 | -18 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5 |  |
| 314 | -44 | -18 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 9  | -51.87  | 9  | 0.00    | 9  | 0.00 | 1 |  |
| 314 | -44 | -18 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 314 | -44 | -18 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 1 |  |
| 315 | -19 | -45 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |  |
| 315 | -19 | -45 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 315 | -19 | -45 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |  |
| 315 | -19 | -45 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |  |
| 315 | -19 | -45 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 315 | -19 | -45 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 315 | -58 | -19 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 7  | 24.48   | 13 | 0.00    | 13 | 0.00 | 7 |  |
| 315 | -58 | -19 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 315 | -58 | -19 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 7 |  |
| 315 | -58 | -19 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 11 | 0.00 | 1 |  |
| 315 | -58 | -19 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 315 | -58 | -19 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 1 |  |
| 316 | -20 | -63 | Max  | 0.00   | 70.46   | 13 | 14.22  | 5 | 21.33  | 1  | 55.27   | 9  | -20.38  | 13 | 0.00 | 1 |  |
| 316 | -20 | -63 | Max  | 130.42 |         |    |        |   | 0.84   | 13 |         |    | 0.47    | 13 |      |   |  |
| 316 | -20 | -63 | Max  | 150.00 | 17.94   | 13 | 14.22  | 5 | 0.00   | 1  | 18.50   | 9  | 0.00    | 13 | 0.00 | 1 |  |
| 316 | -20 | -63 | Min. | 0.00   | 54.14   | 9  | -14.22 | 1 | -21.33 | 5  | 31.97   | 13 | -55.32  | 9  | 0.00 | 1 |  |
| 316 | -20 | -63 | Min. | 130.42 |         |    |        |   | 0.84   | 13 |         |    | 0.47    | 13 |      |   |  |
| 316 | -20 | -63 | Min. | 150.00 | 1.62    | 9  | -14.22 | 1 | 0.00   | 5  | -4.80   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 316 | -65 | -20 | Max  | 0.00   | 8.05    | 9  | 31.09  | 1 | 0.00   | 3  | 18.62   | 13 | 0.00    | 13 | 0.00 | 5 |  |
| 316 | -65 | -20 | Max  | 75.95  |         |    |        |   | 7.08   | 13 |         |    | 7.07    | 13 |      |   |  |
| 316 | -65 | -20 | Max  | 150.00 | -44.47  | 9  | 31.09  | 1 | 46.64  | 1  | -18.15  | 13 | 0.35    | 13 | 0.00 | 5 |  |
| 316 | -65 | -20 | Min. | 0.00   | -27.61  | 13 | -31.09 | 5 | 0.00   | 5  | -32.32  | 9  | 0.00    | 9  | 0.00 | 3 |  |
| 316 | -65 | -20 | Min. | 3.38   |         |    |        |   | 1.05   | 3  |         |    | 0.01    | 3  |      |   |  |
| 316 | -65 | -20 | Min. | 150.00 | -80.13  | 13 | -31.09 | 5 | -46.64 | 5  | -69.09  | 9  | -76.05  | 9  | 0.00 | 3 |  |
| 317 | -21 | -51 | Max  | 0.00   | 70.46   | 13 | 14.22  | 5 | 21.33  | 1  | 55.27   | 9  | -20.38  | 13 | 0.00 | 1 |  |
| 317 | -21 | -51 | Max  | 130.42 |         |    |        |   | 0.84   | 13 |         |    | 0.47    | 13 |      |   |  |
| 317 | -21 | -51 | Max  | 150.00 | 17.94   | 13 | 14.22  | 5 | 0.00   | 1  | 18.50   | 9  | 0.00    | 13 | 0.00 | 1 |  |
| 317 | -21 | -51 | Min. | 0.00   | 54.14   | 9  | -14.22 | 1 | -21.33 | 5  | 31.97   | 13 | -55.32  | 9  | 0.00 | 1 |  |
| 317 | -21 | -51 | Min. | 130.42 |         |    |        |   | 0.84   | 13 |         |    | 0.47    | 13 |      |   |  |
| 317 | -21 | -51 | Min. | 150.00 | 1.62    | 9  | -14.22 | 1 | 0.00   | 5  | -4.80   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 317 | -50 | -21 | Max  | 0.00   | 8.05    | 9  | 31.09  | 1 | 0.00   | 7  | 18.62   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 317 | -50 | -21 | Max  | 75.95  |         |    |        |   | 7.08   | 13 |         |    | 7.07    | 13 |      |   |  |
| 317 | -50 | -21 | Max  | 150.00 | -44.47  | 9  | 31.09  | 1 | 46.64  | 1  | -18.15  | 13 | 0.35    | 13 | 0.00 | 1 |  |
| 317 | -50 | -21 | Min. | 0.00   | -27.61  | 13 | -31.09 | 5 | 0.00   | 1  | -32.32  | 9  | 0.00    | 13 | 0.00 | 5 |  |
| 317 | -50 | -21 | Min. | 3.38   |         |    |        |   | 1.05   | 3  |         |    | 0.01    | 3  |      |   |  |
| 317 | -50 | -21 | Min. | 150.00 | -80.13  | 13 | -31.09 | 5 | -46.64 | 5  | -69.09  | 9  | -76.05  | 9  | 0.00 | 5 |  |
| 318 | -22 | -53 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |  |
| 318 | -22 | -53 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 318 | -22 | -53 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |  |
| 318 | -22 | -53 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |  |
| 318 | -22 | -53 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 318 | -22 | -53 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 318 | -52 | -22 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 5  | 24.48   | 13 | 0.00    | 13 | 0.00 | 5 |  |
| 318 | -52 | -22 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 318 | -52 | -22 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5 |  |
| 318 | -52 | -22 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 11 | 0.00 | 3 |  |
| 318 | -52 | -22 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 318 | -52 | -22 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 3 |  |
| 319 | -23 | -55 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |  |
| 319 | -23 | -55 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 319 | -23 | -55 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |  |
| 319 | -23 | -55 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |  |
| 319 | -23 | -55 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 319 | -23 | -55 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 319 | -54 | -23 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 1  | 24.48   | 13 | 0.00    | 1  | 0.00 | 5 |  |
| 319 | -54 | -23 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 319 | -54 | -23 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5 |  |
| 319 | -54 | -23 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 5  | -51.87  | 9  | 0.00    | 1  | 0.00 | 1 |  |
| 319 | -54 | -23 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 319 | -54 | -23 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 1 |  |
| 320 | -24 | -57 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |  |
| 320 | -24 | -57 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 320 | -24 | -57 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |  |
| 320 | -24 | -57 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |  |
| 320 | -24 | -57 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 320 | -24 | -57 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 320 | -56 | -24 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 7  | 24.48   | 13 | 0.00    | 15 | 0.00 | 1 |  |
| 320 | -56 | -24 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 320 | -56 | -24 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 1 |  |
| 320 | -56 | -24 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 9  | 0.00 | 7 |  |
| 320 | -56 | -24 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 320 | -56 | -24 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 7 |  |
| 322 | -25 | -41 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |  |
| 322 | -25 | -41 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 322 | -25 | -41 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |  |
| 322 | -25 | -41 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |  |
| 322 | -25 | -41 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |  |
| 322 | -25 | -41 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |  |
| 322 | -64 | -25 | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 5  | 24.48   | 13 | 0.00    | 9  | 0.00 | 5 |  |
| 322 | -64 | -25 | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 322 | -64 | -25 | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5 |  |
| 322 | -64 | -25 | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 15 | 0.00 | 3 |  |
| 322 | -64 | -25 | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |  |
| 322 | -64 | -25 | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 |    |         |    |         |    |      |   |  |

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|-----|------|------|------|--------|---------|----|--------|---|--------|----|---------|----|---------|----|------|---|
| 323 | -76  | -26  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 5  | -51.87  | 9  | 0.00    | 9  | 0.00 | 3 |
| 323 | -76  | -26  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 323 | -76  | -26  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 3 |
| 324 | -27  | -79  | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |
| 324 | -27  | -79  | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 324 | -27  | -79  | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 324 | -27  | -79  | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 324 | -27  | -79  | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 324 | -27  | -79  | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 324 | -78  | -27  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 5  | 24.48   | 13 | 0.00    | 13 | 0.00 | 5 |
| 324 | -78  | -27  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 324 | -78  | -27  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5 |
| 324 | -78  | -27  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 9  | 0.00 | 3 |
| 324 | -78  | -27  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 324 | -78  | -27  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 3 |
| 325 | -28  | -81  | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |
| 325 | -28  | -81  | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 325 | -28  | -81  | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 325 | -28  | -81  | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 325 | -28  | -81  | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 325 | -28  | -81  | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 325 | -80  | -28  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 3  | 24.48   | 13 | 0.00    | 13 | 0.00 | 1 |
| 325 | -80  | -28  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 325 | -80  | -28  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 1 |
| 325 | -80  | -28  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 5  | -51.87  | 9  | 0.00    | 9  | 0.00 | 7 |
| 325 | -80  | -28  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 325 | -80  | -28  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 7 |
| 326 | -29  | -83  | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |
| 326 | -29  | -83  | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 326 | -29  | -83  | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 326 | -29  | -83  | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 326 | -29  | -83  | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 326 | -29  | -83  | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 326 | -82  | -29  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 7  | 24.48   | 13 | 0.00    | 13 | 0.00 | 3 |
| 326 | -82  | -29  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 326 | -82  | -29  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 3 |
| 326 | -82  | -29  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 9  | 0.00 | 5 |
| 326 | -82  | -29  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 326 | -82  | -29  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 5 |
| 327 | -30  | -85  | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |
| 327 | -30  | -85  | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 327 | -30  | -85  | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 327 | -30  | -85  | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 327 | -30  | -85  | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 327 | -30  | -85  | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 327 | -84  | -30  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 5  | 24.48   | 13 | 0.00    | 15 | 0.00 | 1 |
| 327 | -84  | -30  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 327 | -84  | -30  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 1 |
| 327 | -84  | -30  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 3  | -51.87  | 9  | 0.00    | 9  | 0.00 | 5 |
| 327 | -84  | -30  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 327 | -84  | -30  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 5 |
| 329 | -32  | -86  | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |
| 329 | -32  | -86  | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 329 | -32  | -86  | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 329 | -32  | -86  | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 329 | -32  | -86  | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 329 | -32  | -86  | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 329 | -87  | -32  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 7  | 24.48   | 13 | 0.00    | 13 | 0.00 | 1 |
| 329 | -87  | -32  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 329 | -87  | -32  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 1 |
| 329 | -87  | -32  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 9  | 0.00 | 5 |
| 329 | -87  | -32  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 329 | -87  | -32  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 5 |
| 330 | -33  | -89  | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |
| 330 | -33  | -89  | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 330 | -33  | -89  | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 330 | -33  | -89  | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 330 | -33  | -89  | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 330 | -33  | -89  | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 330 | -88  | -33  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 7  | 24.48   | 13 | 0.00    | 9  | 0.00 | 5 |
| 330 | -88  | -33  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 330 | -88  | -33  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 5 |
| 330 | -88  | -33  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 1  | -51.87  | 9  | 0.00    | 13 | 0.00 | 3 |
| 330 | -88  | -33  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 330 | -88  | -33  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 3 |
| 331 | -34  | -61  | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |
| 331 | -34  | -61  | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 331 | -34  | -61  | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 331 | -34  | -61  | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 331 | -34  | -61  | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 331 | -34  | -61  | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 331 | -62  | -34  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 1  | 24.48   | 13 | 0.00    | 1  | 0.00 | 1 |
| 331 | -62  | -34  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 331 | -62  | -34  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 1 |
| 331 | -62  | -34  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 5  | -51.87  | 9  | 0.00    | 1  | 0.00 | 5 |
| 331 | -62  | -34  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 331 | -62  | -34  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 5 |
| 332 | -35  | -102 | Max  | 0.00   | 100.71  | 13 | 21.32  | 5 | 31.97  | 1  | 79.42   | 9  | -30.55  | 13 | 0.00 | 1 |
| 332 | -35  | -102 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 332 | -35  | -102 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 332 | -35  | -102 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 332 | -35  | -102 | Min. | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 332 | -35  | -102 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 332 | -101 | -35  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 1  | 24.48   | 13 | 0.00    | 11 | 0.00 | 3 |
| 332 | -101 | -35  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 332 | -101 | -35  | Max  | 1      |         |    |        |   |        |    |         |    |         |    |      |   |





|     |      |      |      |        |         |    |        |   |        |    |         |    |         |    |      |   |
|-----|------|------|------|--------|---------|----|--------|---|--------|----|---------|----|---------|----|------|---|
| 333 | -37  | -103 | Max  | 150.00 | 31.78   | 13 | 21.32  | 5 | 0.00   | 1  | 31.15   | 9  | 0.00    | 13 | 0.00 | 1 |
| 333 | -37  | -103 | Min. | 0.00   | 76.26   | 9  | -21.32 | 1 | -31.97 | 5  | 44.50   | 13 | -82.93  | 9  | 0.00 | 1 |
| 333 | -37  | -103 | Max  | 138.30 |         |    |        |   | 0.75   | 13 |         |    | 0.22    | 13 |      |   |
| 333 | -37  | -103 | Min. | 150.00 | 7.33    | 9  | -21.32 | 1 | 0.00   | 5  | -3.77   | 13 | 0.00    | 9  | 0.00 | 1 |
| 333 | -104 | -37  | Max  | 0.00   | 7.17    | 9  | 46.60  | 1 | 0.00   | 1  | 24.48   | 13 | 0.00    | 13 | 0.00 | 1 |
| 333 | -104 | -37  | Max  | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 333 | -104 | -37  | Max  | 150.00 | -61.75  | 9  | 46.60  | 1 | 69.91  | 1  | -23.78  | 13 | 0.52    | 13 | 0.00 | 1 |
| 333 | -104 | -37  | Min. | 0.00   | -46.29  | 13 | -46.60 | 5 | 0.00   | 7  | -51.87  | 9  | 0.00    | 9  | 0.00 | 5 |
| 333 | -104 | -37  | Min. | 76.09  |         |    |        |   | 10.64  | 13 |         |    | 9.31    | 13 |      |   |
| 333 | -104 | -37  | Min. | 150.00 | -115.22 | 13 | -46.60 | 5 | -69.91 | 5  | -100.14 | 9  | -114.00 | 9  | 0.00 | 5 |
| 334 | -38  | -99  | Max  | 0.00   | 70.46   | 13 | 14.22  | 5 | 21.33  | 1  | 55.27   | 9  | -20.38  | 13 | 0.00 | 1 |
| 334 | -38  | -99  | Max  | 130.42 |         |    |        |   | 0.84   | 13 |         |    | 0.47    | 13 |      |   |
| 334 | -38  | -99  | Max  | 150.00 | 17.94   | 13 | 14.22  | 5 | 0.00   | 1  | 18.50   | 9  | 0.00    | 13 | 0.00 | 1 |
| 334 | -38  | -99  | Min. | 0.00   | 54.14   | 9  | -14.22 | 1 | -21.33 | 5  | 31.97   | 13 | -55.32  | 9  | 0.00 | 1 |
| 334 | -38  | -99  | Min. | 130.42 |         |    |        |   | 0.84   | 13 |         |    | 0.47    | 13 |      |   |
| 334 | -38  | -99  | Min. | 150.00 | 1.62    | 9  | -14.22 | 1 | 0.00   | 5  | -4.80   | 13 | 0.00    | 9  | 0.00 | 1 |
| 334 | -100 | -38  | Max  | 0.00   | 8.05    | 9  | 31.09  | 1 | 0.00   | 5  | 18.62   | 13 | 0.00    | 5  | 0.00 | 5 |
| 334 | -100 | -38  | Max  | 75.95  |         |    |        |   | 7.08   | 13 |         |    | 7.07    | 13 |      |   |
| 334 | -100 | -38  | Max  | 150.00 | -44.47  | 9  | 31.09  | 1 | 46.64  | 1  | -18.15  | 13 | 0.35    | 13 | 0.00 | 5 |
| 334 | -100 | -38  | Min. | 0.00   | -27.61  | 13 | -31.09 | 5 | 0.00   | 1  | -32.32  | 9  | 0.00    | 1  | 0.00 | 1 |
| 334 | -100 | -38  | Min. | 3.38   |         |    |        |   | 1.05   | 3  |         |    | 0.01    | 3  |      |   |
| 334 | -100 | -38  | Min. | 150.00 | -80.13  | 13 | -31.09 | 5 | -46.64 | 5  | -69.09  | 9  | -76.05  | 9  | 0.00 | 1 |

Tipo di combinazione di carico: SLD

| Asta | N1  | N2  | X    | N      | CC       | CC     | CC      | CC     | CC      | CC | CC      | CC | CC       | CC | CC     | CC |
|------|-----|-----|------|--------|----------|--------|---------|--------|---------|----|---------|----|----------|----|--------|----|
|      |     |     | <cm> | <daN>  | Ty       | Mz     | Tz      | My     | Mx      |    |         |    |          |    |        |    |
|      |     |     |      |        | <daN>    | <daNm> | <daN>   | <daNm> | <daNm>  |    |         |    |          |    |        |    |
| 1    | 1   | -5  | Max  | 0.00   | -1047.68 | 2      | 183.25  | 6      | 542.49  | 2  | 235.31  | 16 | 836.66   | 10 | 0.06   | 8  |
| 1    | 1   | -5  | Max  | 330.00 | -858.44  | 2      | 183.25  | 6      | 192.46  | 6  | 235.31  | 16 | 61.83    | 12 | 0.06   | 8  |
| 1    | 1   | -5  | Min. | 0.00   | -1319.71 | 6      | -302.71 | 2      | -412.28 | 6  | -235.31 | 10 | -836.66  | 16 | -0.06  | 2  |
| 1    | 1   | -5  | Min. | 330.00 | -1130.47 | 6      | -302.71 | 2      | -456.46 | 2  | -235.31 | 10 | -61.83   | 14 | -0.06  | 2  |
| 2    | 2   | -10 | Max  | 0.00   | -1395.59 | 6      | 401.41  | 6      | 438.20  | 2  | 288.57  | 14 | 1001.11  | 12 | 0.19   | 10 |
| 2    | 2   | -10 | Max  | 330.00 | -1206.35 | 6      | 401.41  | 6      | 674.29  | 6  | 288.57  | 14 | 50.65    | 10 | 0.19   | 10 |
| 2    | 2   | -10 | Min. | 0.00   | -1546.50 | 2      | -206.98 | 2      | -650.38 | 6  | -288.57 | 12 | -1001.11 | 14 | -0.19  | 16 |
| 2    | 2   | -10 | Min. | 330.00 | -1357.27 | 2      | -206.98 | 2      | -244.84 | 2  | -288.57 | 12 | -50.65   | 16 | -0.19  | 16 |
| 3    | 3   | 203 | Max  | 0.00   | -1576.55 | 2      | 224.41  | 6      | 589.34  | 2  | 318.86  | 14 | 1101.76  | 12 | 0.10   | 14 |
| 3    | 3   | 203 | Max  | 330.00 | -1387.31 | 2      | 224.41  | 6      | 283.17  | 6  | 318.86  | 14 | 49.53    | 12 | 0.10   | 14 |
| 3    | 3   | 203 | Min. | 0.00   | -1624.09 | 6      | -345.42 | 2      | -457.39 | 6  | -318.86 | 12 | -1101.76 | 14 | -0.10  | 12 |
| 3    | 3   | 203 | Min. | 330.00 | -1434.85 | 6      | -345.42 | 2      | -550.54 | 2  | -318.86 | 12 | -49.53   | 14 | -0.10  | 12 |
| 4    | 4   | 204 | Max  | 0.00   | -1423.57 | 2      | 295.03  | 2      | 534.41  | 6  | 281.50  | 12 | 999.60   | 14 | 0.00   | 8  |
| 4    | 4   | 204 | Max  | 330.00 | -1234.34 | 2      | 295.03  | 2      | 439.19  | 2  | 281.50  | 12 | 70.66    | 16 | 0.00   | 8  |
| 4    | 4   | 204 | Min. | 0.00   | -1423.57 | 2      | -295.03 | 6      | -534.41 | 2  | -281.50 | 14 | -999.60  | 10 | -0.00  | 2  |
| 4    | 4   | 204 | Min. | 330.00 | -1234.34 | 2      | -295.03 | 6      | -439.19 | 6  | -281.50 | 14 | -70.66   | 10 | -0.00  | 2  |
| 5    | 5   | 205 | Max  | 0.00   | -1576.55 | 6      | 224.41  | 2      | 589.34  | 6  | 318.86  | 10 | 1101.76  | 16 | 0.10   | 10 |
| 5    | 5   | 205 | Max  | 330.00 | -1387.31 | 6      | 224.41  | 2      | 283.17  | 2  | 318.86  | 10 | 49.53    | 16 | 0.10   | 10 |
| 5    | 5   | 205 | Min. | 0.00   | -1624.09 | 2      | -345.42 | 6      | -457.39 | 2  | -318.86 | 16 | -1101.77 | 10 | -0.10  | 16 |
| 5    | 5   | 205 | Min. | 330.00 | -1434.85 | 2      | -345.42 | 6      | -550.54 | 6  | -318.86 | 16 | -49.53   | 10 | -0.10  | 16 |
| 6    | 6   | -31 | Max  | 0.00   | -1395.59 | 2      | 401.42  | 2      | 438.20  | 6  | 288.57  | 10 | 1001.11  | 16 | 0.19   | 14 |
| 6    | 6   | -31 | Max  | 330.00 | -1206.35 | 2      | 401.42  | 2      | 674.29  | 2  | 288.57  | 10 | 50.65    | 14 | 0.19   | 14 |
| 6    | 6   | -31 | Min. | 0.00   | -1546.50 | 6      | -206.98 | 6      | -650.38 | 2  | -288.57 | 16 | -1001.11 | 10 | -0.19  | 12 |
| 6    | 6   | -31 | Min. | 330.00 | -1357.27 | 6      | -206.98 | 6      | -244.84 | 6  | -288.57 | 16 | -50.65   | 12 | -0.19  | 12 |
| 7    | 7   | -36 | Max  | 0.00   | -1047.68 | 6      | 183.25  | 2      | 542.50  | 6  | 235.31  | 12 | 836.66   | 14 | 0.06   | 6  |
| 7    | 7   | -36 | Max  | 330.00 | -858.44  | 6      | 183.25  | 2      | 192.45  | 2  | 235.31  | 12 | 61.82    | 16 | 0.06   | 6  |
| 7    | 7   | -36 | Min. | 0.00   | -1319.71 | 2      | -302.72 | 6      | -412.28 | 2  | -235.31 | 14 | -836.66  | 12 | -0.06  | 4  |
| 7    | 7   | -36 | Min. | 330.00 | -1130.47 | 2      | -302.72 | 6      | -456.47 | 6  | -235.31 | 14 | -61.83   | 10 | -0.06  | 4  |
| 201  | -4  | -3  | Max  | 0.00   | 38.95    | 6      | 38.95   | 10     | 53.80   | 16 | 216.51  | 2  | -237.61  | 2  | 8.51   | 10 |
| 201  | -4  | -3  | Max  | 133.53 | 38.95    | 6      | 38.95   | 10     | 5.96    | 6  | 152.11  | 2  | 8.51     | 2  | 8.51   | 10 |
| 201  | -4  | -3  | Min. | 0.00   | -38.95   | 2      | -38.95  | 14     | -53.80  | 10 | 216.51  | 2  | -254.62  | 6  | -8.51  | 14 |
| 201  | -4  | -3  | Min. | 133.53 | -38.95   | 2      | -38.95  | 14     | -5.96   | 4  | 152.11  | 2  | -8.51    | 6  | -8.51  | 14 |
| 201  | -5  | -4  | Max  | 0.00   | 95.46    | 6      | 95.46   | 10     | 132.33  | 16 | 470.88  | 2  | -583.82  | 2  | 21.26  | 10 |
| 201  | -5  | -4  | Max  | 79.47  | 95.46    | 6      | 95.46   | 10     | 56.47   | 16 | 432.55  | 2  | -224.85  | 2  | 21.26  | 10 |
| 201  | -5  | -4  | Min. | 0.00   | -95.46   | 2      | -95.46  | 14     | -132.33 | 10 | 470.88  | 2  | -626.33  | 6  | -21.26 | 14 |
| 201  | -5  | -4  | Min. | 79.47  | -95.46   | 2      | -95.46  | 14     | -56.47  | 10 | 432.55  | 2  | -267.37  | 6  | -21.26 | 14 |
| 201  | -6  | -5  | Max  | 0.00   | 180.46   | 2      | 113.05  | 16     | 71.15   | 16 | -361.48 | 2  | 75.14    | 2  | 40.57  | 14 |
| 201  | -6  | -5  | Max  | 54.07  | 180.46   | 2      | 113.05  | 16     | 132.28  | 16 | -387.56 | 2  | -127.35  | 2  | 40.57  | 14 |
| 201  | -6  | -5  | Min. | 0.00   | -61.00   | 8      | -113.05 | 10     | -71.15  | 10 | -633.51 | 6  | -469.22  | 6  | -40.57 | 12 |
| 201  | -6  | -5  | Min. | 54.07  | -61.00   | 8      | -113.05 | 10     | -132.28 | 10 | -659.59 | 6  | -818.79  | 6  | -40.57 | 12 |
| 201  | -7  | -6  | Max  | 0.00   | 125.24   | 2      | 57.84   | 16     | 6.93    | 6  | -81.04  | 2  | 239.10   | 2  | 27.82  | 14 |
| 201  | -7  | -6  | Max  | 133.53 | 125.24   | 2      | 57.84   | 16     | 73.83   | 16 | -145.44 | 2  | 87.89    | 2  | 27.82  | 14 |
| 201  | -7  | -6  | Min. | 0.00   | -5.78    | 8      | -57.84  | 10     | -6.93   | 4  | -353.07 | 6  | 32.49    | 6  | -27.82 | 12 |
| 201  | -7  | -6  | Min. | 133.53 | -5.78    | 8      | -57.84  | 10     | -73.83  | 10 | -417.47 | 6  | -481.97  | 6  | -27.82 | 12 |
| 201  | -8  | -7  | Max  | 0.00   | 65.98    | 2      | 11.09   | 6      | 1.53    | 8  | 199.41  | 2  | 159.71   | 6  | 15.06  | 14 |
| 201  | -8  | -7  | Max  | 46.84  |          |        |         |        | 3.01    | 12 |         |    | 119.11   | 12 |        |    |
| 201  | -8  | -7  | Max  | 133.53 | 65.98    | 2      | 11.09   | 6      | 15.86   | 6  | 135.01  | 2  | 251.85   | 2  | 15.06  | 14 |
| 201  | -8  | -7  | Min. | 0.00   | 53.48    | 8      | -11.09  | 4      | -1.53   | 2  | -72.62  | 6  | 28.58    | 2  | -15.06 | 12 |
| 201  | -8  | -7  | Min. | 46.84  |          |        |         |        | 3.01    | 12 |         |    | 119.11   | 12 |        |    |
| 201  | -8  | -7  | Min. | 133.53 | 53.48    | 8      | -11.09  | 4      | -15.86  | 4  | -137.03 | 6  | 19.74    | 6  | -15.06 | 12 |
| 201  | -9  | -8  | Max  | 0.00   | 112.75   | 6      | 66.56   | 12     | 86.61   | 14 | 479.86  | 2  | -87.55   | 6  | 3.25   | 4  |
| 201  | -9  | -8  | Max  | 133.53 | 112.75   | 6      | 66.56   | 12     | 10.46   | 8  | 415.45  | 2  | 146.96   | 6  | 3.25   | 4  |
| 201  | -9  | -8  | Min. | 0.00   | 6.71     | 4      | -66.56  | 14     | -86.61  | 12 | 207.83  | 6  | -556.44  | 2  | -3.25  | 6  |
| 201  | -9  | -8  | Min. | 133.53 | 6.71     | 4      | -66.56  | 14     | -10.46  | 2  | 143.42  | 6  | 41.33    | 2  | -3.25  | 6  |
| 201  | -10 | -9  | Max  | 0.00   | 167.51   | 6      | 121.33  | 12     | 139.93  | 16 | 717.76  | 2  | -297.42  | 6  | 12.12  | 10 |
| 201  | -10 | -9  | Max  | 45.33  | 167.51   | 6      | 121.33  | 12     | 87.59   | 16 | 695.90  | 2  | -100.31  | 6  | 12.12  | 10 |
| 201  | -10 | -9  | Min. | 0.00   | -48.06   | 4      | -121.33 | 14     | -139.93 | 10 | 445.73  | 6  | -864.12  | 2  | -12.12 | 16 |
| 201  | -10 | -9  | Min. | 45.33  | -48.06   | 4      | -121.33 | 14     | -87.59  | 10 | 423.87  | 6  | -543.69  | 2  | -12.12 | 16 |
| 202  | -11 | -10 | Max  | 0.00   | 132.13   | 2      | 144.49  | 16     | 15.26   | 14 | -596.96 | 2  | -74.00   | 2  | 38.53  | 16 |
| 202  | -11 | -10 | Max  | 88.20  | 132.13   | 2      | 144.49  | 16     | 140.12  | 16 | -639.50 | 2  | -619.28  | 2  | 38.53  | 16 |
| 202  | -11 | -10 | Min. | 0.00   | -207.10  | 6      | -144.49 | 10     | -15.26  | 12 | -718.08 | 6  | -319.60  | 6  | -38.53 | 10 |
| 202  | -11 | -10 | Min. | 88.20  | -207.10  | 6      | -144.49 | 10     | -140.12 | 10 | -760.62 | 6  | -971.71  | 6  | -38.53 | 10 |
| 202  | -12 | -11 | Max  | 0.00   | 75.17    | 2      | 87.54   | 16     | 101.54  | 10 | -316.52 |    |          |    |        |    |



|     |     |     |      |        |         |   |         |    |         |    |         |   |          |   |        |    |
|-----|-----|-----|------|--------|---------|---|---------|----|---------|----|---------|---|----------|---|--------|----|
| 202 | -15 | -14 | Max  | 0.00   | 27.65   | 6 | 94.31   | 12 | 33.44   | 14 | 524.82  | 2 | -108.00  | 6 | 12.61  | 12 |
| 202 | -15 | -14 | Max  | 133.53 | 27.65   | 6 | 94.31   | 12 | 92.49   | 12 | 460.42  | 2 | 388.09   | 6 | 12.61  | 12 |
| 202 | -15 | -14 | Min. | 0.00   | -102.62 | 4 | -94.31  | 14 | -33.44  | 12 | 403.71  | 6 | -407.30  | 2 | -12.61 | 14 |
| 202 | -15 | -14 | Min. | 133.53 | -102.62 | 4 | -94.31  | 14 | -92.49  | 14 | 339.30  | 6 | 250.51   | 2 | -12.61 | 14 |
| 202 | 203 | -15 | Max  | 0.00   | 84.57   | 6 | 151.23  | 12 | 163.35  | 14 | 783.15  | 2 | -682.60  | 6 | 25.36  | 12 |
| 202 | 203 | -15 | Max  | 87.67  | 84.57   | 6 | 151.23  | 12 | 33.32   | 16 | 740.87  | 2 | -120.75  | 6 | 25.36  | 12 |
| 202 | 203 | -15 | Min. | 0.00   | -159.55 | 2 | -151.23 | 14 | -163.35 | 12 | 662.03  | 6 | -1062.58 | 2 | -25.36 | 14 |
| 202 | 203 | -15 | Min. | 87.67  | -159.55 | 2 | -151.23 | 14 | -33.32  | 10 | 619.75  | 6 | -394.55  | 2 | -25.36 | 14 |
| 203 | -16 | 203 | Max  | 0.00   | 159.07  | 2 | 144.82  | 16 | 98.65   | 14 | -582.04 | 2 | -239.99  | 2 | 24.20  | 16 |
| 203 | -16 | 203 | Max  | 45.87  | 159.07  | 2 | 144.82  | 16 | 163.25  | 14 | -604.16 | 2 | -512.02  | 2 | 24.20  | 16 |
| 203 | -16 | 203 | Min. | 0.00   | -113.04 | 8 | -144.82 | 10 | -98.65  | 12 | -750.70 | 6 | -616.35  | 6 | -24.20 | 10 |
| 203 | -16 | 203 | Min. | 45.87  | -113.04 | 8 | -144.82 | 10 | -163.25 | 12 | -772.82 | 6 | -965.75  | 6 | -24.20 | 10 |
| 203 | -17 | -16 | Max  | 0.00   | 104.28  | 2 | 90.03   | 16 | 21.72   | 10 | -301.60 | 2 | 218.49   | 2 | 11.45  | 16 |
| 203 | -17 | -16 | Max  | 133.53 | 104.28  | 2 | 90.03   | 16 | 98.50   | 16 | -366.00 | 2 | -227.25  | 2 | 11.45  | 16 |
| 203 | -17 | -16 | Min. | 0.00   | -58.24  | 8 | -90.03  | 10 | -21.72  | 16 | -470.25 | 6 | 41.83    | 6 | -11.45 | 10 |
| 203 | -17 | -16 | Min. | 133.53 | -58.24  | 8 | -90.03  | 10 | -98.50  | 10 | -534.66 | 6 | -629.12  | 6 | -11.45 | 10 |
| 203 | -18 | -17 | Max  | 0.00   | 45.01   | 2 | 30.76   | 16 | 60.12   | 10 | -21.15  | 2 | 325.52   | 6 | 1.33   | 12 |
| 203 | -18 | -17 | Max  | 133.53 | 45.01   | 2 | 30.76   | 16 | 21.57   | 12 | -85.55  | 2 | 231.23   | 2 | 1.33   | 12 |
| 203 | -18 | -17 | Min. | 0.00   | 1.02    | 8 | -30.76  | 10 | -60.12  | 16 | -189.81 | 6 | 302.48   | 2 | -1.33  | 14 |
| 203 | -18 | -17 | Min. | 133.53 | 1.02    | 8 | -30.76  | 10 | -21.57  | 14 | -254.21 | 6 | 29.07    | 6 | -1.33  | 14 |
| 203 | -19 | -18 | Max  | 0.00   | 60.28   | 6 | 32.50   | 12 | 19.38   | 10 | 259.30  | 2 | 234.73   | 6 | 14.08  | 12 |
| 203 | -19 | -18 | Max  | 133.53 | 60.28   | 6 | 32.50   | 12 | 59.99   | 12 | 194.90  | 2 | 315.22   | 2 | 14.08  | 12 |
| 203 | -19 | -18 | Min. | 0.00   | -14.25  | 4 | -32.50  | 14 | -19.38  | 16 | 90.64   | 6 | 11.96    | 2 | -14.08 | 14 |
| 203 | -19 | -18 | Min. | 133.53 | -14.25  | 4 | -32.50  | 14 | -59.99  | 14 | 26.24   | 6 | 312.77   | 6 | -14.08 | 14 |
| 203 | -20 | -19 | Max  | 0.00   | 119.55  | 6 | 91.77   | 12 | 103.27  | 14 | 539.75  | 2 | -230.53  | 6 | 26.84  | 12 |
| 203 | -20 | -19 | Max  | 133.53 | 119.55  | 6 | 91.77   | 12 | 19.27   | 12 | 475.34  | 2 | 221.99   | 6 | 26.84  | 12 |
| 203 | -20 | -19 | Min. | 0.00   | -73.52  | 4 | -91.77  | 14 | -103.27 | 12 | 371.09  | 6 | -653.01  | 2 | -26.84 | 14 |
| 203 | -20 | -19 | Min. | 133.53 | -73.52  | 4 | -91.77  | 14 | -19.27  | 14 | 306.68  | 6 | 24.73    | 2 | -26.84 | 14 |
| 203 | 204 | -20 | Max  | 0.00   | 159.52  | 6 | 131.73  | 12 | 127.83  | 16 | 701.50  | 2 | -344.64  | 6 | 35.34  | 12 |
| 203 | 204 | -20 | Max  | 20.00  | 159.52  | 6 | 131.73  | 12 | 102.28  | 16 | 691.85  | 2 | -239.04  | 6 | 35.34  | 12 |
| 203 | 204 | -20 | Min. | 0.00   | -113.48 | 4 | -131.73 | 14 | -127.83 | 10 | 532.84  | 6 | -783.83  | 2 | -35.34 | 14 |
| 203 | 204 | -20 | Min. | 20.00  | -113.48 | 4 | -131.73 | 14 | -102.28 | 10 | 523.19  | 6 | -644.50  | 2 | -35.34 | 14 |
| 204 | 204 | -21 | Max  | 0.00   | 159.52  | 2 | 131.73  | 16 | 127.83  | 12 | 701.50  | 6 | -344.64  | 2 | 35.34  | 16 |
| 204 | 204 | -21 | Max  | 20.00  | 159.52  | 2 | 131.73  | 16 | 102.28  | 12 | 691.85  | 6 | -239.04  | 2 | 35.34  | 16 |
| 204 | 204 | -21 | Min. | 0.00   | -113.48 | 8 | -131.73 | 10 | -127.83 | 14 | 532.84  | 2 | -783.83  | 6 | -35.34 | 10 |
| 204 | 204 | -21 | Min. | 20.00  | -113.48 | 8 | -131.73 | 10 | -102.28 | 14 | 523.19  | 2 | -644.50  | 6 | -35.34 | 10 |
| 204 | -21 | -22 | Max  | 0.00   | 119.55  | 2 | 91.77   | 16 | 103.27  | 10 | 539.74  | 6 | -230.53  | 2 | 26.84  | 16 |
| 204 | -21 | -22 | Max  | 133.53 | 119.55  | 2 | 91.77   | 16 | 19.27   | 16 | 475.34  | 6 | 221.99   | 2 | 26.84  | 16 |
| 204 | -21 | -22 | Min. | 0.00   | -73.52  | 8 | -91.77  | 10 | -103.27 | 16 | 371.09  | 2 | -653.01  | 6 | -26.84 | 10 |
| 204 | -21 | -22 | Min. | 133.53 | -73.52  | 8 | -91.77  | 10 | -19.27  | 10 | 306.68  | 2 | 24.73    | 6 | -26.84 | 10 |
| 204 | -22 | -23 | Max  | 0.00   | 60.28   | 2 | 32.50   | 16 | 19.38   | 14 | 259.30  | 6 | 234.73   | 2 | 14.08  | 16 |
| 204 | -22 | -23 | Max  | 133.53 | 60.28   | 2 | 32.50   | 16 | 59.99   | 16 | 194.90  | 6 | 315.22   | 6 | 14.08  | 16 |
| 204 | -22 | -23 | Min. | 0.00   | -14.25  | 8 | -32.50  | 10 | -19.38  | 12 | 90.64   | 2 | 11.96    | 6 | -14.08 | 10 |
| 204 | -22 | -23 | Min. | 133.53 | -14.25  | 8 | -32.50  | 10 | -59.99  | 10 | 26.24   | 2 | 312.77   | 2 | -14.08 | 10 |
| 204 | -23 | -24 | Max  | 0.00   | 45.01   | 6 | 30.76   | 12 | 60.12   | 14 | -21.15  | 6 | 325.52   | 2 | 1.33   | 16 |
| 204 | -23 | -24 | Max  | 133.53 | 45.01   | 6 | 30.76   | 12 | 21.57   | 16 | -85.55  | 6 | 231.23   | 6 | 1.33   | 16 |
| 204 | -23 | -24 | Min. | 0.00   | 1.02    | 4 | -30.76  | 14 | -60.12  | 12 | -189.81 | 2 | 302.48   | 6 | -1.33  | 10 |
| 204 | -23 | -24 | Min. | 133.53 | 1.02    | 4 | -30.76  | 14 | -21.57  | 10 | -254.21 | 2 | 29.06    | 2 | -1.33  | 10 |
| 204 | -24 | -25 | Max  | 0.00   | 104.28  | 6 | 90.03   | 12 | 21.72   | 14 | -301.60 | 6 | 218.48   | 6 | 11.45  | 12 |
| 204 | -24 | -25 | Max  | 133.53 | 104.28  | 6 | 90.03   | 12 | 98.50   | 12 | -366.00 | 6 | -227.25  | 6 | 11.45  | 12 |
| 204 | -24 | -25 | Min. | 0.00   | -58.24  | 4 | -90.03  | 14 | -21.72  | 12 | -470.25 | 2 | 41.82    | 2 | -11.45 | 14 |
| 204 | -24 | -25 | Min. | 133.53 | -58.24  | 4 | -90.03  | 14 | -98.50  | 14 | -534.66 | 2 | -629.12  | 2 | -11.45 | 14 |
| 204 | -25 | 205 | Max  | 0.00   | 159.07  | 6 | 144.82  | 12 | 98.65   | 10 | -582.04 | 6 | -239.99  | 6 | 24.20  | 12 |
| 204 | -25 | 205 | Max  | 45.87  | 159.07  | 6 | 144.82  | 12 | 163.25  | 10 | -604.16 | 6 | -512.02  | 6 | 24.20  | 12 |
| 204 | -25 | 205 | Min. | 0.00   | -113.04 | 4 | -144.82 | 14 | -98.65  | 16 | -750.70 | 2 | -616.35  | 2 | -24.20 | 14 |
| 204 | -25 | 205 | Min. | 45.87  | -113.04 | 4 | -144.82 | 14 | -163.25 | 16 | -772.82 | 2 | -965.75  | 2 | -24.20 | 14 |
| 205 | 205 | -26 | Max  | 0.00   | 84.57   | 2 | 151.23  | 16 | 163.35  | 10 | 783.15  | 6 | -682.60  | 2 | 25.36  | 16 |
| 205 | 205 | -26 | Max  | 87.67  | 84.57   | 2 | 151.23  | 16 | 33.32   | 12 | 740.87  | 6 | -120.75  | 2 | 25.36  | 16 |
| 205 | 205 | -26 | Min. | 0.00   | -159.55 | 6 | -151.23 | 10 | -163.35 | 16 | 662.03  | 2 | -1062.58 | 6 | -25.36 | 10 |
| 205 | 205 | -26 | Min. | 87.67  | -159.55 | 6 | -151.23 | 10 | -33.32  | 14 | 619.75  | 2 | -394.56  | 6 | -25.36 | 10 |
| 205 | -26 | -27 | Max  | 0.00   | 27.65   | 2 | 94.31   | 16 | 33.44   | 10 | 524.82  | 6 | -107.98  | 2 | 12.61  | 16 |
| 205 | -26 | -27 | Max  | 133.53 | 27.65   | 2 | 94.31   | 16 | 92.49   | 16 | 460.42  | 6 | 388.10   | 2 | 12.61  | 16 |
| 205 | -26 | -27 | Min. | 0.00   | -102.62 | 8 | -94.31  | 10 | -33.44  | 16 | 403.70  | 2 | -407.28  | 6 | -12.61 | 10 |
| 205 | -26 | -27 | Min. | 133.53 | -102.62 | 8 | -94.31  | 10 | -92.49  | 10 | 339.30  | 2 | 250.53   | 6 | -12.61 | 10 |
| 205 | -27 | -28 | Max  | 0.00   | -31.62  | 2 | 35.04   | 16 | 92.56   | 14 | 244.38  | 6 | 400.84   | 2 | 0.28   | 6  |
| 205 | -27 | -28 | Max  | 133.53 | -31.62  | 2 | 35.04   | 16 | 136.60  | 16 | 179.97  | 6 | 522.43   | 2 | 0.28   | 6  |
| 205 | -27 | -28 | Min. | 0.00   | -43.35  | 8 | -35.04  | 10 | -92.56  | 12 | 123.26  | 2 | 237.76   | 6 | -0.28  | 4  |
| 205 | -27 | -28 | Min. | 133.53 | -43.35  | 8 | -35.04  | 10 | -136.60 | 10 | 58.86   | 2 | 521.08   | 6 | -0.28  | 4  |
| 205 | -28 | -29 | Max  | 0.00   | 15.91   | 6 | 28.27   | 12 | 136.62  | 14 | -36.07  | 6 | 535.18   | 2 | 13.02  | 12 |
| 205 | -28 | -29 | Max  | 133.53 | 15.91   | 6 | 28.27   | 12 | 101.58  | 16 | -100.47 | 6 | 417.16   | 6 | 13.02  | 12 |
| 205 | -28 | -29 | Min. | 0.00   | -90.88  | 4 | -28.27  | 14 | -136.62 | 12 | -157.19 | 2 | 508.32   | 6 | -13.02 | 14 |
| 205 | -28 | -29 | Min. | 133.53 | -90.88  | 4 | -28.27  | 14 | -101.58 | 10 | -221.59 | 2 | 282.29   | 2 | -13.02 | 14 |
| 205 | -29 | -30 | Max  | 0.00   | 75.17   | 6 | 87.54   | 12 | 101.54  | 14 | -316.52 | 6 | 404.40   | 6 | 25.78  | 12 |
| 205 | -29 | -30 | Max  | 133.53 | 75.17   | 6 | 87.54   | 12 | 15.36   | 12 | -380.92 | 6 | -61.26   | 6 | 25.78  | 12 |
| 205 | -29 | -30 | Min. | 0.00   | -150.15 | 2 | -87.54  | 14 | -101.54 | 12 | -437.64 | 2 | 295.02   | 2 | -25.78 | 14 |
| 205 | -29 | -30 | Min. | 133.53 | -150.15 | 2 | -87.54  | 14 | -15.36  | 14 | -502.04 | 2 | -332.37  | 2 | -25.78 | 14 |
| 205 | -30 | -31 | Max  | 0.00   | 132.13  | 6 | 144.49  | 12 | 15.25   | 10 | -596.96 | 6 | -74.00   | 6 | 38.53  | 12 |
| 205 | -30 | -31 | Max  | 88.20  | 132.13  | 6 | 144.49  | 12 | 140.12  | 12 | -639.50 | 6 | -619.28  | 6 | 38.53  | 12 |
| 205 | -30 | -31 | Min. | 0.00   | -207.10 | 2 | -144.49 | 14 | -15.25  | 16 | -718.08 | 2 | -319.60  | 2 | -38.53 | 14 |
| 205 | -30 | -31 | Min. | 88.20  | -207.10 | 2 | -144.49 | 14 | -140.12 | 14 | -760.62 | 2 | -971.70  | 2 | -38.53 | 14 |
| 206 | -31 | -32 | Max  | 0.00   | 167.52  | 2 | 121.33  | 16 | 139.93  | 12 | 717.76  | 6 | -297.41  | 2 | 12.12  | 14 |
| 206 | -31 | -32 | Max  | 45.33  | 167.52  | 2 | 121.33  | 16 | 87.59   | 12 | 695.90  | 6 | -100.30  | 2 | 12.12  | 14 |
| 206 | -31 | -32 | Min. | 0.00   | -48.05  | 8 | -121.33 | 10 | -139.93 | 14 | 445.73  | 2 | -864.12  | 6 | -12.12 | 12 |
| 206 | -31 | -32 | Min. | 45.33  | -48.05  | 8 | -121.   |    |         |    |         |   |          |   |        |    |



|     |     |     |      |        |        |    |         |    |         |    |         |    |         |    |        |    |
|-----|-----|-----|------|--------|--------|----|---------|----|---------|----|---------|----|---------|----|--------|----|
| 206 | -35 | -36 | Min. | 54.07  | -61.00 | 4  | -113.05 | 14 | -132.28 | 14 | -659.59 | 2  | -818.78 | 2  | -40.57 | 16 |
| 206 | -36 | -37 | Max  | 0.00   | 95.46  | 2  | 95.46   | 14 | 132.33  | 12 | 470.88  | 2  | -583.83 | 6  | 21.26  | 14 |
| 206 | -36 | -37 | Max  | 79.47  | 95.46  | 2  | 95.46   | 14 | 56.48   | 12 | 432.55  | 2  | -224.86 | 6  | 21.26  | 14 |
| 206 | -36 | -37 | Min. | 0.00   | -95.46 | 6  | -95.46  | 10 | -132.33 | 14 | 470.88  | 2  | -626.35 | 2  | -21.26 | 10 |
| 206 | -36 | -37 | Min. | 79.47  | -95.46 | 6  | -95.46  | 10 | -56.48  | 14 | 432.55  | 2  | -267.38 | 2  | -21.26 | 10 |
| 206 | -37 | -38 | Max  | 0.00   | 38.95  | 2  | 38.95   | 14 | 53.79   | 12 | 216.51  | 2  | -237.60 | 6  | 8.51   | 14 |
| 206 | -37 | -38 | Max  | 133.53 | 38.95  | 2  | 38.95   | 14 | 5.96    | 8  | 152.11  | 2  | 8.51    | 6  | 8.51   | 14 |
| 206 | -37 | -38 | Min. | 0.00   | -38.95 | 6  | -38.95  | 10 | -53.79  | 14 | 216.51  | 2  | -254.61 | 2  | -8.51  | 10 |
| 206 | -37 | -38 | Min. | 133.53 | -38.95 | 6  | -38.95  | 10 | -5.96   | 2  | 152.11  | 2  | -8.50   | 2  | -8.51  | 10 |
| 301 | -3  | -60 | Max  | 0.00   | 65.65  | 14 | 5.84    | 6  | 8.75    | 2  | 48.40   | 10 | -30.68  | 14 | 0.00   | 2  |
| 301 | -3  | -60 | Max  | 150.00 | 13.13  | 14 | 5.84    | 6  | 0.00    | 2  | 11.63   | 10 | 0.00    | 14 | 0.00   | 2  |
| 301 | -3  | -60 | Min. | 0.00   | 58.95  | 10 | -5.84   | 2  | -8.75   | 6  | 38.84   | 14 | -45.02  | 10 | 0.00   | 2  |
| 301 | -3  | -60 | Min. | 150.00 | 6.43   | 10 | -5.84   | 2  | 0.00    | 6  | 2.07    | 14 | 0.00    | 10 | 0.00   | 2  |
| 301 | -59 | -3  | Max  | 0.00   | -2.46  | 10 | 12.76   | 2  | 0.00    | 2  | 3.60    | 14 | 0.00    | 2  | 0.00   | 2  |
| 301 | -59 | -3  | Max  | 14.70  |        |    |         |    | 0.56    | 14 |         |    | 0.26    | 14 |        |    |
| 301 | -59 | -3  | Max  | 150.00 | -54.98 | 10 | 12.76   | 2  | 19.14   | 2  | -33.17  | 14 | -22.18  | 14 | 0.00   | 2  |
| 301 | -59 | -3  | Min. | 0.00   | -17.10 | 14 | -12.76  | 6  | 0.00    | 6  | -17.30  | 10 | 0.00    | 2  | 0.00   | 6  |
| 301 | -59 | -3  | Min. | 14.70  |        |    |         |    | 0.56    | 14 |         |    | 0.26    | 14 |        |    |
| 301 | -59 | -3  | Min. | 150.00 | -69.62 | 14 | -12.76  | 6  | -19.14  | 6  | -54.07  | 10 | -53.53  | 10 | 0.00   | 6  |
| 302 | -4  | -47 | Max  | 0.00   | 93.50  | 14 | 8.75    | 6  | 13.12   | 2  | 69.12   | 10 | -45.99  | 14 | 0.00   | 2  |
| 302 | -4  | -47 | Max  | 150.00 | 24.58  | 14 | 8.75    | 6  | 0.00    | 2  | 20.86   | 10 | 0.00    | 14 | 0.00   | 2  |
| 302 | -4  | -47 | Min. | 0.00   | 83.47  | 10 | -8.75   | 2  | -13.12  | 6  | 54.79   | 14 | -67.49  | 10 | 0.00   | 2  |
| 302 | -4  | -47 | Min. | 150.00 | 14.54  | 10 | -8.75   | 2  | 0.00    | 6  | 6.53    | 14 | 0.00    | 10 | 0.00   | 2  |
| 302 | -46 | -4  | Max  | 0.00   | -8.59  | 10 | 19.13   | 2  | 0.00    | 6  | 1.97    | 14 | 0.00    | 6  | 0.00   | 6  |
| 302 | -46 | -4  | Max  | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 302 | -46 | -4  | Max  | 150.00 | -77.52 | 10 | 19.13   | 2  | 28.69   | 2  | -46.29  | 14 | -33.24  | 14 | 0.00   | 6  |
| 302 | -46 | -4  | Min. | 0.00   | -30.53 | 14 | -19.13  | 6  | 0.00    | 2  | -29.36  | 10 | 0.00    | 2  | 0.00   | 2  |
| 302 | -46 | -4  | Min. | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 302 | -46 | -4  | Min. | 150.00 | -99.46 | 14 | -19.13  | 6  | -28.69  | 6  | -77.63  | 10 | -80.24  | 10 | 0.00   | 2  |
| 303 | -6  | -48 | Max  | 0.00   | 93.50  | 14 | 8.75    | 6  | 13.12   | 2  | 69.12   | 10 | -45.99  | 14 | 0.00   | 2  |
| 303 | -6  | -48 | Max  | 150.00 | 24.58  | 14 | 8.75    | 6  | 0.00    | 2  | 20.86   | 10 | 0.00    | 14 | 0.00   | 2  |
| 303 | -6  | -48 | Min. | 0.00   | 83.47  | 10 | -8.75   | 2  | -13.12  | 6  | 54.79   | 14 | -67.49  | 10 | 0.00   | 2  |
| 303 | -6  | -48 | Min. | 150.00 | 14.54  | 10 | -8.75   | 2  | 0.00    | 6  | 6.53    | 14 | 0.00    | 10 | 0.00   | 2  |
| 303 | -49 | -6  | Max  | 0.00   | -8.59  | 10 | 19.13   | 2  | 0.00    | 8  | 1.97    | 14 | 0.00    | 10 | 0.00   | 4  |
| 303 | -49 | -6  | Max  | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 303 | -49 | -6  | Max  | 150.00 | -77.52 | 10 | 19.13   | 2  | 28.69   | 2  | -46.29  | 14 | -33.24  | 14 | 0.00   | 4  |
| 303 | -49 | -6  | Min. | 0.00   | -30.53 | 14 | -19.13  | 6  | 0.00    | 2  | -29.36  | 10 | 0.00    | 14 | 0.00   | 6  |
| 303 | -49 | -6  | Min. | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 303 | -49 | -6  | Min. | 150.00 | -99.46 | 14 | -19.13  | 6  | -28.69  | 6  | -77.63  | 10 | -80.24  | 10 | 0.00   | 6  |
| 304 | -7  | -96 | Max  | 0.00   | 93.50  | 14 | 8.75    | 6  | 13.12   | 2  | 69.12   | 10 | -45.99  | 14 | 0.00   | 2  |
| 304 | -7  | -96 | Max  | 150.00 | 24.58  | 14 | 8.75    | 6  | 0.00    | 2  | 20.86   | 10 | 0.00    | 14 | 0.00   | 2  |
| 304 | -7  | -96 | Min. | 0.00   | 83.47  | 10 | -8.75   | 2  | -13.12  | 6  | 54.79   | 14 | -67.49  | 10 | 0.00   | 2  |
| 304 | -7  | -96 | Min. | 150.00 | 14.54  | 10 | -8.75   | 2  | 0.00    | 6  | 6.53    | 14 | 0.00    | 10 | 0.00   | 2  |
| 304 | -95 | -7  | Max  | 0.00   | -8.59  | 10 | 19.13   | 2  | 0.00    | 6  | 1.97    | 14 | 0.00    | 2  | 0.00   | 2  |
| 304 | -95 | -7  | Max  | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 304 | -95 | -7  | Max  | 150.00 | -77.52 | 10 | 19.13   | 2  | 28.69   | 2  | -46.29  | 14 | -33.24  | 14 | 0.00   | 2  |
| 304 | -95 | -7  | Min. | 0.00   | -30.53 | 14 | -19.13  | 6  | 0.00    | 2  | -29.36  | 10 | 0.00    | 2  | 0.00   | 6  |
| 304 | -95 | -7  | Min. | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 304 | -95 | -7  | Min. | 150.00 | -99.46 | 14 | -19.13  | 6  | -28.69  | 6  | -77.63  | 10 | -80.24  | 10 | 0.00   | 6  |
| 305 | -8  | -66 | Max  | 0.00   | 93.50  | 14 | 8.75    | 6  | 13.12   | 2  | 69.12   | 10 | -45.99  | 14 | 0.00   | 2  |
| 305 | -8  | -66 | Max  | 150.00 | 24.58  | 14 | 8.75    | 6  | 0.00    | 2  | 20.86   | 10 | 0.00    | 14 | 0.00   | 2  |
| 305 | -8  | -66 | Min. | 0.00   | 83.47  | 10 | -8.75   | 2  | -13.12  | 6  | 54.79   | 14 | -67.49  | 10 | 0.00   | 2  |
| 305 | -8  | -66 | Min. | 150.00 | 14.54  | 10 | -8.75   | 2  | 0.00    | 6  | 6.53    | 14 | 0.00    | 10 | 0.00   | 2  |
| 305 | -67 | -8  | Max  | 0.00   | -8.59  | 10 | 19.13   | 2  | 0.00    | 6  | 1.97    | 14 | 0.00    | 14 | 0.00   | 4  |
| 305 | -67 | -8  | Max  | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 305 | -67 | -8  | Max  | 150.00 | -77.52 | 10 | 19.13   | 2  | 28.69   | 2  | -46.29  | 14 | -33.24  | 14 | 0.00   | 4  |
| 305 | -67 | -8  | Min. | 0.00   | -30.53 | 14 | -19.13  | 6  | 0.00    | 4  | -29.36  | 10 | 0.00    | 12 | 0.00   | 6  |
| 305 | -67 | -8  | Min. | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 305 | -67 | -8  | Min. | 150.00 | -99.46 | 14 | -19.13  | 6  | -28.69  | 6  | -77.63  | 10 | -80.24  | 10 | 0.00   | 6  |
| 306 | -9  | -69 | Max  | 0.00   | 93.50  | 14 | 8.75    | 6  | 13.12   | 2  | 69.12   | 10 | -45.99  | 14 | 0.00   | 2  |
| 306 | -9  | -69 | Max  | 150.00 | 24.58  | 14 | 8.75    | 6  | 0.00    | 2  | 20.86   | 10 | 0.00    | 14 | 0.00   | 2  |
| 306 | -9  | -69 | Min. | 0.00   | 83.47  | 10 | -8.75   | 2  | -13.12  | 6  | 54.79   | 14 | -67.49  | 10 | 0.00   | 2  |
| 306 | -9  | -69 | Min. | 150.00 | 14.54  | 10 | -8.75   | 2  | 0.00    | 6  | 6.53    | 14 | 0.00    | 10 | 0.00   | 2  |
| 306 | -68 | -9  | Max  | 0.00   | -8.59  | 10 | 19.13   | 2  | 0.00    | 14 | 1.97    | 14 | 0.00    | 14 | 0.00   | 10 |
| 306 | -68 | -9  | Max  | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 306 | -68 | -9  | Max  | 150.00 | -77.52 | 10 | 19.13   | 2  | 28.69   | 2  | -46.29  | 14 | -33.24  | 14 | 0.00   | 10 |
| 306 | -68 | -9  | Min. | 0.00   | -30.53 | 14 | -19.13  | 6  | 0.00    | 10 | -29.36  | 10 | 0.00    | 10 | 0.00   | 14 |
| 306 | -68 | -9  | Min. | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 306 | -68 | -9  | Min. | 150.00 | -99.46 | 14 | -19.13  | 6  | -28.69  | 6  | -77.63  | 10 | -80.24  | 10 | 0.00   | 14 |
| 307 | -11 | -70 | Max  | 0.00   | 93.50  | 14 | 8.75    | 6  | 13.12   | 2  | 69.12   | 10 | -45.99  | 14 | 0.00   | 2  |
| 307 | -11 | -70 | Max  | 150.00 | 24.58  | 14 | 8.75    | 6  | 0.00    | 2  | 20.86   | 10 | 0.00    | 14 | 0.00   | 2  |
| 307 | -11 | -70 | Min. | 0.00   | 83.47  | 10 | -8.75   | 2  | -13.12  | 6  | 54.79   | 14 | -67.49  | 10 | 0.00   | 2  |
| 307 | -11 | -70 | Min. | 150.00 | 14.54  | 10 | -8.75   | 2  | 0.00    | 6  | 6.53    | 14 | 0.00    | 10 | 0.00   | 2  |
| 307 | -71 | -11 | Max  | 0.00   | -8.59  | 10 | 19.13   | 2  | 0.00    | 8  | 1.97    | 14 | 0.00    | 14 | 0.00   | 6  |
| 307 | -71 | -11 | Max  | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 307 | -71 | -11 | Max  | 150.00 | -77.52 | 10 | 19.13   | 2  | 28.69   | 2  | -46.29  | 14 | -33.24  | 14 | 0.00   | 6  |
| 307 | -71 | -11 | Min. | 0.00   | -30.53 | 14 | -19.13  | 6  | 0.00    | 2  | -29.36  | 10 | 0.00    | 12 | 0.00   | 4  |
| 307 | -71 | -11 | Min. | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 307 | -71 | -11 | Min. | 150.00 | -99.46 | 14 | -19.13  | 6  | -28.69  | 6  | -77.63  | 10 | -80.24  | 10 | 0.00   | 4  |
| 308 | -12 | -72 | Max  | 0.00   | 93.50  | 14 | 8.75    | 6  | 13.12   | 2  | 69.12   | 10 | -45.99  | 14 | 0.00   | 2  |
| 308 | -12 | -72 | Max  | 150.00 | 24.58  | 14 | 8.75    | 6  | 0.00    | 2  | 20.86   | 10 | 0.00    | 14 | 0.00   | 2  |
| 308 | -12 | -72 | Min. | 0.00   | 83.47  | 10 | -8.75   | 2  | -13.12  | 6  | 54.79   | 14 | -67.49  | 10 | 0.00   | 2  |
| 308 | -12 | -72 | Min. | 150.00 | 14.54  | 10 | -8.75   | 2  | 0.00    | 6  | 6.53    | 14 | 0.00    | 10 | 0.00   | 2  |
| 308 | -73 | -12 | Max  | 0.00   | -8.59  | 10 | 19.13   | 2  | 0.00    | 14 | 1.97    | 14 | 0.00    | 14 | 0.00   | 2  |
| 308 | -73 | -12 | Max  | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 308 | -73 | -12 | Max  | 150.00 | -77.52 | 10 | 19.13   | 2  | 28.69   | 2  | -46.29  | 14 | -33.24  | 14 | 0.00   | 2  |
| 308 | -73 | -12 | Min. | 0.00   | -30.53 | 14 | -19.13  | 6  | 0.00    | 10 | -29.36  | 10 | 0.00    | 10 | 0.00   | 2  |
| 308 | -73 | -12 | Min. | 6.13   |        |    |         |    | 0.35    | 14 |         |    | 0.06    | 14 |        |    |
| 308 | -73 | -12 | Min. | 150.00 | -99.46 | 14 | -19.13  | 6  | -28.69  | 6  | -77.63  | 10 | -80.24  | 10 | 0.00   | 2  |
| 309 | -13 | -74 | Max  | 0.00   | 93.50  | 14 | 8.75    | 6  | 13.12   | 2  | 69.12   | 10 | -45.99  | 14 | 0.00   | 2  |
| 309 | -13 | -74 | Max  | 150.00 | 24.58  | 14 | 8.75    | 6  | 0.00    | 2  | 20.86   | 10 | 0.00    | 14 |        |    |



|     |     |     |      |        |        |    |        |   |        |    |        |      |        |    |      |   |
|-----|-----|-----|------|--------|--------|----|--------|---|--------|----|--------|------|--------|----|------|---|
| 310 | -14 | -90 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14   | -67.49 | 10 | 0.00 | 2 |
| 310 | -14 | -90 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14   | 0.00   | 10 | 0.00 | 2 |
| 310 | -91 | -14 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 6  | 1.97   | 14   | 0.00   | 2  | 0.00 | 6 |
| 310 | -91 | -14 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 310 | -91 | -14 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14   | -33.24 | 14 | 0.00 | 6 |
| 310 | -91 | -14 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10   | 0.00   | 6  | 0.00 | 2 |
| 310 | -91 | -14 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 310 | -91 | -14 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10   | -80.24 | 10 | 0.00 | 2 |
| 311 | -15 | -92 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10   | -45.99 | 14 | 0.00 | 2 |
| 311 | -15 | -92 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10   | 0.00   | 14 | 0.00 | 2 |
| 311 | -15 | -92 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14   | -67.49 | 10 | 0.00 | 2 |
| 311 | -15 | -92 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14   | 0.00   | 10 | 0.00 | 2 |
| 311 | -93 | -15 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 2  | 1.97   | 14   | 0.00   | 6  | 0.00 | 2 |
| 311 | -93 | -15 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 311 | -93 | -15 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14   | -33.24 | 14 | 0.00 | 2 |
| 311 | -93 | -15 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 6  | -29.36 | 10   | 0.00   | 2  | 0.00 | 6 |
| 311 | -93 | -15 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 311 | -93 | -15 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10   | -80.24 | 10 | 0.00 | 6 |
| 312 | -16 | -98 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10   | -45.99 | 14 | 0.00 | 2 |
| 312 | -16 | -98 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10   | 0.00   | 14 | 0.00 | 2 |
| 312 | -16 | -98 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14   | -67.49 | 10 | 0.00 | 2 |
| 312 | -16 | -98 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14   | 0.00   | 10 | 0.00 | 2 |
| 312 | -94 | -16 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 10 | 1.97   | 14   | 0.00   | 10 | 0.00 | 6 |
| 312 | -94 | -16 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 312 | -94 | -16 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14   | -33.24 | 14 | 0.00 | 6 |
| 312 | -94 | -16 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 14 | -29.36 | 10   | 0.00   | 14 | 0.00 | 4 |
| 312 | -94 | -16 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 312 | -94 | -16 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10   | -80.24 | 10 | 0.00 | 4 |
| 313 | -17 | -97 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10   | -45.99 | 14 | 0.00 | 2 |
| 313 | -17 | -97 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10   | 0.00   | 14 | 0.00 | 2 |
| 313 | -17 | -97 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14   | -67.49 | 10 | 0.00 | 2 |
| 313 | -17 | -97 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14   | 0.00   | 10 | 0.00 | 2 |
| 313 | -42 | -17 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 6  | 1.97   | 14   | 0.00   | 12 | 0.00 | 6 |
| 313 | -42 | -17 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 313 | -42 | -17 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14   | -33.24 | 14 | 0.00 | 6 |
| 313 | -42 | -17 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10   | 0.00   | 14 | 0.00 | 4 |
| 313 | -42 | -17 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 313 | -42 | -17 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10   | -80.24 | 10 | 0.00 | 4 |
| 314 | -18 | -43 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10   | -45.99 | 14 | 0.00 | 2 |
| 314 | -18 | -43 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10   | 0.00   | 14 | 0.00 | 2 |
| 314 | -18 | -43 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14   | -67.49 | 10 | 0.00 | 2 |
| 314 | -18 | -43 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14   | 0.00   | 10 | 0.00 | 2 |
| 314 | -44 | -18 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 14 | 1.97   | 14   | 0.00   | 14 | 0.00 | 6 |
| 314 | -44 | -18 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 314 | -44 | -18 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14   | -33.24 | 14 | 0.00 | 6 |
| 314 | -44 | -18 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 10 | -29.36 | 10   | 0.00   | 10 | 0.00 | 2 |
| 314 | -44 | -18 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 314 | -44 | -18 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10   | -80.24 | 10 | 0.00 | 2 |
| 315 | -19 | -45 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10   | -45.99 | 14 | 0.00 | 2 |
| 315 | -19 | -45 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10   | 0.00   | 14 | 0.00 | 2 |
| 315 | -19 | -45 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14   | -67.49 | 10 | 0.00 | 2 |
| 315 | -19 | -45 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14   | 0.00   | 10 | 0.00 | 2 |
| 315 | -58 | -19 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 8  | 1.97   | 14   | 0.00   | 14 | 0.00 | 8 |
| 315 | -58 | -19 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 315 | -58 | -19 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14   | -33.24 | 14 | 0.00 | 8 |
| 315 | -58 | -19 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10   | 0.00   | 12 | 0.00 | 2 |
| 315 | -58 | -19 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 315 | -58 | -19 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10   | -80.24 | 10 | 0.00 | 2 |
| 316 | -20 | -63 | Max  | 0.00   | 65.65  | 14 | 5.84   | 6 | 8.75   | 2  | 48.40  | 10   | -30.68 | 14 | 0.00 | 2 |
| 316 | -20 | -63 | Max  | 150.00 | 13.13  | 14 | 5.84   | 6 | 0.00   | 2  | 11.63  | 10   | 0.00   | 14 | 0.00 | 2 |
| 316 | -20 | -63 | Min. | 0.00   | 58.95  | 10 | -5.84  | 2 | -8.75  | 6  | 38.84  | 14   | -45.02 | 10 | 0.00 | 2 |
| 316 | -20 | -63 | Min. | 150.00 | 6.43   | 10 | -5.84  | 2 | 0.00   | 6  | 2.07   | 14   | 0.00   | 10 | 0.00 | 2 |
| 316 | -65 | -20 | Max  | 0.00   | -2.46  | 10 | 12.76  | 2 | 0.00   | 4  | 3.60   | 14   | 0.00   | 14 | 0.00 | 6 |
| 316 | -65 | -20 | Max  | 14.70  |        |    |        |   | 0.56   | 14 |        | 0.26 | 14     |    |      |   |
| 316 | -65 | -20 | Max  | 150.00 | -54.98 | 10 | 12.76  | 2 | 19.14  | 2  | -33.17 | 14   | -22.18 | 14 | 0.00 | 6 |
| 316 | -65 | -20 | Min. | 0.00   | -17.10 | 14 | -12.76 | 6 | 0.00   | 6  | -17.30 | 10   | 0.00   | 10 | 0.00 | 4 |
| 316 | -65 | -20 | Min. | 14.70  |        |    |        |   | 0.56   | 14 |        | 0.26 | 14     |    |      |   |
| 316 | -65 | -20 | Min. | 150.00 | -69.62 | 14 | -12.76 | 6 | -19.14 | 6  | -54.07 | 10   | -53.53 | 10 | 0.00 | 4 |
| 317 | -21 | -51 | Max  | 0.00   | 65.65  | 14 | 5.84   | 6 | 8.75   | 2  | 48.40  | 10   | -30.68 | 14 | 0.00 | 2 |
| 317 | -21 | -51 | Max  | 150.00 | 13.13  | 14 | 5.84   | 6 | 0.00   | 2  | 11.63  | 10   | 0.00   | 14 | 0.00 | 2 |
| 317 | -21 | -51 | Min. | 0.00   | 58.95  | 10 | -5.84  | 2 | -8.75  | 6  | 38.84  | 14   | -45.02 | 10 | 0.00 | 2 |
| 317 | -21 | -51 | Min. | 150.00 | 6.43   | 10 | -5.84  | 2 | 0.00   | 6  | 2.07   | 14   | 0.00   | 10 | 0.00 | 2 |
| 317 | -50 | -21 | Max  | 0.00   | -2.46  | 10 | 12.76  | 2 | 0.00   | 8  | 3.60   | 14   | 0.00   | 10 | 0.00 | 2 |
| 317 | -50 | -21 | Max  | 14.70  |        |    |        |   | 0.56   | 14 |        | 0.26 | 14     |    |      |   |
| 317 | -50 | -21 | Max  | 150.00 | -54.98 | 10 | 12.76  | 2 | 19.14  | 2  | -33.17 | 14   | -22.18 | 14 | 0.00 | 2 |
| 317 | -50 | -21 | Min. | 0.00   | -17.10 | 14 | -12.76 | 6 | 0.00   | 2  | -17.30 | 10   | 0.00   | 14 | 0.00 | 6 |
| 317 | -50 | -21 | Min. | 14.70  |        |    |        |   | 0.56   | 14 |        | 0.26 | 14     |    |      |   |
| 317 | -50 | -21 | Min. | 150.00 | -69.62 | 14 | -12.76 | 6 | -19.14 | 6  | -54.07 | 10   | -53.53 | 10 | 0.00 | 6 |
| 318 | -22 | -53 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10   | -45.99 | 14 | 0.00 | 2 |
| 318 | -22 | -53 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10   | 0.00   | 14 | 0.00 | 2 |
| 318 | -22 | -53 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14   | -67.49 | 10 | 0.00 | 2 |
| 318 | -22 | -53 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14   | 0.00   | 10 | 0.00 | 2 |
| 318 | -52 | -22 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 6  | 1.97   | 14   | 0.00   | 14 | 0.00 | 6 |
| 318 | -52 | -22 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 318 | -52 | -22 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14   | -33.24 | 14 | 0.00 | 6 |
| 318 | -52 | -22 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10   | 0.00   | 12 | 0.00 | 4 |
| 318 | -52 | -22 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        | 0.06 | 14     |    |      |   |
| 318 | -52 | -22 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10   | -80.24 | 10 | 0.00 | 4 |
| 319 | -23 | -55 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10   | -45.99 | 14 | 0.00 | 2 |
| 319 | -23 | -55 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10   | 0.00   | 14 | 0.00 | 2 |
| 319 | -23 | -55 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14   | -67.49 | 10 | 0.00 | 2 |
| 319 | -23 | -55 |      |        |        |    |        |   |        |    |        |      |        |    |      |   |



|     |     |     |      |        |        |    |        |   |        |    |        |    |        |    |      |   |
|-----|-----|-----|------|--------|--------|----|--------|---|--------|----|--------|----|--------|----|------|---|
| 320 | -24 | -57 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 320 | -56 | -24 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 8  | 1.97   | 14 | 0.00   | 16 | 0.00 | 2 |
| 320 | -56 | -24 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 320 | -56 | -24 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 2 |
| 320 | -56 | -24 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10 | 0.00   | 10 | 0.00 | 8 |
| 320 | -56 | -24 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 320 | -56 | -24 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 8 |
| 322 | -25 | -41 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 322 | -25 | -41 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 322 | -25 | -41 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 322 | -25 | -41 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 322 | -64 | -25 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 6  | 1.97   | 14 | 0.00   | 10 | 0.00 | 6 |
| 322 | -64 | -25 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 322 | -64 | -25 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 6 |
| 322 | -64 | -25 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10 | 0.00   | 16 | 0.00 | 4 |
| 322 | -64 | -25 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 322 | -64 | -25 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 4 |
| 323 | -26 | -77 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 323 | -26 | -77 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 323 | -26 | -77 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 323 | -26 | -77 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 323 | -76 | -26 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 4  | 1.97   | 14 | 0.00   | 14 | 0.00 | 6 |
| 323 | -76 | -26 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 323 | -76 | -26 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 6 |
| 323 | -76 | -26 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 6  | -29.36 | 10 | 0.00   | 10 | 0.00 | 4 |
| 323 | -76 | -26 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 323 | -76 | -26 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 4 |
| 324 | -27 | -79 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 324 | -27 | -79 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 324 | -27 | -79 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 324 | -27 | -79 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 324 | -78 | -27 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 6  | 1.97   | 14 | 0.00   | 14 | 0.00 | 6 |
| 324 | -78 | -27 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 324 | -78 | -27 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 6 |
| 324 | -78 | -27 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10 | 0.00   | 10 | 0.00 | 4 |
| 324 | -78 | -27 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 324 | -78 | -27 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 4 |
| 325 | -28 | -81 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 325 | -28 | -81 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 325 | -28 | -81 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 325 | -28 | -81 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 325 | -80 | -28 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 4  | 1.97   | 14 | 0.00   | 14 | 0.00 | 2 |
| 325 | -80 | -28 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 325 | -80 | -28 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 2 |
| 325 | -80 | -28 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 6  | -29.36 | 10 | 0.00   | 10 | 0.00 | 8 |
| 325 | -80 | -28 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 325 | -80 | -28 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 8 |
| 326 | -29 | -83 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 326 | -29 | -83 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 326 | -29 | -83 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 326 | -29 | -83 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 326 | -82 | -29 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 8  | 1.97   | 14 | 0.00   | 14 | 0.00 | 4 |
| 326 | -82 | -29 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 326 | -82 | -29 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 4 |
| 326 | -82 | -29 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10 | 0.00   | 10 | 0.00 | 6 |
| 326 | -82 | -29 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 326 | -82 | -29 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 6 |
| 327 | -30 | -85 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 327 | -30 | -85 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 327 | -30 | -85 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 327 | -30 | -85 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 327 | -84 | -30 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 6  | 1.97   | 14 | 0.00   | 16 | 0.00 | 2 |
| 327 | -84 | -30 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 327 | -84 | -30 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 2 |
| 327 | -84 | -30 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 4  | -29.36 | 10 | 0.00   | 10 | 0.00 | 6 |
| 327 | -84 | -30 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 327 | -84 | -30 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 6 |
| 329 | -32 | -86 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 329 | -32 | -86 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 329 | -32 | -86 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 329 | -32 | -86 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 329 | -87 | -32 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 8  | 1.97   | 14 | 0.00   | 14 | 0.00 | 2 |
| 329 | -87 | -32 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 329 | -87 | -32 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 2 |
| 329 | -87 | -32 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10 | 0.00   | 10 | 0.00 | 6 |
| 329 | -87 | -32 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 329 | -87 | -32 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 6 |
| 330 | -33 | -89 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 330 | -33 | -89 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 330 | -33 | -89 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 330 | -33 | -89 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 330 | -88 | -33 | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 8  | 1.97   | 14 | 0.00   | 10 | 0.00 | 6 |
| 330 | -88 | -33 | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 330 | -88 | -33 | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 6 |
| 330 | -88 | -33 | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 2  | -29.36 | 10 | 0.00   | 14 | 0.00 | 4 |
| 330 | -88 | -33 | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 330 | -88 | -33 | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 4 |
| 331 | -34 | -61 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 331 | -34 | -61 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 331 | -34 | -61 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 331 | -34 | -61 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 331 | -62 | -34 |      |        |        |    |        |   |        |    |        |    |        |    |      |   |



|     |      |      |      |        |        |    |        |   |        |    |        |    |        |    |      |   |
|-----|------|------|------|--------|--------|----|--------|---|--------|----|--------|----|--------|----|------|---|
| 332 | -101 | -35  | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 2  | 1.97   | 14 | 0.00   | 12 | 0.00 | 4 |
| 332 | -101 | -35  | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 332 | -101 | -35  | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 4 |
| 332 | -101 | -35  | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 8  | -29.36 | 10 | 0.00   | 14 | 0.00 | 6 |
| 332 | -101 | -35  | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 332 | -101 | -35  | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 6 |
| 333 | -37  | -103 | Max  | 0.00   | 93.50  | 14 | 8.75   | 6 | 13.12  | 2  | 69.12  | 10 | -45.99 | 14 | 0.00 | 2 |
| 333 | -37  | -103 | Max  | 150.00 | 24.58  | 14 | 8.75   | 6 | 0.00   | 2  | 20.86  | 10 | 0.00   | 14 | 0.00 | 2 |
| 333 | -37  | -103 | Min. | 0.00   | 83.47  | 10 | -8.75  | 2 | -13.12 | 6  | 54.79  | 14 | -67.49 | 10 | 0.00 | 2 |
| 333 | -37  | -103 | Min. | 150.00 | 14.54  | 10 | -8.75  | 2 | 0.00   | 6  | 6.53   | 14 | 0.00   | 10 | 0.00 | 2 |
| 333 | -104 | -37  | Max  | 0.00   | -8.59  | 10 | 19.13  | 2 | 0.00   | 2  | 1.97   | 14 | 0.00   | 14 | 0.00 | 2 |
| 333 | -104 | -37  | Max  | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 333 | -104 | -37  | Max  | 150.00 | -77.52 | 10 | 19.13  | 2 | 28.69  | 2  | -46.29 | 14 | -33.24 | 14 | 0.00 | 2 |
| 333 | -104 | -37  | Min. | 0.00   | -30.53 | 14 | -19.13 | 6 | 0.00   | 8  | -29.36 | 10 | 0.00   | 14 | 0.00 | 6 |
| 333 | -104 | -37  | Min. | 6.13   |        |    |        |   | 0.35   | 14 |        |    | 0.06   | 14 |      |   |
| 333 | -104 | -37  | Min. | 150.00 | -99.46 | 14 | -19.13 | 6 | -28.69 | 6  | -77.63 | 10 | -80.24 | 10 | 0.00 | 6 |
| 334 | -38  | -99  | Max  | 0.00   | 65.65  | 14 | 5.84   | 6 | 8.75   | 2  | 48.40  | 10 | -30.68 | 14 | 0.00 | 2 |
| 334 | -38  | -99  | Max  | 150.00 | 13.13  | 14 | 5.84   | 6 | 0.00   | 2  | 11.63  | 10 | 0.00   | 14 | 0.00 | 2 |
| 334 | -38  | -99  | Min. | 0.00   | 58.95  | 10 | -5.84  | 2 | -8.75  | 6  | 38.84  | 14 | -45.02 | 10 | 0.00 | 2 |
| 334 | -38  | -99  | Min. | 150.00 | 6.43   | 10 | -5.84  | 2 | 0.00   | 6  | 2.07   | 14 | 0.00   | 10 | 0.00 | 2 |
| 334 | -100 | -38  | Max  | 0.00   | -2.46  | 10 | 12.76  | 2 | 0.00   | 6  | 3.60   | 14 | 0.00   | 6  | 0.00 | 6 |
| 334 | -100 | -38  | Max  | 14.70  |        |    |        |   | 0.56   | 14 |        |    | 0.26   | 14 |      |   |
| 334 | -100 | -38  | Max  | 150.00 | -54.98 | 10 | 12.76  | 2 | 19.14  | 2  | -33.17 | 14 | -22.18 | 14 | 0.00 | 6 |
| 334 | -100 | -38  | Min. | 0.00   | -17.10 | 14 | -12.76 | 6 | 0.00   | 2  | -17.30 | 10 | 0.00   | 2  | 0.00 | 2 |
| 334 | -100 | -38  | Min. | 14.70  |        |    |        |   | 0.56   | 14 |        |    | 0.26   | 14 |      |   |
| 334 | -100 | -38  | Min. | 150.00 | -69.62 | 14 | -12.76 | 6 | -19.14 | 6  | -54.07 | 10 | -53.53 | 10 | 0.00 | 2 |

Tipo di combinazione di carico: SLU

| Asta | N1  | N2  |      | X      | N        | CC Ty | CC Mz   | CC Tz | CC My   | CC Mx  | CC       |    |           |    |         |    |
|------|-----|-----|------|--------|----------|-------|---------|-------|---------|--------|----------|----|-----------|----|---------|----|
|      |     |     |      | <cm>   | <daN>    | <daN> | <daNm>  | <daN> | <daNm>  | <daNm> |          |    |           |    |         |    |
| 1    | 1   | -5  | Max  | 0.00   | -284.49  | 21    | -26.42  | 21    | 141.27  | 28     | 2116.46  | 21 | 5046.51   | 28 | 0.08    | 28 |
| 1    | 1   | -5  | Max  | 330.00 | -38.48   | 21    | -26.42  | 21    | -58.68  | 21     | 2116.46  | 21 | 126.12    | 28 | 0.08    | 28 |
| 1    | 1   | -5  | Min. | 0.00   | -2804.14 | 28    | -129.33 | 28    | 28.49   | 21     | -1491.03 | 28 | -7163.35  | 21 | -0.12   | 21 |
| 1    | 1   | -5  | Min. | 330.00 | -2558.14 | 28    | -129.33 | 28    | -285.52 | 28     | -1491.03 | 28 | -179.02   | 21 | -0.12   | 21 |
| 2    | 2   | -10 | Max  | 0.00   | -185.86  | 21    | 251.64  | 28    | -2.67   | 21     | 2893.27  | 21 | 6637.20   | 28 | 1.39    | 28 |
| 2    | 2   | -10 | Max  | 330.00 | 60.15    | 21    | 251.64  | 28    | 556.07  | 28     | 2893.27  | 21 | 126.49    | 21 | 1.39    | 28 |
| 2    | 2   | -10 | Min. | 0.00   | -3654.04 | 28    | 2.21    | 21    | -274.35 | 28     | -2038.28 | 28 | -9421.30  | 21 | -1.97   | 21 |
| 2    | 2   | -10 | Min. | 330.00 | -3408.03 | 28    | 2.21    | 21    | 14.63   | 21     | -2038.28 | 28 | -89.11    | 28 | -1.97   | 21 |
| 3    | 3   | 203 | Max  | 0.00   | -199.06  | 21    | 1.71    | 21    | 174.29  | 28     | 3151.63  | 21 | 7224.05   | 28 | 1.21    | 21 |
| 3    | 3   | 203 | Max  | 330.00 | 46.94    | 21    | 1.71    | 21    | 3.66    | 21     | 3151.63  | 21 | 146.06    | 21 | 1.21    | 21 |
| 3    | 3   | 203 | Min. | 0.00   | -3978.31 | 28    | -159.72 | 28    | -1.98   | 21     | -2220.28 | 28 | -10254.30 | 21 | -0.85   | 28 |
| 3    | 3   | 203 | Min. | 330.00 | -3732.30 | 28    | -159.72 | 28    | -352.80 | 28     | -2220.28 | 28 | -102.89   | 28 | -0.85   | 28 |
| 4    | 4   | 204 | Max  | 0.00   | -344.91  | 21    | 0.00    | 28    | 0.00    | 21     | 1816.71  | 28 | 8696.99   | 21 | 0.00    | 21 |
| 4    | 4   | 204 | Max  | 330.00 | -98.90   | 21    | 0.00    | 28    | 0.00    | 28     | 1816.71  | 28 | 187.08    | 21 | 0.00    | 21 |
| 4    | 4   | 204 | Min. | 0.00   | -3369.62 | 28    | -0.00   | 21    | -0.00   | 28     | -2578.76 | 21 | -6126.94  | 28 | 0.00    | 28 |
| 4    | 4   | 204 | Min. | 330.00 | -3123.61 | 28    | -0.00   | 21    | 0.00    | 21     | -2578.76 | 21 | -131.80   | 28 | 0.00    | 28 |
| 5    | 5   | 205 | Max  | 0.00   | -199.06  | 21    | 1.71    | 21    | 174.29  | 28     | 2220.29  | 28 | 10254.30  | 21 | 0.85    | 28 |
| 5    | 5   | 205 | Max  | 330.00 | 46.94    | 21    | 1.71    | 21    | 3.66    | 21     | 2220.29  | 28 | 102.89    | 28 | 0.85    | 28 |
| 5    | 5   | 205 | Min. | 0.00   | -3978.30 | 28    | -159.72 | 28    | -1.98   | 21     | -3151.63 | 21 | -7224.05  | 28 | -1.21   | 21 |
| 5    | 5   | 205 | Min. | 330.00 | -3732.30 | 28    | -159.72 | 28    | -352.80 | 28     | -3151.63 | 21 | -146.06   | 21 | -1.21   | 21 |
| 6    | 6   | -31 | Max  | 0.00   | -185.86  | 21    | 251.65  | 28    | -2.67   | 21     | 2038.27  | 28 | 9421.29   | 21 | 1.97    | 21 |
| 6    | 6   | -31 | Max  | 330.00 | 60.15    | 21    | 251.65  | 28    | 556.08  | 28     | 2038.27  | 28 | 89.11     | 28 | 1.97    | 21 |
| 6    | 6   | -31 | Min. | 0.00   | -3654.04 | 28    | 2.21    | 21    | -274.36 | 28     | -2893.27 | 21 | -6637.20  | 28 | -1.39   | 28 |
| 6    | 6   | -31 | Min. | 330.00 | -3408.03 | 28    | 2.21    | 21    | 14.63   | 21     | -2893.27 | 21 | -126.49   | 21 | -1.39   | 28 |
| 7    | 7   | -36 | Max  | 0.00   | -284.48  | 21    | -26.42  | 21    | 141.28  | 28     | 1491.03  | 28 | 7163.36   | 21 | 0.12    | 21 |
| 7    | 7   | -36 | Max  | 330.00 | -38.48   | 21    | -26.42  | 21    | -58.68  | 21     | 1491.03  | 28 | 179.02    | 21 | 0.12    | 21 |
| 7    | 7   | -36 | Min. | 0.00   | -2804.15 | 28    | -129.33 | 28    | 28.49   | 21     | -2116.47 | 21 | -5046.51  | 28 | -0.08   | 28 |
| 7    | 7   | -36 | Min. | 330.00 | -2558.14 | 28    | -129.33 | 28    | -285.53 | 28     | -2116.47 | 21 | -126.12   | 28 | -0.08   | 28 |
| 201  | -4  | -3  | Max  | 0.00   | 0.00     | 17    | 221.93  | 28    | 420.66  | 21     | 470.28   | 28 | -70.02    | 21 | 0.00    | 28 |
| 201  | -4  | -3  | Max  | 133.53 | 0.00     | 17    | 221.93  | 28    | 0.00    | 28     | 386.55   | 28 | 0.00      | 28 | 0.00    | 28 |
| 201  | -4  | -3  | Min. | 0.00   | 0.00     | 17    | -315.02 | 21    | -296.35 | 28     | 94.30    | 21 | -572.08   | 28 | 0.00    | 21 |
| 201  | -4  | -3  | Min. | 133.53 | 0.00     | 17    | -315.02 | 21    | 0.00    | 21     | 10.57    | 21 | 0.00      | 21 | 0.00    | 21 |
| 201  | -5  | -4  | Max  | 0.00   | 0.00     | 17    | 665.79  | 28    | 1171.67 | 21     | 1178.59  | 28 | -90.46    | 21 | 0.00    | 28 |
| 201  | -5  | -4  | Max  | 79.47  | 0.00     | 17    | 665.79  | 28    | 420.66  | 21     | 1128.76  | 28 | -70.02    | 21 | 0.00    | 28 |
| 201  | -5  | -4  | Min. | 0.00   | 0.00     | 17    | -945.07 | 21    | -825.43 | 28     | 50.64    | 21 | -1488.85  | 28 | 0.00    | 21 |
| 201  | -5  | -4  | Min. | 79.47  | 0.00     | 17    | -945.07 | 21    | -296.35 | 28     | 0.82     | 21 | -572.07   | 28 | 0.00    | 21 |
| 201  | -6  | -5  | Max  | 0.00   | 129.33   | 28    | 1171.39 | 21    | 538.46  | 21     | 46.06    | 21 | -47.52    | 21 | 179.02  | 21 |
| 201  | -6  | -5  | Max  | 54.07  | 129.33   | 28    | 1171.39 | 21    | 1171.79 | 21     | 12.16    | 21 | -31.78    | 21 | 179.02  | 21 |
| 201  | -6  | -5  | Min. | 0.00   | 26.42    | 21    | -825.23 | 28    | -379.34 | 28     | -1345.65 | 28 | -466.62   | 28 | -126.12 | 28 |
| 201  | -6  | -5  | Min. | 54.07  | 26.42    | 21    | -825.23 | 28    | -825.51 | 28     | -1379.55 | 28 | -1203.33  | 28 | -126.12 | 28 |
| 201  | -7  | -6  | Max  | 0.00   | 129.33   | 28    | 541.34  | 21    | 129.92  | 28     | 36.31    | 21 | 395.08    | 28 | 179.02  | 21 |
| 201  | -7  | -6  | Max  | 57.91  |          |       |         |       | 129.07  | 21     |          |    | -29.59    | 21 |         |    |
| 201  | -7  | -6  | Max  | 133.53 | 129.33   | 28    | 541.34  | 21    | 538.45  | 21     | -47.42   | 21 | -47.52    | 21 | 179.02  | 21 |
| 201  | -7  | -6  | Min. | 0.00   | 26.42    | 21    | -381.37 | 28    | -184.42 | 21     | -603.45  | 28 | -40.10    | 21 | -126.12 | 28 |
| 201  | -7  | -6  | Min. | 57.91  |          |       |         |       | 129.07  | 21     |          |    | -29.59    | 21 |         |    |
| 201  | -7  | -6  | Min. | 133.53 | 26.42    | 21    | -381.37 | 28    | -379.33 | 28     | -687.17  | 28 | -466.62   | 28 | -126.12 | 28 |
| 201  | -8  | -7  | Max  | 0.00   | 129.33   | 28    | 62.49   | 28    | 46.47   | 28     | 138.76   | 28 | 265.69    | 28 | 179.02  | 21 |
| 201  | -8  | -7  | Max  | 94.17  |          |       |         |       | -89.70  | 22     |          |    | 90.76     | 22 |         |    |
| 201  | -8  | -7  | Max  | 133.53 | 129.33   | 28    | 62.49   | 28    | 129.92  | 28     | 55.04    | 28 | 395.08    | 28 | 179.02  | 21 |
| 201  | -8  | -7  | Min. | 0.00   | 26.42    | 21    | -88.71  | 21    | -65.96  | 21     | 26.55    | 21 | -19.66    | 21 | -126.12 | 28 |
| 201  | -8  | -7  | Min. | 42.35  |          |       |         |       | -103.53 | 21     |          |    | -14.04    | 21 |         |    |
| 201  | -8  | -7  | Min. | 133.53 | 26.42    | 21    | -88.71  | 21    | -184.42 | 21     | -57.17   | 21 | -40.10    | 21 | -126.12 | 28 |
| 201  | -9  | -8  | Max  | 0.00   | 129.33   | 28    | 506.36  | 28    | 893.82  | 21     | 880.97   | 28 | 13.80     | 21 | 179.02  | 21 |
| 201  | -9  | -8  | Max  | 26.71  |          |       |         |       | 701.86  | 21     |          |    | 16.06     | 21 |         |    |
| 201  | -9  | -8  | Max  | 133.53 | 129.33   | 28    | 506.36  | 28    | 46.47   | 28     | 797.25   | 28 | 265.69    | 28 | 179.02  | 21 |
| 201  | -9  | -8  | Min. | 0.00   | 26.42    | 21    | -718.76 | 21    | -629.69 | 28     | 16.80    | 21 | -854.80   | 28 | -126.12 | 28 |
| 201  | -9  | -8  | Min. | 26.71  |          |       |         |       | 701.86  | 21     |          |    | 16.06     | 21 |         |    |
| 201  | -9  | -8  | Min. | 133.53 | 26.42    | 21    | -718.76 | 21    | -65.96  | 21     | -66.93   | 21 | -19.66    | 21 | -126.12 | 28 |
| 201  | -10 | -9  | Max  | 0.00   | 129.33   | 28    | 950.22  | 28    | 1505.29 | 21     | 1567.88  | 28 | 42.12     | 21 | 179.02  | 21 |
| 201  | -10 | -9  | Max  | 45     |          |       |         |       |         |        |          |    |           |    |         |    |





|     |     |     |      |        |         |    |          |    |          |    |          |    |          |    |         |    |
|-----|-----|-----|------|--------|---------|----|----------|----|----------|----|----------|----|----------|----|---------|----|
| 205 | -27 | -28 | Min. | 0.00   | -122.31 | 28 | -243.53  | 28 | -700.35  | 28 | 37.93    | 21 | -20.69   | 21 | -52.52  | 21 |
| 205 | -27 | -28 | Min. | 60.49  |         |    |          |    | 1203.23  | 21 |          |    | -9.21    | 21 |         |    |
| 205 | -27 | -28 | Min. | 133.53 | -122.31 | 28 | -243.53  | 28 | -1025.55 | 28 | -45.80   | 21 | -25.94   | 21 | -52.52  | 21 |
| 205 | -28 | -29 | Max  | 0.00   | 24.21   | 21 | 200.33   | 28 | 1455.72  | 21 | 47.68    | 21 | 1388.69  | 28 | 37.00   | 28 |
| 205 | -28 | -29 | Max  | 76.05  |         |    |          |    | 1239.46  | 21 |          |    | -7.81    | 21 |         |    |
| 205 | -28 | -29 | Max  | 133.53 | 24.21   | 21 | 200.33   | 28 | 1076.00  | 21 | -36.04   | 21 | 931.60   | 28 | 37.00   | 28 |
| 205 | -28 | -29 | Min. | 0.00   | -122.31 | 28 | -284.36  | 21 | -1025.54 | 28 | -300.44  | 28 | -25.94   | 21 | -52.53  | 21 |
| 205 | -28 | -29 | Min. | 76.05  |         |    |          |    | 1239.46  | 21 |          |    | -7.81    | 21 |         |    |
| 205 | -28 | -29 | Min. | 133.53 | -122.31 | 28 | -284.36  | 21 | -758.03  | 28 | -384.16  | 28 | -18.17   | 21 | -52.53  | 21 |
| 205 | -29 | -30 | Max  | 0.00   | 24.21   | 21 | 644.19   | 28 | 1075.98  | 21 | 57.43    | 21 | 931.58   | 28 | 37.01   | 28 |
| 205 | -29 | -30 | Max  | 91.60  |         |    |          |    | 238.37   | 21 |          |    | 8.13     | 21 |         |    |
| 205 | -29 | -30 | Max  | 133.53 | 24.21   | 21 | 644.19   | 28 | 102.20   | 28 | -26.29   | 21 | 2.62     | 21 | 37.01   | 28 |
| 205 | -29 | -30 | Min. | 0.00   | -122.31 | 28 | -914.41  | 21 | -758.02  | 28 | -1042.65 | 28 | -18.17   | 21 | -52.53  | 21 |
| 205 | -29 | -30 | Min. | 91.60  |         |    |          |    | 238.37   | 21 |          |    | 8.13     | 21 |         |    |
| 205 | -29 | -30 | Min. | 133.53 | -122.31 | 28 | -914.41  | 21 | -145.07  | 21 | -1126.38 | 28 | -516.61  | 28 | -52.53  | 21 |
| 205 | -30 | -31 | Max  | 0.00   | 24.21   | 21 | 1088.06  | 28 | 102.18   | 28 | 67.19    | 21 | 2.62     | 21 | 37.01   | 28 |
| 205 | -30 | -31 | Max  | 88.20  | 24.21   | 21 | 1088.06  | 28 | 1061.84  | 28 | 11.89    | 21 | 37.50    | 21 | 37.01   | 28 |
| 205 | -30 | -31 | Min. | 0.00   | -122.31 | 28 | -1544.46 | 21 | -145.04  | 21 | -1784.86 | 28 | -516.57  | 28 | -52.53  | 21 |
| 205 | -30 | -31 | Min. | 88.20  | -122.31 | 28 | -1544.46 | 21 | -1507.25 | 21 | -1840.16 | 28 | -2115.20 | 28 | -52.53  | 21 |
| 206 | -31 | -32 | Max  | 0.00   | 129.33  | 28 | 1348.80  | 21 | 1060.45  | 28 | 1567.87  | 28 | 42.12    | 21 | 126.11  | 28 |
| 206 | -31 | -32 | Max  | 45.33  | 129.33  | 28 | 1348.80  | 21 | 629.69   | 28 | 1539.45  | 28 | 13.80    | 21 | 126.11  | 28 |
| 206 | -31 | -32 | Min. | 0.00   | 26.42   | 21 | -950.22  | 28 | -1505.28 | 21 | -48.26   | 21 | -1559.12 | 28 | -179.02 | 21 |
| 206 | -31 | -32 | Min. | 45.33  | 26.42   | 21 | -950.22  | 28 | -893.82  | 21 | -76.68   | 21 | -854.79  | 28 | -179.02 | 21 |
| 206 | -32 | -33 | Max  | 0.00   | 129.33  | 28 | 718.75   | 21 | 629.72   | 28 | 880.97   | 28 | 13.81    | 21 | 126.12  | 28 |
| 206 | -32 | -33 | Max  | 26.71  |         |    |          |    | -701.91  | 21 |          |    | 16.06    | 21 |         |    |
| 206 | -32 | -33 | Max  | 133.53 | 129.33  | 28 | 718.75   | 21 | 65.91    | 21 | 797.25   | 28 | 265.64   | 28 | 126.12  | 28 |
| 206 | -32 | -33 | Min. | 0.00   | 26.42   | 21 | -506.36  | 28 | -893.87  | 21 | 16.80    | 21 | -854.85  | 28 | -179.02 | 21 |
| 206 | -32 | -33 | Min. | 26.71  |         |    |          |    | -701.91  | 21 |          |    | 16.06    | 21 |         |    |
| 206 | -32 | -33 | Min. | 133.53 | 26.42   | 21 | -506.36  | 28 | -46.43   | 28 | -66.92   | 21 | -19.66   | 21 | -179.02 | 21 |
| 206 | -33 | -34 | Max  | 0.00   | 129.33  | 28 | 88.71    | 21 | 65.96    | 21 | 138.76   | 28 | 265.70   | 28 | 126.12  | 28 |
| 206 | -33 | -34 | Max  | 94.16  |         |    |          |    | 89.69    | 22 |          |    | 90.76    | 22 |         |    |
| 206 | -33 | -34 | Max  | 133.53 | 129.33  | 28 | 88.71    | 21 | 184.41   | 21 | 55.03    | 28 | 395.08   | 28 | 126.12  | 28 |
| 206 | -33 | -34 | Min. | 0.00   | 26.42   | 21 | -62.49   | 28 | -46.47   | 28 | 26.55    | 21 | -19.66   | 21 | -179.02 | 21 |
| 206 | -33 | -34 | Min. | 42.35  |         |    |          |    | 103.53   | 21 |          |    | -14.04   | 21 |         |    |
| 206 | -33 | -34 | Min. | 133.53 | 26.42   | 21 | -62.49   | 28 | -129.92  | 28 | -57.17   | 21 | -40.11   | 21 | -179.02 | 21 |
| 206 | -34 | -35 | Max  | 0.00   | 129.33  | 28 | 381.37   | 28 | 184.41   | 21 | 36.31    | 21 | 395.08   | 28 | 126.12  | 28 |
| 206 | -34 | -35 | Max  | 57.91  |         |    |          |    | -129.08  | 21 |          |    | -29.59   | 21 |         |    |
| 206 | -34 | -35 | Max  | 133.53 | 129.33  | 28 | 381.37   | 28 | 379.34   | 28 | -47.42   | 21 | -47.52   | 21 | 126.12  | 28 |
| 206 | -34 | -35 | Min. | 0.00   | 26.42   | 21 | -541.34  | 21 | -129.91  | 28 | -603.45  | 28 | -40.11   | 21 | -179.02 | 21 |
| 206 | -34 | -35 | Min. | 57.91  |         |    |          |    | -129.08  | 21 |          |    | -29.59   | 21 |         |    |
| 206 | -34 | -35 | Min. | 133.53 | 26.42   | 21 | -541.34  | 21 | -538.47  | 21 | -687.17  | 28 | -466.62  | 28 | -179.02 | 21 |
| 206 | -35 | -36 | Max  | 0.00   | 129.33  | 28 | 825.23   | 28 | 379.33   | 28 | 46.07    | 21 | -47.52   | 21 | 126.12  | 28 |
| 206 | -35 | -36 | Max  | 54.07  | 129.33  | 28 | 825.23   | 28 | 825.51   | 28 | 12.17    | 21 | -31.78   | 21 | 126.12  | 28 |
| 206 | -35 | -36 | Min. | 0.00   | 26.42   | 21 | -1171.39 | 21 | -538.45  | 21 | -1345.65 | 28 | -466.60  | 28 | -179.02 | 21 |
| 206 | -35 | -36 | Min. | 54.07  | 26.42   | 21 | -1171.39 | 21 | -1171.78 | 21 | -1379.55 | 28 | -1203.31 | 28 | -179.02 | 21 |
| 206 | -36 | -37 | Max  | 0.00   | 0.00    | 17 | 945.07   | 21 | 825.45   | 28 | 1178.58  | 28 | -90.46   | 21 | 0.00    | 21 |
| 206 | -36 | -37 | Max  | 79.47  | 0.00    | 17 | 945.07   | 21 | 296.37   | 28 | 1128.76  | 28 | -70.01   | 21 | 0.00    | 21 |
| 206 | -36 | -37 | Min. | 0.00   | 0.00    | 17 | -665.79  | 28 | -1171.70 | 21 | 50.64    | 21 | -1488.88 | 28 | -0.00   | 28 |
| 206 | -36 | -37 | Min. | 79.47  | 0.00    | 17 | -665.79  | 28 | -420.68  | 21 | 0.82     | 21 | -572.10  | 28 | -0.00   | 28 |
| 206 | -37 | -38 | Max  | 0.00   | 0.00    | 17 | 315.02   | 21 | 296.35   | 28 | 470.27   | 28 | -70.01   | 21 | 0.00    | 21 |
| 206 | -37 | -38 | Max  | 133.53 | 0.00    | 17 | 315.02   | 21 | 0.01     | 21 | 386.55   | 28 | 0.01     | 28 | 0.00    | 21 |
| 206 | -37 | -38 | Min. | 0.00   | 0.00    | 17 | -221.93  | 28 | -420.65  | 21 | 94.29    | 21 | -572.06  | 28 | 0.00    | 28 |
| 206 | -37 | -38 | Min. | 133.53 | 0.00    | 17 | -221.93  | 28 | -0.01    | 28 | 10.57    | 21 | 0.00     | 21 | 0.00    | 28 |
| 301 | -3  | -60 | Max  | 0.00   | 103.12  | 29 | 0.00     | 17 | 0.00     | 17 | 201.76   | 28 | 138.99   | 21 | 0.00    | 17 |
| 301 | -3  | -60 | Max  | 150.00 | 20.98   | 29 | 0.00     | 17 | 0.00     | 17 | 63.07    | 28 | 0.00     | 21 | 0.00    | 17 |
| 301 | -3  | -60 | Min. | 0.00   | 94.68   | 21 | 0.00     | 17 | 0.00     | 17 | -125.99  | 21 | -198.62  | 28 | 0.00    | 17 |
| 301 | -3  | -60 | Min. | 150.00 | 17.82   | 21 | 0.00     | 17 | 0.00     | 17 | -59.33   | 21 | 0.00     | 21 | 0.00    | 17 |
| 301 | -59 | -3  | Max  | 0.00   | -17.82  | 28 | 0.00     | 17 | 0.00     | 17 | 59.33    | 21 | 0.00     | 21 | 0.00    | 17 |
| 301 | -59 | -3  | Max  | 150.00 | -94.68  | 28 | 0.00     | 17 | 0.00     | 17 | 125.99   | 21 | 138.99   | 21 | 0.00    | 17 |
| 301 | -59 | -3  | Min. | 0.00   | -20.98  | 22 | 0.00     | 17 | 0.00     | 17 | -63.07   | 28 | 0.00     | 21 | 0.00    | 17 |
| 301 | -59 | -3  | Min. | 150.00 | -103.12 | 22 | 0.00     | 17 | 0.00     | 17 | -201.76  | 28 | -198.62  | 28 | 0.00    | 17 |
| 302 | -4  | -47 | Max  | 0.00   | 159.30  | 29 | 0.00     | 17 | 0.00     | 17 | 370.64   | 28 | 302.64   | 21 | 0.00    | 17 |
| 302 | -4  | -47 | Max  | 150.00 | 41.96   | 29 | 0.00     | 17 | 0.00     | 17 | 126.13   | 28 | 0.00     | 21 | 0.00    | 17 |
| 302 | -4  | -47 | Min. | 0.00   | 142.40  | 21 | 0.00     | 17 | 0.00     | 17 | -284.86  | 21 | -372.58  | 28 | 0.00    | 17 |
| 302 | -4  | -47 | Min. | 150.00 | 35.65   | 21 | 0.00     | 17 | 0.00     | 17 | -118.65  | 21 | 0.00     | 21 | 0.00    | 17 |
| 302 | -46 | -4  | Max  | 0.00   | -35.65  | 28 | 0.00     | 17 | 0.00     | 17 | 118.65   | 21 | 0.00     | 21 | 0.00    | 17 |
| 302 | -46 | -4  | Max  | 150.00 | -142.40 | 28 | 0.00     | 17 | 0.00     | 17 | 284.86   | 21 | 302.64   | 21 | 0.00    | 17 |
| 302 | -46 | -4  | Min. | 0.00   | -41.96  | 22 | 0.00     | 17 | 0.00     | 17 | -126.13  | 28 | 0.00     | 28 | 0.00    | 17 |
| 302 | -46 | -4  | Min. | 150.00 | -159.30 | 22 | 0.00     | 17 | 0.00     | 17 | -370.64  | 28 | -372.58  | 28 | 0.00    | 17 |
| 303 | -6  | -48 | Max  | 0.00   | 159.30  | 29 | 0.00     | 17 | 0.00     | 17 | 370.64   | 28 | 302.64   | 21 | 0.00    | 17 |
| 303 | -6  | -48 | Max  | 150.00 | 41.96   | 29 | 0.00     | 17 | 0.00     | 17 | 126.13   | 28 | 0.00     | 21 | 0.00    | 17 |
| 303 | -6  | -48 | Min. | 0.00   | 142.40  | 21 | 0.00     | 17 | 0.00     | 17 | -284.86  | 21 | -372.58  | 28 | 0.00    | 17 |
| 303 | -6  | -48 | Min. | 150.00 | 35.65   | 21 | 0.00     | 17 | 0.00     | 17 | -118.65  | 21 | 0.00     | 21 | 0.00    | 17 |
| 303 | -49 | -6  | Max  | 0.00   | -35.65  | 28 | 0.00     | 17 | 0.00     | 17 | 118.65   | 21 | 0.00     | 21 | 0.00    | 17 |
| 303 | -49 | -6  | Max  | 150.00 | -142.40 | 28 | 0.00     | 17 | 0.00     | 17 | 284.86   | 21 | 302.64   | 21 | 0.00    | 17 |
| 303 | -49 | -6  | Min. | 0.00   | -41.96  | 22 | 0.00     | 17 | 0.00     | 17 | -126.13  | 28 | 0.00     | 28 | 0.00    | 17 |
| 303 | -49 | -6  | Min. | 150.00 | -159.30 | 22 | 0.00     | 17 | 0.00     | 17 | -370.64  | 28 | -372.58  | 28 | 0.00    | 17 |
| 304 | -7  | -96 | Max  | 0.00   | 159.30  | 29 | 0.00     | 17 | 0.00     | 17 | 370.64   | 28 | 302.64   | 21 | 0.00    | 17 |
| 304 | -7  | -96 | Max  | 150.00 | 41.96   | 29 | 0.00     | 17 | 0.00     | 17 | 126.13   | 28 | 0.00     | 21 | 0.00    | 17 |
| 304 | -7  | -96 | Min. | 0.00   | 142.40  | 21 | 0.00     | 17 | 0.00     | 17 | -284.86  | 21 | -372.58  | 28 | 0.00    | 17 |
| 304 | -7  | -96 | Min. | 150.00 | 35.65   | 21 | 0.00     | 17 | 0.00     | 17 | -118.65  | 21 | 0.00     | 21 | 0.00    | 17 |
| 304 | -95 | -7  | Max  | 0.00   | -35.65  | 28 | 0.00     | 17 | 0.00     | 17 | 118.65   | 21 | 0.00     | 21 | 0.00    | 17 |
| 304 | -95 | -7  | Max  | 150.00 | -142.40 | 28 | 0.00     | 17 | 0.00     | 17 | 284.86   | 21 | 302.64   | 21 | 0.00    | 17 |
| 304 | -95 | -7  | Min. | 0.00   | -41.96  | 22 | 0.00     | 17 | 0.00     | 17 | -126.13  | 28 | 0.00     | 28 | 0.00    | 17 |
| 304 | -95 | -7  | Min. | 150.00 | -159.30 | 22 | 0.00     | 17 | 0.00     | 17 | -370.64  | 28 | -372.58  | 28 | 0.00    | 17 |
| 305 | -8  | -66 | Max  | 0.00   | 159.30  | 29 | 0.00     | 17 | 0.00     |    |          |    |          |    |         |    |





|     |     |     |      |        |         |    |      |    |      |    |         |    |         |    |      |    |
|-----|-----|-----|------|--------|---------|----|------|----|------|----|---------|----|---------|----|------|----|
| 307 | -11 | -70 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 307 | -11 | -70 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 307 | -11 | -70 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 307 | -11 | -70 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 29 | 0.00 | 17 |
| 307 | -71 | -11 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 28 | 0.00 | 17 |
| 307 | -71 | -11 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 307 | -71 | -11 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 21 | 0.00 | 17 |
| 307 | -71 | -11 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 308 | -12 | -72 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 308 | -12 | -72 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 308 | -12 | -72 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 308 | -12 | -72 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 29 | 0.00 | 17 |
| 308 | -73 | -12 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 17 | 0.00 | 17 |
| 308 | -73 | -12 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 308 | -73 | -12 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 21 | 0.00 | 17 |
| 308 | -73 | -12 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 309 | -13 | -74 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 309 | -13 | -74 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 309 | -13 | -74 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 309 | -13 | -74 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 29 | 0.00 | 17 |
| 309 | -75 | -13 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 28 | 0.00 | 17 |
| 309 | -75 | -13 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 309 | -75 | -13 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 21 | 0.00 | 17 |
| 309 | -75 | -13 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 310 | -14 | -90 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 310 | -14 | -90 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 310 | -14 | -90 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 310 | -14 | -90 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 29 | 0.00 | 17 |
| 310 | -91 | -14 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 21 | 0.00 | 17 |
| 310 | -91 | -14 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 310 | -91 | -14 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 28 | 0.00 | 17 |
| 310 | -91 | -14 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 311 | -15 | -92 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 311 | -15 | -92 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 311 | -15 | -92 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 311 | -15 | -92 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 29 | 0.00 | 17 |
| 311 | -93 | -15 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 17 | 0.00 | 17 |
| 311 | -93 | -15 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 311 | -93 | -15 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 21 | 0.00 | 17 |
| 311 | -93 | -15 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 312 | -16 | -98 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 312 | -16 | -98 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 312 | -16 | -98 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 312 | -16 | -98 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 17 | 0.00 | 17 |
| 312 | -94 | -16 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 21 | 0.00 | 17 |
| 312 | -94 | -16 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 312 | -94 | -16 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 28 | 0.00 | 17 |
| 312 | -94 | -16 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 313 | -17 | -97 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 313 | -17 | -97 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 313 | -17 | -97 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 313 | -17 | -97 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 17 | 0.00 | 17 |
| 313 | -42 | -17 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 21 | 0.00 | 17 |
| 313 | -42 | -17 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 313 | -42 | -17 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 17 | 0.00 | 17 |
| 313 | -42 | -17 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 314 | -18 | -43 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 314 | -18 | -43 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 314 | -18 | -43 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 314 | -18 | -43 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 17 | 0.00 | 17 |
| 314 | -44 | -18 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 21 | 0.00 | 17 |
| 314 | -44 | -18 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 314 | -44 | -18 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 28 | 0.00 | 17 |
| 314 | -44 | -18 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 315 | -19 | -45 | Max  | 0.00   | 159.30  | 29 | 0.00 | 17 | 0.00 | 17 | 370.64  | 28 | 302.64  | 21 | 0.00 | 17 |
| 315 | -19 | -45 | Max  | 150.00 | 41.96   | 29 | 0.00 | 17 | 0.00 | 17 | 126.13  | 28 | 0.00    | 21 | 0.00 | 17 |
| 315 | -19 | -45 | Min. | 0.00   | 142.40  | 21 | 0.00 | 17 | 0.00 | 17 | -284.86 | 21 | -372.58 | 28 | 0.00 | 17 |
| 315 | -19 | -45 | Min. | 150.00 | 35.65   | 21 | 0.00 | 17 | 0.00 | 17 | -118.65 | 21 | 0.00    | 17 | 0.00 | 17 |
| 315 | -58 | -19 | Max  | 0.00   | -35.65  | 28 | 0.00 | 17 | 0.00 | 17 | 118.65  | 21 | 0.00    | 21 | 0.00 | 17 |
| 315 | -58 | -19 | Max  | 150.00 | -142.40 | 28 | 0.00 | 17 | 0.00 | 17 | 284.86  | 21 | 302.64  | 21 | 0.00 | 17 |
| 315 | -58 | -19 | Min. | 0.00   | -41.96  | 22 | 0.00 | 17 | 0.00 | 17 | -126.13 | 28 | 0.00    | 28 | 0.00 | 17 |
| 315 | -58 | -19 | Min. | 150.00 | -159.30 | 22 | 0.00 | 17 | 0.00 | 17 | -370.64 | 28 | -372.58 | 28 | 0.00 | 17 |
| 316 | -20 | -63 | Max  | 0.00   | 103.12  | 29 | 0.00 | 17 | 0.00 | 17 | 201.76  | 28 | 138.99  | 21 | 0.00 | 17 |
| 316 | -20 | -63 | Max  | 150.00 | 20.98   | 29 | 0.00 | 17 | 0.00 | 17 | 63.07   | 28 | 0.00    | 21 | 0.00 | 17 |
| 316 | -20 | -63 | Min. | 0.00   | 94.68   | 21 | 0.00 | 17 | 0.00 | 17 | -126.00 | 21 | -198.62 | 28 | 0.00 | 17 |
| 316 | -20 | -63 | Min. | 150.00 | 17.82   | 21 | 0.00 | 17 | 0.00 | 17 | -59.33  | 21 | 0.00    | 28 | 0.00 | 17 |
| 316 | -65 | -20 | Max  | 0.00   | -17.82  | 28 | 0.00 | 17 | 0.00 | 17 | 59.33   | 21 | 0.00    | 21 | 0.00 | 17 |
| 316 | -65 | -20 | Max  | 150.00 | -94.68  | 28 | 0.00 | 17 | 0.00 | 17 | 126.00  | 21 | 138.99  | 21 | 0.00 | 17 |
| 316 | -65 | -20 | Min. | 0.00   | -20.98  | 22 | 0.00 | 17 | 0.00 | 17 | -63.07  | 28 | 0.00    | 17 | 0.00 | 17 |
| 316 | -65 | -20 | Min. | 150.00 | -103.12 | 22 | 0.00 | 17 | 0.00 | 17 | -201.76 | 28 | -198.62 | 28 | 0.00 | 17 |
| 317 | -21 | -51 | Max  | 0.00   | 103.12  | 29 | 0.00 | 17 | 0.00 | 17 | 201.76  | 28 | 138.99  | 21 | 0.00 | 17 |
| 317 | -21 | -51 | Max  | 150.00 | 20.98   | 29 | 0.00 | 17 | 0.00 | 17 | 63.07   | 28 | 0.00    | 21 | 0.00 | 17 |
| 317 | -21 | -51 | Min. | 0.00   | 94.68   | 21 | 0.00 | 17 | 0.00 | 17 | -125.99 | 21 | -198.62 | 28 | 0.00 | 17 |
| 317 | -21 | -51 | Min. | 150.00 | 17.82   | 21 | 0.00 | 17 | 0.00 | 17 | -59.33  | 21 | 0.00    | 17 | 0.00 | 17 |
| 317 | -50 | -21 | Max  | 0.00   | -1      |    |      |    |      |    |         |    |         |    |      |    |





|     |      |     |      |        |         |    |      |    |      |    |         |    |         |    |      |    |
|-----|------|-----|------|--------|---------|----|------|----|------|----|---------|----|---------|----|------|----|
| 334 | -38  | -99 | Min. | 0.00   | 94.68   | 21 | 0.00 | 17 | 0.00 | 17 | -125.99 | 21 | -198.62 | 28 | 0.00 | 17 |
| 334 | -38  | -99 | Min. | 150.00 | 17.82   | 21 | 0.00 | 17 | 0.00 | 17 | -59.33  | 21 | 0.00    | 28 | 0.00 | 17 |
| 334 | -100 | -38 | Max  | 0.00   | -17.82  | 28 | 0.00 | 17 | 0.00 | 17 | 59.33   | 21 | 0.00    | 28 | 0.00 | 17 |
| 334 | -100 | -38 | Max  | 150.00 | -94.68  | 28 | 0.00 | 17 | 0.00 | 17 | 125.99  | 21 | 138.99  | 21 | 0.00 | 17 |
| 334 | -100 | -38 | Min. | 0.00   | -20.98  | 22 | 0.00 | 17 | 0.00 | 17 | -63.07  | 28 | 0.00    | 21 | 0.00 | 17 |
| 334 | -100 | -38 | Min. | 150.00 | -103.12 | 22 | 0.00 | 17 | 0.00 | 17 | -201.76 | 28 | -198.62 | 28 | 0.00 | 17 |

Tipo di combinazione di carico: SLE R

| Asta | N1  | N2  |      | X<br><cm> | N<br><daN> | CC Ty<br><daN> | CC Mz<br><daNm> | CC Tz<br><daN> | CC My<br><daNm> | CC Mx<br><daNm> | CC       |    |          |    |        |    |
|------|-----|-----|------|-----------|------------|----------------|-----------------|----------------|-----------------|-----------------|----------|----|----------|----|--------|----|
| 1    | 1   | -5  | Max  | 0.00      | -290.35    | 23             | -23.24          | 23             | 100.31          | 30              | 1410.97  | 23 | 3364.34  | 30 | 0.05   | 30 |
| 1    | 1   | -5  | Max  | 330.00    | -101.12    | 23             | -23.24          | 23             | -51.58          | 23              | 1410.97  | 23 | 84.08    | 30 | 0.05   | 30 |
| 1    | 1   | -5  | Min. | 0.00      | -1970.13   | 30             | -91.85          | 30             | 25.12           | 23              | -994.02  | 30 | -4775.57 | 23 | -0.08  | 23 |
| 1    | 1   | -5  | Min. | 330.00    | -1780.89   | 30             | -91.85          | 30             | -202.80         | 30              | -994.02  | 30 | -119.35  | 23 | -0.08  | 23 |
| 2    | 2   | -10 | Max  | 0.00      | -241.41    | 23             | 175.07          | 30             | -9.76           | 23              | 1928.85  | 23 | 4424.80  | 30 | 0.93   | 30 |
| 2    | 2   | -10 | Max  | 330.00    | -52.17     | 23             | 175.07          | 30             | 386.84          | 30              | 1928.85  | 23 | 84.33    | 23 | 0.93   | 30 |
| 2    | 2   | -10 | Min. | 0.00      | -2553.53   | 30             | 8.78            | 23             | -190.88         | 30              | -1358.85 | 30 | -6280.87 | 23 | -1.31  | 23 |
| 2    | 2   | -10 | Min. | 330.00    | -2364.29   | 30             | 8.78            | 23             | 19.21           | 23              | -1358.85 | 30 | -59.41   | 30 | -1.31  | 23 |
| 3    | 3   | 203 | Max  | 0.00      | -260.40    | 23             | -3.27           | 23             | 120.99          | 30              | 2101.08  | 23 | 4816.03  | 30 | 0.80   | 23 |
| 3    | 3   | 203 | Max  | 330.00    | -71.16     | 23             | -3.27           | 23             | -7.30           | 23              | 2101.08  | 23 | 97.37    | 23 | 0.80   | 23 |
| 3    | 3   | 203 | Min. | 0.00      | -2779.89   | 30             | -110.89         | 30             | 3.48            | 23              | -1480.19 | 30 | -6836.21 | 23 | -0.57  | 30 |
| 3    | 3   | 203 | Min. | 330.00    | -2590.65   | 30             | -110.89         | 30             | -244.94         | 30              | -1480.19 | 30 | -68.59   | 30 | -0.57  | 30 |
| 4    | 4   | 204 | Max  | 0.00      | -351.17    | 23             | 0.00            | 30             | 0.00            | 23              | 1211.14  | 30 | 5798.00  | 23 | 0.00   | 23 |
| 4    | 4   | 204 | Max  | 330.00    | -161.93    | 23             | 0.00            | 30             | 0.00            | 30              | 1211.14  | 30 | 124.72   | 23 | 0.00   | 23 |
| 4    | 4   | 204 | Min. | 0.00      | -2367.64   | 30             | -0.00           | 23             | 0.00            | 30              | -1719.18 | 23 | -4084.63 | 30 | 0.00   | 30 |
| 4    | 4   | 204 | Min. | 330.00    | -2178.41   | 30             | -0.00           | 23             | 0.00            | 23              | -1719.18 | 23 | -87.86   | 30 | 0.00   | 30 |
| 5    | 5   | 205 | Max  | 0.00      | -260.40    | 23             | -3.27           | 23             | 120.99          | 30              | 1480.19  | 30 | 6836.20  | 23 | 0.57   | 30 |
| 5    | 5   | 205 | Max  | 330.00    | -71.16     | 23             | -3.27           | 23             | -7.30           | 23              | 1480.19  | 30 | 68.59    | 30 | 0.57   | 30 |
| 5    | 5   | 205 | Min. | 0.00      | -2779.89   | 30             | -110.89         | 30             | 3.48            | 23              | -2101.08 | 23 | -4816.04 | 30 | -0.80  | 23 |
| 5    | 5   | 205 | Min. | 330.00    | -2590.65   | 30             | -110.89         | 30             | -244.94         | 30              | -2101.08 | 23 | -97.37   | 23 | -0.80  | 23 |
| 6    | 6   | -31 | Max  | 0.00      | -241.41    | 23             | 175.07          | 30             | -9.76           | 23              | 1358.85  | 30 | 6280.86  | 23 | 1.31   | 23 |
| 6    | 6   | -31 | Max  | 330.00    | -52.18     | 23             | 175.07          | 30             | 386.85          | 30              | 1358.85  | 30 | 59.40    | 30 | 1.31   | 23 |
| 6    | 6   | -31 | Min. | 0.00      | -2553.53   | 30             | 8.78            | 23             | -190.89         | 30              | -1928.84 | 23 | -4424.80 | 30 | -0.93  | 30 |
| 6    | 6   | -31 | Min. | 330.00    | -2364.29   | 30             | 8.78            | 23             | 19.21           | 23              | -1928.84 | 23 | -84.33   | 23 | -0.93  | 30 |
| 7    | 7   | -36 | Max  | 0.00      | -290.35    | 23             | -23.24          | 23             | 100.31          | 30              | 994.02   | 30 | 4775.57  | 23 | 0.08   | 23 |
| 7    | 7   | -36 | Max  | 330.00    | -101.12    | 23             | -23.24          | 23             | -51.58          | 23              | 994.02   | 30 | 119.35   | 23 | 0.08   | 23 |
| 7    | 7   | -36 | Min. | 0.00      | -1970.13   | 30             | -91.85          | 30             | 25.12           | 23              | -1410.98 | 23 | -3364.34 | 30 | -0.05  | 30 |
| 7    | 7   | -36 | Min. | 330.00    | -1780.89   | 30             | -91.85          | 30             | -202.81         | 30              | -1410.98 | 23 | -84.08   | 30 | -0.05  | 30 |
| 201  | -4  | -3  | Max  | 0.00      | 0.00       | 18             | 147.95          | 30             | 280.44          | 23              | 333.86   | 30 | -68.11   | 23 | 0.00   | 30 |
| 201  | -4  | -3  | Max  | 133.53    | 0.00       | 18             | 147.95          | 30             | 0.00            | 30              | 269.46   | 30 | 0.00     | 30 | 0.00   | 30 |
| 201  | -4  | -3  | Min. | 0.00      | 0.00       | 18             | -210.02         | 23             | -197.57         | 30              | 83.21    | 23 | -402.81  | 30 | 0.00   | 23 |
| 201  | -4  | -3  | Min. | 133.53    | 0.00       | 18             | -210.02         | 23             | 0.00            | 23              | 18.80    | 23 | 0.00     | 23 | 0.00   | 23 |
| 201  | -5  | -4  | Max  | 0.00      | 0.00       | 18             | 443.86          | 30             | 781.12          | 23              | 822.93   | 30 | -109.28  | 23 | 0.00   | 30 |
| 201  | -5  | -4  | Max  | 79.47     | 0.00       | 18             | 443.86          | 30             | 280.44          | 23              | 784.61   | 30 | -68.11   | 23 | 0.00   | 30 |
| 201  | -5  | -4  | Min. | 0.00      | 0.00       | 18             | -630.05         | 23             | -550.29         | 30              | 70.97    | 23 | -1041.54 | 30 | 0.00   | 23 |
| 201  | -5  | -4  | Min. | 79.47     | 0.00       | 18             | -630.05         | 23             | -197.57         | 30              | 32.64    | 23 | -402.81  | 30 | 0.00   | 23 |
| 201  | -6  | -5  | Max  | 0.00      | 91.85      | 30             | 780.93          | 23             | 358.97          | 23              | -4.07    | 23 | -48.45   | 23 | 119.35 | 23 |
| 201  | -6  | -5  | Max  | 54.07     | 91.85      | 30             | 780.93          | 23             | 781.19          | 23              | -30.15   | 23 | -57.70   | 23 | 119.35 | 23 |
| 201  | -6  | -5  | Min. | 0.00      | 23.24      | 23             | -550.15         | 30             | -252.89         | 30              | -931.88  | 30 | -327.85  | 30 | -84.08 | 30 |
| 201  | -6  | -5  | Min. | 54.07     | 23.24      | 23             | -550.15         | 30             | -550.34         | 30              | -957.96  | 30 | -838.74  | 30 | -84.08 | 30 |
| 201  | -7  | -6  | Max  | 0.00      | 91.85      | 30             | 360.89          | 23             | 86.61           | 30              | 9.77     | 23 | 271.63   | 30 | 119.35 | 23 |
| 201  | -7  | -6  | Max  | 20.26     |            |                |                 |                | -49.83          | 23              |          |    | -17.51   | 23 |        |    |
| 201  | -7  | -6  | Max  | 133.53    | 91.85      | 30             | 360.89          | 23             | 358.97          | 23              | -54.63   | 23 | -48.45   | 23 | 119.35 | 23 |
| 201  | -7  | -6  | Min. | 0.00      | 23.24      | 23             | -254.25         | 30             | -122.94         | 23              | -416.73  | 30 | -18.50   | 23 | -84.08 | 30 |
| 201  | -7  | -6  | Min. | 20.26     |            |                |                 |                | -49.83          | 23              |          |    | -17.51   | 23 |        |    |
| 201  | -7  | -6  | Min. | 133.53    | 23.24      | 23             | -254.25         | 30             | -252.89         | 30              | -481.13  | 30 | -327.85  | 30 | -84.08 | 30 |
| 201  | -8  | -7  | Max  | 0.00      | 91.85      | 30             | 41.66           | 30             | 30.98           | 30              | 98.42    | 30 | 183.21   | 30 | 119.35 | 23 |
| 201  | -8  | -7  | Max  | 93.86     |            |                |                 |                | -59.69          | 24              |          |    | 69.30    | 24 |        |    |
| 201  | -8  | -7  | Max  | 133.53    | 91.85      | 30             | 41.66           | 30             | 86.61           | 30              | 34.01    | 30 | 271.63   | 30 | 119.35 | 23 |
| 201  | -8  | -7  | Min. | 0.00      | 23.24      | 23             | -59.14          | 23             | -43.97          | 23              | 23.61    | 23 | -7.03    | 23 | -84.08 | 30 |
| 201  | -8  | -7  | Min. | 48.96     |            |                |                 |                | -72.93          | 23              |          |    | -1.25    | 23 |        |    |
| 201  | -8  | -7  | Min. | 133.53    | 23.24      | 23             | -59.14          | 23             | -122.94         | 23              | -40.79   | 23 | -18.50   | 23 | -84.08 | 30 |
| 201  | -9  | -8  | Max  | 0.00      | 91.85      | 30             | 337.57          | 30             | 595.88          | 23              | 613.57   | 30 | -14.04   | 23 | 119.35 | 23 |
| 201  | -9  | -8  | Max  | 77.65     |            |                |                 |                | 223.80          | 23              |          |    | 0.51     | 23 |        |    |
| 201  | -9  | -8  | Max  | 133.53    | 91.85      | 30             | 337.57          | 30             | 30.98           | 30              | 549.16   | 30 | 183.21   | 30 | 119.35 | 23 |
| 201  | -9  | -8  | Min. | 0.00      | 23.24      | 23             | -479.17         | 23             | -419.79         | 30              | 37.45    | 23 | -593.10  | 30 | -84.08 | 30 |
| 201  | -9  | -8  | Min. | 77.65     |            |                |                 |                | 223.80          | 23              |          |    | 0.51     | 23 |        |    |
| 201  | -9  | -8  | Min. | 133.53    | 23.24      | 23             | -479.17         | 23             | -43.98          | 23              | -26.95   | 23 | -7.03    | 23 | -84.08 | 30 |
| 201  | -10 | -9  | Max  | 0.00      | 91.85      | 30             | 633.48          | 30             | 1003.53         | 23              | 1086.17  | 30 | -13.05   | 23 | 119.35 | 23 |
| 201  | -10 | -9  | Max  | 18.13     |            |                |                 |                | 840.47          | 23              |          |    | -12.25   | 23 |        |    |
| 201  | -10 | -9  | Max  | 45.33     | 91.85      | 30             | 633.48          | 30             | 595.88          | 23              | 1064.31  | 30 | -14.04   | 23 | 119.35 | 23 |
| 201  | -10 | -9  | Min. | 0.00      | 23.24      | 23             | -899.21         | 23             | -706.97         | 30              | 8.75     | 23 | -1080.55 | 30 | -84.08 | 30 |
| 201  | -10 | -9  | Min. | 18.13     |            |                |                 |                | 840.47          | 23              |          |    | -12.25   | 23 |        |    |
| 201  | -10 | -9  | Min. | 45.33     | 23.24      | 23             | -899.21         | 23             | -419.79         | 30              | -13.11   | 23 | -593.11  | 30 | -84.08 | 30 |
| 202  | -11 | -10 | Max  | 0.00      | 14.46      | 23             | 1029.64         | 23             | 96.70           | 23              | -0.88    | 23 | -12.72   | 23 | 35.02  | 23 |
| 202  | -11 | -10 | Max  | 88.20     | 14.46      | 23             | 1029.64         | 23             | 1004.84         | 23              | -43.42   | 23 | -32.26   | 23 | 35.02  | 23 |
| 202  | -11 | -10 | Min. | 0.00      | -83.22     | 30             | -725.37         | 30             | -68.12          | 30              | -1235.58 | 30 | -358.85  | 30 | -24.67 | 30 |
| 202  | -11 | -10 | Min. | 88.20     | -83.22     | 30             | -725.37         | 30             | -707.90         | 30              | -1278.12 | 30 | -1467.39 | 30 | -24.67 | 30 |
| 202  | -12 | -11 | Max  | 0.00      | 14.46      | 23             | 609.61          | 23             | 505.35          | 30              | 12.96    | 23 | 646.16   | 30 | 35.02  | 23 |
| 202  | -12 | -11 | Max  | 26.71     |            |                |                 |                | -554.53         | 23              |          |    | 14.72    | 23 |        |    |
| 202  | -12 | -11 | Max  | 133.53    | 14.46      | 23             | 609.61          | 23             | 96.70           | 23              | -51.45   | 23 | -12.72   | 23 | 35.02  | 23 |
| 202  | -12 | -11 | Min. | 0.00      | -83.22     | 30             | -429.46         | 30             | -717.33         | 23              | -720.43  | 30 | 12.98    | 23 | -24.67 | 30 |
| 202  | -12 | -11 | Min. | 26.71     |            |                |                 |                | -554.53         | 23              |          |    | 14.72    | 23 |        |    |
| 202  | -12 | -11 | Min. | 133.53    | -83.22     | 30             | -429.46         | 30             | -68.12          | 30              | -784.84  | 30 | -358.86  | 30 | -24.67 | 30 |
| 202  | -13 | -12 | Max  | 0.00      | 14.46      | 23             | 189.57          | 23             | 683.69          | 30              | 26.80    | 23 | 963.29   | 30 | 35.02  | 23 |
| 202  | -13 | -12 | Max  | 55.56     |            |                |                 |                | -865.15         | 23              |          |    | 27.64    | 23 |        |    |
| 202  | -13 | -12 | Max  | 133.53    | 14.46      | 23             | 189.57          | 23             | 505.35          | 30              | -37.61   | 23 | 646.16   | 30 | 35.02  | 23 |
| 202  | -13 | -12 | Min. | 0.00      | -83.22     | 30             | -133.55         | 30             | -970.48         | 23              | -205.28  | 30 | 20.20    | 23 | -24.67 |    |





|     |     |     |      |        |         |    |          |    |          |    |          |    |          |    |         |    |
|-----|-----|-----|------|--------|---------|----|----------|----|----------|----|----------|----|----------|----|---------|----|
| 205 | -30 | -31 | Min. | 88.20  | -83.22  | 30 | -1029.64 | 23 | -1004.83 | 23 | -1278.12 | 30 | -1467.39 | 30 | -35.02  | 23 |
| 206 | -31 | -32 | Max  | 0.00   | 91.85   | 30 | 899.20   | 23 | 706.97   | 30 | 1086.17  | 30 | -13.05   | 23 | 84.08   | 30 |
| 206 | -31 | -32 | Max  | 18.13  |         |    |          |    | -840.46  | 23 |          |    | -12.25   | 23 |         |    |
| 206 | -31 | -32 | Max  | 45.33  | 91.85   | 30 | 899.20   | 23 | 419.79   | 30 | 1064.31  | 30 | -14.04   | 23 | 84.08   | 30 |
| 206 | -31 | -32 | Min. | 0.00   | 23.24   | 23 | -633.48  | 30 | -1003.52 | 23 | 8.75     | 23 | -1080.54 | 30 | -119.34 | 23 |
| 206 | -31 | -32 | Min. | 18.13  |         |    |          |    | -840.46  | 23 |          |    | -12.25   | 23 |         |    |
| 206 | -31 | -32 | Min. | 45.33  | 23.24   | 23 | -633.48  | 30 | -595.88  | 23 | -13.11   | 23 | -593.10  | 30 | -119.34 | 23 |
| 206 | -32 | -33 | Max  | 0.00   | 91.85   | 30 | 479.17   | 23 | 419.81   | 30 | 613.57   | 30 | -14.04   | 23 | 84.08   | 30 |
| 206 | -32 | -33 | Max  | 77.65  |         |    |          |    | -223.81  | 23 |          |    | 0.51     | 23 |         |    |
| 206 | -32 | -33 | Min. | 133.53 | 91.85   | 30 | 479.17   | 23 | 43.94    | 23 | 549.16   | 30 | 183.18   | 30 | 84.08   | 30 |
| 206 | -32 | -33 | Min. | 0.00   | 23.24   | 23 | -337.57  | 30 | -595.91  | 23 | 37.45    | 23 | -593.14  | 30 | -119.35 | 23 |
| 206 | -32 | -33 | Min. | 77.65  |         |    |          |    | -223.81  | 23 |          |    | 0.51     | 23 |         |    |
| 206 | -32 | -33 | Min. | 133.53 | 23.24   | 23 | -337.57  | 30 | -30.96   | 30 | -26.95   | 23 | -7.02    | 23 | -119.35 | 23 |
| 206 | -33 | -34 | Max  | 0.00   | 91.85   | 30 | 59.14    | 23 | 43.97    | 23 | 98.41    | 30 | 183.21   | 30 | 84.08   | 30 |
| 206 | -33 | -34 | Max  | 93.86  |         |    |          |    | 59.69    | 24 |          |    | 69.30    | 24 |         |    |
| 206 | -33 | -34 | Max  | 133.53 | 91.85   | 30 | 59.14    | 23 | 122.94   | 23 | 34.01    | 30 | 271.63   | 30 | 84.08   | 30 |
| 206 | -33 | -34 | Min. | 0.00   | 23.24   | 23 | -41.66   | 30 | -30.98   | 30 | 23.61    | 23 | -7.03    | 23 | -119.35 | 23 |
| 206 | -33 | -34 | Min. | 48.95  |         |    |          |    | 72.92    | 23 |          |    | -1.25    | 23 |         |    |
| 206 | -33 | -34 | Min. | 133.53 | 23.24   | 23 | -41.66   | 30 | -86.61   | 30 | -40.79   | 23 | -18.50   | 23 | -119.35 | 23 |
| 206 | -34 | -35 | Max  | 0.00   | 91.85   | 30 | 254.25   | 30 | 122.94   | 23 | 9.77     | 23 | 271.63   | 30 | 84.08   | 30 |
| 206 | -34 | -35 | Max  | 20.26  |         |    |          |    | 49.83    | 23 |          |    | -17.51   | 23 |         |    |
| 206 | -34 | -35 | Max  | 133.53 | 91.85   | 30 | 254.25   | 30 | 252.90   | 30 | -54.63   | 23 | -48.45   | 23 | 84.08   | 30 |
| 206 | -34 | -35 | Min. | 0.00   | 23.24   | 23 | -360.89  | 23 | -86.61   | 30 | -416.73  | 30 | -18.50   | 23 | -119.35 | 23 |
| 206 | -34 | -35 | Min. | 20.26  |         |    |          |    | 49.83    | 23 |          |    | -17.51   | 23 |         |    |
| 206 | -34 | -35 | Min. | 133.53 | 23.24   | 23 | -360.89  | 23 | -358.98  | 23 | -481.14  | 30 | -327.85  | 30 | -119.35 | 23 |
| 206 | -35 | -36 | Max  | 0.00   | 91.85   | 30 | 550.16   | 30 | 252.89   | 30 | -4.07    | 23 | -48.45   | 23 | 84.08   | 30 |
| 206 | -35 | -36 | Max  | 54.07  | 91.85   | 30 | 550.16   | 30 | 550.34   | 30 | -30.14   | 23 | -57.70   | 23 | 84.08   | 30 |
| 206 | -35 | -36 | Min. | 0.00   | 23.24   | 23 | -780.93  | 23 | -358.96  | 23 | -931.88  | 30 | -327.83  | 30 | -119.35 | 23 |
| 206 | -35 | -36 | Min. | 54.07  | 23.24   | 23 | -780.93  | 23 | -781.19  | 23 | -957.96  | 30 | -838.72  | 30 | -119.35 | 23 |
| 206 | -36 | -37 | Max  | 0.00   | 0.00    | 18 | 630.05   | 23 | 550.30   | 30 | 822.93   | 30 | -109.28  | 23 | 0.00    | 23 |
| 206 | -36 | -37 | Max  | 79.47  | 0.00    | 18 | 630.05   | 23 | 197.58   | 30 | 784.61   | 30 | -68.11   | 23 | 0.00    | 23 |
| 206 | -36 | -37 | Min. | 0.00   | 0.00    | 18 | -443.86  | 30 | -781.13  | 23 | 70.97    | 23 | -1041.56 | 30 | -0.00   | 30 |
| 206 | -36 | -37 | Min. | 79.47  | 0.00    | 18 | -443.86  | 30 | -280.46  | 23 | 32.64    | 23 | -402.83  | 30 | -0.00   | 30 |
| 206 | -37 | -38 | Max  | 0.00   | 0.00    | 18 | 210.02   | 23 | 197.56   | 30 | 333.86   | 30 | -68.11   | 23 | 0.00    | 23 |
| 206 | -37 | -38 | Max  | 133.53 | 0.00    | 18 | 210.02   | 23 | 0.01     | 23 | 269.46   | 30 | 0.01     | 30 | 0.00    | 23 |
| 206 | -37 | -38 | Min. | 0.00   | 0.00    | 18 | -147.95  | 30 | -280.44  | 23 | 83.21    | 23 | -402.81  | 30 | 0.00    | 30 |
| 206 | -37 | -38 | Min. | 133.53 | 0.00    | 18 | -147.95  | 30 | -0.00    | 30 | 18.80    | 23 | 0.00     | 23 | 0.00    | 30 |
| 301 | -3  | -60 | Max  | 0.00   | 73.56   | 31 | 0.00     | 18 | 0.00     | 18 | 137.88   | 30 | 90.13    | 23 | 0.00    | 18 |
| 301 | -3  | -60 | Max  | 150.00 | 13.99   | 31 | 0.00     | 18 | 0.00     | 18 | 42.04    | 30 | 0.00     | 23 | 0.00    | 18 |
| 301 | -3  | -60 | Min. | 0.00   | 67.93   | 23 | 0.00     | 18 | 0.00     | 18 | -80.62   | 23 | -134.94  | 30 | 0.00    | 18 |
| 301 | -3  | -60 | Min. | 150.00 | 11.88   | 23 | 0.00     | 18 | 0.00     | 18 | -39.55   | 23 | 0.00     | 18 | 0.00    | 18 |
| 301 | -59 | -3  | Max  | 0.00   | -11.88  | 30 | 0.00     | 18 | 0.00     | 23 | 39.55    | 23 | 0.00     | 23 | 0.00    | 18 |
| 301 | -59 | -3  | Max  | 150.00 | -67.93  | 30 | 0.00     | 18 | 0.00     | 23 | 80.62    | 23 | 90.13    | 23 | 0.00    | 18 |
| 301 | -59 | -3  | Min. | 0.00   | -13.99  | 24 | 0.00     | 18 | 0.00     | 18 | -42.04   | 30 | 0.00     | 18 | 0.00    | 18 |
| 301 | -59 | -3  | Min. | 150.00 | -73.56  | 24 | 0.00     | 18 | 0.00     | 18 | -137.88  | 30 | -134.94  | 30 | 0.00    | 18 |
| 302 | -4  | -47 | Max  | 0.00   | 111.02  | 31 | 0.00     | 18 | 0.00     | 18 | 250.47   | 30 | 199.23   | 23 | 0.00    | 18 |
| 302 | -4  | -47 | Max  | 150.00 | 27.97   | 31 | 0.00     | 18 | 0.00     | 18 | 84.09    | 30 | 0.00     | 23 | 0.00    | 18 |
| 302 | -4  | -47 | Min. | 0.00   | 99.75   | 23 | 0.00     | 18 | 0.00     | 18 | -186.54  | 23 | -250.92  | 30 | 0.00    | 18 |
| 302 | -4  | -47 | Min. | 150.00 | 23.76   | 23 | 0.00     | 18 | 0.00     | 18 | -79.10   | 23 | 0.00     | 18 | 0.00    | 18 |
| 302 | -46 | -4  | Max  | 0.00   | -23.76  | 30 | 0.00     | 18 | 0.00     | 18 | 79.10    | 23 | 0.00     | 23 | 0.00    | 18 |
| 302 | -46 | -4  | Max  | 150.00 | -99.75  | 30 | 0.00     | 18 | 0.00     | 18 | 186.54   | 23 | 199.23   | 23 | 0.00    | 18 |
| 302 | -46 | -4  | Min. | 0.00   | -27.97  | 24 | 0.00     | 18 | 0.00     | 18 | -84.09   | 30 | 0.00     | 30 | 0.00    | 18 |
| 302 | -46 | -4  | Min. | 150.00 | -111.02 | 24 | 0.00     | 18 | 0.00     | 18 | -250.47  | 30 | -250.92  | 30 | 0.00    | 18 |
| 303 | -6  | -48 | Max  | 0.00   | 111.02  | 31 | 0.00     | 18 | 0.00     | 18 | 250.47   | 30 | 199.23   | 23 | 0.00    | 18 |
| 303 | -6  | -48 | Max  | 150.00 | 27.97   | 31 | 0.00     | 18 | 0.00     | 18 | 84.09    | 30 | 0.00     | 23 | 0.00    | 18 |
| 303 | -6  | -48 | Min. | 0.00   | 99.75   | 23 | 0.00     | 18 | 0.00     | 18 | -186.54  | 23 | -250.92  | 30 | 0.00    | 18 |
| 303 | -6  | -48 | Min. | 150.00 | 23.76   | 23 | 0.00     | 18 | 0.00     | 18 | -79.10   | 23 | 0.00     | 18 | 0.00    | 18 |
| 303 | -49 | -6  | Max  | 0.00   | -23.76  | 30 | 0.00     | 18 | 0.00     | 18 | 79.10    | 23 | 0.00     | 23 | 0.00    | 18 |
| 303 | -49 | -6  | Max  | 150.00 | -99.75  | 30 | 0.00     | 18 | 0.00     | 18 | 186.54   | 23 | 199.23   | 23 | 0.00    | 18 |
| 303 | -49 | -6  | Min. | 0.00   | -27.97  | 24 | 0.00     | 18 | 0.00     | 18 | -84.09   | 30 | 0.00     | 18 | 0.00    | 18 |
| 303 | -49 | -6  | Min. | 150.00 | -111.02 | 24 | 0.00     | 18 | 0.00     | 18 | -250.47  | 30 | -250.92  | 30 | 0.00    | 18 |
| 304 | -7  | -96 | Max  | 0.00   | 111.02  | 31 | 0.00     | 18 | 0.00     | 18 | 250.47   | 30 | 199.23   | 23 | 0.00    | 18 |
| 304 | -7  | -96 | Max  | 150.00 | 27.97   | 31 | 0.00     | 18 | 0.00     | 18 | 84.09    | 30 | 0.00     | 23 | 0.00    | 18 |
| 304 | -7  | -96 | Min. | 0.00   | 99.75   | 23 | 0.00     | 18 | 0.00     | 18 | -186.54  | 23 | -250.92  | 30 | 0.00    | 18 |
| 304 | -7  | -96 | Min. | 150.00 | 23.76   | 23 | 0.00     | 18 | 0.00     | 18 | -79.10   | 23 | 0.00     | 18 | 0.00    | 18 |
| 304 | -95 | -7  | Max  | 0.00   | -23.76  | 30 | 0.00     | 18 | 0.00     | 18 | 79.10    | 23 | 0.00     | 23 | 0.00    | 18 |
| 304 | -95 | -7  | Max  | 150.00 | -99.75  | 30 | 0.00     | 18 | 0.00     | 18 | 186.54   | 23 | 199.23   | 23 | 0.00    | 18 |
| 304 | -95 | -7  | Min. | 0.00   | -27.97  | 24 | 0.00     | 18 | 0.00     | 18 | -84.09   | 30 | 0.00     | 18 | 0.00    | 18 |
| 304 | -95 | -7  | Min. | 150.00 | -111.02 | 24 | 0.00     | 18 | 0.00     | 18 | -250.47  | 30 | -250.92  | 30 | 0.00    | 18 |
| 305 | -8  | -66 | Max  | 0.00   | 111.02  | 31 | 0.00     | 18 | 0.00     | 18 | 250.47   | 30 | 199.23   | 23 | 0.00    | 18 |
| 305 | -8  | -66 | Max  | 150.00 | 27.97   | 31 | 0.00     | 18 | 0.00     | 18 | 84.09    | 30 | 0.00     | 23 | 0.00    | 18 |
| 305 | -8  | -66 | Min. | 0.00   | 99.75   | 23 | 0.00     | 18 | 0.00     | 18 | -186.54  | 23 | -250.92  | 30 | 0.00    | 18 |
| 305 | -8  | -66 | Min. | 150.00 | 23.76   | 23 | 0.00     | 18 | 0.00     | 18 | -79.10   | 23 | 0.00     | 18 | 0.00    | 18 |
| 305 | -67 | -8  | Max  | 0.00   | -23.76  | 30 | 0.00     | 18 | 0.00     | 18 | 79.10    | 23 | 0.00     | 23 | 0.00    | 18 |
| 305 | -67 | -8  | Max  | 150.00 | -99.75  | 30 | 0.00     | 18 | 0.00     | 18 | 186.54   | 23 | 199.23   | 23 | 0.00    | 18 |
| 305 | -67 | -8  | Min. | 0.00   | -27.97  | 24 | 0.00     | 18 | 0.00     | 18 | -84.09   | 30 | 0.00     | 18 | 0.00    | 18 |
| 305 | -67 | -8  | Min. | 150.00 | -111.02 | 24 | 0.00     | 18 | 0.00     | 18 | -250.47  | 30 | -250.92  | 30 | 0.00    | 18 |
| 306 | -9  | -69 | Max  | 0.00   | 111.02  | 31 | 0.00     | 18 | 0.00     | 18 | 250.47   | 30 | 199.23   | 23 | 0.00    | 18 |
| 306 | -9  | -69 | Max  | 150.00 | 27.97   | 31 | 0.00     | 18 | 0.00     | 18 | 84.09    | 30 | 0.00     | 23 | 0.00    | 18 |
| 306 | -9  | -69 | Min. | 0.00   | 99.75   | 23 | 0.00     | 18 | 0.00     | 18 | -186.54  | 23 | -250.92  | 30 | 0.00    | 18 |
| 306 | -9  | -69 | Min. | 150.00 | 23.76   | 23 | 0.00     | 18 | 0.00     | 18 | -79.10   | 23 | 0.00     | 18 | 0.00    | 18 |
| 306 | -68 | -9  | Max  | 0.00   | -23.76  | 30 | 0.00     | 18 | 0.00     | 18 | 79.10    | 23 | 0.00     | 23 | 0.00    | 18 |
| 306 | -68 | -9  | Max  | 150.00 | -99.75  | 30 | 0.00     | 18 | 0.00     | 18 | 186.54   | 23 | 199.23   | 23 | 0.00    | 18 |
| 306 | -68 | -9  | Min. | 0.00   | -27.97  | 24 | 0.00     | 18 | 0.00     | 18 | -84.09   | 30 | 0.00     | 18 | 0.00    | 18 |
| 306 | -68 | -9  | Min. | 150.00 | -111.02 | 24 | 0.00     | 18 | 0.00     | 18 | -250.47  | 30 | -250.92  | 30 | 0.00    | 18 |
| 307 | -11 | -70 | Max  | 0.00   | 111.02  | 31 | 0.00     | 18 | 0.00     | 18 | 250.47   | 30 | 199.23   | 23 | 0.00    | 18 |
| 307 | -11 | -70 | Max  | 150.00 | 27.97   | 31 | 0.00     | 18 |          |    |          |    |          |    |         |    |



|     |     |     |      |        |         |    |      |    |      |    |         |    |         |    |      |    |
|-----|-----|-----|------|--------|---------|----|------|----|------|----|---------|----|---------|----|------|----|
| 309 | -13 | -74 | Max  | 0.00   | 111.02  | 31 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 309 | -13 | -74 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 309 | -13 | -74 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 309 | -13 | -74 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 31 | 0.00 | 18 |
| 309 | -75 | -13 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0.00    | 30 | 0.00 | 18 |
| 309 | -75 | -13 | Max  | 150.00 | -99.75  | 30 | 0.00 | 18 | 0.00 | 18 | 186.54  | 23 | 199.23  | 23 | 0.00 | 18 |
| 309 | -75 | -13 | Min. | 0.00   | -27.97  | 24 | 0.00 | 18 | 0.00 | 18 | -84.09  | 30 | 0.00    | 23 | 0.00 | 18 |
| 309 | -75 | -13 | Min. | 150.00 | -111.02 | 24 | 0.00 | 18 | 0.00 | 18 | -250.47 | 30 | -250.92 | 30 | 0.00 | 18 |
| 310 | -14 | -90 | Max  | 0.00   | 111.02  | 31 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 310 | -14 | -90 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 310 | -14 | -90 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 310 | -14 | -90 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 31 | 0.00 | 18 |
| 310 | -91 | -14 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0.00    | 23 | 0.00 | 18 |
| 310 | -91 | -14 | Max  | 150.00 | -99.75  | 30 | 0.00 | 18 | 0.00 | 18 | 186.54  | 23 | 199.23  | 23 | 0.00 | 18 |
| 310 | -91 | -14 | Min. | 0.00   | -27.97  | 24 | 0.00 | 18 | 0.00 | 18 | -84.09  | 30 | 0.00    | 23 | 0.00 | 18 |
| 310 | -91 | -14 | Min. | 150.00 | -111.02 | 24 | 0.00 | 18 | 0.00 | 18 | -250.47 | 30 | -250.92 | 30 | 0.00 | 18 |
| 311 | -15 | -92 | Max  | 0.00   | 111.02  | 31 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 311 | -15 | -92 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 311 | -15 | -92 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 311 | -15 | -92 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 31 | 0.00 | 18 |
| 311 | -93 | -15 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0.00    | 18 | 0.00 | 18 |
| 311 | -93 | -15 | Max  | 150.00 | -99.75  | 30 | 0.00 | 18 | 0.00 | 18 | 186.54  | 23 | 199.23  | 23 | 0.00 | 18 |
| 311 | -93 | -15 | Min. | 0.00   | -27.97  | 24 | 0.00 | 18 | 0.00 | 18 | -84.09  | 30 | 0.00    | 23 | 0.00 | 18 |
| 311 | -93 | -15 | Min. | 150.00 | -111.02 | 24 | 0.00 | 18 | 0.00 | 18 | -250.47 | 30 | -250.92 | 30 | 0.00 | 18 |
| 312 | -16 | -98 | Max  | 0.00   | 111.02  | 31 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 312 | -16 | -98 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 312 | -16 | -98 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 312 | -16 | -98 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 18 | 0.00 | 18 |
| 312 | -94 | -16 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0.00    | 23 | 0.00 | 18 |
| 312 | -94 | -16 | Max  | 150.00 | -99.75  | 30 | 0.00 | 18 | 0.00 | 18 | 186.54  | 23 | 199.23  | 23 | 0.00 | 18 |
| 312 | -94 | -16 | Min. | 0.00   | -27.97  | 24 | 0.00 | 18 | 0.00 | 18 | -84.09  | 30 | 0.00    | 30 | 0.00 | 18 |
| 312 | -94 | -16 | Min. | 150.00 | -111.02 | 24 | 0.00 | 18 | 0.00 | 18 | -250.47 | 30 | -250.92 | 30 | 0.00 | 18 |
| 313 | -17 | -97 | Max  | 0.00   | 111.02  | 31 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 313 | -17 | -97 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 313 | -17 | -97 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 313 | -17 | -97 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 18 | 0.00 | 18 |
| 313 | -42 | -17 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0.00    | 23 | 0.00 | 18 |
| 313 | -42 | -17 | Max  | 150.00 | -99.75  | 30 | 0.00 | 18 | 0.00 | 18 | 186.54  | 23 | 199.23  | 23 | 0.00 | 18 |
| 313 | -42 | -17 | Min. | 0.00   | -27.97  | 24 | 0.00 | 18 | 0.00 | 18 | -84.09  | 30 | 0.00    | 18 | 0.00 | 18 |
| 313 | -42 | -17 | Min. | 150.00 | -111.02 | 24 | 0.00 | 18 | 0.00 | 18 | -250.47 | 30 | -250.92 | 30 | 0.00 | 18 |
| 314 | -18 | -43 | Max  | 0.00   | 111.02  | 31 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 314 | -18 | -43 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 314 | -18 | -43 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 314 | -18 | -43 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 18 | 0.00 | 18 |
| 314 | -44 | -18 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0.00    | 23 | 0.00 | 18 |
| 314 | -44 | -18 | Max  | 150.00 | -99.75  | 30 | 0.00 | 18 | 0.00 | 18 | 186.54  | 23 | 199.23  | 23 | 0.00 | 18 |
| 314 | -44 | -18 | Min. | 0.00   | -27.97  | 24 | 0.00 | 18 | 0.00 | 18 | -84.09  | 30 | 0.00    | 30 | 0.00 | 18 |
| 314 | -44 | -18 | Min. | 150.00 | -111.02 | 24 | 0.00 | 18 | 0.00 | 18 | -250.47 | 30 | -250.92 | 30 | 0.00 | 18 |
| 315 | -19 | -45 | Max  | 0.00   | 111.02  | 31 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 315 | -19 | -45 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 315 | -19 | -45 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 315 | -19 | -45 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 18 | 0.00 | 18 |
| 315 | -58 | -19 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0.00    | 23 | 0.00 | 18 |
| 315 | -58 | -19 | Max  | 150.00 | -99.75  | 30 | 0.00 | 18 | 0.00 | 18 | 186.54  | 23 | 199.23  | 23 | 0.00 | 18 |
| 315 | -58 | -19 | Min. | 0.00   | -27.97  | 24 | 0.00 | 18 | 0.00 | 18 | -84.09  | 30 | 0.00    | 30 | 0.00 | 18 |
| 315 | -58 | -19 | Min. | 150.00 | -111.02 | 24 | 0.00 | 18 | 0.00 | 18 | -250.47 | 30 | -250.92 | 30 | 0.00 | 18 |
| 316 | -20 | -63 | Max  | 0.00   | 73.56   | 31 | 0.00 | 18 | 0.00 | 18 | 137.88  | 30 | 90.13   | 23 | 0.00 | 18 |
| 316 | -20 | -63 | Max  | 150.00 | 13.99   | 31 | 0.00 | 18 | 0.00 | 18 | 42.04   | 30 | 0.00    | 23 | 0.00 | 18 |
| 316 | -20 | -63 | Min. | 0.00   | 67.93   | 23 | 0.00 | 18 | 0.00 | 18 | -80.62  | 23 | -134.94 | 30 | 0.00 | 18 |
| 316 | -20 | -63 | Min. | 150.00 | 11.88   | 23 | 0.00 | 18 | 0.00 | 18 | -39.55  | 23 | 0.00    | 30 | 0.00 | 18 |
| 316 | -65 | -20 | Max  | 0.00   | -11.88  | 30 | 0.00 | 18 | 0.00 | 18 | 39.55   | 23 | 0.00    | 23 | 0.00 | 18 |
| 316 | -65 | -20 | Max  | 150.00 | -67.93  | 30 | 0.00 | 18 | 0.00 | 18 | 80.62   | 23 | 90.13   | 23 | 0.00 | 18 |
| 316 | -65 | -20 | Min. | 0.00   | -13.99  | 24 | 0.00 | 18 | 0.00 | 18 | -42.04  | 30 | 0.00    | 18 | 0.00 | 18 |
| 316 | -65 | -20 | Min. | 150.00 | -73.56  | 24 | 0.00 | 18 | 0.00 | 18 | -137.88 | 30 | -134.94 | 30 | 0.00 | 18 |
| 317 | -21 | -51 | Max  | 0.00   | 73.56   | 31 | 0.00 | 18 | 0.00 | 18 | 137.88  | 30 | 90.13   | 23 | 0.00 | 18 |
| 317 | -21 | -51 | Max  | 150.00 | 13.99   | 31 | 0.00 | 18 | 0.00 | 18 | 42.04   | 30 | 0.00    | 23 | 0.00 | 18 |
| 317 | -21 | -51 | Min. | 0.00   | 67.93   | 23 | 0.00 | 18 | 0.00 | 18 | -80.62  | 23 | -134.94 | 30 | 0.00 | 18 |
| 317 | -21 | -51 | Min. | 150.00 | 11.88   | 23 | 0.00 | 18 | 0.00 | 18 | -39.55  | 23 | 0.00    | 18 | 0.00 | 18 |
| 317 | -50 | -21 | Max  | 0.00   | -11.88  | 30 | 0.00 | 18 | 0.00 | 18 | 39.55   | 23 | 0.00    | 23 | 0.00 | 18 |
| 317 | -50 | -21 | Max  | 150.00 | -67.93  | 30 | 0.00 | 18 | 0.00 | 18 | 80.62   | 23 | 90.13   | 23 | 0.00 | 18 |
| 317 | -50 | -21 | Min. | 0.00   | -13.99  | 24 | 0.00 | 18 | 0.00 | 18 | -42.04  | 30 | 0.00    | 18 | 0.00 | 18 |
| 317 | -50 | -21 | Min. | 150.00 | -73.56  | 24 | 0.00 | 18 | 0.00 | 18 | -137.88 | 30 | -134.94 | 30 | 0.00 | 18 |
| 318 | -22 | -53 | Max  | 0.00   | 111.02  | 18 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 318 | -22 | -53 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 318 | -22 | -53 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 318 | -22 | -53 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 18 | 0.00 | 18 |
| 318 | -52 | -22 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0.00    | 30 | 0.00 | 18 |
| 318 | -52 | -22 | Max  | 150.00 | -99.75  | 30 | 0.00 | 18 | 0.00 | 18 | 186.54  | 23 | 199.23  | 23 | 0.00 | 18 |
| 318 | -52 | -22 | Min. | 0.00   | -27.97  | 24 | 0.00 | 18 | 0.00 | 18 | -84.09  | 30 | 0.00    | 18 | 0.00 | 18 |
| 318 | -52 | -22 | Min. | 150.00 | -111.02 | 24 | 0.00 | 18 | 0.00 | 18 | -250.47 | 30 | -250.92 | 30 | 0.00 | 18 |
| 319 | -23 | -55 | Max  | 0.00   | 111.02  | 18 | 0.00 | 18 | 0.00 | 18 | 250.47  | 30 | 199.23  | 23 | 0.00 | 18 |
| 319 | -23 | -55 | Max  | 150.00 | 27.97   | 31 | 0.00 | 18 | 0.00 | 18 | 84.09   | 30 | 0.00    | 23 | 0.00 | 18 |
| 319 | -23 | -55 | Min. | 0.00   | 99.75   | 23 | 0.00 | 18 | 0.00 | 18 | -186.54 | 23 | -250.92 | 30 | 0.00 | 18 |
| 319 | -23 | -55 | Min. | 150.00 | 23.76   | 23 | 0.00 | 18 | 0.00 | 18 | -79.10  | 23 | 0.00    | 18 | 0.00 | 18 |
| 319 | -54 | -23 | Max  | 0.00   | -23.76  | 30 | 0.00 | 18 | 0.00 | 18 | 79.10   | 23 | 0       |    |      |    |



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|     |     |     |      |        |          |      |         |         |         |        |         |        |          |         |        |      |    |
|-----|-----|-----|------|--------|----------|------|---------|---------|---------|--------|---------|--------|----------|---------|--------|------|----|
| 2   | 2   | -10 | Max  | 330.00 | -1010.51 | 25   | 110.96  | 32      | 245.11  | 32     | 385.77  | 25     | 16.87    | 25      | 0.19   | 32   |    |
| 2   | 2   | -10 | Min. | 0.00   | -1662.17 | 32   | 77.70   | 25      | -121.06 | 32     | -271.77 | 32     | -1256.17 | 25      | -0.26  | 25   |    |
| 2   | 2   | -10 | Min. | 330.00 | -1472.94 | 32   | 77.70   | 25      | 171.59  | 25     | -271.77 | 32     | -11.88   | 32      | -0.26  | 25   |    |
| 3   | 3   | 203 | Max  | 0.00   | -1304.69 | 25   | -47.87  | 25      | 75.69   | 32     | 420.22  | 25     | 963.21   | 32      | 0.16   | 25   |    |
| 3   | 3   | 203 | Max  | 330.00 | -1115.45 | 25   | -47.87  | 25      | -105.80 | 25     | 420.22  | 25     | 19.48    | 25      | 0.16   | 25   |    |
| 3   | 3   | 203 | Min. | 0.00   | -1808.59 | 32   | -69.40  | 32      | 52.19   | 25     | -296.04 | 32     | -1367.24 | 25      | -0.11  | 32   |    |
| 3   | 3   | 203 | Min. | 330.00 | -1619.35 | 32   | -69.40  | 32      | -153.33 | 32     | -296.04 | 32     | -13.72   | 32      | -0.11  | 32   |    |
| 4   | 4   | 204 | Max  | 0.00   | -1186.97 | 25   | 0.00    | 32      | 0.00    | 25     | 242.23  | 32     | 1159.60  | 25      | 0.00   | 25   |    |
| 4   | 4   | 204 | Max  | 330.00 | -997.73  | 25   | 0.00    | 32      | 0.00    | 32     | 242.23  | 32     | 24.94    | 25      | 0.00   | 25   |    |
| 4   | 4   | 204 | Min. | 0.00   | -1590.26 | 32   | 0.00    | 25      | 0.00    | 32     | -343.83 | 25     | -816.93  | 32      | 0.00   | 32   |    |
| 4   | 4   | 204 | Min. | 330.00 | -1401.02 | 32   | 0.00    | 25      | 0.00    | 25     | -343.83 | 25     | -17.57   | 32      | 0.00   | 32   |    |
| 5   | 5   | 205 | Max  | 0.00   | -1304.69 | 25   | -47.87  | 25      | 75.69   | 32     | 296.04  | 32     | 1367.24  | 25      | 0.11   | 32   |    |
| 5   | 5   | 205 | Max  | 330.00 | -1115.45 | 25   | -47.87  | 25      | -105.80 | 25     | 296.04  | 32     | 13.72    | 32      | 0.11   | 32   |    |
| 5   | 5   | 205 | Min. | 0.00   | -1808.59 | 32   | -69.40  | 32      | 52.19   | 25     | -420.22 | 25     | -963.21  | 32      | -0.16  | 25   |    |
| 5   | 5   | 205 | Min. | 330.00 | -1619.35 | 32   | -69.40  | 32      | -153.33 | 32     | -420.22 | 25     | -19.48   | 25      | -0.16  | 25   |    |
| 6   | 6   | -31 | Max  | 0.00   | -1199.75 | 25   | 110.96  | 32      | -84.84  | 25     | 271.77  | 32     | 1256.17  | 25      | 0.26   | 25   |    |
| 6   | 6   | -31 | Min. | 330.00 | -1010.51 | 25   | 110.96  | 32      | 245.12  | 32     | 271.77  | 32     | 11.88    | 32      | 0.26   | 25   |    |
| 6   | 6   | -31 | Min. | 0.00   | -1662.17 | 32   | 77.71   | 25      | -121.06 | 32     | -385.77 | 25     | -884.96  | 32      | -0.19  | 32   |    |
| 6   | 6   | -31 | Min. | 330.00 | -1472.94 | 32   | 77.71   | 25      | 171.59  | 25     | -385.77 | 25     | -16.87   | 25      | -0.19  | 32   |    |
| 7   | 7   | -36 | Max  | 0.00   | -986.59  | 25   | -51.68  | 25      | 71.32   | 32     | 198.80  | 32     | 955.11   | 25      | 0.02   | 25   |    |
| 7   | 7   | -36 | Max  | 330.00 | -797.36  | 25   | -51.68  | 25      | -114.26 | 25     | 198.80  | 32     | 23.87    | 25      | 0.02   | 25   |    |
| 7   | 7   | -36 | Min. | 0.00   | -1322.55 | 32   | -65.40  | 32      | 56.28   | 25     | -282.19 | 25     | -672.87  | 32      | -0.01  | 32   |    |
| 7   | 7   | -36 | Min. | 330.00 | -1133.31 | 32   | -65.40  | 32      | -144.51 | 32     | -282.19 | 25     | -16.82   | 32      | -0.01  | 32   |    |
| 201 | -4  | -3  | Max  | 0.00   | 0.00     | 19   | 29.59   | 32      | 56.09   | 25     | 237.23  | 32     | -206.84  | 25      | 0.00   | 32   |    |
| 201 | -4  | -3  | Max  | 133.53 | 0.00     | 0.00 | 19      | 29.59   | 32      | 0.00   | 32      | 172.83 | 32       | 0.00    | 32     | 0.00 | 32 |
| 201 | -4  | -3  | Min. | 0.00   | 0.00     | 19   | -42.00  | 25      | -39.51  | 32     | 187.10  | 25     | -273.78  | 32      | 0.00   | 25   |    |
| 201 | -4  | -3  | Min. | 133.53 | 0.00     | 0.00 | 19      | -42.00  | 25      | 0.00   | 25      | 122.70 | 25       | 0.00    | 25     | 0.00 | 25 |
| 201 | -5  | -4  | Max  | 0.00   | 0.00     | 19   | 88.77   | 32      | 156.22  | 25     | 533.04  | 32     | -495.69  | 25      | 0.00   | 32   |    |
| 201 | -5  | -4  | Max  | 79.47  | 0.00     | 0.00 | 19      | 88.77   | 32      | 56.09  | 25      | 494.71 | 32       | -206.84 | 25     | 0.00 | 32 |
| 201 | -5  | -4  | Min. | 0.00   | 0.00     | 19   | -126.01 | 25      | -110.06 | 32     | 382.65  | 25     | -682.14  | 32      | 0.00   | 25   |    |
| 201 | -5  | -4  | Min. | 79.47  | 0.00     | 0.00 | 19      | -126.01 | 25      | -39.51 | 32      | 344.32 | 25       | -273.78 | 32     | 0.00 | 25 |
| 201 | -6  | -5  | Max  | 0.00   | 65.40    | 32   | 156.19  | 25      | 71.79   | 25     | -388.63 | 25     | -164.26  | 25      | 23.87  | 25   |    |
| 201 | -6  | -5  | Max  | 54.07  | 65.40    | 32   | 156.19  | 25      | 156.24  | 25     | -414.71 | 25     | -381.43  | 25      | 23.87  | 25   |    |
| 201 | -6  | -5  | Min. | 0.00   | 51.68    | 25   | -110.03 | 32      | -50.58  | 32     | -574.19 | 32     | -220.14  | 32      | -16.82 | 32   |    |
| 201 | -6  | -5  | Min. | 54.07  | 51.68    | 25   | -110.03 | 32      | -110.07 | 32     | -600.27 | 32     | -537.63  | 32      | -16.82 | 32   |    |
| 201 | -7  | -6  | Max  | 0.00   | 65.40    | 32   | 72.18   | 25      | 17.32   | 32     | -167.01 | 25     | 159.78   | 32      | 23.87  | 25   |    |
| 201 | -7  | -6  | Max  | 133.53 | 65.40    | 32   | 72.18   | 25      | 71.79   | 25     | -231.41 | 25     | -164.25  | 25      | 23.87  | 25   |    |
| 201 | -7  | -6  | Min. | 0.00   | 51.68    | 25   | -50.85  | 32      | -24.59  | 25     | -252.31 | 32     | 101.75   | 25      | -16.82 | 32   |    |
| 201 | -7  | -6  | Min. | 133.53 | 51.68    | 25   | -50.85  | 32      | -50.58  | 32     | -316.71 | 32     | -220.13  | 32      | -16.82 | 32   |    |
| 201 | -8  | -7  | Max  | 0.00   | 65.40    | 32   | 8.33    | 32      | 6.20    | 32     | 69.58   | 32     | 109.87   | 32      | 23.87  | 25   |    |
| 201 | -8  | -7  | Max  | 113.24 |          |      |         |         | -22.19  | 25     |         |        | 102.75   | 25      |        |      |    |
| 201 | -8  | -7  | Min. | 133.53 | 65.40    | 32   | 8.33    | 32      | 17.32   | 32     | 5.17    | 32     | 159.78   | 32      | 23.87  | 25   |    |
| 201 | -8  | -7  | Min. | 0.00   | 51.68    | 25   | -11.83  | 25      | -8.79   | 25     | 54.62   | 25     | 71.82    | 25      | -16.82 | 32   |    |
| 201 | -8  | -7  | Min. | 113.24 |          |      |         |         | -22.19  | 25     |         |        | 102.75   | 25      |        |      |    |
| 201 | -8  | -7  | Min. | 133.53 | 51.68    | 25   | -11.83  | 25      | -24.59  | 25     | -9.79   | 25     | 101.75   | 25      | -16.82 | 32   |    |
| 201 | -9  | -8  | Max  | 0.00   | 65.40    | 32   | 67.51   | 32      | 119.18  | 25     | 391.46  | 32     | -254.05  | 25      | 23.87  | 25   |    |
| 201 | -9  | -8  | Max  | 133.53 | 65.40    | 32   | 67.51   | 32      | 6.20    | 32     | 327.06  | 32     | 109.87   | 32      | 23.87  | 25   |    |
| 201 | -9  | -8  | Min. | 0.00   | 51.68    | 25   | -95.83  | 25      | -83.96  | 32     | 276.24  | 25     | -369.86  | 32      | -16.82 | 32   |    |
| 201 | -9  | -8  | Min. | 133.53 | 51.68    | 25   | -95.83  | 25      | -8.80   | 25     | 211.84  | 25     | 71.82    | 25      | -16.82 | 32   |    |
| 201 | -10 | -9  | Max  | 0.00   | 65.40    | 32   | 126.70  | 32      | 200.71  | 25     | 670.81  | 32     | -455.51  | 25      | 23.87  | 25   |    |
| 201 | -10 | -9  | Max  | 45.33  | 65.40    | 32   | 126.70  | 32      | 119.18  | 25     | 648.95  | 32     | -254.05  | 25      | 23.87  | 25   |    |
| 201 | -10 | -9  | Min. | 0.00   | 51.68    | 25   | -179.84 | 25      | -141.40 | 32     | 455.33  | 25     | -669.01  | 32      | -16.81 | 32   |    |
| 201 | -10 | -9  | Min. | 45.33  | 51.68    | 25   | -179.84 | 25      | -83.96  | 32     | 433.46  | 25     | -369.87  | 32      | -16.81 | 32   |    |
| 202 | -11 | -10 | Max  | 0.00   | -26.02   | 25   | 205.93  | 25      | 19.34   | 25     | -512.65 | 25     | -156.19  | 25      | 7.00   | 25   |    |
| 202 | -11 | -10 | Max  | 88.20  | -26.02   | 25   | 205.93  | 25      | 200.97  | 25     | -555.19 | 25     | -627.10  | 25      | 7.00   | 25   |    |
| 202 | -11 | -10 | Min. | 0.00   | -45.56   | 32   | -145.07 | 32      | -13.62  | 32     | -759.59 | 32     | -225.41  | 32      | -4.94  | 32   |    |
| 202 | -11 | -10 | Min. | 88.20  | -45.56   | 32   | -145.07 | 32      | -141.58 | 32     | -802.12 | 32     | -914.13  | 32      | -4.94  | 32   |    |
| 202 | -12 | -11 | Max  | 0.00   | -26.02   | 25   | 121.92  | 25      | 101.07  | 32     | -291.02 | 25     | 402.06   | 32      | 7.00   | 25   |    |
| 202 | -12 | -11 | Max  | 133.53 | -26.02   | 25   | 121.92  | 25      | 19.34   | 25     | -355.43 | 25     | -156.19  | 25      | 7.00   | 25   |    |
| 202 | -12 | -11 | Min. | 0.00   | -45.56   | 32   | -85.89  | 32      | -143.47 | 25     | -437.70 | 32     | 275.43   | 25      | -4.93  | 32   |    |
| 202 | -12 | -11 | Min. | 133.53 | -45.56   | 32   | -85.89  | 32      | -13.62  | 32     | -502.10 | 32     | -225.41  | 32      | -4.93  | 32   |    |
| 202 | -13 | -12 | Max  | 0.00   | -26.02   | 25   | 37.91   | 25      | 136.74  | 32     | -69.40  | 25     | 599.71   | 32      | 7.00   | 25   |    |
| 202 | -13 | -12 | Max  | 133.53 | -26.02   | 25   | 37.91   | 25      | 101.07  | 32     | -133.80 | 25     | 402.06   | 32      | 7.00   | 25   |    |
| 202 | -13 | -12 | Min. | 0.00   | -45.56   | 32   | -26.71  | 32      | -194.10 | 25     | -115.81 | 32     | 411.09   | 25      | -4.93  | 32   |    |
| 202 | -13 | -12 | Min. | 133.53 | -45.56   | 32   | -26.71  | 32      | -143.47 | 25     | -180.22 | 32     | 275.43   | 25      | -4.93  | 32   |    |
| 202 | -14 | -13 | Max  | 0.00   | -26.02   | 25   | 32.47   | 32      | 93.38   | 32     | 206.07  | 32     | 367.54   | 32      | 7.00   | 25   |    |
| 202 | -14 | -13 | Max  | 133.53 | -26.02   | 25   | 32.47   | 32      | 136.74  | 32     | 141.67  | 32     | 599.71   | 32      | 7.00   | 25   |    |
| 202 | -14 | -13 | Min. | 0.00   | -45.56   | 32   | -46.09  | 25      | -132.55 | 25     | 152.23  | 25     | 250.82   | 25      | -4.93  | 32   |    |
| 202 | -14 | -13 | Min. | 133.53 | -45.56   | 32   | -46.09  | 25      | -194.10 | 25     | 87.82   | 25     | 411.10   | 25      | -4.93  | 32   |    |
| 202 | -15 | -14 | Max  | 0.00   | -26.02   | 25   | 91.65   | 32      | 41.18   | 25     | 527.96  | 32     | -205.39  | 25      | 7.00   | 25   |    |
| 202 | -15 | -14 | Max  | 133.53 | -26.02   | 25   | 91.65   | 32      | 93.38   | 32     | 463.56  | 32     | 367.54   | 32      | 7.00   | 25   |    |
| 202 | -15 | -14 | Min. | 0.00   | -45.56   | 32   | -130.10 | 25      | -29.01  | 32     | 373.85  | 25     | -294.46  | 32      | -4.93  | 32   |    |
| 202 | -15 | -14 | Min. | 133.53 | -45.56   | 32   | -130.10 | 25      | -132.55 | 25     | 309.45  | 25     | 250.82   | 25      | -4.93  | 32   |    |
| 202 | 203 | -15 | Max  | 0.00   | -26.02   | 25   | 150.83  | 32      | 228.88  | 25     | 827.72  | 32     | -689.50  | 25      | 7.00   | 25   |    |
| 202 | 203 | -15 | Max  | 87.67  | -26.02   | 25   | 150.83  | 32      | 41.18   | 25     | 785.44  | 32     | -205.40  | 25      | 7.00   | 25   |    |
| 202 | 203 | -15 | Min. | 0.00   | -45.56   | 32   | -214.10 | 25      | -161.24 | 32     | 573.35  | 25     | -1001.57 | 32      | -4.93  | 32   |    |
| 202 | 203 | -15 | Min. | 87.67  | -45.56   | 32   | -214.10 | 25      | -29.01  | 32     | 531.07  | 25     | -294.46  | 32      | -4.93  | 32   |    |
| 203 | -16 | 203 | Max  | 0.00   | 23.84    | 32   | 206.11  | 25      | 134.17  | 25     | -519.97 | 25     | -340.12  | 25      | 8.79   | 32   |    |
| 203 | -16 | 203 | Max  | 45.87  | 23.84    | 32   | 206.11  | 25      | 228.71  | 25     | -542.10 | 25     | -583.69  | 25      | 8.79   | 32   |    |
| 203 | -16 | 203 | Min. | 0.00   | 21.85    | 25   | -145.20 | 32      | -94.52  | 32     | -769.50 | 32     | -490.20  | 32      | -12.47 | 25   |    |
| 203 | -16 | 203 | Min. | 45.87  | 21.85    | 25   | -145.20 | 32      | -161.12 | 32     | -791.62 | 32     | -848.22  | 32      | -12.47 | 25   |    |
| 203 | -17 | -16 | Max  | 0.00   | 23.84    | 32   | 122.11  | 25      | 20.34   | 32     | -298.35 | 25     | 150.51   | 32      | 8.79   | 32   |    |
| 203 | -17 | -16 | Max  | 133.53 | 23.84    | 32   | 122.11  | 25      | 134.18  | 25     | -362.75 | 25     | -340.13  | 25      | 8.79   | 32   |    |
| 203 | -17 | -16 | Min. | 0.00   | 21.85    | 25   | -86.02  | 32      | -28.88  | 25     | -447.62 | 32     | 101.27   | 25      | -12.47 | 25   |    |
| 20  |     |     |      |        |          |      |         |         |         |        |         |        |          |         |        |      |    |



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|-----|-----|-----|------|--------|--------|----|---------|----|---------|----|---------|----|----------|----|--------|----|
| 204 | 204 | -21 | Max  | 0.00   | 23.84  | 32 | 171.92  | 25 | 133.44  | 32 | 700.51  | 32 | -449.00  | 25 | 12.47  | 25 |
| 204 | 204 | -21 | Max  | 20.00  | 23.84  | 32 | 171.92  | 25 | 109.22  | 32 | 690.87  | 32 | -350.19  | 25 | 12.47  | 25 |
| 204 | 204 | -21 | Min. | 0.00   | 21.85  | 25 | -121.11 | 32 | -189.41 | 25 | 498.87  | 25 | -645.42  | 32 | -8.79  | 32 |
| 204 | 204 | -21 | Min. | 20.00  | 21.85  | 25 | -121.11 | 32 | -155.03 | 25 | 489.22  | 25 | -506.28  | 32 | -8.79  | 32 |
| 204 | -21 | -22 | Max  | 0.00   | 23.84  | 32 | 129.91  | 25 | 109.22  | 32 | 518.04  | 32 | -350.19  | 25 | 12.47  | 25 |
| 204 | -21 | -22 | Max  | 133.53 | 23.84  | 32 | 129.91  | 25 | 18.45   | 25 | 453.63  | 32 | 142.47   | 32 | 12.47  | 25 |
| 204 | -21 | -22 | Min. | 0.00   | 21.85  | 25 | -91.52  | 32 | -155.03 | 25 | 366.52  | 25 | -506.28  | 32 | -8.79  | 32 |
| 204 | -21 | -22 | Min. | 133.53 | 21.85  | 25 | -91.52  | 32 | -13.00  | 32 | 302.12  | 25 | 96.24    | 25 | -8.79  | 32 |
| 204 | -22 | -23 | Max  | 0.00   | 23.84  | 32 | 45.91   | 25 | 18.45   | 25 | 196.15  | 32 | 142.46   | 32 | 12.47  | 25 |
| 204 | -22 | -23 | Max  | 133.53 | 23.84  | 32 | 45.91   | 25 | 79.75   | 25 | 131.75  | 32 | 361.39   | 32 | 12.47  | 25 |
| 204 | -22 | -23 | Min. | 0.00   | 21.85  | 25 | -32.34  | 32 | -12.99  | 32 | 144.90  | 25 | 96.23    | 25 | -8.79  | 32 |
| 204 | -22 | -23 | Min. | 133.53 | 21.85  | 25 | -32.34  | 32 | -56.18  | 32 | 80.50   | 25 | 246.72   | 25 | -8.79  | 32 |
| 204 | -23 | -24 | Max  | 0.00   | 23.84  | 32 | 26.84   | 32 | 79.75   | 25 | -76.73  | 25 | 361.40   | 32 | 12.47  | 25 |
| 204 | -23 | -24 | Max  | 133.53 | 23.84  | 32 | 26.84   | 32 | 28.88   | 25 | -141.13 | 25 | 150.50   | 32 | 12.47  | 25 |
| 204 | -23 | -24 | Min. | 0.00   | 21.85  | 25 | -38.10  | 25 | -56.18  | 32 | -125.73 | 32 | 246.72   | 25 | -8.79  | 32 |
| 204 | -23 | -24 | Min. | 133.53 | 21.85  | 25 | -38.10  | 25 | -20.34  | 32 | -190.14 | 32 | 101.26   | 25 | -8.79  | 32 |
| 204 | -24 | -25 | Max  | 0.00   | 23.84  | 32 | 86.02   | 32 | 28.88   | 25 | -298.35 | 25 | 150.50   | 32 | 12.47  | 25 |
| 204 | -24 | -25 | Max  | 133.53 | 23.84  | 32 | 86.02   | 32 | 94.53   | 32 | -362.75 | 25 | -340.13  | 25 | 12.47  | 25 |
| 204 | -24 | -25 | Min. | 0.00   | 21.85  | 25 | -122.11 | 25 | -20.34  | 32 | -447.62 | 32 | 101.27   | 25 | -8.79  | 32 |
| 204 | -24 | -25 | Min. | 133.53 | 21.85  | 25 | -122.11 | 25 | -134.18 | 25 | -512.02 | 32 | -490.22  | 32 | -8.79  | 32 |
| 204 | -25 | 205 | Max  | 0.00   | 23.84  | 32 | 145.20  | 32 | 94.52   | 32 | -519.97 | 25 | -340.12  | 25 | 12.47  | 25 |
| 204 | -25 | 205 | Max  | 45.87  | 23.84  | 32 | 145.20  | 32 | 161.12  | 32 | -542.10 | 25 | -583.69  | 25 | 12.47  | 25 |
| 204 | -25 | 205 | Min. | 0.00   | 21.85  | 25 | -206.11 | 25 | -134.17 | 25 | -769.50 | 32 | -490.20  | 32 | -8.79  | 32 |
| 204 | -25 | 205 | Min. | 45.87  | 21.85  | 25 | -206.11 | 25 | -228.71 | 25 | -791.63 | 32 | -848.22  | 32 | -8.79  | 32 |
| 205 | 205 | -26 | Max  | 0.00   | -26.02 | 25 | 214.10  | 25 | 161.24  | 32 | 827.72  | 32 | -689.50  | 25 | 4.93   | 32 |
| 205 | 205 | -26 | Max  | 87.67  | -26.02 | 25 | 214.10  | 25 | 29.01   | 32 | 785.44  | 32 | -205.40  | 25 | 4.93   | 32 |
| 205 | 205 | -26 | Min. | 0.00   | -45.56 | 32 | -150.83 | 32 | -228.88 | 25 | 573.35  | 25 | -1001.57 | 32 | -7.00  | 25 |
| 205 | 205 | -26 | Min. | 87.67  | -45.56 | 32 | -150.83 | 32 | -41.18  | 25 | 531.07  | 25 | -294.47  | 32 | -7.00  | 25 |
| 205 | -26 | -27 | Max  | 0.00   | -26.02 | 25 | 130.10  | 25 | 29.00   | 32 | 527.96  | 32 | -205.38  | 25 | 4.93   | 32 |
| 205 | -26 | -27 | Max  | 133.53 | -26.02 | 25 | 130.10  | 25 | 132.55  | 25 | 463.55  | 32 | 367.56   | 32 | 4.93   | 32 |
| 205 | -26 | -27 | Min. | 0.00   | -45.56 | 32 | -91.65  | 32 | -41.17  | 25 | 373.85  | 25 | -294.44  | 32 | -7.00  | 25 |
| 205 | -26 | -27 | Min. | 133.53 | -45.56 | 32 | -91.65  | 32 | -93.38  | 32 | 309.45  | 25 | 250.83   | 25 | -7.00  | 25 |
| 205 | -27 | -28 | Max  | 0.00   | -26.02 | 25 | 46.09   | 25 | 132.55  | 25 | 206.07  | 32 | 367.54   | 32 | 4.93   | 32 |
| 205 | -27 | -28 | Max  | 133.53 | -26.02 | 25 | 46.09   | 25 | 194.10  | 25 | 141.67  | 32 | 599.72   | 32 | 4.93   | 32 |
| 205 | -27 | -28 | Min. | 0.00   | -45.56 | 32 | -32.47  | 32 | -93.38  | 32 | 152.23  | 25 | 250.82   | 25 | -7.00  | 25 |
| 205 | -27 | -28 | Min. | 133.53 | -45.56 | 32 | -32.47  | 32 | -136.74 | 32 | 87.82   | 25 | 411.10   | 25 | -7.00  | 25 |
| 205 | -28 | -29 | Max  | 0.00   | -26.02 | 25 | 26.71   | 32 | 194.10  | 25 | -69.40  | 25 | 599.71   | 32 | 4.93   | 32 |
| 205 | -28 | -29 | Max  | 133.53 | -26.02 | 25 | 26.71   | 32 | 143.47  | 25 | -133.80 | 25 | 402.06   | 32 | 4.93   | 32 |
| 205 | -28 | -29 | Min. | 0.00   | -45.56 | 32 | -37.92  | 25 | -136.74 | 32 | -115.81 | 32 | 411.09   | 25 | -7.00  | 25 |
| 205 | -28 | -29 | Min. | 133.53 | -45.56 | 32 | -37.92  | 25 | -101.07 | 32 | -180.22 | 32 | 275.43   | 25 | -7.00  | 25 |
| 205 | -29 | -30 | Max  | 0.00   | -26.02 | 25 | 85.89   | 32 | 143.46  | 25 | -291.02 | 25 | 402.05   | 32 | 4.93   | 32 |
| 205 | -29 | -30 | Max  | 133.53 | -26.02 | 25 | 85.89   | 32 | 13.63   | 32 | -355.43 | 25 | -156.20  | 25 | 4.93   | 32 |
| 205 | -29 | -30 | Min. | 0.00   | -45.56 | 32 | -121.92 | 25 | -101.07 | 32 | -437.70 | 32 | 275.42   | 25 | -7.00  | 25 |
| 205 | -29 | -30 | Min. | 133.53 | -45.56 | 32 | -121.92 | 25 | -19.34  | 25 | -502.11 | 32 | -225.43  | 32 | -7.00  | 25 |
| 205 | -30 | -31 | Max  | 0.00   | -26.02 | 25 | 145.07  | 32 | 13.62   | 32 | -512.65 | 25 | -156.18  | 25 | 4.94   | 32 |
| 205 | -30 | -31 | Max  | 88.20  | -26.02 | 25 | 145.07  | 32 | 141.58  | 32 | -555.19 | 25 | -627.10  | 25 | 4.94   | 32 |
| 205 | -30 | -31 | Min. | 0.00   | -45.56 | 32 | -205.93 | 25 | -19.34  | 25 | -759.59 | 32 | -225.41  | 32 | -7.00  | 25 |
| 205 | -30 | -31 | Min. | 88.20  | -45.56 | 32 | -205.93 | 25 | -200.97 | 25 | -802.12 | 32 | -914.12  | 32 | -7.00  | 25 |
| 206 | -31 | -32 | Max  | 0.00   | 65.40  | 32 | 179.84  | 25 | 141.39  | 32 | 670.81  | 32 | -455.51  | 25 | 16.81  | 32 |
| 206 | -31 | -32 | Max  | 45.33  | 65.40  | 32 | 179.84  | 25 | 83.96   | 32 | 648.95  | 32 | -254.05  | 25 | 16.81  | 32 |
| 206 | -31 | -32 | Min. | 0.00   | 51.68  | 25 | -126.70 | 32 | -200.70 | 25 | 455.33  | 25 | -669.01  | 32 | -23.87 | 25 |
| 206 | -31 | -32 | Min. | 45.33  | 51.68  | 25 | -126.70 | 32 | -119.18 | 25 | 433.46  | 25 | -369.86  | 32 | -23.87 | 25 |
| 206 | -32 | -33 | Max  | 0.00   | 65.40  | 32 | 95.83   | 25 | 83.96   | 32 | 391.46  | 32 | -254.06  | 25 | 16.82  | 32 |
| 206 | -32 | -33 | Max  | 133.53 | 65.40  | 32 | 95.83   | 25 | 8.79    | 25 | 327.06  | 32 | 109.85   | 32 | 16.82  | 32 |
| 206 | -32 | -33 | Min. | 0.00   | 51.68  | 25 | -67.51  | 32 | -119.18 | 25 | 276.24  | 25 | -369.88  | 32 | -23.87 | 25 |
| 206 | -32 | -33 | Min. | 133.53 | 51.68  | 25 | -67.51  | 32 | -6.19   | 32 | 211.84  | 25 | 71.81    | 25 | -23.87 | 25 |
| 206 | -33 | -34 | Max  | 0.00   | 65.40  | 32 | 11.83   | 25 | 8.79    | 25 | 69.58   | 32 | 109.87   | 32 | 16.82  | 32 |
| 206 | -33 | -34 | Max  | 113.24 |        |    |         |    | 22.19   | 25 |         |    | 102.75   | 25 |        |    |
| 206 | -33 | -34 | Max  | 133.53 | 65.40  | 32 | 11.83   | 25 | 24.59   | 25 | 5.17    | 32 | 159.78   | 32 | 16.82  | 32 |
| 206 | -33 | -34 | Min. | 0.00   | 51.68  | 25 | -8.33   | 32 | -6.20   | 32 | 54.61   | 25 | 71.83    | 25 | -23.87 | 25 |
| 206 | -33 | -34 | Min. | 113.24 |        |    |         |    | 22.19   | 25 |         |    | 102.75   | 25 |        |    |
| 206 | -33 | -34 | Min. | 133.53 | 51.68  | 25 | -8.33   | 32 | -17.32  | 32 | -9.79   | 25 | 101.75   | 25 | -23.87 | 25 |
| 206 | -34 | -35 | Max  | 0.00   | 65.40  | 32 | 50.85   | 32 | 24.59   | 25 | -167.01 | 25 | 159.78   | 32 | 16.82  | 32 |
| 206 | -34 | -35 | Max  | 133.53 | 65.40  | 32 | 50.85   | 32 | 50.58   | 32 | -231.41 | 25 | -164.26  | 25 | 16.82  | 32 |
| 206 | -34 | -35 | Min. | 0.00   | 51.68  | 25 | -72.18  | 25 | -17.32  | 32 | -252.31 | 32 | 101.75   | 25 | -23.87 | 25 |
| 206 | -34 | -35 | Min. | 133.53 | 51.68  | 25 | -72.18  | 25 | -71.80  | 25 | -316.71 | 32 | -220.14  | 32 | -23.87 | 25 |
| 206 | -35 | -36 | Max  | 0.00   | 65.40  | 32 | 110.03  | 32 | 50.58   | 32 | -388.63 | 25 | -164.25  | 25 | 16.82  | 32 |
| 206 | -35 | -36 | Max  | 54.07  | 65.40  | 32 | 110.03  | 32 | 110.07  | 32 | -414.71 | 25 | -381.42  | 25 | 16.82  | 32 |
| 206 | -35 | -36 | Min. | 0.00   | 51.68  | 25 | -156.19 | 25 | -71.79  | 25 | -574.19 | 32 | -220.13  | 32 | -23.87 | 25 |
| 206 | -35 | -36 | Min. | 54.07  | 51.68  | 25 | -156.19 | 25 | -156.24 | 25 | -600.27 | 32 | -537.62  | 32 | -23.87 | 25 |
| 206 | -36 | -37 | Max  | 0.00   | 0.00   | 19 | 126.01  | 25 | 110.06  | 32 | 533.04  | 32 | -495.69  | 25 | 0.00   | 25 |
| 206 | -36 | -37 | Max  | 79.47  | 0.00   | 19 | 126.01  | 25 | 39.52   | 32 | 494.71  | 32 | -206.85  | 25 | 0.00   | 25 |
| 206 | -36 | -37 | Min. | 0.00   | 0.00   | 19 | -88.77  | 32 | -156.23 | 25 | 382.65  | 25 | -682.15  | 32 | 0.00   | 32 |
| 206 | -36 | -37 | Min. | 79.47  | 0.00   | 19 | -88.77  | 32 | -56.09  | 25 | 344.32  | 25 | -273.79  | 32 | 0.00   | 32 |
| 206 | -37 | -38 | Max  | 0.00   | 0.00   | 19 | 42.00   | 25 | 39.51   | 32 | 237.23  | 32 | -206.83  | 25 | 0.00   | 25 |
| 206 | -37 | -38 | Max  | 133.53 | 0.00   | 19 | 42.00   | 25 | 0.00    | 25 | 172.82  | 32 | 0.01     | 32 | 0.00   | 25 |
| 206 | -37 | -38 | Min. | 0.00   | 0.00   | 19 | -29.59  | 32 | -56.09  | 25 | 187.10  | 25 | -273.77  | 32 | 0.00   | 32 |
| 206 | -37 | -38 | Min. | 133.53 | 0.00   | 19 | -29.59  | 32 | 0.00    | 32 | 122.69  | 25 | 0.00     | 25 | 0.00   | 32 |
| 301 | -3  | -60 | Max  | 0.00   | 64.55  | 19 | 0.00    | 19 | 0.00    | 19 | 161.68  | 32 | -11.44   | 25 | 0.00   | 19 |
| 301 | -3  | -60 | Max  | 130.25 |        |    |         |    |         |    |         |    | 0.27     | 25 |        |    |
| 301 | -3  | -60 | Max  | 150.00 | 10.62  | 19 | 0.00    | 19 | 0.00    | 19 | 13.59   | 32 | 0.00     | 25 | 0.00   | 19 |
| 301 | -3  | -60 | Min. | 0.00   | 62.30  | 25 | 0.00    | 19 | 0.00    | 19 | 17.98   | 25 | -56.46   | 32 | 0.00   | 19 |
| 301 | -3  | -60 | Min. | 130.25 |        |    |         |    |         |    |         |    | 0.27     | 25 |        |    |
| 301 | -3  | -60 | Min. | 150.00 | 9.78   | 25 | 0.00    | 19 | 0.00    | 19 | -2.73   | 25 | 0.00     | 19 | 0.00   | 19 |
| 301 | -59 | -3  | Max  | 0.00   | -9.78  | 32 | 0.00    | 19 |         |    |         |    |          |    |        |    |

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|     |     |     |      |        |        |    |      |    |      |    |        |    |        |    |      |    |
|-----|-----|-----|------|--------|--------|----|------|----|------|----|--------|----|--------|----|------|----|
| 302 | -46 | -4  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 303 | -6  | -48 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 303 | -6  | -48 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 303 | -6  | -48 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 303 | -6  | -48 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 303 | -6  | -48 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 303 | -6  | -48 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 303 | -49 | -6  | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 303 | -49 | -6  | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 303 | -49 | -6  | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 303 | -49 | -6  | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 19 | 0.00 | 19 |
| 303 | -49 | -6  | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 303 | -49 | -6  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 304 | -7  | -96 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 304 | -7  | -96 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 304 | -7  | -96 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 304 | -7  | -96 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 304 | -7  | -96 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 304 | -7  | -96 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 304 | -95 | -7  | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 304 | -95 | -7  | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 304 | -95 | -7  | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 304 | -95 | -7  | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 19 | 0.00 | 19 |
| 304 | -95 | -7  | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 304 | -95 | -7  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 305 | -8  | -66 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 305 | -8  | -66 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 305 | -8  | -66 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 305 | -8  | -66 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 305 | -8  | -66 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 305 | -8  | -66 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 305 | -67 | -8  | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 305 | -67 | -8  | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 305 | -67 | -8  | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 305 | -67 | -8  | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 32 | 0.00 | 19 |
| 305 | -67 | -8  | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 305 | -67 | -8  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 306 | -9  | -69 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 306 | -9  | -69 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 306 | -9  | -69 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 306 | -9  | -69 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 306 | -9  | -69 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 306 | -9  | -69 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 306 | -68 | -9  | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 32 | 0.00 | 19 |
| 306 | -68 | -9  | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 306 | -68 | -9  | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 306 | -68 | -9  | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 19 | 0.00 | 19 |
| 306 | -68 | -9  | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 306 | -68 | -9  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 307 | -11 | -70 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 307 | -11 | -70 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 307 | -11 | -70 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 307 | -11 | -70 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 307 | -11 | -70 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 307 | -11 | -70 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 307 | -71 | -11 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 32 | 0.00 | 19 |
| 307 | -71 | -11 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 307 | -71 | -11 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 307 | -71 | -11 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 307 | -71 | -11 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 307 | -71 | -11 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 308 | -12 | -72 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 308 | -12 | -72 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 308 | -12 | -72 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 308 | -12 | -72 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 308 | -12 | -72 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 308 | -12 | -72 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 308 | -73 | -12 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 308 | -73 | -12 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 308 | -73 | -12 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 308 | -73 | -12 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 308 | -73 | -12 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 308 | -73 | -12 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 309 | -13 | -74 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 309 | -13 | -74 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 309 | -13 | -74 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 309 | -13 | -74 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 309 | -13 | -74 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 309 | -13 | -74 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 309 | -75 | -13 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 32 | 0.00 | 19 |
| 309 | -75 | -13 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 309 | -75 | -13 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 309 | -75 | -13 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 309 | -75 | -13 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 309 | -75 | -13 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 310 | -14 | -90 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 310 | -14 | -90 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 310 | -14 | -90 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 310 | -14 | -90 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 310 | -14 | -90 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 310 | -14 | -90 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 310 | -91 | -14 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 310 | -91 | -14 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 310 | -91 | -14 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 310 | -91 | -14 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 32 | 0.00 | 19 |
| 310 | -91 | -14 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 310 | -91 | -14 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.0  |    |        |    |        |    |      |    |





|     |     |     |      |        |        |    |      |    |      |    |        |    |        |    |      |    |
|-----|-----|-----|------|--------|--------|----|------|----|------|----|--------|----|--------|----|------|----|
| 319 | -54 | -23 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 19 | 0.00 | 19 |
| 319 | -54 | -23 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 319 | -54 | -23 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 320 | -24 | -57 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 320 | -24 | -57 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 320 | -24 | -57 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 320 | -24 | -57 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 320 | -24 | -57 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 320 | -24 | -57 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 320 | -56 | -24 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 19 | 0.00 | 19 |
| 320 | -56 | -24 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 320 | -56 | -24 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 320 | -56 | -24 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 320 | -56 | -24 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 320 | -56 | -24 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 322 | -25 | -41 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 322 | -25 | -41 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 322 | -25 | -41 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 322 | -25 | -41 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 322 | -25 | -41 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 322 | -25 | -41 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 322 | -64 | -25 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 32 | 0.00 | 19 |
| 322 | -64 | -25 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 322 | -64 | -25 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 322 | -64 | -25 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 322 | -64 | -25 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 322 | -64 | -25 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 323 | -26 | -77 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 323 | -26 | -77 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 323 | -26 | -77 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 323 | -26 | -77 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 323 | -26 | -77 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 323 | -26 | -77 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 323 | -76 | -26 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 323 | -76 | -26 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 323 | -76 | -26 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 323 | -76 | -26 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 25 | -27.18 | 32 | 0.00   | 19 | 0.00 | 19 |
| 323 | -76 | -26 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 323 | -76 | -26 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 25 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 324 | -27 | -79 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 324 | -27 | -79 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 324 | -27 | -79 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 324 | -27 | -79 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 324 | -27 | -79 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 324 | -27 | -79 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 32 | 0.00 | 19 |
| 324 | -78 | -27 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 19 | 0.00 | 19 |
| 324 | -78 | -27 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 324 | -78 | -27 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 324 | -78 | -27 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 324 | -78 | -27 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 324 | -78 | -27 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 325 | -28 | -81 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 325 | -28 | -81 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 325 | -28 | -81 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 325 | -28 | -81 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 325 | -28 | -81 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 325 | -28 | -81 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 325 | -80 | -28 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 32 | 0.00 | 19 |
| 325 | -80 | -28 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 325 | -80 | -28 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 325 | -80 | -28 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 19 | 0.00 | 19 |
| 325 | -80 | -28 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 325 | -80 | -28 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 326 | -29 | -83 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 326 | -29 | -83 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 326 | -29 | -83 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 326 | -29 | -83 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 326 | -29 | -83 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 326 | -29 | -83 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 326 | -82 | -29 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 32 | 0.00 | 19 |
| 326 | -82 | -29 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 326 | -82 | -29 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 326 | -82 | -29 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 326 | -82 | -29 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 326 | -82 | -29 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 327 | -30 | -85 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 327 | -30 | -85 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 327 | -30 | -85 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 327 | -30 | -85 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 327 | -30 | -85 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 327 | -30 | -85 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 19 | 0.00 | 19 |
| 327 | -84 | -30 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 327 | -84 | -30 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 327 | -84 | -30 | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 327 | -84 | -30 | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 32 | 0.00 | 19 |
| 327 | -84 | -30 | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 327 | -84 | -30 | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 329 | -32 | -86 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 329 | -32 | -86 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 329 | -32 | -86 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 329 | -32 | -86 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 329 | -32 | -86 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 329 | -32 | -86 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 32 | 0.00 | 19 |
| 329 | -87 | -32 | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 32 | 0.00 | 19 |
| 329 | -87 | -32 | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 329 | -87 | -32 | Max  | 150.0  |        |    |      |    |      |    |        |    |        |    |      |    |



|     |      |      |      |        |        |    |      |    |      |    |        |    |        |    |      |    |
|-----|------|------|------|--------|--------|----|------|----|------|----|--------|----|--------|----|------|----|
| 330 | -33  | -89  | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 330 | -33  | -89  | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 330 | -33  | -89  | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 330 | -33  | -89  | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 32 | 0.00 | 19 |
| 330 | -88  | -33  | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 330 | -88  | -33  | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 330 | -88  | -33  | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 330 | -88  | -33  | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 19 | 0.00 | 19 |
| 330 | -88  | -33  | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 330 | -88  | -33  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 331 | -34  | -61  | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 331 | -34  | -61  | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 331 | -34  | -61  | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 331 | -34  | -61  | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 331 | -34  | -61  | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 331 | -34  | -61  | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 32 | 0.00 | 19 |
| 331 | -62  | -34  | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 19 | 0.00 | 19 |
| 331 | -62  | -34  | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 331 | -62  | -34  | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 331 | -62  | -34  | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 331 | -62  | -34  | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 331 | -62  | -34  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 332 | -35  | -102 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 332 | -35  | -102 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 332 | -35  | -102 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 332 | -35  | -102 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 332 | -35  | -102 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 332 | -35  | -102 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 32 | 0.00 | 19 |
| 332 | -101 | -35  | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 332 | -101 | -35  | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 332 | -101 | -35  | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 332 | -101 | -35  | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 19 | 0.00 | 19 |
| 332 | -101 | -35  | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 332 | -101 | -35  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 333 | -37  | -103 | Max  | 0.00   | 92.99  | 19 | 0.00 | 19 | 0.00 | 19 | 98.08  | 32 | -3.92  | 25 | 0.00 | 19 |
| 333 | -37  | -103 | Max  | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 333 | -37  | -103 | Max  | 150.00 | 21.24  | 19 | 0.00 | 19 | 0.00 | 19 | 27.18  | 32 | 0.00   | 25 | 0.00 | 19 |
| 333 | -37  | -103 | Min. | 0.00   | 88.49  | 25 | 0.00 | 19 | 0.00 | 19 | 10.68  | 25 | -93.95 | 32 | 0.00 | 19 |
| 333 | -37  | -103 | Min. | 99.30  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 333 | -37  | -103 | Min. | 150.00 | 19.56  | 25 | 0.00 | 19 | 0.00 | 19 | -5.45  | 25 | 0.00   | 32 | 0.00 | 19 |
| 333 | -104 | -37  | Max  | 0.00   | -19.56 | 32 | 0.00 | 19 | 0.00 | 19 | 5.45   | 25 | 0.00   | 25 | 0.00 | 19 |
| 333 | -104 | -37  | Max  | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 333 | -104 | -37  | Max  | 150.00 | -88.49 | 32 | 0.00 | 19 | 0.00 | 19 | -10.68 | 25 | -3.92  | 25 | 0.00 | 19 |
| 333 | -104 | -37  | Min. | 0.00   | -21.24 | 19 | 0.00 | 19 | 0.00 | 19 | -27.18 | 32 | 0.00   | 25 | 0.00 | 19 |
| 333 | -104 | -37  | Min. | 50.70  |        |    |      |    |      |    |        |    | 1.38   | 25 |      |    |
| 333 | -104 | -37  | Min. | 150.00 | -92.99 | 19 | 0.00 | 19 | 0.00 | 19 | -98.08 | 32 | -93.95 | 32 | 0.00 | 19 |
| 334 | -38  | -99  | Max  | 0.00   | 64.55  | 19 | 0.00 | 19 | 0.00 | 19 | 61.68  | 32 | -11.44 | 25 | 0.00 | 19 |
| 334 | -38  | -99  | Max  | 130.25 |        |    |      |    |      |    |        |    | 0.27   | 25 |      |    |
| 334 | -38  | -99  | Max  | 150.00 | 10.62  | 19 | 0.00 | 19 | 0.00 | 19 | 13.59  | 32 | 0.00   | 25 | 0.00 | 19 |
| 334 | -38  | -99  | Min. | 0.00   | 62.30  | 25 | 0.00 | 19 | 0.00 | 19 | 17.98  | 25 | -56.46 | 32 | 0.00 | 19 |
| 334 | -38  | -99  | Min. | 130.25 |        |    |      |    |      |    |        |    | 0.27   | 25 |      |    |
| 334 | -38  | -99  | Min. | 150.00 | 9.78   | 25 | 0.00 | 19 | 0.00 | 19 | -2.73  | 25 | 0.00   | 32 | 0.00 | 19 |
| 334 | -100 | -38  | Max  | 0.00   | -9.78  | 32 | 0.00 | 19 | 0.00 | 19 | 2.73   | 25 | 0.00   | 25 | 0.00 | 19 |
| 334 | -100 | -38  | Max  | 19.75  |        |    |      |    |      |    |        |    | 0.27   | 25 |      |    |
| 334 | -100 | -38  | Max  | 150.00 | -62.30 | 32 | 0.00 | 19 | 0.00 | 19 | -17.98 | 25 | -11.44 | 25 | 0.00 | 19 |
| 334 | -100 | -38  | Min. | 0.00   | -10.62 | 19 | 0.00 | 19 | 0.00 | 19 | -13.59 | 32 | 0.00   | 25 | 0.00 | 19 |
| 334 | -100 | -38  | Min. | 19.75  |        |    |      |    |      |    |        |    | 0.27   | 25 |      |    |
| 334 | -100 | -38  | Min. | 150.00 | -64.55 | 19 | 0.00 | 19 | 0.00 | 19 | -61.68 | 32 | -56.46 | 32 | 0.00 | 19 |

Tipo di combinazione di carico: SLE Q

| Asta | N1 | N2  | X    | N      | CC Ty    | CC Mz  | CC Tz  | CC My  | CC Mx   | CC |        |    |         |    |      |    |
|------|----|-----|------|--------|----------|--------|--------|--------|---------|----|--------|----|---------|----|------|----|
|      |    |     | <cm> | <daN>  | <daN>    | <daNm> | <daN>  | <daNm> | <daNm>  |    |        |    |         |    |      |    |
| 1    | 1  | -5  | Max  | 0.00   | -1183.69 | 20     | -59.73 | 20     | 65.10   | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 1    | 1  | -5  | Max  | 330.00 | -994.46  | 20     | -59.73 | 20     | -132.00 | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 1    | 1  | -5  | Min. | 0.00   | -1183.69 | 20     | -59.73 | 20     | 65.10   | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 1    | 1  | -5  | Min. | 330.00 | -994.46  | 20     | -59.73 | 20     | -132.00 | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 2    | 2  | -10 | Max  | 0.00   | -1471.05 | 20     | 97.22  | 20     | -106.09 | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 2    | 2  | -10 | Max  | 330.00 | -1281.81 | 20     | 97.22  | 20     | 214.72  | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 2    | 2  | -10 | Min. | 0.00   | -1471.05 | 20     | 97.22  | 20     | -106.09 | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 2    | 2  | -10 | Min. | 330.00 | -1281.81 | 20     | 97.22  | 20     | 214.72  | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 3    | 3  | 203 | Max  | 0.00   | -1600.32 | 20     | -60.50 | 20     | 65.98   | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 3    | 3  | 203 | Max  | 330.00 | -1411.08 | 20     | -60.50 | 20     | -133.68 | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 3    | 3  | 203 | Min. | 0.00   | -1600.32 | 20     | -60.50 | 20     | 65.98   | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 3    | 3  | 203 | Min. | 330.00 | -1411.08 | 20     | -60.50 | 20     | -133.68 | 20 | 0.00   | 20 | 0.00    | 20 | 0.00 | 20 |
| 4    | 4  | 204 | Max  | 0.00   | -1423.57 | 20     | 0.00   | 20     | 0.00    | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 4    | 4  | 204 | Max  | 330.00 | -1234.34 | 20     | 0.00   | 20     | 0.00    | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 4    | 4  | 204 | Min. | 0.00   | -1423.57 | 20     | 0.00   | 20     | 0.00    | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 4    | 4  | 204 | Min. | 330.00 | -1234.34 | 20     | 0.00   | 20     | 0.00    | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 5    | 5  | 205 | Max  | 0.00   | -1600.32 | 20     | -60.50 | 20     | 65.98   | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 5    | 5  | 205 | Max  | 330.00 | -1411.08 | 20     | -60.50 | 20     | -133.68 | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 5    | 5  | 205 | Min. | 0.00   | -1600.32 | 20     | -60.50 | 20     | 65.98   | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 5    | 5  | 205 | Min. | 330.00 | -1411.08 | 20     | -60.50 | 20     | -133.68 | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 6    | 6  | -31 | Max  | 0.00   | -1471.05 | 20     | 97.22  | 20     | -106.09 | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 6    | 6  | -31 | Max  | 330.00 | -1281.81 | 20     | 97.22  | 20     | 214.73  | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 6    | 6  | -31 | Min. | 0.00   | -1471.05 | 20     | 97.22  | 20     | -106.09 | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 6    | 6  | -31 | Min. | 330.00 | -1281.81 | 20     | 97.22  | 20     | 214.73  | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 7    | 7  | -36 | Max  | 0.00   | -1183.69 | 20     | -59.73 | 20     | 65.11   | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 7    | 7  | -36 | Max  | 330.00 | -994.46  | 20     | -59.73 | 20     | -132.01 | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 7    | 7  | -36 | Min. | 0.00   | -1183.69 | 20     | -59.73 | 20     | 65.11   | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 7    | 7  | -36 | Min. | 330.00 | -994.46  | 20     | -59.73 | 20     | -132.01 | 20 | 0.00   | 20 | -0.00   | 20 | 0.00 | 20 |
| 201  | -4 | -3  | Max  | 0.00   | 0.00     | 20     | 0.00   | 20     | 0.00    | 20 | 216.51 | 20 | -246.11 | 20 | 0.00 | 20 |
| 201  | -4 | -3  | Max  | 133.53 | 0.00     | 20     | 0.00   | 20     | 0.00    | 20 | 152.11 | 20 | 0.00    | 20 | 0.00 | 20 |
| 201  | -4 | -3  | Min. | 0.00   | 0.00     | 20     | 0.00   | 20     | 0.00    | 20 | 216.51 | 20 | -246.11 | 20 | 0.00 | 20 |
| 201  |    |     |      |        |          |        |        |        |         |    |        |    |         |    |      |    |

Foggia Solar S.r.l.



CODE

FOM.ENG.REL.005.00

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|     |     |     |      |        |        |    |      |    |      |    |         |        |         |    |       |    |
|-----|-----|-----|------|--------|--------|----|------|----|------|----|---------|--------|---------|----|-------|----|
| 201 | -6  | -5  | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -497.50 | 20     | -197.04 | 20 | 0.00  | 20 |
| 201 | -6  | -5  | Min. | 54.07  | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -523.58 | 20     | -473.07 | 20 | 0.00  | 20 |
| 201 | -7  | -6  | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -217.05 | 20     | 135.80  | 20 | 0.00  | 20 |
| 201 | -7  | -6  | Max  | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -281.46 | 20     | -197.04 | 20 | 0.00  | 20 |
| 201 | -7  | -6  | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -217.05 | 20     | 135.80  | 20 | 0.00  | 20 |
| 201 | -7  | -6  | Min. | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -281.46 | 20     | -197.04 | 20 | 0.00  | 20 |
| 201 | -8  | -7  | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 63.39   | 20     | 94.15   | 20 | 0.00  | 20 |
| 201 | -8  | -7  | Max  | 131.44 |        |    |      |    |      |    |         | 135.81 | 20      |    |       |    |
| 201 | -8  | -7  | Max  | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -1.01   | 20     | 135.80  | 20 | 0.00  | 20 |
| 201 | -8  | -7  | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 63.39   | 20     | 94.15   | 20 | 0.00  | 20 |
| 201 | -8  | -7  | Min. | 131.44 |        |    |      |    |      |    |         | 135.81 | 20      |    |       |    |
| 201 | -8  | -7  | Min. | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -1.01   | 20     | 135.80  | 20 | 0.00  | 20 |
| 201 | -9  | -8  | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 343.84  | 20     | -322.00 | 20 | 0.00  | 20 |
| 201 | -9  | -8  | Max  | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 279.44  | 20     | 94.15   | 20 | 0.00  | 20 |
| 201 | -9  | -8  | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 343.84  | 20     | -322.00 | 20 | 0.00  | 20 |
| 201 | -9  | -8  | Min. | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 279.44  | 20     | 94.15   | 20 | 0.00  | 20 |
| 201 | -10 | -9  | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 581.75  | 20     | -580.77 | 20 | 0.00  | 20 |
| 201 | -10 | -9  | Max  | 45.33  | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 559.88  | 20     | -322.00 | 20 | 0.00  | 20 |
| 201 | -10 | -9  | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 581.75  | 20     | -580.77 | 20 | 0.00  | 20 |
| 201 | -10 | -9  | Min. | 45.33  | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 559.88  | 20     | -322.00 | 20 | 0.00  | 20 |
| 202 | -11 | -10 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -657.52 | 20     | -196.80 | 20 | -0.00 | 20 |
| 202 | -11 | -10 | Max  | 88.20  | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -700.06 | 20     | -795.49 | 20 | -0.00 | 20 |
| 202 | -11 | -10 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -657.52 | 20     | -196.80 | 20 | -0.00 | 20 |
| 202 | -11 | -10 | Min. | 88.20  | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -700.06 | 20     | -795.49 | 20 | -0.00 | 20 |
| 202 | -12 | -11 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -377.08 | 20     | 349.72  | 20 | 0.00  | 20 |
| 202 | -12 | -11 | Max  | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -441.48 | 20     | -196.80 | 20 | 0.00  | 20 |
| 202 | -12 | -11 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -377.08 | 20     | 349.72  | 20 | 0.00  | 20 |
| 202 | -12 | -11 | Min. | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -441.48 | 20     | -196.80 | 20 | 0.00  | 20 |
| 202 | -13 | -12 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -96.63  | 20     | 521.75  | 20 | 0.00  | 20 |
| 202 | -13 | -12 | Max  | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -161.03 | 20     | 349.72  | 20 | 0.00  | 20 |
| 202 | -13 | -12 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -96.63  | 20     | 521.75  | 20 | 0.00  | 20 |
| 202 | -13 | -12 | Min. | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -161.03 | 20     | 349.72  | 20 | 0.00  | 20 |
| 202 | -14 | -13 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 183.82  | 20     | 319.30  | 20 | 0.00  | 20 |
| 202 | -14 | -13 | Max  | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 119.41  | 20     | 521.75  | 20 | 0.00  | 20 |
| 202 | -14 | -13 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 183.82  | 20     | 319.30  | 20 | 0.00  | 20 |
| 202 | -14 | -13 | Min. | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 119.41  | 20     | 521.75  | 20 | 0.00  | 20 |
| 202 | -15 | -14 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 464.26  | 20     | -257.65 | 20 | 0.00  | 20 |
| 202 | -15 | -14 | Max  | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 399.86  | 20     | 319.30  | 20 | 0.00  | 20 |
| 202 | -15 | -14 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 464.26  | 20     | -257.65 | 20 | 0.00  | 20 |
| 202 | -15 | -14 | Min. | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 399.86  | 20     | 319.30  | 20 | 0.00  | 20 |
| 202 | 203 | -15 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 722.59  | 20     | -872.59 | 20 | 0.00  | 20 |
| 202 | 203 | -15 | Max  | 87.67  | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 680.31  | 20     | -257.65 | 20 | 0.00  | 20 |
| 202 | 203 | -15 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 722.59  | 20     | -872.59 | 20 | 0.00  | 20 |
| 202 | 203 | -15 | Min. | 87.67  | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 680.31  | 20     | -257.65 | 20 | 0.00  | 20 |
| 203 | -16 | 203 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -666.37 | 20     | -428.17 | 20 | 0.00  | 20 |
| 203 | -16 | 203 | Max  | 45.87  | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -688.49 | 20     | -738.88 | 20 | 0.00  | 20 |
| 203 | -16 | 203 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -666.37 | 20     | -428.17 | 20 | 0.00  | 20 |
| 203 | -16 | 203 | Min. | 45.87  | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -688.49 | 20     | -738.88 | 20 | 0.00  | 20 |
| 203 | -17 | -16 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -385.92 | 20     | 130.16  | 20 | 0.00  | 20 |
| 203 | -17 | -16 | Max  | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -450.33 | 20     | -428.18 | 20 | 0.00  | 20 |
| 203 | -17 | -16 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -385.92 | 20     | 130.16  | 20 | 0.00  | 20 |
| 203 | -17 | -16 | Min. | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -450.33 | 20     | -428.18 | 20 | 0.00  | 20 |
| 203 | -18 | -17 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -105.48 | 20     | 314.00  | 20 | 0.00  | 20 |
| 203 | -18 | -17 | Max  | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -169.88 | 20     | 130.15  | 20 | 0.00  | 20 |
| 203 | -18 | -17 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -105.48 | 20     | 314.00  | 20 | 0.00  | 20 |
| 203 | -18 | -17 | Min. | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -169.88 | 20     | 130.15  | 20 | 0.00  | 20 |
| 203 | -19 | -18 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 174.97  | 20     | 123.35  | 20 | 0.00  | 20 |
| 203 | -19 | -18 | Max  | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 110.57  | 20     | 313.99  | 20 | 0.00  | 20 |
| 203 | -19 | -18 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 174.97  | 20     | 123.35  | 20 | 0.00  | 20 |
| 203 | -19 | -18 | Min. | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 110.57  | 20     | 313.99  | 20 | 0.00  | 20 |
| 203 | -20 | -19 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 455.42  | 20     | -441.77 | 20 | 0.00  | 20 |
| 203 | -20 | -19 | Max  | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 391.01  | 20     | 123.36  | 20 | 0.00  | 20 |
| 203 | -20 | -19 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 455.42  | 20     | -441.77 | 20 | 0.00  | 20 |
| 203 | -20 | -19 | Min. | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 391.01  | 20     | 123.36  | 20 | 0.00  | 20 |
| 203 | 204 | -20 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 617.17  | 20     | -564.24 | 20 | 0.00  | 20 |
| 203 | 204 | -20 | Max  | 20.00  | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 607.52  | 20     | -441.77 | 20 | 0.00  | 20 |
| 203 | 204 | -20 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 617.17  | 20     | -564.24 | 20 | 0.00  | 20 |
| 203 | 204 | -20 | Min. | 20.00  | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 607.52  | 20     | -441.77 | 20 | 0.00  | 20 |
| 204 | 204 | -21 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 617.17  | 20     | -564.24 | 20 | 0.00  | 20 |
| 204 | 204 | -21 | Max  | 20.00  | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 607.52  | 20     | -441.77 | 20 | 0.00  | 20 |
| 204 | 204 | -21 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 617.17  | 20     | -564.24 | 20 | 0.00  | 20 |
| 204 | 204 | -21 | Min. | 20.00  | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 607.52  | 20     | -441.77 | 20 | 0.00  | 20 |
| 204 | -21 | -22 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 455.42  | 20     | -441.77 | 20 | 0.00  | 20 |
| 204 | -21 | -22 | Max  | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 391.01  | 20     | 123.36  | 20 | 0.00  | 20 |
| 204 | -21 | -22 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 455.42  | 20     | -441.77 | 20 | 0.00  | 20 |
| 204 | -21 | -22 | Min. | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 391.01  | 20     | 123.36  | 20 | 0.00  | 20 |
| 204 | -22 | -23 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 174.97  | 20     | 123.35  | 20 | 0.00  | 20 |
| 204 | -22 | -23 | Max  | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 110.57  | 20     | 313.99  | 20 | 0.00  | 20 |
| 204 | -22 | -23 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 174.97  | 20     | 123.35  | 20 | 0.00  | 20 |
| 204 | -22 | -23 | Min. | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | 110.57  | 20     | 313.99  | 20 | 0.00  | 20 |
| 204 | -23 | -24 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -105.48 | 20     | 314.00  | 20 | 0.00  | 20 |
| 204 | -23 | -24 | Max  | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -169.88 | 20     | 130.15  | 20 | 0.00  | 20 |
| 204 | -23 | -24 | Min. | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -105.48 | 20     | 314.00  | 20 | 0.00  | 20 |
| 204 | -23 | -24 | Min. | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -169.88 | 20     | 130.15  | 20 | 0.00  | 20 |
| 204 | -24 | -25 | Max  | 0.00   | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -385.93 | 20     | 130.15  | 20 | 0.00  | 20 |
| 204 | -24 | -25 | Max  | 133.53 | 23.02  | 20 | 0.00 | 20 | 0.00 | 20 | -450.33 |        |         |    |       |    |



|     |     |     |      |        |        |    |      |    |      |    |         |    |         |    |      |    |
|-----|-----|-----|------|--------|--------|----|------|----|------|----|---------|----|---------|----|------|----|
| 205 | -27 | -28 | Max  | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 119.41  | 20 | 521.76  | 20 | 0.00 | 20 |
| 205 | -27 | -28 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 183.82  | 20 | 319.30  | 20 | 0.00 | 20 |
| 205 | -27 | -28 | Max  | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | 119.41  | 20 | 521.76  | 20 | 0.00 | 20 |
| 205 | -28 | -29 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -96.63  | 20 | 521.75  | 20 | 0.00 | 20 |
| 205 | -28 | -29 | Max  | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -161.03 | 20 | 349.72  | 20 | 0.00 | 20 |
| 205 | -28 | -29 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -96.63  | 20 | 521.75  | 20 | 0.00 | 20 |
| 205 | -28 | -29 | Min. | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -161.03 | 20 | 349.72  | 20 | 0.00 | 20 |
| 205 | -29 | -30 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -377.08 | 20 | 349.71  | 20 | 0.00 | 20 |
| 205 | -29 | -30 | Max  | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -441.48 | 20 | -196.81 | 20 | 0.00 | 20 |
| 205 | -29 | -30 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -377.08 | 20 | 349.71  | 20 | 0.00 | 20 |
| 205 | -29 | -30 | Min. | 133.53 | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -441.48 | 20 | -196.81 | 20 | 0.00 | 20 |
| 205 | -30 | -31 | Max  | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -657.52 | 20 | -196.80 | 20 | 0.00 | 20 |
| 205 | -30 | -31 | Max  | 88.20  | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -700.06 | 20 | -795.49 | 20 | 0.00 | 20 |
| 205 | -30 | -31 | Min. | 0.00   | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -657.52 | 20 | -196.80 | 20 | 0.00 | 20 |
| 205 | -30 | -31 | Min. | 88.20  | -37.49 | 20 | 0.00 | 20 | 0.00 | 20 | -700.06 | 20 | -795.49 | 20 | 0.00 | 20 |
| 206 | -31 | -32 | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 581.75  | 20 | -580.76 | 20 | 0.00 | 20 |
| 206 | -31 | -32 | Max  | 45.33  | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 559.88  | 20 | -322.00 | 20 | 0.00 | 20 |
| 206 | -31 | -32 | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 581.75  | 20 | -580.76 | 20 | 0.00 | 20 |
| 206 | -31 | -32 | Min. | 45.33  | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 559.88  | 20 | -322.00 | 20 | 0.00 | 20 |
| 206 | -32 | -33 | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 343.84  | 20 | -322.01 | 20 | 0.00 | 20 |
| 206 | -32 | -33 | Max  | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 279.44  | 20 | 94.13   | 20 | 0.00 | 20 |
| 206 | -32 | -33 | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 343.84  | 20 | -322.01 | 20 | 0.00 | 20 |
| 206 | -32 | -33 | Min. | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 279.44  | 20 | 94.13   | 20 | 0.00 | 20 |
| 206 | -33 | -34 | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 63.39   | 20 | 94.15   | 20 | 0.00 | 20 |
| 206 | -33 | -34 | Max  | 131.44 |        |    |      |    |      |    |         |    | 135.81  | 20 |      |    |
| 206 | -33 | -34 | Min. | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -1.01   | 20 | 135.80  | 20 | 0.00 | 20 |
| 206 | -33 | -34 | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | 63.39   | 20 | 94.15   | 20 | 0.00 | 20 |
| 206 | -33 | -34 | Min. | 131.44 |        |    |      |    |      |    |         |    | 135.81  | 20 |      |    |
| 206 | -33 | -34 | Min. | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -1.01   | 20 | 135.80  | 20 | 0.00 | 20 |
| 206 | -34 | -35 | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -217.05 | 20 | 135.80  | 20 | 0.00 | 20 |
| 206 | -34 | -35 | Max  | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -281.46 | 20 | -197.04 | 20 | 0.00 | 20 |
| 206 | -34 | -35 | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -217.05 | 20 | 135.80  | 20 | 0.00 | 20 |
| 206 | -34 | -35 | Min. | 133.53 | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -281.46 | 20 | -197.04 | 20 | 0.00 | 20 |
| 206 | -35 | -36 | Max  | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -497.50 | 20 | -197.03 | 20 | 0.00 | 20 |
| 206 | -35 | -36 | Max  | 54.07  | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -523.58 | 20 | -473.06 | 20 | 0.00 | 20 |
| 206 | -35 | -36 | Min. | 0.00   | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -497.50 | 20 | -197.03 | 20 | 0.00 | 20 |
| 206 | -35 | -36 | Min. | 54.07  | 59.73  | 20 | 0.00 | 20 | 0.00 | 20 | -523.58 | 20 | -473.06 | 20 | 0.00 | 20 |
| 206 | -36 | -37 | Max  | 0.00   | 0.00   | 20 | 0.00 | 20 | 0.00 | 20 | 470.88  | 20 | -605.09 | 20 | 0.00 | 20 |
| 206 | -36 | -37 | Max  | 79.47  | 0.00   | 20 | 0.00 | 20 | 0.00 | 20 | 432.55  | 20 | -246.12 | 20 | 0.00 | 20 |
| 206 | -36 | -37 | Min. | 0.00   | 0.00   | 20 | 0.00 | 20 | 0.00 | 20 | 470.88  | 20 | -605.09 | 20 | 0.00 | 20 |
| 206 | -36 | -37 | Min. | 79.47  | 0.00   | 20 | 0.00 | 20 | 0.00 | 20 | 432.55  | 20 | -246.12 | 20 | 0.00 | 20 |
| 206 | -37 | -38 | Max  | 0.00   | 0.00   | 20 | 0.00 | 20 | 0.00 | 20 | 216.51  | 20 | -246.11 | 20 | 0.00 | 20 |
| 206 | -37 | -38 | Max  | 133.53 | 0.00   | 20 | 0.00 | 20 | 0.00 | 20 | 152.11  | 20 | 0.00    | 20 | 0.00 | 20 |
| 206 | -37 | -38 | Min. | 0.00   | 0.00   | 20 | 0.00 | 20 | 0.00 | 20 | 216.51  | 20 | -246.11 | 20 | 0.00 | 20 |
| 206 | -37 | -38 | Min. | 133.53 | 0.00   | 20 | 0.00 | 20 | 0.00 | 20 | 152.11  | 20 | 0.00    | 20 | 0.00 | 20 |
| 301 | -3  | -60 | Max  | 0.00   | 62.30  | 20 | 0.00 | 20 | 0.00 | 20 | 43.62   | 20 | -37.85  | 20 | 0.00 | 20 |
| 301 | -3  | -60 | Max  | 150.00 | 9.78   | 20 | 0.00 | 20 | 0.00 | 20 | 6.85    | 20 | 0.00    | 20 | 0.00 | 20 |
| 301 | -3  | -60 | Min. | 0.00   | 62.30  | 20 | 0.00 | 20 | 0.00 | 20 | 43.62   | 20 | -37.85  | 20 | 0.00 | 20 |
| 301 | -3  | -60 | Min. | 150.00 | 9.78   | 20 | 0.00 | 20 | 0.00 | 20 | 6.85    | 20 | 0.00    | 20 | 0.00 | 20 |
| 301 | -59 | -3  | Max  | 0.00   | -9.78  | 20 | 0.00 | 20 | 0.00 | 20 | -6.85   | 20 | 0.00    | 20 | 0.00 | 20 |
| 301 | -59 | -3  | Max  | 150.00 | -62.30 | 20 | 0.00 | 20 | 0.00 | 20 | -43.62  | 20 | -37.85  | 20 | 0.00 | 20 |
| 301 | -59 | -3  | Min. | 0.00   | -9.78  | 20 | 0.00 | 20 | 0.00 | 20 | -6.85   | 20 | 0.00    | 20 | 0.00 | 20 |
| 301 | -59 | -3  | Min. | 150.00 | -62.30 | 20 | 0.00 | 20 | 0.00 | 20 | -43.62  | 20 | -37.85  | 20 | 0.00 | 20 |
| 302 | -4  | -47 | Max  | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.74  | 20 | 0.00 | 20 |
| 302 | -4  | -47 | Max  | 150.00 | 19.56  | 20 | 0.00 | 20 | 0.00 | 20 | 13.69   | 20 | 0.00    | 20 | 0.00 | 20 |
| 302 | -4  | -47 | Min. | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.74  | 20 | 0.00 | 20 |
| 302 | -4  | -47 | Min. | 150.00 | 19.56  | 20 | 0.00 | 20 | 0.00 | 20 | 13.69   | 20 | 0.00    | 20 | 0.00 | 20 |
| 302 | -46 | -4  | Max  | 0.00   | -19.56 | 20 | 0.00 | 20 | 0.00 | 20 | -13.69  | 20 | 0.00    | 20 | 0.00 | 20 |
| 302 | -46 | -4  | Max  | 150.00 | -88.49 | 20 | 0.00 | 20 | 0.00 | 20 | -61.96  | 20 | -56.74  | 20 | 0.00 | 20 |
| 302 | -46 | -4  | Min. | 0.00   | -19.56 | 20 | 0.00 | 20 | 0.00 | 20 | -13.69  | 20 | 0.00    | 20 | 0.00 | 20 |
| 302 | -46 | -4  | Min. | 150.00 | -88.49 | 20 | 0.00 | 20 | 0.00 | 20 | -61.96  | 20 | -56.74  | 20 | 0.00 | 20 |
| 303 | -6  | -48 | Max  | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.74  | 20 | 0.00 | 20 |
| 303 | -6  | -48 | Max  | 150.00 | 19.56  | 20 | 0.00 | 20 | 0.00 | 20 | 13.69   | 20 | 0.00    | 20 | 0.00 | 20 |
| 303 | -6  | -48 | Min. | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.74  | 20 | 0.00 | 20 |
| 303 | -6  | -48 | Min. | 150.00 | 19.56  | 20 | 0.00 | 20 | 0.00 | 20 | 13.69   | 20 | 0.00    | 20 | 0.00 | 20 |
| 303 | -49 | -6  | Max  | 0.00   | -19.56 | 20 | 0.00 | 20 | 0.00 | 20 | -13.69  | 20 | 0.00    | 20 | 0.00 | 20 |
| 303 | -49 | -6  | Max  | 150.00 | -88.49 | 20 | 0.00 | 20 | 0.00 | 20 | -61.96  | 20 | -56.74  | 20 | 0.00 | 20 |
| 303 | -49 | -6  | Min. | 0.00   | -19.56 | 20 | 0.00 | 20 | 0.00 | 20 | -13.69  | 20 | 0.00    | 20 | 0.00 | 20 |
| 303 | -49 | -6  | Min. | 150.00 | -88.49 | 20 | 0.00 | 20 | 0.00 | 20 | -61.96  | 20 | -56.74  | 20 | 0.00 | 20 |
| 304 | -7  | -96 | Max  | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.74  | 20 | 0.00 | 20 |
| 304 | -7  | -96 | Max  | 150.00 | 19.56  | 20 | 0.00 | 20 | 0.00 | 20 | 13.69   | 20 | 0.00    | 20 | 0.00 | 20 |
| 304 | -7  | -96 | Min. | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.74  | 20 | 0.00 | 20 |
| 304 | -7  | -96 | Min. | 150.00 | 19.56  | 20 | 0.00 | 20 | 0.00 | 20 | 13.69   | 20 | 0.00    | 20 | 0.00 | 20 |
| 304 | -95 | -7  | Max  | 0.00   | -19.56 | 20 | 0.00 | 20 | 0.00 | 20 | -13.69  | 20 | 0.00    | 20 | 0.00 | 20 |
| 304 | -95 | -7  | Max  | 150.00 | -88.49 | 20 | 0.00 | 20 | 0.00 | 20 | -61.96  | 20 | -56.74  | 20 | 0.00 | 20 |
| 304 | -95 | -7  | Min. | 0.00   | -19.56 | 20 | 0.00 | 20 | 0.00 | 20 | -13.69  | 20 | 0.00    | 20 | 0.00 | 20 |
| 304 | -95 | -7  | Min. | 150.00 | -88.49 | 20 | 0.00 | 20 | 0.00 | 20 | -61.96  | 20 | -56.74  | 20 | 0.00 | 20 |
| 305 | -8  | -66 | Max  | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.74  | 20 | 0.00 | 20 |
| 305 | -8  | -66 | Max  | 150.00 | 19.56  | 20 | 0.00 | 20 | 0.00 | 20 | 13.69   | 20 | 0.00    | 20 | 0.00 | 20 |
| 305 | -8  | -66 | Min. | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.74  | 20 | 0.00 | 20 |
| 305 | -8  | -66 | Min. | 150.00 | 19.56  | 20 | 0.00 | 20 | 0.00 | 20 | 13.69   | 20 | 0.00    | 20 | 0.00 | 20 |
| 305 | -67 | -8  | Max  | 0.00   | -19.56 | 20 | 0.00 | 20 | 0.00 | 20 | -13.69  | 20 | 0.00    | 20 | 0.00 | 20 |
| 305 | -67 | -8  | Max  | 150.00 | -88.49 | 20 | 0.00 | 20 | 0.00 | 20 | -61.96  | 20 | -56.74  | 20 | 0.00 | 20 |
| 305 | -67 | -8  | Min. | 0.00   | -19.56 | 20 | 0.00 | 20 | 0.00 | 20 | -13.69  | 20 | 0.00    | 20 | 0.00 | 20 |
| 305 | -67 | -8  | Min. | 150.00 | -88.49 | 20 | 0.00 | 20 | 0.00 | 20 | -61.96  | 20 | -56.74  | 20 | 0.00 | 20 |
| 306 | -9  | -69 | Max  | 0.00   | 88.49  | 20 | 0.00 | 20 | 0.00 | 20 | 61.96   | 20 | -56.7   |    |      |    |









Simbologia

$\Phi_{LT}$  = Coefficiente  $\Phi$  per stabilità laterale membrature inflesse  
 $\Phi_y$  = Coefficiente  $\Phi$  per inflessione intorno all'asse y(c)  
 $\Phi_z$  = Coefficiente  $\Phi$  per inflessione intorno all'asse z(e)  
 $\alpha_{imp}$  = Coefficiente di imperfezione  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}$  = Coefficienti correttivi per il momento flettente  
 $\beta_{LT}$  = Coefficiente per calcolo  $\Phi_{LT}$   
 $\chi_{LT}$  = Coefficiente di riduzione per stabilità laterale membrature inflesse  
 $\chi_y$  = Coefficiente  $\chi$  di riduzione per instabilità intorno all'asse y(c)  
 $\chi_z$  = Coefficiente  $\chi$  di riduzione per instabilità intorno all'asse z(e)  
 $\delta$  <cm> = Spostamento relativo asta  
 $\lambda_y$  = Snellezza adimensionale per inflessione intorno all'asse y(c)  
 $\lambda_z$  = Snellezza adimensionale per inflessione intorno all'asse z(e)  
 $\lambda_{LT}$  = Coefficiente di imperfezione per stabilità laterale membrature inflesse  
 $\lambda_{LT,0}$  = Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse  
 $\lambda_y$  = Snellezza per inflessione intorno all'asse y(c)  
 $\lambda_z$  = Snellezza per inflessione intorno all'asse z(e)  
 $\sigma_{ID,max}$  <daN/cm²> = Tensione ideale massima  
 $\sigma_M$  <daN/cm²> = Tensione normale per momento flettente  
 $\sigma_N$  <daN/cm²> = Tensione normale per sforzo normale  
 $\tau$  <daN/cm²> = Tensione tangenziale per taglio e/o torsione  
 $\psi$  = Coeff. di correzione momento critico per stabilità laterale membrature inflesse  
 $A_{eff}$  <cm²> = Area effettiva per trazione  
 $A_{net}$  <cm²> = Area netta per compressione  
 $A_{area}$  <cm²> = Area  
 $A_{tag,y}$  <cm²> = Area resistente a taglio in dir. Y  
 $A_{tag,z}$  <cm²> = Area resistente a taglio in dir. Z  
 $CC$  = Numero della combinazione delle condizioni di carico elementari  
 $Cod.$  = Codice  
 $Curva$  = Curva di instabilità adottata  
 $D$  <cm> = Distanza  
 $F_{yk}$  <daN/cm²> = Tensione caratteristica di snervamento dell'acciaio  
 $F_{yt}$  <daN/cm²> = Tensione caratteristica di rottura  
 $I_y$  <cm⁴> = Raggio giratorio d'inerzia rispetto all'asse Y  
 $I_z$  <cm⁴> = Raggio giratorio d'inerzia rispetto all'asse Z  
 $J_{\omega}$  <cm⁶> = Costante di ingobbamento  
 $J_y$  <cm⁴> = Momento d'inerzia rispetto all'asse Y  
 $J_z$  <cm⁴> = Momento d'inerzia rispetto all'asse Z  
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}$  = Coefficienti di interazione  
 $L$  <cm> = Lunghezza dell'asta  
 $L_{cr}$  <cm> = Lunghezza di libera inflessione laterale fra ritegni torsionali  
 $M_{cr}$  <daNm> = Momento critico per instabilità flessione torsionale  
 $M_{Ny,c,Rd}$  <daNm> = Resistenza di calcolo a pressoflessione intorno all'asse Y  
 $M_x$  <daNm> = Momento torcente intorno all'asse X  
 $M_y$  <daNm> = Momento flettente intorno all'asse Y  
 $M_y,Ed$  <daNm> = Momento flettente di calcolo intorno all'asse Y  
 $M_y,V,c,Rd$  <daNm> = Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y  
 $M_z$  <daNm> = Momento flettente intorno all'asse Z  
 $M_z,Ed$  <daNm> = Momento flettente di calcolo intorno all'asse Z  
 $N$  <daN> = Sforzo normale  
 $N,Ed$  <daN> = Forza assiale di calcolo  
 $N_c,Rd$  <daN> = Resistenza a compressione  
 $N_{cr,y}$  <daN> = Sforzo normale critico euleriano per inflessione intorno all'asse y(c)  
 $N_{cr,z}$  <daN> = Sforzo normale critico euleriano per inflessione intorno all'asse z(e)  
 $Sez.$  = Numero della sezione  
 $Tipo$  = Tipologia  
 $R_c$  = Rettangolare cava  
 $I_s$  = I stondata  
 $T_p$  = Tipo di acciaio  
 $T_y$  <daN> = Taglio in dir. Y  
 $T_z$  <daN> = Taglio in dir. Z  
 $V,Ed$  <daN> = Forza di taglio di calcolo  
 $V_c,Rd$  <daN> = Resistenza a taglio  
 $V_c,Rd,Red$  <daN> = Resistenza a taglio ridotta  
 $W_y,plac$  <cm²> = Modulo di resistenza plastico intorno all'asse Y  
 $W_{ymin}$  <cm²> = Modulo di resistenza minimo rispetto all'asse Y  
 $W_z,plac$  <cm²> = Modulo di resistenza plastico intorno all'asse Z  
 $W_{zmin}$  <cm²> = Modulo di resistenza minimo rispetto all'asse Z  
 $X_1$  <cm> = Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica  
 $f$  = Fattore di modifica per il coefficiente di riduzione  
 $f_{z,g}$  <cm> = Freccia in direzione Z globale  
 $f_{z,l}$  <cm> = Freccia in direzione Z locale  
 $k_c$  = Coeff. di correzione momento flettente per stabilità laterale membrature inflesse

Caratteristiche profilati utilizzati

| Sez. Cod. | Tipo                   | D  | Area  | Anet  | Aeff  | Jy    | Jz      | Iy      | Iz    | Wymin | Wzmin  | Tp     | Fyk                  | Fyt       |         |
|-----------|------------------------|----|-------|-------|-------|-------|---------|---------|-------|-------|--------|--------|----------------------|-----------|---------|
|           |                        |    | <cm²> | <cm²> | <cm²> | <cm⁴> | <cm⁴>   | <cm⁴>   | <cm⁴> | <cm²> | <cm²>  |        | <daN/cm²>            | <daN/cm²> |         |
| 1         | COLL HEA240            | Is | --    | 76.84 | 76.84 | 76.84 | 7763.40 | 2768.81 | 10.05 | 6.00  | 675.08 | 230.73 | S355 UNI EN 10025-2  | 3550.00   | 5100.00 |
| 2         | TRV PRINC SHS200x200x8 | Rc | --    | 61.44 | 61.44 | 61.44 | 3781.43 | 3781.43 | 7.85  | 7.85  | 378.14 | 378.14 | S355H UNI EN 10210-1 | 3550.00   | 5100.00 |
| 3         | TRV SEC RSH150x100x8   | Rc | --    | 37.44 | 37.44 | 37.44 | 1128.23 | 598.15  | 5.49  | 3.96  | 150.43 | 117.63 | S355H UNI EN 10210-1 | 3550.00   | 5100.00 |

Caratteristiche profilati utilizzati

| Sez. Cod. | Wy,plac                | Wz,plac | Atag,y | Atag,z | J $\omega$ |           |
|-----------|------------------------|---------|--------|--------|------------|-----------|
|           | <cm²>                  | <cm²>   | <cm²>  | <cm²>  | <cm⁶>      |           |
| 1         | COLL HEA240            | 747.99  | 352.10 | 64.54  | 25.18      | 328486.00 |
| 2         | TRV PRINC SHS200x200x8 | 442.62  | 442.62 | 30.72  | 30.72      |           |
| 3         | TRV SEC RSH150x100x8   | 185.42  | 138.62 | 14.98  | 22.46      |           |

Asta n. 1 (1 -5) - Sez. 1 (COLL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3  
 Sollecitazioni: N=-852.25 T<sub>y</sub>=-193.71 M<sub>y</sub>=-676.98 T<sub>y</sub>=-651.83 M<sub>z</sub>=1228.40  
 Tensioni:  $\sigma_N$ =-11.09  $\sigma_{m,d}$ =-632.67  $\tau$ =0.00  $\sigma_{D,max}$ =-643.76 (sfrut=0.19)  
 Tensioni:  $\sigma_N$ =-11.09  $\sigma_{m,d}$ =199.62  $\tau$ =16.31  $\tau_{max}$ =16.31 (sfrut=0.01)  
 Tensioni:  $\sigma_N$ =-11.09  $\sigma_{m,d}$ =-632.67  $\tau$ =0.00  $\sigma_{D,max}$ =643.76 (sfrut=0.19)

- Verifica a taglio Dir. Y [4.2.16] - CC 15 SND X1=2.40 - Classe 2  
 Sollecitazioni: T<sub>y</sub>=117.90  
 V,Ed=117.90 V<sub>c,Rd</sub>=125981.00 V,Ed/V<sub>c,Rd</sub>=0.00

- Verifica a taglio Dir. Z [4.2.16] - CC 15 SND Xl=2.40 - Classe 2  
Sollecitazioni:  $T_z=573.40$   
 $V,Ed=573.40$   $V_c,Rd=49148.50$   $V,Ed/V_c,Rd=0.01$
- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3  
Sollecitazioni:  $N=-284.49$   $T_x=2116.46$   $M_y=7163.35$   $T_y=-26.42$   $M_z=28.49$   
Tensioni:  $\sigma_N=-3.70$   $\sigma_{m,d}=-1073.46$   $\tau=0.00$   $\sigma_{max}=-1077.17$  (sfrut=0.32)  
Tensioni:  $\sigma_N=-3.70$   $\sigma_{m,d}=0.39$   $\tau=143.96$   $\tau_{max}=143.96$  (sfrut=0.07)  
Tensioni:  $\sigma_N=-3.70$   $\sigma_{m,d}=-1073.46$   $\tau=0.00$   $\sigma_{ID,max}=1077.17$  (sfrut=0.32)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3  
Sollecitazioni:  $N,Ed=-284.49$   $M_y,Ed=7163.35$   $M_z,Ed=-58.68$   $L=3.30$   
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $L_{cr}=3.30$  Curva b:  $\alpha_{imp}=0.34$   $k_c=0.94$   $\psi=1.72$   $M,cr=120469.00$   $\lambda_{LT}=0.45$   
 $\lambda_{LT,0}=0.40$   $\Phi_{LT}=0.58$   $\beta_{LT}=0.75$   $f=0.98$   $\chi_{LT}=1.00$   
 $\lambda_y=32.83$  Ncr,  $y=1477550.00$   $\lambda'_y=0.43$  Curva b:  $\Phi_y=0.63$   $\chi_y=0.91$   
 $\lambda_z=54.97$  Ncr,  $z=526968.00$   $\lambda'_z=0.72$  Curva c:  $\Phi_z=0.89$   $\chi_z=0.71$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY:  $0.00+0.30+0.01=0.31$   
Verifica ZZ:  $0.00+0.24+0.01=0.25$
- Verifica Spostamento relativo massimo per singola asta - CC 23  
 $\delta=1.11$  (L/297)
- Asta n. 2 (2 -10) - Sez. 1 (COLL HEA240) - Crit. 1
- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3  
Sollecitazioni:  $N=-1287.17$   $T_x=-217.66$   $M_y=-747.27$   $T_y=838.48$   $M_z=-1432.41$   
Tensioni:  $\sigma_N=-16.75$   $\sigma_{m,d}=-731.50$   $\tau=0.00$   $\sigma_{max}=-748.25$  (sfrut=0.22)  
Tensioni:  $\sigma_N=-16.75$   $\sigma_{m,d}=-28.90$   $\tau=20.95$   $\tau_{max}=20.95$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-16.75$   $\sigma_{m,d}=-731.50$   $\tau=0.00$   $\sigma_{ID,max}=748.25$  (sfrut=0.22)
- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 21 SLU Xl=0.90 - Classe 2  
Sollecitazioni:  $T_y=2.21$   $M_x=-1.97$   
 $V,Ed=2.21$   $V_c,Rd,Red=125817.00$   $V,Ed/V_c,Rd,Red=0.00$
- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 21 SLU Xl=0.90 - Classe 2  
Sollecitazioni:  $T_z=2893.27$   $M_x=-1.97$   
 $V,Ed=2893.27$   $V_c,Rd,Red=49084.60$   $V,Ed/V_c,Rd,Red=0.06$
- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3  
Sollecitazioni:  $N=-185.86$   $T_x=2893.27$   $M_y=9421.30$   $T_y=2.21$   $M_z=-2.67$   $M_x=-1.97$   
Tensioni:  $\sigma_N=-2.42$   $\sigma_{m,d}=-1396.74$   $\tau=6.34$   $\sigma_{max}=-1399.16$  (sfrut=0.41)  
Tensioni:  $\sigma_N=-2.42$   $\sigma_{m,d}=-0.04$   $\tau=196.90$   $\tau_{max}=196.90$  (sfrut=0.10)  
Tensioni:  $\sigma_N=-2.42$   $\sigma_{m,d}=-1396.74$   $\tau=6.34$   $\sigma_{ID,max}=1399.21$  (sfrut=0.41)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3  
Sollecitazioni:  $N,Ed=-185.86$   $M_y,Ed=9421.30$   $M_z,Ed=4.63$   $L=3.30$   
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $L_{cr}=3.30$  Curva b:  $\alpha_{imp}=0.34$   $k_c=0.94$   $\psi=1.76$   $M,cr=123279.00$   $\lambda_{LT}=0.44$   
 $\lambda_{LT,0}=0.40$   $\Phi_{LT}=0.58$   $\beta_{LT}=0.75$   $f=0.98$   $\chi_{LT}=1.00$   
 $\lambda_y=32.83$  Ncr,  $y=1477550.00$   $\lambda'_y=0.43$  Curva b:  $\Phi_y=0.63$   $\chi_y=0.91$   
 $\lambda_z=54.97$  Ncr,  $z=526968.00$   $\lambda'_z=0.72$  Curva c:  $\Phi_z=0.89$   $\chi_z=0.71$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY:  $0.00+0.39+0.00=0.39$   
Verifica ZZ:  $0.00+0.31+0.00=0.32$
- Verifica Spostamento relativo massimo per singola asta - CC 23  
 $\delta=1.44$  (L/229)
- Asta n. 3 (3 203) - Sez. 1 (COLL HEA240) - Crit. 1
- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3  
Sollecitazioni:  $N=-1542.39$   $T_x=233.29$   $M_y=806.45$   $T_y=-754.78$   $M_z=1341.31$   
Tensioni:  $\sigma_N=-20.07$   $\sigma_{m,d}=-700.78$   $\tau=0.00$   $\sigma_{max}=-720.86$  (sfrut=0.21)  
Tensioni:  $\sigma_N=-20.07$   $\sigma_{m,d}=12.90$   $\tau=18.89$   $\tau_{max}=18.89$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-20.07$   $\sigma_{m,d}=-700.78$   $\tau=0.00$   $\sigma_{ID,max}=720.86$  (sfrut=0.21)
- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 21 SLU Xl=0.60 - Classe 2  
Sollecitazioni:  $T_y=1.71$   $M_x=1.21$   
 $V,Ed=1.71$   $V_c,Rd,Red=125881.00$   $V,Ed/V_c,Rd,Red=0.00$
- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 21 SLU Xl=0.60 - Classe 2  
Sollecitazioni:  $T_z=3151.63$   $M_x=1.21$   
 $V,Ed=3151.63$   $V_c,Rd,Red=49109.40$   $V,Ed/V_c,Rd,Red=0.06$
- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3  
Sollecitazioni:  $N=-199.06$   $T_x=3151.63$   $M_y=10254.30$   $T_y=1.71$   $M_z=-1.98$   $M_x=1.21$   
Tensioni:  $\sigma_N=-2.59$   $\sigma_{m,d}=-1519.84$   $\tau=3.88$   $\sigma_{max}=-1522.43$  (sfrut=0.45)  
Tensioni:  $\sigma_N=-2.59$   $\sigma_{m,d}=0.03$   $\tau=214.40$   $\tau_{max}=214.40$  (sfrut=0.11)  
Tensioni:  $\sigma_N=-2.59$   $\sigma_{m,d}=-1519.84$   $\tau=3.88$   $\sigma_{ID,max}=1522.44$  (sfrut=0.45)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3  
Sollecitazioni:  $N,Ed=-199.06$   $M_y,Ed=10254.30$   $M_z,Ed=3.66$   $L=3.30$   
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $L_{cr}=3.30$  Curva b:  $\alpha_{imp}=0.34$   $k_c=0.94$   $\psi=1.77$   $M,cr=123339.00$   $\lambda_{LT}=0.44$   
 $\lambda_{LT,0}=0.40$   $\Phi_{LT}=0.58$   $\beta_{LT}=0.75$   $f=0.98$   $\chi_{LT}=1.00$   
 $\lambda_y=32.83$  Ncr,  $y=1477550.00$   $\lambda'_y=0.43$  Curva b:  $\Phi_y=0.63$   $\chi_y=0.91$   
 $\lambda_z=54.97$  Ncr,  $z=526968.00$   $\lambda'_z=0.72$  Curva c:  $\Phi_z=0.89$   $\chi_z=0.71$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY:  $0.00+0.43+0.00=0.43$   
Verifica ZZ:  $0.00+0.34+0.00=0.34$
- Verifica Spostamento relativo massimo per singola asta - CC 23  
 $\delta=1.56$  (L/211)
- Asta n. 4 (4 204) - Sez. 1 (COLL HEA240) - Crit. 1
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=-1423.57 T<sub>z</sub>=205.78 M<sub>y</sub>=730.75 T<sub>y</sub>=718.93 M<sub>z</sub>=-1302.25  
 Tensioni:  $\sigma_N$ =-18.53  $\sigma_{m,d}$ =-672.64  $\tau$ =0.00  $\sigma_{max}$ =-691.17 (sfrut=0.20)  
 Tensioni:  $\sigma_N$ =-18.53  $\sigma_{m,d}$ =-213.36  $\tau$ =17.98  $\tau_{max}$ =17.98 (sfrut=0.01)  
 Tensioni:  $\sigma_N$ =-18.53  $\sigma_{m,d}$ =-672.64  $\tau$ =0.00  $\sigma_{ID,max}$ =691.17 (sfrut=0.20)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=0.00 - Classe 2  
 Sollecitazioni: T<sub>z</sub>=-2578.76  
 V,Ed=-2578.76 Vc,Rd=49148.50 V,Ed/Vc,Rd=0.05
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.00 - Classe 2  
 Sollecitazioni: N=-344.91 T<sub>z</sub>=-2578.76 M<sub>y</sub>=-8696.99  
 My,Ed=-8696.99 My,V,c,Rd=25289.20  
 N,Ed=-344.91 Nc,Rd=-259785.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=25289.20 My,Ed/MNy,c,Rd=0.34
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3  
 Sollecitazioni: N,Ed=-344.91 My,Ed=-8696.99 Mz,Ed=0.00 L=3.30  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $L_{cr}$ =3.30 Curva b:  $\alpha_{imp}$ =0.34  $k_c$ =0.94  $\psi$ =1.73 M,cr=120721.00  $\lambda_{LT}$ =0.45  
 $\lambda_{LT,0}$ =0.40  $\Phi_{LT}$ =0.58  $\beta_{LT}$ =0.75 f=0.98  $\chi_{LT}$ =1.00  
 $\lambda_1$ =32.83 Ncr,y=1477550.00  $\lambda'_y$ =0.43 Curva b:  $\Phi_y$ =0.63  $\chi_y$ =0.91  
 $\lambda_2$ =54.97 Ncr,z=526968.00  $\lambda'_z$ =0.72 Curva c:  $\Phi_z$ =0.89  $\chi_z$ =0.71  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.36=0.36  
 Verifica ZZ: 0.00+0.29=0.29
- Verifica Spostamento relativo massimo per singola asta - CC 23  
 $\delta$ =1.35 (L/245)

Asta n. 5 (5 205) - Sez. 1 (COLL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-1542.39 T<sub>z</sub>=-233.29 M<sub>y</sub>=-806.45 T<sub>y</sub>=-754.78 M<sub>z</sub>=1341.31  
 Tensioni:  $\sigma_N$ =-20.07  $\sigma_{m,d}$ =-700.78  $\tau$ =0.00  $\sigma_{max}$ =-720.86 (sfrut=0.21)  
 Tensioni:  $\sigma_N$ =-20.07  $\sigma_{m,d}$ =226.89  $\tau$ =18.89  $\tau_{max}$ =18.89 (sfrut=0.01)  
 Tensioni:  $\sigma_N$ =-20.07  $\sigma_{m,d}$ =-700.78  $\tau$ =0.00  $\sigma_{ID,max}$ =720.86 (sfrut=0.21)
- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 21 SLU Xl=0.60 - Classe 2  
 Sollecitazioni: T<sub>y</sub>=1.71 M<sub>z</sub>=-1.21  
 V,Ed=1.71 Vc,Rd,Red=125881.00 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 21 SLU Xl=0.60 - Classe 2  
 Sollecitazioni: T<sub>z</sub>=-3151.63 M<sub>z</sub>=-1.21  
 V,Ed=-3151.63 Vc,Rd,Red=49109.40 V,Ed/Vc,Rd,Red=0.06
- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=-199.06 T<sub>z</sub>=-3151.63 M<sub>y</sub>=-10254.30 T<sub>y</sub>=1.71 M<sub>z</sub>=-1.98 M<sub>z</sub>=-1.21  
 Tensioni:  $\sigma_N$ =-2.59  $\sigma_{m,d}$ =-1519.84  $\tau$ =3.88  $\sigma_{max}$ =-1522.43 (sfrut=0.45)  
 Tensioni:  $\sigma_N$ =-2.59  $\sigma_{m,d}$ =-0.03  $\tau$ =214.40  $\tau_{max}$ =214.40 (sfrut=0.11)  
 Tensioni:  $\sigma_N$ =-2.59  $\sigma_{m,d}$ =-1519.84  $\tau$ =3.88  $\sigma_{ID,max}$ =1522.44 (sfrut=0.45)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3  
 Sollecitazioni: N,Ed=-199.06 My,Ed=-10254.30 Mz,Ed=3.66 L=3.30  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $L_{cr}$ =3.30 Curva b:  $\alpha_{imp}$ =0.34  $k_c$ =0.94  $\psi$ =1.77 M,cr=123339.00  $\lambda_{LT}$ =0.44  
 $\lambda_{LT,0}$ =0.40  $\Phi_{LT}$ =0.58  $\beta_{LT}$ =0.75 f=0.98  $\chi_{LT}$ =1.00  
 $\lambda_1$ =32.83 Ncr,y=1477550.00  $\lambda'_y$ =0.43 Curva b:  $\Phi_y$ =0.63  $\chi_y$ =0.91  
 $\lambda_2$ =54.97 Ncr,z=526968.00  $\lambda'_z$ =0.72 Curva c:  $\Phi_z$ =0.89  $\chi_z$ =0.71  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.43+0.00=0.43  
 Verifica ZZ: 0.00+0.34+0.00=0.34
- Verifica Spostamento relativo massimo per singola asta - CC 23  
 $\delta$ =1.56 (L/211)

Asta n. 6 (6 -31) - Sez. 1 (COLL HEA240) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-1287.17 T<sub>z</sub>=217.66 M<sub>y</sub>=747.27 T<sub>y</sub>=838.48 M<sub>z</sub>=-1432.41  
 Tensioni:  $\sigma_N$ =-16.75  $\sigma_{m,d}$ =-731.50  $\tau$ =0.00  $\sigma_{max}$ =-748.25 (sfrut=0.22)  
 Tensioni:  $\sigma_N$ =-16.75  $\sigma_{m,d}$ =-227.19  $\tau$ =20.95  $\tau_{max}$ =20.95 (sfrut=0.01)  
 Tensioni:  $\sigma_N$ =-16.75  $\sigma_{m,d}$ =-731.50  $\tau$ =0.00  $\sigma_{ID,max}$ =748.25 (sfrut=0.22)
- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 21 SLU Xl=0.90 - Classe 2  
 Sollecitazioni: T<sub>y</sub>=2.21 M<sub>z</sub>=1.97  
 V,Ed=2.21 Vc,Rd,Red=125817.00 V,Ed/Vc,Rd,Red=0.00
- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 21 SLU Xl=0.90 - Classe 2  
 Sollecitazioni: T<sub>z</sub>=-2893.27 M<sub>z</sub>=1.97  
 V,Ed=-2893.27 Vc,Rd,Red=49084.60 V,Ed/Vc,Rd,Red=0.06
- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=-185.86 T<sub>z</sub>=-2893.27 M<sub>y</sub>=-9421.29 T<sub>y</sub>=2.21 M<sub>z</sub>=-2.67 M<sub>z</sub>=1.97  
 Tensioni:  $\sigma_N$ =-2.42  $\sigma_{m,d}$ =-1396.74  $\tau$ =6.34  $\sigma_{max}$ =-1399.16 (sfrut=0.41)  
 Tensioni:  $\sigma_N$ =-2.42  $\sigma_{m,d}$ =0.04  $\tau$ =196.90  $\tau_{max}$ =196.90 (sfrut=0.10)  
 Tensioni:  $\sigma_N$ =-2.42  $\sigma_{m,d}$ =-1396.74  $\tau$ =6.34  $\sigma_{ID,max}$ =1399.20 (sfrut=0.41)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3  
 Sollecitazioni: N,Ed=-185.86 My,Ed=-9421.29 Mz,Ed=4.63 L=3.30  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $L_{cr}$ =3.30 Curva b:  $\alpha_{imp}$ =0.34  $k_c$ =0.94  $\psi$ =1.76 M,cr=123279.00  $\lambda_{LT}$ =0.44  
 $\lambda_{LT,0}$ =0.40  $\Phi_{LT}$ =0.58  $\beta_{LT}$ =0.75 f=0.98  $\chi_{LT}$ =1.00  
 $\lambda_1$ =32.83 Ncr,y=1477550.00  $\lambda'_y$ =0.43 Curva b:  $\Phi_y$ =0.63  $\chi_y$ =0.91  
 $\lambda_2$ =54.97 Ncr,z=526968.00  $\lambda'_z$ =0.72 Curva c:  $\Phi_z$ =0.89  $\chi_z$ =0.71  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.39+0.00=0.39  
 Verifica ZZ: 0.00+0.31+0.00=0.32
- Verifica Spostamento relativo massimo per singola asta - CC 23  
 $\delta$ =1.44 (L/229)

Asta n. 7 (7 -36) - Sez. 1 (COLL HEA240) - Crit. 1

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- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=-852.25 T<sub>z</sub>=193.71 M<sub>y</sub>=676.98 T<sub>y</sub>=-651.83 M<sub>z</sub>=1228.40  
Tensioni:  $\sigma_N=-11.09$   $\sigma_{m,d}=-632.67$   $\tau=0.00$   $\sigma_{max}=-643.76$  (sfrut=0.19)  
Tensioni:  $\sigma_N=-11.09$   $\sigma_{m,d}=19.99$   $\tau=16.31$   $\tau_{max}=16.31$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-11.09$   $\sigma_{m,d}=-632.67$   $\tau=0.00$   $\sigma_{ID,max}=643.76$  (sfrut=0.19)
- Verifica a taglio Dir. Y [4.2.16] - CC 13 SND Xl=2.40 - Classe 2  
Sollecitazioni: T<sub>y</sub>=117.90  
V,Ed=117.90 Vc,Rd=125981.00 V,Ed/Vc,Rd=0.00
- Verifica a taglio Dir. Z [4.2.16] - CC 13 SND Xl=2.40 - Classe 2  
Sollecitazioni: T<sub>z</sub>=-573.40  
V,Ed=-573.40 Vc,Rd=49148.50 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 21 SLU Xl=0.00 - Classe 3  
Sollecitazioni: N=-284.48 T<sub>z</sub>=-2116.47 M<sub>y</sub>=-7163.36 T<sub>y</sub>=-26.42 M<sub>z</sub>=28.49  
Tensioni:  $\sigma_N=-3.70$   $\sigma_{m,d}=-1073.46$   $\tau=0.00$   $\sigma_{max}=-1077.17$  (sfrut=0.32)  
Tensioni:  $\sigma_N=-3.70$   $\sigma_{m,d}=0.39$   $\tau=143.96$   $\tau_{max}=143.96$  (sfrut=0.07)  
Tensioni:  $\sigma_N=-3.70$   $\sigma_{m,d}=-1073.46$   $\tau=0.00$   $\sigma_{ID,max}=1077.17$  (sfrut=0.32)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 21 SLU - Classe 3  
Sollecitazioni: N,Ed=-284.48 M<sub>y</sub>,Ed=-7163.36 M<sub>z</sub>,Ed=-58.68 L=3.30  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
L<sub>cr</sub>=3.30 Curva b:  $\alpha_{imp}=0.34$   $k_c=0.94$   $\psi=1.72$  M,cr=120469.00  $\lambda_{LT}=0.45$   
 $\lambda_{LT,0}=0.40$   $\Phi_{LT}=0.58$   $\beta_{LT}=0.75$   $f=0.98$   $\chi_{LT}=1.00$   
 $\lambda_y=32.83$  Ncr,y=1477550.00  $\lambda'_y=0.43$  Curva b:  $\Phi_y=0.63$   $\chi_y=0.91$   
 $\lambda_z=54.97$  Ncr,z=526968.00  $\lambda'_z=0.72$  Curva c:  $\Phi_z=0.89$   $\chi_z=0.71$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.30+0.01=0.31  
Verifica ZZ: 0.00+0.24+0.01=0.25
- Verifica Spostamento relativo massimo per singola asta - CC 23  
 $\delta=1.11$  (L/297)

Asta n. 201 (-4 -3) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=28.47 T<sub>z</sub>=216.51 M<sub>y</sub>=252.33 T<sub>y</sub>=-94.91 M<sub>z</sub>=131.09 M<sub>x</sub>=-20.73  
Tensioni:  $\sigma_N=0.46$   $\sigma_{m,d}=101.40$   $\tau=3.51$   $\sigma_{max}=101.86$  (sfrut=0.03)  
Tensioni:  $\sigma_N=0.46$   $\sigma_{m,d}=-31.89$   $\tau=11.44$   $\tau_{max}=11.44$  (sfrut=0.01)  
Tensioni:  $\sigma_N=0.46$   $\sigma_{m,d}=101.40$   $\tau=3.51$   $\sigma_{ID,max}=102.04$  (sfrut=0.03)
- Verifica a taglio Dir. Y [4.2.16] - CC 28 SLU Xl=1.34  
Sollecitazioni: T<sub>y</sub>=221.93  
V,Ed=221.93 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.34  
Sollecitazioni: T<sub>z</sub>=386.55  
V,Ed=386.55 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: T<sub>z</sub>=470.28 M<sub>y</sub>=572.08 T<sub>y</sub>=221.93 M<sub>z</sub>=-296.35  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-229.66$   $\tau=0.00$   $\sigma_{max}=-229.66$  (sfrut=0.07)  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-72.10$   $\tau=17.21$   $\tau_{max}=17.21$  (sfrut=0.01)  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-229.66$   $\tau=0.00$   $\sigma_{ID,max}=229.66$  (sfrut=0.07)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: M<sub>y</sub>,Ed=572.08 M<sub>z</sub>,Ed=-296.35 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395380.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395380.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.04+0.02=0.06  
Verifica ZZ: 0.00+0.03+0.02=0.06

Asta n. 201 (-5 -4) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=69.78 T<sub>z</sub>=470.88 M<sub>y</sub>=620.62 T<sub>y</sub>=-232.61 M<sub>z</sub>=322.46 M<sub>x</sub>=-51.80  
Tensioni:  $\sigma_N=1.14$   $\sigma_{m,d}=249.40$   $\tau=8.78$   $\sigma_{max}=250.53$  (sfrut=0.07)  
Tensioni:  $\sigma_N=1.14$   $\sigma_{m,d}=-78.45$   $\tau=26.01$   $\tau_{max}=26.01$  (sfrut=0.01)  
Tensioni:  $\sigma_N=1.14$   $\sigma_{m,d}=249.40$   $\tau=8.78$   $\sigma_{ID,max}=250.99$  (sfrut=0.07)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=774.27  
V,Ed=774.27 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: T<sub>z</sub>=1178.59 M<sub>y</sub>=1488.85 T<sub>y</sub>=665.79 M<sub>z</sub>=-825.43  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-612.01$   $\tau=0.00$   $\sigma_{max}=-612.01$  (sfrut=0.18)  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-200.82$   $\tau=43.13$   $\tau_{max}=43.13$  (sfrut=0.02)  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-612.01$   $\tau=0.00$   $\sigma_{ID,max}=612.01$  (sfrut=0.18)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: M<sub>y</sub>,Ed=1488.85 M<sub>z</sub>,Ed=-825.43 L=0.79  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=10.13$  Ncr,y=12411000.00  $\lambda'_y=0.13$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=10.13$  Ncr,z=12411000.00  $\lambda'_z=0.13$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.11+0.06=0.17  
Verifica ZZ: 0.00+0.09+0.06=0.15

Asta n. 201 (-6 -5) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.54 - Classe 3  
Sollecitazioni: N=-234.46 T<sub>z</sub>=-855.02 M<sub>y</sub>=1315.51 T<sub>y</sub>=104.33 M<sub>z</sub>=129.61 M<sub>x</sub>=22.20  
Tensioni:  $\sigma_N=-3.82$   $\sigma_{m,d}=-382.16$   $\tau=3.76$   $\sigma_{max}=-385.98$  (sfrut=0.11)  
Tensioni:  $\sigma_N=-3.82$   $\sigma_{m,d}=-31.53$   $\tau=35.04$   $\tau_{max}=35.04$  (sfrut=0.02)

Tensioni:  $\sigma_N=-3.82$   $\sigma_{m,d}=-382.16$   $\tau=3.76$   $\sigma_{ID,max}=386.04$  (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU  $X1=0.54$  - Classe 1  
Sollecitazioni:  $T_x=-880.69$   
 $V,Ed=-880.69$   $Vc,Rd=59967.00$   $V,Ed/Vc,Rd=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU  $X1=0.54$  - Classe 3  
Sollecitazioni:  $N=129.33$   $T_x=-1379.55$   $M_y=1203.33$   $T_y=-825.23$   $M_z=-825.51$   $M_x=-126.12$   
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=536.53$   $\tau=21.38$   $\sigma_{max}=538.63$  (sfrut=0.16)  
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=-200.84$   $\tau=71.86$   $\tau_{max}=71.86$  (sfrut=0.04)  
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=536.53$   $\tau=21.38$   $\sigma_{ID,max}=539.91$  (sfrut=0.16)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni:  $M_y,Ed=1203.33$   $M_z,Ed=-825.51$   $L=0.54$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=6.89$  Ncr, $y=26811000.00$   $\lambda'_y=0.09$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=6.89$  Ncr, $z=26811000.00$   $\lambda'_z=0.09$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$   
Verifica YY:  $0.00+0.09+0.06=0.15$   
Verifica ZZ:  $0.00+0.07+0.06=0.13$

Asta n. 201 (-7 -6) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND  $X1=1.34$  - Classe 3  
Sollecitazioni:  $N=-99.91$   $T_x=-612.90$   $M_y=891.36$   $T_y=63.97$   $M_z=94.96$   $M_x=12.88$   
Tensioni:  $\sigma_N=-1.63$   $\sigma_{m,d}=-260.83$   $\tau=2.18$   $\sigma_{max}=-262.46$  (sfrut=0.08)  
Tensioni:  $\sigma_N=-1.63$   $\sigma_{m,d}=-23.10$   $\tau=24.60$   $\tau_{max}=24.60$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-1.63$   $\sigma_{m,d}=-260.83$   $\tau=2.18$   $\sigma_{ID,max}=262.49$  (sfrut=0.08)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 5 SND  $X1=1.09$  - Classe 1  
Sollecitazioni:  $T_y=-16.30$   $M_x=-26.56$   
 $V,Ed=-16.30$   $Vc,Rd,Red=59828.70$   $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 5 SND  $X1=1.09$  - Classe 1  
Sollecitazioni:  $T_z=-601.19$   $M_x=-26.56$   
 $V,Ed=-601.19$   $Vc,Rd,Red=59828.70$   $V,Ed/Vc,Rd,Red=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU  $X1=1.34$  - Classe 3  
Sollecitazioni:  $N=129.33$   $T_x=-687.17$   $M_y=466.62$   $T_y=-381.37$   $M_z=-379.33$   $M_x=-126.12$   
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=223.71$   $\tau=21.38$   $\sigma_{max}=225.82$  (sfrut=0.07)  
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=-92.29$   $\tau=46.52$   $\tau_{max}=46.52$  (sfrut=0.02)  
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=223.71$   $\tau=21.38$   $\sigma_{ID,max}=228.83$  (sfrut=0.07)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 7 SND - Classe 3  
Sollecitazioni:  $N,Ed=-99.91$   $M_y,Ed=891.36$   $M_z,Ed=94.96$   $L=1.34$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=17.02$  Ncr, $y=4395380.00$   $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr, $z=4395380.00$   $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$   
Verifica YY:  $0.00+0.07+0.01=0.07$   
Verifica ZZ:  $0.00+0.05+0.01=0.06$

Asta n. 201 (-8 -7) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND  $X1=1.34$  - Classe 3  
Sollecitazioni:  $N=74.96$   $T_x=330.43$   $M_y=-418.60$   $T_y=-27.02$   $M_z=-38.65$   $M_x=17.23$   
Tensioni:  $\sigma_N=1.22$   $\sigma_{m,d}=120.92$   $\tau=2.92$   $\sigma_{max}=122.14$  (sfrut=0.04)  
Tensioni:  $\sigma_N=1.22$   $\sigma_{m,d}=-9.40$   $\tau=15.01$   $\tau_{max}=15.01$  (sfrut=0.01)  
Tensioni:  $\sigma_N=1.22$   $\sigma_{m,d}=120.92$   $\tau=2.92$   $\sigma_{ID,max}=122.25$  (sfrut=0.04)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 13 SND  $X1=0.00$  - Classe 1  
Sollecitazioni:  $T_y=-17.78$   $M_x=36.71$   
 $V,Ed=-17.78$   $Vc,Rd,Red=59775.80$   $V,Ed/Vc,Rd,Red=0.00$

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 13 SND  $X1=0.00$  - Classe 1  
Sollecitazioni:  $T_z=162.83$   $M_x=36.71$   
 $V,Ed=162.83$   $Vc,Rd,Red=59775.80$   $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU  $X1=1.34$  - Classe 3  
Sollecitazioni:  $N=129.33$   $T_x=55.04$   $M_y=-395.08$   $T_y=62.49$   $M_z=129.92$   $M_x=-126.12$   
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=138.84$   $\tau=21.38$   $\sigma_{max}=140.94$  (sfrut=0.04)  
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=-96.12$   $\tau=23.67$   $\tau_{max}=23.67$  (sfrut=0.01)  
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=138.84$   $\tau=21.38$   $\sigma_{ID,max}=145.73$  (sfrut=0.04)

Asta n. 201 (-9 -8) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND  $X1=0.00$  - Classe 3  
Sollecitazioni:  $N=-69.46$   $T_x=675.28$   $M_y=893.28$   $T_y=-70.34$   $M_z=69.60$   $M_x=7.91$   
Tensioni:  $\sigma_N=-1.13$   $\sigma_{m,d}=-254.64$   $\tau=1.34$   $\sigma_{max}=-255.77$  (sfrut=0.08)  
Tensioni:  $\sigma_N=-1.13$   $\sigma_{m,d}=16.93$   $\tau=26.04$   $\tau_{max}=26.04$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-1.13$   $\sigma_{m,d}=-254.64$   $\tau=1.34$   $\sigma_{ID,max}=255.78$  (sfrut=0.08)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU  $X1=0.97$  - Classe 1  
Sollecitazioni:  $T_y=-718.76$   $M_x=179.02$   
 $V,Ed=-718.76$   $Vc,Rd,Red=59034.60$   $V,Ed/Vc,Rd,Red=0.01$

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU  $X1=0.97$  - Classe 1  
Sollecitazioni:  $T_z=-44.09$   $M_x=179.02$   
 $V,Ed=-44.09$   $Vc,Rd,Red=59034.60$   $V,Ed/Vc,Rd,Red=0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU  $X1=0.00$  - Classe 3  
Sollecitazioni:  $N=129.33$   $T_x=880.97$   $M_y=854.80$   $T_y=506.36$   $M_z=-629.69$   $M_x=-126.12$   
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=392.57$   $\tau=21.38$   $\sigma_{max}=394.68$  (sfrut=0.12)  
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=153.20$   $\tau=53.62$   $\tau_{max}=53.62$  (sfrut=0.03)  
Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=392.57$   $\tau=21.38$   $\sigma_{ID,max}=396.41$  (sfrut=0.12)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni:  $M_y,Ed=854.80$   $M_z,Ed=-629.69$   $L=1.34$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=17.02$  Ncr, $y=4395370.00$   $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$

$\lambda_z=17.02$  Ncr,  $z=4395370.00$   $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.06+0.05=0.11  
 Verifica ZZ: 0.00+0.05+0.05=0.10

Asta n. 201 (-10 -9) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-202.92  $T_x=913.19$   $M_y=1271.24$   $T_y=62.72$   $M_z=-105.97$   $M_x=15.09$   
 Tensioni:  $\sigma_N=-3.30$   $\sigma_{m,d}=-364.20$   $\tau=2.56$   $\sigma_{max}=-367.51$  (sfrut=0.11)  
 Tensioni:  $\sigma_N=-3.30$   $\sigma_{m,d}=-25.78$   $\tau=35.96$   $\tau_{max}=35.96$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=-3.30$   $\sigma_{m,d}=-364.20$   $\tau=2.56$   $\sigma_{ID,max}=367.53$  (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
 Sollecitazioni:  $T_x=988.58$   
 $V_{Ed}=988.58$   $V_{c,Rd}=59967.00$   $V_{Ed/V_{c,Rd}}=0.02$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=129.33  $T_x=1567.88$   $M_y=1559.14$   $T_y=950.22$   $M_z=-1060.46$   $M_x=-126.11$   
 Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=692.75$   $\tau=21.38$   $\sigma_{max}=694.86$  (sfrut=0.21)  
 Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=258.00$   $\tau=78.76$   $\tau_{max}=78.76$  (sfrut=0.04)  
 Tensioni:  $\sigma_N=2.10$   $\sigma_{m,d}=692.75$   $\tau=21.38$   $\sigma_{ID,max}=695.84$  (sfrut=0.21)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni:  $M_y,Ed=1559.14$   $M_z,Ed=-1060.46$   $L=0.45$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=5.78$  Ncr,  $y=38136200.00$   $\lambda'_y=0.08$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=5.78$  Ncr,  $z=38136200.00$   $\lambda'_z=0.08$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.12+0.08=0.19  
 Verifica ZZ: 0.00+0.09+0.08=0.17

Asta n. 202 (-11 -10) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.88 - Classe 3  
 Sollecitazioni: N=-450.80  $T_x=-847.63$   $M_y=1224.88$   $T_y=120.61$   $M_z=106.11$   $M_x=28.64$   
 Tensioni:  $\sigma_N=-7.34$   $\sigma_{m,d}=-351.98$   $\tau=4.86$   $\sigma_{max}=-359.32$  (sfrut=0.11)  
 Tensioni:  $\sigma_N=-7.34$   $\sigma_{m,d}=-25.82$   $\tau=35.86$   $\tau_{max}=35.86$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=-7.34$   $\sigma_{m,d}=-351.98$   $\tau=4.86$   $\sigma_{ID,max}=359.42$  (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.88 - Classe 1  
 Sollecitazioni:  $T_x=-1176.29$   
 $V_{Ed}=-1176.29$   $V_{c,Rd}=59967.00$   $V_{Ed/V_{c,Rd}}=0.02$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.88 - Classe 3  
 Sollecitazioni: N=-122.31  $T_x=-1840.16$   $M_y=2115.20$   $T_y=-1088.06$   $M_z=-1061.85$   $M_x=-37.01$   
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-840.17$   $\tau=6.27$   $\sigma_{max}=-842.16$  (sfrut=0.25)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-258.34$   $\tau=73.62$   $\tau_{max}=73.62$  (sfrut=0.04)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-840.17$   $\tau=6.27$   $\sigma_{ID,max}=842.23$  (sfrut=0.25)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31  $M_y,Ed=2115.20$   $M_z,Ed=-1061.85$   $L=0.88$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=11.24$  Ncr,  $y=10074900.00$   $\lambda'_y=0.15$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=11.24$  Ncr,  $z=10074900.00$   $\lambda'_z=0.15$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.16+0.08=0.24  
 Verifica ZZ: 0.00+0.13+0.08=0.21

Asta n. 202 (-12 -11) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=44.87  $T_x=-332.81$   $M_y=-389.70$   $T_y=-213.31$   $M_z=247.43$   $M_x=-62.81$   
 Tensioni:  $\sigma_N=0.73$   $\sigma_{m,d}=168.49$   $\tau=10.65$   $\sigma_{max}=169.22$  (sfrut=0.05)  
 Tensioni:  $\sigma_N=0.73$   $\sigma_{m,d}=60.20$   $\tau=22.83$   $\tau_{max}=22.83$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=0.73$   $\sigma_{m,d}=168.49$   $\tau=10.65$   $\sigma_{ID,max}=170.22$  (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 1  
 Sollecitazioni:  $T_x=-732.05$   
 $V_{Ed}=-732.05$   $V_{c,Rd}=59967.00$   $V_{Ed/V_{c,Rd}}=0.01$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=-122.31  $T_x=-1042.65$   $M_y=-931.60$   $T_y=-644.19$   $M_z=758.03$   $M_x=-37.01$   
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-446.82$   $\tau=6.27$   $\sigma_{max}=-448.81$  (sfrut=0.13)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=184.42$   $\tau=44.43$   $\tau_{max}=44.43$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-446.82$   $\tau=6.27$   $\sigma_{ID,max}=448.94$  (sfrut=0.13)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31  $M_y,Ed=-931.60$   $M_z,Ed=758.03$   $L=1.34$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=17.02$  Ncr,  $y=4395370.00$   $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,  $z=4395370.00$   $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.07+0.06=0.13  
 Verifica ZZ: 0.00+0.06+0.06=0.11

Asta n. 202 (-13 -12) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-76.52  $T_x=-140.90$   $M_y=-531.57$   $T_y=68.90$   $M_z=-332.90$   $M_x=31.74$   
 Tensioni:  $\sigma_N=-1.25$   $\sigma_{m,d}=-228.61$   $\tau=5.38$   $\sigma_{max}=-229.86$  (sfrut=0.07)  
 Tensioni:  $\sigma_N=-1.25$   $\sigma_{m,d}=80.99$   $\tau=10.54$   $\tau_{max}=10.54$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=-1.25$   $\sigma_{m,d}=-228.61$   $\tau=5.38$   $\sigma_{ID,max}=230.04$  (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 1  
 Sollecitazioni:  $T_x=-259.38$   
 $V_{Ed}=-259.38$   $V_{c,Rd}=59967.00$   $V_{Ed/V_{c,Rd}}=0.00$

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=-122.31  $T_x=-300.44$   $M_y=-1388.69$   $T_y=-200.33$   $M_z=1025.54$   $M_x=-37.00$

Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-638.44$   $\tau=6.27$   $\sigma_{max}=-640.43$  (sfrut=0.19)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=249.51$   $\tau=17.27$   $\tau_{max}=17.27$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-638.44$   $\tau=6.27$   $\sigma_{TD,max}=640.53$  (sfrut=0.19)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=-1388.69 Mz,Ed=1025.54 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395370.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395370.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.10+0.08=0.18  
 Verifica ZZ: 0.00+0.08+0.08=0.16

Asta n. 202 (-14 -13) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=1.34 - Classe 3  
 Sollecitazioni: N=-33.20 T<sub>z</sub>=75.14 M<sub>y</sub>=-522.25 T<sub>y</sub>=85.39 M<sub>z</sub>=332.87  
 Tensioni:  $\sigma_N=-0.54$   $\sigma_{m,d}=-226.14$   $\tau=0.00$   $\sigma_{max}=-226.68$  (sfrut=0.07)  
 Tensioni:  $\sigma_N=-0.54$   $\sigma_{m,d}=-127.06$   $\tau=3.13$   $\tau_{max}=3.13$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-0.54$   $\sigma_{m,d}=-226.14$   $\tau=0.00$   $\sigma_{TD,max}=226.68$  (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
 Sollecitazioni: T<sub>z</sub>=297.01  
 V,Ed=297.01 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
 Sollecitazioni: N=-122.31 T<sub>z</sub>=358.04 M<sub>y</sub>=-1388.69 T<sub>y</sub>=243.53 M<sub>z</sub>=1025.54 M<sub>x</sub>=-37.00  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-638.44$   $\tau=6.27$   $\sigma_{max}=-640.43$  (sfrut=0.19)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-249.51$   $\tau=19.38$   $\tau_{max}=19.38$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-638.44$   $\tau=6.27$   $\sigma_{TD,max}=640.53$  (sfrut=0.19)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=-1388.69 Mz,Ed=1025.54 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395370.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395370.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.10+0.08=0.18  
 Verifica ZZ: 0.00+0.08+0.08=0.16

Asta n. 202 (-15 -14) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-196.20 T<sub>z</sub>=611.83 M<sub>y</sub>=622.32 T<sub>y</sub>=-83.93 M<sub>z</sub>=34.81 M<sub>x</sub>=-9.69  
 Tensioni:  $\sigma_N=-3.19$   $\sigma_{m,d}=-173.78$   $\tau=1.64$   $\sigma_{max}=-176.97$  (sfrut=0.05)  
 Tensioni:  $\sigma_N=-3.19$   $\sigma_{m,d}=-8.47$   $\tau=24.02$   $\tau_{max}=24.02$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=-3.19$   $\sigma_{m,d}=-173.78$   $\tau=1.64$   $\sigma_{TD,max}=177.00$  (sfrut=0.05)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=0.12 - Classe 1  
 Sollecitazioni: T<sub>y</sub>=-975.74 M<sub>x</sub>=52.52  
 V,Ed=-975.74 Vc,Rd,Red=59693.40 V,Ed/Vc,Rd,Red=0.02

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=0.12 - Classe 1  
 Sollecitazioni: T<sub>z</sub>=20.56 M<sub>x</sub>=52.52  
 V,Ed=20.56 Vc,Rd,Red=59693.40 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
 Sollecitazioni: N=-122.31 T<sub>z</sub>=1100.25 M<sub>y</sub>=-854.69 T<sub>y</sub>=687.39 M<sub>z</sub>=700.34 M<sub>x</sub>=-37.00  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-411.23$   $\tau=6.27$   $\sigma_{max}=-413.22$  (sfrut=0.12)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-170.39$   $\tau=46.54$   $\tau_{max}=46.54$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-411.23$   $\tau=6.27$   $\sigma_{TD,max}=413.36$  (sfrut=0.12)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=-854.69 Mz,Ed=700.34 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395370.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395370.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.06+0.05=0.12  
 Verifica ZZ: 0.00+0.05+0.05=0.10

Asta n. 202 (203 -15) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-334.92 T<sub>z</sub>=870.16 M<sub>y</sub>=1335.56 T<sub>y</sub>=-125.54 M<sub>z</sub>=123.11 M<sub>x</sub>=-19.01  
 Tensioni:  $\sigma_N=-5.45$   $\sigma_{m,d}=-385.75$   $\tau=3.22$   $\sigma_{max}=-391.20$  (sfrut=0.12)  
 Tensioni:  $\sigma_N=-5.45$   $\sigma_{m,d}=-29.95$   $\tau=35.05$   $\tau_{max}=35.05$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=-5.45$   $\sigma_{m,d}=-385.75$   $\tau=3.22$   $\sigma_{TD,max}=391.24$  (sfrut=0.12)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
 Sollecitazioni: T<sub>z</sub>=1213.59  
 V,Ed=1213.59 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=-122.31 T<sub>z</sub>=1897.42 M<sub>y</sub>=2309.73 T<sub>y</sub>=1131.26 M<sub>z</sub>=-1209.30 M<sub>x</sub>=-37.00  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-930.61$   $\tau=6.27$   $\sigma_{max}=-932.60$  (sfrut=0.28)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=294.22$   $\tau=75.71$   $\tau_{max}=75.71$  (sfrut=0.04)  
 Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-930.61$   $\tau=6.27$   $\sigma_{TD,max}=932.66$  (sfrut=0.28)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=2309.73 Mz,Ed=-1209.30 L=0.88  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=11.17$  Ncr,y=10197800.00  $\lambda'_y=0.15$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=11.17$  Ncr,z=10197800.00  $\lambda'_z=0.15$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.17+0.09=0.26  
 Verifica ZZ: 0.00+0.14+0.09=0.23

Asta n. 203 (-16 203) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2



- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.46 - Classe 3  
Sollecitazioni: N=-308.53 T<sub>x</sub>=-893.98 M<sub>y</sub>=1291.70 T<sub>y</sub>=-88.16 M<sub>z</sub>=-123.03 M<sub>x</sub>=-17.57  
Tensioni:  $\sigma_N=-5.02$   $\sigma_{m,d}=-374.13$   $\tau=2.98$   $\sigma_{max}=-379.15$  (sfrut=0.11)  
Tensioni:  $\sigma_N=-5.02$   $\sigma_{m,d}=-29.93$   $\tau=35.68$   $\tau_{max}=35.68$  (sfrut=0.02)  
Tensioni:  $\sigma_N=-5.02$   $\sigma_{m,d}=-374.13$   $\tau=2.98$   $\sigma_{ID,max}=379.18$  (sfrut=0.11)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.46 - Classe 1  
Sollecitazioni: T<sub>x</sub>=-1164.04  
V,Ed=-1164.04 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.46 - Classe 3  
Sollecitazioni: N=37.41 T<sub>x</sub>=-1834.87 M<sub>y</sub>=1956.88 T<sub>y</sub>=-1089.03 M<sub>z</sub>=-1208.41 M<sub>x</sub>=65.89  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=837.06$   $\tau=11.17$   $\sigma_{max}=837.67$  (sfrut=0.25)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=294.00$   $\tau=78.32$   $\tau_{max}=78.32$  (sfrut=0.04)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=837.06$   $\tau=11.17$   $\sigma_{ID,max}=837.89$  (sfrut=0.25)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1956.88 Mz,Ed=-1208.41 L=0.46  
amy, amz, aLT=0.95, 0.95, 0.95  
 $\lambda_y=5.85$  Ncr,y=37254500.00  $\lambda'_y=0.08$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=5.85$  Ncr,z=37254500.00  $\lambda'_z=0.08$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.15+0.09=0.24  
Verifica ZZ: 0.00+0.12+0.09=0.21
- Asta n. 203 (-17 -16) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=1.34 - Classe 3  
Sollecitazioni: N=-175.00 T<sub>x</sub>=-655.82 M<sub>y</sub>=917.82 T<sub>y</sub>=80.60 M<sub>z</sub>=81.33 M<sub>x</sub>=8.47  
Tensioni:  $\sigma_N=-2.85$   $\sigma_{m,d}=-264.23$   $\tau=1.44$   $\sigma_{max}=-267.07$  (sfrut=0.08)  
Tensioni:  $\sigma_N=-2.85$   $\sigma_{m,d}=-19.79$   $\tau=25.43$   $\tau_{max}=25.43$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-2.85$   $\sigma_{m,d}=-264.23$   $\tau=1.44$   $\sigma_{ID,max}=267.09$  (sfrut=0.08)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 1  
Sollecitazioni: T<sub>x</sub>=-746.34  
V,Ed=-746.34 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
Sollecitazioni: N=37.41 T<sub>x</sub>=-1147.63 M<sub>y</sub>=1121.91 T<sub>y</sub>=-645.16 M<sub>z</sub>=-708.93 M<sub>x</sub>=65.89  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=484.17$   $\tau=11.17$   $\sigma_{max}=484.78$  (sfrut=0.14)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=172.48$   $\tau=53.17$   $\tau_{max}=53.17$  (sfrut=0.03)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=484.17$   $\tau=11.17$   $\sigma_{ID,max}=485.16$  (sfrut=0.14)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1121.91 Mz,Ed=-708.93 L=1.34  
amy, amz, aLT=0.95, 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395380.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395380.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.08+0.05=0.14  
Verifica ZZ: 0.00+0.07+0.05=0.12
- Asta n. 203 (-18 -17) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 15 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=6.94 T<sub>x</sub>=-167.13 M<sub>y</sub>=-322.42 T<sub>y</sub>=74.96 M<sub>z</sub>=-146.49 M<sub>x</sub>=-3.18  
Tensioni:  $\sigma_N=0.11$   $\sigma_{m,d}=124.00$   $\tau=0.54$   $\sigma_{max}=124.12$  (sfrut=0.04)  
Tensioni:  $\sigma_N=0.11$   $\sigma_{m,d}=-35.64$   $\tau=6.65$   $\tau_{max}=6.65$  (sfrut=0.00)  
Tensioni:  $\sigma_N=0.11$   $\sigma_{m,d}=124.00$   $\tau=0.54$   $\sigma_{ID,max}=124.12$  (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 1  
Sollecitazioni: T<sub>x</sub>=-273.68  
V,Ed=-273.68 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: N=37.41 T<sub>x</sub>=-321.70 M<sub>y</sub>=-840.12 T<sub>y</sub>=-201.30 M<sub>z</sub>=421.37 M<sub>x</sub>=65.90  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=333.60$   $\tau=11.17$   $\sigma_{max}=334.21$  (sfrut=0.10)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=-102.52$   $\tau=22.94$   $\tau_{max}=22.94$  (sfrut=0.01)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=333.60$   $\tau=11.17$   $\sigma_{ID,max}=334.77$  (sfrut=0.10)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=-840.12 Mz,Ed=421.37 L=1.34  
amy, amz, aLT=0.95, 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395370.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395370.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.06+0.03=0.09  
Verifica ZZ: 0.00+0.05+0.03=0.08
- Asta n. 203 (-19 -18) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
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- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=1.34 - Classe 3  
Sollecitazioni: N=50.26 T<sub>x</sub>=48.92 M<sub>y</sub>=-313.10 T<sub>y</sub>=79.20 M<sub>z</sub>=146.18 M<sub>x</sub>=34.32  
Tensioni:  $\sigma_N=0.82$   $\sigma_{m,d}=121.46$   $\tau=5.82$   $\sigma_{max}=122.27$  (sfrut=0.04)  
Tensioni:  $\sigma_N=0.82$   $\sigma_{m,d}=76.18$   $\tau=8.72$   $\tau_{max}=8.72$  (sfrut=0.00)  
Tensioni:  $\sigma_N=0.82$   $\sigma_{m,d}=121.46$   $\tau=5.82$   $\sigma_{ID,max}=122.69$  (sfrut=0.04)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>x</sub>=282.72  
V,Ed=282.72 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
Sollecitazioni: N=37.41 T<sub>x</sub>=336.79 M<sub>y</sub>=-840.10 T<sub>y</sub>=242.56 M<sub>z</sub>=421.36 M<sub>x</sub>=65.90  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=333.59$   $\tau=11.17$   $\sigma_{max}=334.20$  (sfrut=0.10)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=102.51$   $\tau=23.50$   $\tau_{max}=23.50$  (sfrut=0.01)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=333.59$   $\tau=11.17$   $\sigma_{ID,max}=334.76$  (sfrut=0.10)
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=-840.10 Mz,Ed=421.36 L=1.34

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=17.02$  Ncr, $y=4395380.00$   $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$

$\lambda_z=17.02$  Ncr, $z=4395380.00$   $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.06+0.03=0.09

Verifica ZZ: 0.00+0.05+0.03=0.08

Asta n. 203 (-20 -19) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=-212.21 T<sub>z</sub>=660.91 M<sub>y</sub>=956.51 T<sub>y</sub>=-81.87 M<sub>z</sub>=85.74 M<sub>x</sub>=-19.72  
Tensioni:  $\sigma_N=-3.45$   $\sigma_{m,d}=-275.62$   $\tau=3.34$   $\sigma_{max}=-279.08$  (sfrut=0.08)  
Tensioni:  $\sigma_N=-3.45$   $\sigma_{m,d}=-20.86$   $\tau=27.52$   $\tau_{max}=27.52$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-3.45$   $\sigma_{m,d}=-275.62$   $\tau=3.34$   $\sigma_{TD,max}=279.14$  (sfrut=0.08)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=1.09 - Classe 1  
Sollecitazioni: T<sub>y</sub>=-974.36 M<sub>x</sub>=-93.54  
V,Ed=-974.36 Vc,Rd,Red=59479.80 V,Ed/Vc,Rd,Red=0.02

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=1.09 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-42.16 M<sub>x</sub>=-93.54  
V,Ed=-42.16 Vc,Rd,Red=59479.80 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: N=37.41 T<sub>z</sub>=1162.72 M<sub>y</sub>=1162.20 T<sub>y</sub>=686.42 M<sub>z</sub>=-819.12 M<sub>x</sub>=65.90  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=523.96$   $\tau=11.17$   $\sigma_{max}=524.57$  (sfrut=0.16)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=-199.29$   $\tau=53.72$   $\tau_{max}=53.72$  (sfrut=0.03)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=523.96$   $\tau=11.17$   $\sigma_{TD,max}=524.93$  (sfrut=0.16)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1162.20 Mz,Ed=-819.12 L=1.34  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=17.02$  Ncr, $y=4395370.00$   $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr, $z=4395370.00$   $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.09+0.06=0.15  
Verifica ZZ: 0.00+0.07+0.06=0.13

Asta n. 203 (204 -20) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=-309.60 T<sub>z</sub>=822.66 M<sub>y</sub>=1099.35 T<sub>y</sub>=-111.09 M<sub>z</sub>=93.44 M<sub>x</sub>=-25.94  
Tensioni:  $\sigma_N=-5.04$   $\sigma_{m,d}=-315.43$   $\tau=4.40$   $\sigma_{max}=-320.47$  (sfrut=0.09)  
Tensioni:  $\sigma_N=-5.04$   $\sigma_{m,d}=-22.73$   $\tau=34.49$   $\tau_{max}=34.49$  (sfrut=0.02)  
Tensioni:  $\sigma_N=-5.04$   $\sigma_{m,d}=-315.43$   $\tau=4.40$   $\sigma_{TD,max}=320.56$  (sfrut=0.09)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>y</sub>=-1289.38 M<sub>x</sub>=-93.54  
V,Ed=-1289.38 Vc,Rd,Red=59479.80 V,Ed/Vc,Rd,Red=0.02

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=49.45 M<sub>x</sub>=-93.54  
V,Ed=49.45 Vc,Rd,Red=59479.80 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: N=37.41 T<sub>z</sub>=1561.81 M<sub>y</sub>=1473.31 T<sub>y</sub>=908.36 M<sub>z</sub>=-1000.79 M<sub>x</sub>=65.90  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=654.28$   $\tau=11.17$   $\sigma_{max}=654.88$  (sfrut=0.19)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=-243.49$   $\tau=68.33$   $\tau_{max}=68.33$  (sfrut=0.04)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=654.28$   $\tau=11.17$   $\sigma_{TD,max}=655.17$  (sfrut=0.19)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1473.31 Mz,Ed=-1000.79 L=0.20  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=2.55$  Ncr, $y=195939000.00$   $\lambda'_y=0.03$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=2.55$  Ncr, $z=195939000.00$   $\lambda'_z=0.03$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.11+0.07=0.18  
Verifica ZZ: 0.00+0.09+0.07=0.16

Asta n. 204 (204 -21) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

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- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=-309.60 T<sub>z</sub>=822.66 M<sub>y</sub>=1099.35 T<sub>y</sub>=111.09 M<sub>z</sub>=-93.44 M<sub>x</sub>=25.94  
Tensioni:  $\sigma_N=-5.04$   $\sigma_{m,d}=-315.43$   $\tau=4.40$   $\sigma_{max}=-320.47$  (sfrut=0.09)  
Tensioni:  $\sigma_N=-5.04$   $\sigma_{m,d}=-22.73$   $\tau=34.49$   $\tau_{max}=34.49$  (sfrut=0.02)  
Tensioni:  $\sigma_N=-5.04$   $\sigma_{m,d}=-315.43$   $\tau=4.40$   $\sigma_{TD,max}=320.56$  (sfrut=0.09)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>y</sub>=1289.38 M<sub>x</sub>=93.54  
V,Ed=1289.38 Vc,Rd,Red=59479.80 V,Ed/Vc,Rd,Red=0.02

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=49.45 M<sub>x</sub>=93.54  
V,Ed=49.45 Vc,Rd,Red=59479.80 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: N=37.41 T<sub>z</sub>=1561.81 M<sub>y</sub>=1473.30 T<sub>y</sub>=-908.36 M<sub>z</sub>=1000.79 M<sub>x</sub>=-65.90  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=654.28$   $\tau=11.17$   $\sigma_{max}=654.88$  (sfrut=0.19)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=-243.49$   $\tau=68.33$   $\tau_{max}=68.33$  (sfrut=0.04)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=654.28$   $\tau=11.17$   $\sigma_{TD,max}=655.17$  (sfrut=0.19)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1473.30 Mz,Ed=1000.79 L=0.20  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=2.55$  Ncr, $y=195939000.00$   $\lambda'_y=0.03$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=2.55$  Ncr, $z=195939000.00$   $\lambda'_z=0.03$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.11+0.07=0.18  
Verifica ZZ: 0.00+0.09+0.07=0.16

Asta n. 204 (-21 -22) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=-212.21 T<sub>x</sub>=660.91 M<sub>y</sub>=956.51 T<sub>y</sub>=81.87 M<sub>z</sub>=-85.74 M<sub>x</sub>=19.72  
Tensioni:  $\sigma_N=-3.45$   $\sigma_{m,d}=-275.62$   $\tau=3.34$   $\sigma_{max}=-279.08$  (sfrut=0.08)  
Tensioni:  $\sigma_N=-3.45$   $\sigma_{m,d}=-20.86$   $\tau=27.52$   $\tau_{max}=27.52$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-3.45$   $\sigma_{m,d}=-275.62$   $\tau=3.34$   $\sigma_{TD,max}=279.14$  (sfrut=0.08)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=1.09 - Classe 1  
Sollecitazioni: T<sub>y</sub>=974.36 M<sub>x</sub>=93.54  
V,Ed=974.36 Vc,Rd,Red=59479.80 V,Ed/Vc,Rd,Red=0.02

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=1.09 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-42.16 M<sub>x</sub>=93.54  
V,Ed=-42.16 Vc,Rd,Red=59479.80 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: N=37.41 T<sub>x</sub>=1162.71 M<sub>y</sub>=1162.20 T<sub>y</sub>=-686.42 M<sub>z</sub>=819.12 M<sub>x</sub>=-65.90  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=523.96$   $\tau=11.17$   $\sigma_{max}=524.57$  (sfrut=0.16)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=-199.29$   $\tau=53.72$   $\tau_{max}=53.72$  (sfrut=0.03)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=523.96$   $\tau=11.17$   $\sigma_{TD,max}=524.93$  (sfrut=0.16)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1162.20 Mz,Ed=819.12 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395380.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395380.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.09+0.06=0.15  
Verifica ZZ: 0.00+0.07+0.06=0.13

Asta n. 204 (-22 -23) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.34 - Classe 3  
Sollecitazioni: N=50.26 T<sub>x</sub>=48.92 M<sub>y</sub>=-313.10 T<sub>y</sub>=-79.20 M<sub>z</sub>=-146.18 M<sub>x</sub>=-34.32  
Tensioni:  $\sigma_N=0.82$   $\sigma_{m,d}=121.46$   $\tau=5.82$   $\sigma_{max}=122.27$  (sfrut=0.04)  
Tensioni:  $\sigma_N=0.82$   $\sigma_{m,d}=76.17$   $\tau=8.72$   $\tau_{max}=8.72$  (sfrut=0.00)  
Tensioni:  $\sigma_N=0.82$   $\sigma_{m,d}=121.46$   $\tau=5.82$   $\sigma_{TD,max}=122.69$  (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=282.72  
V,Ed=282.72 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
Sollecitazioni: N=37.41 T<sub>x</sub>=336.78 M<sub>y</sub>=-840.10 T<sub>y</sub>=-242.56 M<sub>z</sub>=-421.36 M<sub>x</sub>=-65.90  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=333.59$   $\tau=11.17$   $\sigma_{max}=334.20$  (sfrut=0.10)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=102.51$   $\tau=23.50$   $\tau_{max}=23.50$  (sfrut=0.01)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=333.59$   $\tau=11.17$   $\sigma_{TD,max}=334.76$  (sfrut=0.10)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=-840.10 Mz,Ed=-421.36 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395360.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395360.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.06+0.03=0.09  
Verifica ZZ: 0.00+0.05+0.03=0.08

Asta n. 204 (-23 -24) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=6.94 T<sub>x</sub>=-167.13 M<sub>y</sub>=-322.42 T<sub>y</sub>=-74.96 M<sub>z</sub>=146.49 M<sub>x</sub>=3.18  
Tensioni:  $\sigma_N=0.11$   $\sigma_{m,d}=124.00$   $\tau=0.54$   $\sigma_{max}=124.12$  (sfrut=0.04)  
Tensioni:  $\sigma_N=0.11$   $\sigma_{m,d}=-35.64$   $\tau=6.65$   $\tau_{max}=6.65$  (sfrut=0.00)  
Tensioni:  $\sigma_N=0.11$   $\sigma_{m,d}=124.00$   $\tau=0.54$   $\sigma_{TD,max}=124.12$  (sfrut=0.04)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-273.68  
V,Ed=-273.68 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: N=37.41 T<sub>x</sub>=-321.70 M<sub>y</sub>=-840.12 T<sub>y</sub>=201.30 M<sub>z</sub>=-421.37 M<sub>x</sub>=-65.90  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=333.60$   $\tau=11.17$   $\sigma_{max}=334.21$  (sfrut=0.10)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=-102.52$   $\tau=22.94$   $\tau_{max}=22.94$  (sfrut=0.01)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=333.60$   $\tau=11.17$   $\sigma_{TD,max}=334.77$  (sfrut=0.10)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=-840.12 Mz,Ed=-421.37 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395380.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395380.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.06+0.03=0.09  
Verifica ZZ: 0.00+0.05+0.03=0.08

Asta n. 204 (-24 -25) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.34 - Classe 3  
Sollecitazioni: N=-175.00 T<sub>x</sub>=-655.82 M<sub>y</sub>=917.83 T<sub>y</sub>=-80.60 M<sub>z</sub>=-81.33 M<sub>x</sub>=-8.47  
Tensioni:  $\sigma_N=-2.85$   $\sigma_{m,d}=-264.23$   $\tau=1.44$   $\sigma_{max}=-267.08$  (sfrut=0.08)  
Tensioni:  $\sigma_N=-2.85$   $\sigma_{m,d}=-19.79$   $\tau=25.43$   $\tau_{max}=25.43$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-2.85$   $\sigma_{m,d}=-264.23$   $\tau=1.44$   $\sigma_{TD,max}=267.09$  (sfrut=0.08)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-746.35  
V,Ed=-746.35 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
Sollecitazioni: N=37.41 T<sub>x</sub>=-1147.63 M<sub>y</sub>=1121.92 T<sub>y</sub>=645.17 M<sub>z</sub>=708.94 M<sub>x</sub>=-65.89  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=484.17$   $\tau=11.17$   $\sigma_{max}=484.78$  (sfrut=0.14)

Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=172.48$   $\tau=53.17$   $\tau_{max}=53.17$  (sfrut=0.03)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=484.17$   $\tau=11.17$   $\sigma_{ID,max}=485.17$  (sfrut=0.14)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1121.92 Mz,Ed=708.94 L=1.34  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=17.02$  Ncr,y=4395380.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395380.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.08+0.05=0.14  
Verifica ZZ: 0.00+0.07+0.05=0.12

Asta n. 204 (-25 205) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.46 - Classe 3  
Sollecitazioni: N=-308.52 T<sub>z</sub>=-893.98 M<sub>y</sub>=1291.70 T<sub>y</sub>=88.16 M<sub>z</sub>=123.03 M<sub>x</sub>=17.57  
Tensioni:  $\sigma_N=-5.02$   $\sigma_{m,d}=-374.13$   $\tau=2.98$   $\sigma_{max}=-379.15$  (sfrut=0.11)  
Tensioni:  $\sigma_N=-5.02$   $\sigma_{m,d}=-29.93$   $\tau=35.68$   $\tau_{max}=35.68$  (sfrut=0.02)  
Tensioni:  $\sigma_N=-5.02$   $\sigma_{m,d}=-374.13$   $\tau=2.98$   $\sigma_{ID,max}=379.18$  (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.46 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-1164.04  
V,Ed=-1164.04 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.46 - Classe 3  
Sollecitazioni: N=37.41 T<sub>z</sub>=-1834.87 M<sub>y</sub>=1956.88 T<sub>y</sub>=1089.03 M<sub>z</sub>=1208.42 M<sub>x</sub>=-65.89  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=837.07$   $\tau=11.17$   $\sigma_{max}=837.67$  (sfrut=0.25)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=294.00$   $\tau=78.32$   $\tau_{max}=78.32$  (sfrut=0.04)  
Tensioni:  $\sigma_N=0.61$   $\sigma_{m,d}=837.07$   $\tau=11.17$   $\sigma_{ID,max}=837.90$  (sfrut=0.25)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1956.88 Mz,Ed=1208.42 L=0.46  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=5.85$  Ncr,y=37254500.00  $\lambda'_y=0.08$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=5.85$  Ncr,z=37254500.00  $\lambda'_z=0.08$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.15+0.09=0.24  
Verifica ZZ: 0.00+0.12+0.09=0.21

Asta n. 205 (205 -26) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=-334.92 T<sub>z</sub>=870.16 M<sub>y</sub>=1335.56 T<sub>y</sub>=125.54 M<sub>z</sub>=-123.11 M<sub>x</sub>=19.01  
Tensioni:  $\sigma_N=-5.45$   $\sigma_{m,d}=-385.75$   $\tau=3.22$   $\sigma_{max}=-391.20$  (sfrut=0.12)  
Tensioni:  $\sigma_N=-5.45$   $\sigma_{m,d}=-29.95$   $\tau=35.05$   $\tau_{max}=35.05$  (sfrut=0.02)  
Tensioni:  $\sigma_N=-5.45$   $\sigma_{m,d}=-385.75$   $\tau=3.22$   $\sigma_{ID,max}=391.24$  (sfrut=0.12)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=1213.59  
V,Ed=1213.59 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: N=-122.31 T<sub>z</sub>=1897.42 M<sub>y</sub>=2309.74 T<sub>y</sub>=-1131.26 M<sub>z</sub>=1209.30 M<sub>x</sub>=37.00  
Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-930.61$   $\tau=6.27$   $\sigma_{max}=-932.60$  (sfrut=0.28)  
Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=294.22$   $\tau=75.71$   $\tau_{max}=75.71$  (sfrut=0.04)  
Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-930.61$   $\tau=6.27$   $\sigma_{ID,max}=932.67$  (sfrut=0.28)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: N,Ed=-122.31 My,Ed=2309.74 Mz,Ed=1209.30 L=0.88  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=11.17$  Ncr,y=10197800.00  $\lambda'_y=0.15$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=11.17$  Ncr,z=10197800.00  $\lambda'_z=0.15$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.17+0.09=0.26  
Verifica ZZ: 0.00+0.14+0.09=0.23

Asta n. 205 (-26 -27) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=-196.20 T<sub>z</sub>=611.83 M<sub>y</sub>=622.30 T<sub>y</sub>=83.93 M<sub>z</sub>=-34.81 M<sub>x</sub>=9.69  
Tensioni:  $\sigma_N=-3.19$   $\sigma_{m,d}=-173.77$   $\tau=1.64$   $\sigma_{max}=-176.97$  (sfrut=0.05)  
Tensioni:  $\sigma_N=-3.19$   $\sigma_{m,d}=-8.47$   $\tau=24.02$   $\tau_{max}=24.02$  (sfrut=0.01)  
Tensioni:  $\sigma_N=-3.19$   $\sigma_{m,d}=-173.77$   $\tau=1.64$   $\sigma_{ID,max}=176.99$  (sfrut=0.05)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=0.12 - Classe 1  
Sollecitazioni: T<sub>y</sub>=975.74 M<sub>x</sub>=-52.52  
V,Ed=975.74 Vc,Rd,Red=59693.40 V,Ed/Vc,Rd,Red=0.02

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=0.12 - Classe 1  
Sollecitazioni: T<sub>z</sub>=20.56 M<sub>x</sub>=-52.52  
V,Ed=20.56 Vc,Rd,Red=59693.40 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
Sollecitazioni: N=-122.31 T<sub>z</sub>=1100.25 M<sub>y</sub>=-854.73 T<sub>y</sub>=-687.39 M<sub>z</sub>=-700.37 M<sub>x</sub>=37.00  
Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-411.25$   $\tau=6.27$   $\sigma_{max}=-413.24$  (sfrut=0.12)  
Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-170.40$   $\tau=46.54$   $\tau_{max}=46.54$  (sfrut=0.02)  
Tensioni:  $\sigma_N=-1.99$   $\sigma_{m,d}=-411.25$   $\tau=6.27$   $\sigma_{ID,max}=413.38$  (sfrut=0.12)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: N,Ed=-122.31 My,Ed=-854.73 Mz,Ed=-700.37 L=1.34  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=17.02$  Ncr,y=4395360.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395360.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.06+0.05=0.12  
Verifica ZZ: 0.00+0.05+0.05=0.10

Asta n. 205 (-27 -28) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.34 - Classe 3

Sollecitazioni: N=-33.20 T<sub>x</sub>=75.14 M<sub>y</sub>=-522.25 T<sub>y</sub>=-85.39 M<sub>z</sub>=-332.88  
 Tensioni:  $\sigma_N$ =-0.54  $\sigma_{m,d}$ =-226.14  $\tau$ =0.00  $\sigma_{max}$ =-226.68 (sfrut=0.07)  
 Tensioni:  $\sigma_N$ =-0.54  $\sigma_{m,d}$ =-127.06  $\tau$ =3.13  $\tau_{max}$ =3.13 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =-0.54  $\sigma_{m,d}$ =-226.14  $\tau$ =0.00  $\sigma_{TD,max}$ =226.68 (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=297.01  
 V,Ed=297.01 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
 Sollecitazioni: N=-122.31 T<sub>x</sub>=358.04 M<sub>y</sub>=-1388.70 T<sub>y</sub>=-243.53 M<sub>z</sub>=-1025.55 M<sub>x</sub>=37.00  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-638.45  $\tau$ =6.27  $\sigma_{max}$ =-640.44 (sfrut=0.19)  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-249.51  $\tau$ =19.38  $\tau_{max}$ =19.38 (sfrut=0.01)  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-638.45  $\tau$ =6.27  $\sigma_{TD,max}$ =640.53 (sfrut=0.19)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=-1388.70 Mz,Ed=-1025.55 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y$ =17.02 Ncr,y=4395360.00  $\lambda'_y$ =0.22 Curva a:  $\Phi_y$ =0.53  $\chi_y$ =0.99  
 $\lambda_z$ =17.02 Ncr,z=4395360.00  $\lambda'_z$ =0.22 Curva a:  $\Phi_z$ =0.53  $\chi_z$ =0.99  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.10+0.08=0.18  
 Verifica ZZ: 0.00+0.08+0.08=0.16

Asta n. 205 (-28 -29) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-76.52 T<sub>x</sub>=-140.90 M<sub>y</sub>=-531.57 T<sub>y</sub>=-68.90 M<sub>z</sub>=332.90 M<sub>x</sub>=-31.74  
 Tensioni:  $\sigma_N$ =-1.25  $\sigma_{m,d}$ =-228.61  $\tau$ =5.38  $\sigma_{max}$ =-229.86 (sfrut=0.07)  
 Tensioni:  $\sigma_N$ =-1.25  $\sigma_{m,d}$ =80.99  $\tau$ =10.54  $\tau_{max}$ =10.54 (sfrut=0.01)  
 Tensioni:  $\sigma_N$ =-1.25  $\sigma_{m,d}$ =-228.61  $\tau$ =5.38  $\sigma_{TD,max}$ =230.04 (sfrut=0.07)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=-259.38  
 V,Ed=-259.38 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=-122.31 T<sub>x</sub>=-300.44 M<sub>y</sub>=-1388.69 T<sub>y</sub>=200.33 M<sub>z</sub>=-1025.54 M<sub>x</sub>=37.00  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-638.44  $\tau$ =6.27  $\sigma_{max}$ =-640.43 (sfrut=0.19)  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =249.51  $\tau$ =17.27  $\tau_{max}$ =17.27 (sfrut=0.01)  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-638.44  $\tau$ =6.27  $\sigma_{TD,max}$ =640.53 (sfrut=0.19)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=-1388.69 Mz,Ed=-1025.54 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y$ =17.02 Ncr,y=4395380.00  $\lambda'_y$ =0.22 Curva a:  $\Phi_y$ =0.53  $\chi_y$ =0.99  
 $\lambda_z$ =17.02 Ncr,z=4395380.00  $\lambda'_z$ =0.22 Curva a:  $\Phi_z$ =0.53  $\chi_z$ =0.99  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.10+0.08=0.18  
 Verifica ZZ: 0.00+0.08+0.08=0.16

Asta n. 205 (-29 -30) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=44.87 T<sub>x</sub>=-332.81 M<sub>y</sub>=-389.69 T<sub>y</sub>=213.31 M<sub>z</sub>=-247.42 M<sub>x</sub>=62.81  
 Tensioni:  $\sigma_N$ =0.73  $\sigma_{m,d}$ =168.49  $\tau$ =10.65  $\sigma_{max}$ =169.22 (sfrut=0.05)  
 Tensioni:  $\sigma_N$ =0.73  $\sigma_{m,d}$ =60.20  $\tau$ =22.83  $\tau_{max}$ =22.83 (sfrut=0.01)  
 Tensioni:  $\sigma_N$ =0.73  $\sigma_{m,d}$ =168.49  $\tau$ =10.65  $\sigma_{TD,max}$ =170.22 (sfrut=0.05)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=1.34 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=-732.05  
 V,Ed=-732.05 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=-122.31 T<sub>x</sub>=-1042.65 M<sub>y</sub>=-931.58 T<sub>y</sub>=644.19 M<sub>z</sub>=-758.02 M<sub>x</sub>=37.01  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-446.81  $\tau$ =6.27  $\sigma_{max}$ =-448.80 (sfrut=0.13)  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =184.42  $\tau$ =44.43  $\tau_{max}$ =44.43 (sfrut=0.02)  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-446.81  $\tau$ =6.27  $\sigma_{TD,max}$ =448.94 (sfrut=0.13)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=-931.58 Mz,Ed=-758.02 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y$ =17.02 Ncr,y=4395380.00  $\lambda'_y$ =0.22 Curva a:  $\Phi_y$ =0.53  $\chi_y$ =0.99  
 $\lambda_z$ =17.02 Ncr,z=4395380.00  $\lambda'_z$ =0.22 Curva a:  $\Phi_z$ =0.53  $\chi_z$ =0.99  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.07+0.06=0.13  
 Verifica ZZ: 0.00+0.06+0.06=0.11

Asta n. 205 (-30 -31) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.88 - Classe 3  
 Sollecitazioni: N=-450.80 T<sub>x</sub>=-847.63 M<sub>y</sub>=1224.88 T<sub>y</sub>=-120.61 M<sub>z</sub>=-106.11 M<sub>x</sub>=-28.64  
 Tensioni:  $\sigma_N$ =-7.34  $\sigma_{m,d}$ =-351.98  $\tau$ =4.86  $\sigma_{max}$ =-359.32 (sfrut=0.11)  
 Tensioni:  $\sigma_N$ =-7.34  $\sigma_{m,d}$ =-25.82  $\tau$ =35.86  $\tau_{max}$ =35.86 (sfrut=0.02)  
 Tensioni:  $\sigma_N$ =-7.34  $\sigma_{m,d}$ =-351.98  $\tau$ =4.86  $\sigma_{TD,max}$ =359.42 (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.88 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=-1176.29  
 V,Ed=-1176.29 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.88 - Classe 3  
 Sollecitazioni: N=-122.31 T<sub>x</sub>=-1840.16 M<sub>y</sub>=2115.20 T<sub>y</sub>=1088.06 M<sub>z</sub>=1061.84 M<sub>x</sub>=37.01  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-840.17  $\tau$ =6.27  $\sigma_{max}$ =-842.16 (sfrut=0.25)  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-258.34  $\tau$ =73.62  $\tau_{max}$ =73.62 (sfrut=0.04)  
 Tensioni:  $\sigma_N$ =-1.99  $\sigma_{m,d}$ =-840.17  $\tau$ =6.27  $\sigma_{TD,max}$ =842.23 (sfrut=0.25)

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=2115.20 Mz,Ed=1061.84 L=0.88  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95

$\lambda_y=11.24$  Ncr, $y=10074800.00$   $\lambda'_y=0.15$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=11.24$  Ncr, $z=10074800.00$   $\lambda'_z=0.15$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.16+0.08=0.24  
 Verifica ZZ: 0.00+0.13+0.08=0.21

Asta n. 206 (-31 -32) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-202.92 T<sub>z</sub>=913.19 M<sub>y</sub>=1271.23 T<sub>y</sub>=-62.72 M<sub>z</sub>=105.97 M<sub>x</sub>=-15.09  
 Tensioni:  $\sigma_N=-3.30$   $\sigma_{m,d}=-364.20$   $\tau=2.56$   $\sigma_{max}=-367.50$  (sfrut=0.11)  
 Tensioni:  $\sigma_N=-3.30$   $\sigma_{m,d}=-25.78$   $\tau=35.96$   $\tau_{max}=35.96$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=-3.30$   $\sigma_{m,d}=-364.20$   $\tau=2.56$   $\sigma_{TD,max}=367.53$  (sfrut=0.11)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
 Sollecitazioni: T<sub>z</sub>=988.57  
 V,Ed=988.57 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.02

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=129.33 T<sub>z</sub>=1567.87 M<sub>y</sub>=1559.12 T<sub>y</sub>=-950.22 M<sub>z</sub>=1060.45 M<sub>x</sub>=126.11  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=692.75$   $\tau=21.38$   $\sigma_{max}=694.85$  (sfrut=0.21)  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=258.00$   $\tau=78.76$   $\tau_{max}=78.76$  (sfrut=0.04)  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=692.75$   $\tau=21.38$   $\sigma_{TD,max}=695.84$  (sfrut=0.21)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: M<sub>y</sub>,Ed=1559.12 M<sub>z</sub>,Ed=1060.45 L=0.45

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=5.78$  Ncr, $y=38136200.00$   $\lambda'_y=0.08$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=5.78$  Ncr, $z=38136200.00$   $\lambda'_z=0.08$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.12+0.08=0.19  
 Verifica ZZ: 0.00+0.09+0.08=0.17

Asta n. 206 (-32 -33) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=-69.46 T<sub>z</sub>=675.28 M<sub>y</sub>=893.31 T<sub>y</sub>=70.34 M<sub>z</sub>=-69.61 M<sub>x</sub>=-7.91  
 Tensioni:  $\sigma_N=-1.13$   $\sigma_{m,d}=-254.65$   $\tau=1.34$   $\sigma_{max}=-255.78$  (sfrut=0.08)  
 Tensioni:  $\sigma_N=-1.13$   $\sigma_{m,d}=16.93$   $\tau=26.04$   $\tau_{max}=26.04$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=-1.13$   $\sigma_{m,d}=-254.65$   $\tau=1.34$   $\sigma_{TD,max}=255.79$  (sfrut=0.08)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 21 SLU Xl=0.97 - Classe 1  
 Sollecitazioni: T<sub>y</sub>=718.75 M<sub>x</sub>=-179.02  
 V,Ed=718.75 Vc,Rd,Red=59034.60 V,Ed/Vc,Rd,Red=0.01

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 21 SLU Xl=0.97 - Classe 1  
 Sollecitazioni: T<sub>z</sub>=-44.09 M<sub>x</sub>=-179.02  
 V,Ed=-44.09 Vc,Rd,Red=59034.60 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
 Sollecitazioni: N=129.33 T<sub>z</sub>=880.97 M<sub>y</sub>=854.85 T<sub>y</sub>=-506.36 M<sub>z</sub>=629.72 M<sub>x</sub>=126.12  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=392.59$   $\tau=21.38$   $\sigma_{max}=394.70$  (sfrut=0.12)  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=153.21$   $\tau=53.62$   $\tau_{max}=53.62$  (sfrut=0.03)  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=392.59$   $\tau=21.38$   $\sigma_{TD,max}=396.43$  (sfrut=0.12)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: M<sub>y</sub>,Ed=854.85 M<sub>z</sub>,Ed=629.72 L=1.34

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=17.02$  Ncr, $y=4395360.00$   $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr, $z=4395360.00$   $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
 Verifica YY: 0.00+0.06+0.05=0.11  
 Verifica ZZ: 0.00+0.05+0.05=0.10

Asta n. 206 (-33 -34) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=1.34 - Classe 3  
 Sollecitazioni: N=74.96 T<sub>z</sub>=330.43 M<sub>y</sub>=-418.62 T<sub>y</sub>=27.02 M<sub>z</sub>=38.65 M<sub>x</sub>=-17.23  
 Tensioni:  $\sigma_N=1.22$   $\sigma_{m,d}=120.92$   $\tau=2.92$   $\sigma_{max}=122.14$  (sfrut=0.04)  
 Tensioni:  $\sigma_N=1.22$   $\sigma_{m,d}=-9.40$   $\tau=15.01$   $\tau_{max}=15.01$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=1.22$   $\sigma_{m,d}=120.92$   $\tau=2.92$   $\sigma_{TD,max}=122.25$  (sfrut=0.04)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 15 SND Xl=0.00 - Classe 1  
 Sollecitazioni: T<sub>y</sub>=17.78 M<sub>x</sub>=-36.71  
 V,Ed=17.78 Vc,Rd,Red=59775.80 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 15 SND Xl=0.00 - Classe 1  
 Sollecitazioni: T<sub>z</sub>=162.82 M<sub>x</sub>=-36.71  
 V,Ed=162.82 Vc,Rd,Red=59775.80 V,Ed/Vc,Rd,Red=0.00

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
 Sollecitazioni: N=129.33 T<sub>z</sub>=55.03 M<sub>y</sub>=-395.08 T<sub>y</sub>=-62.49 M<sub>z</sub>=-129.92 M<sub>x</sub>=126.12  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=138.84$   $\tau=21.38$   $\sigma_{max}=140.94$  (sfrut=0.04)  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=-96.12$   $\tau=23.67$   $\tau_{max}=23.67$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=138.84$   $\tau=21.38$   $\sigma_{TD,max}=145.73$  (sfrut=0.04)

Asta n. 206 (-34 -35) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=1.34 - Classe 3  
 Sollecitazioni: N=-99.91 T<sub>z</sub>=-612.90 M<sub>y</sub>=891.36 T<sub>y</sub>=-63.97 M<sub>z</sub>=-94.96 M<sub>x</sub>=-12.88  
 Tensioni:  $\sigma_N=-1.63$   $\sigma_{m,d}=-260.83$   $\tau=2.18$   $\sigma_{max}=-262.46$  (sfrut=0.08)  
 Tensioni:  $\sigma_N=-1.63$   $\sigma_{m,d}=-23.10$   $\tau=24.60$   $\tau_{max}=24.60$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=-1.63$   $\sigma_{m,d}=-260.83$   $\tau=2.18$   $\sigma_{TD,max}=262.49$  (sfrut=0.08)

- Verifica a taglio e torsione Dir. Y [4.2.25] - CC 1 SND Xl=1.09 - Classe 1  
 Sollecitazioni: T<sub>y</sub>=16.31 M<sub>x</sub>=26.56  
 V,Ed=16.31 Vc,Rd,Red=59828.70 V,Ed/Vc,Rd,Red=0.00

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 1 SND Xl=1.09 - Classe 1  
 Sollecitazioni: T<sub>z</sub>=-601.19 M<sub>x</sub>=26.56

V,Ed=-601.19 Vc,Rd,Red=59828.70 V,Ed/Vc,Rd,Red=0.01

- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=1.34 - Classe 3  
Sollecitazioni: N=129.33 T<sub>z</sub>=-687.17 M<sub>y</sub>=466.62 T<sub>y</sub>=381.37 M<sub>z</sub>=379.34 M<sub>x</sub>=126.12  
Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=223.72$   $\tau=21.38$   $\sigma_{max}=225.82$  (sfrut=0.07)  
Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=-92.29$   $\tau=46.52$   $\tau_{max}=46.52$  (sfrut=0.02)  
Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=223.72$   $\tau=21.38$   $\sigma_{ID,max}=228.84$  (sfrut=0.07)
- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 3 SND - Classe 3  
Sollecitazioni: N,Ed=-99.91 My,Ed=891.36 Mz,Ed=-94.96 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395360.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395360.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.07+0.01=0.07  
Verifica ZZ: 0.00+0.05+0.01=0.06
- Asta n. 206 (-35 -36) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 3 SND Xl=0.54 - Classe 3  
Sollecitazioni: N=-234.46 T<sub>z</sub>=-855.02 M<sub>y</sub>=1315.50 T<sub>y</sub>=-104.33 M<sub>z</sub>=-129.61 M<sub>x</sub>=-22.20  
Tensioni:  $\sigma_N=-3.82$   $\sigma_{m,d}=-382.16$   $\tau=3.76$   $\sigma_{max}=-385.98$  (sfrut=0.11)  
Tensioni:  $\sigma_N=-3.82$   $\sigma_{m,d}=-31.53$   $\tau=35.04$   $\tau_{max}=35.04$  (sfrut=0.02)  
Tensioni:  $\sigma_N=-3.82$   $\sigma_{m,d}=-382.16$   $\tau=3.76$   $\sigma_{ID,max}=386.03$  (sfrut=0.11)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.54 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-880.69  
V,Ed=-880.69 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.54 - Classe 3  
Sollecitazioni: N=129.33 T<sub>z</sub>=-1379.55 M<sub>y</sub>=1203.31 T<sub>y</sub>=825.23 M<sub>z</sub>=825.51 M<sub>x</sub>=126.12  
Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=536.52$   $\tau=21.38$   $\sigma_{max}=538.63$  (sfrut=0.16)  
Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=-200.84$   $\tau=71.86$   $\tau_{max}=71.86$  (sfrut=0.04)  
Tensioni:  $\sigma_N=2.11$   $\sigma_{m,d}=536.52$   $\tau=21.38$   $\sigma_{ID,max}=539.90$  (sfrut=0.16)
- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1203.31 Mz,Ed=825.51 L=0.54  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=6.89$  Ncr,y=26811000.00  $\lambda'_y=0.09$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=6.89$  Ncr,z=26811000.00  $\lambda'_z=0.09$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.09+0.06=0.15  
Verifica ZZ: 0.00+0.07+0.06=0.13
- Asta n. 206 (-36 -37) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=69.78 T<sub>z</sub>=470.88 M<sub>y</sub>=620.63 T<sub>y</sub>=232.61 M<sub>z</sub>=-322.47 M<sub>x</sub>=51.80  
Tensioni:  $\sigma_N=1.14$   $\sigma_{m,d}=249.40$   $\tau=8.78$   $\sigma_{max}=250.54$  (sfrut=0.07)  
Tensioni:  $\sigma_N=1.14$   $\sigma_{m,d}=-78.45$   $\tau=26.01$   $\tau_{max}=26.01$  (sfrut=0.01)  
Tensioni:  $\sigma_N=1.14$   $\sigma_{m,d}=249.40$   $\tau=8.78$   $\sigma_{ID,max}=251.00$  (sfrut=0.07)
- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=774.27  
V,Ed=774.27 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: T<sub>z</sub>=1178.58 M<sub>y</sub>=1488.88 T<sub>y</sub>=-665.79 M<sub>z</sub>=825.45  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-612.03$   $\tau=0.00$   $\sigma_{max}=-612.03$  (sfrut=0.18)  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=200.83$   $\tau=43.13$   $\tau_{max}=43.13$  (sfrut=0.02)  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-612.03$   $\tau=0.00$   $\sigma_{ID,max}=612.03$  (sfrut=0.18)
- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=1488.88 Mz,Ed=825.45 L=0.79  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=10.13$  Ncr,y=12411000.00  $\lambda'_y=0.13$  Curva a:  $\Phi_y=0.00$   $\chi_y=1.00$   
 $\lambda_z=10.13$  Ncr,z=12411000.00  $\lambda'_z=0.13$  Curva a:  $\Phi_z=0.00$   $\chi_z=1.00$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.11+0.06=0.17  
Verifica ZZ: 0.00+0.09+0.06=0.15
- Asta n. 206 (-37 -38) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2
- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=28.47 T<sub>z</sub>=216.51 M<sub>y</sub>=252.33 T<sub>y</sub>=94.91 M<sub>z</sub>=-131.09 M<sub>x</sub>=20.73  
Tensioni:  $\sigma_N=0.46$   $\sigma_{m,d}=101.39$   $\tau=3.51$   $\sigma_{max}=101.86$  (sfrut=0.03)  
Tensioni:  $\sigma_N=0.46$   $\sigma_{m,d}=-31.89$   $\tau=11.44$   $\tau_{max}=11.44$  (sfrut=0.01)  
Tensioni:  $\sigma_N=0.46$   $\sigma_{m,d}=101.39$   $\tau=3.51$   $\sigma_{ID,max}=102.04$  (sfrut=0.03)
- Verifica a taglio Dir. Y [4.2.16] - CC 28 SLU Xl=1.34  
Sollecitazioni: T<sub>y</sub>=-221.93  
V,Ed=-221.93 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.00
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.34  
Sollecitazioni: T<sub>z</sub>=386.55  
V,Ed=386.55 Vc,Rd=59967.00 V,Ed/Vc,Rd=0.01
- Verifica in termini tensionali [4.2.4] - CC 28 SLU Xl=0.00 - Classe 3  
Sollecitazioni: T<sub>z</sub>=470.27 M<sub>y</sub>=572.06 T<sub>y</sub>=-221.93 M<sub>z</sub>=296.35  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-229.65$   $\tau=0.00$   $\sigma_{max}=-229.65$  (sfrut=0.07)  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=72.10$   $\tau=17.21$   $\tau_{max}=17.21$  (sfrut=0.01)  
Tensioni:  $\sigma_N=0.00$   $\sigma_{m,d}=-229.65$   $\tau=0.00$   $\sigma_{ID,max}=229.65$  (sfrut=0.07)
- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
Sollecitazioni: My,Ed=572.06 Mz,Ed=296.35 L=1.34  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=17.02$  Ncr,y=4395390.00  $\lambda'_y=0.22$  Curva a:  $\Phi_y=0.53$   $\chi_y=0.99$   
 $\lambda_z=17.02$  Ncr,z=4395390.00  $\lambda'_z=0.22$  Curva a:  $\Phi_z=0.53$   $\chi_z=0.99$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95  
Verifica YY: 0.00+0.04+0.02=0.06

Verifica ZZ: 0.00+0.03+0.02=0.06

Asta n. 301 (-3 -60) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=59.85 T<sub>z</sub>=47.12 M<sub>y</sub>=43.09 T<sub>y</sub>=-14.22 M<sub>z</sub>=21.33

Tensioni: σ<sub>N</sub>=1.60 σ<sub>m,d</sub>=46.78 τ=0.00 σ<sub>max</sub>=48.38 (sfrut=0.01)

Tensioni: σ<sub>N</sub>=1.60 σ<sub>m,d</sub>=15.23 τ=2.42 τ<sub>max</sub>=2.42 (sfrut=0.00)

Tensioni: σ<sub>N</sub>=1.60 σ<sub>m,d</sub>=46.78 τ=0.00 σ<sub>TD,max</sub>=48.38 (sfrut=0.01)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>z</sub>=201.76

V,Ed=201.76 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=94.68 T<sub>z</sub>=201.76 M<sub>y</sub>=198.62

My,Ed=198.62 My,V,c,Rd=6269.10

N,Ed=94.68 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.03

Asta n. 301 (-59 -3) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-56.95 T<sub>z</sub>=-51.26 M<sub>y</sub>=49.31 T<sub>y</sub>=31.09 M<sub>z</sub>=46.64

Tensioni: σ<sub>N</sub>=-1.52 σ<sub>m,d</sub>=-72.43 τ=0.00 σ<sub>max</sub>=-73.95 (sfrut=0.02)

Tensioni: σ<sub>N</sub>=-1.52 σ<sub>m,d</sub>=33.30 τ=2.64 τ<sub>max</sub>=2.64 (sfrut=0.00)

Tensioni: σ<sub>N</sub>=-1.52 σ<sub>m,d</sub>=-72.43 τ=0.00 σ<sub>TD,max</sub>=73.95 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>z</sub>=-201.76

V,Ed=-201.76 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-94.68 T<sub>z</sub>=-201.76 M<sub>y</sub>=198.62

My,Ed=198.62 My,V,c,Rd=6269.10

N,Ed=-94.68 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-94.68 My,Ed=198.62 L=1.50

α<sub>my</sub>, α<sub>mz</sub>, α<sub>LT</sub>=0.95, 0.95, 0.95

λ<sub>1</sub>=27.33 Ncr,y=1039280.00 λ<sub>1,y</sub>=0.36 Curva a: Φ<sub>y</sub>=0.58 χ<sub>y</sub>=0.96

λ<sub>2</sub>=37.85 Ncr,z=541779.00 λ<sub>2,z</sub>=0.50 Curva a: Φ<sub>z</sub>=0.65 χ<sub>z</sub>=0.93

K<sub>yy</sub>, K<sub>yz</sub>, K<sub>zy</sub>, K<sub>zz</sub>=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.03=0.03

Verifica ZZ: 0.00=0.00

Asta n. 302 (-4 -47) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>z</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97

Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=70.12 τ=0.00 σ<sub>max</sub>=72.39 (sfrut=0.02)

Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=22.83 τ=3.45 τ<sub>max</sub>=3.45 (sfrut=0.00)

Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=70.12 τ=0.00 σ<sub>TD,max</sub>=72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>z</sub>=370.64

V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>z</sub>=370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 302 (-46 -4) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91

Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=-108.57 τ=0.00 σ<sub>max</sub>=-110.72 (sfrut=0.03)

Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=49.92 τ=3.78 τ<sub>max</sub>=3.78 (sfrut=0.00)

Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=-108.57 τ=0.00 σ<sub>TD,max</sub>=110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>z</sub>=-370.64

V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>z</sub>=-370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50

α<sub>my</sub>, α<sub>mz</sub>, α<sub>LT</sub>=0.95, 0.95, 0.95

λ<sub>1</sub>=27.33 Ncr,y=1039280.00 λ<sub>1,y</sub>=0.36 Curva a: Φ<sub>y</sub>=0.58 χ<sub>y</sub>=0.96

λ<sub>2</sub>=37.85 Ncr,z=541779.00 λ<sub>2,z</sub>=0.50 Curva a: Φ<sub>z</sub>=0.65 χ<sub>z</sub>=0.93

K<sub>yy</sub>, K<sub>yz</sub>, K<sub>zy</sub>, K<sub>zz</sub>=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

Asta n. 303 (-6 -48) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>z</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97

Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=70.12 τ=0.00 σ<sub>max</sub>=72.39 (sfrut=0.02)

Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=22.83 τ=3.45 τ<sub>max</sub>=3.45 (sfrut=0.00)

Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=70.12 τ=0.00 σ<sub>TD,max</sub>=72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>z</sub>=370.64

V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1



Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 303 (-49 -6) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{max}$ =-110.72 (sfrut=0.03)

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =49.92  $\tau$ =3.78  $\tau_{max}$ =3.78 (sfrut=0.00)

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{TD,max}$ =110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>x</sub>=-370.64

V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=-142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50

$\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95

$\lambda_y$ =27.33 Ncr,y=1039280.00  $\lambda'_y$ =0.36 Curva a:  $\Phi_y$ =0.58  $\chi_y$ =0.96

$\lambda_z$ =37.85 Ncr,z=541779.00  $\lambda'_z$ =0.50 Curva a:  $\Phi_z$ =0.65  $\chi_z$ =0.93

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

Asta n. 304 (-7 -96) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97

Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{max}$ =72.39 (sfrut=0.02)

Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =22.83  $\tau$ =3.45  $\tau_{max}$ =3.45 (sfrut=0.00)

Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{TD,max}$ =72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>x</sub>=370.64

V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 304 (-95 -7) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{max}$ =-110.72 (sfrut=0.03)

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =49.92  $\tau$ =3.78  $\tau_{max}$ =3.78 (sfrut=0.00)

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{TD,max}$ =110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>x</sub>=-370.64

V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=-142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50

$\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95

$\lambda_y$ =27.33 Ncr,y=1039280.00  $\lambda'_y$ =0.36 Curva a:  $\Phi_y$ =0.58  $\chi_y$ =0.96

$\lambda_z$ =37.85 Ncr,z=541779.00  $\lambda'_z$ =0.50 Curva a:  $\Phi_z$ =0.65  $\chi_z$ =0.93

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

Asta n. 305 (-8 -66) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97

Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{max}$ =72.39 (sfrut=0.02)

Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =22.83  $\tau$ =3.45  $\tau_{max}$ =3.45 (sfrut=0.00)

Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{TD,max}$ =72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>x</sub>=370.64

V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 305 (-67 -8) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{max}$ =-110.72 (sfrut=0.03)

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =49.92  $\tau$ =3.78  $\tau_{max}$ =3.78 (sfrut=0.00)

Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{TD,max}$ =110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>x</sub>=-370.64

V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1  
Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
α<sub>my</sub>, α<sub>mz</sub>, α<sub>LT</sub>=0.95, 0.95, 0.95  
λ<sub>y</sub>=27.33 Ncr,y=1039280.00 λ<sub>y</sub>'=0.36 Curva a: Φ<sub>y</sub>=0.58 χ<sub>y</sub>=0.96  
λ<sub>z</sub>=37.85 Ncr,z=541779.00 λ<sub>z</sub>'=0.50 Curva a: Φ<sub>z</sub>=0.65 χ<sub>z</sub>=0.93  
K<sub>yy</sub>, K<sub>yz</sub>, K<sub>zy</sub>, K<sub>zz</sub>=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.06=0.06  
Verifica ZZ: 0.00=0.00

Asta n. 306 (-9 -69) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3  
Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=70.12 τ=0.00 σ<sub>max</sub>=72.39 (sfrut=0.02)  
Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=22.83 τ=3.45 τ<sub>max</sub>=3.45 (sfrut=0.00)  
Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=70.12 τ=0.00 σ<sub>TD,max</sub>=72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1  
Sollecitazioni: T<sub>x</sub>=370.64  
V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1  
Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 306 (-68 -9) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3  
Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=-108.57 τ=0.00 σ<sub>max</sub>=-110.72 (sfrut=0.03)  
Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=49.92 τ=3.78 τ<sub>max</sub>=3.78 (sfrut=0.00)  
Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=-108.57 τ=0.00 σ<sub>TD,max</sub>=110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1  
Sollecitazioni: T<sub>x</sub>=-370.64  
V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1  
Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
α<sub>my</sub>, α<sub>mz</sub>, α<sub>LT</sub>=0.95, 0.95, 0.95  
λ<sub>y</sub>=27.33 Ncr,y=1039280.00 λ<sub>y</sub>'=0.36 Curva a: Φ<sub>y</sub>=0.58 χ<sub>y</sub>=0.96  
λ<sub>z</sub>=37.85 Ncr,z=541779.00 λ<sub>z</sub>'=0.50 Curva a: Φ<sub>z</sub>=0.65 χ<sub>z</sub>=0.93  
K<sub>yy</sub>, K<sub>yz</sub>, K<sub>zy</sub>, K<sub>zz</sub>=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.06=0.06  
Verifica ZZ: 0.00=0.00

Asta n. 307 (-11 -70) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3  
Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=70.12 τ=0.00 σ<sub>max</sub>=72.39 (sfrut=0.02)  
Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=22.83 τ=3.45 τ<sub>max</sub>=3.45 (sfrut=0.00)  
Tensioni: σ<sub>N</sub>=2.27 σ<sub>m,d</sub>=70.12 τ=0.00 σ<sub>TD,max</sub>=72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1  
Sollecitazioni: T<sub>x</sub>=370.64  
V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1  
Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 307 (-71 -11) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3  
Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=-108.57 τ=0.00 σ<sub>max</sub>=-110.72 (sfrut=0.03)  
Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=49.92 τ=3.78 τ<sub>max</sub>=3.78 (sfrut=0.00)  
Tensioni: σ<sub>N</sub>=-2.15 σ<sub>m,d</sub>=-108.57 τ=0.00 σ<sub>TD,max</sub>=110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1  
Sollecitazioni: T<sub>x</sub>=-370.64  
V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1  
Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
α<sub>my</sub>, α<sub>mz</sub>, α<sub>LT</sub>=0.95, 0.95, 0.95  
λ<sub>y</sub>=27.33 Ncr,y=1039280.00 λ<sub>y</sub>'=0.36 Curva a: Φ<sub>y</sub>=0.58 χ<sub>y</sub>=0.96  
λ<sub>z</sub>=37.85 Ncr,z=541779.00 λ<sub>z</sub>'=0.50 Curva a: Φ<sub>z</sub>=0.65 χ<sub>z</sub>=0.93  
K<sub>yy</sub>, K<sub>yz</sub>, K<sub>zy</sub>, K<sub>zz</sub>=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.06=0.06  
Verifica ZZ: 0.00=0.00

Asta n. 308 (-12 -72) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>s</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: T<sub>s</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>s</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 308 (-73 -12) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>s</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1

Sollecitazioni: T<sub>s</sub>=-370.64  
 V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>s</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_1=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_2=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 309 (-13 -74) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>s</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: T<sub>s</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>s</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 309 (-75 -13) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>s</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1

Sollecitazioni: T<sub>s</sub>=-370.64  
 V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>s</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_1=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_2=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 310 (-14 -90) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>s</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: T<sub>s</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>s</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 310 (-91 -14) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{ID,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>z</sub>=-370.64

V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>z</sub>=-370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50

$\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95

$\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$

$\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

Asta n. 311 (-15 -92) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>z</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{ID,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>z</sub>=370.64

V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>z</sub>=370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 311 (-93 -15) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{ID,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>z</sub>=-370.64

V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>z</sub>=-370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50

$\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95

$\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$

$\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

Asta n. 312 (-16 -98) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>z</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{ID,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>z</sub>=370.64

V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>z</sub>=370.64 M<sub>y</sub>=372.58

My,Ed=372.58 My,V,c,Rd=6269.10

N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 312 (-94 -16) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{ID,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>z</sub>=-370.64

V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_1$ =27.33 Ncr,y=1039280.00  $\lambda'_1$ =0.36 Curva a:  $\Phi_y$ =0.58  $\chi_y$ =0.96  
 $\lambda_2$ =37.85 Ncr,z=541779.00  $\lambda'_2$ =0.50 Curva a:  $\Phi_z$ =0.65  $\chi_z$ =0.93  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 313 (-17 -97) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{max}$ =72.39 (sfrut=0.02)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =22.83  $\tau$ =3.45  $\tau_{max}$ =3.45 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{TD,max}$ =72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>x</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 313 (-42 -17) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{max}$ =-110.72 (sfrut=0.03)  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =49.92  $\tau$ =3.78  $\tau_{max}$ =3.78 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{TD,max}$ =110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>x</sub>=-370.64  
 V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_1$ =27.33 Ncr,y=1039280.00  $\lambda'_1$ =0.36 Curva a:  $\Phi_y$ =0.58  $\chi_y$ =0.96  
 $\lambda_2$ =37.85 Ncr,z=541779.00  $\lambda'_2$ =0.50 Curva a:  $\Phi_z$ =0.65  $\chi_z$ =0.93  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 314 (-18 -43) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{max}$ =72.39 (sfrut=0.02)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =22.83  $\tau$ =3.45  $\tau_{max}$ =3.45 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{TD,max}$ =72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>x</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 314 (-44 -18) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{max}$ =-110.72 (sfrut=0.03)  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =49.92  $\tau$ =3.78  $\tau_{max}$ =3.78 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{TD,max}$ =110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>x</sub>=-370.64  
 V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_1$ =27.33 Ncr,y=1039280.00  $\lambda'_1$ =0.36 Curva a:  $\Phi_y$ =0.58  $\chi_y$ =0.96  
 $\lambda_2$ =37.85 Ncr,z=541779.00  $\lambda'_2$ =0.50 Curva a:  $\Phi_z$ =0.65  $\chi_z$ =0.93  
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 315 (-19 -45) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=370.64  
V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06
- Asta n. 315 (-58 -19) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3  
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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3  
Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-370.64  
V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=-142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.06=0.06  
Verifica ZZ: 0.00=0.00
- Asta n. 316 (-20 -63) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3  
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- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=59.85 T<sub>x</sub>=47.12 M<sub>y</sub>=43.09 T<sub>y</sub>=-14.22 M<sub>z</sub>=21.33  
Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=46.78$   $\tau=0.00$   $\sigma_{max}=48.38$  (sfrut=0.01)  
Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=15.23$   $\tau=2.42$   $\tau_{max}=2.42$  (sfrut=0.00)  
Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=46.78$   $\tau=0.00$   $\sigma_{TD,max}=48.38$  (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=201.76  
V,Ed=201.76 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.00
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: N=94.68 T<sub>x</sub>=201.76 M<sub>y</sub>=198.62  
My,Ed=198.62 My,V,c,Rd=6269.10  
N,Ed=94.68 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.03
- Asta n. 316 (-65 -20) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3  
-----
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3  
Sollecitazioni: N=-56.95 T<sub>x</sub>=-51.26 M<sub>y</sub>=49.31 T<sub>y</sub>=31.09 M<sub>z</sub>=46.64  
Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=-72.43$   $\tau=0.00$   $\sigma_{max}=-73.95$  (sfrut=0.02)  
Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=33.30$   $\tau=2.64$   $\tau_{max}=2.64$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=-72.43$   $\tau=0.00$   $\sigma_{TD,max}=73.95$  (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-201.76  
V,Ed=-201.76 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.00
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: N=-94.68 T<sub>x</sub>=-201.76 M<sub>y</sub>=198.62  
My,Ed=198.62 My,V,c,Rd=6269.10  
N,Ed=-94.68 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.03
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni: N,Ed=-94.68 My,Ed=198.62 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.03=0.03  
Verifica ZZ: 0.00=0.00
- Asta n. 317 (-21 -51) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3  
-----
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=59.85 T<sub>x</sub>=47.12 M<sub>y</sub>=43.09 T<sub>y</sub>=-14.22 M<sub>z</sub>=21.33  
Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=46.78$   $\tau=0.00$   $\sigma_{max}=48.38$  (sfrut=0.01)  
Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=15.23$   $\tau=2.42$   $\tau_{max}=2.42$  (sfrut=0.00)  
Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=46.78$   $\tau=0.00$   $\sigma_{TD,max}=48.38$  (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=201.76  
V,Ed=201.76 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.00
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: N=94.68 T<sub>x</sub>=201.76 M<sub>y</sub>=198.62  
My,Ed=198.62 My,V,c,Rd=6269.10  
N,Ed=94.68 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.03

Asta n. 317 (-50 -21) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-56.95 T<sub>z</sub>=-51.26 M<sub>y</sub>=49.31 T<sub>y</sub>=31.09 M<sub>z</sub>=46.64  
Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=-72.43$   $\tau=0.00$   $\sigma_{max}=-73.95$  (sfrut=0.02)

Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=33.30$   $\tau=2.64$   $\tau_{max}=2.64$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=-72.43$   $\tau=0.00$   $\sigma_{TD,max}=73.95$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>z</sub>=-201.76  
V,Ed=-201.76 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.00

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-94.68 T<sub>z</sub>=-201.76 M<sub>y</sub>=198.62  
My,Ed=198.62 My,V,c,Rd=6269.10  
N,Ed=-94.68 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-94.68 My,Ed=198.62 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.03=0.03  
Verifica ZZ: 0.00=0.00

Asta n. 318 (-22 -53) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>z</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>z</sub>=370.64  
V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>z</sub>=370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 318 (-52 -22) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>z</sub>=-370.64  
V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>z</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=-142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.06=0.06  
Verifica ZZ: 0.00=0.00

Asta n. 319 (-23 -55) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3

Sollecitazioni: N=84.82 T<sub>z</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: T<sub>z</sub>=370.64  
V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=142.40 T<sub>z</sub>=370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 319 (-54 -23) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3

Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: T<sub>z</sub>=-370.64  
V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1

Sollecitazioni: N=-142.40 T<sub>z</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10



N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 320 (-24 -57) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1  
 Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 320 (-56 -24) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3  
 Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=-370.64  
 V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1  
 Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 322 (-25 -41) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1  
 Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 322 (-64 -25) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3  
 Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=-370.64  
 V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1  
 Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 323 (-26 -77) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
 Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97



Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=0.00$  - Classe 1  
 Sollecitazioni:  $T_x=370.64$   
 $V,Ed=370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=0.00$  - Classe 1  
 Sollecitazioni:  $N=142.40$   $T_x=370.64$   $M_y=372.58$   
 $My,Ed=372.58$   $My,V,c,Rd=6269.10$   
 $N,Ed=142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $My,Ed/MNy,c,Rd=0.06$

Asta n. 323 (-76 -26) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=1.50$  - Classe 3  
 Sollecitazioni:  $N=-80.47$   $T_x=-73.41$   $M_y=73.92$   $T_y=46.60$   $M_z=69.91$   
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=1.50$  - Classe 1  
 Sollecitazioni:  $T_x=-370.64$   
 $V,Ed=-370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=1.50$  - Classe 1  
 Sollecitazioni:  $N=-142.40$   $T_x=-370.64$   $M_y=372.58$   
 $My,Ed=372.58$   $My,V,c,Rd=6269.10$   
 $N,Ed=-142.40$   $Nc,Rd=-126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $My,Ed/MNy,c,Rd=0.06$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni:  $N,Ed=-142.40$   $My,Ed=372.58$   $L=1.50$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=27.33$   $Ncr,y=1039280.00$   $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$   $Ncr,z=541779.00$   $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$   
 Verifica YY:  $0.00+0.06=0.06$   
 Verifica ZZ:  $0.00=0.00$

Asta n. 324 (-27 -79) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=0.00$  - Classe 3  
 Sollecitazioni:  $N=84.82$   $T_x=67.20$   $M_y=64.60$   $T_y=-21.32$   $M_z=31.97$   
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=0.00$  - Classe 1  
 Sollecitazioni:  $T_x=370.64$   
 $V,Ed=370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=0.00$  - Classe 1  
 Sollecitazioni:  $N=142.40$   $T_x=370.64$   $M_y=372.58$   
 $My,Ed=372.58$   $My,V,c,Rd=6269.10$   
 $N,Ed=142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $My,Ed/MNy,c,Rd=0.06$

Asta n. 324 (-78 -27) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=1.50$  - Classe 3  
 Sollecitazioni:  $N=-80.47$   $T_x=-73.41$   $M_y=73.92$   $T_y=46.60$   $M_z=69.91$   
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=1.50$  - Classe 1  
 Sollecitazioni:  $T_x=-370.64$   
 $V,Ed=-370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=1.50$  - Classe 1  
 Sollecitazioni:  $N=-142.40$   $T_x=-370.64$   $M_y=372.58$   
 $My,Ed=372.58$   $My,V,c,Rd=6269.10$   
 $N,Ed=-142.40$   $Nc,Rd=-126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $My,Ed/MNy,c,Rd=0.06$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni:  $N,Ed=-142.40$   $My,Ed=372.58$   $L=1.50$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=27.33$   $Ncr,y=1039280.00$   $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$   $Ncr,z=541779.00$   $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$   
 Verifica YY:  $0.00+0.06=0.06$   
 Verifica ZZ:  $0.00=0.00$

Asta n. 325 (-28 -81) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=0.00$  - Classe 3  
 Sollecitazioni:  $N=84.82$   $T_x=67.20$   $M_y=64.60$   $T_y=-21.32$   $M_z=31.97$   
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=0.00$  - Classe 1  
 Sollecitazioni:  $T_x=370.64$   
 $V,Ed=370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=0.00$  - Classe 1  
 Sollecitazioni:  $N=142.40$   $T_x=370.64$   $M_y=372.58$   
 $My,Ed=372.58$   $My,V,c,Rd=6269.10$   
 $N,Ed=142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $My,Ed/MNy,c,Rd=0.06$

Asta n. 325 (-80 -28) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3  
Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-370.64  
V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: N=-142.40 T<sub>z</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.06=0.06  
Verifica ZZ: 0.00=0.00
- Asta n. 326 (-29 -83) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=84.82 T<sub>z</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=370.64  
V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: N=142.40 T<sub>z</sub>=370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06
- Asta n. 326 (-82 -29) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3  
Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-370.64  
V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: N=-142.40 T<sub>z</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ , 0.95, 0.95  
 $\lambda_y=27.33$  Ncr,y=1039280.00  $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$  Ncr,z=541779.00  $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
Verifica YY: 0.00+0.06=0.06  
Verifica ZZ: 0.00=0.00
- Asta n. 327 (-30 -85) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3  
Sollecitazioni: N=84.82 T<sub>z</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: T<sub>z</sub>=370.64  
V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=0.00 - Classe 1  
Sollecitazioni: N=142.40 T<sub>z</sub>=370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06
- Asta n. 327 (-84 -30) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3
- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.50 - Classe 3  
Sollecitazioni: N=-80.47 T<sub>z</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: T<sub>z</sub>=-370.64  
V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU Xl=1.50 - Classe 1  
Sollecitazioni: N=-142.40 T<sub>z</sub>=-370.64 M<sub>y</sub>=372.58  
My,Ed=372.58 My,V,c,Rd=6269.10  
N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y$ =27.33 Ncr,y=1039280.00  $\lambda'_y$ =0.36 Curva a:  $\Phi_y$ =0.58  $\chi_y$ =0.96  
 $\lambda_z$ =37.85 Ncr,z=541779.00  $\lambda'_z$ =0.50 Curva a:  $\Phi_z$ =0.65  $\chi_z$ =0.93  
 $K_{yy}$ ,  $K_{yz}$ ,  $K_{zy}$ ,  $K_{zz}$ =0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 329 (-32 -86) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3  
 Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{max}$ =72.39 (sfrut=0.02)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =22.83  $\tau$ =3.45  $\tau_{max}$ =3.45 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{TD,max}$ =72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1  
 Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 329 (-87 -32) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3  
 Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{max}$ =-110.72 (sfrut=0.03)  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =49.92  $\tau$ =3.78  $\tau_{max}$ =3.78 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{TD,max}$ =110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=-370.64  
 V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1  
 Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y$ =27.33 Ncr,y=1039280.00  $\lambda'_y$ =0.36 Curva a:  $\Phi_y$ =0.58  $\chi_y$ =0.96  
 $\lambda_z$ =37.85 Ncr,z=541779.00  $\lambda'_z$ =0.50 Curva a:  $\Phi_z$ =0.65  $\chi_z$ =0.93  
 $K_{yy}$ ,  $K_{yz}$ ,  $K_{zy}$ ,  $K_{zz}$ =0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 330 (-33 -89) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3  
 Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{max}$ =72.39 (sfrut=0.02)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =22.83  $\tau$ =3.45  $\tau_{max}$ =3.45 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{TD,max}$ =72.39 (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=0.00 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=370.64  
 V,Ed=370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=0.00 - Classe 1  
 Sollecitazioni: N=142.40 T<sub>x</sub>=370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=142.40 Nc,Rd=126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

Asta n. 330 (-88 -33) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=1.50 - Classe 3  
 Sollecitazioni: N=-80.47 T<sub>x</sub>=-73.41 M<sub>y</sub>=73.92 T<sub>y</sub>=46.60 M<sub>z</sub>=69.91  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{max}$ =-110.72 (sfrut=0.03)  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =49.92  $\tau$ =3.78  $\tau_{max}$ =3.78 (sfrut=0.00)  
 Tensioni:  $\sigma_N$ =-2.15  $\sigma_{m,d}$ =-108.57  $\tau$ =0.00  $\sigma_{TD,max}$ =110.72 (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU X1=1.50 - Classe 1  
 Sollecitazioni: T<sub>x</sub>=-370.64  
 V,Ed=-370.64 Vc,Rd=43850.90 V,Ed/Vc,Rd=0.01

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU X1=1.50 - Classe 1  
 Sollecitazioni: N=-142.40 T<sub>x</sub>=-370.64 M<sub>y</sub>=372.58  
 My,Ed=372.58 My,V,c,Rd=6269.10  
 N,Ed=-142.40 Nc,Rd=-126583.00 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=6269.10 My,Ed/MNy,c,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=1.50  
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}$ =0.95, 0.95, 0.95  
 $\lambda_y$ =27.33 Ncr,y=1039280.00  $\lambda'_y$ =0.36 Curva a:  $\Phi_y$ =0.58  $\chi_y$ =0.96  
 $\lambda_z$ =37.85 Ncr,z=541779.00  $\lambda'_z$ =0.50 Curva a:  $\Phi_z$ =0.65  $\chi_z$ =0.93  
 $K_{yy}$ ,  $K_{yz}$ ,  $K_{zy}$ ,  $K_{zz}$ =0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

Asta n. 331 (-34 -61) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND X1=0.00 - Classe 3  
 Sollecitazioni: N=84.82 T<sub>x</sub>=67.20 M<sub>y</sub>=64.60 T<sub>y</sub>=-21.32 M<sub>z</sub>=31.97  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =70.12  $\tau$ =0.00  $\sigma_{max}$ =72.39 (sfrut=0.02)  
 Tensioni:  $\sigma_N$ =2.27  $\sigma_{m,d}$ =22.83  $\tau$ =3.45  $\tau_{max}$ =3.45 (sfrut=0.00)

Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=0.00$  - Classe 1  
Sollecitazioni:  $T_2=370.64$   
 $V,Ed=370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=0.00$  - Classe 1  
Sollecitazioni:  $N=142.40$   $T_2=370.64$   $M_y=372.58$   
 $M_y,Ed=372.58$   $M_y,V,c,Rd=6269.10$   
 $N,Ed=142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $M_y,Ed/MNy,c,Rd=0.06$

Asta n. 331 (-62 -34) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=1.50$  - Classe 3  
Sollecitazioni:  $N=-80.47$   $T_2=-73.41$   $M_y=73.92$   $T_y=46.60$   $M_z=69.91$   
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=1.50$  - Classe 1  
Sollecitazioni:  $T_2=370.64$   
 $V,Ed=-370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=1.50$  - Classe 1  
Sollecitazioni:  $N=-142.40$   $T_2=-370.64$   $M_y=372.58$   
 $M_y,Ed=372.58$   $M_y,V,c,Rd=6269.10$   
 $N,Ed=-142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $M_y,Ed/MNy,c,Rd=0.06$

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni:  $N,Ed=-142.40$   $M_y,Ed=372.58$   $L=1.50$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=27.33$   $Ncr,y=1039280.00$   $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$   $Ncr,z=541779.00$   $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$   
Verifica YY:  $0.00+0.06=0.06$   
Verifica ZZ:  $0.00=0.00$

Asta n. 332 (-35 -102) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=0.00$  - Classe 3  
Sollecitazioni:  $N=84.82$   $T_2=67.20$   $M_y=64.60$   $T_y=-21.32$   $M_z=31.97$   
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=0.00$  - Classe 1  
Sollecitazioni:  $T_2=370.64$   
 $V,Ed=370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=0.00$  - Classe 1  
Sollecitazioni:  $N=142.40$   $T_2=370.64$   $M_y=372.58$   
 $M_y,Ed=372.58$   $M_y,V,c,Rd=6269.10$   
 $N,Ed=142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $M_y,Ed/MNy,c,Rd=0.06$

Asta n. 332 (-101 -35) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=1.50$  - Classe 3  
Sollecitazioni:  $N=-80.47$   $T_2=-73.41$   $M_y=73.92$   $T_y=46.60$   $M_z=69.91$   
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{TD,max}=110.72$  (sfrut=0.03)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=1.50$  - Classe 1  
Sollecitazioni:  $T_2=370.64$   
 $V,Ed=-370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=1.50$  - Classe 1  
Sollecitazioni:  $N=-142.40$   $T_2=-370.64$   $M_y=372.58$   
 $M_y,Ed=372.58$   $M_y,V,c,Rd=6269.10$   
 $N,Ed=-142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $M_y,Ed/MNy,c,Rd=0.06$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni:  $N,Ed=-142.40$   $M_y,Ed=372.58$   $L=1.50$   
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=27.33$   $Ncr,y=1039280.00$   $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$   $Ncr,z=541779.00$   $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$   
Verifica YY:  $0.00+0.06=0.06$   
Verifica ZZ:  $0.00=0.00$

Asta n. 333 (-37 -103) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=0.00$  - Classe 3  
Sollecitazioni:  $N=84.82$   $T_2=67.20$   $M_y=64.60$   $T_y=-21.32$   $M_z=31.97$   
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{max}=72.39$  (sfrut=0.02)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=22.83$   $\tau=3.45$   $\tau_{max}=3.45$  (sfrut=0.00)  
Tensioni:  $\sigma_N=2.27$   $\sigma_{m,d}=70.12$   $\tau=0.00$   $\sigma_{TD,max}=72.39$  (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=0.00$  - Classe 1  
Sollecitazioni:  $T_2=370.64$   
 $V,Ed=370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=0.00$  - Classe 1  
Sollecitazioni:  $N=142.40$   $T_2=370.64$   $M_y=372.58$   
 $M_y,Ed=372.58$   $M_y,V,c,Rd=6269.10$   
 $N,Ed=142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $M_y,Ed/MNy,c,Rd=0.06$

Asta n. 333 (-104 -37) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=1.50$  - Classe 3  
Sollecitazioni:  $N=-80.47$   $T_2=-73.41$   $M_y=73.92$   $T_y=46.60$   $M_z=69.91$   
Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{max}=-110.72$  (sfrut=0.03)

Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=49.92$   $\tau=3.78$   $\tau_{max}=3.78$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-2.15$   $\sigma_{m,d}=-108.57$   $\tau=0.00$   $\sigma_{ID,max}=110.72$  (sfrut=0.03)

- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=1.50$  - Classe 1  
 Sollecitazioni:  $T_z=-370.64$   
 $V,Ed=-370.64$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.01$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=1.50$  - Classe 1  
 Sollecitazioni:  $N=-142.40$   $T_z=-370.64$   $M_y=372.58$   
 $My,Ed=372.58$   $My,V,c,Rd=6269.10$   
 $N,Ed=-142.40$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $My,Ed/MNy,c,Rd=0.06$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni:  $N,Ed=-142.40$   $My,Ed=372.58$   $L=1.50$   
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $\lambda_y=27.33$   $Ncr,y=1039280.00$   $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$   $Ncr,z=541779.00$   $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 $Kyy$ ,  $Kyz$ ,  $Kzy$ ,  $Kzz=0.95$ ,  $0.57$ ,  $0.00$ ,  $0.95$   
 Verifica YY:  $0.00+0.06=0.06$   
 Verifica ZZ:  $0.00=0.00$

Asta n. 334 (-38 -99) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=0.00$  - Classe 3  
 Sollecitazioni:  $N=59.85$   $T_z=47.12$   $M_y=43.09$   $T_y=-14.22$   $M_z=21.33$   
 Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=46.78$   $\tau=0.00$   $\sigma_{max}=48.38$  (sfrut=0.01)  
 Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=15.23$   $\tau=2.42$   $\tau_{max}=2.42$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=1.60$   $\sigma_{m,d}=46.78$   $\tau=0.00$   $\sigma_{ID,max}=48.38$  (sfrut=0.01)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=0.00$  - Classe 1  
 Sollecitazioni:  $T_z=201.76$   
 $V,Ed=201.76$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=0.00$  - Classe 1  
 Sollecitazioni:  $N=94.68$   $T_z=201.76$   $M_y=198.62$   
 $My,Ed=198.62$   $My,V,c,Rd=6269.10$   
 $N,Ed=94.68$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $My,Ed/MNy,c,Rd=0.03$

Asta n. 334 (-100 -38) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND  $X1=1.50$  - Classe 3  
 Sollecitazioni:  $N=-56.95$   $T_z=-51.26$   $M_y=49.31$   $T_y=31.09$   $M_z=46.64$   
 Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=-72.43$   $\tau=0.00$   $\sigma_{max}=-73.95$  (sfrut=0.02)  
 Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=33.30$   $\tau=2.64$   $\tau_{max}=2.64$  (sfrut=0.00)  
 Tensioni:  $\sigma_N=-1.52$   $\sigma_{m,d}=-72.43$   $\tau=0.00$   $\sigma_{ID,max}=73.95$  (sfrut=0.02)
- Verifica a taglio Dir. Z [4.2.16] - CC 28 SLU  $X1=1.50$  - Classe 1  
 Sollecitazioni:  $T_z=-201.76$   
 $V,Ed=-201.76$   $Vc,Rd=43850.90$   $V,Ed/Vc,Rd=0.00$
- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 28 SLU  $X1=1.50$  - Classe 1  
 Sollecitazioni:  $N=-94.68$   $T_z=-201.76$   $M_y=198.62$   
 $My,Ed=198.62$   $My,V,c,Rd=6269.10$   
 $N,Ed=-94.68$   $Nc,Rd=126583.00$   $YY$   $n=N,Ed/Nc,Rd=0.00$   $MNy,c,Rd=6269.10$   $My,Ed/MNy,c,Rd=0.03$
- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni:  $N,Ed=-94.68$   $My,Ed=198.62$   $L=1.50$   
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $\lambda_y=27.33$   $Ncr,y=1039280.00$   $\lambda'_y=0.36$  Curva a:  $\Phi_y=0.58$   $\chi_y=0.96$   
 $\lambda_z=37.85$   $Ncr,z=541779.00$   $\lambda'_z=0.50$  Curva a:  $\Phi_z=0.65$   $\chi_z=0.93$   
 $Kyy$ ,  $Kyz$ ,  $Kzy$ ,  $Kzz=0.95$ ,  $0.57$ ,  $0.00$ ,  $0.95$   
 Verifica YY:  $0.00+0.03=0.03$   
 Verifica ZZ:  $0.00=0.00$

Membratura

Asta n. 201 (-3 -4 -5 -6 -7 -8 -9 -10) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni:  $My,Ed=1559.14$   $Mz,Ed=1060.46$   $L=7.13$   
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $Kyy$ ,  $Kyz$ ,  $Kzy$ ,  $Kzz=0.95$ ,  $0.95$ ,  $0.76$ ,  $0.95$   
 Verifica YY:  $0.00+0.12+0.08=0.19$   
 Verifica ZZ:  $0.00+0.09+0.08=0.17$
- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,s}=0.07$  (L/10113)
- Verifica freccia massima carichi totali - CC 30  
 $f_{z,t}=0.16$  (L/4521)

Membratura

Asta n. 202 (-10 -11 -12 -13 -14 -15 203) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni:  $N,Ed=-122.31$   $My,Ed=2309.73$   $Mz,Ed=1209.30$   $L=7.10$   
 $\alpha_{my}$ ,  $\alpha_{mz}$ ,  $\alpha_{LT}=0.95$ ,  $0.95$ ,  $0.95$   
 $\lambda_y=90.50$   $Ncr,y=155474.00$   $\lambda'_y=1.18$  Curva a:  $\Phi_y=1.30$   $\chi_y=0.54$   
 $\lambda_z=90.50$   $Ncr,z=155474.00$   $\lambda'_z=1.18$  Curva a:  $\Phi_z=1.30$   $\chi_z=0.54$   
 $Kyy$ ,  $Kyz$ ,  $Kzy$ ,  $Kzz=0.95$ ,  $0.95$ ,  $0.76$ ,  $0.95$   
 Verifica YY:  $0.00+0.17+0.09=0.26$   
 Verifica ZZ:  $0.00+0.14+0.09=0.23$
- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,s}=0.21$  (L/3326)
- Verifica freccia massima carichi totali - CC 30  
 $f_{z,t}=0.41$  (L/1717)

Membratura

Asta n. 203 (203 -16 -17 -18 -19 -20 204) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3

Sollecitazioni: N,Ed=37.41 My,Ed=1956.88 Mz,Ed=1208.41 L=6.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$   
 Verifica YY:  $0.00+0.15+0.09=0.24$   
 Verifica ZZ:  $0.00+0.12+0.09=0.21$

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=0.07$  (L/8055)

- Verifica freccia massima carichi totali - CC 30  
 $f_{z,1}=0.14$  (L/4165)

## Membratura

Asta n. 204 (204 -21 -22 -23 -24 -25 205) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=37.41 My,Ed=1956.88 Mz,Ed=1208.42 L=6.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$   
 Verifica YY:  $0.00+0.15+0.09=0.24$   
 Verifica ZZ:  $0.00+0.12+0.09=0.21$

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=0.07$  (L/8053)

- Verifica freccia massima carichi totali - CC 30  
 $f_{z,1}=0.14$  (L/4165)

## Membratura

Asta n. 205 (205 -26 -27 -28 -29 -30 -31) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: N,Ed=-122.31 My,Ed=2309.74 Mz,Ed=1209.30 L=7.10  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=90.50$  Ncr,y=155474.00  $\lambda'_y=1.18$  Curva a:  $\Phi_y=1.30$   $\chi_y=0.54$   
 $\lambda_z=90.50$  Ncr,z=155474.00  $\lambda'_z=1.18$  Curva a:  $\Phi_z=1.30$   $\chi_z=0.54$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$   
 Verifica YY:  $0.00+0.17+0.09=0.26$   
 Verifica ZZ:  $0.00+0.14+0.09=0.23$

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,6}=0.21$  (L/3326)

- Verifica freccia massima carichi totali - CC 30  
 $f_{z,1}=0.41$  (L/1718)

## Membratura

Asta n. 206 (-31 -32 -33 -34 -35 -36 -37 -38) - Sez. 2 (TRV PRINC SHS200x200x8) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 3  
 Sollecitazioni: My,Ed=1559.12 Mz,Ed=1060.45 L=7.13  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.95, 0.76, 0.95$   
 Verifica YY:  $0.00+0.12+0.08=0.19$   
 Verifica ZZ:  $0.00+0.09+0.08=0.17$

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,6}=0.07$  (L/10110)

- Verifica freccia massima carichi totali - CC 30  
 $f_{z,1}=0.16$  (L/4521)

## Membratura

Asta n. 301 (-60 -3 -59) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-94.68 My,Ed=198.62 L=3.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=54.65$  Ncr,y=259820.00  $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$   
 $\lambda_z=75.69$  Ncr,z=135445.00  $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$   
 Verifica YY:  $0.00+0.03=0.03$   
 Verifica ZZ:  $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=0.78$  (L/384)  $f_{z,6}=0.04$  (L/8205)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=0.77$  (L/389)  $f_{z,6}=0.03$  (L/11280)

## Membratura

Asta n. 302 (-47 -4 -46) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=54.65$  Ncr,y=259820.00  $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$   
 $\lambda_z=75.69$  Ncr,z=135445.00  $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$   
 $K_{yy}, K_{yz}, K_{zy}, K_{zz}=0.95, 0.57, 0.00, 0.95$   
 Verifica YY:  $0.00+0.06=0.06$   
 Verifica ZZ:  $0.00=0.00$

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=0.82$  (L/367)  $f_{z,6}=0.07$  (L/4101)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=0.80$  (L/374)  $f_{z,6}=0.06$  (L/5195)

## Membratura

Asta n. 303 (-48 -6 -49) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr,  $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr,  $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=0.84$  (L/358)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=0.82$  (L/364)  $f_{z,6}=0.06$  (L/5196)

Membratura

Asta n. 304 (-96 -7 -95) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr,  $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr,  $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=0.89$  (L/336)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=0.87$  (L/342)  $f_{z,6}=0.06$  (L/5193)

Membratura

Asta n. 305 (-66 -8 -67) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr,  $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr,  $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=0.94$  (L/318)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=0.93$  (L/323)  $f_{z,6}=0.06$  (L/5196)

Membratura

Asta n. 306 (-69 -9 -68) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr,  $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr,  $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.00$  (L/301)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=0.98$  (L/305)  $f_{z,6}=0.06$  (L/5195)

Membratura

Asta n. 307 (-70 -11 -71) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr,  $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr,  $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.02$  (L/292)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=1.01$  (L/297)  $f_{z,6}=0.06$  (L/5197)

Membratura

Asta n. 308 (-72 -12 -73) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr,  $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr,  $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.04$  (L/288)  $f_{z,6}=0.07$  (L/4101)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=1.02$  (L/292)  $f_{z,6}=0.06$  (L/5196)

## Membratura

Asta n. 309 (-74 -13 -75) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=1.05$  (L/284)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=1.04$  (L/288)  $f_{z,6}=0.06$  (L/5195)

## Membratura

Asta n. 310 (-90 -14 -91) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=1.07$  (L/280)  $f_{z,6}=0.07$  (L/4101)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=1.05$  (L/284)  $f_{z,6}=0.06$  (L/5195)

## Membratura

Asta n. 311 (-92 -15 -93) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=1.09$  (L/276)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=1.07$  (L/280)  $f_{z,6}=0.06$  (L/5196)

## Membratura

Asta n. 312 (-98 -16 -94) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=1.09$  (L/276)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=1.07$  (L/280)  $f_{z,6}=0.06$  (L/5196)

## Membratura

Asta n. 313 (-97 -17 -42) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=1.06$  (L/283)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=1.04$  (L/287)  $f_{z,6}=0.06$  (L/5195)

## Membratura

Asta n. 314 (-43 -18 -44) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00



- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=1.03$  (L/290)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=1.02$  (L/295)  $f_{z,6}=0.06$  (L/5198)

## Membratura

Asta n. 315 (-45 -19 -58) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=54.65$  Ncr,y=259820.00  $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$   
 $\lambda_z=75.69$  Ncr,z=135445.00  $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=1.00$  (L/298)  $f_{z,6}=0.07$  (L/4103)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=0.99$  (L/303)  $f_{z,6}=0.06$  (L/5196)

## Membratura

Asta n. 316 (-63 -20 -65) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-94.68 My,Ed=198.62 L=3.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=54.65$  Ncr,y=259820.00  $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$   
 $\lambda_z=75.69$  Ncr,z=135445.00  $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.03=0.03  
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=0.94$  (L/319)  $f_{z,6}=0.04$  (L/8208)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=0.93$  (L/322)  $f_{z,6}=0.03$  (L/11300)

## Membratura

Asta n. 317 (-51 -21 -50) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-94.68 My,Ed=198.62 L=3.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=54.65$  Ncr,y=259820.00  $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$   
 $\lambda_z=75.69$  Ncr,z=135445.00  $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.03=0.03  
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=0.94$  (L/319)  $f_{z,6}=0.04$  (L/8208)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=0.93$  (L/322)  $f_{z,6}=0.03$  (L/11300)

## Membratura

Asta n. 318 (-53 -22 -52) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=54.65$  Ncr,y=259820.00  $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$   
 $\lambda_z=75.69$  Ncr,z=135445.00  $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=1.00$  (L/298)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=0.99$  (L/303)  $f_{z,6}=0.06$  (L/5196)

## Membratura

Asta n. 319 (-55 -23 -54) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00  
 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$   
 $\lambda_y=54.65$  Ncr,y=259820.00  $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$   
 $\lambda_z=75.69$  Ncr,z=135445.00  $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$   
 Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95  
 Verifica YY: 0.00+0.06=0.06  
 Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=1.03$  (L/290)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=1.02$  (L/295)  $f_{z,6}=0.06$  (L/5197)

## Membratura

Asta n. 320 (-57 -24 -56) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr, $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr, $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.06$  (L/283)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=1.04$  (L/287)  $f_{z,6}=0.06$  (L/5195)

#### Membratura

Asta n. 322 (-41 -25 -64) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr, $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr, $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.09$  (L/276)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=1.07$  (L/280)  $f_{z,6}=0.06$  (L/5196)

#### Membratura

Asta n. 323 (-77 -26 -76) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr, $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr, $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.09$  (L/276)  $f_{z,6}=0.07$  (L/4103)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=1.07$  (L/280)  $f_{z,6}=0.06$  (L/5197)

#### Membratura

Asta n. 324 (-79 -27 -78) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr, $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr, $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.07$  (L/280)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=1.05$  (L/284)  $f_{z,6}=0.06$  (L/5197)

#### Membratura

Asta n. 325 (-81 -28 -80) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr, $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr, $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.05$  (L/284)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=1.04$  (L/288)  $f_{z,6}=0.06$  (L/5195)

#### Membratura

Asta n. 326 (-83 -29 -82) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

- Verifica di stabilit  aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1

Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr, $y=259820.00$   $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr, $z=135445.00$   $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

$f_{z,1}=1.04$  (L/288)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

$f_{z,1}=1.02$  (L/292)  $f_{z,6}=0.06$  (L/5196)

## Membratura

Asta n. 327 (-85 -30 -84) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-----  
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=1.02$  (L/292)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=1.01$  (L/297)  $f_{z,6}=0.06$  (L/5197)

## Membratura

Asta n. 329 (-86 -32 -87) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-----  
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=1.00$  (L/301)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=0.98$  (L/305)  $f_{z,6}=0.06$  (L/5195)

## Membratura

Asta n. 330 (-89 -33 -88) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-----  
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=0.94$  (L/318)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=0.93$  (L/323)  $f_{z,6}=0.06$  (L/5196)

## Membratura

Asta n. 331 (-61 -34 -62) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

-----  
 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=0.89$  (L/336)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=0.87$  (L/342)  $f_{z,6}=0.06$  (L/5193)

## Membratura

Asta n. 332 (-102 -35 -101) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23

 $f_{z,1}=0.84$  (L/358)  $f_{z,6}=0.07$  (L/4103)

- Verifica freccia massima carichi totali - CC 23

 $f_{z,1}=0.82$  (L/364)  $f_{z,6}=0.06$  (L/5196)

## Membratura

Asta n. 333 (-103 -37 -104) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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 - Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
 Sollecitazioni: N,Ed=-142.40 My,Ed=372.58 L=3.00

 $\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$  $\lambda_1=54.65$  Ncr,y=259820.00  $\lambda'_1=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$  $\lambda_2=75.69$  Ncr,z=135445.00  $\lambda'_2=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$ 

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.06=0.06

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=0.82$  (L/367)  $f_{z,6}=0.07$  (L/4102)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=0.80$  (L/374)  $f_{z,6}=0.06$  (L/5194)

## Membratura

Asta n. 334 (-99 -38 -100) - Sez. 3 (TRV SEC RHS150x100x8) - Crit. 3

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- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1  
Sollecitazioni: N,Ed=-94.68 My,Ed=198.62 L=3.00

$\alpha_{my}, \alpha_{mz}, \alpha_{LT}=0.95, 0.95, 0.95$

$\lambda_y=54.65$  Ncr,y=259820.00  $\lambda'_y=0.72$  Curva a:  $\Phi_y=0.81$   $\chi_y=0.84$

$\lambda_z=75.69$  Ncr,z=135445.00  $\lambda'_z=0.99$  Curva a:  $\Phi_z=1.07$   $\chi_z=0.67$

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95

Verifica YY: 0.00+0.03=0.03

Verifica ZZ: 0.00=0.00

- Verifica freccia massima per soli carichi accidentali - CC 23  
 $f_{z,1}=0.78$  (L/384)  $f_{z,6}=0.04$  (L/8202)

- Verifica freccia massima carichi totali - CC 23  
 $f_{z,1}=0.77$  (L/389)  $f_{z,6}=0.03$  (L/11280)

## 7.0 RISULTATI STRUTTURE FONDAZIONE BESS

### 7.1 Diagrammi tassi di sfruttamento

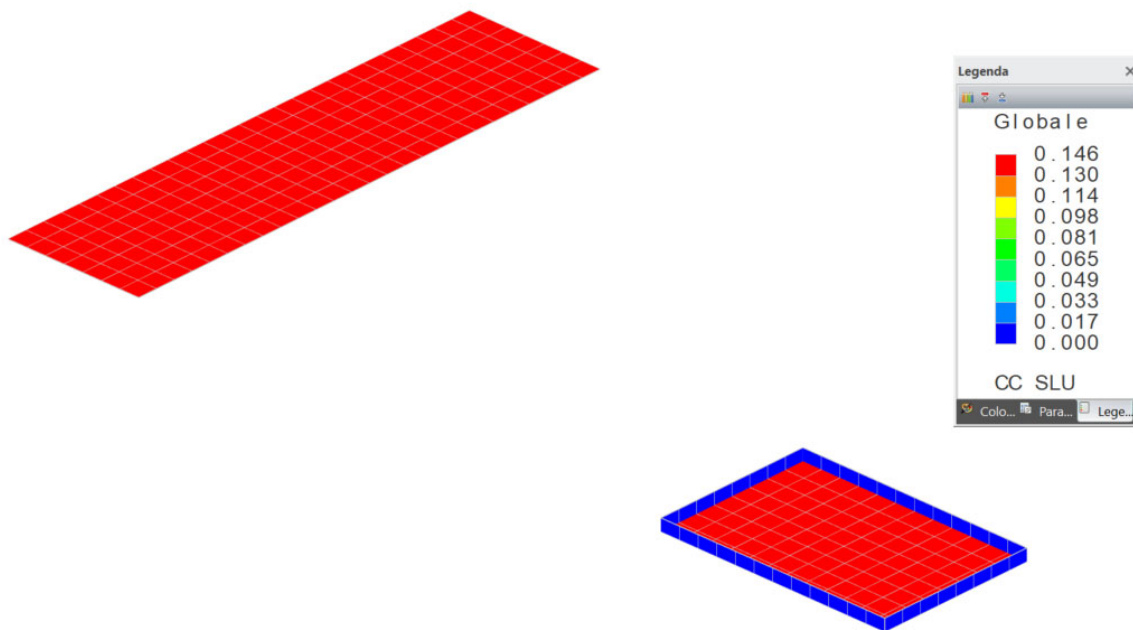
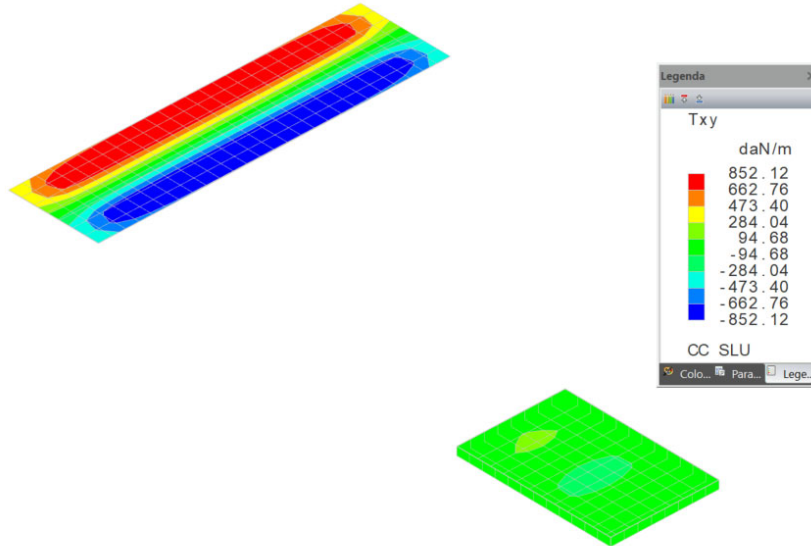


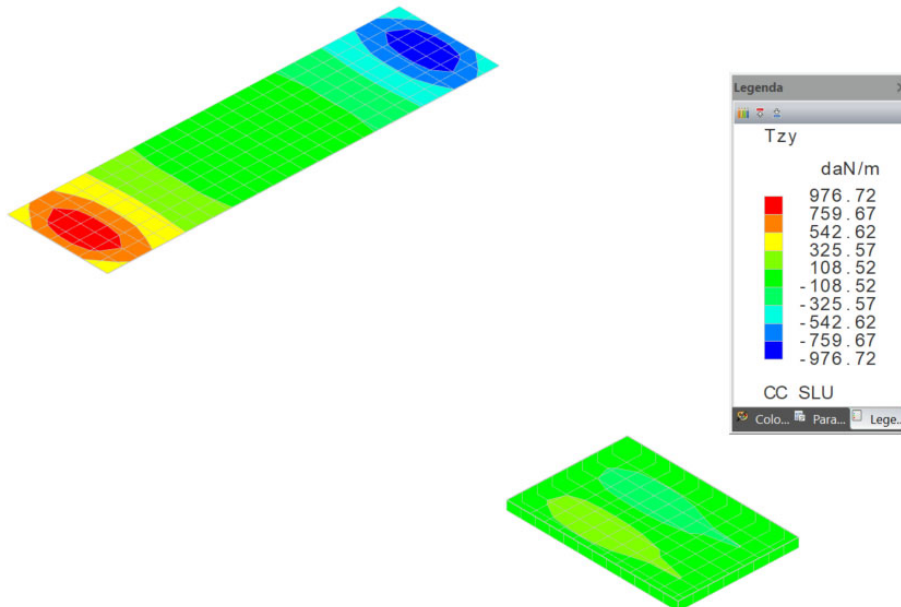
Diagramma tassi di sfruttamento resistenza combo SLU con valore massimo pari a 0,146

**Figure 37: Tassi di sfruttamento SLU (Stato limite ultimo)**

## 7.2 Sollecitazioni

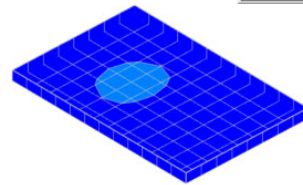
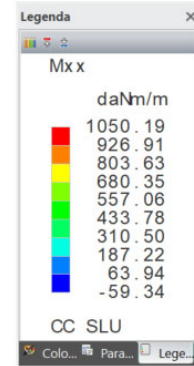
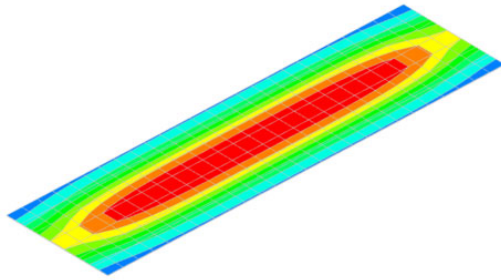


Inviluppo sforzo di taglio in direzione X su faccia con normale Y SLU T<sub>max</sub> = 852,12 daN/m

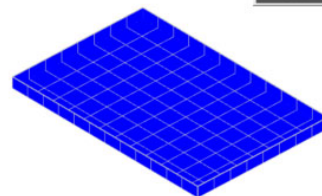
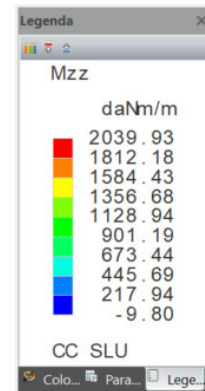
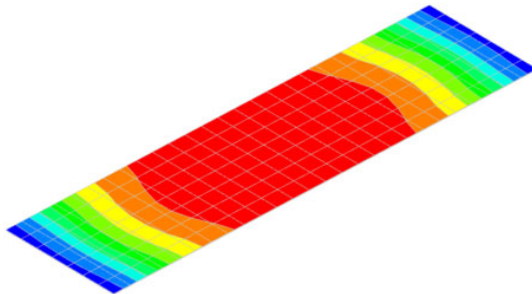


Inviluppo sforzo di taglio in direzione Z su faccia con normale Y SLU T<sub>max</sub> = 976,72 daN/m

**Figure 38: Taglio**



Inviluppo momento che genera tensioni in direzioni X su facce con normale X SLU  $M_{max} = 1050,19 \text{ daN}\times\text{m}/\text{m}$



Inviluppo momento che genera tensioni in direzioni Z su facce con normale Z SLU  $M_{max} = 2039,93 \text{ daN}\times\text{m}/\text{m}$

**Figure 39: Momento Flettente**

## 7.3 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

### Risultati del calcolo

#### Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:  
 ModeSt ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato  
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:  
 Xfinest ver. 9.5.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18  
 Tipo di calcolo: statico  
 Vincoli esterni: Considera sempre vincoli assegnati in modellazione  
 Schematizzazione piani rigidi: nessun impalcato rigido  
 Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

#### Generazione combinazioni

- Lineari: Sì  
 - Valuta spostamenti e non sollecitazioni: No  
 - Buckling: No

#### Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%  
 - Calcolo con offset rigidi dai nodi: No  
 - Uniformare i carichi variabili: No  
 - Massimizzare i carichi variabili: No  
 - Recupero carichi zone rigide: taglio e momento flettente

#### Opzioni del solutore

- Tipo di elemento bidimensionale: QF46  
 - Calcolo sforzo nei nodi: No  
 - Trascura deformabilità a taglio delle aste: No  
 - Analisi dinamica con metodo di Lanczos: Sì  
 - Check sequenza di Sturm: Sì  
 - Analisi non lineare con Newton modificato: No  
 - Usa formulazione secante per buckling: No  
 - Trascura buckling torsionale: No

#### Dati struttura

- Edificio esistente: No  
 - Tipo di opera: Opera ordinaria  
 - Vita nominale  $V_N$ : 50.00  
 - Classe d'uso: Classe II  
 - Forze orizzontali convenzionali per stati limite non sismici: No  
 - Genera stati limite per verifiche di resistenza al fuoco: No

#### Ambienti di carico

##### Simbologia

N = Numero  
 Comm. = Commento  
 1 = G1 - permanenti strutturali  
 2 = G2 - permanenti non strutturali  
 3 = Q - Variabili cat. E  
 F = azioni orizzontali convenzionali  
 SLU = Stato limite ultimo  
 SLR = Stato limite per combinazioni rare  
 SLF = Stato limite per combinazioni frequenti  
 SLQ/D = Stato limite per combinazioni quasi permanenti o di danno  
 S = Sì  
 N = No

| N | Comm.           | 1 | 2 | 3 | SLU | SLR | SLF | SLQ |
|---|-----------------|---|---|---|-----|-----|-----|-----|
| 1 | Calcolo statico | S | S | S | S   | S   | S   | S   |

#### Elenco combinazioni di carico simboliche

##### Simbologia

CC = Numero della combinazione delle condizioni di carico elementari  
 Comm. = Commento  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| CC | Comm.          | TCC   | 1              | 2              | 3              |
|----|----------------|-------|----------------|----------------|----------------|
| 1  | Amb. 1 (SLU)   | SLU   | $\gamma_{max}$ | $\gamma_{max}$ | $\gamma_{max}$ |
| 2  | Amb. 1 (SLE R) | SLE R | 1              | 1              | 1              |
| 3  | Amb. 1 (SLE F) | SLE F | 1              | 1              | $\psi_1$       |
| 4  | Amb. 1 (SLE Q) | SLE Q | 1              | 1              | $\psi_2$       |

Genera le combinazioni con un solo carico di tipo variabile come di base: Sì

Considera sollecitazioni dinamiche con segno dei modi principali: No

#### Combinazioni delle CCE

##### Simbologia

An. = Tipo di analisi  
 L = Lineare  
 NL = Non lineare  
 Bk = Buckling





S = Sì  
 N = No  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Comm. = Commento  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| CC | Comm.          | TCC   | An. | Bk | 1    | 2    | 3    |
|----|----------------|-------|-----|----|------|------|------|
| 1  | Amb. 1 (SLU)   | SLU   | L   | N  | 1.30 | 1.50 | 1.50 |
| 2  | Amb. 1 (SLE R) | SLE R | L   | N  | 1.00 | 1.00 | 1.00 |
| 3  | Amb. 1 (SLE F) | SLE F | L   | N  | 1.00 | 1.00 | 0.90 |
| 4  | Amb. 1 (SLE Q) | SLE Q | L   | N  | 1.00 | 1.00 | 0.80 |

Tensioni sul terreno

Simbologia

$\sigma_t$  = Tensione sul terreno  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Nodo = Numero del nodo  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| Nodo | CC   | TCC | $\sigma_t$<br><daN/cmq> | Nodo | CC   | TCC  | $\sigma_t$<br><daN/cmq> | Nodo | CC  | TCC  | $\sigma_t$<br><daN/cmq> | Nodo | CC | TCC | $\sigma_t$<br><daN/cmq> | Nodo | CC   | TCC | $\sigma_t$<br><daN/cmq> |     |      |
|------|------|-----|-------------------------|------|------|------|-------------------------|------|-----|------|-------------------------|------|----|-----|-------------------------|------|------|-----|-------------------------|-----|------|
| -424 | Max  | 1   | SLU                     | 0.25 | -424 | Min. | 4                       | SLE  | Q   | 0.18 | -423                    | Max  | 1  | SLU | 0.26                    | -423 | Min. | 4   | SLE                     | Q   | 0.18 |
| -422 | Min. | 4   | SLE                     | Q    | 0.19 | -421 | Max                     | 1    | SLU | 0.26 | -421                    | Min. | 4  | SLE | Q                       | 0.19 | -420 | Max | 1                       | SLU | 0.26 |
| -419 | Max  | 1   | SLU                     | 0.25 | -419 | Min. | 4                       | SLE  | Q   | 0.18 | -418                    | Max  | 1  | SLU | 0.26                    | -418 | Min. | 4   | SLE                     | Q   | 0.18 |
| -417 | Min. | 4   | SLE                     | Q    | 0.19 | -416 | Max                     | 1    | SLU | 0.26 | -416                    | Min. | 4  | SLE | Q                       | 0.19 | -415 | Max | 1                       | SLU | 0.26 |
| -414 | Max  | 1   | SLU                     | 0.25 | -414 | Min. | 4                       | SLE  | Q   | 0.18 | -413                    | Max  | 1  | SLU | 0.26                    | -413 | Min. | 4   | SLE                     | Q   | 0.18 |
| -412 | Min. | 4   | SLE                     | Q    | 0.19 | -411 | Max                     | 1    | SLU | 0.26 | -411                    | Min. | 4  | SLE | Q                       | 0.19 | -410 | Max | 1                       | SLU | 0.26 |
| -409 | Max  | 1   | SLU                     | 0.25 | -409 | Min. | 4                       | SLE  | Q   | 0.18 | -408                    | Max  | 1  | SLU | 0.26                    | -408 | Min. | 4   | SLE                     | Q   | 0.18 |
| -407 | Min. | 4   | SLE                     | Q    | 0.19 | -406 | Max                     | 1    | SLU | 0.26 | -406                    | Min. | 4  | SLE | Q                       | 0.19 | -405 | Max | 1                       | SLU | 0.26 |
| -404 | Max  | 1   | SLU                     | 0.25 | -404 | Min. | 4                       | SLE  | Q   | 0.18 | -403                    | Max  | 1  | SLU | 0.26                    | -403 | Min. | 4   | SLE                     | Q   | 0.18 |
| -402 | Min. | 4   | SLE                     | Q    | 0.19 | -401 | Max                     | 1    | SLU | 0.26 | -401                    | Min. | 4  | SLE | Q                       | 0.19 | -400 | Max | 1                       | SLU | 0.26 |
| -399 | Max  | 1   | SLU                     | 0.25 | -399 | Min. | 4                       | SLE  | Q   | 0.18 | -398                    | Max  | 1  | SLU | 0.26                    | -398 | Min. | 4   | SLE                     | Q   | 0.18 |
| -397 | Min. | 4   | SLE                     | Q    | 0.19 | -396 | Max                     | 1    | SLU | 0.26 | -396                    | Min. | 4  | SLE | Q                       | 0.19 | -395 | Max | 1                       | SLU | 0.26 |
| -394 | Max  | 1   | SLU                     | 0.25 | -394 | Min. | 4                       | SLE  | Q   | 0.18 | -393                    | Max  | 1  | SLU | 0.26                    | -393 | Min. | 4   | SLE                     | Q   | 0.18 |
| -392 | Min. | 4   | SLE                     | Q    | 0.19 | -391 | Max                     | 1    | SLU | 0.26 | -391                    | Min. | 4  | SLE | Q                       | 0.19 | -390 | Max | 1                       | SLU | 0.26 |
| -389 | Max  | 1   | SLU                     | 0.25 | -389 | Min. | 4                       | SLE  | Q   | 0.18 | -388                    | Max  | 1  | SLU | 0.26                    | -388 | Min. | 4   | SLE                     | Q   | 0.18 |
| -387 | Min. | 4   | SLE                     | Q    | 0.19 | -386 | Max                     | 1    | SLU | 0.26 | -386                    | Min. | 4  | SLE | Q                       | 0.19 | -385 | Max | 1                       | SLU | 0.26 |
| -379 | Max  | 1   | SLU                     | 0.26 | -379 | Min. | 4                       | SLE  | Q   | 0.19 | -378                    | Max  | 1  | SLU | 0.26                    | -378 | Min. | 4   | SLE                     | Q   | 0.19 |
| -377 | Min. | 4   | SLE                     | Q    | 0.19 | -376 | Max                     | 1    | SLU | 0.26 | -376                    | Min. | 4  | SLE | Q                       | 0.18 | -375 | Max | 1                       | SLU | 0.25 |
| -344 | Max  | 1   | SLU                     | 0.41 | -344 | Min. | 4                       | SLE  | Q   | 0.29 | -343                    | Max  | 1  | SLU | 0.42                    | -343 | Min. | 4   | SLE                     | Q   | 0.29 |
| -342 | Min. | 4   | SLE                     | Q    | 0.29 | -341 | Max                     | 1    | SLU | 0.42 | -341                    | Min. | 4  | SLE | Q                       | 0.29 | -340 | Max | 1                       | SLU | 0.42 |
| -339 | Max  | 1   | SLU                     | 0.42 | -339 | Min. | 4                       | SLE  | Q   | 0.29 | -338                    | Max  | 1  | SLU | 0.42                    | -338 | Min. | 4   | SLE                     | Q   | 0.29 |
| -337 | Min. | 4   | SLE                     | Q    | 0.29 | -336 | Max                     | 1    | SLU | 0.42 | -336                    | Min. | 4  | SLE | Q                       | 0.30 | -335 | Max | 1                       | SLU | 0.42 |
| -334 | Max  | 1   | SLU                     | 0.42 | -334 | Min. | 4                       | SLE  | Q   | 0.30 | -333                    | Max  | 1  | SLU | 0.42                    | -333 | Min. | 4   | SLE                     | Q   | 0.30 |
| -332 | Min. | 4   | SLE                     | Q    | 0.30 | -331 | Max                     | 1    | SLU | 0.42 | -331                    | Min. | 4  | SLE | Q                       | 0.30 | -330 | Max | 1                       | SLU | 0.42 |
| -329 | Max  | 1   | SLU                     | 0.42 | -329 | Min. | 4                       | SLE  | Q   | 0.30 | -328                    | Max  | 1  | SLU | 0.43                    | -328 | Min. | 4   | SLE                     | Q   | 0.30 |
| -327 | Min. | 4   | SLE                     | Q    | 0.30 | -326 | Max                     | 1    | SLU | 0.43 | -326                    | Min. | 4  | SLE | Q                       | 0.30 | -325 | Max | 1                       | SLU | 0.43 |
| -324 | Max  | 1   | SLU                     | 0.43 | -324 | Min. | 4                       | SLE  | Q   | 0.30 | -323                    | Max  | 1  | SLU | 0.43                    | -323 | Min. | 4   | SLE                     | Q   | 0.30 |
| -322 | Min. | 4   | SLE                     | Q    | 0.30 | -321 | Max                     | 1    | SLU | 0.43 | -321                    | Min. | 4  | SLE | Q                       | 0.30 | -320 | Max | 1                       | SLU | 0.43 |
| -319 | Max  | 1   | SLU                     | 0.43 | -319 | Min. | 4                       | SLE  | Q   | 0.30 | -318                    | Max  | 1  | SLU | 0.44                    | -318 | Min. | 4   | SLE                     | Q   | 0.30 |
| -317 | Min. | 4   | SLE                     | Q    | 0.30 | -316 | Max                     | 1    | SLU | 0.44 | -316                    | Min. | 4  | SLE | Q                       | 0.30 | -315 | Max | 1                       | SLU | 0.44 |
| -314 | Max  | 1   | SLU                     | 0.43 | -314 | Min. | 4                       | SLE  | Q   | 0.30 | -313                    | Max  | 1  | SLU | 0.43                    | -313 | Min. | 4   | SLE                     | Q   | 0.30 |
| -312 | Min. | 4   | SLE                     | Q    | 0.31 | -311 | Max                     | 1    | SLU | 0.44 | -311                    | Min. | 4  | SLE | Q                       | 0.31 | -310 | Max | 1                       | SLU | 0.44 |
| -309 | Max  | 1   | SLU                     | 0.44 | -309 | Min. | 4                       | SLE  | Q   | 0.31 | -308                    | Max  | 1  | SLU | 0.44                    | -308 | Min. | 4   | SLE                     | Q   | 0.31 |
| -307 | Min. | 4   | SLE                     | Q    | 0.31 | -306 | Max                     | 1    | SLU | 0.44 | -306                    | Min. | 4  | SLE | Q                       | 0.31 | -305 | Max | 1                       | SLU | 0.44 |
| -304 | Max  | 1   | SLU                     | 0.45 | -304 | Min. | 4                       | SLE  | Q   | 0.31 | -303                    | Max  | 1  | SLU | 0.45                    | -303 | Min. | 4   | SLE                     | Q   | 0.31 |
| -302 | Min. | 4   | SLE                     | Q    | 0.31 | -301 | Max                     | 1    | SLU | 0.45 | -301                    | Min. | 4  | SLE | Q                       | 0.31 | -300 | Max | 1                       | SLU | 0.45 |
| -299 | Max  | 1   | SLU                     | 0.45 | -299 | Min. | 4                       | SLE  | Q   | 0.31 | -298                    | Max  | 1  | SLU | 0.45                    | -298 | Min. | 4   | SLE                     | Q   | 0.31 |
| -297 | Min. | 4   | SLE                     | Q    | 0.31 | -296 | Max                     | 1    | SLU | 0.45 | -296                    | Min. | 4  | SLE | Q                       | 0.32 | -295 | Max | 1                       | SLU | 0.45 |
| -294 | Max  | 1   | SLU                     | 0.45 | -294 | Min. | 4                       | SLE  | Q   | 0.32 | -293                    | Max  | 1  | SLU | 0.45                    | -293 | Min. | 4   | SLE                     | Q   | 0.32 |
| -292 | Min. | 4   | SLE                     | Q    | 0.32 | -291 | Max                     | 1    | SLU | 0.45 | -291                    | Min. | 4  | SLE | Q                       | 0.32 | -290 | Max | 1                       | SLU | 0.45 |
| -289 | Max  | 1   | SLU                     | 0.45 | -289 | Min. | 4                       | SLE  | Q   | 0.32 | -288                    | Max  | 1  | SLU | 0.46                    | -288 | Min. | 4   | SLE                     | Q   | 0.32 |
| -287 | Min. | 4   | SLE                     | Q    | 0.32 | -286 | Max                     | 1    | SLU | 0.46 | -286                    | Min. | 4  | SLE | Q                       | 0.32 | -285 | Max | 1                       | SLU | 0.46 |
| -284 | Max  | 1   | SLU                     | 0.46 | -284 | Min. | 4                       | SLE  | Q   | 0.32 | -283                    | Max  | 1  | SLU | 0.46                    | -283 | Min. | 4   | SLE                     | Q   | 0.32 |
| -282 | Min. | 4   | SLE                     | Q    | 0.32 | -281 | Max                     | 1    | SLU | 0.46 | -281                    | Min. | 4  | SLE | Q                       | 0.32 | -280 | Max | 1                       | SLU | 0.46 |
| -279 | Max  | 1   | SLU                     | 0.46 | -279 | Min. | 4                       | SLE  | Q   | 0.32 | -278                    | Max  | 1  | SLU | 0.46                    | -278 | Min. | 4   | SLE                     | Q   | 0.32 |
| -277 | Min. | 4   | SLE                     | Q    | 0.32 | -276 | Max                     | 1    | SLU | 0.46 | -276                    | Min. | 4  | SLE | Q                       | 0.32 | -275 | Max | 1                       | SLU | 0.46 |
| -274 | Max  | 1   | SLU                     | 0.46 | -274 | Min. | 4                       | SLE  | Q   | 0.32 | -273                    | Max  | 1  | SLU | 0.46                    | -273 | Min. | 4   | SLE                     | Q   | 0.32 |
| -272 | Min. | 4   | SLE                     | Q    | 0.32 | -271 | Max                     | 1    | SLU | 0.46 | -271                    | Min. | 4  | SLE | Q                       | 0.32 | -270 | Max | 1                       | SLU | 0.46 |
| -269 | Max  | 1   | SLU                     | 0.46 | -269 | Min. | 4                       | SLE  | Q   | 0.32 | -268                    | Max  | 1  | SLU | 0.46                    | -268 | Min. | 4   | SLE                     | Q   | 0.32 |
| -267 | Min. | 4   | SLE                     | Q    | 0.32 | -266 | Max                     | 1    | SLU | 0.46 | -266                    | Min. | 4  | SLE | Q                       | 0.32 | -265 | Max | 1                       | SLU | 0.46 |
| -264 | Max  | 1   | SLU                     | 0.46 | -264 | Min. | 4                       | SLE  | Q   | 0.32 | -263                    | Max  | 1  | SLU | 0.47                    | -263 | Min. | 4   | SLE                     | Q   | 0.32 |
| -262 | Min. | 4   | SLE                     | Q    | 0.33 | -261 | Max                     | 1    | SLU | 0.47 | -261                    | Min. | 4  | SLE | Q                       | 0.33 | -260 | Max | 1                       | SLU | 0.47 |
| -259 | Max  | 1   | SLU                     | 0.47 | -259 | Min. | 4                       | SLE  | Q   | 0.33 | -258                    | Max  | 1  | SLU | 0.47                    | -258 | Min. | 4   | SLE                     | Q   | 0.32 |
| -257 | Min. | 4   | SLE                     | Q    | 0.32 | -256 | Max                     | 1    | SLU | 0.47 | -256                    | Min. | 4  | SLE | Q                       | 0.33 | -255 | Max | 1                       | SLU | 0.47 |
| -254 | Max  | 1   | SLU                     | 0.47 | -254 | Min. | 4                       | SLE  | Q   | 0.33 | -253                    | Max  | 1  | SLU | 0.47                    | -253 | Min. | 4   | SLE                     | Q   | 0.33 |
| -252 | Min. | 4   | SLE                     | Q    | 0.33 | -251 | Max                     | 1    | SLU | 0.47 | -251                    | Min. | 4  | SLE | Q                       | 0.33 | -250 | Max | 1                       | SLU | 0.47 |
| -249 | Max  | 1   | SLU                     | 0.47 | -249 | Min. | 4                       | SLE  | Q   | 0.33 | -248                    | Max  | 1  | SLU | 0.47                    | -248 | Min. | 4   | SLE                     | Q   | 0.33 |
| -247 | Min. | 4   | SLE                     | Q    | 0.33 | -246 | Max                     | 1    | SLU | 0.47 | -246                    | Min. | 4  | SLE | Q                       | 0.33 | -245 | Max | 1                       | SLU | 0.47 |
| -244 | Max  | 1   | SLU                     | 0.47 | -244 | Min. | 4                       | SLE  | Q   | 0.33 | -243                    | Max  | 1  | SLU | 0.47                    | -243 | Min. | 4   | SLE                     | Q   | 0.33 |
| -242 | Min. | 4   | SLE                     | Q    | 0.33 | -241 | Max                     | 1    | SLU | 0.47 | -241                    | Min. | 4  | SLE | Q                       | 0.33 | -240 | Max | 1                       | SLU | 0.47 |
| -239 | Max  | 1   | SLU                     | 0.47 | -239 | Min. | 4                       | SLE  | Q   | 0.33 | -238                    | Max  | 1  | SLU | 0.47                    | -238 | Min. | 4   | SLE                     | Q   | 0.33 |
| -237 | Min. | 4   | SLE                     | Q    | 0.33 | -236 | Max                     | 1    | SLU | 0.47 | -236                    | Min. | 4  | SLE | Q                       | 0.33 | -235 | Max | 1                       | SLU | 0.47 |
| -234 | Max  | 1   | SLU                     | 0.47 | -234 | Min. | 4                       | SLE  | Q   | 0.33 | -233                    | Max  | 1  | SLU | 0.47                    | -233 | Min. | 4   | SLE                     | Q   | 0.33 |
| -232 | Min. | 4   | SLE                     | Q    | 0.33 | -231 | Max                     | 1    | SLU | 0.47 | -231                    | Min. | 4  | SLE | Q                       | 0.33 | -230 | Max | 1                       | SLU | 0.47 |
| -229 | Max  | 1   | SLU                     | 0.47 | -229 | Min. | 4                       | SLE  | Q   | 0.33 | -228                    | Max  | 1  | SLU | 0.47                    | -228 | Min. | 4   | SLE                     | Q   | 0.33 |
| -227 | Min. | 4   | SLE                     | Q    | 0.33 | -226 | Max                     | 1    | SLU | 0.47 | -226                    | Min. | 4  | SLE | Q                       | 0.33 | -225 | Max | 1                       | SLU | 0.47 |
| -224 | Max  | 1   | SLU                     | 0.47 | -224 | Min. | 4                       | SLE  | Q   | 0.33 | -223                    | Max  | 1  | SLU | 0.47                    | -223 | Min. | 4   | SLE                     | Q   | 0.33 |
| -222 | Min. | 4   | SLE                     | Q    | 0.33 | -221 | Max                     | 1    | SLU | 0.47 | -221                    | Min. | 4  | SLE | Q                       | 0.33 | -220 | Max | 1                       | SLU | 0.47 |
| -219 | Max  | 1   | SLU                     | 0.47 | -219 | Min. | 4                       | SLE  | Q   | 0.33 | -218                    | Max  | 1  | SLU | 0.47                    | -218 | Min. | 4   | SLE                     | Q   | 0.33 |
| -217 | Min. | 4   | SLE                     | Q    | 0.33 | -216 | Max                     | 1    | SLU | 0.46 | -216</                  |      |    |     |                         |      |      |     |                         |     |      |



|      |      |   |       |      |      |      |   |       |      |      |      |   |       |      |      |      |   |       |      |      |      |   |       |      |      |      |     |       |      |
|------|------|---|-------|------|------|------|---|-------|------|------|------|---|-------|------|------|------|---|-------|------|------|------|---|-------|------|------|------|-----|-------|------|
| -212 | Min. | 4 | SLE Q | 0.33 | -211 | Max  | 1 | SLU   | 0.47 | -211 | Min. | 4 | SLE Q | 0.33 | -210 | Max  | 1 | SLU   | 0.47 | -210 | Min. | 4 | SLE Q | 0.32 |      |      |     |       |      |
| -209 | Max  | 1 | SLU   | 0.46 | -209 | Min. | 4 | SLE Q | 0.32 | -208 | Max  | 1 | SLU   | 0.46 | -208 | Min. | 4 | SLE Q | 0.32 | -207 | Max  | 1 | SLU   | 0.46 | -207 | Min. | 4   | SLE Q | 0.32 |
| -207 | Min. | 4 | SLE Q | 0.32 | -206 | Max  | 1 | SLU   | 0.46 | -206 | Min. | 4 | SLE Q | 0.32 | -205 | Max  | 1 | SLU   | 0.46 | -205 | Min. | 4 | SLE Q | 0.32 |      |      |     |       |      |
| -204 | Max  | 1 | SLU   | 0.46 | -204 | Min. | 4 | SLE Q | 0.32 | -203 | Max  | 1 | SLU   | 0.46 | -203 | Min. | 4 | SLE Q | 0.32 | -202 | Max  | 1 | SLU   | 0.46 | -202 | Min. | 4   | SLE Q | 0.17 |
| -202 | Min. | 4 | SLE Q | 0.32 | -201 | Max  | 1 | SLU   | 0.46 | -201 | Min. | 4 | SLE Q | 0.32 | -200 | Max  | 1 | SLU   | 0.24 | -200 | Min. | 4 | SLE Q | 0.17 |      |      |     |       |      |
| -199 | Max  | 1 | SLU   | 0.24 | -199 | Min. | 4 | SLE Q | 0.18 | -198 | Max  | 1 | SLU   | 0.24 | -198 | Min. | 4 | SLE Q | 0.18 | -197 | Max  | 1 | SLU   | 0.25 | -197 | Min. | 4   | SLE Q | 0.18 |
| -197 | Min. | 4 | SLE Q | 0.18 | -196 | Max  | 1 | SLU   | 0.25 | -196 | Min. | 4 | SLE Q | 0.18 | -195 | Max  | 1 | SLU   | 0.25 | -195 | Min. | 4 | SLE Q | 0.18 |      |      |     |       |      |
| -194 | Max  | 1 | SLU   | 0.25 | -194 | Min. | 4 | SLE Q | 0.18 | -193 | Max  | 1 | SLU   | 0.26 | -193 | Min. | 4 | SLE Q | 0.19 | -192 | Max  | 1 | SLU   | 0.46 | -192 | Min. | 4   | SLE Q | 0.32 |
| -192 | Min. | 4 | SLE Q | 0.32 | -191 | Max  | 1 | SLU   | 0.46 | -191 | Min. | 4 | SLE Q | 0.32 | -190 | Max  | 1 | SLU   | 0.46 | -190 | Min. | 4 | SLE Q | 0.32 |      |      |     |       |      |
| -189 | Max  | 1 | SLU   | 0.46 | -189 | Min. | 4 | SLE Q | 0.32 | -188 | Max  | 1 | SLU   | 0.46 | -188 | Min. | 4 | SLE Q | 0.32 | -187 | Max  | 1 | SLU   | 0.46 | -187 | Min. | 4   | SLE Q | 0.32 |
| -187 | Min. | 4 | SLE Q | 0.32 | -186 | Max  | 1 | SLU   | 0.46 | -186 | Min. | 4 | SLE Q | 0.32 | -185 | Max  | 1 | SLU   | 0.46 | -185 | Min. | 4 | SLE Q | 0.32 |      |      |     |       |      |
| -184 | Max  | 1 | SLU   | 0.24 | -184 | Min. | 4 | SLE Q | 0.17 | -183 | Max  | 1 | SLU   | 0.24 | -183 | Min. | 4 | SLE Q | 0.18 | -182 | Max  | 1 | SLU   | 0.24 | -182 | Min. | 4   | SLE Q | 0.18 |
| -182 | Min. | 4 | SLE Q | 0.18 | -181 | Max  | 1 | SLU   | 0.25 | -181 | Min. | 4 | SLE Q | 0.18 | -180 | Max  | 1 | SLU   | 0.25 | -180 | Min. | 4 | SLE Q | 0.18 |      |      |     |       |      |
| -179 | Max  | 1 | SLU   | 0.25 | -179 | Min. | 4 | SLE Q | 0.18 | -178 | Max  | 1 | SLU   | 0.25 | -178 | Min. | 4 | SLE Q | 0.18 | -177 | Max  | 1 | SLU   | 0.26 | -177 | Min. | 4   | SLE Q | 0.32 |
| -177 | Min. | 4 | SLE Q | 0.19 | -176 | Max  | 1 | SLU   | 0.46 | -176 | Min. | 4 | SLE Q | 0.32 | -175 | Max  | 1 | SLU   | 0.46 | -175 | Min. | 4 | SLE Q | 0.32 |      |      |     |       |      |
| -174 | Max  | 1 | SLU   | 0.46 | -174 | Min. | 4 | SLE Q | 0.32 | -173 | Max  | 1 | SLU   | 0.46 | -173 | Min. | 4 | SLE Q | 0.32 | -172 | Max  | 1 | SLU   | 0.46 | -172 | Min. | 4   | SLE Q | 0.32 |
| -172 | Min. | 4 | SLE Q | 0.32 | -171 | Max  | 1 | SLU   | 0.46 | -171 | Min. | 4 | SLE Q | 0.32 | -170 | Max  | 1 | SLU   | 0.46 | -170 | Min. | 4 | SLE Q | 0.32 |      |      |     |       |      |
| -169 | Max  | 1 | SLU   | 0.46 | -169 | Min. | 4 | SLE Q | 0.32 | -168 | Max  | 1 | SLU   | 0.24 | -168 | Min. | 4 | SLE Q | 0.17 | -167 | Max  | 1 | SLU   | 0.24 | -167 | Min. | 4   | SLE Q | 0.18 |
| -167 | Min. | 4 | SLE Q | 0.18 | -166 | Max  | 1 | SLU   | 0.24 | -166 | Min. | 4 | SLE Q | 0.18 | -165 | Max  | 1 | SLU   | 0.25 | -165 | Min. | 4 | SLE Q | 0.18 |      |      |     |       |      |
| -164 | Max  | 1 | SLU   | 0.25 | -164 | Min. | 4 | SLE Q | 0.18 | -163 | Max  | 1 | SLU   | 0.25 | -163 | Min. | 4 | SLE Q | 0.18 | -162 | Max  | 1 | SLU   | 0.25 | -162 | Min. | 4   | SLE Q | 0.32 |
| -162 | Min. | 4 | SLE Q | 0.18 | -161 | Max  | 1 | SLU   | 0.26 | -161 | Min. | 4 | SLE Q | 0.19 | -152 | Max  | 1 | SLU   | 0.45 | -152 | Min. | 4 | SLE Q | 0.23 |      |      |     |       |      |
| -151 | Max  | 1 | SLU   | 0.45 | -151 | Min. | 4 | SLE Q | 0.32 | -150 | Max  | 1 | SLU   | 0.45 | -150 | Min. | 4 | SLE Q | 0.32 | -149 | Max  | 1 | SLU   | 0.45 | -149 | Min. | 4   | SLE Q | 0.32 |
| -149 | Min. | 4 | SLE Q | 0.32 | -148 | Max  | 1 | SLU   | 0.45 | -148 | Min. | 4 | SLE Q | 0.32 | -147 | Max  | 1 | SLU   | 0.45 | -147 | Min. | 4 | SLE Q | 0.32 |      |      |     |       |      |
| -146 | Max  | 1 | SLU   | 0.45 | -146 | Min. | 4 | SLE Q | 0.32 | -145 | Max  | 1 | SLU   | 0.45 | -145 | Min. | 4 | SLE Q | 0.32 | -144 | Max  | 1 | SLU   | 0.24 | -144 | Min. | 4   | SLE Q | 0.18 |
| -144 | Min. | 4 | SLE Q | 0.17 | -143 | Max  | 1 | SLU   | 0.24 | -143 | Min. | 4 | SLE Q | 0.18 | -142 | Max  | 1 | SLU   | 0.24 | -142 | Min. | 4 | SLE Q | 0.18 |      |      |     |       |      |
| -141 | Max  | 1 | SLU   | 0.25 | -141 | Min. | 4 | SLE Q | 0.18 | -140 | Max  | 1 | SLU   | 0.25 | -140 | Min. | 4 | SLE Q | 0.18 | -139 | Max  | 1 | SLU   | 0.25 | -139 | Min. | 4   | SLE Q | 0.19 |
| -139 | Min. | 4 | SLE Q | 0.18 | -138 | Max  | 1 | SLU   | 0.25 | -138 | Min. | 4 | SLE Q | 0.18 | -137 | Max  | 1 | SLU   | 0.26 | -137 | Min. | 4 | SLE Q | 0.31 |      |      |     |       |      |
| -128 | Max  | 1 | SLU   | 0.45 | -128 | Min. | 4 | SLE Q | 0.31 | -127 | Max  | 1 | SLU   | 0.45 | -127 | Min. | 4 | SLE Q | 0.31 | -124 | Max  | 1 | SLU   | 0.45 | -124 | Min. | 4   | SLE Q | 0.31 |
| -126 | Min. | 4 | SLE Q | 0.31 | -125 | Max  | 1 | SLU   | 0.45 | -125 | Min. | 4 | SLE Q | 0.31 | -122 | Max  | 1 | SLU   | 0.45 | -122 | Min. | 4 | SLE Q | 0.31 |      |      |     |       |      |
| -123 | Max  | 1 | SLU   | 0.45 | -123 | Min. | 4 | SLE Q | 0.31 | -122 | Max  | 1 | SLU   | 0.45 | -122 | Min. | 4 | SLE Q | 0.31 | -119 | Max  | 1 | SLU   | 0.24 | -119 | Min. | 4   | SLE Q | 0.18 |
| -121 | Min. | 4 | SLE Q | 0.31 | -120 | Max  | 1 | SLU   | 0.24 | -120 | Min. | 4 | SLE Q | 0.17 | -117 | Max  | 1 | SLU   | 0.25 | -117 | Min. | 4 | SLE Q | 0.18 |      |      |     |       |      |
| -118 | Max  | 1 | SLU   | 0.24 | -118 | Min. | 4 | SLE Q | 0.18 | -117 | Max  | 1 | SLU   | 0.25 | -117 | Min. | 4 | SLE Q | 0.18 | -114 | Max  | 1 | SLU   | 0.25 | -114 | Min. | 4   | SLE Q | 0.18 |
| -116 | Min. | 4 | SLE Q | 0.18 | -115 | Max  | 1 | SLU   | 0.25 | -115 | Min. | 4 | SLE Q | 0.18 | -114 | Max  | 1 | SLU   | 0.25 | -114 | Min. | 4 | SLE Q | 0.18 |      |      |     |       |      |
| -113 | Max  | 1 | SLU   | 0.26 | -113 | Min. | 4 | SLE Q | 0.19 | -113 | Max  | 1 | SLU   | 0.44 | -113 | Min. | 4 | SLE Q | 0.31 | -110 | Max  | 1 | SLU   | 0.44 | -110 | Min. | 4   | SLE Q | 0.31 |
| -110 | Min. | 4 | SLE Q | 0.31 | -110 | Max  | 1 | SLU   | 0.44 | -110 | Min. | 4 | SLE Q | 0.31 | -109 | Max  | 1 | SLU   | 0.44 | -109 | Min. | 4 | SLE Q | 0.31 |      |      |     |       |      |
| -100 | Max  | 1 | SLU   | 0.44 | -100 | Min. | 4 | SLE Q | 0.31 | -99  | Max  | 1 | SLU   | 0.44 | -99  | Min. | 4 | SLE Q | 0.31 | -98  | Max  | 1 | SLU   | 0.44 | -98  | Min. | 4   | SLE Q | 0.17 |
| -98  | Min. | 4 | SLE Q | 0.31 | -97  | Max  | 1 | SLU   | 0.44 | -97  | Min. | 4 | SLE Q | 0.31 | -94  | Max  | 1 | SLU   | 0.24 | -94  | Min. | 4 | SLE Q | 0.18 |      |      |     |       |      |
| -95  | Max  | 1 | SLU   | 0.24 | -95  | Min. | 4 | SLE Q | 0.18 | -94  | Max  | 1 | SLU   | 0.24 | -94  | Min. | 4 | SLE Q | 0.18 | -91  | Max  | 1 | SLU   | 0.25 | -91  | Min. | 4   | SLE Q | 0.25 |
| -93  | Min. | 4 | SLE Q | 0.18 | -92  | Max  | 1 | SLU   | 0.25 | -92  | Min. | 4 | SLE Q | 0.18 | -89  | Max  | 1 | SLU   | 0.26 | -89  | Min. | 4 | SLE Q | 0.19 |      |      |     |       |      |
| -90  | Max  | 1 | SLU   | 0.25 | -90  | Min. | 4 | SLE Q | 0.18 | -89  | Max  | 1 | SLU   | 0.26 | -89  | Min. | 4 | SLE Q | 0.19 | -78  | Max  | 1 | SLU   | 0.44 | -78  | Min. | 4   | SLE Q | 0.30 |
| -80  | Min. | 4 | SLE Q | 0.30 | -79  | Max  | 1 | SLU   | 0.43 | -79  | Min. | 4 | SLE Q | 0.30 | -76  | Max  | 1 | SLU   | 0.44 | -76  | Min. | 4 | SLE Q | 0.30 |      |      |     |       |      |
| -77  | Max  | 1 | SLU   | 0.44 | -77  | Min. | 4 | SLE Q | 0.30 | -76  | Max  | 1 | SLU   | 0.44 | -76  | Min. | 4 | SLE Q | 0.30 | -73  | Max  | 1 | SLU   | 0.43 | -73  | Min. | 4   | SLE Q | 0.30 |
| -75  | Min. | 4 | SLE Q | 0.30 | -74  | Max  | 1 | SLU   | 0.43 | -74  | Min. | 4 | SLE Q | 0.30 | -71  | Max  | 1 | SLU   | 0.24 | -71  | Min. | 4 | SLE Q | 0.18 |      |      |     |       |      |
| -72  | Max  | 1 | SLU   | 0.24 | -72  | Min. | 4 | SLE Q | 0.17 | -69  | Max  | 1 | SLU   | 0.25 | -69  | Min. | 4 | SLE Q | 0.18 | -68  | Max  | 1 | SLU   | 0.25 | -68  | Min. | 4   | SLE Q | 0.18 |
| -70  | Min. | 4 | SLE Q | 0.18 | -69  | Max  | 1 | SLU   | 0.25 | -66  | Max  | 1 | SLU   | 0.25 | -66  | Min. | 4 | SLE Q | 0.18 | -55  | Max  | 1 | SLU   | 0.43 | -55  | Min. | 4   | SLE Q | 0.30 |
| -67  | Max  | 1 | SLU   | 0.25 | -67  | Min. | 4 | SLE Q | 0.18 | -56  | Max  | 1 | SLU   | 0.43 | -56  | Min. | 4 | SLE Q | 0.30 | -53  | Max  | 1 | SLU   | 0.43 | -53  | Min. | 4   | SLE Q | 0.30 |
| -65  | Min. | 4 | SLE Q | 0.19 | -56  | Max  | 1 | SLU   | 0.43 | -54  | Max  | 1 | SLU   | 0.43 | -54  | Min. | 4 | SLE Q | 0.30 | -50  | Max  | 1 | SLU   | 0.43 | -50  | Min. | 4   | SLE Q | 0.30 |
| -54  | Max  | 1 | SLU   | 0.43 | -54  | Min. | 4 | SLE Q | 0.30 | -51  | Max  | 1 | SLU   | 0.43 | -51  | Min. | 4 | SLE Q | 0.30 | -48  | Max  | 1 | SLU   | 0.44 | -48  | Min. | 4   | SLE Q | 0.17 |
| -52  | Min. | 4 | SLE Q | 0.30 | -51  | Max  | 1 | SLU   | 0.43 | -48  | Max  | 1 | SLU   | 0.24 | -48  | Min. | 4 | SLE Q | 0.17 | -45  | Max  | 1 | SLU   | 0.25 | -45  | Min. | 4   | SLE Q | 0.18 |
| -49  | Max  | 1 | SLU   | 0.43 | -49  | Min. | 4 | SLE Q | 0.30 | -46  | Max  | 1 | SLU   | 0.24 | -46  | Min. | 4 | SLE Q | 0.18 | -43  | Max  | 1 | SLU   | 0.25 | -43  | Min. | 4   | SLE Q | 0.18 |
| -47  | Min. | 4 | SLE Q | 0.18 | -46  | Max  | 1 | SLU   | 0.24 | -43  | Max  | 1 | SLU   | 0.25 | -43  | Min. | 4 | SLE Q | 0.18 | -32  | Max  | 1 | SLU   | 0.42 | -32  | Min. | 4   | SLE Q | 0.30 |
| -44  | Max  | 1 | SLU   | 0.25 | -44  | Min. | 4 | SLE Q | 0.18 | -41  | Max  | 1 | SLU   | 0.26 | -41  | Min. | 4 | SLE Q | 0.19 | -30  | Max  | 1 | SLU   | 0.42 | -30  | Min. | 4   | SLE Q | 0.30 |
| -42  | Min. | 4 | SLE Q | 0.18 | -41  | Max  | 1 | SLU   | 0.26 | -30  | Max  | 1 | SLU   | 0.42 | -30  | Min. | 4 | SLE Q | 0.30 | -27  | Max  | 1 | SLU   | 0.42 | -27  | Min. | 4   | SLE Q | 0.30 |
| -31  | Max  | 1 | SLU   | 0.42 | -31  | Min. | 4 | SLE Q | 0.30 | -28  | Max  | 1 | SLU   | 0.42 | -28  | Min. | 4 | SLE Q | 0.30 | -25  | Max  | 1 | SLU   | 0.42 | -25  | Min. | 4   | SLE Q | 0.30 |
| -29  | Min. | 4 | SLE Q | 0.30 | -28  | Max  | 1 | SLU   | 0.42 | -25  | Max  | 1 | SLU   | 0.42 | -25  | Min. | 4 | SLE Q | 0.30 | -22  | Max  | 1 | SLU   | 0.24 | -22  | Min. | 4   | SLE Q | 0.18 |
| -26  | Max  | 1 | SLU   | 0.42 | -26  | Min. | 4 | SLE Q | 0.30 | -23  | Max  | 1 | SLU   | 0.24 | -23  | Min. | 4 | SLE Q | 0.18 | -20  | Max  | 1 | SLU   | 0.25 | -20  | Min. | 4   | SLE Q | 0.18 |
| -24  | Min. | 4 | SLE Q | 0.17 | -23  | Max  | 1 | SLU   | 0.24 | -21  | Max  | 1 | SLU   | 0.25 | -21  | Min. | 4 | SLE Q | 0.18 | -18  | Max  | 1 | SLU   | 0.25 | -18  | Min. | 4</ |       |      |



|                        | CC | TCC | Nodo | Min. | CC | TCC | Nodo | Max |                        | CC | TCC | Nodo | Min. | CC | TCC | Nodo | Max  |      |
|------------------------|----|-----|------|------|----|-----|------|-----|------------------------|----|-----|------|------|----|-----|------|------|------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -423 | -282 | 1  | SLU | -348 | 709 | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -428 | -516 | 2  | SLE | R    | -352 | -345 |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -24  | -147 | 1  | SLU | -18  | 133 | $M_{xx}$ <daNm/m>      | 1  | SLU | -345 | -0   | 1  | SLU |      | -427 | 0    |
| $M_{zz}$ <daNm/m>      | 1  | SLU | -351 | -0   | 1  | SLU | -427 | 0   | $M_{xz}$ <daNm/m>      | 1  | SLU | -420 | -1   | 1  | SLU |      | -347 | 1    |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU | -420 | -34  | 1  | SLU | -350 | 7   | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -348 | -32  | 1  | SLU |      | -17  | 29   |

Bid. 12

|                        | CC | TCC | Nodo | Min. | CC | TCC | Nodo | Max  |                      | CC                     | TCC | Nodo | Min. | CC   | TCC | Nodo | Max  |      |      |
|------------------------|----|-----|------|------|----|-----|------|------|----------------------|------------------------|-----|------|------|------|-----|------|------|------|------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -344 | -813 | 2  | SLE | R    | -366 | -0                   | $\sigma_{zz}$ <daN/mq> | 1   | SLU  | -72  | -525 | 4   | SLE  | Q    | -360 | -346 |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -96  | -153 | 1  | SLU | -362 | 153  | $M_{xx}$ <daNm/m>    | 1                      | SLU | -200 | -0   | 1    | SLU |      | -360 | 0    |      |
| $M_{zz}$ <daNm/m>      | 1  | SLU | -184 | -0   | 1  | SLU | -360 | 0    | $M_{xz}$ <daNm/m>    | 1                      | SLU | -72  | -1   | 1    | SLU |      | -364 | 1    |      |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU | -200 | -19  | 1  | SLU | -364 | 6    | $\tau_{xy}$ <daN/mq> | 1                      | SLU | -200 | -20  | 1    | SLU |      | -352 | 20   |      |

Bid. 13

|                        | CC | TCC | Nodo | Min. | CC | TCC | Nodo | Max |                        | CC | TCC | Nodo | Min. | CC | TCC | Nodo | Max  |      |
|------------------------|----|-----|------|------|----|-----|------|-----|------------------------|----|-----|------|------|----|-----|------|------|------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -384 | -282 | 1  | SLU | -197 | 709 | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -380 | -516 | 2  | SLE | R    | -373 | -345 |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -369 | -133 | 1  | SLU | -373 | 147 | $M_{xx}$ <daNm/m>      | 1  | SLU | -193 | -0   | 1  | SLU |      | -382 | 0    |
| $M_{zz}$ <daNm/m>      | 1  | SLU | -372 | -0   | 1  | SLU | -382 | 0   | $M_{xz}$ <daNm/m>      | 1  | SLU | -195 | -1   | 1  | SLU |      | -378 | 1    |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU | -380 | -34  | 1  | SLU | -373 | 7   | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -380 | -29  | 1  | SLU |      | -196 | 32   |

Bid. 14

|                        | CC | TCC | Nodo | Min.  | CC | TCC | Nodo | Max  |                      | CC                     | TCC | Nodo | Min. | CC   | TCC | Nodo | Max  |      |      |
|------------------------|----|-----|------|-------|----|-----|------|------|----------------------|------------------------|-----|------|------|------|-----|------|------|------|------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -89  | -1902 | 2  | SLE | R    | -367 | -75                  | $\sigma_{zz}$ <daN/mq> | 1   | SLU  | -41  | -537 | 4   | SLE  | Q    | -359 | -322 |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -137 | -308  | 1  | SLU | -357 | 308  | $M_{xx}$ <daNm/m>    | 1                      | SLU | -177 | -0   | 1    | SLU |      | -359 | 0    |      |
| $M_{zz}$ <daNm/m>      | 1  | SLU | -161 | -0    | 1  | SLU | -359 | 0    | $M_{xz}$ <daNm/m>    | 1                      | SLU | -161 | -1   | 1    | SLU |      | -355 | 1    |      |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU | -17  | -26   | 1  | SLU | -355 | 7    | $\tau_{xy}$ <daN/mq> | 1                      | SLU | -17  | -30  | 1    | SLU |      | -367 | 30   |      |

Verifiche e armature solette/platee

Simbologia

- $\Delta_{sm}$  = Distanza media tra le fessure
- $\Phi_{eq}$  = Diametro equivalente delle barre
- $\epsilon_{sm}$  = Deformazione unitaria media dell'armatura (\*1000)
- $\sigma_c$  = Tensione nel calcestruzzo
- $\sigma_f$  = Tensione nel ferro
- $\sigma_s$  = Tensione nell'acciaio nella sezione fessurata
- $A_{c\text{-eff}}$  = Area di calcestruzzo efficace
- $A_s$  = Area complessiva dei ferri nell'area di calcestruzzo efficace
- Afe I = Area di ferro effettiva totale presente nel punto di verifica, inferiore
- Afe S = Area di ferro effettiva totale presente nel punto di verifica, superiore
- Afe St. = Area di ferro effettiva della staffatura
- CC = Numero della combinazione delle condizioni di carico elementari
- Cf inf = Coprifermo inferiore
- Cf sup = Coprifermo superiore
- Cls = Tipo di calcestruzzo
- DV = Direzione di verifica
- XX = Verifica per momento Mxx
- YY = Verifica per momento Myy
- Fcd = Resistenza di calcolo a compressione del calcestruzzo
- Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo
- Fctd = Resistenza di calcolo a trazione del calcestruzzo
- Fctk = Resistenza caratteristica a trazione del calcestruzzo
- Fyd = Resistenza di calcolo dell'acciaio
- Fyk = Tensione caratteristica di snervamento dell'acciaio
- $K_3$  = Coefficiente per distribuzione deformazioni
- MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y
- Mom = Momento flettente
- My = Momento flettente intorno all'asse Y
- Nodo = Numero del nodo
- Sic. = Sicurezza
- Spess. = Spessore
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- Tp = Tipo di acciaio
- VRcd = Taglio ultimo lato calcestruzzo
- VRsd = Taglio ultimo lato armatura
- Vrdu = Taglio ultimo resistente
- Vsdu = Taglio agente nella direzione del momento ultimo
- Wk = Ampiezza caratteristica delle fessure
- X = Coordinata X del nodo
- Y = Coordinata Y del nodo
- c = Ricoprimento dell'armatura
- ctg $\theta$  = Cotangente dell'angolo di inclinazione dei puntoni di calcestruzzo
- s = Distanza massima tra le barre

Armatura platea a quota 0.00

Caratteristiche delle sezioni e dei materiali utilizzati

| Spess. | Cf sup | Cf inf | Cls    | Fck       | Fctk      | Fcd       | Fctd      | Tp    | Fyk       | Fyd       |
|--------|--------|--------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
| <cm>   | <cm>   | <cm>   |        | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| 50.00  | 3.50   | 3.50   | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Stato limite ultimo - Verifiche a flessione/presoflessione

| Nodo | X     | Y    | DV | CC | TCC | Afe S | Afe I | My      | MRdy      | Sic.   |
|------|-------|------|----|----|-----|-------|-------|---------|-----------|--------|
| <m>  | <m>   | <m>  |    |    |     | <cmq> | <cmq> | <daNm>  | <daNm>    |        |
| -236 | 2.50  | 7.50 | XX | 1  | SLU | 7.70  | 7.70  | 1050.19 | 13950.30  | 13.284 |
| -181 | 23.00 | 4.50 | XX | 1  | SLU | 7.70  | 7.70  | -59.34  | -13950.30 | >100   |
| -403 | 20.50 | 3.00 | XX | 1  | SLU | 7.70  | 7.70  | 96.68   | 13950.30  | >100   |
| -237 | 3.00  | 7.50 | YY | 1  | SLU | 7.70  | 7.70  | 2039.93 | 13950.30  | 6.839  |
| -21  | 23.00 | 1.00 | YY | 1  | SLU | 7.70  | 7.70  | -14.81  | -13950.30 | >100   |
| -403 | 20.50 | 3.00 | YY | 1  | SLU | 7.70  | 7.70  | 215.43  | 13950.30  | 64.757 |



Stato limite ultimo - Verifiche a taglio

| Nodo | X     | Y    | DV | CC | TCC | Aff S | Aff I | Aff St. | Vsdu   | ctgθ | VRcd  | VRsd  | Vrdu     | Sic.   |
|------|-------|------|----|----|-----|-------|-------|---------|--------|------|-------|-------|----------|--------|
| <m>  | <m>   | <m>  |    |    |     | <cmq> | <cmq> | <cmq/m> | <daN>  |      | <daN> | <daN> | <daN>    |        |
| -218 | 1.50  | 6.50 | XX | 1  | SLU | 7.70  | 7.70  |         | 852.12 |      |       |       | 19980.80 | 23.448 |
| -115 | 22.00 | 3.00 | XX | 1  | SLU | 7.70  | 7.70  |         | 179.15 |      |       |       | 19980.80 | >100   |
| -52  | 2.50  | 2.00 | YY | 1  | SLU | 7.70  | 7.70  |         | 976.72 |      |       |       | 19980.80 | 20.457 |
| -413 | 20.50 | 2.00 | YY | 1  | SLU | 7.70  | 7.70  |         | 257.66 |      |       |       | 19980.80 | 77.547 |

Stato limite d'esercizio - Verifiche tensionali

| Nodo | X     | Y    | DV | CC | TCC   | Aff S | Aff I | Mom     | σ <sub>c</sub> | σ <sub>f</sub> |
|------|-------|------|----|----|-------|-------|-------|---------|----------------|----------------|
| <m>  | <m>   | <m>  |    |    |       | <cmq> | <cmq> | <daNm>  | <daN/cmq>      | <daN/cmq>      |
| -237 | 3.00  | 7.50 | XX | 2  | SLE R | 7.70  | 7.70  | 700.12  | 3.20           | 209.00         |
| -236 | 2.50  | 7.50 | XX | 4  | SLE Q | 7.70  | 7.70  | 717.27  | 3.28           | 214.12         |
| -116 | 22.50 | 3.00 | XX | 2  | SLE R | 7.70  | 7.70  | -57.03  | 0.26           | 17.02          |
| -92  | 22.50 | 2.50 | XX | 4  | SLE Q | 7.70  | 7.70  | -48.37  | 0.22           | 14.44          |
| -403 | 20.50 | 3.00 | XX | 4  | SLE Q | 7.70  | 7.70  | 60.92   | 0.28           | 18.19          |
| -403 | 20.50 | 3.00 | XX | 2  | SLE R | 7.70  | 7.70  | 45.94   | 0.21           | 13.71          |
| -236 | 2.50  | 7.50 | YY | 2  | SLE R | 7.70  | 7.70  | 1359.95 | 6.21           | 405.96         |
| -236 | 2.50  | 7.50 | YY | 4  | SLE Q | 7.70  | 7.70  | 1393.26 | 6.36           | 415.90         |
| -21  | 23.00 | 1.00 | YY | 2  | SLE R | 7.70  | 7.70  | -13.16  | 0.06           | 3.93           |
| -21  | 23.00 | 1.00 | YY | 4  | SLE Q | 7.70  | 7.70  | -11.96  | 0.05           | 3.57           |
| -403 | 20.50 | 3.00 | YY | 2  | SLE R | 7.70  | 7.70  | 129.06  | 0.59           | 38.53          |
| -403 | 20.50 | 3.00 | YY | 4  | SLE Q | 7.70  | 7.70  | 152.06  | 0.69           | 45.39          |

Stato limite d'esercizio - Verifiche a fessurazione

| Nodo | X     | Y    | DV | CC | TCC   | c     | s      | K <sub>2</sub> | Φ <sub>eq</sub> | A <sub>sm</sub> | A <sub>s</sub> | A <sub>c eff</sub> | σ <sub>s</sub> | ε <sub>sm</sub> | Wk   |
|------|-------|------|----|----|-------|-------|--------|----------------|-----------------|-----------------|----------------|--------------------|----------------|-----------------|------|
| <m>  | <m>   | <m>  |    |    |       | <mm>  | <mm>   |                |                 | <mm>            | <cmq>          | <cmq>              | <daN/cmq>      |                 | <mm> |
| -236 | 2.50  | 7.50 | XX | 4  | SLE Q | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 214.12         | 0.06            | 0.03 |
| -236 | 2.50  | 7.50 | XX | 3  | SLE F | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 211.56         | 0.06            | 0.03 |
| -92  | 22.50 | 2.50 | XX | 4  | SLE Q | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 14.44          | 0.00            | 0.00 |
| -116 | 22.50 | 3.00 | XX | 3  | SLE F | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 15.73          | 0.00            | 0.00 |
| -403 | 20.50 | 3.00 | XX | 4  | SLE Q | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 18.19          | 0.01            | 0.00 |
| -403 | 20.50 | 3.00 | XX | 3  | SLE F | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 15.95          | 0.00            | 0.00 |
| -236 | 2.50  | 7.50 | YY | 4  | SLE Q | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 415.90         | 0.12            | 0.06 |
| -236 | 2.50  | 7.50 | YY | 3  | SLE F | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 410.93         | 0.12            | 0.06 |
| -21  | 23.00 | 1.00 | YY | 4  | SLE Q | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 3.57           | 0.00            | 0.00 |
| -21  | 23.00 | 1.00 | YY | 3  | SLE F | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 3.75           | 0.00            | 0.00 |
| -403 | 20.50 | 3.00 | YY | 4  | SLE Q | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 45.39          | 0.01            | 0.01 |
| -403 | 20.50 | 3.00 | YY | 3  | SLE F | 28.00 | 200.00 | 0.50           | 14.00           | 309.89          | 9.24           | 875.00             | 41.96          | 0.01            | 0.01 |

Verifiche e armature pareti

Simbologia

- A<sub>sm</sub> = Distanza media tra le fessure
- Φ<sub>eq</sub> = Diametro equivalente delle barre
- ε<sub>sm</sub> = Deformazione unitaria media dell'armatura (\*1000)
- σ<sub>c</sub> = Tensione nel calcestruzzo
- σ<sub>f</sub> = Tensione nel ferro
- σ<sub>s</sub> = Tensione nell'acciaio nella sezione fessurata
- A<sub>c eff</sub> = Area di calcestruzzo efficace
- A<sub>s</sub> = Area complessiva dei ferri nell'area di calcestruzzo efficace
- CC = Numero della combinazione delle condizioni di carico elementari
- Cf = Copriferro
- Cls = Tipo di calcestruzzo
- Fcd = Resistenza di calcolo a compressione del calcestruzzo
- Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo
- Fctd = Resistenza di calcolo a trazione del calcestruzzo
- Fctk = Resistenza caratteristica a trazione del calcestruzzo
- Fyd = Resistenza di calcolo dell'acciaio
- Fyk = Tensione caratteristica di snervamento dell'acciaio
- K<sub>2</sub> = Coefficiente per distribuzione deformazioni
- M'ydy = Momento resistente massimo in campo sostanzialmente elastico intorno all'asse Y
- MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y
- M<sub>y</sub> = Momento flettente intorno all'asse Y
- N = Sforzo normale
- Nu = Sforzo normale ultimo
- Sez. = Sezione di verifica
- Sic. = Sicurezza
- Spess. = Spessore
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- Tp = Tipo di acciaio
- VRcd = Taglio ultimo lato calcestruzzo
- VRsd = Taglio ultimo lato armatura
- Vrdu = Taglio ultimo resistente
- Vsdu = Taglio agente nella direzione del momento ultimo
- Wk = Ampiezza caratteristica delle fessure
- Xf = Coordinata X finale
- Xi = Coordinata X iniziale
- Xv = Coordinata X di verifica
- Zona = Zona di verifica
- Zv = Coordinata Z di verifica
- c = Ricoprimento dell'armatura
- s = Distanza massima tra le barre

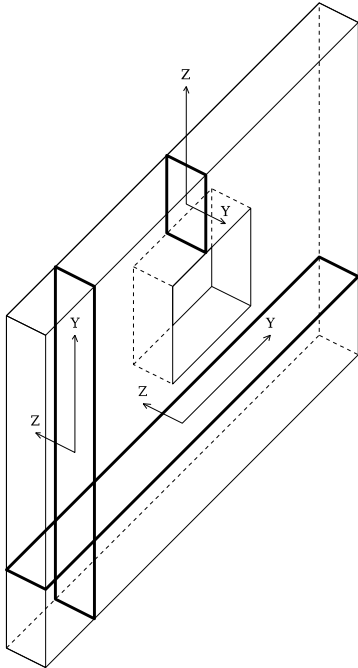


Figura numero 1: Riferimenti sezione

Parete n. 11

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | TP    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
| <cm>  | <cm>   | <cm> | <cm>   | <daN/cm²> | <daN/cm²> | <daN/cm²> | <daN/cm²> |       | <daN/cm²> | <daN/cm²> |
| Oriz. | 15.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali

Stato limite ultimo - Verifiche a flessione/presoflessione

| CC | Zona  | Zv   | Xi   | Xf   | N       | My     | Nu          | MRdy      | Sic. |
|----|-------|------|------|------|---------|--------|-------------|-----------|------|
|    |       | <m>  | <m>  | <m>  | <daN>   | <daNm> | <daN>       | <daNm>    |      |
| 1  | Diff. | 0.00 | 0.00 | 6.00 | -879.92 | -1.07  | -1976440.00 | -17308.10 | >100 |
| 1  | Diff. | 0.15 | 0.00 | 6.00 | -441.17 | -0.38  | -1976440.00 | -17290.60 | >100 |
| 1  | Diff. | 0.30 | 0.00 | 6.00 | -2.42   | 0.32   | -2.42       | 17273.00  | >100 |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv   | Xi   | Xf   | N       | My     | σc        | σt        |
|----|-------|-------|------|------|------|---------|--------|-----------|-----------|
|    |       |       | <m>  | <m>  | <m>  | <daN>   | <daNm> | <daN/cm²> | <daN/cm²> |
| 2  | SLE R | Diff. | 0.00 | 0.00 | 6.00 | -676.65 | -0.65  | 0.07      | 1.02      |
| 4  | SLE Q | Diff. | 0.00 | 0.00 | 6.00 | -676.83 | -0.77  | 0.07      | 1.03      |
| 2  | SLE R | Diff. | 0.15 | 0.00 | 6.00 | -339.15 | -0.22  | 0.03      | 0.51      |
| 4  | SLE Q | Diff. | 0.15 | 0.00 | 6.00 | -339.33 | -0.27  | 0.03      | 0.51      |
| 2  | SLE R | Diff. | 0.30 | 0.00 | 6.00 | -1.65   | 0.20   | 0.00      | 0.03      |
| 4  | SLE Q | Diff. | 0.30 | 0.00 | 6.00 | -1.83   | 0.23   | 0.00      | 0.04      |

Parete n. 12

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | TP    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
| <cm>  | <cm>   | <cm> | <cm>   | <daN/cm²> | <daN/cm²> | <daN/cm²> | <daN/cm²> |       | <daN/cm²> | <daN/cm²> |
| Oriz. | 15.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali

Stato limite ultimo - Verifiche a flessione/presoflessione

| CC | Zona  | Zv   | Xi   | Xf   | N       | My     | Nu          | MRdy      | Sic. |
|----|-------|------|------|------|---------|--------|-------------|-----------|------|
|    |       | <m>  | <m>  | <m>  | <daN>   | <daNm> | <daN>       | <daNm>    |      |
| 1  | Diff. | 0.00 | 0.00 | 4.00 | -582.50 | -0.78  | -1323520.00 | -11770.60 | >100 |
| 1  | Diff. | 0.15 | 0.00 | 4.00 | -290.00 | -0.27  | -1323520.00 | -11759.00 | >100 |
| 1  | Diff. | 0.30 | 0.00 | 4.00 | 2.50    | 0.24   | 2.50        | 11746.90  | >100 |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv   | Xi   | Xf   | N       | My     | σc        | σt        |
|----|-------|-------|------|------|------|---------|--------|-----------|-----------|
|    |       |       | <m>  | <m>  | <m>  | <daN>   | <daNm> | <daN/cm²> | <daN/cm²> |
| 2  | SLE R | Diff. | 0.00 | 0.00 | 4.00 | -448.29 | -0.45  | 0.07      | 1.01      |
| 4  | SLE Q | Diff. | 0.00 | 0.00 | 4.00 | -448.10 | -0.55  | 0.07      | 1.02      |
| 2  | SLE R | Diff. | 0.15 | 0.00 | 4.00 | -223.29 | -0.15  | 0.03      | 0.50      |
| 4  | SLE Q | Diff. | 0.15 | 0.00 | 4.00 | -223.10 | -0.19  | 0.03      | 0.50      |
| 2  | SLE R | Diff. | 0.30 | 0.00 | 4.00 | 1.71    | 0.15   | 0.00      | 0.10      |
| 4  | SLE Q | Diff. | 0.30 | 0.00 | 4.00 | 1.90    | 0.17   | 0.00      | 0.11      |

Parete n. 13

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | TP    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
| <cm>  | <cm>   | <cm> | <cm>   | <daN/cm²> | <daN/cm²> | <daN/cm²> | <daN/cm²> |       | <daN/cm²> | <daN/cm²> |
| Oriz. | 15.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali  
Stato limite ultimo - Verifiche a flessione/presoflessione

| CC | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | Nu<br><daN> | MRdy<br><daNm> | Sic. |
|----|-------|-----------|-----------|-----------|------------|--------------|-------------|----------------|------|
| 1  | Diff. | 0.00      | 0.00      | 6.00      | -879.92    | -1.07        | -1976440.00 | -17308.10      | >100 |
| 1  | Diff. | 0.15      | 0.00      | 6.00      | -441.17    | -0.38        | -1976440.00 | -17290.50      | >100 |
| 1  | Diff. | 0.30      | 0.00      | 6.00      | -2.42      | 0.32         | -2.42       | 17273.10       | >100 |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | $\sigma_c$<br><daN/cm <sup>2</sup> > | $\sigma_f$<br><daN/cm <sup>2</sup> > |
|----|-------|-------|-----------|-----------|-----------|------------|--------------|--------------------------------------|--------------------------------------|
| 2  | SLE R | Diff. | 0.00      | 0.00      | 6.00      | -676.65    | -0.65        | 0.07                                 | 1.02                                 |
| 4  | SLE Q | Diff. | 0.00      | 0.00      | 6.00      | -676.83    | -0.77        | 0.07                                 | 1.03                                 |
| 2  | SLE R | Diff. | 0.15      | 0.00      | 6.00      | -339.15    | -0.22        | 0.03                                 | 0.51                                 |
| 4  | SLE Q | Diff. | 0.15      | 0.00      | 6.00      | -339.33    | -0.27        | 0.03                                 | 0.51                                 |
| 2  | SLE R | Diff. | 0.30      | 0.00      | 6.00      | -1.65      | 0.20         | 0.00                                 | 0.03                                 |
| 4  | SLE Q | Diff. | 0.30      | 0.00      | 6.00      | -1.83      | 0.23         | 0.00                                 | 0.04                                 |

Parete n. 14

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess.<br><cm> | Cf<br><cm> | Cl <sub>s</sub> | F <sub>ck</sub><br><daN/cm <sup>2</sup> > | F <sub>ctk</sub><br><daN/cm <sup>2</sup> > | F <sub>cd</sub><br><daN/cm <sup>2</sup> > | F <sub>ctd</sub><br><daN/cm <sup>2</sup> > | Tp    | F <sub>yk</sub><br><daN/cm <sup>2</sup> > | F <sub>yd</sub><br><daN/cm <sup>2</sup> > |
|-------|----------------|------------|-----------------|-------------------------------------------|--------------------------------------------|-------------------------------------------|--------------------------------------------|-------|-------------------------------------------|-------------------------------------------|
| Oriz. | 15.00          | 4.30       | C32/40          | 332.00                                    | 21.69                                      | 188.13                                    | 14.46                                      | B450C | 4500.00                                   | 3913.04                                   |

Verifiche su sezioni orizzontali  
Stato limite ultimo - Verifiche a flessione/presoflessione

| CC | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | Nu<br><daN> | MRdy<br><daNm> | Sic. |
|----|-------|-----------|-----------|-----------|------------|--------------|-------------|----------------|------|
| 1  | Diff. | 0.00      | 0.00      | 4.00      | -582.66    | -1.14        | -1323520.00 | -11770.60      | >100 |
| 1  | Diff. | 0.15      | 0.00      | 4.00      | -290.16    | -0.43        | -1323520.00 | -11759.00      | >100 |
| 1  | Diff. | 0.30      | 0.00      | 4.00      | 2.34       | 0.27         | 2.34        | 11746.90       | >100 |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | $\sigma_c$<br><daN/cm <sup>2</sup> > | $\sigma_f$<br><daN/cm <sup>2</sup> > |
|----|-------|-------|-----------|-----------|-----------|------------|--------------|--------------------------------------|--------------------------------------|
| 2  | SLE R | Diff. | 0.00      | 0.00      | 4.00      | -448.40    | -0.69        | 0.07                                 | 1.02                                 |
| 4  | SLE Q | Diff. | 0.00      | 0.00      | 4.00      | -448.24    | -0.81        | 0.07                                 | 1.03                                 |
| 2  | SLE R | Diff. | 0.15      | 0.00      | 4.00      | -223.40    | -0.26        | 0.03                                 | 0.51                                 |
| 4  | SLE Q | Diff. | 0.15      | 0.00      | 4.00      | -223.24    | -0.31        | 0.04                                 | 0.51                                 |
| 2  | SLE R | Diff. | 0.30      | 0.00      | 4.00      | 1.60       | 0.17         | 0.00                                 | 0.11                                 |
| 4  | SLE Q | Diff. | 0.30      | 0.00      | 4.00      | 1.76       | 0.20         | 0.00                                 | 0.12                                 |

## 8.0 RISULTATI STRUTTURE FONDAZIONE CABINE

### 8.1 Diagrammi tassi di sfruttamento

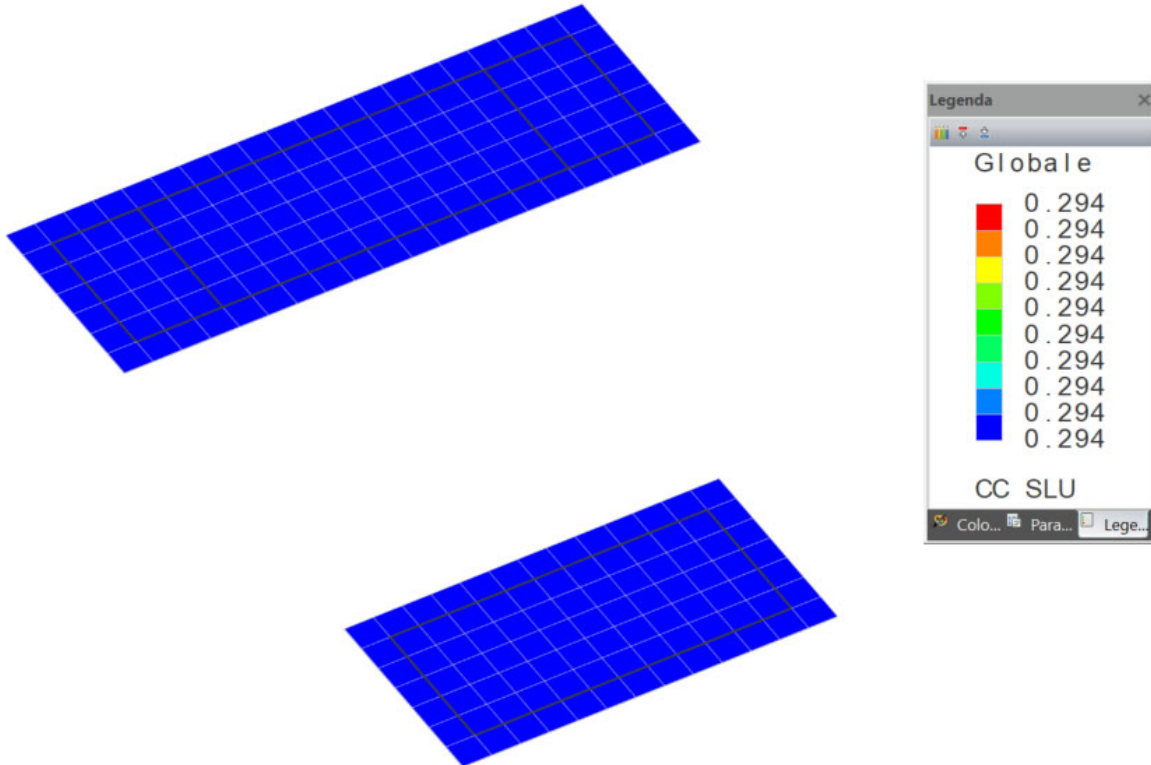
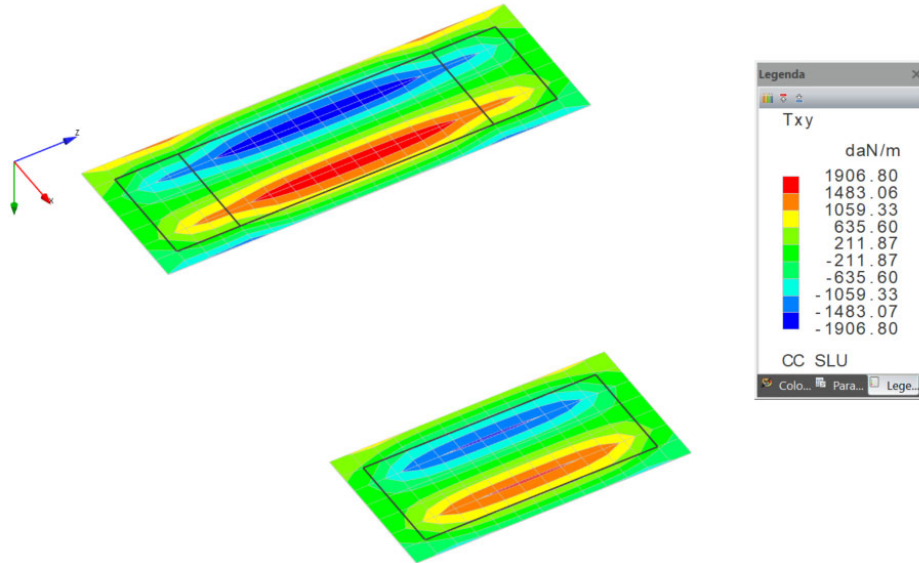


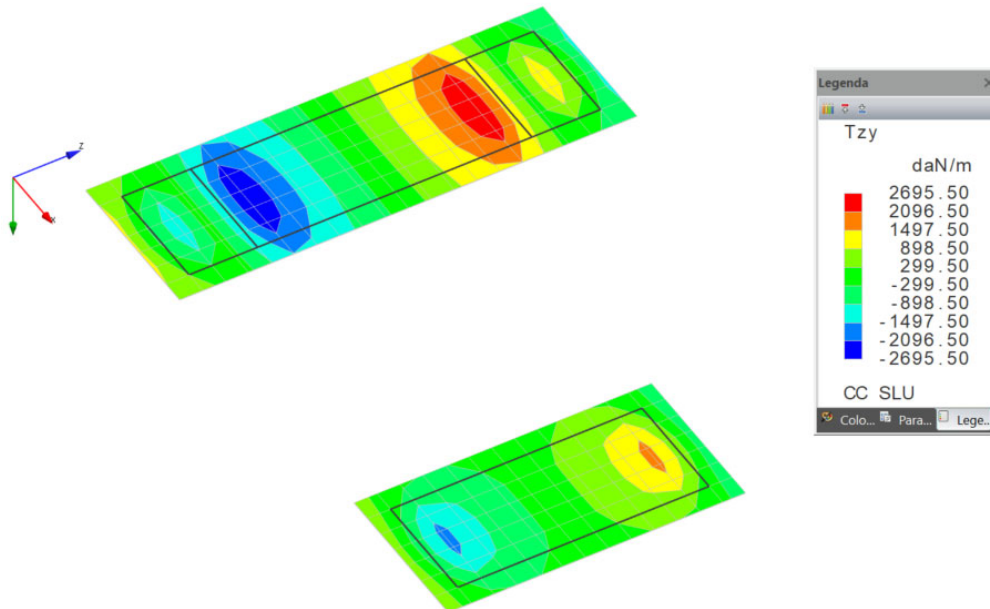
Diagramma tassi di sfruttamento resistenza combo SLU con valore massimo pari a 0,294

**Figure 40: Tassi di sfruttamento SLU (Stato limite ultimo)**

## 8.2 Sollecitazioni



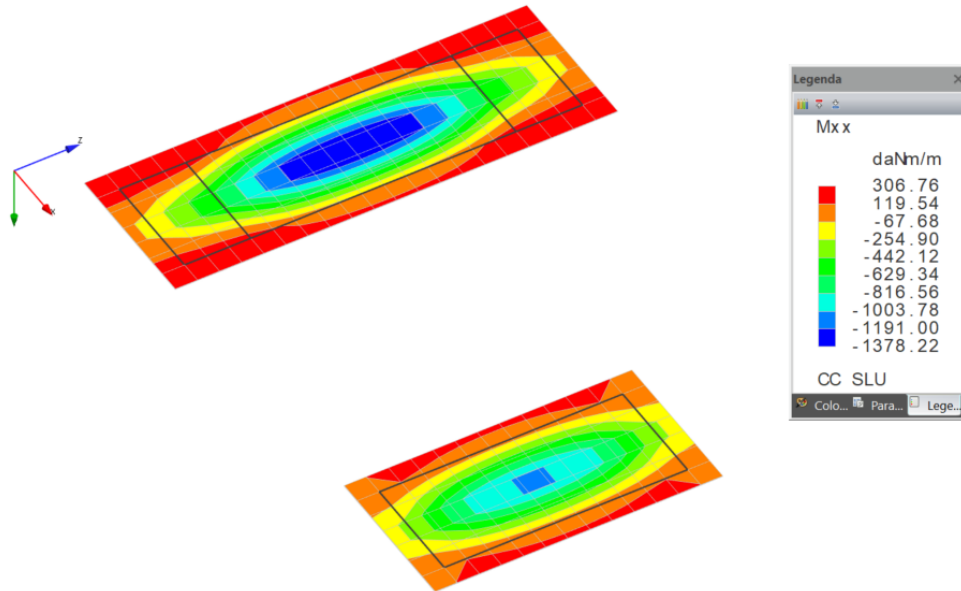
Involuppo sforzo di taglio in direzione X su faccia con normale Y SLU  $T_{max} = 1906,80$  daN/m



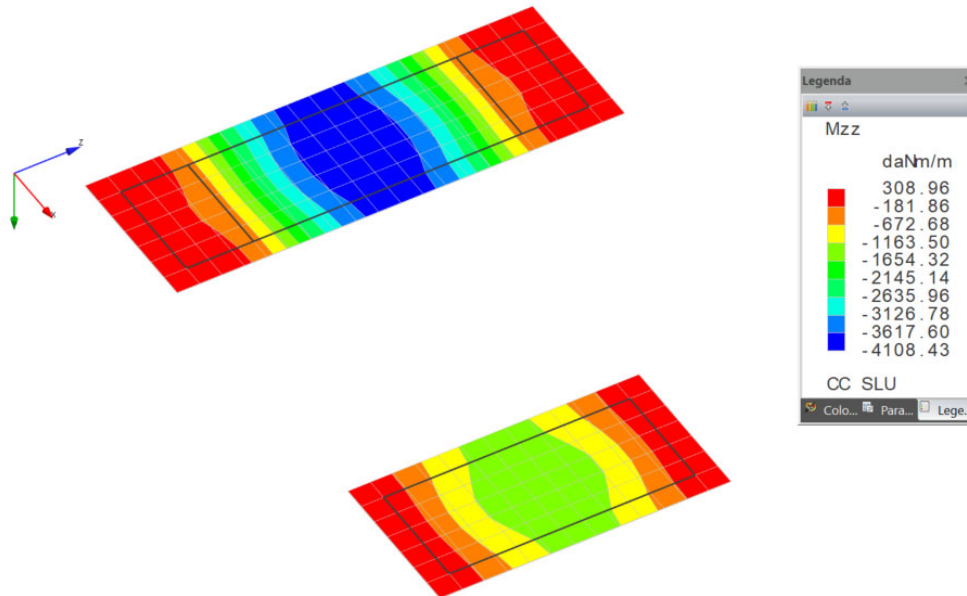
Involuppo sforzo di taglio in direzione Z su faccia con normale Y SLU  $T_{max} = 2695,5$  daN/m

**Figure 41: Taglio**





Inviluppo momento che genera tensioni in direzioni X su facce con normale X SLU Mmax = 1378,22 daN×m/m



Inviluppo momento che genera tensioni in direzioni Z su facce con normale Z SLU Mmax = 4108,43 daN×m/m

**Figure 42: Momento Flettente**

## 8.1 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

### Risultati del calcolo

#### Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:  
 ModeSt ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato  
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:  
 Xfinest ver. 9.5.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18

Tipo di calcolo: statico

Vincoli esterni: Considera sempre vincoli assegnati in modellazione

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

#### Generazione combinazioni

- Lineari: Si
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

#### Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente

#### Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Si
- Check sequenza di Sturm: Si
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

#### Dati struttura

- Edificio esistente: No
- Tipo di opera: Opera ordinaria
- Vita nominale  $V_N$ : 50.00
- Classe d'uso: Classe II
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

#### Ambienti di carico

##### Simbologia

N = Numero

Comm. = Commento

1 = G1 - permanenti strutturali

2 = G2 - permanenti non strutturali

3 = Q - Variabili cat. E

F = azioni orizzontali convenzionali

SLU = Stato limite ultimo

SLR = Stato limite per combinazioni rare

SLF = Stato limite per combinazioni frequenti

SLQ/D = Stato limite per combinazioni quasi permanenti o di danno

S = Si

N = No

| N | Comm.           | 1 | 2 | 3 | SLU | SLR | SLF | SLQ |
|---|-----------------|---|---|---|-----|-----|-----|-----|
| 1 | Calcolo statico | S | S | S | S   | S   | S   | S   |

#### Elenco combinazioni di carico simboliche

##### Simbologia

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| CC | Comm.          | TCC   | 1     | 2     | 3        |
|----|----------------|-------|-------|-------|----------|
| 1  | Amb. 1 (SLU)   | SLU   | y max | y max | y max    |
| 2  | Amb. 1 (SLE R) | SLE R | 1     | 1     | 1        |
| 3  | Amb. 1 (SLE F) | SLE F | 1     | 1     | $\psi_1$ |
| 4  | Amb. 1 (SLE Q) | SLE Q | 1     | 1     | $\psi_2$ |

Genera le combinazioni con un solo carico di tipo variabile come di base: Si

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia



An. = Tipo di analisi  
 L = Lineare  
 NL = Non lineare  
 Bk = Buckling  
 S = Si  
 N = No  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Comm. = Commento  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| CC | Comm.          | TCC   | An. | Bk | 1    | 2    | 3    |
|----|----------------|-------|-----|----|------|------|------|
| 1  | Amb. 1 (SLU)   | SLU   | L   | N  | 1.30 | 1.50 | 1.50 |
| 2  | Amb. 1 (SLE R) | SLE R | L   | N  | 1.00 | 1.00 | 1.00 |
| 3  | Amb. 1 (SLE F) | SLE F | L   | N  | 1.00 | 1.00 | 0.90 |
| 4  | Amb. 1 (SLE Q) | SLE Q | L   | N  | 1.00 | 1.00 | 0.80 |

Tensioni sul terreno

Simbologia  
 $\sigma_t$  = Tensione sul terreno  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Nodo = Numero del nodo  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| Nodo | CC   | TCC | $\sigma_t$<br><daN/cm <sup>2</sup> > | Nodo | CC   | TCC  | $\sigma_t$<br><daN/cm <sup>2</sup> > | Nodo  | CC   | TCC  | $\sigma_t$<br><daN/cm <sup>2</sup> > | Nodo | CC    | TCC  | $\sigma_t$<br><daN/cm <sup>2</sup> > | Nodo | CC | TCC   | $\sigma_t$<br><daN/cm <sup>2</sup> > |      |      |   |       |      |
|------|------|-----|--------------------------------------|------|------|------|--------------------------------------|-------|------|------|--------------------------------------|------|-------|------|--------------------------------------|------|----|-------|--------------------------------------|------|------|---|-------|------|
| -280 | Max  | 1   | SLU                                  | 0.60 | -280 | Min. | 4                                    | SLE Q | 0.41 | -279 | Max                                  | 1    | SLU   | 0.60 | -279                                 | Min. | 4  | SLE Q | 0.41                                 |      |      |   |       |      |
| -278 | Min. | 4   | SLE Q                                | 0.41 | -277 | Max  | 1                                    | SLU   | 0.60 | -277 | Min.                                 | 4    | SLE Q | 0.41 | -276                                 | Max  | 1  | SLU   | 0.60                                 | -276 | Min. | 4 | SLE Q | 0.41 |
| -275 | Max  | 1   | SLU                                  | 0.60 | -275 | Min. | 4                                    | SLE Q | 0.41 | -274 | Max                                  | 1    | SLU   | 0.60 | -274                                 | Min. | 4  | SLE Q | 0.41                                 | -273 | Max  | 1 | SLU   | 0.60 |
| -273 | Min. | 4   | SLE Q                                | 0.41 | -272 | Max  | 1                                    | SLU   | 0.59 | -272 | Min.                                 | 4    | SLE Q | 0.40 | -271                                 | Max  | 1  | SLU   | 0.59                                 | -271 | Min. | 4 | SLE Q | 0.40 |
| -270 | Max  | 1   | SLU                                  | 0.59 | -270 | Min. | 4                                    | SLE Q | 0.40 | -269 | Max                                  | 1    | SLU   | 0.59 | -269                                 | Min. | 4  | SLE Q | 0.40                                 | -268 | Max  | 1 | SLU   | 0.59 |
| -268 | Min. | 4   | SLE Q                                | 0.40 | -267 | Max  | 1                                    | SLU   | 0.59 | -267 | Min.                                 | 4    | SLE Q | 0.40 | -266                                 | Max  | 1  | SLU   | 0.59                                 | -266 | Min. | 4 | SLE Q | 0.40 |
| -265 | Max  | 1   | SLU                                  | 0.59 | -265 | Min. | 4                                    | SLE Q | 0.40 | -264 | Max                                  | 1    | SLU   | 0.58 | -264                                 | Min. | 4  | SLE Q | 0.40                                 | -263 | Max  | 1 | SLU   | 0.58 |
| -263 | Min. | 4   | SLE Q                                | 0.40 | -262 | Max  | 1                                    | SLU   | 0.58 | -262 | Min.                                 | 4    | SLE Q | 0.40 | -261                                 | Max  | 1  | SLU   | 0.58                                 | -261 | Min. | 4 | SLE Q | 0.40 |
| -260 | Max  | 1   | SLU                                  | 0.58 | -260 | Min. | 4                                    | SLE Q | 0.40 | -259 | Max                                  | 1    | SLU   | 0.58 | -259                                 | Min. | 4  | SLE Q | 0.40                                 | -258 | Max  | 1 | SLU   | 0.58 |
| -258 | Min. | 4   | SLE Q                                | 0.40 | -257 | Max  | 1                                    | SLU   | 0.58 | -257 | Min.                                 | 4    | SLE Q | 0.40 | -256                                 | Max  | 1  | SLU   | 0.58                                 | -256 | Min. | 4 | SLE Q | 0.40 |
| -255 | Max  | 1   | SLU                                  | 0.58 | -255 | Min. | 4                                    | SLE Q | 0.40 | -254 | Max                                  | 1    | SLU   | 0.58 | -254                                 | Min. | 4  | SLE Q | 0.40                                 | -253 | Max  | 1 | SLU   | 0.58 |
| -253 | Min. | 4   | SLE Q                                | 0.40 | -252 | Max  | 1                                    | SLU   | 0.58 | -252 | Min.                                 | 4    | SLE Q | 0.40 | -251                                 | Max  | 1  | SLU   | 0.58                                 | -251 | Min. | 4 | SLE Q | 0.40 |
| -250 | Max  | 1   | SLU                                  | 0.58 | -250 | Min. | 4                                    | SLE Q | 0.40 | -249 | Max                                  | 1    | SLU   | 0.58 | -249                                 | Min. | 4  | SLE Q | 0.40                                 | -248 | Max  | 1 | SLU   | 0.57 |
| -248 | Min. | 4   | SLE Q                                | 0.39 | -247 | Max  | 1                                    | SLU   | 0.57 | -247 | Min.                                 | 4    | SLE Q | 0.39 | -246                                 | Max  | 1  | SLU   | 0.57                                 | -246 | Min. | 4 | SLE Q | 0.39 |
| -245 | Max  | 1   | SLU                                  | 0.57 | -245 | Min. | 4                                    | SLE Q | 0.39 | -244 | Max                                  | 1    | SLU   | 0.57 | -244                                 | Min. | 4  | SLE Q | 0.39                                 | -243 | Max  | 1 | SLU   | 0.57 |
| -243 | Min. | 4   | SLE Q                                | 0.39 | -242 | Max  | 1                                    | SLU   | 0.57 | -242 | Min.                                 | 4    | SLE Q | 0.39 | -241                                 | Max  | 1  | SLU   | 0.57                                 | -241 | Min. | 4 | SLE Q | 0.39 |
| -240 | Max  | 1   | SLU                                  | 0.57 | -240 | Min. | 4                                    | SLE Q | 0.39 | -239 | Max                                  | 1    | SLU   | 0.57 | -239                                 | Min. | 4  | SLE Q | 0.39                                 | -238 | Max  | 1 | SLU   | 0.57 |
| -238 | Min. | 4   | SLE Q                                | 0.39 | -237 | Max  | 1                                    | SLU   | 0.56 | -237 | Min.                                 | 4    | SLE Q | 0.39 | -236                                 | Max  | 1  | SLU   | 0.56                                 | -236 | Min. | 4 | SLE Q | 0.39 |
| -235 | Max  | 1   | SLU                                  | 0.57 | -235 | Min. | 4                                    | SLE Q | 0.39 | -234 | Max                                  | 1    | SLU   | 0.57 | -234                                 | Min. | 4  | SLE Q | 0.39                                 | -233 | Max  | 1 | SLU   | 0.57 |
| -233 | Min. | 4   | SLE Q                                | 0.39 | -232 | Max  | 1                                    | SLU   | 0.56 | -232 | Min.                                 | 4    | SLE Q | 0.38 | -231                                 | Max  | 1  | SLU   | 0.56                                 | -231 | Min. | 4 | SLE Q | 0.38 |
| -230 | Max  | 1   | SLU                                  | 0.56 | -230 | Min. | 4                                    | SLE Q | 0.38 | -229 | Max                                  | 1    | SLU   | 0.56 | -229                                 | Min. | 4  | SLE Q | 0.38                                 | -228 | Max  | 1 | SLU   | 0.56 |
| -228 | Min. | 4   | SLE Q                                | 0.38 | -227 | Max  | 1                                    | SLU   | 0.56 | -227 | Min.                                 | 4    | SLE Q | 0.38 | -226                                 | Max  | 1  | SLU   | 0.56                                 | -226 | Min. | 4 | SLE Q | 0.38 |
| -225 | Max  | 1   | SLU                                  | 0.56 | -225 | Min. | 4                                    | SLE Q | 0.38 | -224 | Max                                  | 1    | SLU   | 0.48 | -224                                 | Min. | 4  | SLE Q | 0.33                                 | -223 | Max  | 1 | SLU   | 0.48 |
| -223 | Min. | 4   | SLE Q                                | 0.33 | -222 | Max  | 1                                    | SLU   | 0.48 | -222 | Min.                                 | 4    | SLE Q | 0.33 | -221                                 | Max  | 1  | SLU   | 0.48                                 | -221 | Min. | 4 | SLE Q | 0.33 |
| -220 | Max  | 1   | SLU                                  | 0.48 | -220 | Min. | 4                                    | SLE Q | 0.33 | -219 | Max                                  | 1    | SLU   | 0.48 | -219                                 | Min. | 4  | SLE Q | 0.33                                 | -218 | Max  | 1 | SLU   | 0.48 |
| -218 | Min. | 4   | SLE Q                                | 0.33 | -217 | Max  | 1                                    | SLU   | 0.48 | -217 | Min.                                 | 4    | SLE Q | 0.33 | -216                                 | Max  | 1  | SLU   | 0.56                                 | -216 | Min. | 4 | SLE Q | 0.38 |
| -215 | Max  | 1   | SLU                                  | 0.56 | -215 | Min. | 4                                    | SLE Q | 0.38 | -214 | Max                                  | 1    | SLU   | 0.55 | -214                                 | Min. | 4  | SLE Q | 0.38                                 | -213 | Max  | 1 | SLU   | 0.55 |
| -213 | Min. | 4   | SLE Q                                | 0.38 | -212 | Max  | 1                                    | SLU   | 0.55 | -212 | Min.                                 | 4    | SLE Q | 0.38 | -211                                 | Max  | 1  | SLU   | 0.55                                 | -211 | Min. | 4 | SLE Q | 0.38 |
| -210 | Max  | 1   | SLU                                  | 0.56 | -210 | Min. | 4                                    | SLE Q | 0.38 | -209 | Max                                  | 1    | SLU   | 0.56 | -209                                 | Min. | 4  | SLE Q | 0.38                                 | -208 | Max  | 1 | SLU   | 0.48 |
| -208 | Min. | 4   | SLE Q                                | 0.33 | -207 | Max  | 1                                    | SLU   | 0.48 | -207 | Min.                                 | 4    | SLE Q | 0.33 | -206                                 | Max  | 1  | SLU   | 0.47                                 | -206 | Min. | 4 | SLE Q | 0.33 |
| -205 | Max  | 1   | SLU                                  | 0.47 | -205 | Min. | 4                                    | SLE Q | 0.33 | -204 | Max                                  | 1    | SLU   | 0.47 | -204                                 | Min. | 4  | SLE Q | 0.33                                 | -203 | Max  | 1 | SLU   | 0.47 |
| -203 | Min. | 4   | SLE Q                                | 0.33 | -202 | Max  | 1                                    | SLU   | 0.48 | -202 | Min.                                 | 4    | SLE Q | 0.33 | -201                                 | Max  | 1  | SLU   | 0.48                                 | -201 | Min. | 4 | SLE Q | 0.33 |
| -200 | Max  | 1   | SLU                                  | 0.55 | -200 | Min. | 4                                    | SLE Q | 0.38 | -199 | Max                                  | 1    | SLU   | 0.55 | -199                                 | Min. | 4  | SLE Q | 0.38                                 | -198 | Max  | 1 | SLU   | 0.55 |
| -198 | Min. | 4   | SLE Q                                | 0.38 | -197 | Max  | 1                                    | SLU   | 0.55 | -197 | Min.                                 | 4    | SLE Q | 0.38 | -196                                 | Max  | 1  | SLU   | 0.55                                 | -196 | Min. | 4 | SLE Q | 0.38 |
| -195 | Max  | 1   | SLU                                  | 0.55 | -195 | Min. | 4                                    | SLE Q | 0.38 | -194 | Max                                  | 1    | SLU   | 0.55 | -194                                 | Min. | 4  | SLE Q | 0.38                                 | -193 | Max  | 1 | SLU   | 0.55 |
| -193 | Min. | 4   | SLE Q                                | 0.38 | -192 | Max  | 1                                    | SLU   | 0.47 | -192 | Min.                                 | 4    | SLE Q | 0.33 | -191                                 | Max  | 1  | SLU   | 0.47                                 | -191 | Min. | 4 | SLE Q | 0.33 |
| -190 | Max  | 1   | SLU                                  | 0.47 | -190 | Min. | 4                                    | SLE Q | 0.33 | -189 | Max                                  | 1    | SLU   | 0.47 | -189                                 | Min. | 4  | SLE Q | 0.33                                 | -188 | Max  | 1 | SLU   | 0.47 |
| -188 | Min. | 4   | SLE Q                                | 0.33 | -187 | Max  | 1                                    | SLU   | 0.47 | -187 | Min.                                 | 4    | SLE Q | 0.33 | -186                                 | Max  | 1  | SLU   | 0.47                                 | -186 | Min. | 4 | SLE Q | 0.33 |
| -185 | Max  | 1   | SLU                                  | 0.47 | -185 | Min. | 4                                    | SLE Q | 0.33 | -184 | Max                                  | 1    | SLU   | 0.55 | -184                                 | Min. | 4  | SLE Q | 0.38                                 | -183 | Max  | 1 | SLU   | 0.55 |
| -183 | Min. | 4   | SLE Q                                | 0.38 | -182 | Max  | 1                                    | SLU   | 0.55 | -182 | Min.                                 | 4    | SLE Q | 0.38 | -181                                 | Max  | 1  | SLU   | 0.55                                 | -181 | Min. | 4 | SLE Q | 0.38 |
| -180 | Max  | 1   | SLU                                  | 0.55 | -180 | Min. | 4                                    | SLE Q | 0.38 | -179 | Max                                  | 1    | SLU   | 0.55 | -179                                 | Min. | 4  | SLE Q | 0.38                                 | -178 | Max  | 1 | SLU   | 0.55 |
| -178 | Min. | 4   | SLE Q                                | 0.38 | -177 | Max  | 1                                    | SLU   | 0.55 | -177 | Min.                                 | 4    | SLE Q | 0.38 | -176                                 | Max  | 1  | SLU   | 0.47                                 | -176 | Min. | 4 | SLE Q | 0.33 |
| -175 | Max  | 1   | SLU                                  | 0.47 | -175 | Min. | 4                                    | SLE Q | 0.32 | -174 | Max                                  | 1    | SLU   | 0.47 | -174                                 | Min. | 4  | SLE Q | 0.32                                 | -173 | Max  | 1 | SLU   | 0.47 |
| -173 | Min. | 4   | SLE Q                                | 0.32 | -172 | Max  | 1                                    | SLU   | 0.47 | -172 | Min.                                 | 4    | SLE Q | 0.32 | -171                                 | Max  | 1  | SLU   | 0.47                                 | -171 | Min. | 4 | SLE Q | 0.32 |
| -170 | Max  | 1   | SLU                                  | 0.47 | -170 | Min. | 4                                    | SLE Q | 0.32 | -169 | Max                                  | 1    | SLU   | 0.47 | -169                                 | Min. | 4  | SLE Q | 0.33                                 | -168 | Max  | 1 | SLU   | 0.55 |
| -168 | Min. | 4   | SLE Q                                | 0.38 | -167 | Max  | 1                                    | SLU   | 0.55 | -167 | Min.                                 | 4    | SLE Q | 0.38 | -166                                 | Max  | 1  | SLU   | 0.55                                 | -166 | Min. | 4 | SLE Q | 0.38 |
| -165 | Max  | 1   | SLU                                  | 0.55 | -165 | Min. | 4                                    | SLE Q | 0.38 | -164 | Max                                  | 1    | SLU   | 0.55 | -164                                 | Min. | 4  | SLE Q | 0.38                                 | -163 | Max  | 1 | SLU   | 0.55 |
| -163 | Min. | 4   | SLE Q                                | 0.38 | -162 | Max  | 1                                    | SLU   | 0.55 | -162 | Min.                                 | 4    | SLE Q | 0.38 | -161                                 | Max  | 1  | SLU   | 0.55                                 | -161 | Min. | 4 | SLE Q | 0.38 |
| -160 | Max  | 1   | SLU                                  | 0.47 | -160 | Min. | 4                                    | SLE Q | 0.32 | -159 | Max                                  | 1    | SLU   | 0.47 | -159                                 | Min. | 4  | SLE Q | 0.32                                 | -158 | Max  | 1 | SLU   | 0.47 |
| -158 | Min. | 4   | SLE Q                                | 0.32 | -157 | Max  | 1                                    | SLU   | 0.47 | -157 | Min.                                 | 4    | SLE Q | 0.32 | -156                                 | Max  | 1  | SLU   | 0.47                                 | -156 | Min. | 4 | SLE Q | 0.32 |
| -155 | Max  | 1   | SLU                                  | 0.47 | -155 | Min. | 4                                    | SLE Q | 0.32 | -154 | Max                                  | 1    | SLU   | 0.47 | -154                                 | Min. | 4  | SLE Q | 0.32                                 | -153 | Max  | 1 | SLU   | 0.47 |
| -153 | Min. | 4   | SLE Q                                | 0.32 | -152 | Max  | 1                                    | SLU   | 0.55 | -152 | Min.                                 | 4    | SLE Q | 0.38 | -151                                 | Max  | 1  | SLU   | 0.55                                 | -151 | Min. | 4 | SLE Q | 0.38 |
| -150 | Max  | 1   | SLU                                  | 0.55 | -150 | Min. | 4                                    | SLE Q | 0.38 | -149 | Max                                  | 1    | SLU   | 0.55 | -149                                 | Min. | 4  | SLE Q | 0.38                                 | -148 | Max  | 1 | SLU   | 0.55 |
| -148 | Min. | 4   | SLE Q                                | 0.38 | -147 | Max  | 1                                    | SLU   | 0.55 | -147 | Min.                                 | 4    | SLE Q | 0.38 | -146                                 | Max  | 1  | SLU   | 0.55                                 | -146 | Min. | 4 | SLE Q | 0.38 |
| -145 | Max  | 1   | SLU                                  | 0.55 | -145 | Min. | 4                                    | SLE Q | 0.38 | -144 | Max                                  | 1    | SLU   | 0.47 | -144                                 | Min. | 4  | SLE Q | 0.32                                 | -143 | Max  | 1 | SLU   | 0.47 |
| -143 | Min. | 4   | SLE Q                                | 0.32 | -142 | Max  | 1                                    | SLU   | 0.47 | -142 | Min.                                 | 4    | SLE Q | 0.32 | -141                                 | Max  | 1  | SLU   | 0.47                                 | -141 | Min. | 4 | SLE Q | 0.32 |
| -140 | Max  | 1   | SLU                                  | 0.47 | -140 | Min. | 4                                    | SLE Q | 0.32 | -139 | Max                                  | 1    | SLU   | 0.47 | -139                                 | Min. | 4  | SLE Q | 0.32                                 | -138 | Max  | 1 | SLU   | 0.47 |
| -138 | Min. | 4   | SLE Q                                | 0.32 | -137 | Max  | 1                                    | SLU   | 0.47 | -137 | Min.                                 | 4    | SLE Q | 0.32 | -136                                 | Max  | 1  | SLU   | 0.55                                 | -136 | Min. | 4 | SLE Q | 0.38 |
| -135 | Max  | 1   | SLU                                  | 0.55 | -135 | Min. | 4                                    | SLE Q | 0.38 | -134 | Max                                  | 1    | SLU   | 0.55 | -134                                 | Min. | 4  | SLE Q | 0.38                                 | -133 | Max  | 1 | SLU   | 0.55 |
| -133 | Min. | 4   | SLE Q                                | 0.38 | -132 | Max  | 1                                    | SLU   | 0.55 | -132 | Min.                                 | 4    | SLE Q | 0.38 | -131                                 | Max  | 1  | SLU   | 0.55                                 |      |      |   |       |      |



|      |      |   |       |      |      |      |   |       |      |      |      |   |       |      |      |      |   |       |      |      |      |   |       |      |
|------|------|---|-------|------|------|------|---|-------|------|------|------|---|-------|------|------|------|---|-------|------|------|------|---|-------|------|
| -110 | Max  | 1 | SLU   | 0.47 | -110 | Min. | 4 | SLE Q | 0.32 | -109 | Max  | 1 | SLU   | 0.47 | -109 | Min. | 4 | SLE Q | 0.32 | -108 | Max  | 1 | SLU   | 0.47 |
| -108 | Min. | 4 | SLE Q | 0.32 | -107 | Max  | 1 | SLU   | 0.47 | -107 | Min. | 4 | SLE Q | 0.32 | -106 | Max  | 1 | SLU   | 0.47 | -106 | Min. | 4 | SLE Q | 0.32 |
| -105 | Max  | 1 | SLU   | 0.47 | -105 | Min. | 4 | SLE Q | 0.32 | -104 | Max  | 1 | SLU   | 0.56 | -104 | Min. | 4 | SLE Q | 0.38 | -103 | Max  | 1 | SLU   | 0.56 |
| -103 | Min. | 4 | SLE Q | 0.38 | -102 | Max  | 1 | SLU   | 0.56 | -102 | Min. | 4 | SLE Q | 0.38 | -101 | Max  | 1 | SLU   | 0.56 | -101 | Min. | 4 | SLE Q | 0.38 |
| -100 | Max  | 1 | SLU   | 0.56 | -100 | Min. | 4 | SLE Q | 0.38 | -99  | Max  | 1 | SLU   | 0.56 | -99  | Min. | 4 | SLE Q | 0.38 | -98  | Max  | 1 | SLU   | 0.56 |
| -98  | Min. | 4 | SLE Q | 0.38 | -97  | Max  | 1 | SLU   | 0.56 | -97  | Min. | 4 | SLE Q | 0.38 | -96  | Max  | 1 | SLU   | 0.47 | -96  | Min. | 4 | SLE Q | 0.32 |
| -95  | Max  | 1 | SLU   | 0.47 | -95  | Min. | 4 | SLE Q | 0.32 | -94  | Max  | 1 | SLU   | 0.47 | -94  | Min. | 4 | SLE Q | 0.32 | -93  | Max  | 1 | SLU   | 0.47 |
| -93  | Min. | 4 | SLE Q | 0.32 | -92  | Max  | 1 | SLU   | 0.47 | -92  | Min. | 4 | SLE Q | 0.32 | -91  | Max  | 1 | SLU   | 0.47 | -91  | Min. | 4 | SLE Q | 0.32 |
| -90  | Max  | 1 | SLU   | 0.47 | -90  | Min. | 4 | SLE Q | 0.32 | -89  | Max  | 1 | SLU   | 0.47 | -89  | Min. | 4 | SLE Q | 0.32 | -88  | Max  | 1 | SLU   | 0.57 |
| -88  | Min. | 4 | SLE Q | 0.39 | -87  | Max  | 1 | SLU   | 0.57 | -87  | Min. | 4 | SLE Q | 0.39 | -86  | Max  | 1 | SLU   | 0.57 | -86  | Min. | 4 | SLE Q | 0.39 |
| -85  | Max  | 1 | SLU   | 0.56 | -85  | Min. | 4 | SLE Q | 0.39 | -84  | Max  | 1 | SLU   | 0.56 | -84  | Min. | 4 | SLE Q | 0.39 | -83  | Max  | 1 | SLU   | 0.57 |
| -83  | Min. | 4 | SLE Q | 0.39 | -82  | Max  | 1 | SLU   | 0.57 | -82  | Min. | 4 | SLE Q | 0.39 | -81  | Max  | 1 | SLU   | 0.57 | -81  | Min. | 4 | SLE Q | 0.39 |
| -80  | Max  | 1 | SLU   | 0.47 | -80  | Min. | 4 | SLE Q | 0.32 | -79  | Max  | 1 | SLU   | 0.47 | -79  | Min. | 4 | SLE Q | 0.32 | -78  | Max  | 1 | SLU   | 0.47 |
| -78  | Min. | 4 | SLE Q | 0.32 | -77  | Max  | 1 | SLU   | 0.47 | -77  | Min. | 4 | SLE Q | 0.32 | -76  | Max  | 1 | SLU   | 0.47 | -76  | Min. | 4 | SLE Q | 0.32 |
| -75  | Max  | 1 | SLU   | 0.47 | -75  | Min. | 4 | SLE Q | 0.32 | -74  | Max  | 1 | SLU   | 0.47 | -74  | Min. | 4 | SLE Q | 0.32 | -73  | Max  | 1 | SLU   | 0.47 |
| -73  | Min. | 4 | SLE Q | 0.32 | -72  | Max  | 1 | SLU   | 0.57 | -72  | Min. | 4 | SLE Q | 0.39 | -71  | Max  | 1 | SLU   | 0.57 | -71  | Min. | 4 | SLE Q | 0.39 |
| -70  | Max  | 1 | SLU   | 0.57 | -70  | Min. | 4 | SLE Q | 0.39 | -69  | Max  | 1 | SLU   | 0.57 | -69  | Min. | 4 | SLE Q | 0.39 | -68  | Max  | 1 | SLU   | 0.57 |
| -68  | Min. | 4 | SLE Q | 0.39 | -67  | Max  | 1 | SLU   | 0.57 | -67  | Min. | 4 | SLE Q | 0.39 | -66  | Max  | 1 | SLU   | 0.57 | -66  | Min. | 4 | SLE Q | 0.39 |
| -65  | Max  | 1 | SLU   | 0.57 | -65  | Min. | 4 | SLE Q | 0.39 | -64  | Max  | 1 | SLU   | 0.47 | -64  | Min. | 4 | SLE Q | 0.33 | -63  | Max  | 1 | SLU   | 0.47 |
| -63  | Min. | 4 | SLE Q | 0.32 | -62  | Max  | 1 | SLU   | 0.47 | -62  | Min. | 4 | SLE Q | 0.32 | -61  | Max  | 1 | SLU   | 0.47 | -61  | Min. | 4 | SLE Q | 0.32 |
| -60  | Max  | 1 | SLU   | 0.47 | -60  | Min. | 4 | SLE Q | 0.32 | -59  | Max  | 1 | SLU   | 0.47 | -59  | Min. | 4 | SLE Q | 0.32 | -58  | Max  | 1 | SLU   | 0.47 |
| -58  | Min. | 4 | SLE Q | 0.32 | -57  | Max  | 1 | SLU   | 0.47 | -57  | Min. | 4 | SLE Q | 0.33 | -56  | Max  | 1 | SLU   | 0.58 | -56  | Min. | 4 | SLE Q | 0.40 |
| -55  | Max  | 1 | SLU   | 0.58 | -55  | Min. | 4 | SLE Q | 0.40 | -54  | Max  | 1 | SLU   | 0.58 | -54  | Min. | 4 | SLE Q | 0.40 | -53  | Max  | 1 | SLU   | 0.58 |
| -53  | Min. | 4 | SLE Q | 0.40 | -52  | Max  | 1 | SLU   | 0.58 | -52  | Min. | 4 | SLE Q | 0.40 | -51  | Max  | 1 | SLU   | 0.58 | -51  | Min. | 4 | SLE Q | 0.40 |
| -50  | Max  | 1 | SLU   | 0.58 | -50  | Min. | 4 | SLE Q | 0.40 | -49  | Max  | 1 | SLU   | 0.58 | -49  | Min. | 4 | SLE Q | 0.40 | -48  | Max  | 1 | SLU   | 0.47 |
| -48  | Min. | 4 | SLE Q | 0.33 | -47  | Max  | 1 | SLU   | 0.47 | -47  | Min. | 4 | SLE Q | 0.33 | -46  | Max  | 1 | SLU   | 0.47 | -46  | Min. | 4 | SLE Q | 0.33 |
| -45  | Max  | 1 | SLU   | 0.47 | -45  | Min. | 4 | SLE Q | 0.33 | -44  | Max  | 1 | SLU   | 0.47 | -44  | Min. | 4 | SLE Q | 0.33 | -43  | Max  | 1 | SLU   | 0.47 |
| -43  | Min. | 4 | SLE Q | 0.33 | -42  | Max  | 1 | SLU   | 0.47 | -42  | Min. | 4 | SLE Q | 0.33 | -41  | Max  | 1 | SLU   | 0.47 | -41  | Min. | 4 | SLE Q | 0.33 |
| -40  | Max  | 1 | SLU   | 0.58 | -40  | Min. | 4 | SLE Q | 0.40 | -39  | Max  | 1 | SLU   | 0.58 | -39  | Min. | 4 | SLE Q | 0.40 | -38  | Max  | 1 | SLU   | 0.58 |
| -38  | Min. | 4 | SLE Q | 0.40 | -37  | Max  | 1 | SLU   | 0.58 | -37  | Min. | 4 | SLE Q | 0.40 | -36  | Max  | 1 | SLU   | 0.58 | -36  | Min. | 4 | SLE Q | 0.40 |
| -35  | Max  | 1 | SLU   | 0.58 | -35  | Min. | 4 | SLE Q | 0.40 | -34  | Max  | 1 | SLU   | 0.58 | -34  | Min. | 4 | SLE Q | 0.40 | -33  | Max  | 1 | SLU   | 0.58 |
| -33  | Min. | 4 | SLE Q | 0.40 | -32  | Max  | 1 | SLU   | 0.48 | -32  | Min. | 4 | SLE Q | 0.33 | -31  | Max  | 1 | SLU   | 0.48 | -31  | Min. | 4 | SLE Q | 0.33 |
| -30  | Max  | 1 | SLU   | 0.47 | -30  | Min. | 4 | SLE Q | 0.33 | -29  | Max  | 1 | SLU   | 0.47 | -29  | Min. | 4 | SLE Q | 0.33 | -28  | Max  | 1 | SLU   | 0.47 |
| -28  | Min. | 4 | SLE Q | 0.33 | -27  | Max  | 1 | SLU   | 0.47 | -27  | Min. | 4 | SLE Q | 0.33 | -26  | Max  | 1 | SLU   | 0.48 | -26  | Min. | 4 | SLE Q | 0.33 |
| -25  | Max  | 1 | SLU   | 0.48 | -25  | Min. | 4 | SLE Q | 0.33 | -24  | Max  | 1 | SLU   | 0.59 | -24  | Min. | 4 | SLE Q | 0.40 | -23  | Max  | 1 | SLU   | 0.59 |
| -23  | Min. | 4 | SLE Q | 0.40 | -22  | Max  | 1 | SLU   | 0.59 | -22  | Min. | 4 | SLE Q | 0.40 | -21  | Max  | 1 | SLU   | 0.59 | -21  | Min. | 4 | SLE Q | 0.40 |
| -20  | Max  | 1 | SLU   | 0.59 | -20  | Min. | 4 | SLE Q | 0.40 | -19  | Max  | 1 | SLU   | 0.59 | -19  | Min. | 4 | SLE Q | 0.40 | -18  | Max  | 1 | SLU   | 0.59 |
| -18  | Min. | 4 | SLE Q | 0.40 | -17  | Max  | 1 | SLU   | 0.59 | -17  | Min. | 4 | SLE Q | 0.40 | -16  | Max  | 1 | SLU   | 0.48 | -16  | Min. | 4 | SLE Q | 0.33 |
| -15  | Max  | 1 | SLU   | 0.48 | -15  | Min. | 4 | SLE Q | 0.33 | -14  | Max  | 1 | SLU   | 0.48 | -14  | Min. | 4 | SLE Q | 0.33 | -13  | Max  | 1 | SLU   | 0.48 |
| -13  | Min. | 4 | SLE Q | 0.33 | -12  | Max  | 1 | SLU   | 0.48 | -12  | Min. | 4 | SLE Q | 0.33 | -11  | Max  | 1 | SLU   | 0.48 | -11  | Min. | 4 | SLE Q | 0.33 |
| -10  | Max  | 1 | SLU   | 0.48 | -10  | Min. | 4 | SLE Q | 0.33 | -9   | Max  | 1 | SLU   | 0.48 | -9   | Min. | 4 | SLE Q | 0.33 | -8   | Max  | 1 | SLU   | 0.60 |
| -8   | Min. | 4 | SLE Q | 0.41 | -7   | Max  | 1 | SLU   | 0.60 | -7   | Min. | 4 | SLE Q | 0.41 | -6   | Max  | 1 | SLU   | 0.60 | -6   | Min. | 4 | SLE Q | 0.41 |
| -5   | Max  | 1 | SLU   | 0.60 | -5   | Min. | 4 | SLE Q | 0.41 | -4   | Max  | 1 | SLU   | 0.60 | -4   | Min. | 4 | SLE Q | 0.41 | -3   | Max  | 1 | SLU   | 0.60 |
| -3   | Min. | 4 | SLE Q | 0.41 | -2   | Max  | 1 | SLU   | 0.60 | -2   | Min. | 4 | SLE Q | 0.41 | -1   | Max  | 1 | SLU   | 0.60 | -1   | Min. | 4 | SLE Q | 0.41 |

Sollecitazioni elementi bidimensionali

Simbologia

- $\sigma_{xx}$  = Tensione normale sulle facce perp. all'asse X
- $\sigma_{zz}$  = Tensione normale sulle facce perp. all'asse Z
- $\tau_{xy}$  = Tensione in dir. Y sulle facce perp. all'asse X
- $\tau_{xz}$  = Tensione in dir. Z sulle facce perp. all'asse X
- $\tau_{yz}$  = Tensione in dir. Y sulle facce perp. all'asse Z
- Bid. = Numero del muro/elemento bidimensionale
- CC = Numero della combinazione delle condizioni di carico elementari
- Mxx = Momento che provoca variazione di tensione sulle facce perp. all'asse X
- Mxz = Momento che provoca variazione di tensione tangenziale sulle facce perp. all'asse X
- Mzz = Momento che provoca variazione di tensione sulle facce perp. all'asse Z
- Nodo = Numero del nodo
- TCC = Tipo di combinazioni di carico
  - SLU = Stato limite ultimo
  - SLE R = Stato limite d'esercizio, combinazione rara
  - SLE F = Stato limite d'esercizio, combinazione frequente
  - SLE Q = Stato limite d'esercizio, combinazione quasi permanente

Bid. 3

|                        | CC | TCC | Nodo | Min.  | CC | TCC | Nodo | Max  | CC                     | TCC | Nodo | Min. | CC    | TCC | Nodo | Max  |      |
|------------------------|----|-----|------|-------|----|-----|------|------|------------------------|-----|------|------|-------|-----|------|------|------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -132 | 0     | 1  | SLU | -250 | 0    | $\sigma_{zz}$ <daN/mq> | 1   | SLU  | -130 | 0     | 1   | SLU  | -252 | 0    |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -119 | 0     | 1  | SLU | -152 | 0    | Mxx <daNm/m>           | 1   | SLU  | -148 | -1533 | 1   | SLU  | -256 | 312  |
| Mzz <daNm/m>           | 1  | SLU | -148 | -4128 | 1  | SLU | -21  | 310  | Mxz <daNm/m>           | 1   | SLU  | -258 | -256  | 1   | SLU  | -263 | 256  |
| $\tau_{xy}$ <daN/mq>   | 1  | SLU | -85  | -6258 | 1  | SLU | -244 | 6258 | $\tau_{yz}$ <daN/mq>   | 1   | SLU  | -147 | -5091 | 1   | SLU  | -167 | 5091 |

Bid. 4

|                        | CC | TCC | Nodo | Min.  | CC | TCC | Nodo | Max  | CC                     | TCC | Nodo | Min. | CC    | TCC | Nodo | Max  |      |
|------------------------|----|-----|------|-------|----|-----|------|------|------------------------|-----|------|------|-------|-----|------|------|------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -46  | 0     | 1  | SLU | -208 | 0    | $\sigma_{zz}$ <daN/mq> | 1   | SLU  | -73  | 0     | 1   | SLU  | -221 | 0    |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -90  | 0     | 1  | SLU | -175 | 0    | Mxx <daNm/m>           | 1   | SLU  | -108 | -1146 | 1   | SLU  | -57  | 206  |
| Mzz <daNm/m>           | 1  | SLU | -108 | -1557 | 1  | SLU | -28  | 236  | Mxz <daNm/m>           | 1   | SLU  | -47  | -281  | 1   | SLU  | -27  | 281  |
| $\tau_{xy}$ <daN/mq>   | 1  | SLU | -29  | -4207 | 1  | SLU | -205 | 4207 | $\tau_{yz}$ <daN/mq>   | 1   | SLU  | -106 | -4142 | 1   | SLU  | -127 | 4142 |

Verifiche e armature solette/platee

Simbologia

- $\Delta_{sm}$  = Distanza media tra le fessure
- $\Phi_{eq}$  = Diametro equivalente delle barre
- $\epsilon_{sm}$  = Deformazione unitaria media dell'armatura (\*1000)
- $\sigma_c$  = Tensione nel calcestruzzo
- $\sigma_f$  = Tensione nel ferro
- $\sigma_s$  = Tensione nell'acciaio nella sezione fessurata
- $A_{c\ eff}$  = Area di calcestruzzo efficace
- $A_s$  = Area compressiva dei ferri nell'area di calcestruzzo efficace
- AFE I = Area di ferro effettiva totale presente nel punto di verifica, inferiore
- AFE S = Area di ferro effettiva totale presente nel punto di verifica, superiore
- AFE St. = Area di ferro effettiva della staffatura
- CC = Numero della combinazione delle condizioni di carico elementari
- Cf inf = Copriferro inferiore
- Cf sup = Copriferro superiore
- Cls = Tipo di calcestruzzo
- DV = Direzione di verifica



XX = Verifica per momento Mxx  
YY = Verifica per momento Myy  
Fcd = Resistenza di calcolo a compressione del calcestruzzo  
Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo  
Fctd = Resistenza di calcolo a trazione del calcestruzzo  
Fctk = Resistenza caratteristica a trazione del calcestruzzo  
Fyd = Resistenza di calcolo dell'acciaio  
Fyk = Tensione caratteristica di snervamento dell'acciaio  
K<sub>2</sub> = Coefficiente per distribuzione deformazioni  
MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y  
Mom = Momento flettente  
My = Momento flettente intorno all'asse Y  
Nodo = Numero del nodo  
Sic. = Sicurezza  
Spess. = Spessore  
TCC = Tipo di combinazione di carico  
SLU = Stato limite ultimo  
SLE R = Stato limite d'esercizio, combinazione rara  
SLE F = Stato limite d'esercizio, combinazione frequente  
SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
Tp = Tipo di acciaio  
VRcd = Taglio ultimo lato calcestruzzo  
VRsd = Taglio ultimo lato armatura  
Vrdu = Taglio ultimo resistente  
Vsdu = Taglio agente nella direzione del momento ultimo  
Wk = Ampiezza caratteristica delle fessure  
X = Coordinata X del nodo  
Y = Coordinata Y del nodo  
c = Ricoprimento dell'armatura  
ctgθ = Cotangente dell'angolo di inclinazione dei puntoni di calcestruzzo  
s = Distanza massima tra le barre

Armatura platea a quota 0.00

Caratteristiche delle sezioni e dei materiali utilizzati

| Spess.<br><cm> | Cf sup<br><cm> | Cf inf<br><cm> | Clas   | Fck<br><daN/cm²> | Fctk<br><daN/cm²> | Fcd<br><daN/cm²> | Fctd<br><daN/cm²> | TP    | Fyk<br><daN/cm²> | Fyd<br><daN/cm²> |
|----------------|----------------|----------------|--------|------------------|-------------------|------------------|-------------------|-------|------------------|------------------|
| 50.00          | 3.50           | 3.50           | C32/40 | 332.00           | 21.69             | 188.13           | 14.46             | B450C | 4500.00          | 3913.04          |

Stato limite ultimo - Verifiche a flessione/pressoflessione

| Nodo | X     | Y    | DV | CC | TCC | AfE S | AfE I | My       | MRdy      | Sic.   |
|------|-------|------|----|----|-----|-------|-------|----------|-----------|--------|
| <m>  | <m>   | <m>  |    |    |     | <cmq> | <cmq> | <daNm>   | <daNm>    |        |
| -49  | 1.00  | 2.50 | XX | 1  | SLU | 7.70  | 7.70  | 306.76   | 13950.30  | 45.477 |
| -57  | 11.00 | 2.50 | XX | 1  | SLU | 7.70  | 7.70  | 199.74   | 13950.30  | 69.844 |
| -108 | 12.50 | 4.00 | XX | 1  | SLU | 7.70  | 7.70  | -1013.79 | -13950.30 | 13.761 |
| -164 | 2.50  | 6.00 | XX | 1  | SLU | 7.70  | 7.70  | -1378.22 | -13950.30 | 10.122 |
| -4   | 2.50  | 1.00 | YY | 1  | SLU | 7.70  | 7.70  | 308.96   | 13950.30  | 45.152 |
| -12  | 12.50 | 1.00 | YY | 1  | SLU | 7.70  | 7.70  | 233.07   | 13950.30  | 59.855 |
| -108 | 12.50 | 4.00 | YY | 1  | SLU | 7.70  | 7.70  | -1510.34 | -13950.30 | 9.237  |
| -164 | 2.50  | 6.00 | YY | 1  | SLU | 7.70  | 7.70  | -4108.43 | -13950.30 | 3.396  |

Stato limite ultimo - Verifiche a taglio

| Nodo | X     | Y    | DV | CC | TCC | AfE S | AfE I | AfE St. | Vsdu    | ctgθ | VRcd  | VRsd  | Vrdu     | Sic.   |
|------|-------|------|----|----|-----|-------|-------|---------|---------|------|-------|-------|----------|--------|
| <m>  | <m>   | <m>  |    |    |     | <cmq> | <cmq> | <cmq/m> | <daN>   |      | <daN> | <daN> | <daN>    |        |
| -163 | 2.00  | 6.00 | XX | 1  | SLU | 7.70  | 7.70  |         | 1906.80 |      |       |       | 19980.80 | 10.479 |
| -107 | 12.00 | 4.00 | XX | 1  | SLU | 7.70  | 7.70  |         | 1547.49 |      |       |       | 19980.80 | 12.912 |
| -84  | 2.50  | 3.50 | YY | 1  | SLU | 7.70  | 7.70  |         | 2695.50 |      |       |       | 19980.80 | 7.413  |
| -44  | 12.50 | 2.00 | YY | 1  | SLU | 7.70  | 7.70  |         | 1675.31 |      |       |       | 19980.80 | 11.927 |

Stato limite d'esercizio - Verifiche tensionali

| Nodo | X     | Y    | DV | CC | TCC | AfE S | AfE I | Mom    | σ <sub>c</sub> | σ <sub>s</sub> |        |
|------|-------|------|----|----|-----|-------|-------|--------|----------------|----------------|--------|
| <m>  | <m>   | <m>  |    |    |     | <cmq> | <cmq> | <daNm> | <daN/cm²>      | <daN/cm²>      |        |
| -49  | 1.00  | 2.50 | XX | 2  | SLE | R     | 7.70  | 7.70   | 204.50         | 0.93           | 61.05  |
| -49  | 1.00  | 2.50 | XX | 4  | SLE | Q     | 7.70  | 7.70   | 204.50         | 0.93           | 61.05  |
| -57  | 11.00 | 2.50 | XX | 2  | SLE | R     | 7.70  | 7.70   | 133.16         | 0.61           | 39.75  |
| -57  | 11.00 | 2.50 | XX | 4  | SLE | Q     | 7.70  | 7.70   | 133.16         | 0.61           | 39.75  |
| -125 | 13.00 | 4.50 | XX | 2  | SLE | R     | 7.70  | 7.70   | -675.86        | 3.09           | 201.75 |
| -125 | 13.00 | 4.50 | XX | 4  | SLE | Q     | 7.70  | 7.70   | -675.86        | 3.09           | 201.75 |
| -164 | 2.50  | 6.00 | XX | 2  | SLE | R     | 7.70  | 7.70   | -918.81        | 4.20           | 274.28 |
| -164 | 2.50  | 6.00 | XX | 4  | SLE | Q     | 7.70  | 7.70   | -918.81        | 4.20           | 274.28 |
| -4   | 2.50  | 1.00 | YY | 2  | SLE | R     | 7.70  | 7.70   | 205.97         | 0.94           | 61.49  |
| -4   | 2.50  | 1.00 | YY | 4  | SLE | Q     | 7.70  | 7.70   | 205.97         | 0.94           | 61.49  |
| -12  | 12.50 | 1.00 | YY | 2  | SLE | R     | 7.70  | 7.70   | 155.38         | 0.71           | 46.38  |
| -12  | 12.50 | 1.00 | YY | 4  | SLE | Q     | 7.70  | 7.70   | 155.38         | 0.71           | 46.38  |
| -109 | 13.00 | 4.00 | YY | 2  | SLE | R     | 7.70  | 7.70   | -1006.89       | 4.60           | 300.57 |
| -109 | 13.00 | 4.00 | YY | 4  | SLE | Q     | 7.70  | 7.70   | -1006.89       | 4.60           | 300.57 |
| -164 | 2.50  | 6.00 | YY | 2  | SLE | R     | 7.70  | 7.70   | -2738.95       | 12.51          | 817.61 |
| -164 | 2.50  | 6.00 | YY | 4  | SLE | Q     | 7.70  | 7.70   | -2738.95       | 12.51          | 817.61 |

Stato limite d'esercizio - Verifiche a fessurazione

| Nodo | X     | Y    | DV | CC | TCC | c    | s     | K <sub>2</sub> | Φ <sub>eq</sub> | Δ <sub>sm</sub> | A <sub>s</sub> | A <sub>s,0.95</sub> | σ <sub>s</sub> | ε <sub>sm</sub> | Wk   |      |
|------|-------|------|----|----|-----|------|-------|----------------|-----------------|-----------------|----------------|---------------------|----------------|-----------------|------|------|
| <m>  | <m>   | <m>  |    |    |     | <mm> | <mm>  |                |                 | <mm>            | <cmq>          | <cmq>               | <daN/cm²>      |                 | <mm> |      |
| -49  | 1.00  | 2.50 | XX | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 61.05           | 0.02 | 0.01 |
| -49  | 1.00  | 2.50 | XX | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 61.05           | 0.02 | 0.01 |
| -57  | 11.00 | 2.50 | XX | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 39.75           | 0.01 | 0.01 |
| -57  | 11.00 | 2.50 | XX | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 39.75           | 0.01 | 0.01 |
| -125 | 13.00 | 4.50 | XX | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 201.75          | 0.06 | 0.03 |
| -125 | 13.00 | 4.50 | XX | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 201.75          | 0.06 | 0.03 |
| -164 | 2.50  | 6.00 | XX | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 274.28          | 0.08 | 0.04 |
| -164 | 2.50  | 6.00 | XX | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 274.28          | 0.08 | 0.04 |
| -4   | 2.50  | 1.00 | YY | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 61.49           | 0.02 | 0.01 |
| -4   | 2.50  | 1.00 | YY | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 61.49           | 0.02 | 0.01 |
| -12  | 12.50 | 1.00 | YY | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 46.38           | 0.01 | 0.01 |
| -12  | 12.50 | 1.00 | YY | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 46.38           | 0.01 | 0.01 |
| -109 | 13.00 | 4.00 | YY | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 300.57          | 0.09 | 0.05 |
| -109 | 13.00 | 4.00 | YY | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 300.57          | 0.09 | 0.05 |
| -164 | 2.50  | 6.00 | YY | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 817.61          | 0.24 | 0.13 |
| -164 | 2.50  | 6.00 | YY | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24                | 875.00         | 817.61          | 0.24 | 0.13 |

## 9.0 RISULTATI STRUTTURE INTERRATO LOCALE UTENZE

### 9.1 Diagrammi tassi di sfruttamento

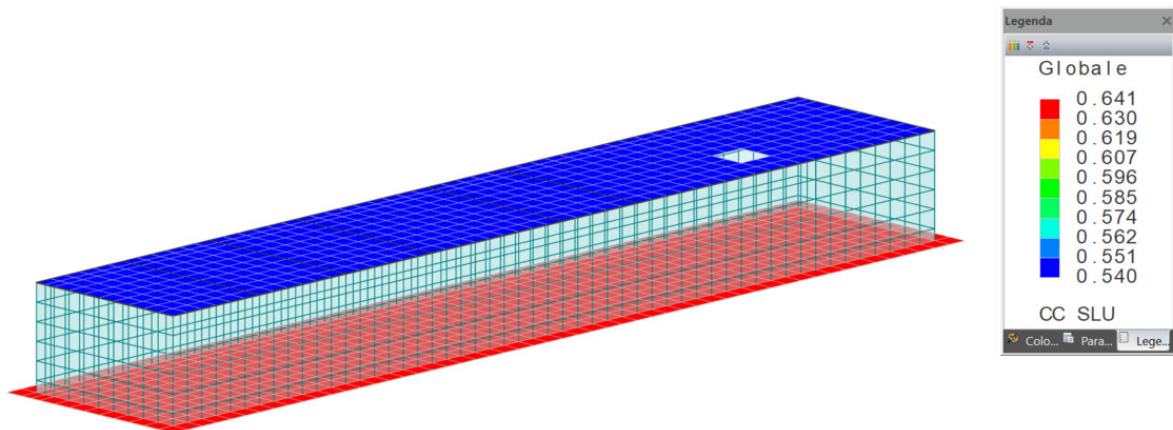


Diagramma tassi di sfruttamento resistenza soletta e platea combo SLU con valore massimo pari a 0,641

**Figure 43: Tassi di sfruttamento SLU (Stato limite ultimo) soletta e platea**

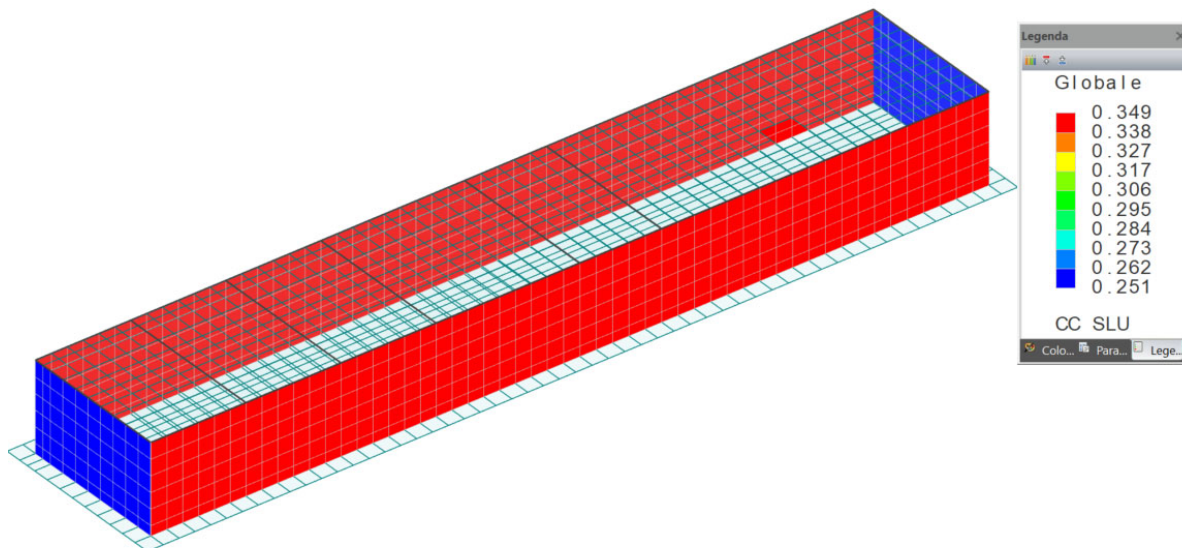
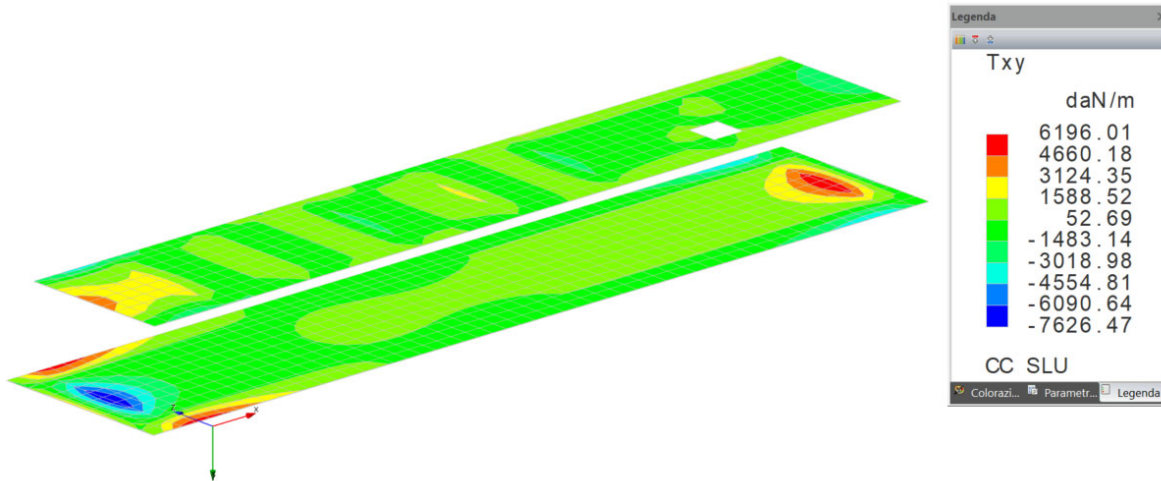


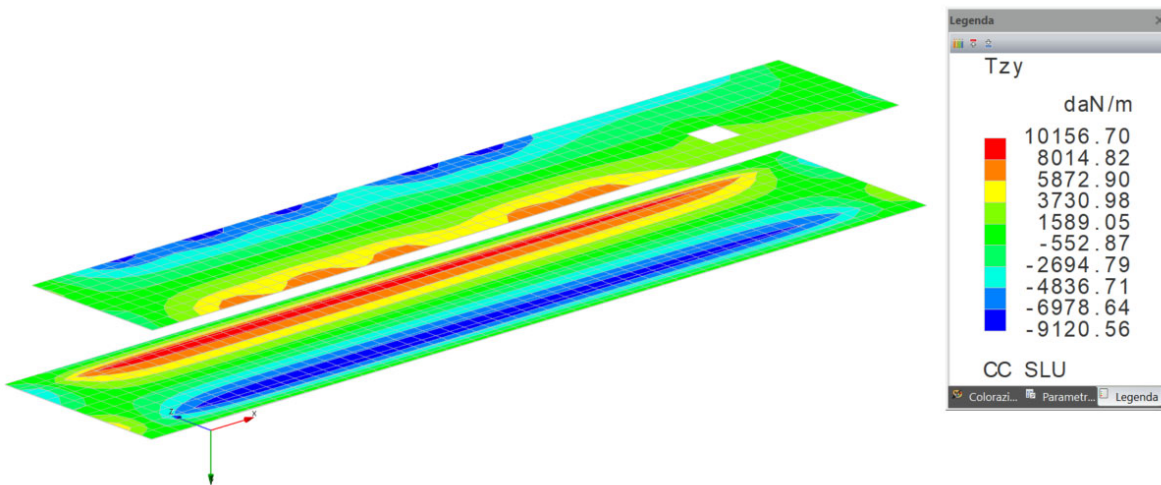
Diagramma tassi di sfruttamento resistenza pareti combo SLU con valore massimo pari a 0,349

**Figure 44: Tassi di sfruttamento SLU (Stato limite ultimo) pareti**

## 9.2 Sollecitazioni

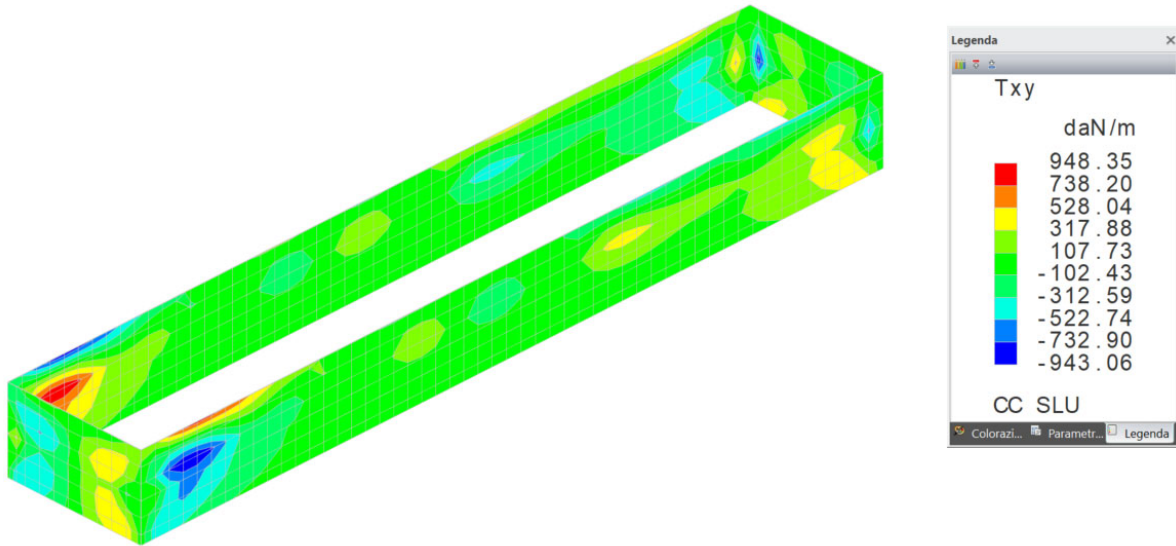


Inviluppo sforzo di taglio in direzione X su faccia con normale Y SLU Tmax = 7626,47 daN/m

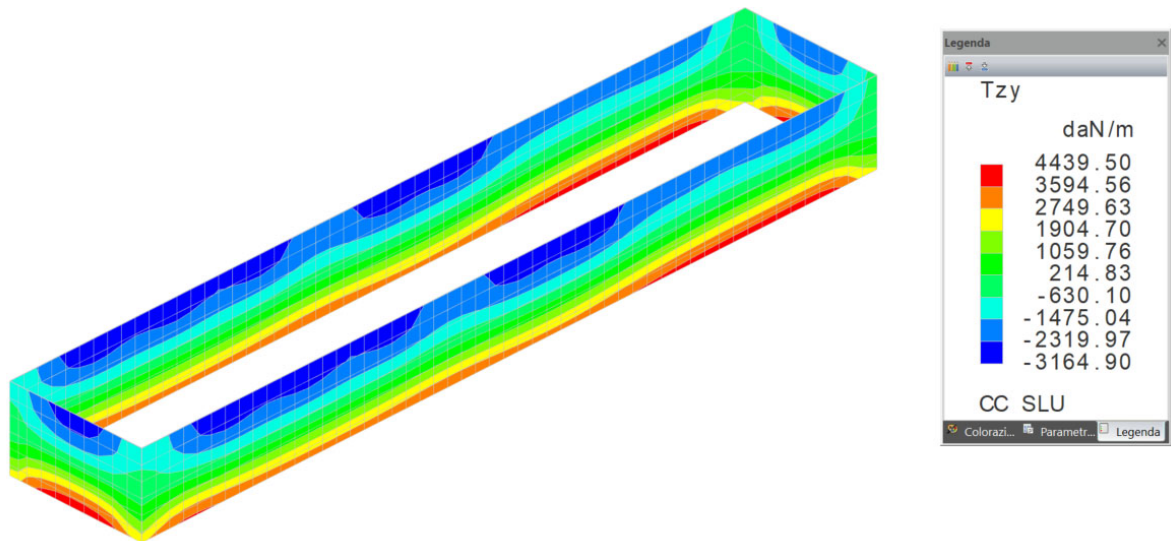


Inviluppo sforzo di taglio in direzione Z su faccia con normale Y SLU Tmax = 10156,70 daN/m

**Figure 45: Taglio solette**



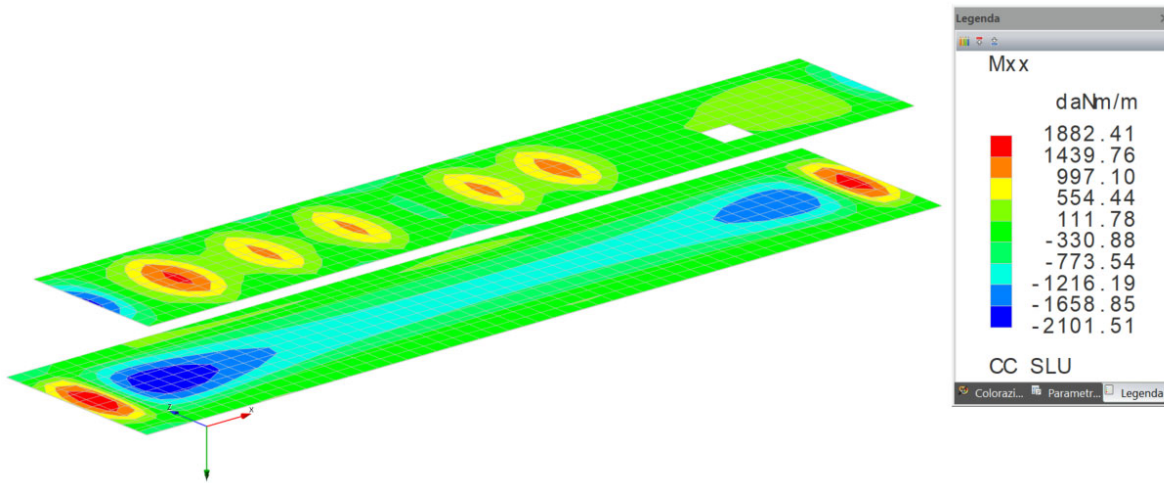
Involuppo sforzo di taglio in direzione X su faccia con normale Y SLU Tmax = 948,35 daN/m



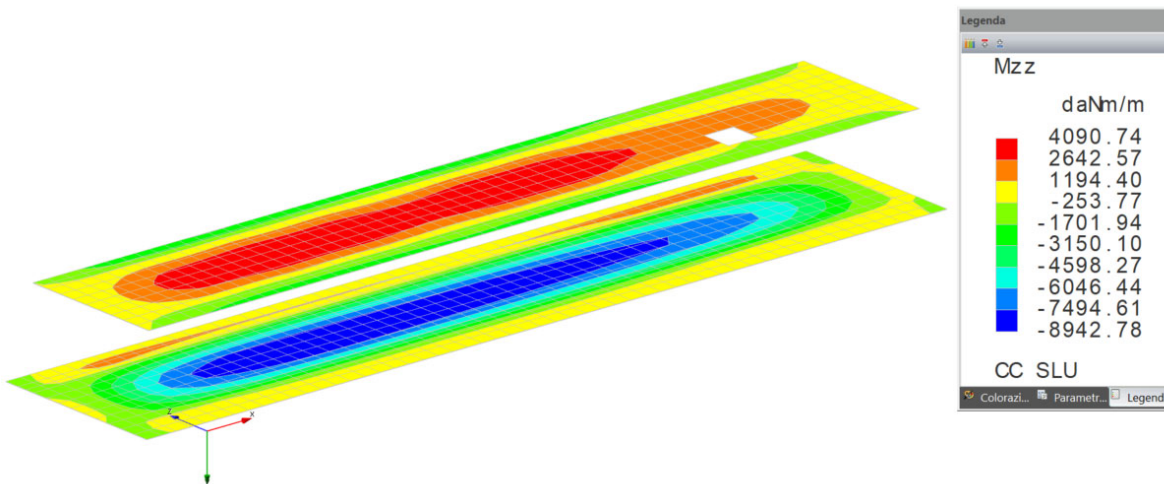
Involuppo sforzo di taglio in direzione Z su faccia con normale Y SLU Tmax = 4439,50 daN/m

**Figure 46: Taglio pareti**



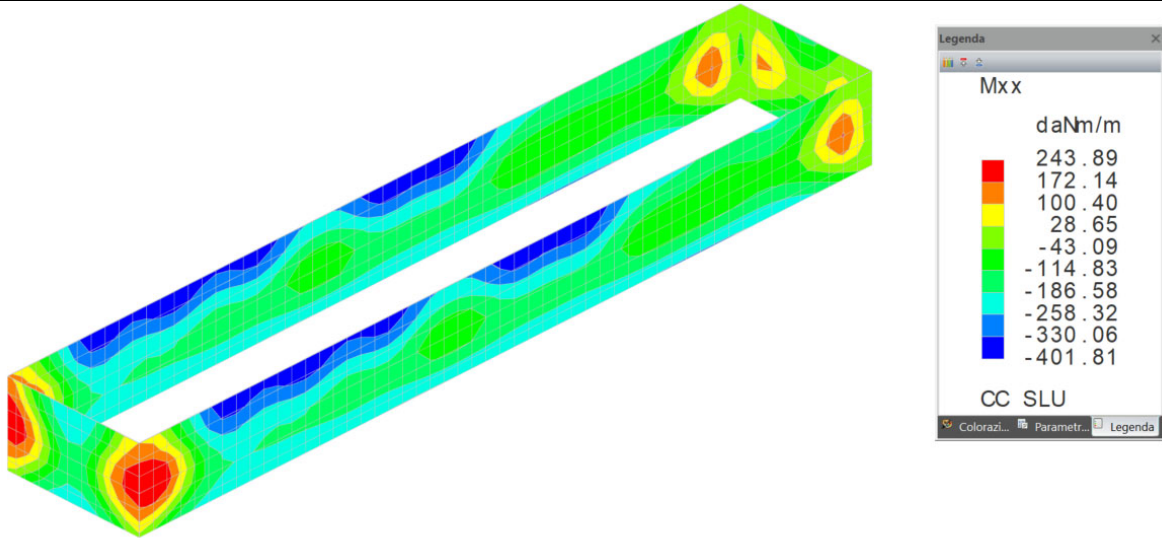


Inviluppo momento che genera tensioni in direzioni X su facce con normale X SLU  $M_{max} = 2101,51 \text{ daN}\times\text{m}/\text{m}$

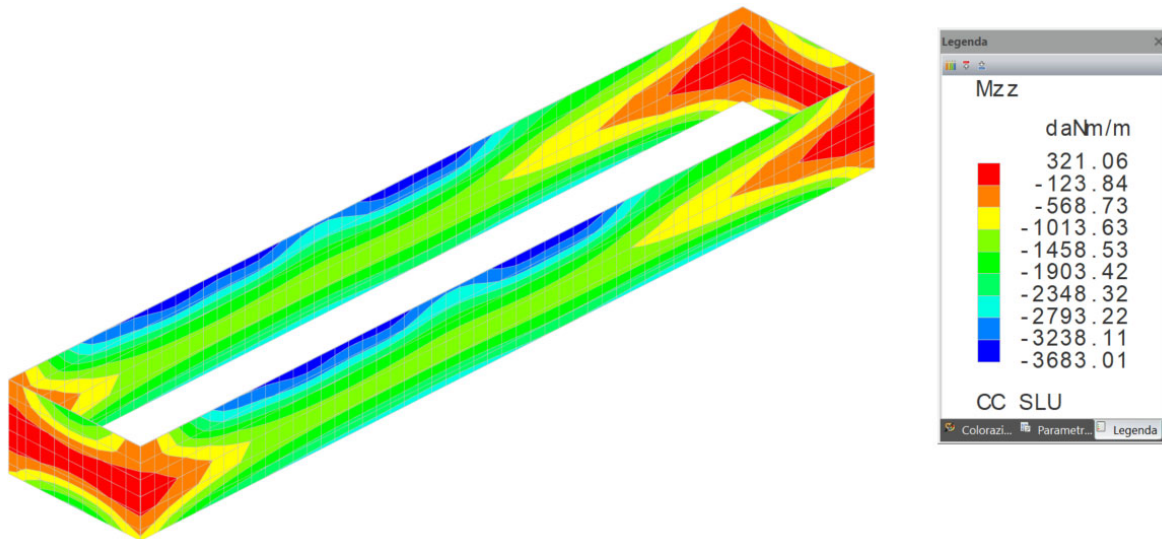


Inviluppo momento che genera tensioni in direzioni Z su facce con normale Z SLU  $M_{max} = 8942,78 \text{ daN}\times\text{m}/\text{m}$

**Figure 47: Momento Flettente solette**



Inviluppo momento che genera tensioni in direzioni X su facce con normale X SLU Mmax = 401,81 daN×m/m



Inviluppo momento che genera tensioni in direzioni Z su facce con normale Z SLU Mmax = 3683,01 daN×m/m

**Figure 48: Momento Flettente pareti**

### 9.3 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

#### Risultati del calcolo

##### Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:  
 ModeSt ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato  
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:  
 Xfinest ver. 9.5.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18

Tipo di calcolo: sismica statica

Vincoli esterni: Considera sempre vincoli assegnati in modellazione

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

##### Generazione combinazioni

- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

##### Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

##### Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

##### Dati struttura

- Sito di costruzione: CQX6+WR Manfredonia FG, Italia LON. 15.76210 LAT. 41.44980  
 Contenuto tra ID reticolo: 30337 30559 30338 30560

##### Simbologia

Ag =Accelerazione orizzontale massima al sito  
 Cc =Coefficiente funzione della categoria del suolo  
 Fo =Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale  
 Ss =Coefficiente di amplificazione stratigrafica  
 Tr =Periodo di ritorno <anni>  
 TCC=Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
 SLD = Stato limite di danno  
 SND = Stato limite di salvaguardia della vita (non dissipativo)  
 Tc\*=Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>

| TCC | Tr  | Ag<br><g> | Fo   | Tc*  | Ss   | Cc   |
|-----|-----|-----------|------|------|------|------|
| SLD | 101 | 0.0761    | 2.57 | 0.34 | 1.50 | 1.49 |
| SLV | 949 | 0.1685    | 2.61 | 0.44 | 1.44 | 1.38 |

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Opera ordinaria
- Vita nominale Vn: 50.00
- Classe d'uso: Classe IV
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 2.70 <m>
- Altezza della struttura: 2.70 <m>
- Numero piani edificio: 0
- Coefficiente 0: 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: Sì
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

##### Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia strutturale: c.a. o prefabbricata a pareti non accoppiate

|            |         |
|------------|---------|
| Periodo T1 | 0.10532 |
|------------|---------|

|                                                              |      |
|--------------------------------------------------------------|------|
| Coeff. $\lambda$ SLD                                         | 1.00 |
| Coeff. $\lambda$ SLV                                         | 1.00 |
| Rapporto di sovrarresistenza ( $\alpha_u/\alpha_s$ )         | 1.10 |
| Valore di riferimento del fattore di comportamento ( $q_0$ ) | 3.00 |
| Fattore riduttivo ( $K_w$ )                                  | 0.50 |
| Fattore riduttivo regolarità in altezza (RR)                 | 1.00 |
| Fattore di comportamento dissipativo (q)                     | 1.50 |
| Fattore di comportamento non dissipativo (qND)               | 1.00 |
| Fattore di comportamento per SLD (qD)                        | 1.00 |

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media  $i \leq 15^\circ$
- Coeff. amplificazione topografica  $S_T$ : 1.00
- Accelerazione di picco del terreno  $A_{gS}$ : 0.242 <math>g</math>
- Fattore di comportamento per sisma verticale (qv): 1.50
- Smorzamento spettro: 5.00%

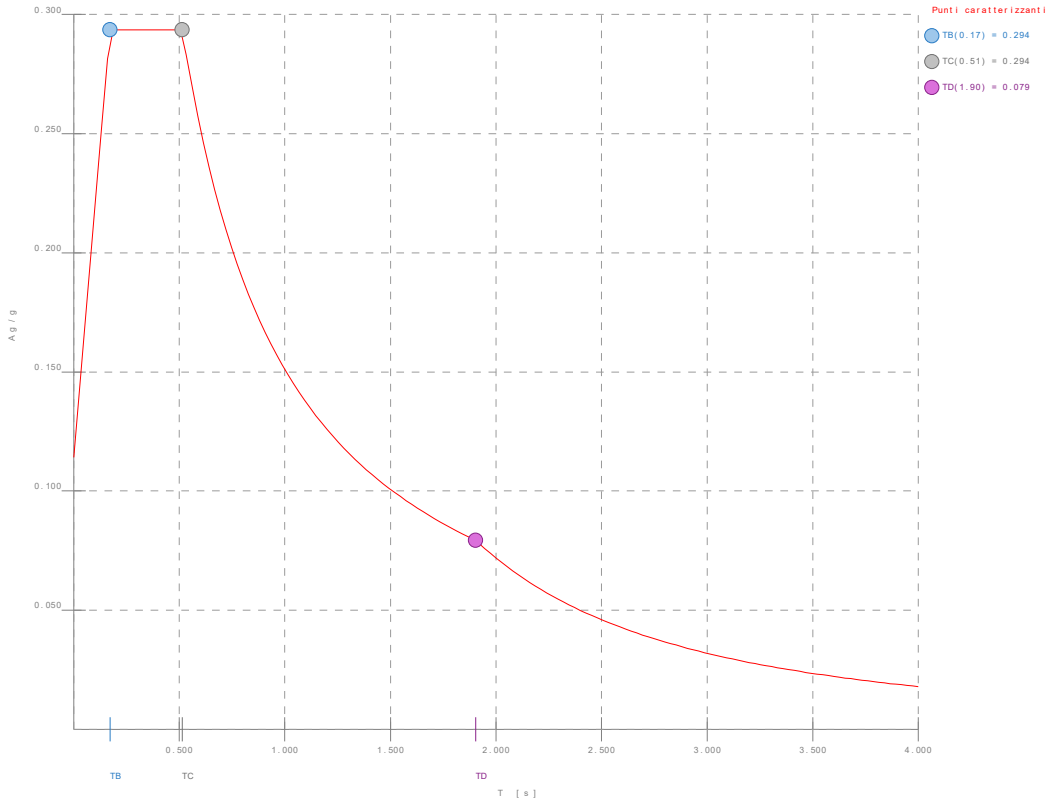


Figura numero 1: Spettro SLD

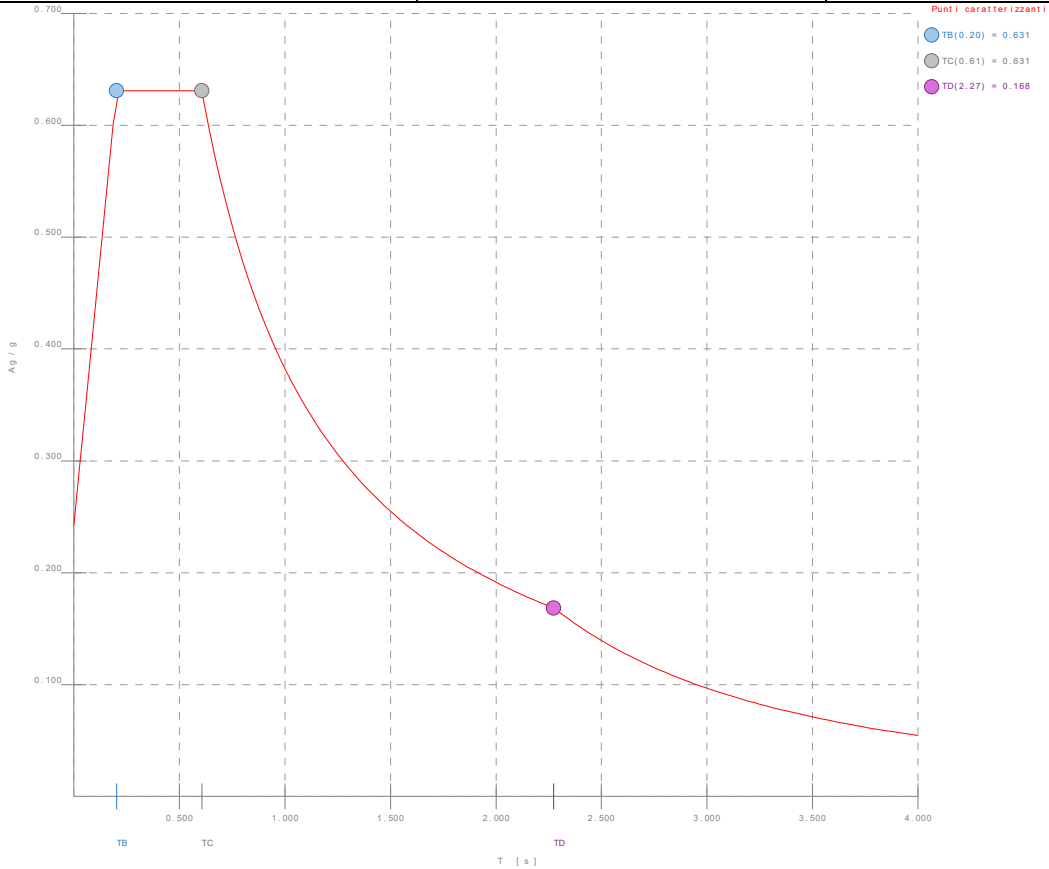


Figura numero 2: Spettro SND

- Angolo di ingresso del sisma: 0.00 <grad>  
- Tipo di combinazione sismica: 30% esteso

Ambienti di carico

Simbologia

N = Numero  
Comm. = Commento  
1 = G1 - permanenti strutturali  
2 = G2 - permanenti non strutturali  
3 = Q - variabili cat. E  
F = azioni orizzontali convenzionali  
SLU = Stato limite ultimo  
SLR = Stato limite per combinazioni rare  
SLF = Stato limite per combinazioni frequenti  
SLQ/D = Stato limite per combinazioni quasi permanenti o di danno  
S = Si  
N = No

| N | Comm.           | 1 | 2 | 3 | S | SLU | SLR | SLF | SLQ |
|---|-----------------|---|---|---|---|-----|-----|-----|-----|
| 1 | Calcolo sismico | S | S | S | S | N   | N   | N   | N   |
| 2 | Calcolo statico | S | S | N | S | S   | S   | S   | S   |

Elenco combinazioni di carico simboliche

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari  
Comm. = Commento  
TCC = Tipo di combinazione di carico  
SLU = Stato limite ultimo  
SLE R = Stato limite d'esercizio, combinazione rara  
SLE F = Stato limite d'esercizio, combinazione frequente  
SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
SLD = Stato limite di danno  
SND = Stato limite di salvaguardia della vita (non dissipativo)

| CC | Comm.          | TCC   | 1            | 2            | 3            | S     |
|----|----------------|-------|--------------|--------------|--------------|-------|
| 1  | Amb. 1 (Sisma) | SLU S | 1            | 1            | $\psi_2$     | 1     |
| 2  | Amb. 2 (SLU)   | SLU   | $\gamma$ max | $\gamma$ max | $\gamma$ max | ----- |
| 3  | Amb. 2 (SLE R) | SLE R | 1            | 1            | 1            | ----- |
| 4  | Amb. 2 (SLE F) | SLE F | 1            | 1            | $\psi_1$     | ----- |
| 5  | Amb. 2 (SLE Q) | SLE Q | 1            | 1            | $\psi_2$     | ----- |

Genera le combinazioni con un solo carico di tipo variabile come di base: S1

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia



An. = Tipo di analisi  
L = Lineare  
NL = Non lineare  
Bk = Buckling  
S = Si  
N = No  
CC = Numero della combinazione delle condizioni di carico elementari  
Comm. = Commento  
TCC = Tipo di combinazione di carico  
SLU = Stato limite ultimo  
SLE R = Stato limite d'esercizio, combinazione rara  
SLE F = Stato limite d'esercizio, combinazione frequente  
SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
SLD = Stato limite di danno  
SND = Stato limite di salvaguardia della vita (non dissipativo)

| CC | Comm.                    | TCC   | An. | Bk | 1    | 2    | 3    | S     | X     | S | Y |
|----|--------------------------|-------|-----|----|------|------|------|-------|-------|---|---|
| 1  | Amb. 1 (SLU S) S +X+0.3Y | SND   | L   | N  | 1.00 | 1.00 | 0.80 | 1.00  | 0.30  |   |   |
| 2  | Amb. 1 (SLE) S +X+0.3Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.80 | 1.00  | 0.30  |   |   |
| 3  | Amb. 1 (SLU S) S +X-0.3Y | SND   | L   | N  | 1.00 | 1.00 | 0.80 | 1.00  | -0.30 |   |   |
| 4  | Amb. 1 (SLE) S +X-0.3Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.80 | 1.00  | -0.30 |   |   |
| 5  | Amb. 1 (SLU S) S -X+0.3Y | SND   | L   | N  | 1.00 | 1.00 | 0.80 | -1.00 | 0.30  |   |   |
| 6  | Amb. 1 (SLE) S -X+0.3Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.80 | -1.00 | 0.30  |   |   |
| 7  | Amb. 1 (SLU S) S -X-0.3Y | SND   | L   | N  | 1.00 | 1.00 | 0.80 | -1.00 | -0.30 |   |   |
| 8  | Amb. 1 (SLE) S -X-0.3Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.80 | -1.00 | -0.30 |   |   |
| 9  | Amb. 1 (SLU S) S +0.3X+Y | SND   | L   | N  | 1.00 | 1.00 | 0.80 | 0.30  | 1.00  |   |   |
| 10 | Amb. 1 (SLE) S +0.3X+Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.80 | 0.30  | 1.00  |   |   |
| 11 | Amb. 1 (SLU S) S -0.3X+Y | SND   | L   | N  | 1.00 | 1.00 | 0.80 | -0.30 | 1.00  |   |   |
| 12 | Amb. 1 (SLE) S -0.3X+Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.80 | -0.30 | 1.00  |   |   |
| 13 | Amb. 1 (SLU S) S +0.3X-Y | SND   | L   | N  | 1.00 | 1.00 | 0.80 | 0.30  | -1.00 |   |   |
| 14 | Amb. 1 (SLE) S +0.3X-Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.80 | 0.30  | -1.00 |   |   |
| 15 | Amb. 1 (SLU S) S -0.3X-Y | SND   | L   | N  | 1.00 | 1.00 | 0.80 | -0.30 | -1.00 |   |   |
| 16 | Amb. 1 (SLE) S -0.3X-Y   | SLD   | L   | N  | 1.00 | 1.00 | 0.80 | -0.30 | -1.00 |   |   |
| 17 | Amb. 2 (SLU)             | SLU   | L   | N  | 1.30 | 1.50 | 1.50 | 0.00  | 0.00  |   |   |
| 18 | Amb. 2 (SLE R)           | SLE R | L   | N  | 1.00 | 1.00 | 1.00 | 0.00  | 0.00  |   |   |
| 19 | Amb. 2 (SLE F)           | SLE F | L   | N  | 1.00 | 1.00 | 0.90 | 0.00  | 0.00  |   |   |
| 20 | Amb. 2 (SLE Q)           | SLE Q | L   | N  | 1.00 | 1.00 | 0.80 | 0.00  | 0.00  |   |   |

Elenco masse nodi

Simbologia  
Mo = Massa orizzontale  
Nodo = Numero del nodo

| Nodo  | Mo <kg> | Nodo  | Mo <kg> | Nodo  | Mo <kg> | Nodo  | Mo <kg> | Nodo  | Mo <kg> | Nodo  | Mo <kg> | Nodo  | Mo <kg> | Nodo  | Mo <kg> | Nodo  | Mo <kg> |       |         |
|-------|---------|-------|---------|-------|---------|-------|---------|-------|---------|-------|---------|-------|---------|-------|---------|-------|---------|-------|---------|
| -1917 | 1342.12 | -1916 | 1711.77 | -1915 | 1711.77 | -1914 | 1711.77 | -1913 | 1711.77 | -1912 | 1711.77 | -1911 | 1711.77 | -1910 | 1711.77 | -1909 | 1711.77 | -1908 | 1711.77 |
| -1907 | 1711.77 | -1906 | 1711.77 | -1905 | 1711.77 | -1904 | 1711.77 | -1903 | 1711.77 | -1902 | 1711.77 | -1901 | 1711.77 | -1899 | 1711.77 | -1898 | 1711.77 | -1897 | 1711.77 |
| -1897 | 2170.49 | -1896 | 1711.77 | -1895 | 1711.77 | -1894 | 1711.77 | -1893 | 1711.77 | -1892 | 2170.49 | -1891 | 1711.77 | -1890 | 1684.39 | -1889 | 1657.00 | -1888 | 1657.00 |
| -1887 | 1657.00 | -1886 | 1657.00 | -1885 | 1657.00 | -1884 | 1657.00 | -1883 | 2115.71 | -1882 | 1657.00 | -1881 | 1657.00 | -1880 | 1657.00 | -1879 | 1657.00 | -1878 | 1657.00 |
| -1877 | 2115.71 | -1876 | 1657.00 | -1875 | 1657.00 | -1874 | 1657.00 | -1873 | 1657.00 | -1872 | 1657.00 | -1871 | 2115.71 | -1870 | 1657.00 | -1869 | 1657.00 | -1868 | 1657.00 |
| -1867 | 1657.00 | -1866 | 1657.00 | -1865 | 1314.74 | -1864 | 1063.46 | -1863 | 181.96  | -1862 | 181.96  | -1861 | 181.96  | -1860 | 181.96  | -1859 | 181.96  | -1858 | 181.96  |
| -1857 | 181.96  | -1856 | 181.96  | -1855 | 181.96  | -1854 | 181.96  | -1853 | 181.96  | -1852 | 181.96  | -1851 | 181.96  | -1850 | 181.96  | -1849 | 181.96  | -1848 | 181.96  |
| -1847 | 181.96  | -1846 | 181.96  | -1845 | 181.96  | -1844 | 1099.39 | -1843 | 181.96  | -1842 | 181.96  | -1841 | 181.96  | -1840 | 181.96  | -1839 | 1099.39 | -1838 | 181.96  |
| -1837 | 179.05  | -1836 | 176.13  | -1835 | 176.13  | -1834 | 176.13  | -1833 | 176.13  | -1832 | 176.13  | -1831 | 176.13  | -1830 | 1093.57 | -1829 | 176.13  | -1828 | 176.13  |
| -1827 | 176.13  | -1826 | 176.13  | -1825 | 176.13  | -1824 | 1093.57 | -1823 | 176.13  | -1822 | 176.13  | -1821 | 176.13  | -1820 | 176.13  | -1819 | 176.13  | -1818 | 1093.57 |
| -1817 | 176.13  | -1816 | 176.13  | -1815 | 176.13  | -1814 | 176.13  | -1813 | 176.13  | -1812 | 1060.54 | -1811 | 1417.94 | -1810 | 242.61  | -1809 | 242.61  | -1808 | 242.61  |
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| -1787 | 242.61  | -1786 | 1465.85 | -1785 | 242.61  | -1784 | 238.73  | -1783 | 234.85  | -1782 | 234.85  | -1781 | 234.85  | -1780 | 234.85  | -1779 | 234.85  | -1778 | 234.85  |
| -1777 | 1458.09 | -1776 | 234.85  | -1775 | 234.85  | -1774 | 234.85  | -1773 | 234.85  | -1772 | 234.85  | -1771 | 1458.09 | -1770 | 234.85  | -1769 | 234.85  | -1768 | 234.85  |
| -1767 | 234.85  | -1766 | 234.85  | -1765 | 1458.09 | -1764 | 234.85  | -1763 | 234.85  | -1762 | 234.85  | -1761 | 234.85  | -1760 | 234.85  | -1759 | 1414.06 | -1758 | 1772.43 |
| -1757 | 303.26  | -1756 | 303.26  | -1755 | 303.26  | -1754 | 303.26  | -1753 | 303.26  | -1752 | 303.26  | -1751 | 303.26  | -1750 | 303.26  | -1749 | 303.26  | -1748 | 303.26  |
| -1747 | 303.26  | -1746 | 303.26  | -1745 | 303.26  | -1744 | 303.26  | -1743 | 303.26  | -1742 | 303.26  | -1741 | 303.26  | -1740 | 303.26  | -1739 | 303.26  | -1738 | 1832.31 |
| -1737 | 303.26  | -1736 | 303.26  | -1735 | 303.26  | -1734 | 303.26  | -1733 | 1832.31 | -1732 | 303.26  | -1731 | 298.41  | -1730 | 293.56  | -1729 | 293.56  | -1728 | 293.56  |
| -1727 | 293.56  | -1726 | 293.56  | -1725 | 293.56  | -1724 | 1822.61 | -1723 | 293.56  | -1722 | 293.56  | -1721 | 293.56  | -1720 | 293.56  | -1719 | 293.56  | -1718 | 1822.61 |
| -1717 | 293.56  | -1716 | 293.56  | -1715 | 293.56  | -1714 | 293.56  | -1713 | 293.56  | -1712 | 1822.61 | -1711 | 293.56  | -1710 | 293.56  | -1709 | 293.56  | -1708 | 293.56  |
| -1707 | 293.56  | -1706 | 1767.57 | -1705 | 1772.43 | -1704 | 303.26  | -1703 | 303.26  | -1702 | 303.26  | -1701 | 303.26  | -1700 | 303.26  | -1699 | 303.26  | -1698 | 303.26  |
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| -1677 | 293.56  | -1676 | 293.56  | -1675 | 293.56  | -1674 | 293.56  | -1673 | 293.56  | -1672 | 1822.61 | -1671 | 1822.61 | -1670 | 293.56  | -1669 | 293.56  | -1668 | 293.56  |
| -1667 | 293.56  | -1666 | 293.56  | -1665 | 1822.61 | -1664 | 293.56  | -1663 | 293.56  | -1662 | 293.56  | -1661 | 293.56  | -1660 | 293.56  | -1659 | 1822.61 | -1658 | 293.56  |
| -1657 | 293.56  | -1656 | 293.56  | -1655 | 293.56  | -1654 | 293.56  | -1653 | 1767.57 | -1652 | 1772.43 | -1651 | 203.26  | -1650 | 203.26  | -1649 | 303.26  | -1648 | 303.26  |
| -1647 | 303.26  | -1646 | 303.26  | -1645 | 303.26  | -1644 | 303.26  | -1643 | 303.26  | -1642 | 303.26  | -1641 | 303.26  | -1640 | 303.26  | -1639 | 303.26  | -1638 | 303.26  |
| -1637 | 303.26  | -1636 | 303.26  | -1635 | 303.26  | -1634 | 303.26  | -1633 | 303.26  | -1632 | 1832.31 | -1631 | 303.26  | -1630 | 303.26  | -1629 | 303.26  | -1628 | 303.26  |
| -1627 | 1832.31 | -1626 | 303.26  | -1625 | 298.41  | -1624 | 293.56  | -1623 | 293.56  | -1622 | 293.56  | -1621 | 293.56  | -1620 | 293.56  | -1619 | 293.56  | -1618 | 1822.61 |
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| -1597 | 303.26  | -1596 | 303.26  | -1595 | 303.26  | -1594 | 303.26  | -1593 | 303.26  | -1592 | 303.26  | -1591 | 303.26  | -1590 | 227.45  | -1589 | 151.63  | -1588 | 227.45  |
| -1587 | 303.26  | -1586 | 303.26  | -1585 | 303.26  | -1584 | 303.26  | -1583 | 303.26  | -1582 | 303.26  | -1581 | 303.26  | -1580 | 303.26  | -1579 | 1832.31 | -1578 | 303.26  |
| -1577 | 303.26  | -1576 | 303.26  | -1575 | 303.26  | -1574 | 1832.31 | -1573 | 303.26  | -1572 | 298.41  | -1571 | 293.56  | -1570 | 293.56  | -1569 | 293.56  | -1568 | 293.56  |
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| -1547 | 1767.57 | -1546 | 1772.43 | -1545 | 303.26  | -1544 | 303.26  | -1543 | 303.26  | -1542 | 303.26  | -1541 | 303.26  | -1540 | 303.26  | -1539 | 303.26  | -1538 | 303.26  |
| -1537 | 151.63  | -1536 | 151.63  | -1535 | 303.26  | -1534 | 303.26  | -1533 | 303.26  | -1532 | 303.26  | -1531 | 303.26  | -1530 | 303.26  | -1529 | 303.26  | -1528 | 303.26  |
| -1527 | 1832.31 | -1526 | 303.26  | -1525 | 303.26  | -1524 | 303.26  | -1523 | 303.26  | -1522 | 1832.31 | -1521 | 303.26  | -1520 | 298.41  | -1519 | 293.56  | -1518 | 293.56  |
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| -1507 | 1822.61 | -1506 | 293.56  | -1505 | 293.56  | -1504 | 293.56  | -1503 | 293.56  | -1502 | 293.56  | -1501 | 1822.61 | -1500 | 293.56  | -1499 | 293.56  | -1498 | 293.56  |
| -1497 | 293.56  | -1496 | 293.56  | -1495 | 1767.57 | -1494 | 1772.43 | -1493 | 303.26  | -1492 | 303.26  | -1491 | 303.26  | -1490 | 303.26  | -1489 | 303.26  | -1488 | 303.26  |
| -1487 | 303.26  | -1486 | 303.26  | -1485 | 227.45  | -1484 | 151.63  | -1483 | 227.45  | -1482 | 303.26  | -1481 | 303.26  | -1480 | 303.26  | -1479 | 303.26  | -1478 | 303.26  |
| -1477 | 303.26  | -1476 | 303.26  | -1475 | 303.26  | -1474 | 1832.31 | -1473 | 303.26  | -1472 | 303.26  | -1471 | 303.26  | -1470 | 303.26  | -1469 | 1832.31 | -1468 | 303.26  |
| -1467 | 298.41  | -1466 | 293.56  | -1465 | 293.56  | -1464 | 293.56  | -1463 | 293.56  | -1462 | 293.56  | -1461 | 293.56  | -1460 | 1822.61 | -1459 | 293.56  | -1458 | 293.56  |











|      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| -812 | 0.00 | 0.00 | 4.02 | 4.02 | -811 | 0.00 | 0.00 | 3.95 | 3.95 | -810 | 0.00 | 0.00 | 3.95 | 3.95 | -809 | 0.00 | 0.00 | 3.95 | 3.95 | -808 | 0.00 | 0.00 | 3.95 | 3.95 |
| -807 | 0.00 | 0.00 | 3.95 | 3.95 | -806 | 0.00 | 0.00 | 3.95 | 3.95 | -805 | 0.00 | 0.00 | 3.95 | 3.95 | -804 | 0.00 | 0.00 | 3.95 | 3.95 | -803 | 0.00 | 0.00 | 3.95 | 3.95 |
| -802 | 0.00 | 0.00 | 3.95 | 3.95 | -801 | 0.00 | 0.00 | 3.95 | 3.95 | -800 | 0.00 | 0.00 | 3.95 | 3.95 | -799 | 0.00 | 0.00 | 3.95 | 3.95 | -798 | 0.00 | 0.00 | 3.95 | 3.95 |
| -797 | 0.00 | 0.00 | 3.95 | 3.95 | -796 | 0.00 | 0.00 | 3.95 | 3.95 | -795 | 0.00 | 0.00 | 3.95 | 3.95 | -794 | 0.00 | 0.00 | 3.95 | 3.95 | -793 | 0.00 | 0.00 | 3.95 | 3.95 |
| -792 | 0.00 | 0.00 | 3.95 | 3.95 | -791 | 0.00 | 0.00 | 3.95 | 3.95 | -790 | 0.00 | 0.00 | 3.95 | 3.95 | -789 | 0.00 | 0.00 | 3.95 | 3.95 | -788 | 0.00 | 0.00 | 3.95 | 3.95 |
| -787 | 0.00 | 0.00 | 3.20 | 3.20 | -786 | 0.00 | 0.00 | 2.45 | 2.45 | -785 | 0.00 | 0.00 | 2.45 | 2.45 | -784 | 0.00 | 0.00 | 3.27 | 3.27 | -783 | 0.00 | 0.00 | 3.27 | 3.27 |
| -782 | 0.00 | 0.00 | 4.08 | 4.08 | -781 | 0.00 | 0.00 | 4.08 | 4.08 | -780 | 0.00 | 0.00 | 4.08 | 4.08 | -779 | 0.00 | 0.00 | 4.08 | 4.08 | -778 | 0.00 | 0.00 | 4.08 | 4.08 |
| -777 | 0.00 | 0.00 | 4.08 | 4.08 | -776 | 0.00 | 0.00 | 4.08 | 4.08 | -775 | 0.00 | 0.00 | 4.08 | 4.08 | -774 | 0.00 | 0.00 | 4.08 | 4.08 | -773 | 0.00 | 0.00 | 4.08 | 4.08 |
| -772 | 0.00 | 0.00 | 4.08 | 4.08 | -771 | 0.00 | 0.00 | 4.08 | 4.08 | -770 | 0.00 | 0.00 | 4.08 | 4.08 | -769 | 0.00 | 0.00 | 4.08 | 4.08 | -768 | 0.00 | 0.00 | 4.08 | 4.08 |
| -767 | 0.00 | 0.00 | 4.08 | 4.08 | -766 | 0.00 | 0.00 | 4.08 | 4.08 | -765 | 0.00 | 0.00 | 4.08 | 4.08 | -764 | 0.00 | 0.00 | 4.08 | 4.08 | -763 | 0.00 | 0.00 | 4.08 | 4.08 |
| -762 | 0.00 | 0.00 | 4.08 | 4.08 | -761 | 0.00 | 0.00 | 4.08 | 4.08 | -760 | 0.00 | 0.00 | 4.08 | 4.08 | -759 | 0.00 | 0.00 | 4.08 | 4.08 | -758 | 0.00 | 0.00 | 4.08 | 4.08 |
| -757 | 0.00 | 0.00 | 4.08 | 4.08 | -756 | 0.00 | 0.00 | 4.08 | 4.08 | -755 | 0.00 | 0.00 | 4.08 | 4.08 | -754 | 0.00 | 0.00 | 4.08 | 4.08 | -753 | 0.00 | 0.00 | 4.08 | 4.08 |
| -752 | 0.00 | 0.00 | 4.08 | 4.08 | -751 | 0.00 | 0.00 | 4.08 | 4.08 | -750 | 0.00 | 0.00 | 4.08 | 4.08 | -749 | 0.00 | 0.00 | 4.08 | 4.08 | -748 | 0.00 | 0.00 | 4.08 | 4.08 |
| -747 | 0.00 | 0.00 | 4.08 | 4.08 | -746 | 0.00 | 0.00 | 4.08 | 4.08 | -745 | 0.00 | 0.00 | 4.08 | 4.08 | -744 | 0.00 | 0.00 | 4.08 | 4.08 | -743 | 0.00 | 0.00 | 4.08 | 4.08 |
| -742 | 0.00 | 0.00 | 4.08 | 4.08 | -741 | 0.00 | 0.00 | 4.02 | 4.02 | -740 | 0.00 | 0.00 | 3.95 | 3.95 | -739 | 0.00 | 0.00 | 3.95 | 3.95 | -738 | 0.00 | 0.00 | 3.95 | 3.95 |
| -737 | 0.00 | 0.00 | 3.95 | 3.95 | -736 | 0.00 | 0.00 | 3.95 | 3.95 | -735 | 0.00 | 0.00 | 3.95 | 3.95 | -734 | 0.00 | 0.00 | 3.95 | 3.95 | -733 | 0.00 | 0.00 | 3.95 | 3.95 |
| -732 | 0.00 | 0.00 | 3.95 | 3.95 | -731 | 0.00 | 0.00 | 3.95 | 3.95 | -730 | 0.00 | 0.00 | 3.95 | 3.95 | -729 | 0.00 | 0.00 | 3.95 | 3.95 | -728 | 0.00 | 0.00 | 3.95 | 3.95 |
| -727 | 0.00 | 0.00 | 3.95 | 3.95 | -726 | 0.00 | 0.00 | 3.95 | 3.95 | -725 | 0.00 | 0.00 | 3.95 | 3.95 | -724 | 0.00 | 0.00 | 3.95 | 3.95 | -723 | 0.00 | 0.00 | 3.95 | 3.95 |
| -722 | 0.00 | 0.00 | 3.95 | 3.95 | -721 | 0.00 | 0.00 | 3.95 | 3.95 | -720 | 0.00 | 0.00 | 3.95 | 3.95 | -719 | 0.00 | 0.00 | 3.95 | 3.95 | -718 | 0.00 | 0.00 | 3.95 | 3.95 |
| -717 | 0.00 | 0.00 | 3.95 | 3.95 | -716 | 0.00 | 0.00 | 4.02 | 4.02 |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |

Totale forze sismiche

|           |           |
|-----------|-----------|
| Fx        | Fy        |
| <daN>     | <daN>     |
| 113187.00 | 113187.00 |

Elenco forze sismiche nodali allo SND

| Nodo  | cx   | cy   | Fx <daN> | Fy <daN> | Nodo  | cx   | cy   | Fx <daN> | Fy <daN> | Nodo  | cx   | cy   | Fx <daN> | Fy <daN> | Nodo  | cx   | cy     | Fx <daN> | Fy <daN> |
|-------|------|------|----------|----------|-------|------|------|----------|----------|-------|------|------|----------|----------|-------|------|--------|----------|----------|
| -1917 | 0.00 | 0.00 | 656.00   | 656.00   | -1916 | 0.00 | 0.00 | 836.68   | 836.68   | -1915 | 0.00 | 0.00 | 836.68   | 836.68   | -1914 | 0.00 | 0.00   | 836.68   | 836.68   |
| -1913 | 0.00 | 0.00 | 836.68   | 836.68   | -1912 | 0.00 | 0.00 | 836.68   | 836.68   | -1911 | 0.00 | 0.00 | 836.68   | 836.68   | -1910 | 0.00 | 0.00   | 836.68   | 836.68   |
| -1909 | 0.00 | 0.00 | 836.68   | 836.68   | -1908 | 0.00 | 0.00 | 836.68   | 836.68   | -1907 | 0.00 | 0.00 | 836.68   | 836.68   | -1906 | 0.00 | 0.00   | 836.68   | 836.68   |
| -1905 | 0.00 | 0.00 | 836.68   | 836.68   | -1904 | 0.00 | 0.00 | 836.68   | 836.68   | -1903 | 0.00 | 0.00 | 836.68   | 836.68   | -1902 | 0.00 | 0.00   | 836.68   | 836.68   |
| -1901 | 0.00 | 0.00 | 836.68   | 836.68   | -1900 | 0.00 | 0.00 | 836.68   | 836.68   | -1899 | 0.00 | 0.00 | 836.68   | 836.68   | -1898 | 0.00 | 0.00   | 836.68   | 836.68   |
| -1897 | 0.00 | 0.00 | 1060.89  | 1060.89  | -1896 | 0.00 | 0.00 | 836.68   | 836.68   | -1895 | 0.00 | 0.00 | 836.68   | 836.68   | -1894 | 0.00 | 0.00   | 836.68   | 836.68   |
| -1893 | 0.00 | 0.00 | 836.68   | 836.68   | -1892 | 0.00 | 0.00 | 1060.89  | 1060.89  | -1891 | 0.00 | 0.00 | 836.68   | 836.68   | -1890 | 0.00 | 0.00   | 823.29   | 823.29   |
| -1889 | 0.00 | 0.00 | 809.90   | 809.90   | -1888 | 0.00 | 0.00 | 809.90   | 809.90   | -1887 | 0.00 | 0.00 | 809.90   | 809.90   | -1886 | 0.00 | 0.00   | 809.90   | 809.90   |
| -1885 | 0.00 | 0.00 | 809.90   | 809.90   | -1884 | 0.00 | 0.00 | 809.90   | 809.90   | -1883 | 0.00 | 0.00 | 1034.11  | 1034.11  | -1882 | 0.00 | 0.00   | 809.90   | 809.90   |
| -1881 | 0.00 | 0.00 | 809.90   | 809.90   | -1880 | 0.00 | 0.00 | 809.90   | 809.90   | -1879 | 0.00 | 0.00 | 809.90   | 809.90   | -1878 | 0.00 | 0.00   | 809.90   | 809.90   |
| -1877 | 0.00 | 0.00 | 1034.11  | 1034.11  | -1876 | 0.00 | 0.00 | 809.90   | 809.90   | -1875 | 0.00 | 0.00 | 809.90   | 809.90   | -1874 | 0.00 | 0.00   | 809.90   | 809.90   |
| -1873 | 0.00 | 0.00 | 809.90   | 809.90   | -1872 | 0.00 | 0.00 | 809.90   | 809.90   | -1871 | 0.00 | 0.00 | 1034.11  | 1034.11  | -1870 | 0.00 | 0.00   | 809.90   | 809.90   |
| -1869 | 0.00 | 0.00 | 809.90   | 809.90   | -1868 | 0.00 | 0.00 | 809.90   | 809.90   | -1867 | 0.00 | 0.00 | 809.90   | 809.90   | -1866 | 0.00 | 0.00   | 809.90   | 809.90   |
| -1865 | 0.00 | 0.00 | 642.62   | 642.62   | -1864 | 0.00 | 0.00 | 519.79   | 519.79   | -1863 | 0.00 | 0.00 | 88.94    | 88.94    | -1862 | 0.00 | 0.00   | 88.94    | 88.94    |
| -1861 | 0.00 | 0.00 | 88.94    | 88.94    | -1860 | 0.00 | 0.00 | 88.94    | 88.94    | -1859 | 0.00 | 0.00 | 88.94    | 88.94    | -1858 | 0.00 | 0.00   | 88.94    | 88.94    |
| -1857 | 0.00 | 0.00 | 88.94    | 88.94    | -1856 | 0.00 | 0.00 | 88.94    | 88.94    | -1855 | 0.00 | 0.00 | 88.94    | 88.94    | -1854 | 0.00 | 0.00   | 88.94    | 88.94    |
| -1853 | 0.00 | 0.00 | 88.94    | 88.94    | -1852 | 0.00 | 0.00 | 88.94    | 88.94    | -1851 | 0.00 | 0.00 | 88.94    | 88.94    | -1850 | 0.00 | 0.00   | 88.94    | 88.94    |
| -1849 | 0.00 | 0.00 | 88.94    | 88.94    | -1848 | 0.00 | 0.00 | 88.94    | 88.94    | -1847 | 0.00 | 0.00 | 88.94    | 88.94    | -1846 | 0.00 | 0.00   | 88.94    | 88.94    |
| -1845 | 0.00 | 0.00 | 88.94    | 88.94    | -1844 | 0.00 | 0.00 | 537.36   | 537.36   | -1843 | 0.00 | 0.00 | 88.94    | 88.94    | -1842 | 0.00 | 0.00   | 88.94    | 88.94    |
| -1841 | 0.00 | 0.00 | 88.94    | 88.94    | -1840 | 0.00 | 0.00 | 88.94    | 88.94    | -1839 | 0.00 | 0.00 | 537.36   | 537.36   | -1838 | 0.00 | 0.00   | 88.94    | 88.94    |
| -1837 | 0.00 | 0.00 | 87.51    | 87.51    | -1836 | 0.00 | 0.00 | 86.09    | 86.09    | -1835 | 0.00 | 0.00 | 86.09    | 86.09    | -1834 | 0.00 | 0.00   | 86.09    | 86.09    |
| -1833 | 0.00 | 0.00 | 86.09    | 86.09    | -1832 | 0.00 | 0.00 | 86.09    | 86.09    | -1831 | 0.00 | 0.00 | 86.09    | 86.09    | -1830 | 0.00 | 0.00   | 534.51   | 534.51   |
| -1829 | 0.00 | 0.00 | 86.09    | 86.09    | -1828 | 0.00 | 0.00 | 86.09    | 86.09    | -1827 | 0.00 | 0.00 | 86.09    | 86.09    | -1826 | 0.00 | 0.00   | 86.09    | 86.09    |
| -1825 | 0.00 | 0.00 | 86.09    | 86.09    | -1824 | 0.00 | 0.00 | 534.51   | 534.51   | -1823 | 0.00 | 0.00 | 86.09    | 86.09    | -1822 | 0.00 | 0.00   | 86.09    | 86.09    |
| -1821 | 0.00 | 0.00 | 86.09    | 86.09    | -1820 | 0.00 | 0.00 | 86.09    | 86.09    | -1819 | 0.00 | 0.00 | 86.09    | 86.09    | -1818 | 0.00 | 0.00   | 534.51   | 534.51   |
| -1817 | 0.00 | 0.00 | 86.09    | 86.09    | -1816 | 0.00 | 0.00 | 86.09    | 86.09    | -1815 | 0.00 | 0.00 | 86.09    | 86.09    | -1814 | 0.00 | 0.00   | 86.09    | 86.09    |
| -1813 | 0.00 | 0.00 | 86.09    | 86.09    | -1812 | 0.00 | 0.00 | 518.37   | 518.37   | -1811 | 0.00 | 0.00 | 693.06   | 693.06   | -1810 | 0.00 | 0.00   | 118.58   | 118.58   |
| -1809 | 0.00 | 0.00 | 118.58   | 118.58   | -1808 | 0.00 | 0.00 | 118.58   | 118.58   | -1807 | 0.00 | 0.00 | 118.58   | 118.58   | -1806 | 0.00 | 0.00   | 118.58   | 118.58   |
| -1805 | 0.00 | 0.00 | 118.58   | 118.58   | -1804 | 0.00 | 0.00 | 118.58   | 118.58   | -1803 | 0.00 | 0.00 | 118.58   | 118.58   | -1802 | 0.00 | 0.00   | 118.58   | 118.58   |
| -1801 | 0.00 | 0.00 | 118.58   | 118.58   | -1800 | 0.00 | 0.00 | 118.58   | 118.58   | -1799 | 0.00 | 0.00 | 118.58   | 118.58   | -1798 | 0.00 | 0.00   | 118.58   | 118.58   |
| -1797 | 0.00 | 0.00 | 118.58   | 118.58   | -1796 | 0.00 | 0.00 | 118.58   | 118.58   | -1795 | 0.00 | 0.00 | 118.58   | 118.58   | -1794 | 0.00 | 0.00   | 118.58   | 118.58   |
| -1793 | 0.00 | 0.00 | 118.58   | 118.58   | -1792 | 0.00 | 0.00 | 118.58   | 118.58   | -1791 | 0.00 | 0.00 | 716.48   | 716.48   | -1790 | 0.00 | 0.00   | 118.58   | 118.58   |
| -1789 | 0.00 | 0.00 | 118.58   | 118.58   | -1788 | 0.00 | 0.00 | 118.58   | 118.58   | -1787 | 0.00 | 0.00 | 118.58   | 118.58   | -1786 | 0.00 | 0.00   | 716.48   | 716.48   |
| -1785 | 0.00 | 0.00 | 118.58   | 118.58   | -1784 | 0.00 | 0.00 | 116.69   | 116.69   | -1783 | 0.00 | 0.00 | 114.79   | 114.79   | -1782 | 0.00 | 0.00   | 114.79   | 114.79   |
| -1781 | 0.00 | 0.00 | 114.79   | 114.79   | -1780 | 0.00 | 0.00 | 114.79   | 114.79   | -1779 | 0.00 | 0.00 | 114.79   | 114.79   | -1778 | 0.00 | 0.00   | 114.79   | 114.79   |
| -1777 | 0.00 | 0.00 | 712.68   | 712.68   | -1776 | 0.00 | 0.00 | 114.79   | 114.79   | -1775 | 0.00 | 0.00 | 114.79   | 114.79   | -1774 | 0.00 | 0.00   | 114.79   | 114.79   |
| -1773 | 0.00 | 0.00 | 114.79   | 114.79   | -1772 | 0.00 | 0.00 | 114.79   | 114.79   | -1771 | 0.00 | 0.00 | 712.68   | 712.68   | -1770 | 0.00 | 0.00</ |          |          |







|      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| -821 | 0.00 | 0.00 | 8.10 | 8.10 | -820 | 0.00 | 0.00 | 8.10 | 8.10 | -819 | 0.00 | 0.00 | 8.10 | 8.10 | -818 | 0.00 | 0.00 | 8.10 | 8.10 |
| -817 | 0.00 | 0.00 | 8.10 | 8.10 | -816 | 0.00 | 0.00 | 8.10 | 8.10 | -815 | 0.00 | 0.00 | 8.10 | 8.10 | -814 | 0.00 | 0.00 | 8.10 | 8.10 |
| -813 | 0.00 | 0.00 | 8.10 | 8.10 | -812 | 0.00 | 0.00 | 7.97 | 7.97 | -811 | 0.00 | 0.00 | 7.84 | 7.84 | -810 | 0.00 | 0.00 | 7.84 | 7.84 |
| -809 | 0.00 | 0.00 | 7.84 | 7.84 | -808 | 0.00 | 0.00 | 7.84 | 7.84 | -807 | 0.00 | 0.00 | 7.84 | 7.84 | -806 | 0.00 | 0.00 | 7.84 | 7.84 |
| -805 | 0.00 | 0.00 | 7.84 | 7.84 | -804 | 0.00 | 0.00 | 7.84 | 7.84 | -803 | 0.00 | 0.00 | 7.84 | 7.84 | -802 | 0.00 | 0.00 | 7.84 | 7.84 |
| -801 | 0.00 | 0.00 | 7.84 | 7.84 | -800 | 0.00 | 0.00 | 7.84 | 7.84 | -799 | 0.00 | 0.00 | 7.84 | 7.84 | -798 | 0.00 | 0.00 | 7.84 | 7.84 |
| -797 | 0.00 | 0.00 | 7.84 | 7.84 | -796 | 0.00 | 0.00 | 7.84 | 7.84 | -795 | 0.00 | 0.00 | 7.84 | 7.84 | -794 | 0.00 | 0.00 | 7.84 | 7.84 |
| -793 | 0.00 | 0.00 | 7.84 | 7.84 | -792 | 0.00 | 0.00 | 7.84 | 7.84 | -791 | 0.00 | 0.00 | 7.84 | 7.84 | -790 | 0.00 | 0.00 | 7.84 | 7.84 |
| -789 | 0.00 | 0.00 | 7.84 | 7.84 | -788 | 0.00 | 0.00 | 7.84 | 7.84 | -787 | 0.00 | 0.00 | 6.35 | 6.35 | -786 | 0.00 | 0.00 | 4.86 | 4.86 |
| -785 | 0.00 | 0.00 | 4.86 | 4.86 | -784 | 0.00 | 0.00 | 6.48 | 6.48 | -783 | 0.00 | 0.00 | 6.48 | 6.48 | -782 | 0.00 | 0.00 | 8.10 | 8.10 |
| -781 | 0.00 | 0.00 | 8.10 | 8.10 | -780 | 0.00 | 0.00 | 8.10 | 8.10 | -779 | 0.00 | 0.00 | 8.10 | 8.10 | -778 | 0.00 | 0.00 | 8.10 | 8.10 |
| -777 | 0.00 | 0.00 | 8.10 | 8.10 | -776 | 0.00 | 0.00 | 8.10 | 8.10 | -775 | 0.00 | 0.00 | 8.10 | 8.10 | -774 | 0.00 | 0.00 | 8.10 | 8.10 |
| -773 | 0.00 | 0.00 | 8.10 | 8.10 | -772 | 0.00 | 0.00 | 8.10 | 8.10 | -771 | 0.00 | 0.00 | 8.10 | 8.10 | -770 | 0.00 | 0.00 | 8.10 | 8.10 |
| -769 | 0.00 | 0.00 | 8.10 | 8.10 | -768 | 0.00 | 0.00 | 8.10 | 8.10 | -767 | 0.00 | 0.00 | 8.10 | 8.10 | -766 | 0.00 | 0.00 | 8.10 | 8.10 |
| -765 | 0.00 | 0.00 | 8.10 | 8.10 | -764 | 0.00 | 0.00 | 8.10 | 8.10 | -763 | 0.00 | 0.00 | 8.10 | 8.10 | -762 | 0.00 | 0.00 | 8.10 | 8.10 |
| -761 | 0.00 | 0.00 | 8.10 | 8.10 | -760 | 0.00 | 0.00 | 8.10 | 8.10 | -759 | 0.00 | 0.00 | 8.10 | 8.10 | -758 | 0.00 | 0.00 | 8.10 | 8.10 |
| -757 | 0.00 | 0.00 | 8.10 | 8.10 | -756 | 0.00 | 0.00 | 8.10 | 8.10 | -755 | 0.00 | 0.00 | 8.10 | 8.10 | -754 | 0.00 | 0.00 | 8.10 | 8.10 |
| -753 | 0.00 | 0.00 | 8.10 | 8.10 | -752 | 0.00 | 0.00 | 8.10 | 8.10 | -751 | 0.00 | 0.00 | 8.10 | 8.10 | -750 | 0.00 | 0.00 | 8.10 | 8.10 |
| -749 | 0.00 | 0.00 | 8.10 | 8.10 | -748 | 0.00 | 0.00 | 8.10 | 8.10 | -747 | 0.00 | 0.00 | 8.10 | 8.10 | -746 | 0.00 | 0.00 | 8.10 | 8.10 |
| -745 | 0.00 | 0.00 | 8.10 | 8.10 | -744 | 0.00 | 0.00 | 8.10 | 8.10 | -743 | 0.00 | 0.00 | 8.10 | 8.10 | -742 | 0.00 | 0.00 | 8.10 | 8.10 |
| -741 | 0.00 | 0.00 | 7.97 | 7.97 | -740 | 0.00 | 0.00 | 7.84 | 7.84 | -739 | 0.00 | 0.00 | 7.84 | 7.84 | -738 | 0.00 | 0.00 | 7.84 | 7.84 |
| -737 | 0.00 | 0.00 | 7.84 | 7.84 | -736 | 0.00 | 0.00 | 7.84 | 7.84 | -735 | 0.00 | 0.00 | 7.84 | 7.84 | -734 | 0.00 | 0.00 | 7.84 | 7.84 |
| -733 | 0.00 | 0.00 | 7.84 | 7.84 | -732 | 0.00 | 0.00 | 7.84 | 7.84 | -731 | 0.00 | 0.00 | 7.84 | 7.84 | -730 | 0.00 | 0.00 | 7.84 | 7.84 |
| -729 | 0.00 | 0.00 | 7.84 | 7.84 | -728 | 0.00 | 0.00 | 7.84 | 7.84 | -727 | 0.00 | 0.00 | 7.84 | 7.84 | -726 | 0.00 | 0.00 | 7.84 | 7.84 |
| -725 | 0.00 | 0.00 | 7.84 | 7.84 | -724 | 0.00 | 0.00 | 7.84 | 7.84 | -723 | 0.00 | 0.00 | 7.84 | 7.84 | -722 | 0.00 | 0.00 | 7.84 | 7.84 |
| -721 | 0.00 | 0.00 | 7.84 | 7.84 | -720 | 0.00 | 0.00 | 7.84 | 7.84 | -719 | 0.00 | 0.00 | 7.84 | 7.84 | -718 | 0.00 | 0.00 | 7.84 | 7.84 |
| -717 | 0.00 | 0.00 | 7.84 | 7.84 | -716 | 0.00 | 0.00 | 7.97 | 7.97 |      |      |      |      |      |      |      |      |      |      |

Totali forze sismiche

|           |           |
|-----------|-----------|
| <b>Fx</b> | <b>Fy</b> |
| <daN>     | <daN>     |
| 224360.00 | 224360.00 |

Domanda in duttilità di curvatura

Direzione X  $\mu_{edX}$ =29.69

Direzione Y  $\mu_{edY}$ =29.69

Tensioni sul terreno

Simbologia

$\sigma_t$  = Tensione sul terreno

CC = Numero della combinazione delle condizioni di carico elementari

Nodo = Numero del nodo

TCC = Tipo di combinazioni di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

SLD = Stato limite di danno

SND = Stato limite di salvaguardia della vita (non dissipativo)

| Nodo | CC   | TCC | $\sigma_t$ | Nodo  | CC   | TCC  | $\sigma_t$ | Nodo | CC    | TCC  | $\sigma_t$ | Nodo | CC  | TCC   | $\sigma_t$ | Nodo | CC | TCC | $\sigma_t$ |      |      |    |     |      |
|------|------|-----|------------|-------|------|------|------------|------|-------|------|------------|------|-----|-------|------------|------|----|-----|------------|------|------|----|-----|------|
|      |      |     | <daN/cm²>  |       |      |      | <daN/cm²>  |      |       |      | <daN/cm²>  |      |     |       | <daN/cm²>  |      |    |     | <daN/cm²>  |      |      |    |     |      |
| -715 | Max  | 9   | SND        | 0.91  | -715 | Min. | 15         | SND  | -0.02 | -714 | Max        | 9    | SND | 0.91  | -714       | Min. | 15 | SND | -0.01      | -713 | Max  | 9  | SND | 0.91 |
| -713 | Min. | 15  | SND        | -0.01 | -712 | Max  | 9          | SND  | 0.91  | -712 | Min.       | 15   | SND | -0.00 | -711       | Max  | 9  | SND | 0.91       | -711 | Min. | 15 | SND | 0.00 |
| -710 | Max  | 9   | SND        | 0.91  | -710 | Min. | 15         | SND  | 0.01  | -709 | Max        | 9    | SND | 0.90  | -709       | Min. | 15 | SND | 0.01       | -708 | Max  | 9  | SND | 0.90 |
| -708 | Min. | 15  | SND        | 0.01  | -707 | Max  | 9          | SND  | 0.90  | -707 | Min.       | 15   | SND | 0.02  | -706       | Max  | 9  | SND | 0.90       | -706 | Min. | 15 | SND | 0.02 |
| -705 | Max  | 9   | SND        | 0.90  | -705 | Min. | 15         | SND  | 0.03  | -704 | Max        | 9    | SND | 0.90  | -704       | Min. | 15 | SND | 0.03       | -703 | Max  | 9  | SND | 0.90 |
| -703 | Min. | 15  | SND        | 0.03  | -702 | Max  | 9          | SND  | 0.90  | -702 | Min.       | 15   | SND | 0.04  | -701       | Max  | 9  | SND | 0.90       | -701 | Min. | 15 | SND | 0.04 |
| -700 | Max  | 9   | SND        | 0.90  | -700 | Min. | 15         | SND  | 0.04  | -699 | Max        | 9    | SND | 0.90  | -699       | Min. | 15 | SND | 0.05       | -698 | Max  | 9  | SND | 0.90 |
| -698 | Min. | 15  | SND        | 0.05  | -697 | Max  | 9          | SND  | 0.90  | -697 | Min.       | 15   | SND | 0.05  | -696       | Max  | 9  | SND | 0.90       | -696 | Min. | 15 | SND | 0.06 |
| -695 | Max  | 9   | SND        | 0.90  | -695 | Min. | 15         | SND  | 0.06  | -694 | Max        | 9    | SND | 0.90  | -694       | Min. | 15 | SND | 0.06       | -693 | Max  | 9  | SND | 0.90 |
| -693 | Min. | 15  | SND        | 0.07  | -692 | Max  | 9          | SND  | 0.90  | -692 | Min.       | 15   | SND | 0.07  | -691       | Max  | 9  | SND | 0.90       | -691 | Min. | 15 | SND | 0.07 |
| -690 | Max  | 9   | SND        | 0.90  | -690 | Min. | 15         | SND  | 0.08  | -689 | Max        | 9    | SND | 0.90  | -689       | Min. | 15 | SND | 0.08       | -688 | Max  | 11 | SND | 0.90 |
| -688 | Min. | 13  | SND        | 0.08  | -687 | Max  | 11         | SND  | 0.90  | -687 | Min.       | 13   | SND | 0.08  | -686       | Max  | 11 | SND | 0.91       | -686 | Min. | 13 | SND | 0.08 |
| -685 | Max  | 11  | SND        | 0.91  | -685 | Min. | 13         | SND  | 0.08  | -684 | Max        | 11   | SND | 0.91  | -684       | Min. | 13 | SND | 0.08       | -683 | Max  | 11 | SND | 0.91 |
| -683 | Min. | 13  | SND        | 0.08  | -682 | Max  | 11         | SND  | 0.92  | -682 | Min.       | 13   | SND | 0.08  | -681       | Max  | 11 | SND | 0.92       | -681 | Min. | 13 | SND | 0.08 |
| -680 | Max  | 11  | SND        | 0.92  | -680 | Min. | 13         | SND  | 0.08  | -679 | Max        | 11   | SND | 0.93  | -679       | Min. | 13 | SND | 0.08       | -678 | Max  | 11 | SND | 0.93 |
| -678 | Min. | 13  | SND        | 0.08  | -677 | Max  | 11         | SND  | 0.93  | -677 | Min.       | 13   | SND | 0.08  | -676       | Max  | 11 | SND | 0.94       | -676 | Min. | 13 | SND | 0.08 |
| -675 | Max  | 11  | SND        | 0.94  | -675 | Min. | 13         | SND  | 0.08  | -674 | Max        | 11   | SND | 0.94  | -674       | Min. | 13 | SND | 0.08       | -673 | Max  | 11 | SND | 0.95 |
| -673 | Min. | 13  | SND        | 0.08  | -672 | Max  | 11         | SND  | 0.95  | -672 | Min.       | 13   | SND | 0.08  | -671       | Max  | 11 | SND | 0.95       | -671 | Min. | 13 | SND | 0.08 |
| -670 | Max  | 11  | SND        | 0.96  | -670 | Min. | 13         | SND  | 0.08  | -669 | Max        | 11   | SND | 0.96  | -669       | Min. | 13 | SND | 0.07       | -668 | Max  | 11 | SND | 0.96 |
| -668 | Min. | 13  | SND        | 0.07  | -667 | Max  | 11         | SND  | 0.97  | -667 | Min.       | 13   | SND | 0.07  | -666       | Max  | 11 | SND | 0.97       | -666 | Min. | 13 | SND | 0.07 |
| -665 | Max  | 11  | SND        | 0.98  | -665 | Min. | 13         | SND  | 0.07  | -664 | Max        | 11   | SND | 0.98  | -664       | Min. | 13 | SND | 0.07       | -663 | Max  | 11 | SND | 0.98 |
| -663 | Min. | 13  | SND        | 0.06  | -662 | Max  | 11         | SND  | 0.99  | -662 | Min.       | 13   | SND | 0.06  | -661       | Max  | 11 | SND | 0.99       | -661 | Min. | 13 | SND | 0.06 |
| -660 | Max  | 9   | SND        | 0.83  | -660 | Min. | 15         | SND  | 0.06  | -659 | Max        | 9    | SND | 0.83  | -659       | Min. | 15 | SND | 0.07       | -658 | Max  | 9  | SND | 0.83 |
| -658 | Min. | 15  | SND        | 0.07  | -657 | Max  | 9          | SND  | 0.83  | -657 | Min.       | 15   | SND | 0.07  | -656       | Max  | 9  | SND | 0.83       | -656 | Min. | 15 | SND | 0.08 |
| -655 | Max  | 9   | SND        | 0.83  | -655 | Min. | 15         | SND  | 0.08  | -654 | Max        | 9    | SND | 0.83  | -654       | Min. | 15 | SND | 0.09       | -653 | Max  | 9  | SND | 0.82 |
| -653 | Min. | 15  | SND        | 0.09  | -652 | Max  | 9          | SND  | 0.82  | -652 | Min.       | 15   | SND | 0.09  | -651       | Max  | 9  | SND | 0.82       | -651 | Min. | 15 | SND | 0.10 |
| -650 | Max  | 9   | SND        | 0.82  | -650 | Min. | 15         | SND  | 0.10  | -649 | Max        | 9    | SND | 0.82  | -649       | Min. | 15 | SND | 0.10       | -648 | Max  | 9  | SND | 0.82 |
| -648 | Min. | 15  | SND        | 0.11  | -647 | Max  | 9          | SND  | 0.82  | -647 | Min.       | 15   | SND | 0.11  | -646       | Max  | 9  | SND | 0.82       | -646 | Min. | 15 | SND | 0.11 |
| -645 | Max  | 9   | SND        | 0.82  | -645 | Min. | 15         | SND  | 0.12  | -644 | Max        | 9    | SND | 0.82  | -644       | Min. | 15 | SND | 0.12       | -643 | Max  | 9  | SND | 0.82 |
| -643 | Min. | 15  | SND        | 0.12  | -642 | Max  | 9          | SND  | 0.82  | -642 | Min.       | 15   | SND | 0.13  | -641       | Max  | 9  | SND | 0.82       | -641 | Min. | 15 | SND | 0.13 |
| -640 | Max  | 9   | SND        | 0.82  | -640 | Min. | 15         | SND  | 0.13  | -639 | Max        | 9    | SND | 0.82  | -639       | Min. | 15 | SND | 0.14       | -638 | Max  | 9  | SND | 0.82 |
| -638 | Min. | 15  | SND        | 0.14  | -637 | Max  | 9          | SND  | 0.82  | -637 | Min.       | 15   | SND | 0.14  | -636       | Max  | 9  | SND | 0.82       | -636 | Min. | 15 | SND | 0.14 |
| -635 | Max  | 9   | SND        | 0.82  | -635 | Min. | 15         | SND  | 0.15  | -634 | Max        | 9    | SND | 0.82  | -634       | Min. | 15 | SND | 0.15       | -633 | Max  | 11 | SND | 0.82 |
| -633 | Min. | 13  |            |       |      |      |            |      |       |      |            |      |     |       |            |      |    |     |            |      |      |    |     |      |





|      |      |    |     |      |      |      |    |     |      |      |      |    |     |      |      |      |    |     |      |      |      |    |     |      |
|------|------|----|-----|------|------|------|----|-----|------|------|------|----|-----|------|------|------|----|-----|------|------|------|----|-----|------|
| -345 | Max  | 17 | SLU | 0.69 | -345 | Min. | 3  | SND | 0.44 | -344 | Max  | 17 | SLU | 0.69 | -344 | Min. | 3  | SND | 0.44 | -343 | Max  | 17 | SLU | 0.70 |
| -343 | Min. | 3  | SND | 0.44 | -342 | Max  | 17 | SLU | 0.70 | -342 | Min. | 3  | SND | 0.44 | -341 | Max  | 17 | SLU | 0.70 | -341 | Min. | 3  | SND | 0.44 |
| -340 | Max  | 17 | SLU | 0.71 | -340 | Min. | 3  | SND | 0.43 | -339 | Max  | 17 | SLU | 0.71 | -339 | Min. | 3  | SND | 0.43 | -338 | Max  | 17 | SLU | 0.71 |
| -338 | Min. | 3  | SND | 0.43 | -337 | Max  | 17 | SLU | 0.72 | -337 | Min. | 3  | SND | 0.43 | -336 | Max  | 17 | SLU | 0.72 | -336 | Min. | 3  | SND | 0.43 |
| -335 | Max  | 17 | SLU | 0.72 | -335 | Min. | 3  | SND | 0.43 | -334 | Max  | 17 | SLU | 0.73 | -334 | Min. | 3  | SND | 0.43 | -333 | Max  | 17 | SLU | 0.73 |
| -333 | Min. | 3  | SND | 0.43 | -332 | Max  | 17 | SLU | 0.74 | -332 | Min. | 3  | SND | 0.43 | -331 | Max  | 17 | SLU | 0.74 | -331 | Min. | 3  | SND | 0.43 |
| -330 | Max  | 17 | SLU | 0.62 | -330 | Min. | 5  | SND | 0.34 | -329 | Max  | 17 | SLU | 0.63 | -329 | Min. | 5  | SND | 0.35 | -328 | Max  | 17 | SLU | 0.63 |
| -328 | Min. | 5  | SND | 0.35 | -327 | Max  | 17 | SLU | 0.63 | -327 | Min. | 5  | SND | 0.36 | -326 | Max  | 17 | SLU | 0.62 | -326 | Min. | 5  | SND | 0.36 |
| -325 | Max  | 17 | SLU | 0.63 | -325 | Min. | 5  | SND | 0.36 | -324 | Max  | 17 | SLU | 0.63 | -324 | Min. | 5  | SND | 0.37 | -323 | Max  | 17 | SLU | 0.63 |
| -323 | Min. | 5  | SND | 0.37 | -322 | Max  | 17 | SLU | 0.63 | -322 | Min. | 5  | SND | 0.38 | -321 | Max  | 17 | SLU | 0.63 | -321 | Min. | 5  | SND | 0.38 |
| -320 | Max  | 17 | SLU | 0.63 | -320 | Min. | 5  | SND | 0.38 | -319 | Max  | 17 | SLU | 0.63 | -319 | Min. | 5  | SND | 0.39 | -318 | Max  | 17 | SLU | 0.63 |
| -318 | Min. | 5  | SND | 0.39 | -317 | Max  | 17 | SLU | 0.64 | -317 | Min. | 11 | SND | 0.40 | -316 | Max  | 17 | SLU | 0.64 | -316 | Min. | 11 | SND | 0.40 |
| -315 | Max  | 17 | SLU | 0.64 | -315 | Min. | 11 | SND | 0.40 | -314 | Max  | 17 | SLU | 0.64 | -314 | Min. | 11 | SND | 0.40 | -313 | Max  | 17 | SLU | 0.64 |
| -313 | Min. | 11 | SND | 0.41 | -312 | Max  | 17 | SLU | 0.64 | -312 | Min. | 11 | SND | 0.41 | -311 | Max  | 17 | SLU | 0.65 | -311 | Min. | 11 | SND | 0.41 |
| -310 | Max  | 17 | SLU | 0.65 | -310 | Min. | 11 | SND | 0.41 | -309 | Max  | 17 | SLU | 0.65 | -309 | Min. | 11 | SND | 0.42 | -308 | Max  | 17 | SLU | 0.65 |
| -308 | Min. | 11 | SND | 0.42 | -307 | Max  | 17 | SLU | 0.66 | -307 | Min. | 11 | SND | 0.42 | -306 | Max  | 17 | SLU | 0.66 | -306 | Min. | 11 | SND | 0.42 |
| -305 | Max  | 17 | SLU | 0.66 | -305 | Min. | 11 | SND | 0.43 | -304 | Max  | 17 | SLU | 0.66 | -304 | Min. | 11 | SND | 0.43 | -303 | Max  | 17 | SLU | 0.66 |
| -303 | Min. | 9  | SND | 0.43 | -302 | Max  | 17 | SLU | 0.67 | -302 | Min. | 9  | SND | 0.43 | -301 | Max  | 17 | SLU | 0.67 | -301 | Min. | 9  | SND | 0.43 |
| -300 | Max  | 17 | SLU | 0.67 | -300 | Min. | 9  | SND | 0.43 | -299 | Max  | 17 | SLU | 0.67 | -299 | Min. | 9  | SND | 0.43 | -298 | Max  | 17 | SLU | 0.67 |
| -298 | Min. | 9  | SND | 0.43 | -297 | Max  | 17 | SLU | 0.68 | -297 | Min. | 9  | SND | 0.43 | -296 | Max  | 17 | SLU | 0.68 | -296 | Min. | 9  | SND | 0.43 |
| -295 | Max  | 17 | SLU | 0.68 | -295 | Min. | 9  | SND | 0.43 | -294 | Max  | 17 | SLU | 0.68 | -294 | Min. | 9  | SND | 0.43 | -293 | Max  | 17 | SLU | 0.68 |
| -293 | Min. | 9  | SND | 0.43 | -292 | Max  | 17 | SLU | 0.69 | -292 | Min. | 9  | SND | 0.43 | -291 | Max  | 17 | SLU | 0.69 | -291 | Min. | 9  | SND | 0.43 |
| -290 | Max  | 17 | SLU | 0.69 | -290 | Min. | 9  | SND | 0.44 | -289 | Max  | 17 | SLU | 0.69 | -289 | Min. | 1  | SND | 0.44 | -288 | Max  | 17 | SLU | 0.70 |
| -288 | Min. | 1  | SND | 0.43 | -287 | Max  | 17 | SLU | 0.70 | -287 | Min. | 1  | SND | 0.43 | -286 | Max  | 17 | SLU | 0.70 | -286 | Min. | 1  | SND | 0.43 |
| -285 | Max  | 17 | SLU | 0.71 | -285 | Min. | 1  | SND | 0.43 | -284 | Max  | 17 | SLU | 0.71 | -284 | Min. | 1  | SND | 0.43 | -283 | Max  | 17 | SLU | 0.71 |
| -283 | Min. | 1  | SND | 0.43 | -282 | Max  | 17 | SLU | 0.72 | -282 | Min. | 1  | SND | 0.43 | -281 | Max  | 17 | SLU | 0.72 | -281 | Min. | 1  | SND | 0.43 |
| -280 | Max  | 17 | SLU | 0.72 | -280 | Min. | 1  | SND | 0.42 | -279 | Max  | 17 | SLU | 0.73 | -279 | Min. | 1  | SND | 0.42 | -278 | Max  | 17 | SLU | 0.73 |
| -278 | Min. | 1  | SND | 0.42 | -277 | Max  | 17 | SLU | 0.74 | -277 | Min. | 1  | SND | 0.42 | -276 | Max  | 17 | SLU | 0.74 | -276 | Min. | 1  | SND | 0.42 |
| -275 | Max  | 17 | SLU | 0.62 | -275 | Min. | 11 | SND | 0.30 | -274 | Max  | 17 | SLU | 0.62 | -274 | Min. | 11 | SND | 0.30 | -273 | Max  | 17 | SLU | 0.63 |
| -273 | Min. | 11 | SND | 0.30 | -272 | Max  | 17 | SLU | 0.63 | -272 | Min. | 11 | SND | 0.30 | -271 | Max  | 17 | SLU | 0.63 | -271 | Min. | 11 | SND | 0.30 |
| -270 | Max  | 17 | SLU | 0.63 | -270 | Min. | 11 | SND | 0.31 | -269 | Max  | 17 | SLU | 0.63 | -269 | Min. | 11 | SND | 0.31 | -268 | Max  | 17 | SLU | 0.63 |
| -268 | Min. | 11 | SND | 0.31 | -267 | Max  | 17 | SLU | 0.63 | -267 | Min. | 11 | SND | 0.31 | -266 | Max  | 17 | SLU | 0.63 | -266 | Min. | 11 | SND | 0.31 |
| -265 | Max  | 17 | SLU | 0.63 | -265 | Min. | 11 | SND | 0.32 | -264 | Max  | 17 | SLU | 0.63 | -264 | Min. | 11 | SND | 0.32 | -263 | Max  | 17 | SLU | 0.64 |
| -263 | Min. | 11 | SND | 0.32 | -262 | Max  | 17 | SLU | 0.64 | -262 | Min. | 11 | SND | 0.33 | -261 | Max  | 17 | SLU | 0.64 | -261 | Min. | 11 | SND | 0.33 |
| -260 | Max  | 17 | SLU | 0.64 | -260 | Min. | 11 | SND | 0.33 | -259 | Max  | 17 | SLU | 0.64 | -259 | Min. | 11 | SND | 0.33 | -258 | Max  | 17 | SLU | 0.64 |
| -258 | Min. | 11 | SND | 0.34 | -257 | Max  | 17 | SLU | 0.65 | -257 | Min. | 11 | SND | 0.34 | -256 | Max  | 17 | SLU | 0.65 | -256 | Min. | 11 | SND | 0.34 |
| -255 | Max  | 17 | SLU | 0.65 | -255 | Min. | 11 | SND | 0.34 | -254 | Max  | 17 | SLU | 0.65 | -254 | Min. | 11 | SND | 0.35 | -253 | Max  | 17 | SLU | 0.66 |
| -253 | Min. | 11 | SND | 0.35 | -252 | Max  | 17 | SLU | 0.66 | -252 | Min. | 11 | SND | 0.35 | -251 | Max  | 17 | SLU | 0.66 | -251 | Min. | 11 | SND | 0.35 |
| -250 | Max  | 17 | SLU | 0.66 | -250 | Min. | 11 | SND | 0.36 | -249 | Max  | 17 | SLU | 0.66 | -249 | Min. | 11 | SND | 0.36 | -248 | Max  | 17 | SLU | 0.67 |
| -248 | Min. | 9  | SND | 0.36 | -247 | Max  | 17 | SLU | 0.67 | -247 | Min. | 9  | SND | 0.36 | -246 | Max  | 17 | SLU | 0.67 | -246 | Min. | 9  | SND | 0.36 |
| -245 | Max  | 17 | SLU | 0.67 | -245 | Min. | 9  | SND | 0.36 | -244 | Max  | 17 | SLU | 0.67 | -244 | Min. | 9  | SND | 0.36 | -243 | Max  | 17 | SLU | 0.68 |
| -243 | Min. | 9  | SND | 0.36 | -242 | Max  | 17 | SLU | 0.68 | -242 | Min. | 9  | SND | 0.36 | -241 | Max  | 17 | SLU | 0.68 | -241 | Min. | 9  | SND | 0.36 |
| -240 | Max  | 17 | SLU | 0.68 | -240 | Min. | 9  | SND | 0.36 | -239 | Max  | 17 | SLU | 0.69 | -239 | Min. | 9  | SND | 0.36 | -238 | Max  | 17 | SLU | 0.69 |
| -238 | Min. | 9  | SND | 0.36 | -237 | Max  | 17 | SLU | 0.69 | -237 | Min. | 9  | SND | 0.36 | -236 | Max  | 17 | SLU | 0.69 | -236 | Min. | 9  | SND | 0.36 |
| -235 | Max  | 17 | SLU | 0.69 | -235 | Min. | 9  | SND | 0.36 | -234 | Max  | 17 | SLU | 0.70 | -234 | Min. | 9  | SND | 0.36 | -233 | Max  | 17 | SLU | 0.70 |
| -233 | Min. | 9  | SND | 0.36 | -232 | Max  | 17 | SLU | 0.70 | -232 | Min. | 9  | SND | 0.37 | -231 | Max  | 17 | SLU | 0.70 | -231 | Min. | 9  | SND | 0.37 |
| -230 | Max  | 17 | SLU | 0.71 | -230 | Min. | 9  | SND | 0.37 | -229 | Max  | 17 | SLU | 0.71 | -229 | Min. | 9  | SND | 0.37 | -228 | Max  | 17 | SLU | 0.71 |
| -228 | Min. | 9  | SND | 0.37 | -227 | Max  | 17 | SLU | 0.72 | -227 | Min. | 9  | SND | 0.37 | -226 | Max  | 17 | SLU | 0.72 | -226 | Min. | 9  | SND | 0.37 |
| -225 | Max  | 17 | SLU | 0.73 | -225 | Min. | 9  | SND | 0.37 | -224 | Max  | 17 | SLU | 0.73 | -224 | Min. | 9  | SND | 0.37 | -223 | Max  | 17 | SLU | 0.73 |
| -223 | Min. | 9  | SND | 0.37 | -222 | Max  | 17 | SLU | 0.74 | -222 | Min. | 9  | SND | 0.37 | -221 | Max  | 17 | SLU | 0.74 | -221 | Min. | 9  | SND | 0.37 |
| -220 | Max  | 13 | SND | 0.68 | -220 | Min. | 11 | SND | 0.22 | -219 | Max  | 13 | SND | 0.68 | -219 | Min. | 11 | SND | 0.22 | -218 | Max  | 13 | SND | 0.67 |
| -218 | Min. | 11 | SND | 0.22 | -217 | Max  | 13 | SND | 0.67 | -217 | Min. | 11 | SND | 0.23 | -216 | Max  | 13 | SND | 0.67 | -216 | Min. | 11 | SND | 0.23 |
| -215 | Max  | 13 | SND | 0.67 | -215 | Min. | 11 | SND | 0.23 | -214 | Max  | 13 | SND | 0.67 | -214 | Min. | 11 | SND | 0.23 | -213 | Max  | 13 | SND | 0.67 |
| -213 | Min. | 11 | SND | 0.24 | -212 | Max  | 13 | SND | 0.66 | -212 | Min. | 11 | SND | 0.24 | -211 | Max  | 13 | SND | 0.66 | -211 | Min. | 11 | SND | 0.24 |
| -210 | Max  | 13 | SND | 0.66 | -210 | Min. | 11 | SND | 0.24 | -209 | Max  | 13 | SND | 0.66 | -209 | Min. | 11 | SND | 0.25 | -208 | Max  | 13 | SND | 0.66 |
| -208 | Min. | 11 | SND | 0.25 | -207 | Max  | 13 | SND | 0.66 | -207 | Min. | 11 | SND | 0.25 | -206 | Max  | 13 | SND | 0.66 | -206 | Min. | 11 | SND | 0.26 |
| -205 | Max  | 13 | SND | 0.66 | -205 | Min. | 11 | SND | 0.26 | -204 | Max  | 13 | SND | 0.66 | -204 | Min. | 11 | SND | 0.26 | -203 | Max  | 13 | SND | 0.66 |
| -203 | Min. | 11 | SND | 0.27 | -202 | Max  | 13 | SND | 0.66 | -202 | Min. | 11 | SND | 0.27 | -201 | Max  | 13 | SND | 0.66 | -201 | Min. | 11 | SND | 0.27 |
| -200 | Max  | 13 | SND | 0.66 | -200 | Min. | 11 | SND | 0.27 | -199 | Max  | 13 | SND | 0.66 | -199 | Min. | 11 | SND | 0.28 | -198 | Max  | 13 | SND | 0.67 |
| -198 | Min. | 11 | SND | 0.28 | -197 | Max  | 13 | SND | 0.66 | -197 | Min. | 11 | SND | 0.28 | -196 | Max  | 17 | SLU | 0.66 | -196 | Min. | 11 | SND | 0.28 |
| -195 | Max  | 17 | SLU | 0.67 | -195 | Min. | 11 | SND | 0.29 | -194 | Max  | 17 | SLU | 0.67 | -194 | Min. | 11 | SND | 0.29 | -193 | Max  | 17 | SLU | 0.67 |
| -193 | Min. | 9  | SND | 0.29 | -192 | Max  | 17 | SLU | 0.67 | -192 | Min. | 9  | SND | 0.29 | -191 | Max  | 17 | SLU | 0.67 | -191 | Min. | 9  | SND | 0.29 |
| -190 | Max  | 17 | SLU | 0.68 | -190 | Min. | 9  | SND | 0.29 | -189 | Max  | 17 | SLU | 0.68 | -189 | Min. | 9  | SND | 0.29 | -188 | Max  | 17 | SLU | 0.68 |
| -188 | Min. | 9  | SND | 0.29 | -187 | Max  | 17 | SLU | 0.68 | -187 | Min. | 9  | SND | 0.29 | -186 | Max  | 17 | SLU | 0.69 | -186 | Min. | 9  | SND | 0.29 |
| -185 | Max  | 17 | SLU | 0.69 | -185 | Min. | 9  | SND | 0.29 | -184 | Max  | 17 | SLU | 0.69 | -184 | Min. | 9  | SND | 0.29 | -183 | Max  | 17 | SLU | 0.69 |
| -183 | Min. | 9  | SND | 0.29 | -182 | Max  | 17 | SLU | 0.69 | -182 | Min. |    |     |      |      |      |    |     |      |      |      |    |     |      |



|     |      |    |     |       |     |      |    |     |       |     |      |    |     |       |     |      |    |     |       |     |      |    |     |       |
|-----|------|----|-----|-------|-----|------|----|-----|-------|-----|------|----|-----|-------|-----|------|----|-----|-------|-----|------|----|-----|-------|
| -93 | Min. | 11 | SND | 0.12  | -92 | Max  | 13 | SND | 0.82  | -92 | Min. | 11 | SND | 0.13  | -91 | Max  | 13 | SND | 0.82  | -91 | Min. | 11 | SND | 0.13  |
| -90 | Max  | 13 | SND | 0.82  | -90 | Min. | 11 | SND | 0.13  | -89 | Max  | 13 | SND | 0.82  | -89 | Min. | 11 | SND | 0.13  | -89 | Max  | 13 | SND | 0.82  |
| -88 | Min. | 11 | SND | 0.14  | -87 | Max  | 13 | SND | 0.82  | -87 | Min. | 11 | SND | 0.14  | -86 | Max  | 13 | SND | 0.82  | -86 | Min. | 11 | SND | 0.14  |
| -85 | Max  | 13 | SND | 0.82  | -85 | Min. | 11 | SND | 0.15  | -84 | Max  | 13 | SND | 0.82  | -84 | Min. | 11 | SND | 0.15  | -84 | Max  | 15 | SND | 0.82  |
| -83 | Min. | 9  | SND | 0.15  | -82 | Max  | 15 | SND | 0.82  | -82 | Min. | 9  | SND | 0.15  | -81 | Max  | 15 | SND | 0.82  | -81 | Min. | 9  | SND | 0.15  |
| -80 | Max  | 15 | SND | 0.83  | -80 | Min. | 9  | SND | 0.15  | -79 | Max  | 15 | SND | 0.83  | -79 | Min. | 9  | SND | 0.15  | -79 | Max  | 15 | SND | 0.83  |
| -78 | Min. | 9  | SND | 0.15  | -77 | Max  | 15 | SND | 0.84  | -77 | Min. | 9  | SND | 0.15  | -76 | Max  | 15 | SND | 0.84  | -76 | Max  | 15 | SND | 0.15  |
| -75 | Max  | 15 | SND | 0.84  | -75 | Min. | 9  | SND | 0.15  | -74 | Max  | 15 | SND | 0.84  | -74 | Min. | 9  | SND | 0.15  | -74 | Max  | 15 | SND | 0.85  |
| -73 | Min. | 9  | SND | 0.15  | -72 | Max  | 15 | SND | 0.85  | -72 | Min. | 9  | SND | 0.15  | -71 | Max  | 15 | SND | 0.85  | -71 | Min. | 9  | SND | 0.15  |
| -70 | Max  | 15 | SND | 0.86  | -70 | Min. | 9  | SND | 0.15  | -69 | Max  | 15 | SND | 0.86  | -69 | Min. | 9  | SND | 0.15  | -69 | Max  | 15 | SND | 0.86  |
| -68 | Min. | 9  | SND | 0.15  | -67 | Max  | 15 | SND | 0.87  | -67 | Min. | 9  | SND | 0.15  | -66 | Max  | 15 | SND | 0.87  | -66 | Min. | 9  | SND | 0.15  |
| -65 | Max  | 15 | SND | 0.88  | -65 | Min. | 9  | SND | 0.15  | -64 | Max  | 15 | SND | 0.88  | -64 | Min. | 9  | SND | 0.15  | -64 | Max  | 15 | SND | 0.88  |
| -63 | Min. | 9  | SND | 0.15  | -62 | Max  | 15 | SND | 0.89  | -62 | Min. | 9  | SND | 0.15  | -61 | Max  | 15 | SND | 0.89  | -61 | Min. | 9  | SND | 0.14  |
| -60 | Max  | 15 | SND | 0.90  | -60 | Min. | 9  | SND | 0.14  | -59 | Max  | 15 | SND | 0.90  | -59 | Min. | 9  | SND | 0.14  | -59 | Max  | 15 | SND | 0.90  |
| -58 | Min. | 9  | SND | 0.14  | -57 | Max  | 15 | SND | 0.91  | -57 | Min. | 9  | SND | 0.14  | -56 | Max  | 15 | SND | 0.91  | -56 | Min. | 9  | SND | 0.14  |
| -55 | Max  | 13 | SND | 0.91  | -55 | Min. | 11 | SND | -0.02 | -54 | Max  | 13 | SND | 0.91  | -54 | Min. | 11 | SND | -0.01 | -54 | Max  | 13 | SND | 0.91  |
| -53 | Min. | 11 | SND | -0.01 | -52 | Max  | 13 | SND | 0.91  | -52 | Min. | 11 | SND | -0.00 | -51 | Max  | 13 | SND | 0.91  | -51 | Min. | 11 | SND | -0.00 |
| -50 | Max  | 13 | SND | 0.90  | -50 | Min. | 11 | SND | 0.00  | -49 | Max  | 13 | SND | 0.90  | -49 | Min. | 11 | SND | 0.01  | -49 | Max  | 13 | SND | 0.90  |
| -48 | Min. | 11 | SND | 0.01  | -47 | Max  | 13 | SND | 0.90  | -47 | Min. | 11 | SND | 0.02  | -46 | Max  | 13 | SND | 0.90  | -46 | Min. | 11 | SND | 0.02  |
| -45 | Max  | 13 | SND | 0.90  | -45 | Min. | 11 | SND | 0.02  | -44 | Max  | 13 | SND | 0.90  | -44 | Min. | 11 | SND | 0.03  | -44 | Max  | 13 | SND | 0.90  |
| -43 | Min. | 11 | SND | 0.03  | -42 | Max  | 13 | SND | 0.90  | -42 | Min. | 11 | SND | 0.04  | -41 | Max  | 13 | SND | 0.90  | -41 | Min. | 11 | SND | 0.04  |
| -40 | Max  | 13 | SND | 0.90  | -40 | Min. | 11 | SND | 0.04  | -39 | Max  | 13 | SND | 0.90  | -39 | Min. | 11 | SND | 0.05  | -39 | Max  | 13 | SND | 0.90  |
| -38 | Min. | 11 | SND | 0.05  | -37 | Max  | 13 | SND | 0.90  | -37 | Min. | 11 | SND | 0.05  | -36 | Max  | 13 | SND | 0.90  | -36 | Min. | 11 | SND | 0.06  |
| -35 | Max  | 13 | SND | 0.90  | -35 | Min. | 11 | SND | 0.06  | -34 | Max  | 13 | SND | 0.90  | -34 | Min. | 11 | SND | 0.06  | -34 | Max  | 13 | SND | 0.90  |
| -33 | Min. | 11 | SND | 0.07  | -32 | Max  | 13 | SND | 0.90  | -32 | Min. | 11 | SND | 0.07  | -31 | Max  | 13 | SND | 0.90  | -31 | Min. | 11 | SND | 0.07  |
| -30 | Max  | 13 | SND | 0.90  | -30 | Min. | 11 | SND | 0.07  | -29 | Max  | 13 | SND | 0.90  | -29 | Min. | 11 | SND | 0.08  | -29 | Max  | 15 | SND | 0.90  |
| -28 | Min. | 9  | SND | 0.08  | -27 | Max  | 15 | SND | 0.90  | -27 | Min. | 9  | SND | 0.08  | -26 | Max  | 15 | SND | 0.90  | -26 | Min. | 9  | SND | 0.08  |
| -25 | Max  | 15 | SND | 0.91  | -25 | Min. | 9  | SND | 0.08  | -24 | Max  | 15 | SND | 0.91  | -24 | Min. | 9  | SND | 0.08  | -24 | Max  | 15 | SND | 0.91  |
| -23 | Min. | 9  | SND | 0.08  | -22 | Max  | 15 | SND | 0.91  | -22 | Min. | 9  | SND | 0.08  | -21 | Max  | 15 | SND | 0.92  | -21 | Min. | 9  | SND | 0.08  |
| -20 | Max  | 15 | SND | 0.92  | -20 | Min. | 9  | SND | 0.08  | -19 | Max  | 15 | SND | 0.92  | -19 | Min. | 9  | SND | 0.08  | -19 | Max  | 15 | SND | 0.93  |
| -18 | Min. | 9  | SND | 0.08  | -17 | Max  | 15 | SND | 0.93  | -17 | Min. | 9  | SND | 0.08  | -16 | Max  | 15 | SND | 0.93  | -16 | Min. | 9  | SND | 0.08  |
| -15 | Max  | 15 | SND | 0.94  | -15 | Min. | 9  | SND | 0.08  | -14 | Max  | 15 | SND | 0.94  | -14 | Min. | 9  | SND | 0.08  | -14 | Max  | 15 | SND | 0.94  |
| -13 | Min. | 9  | SND | 0.08  | -12 | Max  | 15 | SND | 0.95  | -12 | Min. | 9  | SND | 0.08  | -11 | Max  | 15 | SND | 0.95  | -11 | Min. | 9  | SND | 0.08  |
| -10 | Max  | 15 | SND | 0.96  | -10 | Min. | 9  | SND | 0.07  | -9  | Max  | 15 | SND | 0.96  | -9  | Min. | 9  | SND | 0.07  | -9  | Max  | 15 | SND | 0.96  |
| -8  | Min. | 9  | SND | 0.07  | -7  | Max  | 15 | SND | 0.97  | -7  | Min. | 9  | SND | 0.07  | -6  | Max  | 15 | SND | 0.97  | -6  | Min. | 9  | SND | 0.07  |
| -5  | Max  | 15 | SND | 0.97  | -5  | Min. | 9  | SND | 0.07  | -4  | Max  | 15 | SND | 0.98  | -4  | Min. | 9  | SND | 0.07  | -4  | Max  | 15 | SND | 0.98  |
| -3  | Min. | 9  | SND | 0.06  | -2  | Max  | 15 | SND | 0.99  | -2  | Min. | 9  | SND | 0.06  | -1  | Max  | 15 | SND | 0.99  | -1  | Min. | 9  | SND | 0.06  |

Sollecitazioni elementi bidimensionali

Simbologia

- $\sigma_{xx}$  = Tensione normale sulle facce perp. all'asse X
- $\sigma_{zz}$  = Tensione normale sulle facce perp. all'asse Z
- $\tau_{xy}$  = Tensione in dir. Y sulle facce perp. all'asse X
- $\tau_{xz}$  = Tensione in dir. Z sulle facce perp. all'asse X
- $\tau_{zy}$  = Tensione in dir. Y sulle facce perp. all'asse Z
- Bid. = Numero del muro/elemento bidimensionale
- CC = Numero della combinazione delle condizioni di carico elementari
- Mxx = Momento che provoca variazione di tensione sulle facce perp. all'asse X
- Mxz = Momento che provoca variazione di tensione tangenziali sulle facce perp. all'asse X
- Mzz = Momento che provoca variazione di tensione sulle facce perp. all'asse Z
- Nodo = Numero del nodo
- TCC = Tipo di combinazione di carico
- SLU = Stato limite ultimo
- SLE R = Stato limite d'esercizio, combinazione rara
- SLE F = Stato limite d'esercizio, combinazione frequente
- SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- SLD = Stato limite di danno
- SND = Stato limite di salvaguardia della vita (non dissipativo)

Bid. 7

|                        | CC | TCC | Nodo | Min.   | CC | TCC | Nodo | Max   |                        | CC | TCC | Nodo | Min.   | CC | TCC | Nodo | Max   |
|------------------------|----|-----|------|--------|----|-----|------|-------|------------------------|----|-----|------|--------|----|-----|------|-------|
| $\sigma_{xx}$ <daN/mq> | 1  | SND | -155 | 0      | 1  | SND | -185 | 0     | $\sigma_{zz}$ <daN/mq> | 1  | SND | -563 | 0      | 1  | SND | -621 | 0     |
| $\tau_{xz}$ <daN/mq>   | 1  | SND | -446 | 0      | 1  | SND | -184 | 0     | Mxx <daNm/m>           | 17 | SLU | -337 | -2165  | 17 | SLU | -278 | 2894  |
| Mzz <daNm/m>           | 17 | SLU | -348 | -9189  | 15 | SND | -576 | 7225  | Mxz <daNm/m>           | 15 | SND | -498 | -3147  | 11 | SND | -168 | 3112  |
| $\tau_{zy}$ <daN/mq>   | 17 | SLU | -124 | -20832 | 17 | SLU | -618 | 21881 | $\tau_{xy}$ <daN/mq>   | 17 | SLU | -332 | -18279 | 17 | SLU | -384 | 14915 |

Bid. 8

|                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |
|------------------------|----|-----|-------|--------|----|-----|-------|-------|------------------------|----|-----|-------|--------|----|-----|-------|-------|
| $\sigma_{xx}$ <daN/mq> | 13 | SND | -1882 | -76385 | 11 | SND | -1880 | 72869 | $\sigma_{zz}$ <daN/mq> | 17 | SLU | -794  | -49699 | 13 | SND | -788  | 24790 |
| $\tau_{xz}$ <daN/mq>   | 9  | SND | -789  | -28124 | 11 | SND | -838  | 28759 | Mxx <daNm/m>           | 15 | SND | -812  | -740   | 11 | SND | -635  | 394   |
| Mzz <daNm/m>           | 15 | SND | -811  | -7419  | 11 | SND | -814  | 3968  | Mxz <daNm/m>           | 9  | SND | -1161 | -509   | 15 | SND | -1869 | 572   |
| $\tau_{zy}$ <daN/mq>   | 11 | SND | -1310 | -19325 | 15 | SND | -811  | 21670 | $\tau_{xy}$ <daN/mq>   | 15 | SND | -1287 | -4651  | 15 | SND | -912  | 4967  |

Bid. 9

|                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo | Max   |                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |
|------------------------|----|-----|-------|--------|----|-----|------|-------|------------------------|----|-----|-------|--------|----|-----|-------|-------|
| $\sigma_{xx}$ <daN/mq> | 3  | SND | -1547 | -7891  | 15 | SND | -787 | 8627  | $\sigma_{zz}$ <daN/mq> | 17 | SLU | -777  | -50442 | 15 | SND | -787  | 32183 |
| $\tau_{xz}$ <daN/mq>   | 11 | SND | -1145 | -35517 | 15 | SND | -903 | 35479 | Mxx <daNm/m>           | 17 | SLU | -1600 | -272   | 11 | SND | -1281 | 339   |
| Mzz <daNm/m>           | 17 | SLU | -775  | -2005  | 17 | SLU | -895 | 195   | Mxz <daNm/m>           | 11 | SND | -167  | -438   | 15 | SND | -1267 | 445   |
| $\tau_{zy}$ <daN/mq>   | 17 | SLU | -1600 | -9634  | 17 | SLU | -777 | 14610 | $\tau_{xy}$ <daN/mq>   | 17 | SLU | -1279 | -2873  | 17 | SLU | -1269 | 2730  |

Bid. 10

|                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |
|------------------------|----|-----|-------|--------|----|-----|-------|-------|------------------------|----|-----|-------|--------|----|-----|-------|-------|
| $\sigma_{xx}$ <daN/mq> | 5  | SND | -1272 | -11371 | 13 | SND | -659  | 7033  | $\sigma_{zz}$ <daN/mq> | 17 | SLU | -329  | -40885 | 13 | SND | -786  | 29249 |
| $\tau_{xz}$ <daN/mq>   | 13 | SND | -1150 | -31842 | 9  | SND | -1146 | 31791 | Mxx <daNm/m>           | 17 | SLU | -776  | -214   | 13 | SND | -963  | 162   |
| Mzz <daNm/m>           | 17 | SLU | -776  | -1895  | 17 | SLU | -1024 | 352   | Mxz <daNm/m>           | 15 | SND | -1156 | -359   | 9  | SND | -274  | 358   |
| $\tau_{zy}$ <daN/mq>   | 17 | SLU | -1274 | -7762  | 17 | SLU | -778  | 14915 | $\tau_{xy}$ <daN/mq>   | 17 | SLU | -1211 | -4095  | 17 | SLU | -1016 | 3474  |

Bid. 11

|                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |
|------------------------|----|-----|-------|--------|----|-----|-------|-------|------------------------|----|-----|-------|--------|----|-----|-------|-------|
| $\sigma_{xx}$ <daN/mq> | 9  | SND | -1353 | -76468 | 15 | SND | -1352 | 72700 | $\sigma_{zz}$ <daN/mq> | 17 | SLU | -723  | -49644 | 9  | SND | -57   | 23412 |
| $\tau_{xz}$ <daN/mq>   | 15 | SND | -766  | -29192 | 13 | SND | -59   | 28047 | Mxx <daNm/m>           | 11 | SND | -741  | -741   | 15 | SND | -85   | 394   |
| Mzz <daNm/m>           | 11 | SND | -81   | -7426  | 15 | SND | -84   | 3970  | Mxz <daNm/m>           | 11 | SND | -1216 | -572   | 13 | SND | -966  | 506   |
| $\tau_{zy}$ <daN/mq>   | 15 | SND | -1239 | -19312 | 11 | SND | -80   | 21684 | $\tau_{xy}$ <daN/mq>   | 11 | SND | -716  | -5059  | 11 | SND | -1337 | 4852  |





Bid. 12

|                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |                        | CC | TCC | Nodo  | Min.   | CC | TCC | Nodo  | Max   |
|------------------------|----|-----|-------|--------|----|-----|-------|-------|------------------------|----|-----|-------|--------|----|-----|-------|-------|
| $\sigma_{xx}$ <daN/mq> | 13 | SND | -1878 | -77457 | 11 | SND | -1827 | 77743 | $\sigma_{zz}$ <daN/mq> | 13 | SND | -1536 | -19239 | 13 | SND | -1588 | 7214  |
| $t_{xz}$ <daN/mq>      | 15 | SND | -1653 | -28623 | 9  | SND | -1547 | 28695 | $M_{xx}$ <daNm/m>      | 17 | SLU | -1601 | -1838  | 17 | SLU | -1606 | 1671  |
| $M_{zz}$ <daNm/m>      | 11 | SND | -1840 | -6294  | 17 | SLU | -1613 | 4262  | $M_{xz}$ <daNm/m>      | 17 | SLU | -1444 | -1281  | 17 | SLU | -1763 | 1262  |
| $t_{xy}$ <daN/mq>      | 17 | SLU | -1876 | -27754 | 17 | SLU | -1348 | 25870 | $t_{xy}$ <daN/mq>      | 17 | SLU | -1869 | -13059 | 17 | SLU | -1548 | 12839 |

Verifiche e armature solette/platee

Simbologia

- $\Delta_{sm}$  = Distanza media tra le fessure
- $\Phi_{eq}$  = Diametro equivalente delle barre
- $\epsilon_{sm}$  = Deformazione unitaria media dell'armatura (\*1000)
- $\sigma_c$  = Tensione nel calcestruzzo
- $\sigma_f$  = Tensione nel ferro
- $\sigma_s$  = Tensione nell'acciaio nella sezione fessurata
- $A_{c\ eff}$  = Area di calcestruzzo efficace
- $A_s$  = Area complessiva dei ferri nell'area di calcestruzzo efficace
- AFe I = Area di ferro effettiva totale presente nel punto di verifica, inferiore
- AFe S = Area di ferro effettiva totale presente nel punto di verifica, superiore
- AFe St. = Area di ferro effettiva della staffatura
- CC = Numero della combinazione delle condizioni di carico elementari
- Cf inf = Copriferro inferiore
- Cf sup = Copriferro superiore
- Cls = Tipo di calcestruzzo
- DV = Direzione di verifica  
XX = Verifica per momento Mxx  
YY = Verifica per momento Myy
- Fcd = Resistenza di calcolo a compressione del calcestruzzo
- Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo
- Fctd = Resistenza di calcolo a trazione del calcestruzzo
- Fctk = Resistenza caratteristica a trazione del calcestruzzo
- Fyd = Resistenza di calcolo dell'acciaio
- Fyk = Tensione caratteristica di snervamento dell'acciaio
- K<sub>2</sub> = Coefficiente per distribuzione deformazioni
- M' ydy = Momento resistente massimo in campo sostanzialmente elastico intorno all'asse Y
- MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y
- Mom = Momento flettente
- My = Momento flettente intorno all'asse Y
- Nodo = Numero del nodo
- Sic. = Sicurezza
- Spess. = Spessore
- TCC = Tipo di combinazione di carico  
SLU = Stato limite ultimo  
SLE R = Stato limite d'esercizio, combinazione rara  
SLE F = Stato limite d'esercizio, combinazione frequente  
SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
SLD = Stato limite di danno  
SND = Stato limite di salvaguardia della vita (non dissipativo)
- Tp = Tipo di acciaio
- VRcd = Taglio ultimo lato calcestruzzo
- VRsd = Taglio ultimo lato armatura
- Vrdu = Taglio ultimo resistente
- Vsdu = Taglio agente nella direzione del momento ultimo
- Wk = Ampiezza caratteristica delle fessure
- X = Coordinata X del nodo
- Y = Coordinata Y del nodo
- c = Ricoprimento dell'armatura
- ctg $\theta$  = Cotangente dell'angolo di inclinazione dei puntoni di calcestruzzo
- s = Distanza massima tra le barre

Armatura platea a quota 0.00

Caratteristiche delle sezioni e dei materiali utilizzati

| Spess. | Cf sup | Cf inf | Cls    | Fck                 | Fctk                | Fcd                 | Fctd                | Tp    | Fyk                 | Fyd                 |
|--------|--------|--------|--------|---------------------|---------------------|---------------------|---------------------|-------|---------------------|---------------------|
| <cm>   | <cm>   | <cm>   |        | <daN/cm<sup>2</sup> | <daN/cm<sup>2</sup> | <daN/cm<sup>2</sup> | <daN/cm<sup>2</sup> |       | <daN/cm<sup>2</sup> | <daN/cm<sup>2</sup> |
| 50.00  | 3.50   | 3.50   | C32/40 | 332.00              | 21.69               | 188.13              | 14.46               | B450C | 4500.00             | 3913.04             |

Stato limite ultimo - Verifiche a flessione/pressoflessione

| Nodo | X     | Y    | DV | CC | TCC | AFe S           | AFe I           | My       | MRdy      | Sic.  |
|------|-------|------|----|----|-----|-----------------|-----------------|----------|-----------|-------|
| <m>  | <m>   | <m>  |    |    |     | <cm<sup>2</sup> | <cm<sup>2</sup> | <daNm>   | <daNm>    |       |
| -337 | 1.32  | 3.50 | XX | 17 | SLU | 7.70            | 7.70            | -2101.51 | -13950.30 | 6.638 |
| -332 | -1.10 | 3.50 | XX | 17 | SLU | 7.70            | 7.70            | 1882.41  | 13950.30  | 7.411 |
| -348 | 6.64  | 3.50 | YY | 17 | SLU | 7.70            | 7.70            | -8942.78 | -13950.30 | 1.560 |
| -652 | 21.00 | 5.60 | YY | 17 | SLU | 7.70            | 7.70            | 1533.56  | 13950.30  | 9.097 |

Stato limite elastico - Verifiche a flessione/pressoflessione

| Nodo | X     | Y    | DV | CC | TCC | AFe S           | AFe I           | My       | M' ydy    | Sic.  |
|------|-------|------|----|----|-----|-----------------|-----------------|----------|-----------|-------|
| <m>  | <m>   | <m>  |    |    |     | <cm<sup>2</sup> | <cm<sup>2</sup> | <daNm>   | <daNm>    |       |
| -337 | 1.32  | 3.50 | XX | 5  | SND | 7.70            | 7.70            | -1889.61 | -13172.80 | 6.971 |
| -387 | -1.10 | 4.00 | XX | 11 | SND | 7.70            | 7.70            | 1452.92  | 13172.80  | 9.066 |
| -242 | 8.58  | 2.50 | YY | 15 | SND | 7.70            | 7.70            | -7958.61 | -13172.80 | 1.655 |
| -577 | 11.00 | 5.30 | YY | 15 | SND | 7.70            | 7.70            | 6057.26  | 13172.80  | 2.175 |

Stato limite ultimo - Verifiche a taglio

| Nodo | X     | Y    | DV | CC | TCC | AFe S           | AFe I           | AFe St.         | Vsdu               | ctg $\theta$ | VRcd  | VRsd  | Vrdu     | Sic.  |
|------|-------|------|----|----|-----|-----------------|-----------------|-----------------|--------------------|--------------|-------|-------|----------|-------|
| <m>  | <m>   | <m>  |    |    |     | <cm<sup>2</sup> | <cm<sup>2</sup> | <cm<sup>2</sup> | <cm<sup>2</sup>/m> |              | <daN> | <daN> | <daN>    |       |
| -333 | -0.62 | 3.50 | XX | 17 | SLU | 7.70            | 7.70            |                 | 7626.47            |              |       |       | 19980.80 | 2.620 |
| -333 | -0.62 | 3.50 | XX | 5  | SND | 7.70            | 7.70            |                 | 6298.90            |              |       |       | 19980.80 | 3.172 |
| -563 | 4.22  | 5.30 | YY | 17 | SLU | 7.70            | 7.70            |                 | 10156.70           |              |       |       | 19980.80 | 1.967 |
| -560 | 2.77  | 5.30 | YY | 5  | SND | 7.70            | 7.70            |                 | 8107.88            |              |       |       | 19980.80 | 2.464 |

Stato limite d'esercizio - Verifiche tensionali

| Nodo | X     | Y    | DV | CC | TCC | AFe S           | AFe I           | Mom    | $\sigma_c$          | $\sigma_f$          |         |
|------|-------|------|----|----|-----|-----------------|-----------------|--------|---------------------|---------------------|---------|
| <m>  | <m>   | <m>  |    |    |     | <cm<sup>2</sup> | <cm<sup>2</sup> | <daNm> | <daN/cm<sup>2</sup> | <daN/cm<sup>2</sup> |         |
| -337 | 1.32  | 3.50 | XX | 18 | SLE | R               | 7.70            | 7.70   | -1487.87            | 6.80                | 444.15  |
| -337 | 1.32  | 3.50 | XX | 20 | SLE | Q               | 7.70            | 7.70   | -1464.65            | 6.69                | 437.22  |
| -332 | -1.10 | 3.50 | XX | 18 | SLE | R               | 7.70            | 7.70   | 1311.17             | 5.99                | 391.40  |
| -332 | -1.10 | 3.50 | XX | 20 | SLE | Q               | 7.70            | 7.70   | 1298.21             | 5.93                | 387.53  |
| -348 | 6.64  | 3.50 | YY | 18 | SLE | R               | 7.70            | 7.70   | -6335.06            | 28.94               | 1891.10 |



|      |      |      |    |    |     |   |      |      |          |       |         |
|------|------|------|----|----|-----|---|------|------|----------|-------|---------|
| -348 | 6.64 | 3.50 | YY | 20 | SLE | Q | 7.70 | 7.70 | -6227.31 | 28.45 | 1858.93 |
| -613 | 1.80 | 5.60 | YY | 18 | SLE | R | 7.70 | 7.70 | 1056.70  | 4.83  | 315.44  |
| -613 | 1.80 | 5.60 | YY | 20 | SLE | Q | 7.70 | 7.70 | 1053.13  | 4.81  | 314.37  |

Stato limite d'esercizio - Verifiche a fessurazione

| Nodo | X     | Y    | DV   | CC   | TCC  | c    | s     | K <sub>2</sub> | Φ <sub>eq</sub> | Δ <sub>sm</sub> | A <sub>s</sub> | A <sub>c eff</sub> | σ <sub>s</sub> | ε <sub>sm</sub> | Wk   |      |
|------|-------|------|------|------|------|------|-------|----------------|-----------------|-----------------|----------------|--------------------|----------------|-----------------|------|------|
| <cm> | <cm>  | <cm> | <mm> | <mm> | <mm> | <mm> | <mm>  | <mm>           | <mm>            | <mm>            | <cmq>          | <cmq>              | <daN/cmq>      | <mm>            | <mm> |      |
| -337 | 1.32  | 3.50 | XX   | 20   | SLE  | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 437.22          | 0.13 | 0.07 |
| -337 | 1.32  | 3.50 | XX   | 19   | SLE  | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 440.68          | 0.13 | 0.07 |
| -332 | -1.10 | 3.50 | XX   | 20   | SLE  | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 387.53          | 0.11 | 0.06 |
| -332 | -1.10 | 3.50 | XX   | 19   | SLE  | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 389.47          | 0.11 | 0.06 |
| -348 | 6.64  | 3.50 | YY   | 20   | SLE  | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 1858.93         | 0.54 | 0.29 |
| -348 | 6.64  | 3.50 | YY   | 19   | SLE  | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 1875.01         | 0.55 | 0.29 |
| -613 | 1.80  | 5.60 | YY   | 20   | SLE  | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 314.37          | 0.09 | 0.05 |
| -613 | 1.80  | 5.60 | YY   | 19   | SLE  | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 314.90          | 0.09 | 0.05 |

Armatura soletta a quota 2.70

Caratteristiche delle sezioni e dei materiali utilizzati

| Spess. | Cf sup | Cf inf | Clis   | Fck       | Fctk      | Fcd       | Fctd      | TP    | Fyk       | Fyd       |
|--------|--------|--------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
| <cm>   | <cm>   | <cm>   |        | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| 30.00  | 3.00   | 3.00   | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Stato limite ultimo - Verifiche a flessione/pressoflessione

| Nodo  | X     | Y    | DV   | CC   | TCC  | A FE S | A FE I | My       | MRdy     | Sic.  |
|-------|-------|------|------|------|------|--------|--------|----------|----------|-------|
| <cm>  | <cm>  | <cm> | <mm> | <mm> | <mm> | <cmq>  | <cmq>  | <daNm>   | <daNm>   |       |
| -1606 | 1.80  | 3.50 | XX   | 17   | SLU  | 7.70   | 7.70   | 1593.60  | 7983.84  | 5.010 |
| -1600 | -1.10 | 3.50 | XX   | 17   | SLU  | 7.70   | 7.70   | -1791.82 | -7983.84 | 4.456 |
| -1612 | 4.71  | 3.50 | YY   | 17   | SLU  | 7.70   | 7.70   | 4090.74  | 7983.84  | 1.952 |
| -1877 | 4.71  | 5.60 | YY   | 17   | SLU  | 7.70   | 7.70   | -3261.62 | -7983.84 | 2.448 |

Stato limite elastico - Verifiche a flessione/pressoflessione

| Nodo  | X     | Y    | DV   | CC   | TCC  | A FE S | A FE I | My       | M'ydy    | Sic.  |
|-------|-------|------|------|------|------|--------|--------|----------|----------|-------|
| <cm>  | <cm>  | <cm> | <mm> | <mm> | <mm> | <cmq>  | <cmq>  | <daNm>   | <daNm>   |       |
| -1553 | 1.80  | 3.00 | XX   | 9    | SND  | 7.70   | 7.70   | 1103.75  | 7491.58  | 6.787 |
| -1547 | -1.10 | 3.00 | XX   | 9    | SND  | 7.70   | 7.70   | -1262.49 | -7491.58 | 5.934 |
| -1523 | 12.50 | 2.50 | YY   | 9    | SND  | 7.70   | 7.70   | 3628.49  | 7491.58  | 2.065 |
| -1893 | 12.50 | 5.60 | YY   | 11   | SND  | 7.70   | 7.70   | -6278.14 | -7491.58 | 1.193 |

Stato limite ultimo - Verifiche a taglio

| Nodo  | X     | Y    | DV   | CC   | TCC  | A FE S | A FE I | A FE St | Vsdu    | ctgθ | VRcd  | VRsd  | Vrdu     | Sic.  |
|-------|-------|------|------|------|------|--------|--------|---------|---------|------|-------|-------|----------|-------|
| <cm>  | <cm>  | <cm> | <mm> | <mm> | <mm> | <cmq>  | <cmq>  | <cmq/m> | <daN>   |      | <daN> | <daN> | <daN>    |       |
| -1601 | -0.62 | 3.50 | XX   | 17   | SLU  | 7.70   | 7.70   |         | 3221.68 |      |       |       | 13819.80 | 4.290 |
| -1548 | -0.62 | 3.00 | XX   | 9    | SND  | 7.70   | 7.70   |         | 2333.69 |      |       |       | 13819.80 | 5.922 |
| -1824 | 4.71  | 5.30 | YY   | 17   | SLU  | 7.70   | 7.70   |         | 7461.17 |      |       |       | 13819.80 | 1.852 |
| -1839 | 12.00 | 5.30 | YY   | 9    | SND  | 7.70   | 7.70   |         | 6965.19 |      |       |       | 13819.80 | 1.984 |

Stato limite d'esercizio - Verifiche tensionali

| Nodo  | X     | Y    | DV   | CC   | TCC  | A FE S | A FE I | Mom    | σ <sub>c</sub> | σ <sub>f</sub> |         |
|-------|-------|------|------|------|------|--------|--------|--------|----------------|----------------|---------|
| <cm>  | <cm>  | <cm> | <mm> | <mm> | <mm> | <cmq>  | <cmq>  | <daNm> | <daN/cmq>      | <daN/cmq>      |         |
| -1606 | 1.80  | 3.50 | XX   | 18   | SLE  | R      | 7.70   | 7.70   | 1095.23        | 11.73          | 575.00  |
| -1606 | 1.80  | 3.50 | XX   | 20   | SLE  | Q      | 7.70   | 7.70   | 1076.03        | 11.53          | 564.91  |
| -1600 | -1.10 | 3.50 | XX   | 18   | SLE  | R      | 7.70   | 7.70   | -1242.59       | 13.31          | 652.36  |
| -1600 | -1.10 | 3.50 | XX   | 20   | SLE  | Q      | 7.70   | 7.70   | -1211.54       | 12.98          | 636.05  |
| -1612 | 4.71  | 3.50 | YY   | 18   | SLE  | R      | 7.70   | 7.70   | 2864.36        | 30.69          | 1503.79 |
| -1612 | 4.71  | 3.50 | YY   | 20   | SLE  | Q      | 7.70   | 7.70   | 2786.78        | 29.86          | 1463.06 |
| -1877 | 4.71  | 5.60 | YY   | 18   | SLE  | R      | 7.70   | 7.70   | -2257.96       | 24.19          | 1185.43 |
| -1877 | 4.71  | 5.60 | YY   | 20   | SLE  | Q      | 7.70   | 7.70   | -2202.63       | 23.60          | 1156.38 |

Stato limite d'esercizio - Verifiche a fessurazione

| Nodo  | X     | Y    | DV   | CC   | TCC  | c    | s     | K <sub>2</sub> | Φ <sub>eq</sub> | Δ <sub>sm</sub> | A <sub>s</sub> | A <sub>c eff</sub> | σ <sub>s</sub> | ε <sub>sm</sub> | Wk   |      |
|-------|-------|------|------|------|------|------|-------|----------------|-----------------|-----------------|----------------|--------------------|----------------|-----------------|------|------|
| <cm>  | <cm>  | <cm> | <mm> | <mm> | <mm> | <mm> | <mm>  | <mm>           | <mm>            | <mm>            | <cmq>          | <cmq>              | <daN/cmq>      | <mm>            | <mm> |      |
| -1606 | 1.80  | 3.50 | XX   | 20   | SLE  | Q    | 23.00 | 200.00         | 0.50            | 14.00           | 177.54         | 9.24               | 750.00         | 564.91          | 0.16 | 0.05 |
| -1606 | 1.80  | 3.50 | XX   | 19   | SLE  | F    | 23.00 | 200.00         | 0.50            | 14.00           | 177.54         | 9.24               | 750.00         | 569.95          | 0.17 | 0.05 |
| -1600 | -1.10 | 3.50 | XX   | 20   | SLE  | Q    | 23.00 | 200.00         | 0.50            | 14.00           | 177.54         | 9.24               | 750.00         | 636.05          | 0.19 | 0.06 |
| -1600 | -1.10 | 3.50 | XX   | 19   | SLE  | F    | 23.00 | 200.00         | 0.50            | 14.00           | 177.54         | 9.24               | 750.00         | 644.21          | 0.19 | 0.06 |
| -1612 | 4.71  | 3.50 | YY   | 20   | SLE  | Q    | 23.00 | 200.00         | 0.50            | 14.00           | 177.54         | 9.24               | 750.00         | 1463.06         | 0.43 | 0.13 |
| -1612 | 4.71  | 3.50 | YY   | 19   | SLE  | F    | 23.00 | 200.00         | 0.50            | 14.00           | 177.54         | 9.24               | 750.00         | 1483.42         | 0.43 | 0.13 |
| -1877 | 4.71  | 5.60 | YY   | 20   | SLE  | Q    | 23.00 | 200.00         | 0.50            | 14.00           | 177.54         | 9.24               | 750.00         | 1156.38         | 0.34 | 0.10 |
| -1877 | 4.71  | 5.60 | YY   | 19   | SLE  | F    | 23.00 | 200.00         | 0.50            | 14.00           | 177.54         | 9.24               | 750.00         | 1170.90         | 0.34 | 0.10 |

Verifiche e armature pareti

Simbologia

- Δ<sub>sm</sub> = Distanza media tra le fessure
- Φ<sub>eq</sub> = Diametro equivalente delle barre
- ε<sub>sm</sub> = Deformazione unitaria media dell'armatura (\*1000)
- σ<sub>c</sub> = Tensione nel calcestruzzo
- σ<sub>f</sub> = Tensione nel ferro
- σ<sub>s</sub> = Tensione nell'acciaio nella sezione fessurata
- A<sub>c eff</sub> = Area di calcestruzzo efficace
- A<sub>s</sub> = Area complessiva dei ferri nell'area di calcestruzzo efficace
- CC = Numero della combinazione delle condizioni di carico elementari
- Cf = Copriferro
- Clis = Tipo di calcestruzzo
- Fcd = Resistenza di calcolo a compressione del calcestruzzo
- Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo
- Fctd = Resistenza di calcolo a trazione del calcestruzzo
- Fctk = Resistenza caratteristica a trazione del calcestruzzo
- Fyd = Resistenza di calcolo dell'acciaio
- Fyk = Tensione caratteristica di snervamento dell'acciaio
- K<sub>2</sub> = Coefficiente per distribuzione deformazioni
- M'ydy = Momento resistente massimo in campo sostanzialmente elastico intorno all'asse Y
- MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y
- My = Momento flettente intorno all'asse Y
- N = Sforzo normale
- Nu = Sforzo normale ultimo
- Sez. = Sezione di verifica
- Sic. = Sicurezza
- Spess. = Spessore

TCC =Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
 SLD = Stato limite di danno  
 SND = Stato limite di salvaguardia della vita (non dissipativo)

TP =Tipo di acciaio  
 Ty =Taglio in dir. Y  
 VRcd =Taglio ultimo lato calcestruzzo  
 VRsd =Taglio ultimo lato armatura  
 Vrdu =Taglio ultimo resistente  
 Vsdu =Taglio agente nella direzione del momento ultimo  
 Wk =Ampiezza caratteristica delle fessure  
 Xf =Coordinata X finale  
 Xi =Coordinata X iniziale  
 Xv =Coordinata X di verifica  
 Zona =Zona di verifica  
 Zv =Coordinata Z di verifica  
 c =Ricoprimento dell'armatura  
 s =Distanza massima tra le barre

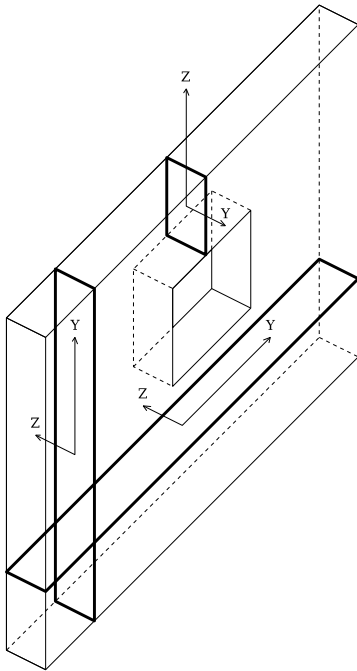


Figura numero 3: Riferimenti sezione

Parete n. 8

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess.<br><cm> | Cf<br><cm> | ClS    | Fck<br><daN/cm²> | Fctk<br><daN/cm²> | Fcd<br><daN/cm²> | Fctd<br><daN/cm²> | TP    | Fyk<br><daN/cm²> | Fyd<br><daN/cm²> |
|-------|----------------|------------|--------|------------------|-------------------|------------------|-------------------|-------|------------------|------------------|
| Oriz. | 30.00          | 4.30       | C32/40 | 332.00           | 21.69             | 188.13           | 14.46             | B450C | 4500.00          | 3913.04          |

Verifiche su sezioni orizzontali

Stato limite ultimo - Verifiche a flessione/presoflessione

| CC | TCC | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | Nu<br><daN> | MRdy<br><daNm> | Sic.  |
|----|-----|-------|-----------|-----------|-----------|------------|--------------|-------------|----------------|-------|
| 17 | SLU | Diff. | 0.00      | 0.00      | 25.60     | -325456.00 | 71673.60     | -325456.00  | 236748.00      | 3.303 |
| 17 | SLU | Diff. | 1.35      | 0.00      | 25.60     | -288067.00 | 23531.90     | -288067.00  | 232517.00      | 9.881 |
| 17 | SLU | Diff. | 2.70      | 0.00      | 25.60     | -257524.00 | 79902.60     | -257524.00  | 229058.00      | 2.867 |

Stato limite elastico - Verifiche a flessione/presoflessione

| CC | TCC | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | Nu<br><daN> | M'ydy<br><daNm> | Sic.   |
|----|-----|-------|-----------|-----------|-----------|------------|--------------|-------------|-----------------|--------|
| 13 | SND | Diff. | 0.00      | 0.00      | 25.60     | -161651.00 | 158567.00    | -161651.00  | 198166.00       | 1.250  |
| 13 | SND | Diff. | 1.35      | 0.00      | 25.60     | -150960.00 | 18804.70     | -150960.00  | 196928.00       | 10.472 |
| 11 | SND | Diff. | 2.70      | 0.00      | 25.60     | -210532.00 | 130104.00    | -210532.00  | 203824.00       | 1.567  |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC | Zona | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | σc<br><daN/cm²> | σt<br><daN/cm²> |        |
|----|-----|------|-----------|-----------|-----------|------------|--------------|-----------------|-----------------|--------|
| 18 | SLE | R    | Diff.     | 0.00      | 0.00      | 25.60      | -229308.00   | 49289.50        | 22.77           | 528.44 |
| 20 | SLE | Q    | Diff.     | 0.00      | 0.00      | 25.60      | -226206.00   | 49228.40        | 22.76           | 533.89 |
| 18 | SLE | R    | Diff.     | 1.35      | 0.00      | 25.60      | -200483.00   | 17649.20        | 7.15            | 84.91  |
| 20 | SLE | Q    | Diff.     | 1.35      | 0.00      | 25.60      | -197325.00   | 16759.10        | 6.79            | 81.36  |
| 18 | SLE | R    | Diff.     | 2.70      | 0.00      | 25.60      | -176993.00   | 55876.90        | 26.45           | 787.23 |
| 20 | SLE | Q    | Diff.     | 2.70      | 0.00      | 25.60      | -173817.00   | 54200.50        | 25.64           | 758.57 |

Stato limite d'esercizio - Verifiche a fessurazione

| CC | TCC | Zona | Zv | Xi | Xf | N | My | c | s | K2 | Φsq | Δsm | A_s | A_c eff | σ_s | ε_sm | Wk |
|----|-----|------|----|----|----|---|----|---|---|----|-----|-----|-----|---------|-----|------|----|
|----|-----|------|----|----|----|---|----|---|---|----|-----|-----|-----|---------|-----|------|----|



|    |       | <m>   | <m>  | <m>  | <daN> | <daNm>     | <mm>     | <mm>  |        | <mm> | <cmq> | <cmq>  | <daN/cmq> | <mm>     |        |      |      |
|----|-------|-------|------|------|-------|------------|----------|-------|--------|------|-------|--------|-----------|----------|--------|------|------|
| 20 | SLE Q | Diff. | 0.00 | 0.00 | 25.60 | -226206.00 | 49228.40 | 37.00 | 149.21 | 0.50 | 12.00 | 179.15 | 194.53    | 17045.00 | 533.89 | 0.16 | 0.05 |
| 19 | SLE F | Diff. | 0.00 | 0.00 | 25.60 | -227757.00 | 49258.90 | 37.00 | 149.21 | 0.50 | 12.00 | 178.98 | 194.53    | 17018.10 | 531.16 | 0.15 | 0.05 |
| 20 | SLE Q | Diff. | 2.70 | 0.00 | 25.60 | -173817.00 | 54200.50 | 37.00 | 149.21 | 0.50 | 12.00 | 186.41 | 194.53    | 18221.80 | 758.57 | 0.22 | 0.07 |
| 19 | SLE F | Diff. | 2.70 | 0.00 | 25.60 | -175405.00 | 55038.70 | 37.00 | 149.21 | 0.50 | 12.00 | 186.50 | 194.53    | 18237.00 | 772.90 | 0.23 | 0.07 |

Parete n. 9

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | TP    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
| <cm>  | <cm>   | <cm> | <cm>   | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| Oriz. | 30.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali

Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC/TCC | Zona | Zv    | Xi   | Xf   | N     | My        | Nu      | MRdy      | Sic.      |        |
|--------|------|-------|------|------|-------|-----------|---------|-----------|-----------|--------|
|        |      | <m>   | <m>  | <m>  | <daN> | <daNm>    | <daN>   | <daNm>    |           |        |
| 17     | SLU  | Diff. | 0.00 | 0.00 | 4.60  | -46579.50 | 9162.70 | -46579.50 | 35324.00  | 3.855  |
| 17     | SLU  | Diff. | 1.35 | 0.00 | 4.60  | -37816.30 | -599.02 | -37816.30 | -34326.60 | 57.304 |
| 17     | SLU  | Diff. | 2.70 | 0.00 | 4.60  | -32274.70 | 7444.86 | -32274.70 | 33694.90  | 4.526  |

Stato limite elastico - Verifiche a flessione/pressoflessione

| CC/TCC | Zona | Zv    | Xi   | Xf   | N     | My        | Nu      | M' ydy    | Sic.      |        |
|--------|------|-------|------|------|-------|-----------|---------|-----------|-----------|--------|
|        |      | <m>   | <m>  | <m>  | <daN> | <daNm>    | <daN>   | <daNm>    |           |        |
| 7      | SND  | Diff. | 0.00 | 0.00 | 4.60  | -38294.40 | 6427.91 | -38294.40 | 30853.80  | 4.800  |
| 3      | SND  | Diff. | 1.35 | 0.00 | 4.60  | -23044.30 | -627.32 | -23044.30 | -29050.90 | 46.310 |
| 7      | SND  | Diff. | 2.70 | 0.00 | 4.60  | -22389.40 | 5120.71 | -22389.40 | 28973.30  | 5.658  |

Stato limite d'esercizio - Verifiche tensionali

| CC/TCC | Zona  | Zv    | Xi   | Xf   | N     | My        | σc        | σt        |        |
|--------|-------|-------|------|------|-------|-----------|-----------|-----------|--------|
|        |       | <m>   | <m>  | <m>  | <daN> | <daNm>    | <daN/cmq> | <daN/cmq> |        |
| 18     | SLE R | Diff. | 0.00 | 0.00 | 4.60  | -32717.40 | 6310.32   | 17.24     | 401.95 |
| 20     | SLE Q | Diff. | 0.00 | 0.00 | 4.60  | -32306.60 | 6277.78   | 17.17     | 403.37 |
| 18     | SLE R | Diff. | 1.35 | 0.00 | 4.60  | -26243.20 | -330.93   | 2.23      | 31.56  |
| 20     | SLE Q | Diff. | 1.35 | 0.00 | 4.60  | -25890.90 | -364.35   | 2.25      | 31.68  |
| 18     | SLE R | Diff. | 2.70 | 0.00 | 4.60  | -22057.80 | 5205.75   | 14.61     | 405.47 |
| 20     | SLE Q | Diff. | 2.70 | 0.00 | 4.60  | -21721.70 | 5051.75   | 14.15     | 388.58 |

Stato limite d'esercizio - Verifiche a fessurazione

| CC/TCC | Zona  | Zv    | Xi   | Xf   | N     | My        | c       | s     | K2     | Φeq  | Δsm   | As     | Ao eff | σs        | εsm    | Wk   |      |
|--------|-------|-------|------|------|-------|-----------|---------|-------|--------|------|-------|--------|--------|-----------|--------|------|------|
|        |       | <m>   | <m>  | <m>  | <daN> | <daNm>    | <mm>    | <mm>  |        |      | <mm>  | <cmq>  | <cmq>  | <daN/cmq> |        | <mm> |      |
| 20     | SLE Q | Diff. | 0.00 | 0.00 | 4.60  | -32306.60 | 6277.78 | 37.00 | 188.08 | 0.50 | 12.00 | 204.05 | 28.27  | 3064.29   | 403.37 | 0.12 | 0.04 |
| 19     | SLE F | Diff. | 0.00 | 0.00 | 4.60  | -32512.00 | 6294.05 | 37.00 | 188.08 | 0.50 | 12.00 | 203.90 | 28.27  | 3060.77   | 402.65 | 0.12 | 0.04 |
| 20     | SLE Q | Diff. | 2.70 | 0.00 | 4.60  | -21721.70 | 5051.75 | 37.00 | 188.08 | 0.50 | 12.00 | 210.15 | 28.27  | 3207.87   | 388.58 | 0.11 | 0.04 |
| 19     | SLE F | Diff. | 2.70 | 0.00 | 4.60  | -21889.70 | 5128.75 | 37.00 | 188.08 | 0.50 | 12.00 | 210.36 | 28.27  | 3212.88   | 397.02 | 0.12 | 0.04 |

Parete n. 10

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | TP    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
| <cm>  | <cm>   | <cm> | <cm>   | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| Oriz. | 30.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali

Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC/TCC | Zona | Zv    | Xi   | Xf   | N     | My        | Nu       | MRdy      | Sic.      |        |
|--------|------|-------|------|------|-------|-----------|----------|-----------|-----------|--------|
|        |      | <m>   | <m>  | <m>  | <daN> | <daNm>    | <daN>    | <daNm>    |           |        |
| 17     | SLU  | Diff. | 0.00 | 0.00 | 4.60  | -38480.80 | 8627.24  | -38480.80 | 34402.70  | 3.988  |
| 17     | SLU  | Diff. | 1.35 | 0.00 | 4.60  | -33769.50 | -1125.23 | -33769.50 | -33865.60 | 30.097 |
| 17     | SLU  | Diff. | 2.70 | 0.00 | 4.60  | -29889.50 | 4960.43  | -29889.50 | 33423.10  | 6.738  |

Stato limite elastico - Verifiche a flessione/pressoflessione

| CC/TCC | Zona | Zv    | Xi   | Xf   | N     | My        | Nu      | M' ydy    | Sic.      |        |
|--------|------|-------|------|------|-------|-----------|---------|-----------|-----------|--------|
|        |      | <m>   | <m>  | <m>  | <daN> | <daNm>    | <daN>   | <daNm>    |           |        |
| 5      | SND  | Diff. | 0.00 | 0.00 | 4.60  | -20938.80 | 5788.16 | -20938.80 | 28802.00  | 4.976  |
| 7      | SND  | Diff. | 1.35 | 0.00 | 4.60  | -20387.20 | -982.27 | -20387.20 | -28736.00 | 29.255 |
| 1      | SND  | Diff. | 2.70 | 0.00 | 4.60  | -20787.10 | 3462.88 | -20787.10 | 28783.50  | 8.312  |

Stato limite d'esercizio - Verifiche tensionali

| CC/TCC | Zona  | Zv    | Xi   | Xf   | N     | My        | σc        | σt        |        |
|--------|-------|-------|------|------|-------|-----------|-----------|-----------|--------|
|        |       | <m>   | <m>  | <m>  | <daN> | <daNm>    | <daN/cmq> | <daN/cmq> |        |
| 18     | SLE R | Diff. | 0.00 | 0.00 | 4.60  | -27314.20 | 5948.86   | 16.54     | 431.06 |
| 20     | SLE Q | Diff. | 0.00 | 0.00 | 4.60  | -26910.30 | 5917.86   | 16.47     | 432.77 |
| 18     | SLE R | Diff. | 1.35 | 0.00 | 4.60  | -23543.80 | -682.52   | 2.51      | 33.79  |
| 20     | SLE Q | Diff. | 1.35 | 0.00 | 4.60  | -23194.30 | -715.60   | 2.53      | 33.90  |
| 18     | SLE R | Diff. | 2.70 | 0.00 | 4.60  | -20467.00 | 3548.61   | 9.51      | 197.12 |
| 20     | SLE Q | Diff. | 2.70 | 0.00 | 4.60  | -20131.80 | 3395.46   | 9.05      | 181.26 |

Stato limite d'esercizio - Verifiche a fessurazione

| CC/TCC | Zona  | Zv    | Xi   | Xf   | N     | My        | c       | s     | K2     | Φeq  | Δsm   | As     | Ao eff | σs        | εsm    | Wk   |      |
|--------|-------|-------|------|------|-------|-----------|---------|-------|--------|------|-------|--------|--------|-----------|--------|------|------|
|        |       | <m>   | <m>  | <m>  | <daN> | <daNm>    | <mm>    | <mm>  |        |      | <mm>  | <cmq>  | <cmq>  | <daN/cmq> |        | <mm> |      |
| 20     | SLE Q | Diff. | 0.00 | 0.00 | 4.60  | -26910.30 | 5917.86 | 37.00 | 188.08 | 0.50 | 12.00 | 208.45 | 28.27  | 3167.96   | 432.77 | 0.13 | 0.04 |
| 19     | SLE F | Diff. | 0.00 | 0.00 | 4.60  | -27112.30 | 5933.36 | 37.00 | 188.08 | 0.50 | 12.00 | 208.30 | 28.27  | 3164.30   | 431.91 | 0.13 | 0.04 |
| 20     | SLE Q | Diff. | 2.70 | 0.00 | 4.60  | -20131.80 | 3395.46 | 37.00 | 188.08 | 0.50 | 12.00 | 197.60 | 28.27  | 2912.26   | 181.26 | 0.05 | 0.02 |
| 19     | SLE F | Diff. | 2.70 | 0.00 | 4.60  | -20299.40 | 3472.04 | 37.00 | 188.08 | 0.50 | 12.00 | 198.32 | 28.27  | 2929.21   | 189.17 | 0.06 | 0.02 |

Parete n. 11

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | TP    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
| <cm>  | <cm>   | <cm> | <cm>   | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| Oriz. | 30.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali

Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC/TCC | Zona | Zv    | Xi   | Xf   | N     | My         | Nu       | MRdy       | Sic.      |       |
|--------|------|-------|------|------|-------|------------|----------|------------|-----------|-------|
|        |      | <m>   | <m>  | <m>  | <daN> | <daNm>     | <daN>    | <daNm>     |           |       |
| 17     | SLU  | Diff. | 0.00 | 0.00 | 25.60 | -325198.00 | 71638.00 | -325198.00 | 236719.00 | 3.304 |
| 17     | SLU  | Diff. | 1.35 | 0.00 | 25.60 | -287503.00 | 23570.70 | -287503.00 | 232453.00 | 9.862 |
| 17     | SLU  | Diff. | 2.70 | 0.00 | 25.60 | -257023.00 | 80005.20 | -257023.00 | 229002.00 | 2.862 |

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Stato limite elastico - Verifiche a flessione/presoflessione

| CC | TCC | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | Nu<br><daN> | M' ydy<br><daNm> | Sic.   |
|----|-----|-------|-----------|-----------|-----------|------------|--------------|-------------|------------------|--------|
| 11 | SND | Diff. | 0.00      | 0.00      | 25.60     | -161614.00 | 158435.00    | -161614.00  | 198162.00        | 1.251  |
| 9  | SND | Diff. | 1.35      | 0.00      | 25.60     | -150587.00 | 19078.10     | -150587.00  | 196885.00        | 10.320 |
| 13 | SND | Diff. | 2.70      | 0.00      | 25.60     | -210178.00 | 129681.00    | -210178.00  | 203783.00        | 1.571  |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC | Zona | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | $\sigma_c$<br><daN/cm <sup>2</sup> > | $\sigma_s$<br><daN/cm <sup>2</sup> > |        |
|----|-----|------|-----------|-----------|-----------|------------|--------------|--------------------------------------|--------------------------------------|--------|
| 18 | SLE | R    | Diff.     | 0.00      | 0.00      | 25.60      | -229120.00   | 49264.00                             | 22.76                                | 528.32 |
| 20 | SLE | Q    | Diff.     | 0.00      | 0.00      | 25.60      | -226032.00   | 49202.10                             | 22.75                                | 533.72 |
| 18 | SLE | R    | Diff.     | 1.35      | 0.00      | 25.60      | -200077.00   | 17679.80                             | 7.16                                 | 84.98  |
| 20 | SLE | Q    | Diff.     | 1.35      | 0.00      | 25.60      | -196937.00   | 16787.50                             | 6.80                                 | 81.42  |
| 18 | SLE | R    | Diff.     | 2.70      | 0.00      | 25.60      | -176632.00   | 55955.40                             | 26.49                                | 789.77 |
| 20 | SLE | Q    | Diff.     | 2.70      | 0.00      | 25.60      | -173474.00   | 54275.40                             | 25.68                                | 761.00 |

Stato limite d'esercizio - Verifiche a fessurazione

| CC | TCC | Zona | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | c<br><mm> | s<br><mm> | K <sub>2</sub> | $\Phi_{eq}$ | $\Delta_{sm}$<br><mm> | $A_s$<br><cm <sup>2</sup> > | $A_{c\ eff}$<br><cm <sup>2</sup> > | $\sigma_s$<br><daN/cm <sup>2</sup> > | $\epsilon_{sm}$ | Wk<br><mm> |      |
|----|-----|------|-----------|-----------|-----------|------------|--------------|-----------|-----------|----------------|-------------|-----------------------|-----------------------------|------------------------------------|--------------------------------------|-----------------|------------|------|
| 20 | SLE | Q    | Diff.     | 0.00      | 0.00      | 25.60      | -226032.00   | 49202.10  | 37.00     | 149.21         | 0.50        | 12.00                 | 179.15                      | 194.53                             | 17046.00                             | 533.72          | 0.16       | 0.05 |
| 19 | SLE | F    | Diff.     | 0.00      | 0.00      | 25.60      | -227576.00   | 49233.10  | 37.00     | 149.21         | 0.50        | 12.00                 | 178.99                      | 194.53                             | 17019.30                             | 531.01          | 0.15       | 0.05 |
| 20 | SLE | Q    | Diff.     | 2.70      | 0.00      | 25.60      | -173474.00   | 54275.40  | 37.00     | 149.21         | 0.50        | 12.00                 | 186.46                      | 194.53                             | 18230.00                             | 761.00          | 0.22       | 0.07 |
| 19 | SLE | F    | Diff.     | 2.70      | 0.00      | 25.60      | -175053.00   | 55115.40  | 37.00     | 149.21         | 0.50        | 12.00                 | 186.55                      | 194.53                             | 18245.30                             | 775.38          | 0.23       | 0.07 |

## 10.0 RISULTATI STRUTTURE FONDAZIONE TRASFORMATORE MT/AT

### 10.1 Diagrammi tassi di sfruttamento

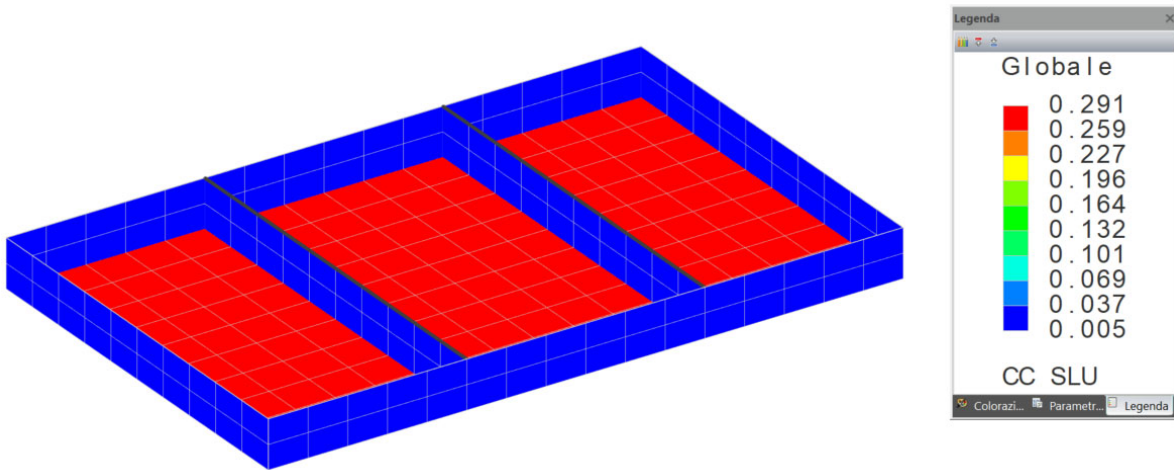
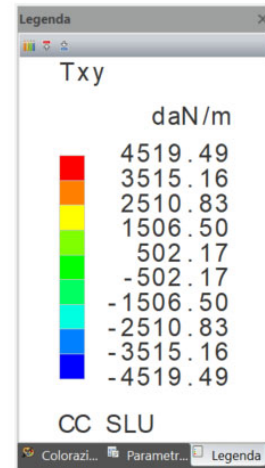
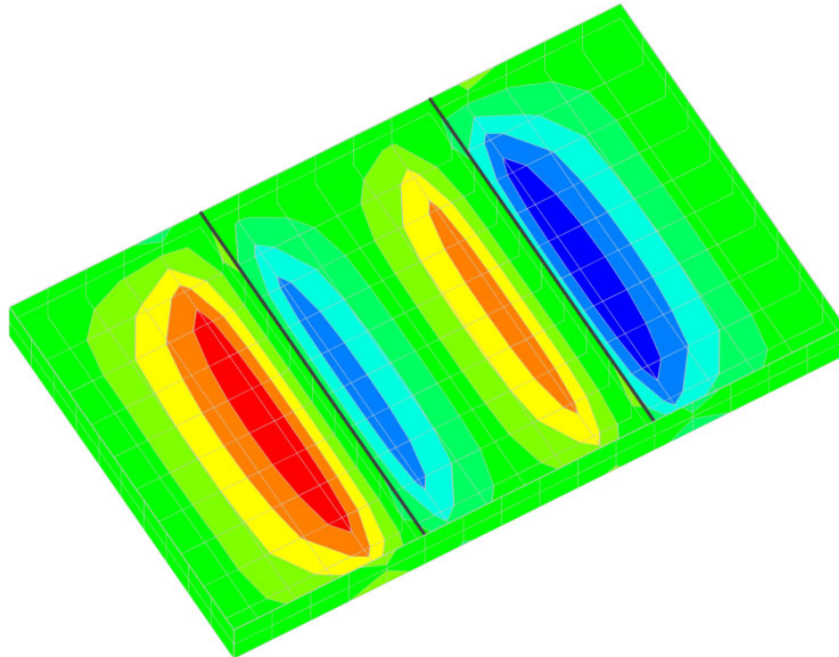


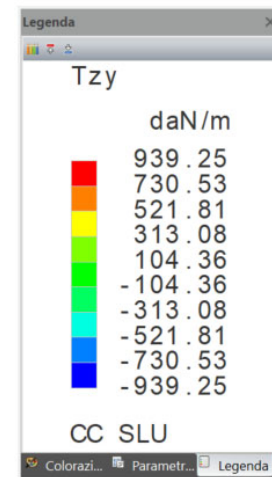
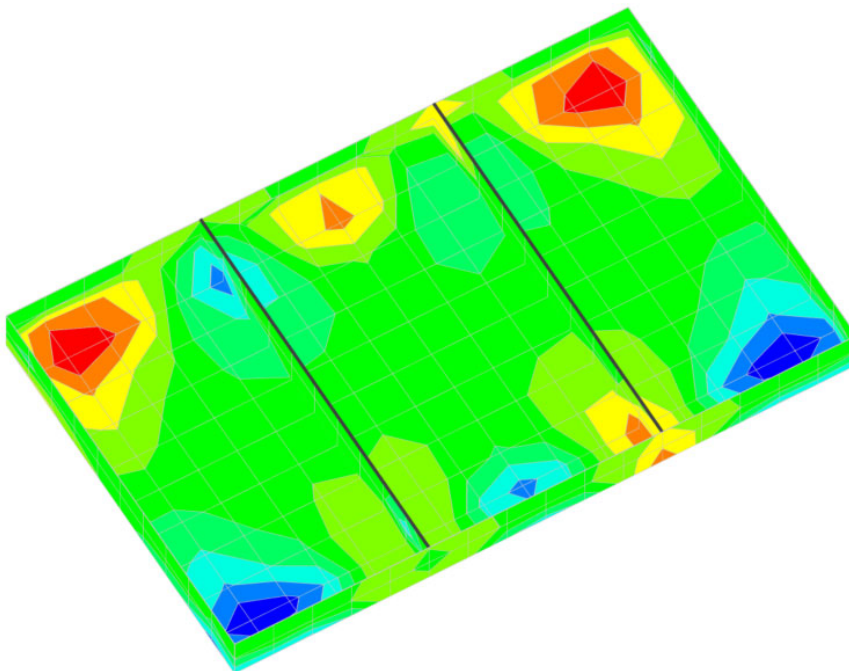
Diagramma tassi di sfruttamento resistenza combo SLU con valore massimo pari a 0,291

**Figure 49: Tassi di sfruttamento SLU (Stato limite ultimo)**

## 10.2 Sollecitazioni

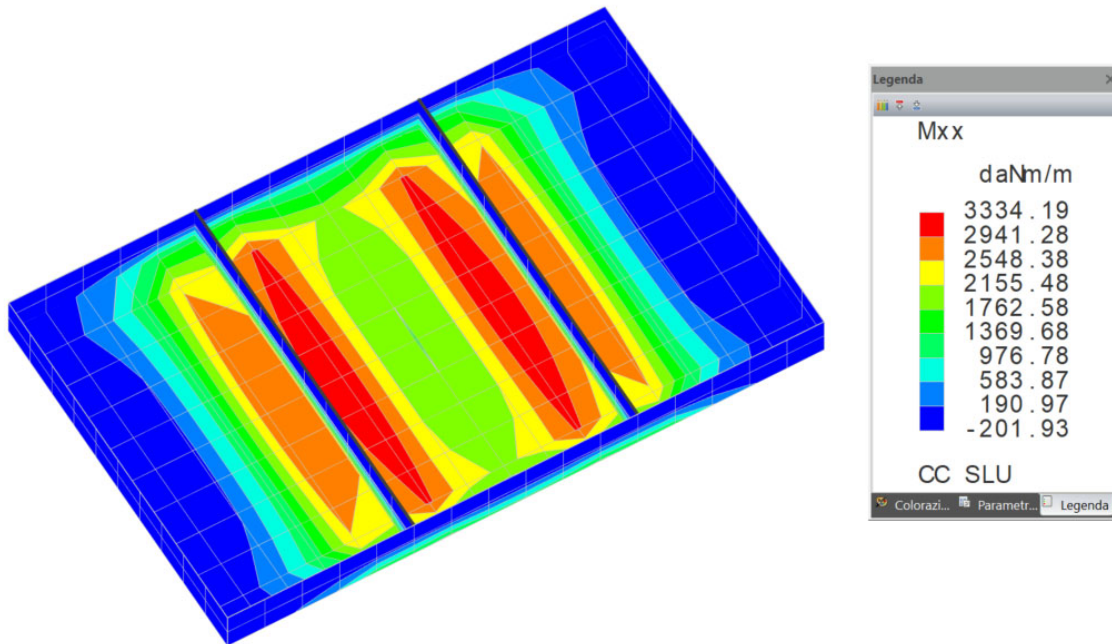


Inviluppo sforzo di taglio in direzione X su faccia con normale Y SLU Tmax = 4519,49 daN/m

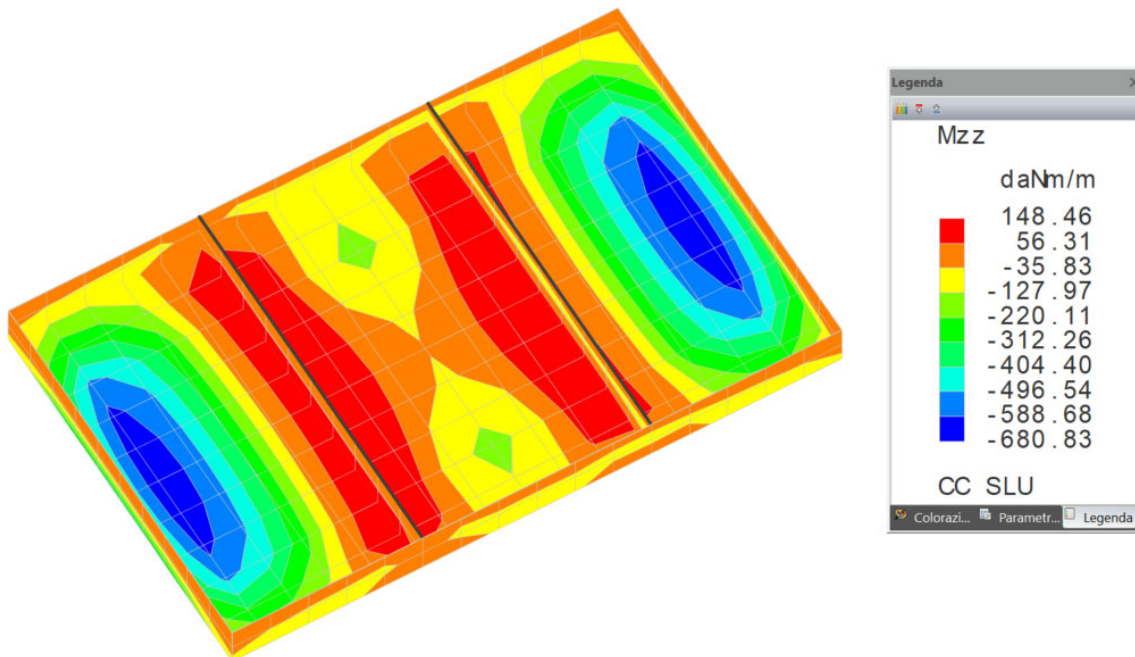


Inviluppo sforzo di taglio in direzione Z su faccia con normale Y SLU Tmax = 939,25 daN/m

**Figure 50: Taglio**



Inviluppo momento che genera tensioni in direzioni X su facce con normale X SLU  $M_{max} = 3334,19 \text{ daN}\times\text{m}/\text{m}$



Inviluppo momento che genera tensioni in direzioni Z su facce con normale Z SLU  $M_{max} = 680,83 \text{ daN}\times\text{m}/\text{m}$

**Figure 51: Momento Flettente**



## 10.3 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

### Risultati del calcolo

#### Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:  
 ModeSt ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato  
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:  
 Xfinest ver. 9.5.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18  
 Tipo di calcolo: statico  
 Vincoli esterni: Considera sempre vincoli assegnati in modellazione  
 Schematizzazione piani rigidi: nessun impalcato rigido  
 Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

#### Generazione combinazioni

- Lineari: Sì  
 - Valuta spostamenti e non sollecitazioni: No  
 - Buckling: No

#### Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%  
 - Calcolo con offset rigidi dai nodi: No  
 - Uniformare i carichi variabili: No  
 - Massimizzare i carichi variabili: No  
 - Recupero carichi zone rigide: taglio e momento flettente

#### Opzioni del solutore

- Tipo di elemento bidimensionale: QF46  
 - Calcolo sforzo nei nodi: No  
 - Trascura deformabilità a taglio delle aste: No  
 - Analisi dinamica con metodo di Lanczos: Sì  
 - Check sequenza di Sturm: Sì  
 - Analisi non lineare con Newton modificato: No  
 - Usa formulazione secante per buckling: No  
 - Trascura buckling torsionale: No

#### Dati struttura

- Edificio esistente: No  
 - Tipo di opera: Opera ordinaria  
 - Vita nominale  $V_n$ : 50.00  
 - Classe d'uso: Classe II  
 - Forze orizzontali convenzionali per stati limite non sismici: No  
 - Genera stati limite per verifiche di resistenza al fuoco: No

#### Ambienti di carico

##### Simbologia

N = Numero  
 Comm. = Commento  
 1 = G1 - permanenti strutturali  
 2 = G2 - permanenti non strutturali  
 3 = Q - Variabili cat.E  
 F = azioni orizzontali convenzionali  
 SLU = Stato limite ultimo  
 SLR = Stato limite per combinazioni rare  
 SLF = Stato limite per combinazioni frequenti  
 SLQ/D = Stato limite per combinazioni quasi permanenti o di danno  
 S = Sì  
 N = No

| N | Comm.           | 1 | 2 | 3 | SLU | SLR | SLF | SLQ |
|---|-----------------|---|---|---|-----|-----|-----|-----|
| 1 | Calcolo statico | S | S | S | S   | S   | S   | S   |

#### Elenco combinazioni di carico simboliche

##### Simbologia

CC = Numero della combinazione delle condizioni di carico elementari  
 Comm. = Commento  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| CC | Comm.          | TCC   | 1              | 2              | 3              |
|----|----------------|-------|----------------|----------------|----------------|
| 1  | Amb. 1 (SLU)   | SLU   | $\gamma_{max}$ | $\gamma_{max}$ | $\gamma_{max}$ |
| 2  | Amb. 1 (SLE R) | SLE R | 1              | 1              | 1              |
| 3  | Amb. 1 (SLE F) | SLE F | 1              | 1              | $\psi_1$       |
| 4  | Amb. 1 (SLE Q) | SLE Q | 1              | 1              | $\psi_2$       |

Genera le combinazioni con un solo carico di tipo variabile come di base: Sì

Considera sollecitazioni dinamiche con segno dei modi principali: No

#### Combinazioni delle CCE

##### Simbologia

An. = Tipo di analisi  
 L = Lineare  
 NL = Non lineare  
 Bk = Buckling



S = S1  
 N = No  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Comm. = Commento  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| CC | Comm.          | TCC   | An. | Bk | 1    | 2    | 3    |
|----|----------------|-------|-----|----|------|------|------|
| 1  | Amb. 1 (SLU)   | SLU   | L   | N  | 1.30 | 1.50 | 1.50 |
| 2  | Amb. 1 (SLE R) | SLE R | L   | N  | 1.00 | 1.00 | 1.00 |
| 3  | Amb. 1 (SLE F) | SLE F | L   | N  | 1.00 | 1.00 | 0.90 |
| 4  | Amb. 1 (SLE Q) | SLE Q | L   | N  | 1.00 | 1.00 | 0.80 |

Tensioni sul terreno

Simbologia

$\sigma_t$  = Tensione sul terreno  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Nodo = Numero del nodo  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| Nodo | CC   | TCC | $\sigma_t$<br><daN/cm <sup>2</sup> > | Nodo | CC   | TCC  | $\sigma_t$<br><daN/cm <sup>2</sup> > | Nodo | CC  | TCC  | $\sigma_t$<br><daN/cm <sup>2</sup> > | Nodo | CC | TCC | $\sigma_t$<br><daN/cm <sup>2</sup> > |      |
|------|------|-----|--------------------------------------|------|------|------|--------------------------------------|------|-----|------|--------------------------------------|------|----|-----|--------------------------------------|------|
| -493 | Max  | 1   | SLU                                  | 0.54 | -493 | Min. | 4                                    | SLE  | Q   | 0.38 | -492                                 | Max  | 1  | SLU | 0.54                                 |      |
| -491 | Min. | 4   | SLE                                  | Q    | 0.38 | -485 | Max                                  | 1    | SLU | 0.55 | -485                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -483 | Max  | 1   | SLU                                  | 0.56 | -483 | Min. | 4                                    | SLE  | Q   | 0.39 | -482                                 | Max  | 1  | SLU | 0.56                                 |      |
| -481 | Min. | 4   | SLE                                  | Q    | 0.39 | -480 | Max                                  | 1    | SLU | 0.56 | -480                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -476 | Max  | 1   | SLU                                  | 0.56 | -476 | Min. | 4                                    | SLE  | Q   | 0.39 | -475                                 | Max  | 1  | SLU | 0.56                                 |      |
| -474 | Min. | 4   | SLE                                  | Q    | 0.39 | -473 | Max                                  | 1    | SLU | 0.55 | -473                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -466 | Max  | 1   | SLU                                  | 0.54 | -466 | Min. | 4                                    | SLE  | Q   | 0.38 | -465                                 | Max  | 1  | SLU | 0.54                                 |      |
| -464 | Min. | 4   | SLE                                  | Q    | 0.37 | -463 | Max                                  | 1    | SLU | 0.54 | -463                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -456 | Max  | 1   | SLU                                  | 0.55 | -456 | Min. | 4                                    | SLE  | Q   | 0.38 | -455                                 | Max  | 1  | SLU | 0.55                                 |      |
| -454 | Min. | 4   | SLE                                  | Q    | 0.39 | -453 | Max                                  | 1    | SLU | 0.56 | -453                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -451 | Max  | 1   | SLU                                  | 0.56 | -451 | Min. | 4                                    | SLE  | Q   | 0.39 | -448                                 | Max  | 1  | SLU | 0.56                                 |      |
| -447 | Min. | 4   | SLE                                  | Q    | 0.39 | -446 | Max                                  | 1    | SLU | 0.55 | -446                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -444 | Max  | 1   | SLU                                  | 0.55 | -444 | Min. | 4                                    | SLE  | Q   | 0.38 | -443                                 | Max  | 1  | SLU | 0.54                                 |      |
| -437 | Min. | 4   | SLE                                  | Q    | 0.38 | -436 | Max                                  | 1    | SLU | 0.54 | -436                                 | Min. | 4  | SLE | Q                                    | 0.37 |
| -434 | Max  | 1   | SLU                                  | 0.54 | -434 | Min. | 4                                    | SLE  | Q   | 0.38 | -433                                 | Max  | 1  | SLU | 0.54                                 |      |
| -427 | Min. | 4   | SLE                                  | Q    | 0.38 | -426 | Max                                  | 1    | SLU | 0.55 | -426                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -424 | Max  | 1   | SLU                                  | 0.56 | -424 | Min. | 4                                    | SLE  | Q   | 0.39 | -423                                 | Max  | 1  | SLU | 0.56                                 |      |
| -422 | Min. | 4   | SLE                                  | Q    | 0.39 | -419 | Max                                  | 1    | SLU | 0.56 | -419                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -417 | Max  | 1   | SLU                                  | 0.55 | -417 | Min. | 4                                    | SLE  | Q   | 0.39 | -416                                 | Max  | 1  | SLU | 0.55                                 |      |
| -415 | Min. | 4   | SLE                                  | Q    | 0.38 | -414 | Max                                  | 1    | SLU | 0.54 | -414                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -407 | Max  | 1   | SLU                                  | 0.54 | -407 | Min. | 4                                    | SLE  | Q   | 0.37 | -406                                 | Max  | 1  | SLU | 0.53                                 |      |
| -405 | Min. | 4   | SLE                                  | Q    | 0.38 | -404 | Max                                  | 1    | SLU | 0.54 | -404                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -397 | Max  | 1   | SLU                                  | 0.55 | -397 | Min. | 4                                    | SLE  | Q   | 0.39 | -396                                 | Max  | 1  | SLU | 0.55                                 |      |
| -395 | Min. | 4   | SLE                                  | Q    | 0.39 | -394 | Max                                  | 1    | SLU | 0.56 | -394                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -390 | Max  | 1   | SLU                                  | 0.56 | -390 | Min. | 4                                    | SLE  | Q   | 0.39 | -389                                 | Max  | 1  | SLU | 0.56                                 |      |
| -388 | Min. | 4   | SLE                                  | Q    | 0.39 | -387 | Max                                  | 1    | SLU | 0.55 | -387                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -385 | Max  | 1   | SLU                                  | 0.54 | -385 | Min. | 4                                    | SLE  | Q   | 0.38 | -379                                 | Max  | 1  | SLU | 0.54                                 |      |
| -378 | Min. | 4   | SLE                                  | Q    | 0.37 | -377 | Max                                  | 1    | SLU | 0.53 | -377                                 | Min. | 4  | SLE | Q                                    | 0.37 |
| -375 | Max  | 1   | SLU                                  | 0.54 | -375 | Min. | 4                                    | SLE  | Q   | 0.38 | -369                                 | Max  | 1  | SLU | 0.55                                 |      |
| -368 | Min. | 4   | SLE                                  | Q    | 0.39 | -367 | Max                                  | 1    | SLU | 0.55 | -367                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -365 | Max  | 1   | SLU                                  | 0.56 | -365 | Min. | 4                                    | SLE  | Q   | 0.39 | -364                                 | Max  | 1  | SLU | 0.56                                 |      |
| -361 | Min. | 4   | SLE                                  | Q    | 0.39 | -360 | Max                                  | 1    | SLU | 0.56 | -360                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -358 | Max  | 1   | SLU                                  | 0.55 | -358 | Min. | 4                                    | SLE  | Q   | 0.39 | -357                                 | Max  | 1  | SLU | 0.55                                 |      |
| -356 | Min. | 4   | SLE                                  | Q    | 0.38 | -350 | Max                                  | 1    | SLU | 0.54 | -350                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -348 | Max  | 1   | SLU                                  | 0.53 | -348 | Min. | 4                                    | SLE  | Q   | 0.37 | -347                                 | Max  | 1  | SLU | 0.54                                 |      |
| -346 | Min. | 4   | SLE                                  | Q    | 0.38 | -340 | Max                                  | 1    | SLU | 0.55 | -340                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -338 | Max  | 1   | SLU                                  | 0.55 | -338 | Min. | 4                                    | SLE  | Q   | 0.39 | -337                                 | Max  | 1  | SLU | 0.56                                 |      |
| -336 | Min. | 4   | SLE                                  | Q    | 0.39 | -335 | Max                                  | 1    | SLU | 0.56 | -335                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -331 | Max  | 1   | SLU                                  | 0.56 | -331 | Min. | 4                                    | SLE  | Q   | 0.39 | -330                                 | Max  | 1  | SLU | 0.55                                 |      |
| -329 | Min. | 4   | SLE                                  | Q    | 0.39 | -328 | Max                                  | 1    | SLU | 0.55 | -328                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -321 | Max  | 1   | SLU                                  | 0.54 | -321 | Min. | 4                                    | SLE  | Q   | 0.38 | -320                                 | Max  | 1  | SLU | 0.53                                 |      |
| -145 | Min. | 4   | SLE                                  | Q    | 0.37 | -144 | Max                                  | 1    | SLU | 0.54 | -144                                 | Min. | 4  | SLE | Q                                    | 0.38 |
| -137 | Max  | 1   | SLU                                  | 0.55 | -137 | Min. | 4                                    | SLE  | Q   | 0.38 | -136                                 | Max  | 1  | SLU | 0.55                                 |      |
| -135 | Min. | 4   | SLE                                  | Q    | 0.39 | -134 | Max                                  | 1    | SLU | 0.56 | -134                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -132 | Max  | 1   | SLU                                  | 0.56 | -132 | Min. | 4                                    | SLE  | Q   | 0.39 | -129                                 | Max  | 1  | SLU | 0.56                                 |      |
| -128 | Min. | 4   | SLE                                  | Q    | 0.39 | -127 | Max                                  | 1    | SLU | 0.55 | -127                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -125 | Max  | 1   | SLU                                  | 0.55 | -125 | Min. | 4                                    | SLE  | Q   | 0.38 | -124                                 | Max  | 1  | SLU | 0.54                                 |      |
| -118 | Min. | 4   | SLE                                  | Q    | 0.38 | -117 | Max                                  | 1    | SLU | 0.53 | -117                                 | Min. | 4  | SLE | Q                                    | 0.37 |
| -115 | Max  | 1   | SLU                                  | 0.54 | -115 | Min. | 4                                    | SLE  | Q   | 0.38 | -114                                 | Max  | 1  | SLU | 0.54                                 |      |
| -108 | Min. | 4   | SLE                                  | Q    | 0.38 | -107 | Max                                  | 1    | SLU | 0.55 | -107                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -105 | Max  | 1   | SLU                                  | 0.56 | -105 | Min. | 4                                    | SLE  | Q   | 0.39 | -104                                 | Max  | 1  | SLU | 0.56                                 |      |
| -103 | Min. | 4   | SLE                                  | Q    | 0.39 | -100 | Max                                  | 1    | SLU | 0.56 | -100                                 | Min. | 4  | SLE | Q                                    | 0.39 |
| -98  | Max  | 1   | SLU                                  | 0.55 | -98  | Min. | 4                                    | SLE  | Q   | 0.39 | -97                                  | Max  | 1  | SLU | 0.55                                 |      |
| -96  | Min. | 4   | SLE                                  | Q    | 0.38 | -95  | Max                                  | 1    | SLU | 0.54 | -95                                  | Min. | 4  | SLE | Q                                    | 0.38 |
| -88  | Max  | 1   | SLU                                  | 0.53 | -88  | Min. | 4                                    | SLE  | Q   | 0.37 | -87                                  | Max  | 1  | SLU | 0.54                                 |      |
| -86  | Min. | 4   | SLE                                  | Q    | 0.38 | -85  | Max                                  | 1    | SLU | 0.54 | -85                                  | Min. | 4  | SLE | Q                                    | 0.38 |
| -78  | Max  | 1   | SLU                                  | 0.55 | -78  | Min. | 4                                    | SLE  | Q   | 0.39 | -77                                  | Max  | 1  | SLU | 0.55                                 |      |
| -76  | Min. | 4   | SLE                                  | Q    | 0.39 | -75  | Max                                  | 1    | SLU | 0.56 | -75                                  | Min. | 4  | SLE | Q                                    | 0.39 |
| -71  | Max  | 1   | SLU                                  | 0.56 | -71  | Min. | 4                                    | SLE  | Q   | 0.39 | -70                                  | Max  | 1  | SLU | 0.56                                 |      |
| -69  | Min. | 4   | SLE                                  | Q    | 0.39 | -68  | Max                                  | 1    | SLU | 0.55 | -68                                  | Min. | 4  | SLE | Q                                    | 0.39 |
| -66  | Max  | 1   | SLU                                  | 0.54 | -66  | Min. | 4                                    | SLE  | Q   | 0.38 | -60                                  | Max  | 1  | SLU | 0.54                                 |      |
| -59  | Min. | 4   | SLE                                  | Q    | 0.37 | -58  | Max                                  | 1    | SLU | 0.54 | -58                                  | Min. | 4  | SLE | Q                                    | 0.37 |
| -56  | Max  | 1   | SLU                                  | 0.54 | -56  | Min. | 4                                    | SLE  | Q   | 0.38 | -50                                  | Max  | 1  | SLU | 0.55                                 |      |
| -49  | Min. | 4   | SLE                                  | Q    | 0.39 | -48  | Max                                  | 1    | SLU | 0.55 | -48                                  | Min. | 4  | SLE | Q                                    | 0.39 |
| -46  | Max  | 1   | SLU                                  | 0.56 | -46  | Min. | 4                                    | SLE  | Q   | 0.39 | -45                                  | Max  | 1  | SLU | 0.56                                 |      |
| -42  | Min. | 4   | SLE                                  | Q    | 0.39 | -41  | Max                                  | 1    | SLU | 0.56 | -41                                  | Min. | 4  | SLE | Q                                    | 0.39 |
| -39  | Max  | 1   | SLU                                  | 0.55 | -39  | Min. | 4                                    | SLE  | Q   | 0.39 | -38                                  | Max  | 1  | SLU | 0.55                                 |      |
| -37  | Min. | 4   | SLE                                  | Q    | 0.38 | -31  | Max                                  | 1    | SLU | 0.54 | -31                                  | Min. | 4  | SLE | Q                                    | 0.38 |
| -29  | Max  | 1   | SLU                                  | 0.54 | -29  | Min. | 4                                    | SLE  | Q   | 0.38 | -28                                  | Max  | 1  | SLU | 0.54                                 |      |
| -27  | Min. | 4   | SLE                                  | Q    | 0.38 | -21  | Max                                  | 1    | SLU | 0.55 | -21                                  | Min. | 4  | SLE | Q                                    | 0.38 |
| -19  | Max  | 1   | SLU                                  | 0.56 | -19  | Min. | 4                                    | SLE  | Q   | 0.39 | -18                                  | Max  | 1  | SLU | 0.56                                 |      |



|     |      |   |       |      |     |      |   |       |      |     |      |   |       |      |     |      |   |       |      |     |      |   |       |      |     |      |   |       |      |
|-----|------|---|-------|------|-----|------|---|-------|------|-----|------|---|-------|------|-----|------|---|-------|------|-----|------|---|-------|------|-----|------|---|-------|------|
| -17 | Min. | 4 | SLE Q | 0.39 | -16 | Max  | 1 | SLU   | 0.56 | -16 | Min. | 4 | SLE Q | 0.39 | -13 | Max  | 1 | SLU   | 0.56 | -13 | Min. | 4 | SLE Q | 0.39 |     |      |   |       |      |
| -12 | Max  | 1 | SLU   | 0.56 | -12 | Min. | 4 | SLE Q | 0.39 | -11 | Max  | 1 | SLU   | 0.56 | -11 | Min. | 4 | SLE Q | 0.39 | -10 | Max  | 1 | SLU   | 0.55 | -10 | Min. | 4 | SLE Q | 0.39 |
| -10 | Min. | 4 | SLE Q | 0.39 | -9  | Max  | 1 | SLU   | 0.55 | -9  | Min. | 4 | SLE Q | 0.38 | -8  | Max  | 1 | SLU   | 0.54 | -8  | Min. | 4 | SLE Q | 0.38 | -8  | Min. | 4 | SLE Q | 0.38 |
| -2  | Max  | 1 | SLU   | 0.54 | -2  | Min. | 4 | SLE Q | 0.38 | -1  | Max  | 1 | SLU   | 0.54 | -1  | Min. | 4 | SLE Q | 0.38 |     |      |   |       |      |     |      |   |       |      |

Sollecitazioni elementi bidimensionali  
Simbologia

$\sigma_{xx}$  = Tensione normale sulle facce perp. all'asse X  
 $\sigma_{zz}$  = Tensione normale sulle facce perp. all'asse Z  
 $\tau_{xy}$  = Tensione in dir. Y sulle facce perp. all'asse X  
 $\tau_{xz}$  = Tensione in dir. Z sulle facce perp. all'asse X  
 $\tau_{zy}$  = Tensione in dir. Y sulle facce perp. all'asse Z  
Bid. = Numero del muro/elemento bidimensionale  
CC = Numero della combinazione delle condizioni di carico elementari  
Mxx = Momento che provoca variazione di tensione sulle facce perp. all'asse X  
Mxz = Momento che provoca variazione di tensione tangenziale sulle facce perp. all'asse X  
Mzz = Momento che provoca variazione di tensione sulle facce perp. all'asse Z  
Nodo = Numero del nodo  
TCC = Tipo di combinazione di carico  
SLU = Stato limite ultimo  
SLE R = Stato limite d'esercizio, combinazione rara  
SLE F = Stato limite d'esercizio, combinazione frequente  
SLE Q = Stato limite d'esercizio, combinazione quasi permanente

Bid. 8

|                        | CC | TCC | Nodo | Min.  | CC | TCC | Nodo | Max  |                        | CC | TCC | Nodo | Min.   | CC | TCC | Nodo | Max   |
|------------------------|----|-----|------|-------|----|-----|------|------|------------------------|----|-----|------|--------|----|-----|------|-------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -103 | 0     | 1  | SLU | -406 | 0    | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -136 | 0      | 1  | SLU | -42  | 0     |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -134 | 0     | 1  | SLU | -16  | 0    | Mxx <daNm/m>           | 1  | SLU | -327 | -208   | 1  | SLU | -331 | 4135  |
| Mzz <daNm/m>           | 1  | SLU | -144 | -724  | 1  | SLU | -98  | 215  | Mxz <daNm/m>           | 1  | SLU | -456 | -452   | 1  | SLU | -49  | 452   |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU | -31  | -2452 | 1  | SLU | -492 | 2452 | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -338 | -10613 | 1  | SLU | -359 | 10613 |

Bid. 9

|                        | CC | TCC   | Nodo | Min.  | CC | TCC | Nodo | Max   |                        | CC | TCC | Nodo | Min.  | CC | TCC   | Nodo | Max  |
|------------------------|----|-------|------|-------|----|-----|------|-------|------------------------|----|-----|------|-------|----|-------|------|------|
| $\sigma_{xx}$ <daN/mq> | 2  | SLE R | -1   | 1465  | 1  | SLU | -535 | 30957 | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -407 | -2652 | 2  | SLE R | -697 | -413 |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU   | -523 | -7133 | 1  | SLU | -579 | 7133  | Mxx <daNm/m>           | 1  | SLU | -579 | -16   | 1  | SLU   | -641 | 16   |
| Mzz <daNm/m>           | 1  | SLU   | -612 | -7    | 1  | SLU | -583 | 30    | Mxz <daNm/m>           | 1  | SLU | -575 | -41   | 1  | SLU   | -523 | 41   |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU   | -583 | -1817 | 1  | SLU | -30  | 99    | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -494 | -901  | 1  | SLU   | -701 | 901  |

Bid. 10

|                        | CC | TCC | Nodo | Min.    | CC | TCC   | Nodo | Max   |                        | CC | TCC | Nodo | Min.  | CC | TCC | Nodo | Max  |
|------------------------|----|-----|------|---------|----|-------|------|-------|------------------------|----|-----|------|-------|----|-----|------|------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -512 | -118904 | 2  | SLE R | -521 | -2262 | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -512 | -5448 | 1  | SLU | -620 | 406  |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -10  | -21492  | 1  | SLU   | -513 | 21492 | Mxx <daNm/m>           | 1  | SLU | -522 | -51   | 1  | SLU | -630 | 143  |
| Mzz <daNm/m>           | 1  | SLU | -20  | -79     | 2  | SLE R | -639 | -5    | Mxz <daNm/m>           | 1  | SLU | -10  | -127  | 1  | SLU | -513 | 127  |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU | -522 | -75     | 1  | SLU   | -503 | 1443  | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -513 | -3336 | 1  | SLU | -621 | 3336 |

Bid. 11

|                        | CC | TCC   | Nodo | Min.  | CC | TCC | Nodo | Max   |                        | CC | TCC | Nodo | Min.  | CC | TCC   | Nodo | Max  |
|------------------------|----|-------|------|-------|----|-----|------|-------|------------------------|----|-----|------|-------|----|-------|------|------|
| $\sigma_{xx}$ <daN/mq> | 2  | SLE R | -464 | 1465  | 1  | SLU | -566 | 30957 | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -87  | -2652 | 2  | SLE R | -729 | -413 |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU   | -464 | -7133 | 1  | SLU | -58  | 7133  | Mxx <daNm/m>           | 1  | SLU | -522 | -16   | 1  | SLU   | -696 | 16   |
| Mzz <daNm/m>           | 1  | SLU   | -611 | -7    | 1  | SLU | -526 | 30    | Mxz <daNm/m>           | 1  | SLU | -58  | -41   | 1  | SLU   | -464 | 41   |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU   | -526 | -1817 | 1  | SLU | -582 | 99    | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -729 | -901  | 1  | SLU   | -644 | 901  |

Bid. 12

|                        | CC | TCC | Nodo | Min.    | CC | TCC   | Nodo | Max   |                        | CC | TCC | Nodo | Min.  | CC | TCC | Nodo | Max  |
|------------------------|----|-----|------|---------|----|-------|------|-------|------------------------|----|-----|------|-------|----|-----|------|------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -593 | -118904 | 2  | SLE R | -584 | -2262 | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -593 | -5448 | 1  | SLU | -710 | 406  |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU | -484 | -21492  | 1  | SLU   | -592 | 21492 | Mxx <daNm/m>           | 1  | SLU | -583 | -51   | 1  | SLU | -711 | 143  |
| Mzz <daNm/m>           | 1  | SLU | -474 | -79     | 2  | SLE R | -702 | -5    | Mxz <daNm/m>           | 1  | SLU | -484 | -127  | 1  | SLU | -592 | 127  |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU | -583 | -75     | 1  | SLU   | -602 | 1443  | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -592 | -3336 | 1  | SLU | -720 | 3336 |

Bid. 13

|                        | CC | TCC   | Nodo | Min.  | CC | TCC   | Nodo | Max  |                        | CC | TCC | Nodo | Min.   | CC | TCC   | Nodo | Max   |
|------------------------|----|-------|------|-------|----|-------|------|------|------------------------|----|-----|------|--------|----|-------|------|-------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU   | -417 | -411  | 1  | SLU   | -564 | 6004 | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -330 | -17524 | 2  | SLE R | -524 | -5582 |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU   | -711 | -2457 | 1  | SLU   | -504 | 2457 | Mxx <daNm/m>           | 1  | SLU | -593 | -33    | 1  | SLU   | -694 | 81    |
| Mzz <daNm/m>           | 2  | SLE R | -524 | 5     | 1  | SLU   | -40  | 103  | Mxz <daNm/m>           | 1  | SLU | -446 | -219   | 1  | SLU   | -40  | 219   |
| $\tau_{zy}$ <daN/mq>   | 1  | SLU   | -580 | -2060 | 2  | SLE R | -694 | -47  | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -642 | -1883  | 1  | SLU   | -580 | 1883  |

Bid. 14

|                        | CC | TCC   | Nodo | Min.  | CC | TCC   | Nodo | Max  |                        | CC | TCC | Nodo | Min.   | CC | TCC   | Nodo | Max   |
|------------------------|----|-------|------|-------|----|-------|------|------|------------------------|----|-----|------|--------|----|-------|------|-------|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU   | -425 | -411  | 1  | SLU   | -565 | 6004 | $\sigma_{zz}$ <daN/mq> | 1  | SLU | -338 | -17524 | 2  | SLE R | -525 | -5582 |
| $\tau_{xz}$ <daN/mq>   | 1  | SLU   | -699 | -2457 | 1  | SLU   | -643 | 2457 | Mxx <daNm/m>           | 1  | SLU | -695 | -81    | 1  | SLU   | -630 | 33    |
| Mzz <daNm/m>           | 1  | SLU   | -483 | -103  | 2  | SLE R | -581 | -5   | Mxz <daNm/m>           | 1  | SLU | -48  | -219   | 1  | SLU   | -454 | 219   |
| $\tau_{zy}$ <daN/mq>   | 2  | SLE R | -647 | 47    | 1  | SLU   | -512 | 2060 | $\tau_{xy}$ <daN/mq>   | 1  | SLU | -699 | -1883  | 1  | SLU   | -525 | 1883  |

Verifiche e armature solette/platee

Simbologia

$\Delta_{sm}$  = Distanza media tra le fessure  
 $\Phi_{eq}$  = Diametro equivalente delle barre  
 $\epsilon_{sm}$  = Deformazione unitaria media dell'armatura (\*1000)  
 $\sigma_c$  = Tensione nel calcestruzzo  
 $\sigma_f$  = Tensione nel ferro  
 $\sigma_s$  = Tensione nell'acciaio nella sezione fessurata  
 $A_{c\ eff}$  = Area di calcestruzzo efficace  
 $A_s$  = Area complessiva dei ferri nell'area di calcestruzzo efficace  
AFE I = Area di ferro effettiva totale presente nel punto di verifica, inferiore  
AFE S = Area di ferro effettiva totale presente nel punto di verifica, superiore  
AFE St. = Area di ferro effettiva della staffatura  
CC = Numero della combinazione delle condizioni di carico elementari  
Cf inf = Copriferro inferiore  
Cf sup = Copriferro superiore



Cls = Tipo di calcestruzzo  
 DV = Direzione di verifica  
 XX = Verifica per momento Mxx  
 YY = Verifica per momento Myy  
 Fcd = Resistenza di calcolo a compressione del calcestruzzo  
 Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo  
 Fctd = Resistenza di calcolo a trazione del calcestruzzo  
 Fctk = Resistenza caratteristica a trazione del calcestruzzo  
 Fyd = Resistenza di calcolo dell'acciaio  
 Fyk = Tensione caratteristica di snervamento dell'acciaio  
 K<sub>2</sub> = Coefficiente per distribuzione deformazioni  
 MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y  
 Mom = Momento flettente  
 My = Momento flettente intorno all'asse Y  
 Nodo = Numero del nodo  
 Sic. = Sicurezza  
 Spess. = Spessore  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
 Tp = Tipo di acciaio  
 VRcd = Taglio ultimo lato calcestruzzo  
 VRsd = Taglio ultimo lato armatura  
 Vrdu = Taglio ultimo resistente  
 Vsdu = Taglio agente nella direzione del momento ultimo  
 Wk = Ampiezza caratteristica delle fessure  
 X = Coordinata X del nodo  
 Y = Coordinata Y del nodo  
 c = Ricoprimento dell'armatura  
 ctgθ = Cotangente dell'angolo di inclinazione dei puntoni di calcestruzzo  
 s = Distanza massima tra le barre

Armatura platea a quota 0.00

Caratteristiche delle sezioni e dei materiali utilizzati

| Spess.<br><cm> | Cf sup<br><cm> | Cf inf<br><cm> | Cls    | Fck<br><daN/cm²> | Fctk<br><daN/cm²> | Fcd<br><daN/cm²> | Fctd<br><daN/cm²> | Tp    | Fyk<br><daN/cm²> | Fyd<br><daN/cm²> |
|----------------|----------------|----------------|--------|------------------|-------------------|------------------|-------------------|-------|------------------|------------------|
| 50.00          | 3.50           | 3.50           | C32/40 | 332.00           | 21.69             | 188.13           | 14.46             | B450C | 4500.00          | 3913.04          |

Stato limite ultimo - Verifiche a flessione/pressoflessione

| Nodo | X     | Y    | DV | CC | TCC | AfE   | S     | AfE     | I         | My     | MRdy   | Sic. |
|------|-------|------|----|----|-----|-------|-------|---------|-----------|--------|--------|------|
| <cm> | <cm>  | <cm> |    |    |     | <cm²> | <cm²> | <daNm>  | <daNm>    | <daNm> | <daNm> |      |
| -330 | 14.50 | 6.50 | XX | 1  | SLU | 7.70  | 7.70  | 4055.96 | 13950.30  | 3.439  |        |      |
| -321 | 12.50 | 6.50 | XX | 1  | SLU | 7.70  | 7.70  | -201.93 | -13950.30 | 69.085 |        |      |
| -348 | 20.00 | 6.50 | YY | 1  | SLU | 7.70  | 7.70  | -723.91 | -13950.30 | 19.271 |        |      |
| -98  | 14.50 | 5.50 | YY | 1  | SLU | 7.70  | 7.70  | 188.47  | 13950.30  | 74.017 |        |      |

Stato limite ultimo - Verifiche a taglio

| Nodo | X     | Y    | DV | CC | TCC | AfE   | S     | AfE   | I     | AfE St. | Vsdu    | ctgθ | VRcd  | VRsd  | Vrdu     | Sic.   |
|------|-------|------|----|----|-----|-------|-------|-------|-------|---------|---------|------|-------|-------|----------|--------|
| <cm> | <cm>  | <cm> |    |    |     | <cm²> | <cm²> | <cm²> | <cm²> | <cm²/m> | <daN>   |      | <daN> | <daN> | <daN>    |        |
| -339 | 18.00 | 6.50 | XX | 1  | SLU | 7.70  | 7.70  |       |       |         | 4519.49 |      |       |       | 19980.80 | 4.421  |
| -28  | 19.50 | 4.00 | YY | 1  | SLU | 7.70  | 7.70  |       |       |         | 1205.96 |      |       |       | 19980.80 | 16.568 |

Stato limite d'esercizio - Verifiche tensionali

| Nodo | X     | Y    | DV | CC | TCC | AfE   | S     | AfE    | I       | Mom    | σ <sub>c</sub> | σ <sub>f</sub> |
|------|-------|------|----|----|-----|-------|-------|--------|---------|--------|----------------|----------------|
| <cm> | <cm>  | <cm> |    |    |     | <cm²> | <cm²> | <daNm> | <daNm>  | <daNm> | <daN/cm²>      | <daN/cm²>      |
| -338 | 17.50 | 6.50 | XX | 2  | SLE | R     | 7.70  | 7.70   | 2701.40 | 12.34  | 806.40         |                |
| -338 | 17.50 | 6.50 | XX | 4  | SLE | Q     | 7.70  | 7.70   | 2701.40 | 12.34  | 806.40         |                |
| -347 | 19.50 | 6.50 | XX | 2  | SLE | R     | 7.70  | 7.70   | -156.04 | 0.71   | 46.58          |                |
| -347 | 19.50 | 6.50 | XX | 4  | SLE | Q     | 7.70  | 7.70   | -156.04 | 0.71   | 46.58          |                |
| -348 | 20.00 | 6.50 | YY | 2  | SLE | R     | 7.70  | 7.70   | -510.03 | 2.33   | 152.25         |                |
| -348 | 20.00 | 6.50 | YY | 4  | SLE | Q     | 7.70  | 7.70   | -510.03 | 2.33   | 152.25         |                |
| -425 | 17.50 | 8.00 | YY | 2  | SLE | R     | 7.70  | 7.70   | 103.75  | 0.47   | 30.97          |                |
| -425 | 17.50 | 8.00 | YY | 4  | SLE | Q     | 7.70  | 7.70   | 103.75  | 0.47   | 30.97          |                |

Stato limite d'esercizio - Verifiche a fessurazione

| Nodo | X     | Y    | DV | CC | TCC | c    | s     | K <sub>2</sub> | Φ <sub>eq</sub> | Δ <sub>sm</sub> | A <sub>s</sub> | A <sub>s</sub> eff | σ <sub>s</sub> | ε <sub>sm</sub> | Wk   |      |
|------|-------|------|----|----|-----|------|-------|----------------|-----------------|-----------------|----------------|--------------------|----------------|-----------------|------|------|
| <cm> | <cm>  | <cm> |    |    |     | <mm> | <mm>  |                |                 | <mm>            | <cm²>          | <cm²>              | <daN/cm²>      |                 | <mm> |      |
| -338 | 17.50 | 6.50 | XX | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 806.40          | 0.23 | 0.12 |
| -338 | 17.50 | 6.50 | XX | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 806.40          | 0.23 | 0.12 |
| -347 | 19.50 | 6.50 | XX | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 46.58           | 0.01 | 0.01 |
| -347 | 19.50 | 6.50 | XX | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 46.58           | 0.01 | 0.01 |
| -348 | 20.00 | 6.50 | YY | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 152.25          | 0.04 | 0.02 |
| -348 | 20.00 | 6.50 | YY | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 152.25          | 0.04 | 0.02 |
| -425 | 17.50 | 8.00 | YY | 4  | SLE | Q    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 30.97           | 0.01 | 0.00 |
| -425 | 17.50 | 8.00 | YY | 3  | SLE | F    | 28.00 | 200.00         | 0.50            | 14.00           | 309.89         | 9.24               | 875.00         | 30.97           | 0.01 | 0.00 |

Verifiche e armature pareti

Simbologia

Δ<sub>sm</sub> = Distanza media tra le fessure  
 Φ<sub>eq</sub> = Diametro equivalente delle barre  
 ε<sub>sm</sub> = Deformazione unitaria media dell'armatura (\*1000)  
 σ<sub>c</sub> = Tensione nel calcestruzzo  
 σ<sub>f</sub> = Tensione nel ferro  
 σ<sub>s</sub> = Tensione nell'acciaio nella sezione fessurata  
 A<sub>c</sub> eff = Area di calcestruzzo efficace  
 A<sub>s</sub> = Area complessiva dei ferri nell'area di calcestruzzo efficace  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Cf = Copriferro  
 Cls = Tipo di calcestruzzo  
 Fcd = Resistenza di calcolo a compressione del calcestruzzo  
 Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo  
 Fctd = Resistenza di calcolo a trazione del calcestruzzo  
 Fctk = Resistenza caratteristica a trazione del calcestruzzo  
 Fyd = Resistenza di calcolo dell'acciaio  
 Fyk = Tensione caratteristica di snervamento dell'acciaio  
 K<sub>2</sub> = Coefficiente per distribuzione deformazioni  
 M'ydy = Momento resistente massimo in campo sostanzialmente elastico intorno all'asse Y

MRdy =Momento resistente allo stato limite ultimo intorno all'asse Y  
 My =Momento flettente intorno all'asse Y  
 N =Sforzo normale  
 Nu =Sforzo normale ultimo  
 Sez. =Sezione di verifica  
 Sic. =Sicurezza  
 Spess. =Spessore  
 TCC =Tipo di combinazione di carico  
     SLU = Stato limite ultimo  
     SLE R = Stato limite d'esercizio, combinazione rara  
     SLE F = Stato limite d'esercizio, combinazione frequente  
     SLE Q = Stato limite d'esercizio, combinazione quasi permanente  
 Tp =Tipo di acciaio  
 VRcd =Taglio ultimo lato calcestruzzo  
 VRsd =Taglio ultimo lato armatura  
 Vrdu =Taglio ultimo resistente  
 Vsdu =Taglio agente nella direzione del momento ultimo  
 Wk =Ampiezza caratteristica delle fessure  
 Xf =Coordinata X finale  
 Xi =Coordinata X iniziale  
 Xv =Coordinata X di verifica  
 Zona =Zona di verifica  
 Zv =Coordinata Z di verifica  
 c =Ricoprimento dell'armatura  
 s =Distanza massima tra le barre

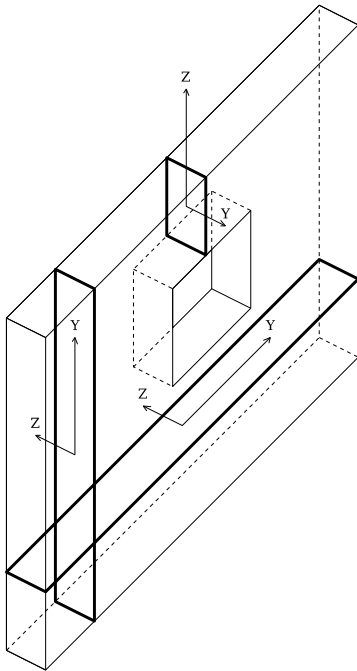


Figura numero 1: Riferimenti sezione

Parete n. 9

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess.<br><cm> | Cf<br><cm> | Cls    | Fck<br><daN/cmq> | Fctk<br><daN/cmq> | Fcd<br><daN/cmq> | Fctd<br><daN/cmq> | Tp    | Fyk<br><daN/cmq> | Fyd<br><daN/cmq> |
|-------|----------------|------------|--------|------------------|-------------------|------------------|-------------------|-------|------------------|------------------|
| Oriz. | 30.00          | 4.30       | C32/40 | 332.00           | 21.69             | 188.13           | 14.46             | B450C | 4500.00          | 3913.04          |

Verifiche su sezioni orizzontali

Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | Nu<br><daN> | MRdy<br><daNm> | Sic. |
|----|-------|-----------|-----------|-----------|------------|--------------|-------------|----------------|------|
| 1  | Diff. | 0.00      | 0.00      | 5.00      | -4306.08   | -178.63      | -4306.08    | -32928.50      | >100 |
| 1  | Diff. | 0.30      | 0.00      | 5.00      | -2843.58   | -6.43        | -3060980.00 | -32760.90      | >100 |
| 1  | Diff. | 0.60      | 0.00      | 5.00      | -321.81    | 5.47         | -321.81     | 32470.90       | >100 |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | $\sigma_c$<br><daN/cmq> | $\sigma_s$<br><daN/cmq> |
|----|-------|-------|-----------|-----------|-----------|------------|--------------|-------------------------|-------------------------|
| 2  | SLE R | Diff. | 0.00      | 0.00      | 5.00      | -3174.87   | -107.53      | 0.33                    | 4.40                    |
| 4  | SLE Q | Diff. | 0.00      | 0.00      | 5.00      | -3174.87   | -107.53      | 0.33                    | 4.40                    |
| 2  | SLE R | Diff. | 0.30      | 0.00      | 5.00      | -2049.87   | -0.99        | 0.13                    | 1.94                    |
| 4  | SLE Q | Diff. | 0.30      | 0.00      | 5.00      | -2049.87   | -0.99        | 0.13                    | 1.94                    |
| 2  | SLE R | Diff. | 0.60      | 0.00      | 5.00      | -215.55    | 3.62         | 0.02                    | 0.25                    |
| 4  | SLE Q | Diff. | 0.60      | 0.00      | 5.00      | -215.55    | 3.62         | 0.02                    | 0.25                    |

Parete n. 10

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez. | Spess.<br><cm> | Cf<br><cm> | Cls | Fck<br><daN/cmq> | Fctk<br><daN/cmq> | Fcd<br><daN/cmq> | Fctd<br><daN/cmq> | Tp | Fyk<br><daN/cmq> | Fyd<br><daN/cmq> |
|------|----------------|------------|-----|------------------|-------------------|------------------|-------------------|----|------------------|------------------|
|------|----------------|------------|-----|------------------|-------------------|------------------|-------------------|----|------------------|------------------|



|       |       |      |        |        |       |        |       |       |         |         |
|-------|-------|------|--------|--------|-------|--------|-------|-------|---------|---------|
| Oriz. | 30.00 | 4.30 | C32/40 | 332.00 | 21.69 | 188.13 | 14.46 | B450C | 4500.00 | 3913.04 |
|-------|-------|------|--------|--------|-------|--------|-------|-------|---------|---------|

Verifiche su sezioni orizzontali  
Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC | Zona  | Zv   | Xi   | Xf   | N        | My     | Nu          | MRdy     | Sic.   |
|----|-------|------|------|------|----------|--------|-------------|----------|--------|
|    |       | <m>  | <m>  | <m>  | <daN>    | <daNm> | <daN>       | <daNm>   |        |
| 1  | Diff. | 0.00 | 0.00 | 8.00 | -8006.33 | 768.95 | -8006.33    | 51599.40 | 67.104 |
| 1  | Diff. | 0.30 | 0.00 | 8.00 | -5407.74 | 294.57 | -5407.74    | 51300.10 | >100   |
| 1  | Diff. | 0.60 | 0.00 | 8.00 | -3067.74 | 3.75   | -4886950.00 | 51031.10 | >100   |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv   | Xi   | Xf   | N        | My     | σc        | σt        |
|----|-------|-------|------|------|------|----------|--------|-----------|-----------|
|    |       |       | <m>  | <m>  | <m>  | <daN>    | <daNm> | <daN/cmq> | <daN/cmq> |
| 2  | SLE R | Diff. | 0.00 | 0.00 | 8.00 | -5764.85 | 541.08 | 0.73      | 8.44      |
| 4  | SLE Q | Diff. | 0.00 | 0.00 | 8.00 | -5764.85 | 541.08 | 0.73      | 8.44      |
| 2  | SLE R | Diff. | 0.30 | 0.00 | 8.00 | -3826.11 | 203.72 | 0.31      | 3.92      |
| 4  | SLE Q | Diff. | 0.30 | 0.00 | 8.00 | -3826.11 | 203.72 | 0.31      | 3.92      |
| 2  | SLE R | Diff. | 0.60 | 0.00 | 8.00 | -2026.11 | 2.43   | 0.08      | 1.22      |
| 4  | SLE Q | Diff. | 0.60 | 0.00 | 8.00 | -2026.11 | 2.43   | 0.08      | 1.22      |

Parete n. 11

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | Tp    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
|       | <cm>   | <cm> |        | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| Oriz. | 30.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali  
Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC | Zona  | Zv   | Xi   | Xf   | N        | My      | Nu       | MRdy      | Sic. |
|----|-------|------|------|------|----------|---------|----------|-----------|------|
|    |       | <m>  | <m>  | <m>  | <daN>    | <daNm>  | <daN>    | <daNm>    |      |
| 1  | Diff. | 0.00 | 0.00 | 5.00 | -4306.08 | -178.63 | -4306.08 | -32928.40 | >100 |
| 1  | Diff. | 0.30 | 0.00 | 5.00 | -1784.31 | -31.31  | -1784.31 | -32639.10 | >100 |
| 1  | Diff. | 0.60 | 0.00 | 5.00 | -321.81  | 5.47    | -321.81  | 32471.30  | >100 |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv   | Xi   | Xf   | N        | My      | σc        | σt        |
|----|-------|-------|------|------|------|----------|---------|-----------|-----------|
|    |       |       | <m>  | <m>  | <m>  | <daN>    | <daNm>  | <daN/cmq> | <daN/cmq> |
| 2  | SLE R | Diff. | 0.00 | 0.00 | 5.00 | -3174.87 | -107.53 | 0.33      | 4.40      |
| 4  | SLE Q | Diff. | 0.00 | 0.00 | 5.00 | -3174.87 | -107.53 | 0.33      | 4.40      |
| 2  | SLE R | Diff. | 0.30 | 0.00 | 5.00 | -1340.55 | -17.31  | 0.11      | 1.49      |
| 4  | SLE Q | Diff. | 0.30 | 0.00 | 5.00 | -1340.55 | -17.31  | 0.11      | 1.49      |
| 2  | SLE R | Diff. | 0.60 | 0.00 | 5.00 | -215.55  | 3.62    | 0.02      | 0.25      |
| 4  | SLE Q | Diff. | 0.60 | 0.00 | 5.00 | -215.55  | 3.62    | 0.02      | 0.25      |

Parete n. 12

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | Tp    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
|       | <cm>   | <cm> |        | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| Oriz. | 30.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali  
Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC | Zona  | Zv   | Xi   | Xf   | N        | My     | Nu          | MRdy     | Sic.   |
|----|-------|------|------|------|----------|--------|-------------|----------|--------|
|    |       | <m>  | <m>  | <m>  | <daN>    | <daNm> | <daN>       | <daNm>   |        |
| 1  | Diff. | 0.00 | 0.00 | 8.00 | -8006.33 | 768.95 | -8006.33    | 51599.70 | 67.104 |
| 1  | Diff. | 0.30 | 0.00 | 8.00 | -5407.74 | 294.57 | -5407.74    | 51300.50 | >100   |
| 1  | Diff. | 0.60 | 0.00 | 8.00 | -3067.74 | 3.75   | -4886950.00 | 51031.10 | >100   |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv   | Xi   | Xf   | N        | My     | σc        | σt        |
|----|-------|-------|------|------|------|----------|--------|-----------|-----------|
|    |       |       | <m>  | <m>  | <m>  | <daN>    | <daNm> | <daN/cmq> | <daN/cmq> |
| 2  | SLE R | Diff. | 0.00 | 0.00 | 8.00 | -5764.85 | 541.08 | 0.73      | 8.44      |
| 4  | SLE Q | Diff. | 0.00 | 0.00 | 8.00 | -5764.85 | 541.08 | 0.73      | 8.44      |
| 2  | SLE R | Diff. | 0.30 | 0.00 | 8.00 | -3826.11 | 203.72 | 0.31      | 3.92      |
| 4  | SLE Q | Diff. | 0.30 | 0.00 | 8.00 | -3826.11 | 203.72 | 0.31      | 3.92      |
| 2  | SLE R | Diff. | 0.60 | 0.00 | 8.00 | -2026.11 | 2.43   | 0.08      | 1.22      |
| 4  | SLE Q | Diff. | 0.60 | 0.00 | 8.00 | -2026.11 | 2.43   | 0.08      | 1.22      |

Parete n. 13

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | Tp    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
|       | <cm>   | <cm> |        | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| Oriz. | 60.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

Verifiche su sezioni orizzontali  
Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC | Zona  | Zv   | Xi   | Xf   | N         | My      | Nu          | MRdy      | Sic. |
|----|-------|------|------|------|-----------|---------|-------------|-----------|------|
|    |       | <m>  | <m>  | <m>  | <daN>     | <daNm>  | <daN>       | <daNm>    |      |
| 1  | Diff. | 0.00 | 0.00 | 5.00 | -48017.60 | -645.48 | -5882980.00 | -80975.30 | >100 |
| 1  | Diff. | 0.30 | 0.00 | 5.00 | -45092.60 | -154.38 | -5882980.00 | -80203.20 | >100 |
| 1  | Diff. | 0.60 | 0.00 | 5.00 | -43485.40 | -0.20   | -5882980.00 | -79779.80 | >100 |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv   | Xi   | Xf   | N         | My      | σc        | σt        |
|----|-------|-------|------|------|------|-----------|---------|-----------|-----------|
|    |       |       | <m>  | <m>  | <m>  | <daN>     | <daNm>  | <daN/cmq> | <daN/cmq> |
| 2  | SLE R | Diff. | 0.00 | 0.00 | 5.00 | -32660.30 | -423.11 | 1.19      | 17.54     |
| 4  | SLE Q | Diff. | 0.00 | 0.00 | 5.00 | -32660.30 | -423.11 | 1.19      | 17.54     |
| 2  | SLE R | Diff. | 0.30 | 0.00 | 5.00 | -30410.30 | -100.88 | 1.02      | 15.16     |
| 4  | SLE Q | Diff. | 0.30 | 0.00 | 5.00 | -30410.30 | -100.88 | 1.02      | 15.16     |
| 2  | SLE R | Diff. | 0.60 | 0.00 | 5.00 | -29008.30 | -0.16   | 0.94      | 14.07     |
| 4  | SLE Q | Diff. | 0.60 | 0.00 | 5.00 | -29008.30 | -0.16   | 0.94      | 14.07     |

Parete n. 14

Caratteristiche delle sezioni e dei materiali utilizzati

| Sez.  | Spess. | Cf   | Cls    | Fck       | Fctk      | Fcd       | Fctd      | Tp    | Fyk       | Fyd       |
|-------|--------|------|--------|-----------|-----------|-----------|-----------|-------|-----------|-----------|
|       | <cm>   | <cm> |        | <daN/cmq> | <daN/cmq> | <daN/cmq> | <daN/cmq> |       | <daN/cmq> | <daN/cmq> |
| Oriz. | 60.00  | 4.30 | C32/40 | 332.00    | 21.69     | 188.13    | 14.46     | B450C | 4500.00   | 3913.04   |

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Verifiche su sezioni orizzontali

Stato limite ultimo - Verifiche a flessione/pressoflessione

| CC | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | Nu<br><daN> | MRdy<br><daNm> | Sic. |
|----|-------|-----------|-----------|-----------|------------|--------------|-------------|----------------|------|
| 1  | Diff. | 0.00      | 0.00      | 5.00      | -48017.60  | 645.48       | -5882980.00 | 80976.00       | >100 |
| 1  | Diff. | 0.30      | 0.00      | 5.00      | -46410.40  | 172.95       | -5882980.00 | 80551.00       | >100 |
| 1  | Diff. | 0.60      | 0.00      | 5.00      | -43485.40  | 0.20         | -5882980.00 | 79779.50       | >100 |

Stato limite d'esercizio - Verifiche tensionali

| CC | TCC   | Zona  | Zv<br><m> | Xi<br><m> | Xf<br><m> | N<br><daN> | My<br><daNm> | $\sigma_e$<br><daN/cm <sup>2</sup> > | $\sigma_f$<br><daN/cm <sup>2</sup> > |
|----|-------|-------|-----------|-----------|-----------|------------|--------------|--------------------------------------|--------------------------------------|
| 2  | SLE R | Diff. | 0.00      | 0.00      | 5.00      | -32660.30  | 423.11       | 1.19                                 | 17.54                                |
| 4  | SLE Q | Diff. | 0.00      | 0.00      | 5.00      | -32660.30  | 423.11       | 1.19                                 | 17.54                                |
| 2  | SLE R | Diff. | 0.30      | 0.00      | 5.00      | -31258.30  | 113.11       | 1.05                                 | 15.62                                |
| 4  | SLE Q | Diff. | 0.30      | 0.00      | 5.00      | -31258.30  | 113.11       | 1.05                                 | 15.62                                |
| 2  | SLE R | Diff. | 0.60      | 0.00      | 5.00      | -29008.30  | 0.16         | 0.94                                 | 14.08                                |
| 4  | SLE Q | Diff. | 0.60      | 0.00      | 5.00      | -29008.30  | 0.16         | 0.94                                 | 14.08                                |

## 11.0 RISULTATI STRUTTURE FONDAZIONE TRASFORMATORE MT/BT

### 11.1 Diagrammi tassi di sfruttamento

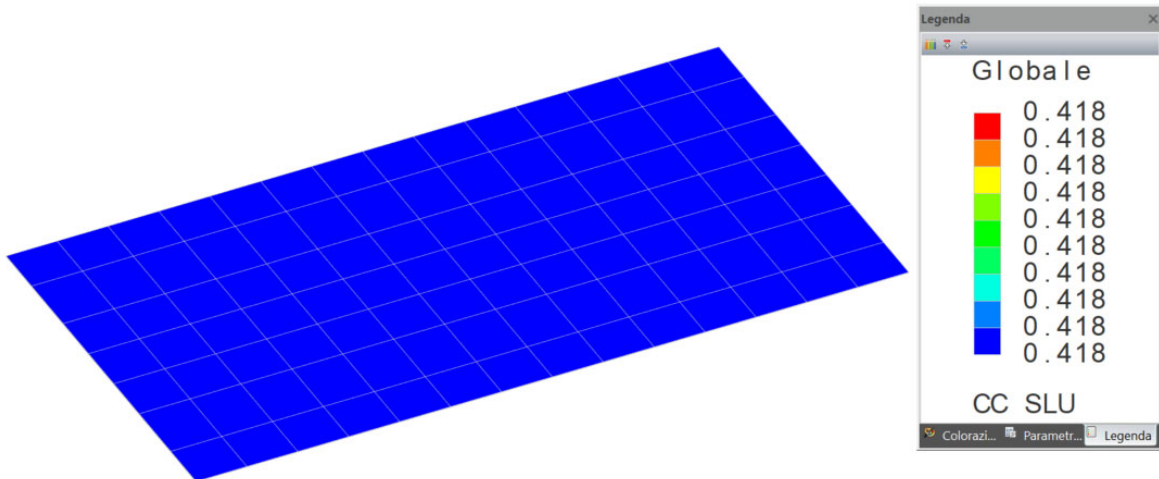
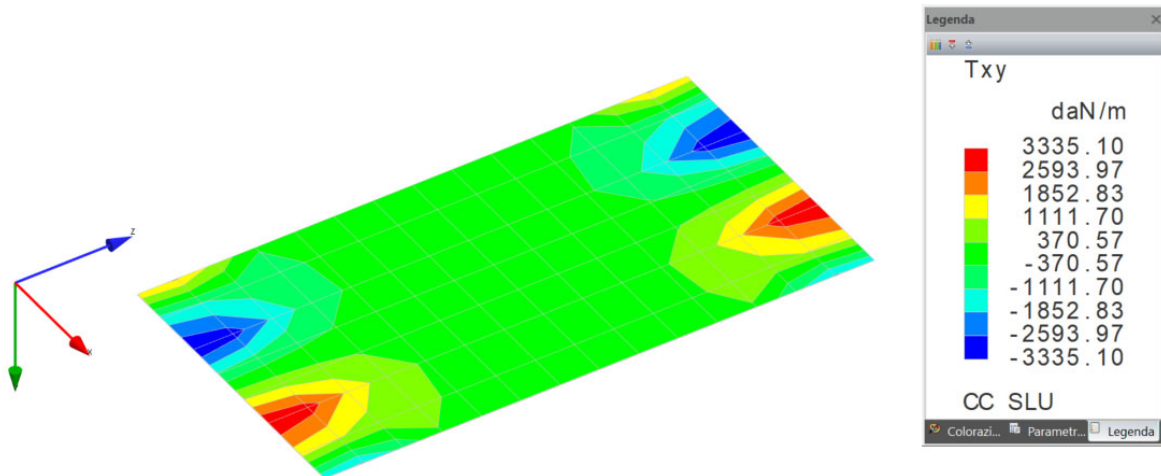


Diagramma tassi di sfruttamento resistenza combo SLU con valore massimo pari a 0,418

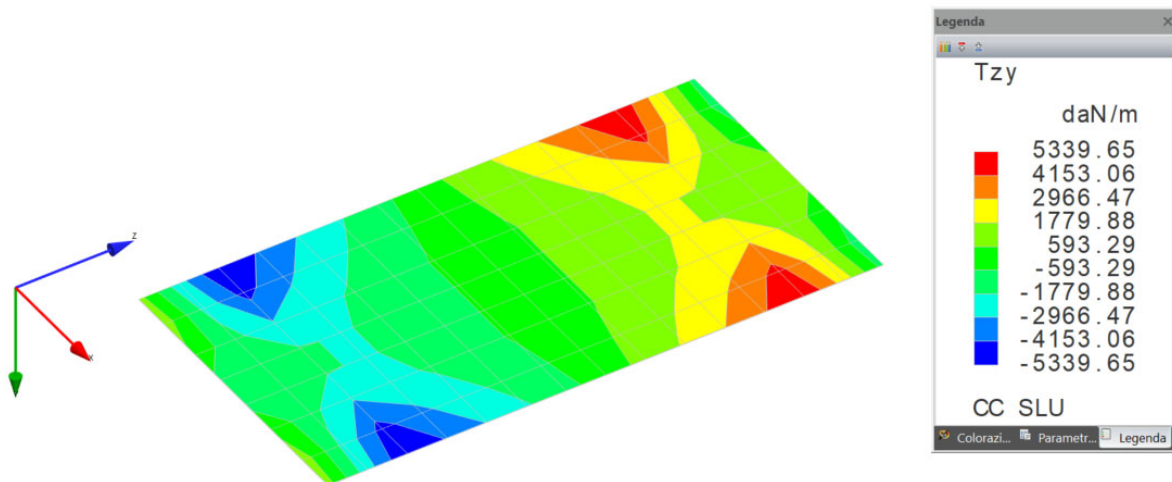
**Figure 52: Tassi di sfruttamento SLU (Stato limite ultimo)**



## 11.2 Sollecitazioni

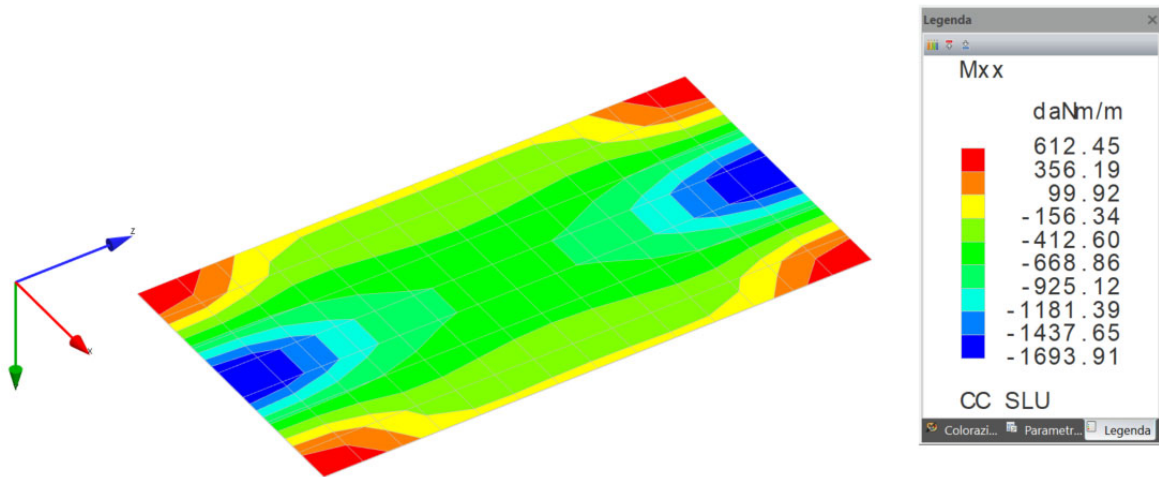


Involuppo sforzo di taglio in direzione X su faccia con normale Y SLU Tmax = 3335,10 daN/m

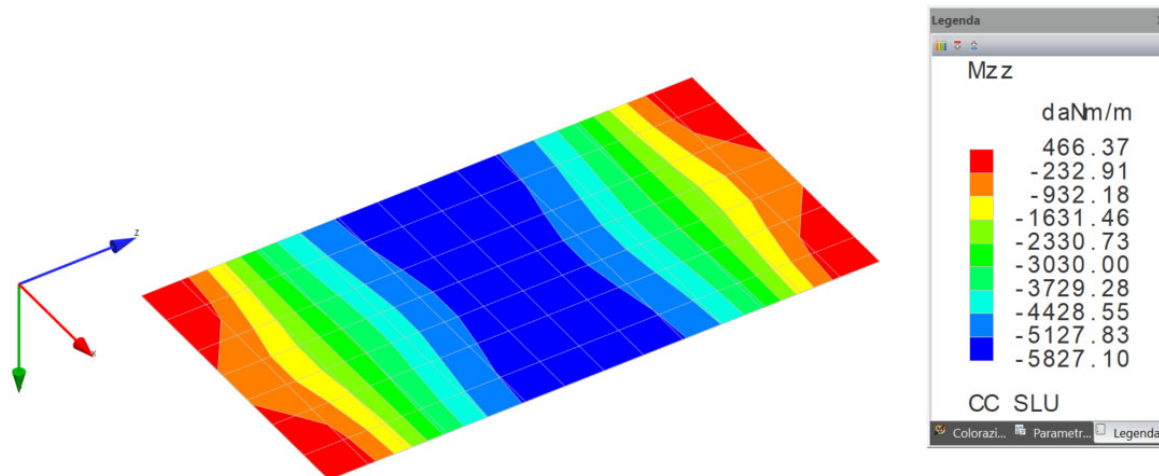


Involuppo sforzo di taglio in direzione Z su faccia con normale Y SLU Tmax = 5339,65 daN/m

**Figure 53: Taglio**



Involuppo momento che genera tensioni in direzioni X su facce con normale X SLU  $M_{max} = 1693,91 \text{ daN}\times\text{m/m}$



Involuppo momento che genera tensioni in direzioni Z su facce con normale Z SLU  $M_{max} = 5827,10 \text{ daN}\times\text{m/m}$

**Figure 54: Momento Flettente**

## 11.3 Tabulati di calcolo

Si riportano i tabulati di calcolo elaborati come output dal programma di calcolo.

### Risultati del calcolo

#### Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:  
 Modest ver. 8.28, licenza n. 7279, prodotto da Tecnisoft s.a.s. - Prato  
 La struttura è stata calcolata utilizzando come solutore agli elementi finiti:  
 Xfinest ver. 9.3.3, licenza n. 3451, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18

Tipo di calcolo: statico

Vincoli esterni: Considera sempre vincoli assegnati in modellazione

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

#### Generazione combinazioni

- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

#### Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente

#### Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

#### Dati struttura

- Edificio esistente: No
- Tipo di opera: Opera ordinaria
- Vita nominale  $V_N$ : 50.00
- Classe d'uso: Classe II
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

#### Ambienti di carico

##### Simbologia

N = Numero

Comm. = Commento

1 = G1 - permanenti strutturali

2 = G2 - permanenti non strutturali

3 = Q - variabili cat. E

F = azioni orizzontali convenzionali

SLU = Stato limite ultimo

SLR = Stato limite per combinazioni rare

SLF = Stato limite per combinazioni frequenti

SLQ/D = Stato limite per combinazioni quasi permanenti o di danno

S = Sì

N = No

| N | Comm.           | 1 | 2 | 3 | SLU | SLR | SLF | SLQ |
|---|-----------------|---|---|---|-----|-----|-----|-----|
| 1 | Calcolo statico | S | S | S | S   | S   | S   | S   |

#### Elenco combinazioni di carico simboliche

##### Simbologia

CC = Numero della combinazione delle condizioni di carico elementari

Comm. = Commento

TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| CC | Comm.          | TCC   | 1              | 2              | 3              |
|----|----------------|-------|----------------|----------------|----------------|
| 1  | Amb. 1 (SLU)   | SLU   | $\gamma_{max}$ | $\gamma_{max}$ | $\gamma_{max}$ |
| 2  | Amb. 1 (SLE R) | SLE R | 1              | 1              | 1              |
| 3  | Amb. 1 (SLE F) | SLE F | 1              | 1              | $\psi_1$       |
| 4  | Amb. 1 (SLE Q) | SLE Q | 1              | 1              | $\psi_2$       |

Genera le combinazioni con un solo carico di tipo variabile come di base: No

Considera sollecitazioni dinamiche con segno dei modi principali: No

#### Combinazioni delle CCE

##### Simbologia

An. = Tipo di analisi

L = Lineare

NL = Non lineare

Bk = Buckling

S = Sì



N = No  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Comm. = Commento  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| CC | Comm.          | TCC   | An. | Bk | 1    | 2    | 3    |
|----|----------------|-------|-----|----|------|------|------|
| 1  | Amb. 1 (SLU)   | SLU   | L   | N  | 1.30 | 1.50 | 1.50 |
| 2  | Amb. 1 (SLE R) | SLE R | L   | N  | 1.00 | 1.00 | 1.00 |
| 3  | Amb. 1 (SLE F) | SLE F | L   | N  | 1.00 | 1.00 | 0.90 |
| 4  | Amb. 1 (SLE Q) | SLE Q | L   | N  | 1.00 | 1.00 | 0.80 |

Tensioni sul terreno

Simbologia

$\sigma_t$  = Tensione sul terreno  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Nodo = Numero del nodo  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

| Nodo | CC   | TCC | $\sigma_t$ | Nodo | CC   | TCC  | $\sigma_t$ | Nodo | CC  | TCC  | $\sigma_t$ | Nodo | CC | TCC | $\sigma_t$ | Nodo | CC   | TCC | $\sigma_t$ |      |      |
|------|------|-----|------------|------|------|------|------------|------|-----|------|------------|------|----|-----|------------|------|------|-----|------------|------|------|
|      |      |     | <daN/cmq>  |      |      |      | <daN/cmq>  |      |     |      | <daN/cmq>  |      |    |     | <daN/cmq>  |      |      |     | <daN/cmq>  |      |      |
| -248 | Max  | 1   | SLU        | 0.38 | -248 | Min. | 4          | SLE  | Q   | 0.26 | -247       | Max  | 1  | SLU | 0.38       | -246 | Max  | 1   | SLU        | 0.38 |      |
| -246 | Min. | 4   | SLE        | Q    | 0.26 | -245 | Max        | 1    | SLU | 0.38 | -244       | Max  | 1  | SLU | 0.38       | -244 | Min. | 4   | SLE        | Q    | 0.26 |
| -243 | Max  | 1   | SLU        | 0.38 | -243 | Min. | 4          | SLE  | Q   | 0.26 | -242       | Max  | 1  | SLU | 0.38       | -242 | Min. | 4   | SLE        | Q    | 0.26 |
| -241 | Min. | 4   | SLE        | Q    | 0.26 | -240 | Max        | 1    | SLU | 0.37 | -240       | Min. | 4  | SLE | Q          | 0.26 | -239 | Max | 1          | SLU  | 0.37 |
| -238 | Max  | 1   | SLU        | 0.37 | -238 | Min. | 4          | SLE  | Q   | 0.26 | -237       | Max  | 1  | SLU | 0.37       | -237 | Min. | 4   | SLE        | Q    | 0.26 |
| -236 | Min. | 4   | SLE        | Q    | 0.26 | -235 | Max        | 1    | SLU | 0.37 | -235       | Min. | 4  | SLE | Q          | 0.26 | -234 | Max | 1          | SLU  | 0.37 |
| -233 | Max  | 1   | SLU        | 0.37 | -233 | Min. | 4          | SLE  | Q   | 0.26 | -232       | Max  | 1  | SLU | 0.36       | -232 | Min. | 4   | SLE        | Q    | 0.25 |
| -231 | Min. | 4   | SLE        | Q    | 0.25 | -230 | Max        | 1    | SLU | 0.36 | -230       | Min. | 4  | SLE | Q          | 0.25 | -229 | Max | 1          | SLU  | 0.36 |
| -228 | Max  | 1   | SLU        | 0.36 | -228 | Min. | 4          | SLE  | Q   | 0.25 | -227       | Max  | 1  | SLU | 0.36       | -227 | Min. | 4   | SLE        | Q    | 0.25 |
| -226 | Min. | 4   | SLE        | Q    | 0.25 | -225 | Max        | 1    | SLU | 0.36 | -225       | Min. | 4  | SLE | Q          | 0.25 | -224 | Max | 1          | SLU  | 0.35 |
| -223 | Max  | 1   | SLU        | 0.35 | -223 | Min. | 4          | SLE  | Q   | 0.24 | -222       | Max  | 1  | SLU | 0.35       | -222 | Min. | 4   | SLE        | Q    | 0.24 |
| -221 | Min. | 4   | SLE        | Q    | 0.24 | -220 | Max        | 1    | SLU | 0.35 | -220       | Min. | 4  | SLE | Q          | 0.24 | -219 | Max | 1          | SLU  | 0.35 |
| -218 | Max  | 1   | SLU        | 0.35 | -218 | Min. | 4          | SLE  | Q   | 0.24 | -217       | Max  | 1  | SLU | 0.35       | -217 | Min. | 4   | SLE        | Q    | 0.25 |
| -216 | Min. | 4   | SLE        | Q    | 0.24 | -215 | Max        | 1    | SLU | 0.34 | -215       | Min. | 4  | SLE | Q          | 0.24 | -214 | Max | 1          | SLU  | 0.34 |
| -213 | Max  | 1   | SLU        | 0.34 | -213 | Min. | 4          | SLE  | Q   | 0.24 | -212       | Max  | 1  | SLU | 0.34       | -212 | Min. | 4   | SLE        | Q    | 0.24 |
| -211 | Min. | 4   | SLE        | Q    | 0.24 | -210 | Max        | 1    | SLU | 0.34 | -210       | Min. | 4  | SLE | Q          | 0.24 | -209 | Max | 1          | SLU  | 0.34 |
| -208 | Max  | 1   | SLU        | 0.34 | -208 | Min. | 4          | SLE  | Q   | 0.24 | -207       | Max  | 1  | SLU | 0.34       | -207 | Min. | 4   | SLE        | Q    | 0.24 |
| -206 | Min. | 4   | SLE        | Q    | 0.24 | -205 | Max        | 1    | SLU | 0.34 | -205       | Min. | 4  | SLE | Q          | 0.24 | -204 | Max | 1          | SLU  | 0.34 |
| -203 | Max  | 1   | SLU        | 0.34 | -203 | Min. | 4          | SLE  | Q   | 0.24 | -202       | Max  | 1  | SLU | 0.34       | -202 | Min. | 4   | SLE        | Q    | 0.24 |
| -201 | Min. | 4   | SLE        | Q    | 0.24 | -192 | Max        | 1    | SLU | 0.34 | -192       | Min. | 4  | SLE | Q          | 0.23 | -191 | Max | 1          | SLU  | 0.34 |
| -190 | Max  | 1   | SLU        | 0.34 | -190 | Min. | 4          | SLE  | Q   | 0.23 | -189       | Max  | 1  | SLU | 0.34       | -189 | Min. | 4   | SLE        | Q    | 0.23 |
| -188 | Min. | 4   | SLE        | Q    | 0.23 | -187 | Max        | 1    | SLU | 0.34 | -187       | Min. | 4  | SLE | Q          | 0.23 | -186 | Max | 1          | SLU  | 0.34 |
| -185 | Max  | 1   | SLU        | 0.34 | -185 | Min. | 4          | SLE  | Q   | 0.23 | -176       | Max  | 1  | SLU | 0.33       | -176 | Min. | 4   | SLE        | Q    | 0.23 |
| -175 | Min. | 4   | SLE        | Q    | 0.23 | -174 | Max        | 1    | SLU | 0.33 | -174       | Min. | 4  | SLE | Q          | 0.23 | -173 | Max | 1          | SLU  | 0.33 |
| -172 | Max  | 1   | SLU        | 0.33 | -172 | Min. | 4          | SLE  | Q   | 0.23 | -171       | Max  | 1  | SLU | 0.33       | -171 | Min. | 4   | SLE        | Q    | 0.23 |
| -170 | Min. | 4   | SLE        | Q    | 0.23 | -169 | Max        | 1    | SLU | 0.33 | -169       | Min. | 4  | SLE | Q          | 0.23 | -152 | Max | 1          | SLU  | 0.34 |
| -151 | Max  | 1   | SLU        | 0.34 | -151 | Min. | 4          | SLE  | Q   | 0.23 | -150       | Max  | 1  | SLU | 0.34       | -150 | Min. | 4   | SLE        | Q    | 0.23 |
| -149 | Min. | 4   | SLE        | Q    | 0.23 | -148 | Max        | 1    | SLU | 0.34 | -148       | Min. | 4  | SLE | Q          | 0.23 | -147 | Max | 1          | SLU  | 0.34 |
| -146 | Max  | 1   | SLU        | 0.34 | -146 | Min. | 4          | SLE  | Q   | 0.23 | -145       | Max  | 1  | SLU | 0.34       | -145 | Min. | 4   | SLE        | Q    | 0.23 |
| -128 | Min. | 4   | SLE        | Q    | 0.24 | -127 | Max        | 1    | SLU | 0.34 | -127       | Min. | 4  | SLE | Q          | 0.24 | -126 | Max | 1          | SLU  | 0.34 |
| -125 | Max  | 1   | SLU        | 0.34 | -125 | Min. | 4          | SLE  | Q   | 0.24 | -124       | Max  | 1  | SLU | 0.34       | -124 | Min. | 4   | SLE        | Q    | 0.24 |
| -123 | Min. | 4   | SLE        | Q    | 0.24 | -122 | Max        | 1    | SLU | 0.34 | -122       | Min. | 4  | SLE | Q          | 0.24 | -121 | Max | 1          | SLU  | 0.34 |
| -104 | Max  | 1   | SLU        | 0.34 | -104 | Min. | 4          | SLE  | Q   | 0.24 | -103       | Max  | 1  | SLU | 0.34       | -103 | Min. | 4   | SLE        | Q    | 0.24 |
| -102 | Min. | 4   | SLE        | Q    | 0.24 | -101 | Max        | 1    | SLU | 0.34 | -101       | Min. | 4  | SLE | Q          | 0.24 | -100 | Max | 1          | SLU  | 0.34 |
| -99  | Max  | 1   | SLU        | 0.34 | -99  | Min. | 4          | SLE  | Q   | 0.24 | -98        | Max  | 1  | SLU | 0.34       | -98  | Min. | 4   | SLE        | Q    | 0.24 |
| -97  | Min. | 4   | SLE        | Q    | 0.24 | -80  | Max        | 1    | SLU | 0.35 | -80        | Min. | 4  | SLE | Q          | 0.25 | -79  | Max | 1          | SLU  | 0.35 |
| -78  | Max  | 1   | SLU        | 0.35 | -78  | Min. | 4          | SLE  | Q   | 0.24 | -77        | Max  | 1  | SLU | 0.35       | -77  | Min. | 4   | SLE        | Q    | 0.24 |
| -76  | Min. | 4   | SLE        | Q    | 0.24 | -75  | Max        | 1    | SLU | 0.35 | -75        | Min. | 4  | SLE | Q          | 0.24 | -74  | Max | 1          | SLU  | 0.35 |
| -73  | Max  | 1   | SLU        | 0.35 | -73  | Min. | 4          | SLE  | Q   | 0.25 | -56        | Max  | 1  | SLU | 0.36       | -56  | Min. | 4   | SLE        | Q    | 0.25 |
| -55  | Min. | 4   | SLE        | Q    | 0.25 | -54  | Max        | 1    | SLU | 0.36 | -54        | Min. | 4  | SLE | Q          | 0.25 | -53  | Max | 1          | SLU  | 0.36 |
| -52  | Max  | 1   | SLU        | 0.36 | -52  | Min. | 4          | SLE  | Q   | 0.25 | -51        | Max  | 1  | SLU | 0.36       | -51  | Min. | 4   | SLE        | Q    | 0.25 |
| -50  | Min. | 4   | SLE        | Q    | 0.25 | -49  | Max        | 1    | SLU | 0.36 | -49        | Min. | 4  | SLE | Q          | 0.25 | -32  | Max | 1          | SLU  | 0.37 |
| -31  | Max  | 1   | SLU        | 0.37 | -31  | Min. | 4          | SLE  | Q   | 0.26 | -30        | Max  | 1  | SLU | 0.37       | -30  | Min. | 4   | SLE        | Q    | 0.26 |
| -29  | Min. | 4   | SLE        | Q    | 0.26 | -28  | Max        | 1    | SLU | 0.37 | -28        | Min. | 4  | SLE | Q          | 0.26 | -27  | Max | 1          | SLU  | 0.37 |
| -26  | Max  | 1   | SLU        | 0.37 | -26  | Min. | 4          | SLE  | Q   | 0.26 | -25        | Max  | 1  | SLU | 0.37       | -25  | Min. | 4   | SLE        | Q    | 0.26 |
| -8   | Min. | 4   | SLE        | Q    | 0.26 | -7   | Max        | 1    | SLU | 0.38 | -7         | Min. | 4  | SLE | Q          | 0.26 | -6   | Max | 1          | SLU  | 0.38 |
| -5   | Max  | 1   | SLU        | 0.38 | -5   | Min. | 4          | SLE  | Q   | 0.26 | -4         | Max  | 1  | SLU | 0.38       | -4   | Min. | 4   | SLE        | Q    | 0.26 |
| -3   | Min. | 4   | SLE        | Q    | 0.26 | -2   | Max        | 1    | SLU | 0.38 | -2         | Min. | 4  | SLE | Q          | 0.26 | -1   | Max | 1          | SLU  | 0.38 |

Sollecitazioni elementi bidimensionali

Simbologia

$\sigma_{xx}$  = Tensione normale sulle facce perp. all'asse X  
 $\sigma_{zz}$  = Tensione normale sulle facce perp. all'asse Z  
 $\tau_{xy}$  = Tensione in dir. Y sulle facce perp. all'asse X  
 $\tau_{xz}$  = Tensione in dir. Z sulle facce perp. all'asse X  
 $\tau_{zy}$  = Tensione in dir. Y sulle facce perp. all'asse Z  
 Bid. = Numero del muro/elemento bidimensionale  
 CC = Numero della combinazione delle condizioni di carico elementari  
 Mxx = Momento che provoca variazione di tensione sulle facce perp. all'asse X  
 Mxz = Momento che provoca variazione di tensione tangenziali sulle facce perp. all'asse X  
 Mzz = Momento che provoca variazione di tensione sulle facce perp. all'asse Z  
 Nodo = Numero del nodo  
 TCC = Tipo di combinazione di carico  
 SLU = Stato limite ultimo  
 SLE R = Stato limite d'esercizio, combinazione rara  
 SLE F = Stato limite d'esercizio, combinazione frequente  
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente

Bid. 8

|                        | CC | TCC | Nodo | Min. | CC | TCC | Nodo | Max | CC                     | TCC | Nodo | Min. | CC | TCC | Nodo | Max  |   |
|------------------------|----|-----|------|------|----|-----|------|-----|------------------------|-----|------|------|----|-----|------|------|---|
| $\sigma_{xx}$ <daN/mq> | 1  | SLU | -147 | 0    | 1  | SLU | -213 | 0   | $\sigma_{zz}$ <daN/mq> | 1   | SLU  | -127 | 0  | 1   | SLU  | -223 | 0 |



|                   |   |     |      |        |   |     |      |       |                   |   |     |      |       |   |     |      |      |
|-------------------|---|-----|------|--------|---|-----|------|-------|-------------------|---|-----|------|-------|---|-----|------|------|
| $t_{xz}$ <daN/mq> | 1 | SLU | -150 | 0      | 1 | SLU | -217 | 0     | Mxx <daNm/m>      | 1 | SLU | -28  | -1869 | 1 | SLU | -25  | 612  |
| Mzz <daNm/m>      | 1 | SLU | -175 | -5827  | 1 | SLU | -25  | 466   | Mxz <daNm/m>      | 1 | SLU | -50  | -627  | 1 | SLU | -226 | 627  |
| $t_{xy}$ <daN/mq> | 1 | SLU | -26  | -11989 | 1 | SLU | -234 | 11989 | $t_{xy}$ <daN/mq> | 1 | SLU | -235 | -9196 | 1 | SLU | -238 | 9196 |

Verifiche e armature solette/platee

Simbologia

- $\Delta_{sm}$  = Distanza media tra le fessure
- $\Phi_{eq}$  = Diametro equivalente delle barre
- $\epsilon_{sm}$  = Deformazione unitaria media dell'armatura (\*1000)
- $\sigma_c$  = Tensione nel calcestruzzo
- $\sigma_r$  = Tensione nel ferro
- $\sigma_s$  = Tensione nell'acciaio nella sezione fessurata
- $A_{c\ eff}$  = Area di calcestruzzo efficace
- $A_s$  = Area complessiva dei ferri nell'area di calcestruzzo efficace
- AfE I = Area di ferro effettiva totale presente nel punto di verifica, inferiore
- AfE S = Area di ferro effettiva totale presente nel punto di verifica, superiore
- AfE St. = Area di ferro effettiva della staffatura
- CC = Numero della combinazione delle condizioni di carico elementari
- Cf inf = Copriferro inferiore
- Cf sup = Copriferro superiore
- Cls = Tipo di calcestruzzo
- DV = Direzione di verifica  
XX = Verifica per momento Mxx  
YY = Verifica per momento Myy
- Fcd = Resistenza di calcolo a compressione del calcestruzzo
- Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo
- Fctd = Resistenza di calcolo a trazione del calcestruzzo
- Fctk = Resistenza caratteristica a trazione del calcestruzzo
- Fyd = Resistenza di calcolo dell'acciaio
- Fyk = Tensione caratteristica di snervamento dell'acciaio
- $K_2$  = Coefficiente per distribuzione deformazioni
- MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y
- Mom = Momento flettente
- My = Momento flettente intorno all'asse Y
- Nodo = Numero del nodo
- Sic. = Sicurezza
- Spess. = Spessore
- TCC = Tipo di combinazione di carico  
SLU = Stato limite ultimo  
SLE R = Stato limite d'esercizio, combinazione rara  
SLE F = Stato limite d'esercizio, combinazione frequente  
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
- TP = Tipo di acciaio
- VRcd = Taglio ultimo lato calcestruzzo
- VRsd = Taglio ultimo lato armatura
- Vrdu = Taglio ultimo resistente
- Vsdu = Taglio agente nella direzione del momento ultimo
- Wk = Ampiezza caratteristica delle fessure
- X = Coordinata X del nodo
- Y = Coordinata Y del nodo
- c = Ricoprimento dell'armatura
- ctg $\theta$  = Cotangente dell'angolo di inclinazione dei puntoni di calcestruzzo
- s = Distanza massima tra le barre

Armatura platea a quota 0.00

Caratteristiche delle sezioni e dei materiali utilizzati

| Spess. <cm> | Cf sup <cm> | Cf inf <cm> | Cls    | Fck <daN/cm <sup>2</sup> > | Fctk <daN/cm <sup>2</sup> > | Fcd <daN/cm <sup>2</sup> > | Fctd <daN/cm <sup>2</sup> > | TP    | Fyk <daN/cm <sup>2</sup> > | Fyd <daN/cm <sup>2</sup> > |
|-------------|-------------|-------------|--------|----------------------------|-----------------------------|----------------------------|-----------------------------|-------|----------------------------|----------------------------|
| 50.00       | 3.50        | 3.50        | C32/40 | 332.00                     | 21.69                       | 188.13                     | 14.46                       | B450C | 4500.00                    | 3913.04                    |

Stato limite ultimo - Verifiche a flessione/pressoflessione

| Nodo | X    | Y    | DV | CC | TCC | AfE S | AfE I | My       | MRdy      | Sic.   |
|------|------|------|----|----|-----|-------|-------|----------|-----------|--------|
| <cm> | <cm> | <cm> |    |    |     | <cmq> | <cmq> | <daNm>   | <daNm>    |        |
| -1   | 0.88 | 1.00 | XX | 1  | SLU | 7.70  | 7.70  | 612.45   | 13950.30  | 22.778 |
| -4   | 2.50 | 1.00 | XX | 1  | SLU | 7.70  | 7.70  | -1693.91 | -13950.30 | 8.236  |
| -1   | 0.88 | 1.00 | YY | 1  | SLU | 7.70  | 7.70  | 466.37   | 13950.30  | 29.913 |
| -169 | 0.88 | 4.50 | YY | 1  | SLU | 7.70  | 7.70  | -5827.10 | -13950.30 | 2.394  |

Stato limite ultimo - Verifiche a taglio

| Nodo | X    | Y    | DV | CC | TCC | AfE S | AfE I | AfE St. | Vsdu    | ctg $\theta$ | VRcd  | VRsd  | Vrdu     | Sic.  |
|------|------|------|----|----|-----|-------|-------|---------|---------|--------------|-------|-------|----------|-------|
| <cm> | <cm> | <cm> |    |    |     | <cmq> | <cmq> | <cmq/m> | <daN>   |              | <daN> | <daN> | <daN>    |       |
| -3   | 2.00 | 1.00 | XX | 1  | SLU | 7.70  | 7.70  |         | 3335.10 |              |       |       | 19980.80 | 5.991 |
| -49  | 0.88 | 2.00 | YY | 1  | SLU | 7.70  | 7.70  |         | 5339.65 |              |       |       | 19980.80 | 3.742 |

Stato limite d'esercizio - Verifiche tensionali

| Nodo | X    | Y    | DV | CC | TCC   | AfE S | AfE I | Mom      | $\sigma_c$             | $\sigma_r$             |
|------|------|------|----|----|-------|-------|-------|----------|------------------------|------------------------|
| <cm> | <cm> | <cm> |    |    |       | <cmq> | <cmq> | <daNm>   | <daN/cm <sup>2</sup> > | <daN/cm <sup>2</sup> > |
| -1   | 0.88 | 1.00 | XX | 2  | SLE R | 7.70  | 7.70  | 408.30   | 1.87                   | 121.88                 |
| -1   | 0.88 | 1.00 | XX | 4  | SLE Q | 7.70  | 7.70  | 408.30   | 1.87                   | 121.88                 |
| -4   | 2.50 | 1.00 | XX | 2  | SLE R | 7.70  | 7.70  | -1129.27 | 5.16                   | 337.10                 |
| -4   | 2.50 | 1.00 | XX | 4  | SLE Q | 7.70  | 7.70  | -1129.27 | 5.16                   | 337.10                 |
| -1   | 0.88 | 1.00 | YY | 2  | SLE R | 7.70  | 7.70  | 310.91   | 1.42                   | 92.81                  |
| -1   | 0.88 | 1.00 | YY | 4  | SLE Q | 7.70  | 7.70  | 310.91   | 1.42                   | 92.81                  |
| -169 | 0.88 | 4.50 | YY | 2  | SLE R | 7.70  | 7.70  | -3884.74 | 17.75                  | 1159.64                |
| -169 | 0.88 | 4.50 | YY | 4  | SLE Q | 7.70  | 7.70  | -3884.74 | 17.75                  | 1159.64                |

Stato limite d'esercizio - Verifiche a fessurazione

| Nodo | X    | Y    | DV | CC | TCC   | c     | s      | $K_2$ | $\Phi_{eq}$ | $\Delta_{sm}$ | $A_s$              | $A_{c\ eff}$       | $\sigma_s$             | $\epsilon_{sm}$ | Wk   |
|------|------|------|----|----|-------|-------|--------|-------|-------------|---------------|--------------------|--------------------|------------------------|-----------------|------|
| <cm> | <cm> | <cm> |    |    |       | <mm>  | <mm>   |       |             | <mm>          | <cm <sup>2</sup> > | <cm <sup>2</sup> > | <daN/cm <sup>2</sup> > |                 | <mm> |
| -1   | 0.88 | 1.00 | XX | 4  | SLE Q | 28.00 | 200.00 | 0.50  | 14.00       | 309.89        | 9.24               | 875.00             | 121.88                 | 0.04            | 0.02 |
| -1   | 0.88 | 1.00 | XX | 3  | SLE F | 28.00 | 200.00 | 0.50  | 14.00       | 309.89        | 9.24               | 875.00             | 121.88                 | 0.04            | 0.02 |
| -4   | 2.50 | 1.00 | XX | 4  | SLE Q | 28.00 | 200.00 | 0.50  | 14.00       | 309.89        | 9.24               | 875.00             | 337.10                 | 0.10            | 0.05 |
| -4   | 2.50 | 1.00 | XX | 3  | SLE F | 28.00 | 200.00 | 0.50  | 14.00       | 309.89        | 9.24               | 875.00             | 337.10                 | 0.10            | 0.05 |
| -1   | 0.88 | 1.00 | YY | 4  | SLE Q | 28.00 | 200.00 | 0.50  | 14.00       | 309.89        | 9.24               | 875.00             | 92.81                  | 0.03            | 0.01 |
| -1   | 0.88 | 1.00 | YY | 3  | SLE F | 28.00 | 200.00 | 0.50  | 14.00       | 309.89        | 9.24               | 875.00             | 92.81                  | 0.03            | 0.01 |
| -169 | 0.88 | 4.50 | YY | 4  | SLE Q | 28.00 | 200.00 | 0.50  | 14.00       | 309.89        | 9.24               | 875.00             | 1159.64                | 0.34            | 0.18 |
| -169 | 0.88 | 4.50 | YY | 3  | SLE F | 28.00 | 200.00 | 0.50  | 14.00       | 309.89        | 9.24               | 875.00             | 1159.64                | 0.34            | 0.18 |

## 12.0 VALUTAZIONE DEI RISULTATI E GIUDIZIONE MOTIVATO SULLA LORO ACCETTABILITA'

Il programma di calcolo utilizzato Modest è idoneo a riprodurre nel modello matematico il comportamento della struttura e gli elementi finiti disponibili e utilizzati sono rappresentativi della realtà costruttiva. Le funzioni di controllo disponibili, innanzitutto quelle grafiche, consentono di verificare la riproduzione della realtà costruttiva ed accertare la corrispondenza del modello con la geometria strutturale e con le condizioni di carico ipotizzate. In ogni caso sono stati effettuati alcuni controlli dimensionali con gli strumenti software a disposizione dell'utente. Tutte le proprietà di rilevanza strutturale (materiali, sezioni, carichi, sconnessioni, etc.) sono state controllate attraverso le funzioni di indagine specificatamente previste.

Sono state sfruttate le funzioni di autodiagnostica presenti nel software che hanno accertato che non sussistono difetti formali di impostazione.

È stato accertato che le risultanti delle azioni verticali sono in equilibrio con i carichi applicati.

Sono state controllate le azioni taglianti di piano ed accertata la loro congruenza con quella ricavabile da semplici ed agevoli elaborazioni. Le sollecitazioni prodotte da alcune combinazioni di carico di prova hanno prodotto valori prossimi a quelli ricavabili adottando consolidate formulazioni ricavate dalla Scienza delle Costruzioni. Anche le deformazioni risultano prossime ai valori attesi. Il dimensionamento e le verifiche di sicurezza hanno determinato risultati che sono in linea con casi di comprovata validità, confortati anche dalla propria esperienza.

## 13.0 INFORMAZIONI INTEGRATIVE SULL'USO DEI CODICI DI CALCOLO

### Codice di calcolo adottato, solutore e affidabilità dei risultati

**Titolo del codice di calcolo:** Modest;

**Autore, produttore e distributore:** Tecnisoft s.a.s., via F. Ferrucci 203/C, 59100 Prato (PO);

**Versione:** Modest Versione 8.28

**Estremi della licenza d'uso o di altra forma di autorizzazione all'uso:** numero di licenza 7279

## AFFIDABILITA' DEL CODICE DI CALCOLO

In base a quanto richiesto al par. 10.2 del D.M. 17.01.2018 (Norme Tecniche per le Costruzioni) il produttore e distributore Tecnisoft s.a.s. espone la seguente relazione riguardante il solutore numerico e, più in generale, la procedura di analisi e dimensionamento Modest.

Si fa presente che sul proprio sito è disponibile sia il manuale teorico del solutore sia il documento comprendente i numerosi esempi di validazione.

Si riporta nel seguito la dichiarazione di affidabilità fornita dalla software house.



Strumenti solidi come i vostri progetti

Tecnisoft s.a.s. di Papi Paolo Luca & C.  
Via F. Ferrucci, 203/C - 59100 Prato  
Tel. 0574 583421 - Fax 0574 592705  
C.F. e P.IVA 01555190972  
R.E.A. C.C.I.A.A. Prato n. 421503

### **DICHIARAZIONE DI AFFIDABILITÀ DEL PROGRAMMA MODEST**

Facendo seguito a quanto richiesto dalle Norme Tecniche per le Costruzioni, la società Tecnisoft s.a.s. produttrice e distributrice del programma ModeSt, dichiara quanto segue.

Il programma ModeSt è un pre-post processore per solutori ad elementi finiti prodotti da altre società ed alle quali si rimanda per i relativi test di affidabilità. Si segnala comunque che i solutori supportati sono di riconosciuta fama nazionale e internazionale e di comprovata affidabilità (Xfinest, SAP2000) e che vengono distribuiti con i relativi test di validazione.

ModeSt contiene comunque al suo interno procedure che l'utente può attivare per il controllo di congruenza sui dati introdotti, procedure che riconoscono in automatico la presenza dei più tipici errori di modellazione.

Al termine del calcolo sono interrogabili sia numericamente che graficamente tutti i risultati, per consentire la valutazione della bontà della modellazione effettuata.

Le procedure di progettazione delle armature degli elementi in c.a. o di verifica degli elementi in acciaio, legno o muratura segnalano sempre le situazioni in cui non sono soddisfatte le condizioni di verifica previste dalla normativa ed implementate nel software. Anche in questo caso si possono effettuare controlli grafici e numerici su stati tensionali, domini di rottura, ecc.

Le procedure di progetto e verifica sono state testate con numerosi esempi reperiti in letteratura o risolti manualmente. Tali esempi sono riportati all'interno di un manuale fornito insieme al programma.

Prato, 30 maggio 2011

Tecnisoft s.a.s.  
Socio Accomandatario

