REGIONE SICILIANA







COMUNE DI VILLALBA



COMUNE DI MUSSOMELI



II Committente:



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II Progettista:





dott. ing. VITTORIO RANDAZZO



Titolo del progetto:

PARCO EOLICO "SCRUDATO" POTENZA NOMINALE 39,6 MW

Elaborato:			

Codice Elaborato:

PROGETTO DEFINITIVO

NPS4_CAM_D10_REL

TITOLO ELABORATO:

RELAZIONE DI PREDIMENSIONAMENTO DELLE FONDAZIONI

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2. RELAZIONE DI CALCOLO

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RELAZIONE TECNICA

OGGETTO: Predimensionamento opere di fondazione per il parco eolico "Scrudato" sito nel comune di Cammarata (AG) in C.da Macinella.

GENERALITA'.

La seguente relazione di calcolo preliminare si riferisce al plinto di fondazione della torreaerogeneratore del tipo SG 6.6-170 da installarsi in agro del comune di Cammarata della provincia di Agrigento.

Tutte le calcolazioni sono state eseguite nel rispetto dei metodi della Scienza delle Costruzioni ed in ossequio alle normative attualmente vigenti. In particolare, il criterio di progettazione e verifica adottato è quello degli stati limite.

Il pre-dimensionamento geometrico delle opere in calcestruzzo armato e il progetto delle relative armature, ha come supporto le sollecitazioni al piede della torre fornite dal produttore dell'aerogeneratore.

Sulla scorta dei risultati delle prove sui terreni oggetto dell'intervento di che trattasi di cui alla relazione geologica redatta dal Dott. Geol. Giuseppe Massimo Volo si sono individuate le caratteristiche geotecniche degli stessi nonché la scelta della tipologia fondale da porre in essere. La quantificazione delle opere sarà eseguita in fase di progettazione esecutiva, a valle di una più dettagliata indagine geologica e geotecnica come previsto dalle normative vigenti.

Il rotore dell'aerogeneratore Siemens Gamesa SG 6.6-170 ha un diametro di 170 m, cui corrisponde un'area spazzata di circa 22.697,00 m².

Esso è costituito da tre pale rotoriche che sviluppano la potenza nominale effettiva di 6600 KW.

La turbina eolica è installata in sommità di una torre tubolare costituita da n. 4 elementi troncoconici in acciaio di differenti dimensioni, che raggiungono un'altezza al mozzo di 115 ml o 135 ml ed un'altezza complessiva di 200 o 220 ml dal piano campagna.

2. DESCRIZIONE.

Il plinto calcolato è costituito da un prisma regolare a base circolare sormontato da un cilindro di cui di seguito si riportano le caratteristiche geometriche.

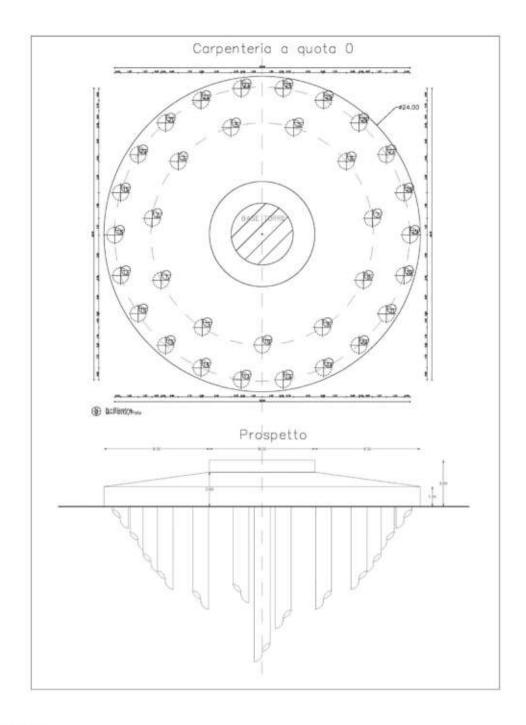




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Sulla base delle caratteristiche dei terreni interessati, evidenziate dai risultati delle prove di cui alla relazione geologica a firma del dott. Volo, si ritiene opportuno porre il plinto di fondazione su fondazione indiretta costituita da n.33 pali dello Φ = 120 cm disposti su due file concentriche, disposti secondo la figura, ammorsati nei terreni fondali per 25,00 mt,. La distanza fra i pali della fila esterna e il centro della fondazione (Dext) è di 11,20 mt, mentre quella fra i pali della fila interna e il centro della fondazione (Dint) è di 8,44 mt. L'interasse tra i pali è pari a 3.20 mt. per la fila esterna e a 4.82 mt. per la fila interna.

Nell'esecuzione del progetto, nel calcolo strutturale, e nelle modalità di posa in opera si è fatto riferimento alla seguente normativa:

Legge 5 Novembre 1971 n.1086 (G.U. 21 dicembre 1971 n.321) "Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica"; D.M. del 24/1/1986 - Norme tecniche relative alle costruzioni sismiche;

Legge 2 febbraio 1974 n.64 (G.U. 21 marzo 1974 n.76) "Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche" Indicazioni progettive per le nuove costruzioni in zone sismiche a cura del Ministero per la Ricerca scientifica - Roma 1981;

D.M. Infrastrutture Trasporti 14 gennaio 2008 (G.U. 4 febbraio 2008 n.29 - Suppl. Ord.) "Norme tecniche per le costruzioni" Inoltre, in mancanza di specifiche indicazioni, ad indicazione della norma precedente e per quanto con esse non in contrasto, sono state utilizzate le indicazioni contenute nella Circolare 2 febbraio 2009 n.617 del Ministero delle Infrastrutture e dei Trasporti (G.U. 26 febbraio 2009 n. 27 - Suppl. Ord.) "Istruzioni per l'applicazione delle 'Norme Tecniche per le costruzioni' di cui al D.M. 14 gennaio 2008" e successive modifiche ed integrazioni di cui al DM del 17/01/2018:

Circolare 2 febbraio 2009 n.617 del Ministero delle Infrastrutture e dei Trasporti (G.U. 26 febbraio 2009 n. 27 – Suppl. Ord.) "Istruzioni per l'applicazione delle 'Norme Tecniche per le costruzioni' di cui al D.M. 14 gennaio 2008" e successive modifiche ed integrazioni con la Circolare n.7 del 21/01/2019;

IEC 61400-1, 2° Edition, February 1999. Wind turbine generator system – Part 1: Safety requirements;





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UNI 9858. Concrete. Performance, production, placing and compliance criteria.

UNI ENV 1992-1-1 del 31-01-1993 Eurocodice 2. Progettazione delle strutture di calcestruzzo.

Inoltre per il calcolo di progetto della torre di sostegno dell'aerogeneratore, eseguito dal produttore, le sollecitazioni massime sono state determinate sulla scorta di quanto previsto dalle:

- EC_Ed3_NCV_00_08010000_A_10_07_17p0 per l'azione FXTB;
- IEC_Ed3_NCV_60_01030000_A_05_12p0 per l'azione FYZTB;
- EC_Ed3_NCV_60_01040000_B_02_01_01_11p0 per il momento MXTB;
- IEC Ed3 NCV 60 01030000 A 05 12p0 per il momento MYTB.

Per la struttura in esame, in riferimento ai carichi "Extreme Loads" inclusi l'azione sismica e la sicurezza, per analogia si sono utilizzati i carichi provenienti da strutture con analoghe caratteristiche, realizzate in siti con caratteristiche similari in termini di azioni (vento, sismica, ecc). In dettaglio:

Tabella 1

Load case	DLC Type	Load factor	F _{xy} (kN)	F ₂ (kN)	M _{xy} (kNm)	Mxy+ΔMxy (kNm)	Mz (kNm)
ULS without Psf	Α	1.0	1498	6566	179651	185069	2231
ULS with Psf	А	1.1 0.9	1648	7222 5909	197616	203034	2454
ULS with Psf (Torsion)	N	1.35/1.1° 0.9	441	6985 * 5715	49389	54806	18061

Table 2 SG 6.6-170 T115-58B Factored/Unfactored Extreme loads at base of the tower

Il carico prodotto dal vento non sarà mai statico su una sola direzione, ma potrà variare su 360 gradi, per tale motivo nella progettazione delle armature si prende in considerazione la zona più sollecitata per il calcolo delle armature all'interno del plinto, armando in modo omogeneo (in senso radiale e concentrica) tutti i 360 gradi che compongono il plinto di fondazione.

Ai carichi verticali, oltre al peso della torre, della navicella e del rotore contemplati nella ipotesi di carico precedente, va sommato il peso del plinto di fondazione di entità non trascurabile.

Il software strutturale utilizzato, in automatico genera il peso proprio della struttura di fondazione, in base al materiale impiegato e alla geometria del plinto stabilita dal progettista.





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In questa relazione di calcolo, avente come finalità il pre-dimensionamento delle strutture, è stata analizzata la condizione più gravosa.

I dati inseriti nel software strutturale, derivano dalla combinazione della condizione Extreme 6.1 con il peso proprio G1 moltiplicati per il coefficiente parziale 1.35, così come previsto dalla IEC 61400-1.

3. OPERE DI FONDAZIONE.

Come anticipato nei paragrafi precedenti le fondazioni saranno di tipo indiretto con pali dello Φ 120 cm ammorsati, superato il primo strato di terreno agrario dello spessore di circa 1,00 mt, nelle argille brecciate di colore nocciola per circa 4,50 mt e successivamente nelle argille brecciate grigio-azzurre fino a fondo foro.

La testa dei pali sarà ammorsata ad una plinto di fondazione di spessore variabile al cui culmine verrà collocata la torre-aerogeneratore. Detto plinto è stato discretizzato con elementi tipo shell di sezione variabile.

Per i terreni interessati dall'ammorsamento dei pali si sono utilizzati i seguenti valori:

- Strato n.1 Terreno agrario da mt 0,00 a mt. 1,00;
- Strato n.2 Argille brecciate di colore nocciola da mt 1,00 a mt. 4,50 :
- Peso per unità di volume (γ_a) = 1.947 [daN/m³];
- Peso di volume saturo (γ_s) = 2.030 [daN/m³];
- Angolo di attrito interno (φ')= 19,18°;
- Coesione non drenata (C_u)= 0,611 [daN/cm²];
- Coesione drenata (C')= 0,319 [daN/cm²];
- 3. Strato n.2 Argille brecciate grigio-azzurre da mt 4,50 a mt. 20,00 :
- Peso per unità di volume (γ_a) = 1.997 [daN/m³];
- Peso di volume saturo (γ_s) = 2.130 [daN/m³];
- Angolo di attrito interno (φ')= 22,23°;
- Coesione non drenata (C_u)= 1,309 [daN/cm²];
- Coesione drenata (C')= 0,471 [daN/cm²];

Materiali utilizzati:





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1. Plinto di fondazione.

Calcestruzzo classe C40/50:

- P <daN/mc>2500;
- E <daN/cmq>355471.00;
- G <daN/cmq>161578.00;
- v =0.1;
- $\alpha = 1.00E-05$.

Tipo di acciaio B450C:

- E <daN/cmq>2060000.00;
- F_{vk} <daN/cmq> 4500
- 2. Pali di fondazione.

Calcestruzzo classe C30/37:

- P <daN/mc>2500;
- E <daN/cmq>330194.00;
- G <daN/cmq>159036.00;
- v =0.1;
- α= 1.00E-05.

Tipo di acciaio B450C:

- E <daN/cmq>2060000.00;
- F_{vk} <daN/cmq> 4500

Per i dettagli vedasi la relazione geologica e la relazione di calcolo allegate.

4. CARATTERISTICHE DEL PROGRAMMA DI CALCOLO E PROGETTO DELLE ARMATURE.

4.1 Programma di calcolo

Si tratta di una procedura volta alla progettazione di strutture in c.a. in zona sismica e non, che si avvale come solutori dei programmi agli elementi finiti (F.E.M.) . Il plinto di fondazione è stato modellato con elementi di tipo bidimensionale (Shell), di spessore variabile, a comportamento flessionale-membranale.





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La colonna stratigrafica inserita per il calcolo dello stato tensionale e deformativo dei pali di fondazione è dedotta dai valori riportati nella relazione geologica.

Il programma è rappresentato da un pre-processore per la generazione dei file di input del solutore agli elementi finiti e da un post-processore per il calcolo delle sezioni e la generazione delle armature secondo la legislazione vigente.

Le figure seguenti mostrano la struttura discretizzata secondo il modello di calcolo adottato:

VISTA ASSONOMETRICA

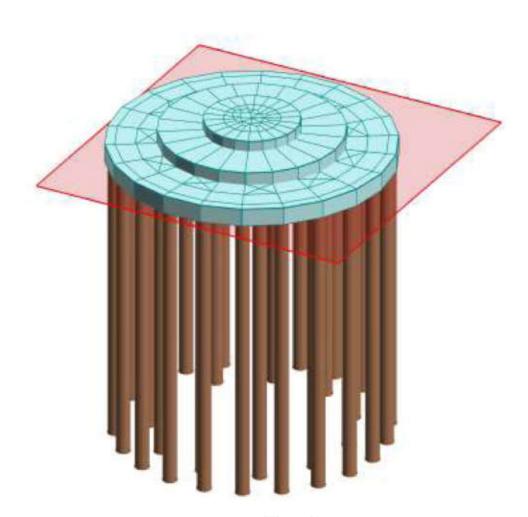


Figura 2





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PLANIMETRIA

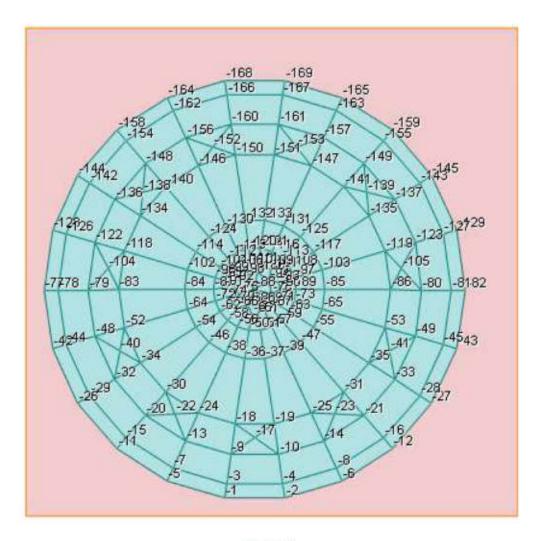


Figura 3

Le dimensioni dell'armatura superiore o inferiore della platea vengono determinate seguendo l'approccio Wood Armer-Armer per trovare i momenti di progetto sui quali dimensionare l'armatura. In questo modo infatti non si trascura il contributo del momento torcente mxy che agisce sui lati dell'elemento shell.





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Nella figura successiva si riportano i diagrammi di Wood Armer, utilizzati per il calcolo delle armature, dei momenti Mx ed Mzz:

PARTICOLARE DEL DIAGRAMMA DI WOOD ARMER RELATIVO A Mxx.

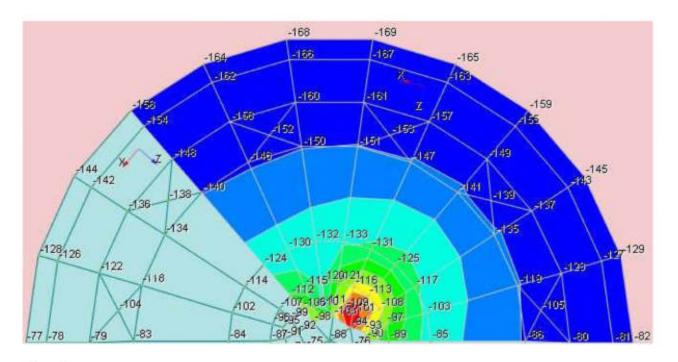
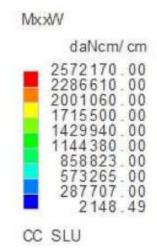


Figura 4







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PARTICOLARE DEL DIAGRAMMA DI WOOD ARMER RELATIVO A MZZ.

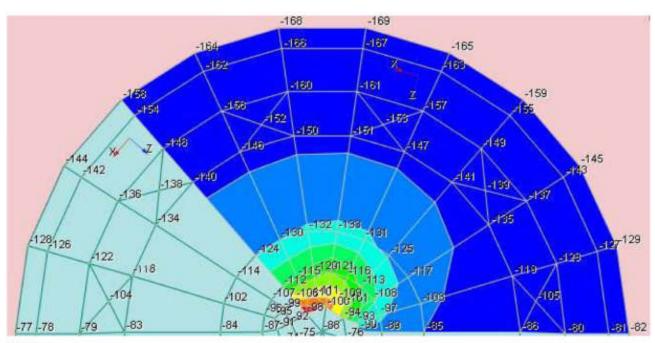
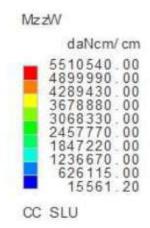


Figura 5







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4.2 Progetto delle armature.

Partendo dalle sollecitazioni valutate nella condizione di carico definita nel paragrafo 2 è stata calcolata l'armatura da adottare, riportata nelle Figure seguenti. Si rimanda ai tabulati di calcolo per i dettagli.

Dal progetto delle sezioni più sollecitate, in direzione x e z (vedi assi locali in figura) dei singoli elementi shell della fondazione, individuate in corrispondenza alla testa dei pali e alla sezione d'attacco al nucleo centrale, si evince quanto rappresentato di seguito:

ARMATURA RADIALE E CONCENTRICA

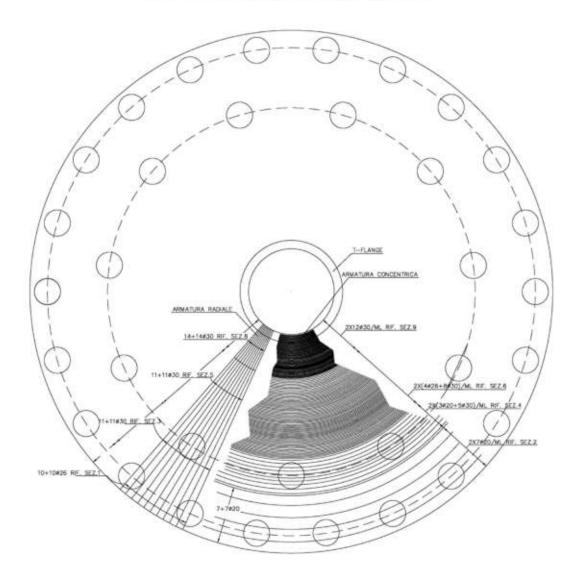


Figura 6





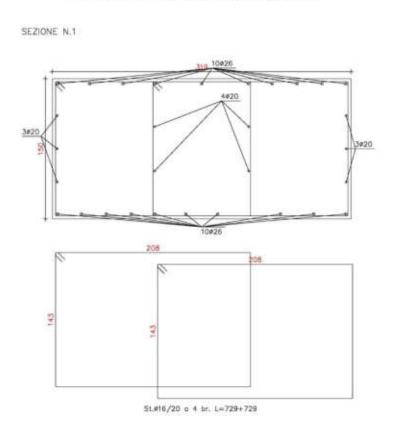
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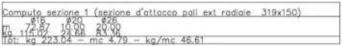
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ARMATURA DELLE SEZIONI TIPO





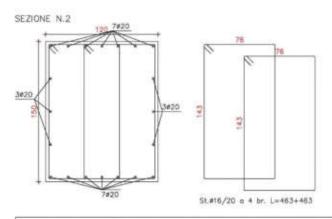


Figura 7

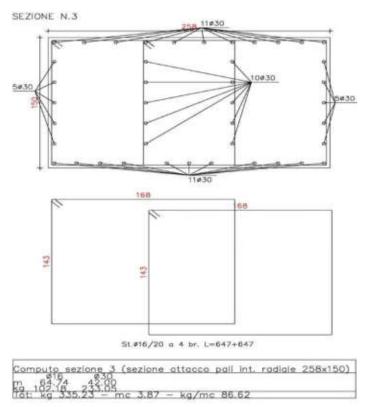




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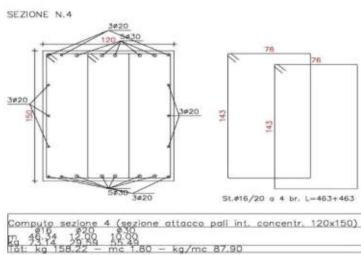


Figura 8





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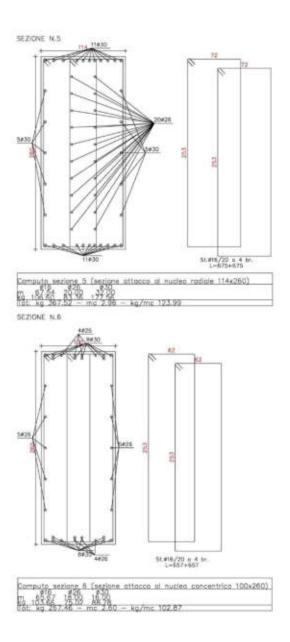


Figura 9

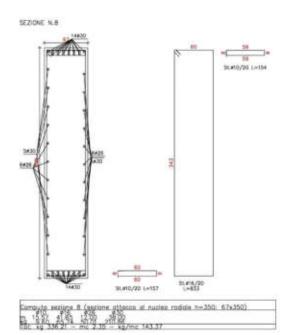


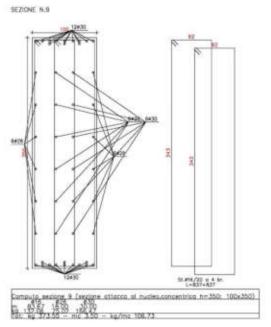


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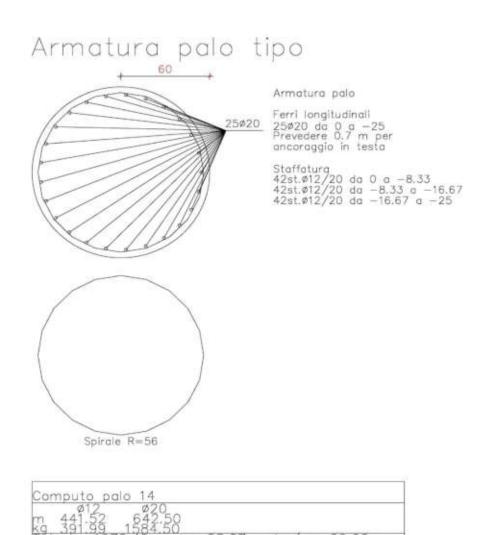
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ARMATURA DEL PALO TIPO



mc 28.27 - kg/mc 69.90





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RELAZIONE DI CALCOLO

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Da 0 a -25	80
Palo n. 16	83
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Da 0 a -25	88
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Da 0 a -25	99
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Introduzione

Sistemi di riferimento

Le poprimate, i carrohi consentrati, i redomenti. Le reacioni vincolari e gli appatamenti dei 3000 sono riferiti ad una tono poptos portes no globole sur l'appa 7 vent privin velto velto. Ello. I parichi i poposinate loca i e le zo legitatio i de le 7877 sono riferite ad una terna desta cartesiana loca e cos

- lassé X poi in de la poi l'asse pe l'asta e con varso pa incho inizia e at rodo tinates
- immaginando la trave a sezione rettangolare l'asse / e parallelo alla base e l'asse / è parallelo all'altezza. La ritazione ver l'abini nomporta pullari dal regulatione di latta in termi lossie.

ai puo immaginare la terma locale di un'asta comunque disposta nello spazio come derivante da quella globale dopo una serie

- ina rotatione "Itorno a l'asse 7 die cont. L'asse 8 à colodinere con la prolex one ce l'asse del l'asta sul pland
- was time as one lungs is supposed that define a in made on operate Portigions an interession is professional access in L'ale dell'asta su lipiano or zuo Lalez
- una trasiszione lungo l'asse E che porti l'origine a considere con il cosò inociale sell'asta;
 una considere intervada "succe Modes" dell'olto decidere l'asse Monovina decenva l'ores dell'asta;
 una considere intervada "succe Modes" dell'olto puri al modescione del l'ort.

In praticalle travi prive ŝi rotazione avranno sempre l'assel rivolto verso l'alto e l'asse Y nel piano ŝel solaĵo, mentre ŝ plusto prive d'empluzione, venomo l'amma Modes e ola l'acce Miglok e per l'amma Report pont le pina controverso e l'amma Modes X globale. Par puare vilmui che per i praestri la "Base" A l'Italo vera lelo a M.

To exclination out as it common in movest with local large interpretable TRAINSTONALT value. Mixture with the contraction of th pestra partes analitora e post petinita:

- crigine nel primo nodo dell'elemento/
- nació Microtico dente como la complia gence di Epirimo de 11 acceptado activo de 11a enercia;
- asse Mide in to come promotho vettoria e tra il versore dell'asse Mie il verzore della polyungente il primo e il pranto nodo, Assell a formare con gli altri due una terna destrorsa.

Praticarente un eferento vertica e con l'asse X foca e combinente con l'asse X g chafe ha anche qui affir lazzi commoidenti con quelli globali.

Rotazioni e momenti

Segue to ' i principio acollato per t...' i tariori the zono positivi se CONTROVIRGI agrillazzi, a che i morenti tonocentrati e le rotazioni impresse in coordinate globali risultano positivi se CDALCVARYL al segno positivo delle rotazioni. Il segno positivo dei noment, e las le no naion. A cum la commisa por l'osservatione poste no l'omigilise Michaelle. M. Minust. Lu. 3, 7 mota an XI. In chat da Albrillio ente acettare, a regola della randicestratione por l'os n'yotub net a direzio e de l'assey, la ritazione she porta a shiudere il palmo della mano corrisponde al segno positivo.

Normativa di riferimento

Talhorma, "valor initier" ne loce la seguente:

- Legge n. 64 del 1/2/1974 Provvedimenti per le costruccioni con parcicolari prescrizzoni per le cone sismiche.
- D.M. delizatif / red ... Notice beautifule trends we also be bracket in a same tree.
- Exquere, 1609 del p/11/1977 Economy of the discription on a poximal charge crash covariation, runnic, form, la comession present est a l'élan Ultura mella i " .:A .
- D.M. do: 14/2/1992 Morme Texaciones part l'appeaux dux une response in mula, avenua de programpropera d'obtant duras meta Linhet.
- D.M. on 1977/1896 Norma takan mas part Paskin, lauk wa le opark in www. namatale e praswapansese as pert talatin. Trak meta libbet
- D.M. do: 16/1/1996 Norma teachings pain to contraviant in a long standard
- Circolare d. 21747 del 20/7/1981 Legge n. 219 del 14/7/1981 Art. 10 Estrucioni relative al rafforcamento degli en 2006 nombre de masgitti de la serio.
- Regione Autinoma Priuli venezia Ciulia Legge Regionale n. 20 del 20/0/1977 Documentazione tecnica per la progettazione e objector o operator objector degli a di 0.00 Documento Feodora, n. 3 Reproduceda ioni per la negacione degli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione degli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione degli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione degli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione degli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione degli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione de gli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione de gli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione de gli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione de gli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione de gli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione de gli a di 0.00- Pocumento Feodora, n. 3 Reproduceda ioni per la negacione de gli a di 0.00- Pocumento Feodora de gli a di 0.00- Pocumento Feodora di 0.00- Pocumento Pocument as of as consider a coperation of parmix force with utilities energy free of of communications.
- D.M. on 1997/17/1987 Norma Totalism on a consept. Toral, again toral action also despit with a manufactor of its conconsettionne tou
- Marine Terminder C.M.R. of 10011-85 cm [1974/1895 Continuation of acceptable Entraction open conditioned, Intersecutions, I con autore la rancterió el
- Morma Torricks C.M.R. n. 1986a-84 or 14/12/1984 Ediruzion dorn i drogetto, Polasuzione od i montro o de la edittum prefablo date in conglemenato cerentiz e e per le scrutture coscruite de siatem finoscriationale i accidio i Tatrizio i per il calcolo, l'esecuzione, il collaudo e la manutenzione.
- 1.85 de 1077/1995 Tabricio I veri favolicació e delle "Morre Decolore per le costrizio i in roce aixi chefici cui al D.M. del 15/1/1995.
- Fundaccióne de la Progettlaz che de la surultura di l'agno.
- DTN 1050 Metzeri of war files pair in a check
- D.M. del 17/1/2018 | Norme techniche per le costrucioni.

- Circolare n. 7 del 21/1/2019 Istruzioni per l'applicazione dell'«Aggiornamento delle "Norme tecniche per le costruzioni"» di cui al decreto ministeriale 17 gennaio 2018.
- Documento Tecnico CNR-DT 200 R1/2012 Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati.
- Eurocodice 3 Progettazione delle strutture in acciaio.

Unità di misura

Le unità di misura adottate sono le sequenti:

- lunghezze : m
- forze : daN
- masse : kg
- temperature : gradi centigradi
- angoli : gradi sessadecimali o radianti

Geometria

Elenco vincoli nodi

Simbologia

Comm. = Commento

Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Ly = Lunghezza (dir. Y locale)

Lz = Larghezza (dir. Z locale)

RL = Rotazione libera

Rx = Rotazione intorno all'asse X (L=libera, B=bloccata, E=elastica) Ry = Rotazione intorno all'asse Y (L=libera, B=bloccata, E=elastica) Rz = Rotazione intorno all'asse Z (L=libera, B=bloccata, E=elastica)

Sx = Spostamento in dir. X (L=libero, B=bloccato, E=elastico)
Sy = Spostamento in dir. Y (L=libero, B=bloccato, E=elastico)
Sz = Spostamento in dir. Z (L=libero, B=bloccato, E=elastico)

TV - Tipo vincolo se valutato da stratigrafia

SP = Plinto senza pali

CP = Palo o plinto con pali

Vn = Numero del vincolo nodo

Vn	Comm.	TV	Sx	sy	Sz	Rx	Ry	Rz	RL	Ly <m></m>	Lz <m></m>	Kt <dan cmc=""></dan>
1	Libero		I,	L	L	Z.	L.	L				
4	palo	CP	E	E	E	Ë	E	В			6 8	f(strat.)
4	palo	SP	В	В	E	В	В	В				f(strat.)

Elenco costanti elastiche nodali

Simbologia

KRx = Costante elastica intorno all'asse X

KRy = Costante elastica intorno all'asse Y

KRz = Costante elastica intorno all'asse Z

Kx = Costante elastica in dir. X

Ky = Costante elastica in dir. Y

Kz = Costante elastica in dir. Z

Nodo - Numero del nodo

Nodo	Kx <dan cm=""></dan>	Ky <dan cm=""></dan>	Kz <dan cm=""></dan>	KRx <danm rad=""></danm>	KRy <danm rad=""></danm>	KRz <danm rad=""></danm>
-167	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-166	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-163	23177.10	23177.10	141442.00	53208800.00	53208800.00	++ 1
-162	23177.10	23177.10	141442.00	53208800.00	53208800.00	++
-155	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-154	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-153	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-152	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-143	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-142	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-139	23177.18	23177.10	141442.00	53208800.00	53208800.00	
-138	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-127	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-126	23177.10	23177.10	141442.00	53208800.00	53208800.00	44
-105	23177.10	23177.10	141442.00	53208800.00	53208800.00	+-
-104	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-81	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-78	23177.10	23177.10	141442.00	53208800.00	53208800.00	m ==
-45	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-44	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-41	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-40	23177,10	23177.10	141442.00	53208800.00	53208800.00	e-
-29	23177.10	23177.10	141442.00	53208800.00	53208800.00	

-28	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-23	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-22	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-17	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-16	23177.10	23177,10	141442.00	53208800.00	53208800.00	
-15	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-8	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-7	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-4	23177.10	23177.10	141442.00	53208800.00	53208800.00	
-3	23177.10	23177.10	141442.00	53208800.00	53208800.00	

Elenco nodi

Simbologia

Imp. = Numero dell'impalcato
Nodo = Numero del nodo
Vn = Numero del vincolo nodo
X = Coordinata X del nodo
Y = Coordinata Y del nodo

Nodo	X	Y	Z	Imp.	vn
-169	<m> 13.21</m>	23.38	0.00	0	1
-168	9.79	_	_	-0	1
-167	13.09		0.00	- 0	4
	_		_		-
-166	9.91	_	0.00	0	4
-165	16.4B	and the second second	0.00	0	1
-164	6.51		0.00	- 0	1
-163	16,15		0.00	. 0	4
+162	6.B5		0.00	. 0	4
-161	12.85	20,90	-	0	1
-160	10.15	20,90	0.00	- 0	1
-159	19.36	20.57	0.00	- 0	-1
-158	3.64	20.57	0.00	Ð	1
-157	15.44	20.34	0.00	0	1
-156	7.56	20.14	0.00	- 0	1
-155	18.84	19,96	0.00	- 0	4
-154	4.16	19,96	0.00	. 0	4
-153	13.88	19.60	0.00	0	4
-152	9.12	19.60	0.00	Ð	4
-151	12.61	19,16	0.00	- 0	1
-150	10.39	19,16	0.00	- 0	1
-149	17.72	18.67	0.00	.0	1
-148	5.28	18.67	0.00	Ð	1
-147	14.72	18.54	_	- 0	1
-146	8.28	18.54	-	- 0	1
-145	21.56	17.99	0.00	0	1
-144	1.40		0.00	0	1
-143	20.92	17.55	0.00	0	4
-142	2.08	17.55	0.00	- 0	4
-141	16.57	17.35	0.00	0	1
7.40	-	17,35	0.00		1
-139				0	-
-	-		0.00	- 0	4
-138	5.12	17.03	0.00	- 0	4
-137	19.49	16.62	0.00	- 0	1
-136	3.51	16.62	0.00	. 0	1
-135	18.01	15,69	0.00	Ð	1
-134	4.99	15,69	0.00	- 0	1
-133	12.06	15.43	0.00	- 0	1
-132	10.94		0.00	Ð	1
-131	13.15	15.11	0.00	- 0	1
-1.30	9.85		0.00	0	1
-129	23.01	14.87	0.00	- 0	1
-128	-0.01	14,87	0.00	. 0	-1
-127	22.25	_	0.00	. 0	4
-126	0.75		0.00	Đ	.4
-125	14.11	14.50	0.00	- 0	1
-124	8.89	14.50	0.00	- 0	1
-123	20.67	14.17	0.00	- 0	. 1
-122	2,39	14,17	0.00	0	1
-121	11.83	13.83	0.00	0	-1
-120	11.17	13,83		- 0	_
-119	18.93	-	0.00	0	-
-118	4.07		0.00	0	_
-117	14.86	_	0.00	0	1
And f	4.1 + 0.0	水が水が大	9.0.00		1 4

-114 -117 -117 -111					
11.0 11.2 -111	10.52	13,64	0.00	С	_
-11z -111	8114	13,64	0,00	С	-
11	13.04	1318	0.00	10	
_	3.98	13.118	0.00	10	
	11.06	10.90	0.00	1;	-
-110	101.8%	10.00	0.00	1;	-
$\overline{}$	12.12	12,77		C	
				-	-
_	10.48	12,77	0,00	С	
1.00	30560	12.11	0.00	10	
1000	10147	12.76	0.00	10	•
-170-	19.335	100,00	0.00	1;	Ŀ
-104	9.15	100.00	0.00	1;	ć
-103	17.35	11.61	0.00	С	-
-100	7.85	11.6	0.00	Č	-
-				-	-
_		//	0.00	- 13	
	T1 187	12.76	0.00	1:	
-55	0.97	10.35	0.00	1;	٠
-5:	10.396	77.23	0.00	1;	-
-97	10.75	11.16	0.00	С	
-90	9.24	11.16	0.00	С	·
	9.85	12.07	0.00	13	÷
$\overline{}$		70.02		1:	-
_					<u> </u>
$\overline{}$	12.00	11.39	0.00	- 0	_
-90	10.28	11.83	0,00	С	_
-91	9.75	11.61	0.00	С	-
-4	TT1.93	113	0.00	1:	
$\overline{}$	13.85	116	0.00	1:	
	11.50	11.50	0.00	10	-
-87	0.75	11.50	0.00	10	-
$\overline{}$				_	-
_	10.24	11,40	0.00	C	
-11	17,40	11,40	0,00	С	_
::1	7.36	11.73	0.00	1:	
::.:	3178	11.73	0.00	1:	
-85	231.50	11.49	0.00	1;	-
-31	07.70	11.4%	0.00	1;	
-10		11,40	0.00	C	
$\overline{}$				-	-
-79	2,00	11,40	0,00	С	_
7::	0.30	11.73	0.00	1:	_
22	0.50	11.73	0.00	10	·
-776	17.45	11.77	0.00	1;	-
	10.56	11.77	0.00	1;	-
-74	9.90	11.00	0.00	С	·
$\overline{}$	10.75		0.00	C	_
92		10.84		10	-
	92.01		0.00	-	
21	171,89	10.70	0.00	10	-
	100,700	10.70	0.00	1;	
-6.9	11,181	10.00	0.00	1;	
	11.10	10,60	0.00	C	-
	12.48	10,44	0.00	С	
_	10.55		0.00	1:	·
	135		0.00	10	·
-64	7.65	70.97	0.00	10	-
					-
	13.48	10.23	0.00	- 0	
-01	0.52	10,00	0.00	C	<u> </u>
-51	11.67	10.08	0,00	С	<u> </u>
osi (Т 133	10.08	0.00	10	•
	13.04	9.77	0.00	10	·
77.44	0.06			1;	·
-j- 3		9.77	0.100		
-j- 3			0.00	- 10	-
-,- 's	17.48	÷.%	0.00		-
	12.48 10.52	9.36	0.00 0.00	1: C	-
-54 -53 -53 -25 -25	12.48 10.52 14.8€	9.36 9.36 9.34	0.00 0.00 0.00	0 0	
-5.4 -5.5 -5.5 -5.5 -5.4	12.48 10.52 14.88 8.14	9.36 9.36 9.34 4.34	0.00 0.00 0.00 0.00	0 0	- 1 - 1 - 1
-5 % -5 % -5 % -5 5 % -5 5 % -5 4 %	12.48 10.52 14.88 8.14 18.93	9.36 9.26 9.24 9.34 4.31	0.00 0.00 0.00 0.00 0.00	0 0	
-5 % -5 % -5 % -5 % -5 % -5 % -6 % -6 % -6 %	12.48 10.52 14.88 8.14 18.93	9.36 9.26 9.24 9.37 9.37	0.00 0.00 0.00 0.00 0.00	0 0	
-24 -25 -25 -21 -21	12.48 10.52 14.88 8.14 18.98 4.07 11.83	9.36 9.36 9.34 9.37 9.37	0.00 0.00 0.00 0.00 0.00 0.00	0 0 0	
+59 +50 +50 +50 +50 +50 +50 +51 +50	12.48 10.52 14.88 8.14 18.98 4.07 11.83	9.76 9.76 9.76 9.87 9.87 9.87	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0 0	
+59 +50 +50 +50 +50 +50 +50 +51 +50	12.48 10.52 14.88 8.14 18.98 4.07 11.83	9.76 9.76 9.76 9.87 9.87 9.87	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0 0 0	
-29 -29 -20 -20 -21 -21 -21 -21 -20 -4	12.40 10.52 14.86 8.14 18.93 4.04 11.83 11.17 20.87	9.36 9.34 9.34 9.37 9.37 9.47 9.27	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0 0 0 0 0	
-59 -59 -50 -50 -51 -51 -51 -50 4 4	12.46 10.52 14.86 8.14 18.98 4.04 10.83 10.17 20.87	9.19 9.26 9.24 9.37 9.31 9.41 9.47 9.47	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 0 0 0 0	
	12.46 10.52 14.86 8.07 18.98 4.07 153 117 26.87 7.89	9.19 9.26 9.24 9.37 9.31 9.27 9.27 9.27 9.283 9.483	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	12.46 10.52 14.86 8.17 18.93 4.07 11.83 11.17 20.87 12.11 14.11	9.19 9.26 9.24 9.37 9.31 9.27 9.27 0.83 0.83 9.40	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	12.46 10.52 14.96 8.14 18.98 4.07 11.53 11.17 70.87 14.11 9.89 14.11	9.19 9.26 9.24 9.37 9.31 9.41 9.47 9.47 9.43 9.43 9.40 9.40	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	12.46 10.52 14.86 8.17 18.98 4.07 11.83 11.17 20.87 71.89 14.11 9.69 20.25 0.75	9.39 9.24 9.37 9.37 9.37 9.47 9.47 9.47 9.43 9.40 9.40	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	12.48 10.52 14.56 8.14 18.98 4.07 11.53 11.17 20.87 14.11 9.88 12.25 0.75 23.01	9.36 9.26 9.24 9.37 9.37 9.47 9.47 9.47 9.48 9.48 9.48 9.48	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	12.48 10.52 14.56 8.14 18.98 4.07 11.53 11.17 20.87 14.11 9.88 12.25 0.75 23.01	9.39 9.24 9.37 9.37 9.37 9.47 9.47 9.47 9.43 9.40 9.40	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0		
	12.46 10.52 14.86 8.17 18.98 4.07 11.83 11.17 20.87 71.89 14.11 9.69 20.25 0.75	9.19 9.26 9.24 9.37 9.37 9.47 6.47 6.83 6.83 6.46 8.27 8.27	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0		

-39	13.15	7.87	0.00	0	1
-38	9.85	7.87	0.00	0	1
-37	12.06	7.55	0.00	0	1
-36	10.94	7,55	0.00	- 0	1
-35	18.01	7.31	0.00	0.	1
-34	4.99	7.31	0.00	Ð	1
-33	19.49	6.37	0.00	.0	1
-32	3.51	6.37	0.00	0	1
-31	16.57	5.65	0.00	- 0	1
-30	6.43	5.69	0.00	- 0	1
-29	2.08	5.45	0.00	0	4
-58	20.92	5.43	0.00	0	4
-27	21.56	5.01	0.00	0	1
-26	1,40	5.01	0.00	. 0	1
-25	14.72	4.46	0.00	0	1
-24	8.28	4.46	0.00	0	1
-23	16.06	4,40	0.00	. 0	4
-22	6.94	4.40	0.00	- 0	4
-21	17.72	4.32	0.00	Ð	1
-20	5.28	4.32	0.00	0	1
-19	12.61	3.84	0.00	0	1
-18	10.39	3.84	0.00	0	1
-17	11.50	3.06	0.00	. 0	4
-16	18.84	3.04	0.00	0	- 4
-15	4.16	3.04	0.00	Ð	4
-14	15.44	2.86	0.00	0	1
-13	7.56	2.86	0.00	0	1
-12	19.36	2.43	0.00	Ð	1
-11	3.64	2.43	0,00	0	1
-10	12.85	2.10	0.00	- 0	1
-9	10.15	2.10	0.00	0	1
-8	16.15	1.32	0.00	- 0	4
-7	6.85	1.32	0.00	0	4
-6	16.4B	0.58	0.00	0	1
-5	6.51	0.58	0.00	- 0	1
-4	13,09	0,42	0.00	. 0	4
-3	9.91	0.42	0.00	. 0	4
-2	13.21	-0.38	0.00	Ð	1
-1	9.79	-0.38	0.00	- 0	1

Elenco materiali

Simbologia

α = Coeff. di dilatazione termica ν = Coeff. di Poisson

Comm. = Commento

E = Modulo elastico

G = Modulo elastico tangenziale

Mat. = Numero del materiale

P = Peso specifico

Mat.	Comm.	P <dan mc=""></dan>	E <dan cmq=""></dan>	G <dan cmq=""></dan>	ν	α
10	Calcestruzzo classe C40/50	2500	355471.00	161578.00	0.1	1.00E-05

Elenco sezioni aste

Simbologia

B = Base

C = Numero del criterio di progetto

Comm. = Commento
Crit. C.F. = Criterio di progetto collegamento finale
Crit. C.I. = Criterio di progetto collegamento iniziale

H = Altezza

Ma = Numero del materiale

Mem. - Membratura G = Generica

Sez. = Numero della sezione Tipo = Tipologia R = Rettangolare

Ver. = Verifica prevista C = Cemento armato

Sez.	Comm.	Tipo	Mem.	Ver.	B <cm></cm>	H <cm>></cm>	Ma	c	Crit. C.I.	Crit. C.F.
1	Sezione d'attacco pali ext radiale 319x150	B	G	C	319.00	150.00	10	3		
- 2	Sezione attacco testa pali ext concentr. 120x150	R	G	C	120.00	150.00	10	3		
- 3	Sezione attacco pali int. radiale 258x150	R	G	C .	258.00	150.00	10	3		
4	Sezione attacco pali int. concentr. 120x150	R	G	C	120,00	150.00	10	3		
.5	Sezione attacco al nucleo radiale 114x260	R	G	C	114.00	260.00	10	3		

- 6	Sezione attacco al nucleo concentrica 100x260	R	G	C	100.00 260.00	10	0 3
7	Sezione attacco al nucleo concentrica H=350 114x350	R	G	C	114.00 350.00	10	0 3
8	Sexione attacco al nucleo radiale N=350: 67x350	R	G	C:	67.00 350.00	10	0 3
- 9	Sezione attacco al nucleo, concentrica H=350: 100x350	R	G	C.	100.00 350.00	10	0 3
10	SEZIONE ATTACCO POST. DEL PALO POSTERIORE: 258X260	R	G.	C	258.00 260.00	10	0 3

Elenco tipi elementi bidimensionali

Simbologia

Ang. att. = Angolo di attrito Ang. dil. = Angolo di dilatanza

Coes. - Coesione Comm. - Commento Crit. - Numero del criterio di progetto

DP = Drucker-Prager

Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Mat. = Numero del materiale

Spess. - Spessore

Tb = Numero del tipo muro/elemento bidimensionale

Tipo = Tipologia F = Membranale e Flessionale

M = Membranale

W-RC = Winkler resistente solo a compressione

W-RTC - Winkler resistente a trazione e a compressione

Uso = Utilizzo

S = Soletta/Platea

Tb	Comm.	Tipo	Uso	Spess.	Kt <dan cmc=""></dan>		Ang. att. <grad></grad>	Coes.	Ang. dil. <grad></grad>	Crit.	Mat.
-1	Platea h=1.50 mt	E	S	150.00		N	0.00	0.00	0.00	- 3	10
-2	Platea H=2.6 mt	F	S	260,00		N	0.00	0.00	0.00	. 3	10
3	Platea H= 3.50 mt	F	S	350.00		N	0.00	0.00	0.00	- 3	10

Elenco elementi bidimensionali

Simbologia

Bid. = Numero del muro/elemento bidimensionale Dyl = Scost. filo fisso Yl Dy2 = Scost. filo fisso Y2

FF = Filo fisso

Kt = Coeff. di sottofondo su suolo elastico alla Winkler

NN = Nodi

Tb = Numero del tipo muro/elemento bidimensionale

Bid.	Tb	FF			Kt <dan cmc=""></dan>	NN
2	2	33	0.00	0.00		-140 -134 -114 -124
2	2	33	0.00	0.00		-146 -140 -124 -130
- 2	2	33	0.00	0.00		-52 -34 -54 -64
- 2	. 2	33	0.00	0.00		-83 -52 -64 -84
2	2	33	0.00	0.00		-150 -146 -130 -132
2	. 2	33	0.00	0.00		-151 -150 -132 -133
2	2	33	0.00	0.00		-147 -151 -133 -133
- 2	2	33	0.00	0.00		-141 -147 -131 -125
2	2	33	0.00	0.00		-135 -141 -125 -117
2	2	33	0.00	0.00	Į.	-119 -135 -117 -103
2	2	33	0.00	0.00		-86 -119 -103 -85
.2	-2	33	0.00	0.00		-53 -86 -85 -65
2	2	33	0.00	0.00		-35 -53 -65 -55
2	2	33	0.00	0.00		-31 -35 -55 -47
- 2	2	33	0.00	0.00		-25 -31 -47 -39
2	2	33	0.00	0.00		-19 -25 -39 -37
2	2	33	0.00	0.00		-18 -19 -37 -36
2	2	33	0.00	0.00		-24 -18 -36 -38
2	1	33	0.00	0.00		-13 -9 -18 -24
2	1	33	0.00	0.00		-163 -167 -161 -157
- 2	1	33	0.00	0.00		-160 -152 -150
- 2	1	33	0.00	0.00	1	-169 -168 -166 -167
2	. 1	33	0.00	0.00		-32 -20 -30 -34
-2	1	33	0.00	0.00		-155 -163 -157 -149
2	1	33	0.00	0.00		-152 -146 -150
2	1	33	0.00	0.00		-143 -155 -149 -137
- 2	1	33	0.00	0.00		-79 -48 -52 -83
2	1	33	0.00	0.00		-77 -42 -44 -78
2	-1	33	0.00	0.00		-152 -156 -146
- 2	1	33	0.00	0.00		-128 -77 -78 -126
2	2	33	0.00	0.00		-118 -83 -84 -102
2	2	33	0.00	0.00		-134 -118 -102 -114
.2	1	33	0.00	0.00		-136 -122 -118 -134
- 2	1	33	0.00	0.00		-144 -128 -126 -142

-	_	20	0.00	[: .cc	-161 103 157
			0.00	0.00	-108 144 141 154
	·	-	0.00	-	166 146 146 148
	-	-		-	Te/ Tep 154 165
	Н		0.00		
- 7			0.000		-149 -141 -119
		.i.i	0.,00	0.00	-1.687 -1.697 -1.697 -1.679
	_	2	0.00	0.00	-101 100 150 151
		22	0.00	0.00	-109 100 103 155
-	-		0.00		Tag Tag 180
-4	-	-		-	145 Ad 35 145 Tay 156 173
		-	0.00	$\overline{}$	14a (15a (15a (143
- 7	•		0.00		-149 -150 -140 -141
		.1.1	0.00	0.00	-160 -164 -166 -166
	_	20	0.00	0.00	-141 130 139
			0.00	0.00	-113 140 143 127
	·	-	0.00	-	123 127 136 119
-			0.00	-	127 145 130 168
	-	_		-	
		_	0.00	$\overline{}$	-15% -14% -15%
			0.00		-80 -104 -107 -80
	_	20	0.00	0.00	-49 SO 86 DB
	-	2	0.00	0.00	-43 82 81 43
	·		0.00	_	163 (161 (177
-		_	0.00	-	-91 -177 -177 -(9)
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	Щ		0.00	$\overline{}$	-01 -00 -05 -21
			0.00	$\overline{}$	-17 43 47 18
	-	2.2	0.00	0.00	-101 101 153
	•		0.00		45 81 80 49
			0.00	$\overline{}$	TC 17 Ta Ta
-	-		0.00	$\overline{}$	-00 -24 -29 -00
-			0.00		-160 -156 -150
- :	Щ				
	_		0.00	0.00	-11 27 28 10
1 1	2	20	0.00	[: .cc]	-34 30 46 04
		33	0.00	0.00	ad or 38 46
	3	-	0.00	-	16 38 36 55
- :	-:	_	0.00	0.00	-54 -46 -50 -60
$\overline{}$				$\overline{}$	
			0.00	$\overline{}$	-64 -54 -0 × -00
			0.00	0.00	-84 84 72 87
	2	2.2	0.00	[0.00]	-102 84 87 <i>96</i>
	3	33	0.00	0.00	117 162 98 107
	33	33	0.00	0.00	124 - 114 - 100 - 113
- :	-1				
			ir nai	n ne	4100 4104 4100 4115
-			0.00 e.oc	0.00 7.00	-100 -104 -110 -115 -104 -100 -11100
	-;	.ii	0.00	0.00	-132 -130 -115 -130
- :	11	77 22	0.00 0.00	0.00 0.00	-122 -120 -115 -100 -130 -131 -126 -121
	-;	77 22	0.00	0.00	-132 -130 -115 -100 -130 -131 -120 -121 -131 -133 -121 -118
- :	J. 01	200	0.00 0.00 0.00	0.00 0.00	H132 H130 H115 H100 H130 130 120 121 H131 133 121 118 H23 131 118 118
0.0	20 00 20	90 22 33	0.00 0.00 0.00	0.00 0.00 0.00 0.00	-102 -100 -115 -100 -130 -130 -120 -121 -131 -133 -121 -116 -120 -121 -116 -113 -117 -126 -114 -108
5 0 0 ×	20 00 20	30 20 33 33	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	-102 -100 -115 -100 -130 -130 -120 -121 -131 -133 -121 -116 -120 -121 -116 -113 -117 -126 -114 -108
: ::	10 0 0 20 20 m	33 33 33 33	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	H102 H100 H104 H100 H100 H20 H20 H20 H101 H30 H20 H20 H20 H30 H30 H30 H30 H101 H101 H103 H40 H100 H101 H103 H40
0000	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	33 33 33 33 33	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	H102 H100 H104 H100 H100 100 120 L21 H101 100 121 L16 T24 130 131 138 T17 126 134 138 H100 H100 H00 H00 H000 H100 H00 H00
000000	10 0 0 20 20 m	33 33 33 33 33 33 33	0.00 0.00 0.00 0.00 0.00 0.00 0.00	6.00 6.00 6.00 6.00 6.00 6.00 6.00	-102 -100 -116 -100 -130 -130 -120 -121 -131 -133 -121 -116 -120 -121 -116 -118 -103 -117 -108 -47 -36 -103 -47 -46 -50 -85 -86 -76
00000000	12 12 12 22 22 22 22 23 24 24 2	90 90 93 93 90 90 90	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	H102 H100 H116 H100 H102 H102 H20 H21 H101 H003 H21 H106 H22 H303 H21 H106 H22 H22 H22 H30 H23 H107 H23 H27 H30 H107 H27 H28 H30 H50 H27 H28 H50 H50 H27 H30 H50 H50 H50 H30
000000	20 0 0 20 20 20 20 20 0 0 0 20	33 33 33 33 33 33 33 33 33 33	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	-102 -100 -104 -100 -119 -100 -119 -120 -120 -120 -120 -120 -120 -120 -120
	20 0 0 20 20 20 20 20 20 20 20 20 20 20	33 33 33 33 33 33 33 33 33	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	H102 H100 H116 H100 H102 H102 H20 H21 H101 H003 H21 H106 H22 H303 H21 H106 H22 H22 H22 H30 H23 H107 H23 H27 H30 H107 H27 H28 H30 H50 H27 H28 H50 H50 H27 H30 H50 H50 H50 H30
00000000	12 0 0 2 2 2 2 1 1 1 1 0 0 X X	33 33 33 33 33 33 33 33 33	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	-102 -100 -116 -100 -119 -100 -119 -120 -120 -120 -120 -120 -120 -120 -120
	11	20 20 33 33 33 33 33 33 33 33 33 33 33 33 33	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	-102 -100 -104 -100 -132 -120 -132 -120 -121 -120 -121 -120 -121 -120 -122 -122
		30 30 30 30 30 30 30 30 30 30 30 30 30 3	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	C.000 C.000 C.000 C.000 C.000 C.000 C.000 C.000 C.000 C.000 C.000 C.000 C.000	-102 -100 -114 -100 -130 130 120 121 -131 133 121 126 -132 133 121 136 -132 134 134 138 -133 134 134 138 -133 -134 134 138 -133 -134 134 -133 -134 134 -134 134 134 -134 134 134 -134 134 134 -134 134 134 -134 134 134 -134 134 134 -134 134 134
		33 33 33 33 33 33 33 33 33 33 33	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	-102 -100 -104 -100 -1192 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -120
	2	30 30 30 30 30 30 30 30 30 30 30 30 30 3	0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	H102 H100 H104 H100 H100 100 120 120 H101 100 121 121 H101 100 100 100 H102 100 100 100 H103 H103 H004 H00 H103 H103 H004 H00 H00 85 80 70 H00 85 70 80 H00 85 80 80 H00 85 86 70
		20 20 20 20 20 20 20 20 20 20 20 20 20 2	0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	-102 -100 -104 -100 -119 -100 -1190 -120 -120 -120 -120 -120 -120 -120 -12
		90 33 33 33 33 33 33 33 33 33 33 33 33 33	0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	-102 -100 -116 -100 -1192 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -120
		90 90 90 90 90 90 90 90 90 90 90 90 90 9	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	100 100 100 100 100 100 120
		90 90 90 90 90 90 90 90 90 90 90 90 90 9	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	-102 -100 -116 -100 -1192 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -121 -120 -120
		90 00 00 00 00 00 00 00 00 00 00 00 00 0	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	100 100 100 100 100 100 120
		000 000 000 000 000 000 000 000 000 00	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	-102 -100 -114 -100 -132 -132 -123 -121 -131 -133 -121 -136 -132 -133 -121 -136 -133 -134 -134 -138 -134 -135 -134 -138 -135 -137 -138 -144 -135 -137 -138 -144 -135 -137 -138 -144 -135 -137 -138 -144 -136 -137 -137 -136 -138 -138 -137 -136 -138 -138 -137 -138
		000 000 000 000 000 000 000 000 000 00	0,000 0 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	100 100 100 100 100 100 120
		50 00 00 00 00 00 00 00 00 00 00 00 00 0	0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	100 100 100 100 100 100 120
		00 00 00 00 00 00 00 00 00 00 00 00 00	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	100 100 100 100 100 100 120
		30 00 00 00 00 00 00 00 00 00 00 00 00 0	0.000 0.000	0.000 0.000	102 103 104 103 124 125
			0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	102 103 104 103 124 125
			0.000 0.000	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	102 103 104 103 124 125
		000 000 000 000 000 000 000 000 000 00	0.000 0.000	0.000 0.000	102 103 104 103 124 125
		000 000 000 000 000 000 000 000 000 00	0,000 0 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,00	0.000 0.000	100 100
		000 000 000 000 000 000 000 000 000 00	0,000 0 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,00	0.000 0.000	100 100 100 100 100 100 100 120
		000 000 000 000 000 000 000 000 000 00	0,000 0 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,00	0.000 0.000	100 100 100 100 100 100 120
			0.000 0.000	0.000 0.000	100
			0,000 0 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,00	0.000 0.000	100 100
			0.000 0.000	0.000 0.000	100 100
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			0,000 0 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,00	0.000 0.000	HIGH
			0,000 0,000	0.000 0.000	100
			0,000 0,000	0.000 0.000	100
			0,000 0,000	0.000 0.000	100

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1	2	23	0.00	6.00 6.00	-106 98 110
	2	20	0.00	0.00	-7G 73 89 90
-	3	33	0.00	0.00	5 a 5 f 33 ac
	_	_	0.00		26 90 93 -41
	-;	_	0.00		-94 -90 -97 -100
<u> </u>	- 1	_	0.00		-69 -57 -59 -67
		_			
1	2	-	0.00	0.00	-09 63 7L 67
	2	22	0.00	0.00	-S9 67 7L 7S
/	- 3	33	0.100	0.00	7a C 63 7a
	3	33	0.00	0.00	67 G 77 M
- :	-;	.,.,	0.00	6.100	-1/5 -(i): -9(i -9f)
- :	- 1		0.00		-1707 - 490 - 490 - 490
	-				
	-		0.00	0.00	-95 87 9L 90
	2		0.00	0.00	-98 100 00 00
	- 3	33	0.00	0.00	TTT 107 99 108
/	- 3	33	0.00	0.00	an 95 31 az
	-;		0.00	0.00	-115 -110 -106 -110
	7	777	0.00	0.00	-1/00 -500 -00 -1/4
	-		0.00	0.00	-10 28 22 11
	-				-E L6 11 14
	-		0.00	0.00	
	-		0.00		4 8 14 10
- :	·		0.00		-3 -4 -10 -8
	Γ.	.1.1	0.,00	0.00	-3 -3 -9 -13
	_	2.2	0.00	0.00	-10 7 10 20
	_		0.00	0.00	-107 100 100 101
-		-	0.00		29 15 10 az
		_	6.00		11 39 37 16
			0.00		-6 -10 -10 -6
					-1/3 -44 -4(1 -1/4 -1/3 -44 -4(1 -1/4
			0.00	0.00	-/FF -FH -/-
	-		0.00	0.00	-116 78 79 122
- 1	_	23	0.00	0.00	-1 6 E 4
/		33	0.00	0.00	T40 126 132 138
-		33	0.00	0.00	1 " 4 3
- :		.1.1	0.00	0.00	-154 -140 -1166 -146
	•		0.00		-# -1 -# -# -#
	_		0.00	0.00	-11 5 7 15
	-			0.00	-102 104 148 156
	-		0.00		-132 114 165 136
		-	0.00		76 TT TB 78
		_	0.00		42 (8 79 44
			0.00		-160 -160 -156 -160
- 7		:::	0.00	0.00	-149 -129 -139
	_	20	0.00	0.00	-110 80 105
	_	23	0.00	0.00	-110 110 100
				0.00	Td.: 85 80
		_	0.00		T23 105 80
				0.00	3 -1(5 -4)
- :		_		6.00	3 -41 -44
	\vdash	-			
	-			0.00	-41 35 22
	-		0.00		-41 33 40
	Ŀ			0.00	AT 49 113
		33	0.100	0.00	25 db 17
	·	.i.i	0.00	0.00	-02 -14 -21
		.1.1	0.00	0.00	-21 -33 -x1
	Н			0.00	-18 17 13
	⊢			0.00	-18 9 17
	-				
				0.00	17 9 10
				0.00	Tal. 17 10
	·		0.00		-30 -30 -22
- :				0.00	-cc -co -cc
		.i.i	10.00		
					-00 13 24
	_	22	0.00	0.00	-00 13 04 -30 22 04
		22	0,00 0,00	0.00 0.00	-30 22 24
1	-	22 22 33	0.00 0.00 0.00	0.00 0.00 0.00	-30 22 24 -52 48 40
- /	-	33 33 33	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	-30 22 24 -52 48 40 -45 80 40
- 1 - 1 - 1		22 23 33 E	0.00 0.00 0.00 0.00 0.00	6.00 6.00 6.00 6.00 6.00	-36 22 24 62 63 66 66 66 66 66 66
		20 20 30 30 30 30 30	0.00 0.00 0.00 0.00 0.00	6.00 6.00 6.00 6.00 6.00 6.00	-30 22 24 -32 48 70 -40 -30 -40 -40 -00 -34 -51 40 34
- 1 - 1 - 1		000000000000000000000000000000000000000	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00	-30 22 24 -32 48 40 -40 -30 40 -40 -30 -34 -50 40 24 -100 104 105
		000000000000000000000000000000000000000	0.00 0.00 0.00 0.00 0.00 0.00	6.00 6.00 6.00 6.00 6.00 6.00	-30 22 24 -32 48 40 -40 -30 40 -40 -30 -34 -50 40 24 -100 104 105
0 × × 6 0 0		00 00 00 00 00 00 00 00	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00	-30 22 24 -32 48 40 -40 -30 40 -40 -30 -34 -50 40 34 -100 104 105
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		20 20 33 33 33 33 33 33 33	0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	130 22 24 24 28 78 70 46 36 70 46 47 47 47 47 47 47 47
		20 33 33 33 33 33 33 33 33 33	0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06	2.000 2.000 0.000 0.000 0.000 2.000 0.000 0.000 0.000	130 22 24 28 78 70 46 87 70 46 47 47 47 47 47 47 47
		20 20 33 33 33 33 33 33 33 33	0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	130 22 24 28 78 70 46 87 70 46 47 47 47 47 47 47 47
		20 20 33 33 33 33 33 33 33 33 33	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	130 22 24 24 28 78 70 26 27 28 70 28 27 28 28 28 28 28 28
		20 20 33 33 33 33 33 33 33 33 33	0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	130 22 24 28 78 70 46 87 70 46 47 47 47 47 47 47 47

Elenco tipi plinti/pali

Simbologia

Comm. = Commento Crit. = Numero del criterio di progetto Dp = Diametro pali Lp = Lunghezza pali R = Rotazione testa B - Bloccata L = Libera Tipo = Tipologia

P = Palo

Tl = Numero del tipo plinto/palo

Tp = Tipo palo

T = Trivellato

T1	Tipo	Tp	Comm.	Lip <m>></m>	R	Dp <m></m>	Crit.
1	P	Ť	Palo singolo	25.00	L	1.20	· 3

Elenco plinti/pali

Simbologia

Kt = Coeff. di sottofondo su suolo elastico alla Winkler Nodo = Nodo plinto/palo PL = Plinto/Palo Tl = Numero del tipo plinto/palo

PL	Tl	Nodo	Kt <dan cmc=""></dan>
1	1	-40	
2	1	-104	
3	1	-138	
4	1	-152	
5	1	-153	
6	1	-139	
-7	1	-105	
8	1	-41	
9	1	-23	
10	1	-17	Ant.
11	1	-22	
12	1	-4	
13	1	-3	
14	1	-7	
15	1	-15	
16	1	-29	
17	1	-44	
18	1	-78	
19	1	-126	
20	1	-142	
21	1	-154	
22	1	-162	
23	1	-166	
24	1	-167	
25	1	-163	
26	1	-155	TT-
27	1	-143	Her.
28	1	-127	
29	1	-81	
30	1	-45	
31	1	-28	(0.0 (m) m)
32	1	-16	
33	1	-8	

Carichi

Elenco tipi CCE

Simbologia

y max = Coeff. y max y min. = Coeff. y min. ψ_0 - Coeff. ψ_0 $\psi_{0,s}$ = Coeff. ψ_{0} sismico (D.M. 96) ψ_1 = Coeff. ψ_1 ψ_2 = Coeff. ψ_2 Comm. - Commento Durata = Durata del carico P = Permanente Tipo = Tipologia G = Permanente Qv = Variabile vento

Tipo CCE = Tipo condizione di carico elementare

Tipo CCE	Comm.	Tipo	Durata	γ min.	у таж	\$ 0	V 1	\$ 2	Ψ0,s
1	D.M. 18 Permanenti strutturali	G	P	1.00	1.35				

Condizioni di carico elementari

Simbologia

```
CCE = Numero della condizione di carico elementare
Comm. - Commenta
Dir. - Direzione del vento
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Sic. = Contributo alla sicurezza
S = a sfavore
Tipo - Tipología di pressione vento
M = Massimizzata
E = Esterna
I - Interna
Tipo CCE - Tipo di CCE per calcolo agli stati limite
Var. = Tipo di variabilità
B = di base
s = Coeff. di riduzione (T.A. o S.L. D.M. 96)
```

CCE	Comm.	Tipo CCE	Sic.	Var.	8	Dir.	Tipo	Mx	му	Mz	Јрж	Jpy	Jpz
1		1	S		1.00			1.00	1.00	0.00	0.00	0.00	1.00

Elenco carichi nodiCondizione di carico n. 1: Carichi concentrati

Simbologia

and the same of th			
ponente X	della	forza	applicata
ponente Y	della	forza	applicata
ponente Z	della	forza	applicata
ento into	rno all	'asse	X
ento into	rno all	'asse	Y
ento into	rno all	'asse	2
umero del	nodo		
	ponente X ponente Y ponente Z ento into ento into ento into	ponente X della ponente Y della ponente Z della ento intorno all ento intorno all	ponente X della forza ponente Y della forza ponente Z della forza ento intorno all'asse ento intorno all'asse ento intorno all'asse

Nodo	Fx	Fy	Fz	Mx	My	Mz
	<dan></dan>	<dan></dan>	<dan></dan>	<danm></danm>	<danm></danm>	<danm></danm>
-RR	164800.00	0.00	722200.00	20303400.00	0.00	1806100.00

Elenco carichi elementi bidimensionaliCondizione di carico n. 1: Carichi uniformi

Simbologia

```
Bid. = Numero del muro/elemento bidimensionale
DC = Direzione del carico
G = secondo gli assi globali
L = secondo gli assi locali
N1 = Nodol
N2 = Nodo2
N3 = Nodo3
N4 = Nodo4
Ox = Carico in dir. X
Qy = Carico in dir. Y
Qz = Carico in dir. Z
T - Tipo di carico
PP = Peso proprio
M = Manuale
```

Bid.	N1	N2	м3	N4	т	DC	Qx <dan mq=""></dan>	Qy <dan mq=""></dan>	Qz <dan mq=""></dan>
2					М	Œ	0.00	0.00	2730.00

Elenco peso proprio elementi bidimensionali

Simbologia

Comm. = Commento Mat. = Materiale P = Peso specifico PQ = Peso specifico per unità di superficie Spess. = Spessore Tb = Numero del tipo muro/elemento bidimensionale

122	120000-01	Spess.	97300	P	PO
Tb	Comm.	<cm></cm>	Mat.	<dan mc=""></dan>	<dan mg=""></dan>

1	Platea h=1.50 mt	150.00	Calcestruzzo	classe	C40/50	2500.00	3750.00
2	Platea H=2.6 mt	260.00	Calcestruzzo	classe	C40/50	2500.00	6500.00
3	Platea H= 3.50 mt	350.00	Calcestruzzo	classe	C40/50	2500.00	8750.00

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con: ModeSt ver. 8.26, licenza n. 7116, prodotto da Tecnisoft s.a.s. - Prato La struttura è stata calcolata utilizzando come solutore agli elementi finiti: Xfinest ver. 9.4.3, prodotto da Ce.A.S. S.r.1. - Milano Tipo di normativa: stati limite D.M. 18

Tipo di calcolo: statico

Vincoli esterni: Considera sempre vincoli assegnati in modellazione

Schematizzazione piani rigidi: nessun impalcato rigido

Modalità di recupero masse secondarie: mantenere sul nodo masse e forze relative

Generazione combinazioni

- Lineari: Sl
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente

Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Si
- Check sequenza di Sturm: Si
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

Dati struttura

- Edificio esistente: No
- Tipo di opera: Grande opera
- Vita nominale V_N: 100.00
- Classe d'uso: Classe III
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Ambienti di caricoSimbologia

N = Numero Comm. = Commento F = azioni orizzontali convenzionali SLU = State limite ultimo SLR - Stato limite per combinazioni rare SLF = Stato limite per combinazioni frequenti SIQ/D = Stato limite per combinazioni quasi permanenti o di danno S = S1 N = No

N	Comm.	1	SLU	SLR	SLF	SLQ
1	Calcolo statico	S	S	S	S	S

Elenco combinazioni di carico simboliche

Simbologia

CC = Mumero della combinazione delle condizioni di carico elementari Comm. = Commento TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara

SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

cc		Co	mm.	TCC	1		
1	Amb.	1	(SIAI)	SLU	y max		
2	Amb.	1	(SLE R)	SLE R	1		
3	Amb.	1	(SLE F)	SLE F	1		
4	Amb.	1	(SLE Q)	SLE Q	1		

Genera le combinazioni con un solo carico di tipo variabile come di base: No

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

```
An. = Tipo di analisi
L = Lineare
NL = Non lineare
Bk = Buckling
S = Si
N = No
CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
```

CC		Ca	mm.	TCC	An.	Bk	1
1	Amb.	1	(SLU)	SLU	L	N	1.35
2	Amb.	1	(SLE R)	SLE R	L.	N	1.00
3	Amb.	1	(SLE F)	SLE F	L	N.	1.00
4	Amb.	1	(SLE Q)	SLE Q	L	N	1.00

Spostamenti dei nodi

Simbologia

```
CC = Numero della combinazione delle condizioni di carico elementari
Nodo = Numero del nodo
Rx = Rotazione intorno all'asse X
Ry = Rotazione intorno all'asse Y
Rz = Rotazione intorno all'asse Z
Sx = Spostamento indir. X
Sy = Spostamento in dir. X
Sy = Spostamento in dir. Z
TCC = Tipo di combinazione di carico
SIU = Stato limite ultimo
SIE R = Stato limite d'esercizio, combinazione rara
SIE F = Stato limite d'esercizio, combinazione frequente
SIE Q = Stato limite d'esercizio, combinazione quasi permanente
```

I valori degli spostamenti nodali per CC di tipo sismico sono amplificati come da normativa

Nodo		Sx <cm></cm>	cc	TCC	Sy <cm></cm>	cc	TCC	Sz <cm></cm>	cc	TCC	Rx <rad></rad>	cc	TCC	Ry <rad></rad>	œ	TCC	Rz <rad></rad>	cc	TCC
-169	Max	-0.18	2	SLE R	-0.00	2	SLE R	-1.71	2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	2	SLE
-169	Min.	+0.25	1	SLU	-0.01	1	SLU	-2.31	1	SLU	0.00	1	SLU	0.00	1	SLU	0.00	1	SLU
-168	Max	-0.18	2	SLE R	0.01	1	SLU	-1.71	2	SLE R	0.00	2	SLE R	0.00	1	SLU	0.00	2	SLE
-168	Міп.	-0.25	1	SLU	0.00	2	SLE R	-2,31	. 1	SLU .	0.00	1	SLU	0.00	-2	SLE R	0.00	1	SLU
-167	Max	-0.18	2	SLE R	-0.00	2	SLE R	-1.70	2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	1	SLU
-167	Min.	-0.25	1	SLU	-0.01	1	SIJ	-2.30	1	SLU	0.00	1	SLU	0.00	1	SLU	0.00	1	SLU
-166	Max	-0.18	2	SLE R	0.01	1	SLU	-1.70	2	SLE R	0.00	.2	SLE R	0.00	1	SLU	0.00	1	SLU
-166	Min.	-0.25	1	SLU	0.00	2	SLE R	-2.30	1	SLU	0.00	1	SLU	0.00	2	SLE R	0.00	-1	SLU
-165	Max	-0.19	2	SLE R	-0.01	2	SLE R	-1.64	2	SLE R	0.00	2	SLE R	0.00	. 2	SLE R	0.00	2	SLE
-165	Min.	-0.25	1	SLU	-0.02	1	SLU	-2.21	1	SLU	0.00	1	SLU	0.200	1	SLU	0.00	1	SLU
-164	Max	-0.19	2	SLE R	0.02	1	SLU	-1.64	2	SLE R	0.00	2	SLE R	0.00	1	SLU	0.00	2	SLE
-164	Min.	-0.25	1	SLU	0.01	2	SLE R	-2.21	1	SLU	0.00	1	SLU	0.00	. 2	SLE R	0.00	1	SLU
-163	Max	-0.19	2	SLE R	-0.01	. 2	SLE R	-1.64	2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	1	SLU
-163	Min.	-0.25	1	SLU	-0.02	1	SLU	-2.21	1	SLU	0.00	1	SLU	0.00	1	SLU	0.00	1	SLU
-162	Max	-0.19	2	SLE R	0.02	1	SLU	-1.64	2	SLE R	0.00	2	SLE R	0.00	1	SLU	0.00	1	SLU
-162	Min.	-0.25	1	SLU	0.01	2	SLE R	-2.21	1	SLU	0.00	1	SLU	0.00	2	SLE R	0.00	1	SLU
-161	Max	-0.19	2	SLE R	-0.00	. 2	SLE R	-1.69	-2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	. 2	SLE
-161	Min.	-0.26	1	SLU	-0.01	1	SLU	-2.29	1	SLU	0.00	1	SLU	0.00	1	SLU	0.00	1	SLU
-160	Max	-0.19	2	SLE R	0.00	1	SIU	-1.70	2	SLE R	0.00	2	SLE R	0.00	1	SLU	0.00	2	SLE
-160	Min.	-0.26	1	SLU	0.00	2	SLE R	-2,29	1	SLU	0.00	1	SLU	0.00	2	SLE R	0.00	1	SLU
-159	Max	-0.19	2	SLE R	-0.02	2	SLE R	-1.50	2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	2	SLE
-159	Min.	-0.26	1	SLU	-0.03	1	SLU	-2.03	1	SLU	0.00	1	SLU	0.00	1	SLU	0.00	I	SLU
-158	Max	-0.19	2	SLE R	0.03	1	SLU	-1.51	2	SLE R	0.00	2	SLE R	0.60	1	SLU	0.00	2	SLE.
-158	Min.	-0.26	1	SLU	0.02	2	SLE R	-2,03	-1	SLU	0.00	1	SLU	0.00	2	SLE R	0.00	1	SLU
-157	Max	-0.19	2	SLE R	-0.01	2	SLE R	-1.63	- 2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	-2	SLE
-157	Min.	-0.26	1	SLU	-0.02	1	SLU	-2.20	1	SLU	0.00	1	SLU	0.00	1	SLU	0.00	1	SLU
-156	Max	-0.19	2	SLE R	0.02	1	SLU	-1.63	2	SLE R	0.00	2	SLE R	0.00	1	SLU	0.00	2	SLE
-156	Min.	-0.26	1	SLU	0.01	2	SLE R	-2.21	1	SLU	0.00	1	SLU	0.00	. 5	SLE R	0.00	1	SLU
-155	Max	-0.19	2	SLE R	-0.02	2	SLE R	-1.51	2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	1	SLU
-155	Min.	-0.26	1	SLU	-0.03	. 1	SLU	-2.03	1	SLU	0.00	1	SLU	0.00	1	SLU	0.00	1	SLU
-154	Max	-0.19	2	SLE R	0.03	1	SLU	-1.51	2	SLE R	0.00	2	SLE R	0.00	1	SLU	0.00	1	SLU
-154	Min.	-0.26	1	SLU	0.02	2	SLE R	-2.04	1	SLU	0.00	1	SLU	0.00	2	SLE R	0.00	1	SLU
-153	Max	-0.19	2	SLE R	-0.01	2	SLE R	-1.65	2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	1	SLU
-153	Min.	-0.26	1	SLU	-0.01	1	SLU	-2.23	1	SLU	0.00	1	SLU	0.00	- 1	SLU	0.00	1	SLU
-152	Max	-0.19	2	SLE R	0.01	1	SLU	-1.65	2	SLE R	0.00	2	SLE R	0.00	1	SLU	0.00	1	SLU
-152	Min.	-0.26	1	SLU	0.01	2	SLE R	-2.23	1	SLU	0.00	1	SLU	0.00	2	SLE R	0.00	1	SLU
-151	Max:	-0.19	2	SLE R	-0.00	2	SLE R	-1.66	2	SLE R	0.00	2	SLE R	0.00	2	SLE R	0.00	2	SLE
-151	Min.	-0.26	1	SLU	-0.00	1	SLU	-2.24	1	SLU	0.00	1	SLU	0.00	1	SLU	0.00	1	SIAI
-150	Max	-0.19	2	SLE R	0.00	1	SLU	-1.66	2	SLE R	0.00	2	SLE R	0.00	1	SLU	0.00	2	SLE

										F	∂elaz	ioi	ne di	calc	olo	5			
-100	MLT.	-0.16	۱.	920	0.00	1	ى طات	-2,14	۱ -	أ ربيع	0.00	<u> </u>	SEU	0.00		ال علالاً	6.00	:	SEC
-149	Max	-0.10	2	912 0	-0.02	C.	ک طات	-1,52	C.	912 J	0.00	2	SLE R	0,66	cı	9 <u>4</u> 2	0.00	-	SLE R
1.4%	И г.	0.26	·	97.0	0.00	=	STO	4.4.	·	97.0	0.00	•	STC	0.00	٠	970	0.00	·	STU
1.1:	Haz	0.20		977.5	0.00	=	SIC	1.4"		977.5	0.00	-:	ят в	0.00	٠	975	0.00	٠:	STR R
-14%	М г.	-0.00	Ŀ	97.0	0.00		आह २	-0.7cm	Ŀ	97.0	0.00	·	31.0	0.00	/	977 R	0.00	·	31.0
	Max	-0.00	_	97 T R	-0.00	٠.	आह २	-" . fc"	_	97 T R	0.00	- ":	साम	0.00	/	977 R	0.00	- ":	31 T E
_	Mir.	-0.16	<u> </u>	9_J	-0.01	1	öL.	-2.17	-	Y_ J	0.00	-	SEU	0.00	_	لدو	0.00	-	SEU
-146	Max	-0.10	- 2	922.0	0.01	1	oL.	-1.51	2	_	0.00	2		0,00	-	92J	0.00	- 2	SLE R
_	H r.	0.76		97.7 97.7 T	0.01		SIF 3	4.17		97.7 97.7 5	0.00	<u> </u>	STU	0.00		977 7	0.00	<u> </u>	310
-14-	Maz Mir.	-0.20 -0.07	H	97 TI	-0.03 -0.04	1	STE B STU	-1.78	H	97 D	0.00	-	धान ह	0.00	-	977 T. 978	0.00	-	STOR
- 44	_	-0.00	Η,	9773	0.04	_	310	-1.32		57 T S	0.00		31 7 F	0.00		97.0	0.00		31 7 F
-144	_	-0.17	ŕ	Y_J	0.03	÷	ى طات	-1.78	ŕ	A 1	0.00	H	SEC	0.00	2	9 AZ 0	0.00	H	SEU
-143	Max	-0.10	2	9_2 /	-0.03	-	۰. طات ۲. طات	-1,30	2	Y_2 /	0.00	2		0.00	2	9 A 7	0.00	1	SEU
14.5	н г.	0.27	-	97.0	0.04		SIC	1.73	-	97.0	0.00	-	STC	0.00	·	970	0.00	-	STC
1.47	Haz	0.20		977.5	0.04	ï	SIC	13		:: T T	0.00	-:	ят в	0.00		970	0.00		STU
-140	М г.	-0.00	·	97.0	0.0%	.:	आह २	47.79	·	97.0	0.00	-	31.0	0.00	-	977 S	0.00	-	31.0
-141	Max	-0.00	7	97 T R	-0.00		সাদ ৪	-1.50		97 T R	0.00	":	RITE	0.00	/	977 S	0.00	11	31 T E
-141	Mir.,	-0.17	_	9_J	-0.02	1	ت.Lc	-2.00	_	Y_ J	0.00	-	SEC	0.00	-	943	0.00	-	SEU
-140	Маж	-0.10	2	912.0	0.02	1	۵Lu	-1,50	2	912.0	0.00	2	SLE R	0.00	-	943	0.00	2	SLE R
1.40	н г.	0.77	Ŀ	97.0	0.01	/	SIFR	41.03	Ŀ	97.0	0.00	Ŀ	STC	0.00		977 7.	0.00	Ŀ	STC
-1,39	Mhix	-0.00	4	97.7 R	-0.00		সাদ ২		4	97.7 R	0.00	1	31 T E	0.00	/	977 R	0.00	Ļ.	31.0
-1,39	М г.	-0.00	Ŀ	97.0	-0.00	-	SIL	-1,94	Ľ	97.0	0.00	Ļ.	31.0	0.00	Ľ.	9701	0.00	Ľ	31.0
	Max	-0.10	12	922.0	0.02	1	aL.	-1,44	\perp^2	9 <u>_2</u> 2	0.00	2		0.00	-	94J 8 2 .	0.00	 -	SEU
1.33	Min.	-0.17	-	910 977 7	0.02	-	01E 0	-1,94	-	910 977.5	0.00	-	SEU SEU D	0.00		825 C	0.00	 -	SIC R
1.27	Maz Mort	0.20	-	10 TO	0.03	1	STE R		H	10 TO	0.00	H	STOR	0.00	-	970 970	0.00	+:	STU
-176	Mox	-0.00		9773	0.00	1	SIL	-1.25		977.3	0.00		31 T B	0.00	-	9701	0.00	٠.	31 T B
-17.716	М г.	-0.07	Ť	97.0	0.00	7	SIF R	-1,32	Ť	97.0	0.00	÷	31.0	0.00		977 S	0.00	-	31.0
-130	Max	-0.10	2	9_2 /	-0.02		ک طات	-1.36	2	9_2 /	0.00	2	SLE R	0.00	2	922.7	0.00	2	SLE R
-130	Mir.,	-0.18	-	Y_ J	-0.02	1	۵Lu	-1,20	-	Y_ J	0.00	-	SEU	0.00	-	950	0.00	-	SEU
1.4	Haz	0.26		977.5	0.00	=	STO	1.56		977.5	0.00	-:	ят в	0.00	٠	970	0.00	-:	STO R
	Η г.	0.28	·	97.0	0.00	1	សាគ ខ	1.:3	·	97.0	0.00	·	STC	0.00	:	T.	0.00	·	BTC
-1,77	Mhix	-0.61	_	97 T R	-0.00		সাদ ২	-1.4a	_	9773	0.00	η:	सामा	0.00	/	977 R	0.00	- 11	साम ह
-1,7,7	М г.	-0.00	Ľ	97.01	-0.00	_	SIU	7.	Ľ	97.0	-0.00	Ŀ	31.0	0.00		9701	0.00	Ŀ	31.0
-131	Max	-0.10	2	922.0	0.00	1	ت.L.	-1,43	2	9 <u></u> ,	0.00	2	_	0.00	-	لدو	0.00	2	SLE E
-131 1.41	Mir. Maz	-0.28 0.21	-	910 977 7	0.00	-	SIF 3	-1.96	-	910 977.5	-0.00	-	SEU SEU R	0.00	2	877 J	0.00	-	SEU SEU R
11	И г.	0.28	Η.	97.0	0.00		SIC	1 , 40	Η.	97.0	0.00	H	STU	0.00		970	0.00	<u> </u>	STU
-1,340	Mhox	-0.01		577.3	0.01	1	310	-1.47		577 3	0.00	-	31 T F	0.00		970	0.00	100	31 7 F
-1,30	М г.	-0.08	┍	97.0	0.00		आह २	-1.97	┍	97.0	-0.00	·	31 tr	0.00	7	977 R	0.00	·	31.0
-119	Мак	-0.11	2	9_2 /	-0.03	-	ى طات	-1,00	2	Y_2 0	0.00	2	SLE E	0.00	2	922.0	0.00	2	SLE R
-119	MLT.	-0.18	-	9_J	-0.04		۵Lu	-1.48	-	Y_ J	0.00	-	SEU	0.00	1	940	0.00	-	SEU
17:	Haz.	0.7		977.5	0.04	Ξ	SIC	1.03		977.7	0.00	::	ят в	0.00		970	0.00	٠:	STO R
	н г.	0.28	Ŀ	97.0	0.03		STF 3	1.48	Ŀ	97.0	0.00	·	STU	0.00		977 7	0.00	Ŀ	BTC
-1000	_	-0.00	-	97 T R	-0.10%	_	आह २	_	4	97 7 R	0.00	- 1	31 T F	0.00	/	977 R	0.00	_	31.0
	М г.	-0.00	Ĺ	97.0	-0.04		SIL	-1.70	Ĺ	97.0	0.00	Ļ	31.0	0.00	_	9701	0.00	-	31.0
-110	Min.	-0.11	-	9_2 /	0.04	1	ملت کاطات	-1.11 -1.10	-	9_2 2	0.00	1	SLE R	0,00	-	السائ	0.00	_	SEU
	_	-0.18 0.71	-	910 977 7	0.00	-	STER		-	910 977.5	0.00	-	SEU STOR	0.00	-	922 J 977 D	0.00	-	SEC SEC R
	Maz Mort	0.28	 	97.7	0.01		STU	1.56	H	97.0	0.00	Ë	STU	0.00	H	970	0.00	- -	31 C
-104	_	-0.51	7	9773	0.01		310	-1.34	7	9773	0.00	7	31 T F	0.00	·	9701	0.00	1	31 T F
_	Mir.	-0.00	Г	97.0	0.01		आह ३	_	Г	97.0	-0.00	F	31.0	0.00	-	977 B	0.00	_	31.0
-113	Мак	-0.11	2	9120	-0.03	1	ک طات	-1.13	C.	Y_2 0	0.00	2	SLE R	0,00	2	922.0	0.00	2	SLE R
-113	Mir.,	-0.18	_	Y_ J	-0.03	1	ت.Lد	-1,23	_	Y_ J	0.00	-	SEU	0.00	_	الدة	0.00	-	SEU
	Haz.	0.7		977.5	0.03		STO	1.1.:		977.	0.00	::		0.00		970	0.00	.:	STT R
		0.28	Ļ.	97.0	0.03		STF R	1.56	Ľ	97.0	0.00		STC	0.00		977 7.	0.00	<u>.</u>	BTC
_	Mhox	-0.01	4	97 T R	-0.00	_	সাদ ৪		4	97 T R	0.00	-:	31 T F	0.00	/	977 R	0.00	_	31 T F
	Mir.	-0.00	بَ	97 (I	-0.00		STU	-1.70	Ļ	97.01 00.00	-0.00	Ļ	31.0	0.00	Ė	9701	0.00	_	31.0
-110	Max Min.	-0.11	12	822.0	0.00	-	oL.	-1,30	1	822.0	-0.00	1	SLE R	_	-	السائ مارس	0.00	_	SLE E
	Min.	-0.18	-	910 977 7	0.00	-	SIF 3	-1.79	-	910 977.5	-0.00 -0.00	-	SEC STOR	0.00		922 J 977 J	6.00	_	SEU SEU R
_	Maz Mir.	0.28	 	10 TO	0.03		STU	1.18	H	107.77	0.00	-:	91 G R	0.00	-	97.01	0.00	 	STO R
-113	_	-0.00	7	9773	_		310	-1.18		9773	_	2	31 T F	0.00		9701	0.00	2	31 T F
	Mir.	-0.18	Ĺ	Y_J	0.02	-	ک طات	-1.50	-	Y_J	-0.00	Ė	SEC	0.00	2	9 AZ 3	0.00	-	SEC
-117	_	-0.11	2	9_2 /	-0.01	-	ک طات	-1,17	2		0.00	2	SLE R		2		0.00	-	SLE R
	И г.	0.28	·	97.0	0.01	1	STO	1.95	·	97.0	0.00		STC	0.00		9701	0.00	·	STC
115	Haz.	0.7		977.5	0.00	7	នាខេ	1		977.5	0.00	.:	STT R	0.00		977 7.	0.00	.:	STT R
-116	М г.	-0.00	Ŀ	97.0	-0.00	1	3100	-1,79	Ē	97.0	-0.00	·	31 m	0.00	·	9701	0.00	Ŀ	31.0
-11.5	_	-0.01	/	97 T R	0.01	1	310		1	9773	0.00	1	31 T F	0.00	·	97.0	0.00		31 T F
_	Mir.	-0.18	-	91. J	0.00		ک طات	-1.76	-	9_J	-0.00	-	SEC	0.00	2	9 <u>22</u> 0	0.00	_	SEU
-114	_	-0.11	2		0.01	1	aL.	-1,18	2	_	0.00	2		0.00	-	923	0.00	2	SLE E
-	H r.	0.28	Ë	97.77 97.77 T	0.00	-	SIF 3	1.77	Ë	9000 90000	0.00	Ė	STU	9.00	-:-	977 T	0.00	<u> </u>	STU
-	Maz Mort	-0.7%	H	97 TI	-0.00 -0.01	-	STE B STU	-1.27	H	97 TI	-0.00 -0.00	۳	धान ह	0.00		977 (5. 978)	0.00	1	धारा ह
-110	_	-0.00		97 7 R	10.00	_	SIU	-1.57	H	97 7 R	7.100	-	31 T F	0.00	-	9781	0.00	_	31 T F
<u> </u>			<u> </u>	· `						· `					_				

										F	Relaz	ioi	ne di	calc	ole	5			
-111	Min.	-0.18	۱.	9_0	0.00	1 :	ى علت	-1.74	۱.	أربوا	-0.00	Ĭ :	SEU	0.00		ر تسوراً	0.00	1 :	SEC
	Маж	-0.11	2	9220	0.00	1	۵L۷	-1,14	2	Y_2 0	-0.00	2	SLE R	0.66	-	السلا	0.00	-	SLE R
. 11	И г.	0.28	·	97.0	0.00	1	ខាត	1.58	٠	97.0	0.00	·	STU	0.00		977 7	0.00	·	STC
110	Haz.	0.7		977.5	0.00	ï	STO	1.73	:	977.7	0.00	٠:	STO R	0.00	٠	9721	0.00	٠:	STT R
-110	М г.	-0.00	Ŀ	97.0	0.00	:	সাদ ২	±1.50	_	97.01	-0.00	•	31.0	0.00	/	977 R	0.00	•	31.0
_		-0.01	_	97 T R	-0.00		সাদ ২	-1.579	4	9773	11 11	- 1	R CIE	0.00		9701	0.00	- 1	साराह
	Mir.	-0.18	<u> </u>	9_J	-0.01	1	۵L.	-1.56	-	9_J	-0.00	<u> </u>	SEU	0.00	2		0.00	-	SEU
-108	Max	-0.11	-	81.0 81.0	-0.01	-	ک طلت دورت	-1,5_	-	9 <u>_2</u> 2	0.00	2	SLE R	0.00	- 2	9 <u>22</u> 0	0.00	2	SLE E
165	Maz.	0.23		:: .) :: 7 7 7	0.00	-	STO	1.04		197 TO T	0.00	<u> </u>	STO STOR	0.00		9757 9757	0.00	<u> </u>	STC STC R
-1777	Mir.	-0.0%	⊢	97.0	0.07	-	STE R	-1.34	H	97 O	-0.00	-	31.0	0.00		977 3	0.00	-	31.0
-17.5	_	-0.01		5773	0.07	1	310	-1.57		9773		-	31 7 B	0.00	÷	97.0	0.00	2	31 7 F
-100	Mir.,	-0.10	-	Y_ J	0.01	-	ى طات	-1.55		Y_ J	-0.00	<u> </u>	SEU	0.00	2	922.0	0.00	-	SEU
-100	Max	-0.11	2	9_2 0	-0.02	2	ک طات	-1.67	2	9_2 0	0.00	2	SLE R	0,00	2	922.0	6.00	-	SEU
100	н г.	0.73	·	97.0	0.03	ï	STO	1.4.:		97.0	0.00		ST C	0.00		9701	0.00	·	STC
1.04	Haz	0.7		977.5	0.03	ï	STO	1.07	:	977.7	0.00	٠:	STO R	0.00		9721	0.00	·	STC
-104	Мir.	-0.0%	·	97.01	0.00		आह २	-1.4a	Ė	97.01	-0.100	-	31 t.	0.00	/	977 R	0.00	-	31.0
-170.3	Max	-0.51	\perp	97 T R	-0.00	:	সাদ্ভ		_	9773	0.00	-:	ST T F	0.00	_	957 R	0.00	":	31 T E
-103	Mir.	-0.10	<u> </u>	870	-0.02	-	ōL.	-1.58	_	91 J	-0.00	<u> </u>	SEU	9,66	_	الدة	0.00	-	SEU
-101	Max	-0.11	12	912 J	0.01	1	öL.	-1.17	-	Y_2 2	0.00	2	SLE R	9,00	-	الدو	0.00	2	SLE R
102	Иr.	0.23	H	97.0	0.01	4	STF 3	1.58	Ė	97.77 97.77 B	0.00	<u> </u>	STU	0.00	··	977 7	0.00		STU
-101 -101	Mhox Milinia	-0.00 -0.00	H	97.7 K	-0.00 -0.00	7	STER STU	-1.61 -1.63	H	97.71 R	-0.00 -0.00	 	सामा सामा	0.00	-	970) 977) R	0.00	-	सारा ह
-100	м г.	-0.11	^	9_2 /	0.00	-	اد. کاطات	-1,10	_	9_2 J	-0.00	2		0.00	H	877 871 ×	-0.00	,	310 315 E
-100	Mir.	-0.13	۲	9_J	0.00	1	۸ عدد ملد	-1.52	Ë	9_J	-0.00	+	SEC	0.00	2	5 A 7	-0.00	-	SLU
	Haz.	0.7	Ē	977.5	0.00	-	SIC	1.18	Ē	::	0.00	-	SEC B	0.00	Ť	970	0.00	-	STO R
	И г.	0.23	ŀ	97.0	0.00	-	SIFR	1 . 13	·	107.07	0.00	<u> </u>	STC	0.00		::	0.00	Ť	STC
-93	Mhox	-0.01		97 T R	0.01	1	SIU	-1.18		9773	-0.00	":	31 T. F.	0.00	7	977 S	-0.00	":	31 T. F.
-5:	М r.	-0.0%	·	97.0	0.00	:	সাদ ২	-1,50	ŀ	97.01	-0.00	-	31 t.	0.00	·	9701	-0.00	·	31.0
-97	Max	-0.11	2	9220	-0.01		ک طات	-1,13	cı	912 0	0.00	2	SLE R	0,66	2	922.0	0.00	2	SLE R
-97	Mir.	-0.10		Y_ J	-0.01	1	۵L۷	-1,53	-	Y_ J	-0.00	-	SEU	0.00	-	السلا	0.00	-	SEU
40	Ha/	0.7		977.	6.00	-	STO	1.1.:	-	:::	0.00	-:	STT R	0.00	·	97.0	0.00	-:	STT R
	И г.	0.73	Ŀ	97.0	0.00	-	STF 3	1 . 1	Ŀ	97.71	0.00		er c	0.00		977 7	0.00		STU
_	Mhix	-0.01	+	97 7 R	0.07	1	SIU	-1.14	4	97 7 R	-0.100	-	31 7 F	0.00		9701	0.00	-	31 7 F
-9.5 -94	Mar.	-0.09 -0.11	_	910 912 0	-0.00		STE R	-1.13	2	97.0 92.2 0	-0.00 -0.00	-	31 U	0.00	\vdash	977 R 940	-0.00 -0.00	,	SLE R
_	Max Min.	-0.13	<u> </u>	9_0	-0.00	1	ک طلت ملت	-1,13	_	9_J	-0.00	- 2	SLE R SLU	0.00	2		-0.00	-	SEU
40	Haz	0.27	- -	977.5	0.00	-	SIFR	1.13		::	0.00	-	STO R	0.00	-	977 7	0.00	-	STO R
4.1	Η г.	0.23	·	97.0	0.00	-	STO	1.40	$\overline{}$	97.71	0.00	-	STU	0.00	·	97.0	0.00		STU
-90	Max	-0.02	7	577.3	0.00	1	310	-1.1%	$\overline{}$	977.3	_	7	31 T F	0.00	·	9701	-0.00	73	31 T E
-97	М г.	-0.0%	一	97.0	0.00		आह ३	-1.51	┍	97.0	-0.00	-	31 t.	0.00	7	977 R	-0.00	-	31 tr
-91	Max	-0.12	2	912 0	0.01	1	۵Lu	-1.10	cı	Y_2 0	-0.00	2	SLE R	0.00	-	السلا	0.00	2	SLE R
-91	MLT.	-0.10	_	9_J	0.01	-	ک طات	-1,48	-	Y_ J	-0.00	-	SEU	0,00	2	ų Ų	0.00	-	SEU
-11.	Haz.	0.77		977.5	0.00	_	ខា ខេ	1.03		977.7	0.00	-:	STO R	0.00		977 7	0.00	٠:	STR R
-	И г.	0.73	Ŀ	97.0	0.00	-	STO	1.47	·	97.0	0.00	·	STU	0.00	·	9701	0.00	·	STU
_	Mhox	-0.02	-	97 T R	-001	-	সাদ ২	_	4	977 3	_		31 7 F	0.00	4	977 R	0.00	- 1	31 T E
	М г.	-0.09	Ĺ	97.0	-0.01	1	SIL	-1.4	Ļ	97.01	-0.00	-	31 1.	0.00		9781	0.00	_	31.0
	Max	-0.12	12	9_2 0	0.00	-	ى طلت	-1.10	-2	9 <u>_2</u> 2	_	1 -	SLE E	0.00	2	8 22 0	-0.01		SLE E
	Mir., Maz	-0.20 0.20	-	910 977 7	0.00	-	SEC SEC	-1,40	H	920	-0.00	-	SEU STOR	0.00	-	950 970	-0.01 0.00	-	SEC SEC R
_	ияz И г.	0.23	 	97.7	0.01	-	STF 3	1.46	H	107.77	0.00	 ;	STU	0.00		::	0.00	-	31 C
	Max	-0.02	7	9773	-0.00	:	आह २			9773	_	7	31 T B	0.00		977 3	0.00	2	31 T B
	Mir.	-0.09	Ť	97.0	-0.000	_	SIL	-1.34	F	97.0	-0.00	_	31.0	0.00	·	9701	0.00	-	31.0
	Max	-0.12	2	9_2 /	-0.01	1	ک طات	-1.00	2	9_£ ,	_	-	SLE E	0.00	2		0.00	2	SLE R
-17	Mir.	-0.10	Ŀ	Y_ J	-0.02	1	تLد	-1,40	_	Y_ J	-0.00	-	SEC	0.00	_	لبي	0.00		SEC
	Haz.	0.27	<u></u>	977.5	0.00	ï	SIC	1.00	Ë	::	0.00	:	STT R	0.00	Ŀ	9777	0.00	.:	STO R
	И г.	0.23	Ļ.	97.0	0.01	4	STF R	1.43	Ŀ	97.0	0.00		BT C	0.00		977 7	0.00		BTC
	Mhix	-0.02	4	97 T R	0.0%	1	310	-0.99	\vdash	977 3		-	31 T F	0.00	Ľ.	9701	0.00	-:	31 T F
	Mir.	-0.09	بَ	97 (I	0.00	Ë	ALE S	_	Ļ	97 (I	-0.00	_	31 (0.00	4	977 R	0.00	Ë	31.0
_	Max	-0.12 -0.13	12	822.0	-0.03	-	ک طلت دا	-0.84	1	9_2 /	_	_	SLE R	0.00	-2	8 AZ 0	0.00	1 2	SLE E
	Міг. Мах		-	910 977 7	-0.04	-	STF R	-1,14	-	910 977.5	-0.00	-	SEU SEU R	0.00	-	940 977 5	0.00	-	SEC
	Маи. М. г.	0.27	<u> </u>	10 TO	0.03	-	STU	0.67	H	117.77	0.00	-:	91 G R	0.00		97.0	0.00	 .	STU
	Max	-0.02	<u> </u>	57 7 R	_	-	SIF R	_	\vdash	57 T S			31 T B	0.00		977 K		-	31 T F
	Mir.	-0.10	Ė	9_J	-0.04	1		-1.16	É	9_J	-0.00	Ė	SEU	0.00	É	7 9 <u></u> .	0.00	Ė	SEU
_	Max	-0.12	2	Y_2 /	0.04	_	oL.	-0.90	- 2		_	2			Ē	9 <u>-</u> J	0.00	2	SLE R
	И г.	0.23	·	97.0	0.03	-	SIFR	1.76	·	:07.07	0.00	-	STC	0.00		977 7	0.00	·	STC
7::	Haz.	0.27		977.5	0.04	1	SIC	0.67	·	977.7	0.00	.:	STO R	0.00	·	97.01	0.00	·	STC
±'y 3	М г.	-0.0%	Ŀ	97.0	0.0%	7	সাদ ৪	-1.18	·	97.0	-0.00	·	31 L	0.00	7	977 R	0.00	·	31.0
-777	Max	-0.02	/	97 T R	0.04	1	310	-0.94	_	977.3	_	1	31 T F	0.00	·	97.0	0.00	- 1	31 T F
_	Mir.	-0.10	-	9_J	0.03	_	ک طات	-1,14		91 J	-0.00	-	SEU	0,00	2	875 0	0.00	-	SEU
	Max	-0.12	2	922 0	-0.00	-	ک طات	-1.06	2	Y_2 /	_	2	SLE R	0.00	2	9 <u>22</u> 0	-0.00	2	SLE R
\vdash	H r.	0.23	<u>.</u>	97.0	6.00	-	810	1.43	Ë	187 D	0.00	<u> </u>	STU	0.00		97.01	0.00	H	31 C
-	Ha	9.27	 	977 C	0.00	-	SIC P	-1.00	H	977 T		1	917 R	0.00	\vdash	9701 6771 5	-0.00	1	31 T R
_	Mor. Mox	-0.09 -0.02	\vdash	97.0 97.7 K	0.01		STER STU	-1.4% -1.64	\vdash	97.0 97.7 S	-0.00 -0.00		STO E	0.00	+	977 R 978	-0.00 0.00		साम ह
- : 4	PELIX	/	_	<u> </u>			.51			<u> </u>	·		31 1 F		<u> </u>	1.1	1	ι.	11 1 P

										F	Relaz	ioi	ne di	calc	ole	>			
-74	Mir.	-0.10	L-	9_J	0.01	1	ى طات	-1,40	L-	Y_ J	-0.00	<u>:</u>	SEC	0.00	2	ال تحدي	0.00		SEC
-	Max	-0.12	2	875 0	-0.01	-	ک طلت	-1,51	2	875 3	-0.00	2	SLE E		2	875.0	0.00	2	SLE R
	Hr.	9.36	<u>.</u>	97.0	6.00	-		16	<u>.</u>	::70 ::	0.00	<u> </u>	STU	0.00		::727	0.00		31 C
-72	Маи Мого	-0.20 -0.20		97.71.73 97.71	0.00	- 1	STO STER	-1.01 -1.37		97.7.5 97.0	-0.00	-:	धारा ह	0.00	_	970 970 S	0.00	-:	धार स्ट
-	Marx	-0.02	-	57 T R	-0.00		SIF S	-1.700		57 T S	-0.10		31 7 F	0.00		577 S	0.00		31 T F
	Mir.	-0.30	Ĺ	Y_J	-0.01	1	ت. داد	-1,33	Ė	Y_J	-0.00	Ė	SEU	0.00	_	ر بر بر الساب	0.00	Ė	SEU
-	Max	-0.12	2	9_2 /	0.01	1	۵Lu	-1.00	2	Y_2 0	-0.00	2	SLE E	0.00	_	الدة	0.00	2	SLE R
790	И г.	0.56		97.0	0.00	7	នាខេ	٠	·	97.01	0.00		STC	0.00		977 7	0.00	·	STC
0.4	Haz.	0.27	:	977.5	0.00	1	នាខេ	0.3		977.7	0.00	٠:	STO R	0.00		977 7	0.00	٠:	STO R
-6.9	М г.	-0.30	Ė	97.0	-0.100	1	SIU	-1,34	·	97.01	-0.100	-	31.0	0.00	·	97.01	-0.000	-	31.0
	Mhix	-0.02	_	5773	0.00	_	310	-0.99	_	577.3		- 1	ALL E	0.00	·	97.01	-0.00	- 1	ALE.
-	Mir.	-0.30	-	9_J	0.00	-	ک طلت	-1,30	-	9_J	-0.00	-	SEU	0.00	2	822.0	-0.00		SEU
-57	Max	-0.12	2	922.0	-0.01		ک طات	-0.97	- 2	Y_2 0	-0.00	2	SLE E	0.00	2	9 <u>- 2</u> 9	0.00		
67	И г. Изи	0.20		97.77 97.77 T	0.00	-	STO	0.47		197 TO T	0.00	١.	STC STC R	0.00		99767 99767	0.00	<u> </u>	STC STC R
-	М г.	-0.30		97.0	0.01	-	STE R	-1.31		57.01	-0.00	-	31.0	0.00		977 S	0.00		31.0
-6	Max	-0.02	7	9773	-0.00	-	SIF R	-0.95		9773	0.00	7	31 7 F	0.00	Ź	977 K	0.00	73	31 T F
-50	Mir.	-0.30	-	9_0	-0.01	_	ōL.	-1,18	├ -	Y_ J	-0.00	Ŀ	SEC	0.00	_	الساة	0.00	<u>:</u>	SEU
-54	Мак	-0.12	2	9220	0.02	1	۵L۷	-0.99	2	Y_2 0	0.00	2	SLE E	0.00	-	الساة	0.00	2	SLE E
61	Иτ.	0.56	·	97.0	6.00	1	នាខេ	1.78	·	97.0	0.00	·	STU	0.00		977 7	0.00	·	STC
-6.7	Max	-0.02	1	97 T R	-0.107		आह २	-0.9a	4	977.3	-0.100	1	31 T F	0.00	/	977 R	0.00	- 73	31 T F
-	М г.	-0.20	Ŀ	97.0	-0.01	-		-1.00	L	97.0	-0.00		31.0	0.00		97.01	0.00	-	31.0
-52	Max	-0.12	2	922.0	0.01	1		-0.93	2	V - 2	-0.00	2	SLE E	0.00	-	لدي	0.00	2	_
-51	Mir.	-0.30	-	910 977 7	0.01	-	SIC SIC	-1.18	-	910 910	-0.00 -0.00	 -	SEC	9,66	2	922 J	0.00	-	SEC.
-	Иаи Ипп.	0.20		97.77	0.00	-	STF 3	0.93		117.77	0.00	-:	STOR	0.00		97.01	0.00	-:	STO R
-670	Max	-0.02	Н	57 7 K	0.00	- :	STE S	-0.93		97 T S	-0.100	-	31 T B	0.00		9701	0.00		31 T B
-670	Мr.	-0.70	÷	97.0	0.00	-	SIU	-1.5	H	97.01	-0.00	÷	31.0	0.00	7	977 K	0.00	Ė	31.0
-19	Max	-0.12	2	9220	-0.00	-	ک طات	-0.20	2	9_2 0	-0.00	2	SLE R	0.00	2	922.0	0.00	2	SLE R
-19	Mir.,	-0.30	-	9_J	-0.01	1	۵Lu	-1,11	-	9_J	-0.00	-	SEC	0.00	-	الساة	0.00	<u>:</u>	SEC
-:::	Haz.	0.75	:	977.5	6.00	Ţ	SIC	0.63		977.7	0.00	٠:	ят в	0.00	·	970	0.00	٠:	STOR
	Иυ.	0.56	·	97.0	0.00	/	STF 3	1.7	Ŀ	97.0	0.00	·	STC	0.00		977 7	0.00	·	STC
-,-12	Maix	-0.02	4	97 T R	-0.00		সাদ ৪	-0.30	4	977 3	-0.00	- 1	31 T F	0.00	4	977 R	0.00	- 11	31 T F
-	М г.	-0.30	Ļ	97.0	-0.01	-	SIL	-1.10	Ĺ	97.0	-0.00	Ļ	31.0	0.00	Ľ	9701	0.00	_	31.0
_	Max Min.	-0.12 -0.30	-	877 N	0.00	1	ىلت كى طلت	-0.26 -1.16	-	9_2 J 9_J	-0.00	2	SLE R	0,00	-	رسو د کسو	0.00	2	SLE R
	Haz	0.20		977.5	0.00	-	SIFR	0.55	-	::	0.00	-:	SIT R	0.00	-	977 5	0.00	-:	SIT R
-:-	Η г.	0.56	·	97.0	0.01		STO	1.1.:	ŀ	97.0	0.00	Ť	STC	0.00		97,01	0.00	-	STC
4	Max	-0.02	7	97 T R	0.01	1	310	-0.95	7	97 T R	-0.00	7	31 T F	0.00	·	97.0	0.00	7.	31 T. F.
-::4	М г.	-0.20	·	97.0	0.01	٠.	সাদ ৪	-1.1a	Ŀ	97.01	-0.100	·	31.0	0.00	7	977 R	0.00	-	31 t.
-	Мак	-0.12	cı	9220	_	C.	ک طات	_	2	9220	_	2	_		2	922.0	0.00	2	SLE E
	Mir.	-0.30	_	Y_ J	-0.03		۵L۰	-1.08	-	Y_ J	-0.00	-	SEC	0.00	-	الدة	0.00		SEU
-	H4/	0.27	<u> </u>	977 T	0.03		SIC	0.56	<u>.</u>	::	0.100	-:				9701	0.00	-:	STO R
	Mor. Mox	-0.02	<u> </u>	97.7 97.7 K	-0.00 -0.00	-	STER STER	-0.94	<u> </u>	97.77 S	-0.00	٠.	STO A	0.00	_	977 S	0.00	- ~	STU STU B
-	мих Мис.	-0.30	÷	97.0	-0.00	-	SIL	-1.11	l÷	97 (I	-0.10	÷	31.0	0.00	·	9701	0.00	-	31.0
	Max	-0.12	2		_		εL.	-0.84	2	<u> </u>	_	2	SLE E	0.00	-	السابخ	0.00	2	
	Mir.	-0.30	-	9_J	0.00		ک طات		-	Y_ J	-0.00	-	SEC	0.00	2	9 E 7	0.00	-	SEC
4	H47	0.7"		977.5	0.03	1	SIFR	0.77		::	0.00	٠:	ा गा	0.00		977.5	0.00	٠:	STOR
1 -	Иυ.	0.56		97.0	0.03	Ξ	SIC	0.97	Ŀ	97.0	0.00	·	STC	0.00	·	97.0	0.00	·	STC
_	Max	-0.02	/	97 T R	_		SIU	-0.02	_	977 3	_	1	सामा	0.00	·	97.0	0.00	- 13	साराह
-	М г.	-0.20	Ŀ	97.0	0.0%	-	সাদ্ভ	_	Ľ	97.0	-0.00	<u>.</u>	31.0	0.00	/	977 K	0.00		31.0
-	Max	-0.10 -0.30	2	_	-0.01	- 1	ک طلت دا	-0.76 -1.60	2	9 <u>_2</u> 2	-0.00 -0.00	2	_	0.00	2	8 AZ 0	6.00	- 2	_
\vdash	Min. Maz	0.23	-	910 977 7	-0.01		SEC SEC	0.76	-	910 910	-0.00	-:	SEU SEU R	0.00	-	920 970	0.00	-:	SIC R
	нπ.	0.56	-	97.0	0.01	-	STF 3	1.03	H	107.00	0.00	Ë	STU	0.00		977 7	0.00		STU
_	Max	-0.02		9773	-0.0%		आहर	-0.64	7	97 7 B	0.00	7	31 T F	0.00		977 R	0.00	-	31.0
	М г.	-0.30	·	97.01	-0.04	1	SIU	-0.30	·	97.0	-0.00		31.0	0.00		97.01	0.00	-	31.0
-	Мак	-0.12	2	9120	_	$\overline{}$	۵Lu	-0.54	2	9120	_	2	SLE R		-	الدة	0.00	-	SEC
	Mir.	-0.30	_	9_J	0.03	C I	ک طات	-0.27	-	91 J	-0.00	-	SEC	0.00	2	875 0	0.00	-	SEC
	H4/	0.27	<u> </u>	:: T T	_		SIF 3		Ë	::	_	-:		0.00		977 T	0.00	-:	STT R
-	И г.	0.36	Ŀ	97.7 97.7 K	6.04		810	0.5	Ë	97.77 S	0.00	<u>.</u>	STC	0.00	ŀ.	9777	0.00		37.7.5
-	Minx Min.	-0.02 -0.30	Ľ	870	0.04	1	SILE K	-0.60 -0.81	Ľ	877	-0.00 -0.00	H	SID R	0.00	_	9701 9122 (7	6.00	H	SIT F
-	Max	-0.20	2		_	_	ک طات ک طات	-0.07	2	8_2 J		1	SLE R		2	8 TO 19	0.00	Ŧ	SEC
	Иr.	0.56	Ė	97.0	0.03		SIC	0.4	Ť	197.07	0.00	Ť	STC	0.00	Ť	97.01	0.00	Ē	STC
	Haz	0.23		977.	0.03		STO	0.57		::	0.00	.:	STT R	0.00	·	9777	0.00		STC
-40	М г.	-0.30	Ŀ	97.0	0.00	:	সাদ ২			97.0	-0.00	·	31.0	0.00	/	977 R	0.00		31.0
-,* 9	Max	-0.03	1	97 T R	_		সাচহ	-0.700	1	9773		7	R C IF	0.00	/	977 R	0.00	13	31 T E
-	Mir.	-0.31	-	Y_ J	-0.01		تLد	-0.99	_	Y_ J	-0.00	-	SEC	0.00	-	Yal	0.00	-	SEC
-	Max	-0.13	2	922.0		1	aL.	-0.70	2	Y_2 /		2	SLE R	0.00	-	السلا	0.00	2	SLE R
	H r.	9.36	Ë	97.0	6.00	-	SIF 3	0.00	<u>.</u>	187 D	0.00	Ë	910	0.00		::T7 T	0.00		910
-	Маи Мого	0.23 -0.21	H	977 T	-0.00	-	STE B STU	-0.91	H	907 0 900	-0.00	H	धान ह	0.00	.	977 D 978	0.00		आसा ह
-	Minx	-0.03		97 7 R	_	_	SIU	-0.67	H	97 7 R	_	-	31 T B	0.00		9781 9781	0.00	13	31 T F
			Ĺ	· `						· `					_	ı			

										F	}elaz	io	ne di	calc	olo	,			
-36	MLT.	-0.31	۱.	920	0.00	1 1	ى طات	-0.92	l -	Y_0	-0.00	:	SEC	0.00	2	ال تعدي	0.00	:	SEC
	Мак	-0.10		922 0	-0.02		ک طات	-0.00		Y_2 0	0.00	2	SLE R	0.00	2		0.00	2	SLE P
:	Η г.	0.55	·	::7:71	0.00	1	STO	0.55	·	97.0	0.00	·	STC	0.00	•	9701	0.00	·	STC
.: 1	Haz	0.23		:: T.	0.00	1	STO	0.53		977.5	0.00	-:	STR R	0.00		9777	0.00	٠:	STO R
-24	М г.	-0.17%	٠	97.01	0.00	٠.	आह २	-0.95	·	97.01	-0.100	•	31.0	0.00	1	Š	0.00	•	31.0
-200	Max	-0.079	1	577 3	-0.00		आह २	-0.52	1	9773	0.00		R C TE	0.00	/	977 R	0.00		31 T F
	Mir.	-0.31	_	9_J	-0.03	1	۵Lc	-0.71	_	Y_ J	-0.00	-	SEU	0.00	-	الدة	0.00	-	SEU
-31	Мак	-0.10	2	912 0	0.03	1	5Lc	-0.02	2	822 0	0.00	2	SLE R	0.00	-	التاك	0.00	2	3LE 1
	Иτ.	0.55	Ŀ	97.0	0.00	_	SIFR	0.77	Ŀ	97.0	0.00	·	STC	0.00		977 7	0.00	·	STC
ı:T	Haz.	0.73		:::	6.00	_	STER	0.48		977 T	0.00	-:	STT R	0.00	-:	977 7	0.00	-:	STT R
	М г.	-0.31	Ŀ	97.0	-0.00	_	MU	-0.65	Ľ	97.0	-0.000	Ŀ	31.0	0.00	•	97.0	0.00	·	31.0
-,270	Max	-0.03	_	577 3	0.00	_	310	-0.48	_	577 3	0.00	- 1	31 7 F	0.00		9701	0.00	-:	31 T F
-36	MT.L.	-0.31	-	9_J	0.01		ک طات	-0.03	-	870	-0.00	-	SEU	0.00	2	875.0	0.00	-	SEC
-129	Max	-0.10	2		0.03	_	aL.	-0.40	2		0.00	2	SLE E	9,00	-	92J	0.00	-	SEU
	И г.	0.57	<u>.</u>	97.0	0.03	-	STE R	0.57	<u> </u>	97.0	0.00	Ľ.	OT C	0.00		977 7	0.00	<u> </u>	STU
/:	H4/	0.23	<u>.</u>	977.7	0.03	_	STE R	0.4"		977 T	0.00	-:	OTT R	0.00		977 T	0.00	-	STC
-0.0	М г.	-0.00 -0.00	Н	97.0 97.7 K	-00%	_	STO STER	-0.57 -0.78	H	97.01 97.71 S	-0.00	-	31.0	0.00		9701 9701 S	0.00		31.0
-00	Minx		Ľ						\vdash	-	0.00	<u> </u>	31 7 F	0.00	-		0.00		31 7 F
	Min. Max	-0.32 -0.13	-	912 J	-0.04 0.04	_	alu alu	-0.32 -0.38	-	913 J	-0.00	-	SLU SLE R	0.00	-	لدو لدو	0.00	-	SEC
	мак И г.	9.27	Η-	ST0	0.08	-	SIF R	0.5	Η-	511 D	0.00	۲.	SES E	0.00	-	922 977 7	0.00	-	SIT R
	n n. Max	-0.04	-	977.3	-0.05	_	SIF S	-0.3a		97 7 B	0.00	٠.	31 T F	0.00		977 S	0.00	-:	31 7 F
-0.5	мих Мога	-0.32	۲	97.0	-0.00	_	SIL	-0.5	H	57 D	-0.00	÷	31.1.	0.00	-	9701	0.00	-	311.
	Max	-0.14	2		0.01	-	aL.	-0.38	2	9_2 J	0.00	,	SLE E	9,00		2 m	0.00	2	
	Mir.	-0.32	广	9_0	0.01	-	516 516 K	-0.51	⊢	9_0	-0.00	-	SEU	0.00	- 21	875.0	0.00	-	SEU
	Haz.	0.27		::	0.01	-	SIFR	0.27		1577.7	0.00	-:	STT R	0.00		977 7	0.00	-	STC
	И г.	0.5"	·	::7:71	0.00	-	STO	0.50	·	97.0	0.00	Ħ	STC	0.00		9701	0.00		STC
-5151	Max	-0.04		57 T R	0.00	1	SIU	-0.37	7	97.7 K	0.00	1	31 T. F.	0.00		9781	0.00	·	31.0
-00	М г.	-0.32	·	97.0	0.07		সাট হ	-0.50	·	97.0	-0.00	·	31.0	0.00	1	977 K	0.00	·	31.0
-11	Маж	-0.14	2	9220	-0.02	-	ک طات	-0.36	2	912 J	0.00	2	SLE R	0.00	2	922.0	0.00	2	31£ E
-11	Mir.	-0.32	-	Y_ J	-0.02	1	δLu	-0.48	-	Y_ J	-0.00	-	SEU	0.00	ľ	السلا	0.00	-	SEU
20	Ha/	0.27		:::	0.00	7	810	0.56		977.7	0.00	-:	ят в	0.00	٠	970	0.00	٠:	ят в
20	Иυ.	0.55	Ŀ	97.0	0.00	_	STER	0.43	Ŀ	97.0	0.00	·	STC	0.00		977 7	0.00	·	STC
	Max	-0.04	4	97.7 R	-0.00	_	সাচ্ছ	-0.32	4	97.7 R	0.00	- 1	सामा	0.00	/	977 R	0.00	- ":	R CTF
	М г.	-0.32	Ŀ	97.0	-0.00	_	SIU	-0.44	Ľ	97 TI	-0.00	Ŀ	31.0	0.00		9701	0.00		31.0
	Max	-0.14	2		0.00	-	5Lc	-0.30	2		0.00	2	SLE R	0.00	-	لدو	0.00	2	SLE E
	Mir.	-0.32	-	9_0	0.00	_	SIF R	-0.44	-	910 977 5	-0.00	 -	SEU	9,66		912 J	6.00	-	SEU
	Иаи И г.	0.27	ŀ	977 T.	0.00	-	STE B STO	0.26		::7.77	0.00	-:	STOR	0.00		970	0.00		ST C
	Max	-0.04	Η,	9773	-0.00	-	ore STER	-0.04		97 7 R	0.00		31 T B	0.00	_	977 S	0.00	-	31.0
	M r.	-0.32	Ť	97.0	-0.000	1	310	-0.33	Ť	97.0	-0.00	÷	31.0	0.00	÷	970	0.00	-	31.0
	Max	-0.14	2	922.0			۵L.	-0.13	2	9_£ 0		2	SLE E	0,00	_	الساة	6.00	Ŀ	SEU
	Mir.	-0.32	Η-	Y_J	0.02		ک طات ک	-0.33		Y_J	-0.00	_	SEU	0.00	2	9 AZ 0	0.00	-	SEU
	Ha/	0.27		::	0.01	-	STER	0.77		977 T	0.00	-	STT R	0.00		977 5	0.00	.:	STT R
	И г.	0.55		97.0	0.01	ï	SIC	0.53	·	97.0	0.00		STC	0.00		9701	0.00		STC
-1.3	Max	-0.04	/	97 7 R	0.01	1	SIU	-0.04		97 T R	0.00	":	31 T. F.	0.00		9701	0.00	":	31 T. F.
-1.3	М г.	-0.32		97.0	0.07		आह ३	-0.7%	·	97.01	-0.100	-	31.0	0.00	/	977 R	0.00	-	31.0
-11	Маж	-0.14	2	922.0	-0.02	1	ک طات	-0.10	2	912 0	0.00	2	SLE R	0.00	2	922.0	0.00	2	SLE E
-11	Mir.	-0.32	_	Y_ J	-0.03	_	۵Lu	-0.16	_	9_J	-0.00	-	SEU	0.00	_	السلا	0.00	-	SEU
	Ha/	0.27	Ë	:::	0.03		STO	0.13	<u> </u>	:::	0.00	٠:	STT R	0.00		9770	0.00	-:	STR
	Η г.	0.55	Ŀ	97.0	0.00	_	STF R	0.26	Ľ	97.0	0.00	Ľ.	STU	0.00		977 7	0.00	Ľ.	STU
	Marx	-0.04	4	9773		_	সাদ হ	-0.10	4	977 3	0.00	- 1	31 T F	0.00	_	9701	0.00	- 1	31 T F
	М г.	-0.23	Ŀ	97.0	-0.01	-	MU	-0.04	Ľ	97.01 	-0.00	Ļ.	31.0	0.00	/	977 R	0.00	Ë	31.0
	Max	-0.24	1	9 <u>12</u> 0	_	-	ملات	-0.18	1	9 <u>_2</u> 2	0.00	- 2	SLE R	0.00	2	922 J	0.00	- 2	SLE E
	Mir.	-0.30	-	910 977 7	0.00	-	ALL A	-0.14	-	910 977.5	-0.00	-	SEU SEU D	9,66	-	950 977 T	0.00	-	SEC
	Иаи Ипп.	0.27	H	10 TO	0.00	_	SIF B SIC	0.10	H	::	0.00	H	STOR	0.00		97.01 97.01	0.00		STU
	Mox	-0.04		97 7 R	_	-	SIU	-0.12		977 K	0.00	-	31 T. F.	0.00	-	9701	0.00	-	31.0
	Mar.	-0.33	ŕ	97.0	0.07	_	SIE R	-0.16	ŕ	57.0	-0.00	۰	31.0	0.00	$\overline{}$	977 S	0.00	·	31.0
	Max	-0.13	2	9_2 J	-0.01	_	ک طلت	-0.06	2	8_2 J	0.00	7	SLE R	0.00	- 2	8 AZ 0	0.00	2	SLE R
	Mir.	-0.33	Ē	Y_J	-0.02	_	ole A	-0.08	<u> </u>	Y_J	-0.00	=	SEU	0.00	Ē	871 27	0.00	-	SEU
	Haz	0.73	Ē	:::	0.00	-	810	0.00	Ē	:::	0.00	- <u>-</u> -	STI R	0.00	Ē	9770	0.00	Ē	STC
	н г.	0.53		97.0	0.00	-	STF R	0.08	-	97.0	0.00		STC	0.00		977 7.	0.00	.:	STT R
-4	Max	-0.fa	/	97.7 R	-0.00		সাচহ	-0.05	/	97.7 R	0.00	7	साम ह	0.00	1	977 R	0.00		31.0
-4	MLT.	-0.30		9_J	-0.01	1	δLc	-0.67	L-	Y_ J	-0.00	-	SEU	0.00		لدع	0.00		SEU
-3	Мак	-0.13	2	922.0	0.01	1	۵Lc	-0,69	2	912 0	0.00	2	SLE E	0.00	_	الدة	0.00	-	SEU
.:	И г.	0.43	Ŀ	97.0	0.00		STF R	0.07	Ŀ	97.0	0.00	·	STU	0.00		977 7.	0.00	·	STU
	Haz.	0.73	<u> </u>	977.7	0.00		STE R	0.0	Ľ	97.0	0.00	-:	STT R	0.00		977 7	0.00	-:	STT R
-:"	М г.	-0.39	Ë	97.0 97.7 S	-0.01	_	310	0.01	<u> </u>	57 T R	-0.00	<u> </u>	31.0	0.00	_	9701	0.00	Ë	31.0
_1	Marx	-0.05			111 71	. 1	3100	0.62		97.01	0.00		31 T B	0.00		9.731	Louis		31 T. B.

0,00

0 31 T B 0.00

1 SEC

0.00

31 T F

97.01

2 922 0 0.00

Min = -2.31Mix = 0.04

-1 Max | -0.0a

-1 Min. -0.33

2 STR 3 0.01

0.01 1 STO 0.00 1 SIE K

0.62

1 97.0

2 912 0 -0100

0.00

Simbologia

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CC = Numero della combinazione delle condizioni di carico elementari
CC - Numero della combinazione delle condizioni di ca

Fx = Reazione vincolare (forza) in dir. X

Fy = Reazione vincolare (forza) in dir. Y

Fz = Reazione vincolare (forza) in dir. Z

Mx = Reazione vincolare (momento) intorno all'asse X

My = Reazione vincolare (momento) intorno all'asse Y

Mz = Reazione vincolare (momento) intorno all'asse Z

Nodo = Numero del nodo

TCC = Tipo di combinazione di carico
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Nodo = Numero del nodo
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente

Nodo		8	TCC	Fx <dan></dan>	cc	TCC	Fy <dan></dan>	œ	TCC	Fz <dan></dan>	œ	TCC	Mx <danm></danm>	œ	TCC	My <danm></danm>	cc	TCC	Mz <danm></danm>
-167	Max	1	SLU	5775.78	1	SLU	139.45	1	SIU	325212.00	1	SLU	4784.90	1	SLU	7112.64	1	SLU	21286.00
-167	Min	2	SLE R	427B.35	.2	SLE R	103.30	2	SLE R	240898.00	2	SLE R	3544.37	2	SLE R	5268.62	1	SLU	15767.40
-166	Max	1	SLU	5774.99	2	SLE R	-102.14	- 1	SLU	325273.00	1	SIJI	4780.05	2	SLE R	-5160.46	1	SLU	19014.00
-166	Min	2	SLE R	4277.77	1	SLU	-137.89	2	SIE R	240943.00	- 2	SLE R	3540.78	.2	SLE R	-6966.63	1	SLU	14084.40
-163	Max	1	SLU	5857.57	1	SLU	408.31	1	SIU	312389.00	1	SLU	10679.60	1	SLU	19788.80	1	SLU	22122.90
163	Min	2	SLE B	4338.94	2	SLE R	302.46	2	SLE R	231400.00	2	SLE R	7910.80	2	SLE R	14658.40	1	SLU	16387.36
162	Max	1	SLU	5856.31	2	SLE R	-302.39	1	SLU	312560.00	1	SLU	10688.80	2	SLE R	-14574.30	1	SLU	20092.46
162	Min	2	SLE R	4338.00	1	SLU	-408.23	2	SLE R	231526.00	2	SLE R	7917.60	2	SLE R	-19675.30	1	SLU	14883.30
155	Max	1	SLU	6009.55	1	SLU	641.18	1	SLU	287771.00	1	SLU	20713.80	1	SLU	28716.10	1	SLU	21760.16
-155	Min	2	SLE R	4451.52	2	SLE R	474.95	2	SLE R	213163.00	2	SLE R	15343.50	2	SLE R	21271.20	1	SLU	16118.69
-154	Max	1	SLU	6007.07	2	SLE R	-474.67	1	SIU	287981.00	1	SLU	20770.30	2	SLE R	-21236.70	1	SLU	16246.8
154	Min	2	SLE R	4449.68	1	SLU	-640.81	2	SLE R	213319.00	2	SLE R	15385.40	2	SLE R	-28669.60	1	SLU	12034.7
153	Max	I	SLU	6038.81	1	SLU	208.03	1	SIU	315619.00	1	SLU	21458.00	1	SLU	10734.80	T	SLU	159637.0
153	Mån	2	SLE R	4473.19	2	SLE R	154.10	2	SLE R	233792.00	2	SLE R	15894.80	2	SLE R	7951.73	- 1	SLU	118249.0
-152	Max	1	SLU	6042.70	2	SLE R	-156.07	1	SIU	315710.00	1	SLU	21456.20	2	SLE R	-7848.29	1	SLU	147466.0
152	Min	2	SLE R	4476.07	3	SLU	-210.70	2	SLE R	233859.00	2	SLE R	15893.50	2	SLE R	-10595.20	1	SLU	109234.0
143	Max	7	SIL	6224.89	+	SLU	820.64	-	SIU	253546.00	4	STU	32975.90	1	SLU	32425.90	7	SLU	21451.0
143	Min	2	SLE R	4611.03	2	SLE R	607.88	2	SLE R	187812.00	2	SLE R	24426.60	0	SLE R	24019.20	+	SLU	15889.7
_	-	_	-	6222.70	2			- 6			4			2			4		17192.5
142	Max	1	SLU SIF D		-	SLE R	-608,09	- 2	SLU	253743.00	1	SLU	33060.30	6	SLE R	200 0 100 0 100	1	SLU	
142	Min	2	O'sets 15	4609.41	1	SLU	-820,92	4	SLE R	187958.00	6	SLE R	24489,10	6	SLE R	-32330.90	1	SLU	12735.2
_	-	1	SLU	6270.22	1	SLU	558.54	1	SLU	274241.00	1	SLU	37079.00	1	SLU	24873.20	1	SLU	162497.0
139	_	2	SLE R	4644.61	2	SLE R	413,73	2	SLE R	203142.00	2	SIE R	27465.90	- 2	SLE R	18424.60	-1	SLU	120368.0
138	-	1	SLU	6268.79	2	SLE R	-411.90	1	SLU	274379.00	1	SLU	37336,20	2	SLE R	-18504.80	1	SLU	126253.0
138	-	2	SLE R	4643.55	1	SLU	-556.06	- 2	SLE R	203244.00	2	SLE R	27656.40	2	SLE R	-24981.40	1	SLU	93520.9
127	Max	1	SLU	6476,40	-1	SLU	929,59	1	SLU	212189.00	1	SLU	44873.60	1	SLU	30881.60	1	SLU	21968.4
127	Min	2	SLE R	4797.33	- 2	SLE R	688,59	2	SIE R	157177.00	- 2	SLE R	33239,70	2	SLE R	22875.20	1	SLU	16272.9
126	Max	1	SLU	6475.78	2	SLE R	-689.44	1	SLU	212368.00	1	SIU	44827.10	2	SLE R	-22884.00	1	SLU	17406.B
126	Min	2	SLE R	4796.87	1	SLU	-930.75	2	SLE R	157310.00	2	SLE R	33205.30	2	SLE B	-30893.40	1	SLU	12893.9
105	Max	1	SILI	6649.98	1	SLU	719.13	1	SIU	204511.00	1	SIJJ	55915.30	1	SLU	22826.90	1	SLU	167834.0
105	Min	2	SLE R	4925.91	2	SLE R	532.69	2	SLE R	151490.00	2	SLE R	41418.70	2	SLE R	16908.80	1	SLU	124322.0
104	Max	1	SLU	6647.96	2	SLE R	-535.21	-1	SLU	204703.00	1	SIU	55868.70	2	SLE R	-16910.80	.1	SLU	123266.0
104	Min	2	SLE R	4924.41	1	SLU	-722,53	2	SLE R	151632.00	2	SLE R	41384.20	2	SLE R	-22829.50	1	SLU	91308.3
-81	Max	1	SLU	6757.66	1	SLU	963,45	1	SLU	166267.00	1	SLU	54146.30	1	SLU	25252.60	1	SLU	20584.1
-81	Min	2	SLE R	5005.68	2	SLE R	713.67	2	SLE R	123161.00	2	SLE R	40108.40	2	SLE R	18705.60	1	SLU	15247.5
-78	Max	1	SLU	6757.23	2	SLE B	-715.09	1	SIU	166477.00	1	SIU	54140.50	2	SLE R	-18667.10	1	SLU	15268.9
-78	_	2	SLE R	5005.36	1	SLU	-965.38	2	SLE R	123316.00	2	SLE R	40104.10	2	SLE R	-25200.60	1	SLU	11310.3
-45	Max	1	SLU	7017.10	1	SLU	919,22	1	STII	122242.00	1	SLU	59193,90	1	SLU	17945.20	1	SLU	21711.6
-45	Min	2	SLE R	5197.85	.5	SLE R	680.90	- 2	SLE R	90549.90	2	SLE R	43847.30	2	SLE R	13292.70	1	SLU	16082.7
_	Max	1	SLU	7018.75	2	SLE R	-680.41	1	SIU	122467.00	4	SLU	59119.70	2	SLE R	-13241.10	7	SLU	20690.2
-44		2	SLE R	5199.08	-	SLU	-918,56	- 2	SLE R	90716.20	2	SLE B	43792.40	2	SLE R	-17875.50	7	SLU	15326.0
_	-	1			-						- 4			2	-		7	-	
_	Max	-	SLU	7051.77	-	SLU	657.85	-	SLU	128535.00	-	SLU	64491.40	-	SLU	10929.70	-	SLU	161962.0
_	Min	_	_	5223.53	-	SLE R		-	SLE R		_	_	47771.40	_	SLE R	8096.04	_	_	119972.0
	-	_	SLU	7055.80	-	_	-486,98	-	SLU	128741.00	-	_	64490.00	-	_		-	-	-
_	Min	_		5226.52	-	SLU	-657.42	-	SLE R		_	SLE R		_	SLE R		1	SLU	
_	Max	_	-	7266.56	-	-	-594.46	-	THE RESIDENCE AND ADDRESS OF THE PERSON NAMED IN	81184.60	_	The Real Property lies	60509.70	_	Printer and Printers and	THE RESERVE AND PARTY AND PARTY.	1	-	16418.1
	Min	_	SLE R	-	-	SLU	-802,52	•	SLE R	60136.70	-	SLE B	44822.00	.2	SLE R	-10373.50	1	SLU	
	Max	_		7265.62	-	SLU	800.64	_	SLU	80635.20	_	SLU	60527.60	_	SLU	10374.60	_	SLU	
-28	Min	_		5381.94		SLE R	593,07	-	SIE R	59729.80	_			_	SLE R	7684.90	1	SLU	15900.4
_	Max	_	SLU	7354.68	_	SLU	387.35	-	SLU	70710.80	_		62440.60	_	SLU	2004.95	1	_	161850.0
-23	Min	2	SLE R	5447.91	_	SLE R		-	SLE R	52378.40	2	SLE R	46252.30	2	SLE R	1485.15	1	SLU	119889.0
-22	Max	1	SIU	7356.74	2	SLE R	-284.42	1	SLU	70857.90	1	SIJJ	62478.10	2	SLE R	-1427.50	1	SLU	156344.0
-22	Min	2	SLE R	5449.44	1	SLU	-383,97	2	SLE R	52487,40	2	SLE R	46280,10	2	SLE R	-1927.12	1	SLU	115810.0
-17	Max	1	SLU	7463.04	1	SLU	0.38	1	SLU	49182.60	1	SLU	59871.20	1	SLU	47.77	1	SLU	164169.0
-17	Min	2	SLE R	5528.18	2	SLE R	0.28		SLE R	36431.60	2	SLE R	44349.10	2	SLE R	35.38	1	SLU	121607.0
-16	Max	1	SLU	7464.38	1	SLU	623.03		SLU	46634.90	1	SLU	59187.90	1	SLU	4732.68	_	SLU	21302.3
	Min			5529.17	-	SLE R	_	_	SLE R		_	_	_	_		3505.69	_	SLU	
_	Max	1	_	7464.87	-	SLE R	-	-	SLU	46827.10	-	SLU	59215.90	_	SLE R	-3453.80	1	SLU	100000000000000000000000000000000000000
	Min	_	_	5529.53	-	SLU	-621.44	-	SLE R	34686.80	_		43863.60	-	SLE R	-4662.64	1	SLU	
_	Max	1		7608.59	-	SLU	392.10	-	SLU	22207.30	-	SLU	56863.60	1	SLU	1420.21	1	SLU	
_	Min			5636.00	_	SLE R		-	SLE R		_	_	42121.10		SLE R	1052.01	+	SLU	
	COLUMN TO SERVICE A SERVIC	- 6	Della P	2020+00	1 6	Service 18	£30.44	1.6	State of	+4/243.30	6	See R	SEKEL + LU	- 6	OLE IN	-987.42	+	PATRIC	7000340

-7 Min	2	SLE I	5637,87	1	SLU	-392.01	2	SLE R	16541.40	2	SIE R	42136.90	2	SLE R	-1333.02	1	SLU	14093,40
-4 Max	1	SLU	7683.84	-1	SLU	135.90	1	SLU	9426.53	1	SLU	55210.30	1	SLU	270.25	1	SLU	20776.40
-4 Min	2	SLE F	R 5691.73	- 2	SLE R	100.67	2	SLE R	6982.62	2	SLE R	40896.50	2	SLE R	200.19	1	SLU	15389.90
-3 Max	1	SLU	7682.76	2	SLE R	-100.45	1	SLU	9469.03	1	SLU	55220,30	2	SLE R	-125.55	1	SLU	22109.60
-3 Min	2	SLE F	R 5690.93	1	SLU	-135,61	2	SLE R	7014.10	2	SLE R	40903.90	2	SLE R	-169.49	1	SLU	16377.50

Sollecitazioni elementi bidimensionali

Simbologia

 σ_{XX} = Tensione normale sulle facce perp. all'asse X $\sigma_{\rm ZZ}$ = Tensione normale sulle facce perp. all'asse Z $\tau_{\rm XV}$ = Tensione in dir. Y sulle facce perp. all'asse X $\tau_{\rm XZ}$ = Tensione in dir. Z sulle facce perp. all'asse X $\tau_{\rm ZV}$ = Tensione in dir. Y sulle facce perp. all'asse Z Bid. = Numero del muro/elemento bidimensionale CC = Numero della combinazione delle condizioni di carico elementari Mxx = Momento che provoca variazione di tensione sulle facce perp. all'asse X Mxz = Momento che provoca variazione di tensione tangenziale sulle facce perp. all'asse X Mzz = Momento che provoca variazione di tensione sulle facce perp. all'asse Z Nodo = Numero del nodo

TCC = Tipo di combinazione di carico

SLU - Stato limite ultimo

SLE R = Stato limite d'esercizio, combinazione rara SLE F = Stato limite d'esercizio, combinazione frequente

SLE Q = Stato limite d'esercizio, combinazione quasi permanente

Bid. 2

	∞	TCC	Nodo	Min.	CC	TCC	Nodo	Max		cc	TCC	Nodo	Min.	CC	TOC	Nodo	Max
$\sigma_{\times\times}$ <dan mq=""></dan>	1	SLU	-109	-114779	-1	SLU	-75	101090	σ _{ZZ} <dan mq2<="" td=""><td>- 1</td><td>SLU</td><td>-75</td><td>-118674</td><td>1</td><td>SLU</td><td>-101</td><td>116315</td></dan>	- 1	SLU	-75	-118674	1	SLU	-101	116315
τ _{XZ} <dan mq=""></dan>	1	SLU	-76	-110710	1	SLU	-110	107438	Mxx <danm m=""></danm>	- 1	SLU	-88	-9149480	1	SIJ	-100	11141500
Mzz <danm m=""></danm>	1	SLU	-66	-2219210	1	SLU	-75	4845330	Mxz <danm m=""></danm>	1	SLU	-88	-5840780	1	SIAI	-88	4055160
τ _{ZY} <dan mq=""></dan>	1	SLU	-98	-380642	1	SLU	-111	292400	τ _{×y} <dan mq=""></dan>	1	SLU	+88	-282519	1	SLU	-88	596757

Criteri di progetto utilizzati

Sezioni generiche

Generali	
Stampe	
Wine of colonians	Tatone

Specifici	3
Materiali	
-Considera come elemento esistente	No
-Calcestruzzo	
-Livello di conoscenza	LC2
-Fattore di confidenza	1,20
-Tipo di calcestruzzo	C40/50
-Rck calcestruzzo	500.00
-Modulo elastico <dan cmq=""></dan>	355471.00
-Resistenza caratteristica cilindrica (Fck)	415.00
-Resistenza caratteristica a trazione (Fctk)	25.17
-Resistenza media (Fcm) <dan cmq=""></dan>	495.00
-Resistenza media a trazione (Fctm) <dan cmq=""></dan>	35.96
-σ amm. calcestruzzo <dan cmq=""></dan>	147.50
-tc0 <dan cmg=""></dan>	8.70
-tc1 <dan cmg=""></dan>	24.00
-Riduci Fcd per tutte le verifiche secondo il D.M. 18	Si.
-Y _C per stati limite ultimi	
-Automatico	×
-Pari a	
-Acciaio	
-Livello di conoscenza	TCS
-Fattore di confidenza	1.20
-Tipo di acciaio	B450C
-Modulo elastico <dan cmq=""></dan>	2060000.00
-Tensione caratteristica di snervamento (Fyk) <dan cmq=""></dan>	4500.00
-Tensione media di snervamento (Fym) <dan cmq=""></dan>	4500.00
-Sigma amm. acciaio <dan cmg=""></dan>	2600.00
-Sigma amm. reti e tralicci <dan cmq=""></dan>	2600.00
-Allungamento per verifiche di duttilità (Agt) <%>	4.00
-γ _S per stati limite ultimi	
-Automatico	×
-Pari a	

-Coeff, di omogeneizzazione	15.00
Parametri per analisi pushover	
Numero fibre	200.00
Fattore di confinamento nucleo interno	1.00
Fattore di incrudimento acciaio <%>	0.10
Posizione barre e normativa	
Copriferro reale al bordo staffa <cm></cm>	2.50
Diametro staffa teorica <mm></mm>	8.00
Distanza fra ferri su più strati <cm></cm>	1.00
Verifica con barre in posizione teorica	Si
-Copriferro <cm></cm>	3,00
Mormativa di riferimento	
-Relativa alle travi	
-Relativa ai pilastri	
-Relativa solo al controllo sulle tensioni	×
Elemento dissipativo	No
Verifiche secondo Circ. 65 del 10/04/97	No
Verifiche e sollecitazioni	
Passo di verifica <m></m>	0.50
Integrare lo scorrimento lungo il tratto	51
-Lunghezza del tratto <m></m>	1.00
Verifiche a pressoflessione	Si
Verifiche a flessione/pressoflessione retta -Considera My	No
-Considera My -Considera Mz	
-Considera My e Mz	
Verifiche di stabilità in direzione Z locale	No
-Coeff. Qb	100
Integrare lo scorrimento lungo il tratto	No
-Coeff. 8	
Tipo verifica di stabilità	
-Per N*Ω-M e per N-c*M (standard)	Si
-Per N*Ω-c*M (doppia)	No
-Per N*Ω (sforzo normale e momento nullo)	No
-Per c*M (momento e sforzo normale nullo)	No
was the same of th	
Verifiche a taglio Modalită di calcolo Vrdu	-
-Considera Vrdu minimo	
-Considera Vrdu minimo -Considera Vrdu calcolato in corrispondenza di bw minimo	
-Considera Vrdu in corrispondenza di bw medio	×
-Considera Vrdu in corrispondenza di bw massimo	_ ^
-Considera sempre Af Staffe non proiettata in direzione del taglio	Si
-Verifica a taglio con traliccio ad inclinazione variabile	Si
-Limita ctg θ a	2,50
Dati per progettazione agli stati limite Condizioni ambientali	
-Ordinarie	×
-Aggressive	-
-Molto aggressive	
	No
Usa dominio N-M per flessioni rette	
Usa dominio N-M per flessioni rette -Ricerca della sicurezza con sforzo normale costante	
-Ricerca della sicurezza con sforzo normale costante	
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante	No
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D	No
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse	No
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D	No 30.00
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto	
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione	
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione	
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione Dati per verifiche di resistenza al fuoco	30.00
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione Dati per verifiche di resistenza al fuoco -Tempo di verifica (REI) <minuti> Dimensione MESH <cm></cm></minuti>	30.00
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione Dati per verifiche di resistenza al fuoco -Tempo di verifica (REI) <minuti> Dimensione MESH <cm> -Passo di calcolo <secondi></secondi></cm></minuti>	30.00 120.00 2.00
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione Dati per verifiche di resistenza al fuoco -Tempo di verifica (REI) <minuti> Dimensione MESH <cm></cm></minuti>	30.00 120.00 2.00 10.00
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione Dati per verifiche di resistenza al fuoco -Tempo di verifica (REI) <minuti> Dimensione MESH <cm> -Passo di calcolo <secondi> -Temperatura ambiente <c°></c°></secondi></cm></minuti>	30.00 120.00 2.00 10.00 20.00
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione Dati per verifiche di resistenza al fuoco -Tempo di verifica (REI) <minuti> Dimensione MESH <cm> -Passo di calcolo <secondi> -Temperatura ambiente <c°> -Coeff. di convezione a temperatura ambiente <w k="" mq=""> -Tipo di aggregati</w></c°></secondi></cm></minuti>	30.00 120.00 2.00 10.00 20.00 9.00
-Ricerca della sicurezza con sforzo normale costante -Ricerca della sicurezza con eccentricità costante Controllo rapporto X/D Classificazione barre tese/compresse -Solo le barre con deformazione percentuale rispetto alla barra più tesa/compressa non inferiore a <%> -In funzione della deformazione Dati per verifiche di resistenza al fuoco -Tempo di verifica (REI) <minuti> Dimensione MESH <cm> -Paaso di calcolo <secondi> -Temperatura ambiente <c°> -Coeff. di convezione a temperatura ambiente <w k="" mq=""></w></c°></secondi></cm></minuti>	30.00 120.00 2.00 10.00 20.00 9.00 SILICEI

Plinti/Pali

Conorul i		
Generarr		

E 75 150A 000		
Parametri di progetto Progettazione e verifica dell'armatura con sollecitazioni più grav		
Progettazione e verifica dell'atmatura con sollecitazioni più grav	rose Si	
Parametri di disegno		
Scala disegno plinti	25.00	
Disegno ancoraggi non necessari	Si	
Copriferro per calcolo lunghezze ferri plinto <cm></cm>	3.00	
Copriferro per calcolo lungbezze ferri bicchiere <cm> Calcolo lungbezza ferri semplificato</cm>	2,00 Si	
Diametro per calcolo lunghezze ferri plinto <mm></mm>	10.00	
Diametro per calcolo lunghezze ferri bicchiere <mm></mm>	10.00	
Stampe		
Tipo di relazione	Estesa	_
Specifici		3
Materiali		
-Considera come elemento esistente	_	No
-Calcestruzzo	_	LC2
-Livello di conoscenza -Fattore di confidenza	_	1,20
-Tipo di calcestruzzo		10/37
-Rick calcestruzzo		70.00
-Modulo elastico <dan cmg=""></dan>	33019	_
-Resistenza caratteristica cilindrica (Fck)		17,10
-Resistenza caratteristica a trazione (Fctk)		20.59
-Resistenza media (Fcm) <dan cmq=""></dan>		37.10
-Resistenza media a trazione (Fctm) <dan cmq=""></dan>	2	29.42
-d amm. calcestruzzo <dan cmg=""></dan>	11	15.00
-tc0 <dan cmg=""></dan>		6.90
-tcl <dan omq=""></dan>	. 2	20.30
-Riduci Fcd per tutte le verifiche secondo il D.M. 18	_	Si
-γ _C per stati limite ultimi		
-Automatico		- 2
-Pari a		
-Acciaio	_	***
-Livello di conoscenza -Fattore di confidenza	-	LC2
-Tipo di acciaio		34500
-Modulo elastico <dan cmg=""></dan>	206000	
-Tensione caratteristica di snervamento (Fyk) <dan cmq=""></dan>	-	00.00
-Tensione media di snervamento (Fym) <dan cmq=""></dan>	450	00.00
-Sigma amm. acciaio <dan cmq=""></dan>	260	00.00
-Sigma amm. reti e tralicci <dan cmq=""></dan>	260	00.00
-Allungamento per verifiche di duttilità (Agt) <%>		4.00
-γ _S per stati limite ultimi		
-Automatico		>
-Pari a		
-Coeff. di omogeneizzazione	1	15.00
Parametri di calcolo		
Copriferro teorico di calcolo <cm></cm>	5 1	4,00
Angolo limite plinti snelli/tozzi <grad></grad>	3	30.00
Considerare snelli plinti ambigui		Si
Peso specifico calcestruzzo plinto <dan mc=""></dan>		10,00
Sovraccarichi agenti sul plinto <dan mq=""></dan>		0.00
Sollecitazioni dissipative amplificate	_	Si
Detrazione peso proprio e sovraccarichi	_	Si
Calcolo momenti con metodo dei trapezi Sezione verifica plinti a bicchiere		Si
-A filo parete		,
-In asse alla parete		_
Raffittimento armatura zona centrale		No
Armatura base	-	- 00
Elenco diametri utilizzabili 1 <mm> Elenco diametri utilizzabili 2 <mm></mm></mm>	_	20
Elenco diametri utilizzabili 2 cmm>		
Elenco diametri utilizzabili 4 (mm)		
Elenco diametri utilizzabili 5 <pre>cmp></pre>		_
Elenco diametri utilizzabili 6 <nm></nm>		_
Elenco diametri utilizzabili 7 <mm></mm>		
Plenco diguecti actitissoptit / Anno		
Passi utilizzabili		
A CANADA DA CANA		5.00
Passi utilizzabili	2	5.00 25.00 2.00

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######################################	90.00 91 10.00 91 90.00 90.00 90.00 14.00 9.00 9.00 9.00 9.00
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Staffini verticali di montaggio PAR o'slanza (200) Lughama niavolio alalleni o'trocca i -Rome proportiado del mistore olinis, <00 -Duico ferro longo il perimetro del plinto Armature a punzonamento Plenco diametri utilizzabili i dumb Tienco diametri utilizzabili i dumb Tienco diametri utilizzabili i dumb Tienco diametri i i i vend'il a sumb Tienco diametri i i i vend'il a sumb Tienco diametri utilizzabili 6 dumb Plenco diametri utilizzabili 6 dumb Plenco diametri utilizzabili 7 dumb Plenco diametri utilizzabili 8 dumb Plenco diametri utilizzabili 8 dumb Plenco diametri utilizzabili 8 dumb Plenco del del dumb Plenco diametri utilizzabili 8 dumb Plenco del del del dumb Plenco del dumb Plenco del dumb Plenco del dumb Plenco del del dumb Plenco del dumb Ple	93 2000 0000 1000 1000 000 000 93
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Flenct distatri utilizabili 1 0mm/ The toddiatetri 1 1 isyadii 3 mmm/ The toddiatetri utilizabili 4 0mm/ Flenct distatri utilizabili 5 0mm/ Flenct distatri utilizabili 7 0mm/ Flenct distatri	6.00 17.00 7.00 2.00 6.00 7.00
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Copriferro reale al bordo staffa <cm></cm>	4.00
Diametro staffa teorica <mm></mm>	12.00
Max distanza fra i ferri <cm></cm>	25.00
Min. interferro ammissibile <cm></cm>	5.00
Min, numero ferri	25.00
Alleggerimento ferri longitudinali	No
-Alla quota indicata <cm></cm>	
-Come percentuale della lunghezza del palo	0.00
-Min. ferri rimanenti dopo alleggerimento	× ×
-Pari a	0.00
-Percentuale dell'armatura di testa del palo	
Prostruce a taulio pali	
Armatura a taglio pali	0.00
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-Minimo <cm></cm>	
-Massimo <cm></cm>	
-Incremento <cm></cm>	
Tipo di minimizzazione staffatura	
-Minimizza il numero delle staffe	5.00
-Minimizza il peso delle staffe	20.00
Staffatura a spirale	5.00
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-Usa formulazione sezioni generiche	
-Considera rettangolo inscritto con B/H pari a	×
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-Considera Vrdu minimo	
-Considera Vrdu calcolato in corrispondensa di bw minimo	
-Considera Vrdu in corrispondenza di bw medio	1.00
-Considera Vrdu in corrispondenza di bw massimo	
-Considera sempre Af Staffe non proiettata in direzione del taglio	
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alla barra più tesa/compressa non inferiore a <%>	
-In funzione della deformazione	Si
Capacità portante	
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-Pari a	
-Automatica	

Solette/Platee

Generali	
Parametri di progetto	
Progetto e verifica con metodo d'integrazione	No
-Massima dimensione della linea d'integrazione	1.00
Calcolo armature con metodo di Wood	No
Accoppia pilastri per calcolo punzonamento	Si
-Massima distanza come un moltiplicatore dello spessore	1.50
Armatura a taglio	
Controllo resistenza a taglio allo S.L.U. DM 96	No
Verifica con taglio totale	No
Progetta a taglio con traliccio ad inclinazione variabile	Si
-In Classe A limita ctg 0 a	2.50
-In Classe B limita ctg 0 a	2.50
Parametri di disegno	
Disposizione disegno	2A
Particolari nel disegno principale	
-Eliminare le quotature	No

-Eliminare le campiture	No
-Eliminare la numerazione dei pilastri	. No
-Eliminare la numerazione delle travi e dei muri	No
Particolari nei disegni secondari	
-Eliminare le quotature	Si
-Eliminare le campiture	Si
-Eliminare la numerazione dei pilastri	Si
-Eliminare la numerazione delle travi e dei muri	SI
Disegno armatura diffusa	No
Posizione particolari punzonamento	In automatico
Copriferro per calcolo lunghezza ferri <cm></cm>	3,50
Risvoltare al bordo i ferri	
-Inferiori	Si
-Superiori	51
Lunghezza risvolti ferri al bordo	Pari all'altezsa meno due volte il copriferro
Disegno particolare ferri al bordo	Si
Scala disegno particolare ferri al bordo	20.00
Calcolo lunghezza ferri semplificato	No
Stampe	
Tipo di relazione	Estesa

Stampe	
Tipo di relazione	_
Specifici	3
Materiali	
-Considera come elemento esistente	No
-Calcestruzzo	
-Livello di conoscenza	LC2
-Fattore di confidenza	1.20
-Tipo di calcestruzzo	C40/50
-Rck calcestruzzo	500.00
-Modulo elastico <dan cmg=""></dan>	355471.00
-Resistenza caratteristica cilindrica (Fck)	415.00
-Resistenza caratteristica a trazione (Fctk)	25,17
-Resistenza media (Fcm) <dan cmq=""></dan>	495.00
-Resistenza media a trazione (Fctm) <dan cmq=""></dan>	35.96
-d amm. calcestruzzo <dan cmq=""></dan>	147.50
-tc0 <dan cmq=""></dan>	8.70
-tel <dan eng=""></dan>	24.00
-Riduci Fcd per tutte le verifiche secondo il D.M. 18	si
-Yc per stati limite ultimi	
-Automatics	×
-Pari a	1
-Acciaio	1
-Livello di conoscenza	LC2
-Fattore di confidenza	1,20
-Tipo di acciaio	B450C
-Modulo elastico <dan cmg=""></dan>	2060000.00
-Tensione caratteristica di snervamento (Fyk) <dan cmq=""></dan>	4500.00
-Tensione media di snervamento (Fym) <dan cmq=""></dan>	4500.00
-Sigma amm. acciaio <dan cmq=""></dan>	2600.00
-Sigma amm. reti e tralicci <dan cmq=""></dan>	2600.00
-Allungamento per verifiche di duttilità (Agt) <%>	4.00
-v _s per stati limite ultimi	
-Automatico	- 8
-Pari a	
-Coeff. di omogeneizzazione	15.00
	75105
Parametri di calcolo	
Parametri di progetto secondo il D.M. 18	
-Elemento dissipativo	No
-Sollecitazioni dissipative amplificate per elementi di fondazione	Si
Angolo d'armatura <grad></grad>	0.00
Copriferro teorico superiore <cm></cm>	3.00
Copriferro teorico inferiore <cm></cm>	3,00
Tipo di progetto in doppia armatura	
-Tensione pari ai valori amm.	
-Tensione pari ai valori amm. con AfComp/AfTesa minore o pari a	1.00
-Tensione pari ai valori amm. con AfComp/AfTesa pari a	+
Min. percentuale di regolamento	-
-Platee di fondazione su suolo elastico	No
-Solette di elevazione	Si
Controlla min. armatura di ripartizione	No
Armatura a flessione	
Elenco diametri utilizzabili 1 <mm></mm>	10
Elenco diametri utilizzabili 2 <mm></mm>	12

Relazione di cak	
Elemon dizmetri uzilizzabili 2 (mm/)	_4
Elenco diametri umilizabili 4 mm/2 Tienco diametri umilizzabili 5 mm/2	_6
The top diageout in a linear transformer The top diageout in a linear transformer	
Thermodian of intermediate same	
Figure at it washi	
-Minimo Kenk	10,00
-Maasame Kod>	30,00
Tichere to some	5.00
Doi on izzazio e interassi arzatura	E::
- 3camparx	
-Nest in interest without the control of the contro	
-Mella stessa posizione	
Uniformizzacione Sizmetri armatura	: 4
Dempire Well a shexed time. 'ore	
-Ned in street, poet allows	
Tipo billot in illingione minature al filosofore	
-Minimizza il numero dei ferri	
-Minimizza il pesi complessivo dei ferri	Х
Verifiche a taglio	
740 d' protint veril de 40.10 protint d' protonemento	10:: 10::
"Zeold' prot's, verifica Zouto min'/biole Ziona i	K::
Ancoraggi	
Falthore will i'd. k one per a corraggio Terr	1.00
Tim glosska inmensigg Frankline	
-Called The Tunwiknes ox The Sigmaff	×
-imposta come multiplo del diametro	
Lunghezza andoraggi ferri punconamento	
Cathorata in unzione de la Signat	
Emposta Core m'vio de d. aretro	
Armatura a punzonamento	
Faltbore minifdur one a veura so etua/via.ea	0.30
Morifico, a rexia ecretic/ata o	9
A larger or place to provide a formation state.	F. 000
Bistanza dal borát libero (B.X. 90/88)	
-Distanza come un moltoplicatore dello apessore	1.00
Figures regular at Koro	
Tipo di arrabura a vi zonamento	
-Ratio in Conne. program -Ratio di Iversa vertica Corisposta media relata	×
-Controlla presenzioni ECI	: 4
Woltiplicatore altesza utile per valutare perimetro efficace (D.M. 18)	1.00
Tot terranza of ipos ufo larento barre	
Figures cone un netto prices premier a spessore	0.10
-Bir maka makata . Komb	
7 arto digratri u 1 i znatli 1 summb	./
Elemon dismetri upilizbabili 2 mm/	_4 _6
Elenco dismetri utilizzabili 2 (mm/)	_6
The nondiaretrial in invanition samp	. 8
The soldierethin of izzaofti o somo	"1:
7 area dispetsion to vention sumb	
Passo diametria. Nai venelli vammus Basso utilopsabilo	
-Minimo Kenik	16,00
Marking (C.O.)	-00,00
Tionere Lo samo	×.100
Elposition of aviant aratum a prozonare do	
-Minuria au munora un libero	×
-Minimizza il pesi complessivo dei ferri	
Dati per progettazione agli stati limite	
Condinioni antientali	
Cr. radia	
Aggressive -Motor processo	
Control o modernio X/7:	Y::
Classificatione barre tese/compresse	1
-Sol: le barre con deformazione percentuale rispetto	
a la barra più tesa/compressa no i interiore a 385	30.00
To finitione detraide on azione	

Simbologia Δ_{SM} - Distanza media tra le fessure Φ_{eQ} = Diametro equivalente delle barre esm = Deformazione unitaria media dell'armatura (*1000) σ_{C} = Tensione nel calcestruzzo $\sigma_{\rm f}$ = Tensione nel ferro σg = Tensione nell'acciaio nella sezione fessurata A_{C eff} = Area di calcestruzzo efficace As = Area complessiva dei ferri nell'area di calcestruzzo efficace AfE I = Area di ferro effettiva totale presente nel punto di verifica, inferiore AfE S - Area di ferro effettiva totale presente nel punto di verifica, superiore AfE St. = Area di ferro effettiva della staffatura CC = Numero della combinazione delle condizioni di carico elementari Cf inf - Copriferro inferiore Cf sup = Copriferro superiore Cls = Tipo di calcestruzzo DV = Direzione di verifica XX = Verifica per momento Mxx YY = Verifica per momento Myy Fcd = Resistenza di calcolo a compressione del calcestruzzo Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo Fctd = Resistenza di calcolo a trazione del calcestruzzo Fctk = Resistenza caratteristica a trazione del calcestruzzo Fyd - Resistenza di calcolo dell'acciaio Fyk = Tensione caratteristica di snervamento dell'acciaio K2 = Coefficiente per distribuzione deformazioni MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y Mom - Momento flettente My = Momento flettente intorno all'asse Y Nodo = Numero del nodo Sic. = Sicurezza Spess. = Spessore TCC = Tipo di combinazione di carico SLU - Stato limite ultimo SLE R = Stato limite d'esercizio, combinazione rara SLE F = Stato limite d'esercizio, combinazione frequente SLE Q = Stato limite d'esercizio, combinazione quasi permanente Tp = Tipo di acciaio VRcd = Taglio ultimo lato calcestruzzo VRsd - Taglio ultimo lato armatura Vrdu = Taglio ultimo resistente

Armatura soletta a quota 0.00

s = Distanza massima tra le barre

X = Coordinata X del nodo
Y = Coordinata Y del nodo
c = Ricoprimento dell'armatura

Caratteristiche delle sezioni e dei materiali utilizzati

Vsdu = Taglio agente nella direzione del momento ultimo

ctg0 = Cotangente dell'angolo di inclinazione dei puntoni di calcestruzzo

Wk = Ampiezza caratteristica delle fessure

Spess.	Cf sup	Cf inf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fcd. <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
350.00	3.00	3.00	C40/50	415.00	25.17	235.17	16.78	5450C	4500.00	3913.04
260.00	3.00	3.00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.04
150.00	3.00	3.00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.04

Stato limite ultimo - Verifiche a flessione/pressoflessione

Nodo	X <m></m>	Y <m></m>	DV	cc	TCC	AfE S <cmq></cmq>	AfE I <cmq></cmq>	My <danm></danm>	MRdy <danm></danm>	Sic.
-125	14.11	14.50	XX	1	SLU	7.54	13.40	718064.00	134210.00	0.187
-125	14.11	14.50	XX	1	SLU	7.54	13.40	718064.00	134210.00	0.187
-18	10.39	3,84	ХX	1	SLU	7.54	13.40	-2996.51	-75874.20	25.321
-151	12.61	19.16	XX	1	SLU	5.13	13.40	253181.00	76511.40	0.302
-141	16.57	17.35	XX	1	SLU	5.13	13.40	243355.00	76511.40	0.314
-17	11.50	3.06	XX	1	SLU	5,13	13.40	-8418.92	-29821.60	3.542
-99	9.97	12,35	XX	1	SLU	13.40	13.40	1214140.00	181420.00	0.149
-109	12.12	12.77	XX	1	SLU	13.40	13.40	1024710.00	181420.00	0.177
-66	10.55	10.44	XX	1	SLU	13.40	13.40	-327855.00	-181420.00	0.553
-132	10.94	15.43	YY	1	SLU	13,40	13.40	1222170.00	134214.00	0.110
-132	10.94	15.43	YY	1	SLU	13.40	13.40	1222170.00	134214.00	0.110
-37	12.06	7.55	YY	1	SLU	13.40	13.40	-520744.00	-134214.00	0.258
-19	12.61	3.84	YY	1	SLU	13.40	13.40	-134209.00	-76518.00	0.570
-150	10.39	19.16	YY	1	SLU	13,40	13.40	433701.00	76518.00	0.176
-150	10.39	19.16	YY	1	SLU	13.40	13.40	433701.00	76518.00	0.176
-69	11.91	10.61	YY	1	SLU	13.40	13.40	-4202760.00	-181420.00	0.043
-88	11.50	11.50	YY	1	SLU	13.40	13.40	511975.00	181420.00	0.354
-100	11.64	12.46	ΥY	1	SLU	13.40	13.40	6064350.00	181420.00	0.030

Stato limite ultimo - Verifiche a taglio

Nodo	X <m></m>	Y <m></m>	DV	cc	TCC	<cmq></cmq>	<amq></amq>	AfE St. <mq m=""></mq>	Vsdu <dan></dan>	ctg0	VRcd <dan></dan>	VRsd <dan></dan>	Vrdu <dan></dan>	Sic.
-125	14.11	14.50	XX	1	SLU	7.54	13.40	3	210652.00			2	83813.30	0,398
-141	16.57	17.35	XX	1	SLU	5.13	13.40		98826.20			- 5	53081.80	0.537
-109	12.12	12.77	XX	1	SLU	13,40	13.40		578931.00				108042.00	0.187
-132	10.94	15.43	YY	1	SLU	13.40	13.40		257247.00				83813.30	0.326
-150	10.39	19,16	YY	1	SLU	13.40	13.40		134370.00				53081.80	0.395
-88	11.50	11.50	YY	1	SLU	13.40	13.40	(1456390.00		1 8	1 78	108042.00	0.074

Stato limite d'esercizio - Verifiche tensionali

Nodo	X <m></m>	Y ≪m>	DV	cc	TCC	AfE S <mq></mq>	AfE I <mq></mq>	Mom <danm></danm>	σ _c <dan cmg=""></dan>	σ _f <dan cmq=""></dan>
-125	14.11	14.50	XX	2	SLE R	7.54	13.40	531899.00	137.25	16021.10
-125	14.11	14.50	XX	4	SLE Q	7.54	13.40	531899.00	137.25	16021.10
-18	10.39	3.84	XX	2	SLE R	7.54	13.40	-2219.64	0.71	117.55
-18	10.39	3.84	XX	4	SLE Q	7.54	13.40	-2219.64	0.71	117.55
-151	12.61	19.16	XX	2	SLE R	5.13	13.40	187541.00	115.93	9995.00
-151	12.61	19.16	XX	- 4	SLE Q	5.13	13.40	187541.00	115.93	9995.00
-17	11.50	3.06	XX	2	SLE R	5.13	13,40	-6236,24	5.46	850.19
-17	11.50	3.06	XX	4	SLE Q	5.13	13.40	-6236.24	5.46	850.19
~99	9.97	12.35	XX	2	SLE R	13.40	13,40	899367.00	143.00	19935.30
-99	9.97	12.35	XX	4	SLE Q	13.40	13,40	899367.00	143.00	19935.30
-66	10.55	10.44	XX	2	SLE R	13.40	13.40	-242856.00	38.61	5383.11
-66	10.55	10,44	XX	4	SLE Q	13,40	13,40	-242856.00	38.61	5383.11
-132	10.94	15.43	YY	.2	SLE R	13.40	13.40	905313.00	226.82	27210.90
-132	10.94	15,43	YY	-4	SLE Q	13,40	13.40	905313.00	226.82	27210.90
-37	12.06	7,55	YY	2	SLE R	13.40	13,40	-385736.00	96.64	11594.00
-37	12.06	7.55	YY	4	SLE Q	13.40	13,40	-385736.00	96.64	11594.00
-19	12.61	3.84	YY	2	SLE R	13.40	13,40	-99414.10	58.17	5274.83
-19	12.61	3.84	YY	4	SLE Q	13.40	13.40	-99414.10	58.17	5274.83
-150	10.39	19.16	YY	2	SLE R	13.40	13,40	321260.00	187.99	17045.80
-150	10.39	19.16	YY	4	SLE Q	13.40	13,40	321260.00	187.99	17045.80
-69	11.91	10,61	ΥY	2	SLE R	13.40	13,40	-3113150.00	494.99	69005.B0
-69	11.91	10.61	YY	4	SLE Q	13.40	13.40	-3113150.00	494.99	69005.B0
-100	11.64	12.46	YY	2	SLE R	13,40	13.40	4492110.00	714.25	99571.70
-100	11.64	12.46	YY	4	SLE Q	13.40	13.40	4492110.00	714,25	99571.70

Stato limite d'esercizio - Verifiche a fessurazione

Nodo	X <m></m>	Y <m></m>	DV	cc	TCC	c <mm></mm>	s <mm></mm>	K 2	Φeq	Δ _{BM}	A _s	Ac eff <cmq></cmq>	σ _s <dan cmq=""></dan>	esm	Wk <mm></mm>
-125	14.11	14.50	XX	4	SLE Q	22,00	150.00	0.50	16.00	1730.52	15.41	750.00	16021.10	7.40	21.76
-125	14.11	14.50	XX	- 3	SLE F	22,00	150.00	0.50	16.00	1730.52	15.41	750.00	16021,10	7.21	21,20
-18	10.39	3.84	XX	4	SLE Q	24.00	150.00	0.50	12.00	1789.35	8.67	750.00	117.55	0.03	0.10
-18	10.39	3.84	XX	3	SLE F	24.00	150.00	0.50	12,00	1789.35	8.67	750.00	117.55	0.03	0.10
-151	12.61	19,16	XX	4	SLE Q	22.00	150.00	0.50	16.00	961.61	15.41	750.00	9995.00	4.47	7.31
-151	12.61	19,16	XX	3	SLE F	22.00	150.00	0.50	16.00	961.61	15.41	750.00	9995.00	4.28	7.00
-17	11.50	3.06	XX	4	SLE Q	23.00	300.00	0.50	14,00	1028.20	6.67	750.00	850.19	0.25	0.43
-17	11.50	3.06	XX	- 3	SLE F	23.00	300.00	0.50	14.00	1028.20	6.67	750.00	850,19	0.25	0.43
-99	9.97	12.35	XX	4	SLE Q	22.00	150.00	0.50	16,00	2372.18	15.41	750.00	19935.30	9.30	37,49
-99	9.97	12.35	XX	3	SLE F	22.00	150.00	0.50	16.00	2372.18	15.41	750.00	19935.30	9.11	36.73
-66	10.55	10.44	XX	4	SLE Q	22.00	150.00	0.50	16.00	2372.18	15.41	750.00	5383.11	2.23	9.00
-66	10.55	10.44	XX	3	SLE F	22.00	150.00	0.50	16.00	2372.18	15.41	750.00	5383.11	2.04	8.24
-132	10.94	15.43	YY	4	SLE Q	22.00	150.00	0.50	16.00	1735.78	15.41	750.00	27210.90	12.83	37.86
-132	10.94	15.43	YY	3	SLE F	22,00	150.00	0,50	16.00	1735.78	15.41	750.00	27210.90	12.64	37.30
-37	12.06	7,55	YY	4	SLE Q	22,00	150.00	0.50	16.00	1735.78	15.41	750.00	11594.00	5.25	15,49
-37	12.06	7.55	YY	3	SLE F	22.00	150.00	0.50	16.00	1735.78	15.41	750.00	11594.00	5.06	14.92
-19	12.61	3.84	YY	4	SLE Q	22.00	150.00	0,50	16,00	968.51	15.41	750.00	5274.83	2.18	3.59
-19	12.61	3.84	YY	3	SLE F	22.00	190.00	0.50	16.00	968.51	15.41	750.00	5274.83	1.99	3,28
-150	10.39	19,16	YY	4	SLE Q	22.00	150.00	0.50	16,00	968.51	15,41	750.00	17045.80	7.89	13.00
-150	10.39	19.16	YY	. 3	SLE F	22.00	150.00	0.50	16.00	968.51	15.41	750.00	17045.80	7.70	12,68
+69	11,91	10.61	YY	4	SLE Q	22.00	150.00	0.50	16.00	2372.18	15,41	750.00	69005,80	33.12	133,55
-69	11.91	10.61	YY	3	SLE F	22.00	150.00	0.50	16.00	2372.18	15.41	750.00	69005.80	32.93	132.79
-100	11.64	12.46	YY	4	SLE Q	22.00	150.00	0.50	16.00	2372.18	15.41	750.00	99571.70	47.96	193.39
-100	11.64	12,46	YY	3	SLE F	22.00	150.00	0.50	16.00	2372.18	15.41	750.00	99571.70	47.77	192.62

Verifiche e armature plinti/pali

Simbologia

Simbologia

Az = Azioni ed effetti sul plinto/palo

RVN = Reazioni vincolari agenti

TAG = Effetti dovuti ai tagli

ECC = Effetti dovuti all'eccentricità

PP = Effetti dovuti all peso proprio

SVR = Effetti dovuti ai sovraccarichi e al peso del terreno

TOT = Azioni totali di calcolo

CC = Numero della combinazione delle condizioni di carico elementari

Caso = Caso di verifica

Cf = Copriferro

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Cls = Tipo di calcestruzzo
Fcd = Resistenza di calcolo a compressione del calcestruzzo
Fck - Resistenza caratterística cilindrica a compressione del calcestruzzo
Fotd = Resistenza di calcolo a trazione del calcestruzzo
Fctk = Resistenza caratteristica a trazione del calcestruzzo
Fyd = Resistenza di calcolo dell'acciaio
Fyk = Tensione caratteristica di snervamento dell'acciaio
Mx = Momento intorno all'asse X
My = Momento Intorno all'asse Y
Mz = Momento intorno all'asse Z
N = Sforzo normale
Palo = Numero del palo
R = Raggio
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q - Stato limite d'esercizio, combinazione quasi permanente
Tp = Tipo di acciaio
Tx = Taglio in dir. X
Ty = Taglio in dir. Y
```

Palo n. 1

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	,
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 1 (-40)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	128741.00	7055.80	-657.42	64490.00	-10882.50
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC				0.00	0.00
	. 1	SLU	TOT	128741.00	7055.80	-657.42	64490.00	-10882.50
2	2	SLE R	RVN	95363.70	5226.52	-486.98	47770.40	-8061.09
	. 2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	95363.70	5226.52	-486.98	47770.40	-8061.09
3	3	SLE F	RVN	95363.70	5226.52	-486.98	47770.40	-8061.09
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	-3	SLE F	TOT	95363.70	5226.52	-486.98	47770.40	-8061.09
- 4	4	SLE Q	RVN	95363.70	5226.52	-486.98	47770.40	-8061.09
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00
	4	SIE Q	TOT	95363.70	5226.52	-486.98	47770.40	-B061.09

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	. 1	SLU	. 1	-128741.00	-7055.80	657.42	-64490.00	10882.50
- 2	2	SLE R	1	-95363.70	-5226.52	486.98	-47770.40	8061.09
3	3	SLE F	1	-95363.70	-5226.52	486.98	-47770.40	8061.09
- 4	4	SIE Q	1	-95363.70	-5226.52	486.98	-47770.40	8061.09

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SIU	-128741.00	64233.50	10839.20	-128741.00	195562.00	34234.00	2-3	170.00	3.048
- 2	59.52	1	SLU	-129054.00	67622.40	11411.10	-129054.00	195675.00	34254.90	2-3	170.00	2.897
- 3	119.05	1	STU	-128002.00	69615.20	11747.30	-128002.00	195297.00	34184.60	2-3	170.00	2.808
4	178.57	1	SLU	-126953.00	70417.10	11882.70	-126953.00	194921.00	34114.50	2-3	170.00	2.771
.5	238.09	1	SIJ	-125909.00	70217.00	11848.90	-125909,00	194546.00	34044.60	2-3	170.00	2.774
- 6	297.62	1	SLU	-124868.00	69187.30	11675.10	-124868.00	194172.00	33975.10	2-3	170.00	2.809
7	357.14	1	SLU	-123832.00	67421.40	11377.10	-123832.00	193800.00	33905.80	2-3	170.00	2.877
8	416.67	1	SLU	-120867.00	64822.30	10938.60	-120867.00	192735.00	33707.50	2-3	170.00	2,976

							Relazio	one di ca	Icolo			
9	476.19	1	SLU	-117909.00	61523.50	10381.90			33508.70	2-3	170.00	3.119
10	535.71	1	SIA	-114957.00	57712.00	9738.72	-114957.00	190602.00	33309.90	2-3	170.00	3.306
11	595.24	1	SIU	-112012.00	53550.60	9036.49	-112012.00	189489.00	33209.40	2-3	170.00	3.542
12	654.76	1	SIJJ	-109072.00	49178.80	8298.77	-109072.00	188375.00	33111.30	2-3	170.00	3.835
13	714.29	1	SLU	-106138.00	44715.10	7545.53	-106138.00	187259.00	33016.00	2-3	170.00	4.193
14	773.81	1	SLU	+103210.00	40258.10	6793.43	-103210.00	186143.00	32919.80	2-3	170.00	4.630
15	833.33	1	SIU	-100288.00	35888.90	6056.13	-100288.00	185029.00	32823.00	2-3	170.00	5.163
15	892,86	1	SIU	-97370.60	31672.20	5344.58	-97370.60	184188.00	30689.80	2-3	170.62	5.813
17	952.38	1	SLU	-94458.70	27658.80	4657.33	~94458.70	183069.00	30601.60	2-3	170.62	6.617
18	1011.90	1	SIJ	-91551.80	23886.70	4030.80	-91551.80	181949.00	30497.50	2-3	170.62	7.616
19	1071.43	1	SLU	-88649.90	20382.80	3439.53	-B8649.90	180815.00	30295.60	2-3	170.62	8.869
20	1130.95	1	SLU	-85752.70	17164.70	2896.49	-B5752.70	179677.00	30092,60	2-3	170,62	10.466
21	1190.48	1	SIAJ	-82860.10	14241.80	2403.25	-82860.10	178541.00	29890.00	2-3	170.62	12.534
22	1250.00	-1	SLU	-79971.90	11616.50	1960.25	-79971,90	177404.00	29687,10	2-3	170.62	15.268
23	1309.52	1	SLU	-77088.10	9285.81	1566.95	-77088.10	175962.00	31273.80	2-3	170.00	18.978
24	1369.05	1	SIJ	-74208.40	7241.96	1222.06	-7420B.40	174823.00	31065.40	2-3	170.00	24.177
25	1428.57	1	SIJ	-71332.60	5473.51	923.64	-71332,60	173681.00	30855.80	2-3	170.00	31.779
26	1488.10	1	SLU	-68460.70	3966.14	569.27	-2571250.00	172538.00	30646.00	2-3	170.00	37.558
27	1547.62	1	SLU	-65592.40	2703.36	456.18	-2571250.00	171396.00	30436.40	2-3	170.00	39.200
28	1607.14	1	SIU	-62727.70	1667.12	281.32	-2571250.00	170250.00	30226.00	2-3	170.00	40.991
29	1666.67	1	SLU	-59866.40	838.28	141.46	-2571250.00	169103.00	30014.90	2-3	170.00	42,950

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-164710.00

-163589.00

-162467.00

161343.00

-160179.00

-159006.00

-156649.00

-155471.00

29804.10

-28978.00

-28767.60

-28557.50

28346.70

28135.20

-28013.60

27910.70

-27715.80

27616.50

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2380.95

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-57008.20

-54153.10

-51300.90

-48451.50

-45604.70

-42760.30

-39918.20

-37078.20

-34240.20

-31404.10

-28569.70

-25736.70

-22905.20

-20074.90

SIA

SLU

SIU

SIJI

197.04

-603.20

-802.48

-894.40

-898.47

-833.83

-719.28

-573.27

-413.96

-259.27

-126.95

0.00

-46.70

-101.79

-135.42

-150.93

-151.61

-140.71

-121.38

-96.74

-69.B5

-43.75

-21.42

-5.85

0.00

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
- 1	0.00	1	SIA	7055.80	-657.42	0.85	11.31	7086.36	1.00	32294.70	350109.00	32294.70	4.557
2	59.52	1	SLU	4504.56	-419.71	0.85	11.31	4524.07	1.00	32294.70	350154,00	32294.70	7.138
3	119.05	1	SLU	2314.79	-215.68	0.85	11.31	2324.81	1.00	32294.70	350003.00	32294.70	13.891
-4	178.57	1	SILI	459.31	-42.80	0.85	11.31	461.30	1.00	32294.70	349853.00	32294.70	70.008
- 5	238.09	1	SIJ	-1089.57	101.52	0.85	11.31	1094.29	1.00	32294.70	349703.00	32294.70	29.512
- 6	297.62	1	SIU	-2359.67	219.86	0.85	11.31	2369.90	1.00	32294.70	349554.00	32294.70	13.627
7	357.14	-1	SLU	-3698.87	344.64	0.85	11,31	3714.89	1.00	32294.70	349406.00	32294.70	8.693
. 8	416.67	1	SLU	-5059.12	471.38	0.85	11.31	50B1.03	1.00	32294.70	348981.00	32294.70	6.356
9	476.19	1	SLU	-6080.34	566.53	0.85	11.31	6106.68	1.00	32294.70	348557.00	32294.70	5.288
1.0	535.71	1	SLU	-6805.28	634.08	0.85	11.31	6834.76	1.00	32294.70	348135.00	32294.70	4.725
11	595.24	1	SIJ	-7274.26	677.78	0.85	11.31	7305.77	1.00	32294.70	347713.00	32294.70	4.420
12	654.76	1	SLU	-7524.89	701.13	0.85	11.31	7557.49	1,00	32294.70	347291.00	32294.70	4.273
13	714.29	1	SLU	-7591.89	707.37	0.85	11,31	7624.78	1.00	32294.70	346871.00	32294.70	4,236
14	773.81	1	SIU	-7506,98	699.46	0.85	11.31	7539.50	1.00	32294.70	346452,00	32294.70	4.283
15	833.33	1	SLU	-7298.84	680.07	0.85	11.31	7330.46	1.00	32294.70	346033.00	32294.70	4,406
16	892.86	1	SLU	~6993.19	651.59	0.85	11.31	7023.48	1.00	32294.70	345615.00	32294.70	4.598
17	952.38	1	SIU	-6612.82	616.15	0.85	11.31	6641.46	1.00	32294.70	345198.00	32294.70	4.863
18	1011,90	1	SIU	-6177.73	575.61	0.85	11.31	6204.49	1.00	32294.70	344782.00	32294.70	5.205
19	1071.43	1	SLU	-5705.32	531.59	0.85	11.31	5730.03	1.00	32294.70	344366.00	32294.70	5.636
20	1130.95	1	SLU	-5210.48	485.49	0.85	11.31	5233.05	1.00	32294.70	343951.00	32294.70	6.171
21	1190.48	1	SIA	-4705.87	438.47	0.85	11.31	4726.26	1.00	32294.70	343537.00	32294.70	6,833
22	1250.00	1	SLU	-4202.06	391.53	0.85	11.31	4220.26	1.00	32294.70	343123.00	32294.70	7.652
23	1309.52	1	SLU	-3707.74	345.47	0.85	11.31	3723.80	1.00	32294.70	342710.00	32294.70	8.673
24	1369.05	1	SIJ	-3229.93	300.95	0.85	11.31	3243.92	1,00	32294.70	342298.00	32294.70	9.955
25	1428.57	1	SLU	-2774.17	258.48	0.85	11.31	2786.19	1.00	32294.70	341886.00	32294.70	11.591
26	1488,10	1	SLU	-2344.73	218.47	0.85	11.31	2354.88	1.00	32294.70	341474.00	32294.70	13.714
27	1547.62	1	SLU	-1944.75	181.20	0.85	11.31	1953.17	1.00	32294.70	341064.00	32294.70	16.535
28	1607.14	1	SLU	-1576.45	146.88	0.85	11.31	1583.27	1.00	32294.70	340653.00	32294.70	20.397
29	1666.67	1	SEU	-1241.27	115.66	0.85	11.31	1246.65	1.00	32294.70	340243.00	32294.70	25.905
30	1726.19	1	SIJ	-940.04	87.59	0.85	11.31	944.11	1.00	32294.70	339834.00	32294.70	34.207
31	1785,71	1	SLU	-673,07	62.71	0.85	11.31	675.98	1.00	32294.70	339425.00	32294.70	47.775
32	1845.24	1	SLU	-440.30	41.03	0.85	11.31	442.21	1.00	32294.70	339016,00	32294.70	73.030
33	1904.76	1	SLU	-241.43	22.50	0.85	11.31	242.47	1.00	32294.70	338608.00	32294.70	>100
34	1964.29	1	SIAI	-75.95	7.08	0.85	11.31	76.28	1.00	32294.70	338200.00	32294.70	>100
35	2023.81	1	SLU	56.74	-5.29	0.85	11.31	56.98	1,00	32294.70	337793.00	32294.70	>100
36	2083.33	1	SIU	157,25	-14.65	0.85	11.31	157.93	1.00	32294.70	337386.00	32294.70	>100
37	2142.86	1	SLU	226.18	-21.07	0.85	11.31	227.16	1.00	32294.70	336979,00	32294.70	>100
38	2202.38	1	SLU	264.07	-24.61	0.85	11.31	265.22	1.00	32294.70	336573.00	32294.70	>100

39	2261.90	1	SLU	271.38	-25.29	0.85	11.31	272.56	1.00	32294.70	336166.00	32294.70	>100
40	2321.43	1	SLU	248.44	-23.15	0.85	11.31	249.52	1.00	32294.70	335760.00	32294.70	>100
41	2380.95	1	SILI	195.49	-18.21	0.85	11.31	196.33	1.00	32294.70	335355.00	32294.70	>100
42	2440.48	1	SIJJ	112.65	-10.50	0.85	11.31	113.14	1.00	32294.70	334949.00	32294.70	>100

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <mq></mq>	AfC <max< th=""><th>o <dan cmg=""></dan></th><th>of cdsN/cmm</th></max<>	o <dan cmg=""></dan>	of cdsN/cmm
44	0.00	2	SLE R				-		43.38	646.02
45	59.52	2	SLE R		8452.63	50090.60		-	45.99	721.95
46	119.05	-	SLE R			51566.80		_	47.60	776.28
47	178.57	2	SLE R	-94732.90	8801.97	52160.80	40.84	37.70	48.27	801.88
48	238.09	2	SLE R	-94149.40	8776.95	52012.60	40.84	37.70	48.16	802.74
49	297,62	2	SLE B	-93568.80	8648.25	51249.90	40.84	37.70	47.39	783.01
50	357.14	2	SLE R		8427.51	49941.80		37.70	46.05	745.20
51	416.67	2	SLE R	-90810.40		48016.50	_	_	44.17	702.86
52	476.19	-	SLE R			45573.00			41.75	643.82
53	535.71	2	SLE R	-86463.30 -84296.80		42749.70			38.93 35.84	573.33 496.17
55	654.76	2	SLE R	-	6147.24	36428.80	interestation or a	_	32,61	447.37
56	714.29	_	SLE R					_	29.35	404.25
57	773.81	_	SLE R			29820.80	_		26,14	361.80
58	833.33	2	SLE R	-75674.70		26584.30		43.98	23.09	321.16
59	892.86	2	SLE R	-73529.60	3958.95	23460.90	28,27	50.27	20.26	283.33
50	952.38	2	SLE R	-71388.50	3457,28	20488.00	28,27	50.27	17,72	249.08
61	1011.90	-	SLE R		2985.78	17693.BO	21.99	56.55	15.49	218.88
62	1071.43	-	SLE R		2547.80	15098.40	21.99	_	13,58	192.78
63	1130.95	2	SLE R	-64987.60	2145.55	12714.60	-	62.83	11.96	170.53
64	1190,48	-	SLE R	-62861.10		10549.50 8604.82		78.54	10.59	151.60
_	1250.00	2	SLE R		1452.03	6878.38	_	78.54	9.41 8.34	135.15
67	1369.05	2	SLE R	-56501.30		5364.42		78.54	7.38	106.98
68	1428.57	2	SLE R	-54387.60	684.17	4054.45		78.54	6,53	95.10
69	1488.10	2	SLE R			2937.88		78.54	5.77	84.60
.70	1547.62	2	SLE R	-50168.80	337.91	2002.49	0.00	78.54	5.12	75.39
71	1607.14	2	SLE R	-48063.50	208.39	1234.91	0.00	78.54	4.55	67.37
72	1666.67	2	SLE R		_	620.95	0.00	78.54	4.06	60,45
73	1726,19	2	SLE R		24.63	145.96	0.00		3.64	54.51
	1785.71	-	SLE R	-41762.70		-204.98	_	78.54	3.50	52.38
75	1845.24	2	SLE R	-39667.00	-75.40	-446.82	_	78.54	3,46	51.55
7.6	1904.76	2	SLE R	-37573.50 -35482.00	-100.31 -111.80	-594.43 -662.52		78.54	3,36	50.05 47.99
78	2023.81	2	SLE R	-33392.30	-112.31	+665.53	THE RESIDENCE OF THE PERSON NAMED IN	78.54	3.06	45.46
79		2	SLE R			-617.65		78.54	2.87	42.58
80	2142.86	2	SLE R	-29218.40	-89.91	-532.80	_	78.54	2,65	39.43
81	2202.38	2	SLE R	-27133.80	-71.66	~424.65	0.00	78.54	2.43	36.11
82	2261.90	2	SLE R	-25050.70	-51.74	-306.63	0.00	78.54	2,20	32.73
83	2321.43	2	SLE R	-22968.90	-	-192.05	0.00	78.54	1.97	29.38
_	2380.95	-	SLE R			-94.04	-	78.54	1.75	26.14
	2440.48			-18808.90						23.12
87	0.00	_		-16730.50 -95363.70			0.00			20.40
88				-95908.90					45.99	721.95
89				-95319.40						776.28
90				-94732.90						801.88
91	The state of the s			-94149.40					48.16	802.74
92	297.62	4	SLE Q	-93568,80	8648.25	51249.90	40.84	37.70	47.39	783.01
93				-92991.20						745.20
94				-90810.40						702.86
9.5		_		-88634.50						643.82
96				-86463.30						573.33 496.17
98				-84296.80 -82134.80					32.61	447.37
99	and the second second second			-79977.20						404.25
100				-77823.80						361.80
101				-75674.70						321.16
102	892,86	4		-73529.60						283.33
103	952.38	4	SLE Q	-71388.50	3457.28	20488.00	28.27	50.27	17.72	249.08
	1011.90			-69251.20						218.88
_	1071.43			-67117.60					13.58	192.78
_	1130.95	_	_	-64987.60				_		170.53
_	1190,48	-		-62861.10						151.60
	1250.00			-60737.90						135.15
	1309.52			-58618.00 -56501.30				78.54		120.31
_	1428.57	_		-54387.60			_	78.54	6.53	95.10
100	1488.10	_		-52276.80			_	_		84.60

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113	1547.62	4	SLE Q	-50168.80	337,91	2002.49	0.00	78.54	5.12	75.39
114	1607.14	4	SLE Q	-48063.50	208.39	1234.91	0.00	78.54	4.55	67.37
115	1666.67	4	SLE Q	-45960.80	104.78	620.95	0.00	78.54	4.06	60.45
116	1726.19	4	SLE Q	-43860.60	24.63	145.96	0.00	78.54	3.64	54.51
117	1785.71	4	SLE Q	-41762.70	-34.59	-204.98	0.00	78.54	3.50	52.38
118	1845.24	4	SLE Q	-39667.00	-75.40	-446.82	0.00	78.54	3.46	51.55
119	1904.76	4	SLE Q	-37573.50	-100.31	-594.43	0.00	78.54	3.36	50.05
120	1964.29	4	SLE Q	-35482.00	-111.80	-662.52	0.00	78.54	3,23	47.99
121	2023.81	4	SLE Q	-33392,30	-112.31	~665.53	0.00	78.54	3.06	45.46
122	2083,33	4	SLE Q	-31304.50	-104.23	-617.65	0.00	78.54	2.87	42.58
123	2142.86	4	SLE Q	-29218.40	-89.91	-532.80	0.00	78.54	2,65	39.43
124	2202,38	4	SLE Q	-27133.80	-71.66	-424.65	0.00	78.54	2,43	36.11
125	2261.90	4	SLE Q	-25050.70	-51.74	-306.63	0.00	78.54	2.20	32.73
126	2321.43	4	SLE Q	-22968.90	-32.41	-192.05	0.00	78.54	1.97	29.38
127	2380.95	4	SLE Q	-20888.40	-15.87	-94.04	0.00	78.54	1.75	26.14
128	2440.48	4	SLE Q	-18808.90	-4.33	-25.68	0.00	78.54	1.54	23.12
129	2500.00	4	SLE Q	-16730.50	0.00	0.00	0.00	78.54	1.36	20.40

Stato	limite	d'esercizio	- Verifiche	a	fessurazione
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Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <dann></dann>	c <mm></mm>	5 <mm></mm>	K 2	•eq	Δ _{SM}	A _B	Ac eff <cmq></cmq>	σ _{ii} <dan cmq=""></dan>	€ _{ED}	Wk <mm></mm>
87	0.00	4	SLE Q	-95363.70	47580.30	8029.03	46.00	136.36	0.50	20.00	189.78	21.99	1075.18	646.02	0.19	0.06
88	59,52	4	SLE Q	-95908.90	50090.60	8452.63	46.00	136.36	0.50	20.00	191.69	21.99	1096.18	721.95	0.21	0.07
89	119.05	4	SLE Q	-95319.40	51566.80	8701.73	45.00	136.36	0.50	20.00	193.06	21.99	1111.21	776.28	0.23	0.07
90	178.57	4	SLE Q	-94732.90	52160,80	8801,97	46.00	136.36	0.50	20.00	193.71	21.99	1118.38	801.88	0.23	0.08
91	238.09	4	SLE Q	-94149.40	52012.60	8776.95	46.00	136.36	0.50	20.00	193.83	21.99	1119.71	802.74	0.23	0.08
92	297.62	4	SLE Q	-93568.80	51249.90	8648.25	46.00	136.36	0.50	20.00	193.52	21.99	1116.26	783.01	0.23	0.08
93	357.14	4	SIE Q	-92991.20	49941.80	8427.51	46,00	136.36	0.50	20,00	192.78	21.99	1108.18	745.20	0.22	0.07
94	416.67	4	SLE Q	-90810.40	48016.50	8102.63	46.00	136.36	0.50	20.00	192.18	21.99	1101.56	702.86	0.20	0.07
95	476.19	4	SLE Q	-88634.50	45573.00	7690.29	46.00	136.36	0.50	20.00	191.06	21.99	1089.19	643.82	0.19	0.06
96	535,71	4	SLE Q	-86463.30	42749.70	7213.87	46.00	136.36	0.50	20.00	205.62	18.85	1070.80	573.33	0.17	0.06
97	595.24	4	SLE Q	-84296.80	39667.10	6693.70	46.00	136.36	0.50	20.00	202,94	18.85	1045.63	496.17	0.14	0.05
98	654.76	4	SLE Q	-82134.80	36428.80	6147.24	46.00	136.36	0.50	20.00	199,43	18.85	1012.47	416.64	0.12	0.04
99	714.29	4	SLE Q	-79977.20	33122.30	5589.28	46.00	136.36	0.50	20,00	215.44	15.71	969.46	338.59	0.10	0.04
100	773.81	4	SLE Q	-77823.80	29820.80	5032.17	46.00	136.36	0.50	20.00	208.06	15.71	911.56	265.35	0.08	0.03
101	833,33	4	SLE Q	-75674.70	26584.30	4486.02	46.00	136.36	0.50	20.00	198.13	15.71	833.54	199.64	0.06	0.00
102	892.86	4	SLE Q	-73529.60	23460.90	3958.95	46.00	136.36	0.50	20.00	184,88	15.71	729.48	143.30	0.04	0.01
103	952,38	4	SLE Q	-71388.50	20488.00	3457.28	46.00	136.36	0.50	20,00	184,70	12.57	582,47	97.14	0.03	0.03
104	1011.90	4	SLE Q	-69251.20	17693.80	2985.78	46.00	136.36	0.50	20.00	183.07	9.42	429.18	60.98	0.02	0.03
105	1071.43	4	SLE Q	-67117.60	15098.40	2547.80	46.00	136.36	0.50	20.00	150.60	9.42	276.17	33.65	0.01	0.00
130	0.00	3	SLE F	-95363.70	47580.30	8029.03	46.00	136.36	0.50	20,00	189,78	21.99	1075,18	646+02	0.19	0.00
131	59.52	3	SLE F	-95908.90	50090.60	8452.63	46.00	136.36	0.50	20.00	191,69	21.99	1096.18	721.95	0.21	0.07
132	119.05	3	SLE F	-95319.40	51566.80	8701.73	46.00	136,36	0.50	20.00	193.06	21.99	1111.21	776.28	0.23	0.0
133	178.57	3	SLE F	-94732.90	52160.80	8801.97	46.00	136.36	0.50	20.00	193.71	21.99	1118.38	801.88	0.23	0.08
134	238.09	3	SLE F	-94149.40	52012.60	8776.95	46.00	136.36	0.50	20.00	193.83	21.99	1119.71	802.74	0.23	0.08
135	297.62	3	SLE F	-93568.80	51249.90	8648.25	46.00	136.36	0.50	20.00	193.52	21.99	1116.26	783.01	0.23	0.08
136	357.14	.3	SLE F	-92991.20	49941.80	8427.51	46.00	136.36	0.50	20.00	192.78	21.99	1108.18	745.20	0.22	0.07
137	416.67	3	SLE F	-90B10.40	48016.50	8102.63	46.00	136.36	0.50	20.00	192.18	21.99	1101.56	702.86	0.20	0.03
138	476,19	3	SLE F	-88634.50	45573.00	7690.29	46.00	136.36	0.50	20.00	191.06	21.99	1089.19	643,82	0.19	0.00
139	535.71	-3	SLE F	-86463.30	42749.70	7213.87	46.00	136.36	0.50	20.00	205.62	18.85	1070.80	573.33	0.17	0.00
140	595,24	3	SIE F	-84296.80	39667.10	6693.70	46.00	136.36	0.50	20.00	202,94	18.85	1045.63	496.17	0.14	0.05
141	654.76	3	SLE F	-82134.80	36428.80	6147.24	46.00	136.36	0.50	20.00	199.43	18.85	1012.47	416.64	0.12	0.04
142	714.29	3	SLE F	-79977.20	33122.30	5589.28	46.00	136.36	0.50	20.00	215.44	15.71	969.46	338.59	0.10	0.04
143	773.81	3	SLE F	-77823.80	29820.80	5032.17	46.00	136.36	0.50	20,00	208.06	15.71	911.56	265.35	0.08	0.03
144	833.33	3	SLE F	-75674.70	26584.30	4486.02	46.00	136.36	0.50	20.00	198.13	15.71	833.54	199.64	0.06	0.02
145	892.86	3	SLE F	-73529.60	23460.90	3958.95	46.00	136,36	0.50	20.00	184,88	15.71	729.48	143.30	0.04	0.01
146	952.38	3	SLE F	-71388.50	20488.00	3457.28	46,00	136.36	0.50	20.00	184.70	12.57	582.47	97.14	0.03	0.03
147	1011.90	3	SLE F	-69251.20	17693.80	2985.78	46.00	136.36	0.50	20.00	183.07	9,42	429.18	60.98	0.02	0.01
148	1071.43	3	SLE F	-67117.60	15098.40	2547.80	46.00	136.36	0.50	20.00	150.60	9.42	276.17	33.65	0.01	0.00

Verifiche principali

Caso	Tipo
4	SLU N cost - min. sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
48	C.Rare - Sf max (max traz.)
65	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
91	C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 2

Caratteristiche del pe	alo e	dei	materiali	utilizzati
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R	Cf	01-	Fck	Fetk	Fod	Fetd	-	Fyk	Fyd
<cm></cm>	<cm></cm>	CTS	<dan cmg=""></dan>	<dan cmg=""></dan>	<dan cmq=""></dan>	<dan cmq=""></dan>	тр	<dan cmg=""></dan>	<dan cmq=""></dan>

1	60.00 6.	00 030/37	307.10	20.59	174.02	13.73 B450C	4300.00	3913.0

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti.

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	M2 <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 2 (-104)

Caso	oc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1.	1	SIAI	RVN	204703.00	6547.96	-722.53	55868.70	-22829.50
	. 1	SLU	TAG				0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SLU	TOT	204703.00	6647.96	-722.53	55868.70	-22829.50
2	2	SLE R	RVN	151632.00	4924.41	-535.21	41384.20	-16910.80
	2	SLE R	TAG				0,00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	151632.00	4924.41	-535.21	41384.20	-16910.80
- 3	.3	SLE F	RVN	151632.00	4924.41	-535.21	41384.20	-16910.80
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	151632.00	4924.41	-535.21	41384.20	-16910.80
4	4	SLE Q	RVN	151632.00	4924,41	-535.21	41384,20	-16910.80
	4	SLE Q	TAG				0.00	0.00
	4	SIE Q	ECC				0.00	0.00
	-4	SLE Q	TOT	151632.00	4924.41	-535.21	41384.20	-16910.80

Sollecitazioni nei pali

Caso	8	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-204703.00	-6647.96	722.53	-55868.70	22829.50
2	2	SLE R	1	-151632.00	-4924.41	535.21	-41384.20	16910.80
3	3	SLE F	1	-151632.00	-4924.41	535.21	-41384.20	16910.80
-4	4	SLE Q	. 1	-151632.00	-4924.41	535.21	-41384.20	16910.80

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-204703.00	55644.40	22737.80	-204703.00	208278.00	86386.20	2-3	157.50	3.75
2	59.52	1	SIA	-204488.00	58655.40	23968.20	-204488.00	208211.00	86356.10	2-3	157.50	3,55
.3	119.05	1	SIU	-202382.00	60445.40	24699.70	-202382.00	207548.00	86060.70	2-3	157.50	3.44
4	178.57	1	SIJ	-200283.00	61193.10	25005.20	-200283.00	206887.00	85766.30	2-3	157.50	3.38
5	238.09	1	SLU	-198189.00	61063.50	24952.20	-198189.00	206228.00	85472.70	2-3	157.50	3.38
- 6	297.62	1	SLU	-196102.00	60207.00	24602,30	-196102.00	205568.00	85178.10	2-3	157.50	3.42
- 7	357.14	1	SIU	-194021.00	58704.80	23988.40	-194021.00	204909.00	84882,80	2-3	157.50	3,49
- 8	416.67	1	SIJ	-189272.00	56471.20	23075.70	-189272.00	203402.00	84209.00	2-3	157.50	3,60
9	476.19	1	SLU	-184534.00	53622.40	21911.60	-184534.00	201892.00	83532.20	2-3	157.50	3,77
10	535.71	1	SIJ	-179806.00	50322.00	20563.00	-179806.00	200381.00	82853.40	2-3	157.50	3.98
11	595.24	1	SLU	-175087.00	46712.30	19087.90	-175087.00	198867.00	82172.40	2-3	157.50	4.26
12	654.76	1	SLU	-170378.00	42915.40	17536.40	-170378.00	197350.00	81488.80	2-3	157.50	4,60
13	714.29	1	SIA	-165678.00	39034.90	15950.80	-165678.00	195832.00	80803.80	2-3	157.50	5.02
14	773.81	1	SLU	-160986.00	35157.40	14366.30	-160986.00	194311.00	80115,30	2-3	157.50	5.53
15	833.33	1	SIU	-156304.00	31353.80	12812.00	-156304.00	192789.00	79426.60	2-3	157.50	6.15
16	892.86	1	SIU	-151629.00	27681.10	11311.20	-151629.00	191263.00	78733.40	2-3	157.50	6.91
17	952,38	1	SLU	-146963.00	24183.60	9882.10	-146963.00	189737.00	78041,10	2-3	157.50	7,85
18	1011.90	1	SLU	-142305.00	20895.00	8538.26	-142305.00	188207.00	77343.20	2-3	157.50	9.01
19	1071.43	.1	SLU	-137654.00	17838.90	7289.47	-137654.00	186676.00	76646.50	2-3	157.50	10.47
20	1130.95	1	SIU	-133011.00	15031.00	6142.07	-133011.00	185141.00	75946,70	2-3	157.50	12.32
21	1190.48	1	SIAI	-128375.00	12479.50	5099.48	-128375.00	183498.00	75373,80	2-3	157.50	14.71
22	1250.00	1	SIU	-123746.00	10187.00	4162.70	-123746,00	181847.00	74801.50	2-3	157.50	17.86
23	1309,52	1	SLU	-119123,00	8150.93	3330.69	-2571250,00	180195.00	74228,30	2-3	157.50	21.58
24	1369.05	1	SIA	-114507.00	6364.62	2600.76	-2571250.00	178536.00	73655.90	2-3	157.50	22.45
25	1428,57	1	SIU	-109897.00	4818.26	1968.88	-2571250.00	176875.00	73082.70	2-3	157.50	23.39
26	1488.10	1	SIU	-105293.00	3499.49	1429.99	-2571250.00	175208.00	72510.50	2-3	157.50	24.42
27	1547.62	1	SIU	-100695.00	2394.02	978.26	-2571250.00	173537.00	71937.90	2-3	157.50	25.53
28	1607.14	1	SLU	-96101.50	1486.17	607.29	-2571250.00	171862.00	71366,20	2-3	157.50	26.75
29	1666.67	1	SIU	-91513.50	759.33	310.28	-2571250.00	170182.00	70794,40	2-3	157.50	28,09
30	1726.19	1	SIJ	-86930.50	196,28	80.20	-2571250.00	168499.00	70223.50	2-3	157.50	29.57
31	1785.71	1	SLU	-82352.10	-220.50	-90.10	-2571250.00	-167096.00	-68709.10	2-3	337.50	31.22
	1845.24	1	SLU	-77778.20	-508.57	-207.82	-2571250.00	-165477.00	-67941.00	2-3	337.50	33.05

33	1904.76	1	SLU	-73208.40	-685.44	-280.09	-2571250.00	-163838.00	-67189.70	2-3	337.50	35.122
34	1964.29	1	SIA	-68642.50	-768.39	-313.99	-2571250.00	-162196.00	-66436.40	2-3	337.50	37.459
35	2023.81	1	SIU	-64080.40	-774.42	~316.45	-2571250,00	-160551.00	-65680.50	2-3	337.50	40.125
36	2083.33	1	SLU	-59521.60	-720.24	-294.31	-2571250.00	-158903.00	-64923.80	2-3	337.50	43.199
37	2142.86	1	SLU	-54966.10	-622.22	-254.25	-2571250.00	-157225.00	-64197.90	2-3	337.50	46.779
38	2202.38	1	SLU	-50413.50	-496.46	-202.87	-2571250.00	-155456.00	-63583,40	2-3	337.50	51.003
39	2261.90	1	SLU	-45863.60	-358.79	-146.61	-2571250.00	-153676.00	-62971.90	2-3	337.50	56.063
40	2321,43	1	SLU	-41316,20	-224.87	-91.89	-2571250.00	-151895.00	-62358.90	2-3	337.50	62.233
41	2380.95	1	SLU	-36771.00	-110.17	-45.02	-2571250.00	-150103.00	-61749.70	2-3	337.50	69,926
42	2440.48	1	SIJ	-32227.70	-30.10	-12.30	-2571250.00	-148310.00	-61138,60	2-3	337.50	79.784
43	2500.00	1	SLU	-27686.20	0.00	0.00	-2571250.00					92.871

Stato limite ultimo - Verifiche a taglio

Caso	X <cm></cm>	œ	TOC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	6647.96	-722.53	0.85	11.31	6687.11	1.00	32294.70	360990.00	32294.70	4.829
2	59.52	1	SLU	4275.18	-464.64	0.85	11.31	4300.35	1.00	32294.70	360959.00	32294.70	7.510
3	119.05	1	SIA	2237,61	-243.19	0.85	11.31	2250.78	1.00	32294.70	360657.00	32294.70	14.348
- 4	178.57	1	SLU	510.17	-55.45	0.85	11.31	513.17	1.00	32294.70	360356.00	32294.70	62.931
- 5	238.09	1	SIU	-932.73	101.37	0.85	11.31	938.22	1.00	32294.70	360057.00	32294.70	34.421
- 6	297.62	1	SIJJ	-2116.81	230.06	0.85	11.31	2129.27	1.00	32294.70	359758.00	32294.70	15.167
7	357.14	1	SLU	-3366.63	365,90	0.85	11.31	3386.45	1.00	32294.70	359460.00	32294.70	9.536
8	416.67	1	SLU	-4637.46	504.02	0.85	11.31	4664.77	1,00	32294.70	358779.00	32294.70	6,923
9	476,19	1	SLU	-5593.18	607.89	0.85	11.31	5626.11	1.00	32294.70	358101.00	32294.70	5.740
10	535.71	1	SLU	-6273.38	681.82	0.85	11,31	6310.32	1.00	32294.70	357423.00	32294.70	5.118
11	595.24	1	SLU	-6715,46	729.86	0.85	11.31	6755.01	1,00	32294.70	356747.00	32294.70	4.781
12	654.76	1	SLU	-6954.31	755.82	0.85	11.31	6995.26	1.00	32294.70	356073.00	32294.70	4.617
13	714,29	1	SLU	-7022.14	763.19	0.85	11.31	7063.49	1.00	32294.70	355400.00	32294.70	4.572
14	773.81	1	SLU	-6948.38	755.18	0.85	11.31	6989.30	1.00	32294.70	354728.00	32294.70	4,621
15	833.33	1	SIU	-6759.70	734.67	0.85	11.31	6799.51	1.00	32294.70	354057.00	32294.70	4.750
16	892.86	1	SIN	-6479.96	704.27	0.85	11.31	6518.12	1.00	32294.70	353387.00	32294.70	4.955
17	952.38	1	SLU	-6130.36	666.27	0.85	11.31	6166.46	1.00	32294.70	352719.00	32294.70	5.237
18	1011.90	1	SLU	-5729.49	622.70	0.85	11.31	5763.23	1.00	32294.70	352052.00	32294.70	5.604
19	1071.43	1	SLU	-5293.52	575.32	0.85	11.31	5324,69	1.00	32294.70	351386.00	32294.70	6,065
20	1130.95	1	SIJ	-4836.33	525.63	0.85	11.31	4864,81	1.00	32294.70	350721.00	32294.70	6.638
21	1190.48	1	SLU	-4369.70	474.92	0.85	11.31	4395.43	1.00	32294.70	350056.00	32294.70	7.347
22	1250.00	1	SLU	-3903.47	424.25	0.85	11.31	3926.45	1.00	32294.70	349393.00	32294.70	8.225
23	1309.52	1	SIJ	-3445.74	374.50	0.85	11.31	3466.03	1.00	32294.70	348731.00	32294.70	9.318
24	1369.05	1	SIM	~3003.06	326.38	0.85	11.31	3020.75	1,00	32294.70	348070.00	32294.70	10.591
25	1428,57	1	SIU	-2580,63	280,47	0.85	11.31	2595.82	1.00	32294.70	347410.00	32294.70	12,441
26	1488,10	1	SLU	-2182.41	237.19	0.85	11.31	2195.26	1.00	32294.70	346750.00	32294.70	14,711
27	1547.62	1	SIL	-1811.36	196.87	0.85	11.31	1822.03	1.00	32294.70	346092.00	32294.70	17.725
28	1607.14	1	SIU	-1469.57	159.72	0.85	11,31	1478.22	1.00	32294.70	345434.00	32294.70	21.847
29	1666.67	1	SIU	-1158.40	125.90	0.85	11.31	1165.22	1.00	32294.70	344776.00	32294.70	27.71
30	1726.19	1	SLU	-878.63	95.49	0.85	11.31	883.80	1.00	32294.70	344120.00	32294.70	36.541
31	1785.71	1	SLU	-630.57	68.53	0.85	11,31	634.28	1.00	32294.70	343464,00	32294.70	50.915
32	1845,24	1	SLU	-414.20	45.02	0.85	11.31	416.64	1.00	32294.70	342809.00	32294.70	77.513
33	1904.76	1	SLU	-229.23	24.91	0.85	11.31	230.58	1.00	32294.70	342154.00	32294.70	>100
34	1964.29	1	SLU	-75.20	8.17	0.85	11.31	75.65	1.00	32294.70	341500.00	32294.70	>100
35	2023.81	-1	SIU	48.41	-5.26	0.85	11.31	48.70	1.00	32294.70	340847.00	32294.70	>100
36	2083.33	1	SLU	142.19	-15.45	0.85	11.31	143.02	1,00	32294.70	340194.00	32294.70	>100
37	2142.86	1	SLU	206.67	-22,46	0.85	11.31	207.89	1.00	32294.70	339541.00	32294.70	>100
38	2202,38	1	SIU	242,37	-26.34	0.85	11.31	243.79	1.00	32294.70	338889.00	32294.70	>100
39	2261,90	1	SLU	249.68	-27.14	0.85	11.31	251.15	1.00	32294.70	338238.00	32294.70	>100
40	2321.43	1	SIA	228.93	-24.88	0.85	11.31	230.28	1.00	32294.70	337586.00	32294.70	>100
41	2380.95	1	SIU	180.32	-19.60	0.85	11.31	181.39	1.00	32294.70	336935.00	32294.70	>100
42	2440.48	1	SIJJ	104.00	-11.30	0.85	11.31	104.61	1.00	32294.70	336284.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	Afc <amq></amq>	σ ₀ <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-151632.00	16842.80	41238.00	28.27	50.27	38.18	534.34
45	59.52	2	SLE R	-151786.00	17754.20	43448.50	28.27	50.27	40.20	561.08
46	119.05	2	SLE R	-150416.00	18296.00	44774.40	31.42	47.12	41.45	577.26
47	178,57	2	SLE R	-149051.00	18522.40	4532B.20	31.42	47,12	41.99	584.14
48	238.09	2	SLE R	-147690.00	18483.10	45232.20	31.42	47.12	41.91	582.85
49	297.62	2	SLE B	-146334.00	18223.90	44597.80	31.42	47.12	41.32	574.71
50	357.14	2	SLE R	-144983.00	17769.20	43485.10	31,42	47,12	40.26	560.53
51	416.67	2	SLE B	-141481.00	17093.10	41830.50	31.42	47.12	38.72	539.42
52	476.19	2	SLE B	-137986.00	16230.80	39720.30	28.27	50.27	36.75	512.78
53	535,71	- 2	SLE R	-134499.00	15231.80	37275.50	28.27	50.27	34.51	482.41
54	595,24	2	SLE R	-131019.00	14139.20	34601.70	28.27	50.27	32,11	449.93
55	654.76	2	SLE B	-127546.00	12989.90	31789.20	25.13	53.41	29,66	416.73
56	714.29	2	SLE R	-124080.00	11815.40	28914.80	21.99	56.55	27.25	383.96
5.7	773.81	2	SLE B	-120621.00	10641.70	26042.50	21.99	56.55	24.94	352.50
.58	833,33	2	SLE B	-117168.00	9490.40	23225.00	15.71	62,83	22,78	322.94
59	892,86	2	SLE B	-113721.00	8378.70	20504.50	12.57	65.97	20.79	295.59

-		10.00	A BANKS OF THE PARTY.
NO	lazione	OI CO	Olcole.
1/6	Idalionie	ui cc	

	Ž	2				W			ne di cal	
- 50	952,38	_		-110281.00			_	75.40		
_	1011.90	2	SLE R	-106846.00	6324.64	15477.70	0.00	78.54	17.32	247.65
62	1071.43	2	SLE R	-103417.00	5399.61	13214.00	0.00	78.54	15.77	226.30
63	1130.95	2	SLE R	-99993.90	4549.68	11134.00	0.00	78.54	14.34	206.35
64	1190,48	2	SLE R	-96575.90	3777.39	9244.09	0.00	78.54	13.00	187.85
65	1250.00	2	SLE R	-93163.10	3083.48	7545.95	0.00	78.54	11.78	170.81
.66	1309.52	2	SLE R	-89755.30	2467.18	6037.72	0.00	78.54	10.66	155.22
67	1369.05	2	SLE R	-86352.30	1926.49	4714.53	0.00	78,54	9.65	141.04
-68	1428.57	2	SLE R	-82953.90	1458.43	3569.08	0.00	78.54	8.73	128.21
69	1488.10	_	SLE R		1059.25	2592.21	_	78.54	7.91	116.66
_	1547.62		SLE R		724.64	1773.35	_	78.54	7.18	106.32
-	1607.14	_	SLE R	-	449.85	1100.87	_	78.54	6.53	97.09
	1666.67	-	SLE R		229.84	562.47	_	78.54	5.95	88.88
	1726.19	-	SLE R		59.41	145.39	_	78.54	5.45	81,60
	1785.71	_	SLE R		-66.74	-163.33	-	78.54	5.18	77.63
	1845.24	_	SLE R		-153.94		_	78.54	5.03	75.14
_	-	_	_		-207.47		-			-
_	1904.76	_	SLE R			-507.73		78.54	4.83	72.03
_	1964.29	-	SLE B		-232.58	-569.18	-	78.54	4.59	68.39
_	2023,81	_	SLE R		-234,41	-573.64	_	78.54	4,32	64.32
_	2083.33	_	SLE R		-218.01	-533.51		78.54	4.02	59.92
	2142.86	_	SLE R		-188.34	-460.90	_	78.54	3.71	55.28
_	2202.38	_	SLE R		-150.27	-367.75	-	78.54	3.38	50.48
82	2261,90	2	SLE R	-35761.40	-108.60	-265.77	0.00	78,54	3.06	45.62
83	2321.43	2	SLE R	-32410.80	-68.06	-166.57	0.00	78.54	2.73	40.78
84	2380.95	2	SLE R	-29061.90	-33.35	-81.61	0.00	78.54	2.41	36.05
85	2440.48	2	SLE R	-25714.50	-9.11	-22.30	0.00	78.54	2.10	31.52
86	2500.00	2	SLE R	-22368.60	0.00	0.00	0.00	78.54	1.82	27.27
87	0.00	4	SLE Q	-151632.00	16842.80	41218.00	28.27	50.27	38.18	534.34
88	59.52	4	SLE Q	-151786.00	17754.20	43448.50	28.27	50.27	40.20	561.08
89	119.05	4	SLE Q	-150416.00	18296.00	44774.40	31.42	47.12	41,45	577,26
90	178.57	-	SLE Q			45328.20	31.42	47.12	41.99	584.14
91	238.09	4	SLE Q	-147690.00	18483.10	45232.20	31.42	47.12	41.91	582.85
92	297.62	4	SLE Q	-146334.00	18223.90	44597.80	31.42	47.12	41.32	574.71
93		_	SLE Q			43485.10	_	47.12	40.26	560.53
94			SLE Q				_	47.12	38.72	539.42
95	-	_	SLE Q	The state of the s	-	and the second second	and the same of	50,27	36,75	512.78
96		_	_	-134499.00			_	50.27	34.51	482.41
97	595.24	_	SIE Q				_	50.27	32,11	449.93
98		_	SLE Q	7-1-1-2-1-2-1-2-1			_	_	29.66	416.73
99	-		SLE Q				_	56.55	27.25	383.96
100	773.81	-			10641.70			-	24.94	352.50
	833.33	_			9490.40					322,94
101		_					15.71	62,83	22,78	
102		_	-			20504.50		-	20.79	295.59
				-110281.00						
	1011.90	_		-106846.00			_	78,54		
	1071.43			-103417.00		13214.00		78.54		226.30
-	1130.95			-99993.90						
_	1190.48			-96575.90		9244.09	_	-		
_	1250,00		SLE Q					78,54		170.81
$\overline{}$	1309.52			-89755.30			_	78.54		
_	1369.05		SLE Q				_	78.54		
_	1428.57		SLE Q					78.54		
_	1488.10		SLE Q					78.54		The second secon
	1547.62		SLE Q					78.54		
	1607.14		SLE Q					78,54		
	1666.67			-69403.20				78.54	-	
	1726,19		SLE Q					78.54		
_	1785.71		SLE Q					78.54		
-	1845.24		SLE Q					78.54		
	1904.76		SLE Q					78.54	ALC DATE OF THE PARTY NAMED IN	
	1964.29		SLE Q		-232,58	-569.18	0.00	78.54	4.59	68.39
121	2023.81		SLE Q			-573.64	0.00	78.54	4,32	64.32
	2083.33		SLE Q	-45825.60	-218.01			78.54	4.02	59.92
123	2142.86		SLE Q			-460.90	0.00	78.54	3.71	55.28
	2202,38		SLE Q				_	78.54		
	2261.90		SLE Q		THE RESERVE OF THE PERSON NAMED IN	THE RESERVE AND ADDRESS OF THE PARTY OF THE		78.54		The second secon
	2321.43		SLE Q					78.54		
-			SLE Q					78.54		36.05
127	2380.95	- 2	100000						1000000	
_	2440.48		SLE Q				0.00	78.54	2,10	31,52
128		4		-25714.50		-22.30	_	78.54 78.54		31.52 27.27

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	Φeq	Δ _{EIII}		Ac eff <mq></mq>	σ _S <dan cmq=""></dan>	€ _{SM}	Wk <mm></mm>
87	0.00	4	SLE Q	-151632.00	41218.00	16842.80	46.00	136.36	0.50	20.00	183.04	12.57	572.01	212.49	0.06	0.02
88	59.52	4	SLE Q	-151786.00	43448,50	17754.20	46.00	136.36	0.50	20.00	194.37	12.57	643.23	254.07	0.07	0.02
89	119.05	4	SLE Q	-150416.00	44774.40	18296.00	46.00	136.36	0.50	20.00	180.85	15.71	697.86	286.71	0.08	0.03

		Relazione di calcolo														
90	178.57	4	SLE C	-149051.00	45328.20	18522.40			10000000			15.71	727.24	304.57	0.09	0.03
91	238.09	4	SLE Q	-147690.00	45232.20	18483.10	46.00	136.36	0.50	20.00	185.76	15.71	736.40	308.71	0.09	0.03
92	297.62	4	SLE C	-146334.00	44597.80	18223.90	46.00	136.36	0.50	20.00	184.95	15.71	730.06	301.10	0.09	0.03
-93	357.14	4	SLE C	-144983.00	43485.10	17769.20	46.00	136.36	0.50	20.00	182.20	15.71	708.46	283.27	0.08	0.03
94	416.67	4	SLE C	-141481.00	41830.50	17093.10	46.00	136.36	0.50	20.00	179.65	15,71	688.38	263.76	0.08	0.02
95	476.19	4	SLE Q	-137986.00	39720.30	16230.80	46.00	136.36	0.50	20.00	195.61	12.57	651.03	235.37	0.07	0.02
96	535.71	4	SLE C	-134499.00	37275.50	15231.80	46.00	136.36	0.50	20.00	187.26	12.57	598.53	201.63	0.06	0.02
97	595.24	4	SLE C	-131019.00	34601.70	14139.20	46.00	136,36	0.50	20.00	176.81	12.57	532.89	165.69	0.05	0.01
98	654.76	4	SLE (-127546.00	31789.20	12989.90	45.00	136,36	0.50	20.00	188.82	9.42	456.28	130.14	0.04	0.01
99	714.29	4	SLE Q	-124080.00	28914.80	11815.40	46.00	136,36	0.50	20.00	170.75	9.42	371.12	96.88	0.03	0.01
100	773.B1	4	SLE Q	-120621.00	26042.50	10641.70	46.00	136.36	0.50	20.00	181.47	6.28	281,08	67.12	0.02	0.01
101	833.33	4	SLE Q	-117168.00	23225.00	9490.40	46.00	136.36	0.50	20.00	213,87	3,14	191.44	41,42	0.01	0.00
130	0.00	3	SLE F	-151632.00	41218.00	16842.80	46.00	136,36	0.50	20.00	183.04	12.57	572.01	212.49	0.06	0.02
131	59.52	3	SLE F	-151786.00	43448.50	17754.20	46.00	136,36	0.50	20.00	194.37	12.57	643.23	254.07	0.07	0.02
132	119.05	3	SLE F	-150416.00	44774.40	18296.00	46.00	136.36	0.50	20.00	180.85	15.71	697.86	286.71	0.08	0.03
133	178.57	3	SLE F	-149051.00	45328,20	18522.40	46.00	136.36	0.50	20.00	184.59	15.71	727.24	304.57	0.09	0.03
134	238.09	3	SLE F	-147690.00	45232.20	18483.10	46.00	136.36	0.50	20,00	185.76	15.71	736.40	308.71	0.09	0.03
135	297.62	3	SLE F	-146334.00	44597.80	18223.90	46.00	136.36	0.50	20.00	184.95	15.71	730.06	301.10	0.09	0.03
136	357.14	3	SLE F	-144983.00	43485.10	17769.20	46.00	136.36	0.50	20.00	182.20	15.71	708.46	283.27	0.08	0.03
137	416.67	3	SLE F	-141481.00	41830.50	17093.10	46.00	136,36	0.50	20.00	179.65	15.71	688.38	263.76	0.08	0.02
138	476.19	3	SLE F	-137986.00	39720.30	16230.80	46.00	136.36	0.50	20.00	195.61	12.57	651.03	235.37	0.07	0.02
139	535.71	3	SLE F	-134499.00	37275.50	15231.80	46.00	136,36	0.50	20.00	187.26	12.57	598.53	201.63	0.06	0.02
140	595.24	3	SLE F	-131019.00	34601.70	14139.20	46.00	136.36	0.50	20.00	176.81	12.57	532.89	165.69	0.05	0.01
141	654.76	3	SLE P	-127546.00	31789.20	12989.90	46.00	136.36	0.50	20.00	188.82	9.42	456.28	130,14	0.04	0.01
142	714.29	3	SLE F	-124080.00	28914.80	11815.40	46.00	136.36	0.50	20.00	170.75	9,42	371.12	96,88	0.03	0.01
143	773.81	3	SLE F	-120621.00	26042,50	10641.70	46.00	136.36	0.50	20.00	181.47	.6.28	281.08	67,12	0.02	0.01
144	833.33	3	SLE F	-117168.00	23225.00	9490.40	46.00	136,36	0.50	20,00	213.87	3.14	191.44	41.42	0.01	0.00

Verifiche	princi	pali
PARTICIPATION NAMED IN	-	-

Caso	Tipo
- 5	SLU N cost - min. sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
48	C.Rare - Sf max (max traz.)
61	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
91	C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
104	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 3

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf (m)	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmc=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti.

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 3 (-138

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SIJ	RVN	274379.00	6268.79	-556.06	37336.20	-24981.40
	1	SLU	TAG		V.————		0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SLU	TOT	274379.00	6268.79	-556.06	37336.20	-24981.40
.2	2	SLE R	RVN	203244.00	4643.55	-411.90	27656.40	-18504.80
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	. 2	SLE R	TOT	203244.00	4643.55	-411.90	27656.40	-18504.80
- 3	.3	SLE F	RVN	203244.00	4643.55	-411.90	27656.40	-18504.80
	. 3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SIE F	TOT	203244.00	4643.55	-411.90	27656.40	-18504,80
4	4	SLE Q	RVN	203244.00	4643.55	-411.90	27656.40	-18504.80
	4	SIE Q	TAG				0.00	0.00
	-6	SLE Q	ECC				0.00	0.00
	4	SLE Q	TOT	203244.00	4643.55	-411.90	27656.40	-18504.80

37

Sollecitazioni nei pali

Caso	oc	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mix <danm></danm>	My <danm></danm>
1	.1	SLU	. 1	-274379.00	-6268.79	556.06	-37336.20	24981.40
2	2	SLE R	. 1	-203244+00	-4643.55	411.90	-27656.40	18504.80
3	3	SLE F	1	-203244.00	-4643.55	411,90	-27656.40	18504.80
4	4	SLE Q	1	-203244.00	-4643.55	411.90	-27656.40	18504.80

Da 0 a -25

Stato	limite	ultimo -	Verifiche a	flessione/	pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SIJ	-274379.00	37169.30	24869.80	-274379.00	206117.00	137723.00	2-3	146.25	5.54
2	59.52	1	SLU	-273680.00	39782.80	26618.40	-273680.00	205935.00	137605.00	2-3	146.25	5.17
3	119.05	1	SIJ	-270608.00	41486.90	27758.60	-27060B.00	205135.00	137083.00	2+3	146.25	4.94
.4	178.57	1	SIJ	-267543.00	42410.80	28376.80	-267543.00	204332.00	136560.00	2-3	146.25	4.81
5	238.09	1	SLU	-264488.00	42673.80	28552.80	-2644BB.00	203529.00	136038.00	2-3	146.25	4.76
- 6	297.62	1	SIU	-261440.00	42385.50	28359.90	-261440.00	202728.00	135516.00	2-3	146.25	4.78
7	357.14	- 1	SLU	-258401.00	41602.80	27836.20	-258401,00	201926,00	134994.00	2-3	146.25	4.85
8	416.67	1	SLU	-252017.00	40253.70	26933.50	-252017.00	200233.00	133892.00	2-3	146.25	4.97
.9	476.19	1	SILI	-245646.00	38422.10	25708.00	-245646.00	198534.00	132787.00	2-3	146.25	5.16
10	535.71	1	SIJ	-239288.00	36228.80	24240.50	-239288.00	196832.00	131679.00	2-3	146.25	5.43
11	595.24	1	SLU	-232943.00	33779.60	22601.80	-232943.00	195120.00	130567.00	2-3	146.25	5.77
12	654.76	1	SLU	-226610.00	31165.80	20852.90	-226610.00	193404.00	129452.00	2-3	146.25	6.20
13	714.29	1	SIJ	-220290.00	28465.20	19045.90	-220290.00	191682.00	128334.00	2-3	146.25	6.73
14	773.81	1	SLU	-213981.00	25743.20	17224.60	-213981.00	189954.00	127213.00	2-3	146.25	7.38
15	833.33	1	SIU	-207684.00	23053.90	15425.20	-207684.00	188222.00	126090.00	2-3	146.25	8.16
16	892,86	1	SIJ	-201398.00	20441.00	13677.00	-201398.00	186483.00	124963.00	2-3	146.25	9.12
17	952.38	1	SLU	-195123.00	17939.30	12003.10	-195123.00	184774.00	123705.00	2-3	146.25	10.30
18	1011,90	1	SIA	-188858.00	15575.20	10421.30	-188858,00	183079.00	122372.00	2-3	146.25	11.75
19	1071.43	1	SIU	-182604.00	13368.20	8944.59	-182604.00	181378.00	121028.00	2-3	146.25	13,55
20	1130,95	1	SLU	-176359.00	11331.30	7581.74	-2571250.00	179673.00	119680.00	2-3	146.25	14.58
21	1190.48	1	SIA	-170124.00	9472.51	6338.00	-2571250.00	177962.00	118326.00	2-3	146.25	15.11
22	1250.00	1	SIJJ	-163897.00	7795.03	5215.61	-2571250.00	176141.00	117042.00	2-3	146.25	15.68
23	1309.52	1	SIJ	-157680.00	6298.46	4214.26	-2571250,00	174244.00	115807.00	2-3	146.25	16,30
24	1369,05	1	SLU	-151471.00	4979,28	3331.60	-2571250.00	172329.00	114572.00	2-3	146.25	16.97
25	1428.57	1	SLU	-145270.00	3831.42	2563.58	-2571250.00	170379.00	113349.00	2-3	146.25	17.70
26	1488.10	1	SIJ	-139077.00	2846.87	1904.82	-2571250.00	168422.00	112124.00	2-3	146.25	18.48
27	1547.62	1	SLU	-132892.00	2016.07	1348.94	-2571250.00	166455.00	110894.00	2-3	146.25	19.34
28	1607.14	1	SLU	-126713.00	1328.35	888.79	-2571250.00	164477.00	109661.00	2-3	146.25	20.29
29	1666.67	1	SIJ	-120542.00	772.23	516.69	-2571250.00	162493.00	108425.00	2-3	146.25	21.33
30	1726.19	1	SLU	-114377.00	335,69	224.61	-2571250.00	160498.00	107185.00	2-3	146,25	22.48
31	1785,71	1	SIU	-108217.00	6.44	4.31	-2571250,00	158494.00	105942.00	2-3	146.25	23.76
32	1845.24	1	SIJ	-102064.00	-227.97	-152.54	-2571250.00	-156676.00	-104737.00	2-3	326.25	25.19
33	1904.76	1	SLU	-95916.50	-379.99	-254.25	-2571250.00	-154820.00	-103273.00	2-3	326.25	26.80
34	1964.29	1	SIU	-89773.90	-461.96	-309.10	-2571250.00	-152958.00	-101805.00	2-3	326.25	28.64
35	2023.81	1	SIA	-83636.10	-486.07	-325.23	-2571250.00	-150999.00	-100398.00	2-3	326.25	30.74
36	2083.33	1	SIJ	-77502.80	-464,33	-310,68	-2571250.00	-148935.00	-99061.70	2-3	326,25	33,17
37	2142.86	1	SLU	-71373.70	-408.55	-273.36	-2571250.00	-146864.00	-97720.50	2-3	326.25	36.02
38	2202.38	1	SIU	-65248.30	-330.35	-221.03	-2571250.00	-144780.00	-96371.30	2+3	326.25	39.40
39	2261.90	1	SIJ	-59126,50	-241.18	-161.37	-2571250.00	-142687.00	-95015.90	2-3	326.25	43.48
40	2321.43	1	SIJ	-53007.90	-152.37	-101.95	-2571250.00	-140587.00	-93655.10	2-3	326.25	48.50
41	2380.95	1	SLU	-46892.10	-75.13	-50.27	-2571250.00	-138476.00	-92287.80	2-3	326.25	54.83
42	2440.48	1	SLU	-4077B.80	-20.64	-13.81	-2571250,00	-136355.00	-90914.10	2-3	326.25	63.05
43	2500.00	1	SLU	-34667.70	0.00	0.00	-2571250.00					74.16

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIU	6268.79	-556.06	0.85	11.31	6293.40	1.00	32294.70	370970.00	32294.70	5.132
2	59.52	1	SLU	4301.75	-381.58	0.85	11.31	4318.64	1.00	32294.70	370870.00	32294.70	7.478
3	119.05	1	SIU	2604.02	-230.99	0.85	11.31	2614.25	1.00	32294.70	370430.00	32294.70	12.353
4	178,57	1	SIU	1156.50	-102.59	0.85	11.31	1161.05	1.00	32294.70	369991.00	32294.70	27.815
5	238.09	1	SLU	-60.52	5.37	0.85	11.31	60.75	1.00	32294.70	369553.00	32294.70	>100
.6	297.62	1	SIU	-1067.01	94.65	0.85	11.31	1071.20	1.00	32294.70	369117.00	32294.70	30,148
7	357.14	1	SLU	-2141.16	189.93	0.85	11.31	2149.57	1.00	32294.70	368681.00	32294.70	15.024
- 8	416.67	1	SLU	-3245.36	287.87	0.85	11.31	3258.10	1.00	32294.70	367767.00	32294.70	9.912
9	476.19	1	SIJJ	-4090.00	362.80	0.85	11.31	4106.06	1,00	32294.70	366854.00	32294.70	7.865
10	535.71	1	SLU	-4706.68	417.50	0.85	11.31	4725.16	1.00	32294.70	365944.00	32294.70	6.835
11	595,24	1	SLU	-5125.38	454.64	0.85	11.31	5145.50	1.00	32294.70	365035,00	32294.70	6.276
12	654.76	1	SIAJ	-5374.18	476.71	0.85	11.31	5395.28	1.00	32294.70	364128.00	32294.70	5.986
13	714.29	1	SLU	-5479.14	486.02	0.85	11.31	5500.66	1.00	32294.70	363222.00	32294.70	5.871
14	773.81	1	SIU	-5464.18	484.69	0.85	11.31	5485.63	1.00	32294.70	362319.00	32294.70	5.887
15	833.33	1	SLU	-5351.01	474.65	0.85	11.31	5372.02	1.00	32294.70	361417.00	32294.70	6.012
16	892,86	1	SLU	-5159.20	457.64	0.85	11.31	5179.46	1.00	32294.70	360516,00	32294.70	6.235

									MAL	OIL GI	ouloolo		
17	952.38	1	SLU	-4906.17	435,19	0.85	11.31	4925.43	1.00	32294.70	359617.00	32294.70	6.557
18	1011.90	1	SIA	-4607.28	408.68	0.85	11.31	4625.37	1.00	32294.70	358720.00	32294.70	6.982
19	1071.43	1	SIU	-4275.95	379.29	0.85	11.31	4292.74	1.00	32294.70	357824.00	32294.70	7.523
20	1130.95	1	SIJJ	-3923.76	348.05	0.85	11.31	3939.17	1.00	32294.70	356930.00	32294.70	8.198
21	1190,48	1	SLU	-3560,58	315.83	0.85	11.31	3574.56	1.00	32294.70	356036.00	32294.70	9.035
22	1250.00	1	SIU	-3194.72	283,38	0.85	11.31	3207.26	1.00	32294.70	355145.00	32294.70	10.069
23	1309.52	1	SLU	-2833.07	251.30	0.85	11.31	2844.20	1.00	32294.70	354254.00	32294.70	11.355
24	1369.05	1	SIU	-2481.27	220.10	0.85	11.31	2491.01	1.00	32294.70	353365.00	32294.70	12.964
25	1428.57	1	SLU	-2143.80	190.16	0.85	11.31	2152.21	1.00	32294.70	352477.00	32294.70	15.005
26	1488.10	1	SIU	-1824.16	161.81	0.85	11.31	1831.32	1.00	32294.70	351589.00	32294.70	17.635
27	1547.62	1	SLU	-1525.01	135.27	0.85	11.31	1530.99	1,00	32294.70	350703.00	32294.70	21.094
28	1607.14	1	SLU	-1248.26	110.72	0.85	11.31	1253.17	1.00	32294.70	34981B.00	32294.70	25,770
29	1666.67	1	SIJ	-995,25	88.28	0.85	11.31	999.16	1.00	32294.70	348934.00	32294.70	32,322
30	1726.19	-1	SLU	-766.78	68.02	0.85	11.31	769.79	1.00	32294.70	348051.00	32294.70	41.953
31	1785.71	1	SIU	-563.28	49.97	0.85	11.31	565.50	1.00	32294.70	347169.00	32294.70	57,109
32	1845.24	1	SIJI	-384.87	34.14	0.85	11.31	386.38	1.00	32294.70	346288.00	32294.70	83.582
33	1904.76	1	SIJ	-231.44	20.53	0.85	11.31	232.35	1.00	32294.70	345407.00	32294.70	>100
34	1964.29	1	SLU	-102.73	9.11	0.85	11.31	103.14	1.00	32294.70	344527.00	32294.70	>100
35	2023.81	1	SLU	1.61	-0.14	0.85	11.31	1.62	1.00	32294.70	343648,00	32294.70	>100
36	2083.33	1	SLU	81.97	-7.27	0.85	11.31	B2.30	1.00	32294.70	342770.00	32294.70	>100
37	2142.86	1	SLU	138.76	-12.31	0.85	11.31	139.30	1,00	32294.70	341892.00	32294.70	>100
38	2202.38	1	SLU	172.32	-15.29	0.85	11.31	172.99	1.00	32294.70	341014.00	32294.70	>100
39	2261.90	1	SIJJ	182.96	-16.23	0.85	11.31	183.68	1.00	32294.70	340137.00	32294.70	>100
40	2321.43	1	SLU	170.92	-15.16	0.85	11.31	171.59	1.00	32294.70	339261.00	32294.70	>100
41	2380.95	1	SLU	136,36	-12.10	0.85	11,31	136.89	1.00	32294.70	338385.00	32294.70	>100
42	2440.48	1	SLU	79.37	-7.04	0.85	11.31	79.68	1.00	32294.70	337509.00	32294.70	>100

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <cmq></cmq>	σ _□ <dan cmq=""></dan>	of <dan cmq2<="" th=""></dan>
44	0.00	2	SLE R	-203244.00	18422.10	27532.80	0.00	78.54	33.66	480.93
45	59.52	2	SLE R	-203039.00	19717.30	29468.70	3.14	75.40	34.87	497.46
46	119.05	2	SLE R	-200953.00	20562.00	30731.00	9,42	69.11	35.54	506.34
47	178.57	2	SLE R	-198874.00	21019.90	31415.40	12.57	65.97	35.85	510.30
48	238.09	2	SLE R	-196800.00	21150.20	31610.20	12.57	65.97	35.84	509.83
49	297.62	2	SLE R	-194733.00	21007.30	31396.70	12.57	65.97	35,55	505.67
50	357.14	2	SLE R	-192672.00	20619.40	30816.90	12.57	65.97	35.00	497.93
51	416.67	2	SLE R	-187958.00	19950.80	29817,60	12.57	65,97	33.97	483.46
52	476.19	2	SLE R	-183254.00	19042.90	28460.80	12.57	65.97	32.71	465.72
53	535.71	2	SLE R	-178560.00	17955.90	26836.20	6.28	72.26	31.27	445.6
54	595.24	2	SLE R	-173875.00	16742.00	25022,00	0.00	78.54	29.72	424.13
55	654.76	2	SLE R	-169200.00	15446.60	23085.80	0.00	78.54	28.12	401.80
56	714.29	2	SLE R	-164534.00	14108.10	21085.40	0.00	78.54	26.50	379.14
57	773.81	2	SLE R	-159876.00	12759.00	19069.00	0.00	78.54	24.86	356.39
58	833.33	2	SLE R	-155228.00	11426.10	17076.90	0.00	78,54	23.24	333.8
59	892.86	2	SLE R	-150587.00	10131.10	15141.50	0.00	78.54	21.66	311.83
60	952.38	2	SLE R	-145955.00	8891.17	13288.40	0.00	78.54	20.13	290.4
61	1011.90	2	SLE R	-141330.00	7719.48	11537.20	0.00	78.54	18.67	270.00
62	1071.43	2	SLE R	-136713.00	6625.62	9902.37	0.00	78.54	17.27	250.53
63	1130.95	2	SLE R	-132103.00	5616.10	8393.59	0.00	78.54	15.96	232.1
64	1190.48	2	SLE R	-127501.00	4694.81	7016.67	0.00	78.54	14.73	214.8
65	1250.00	- 2	SLE R	-122905.00	3863.41	5774.09	0.00	78.54	13.58	198.7
66	1309.52	2	SLE R	-118316.00	3121.68	4665.53	0.00	78.54	12.52	183.7
67	1369.05	2	SLE R	-113733.00	2467.B5	3688.35	0.00	78.54	11.54	169.90
68	1428.57	2	SLE R	-109156.00	1898.95	2838.09	0.00	78.54	10.64	157.17
69	1488.10	2	SLE R	-104585.00	1410.98	2108.79	0.00	78.54	9.81	145.3
7.0	1547.62	2	SLE R	-100020.00	999.22	1493.39	0.00	78.54	9.06	134.59
71	1607.14	2	SLE R	-95460.30	658.36	983.96	0.00	78.54	8.37	124.73
72	1666.67	2	SLE R	-90905.50	382.74	572.02	0.00	78.54	7.75	115.68
73	1726.19	2	SLE R	-86355.60	166.38	248.66	0.00	78.54	7.17	107.39
74	1785.71	2	SLE B	-81810.40	3.19	4.77	0.00	78.54	6.65	99.79
75	1845,24	2	SLE B	-77269.50	-112.99	-168.87	0.00	78.54	6.39	95.63
7.6	1904.76	2	SLE R	-72732.80	-188.33	-281.48	0.00	78,54	6,09	91.03
77	1964.29	2	SLE R	-68199.90	-228.96	-342.19	0.00	78,54	5.76	86.04
78	2023.81	2	SLE R	-63670.80	-240.91	-360.05	0.00	78.54	5.40	80.60
79	2083.33	2	SLE R	-59145.00	-230.13	-343.95	0.00	78.54	5.02	75.0
80	2142.86	2	SLE R	-54622.40	-202.49	-302.63	0.00	78,54	4.63	69.13
81	2202.38	2	SLE R	-50102.80	-163.73	-244.70	0.00	78.54	4.22	63.13
82	2261.90	2	SLE R	-45585.80	-119.53	-178.65	0.00	78.54	3,82	57.09
83	2321.43	2	SLE R	-41071.30	-75.52	-112.86	0.00	78.54	3.41	51.03
84	2380.95	2	SIE R	-36559.00	-37,24	-55.65	0.00	78.54	3.01	45.04
85	2440.48	2	SLE R	-32048.60	-10.23	-15,29	0.00	78.54	2.61	39,20
86	2500.00	2	SLE R	-27540.00	0.00	0.00	0.00	78.54	2.24	33.58
87	0.00	4	SLE O	-203244.00	18422,10	27532.80	0.00	78.54	33.66	480.95
88	59.52	4	SLE O	-203039.00	19717.30	29468.70	3.14	75.40	34.87	497.40
89	119.05	4	-	-200953.00	20562.00	30731.00	9.42	69.11	35.54	506.34
90	178.57	4	SLE Q	-198874.00	21019.90	31415.40	12.57	65.97	35.85	510.30

	g					w s			ne di calc	
91	238.09	4	SLE (-196800.00	21150.20	31610.20	12.57	65.97	35.84	509.85
92	297.62	4	SLE Ç	-194733.00	21007.30	31396.70	12.57	65.97	35.55	505.61
93	357.14	4	SLE C	-192672.00	20619.40	30816.90	12.57	65.97	35.00	497.93
94	416.67	4	SIE (-187958.00	19950.80	29817.60	12.57	65.97	33.97	483.46
95	476.19	4	SLE C	-183254.00	19042.90	28460.80	12.57	65.97	32.71	465.72
96	535.71	4	SLE C	-178560.00	17955.90	26836.20	6.28	72.26	31.27	445.67
97	595,24	4	SLE C	-173875.00	16742.00	25022,00	0.00	78.54	29.72	424,13
98	654.76	4	SLE C	-169200.00	15446.60	23085.80	0.00	78,54	28.12	401.80
99	714.29	4	SLE C	-164534.00	14108.10	21085.40	0.00	78.54	26.50	379.14
100	773.81	4	SLE C	-159876.00	12759.00	19069.00	0.00	78.54	24.86	356.39
101	833.33	4	SLE C	-155228.00	11426.10	17076.90	0.00	78.54	23.24	333.85
102	892.86	4	SLE C	-150587.00	10131.10	15141.50	0.00	78.54	21.66	311.81
103	952.38	4	SLE C	-145955.00	8891.17	13288.40	0.00	78.54	20.13	290.47
104	1011.90	4	SLE (-141330.00	7719.48	11537.20	0.00	78.54	18.67	270.00
105	1071.43	4	SLE C	-136713.00	6625.62	9902.37	0.00	78.54	17.27	250.53
106	1130.95	4	SLE Q	-132103.00	5616.10	8393.59	0.00	78,54	15.96	232.14
107	1190,48	4	SLE C	-127501.00	4694.81	7016.67	0.00	78.54	14.73	214.87
108	1250.00	4	SLE C	-122905.00	3863.41	5774.09	0.00	78.54	13.58	198.74
109	1309.52	4	SLE C	-118316.00	3121.68	4665.53	0.00	78.54	12.52	183.76
110	1369.05	4	SLE C	-113733.00	2467.85	3688.35	0.00	78.54	11,54	169.90
111	1428.57	4	SLE Ç	-109156.00	1898.95	2838.09	0.00	78.54	10.64	157.12
112	1488.10	4	SLE C	-104585.00	1410.98	2108.79	0.00	78.54	9.81	145.37
113	1547.62	4	SLE (-100020.00	999.22	1493.39	0.00	78,54	9.06	134.59
114	1607.14	4	SLE C	-95460.30	658.36	983.96	0.00	78.54	8.37	124,72
115	1666.67	4	SLE C	-90905.50	382,74	572.02	0.00	78.54	7.75	115.68
116	1726.19	4	SLE C	-86355.60	166.38	248.66	0.00	78.54	7.17	107.39
117	1785.71	4	SLE C	-81810.40	3.19	4.77	0.00	78.54	6.65	99.79
118	1845.24	4	SLE C	-77269.50	-112.99	-168.87	0.00	78.54	6.39	95.63
119	1904.76	4	SLE C	-72732.80	-188.33	-281.48	0.00	78.54	6.09	91.05
120	1964.29	4	SLE C	-68199.90	-228.96	-342.19	0.00	78.54	5.76	86.04
121	2023.81	4	SLE C	-63670.80	-240.91	-360.05	0.00	78.54	5.40	80.66
122	2083.33	4	SLE C	-59145.00	-230.13	-343.95	0.00	78,54	5.02	75.01
123	2142.86	4	SLE C	-54622.40	-202.49	-302.63	0.00	78.54	4,63	69.15
124	2202.38	4	SLE C	-50102.80	-163.73	-244.70	0.00	78.54	4.22	63.15
125	2261.90	4	SIE C	-45585.80	-119.53	-178.65	0.00	78.54	3.82	57.09
126	2321.43	4	-	-41071.30	-75.52	-112.86	0.00	78.54	3.41	51,03
127	_	_	SLE C				0.00	-	3.01	45.04
128	2440.48	4	_				0.00	78.54	2.61	39,20

Veri	fiche	princi	nali
AFTT	TT-010E	DAY THEFT	MELLA

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
5	SLU N cost - min. sic.
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
4.9	C.Rare - Sf max (max traz.)
56	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
.92	C.Q.Per Sf max (max traz.)
99	C.Q.Per Sc max (min. compr.)

0.00

Palo n. 4

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20,59	174.02	13.73	8450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti.

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 4 (-152)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
:1	1	SIA	RVN	315710.00	6042.70	-210.70	21456.20	-10595.20
	1	SIA	TAG				0.00	0.00
	1	SIAJ	ECC				0.00	0.00
	1	SLU	TOT	315710.00	6042.70	-210.70	21456.20	-10595,20
- 2	2	SLE R	RVN	233859.00	4476.07	-156.07	15893.50	-7848.29
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	233859.00	4476.07	-156.07	15893.50	-7848,29

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3	SIE	F	RVN	233859.00	4476.07	-156.07	15893.50	-7848.29
3	SLE	F	TAG		J		0.00	0.00
3	SLE	F	ECC				0.00	0.00
3	SLE	F	TOT	233859.00	4476.07	-156.07	15893.50	-7848.29
4	SIE	Q	BVN	233859.00	4476.07	-156.07	15893.50	-7848.29
4	SLE	Q	TAG				0.00	0.00
4	SLE	Q	ECC		ÿ		0.00	0.00
4	SLE	Q	TOT	233859.00	4476.07	-156.07	15893.50	-7848,29
	3 4 4	3 SLE 3 SLE 3 SLE 4 SLE 4 SLE	3 SLE F 3 SLE F 3 SLE F 4 SLE Q 4 SLE Q 4 SLE Q	3 SLE F TAG 3 SLE F ECC 3 SLE F TOT 4 SLE Q RVN 4 SLE Q TAG 4 SLE Q ECC	3 SLE F TAG 3 SLE F ECC 3 SLE F TOT 233859.00 4 SLE Q RVN 233859.00 4 SLE Q TAG 4 SLE Q ECC	3 SLE F TAG 3 SLE F ECC 3 SLE F TOT 233859.00 4476.07 4 SLE Q RVN 233859.00 4476.07 4 SLE Q TAG 4 SLE Q ECC	3 SLE F TAG 3 SLE F ECC 3 SLE F TOT 233859.00 4476.07 -156.07 4 SLE Q RVN 233859.00 4476.07 -156.07 4 SLE Q TAG 4 SLE Q ECC	3 SLE F TAG 0.00 3 SLE F ECC 0.00 3 SLE F TOT 233859.00 4476.07 -156.07 15893.50 4 SLE Q EVN 233859.00 4476.07 -156.07 15893.50 4 SLE Q TAG 0.00 4 SLE Q ECC 0.00

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	. 1	-315710.00	-6042.70	210.70	-21456.20	10595.20
- 2	2	SLE R	1	-233859.00	-4476.07	156.07	-15893.50	7848.29
- 3	3	SLE F	- 1	-233859,00	-4476.07	156.07	-15893.50	7848,29
.4	4	SIE Q	1	-233859.00	-4476.07	156.07	-15893.50	7848.29

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ		N <dan></dan>	My <danm></danm>	Mz <danm></danm>	ssoflessione Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SLU	-315710.00	21322.90	10529.40	-2571250.00	233681.00	115344,00	2-3	153.75	8,144
2	59.52	1	SLU	-314723.00	24152.60	11926.70	-2571250.00	233428.00	115223.00	2-3	153.75	8.170
- 3	119.05	1	SLU	-311077.00	26253.70	12964.20	-2571250.00	232491.00	114774.00	2-3	153.75	8,266
-4	178.57	1	SLU	-307441.00	27721.40	13689.00	-307441.00	231550.00	114323.00	2+3	153.75	8.352
5	238.09	1	SLU	-303815.00	28644.90	14145.00	-303815.00	230610.00	113873.00	2-3	153.75	B.051
- 6	297.62	1	SLU	-300198.00	29106.60	14373.00	-300198.00	229671.00	113424.00	2-3	153.75	7.891
7	357,14	1	SLU	-296590.00	29145.10	14392.00	-296590,00	228728,00	112973,00	2-3	153.75	7,848
- 8	416,67	1	SLU	-289235.00	28687.10	14165.90	-289235.00	226790.00	112038.00	2-3	153.75	7.906
.9	476,19	1	SILI	-281896.00	27793.90	13724.80	-281896.00	224841.00	110925.00	2+3	153.75	8.088
10	535.71	1	SLU	-274571.00	26560.70	13115.80	-274571.00	222884.00	109805.00	2-3	153.75	8.388
11	595.24	1	SLU	-267261.00	25071.90	12380.60	-267261.00	220920.00	108680.00	2-3	153.75	8.805
12	654.76	1	SEU	-259966.00	23401.10	11555.60	-259966.00	218860.00	107627.00	2-3	153.75	9.345
13	714.29	1	SLU	-252684.00	21611.90	10672.10	-252684.00	216707.00	106640.00	2-3	153.75	10.020
14	773.81	1	SLU	-245417.00	19758.90	9757.05	-2571250.00	214543.00	105647.00	2-3	153.75	10.477
15	833.33	1	SIJJ	-238162.00	17887.70	8833.06	-2571250.00	212371.00	104615.00	2-3	153.75	10.796
16	892.86	1	SLU	-230920.00	16036.40	7918.84	-2571250.00	210188.00	103569.00	2-3	153.75	11.139
1.7	952.38	1	SIU	-223690.00	14235.50	7029.59	-2571250.00	207992.00	102516.00	2-3	153.75	11.495
18	1011.90	1	SIAI	-216473.00	12509,70	6177.36	-2571250.00	205786.00	101458.00	2-3	153.75	11.878
19	1071.43	1	SIU	-209267.00	10877.60	5371,40	-2571250,00	203570.00	100396.00	2-3	153.75	12.287
20	1130.95	1	SLU	-202072.00	9352.90	4618.51	-2571250,00	201340,00	99327,30	2-3	153.75	12,724
21	1190.48	1	SLU	-194888.00	7945.10	3923.33	-2571250.00	199100.00	98254.00	2~3	153.75	13.194
22	1250.00	1	SILI	-187714.00	6659.88	3288.68	-2571250.00	196851.00	97176,60	2-3	153.75	13.698
23	1309.52	1	SIU	-180551.00	5499.77	2715.81	-2571250.00	194591.00	96094.60	2-3	153.75	14.241
24	1369.05	1	SIU	-173397.00	4464.65	2204.67	-2571250.00	192319.00	95007.10	2-3	153.75	14.829
25	1428.57	1	SLU	-166253.00	3552.24	1754.11	-2571250.00	190038.00	93915.80	2-3	153.75	15.466
26	1488.10	1	SLU	-159117.00	2758.43	1362,13	-2571250.00	187749.00	92820.70	2-3	153.75	16,159
2.7	1547.62	1	SLU	-151990.00	2077.75	1026.00	-2571250.00	185449.00	91720.80	2-3	153.75	16,917
28	1607,14	1	SLU	-144872.00	1503.59	742.48	-2571250.00	183139.00	90617.00	2-3	153.75	17.748
29	1666.67	1	SIJ	-137761.00	1028.55	507.90	-2571250.00	180821.00	89509.90	2-3	153.75	18.665
30	1726.19	1	SLU	-130657.00	644.62	318.31	-2571250.00	178494.00	88398.90	2+3	153.75	19.679
31	1785,71	1	SLU	-123560.00	343.36	169.55	-2571250,00	176158.00	87284.30	2-3	153.75	20,810
32	1845.24	1	SIU	-116470.00	116.11	57.34	-2571250,00	173824.00	86113.40	2-3	153.75	22.076
33	1904.76	1	SLU	-109387.00	-45.94	-22,68	-2571250.00	-171388.00	-84545,20	2-3	333.75	23.506
34	1964.29	1	SLU	-102309.00	-151.65	-74.89	-2571250.00	-168918.00	-83411.00	2-3	333.75	25.132
35	2023.81	1	SIU	-95236.20	-209.85	-103.62	-2571250,00	-166438.00	-82242.40	2-3	333.75	26.999
36	2083.33	1	SIU	-88168.90	-229.32	-113.24	-2571250.00	-163949.00	-81053.30	2-3	333.75	29,163
37	2142.86	1	SLU	-81106.30	-218.73	-108.01	-2571250.00	-161451.00	-79860.50	2-3	333.75	31.702
38	2202.38	1	SLU	-74048.10	-186.69	-92,19	-2571250.00	-158943.00	-78663.80	2-3	333.75	34.724
39	2261.90	1	SLU	-66993.80	-141.70	-69.97	-2571250.00	-156423.00	-77463.00	2-3	333.75	38.380
40	2321,43	1	SLU	-59943,20	-92.18	-45.52	-2571250.00	-153894.00	-76259.10	2-3	333.75	42.895
41	2380.95	1	SLU	-52895.70	-46,51	-22.97	-2571250.00	-151358.00	-75052.10	2-3	333.75	48.610
42	2440,48	1	SLU	-45851,10	-13,01	-6.42	-2571250,00	-148810.00	-73841,80	2-3	333.75	56.078
43	2500.00	1	SLU	-38808.90	0.00	0.00	-2571250.00					66,254

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIA	6042.70	-210.70	0.85	11.31	6046.37	1.00	32294.70	376890.00	32294.70	5.341
2	59.52	1	SIU	4585.88	-159.90	0.85	11.31	4588,67	1.00	32294.70	376749.00	32294.70	7.038
3	119.05	1	SIU	3312.66	-115.51	0.85	11.31	3314.68	1.00	32294.70	376227,00	32294.70	9.743
4	178.57	1	SLU	2212.01	-77.13	0.85	11.31	2213.36	1.00	32294.70	375706.00	32294.70	14.591
- 5	238.09	1	SLU	1272.13	-44.36	0.85	11,31	1272.90	1.00	32294.70	375186.00	32294.70	25,371
.6	297.62	1	SLU	480.70	-16.76	0.85	11.31	481.00	1.00	32294.70	374668.00	32294.70	67.141
7	357.14	1	SLU	-385,13	13.43	0.85	11.31	385.37	1.00	32294.70	374152.00	32294.70	83.802

								L	Hazi	one ui	Calcolo		
- 8	416.67	1	SLU	-1296.56	45.21	0.85	11.31	1297.35	1.00	32294.70	373098,00	32294.70	24.893
. 9	476.19	1	SLU	-2018.86	70.40	0.85	11.31	2020.09	1.00	32294.70	372047.00	32294.70	15.987
1.0	535.71	1	SIU	-2573.14	89.72	0.85	11.31	2574.70	1.00	32294.70	370998.00	32294.70	12.543
11	595.24	1	SLU	-2979.70	103.90	0.85	11.31	2981.52	1.00	32294.70	369950.00	32294.70	10.832
12	654.76	1	SLU	-3257.83	113.60	0.85	11.31	3259.81	1.00	32294.70	368905.00	32294.70	9.907
13	714.29	1	SLU	-3425.62	119.45	0.85	11.31	3427.70	1.00	32294.70	367862.00	32294.70	9.422
14	773.81	1	SLU	-3499.85	122.04	0.85	11.31	3501.98	1.00	32294.70	366821.00	32294.70	9.222
15	833.33	ĭ	SLU	-3495,96	121.90	0.85	11.31	3498.09	1.00	32294.70	365782.00	32294.70	9.232
1.6	892.86	14	SLU	-3427.99	119.53	0.85	11.31	3430.07	1.00	32294.70	364745.00	32294.70	9.415
17	952.38	- 1	SIJ	-3308.57	115.37	0.85	11.31	3310.58	1.00	32294.70	363709.00	32294.70	9.755
18	1011.90	1	SLU	-3148.98	109.80	0.85	11.31	3150.90	1,00	32294.70	362676.00	32294.70	10.249
19	1071.43	1	SLU	-2959.19	103.18	0.85	11.31	2960.99	1,00	32294.70	361643.00	32294.70	10.907
20	1130.95	1	SIAJ	-2747.90	95.82	0.85	11.31	2749.57	1.00	32294.70	360613.00	32294.70	11,745
21	1190.48	-1	SLU	-2522.64	87,96	0.85	11.31	2524.17	1.00	32294.70	359584,00	32294.70	12,794
22	1250.00	1	SIU	-2289.83	79.84	0.85	11.31	2291.22	1.00	32294.70	358556.00	32294.70	14.095
23	1309.52	1	SLU	-2054.91	71.65	0.85	11.31	2056.16	1.00	32294.70	357530.00	32294.70	15.706
24	1369.05	1	SIU	-1822.39	63.54	0.85	11.31	1823.49	1.00	32294.70	356505.00	32294.70	17.710
25	1428.57	1	SLU	-1595.96	55.65	0.85	11.31	1596.93	1.00	32294.70	355482.00	32294.70	20.223
26	1488,10	1	SLU	-1378.61	48.07	0.85	11.31	1379.45	1.00	32294.70	354460,00	32294.70	23,411
27	1547,62	1	SIU	-1172.66	40.89	0.85	11.31	1173.37	1.00	32294.70	353439,00	32294.70	27.523
28	1507.14	1	SLU	-979.90	34.17	0.85	11.31	980.50	1.00	32294.70	352419.00	32294.70	32.937
29	1666.67	1	SIU	-801.65	27.95	0.85	11.31	802.14	1.00	32294.70	351401.00	32294.70	40.261
30	1726.19	1	SIU	-638.85	22.28	0.85	11.31	639.23	1.00	32294.70	350383.00	32294.70	50.521
31	1785.71	1	SLU	-492.08	17.16	0.85	11.31	492.38	1.00	32294.70	349367.00	32294.70	65.588
32	1845.24	1	SLU	-361.73	12.61	0.85	11,31	361.95	1.00	32294.70	348351.00	32294.70	89.225
33	1904.76	1	SIU	-247.93	8.65	0.85	11.31	248.08	1.00	32294.70	347337.00	32294.70	>100
34	1964.29	1	SLU	-150.72	5.26	0.85	11.31	150.81	1.00	32294.70	346323.00	32294.70	>100
35	2023.81	1	SLU	-69.99	2.44	0.85	11.31	70.03	1.00	32294.70	345310.00	32294.70	>100
36	2083.33	1	SIJJ	-5.62	0.20	0.85	11.31	5.62	1.00	32294.70	344297.00	32294.70	>100
37	2142,86	1	SIJ	42,58	-1.48	0.85	11.31	42.60	1.00	32294.70	343286,00	32294.70	>100
38	2202.38	1	SLU	74,77	-2.61	0.85	11.31	74.81	1,00	32294.70	342275.00	32294.70	>100
39	2261,90	1	SLU	91.11	-3.18	0.85	11.31	91.16	1,00	32294.70	341264.00	32294.70	>100
40	2321.43	1	SLU	91.73	-3.20	0.85	11,31	91.78	1.00	32294.70	340254.00	32294.70	>100
41	2380.95	1	SLU	76.72	-2.68	0.85	11.31	76.77	1,00	32294.70	339245.00	32294.70	>100
42	2440.48	1	SLU	46.14	-1.61	0.85	11.31	46.16	1.00	32294.70	338236.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <amq></amq>	σ _□ <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-233859.00	7799.54	15794.80	0.00	78.54	28.03	408,43
45	59,52	2	SLE R	-233441.00	8834.56	17890.80	0.00	78.54	29.19	424.28
46	119.05	2	SLE R	-230931.00	9603.11	19447.20	0.00	78.54	29.88	433.37
47	178.57	2	SLE R	-228428.00	10140.00	20534.40	0.00	78.54	30.30	438.80
48	238.09	2	SLE R	-225932.00	10477.80	21218.40	0.00	78.54	30.49	441.10
49	297,62	2	SLE R	-223443.00	10646.70	21560.40	0.00	78,54	30.48	440.73
50	357.14	2	SLE R	-220961.00	10660.70	21588.90	0.00	78.54	30.29	437.93
51	416.67	2	SLE R	-215527.00	10493.20	21249.70	0.00	78.54	29.66	428.66
52	476.19	2	SLE R	-210106.00	10166.50	20588.10	0.00	78.54	28.84	416.88
53	535.71	2	SLE R	-204696.00	9715.44	19674.60	0.00	78.54	27.88	403.15
54	595.24	2	SLE R	-199297.00	9170.84	18571.80	0.00	78.54	26.81	387.96
55	654.76	2	SLE R	-193908.00	8559.68	17334.10	0.00	78.54	25.66	371.73
56	714.29	2	SLE R	-188530.00	7905.25	16008.80	0.00	78.54	24.47	354.83
57	773.81	2	SLE R	-183162.00	7227.44	14636.20	0.00	78.54	23.25	337.5
58	833.33	2	SLE R	-177804.00	6543.01	13250.20	0.00	78.54	22.02	320.22
59	892.86	2	SLE R	-172455.00	5865.81	11878.80	0.00	78.54	20.80	302.99
50	952.38	2	SLE R	-167116.00	5207.10	10544.80	0.00	78.54	19.61	286.0
61	1011.90	2	SLE R	-161785.00	4575.82	9266.45	0.00	78.54	18.44	269.59
62	1071.43	2	SLE R	-156463.00	3978.82	8057.46	0.00	78.54	17.32	253.66
63	1130.95	2	SLE R	-151150.00	3421.12	6928.07	0.00	78.54	16.24	238.37
64	1190.48	2	SLE R	-145845.00	2906.17	5885.26	0.00	78.54	15.22	223.76
65	1250.00	2	SLE R	-140547.00	2436.06	4933.24	0.00	78.54	14.24	209.8
66	1309.52	2	SLE B	-135257.00	2011.71	4073.90	0.00	78.54	13,32	196.73
67	1369.05	2	SLE R	-129975.00	1633.09	3307.15	0.00	78.54	12.45	184.29
68	1428.57	2	SLE R	-124699,00	1299.34	2631.29	0.00	78.54	11.64	172.58
69	1488.10	2	SLE R	-119430.00	1008.98	2043.28	0.00	78.54	10.87	161.56
70	1547.62	2	SLE R	-114167.00	760.00	1539.07	0.00	78.54	10.16	151.23
71	1607.14	2	SLE R	-108911.00	549.99	1113.77	0.00	78.54	9.49	141.48
72	1666.67	2	SLE R	-103660.00	376.23	761.89	0.00	78.54	8.86	132.33
73	1726,19	2	SLE R	-98415.20	235.79	477.49	0.00	78.54	8,27	123.72
74	1785.71	2	SLE R	-93175.40	125.59	254.34	0.00	78.54	7.72	115.59
75	1845.24	2	SLE R	-87940.60	42.47	86.01	0.00	78.54	7.20	107.89
76	1904.76	2	SLE R	-82710.50	-16.BO	-34,03	0.00	78.54	6,74	101.13
77	1964.29	2	SLE R	-77484.90	-55.47	-112.33	0.00	78.54	6.36	95.35
78	2023.81	2	SLE R	-72263.40	-76.76	-155.44	0.00	78.54	5.96	89.33
79	2083.33	2	SLE R	-67045.80	-83.88	-169.86	0.00	78,54	5.55	83.08
80	2142.86	2	SLE R	-61831.80	-80.01	-162.02	0.00	78.54	5.12	76.66
81	2202.38	2	SLE R	-56621.10	-68.29	-138.29	0.00	78,54	4.68	70.12

		. 2		1	F					ne di calc	
_	2261.90	_	SLE	-				-	78.54	4.24	63.51
83		2	-	R	-46208.50	-33.72	-68.28	0.00	78.54	3.79	56.88
84		2	-	R	-41006.10	-17.01	-34.45	0.00	78.54	3.35	50.27
85	2440.48	2	-	R	-35805.90	-4.76	-9.64	0.00	78.54	2.92	43.73
86	2500,00	2	-	R	-30607.60	0.00	0.00	0.00	78.54	2.49	37.32
87	0.00	_	-	Q	-233859.00	7799.54	15794.80	0.00	78.54	28.03	408.43
88	59,52	_		Q	-233441.00	8834.56	17890.80	0.00	78.54	29.19	424.28
89	119.05	_	-	Q	-230931.00	9603.11	19447.20	0.00	78,54	29.88	433.37
90	178.57	4	SLE	Q	-228428.00	10140.00	20534.40	0.00	78.54	30.30	438.80
91	238.09	4	SLE	Q	-225932.00	10477.BO	21218.40	0.00	78,54	30.49	441.10
-92	297.62	4	SLE	Q	-223443.00	10646.70	21560.40	0.00	78.54	30.48	440.73
93	357.14	4	SLE	Q	-220961.00	10660.70	21588.90	0.00	78,54	30.29	437.93
94	416.67	4	SLE	Q	-215527.00	10493.20	21249.70	0.00	78.54	29.66	428.6
95	476.19	4	SLE	Q	-210106.00	10166.50	20588.10	0.00	78.54	28.84	416.88
96	535.71	- 6	SLE	Q	-204696.00	9715.44	19674.60	0.00	78.54	27.88	403.13
97	595.24	4	SLE	Ò	-199297.00	9170.84	18571.80	0.00	78.54	26.81	387.90
98	654.76	4	SLE	Ò	-193908.00	8559.68	17334.10	0.00	78.54	25.66	371,7
99	714.29	4	SLE	Q	-188530.00	7905.25	16008.80	0.00	78.54	24.47	354.8
100	773.81	4	SLE	Q	-183162.00	7227.44	14636.20	0.00	78.54	23.25	337.5
101	833.33	4	SLE	Q	-177804.00	6543.01	13250.20	0.00	78.54	22.02	320.2
102	892.86	4	SLE	Q	-172455.00	5865.B1	11878.80	0.00	78.54	20.80	302.9
103	952.38	4	SLE	Q	-167116.00	5207.10	10544.80	0.00	78.54	19.61	286.0
104	1011.90	4	SLE	Q	-161785.00	4575.82	9266.45	0.00	78,54	18.44	269.5
105	1071.43	4	SLE	Q	-156463.00	3978.82	8057.46	0.00	78.54	17.32	253.6
106	1130.95	4	SLE	Q	-151150.00	3421.12	6928.07	0.00	78.54	16.24	238.3
107	1190.48	4	SLE	Q	-145845.00	2906.17	5885.26	0.00	78.54	15.22	223.7
108	1250.00	- 4	SLE	Q	-140547.00	2436.06	4933.24	0.00	78.54	14.24	209.8
109	1309.52	4	SLE	Q	-135257.00	2011.71	4073.90	0.00	78.54	13.32	196.7
110	1369.05	4	SLE	Q	-129975.00	1633.09	3307.15	0.00	78.54	12,45	184.2
111	1428.57	4	SLE	Q	-124699.00	1299.34	2631.29	0.00	78.54	11.64	172.5
112	1488.10	4	SLE	Q	-119430.00	1008.98	2043.28	0.00	78.54	10.87	161.5
113	1547.62	4	SLE	Q	-114167.00	760.00	1539.07	0.00	78.54	10.16	151.2
114	1607.14	4	SLE	o	-108911.00	549.99	1113.77	0.00	78.54	9,49	141.4
115	1666.67	4	SLE	a	-103660.00	376.23	761.89	0.00	78.54	8.86	132.3
116	1726.19	4	SIE	Q	-98415.20	235.79	477.49	0.00	78.54	8.27	123.7
117	1785.71	4	SLE	Ó	-93175,40	125.59	254.34	0.00	78.54	7.72	115.5
118	1845.24	4	SLE	Q	-87940.60	42.47	86.01	0.00	78.54	7.20	107.8
119	1904.76	4	SLE	Ö	-82710.50	-16.80	-34.03	0.00	78.54	6.74	101.1
120	1964,29	4	SLE	ò	-77484.90	-55.47	-112.33	0.00	78.54	6,36	95.3
121	2023.81	4	-	Q	-72263.40	-76.76	-155.44	0.00	78.54	5.96	89.3
122	2083.33	_		a	-67045.80	-83.88	-169.86	0.00	78.54	5.55	83.0
123		_	SLE	0	-61831.80	-80.01	-162.02	0.00	78.54	5.12	76.6
124		_	_	0	-56621.10	-68.29	-138.29	0.00	78.54	4.68	70.1
125		-	-	0	-51413.40	-51.83	-104.96	0.00	78.54	4.24	63.5
126		_	_	O.	-46208.50	-33.72	-68.28	0.00	78.54	3,79	56.8
127	2380.95	4		O.	-41006.10	-17.01	-34.45	0.00	78.54	3.35	50.2
128		4	_	Q.	-35805.90	-4.76	-9.64	0.00	78.54	2.92	43.7
m 50,50	# 4 4 A A A B B	- 9	47.0000	yé.		79.0-11.52	0.00	26.4.20.20	5 K 5 W 7	Ter # 10 Tex	TRACE 8 (1)

Verifiche principali

Caso	Tipo										
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio										
.7	SLU N cost - min. sic.										
.48	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)										
86	C.Rare - Sc max (min. compr.), C.Rare - Sf max (max traz.)										
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)										
129	C.Q.Per Sc max (min. compr.), C.Q.Per Sf max (max traz.)										

129 2500.00 4 SLE Q -30607.60 0.00 0.00 0.00 78.54

Palo n. 5

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf C1.00 6.00 C30/		Fck <dan cmq=""></dan>	Fctk <dan cmg=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

37.32

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 5 (-153)

Caso	oc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	315619.00	6038.81	208.03	21458.00	10734.80

43

0.00	0.00				TAG	SLU	1	
0.00	0.00				ECC	SLU	1	
10734.80	21458.00	208.03	6038.81	315619.00	TOT	SLU	1	
7951.73	15894.80	154.10	4473.19	233792.00	RVN	SLE R	2	- 2
0.00	0.00		î î		TAG	SLE R	2	
0.00	0.00		8 8		ECC	SLE R	2	
7951.73	15894.80	154.10	4473.19	233792.00	TOT	SLE R	2	
7951.73	15894.80	154.10	4473.19	233792.00	RVN	SLE F	3	- 3
0.00	0.00			_	TAG	SLE F	3	-
0.00	0.00				ECC	SLE F	3	
7951.73	15894.80	154,10	4473.19	233792.00	TOT	SLE F	3	
7951.73	15894.80	154.10	4473.19	233792.00	RVN	SLE Q	4	4
0.00	0.00	- 3			TAG	SIR Q	4	
0.00	0.00				ECC	SIE Q	4	
7951.73	15894.80	154.10	4473.19	233792.00	TOT	SLE Q	4	

Sollecitazioni nei pali

Caso	cc	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SIU	1	-315619,00	-6038.81	-208.03	-21458.00	-10734,80
- 2	2	SLE R	1	-233792.00	-4473.19	-154.10	-15894.80	-7951.73
- 3	3	SLE F	1	-233792.00	-4473.19	-154.10	-15894.80	-7951.73
4	4	SLE Q	. 1	-233792.00	-4473.19	-154.10	-15894.80	-7951.73

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-315619.00	21325.00	-10668.30	-2571250.00	233644.00	-115097.00	2-3	206.25	8.14
2	59.52	1	SLU	-314633.00	24144.90	-12079.10	-2571250.00	233380.00	-114970.00	2-3	206.25	8,172
-3	119.05	1	SLU	-310989.00	26237.90	-13126.10	-2571250.00	232402.00	-114499.00	2-3	206.25	8.268
4	178.57	1	SIJ	-307354.00	27698.80	-13857,00	-307354.00	231417.00	-114027.00	2-3	206.25	8.33(
.5	238.09	1	SIJJ	-303729.00	28616.60	-14316.10	~303729.00	230434.00	-113555.00	2-3	206,25	8.02
- 6	297.62	1	SLU	-300113.00	29073.70	-14544.80	-300113.00	229452.00	-113084.00	2-3	206.25	7.869
.7	357.14	1	SLU	-296507.00	29108.50	-14562.20	-296507.00	228464.00	-112611.00	2-3	206.25	7.82
. 8	416.67	1	SIAI	-289154.00	28648.20	-14331.90	-289154.00	226446.00	-111643.00	2-3	206.25	7.88
9	476.19	1	SIAJ	-281816.00	27753.70	-13884.40	-281816.00	224414.00	-110670.00	2-3	206.25	8.06
10	535.71	1	SLU	-274494.00	26520,30	-13267,40	-274494.00	222371.00	-109693.00	2-3	206.25	8.36
11	595.24	1	SIN	-267186.00	25031.90	-12522.80	-267186.00	220320.00	-108712.00	2-3	206.25	8.778
12	654.76	1	SILI	-259893.00	23362.20	-11687.50	-259893.00	218260.00	-107727.00	2-3	206.25	9.31
13	714.29	1	SIJJ	-252613.00	21574.70	-10793.20	-252613.00	216187.00	-106736.00	2-3	206.25	9.99
14	773.81	1	SIU	-245348.00	19723.60	-9867.18	-2571250.00	214106.00	-105741.00	2-3	206.25	10.480
15	833,33	1	SLU	-238095.00	17854.70	-8932.23	-2571250.00	212018.00	-104743.00	2-3	206.25	10.79
16	892,86	1	SLU	-230855.00	16005.80	-8007,26	-2571250.00	209919.00	-103740.00	2-3	206,25	11.13
17	952.38	1	SLU	-223628.00	14207.50	-7107.64	-2571250.00	207810.00	-102733.00	2-3	206.25	11.49
18	1011.90	1	SLU	-216412.00	12484.30	-6245.54	-2571250.00	205695.00	-101722.00	2-3	206.25	11.88
19	1071.43	1	SIJJ	-209208.00	10854.70	-5430.32	-2571250.00	203571.00	-100708.00	2-3	206.25	12.29
2.0	1130.95	1	SLU	-202016.00	9332.54	~4668.82	-2571250.00	201438.00	-99689.00	2-3	206.25	12.72
21	1190.48	1	SLU	-194834.00	7927.15	-3965.74	-2571250.00	199325.00	-98468,40	2-3	206.25	13.19
22	1250.00	1	SIU	-187662.00	6644.21	-3323.92	-2571250.00	197210.00	-97200.60	2-3	206.25	13.70
23	1309.52	1	SLU	-180501.00	5486.24	-2744.62	-2571250.00	195086.00	-95919.10	2-3	206.25	14.24
24	1369.05	1	SLU	-173349.00	4453.10	-2227.76	-2571250.00	192881.00	-94701.00	2-3	206.25	14.83
25	1428.57	1	SIU	-166207.00	3542.49	-1772.21	-2571250.00	190559.00	-93580.40	2-3	206.25	15.47
26	1488.10	1	SIJJ	-159074.00	2750.31	-1375.91	-2571250.00	188225.00	-92454.10	2-3	206.25	16.16
27	1547.62	1	SLU	-151949.00	2071.08	-1036.11	-2571250.00	185875.00	-91320.60	2-3	206.25	16.92
28	1607,14	1	SLU	-144832.00	1498.21	-749.51	-2571250.00	183512.00	-90181.20	2-3	206.25	17.75
29	1666.67	1	SIU	-137723.00	1024.29	-512.42	-2571250.00	181137.00	-89037.60	2-3	206.25	18.67
30	1726.19	1	SLU	-130621.00	641.31	-320.83	-2571250.00	178717.00	-87919.80	2-3	206.25	19.68
31	1785.71	2	SLU	-123527.00	340.86	-170.53	-2571250.00	176283.00	-86797.30	2-3	206.25	20.81
32	1845.24	1	SIJ	-116439.00	114.28	-57.17	-2571250.00	173835.00	-85670.70	2-3	206.25	22.08
. 33	1904.76	1	SIU	-109357.00	-47.22	23.63	-2571250.00	-171508.00	84721.80	2-3	26.25	23.51
34	1964.29	1	SLU	-102281,00	-152.51	76.30	-2571250.00	-169194.00	83320.50	2-3	26.25	25.13
35	2023.81	1	SIAJ	-95210.80	-210.38	105.25	-2571250.00	-166873.00	81909.50	2-3	26.25	27.00
36	2083.33	1	SLU	-88145.50	-229.61	114.87	-2571250.00	-164354.00	80686.90	2-3	26.25	29.17
37	2142.86	1	SEU	-81085.00	-218.87	109.49	-2571250.00	-161816.00	79463.50	2-3	26.25	31.71
38	2202.38	1	SLU	-74028.80	-186.73	93.42	-2571250.00	-159262.00	78233.10	2-3	26.25	34.733
39	2261,90	1	SLU	-66976.60	-141.69	70.88	-2571250.00	-156693.00	76996.90	2-3	26.25	38.390
40	2321.43	1	SLU	-59928.00	-92.15	46,10	-2571250.00	-154111.00	75755.40	2-3	26.25	42.90
41	2380.95	1	SLU	-52882.60	-46.49	23.26	-2571250.00	-151516.00	74508.70	2-3	26.25	48.623
42	2440.48	1	SIA	-45840.00	-13.00	6.51	-2571250.00	-148908.00	73256.70	2-3	26.25	56.093
43	2500.00	1	SLU	-38799.90	0.00	0.00	-2571250.00					66.269

Stato limite ultimo - Verifiche a taglio

	х	44		Ty	Tz	bw	Asw	Vsdu		VRsd	VRcd	Vrdu	
Caso	<cm></cm>	oc	TCC	<dan></dan>	<dan></dan>	<m></m>	<cmq></cmq>	<dan></dan>	ctge	<dan></dan>	<dan></dan>	<dan></dan>	Sic.
- 1	0.00	1	SIJ	6038.81	208.03	0.85	11.31	6042.39	1.00	32294.70	376877.00	32294.70	5.345
2	59.52	1	SLU	4581,12	157.82	0.85	11.31	4583.83	1.00	32294.70	376736.00	32294.70	7.045
3	119,05	1	SLU	3307.21	113.93	0.85	11.31	3309.18	1.00	32294.70	376214.00	32294.70	9.759
4	178.57	1	SLU	2206.05	76.00	0.85	11.31	2207.36	1.00	32294.70	375693.00	32294.70	14,630
5	238.09	1	SLU	1265.81	43.61	0.85	11.31	1266.56	1.00	32294.70	375174.00	32294.70	25.498
- 6	297.62	1	SLU	474.16	16.33	0.85	11.31	474.44	1.00	32294.70	374656.00	32294.70	68.070
- 7	357,14	1	SLU	-391.83	-13.50	0.85	11.31	392.06	1.00	32294.70	374140.00	32294.70	82.372
8	416.67	1	SLU	-1303.30	+44.90	0.85	11.31	1304.07	1.00	32294.70	373086.00	32294.70	24.765
:9	476.19	1	SIAI	-2025.51	-69.78	0.85	11.31	2026.71	1.00	32294.70	372035.00	32294.70	15.934
1.0	535.71	1	SIU	-2579,60	-88.86	0.85	11.31	2581.13	1.00	32294.70	370986.00	32294.70	12,512
11	595.24	1	SLU	-2985.89	-102.86	0.85	11.31	2987.66	1.00	32294.70	369940.00	32294.70	10.809
12	654.76	1	SLU	-3263.68	-112.43	0.85	11.31	3265.62	1.00	32294.70	368895.00	32294.70	9.889
13	714.29	1	SIU	-3431.09	-118.20	0.85	11.31	3433.12	1.00	32294.70	367852.00	32294.70	9.407
14	773.81	1	SIJ	-3504.90	-120.74	0.85	11.31	3506.98	1.00	32294.70	366812,00	32294.70	9.209
15	833.33	1	SLU	-3500.58	-120.59	0.85	11.31	3502.66	1.00	32294.70	365773.00	32294.70	9.220
16	892.86	1	SLU	-3432.17	-118.23	0.85	11.31	3434.20	1.00	32294.70	364736,00	32294.70	9.404
17	952.38	1	SLU	-3312.31	-114.11	0.85	11.31	3314.28	1.00	32294.70	363700.00	32294.70	9.744
18	1011.90	1	SLU	-3152.30	-108.59	0.85	11.31	3154.17	1.00	32294.70	362667.00	32294.70	10.239
19	1071.43	1	SIU	-2962.09	-102.04	0.85	11.31	2963.85	1.00	32294.70	361635.00	32294.70	10.896
20	1130.95	1	SIU	-2750.41	-94.75	0.85	11.31	2752.04	1.00	32294.70	360605.00	32294.70	11.735
21	1190.48	1	SIA	-2524.77	-86.98	0.85	11.31	2526.27	1.00	32294.70	359576.00	32294.70	12.784
22	1250.00	1	SLU	-2291.62	-78.94	0.85	11.31	2292.98	1.00	32294.70	358549.00	32294.70	14.084
23	1309.52	1	SIJ	-2056.38	-70.84	0.85	11.31	2057.60	1.00	32294.70	357523.00	32294.70	15.695
24	1369.05	1	SLU	-1823.57	-62.82	0.85	11.31	1824.65	1.00	32294.70	356499.00	32294.70	17.699
25	1428.57	1	SEU	+1596.88	-55.01	0.85	11.31	1597.83	1.00	32294.70	355475.00	32294.70	20.212
26	1488.10	1	SLU	-1379.29	+47.52	0.85	11.31	1380.11	1.00	32294.70	354454.00	32294.70	23.400
27	1547.62	1	SIU	-1173.14	-40.41	0.85	11.31	1173.83	1.00	32294.70	353433.00	32294.70	27.512
28	1607.14	1	SIU	-980.20	-33.77	0.85	11.31	980.78	1.00	32294.70	352414.00	32294.70	32.928
29	1666.67	1	SLU	-801.79	-27.62	0.85	11.31	802.27	1.00	32294.70	351395.00	32294.70	40.254
30	1726.19	1	SIJ	-638.85	-22.01	0.85	11.31	639.23	1,00	32294.70	350378.00	32294.70	50.521
31	1785,71	1	SIJ	-491.98	-16.95	0.85	11.31	492.27	1.00	32294.70	349362.00	32294.70	65.604
32	1845.24	1	SIU	-361.53	-12,45	0.85	11.31	361.75	1.00	32294.70	348347.00	32294.70	89.274
33	1904.76	1	SLU	-247.67	-8.53	0.85	11.31	247,82	1.00	32294.70	347332,00	32294.70	>100
34	1964.29	1	SIM	-150.41	~5.18	0.85	11.31	150.49	1.00	32294.70	346319.00	32294.70	>100
35	2023.81	1	SILI	-69.65	+2.40	0.85	11.31	69.69	1.00	32294.70	345306.00	32294.70	>100
36	2083.33	1	SIU	-5,27	-0.18	0.85	11.31	5.27	1.00	32294.70	344294,00	32294.70	>100
37	2142.86	1	SLU	42.92	1.48	0.85	11.31	42.95	1.00	32294.70	343283.00	32294.70	>100
38	2202.38	1	SLU	75.09	2.59	0.85	11,31	75.14	1.00	32294.70	342272.00	32294.70	>100
39	2261.90	1	SLU	91,40	3.15	0.85	11.31	91.46	1.00	32294.70	341262.00	32294.70	>100
40	2321.43	1	SLU	91.97	3.17	0.85	11.31	92.03	1.00	32294.70	340252.00	32294.70	>100
41	2380.95	1	SLU	76.90	2.65	0.85	11.31	76.94	1.00	32294.70	339243.00	32294.70	>100
42	2440.48	1	SIU	46.23	1.59	0.85	11.31	46.26	1.00	32294.70	338234.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <mq></mq>	σ _□ <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-233792.00	-7902.44	15796.30	0.00	78,54	28.04	409.35
45	59.52	2	SLE R	-233375.00	-8947.45	17885.10	0.00	78.54	29.20	425.27
4.6	119.05	2	SLE R	-230865.00	-9723.04	19435.50	0.00	78.54	29.89	434.42
47	178.57	2	SLE R	-228363.00	-10264.40	20517.60	0.00	78.54	30.30	439.88
48	238.09	2	SLE R	-225868.00	-10604.50	21197.50	0.00	78.54	30,49	442.19
49	297.62	2	SLE R	-223380.00	-10773.90	21536,10	0.00	78,54	30.48	441,82
50	357.14	2	SLE R	-220899.00	-10786.80	21561,90	0.00	78.54	30.29	439.00
51	416.67	2	SLE R	-215467.00	-10616.20	21220.90	0.00	78.54	29.66	429.69
52	475.19	2	SLE R	-210047.00	-10284.80	20558.30	0.00	78.54	28.84	417.87
53	535.71	2	SLE R	-204639.00	-9827.67	19644.60	0.00	78.54	27.88	404.08
54	595.24	2	SLE R	-199241.00	-9276.12	18542.10	0.00	78,54	26,81	388,83
55	654.76	2	SLE R	-193854.00	-8657.37	17305.30	0.00	78.54	25.66	372.53
56	714.29	2	SLE R	-188477.00	-7994.97	15981,20	0.00	78.54	24.47	355.55
57	773.81	2	SLE R	-183111.00	-7309.02	14610.10	0.00	78.54	23.24	338.22
58	833.33	2	SLE R	-177754.00	-6616.46	13225.70	0.00	78,54	22.02	320.80
59	892.86	2	SLE R	-172407.00	-5931.30	11856.10	0.00	78.54	20.80	303.50
60	952.38	2	SLE R	-167069.00	-5264.92	10524.10	0.00	78,54	19,60	286.51
61	1011.90	2	SLE R	-161740.00	~4626.33	9247.61	0.00	78.54	18.44	269.97
62	1071.43	2	SLE R	-156420.00	-4022.46	8040.53	0.00	78.54	17.32	253.98
63	1130.95	2	SLE R	-151108.00	-3458.38	6913.00	0.00	78.54	16.24	238.63
64	1190.48	2	SLE R	-145804.00	-2937.58	5871.97	0.00	78.54	15.21	223.98
65	1250.00	2	SLE B	-140509.00	-2462.16	4921.64	0.00	78.54	14.24	210.04
66	1309.52	2	SLE R	-135220.00	-2033.05	4063.88	0.00	78.54	13.32	196.84
67	1369.05	2	SLE R	-129939,00	-1650,20	3298.59	0.00	78,54	12.45	184.38
68	1428.57	2	SLE R	-124665.00	-1312.75	2624.06	0.00	78.54	11.63	172.65
69	1488.10	2	SLE R	-119397.00	-1019.19	2037.27	0.00	78.54	10.87	161.60
70	1547.62	2	SLE R	-114136.00	-767.49	1534.14	0.00	78.54	10.16	351.23
71	1607.14	2	SLE R	-108881.00	-555.20	1109.79	0.00	78.54	9.49	141.49
72	1666.67	2	SLE R	-103632.00	-379.57	758.73	0.00	7B.54	8.86	132.32

							Rela	zion	e di calc	olo
73	1726.19	2	SLE R	-98388.80	-237.65	475.05		78.54	8.27	123.70
74	-	_	SLE R	-93150.50	-126.31	252.49		78.54	7.72	115.56
75	1845.24	2	SLE R	-87917.20	-42.35	84.66	0.00	78,54	7.19	107.86
76	1904.76	2	SLE R	-82688.70	17.50	-34.98	0.00	78.54	6.74	101.09
77	1964.29	2	SLE R	-77464.60	56.52	-112.97	0.00	78.54	6.36	95.33
78	2023.81	2	SLE R	-72244.60	77.96	-155.84	0.00	7B.54	5.96	89.30
79	2083.33	2	SLE R	-67028.50	85,09	-170.09	0.00	78.54	5.55	83.06
80	2142.86	2	SLE R	-61816.00	81.11	-162.13	0.00	78.54	5.12	76.64
81	2202.38	2	SLE R	-56606.80	69,20	-138,32	0.00	78.54	4.68	70.10
-82	2261.90	2	SLE R	-51400.70	52.51	-104.95	0.00	78,54	4.24	63.49
83	2321.43	2	SLE R	-46197.30	34.15	-68,26	0.00	78.54	3.79	56.86
84	2380.95	2	SLE R	-40996.40	17.23	-34.43	0.00	78.54	3.35	50.25
85	2440.48	2	SLE R	-35797.70	4.82	-9.63	0.00	78.54	2.92	43.72
86	2500.00	2	SLE R	-30600.90	0.00	0.00	0.00	78.54	2.49	37,31
87	0.00	4	SLE Q	-233792.00	-7902.44	15796.30	0.00	78.54	28.04	409.35
88	59.52	4	SLE Q	-233375.00	-8947.45	17885.10	0.00	78,54	29.20	425.27
89	119.05		SLE Q	-230865.00	-9723.04	19435.50	0.00	78,54	29.89	434,42
90	178,57	4	SLE Q	-228363.00	-10264,40	20517.60	0.00	78.54	30.30	439.88
91	238.09	4	SLE Q	-225868.00	-10604.50	21197.50	0.00	78.54	30.49	442.19
92	297.62	4	SLE Q	-223380.00	-10773.90	21536.10	0.00	78.54	30.48	441.82
93	357,14	4	SLE Q	-220899.00	-10786.80	21561.90	0.00	78.54	30.29	439.00
94	416.67	4	SLE Q	-215467.00	-10616,20	21220.90	0.00	78.54	29.66	429.69
95	476.19	4	SLE Q	-210047.00	-10284.80	20558.30	0.00	78,54	28.84	417.8
96	535.71	4	SLE Q	-204639.00	-9827.67	19644.60	0.00	78.54	27.88	404.08
97	595.24	4	SLE Q	-199241.00	-9276,12	18542.10	0.00	78,54	26.81	388.83
98	654.76	4	SLE Q	-193854.00	-8657.37	17305.30	0.00	7B.54	25.66	372.53
99	714.29		SLE Q	-188477.00	-7994.97	15981.20	0.00	78.54	24.47	355.55
100	773.81	4	SLE Q	-183111.00	-7309.02	14610.10	0.00	78.54	23.24	338.22
101	833.33	4	SLE Q	-177754.00	-6616.46	13225.70	0.00	78.54	22.02	320.80
102	892,86	4	SLE Q	-172407.00	-5931,30	11856,10	0.00	78.54	20.80	303.50
103	952.38	4	SLE Q	-167069.00	-5264.92	10524+10	0.00	78.54	19.60	286.5
104		_	SLE Q	-161740.00	-4626.33	9247.61	0.00	78,54	18.44	269.9
105	1071.43	4	SLE Q	-156420.00	-4022.46	8040.53	0.00	78.54	17.32	253.98
106	1130.95	_	SLE Q	-151108.00	-3458.38	6913.00	0.00	78+54	16.24	238.63
107	1190.48	4	SIE Q	-145804.00	-2937.58	5871.97	0.00	78.54	15.21	223.98
108	1250.00	4	SLE Q	-140509.00	-2462.16	4921.64	0,00	78,54	14.24	210.04
	1309.52	-	SLE Q		~2033.05	4063.88	0.00	78.54	13.32	196.84
_	1369.05	4	SIE Q	-129939.00	-1650.20	3298.59	_	78.54	12.45	184.38
_	1428.57	_	SLE Q		-1312.75	2624.06		78,54	11.63	172.63
_	1488,10	-	SLE Q	-119397.00	-1019.19			78,54	10.87	161.60
_	1547.62	_	SLE Q		-767.49			78.54	10.16	151.23
	1607.14	_		-108881.00				78.54		141.45
_	1666.67		SLE Q		-379.57		-	78.54	8.86	132.32
	1726.19	_	SLE Q		-237.65		_	78,54		123.70
	1785.71		SLE Q				-	78,54	_	115.50
	1845.24		SLE Q		-42.35			78.54		107.80
-	1904.76		SLE Q			-		78.54		101.09
	1964,29		SLE Q			-112.97	-	78,54		95.33
_	2023,81		SLE Q					78.54		89,30
	2083.33		SLE Q				_	78.54	_	83.0
_	2142.86		SLE Q		81.11		-	78.54	5,12	76.6
	2202.38		SLE Q					78,54		70.10
	2261.90		SLE Q		-		-	78,54		63.45
_	2321.43	_	SLE Q					78.54	3.79	56.80
127	2380.95	- 4	SLE Q	-40996.40	17.23	-34.43	0.00	78.54	3.35	50.25

Verifiche principali

Caso	Tipo								
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio								
.7	SLU N cost - min. sic.								
48	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)								
86	C.Rare - Sc max (min. compr.), C.Rare - Sf max (max traz.)								
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)								
129	C.Q.Per Sc max (min. compr.), C.Q.Per Sf max (max traz.)								

Palo n. 6

Caratteristiche del palo e dei materiali utilizzati

-35797.70

R <cm>></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>	
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04	

Le sollècitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti.

0.00

Azioni ed effetti comuni

	****			- Committee	_
	Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
	PP	0.00	0.00	0.00	
١	SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 6 (-139)

Caso	8	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	274241.00	6270.22	558.54	37079.00	24873.20
	1	SLU	TAG				0.00	0.00
	1	SIAI	ECC				0.00	0.00
	1	SLU	TOT	274241.00	6270.22	558.54	37079.00	24873.20
2	2	SLE R	RVN	203142.00	4644.61	413.73	27465.90	18424.60
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	203142.00	4644.61	413.73	27465.90	18424.60
- 3	3	SLE F	RVN	203142.00	4644.61	413.73	27465.90	18424.60
	3	SLE F	TAG			- 1	0.00	0.00
	3	SLE F	ECC				0.00	0.00
	. 3	SLE F	TOT	203142.00	4644.61	413.73	27465.90	18424.60
-4	4	SLE Q	RVN	203142.00	4644.61	413.73	27465.90	18424.60
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC	3			0.00	0.00
	4	SLE Q	TOT	203142.00	4644.61	413.73	27465.90	18424.60

Sollecitazioni nei pali

Caso CC TCC		Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>	
1	1	SLU	1	-274241.00	-6270.22	-558.54	-37079.00	-24873.20
.2	2	SLE R	1	-203142.00	-4644.61	-413.73	-27465.90	-18424.60
3	3	SLE F	1	-203142.00	-4644.61	-413.73	-27465.90	-18424.60
4	4	SLE Q	1	-203142.00	-4644.61	-413.73	-27465,90	-18424,60

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	oc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SIAI	-274241.00	36912.70	-24761.70	-274241.00	206383.00	-137991.00	2-3	213.75	5.58
- 2	59,52	1	SIU	-273543.00	39526.40	-26515.00	-273543.00	206211.00	-137860.00	2-3	213.75	5.21
- 3	119.05	1	SLU	-270473.00	41234.30	-27660.70	-270473.00	205453.00	-137285.00	2-3	213.75	4.97
- 4	178.57	1	SIU	-267411.00	42164.70	-28284.80	-267411.00	204693.00	-136708.00	2-3	213.75	4.84
5	238.09	1	SILI	-264357.00	42436.50	-28467.20	-264357.00	203934.00	-136131.00	2-3	213.75	4.79
- 6	297,62	1	SIU	-261311.00	42158.80	-28280.90	-261311.00	203176.00	-135554.00	2-3	213.75	4.81
7	357.14	1	SIU	-258274.00	41388.20	-27763.90	-258274.00	202418.00	-134978.00	2-3	213.75	4.88
8	416.67	1	SLU	-251893.00	40052.80	-26868.10	-251893.00	200749.00	-133806.00	2-3	213.75	5.00
9	476.19	1	SLU	-245525.00	38236.00	-25649.40	-245525.00	198983.00	-132682.00	2-3	213.75	5,19
-10	535,71	-1	SIU	-239170.00	36058.20	-24188.50	-239170.00	197219.00	-131530.00	2-3	213.75	5.46
11	595.24	1	SLU	-232828.00	33624.80	-22556.10	-232828.00	195442.00	-130371.00	2-3	213.75	5.80
12	654.76	1	SIU	-226499.00	31026.70	-20813.20	-226499.00	193660.00	-129209.00	2-3	213.75	6.23
13	714.29	1	SLU	-220182.00	28341.40	-19011.90	-220182.00	191871.00	-128044.00	2-3	213.75	6.75
14	773.81	1	SLU	-213876.00	25634,20	-17195.80	-213876.00	190071.00	-126872.00	2-3	213.75	7,40
15	833.33	1	SIU	-207582.00	22958.90	-15401.20	-2075B2.00	188267.00	-125698.00	2-3	213.75	8.18
16	892.86	1	SLU	-201300.00	20359.20	-13657.30	-201300.00	186455.00	-124520.00	2-3	213.75	9.14
17	952.38	1	SLU	-195028.00	17869.70	-11987.30	-195028.00	184634.00	-123337.00	2-3	213.75	10.31
18	1011.90	1	SIU	-188766.00	15516.90	-10409.00	-188766.00	182808.00	-122152.00	2-3	213.75	11.76
19	1071,43	1	SIU	-182515.00	13320,10	-8935.34	-182515.00	180973.00	-120962.00	2-3	213.75	13.57
20	1130.95	1	SLU	-176273,00	11292.40	-7575.12	-2571250.00	179131.00	-119769.00	2-3	213.75	14.58
21	1190.48	1	SLU	-170041.00	9441.67	+6333.64	-2571250.00	177284.00	-110573.00	2-3	213.75	15.12
22	1250.00	1	SIJ	-163818.00	7771.32	+5213.14	-2571250.00	175427.00	-117373.00	2-3	213,75	15.69
23	1309.52	1	SLU	-157604.00	6280.94	-4213.37	-2571250.00	173565.00	-116171.00	2-3	213.75	16.31
24	1369.05	1	SLU	-151398.00	4967.03	-3331.97	-2571250.00	171696.00	-114966.00	2-3	213.75	16.98
25	1428,57	1	SLU	-145200.00	3823.60	-2564.94	-2571250.00	169819.00	-113758.00	2-3	213.75	17.70
26	1408.10	1	SLU	-139011.00	2842.70	-1906.93	-2571250.00	167938.00	-112548.00	2-3	213.75	18,49
27	1547.62	1	SIU	-132828.00	2014.83	-1351.58	-2571250.00	166047.00	-111335.00	2-3	213.75	19.35
28	1607.14	1	SIM	-126653.00	1329,38	-891.77	-2571250.00	164151.00	-110119.00	2-3	213,75	20.30
29	1666.67	1	SLU	-120484.00	774.95	-519.85	-2571250.00	162250.00	-108902.00	2-3	213.75	21.34
30	1726.19	3.5	SEU	-114322.00	339.60	-227.81	-2571250.00	160360.00	-107623.00	2-3	213.75	22.49
31	1785,71	1	SLU	-108166.00	11.07	-7.43	-2571250.00	158514.00	-106180.00	2-3	213.75	23.77
32	1845,24	1	SIU	-102016.00	-223.00	149.59	-2571250.00	-156472.00	104669.00	2-3	33.75	25,20
33	1904.76	1	SLU	-95871.60	-375.00	251.56	-2571250.00	-154461.00	103379.00	2-3	33.75	26.82
34	1964.29	1	SLU	-89732.10	-457.21	306.71	-2571250.00	-152445.00	102085.00	2-3	33.75	28.65
35	2023.81	1	SIA	-83597.50	-481.77	323.18	-2571250.00	-150422.00	100788.00	2-3	33.75	30.75
36	2083.33	1	SLU	-77467.30	-460.62	308.99	-2571250.00	-148389.00	99485.10	2-3	33.75	33.19

37	2142.86	1	SLU	-71341.20	-405.51	272.03	-2571250.00	-146352.00	98179.00 2-3	33.75	36.041
38	2202.38	1	SLU	-65219.00	-328.03	220.05	-2571250.00	-144308.00	96868.10 2-3	33.75	39,425
39	2261.90	1	SIU	-59100.30	-239.56	160.70	-2571250.00	-142256.00	95553.10 2-3	33.75	43.507
40	2321.43	1	SIJJ	-52984.80	-151.38	101.55	-2571250.00	-140201.00	94234.70 2-3	33.75	48.528
41	2380,95	1	SLU	-46872.10	-74.66	50.08	-2571250.00	-138136.00	92911.80 2-3	33.75	54.857
42	2440.48	1	SLU	-40761.90	-20.51	13.76	-2571250.00	-136067.00	91585.80 2-3	33.75	63.080
43	2500.00	1	SIA	-34653.90	0.00	0.00	-2571250.00				74.198

Stato limite ultimo - Verifiche a taglio

Caso	X <cm></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIJJ	6270.22	558.54	0.85	11.31	6295.05	1.00	32294.70	370950.00	32294.70	5.130
- 2	59.52	1	SLU	4309.24	383.86	0.85	11.31	4326.30	1.00	32294.70	370850.00	32294.70	7.463
3	119.05	1	SLU	2616.50	233.07	0.85	11.31	2626.86	1.00	32294.70	370410.00	32294.70	12.294
4	178,57	- 5	SIJJ	1173.02	104.49	0.85	11.31	1177.66	1.00	32294.70	369972.00	32294.70	27.423
:5	238,09	1	SLU	-40.83	-3.64	0.85	11.31	40.99	1.00	32294.70	369534.00	32294.70	>100
.6	297.62	1	SIA	-1044.91	-93.08	0.85	11.31	1049.04	1.00	32294.70	369098.00	32294.70	30.785
7	357.14	1	SIU	-2116.79	-188.56	0.85	11.31	2125.17	1.00	32294.70	368663.00	32294.70	15,196
В	416.67	2	SLU	-3218.98	-286.74	0.85	11.31	3231.72	1.00	32294.70	367749.00	32294.70	9.993
9	476.19	1	SIU	-4062.45	-361.88	0.85	11.31	4078.54	1.00	32294.70	366837.00	32294.70	7.918
10	535.71	1	SIA	-4678.68	-416.77	0.85	11.31	4697.21	1.00	32294.70	365927.00	32294.70	6.B75
11	595.24	1	SIJ	-5097.52	-454,0B	0.85	11.31	5117,70	1.00	32294.70	365018.00	32294.70	6.310
12	654.76	1	SLU	-5346.94	-476.30	0.85	11.31	5368.12	1,00	32294.70	364112.00	32294.70	6.016
13	714.29	1	SLU	-5452.92	-485.74	0.85	11.31	5474.51	1.00	32294.70	363207.00	32294.70	5.899
14	773.81	1	SIJ	-5439.26	-484.52	0.85	11.31	5460.80	1.00	32294.70	362304.00	32294.70	5.914
15	833.33	1	SLU	-5327.63	-474.58	0.85	11.31	5348.72	1,00	32294.70	361402.00	32294.70	6.038
16	892.86	1	SIJ	-5137.50	-457.64	0.85	11.31	5157.85	1.00	32294.70	360502.00	32294.70	6.261
17	952,38	1	SLU	-4886.26	-435.26	0.85	11.31	4905.60	1.00	32294.70	359604,00	32294.70	6.583
18	1011.90	1	SLU	-4589.20	-408.80	0.85	11.31	4607.37	1.00	32294.70	358707.00	32294.70	7.009
19	1071.43	1	SILI	-4259.72	-379.45	0.85	11,31	4276.58	1.00	32294.70	357811.00	32294.70	7.552
20	1130.95	1	SLU	-3909.34	-348.24	0.85	11.31	3924.82	1.00	32294.70	356917.00	32294.70	8.228
21	1190.48	1	SLU	-3547.92	-316.04	0.85	11.31	3561.97	1.00	32294.70	356025.00	32294.70	9.067
22	1250.00	1	SLU	-3183.76	-283.60	0.85	11.31	3196.36	1.00	32294.70	355133.00	32294.70	10.104
23	1309,52	1	SLU	-2823.71	-251.53	0.85	11.31	2834,89	1.00	32294.70	354243.00	32294.70	11.392
24	1369.05	1	SIJ	-2473.41	-220.33	0.85	11.31	2483.20	1.00	32294.70	353354.00	32294.70	13.003
25	1428.57	1	SIU	-2137.32	-190.39	0.85	11.31	2145.78	1.00	32294.70	352467,00	32294.70	15.050
26	1488.10	1	SLU	-1818.95	-162.03	0.85	11.31	1826.15	1.00	32294.70	351580.00	32294.70	17.685
27	1547.62	1	SIJ	-1520.95	-135.48	0.85	11.31	1526.97	1.00	32294.70	350694.00	32294.70	21.149
28	1607.14	1	SIM	-1245.24	-110.92	0.85	11.31	1250.17	1,00	32294.70	349810.00	32294.70	25.832
29	1666.67	1	SIN	-993.14	-88.47	0.85	11.31	997.08	1.00	32294.70	348926.00	32294.70	32.389
30	1726.19	1	SLU	-765.47	-68.19	0.85	11.31	768.50	1.00	32294.70	348044,00	32294.70	42.023
31	1785.71	1	SIU	-562.66	-50.12	0.85	11.31	564.89	1.00	32294.70	347162.00	32294.70	57.170
32	1845.24	1	SILI	-384.82	-34,28	0.85	11.31	386.35	1.00	32294.70	346281,00	32294.70	83.590
33	1904.76	1	SIJ	-231,86	-20.65	0.85	11.31	232.78	1.00	32294.70	345401,00	32294.70	>100
34	1964.29	1	SIJJ	-103.52	-9.22	0.85	11.31	103.93	1.00	32294.70	344521.00	32294.70	>100
35	2023.81	1	SLU	0.55	0.05	0.85	11,31	0.55	1.00	32294.70	343643.00	32294.70	>100
36	2083.33	1	SLU	80.74	7.19	0.85	11.31	B1.06	1.00	32294.70	342764.00	32294.70	>100
37	2142.86	1	SLU	137.44	12.24	0.85	11.31	137.98	1.00	32294.70	341887.00	32294.70	>100
38	2202.38	1	SLU	171.00	15.23	0.85	11.31	171.68	1.00	32294.70	341010.00	32294.70	>100
39	2261,90	1	SIJJ	181.74	16.19	0.85	11.31	182.46	1.00	32294.70	340134.00	32294.70	>100
40	2321.43	1	SLU	169.88	15.13	0.85	11.31	170.55	1,00	32294.70	339258.00	32294.70	>100
41	2380.95	1	SLU	135,58	12.08	0.85	11.31	136.11	1.00	32294.70	338382.00	32294.70	>100
42	2440.48	1	SLU	78.94	7.03	0.85	11.31	79,25	1.00	32294.70	337507.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <cmq></cmq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE	-203142.00	-18342.00	27342.80	0.00	78.54	33.54	478.30
45	59.52	2	SLE I	-202938.00	-19640.80	29278.80	3.14	75,40	34,76	494,70
46	119.05	2	SLE I	R-200853.00	-20489.40	30543.90	9.42	69.11	35.43	503.52
47	178.57	2	SLE 1	-198775.00	-20951.70	31233.10	9.42	69,11	35.74	507.46
48	238.09	2	SLE 1	-196703.00	-21086.80	31434,50	12.57	65,97	35.73	507.06
49	297.62	2	SLE I	-194638.00	-20948.80	31228.80	12,57	65.97	35.44	502.89
50	357.14	2	SLE	R -192578.00	-20565.90	30657.90	9.42	69,11	34.90	495.33
51	416.67	2	SLE	R-187866.00	-19902.30	29668,70	9.42	69,11	33.88	481.00
52	476.19	2	SLE I	-183165.00	-18999.50	28322.90	9.42	69.11	32.62	463.42
53	535.71	2	SLE I	-178473.00	-17917.40	26709.80	9.42	69.11	31.19	443.55
54	595,24	2	SLE I	-173791.00	-16708.20	24907.30	0.00	78,54	29.66	422,20
55	654.76	2	SLE I	-169118.00	-15417.20	22982.70	0.00	78,54	28.06	400.05
56	714.29	2	SLE !	R -164454.00	-14082.90	20993.60	0.00	78.54	26.44	377,57
57	773.81	2	SLE I	-159799.00	-12737.70	18988.30	0.00	78.54	24.82	354.98
58	833.33	2	SLE I	R -155152.00	-11408.30	17006.60	0.00	78.54	23.20	332.60
59	892,86	2	SLE I	R-150514.00	-10116.50	15080.90	0.00	78.54	21.63	310.70
60	952.38	2	SLE I	3-145884.00	-B879.50	13236.80	0.00	78.54	20.10	289.51
61	1011.90	2	SLE I	3-141262.00	-7710.38	11494.00	0.00	78.54	18.64	269.17
62	1071.43	2	SLE I	-136647.00	-6618.77	9866.72	0.00	78.54	17.25	249.82
63	1130.95	2	SLE	R -132040.00	-5611.20	8364,72	0.00	78.54	15.94	231.54

214.	14.71	78.54	0.00	6993.83	-4691.58	-127440.00	SLE R	2	1190.48	54
198.	13.57	78.54	0.00	5756.54	-3861.59	-122846.00	SLE R	2	1250.00	65
183.	12.51	78.54	0.00	4652.55	-3121.01	-118259.00	SLE R	2	1309.52	66
169.	11.53	78.54	-	3679,28	-2468.13	-113679.00	SLE R	2	1369.05	_
156.5	10,63	78,54	-	2832.30	-1899.96	-109104.00	SLE R	_	1428.57	_
145.	9.81	78.54		2105.70	-1412.54	-104536.00	SLE R	-	1488.10	_
134.	9.06	78.54		1492.46	-1001.17	-99973.00	SLE R	$\overline{}$	1547.62	7.0
124.0	8.37	78.54	-	984.73	-660.57	-95415.50	SLE R	_	1607.14	_
115.0	7.74	78.54	-	574.04 251.55	-385.08 -168.75	-90863.00 -86315.40	SLE R	_	1655.57 1726.19	_
99.	6.65	78.54	-	8.20	-5.50	-81772.50	SLE R	_	1785.71	_
95.3	6.38	78.54	_	-165,19	110.81	-77233.90	SLE R	_	1845.24	
90.5	6.08	78,54		-277.78	186.34	-72699.50	SLE R	_	1904.76	-
85.9	5.75	78.54	-	-338.68	227,19	-68169,00	SLE R	$\overline{}$	1964.29	77
80.	5.40	78.54	0.00	-356.87	239.39	-63642.10	SLE R	2	2023.81	78
74.	5.02	78.54	0.00	-341,20	228.88	-59118.70	SLE R	2	2083.33	79
69.	4.63	78.54	0.00	-300,38	201,50	-54598.40	SLE R	2	2142.86	80
63.	4.22	78.54	0.00	-242.98	163.00	-50081.10	SLE R	2	2202.38	81
57.0	3.81	78.54	0.00	-177,45	119.04	-45566.40	SLE R	2	2261.90	82
51.0	3.41	78.54		-112.13	75,22	-41054.20	SLE R	_	2321.43	83
45.	3.00	78.54	-	-55,30	37,10	-36544.20	SLE R	$\overline{}$	2380.95	84
39.	2.61	78.54	-	-15.19	10,19	-32036.10	SLE R	-	2440.48	85
33.	2.24	78,54		0.00	0.00	-27529.80	SLE R	_	2500.00	86
478.	33.54	78.54	_	27342.80	-18342.00	-203142.00	SLE Q	_	0.00	87
494.	34.76	75,40		29278.80	-19640.80		SLE Q	$\overline{}$	59.52	88
503.3	35.43	69,11	-		-20489.40	-200853.00	SLE Q	_	119.05	89
507.	35.74	65.97		31233.10 31434.50	-20951,70 -21086.80	-198775.00 -196703.00	SLE Q	-	178.57	90
502.0	35.44	65.97			-21086.80		SLE Q	\rightarrow	238.09	92
495.3	34.90	69.11	9.42	30657.90	-20565.90	-192578.00	SLE Q	$\overline{}$	357.14	93
481.6	33.88	69.11	_		-19902.30		SLE Q	_	416.67	94
463.	32.62	69,11	-	28322.90	-18999.50	-183165.00	SLE Q	-	476,19	95
443.	31.19	69,11			-17917.40	-178473.00	SLE Q	_	535.71	96
422.	29.66	78+54		24907.30	-16708.20	-173791.00	SLE Q	_	595.24	97
400.0	28.06	78.54	0.00	22982.70	-15417.20	-169118.00	SIE Q	4	654.76	98
377.	26.44	78.54	0,00	20993.60	-14082.90	-164454.00	SLE Q	4	714.29	99
354.	24.82	78.54	0.00	18988.30	-12737.70	-159799.00	SLE Q	4	773.81	100
332.	23.20	78.54	0.00	17006.60	-11408.30	-155152.00	SIE Q	4	833.33	101
310.	21.63	78,54	-	15080.90	-10116.50	-150514.00	SLE Q	4	892.86	102
289.	20.10	78,54		13236.80	-8879,50	-145884.00	SLE Q	_	952.38	103
269.	18.64	78.54			-7710.38		SLE Q		1011.90	_
249.	17.25					-136647.00			1071,43	
231.	15.94					-132040.00			1130.95	
214.	14.71		-			-127440.00 -122846.00			1250.00	
183.	12.51	78.54				-118259.00	_	_	1309.52	_
169.	11.53	78.54				-113679.00			1369.05	_
156.	10.63	78.54				-109104.00			1428,57	
145.	9.81		THE RESERVE OF THE PERSON NAMED IN	The second second		-104536.00				
134.	9.06	78.54		1492.46			SLE Q		1547.62	
124.	8.37			984.73	-660.57	-95415.50			1607.14	114
115.	7.74	78+54	0.00	574.04		-90863.00	SLE Q	4	1666.67	_
107.	7.17	78,54		The second second second			SLE Q		1726.19	-
99.	6.65	78.54					SLE Q		1785.71	
95.	6.38			-165.19		-77233.90				
90.	6.08	_	_			-72699.50		_	1904.76	
85.	5.75	78.54					SLE Q		1964.29	_
80.	5.40	78.54					SLE Q		2023.81	
74.	5.02	78.54					SLE Q		2083.33	
69.	4.22	78.54 78.54		- Annual Section 1	201.50		SLE Q		2142.86	
57.0	3.81						SLE Q		2261.90	
51.6	3.41		_				SLE Q		2321.43	_
45.0	3.00	78.54		-55.30		-36544.20	SLE Q		2380.95	_
39.	2.61	78,54					SLE Q		2440.48	_
3-10-10	2.24		0.00		0.00				2500.00	- Annual Contract of

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
- 5	SLU N cost - min. sic.
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
49	C.Rare - Sf max (max traz.)
56	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
92	C.Q.Per Sf max (max traz.)
99	C.Q.Per Sc max (min. compr.)

Palo n. 7

Caratteristiche del palo e dei materiali utilizzati

R Cf <cm> C</cm>		Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>	
60.00	6.00	C30/37	307,10	20.59	174.02	13.73	B450C	4300.00	3913.04	

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>	
PP	0.00	0.00	0.00		
SVR	0.00				

Azioni ed effetti - Plinto/Palo n. 7 (-105)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>	
- 1	- 2	SLU	RVN	204511.00	6649.98	719.13	55915.30	22826.90	
	1	SLU	TAG		6 0	3	0.00	0.00	
	1	SLU	ECC				0.00	0.00	
	1	SIA	TOT	204511.00	6649.98	719.13	55915.30	22826.90	
/2	.2	SLE R	EVN	151490.00	4925.91	532.69	41418.70	16908.80	
	2	SLE R	TAG				0.00	0.00	
	2	SLE R	ECC				0.00	0.00	
	2	SLE R	TOT	151490.00	4925.91	532,69	41418.70	16908.BC	
- 3	3	SLE F	BVN	151490.00	4925.91	532.69	41418.70	16908.80	
	. 3	SLE F	TAG				0.00	0.00	
	3	SLE F	ECC				0.00	0.00	
	3	SLE F	TOT	151490.00	4925.91	532.69	41418.70	16908.80	
4	4	SLE Q	RVN	151490.00	4925.91	532.69	41418.70	16908.80	
	4	SLE Q	TAG			- 3	0.00	0.00	
	4	SLE Q	ECC				0.00	0.00	
	4	SLE Q	TOT	151490.00	4925.91	532.69	41418.70	16908.80	

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>	
1	1	SLU	1	-204511.00	-6649.98	-719.13	-55915.30	-22826.90	
- 2	2	SLE R	1	-151490.00	-4925.91	-532.69	-41418.70	-16908.80	
- 3	3	SLE F	1	-151490.00	-4925.91	-532.69	-4141B.70	-16908.80	
4	4	SLE Q	. 1	-151490.00	-4925.91	-532.69	-41418.70	-16908.80	

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-204511.00	55690.80	-22735.30	-204511.00	208420.00	-86103.60	2-3	202.50	3.749
- 2	59,52	1	SIU	-204298.00	58702.80	-23964.90	-204298.00	208351.00	-86080.20	2-3	202.50	3.555
.3	119.05	1	SIJ	-202194.00	60492.90	-24695.70	-202194.00	207670.00	-85848.40	2-3	202.50	3,439
- 4	178.57	1	SIJ	-200097.00	61240.20	-25000.80	-200097.00	206990.00	-85617.00	2-3	202.50	3.386
- 5	238.09	1	SLU	-198006.00	61109.60	-24947.50	-198006.00	206313.00	-85385.80	2-3	202.50	3,383
- 6	297,62	1	SLU	-195922.00	60251.70	-24597,20	-195922.00	205635.00	-85155,20	2-3	202,50	3,420
- 7	357.14	1	SLU	-193843.00	58747.70	-23983.20	-193843.00	204956.00	-84925.10	2+3	202.50	3.496
.8	416,67	1	SLU	-189099.00	56511.80	-23070.50	-189099.00	203406.00	-84398.50	2-3	202,50	3.608
9	476.19	1	SLU	-184365.00	53660.40	-21906.40	-184365.00	201852.00	-83871.60	2-3	202.50	3.771
10	535.71	1	SLU	-179642.00	50357.30	-20557.90	-179642.00	200294.00	-83344.20	2-3	202.50	3.989
11	595.24	1	SEU	-174927.00	46744.60	-19083.10	-174927.00	198735.00	-82800.50	2-3	202.50	4.264
12	654.76	1	SIJJ	-170223.00	42944.80	-17531.80	-170223.00	197172.00	-82242.20	2-3	202,50	4.600
13	714,29	1	SIJ	-165527.00	39061.40	-15946.50	-165527,00	195607.00	-81683,30	2-3	202,50	5.024
14	773.81	1	SLU	-160840.00	35181.00	-14362.30	-160840.00	194038.00	-81124.20	2-3	202.50	5.535
15	833,33	.1	SLU	-156162.00	31374.60	-12808.40	-156162.00	193271.00	-78318.10	2-3	201.88	6.15
16	892.86	1	SLU	-151492.00	27699.10	-11307.90	-151492.00	191694.00	-77763.50	2-3	201.88	6.914
17	952,38	1	SLU	-146830,00	24199,20	-9879.12	-146830.00	189335.00	-79194.40	2-3	202.50	7.852
18	1011.90	1	SLU	-142177.00	20908.20	-8535.61	-142177.00	187764.00	-78461.80	2-3	202.50	9.011
19	1071.43	-1	SLU	-137530.00	17850.10	-7287.14	-137530.00	186193.00	-77730.30	2-3	202.50	10.465
20	1130.95	1	SLU	-132892.00	15040.20	-6140.03	-132892.00	184616.00	-76991.50	2-3	202.50	12.313
21	1190.48	1	SIU	-128260.00	12487.00	-5097.72	-128260.00	183038.00	-76254,20	2-3	202.50	14.701
- 22	1250.00	1	SIJ	-123635.00	10193.00	-4161.20	-123635.00	181454.00	-75509,20	2-3	202.50	17,851
23	1309.52	1	SLU	-119017.00	8155.54	-3329.43	-2571250.00	179870.00	-74765.90	2-3	202.50	21.604
24	1369.05	1	SLU	-114405.00	6368.06	-2599.71	-2571250.00	178279,00	-74015.20	2-3	202.50	22.475
25	1428.57	1	SIM	-109800.00	4820.71	-1968.01	-2571250.00	176689.00	-73265.80	2-3	202.50	23,418
26	1488.10	1	SIU	-105200.00	3501.10	-1429.30	-2571250.00	175092.00	-72509.60	2-3	202.50	24.442
27	1547.62	1	SLU	-100606.00	2394.95	-977.72	-2571250.00	173495.00	-71754.00	2-3	202.50	25,558

	 Color Methodolo, New York 	11.00	ATTENDED OF	Party Party Barriery
RO	lazione	rd1	00	COLO
1/6	Idaliulie	u	La	CUIU

			4	Company of the second of the s								
28	1607,14	1	SLU	-96017.00	1486.55	-606.87	-2571250.00	171893.00	-70992.90	2-3	202.50	26,779
29	1666.67	1	SIA	-91433.40	759.29	-309.97	-2571250.00	170289.00	-70231.10	2-3	202.50	28.122
30	1726.19	1	SLU	-86854.80	195.92	-79.98	-2571250.00	168680.00	-69464.50	2-3	202.50	29.604
31	1785,71	1	SLU	-82280.80	-221.07	90.25	-2571250.00	-166784.00	69644.50	2-3	22.50	31,250
32	1845.24	1	SLU	-77711.20	-509.28	207.91	-2571250.00	-165094.00	69075.10	2-3	22.50	33.087
33	1904.76	1	SLU	-73145.70	-686.21	280.14	-2571250.00	-164094.00	66622.60	2-3	21.88	35.152
3.4	1964.29	1	SIJ	-68584.20	-769.16	314.00	-2571250.00	-162391.00	66060.80	2-3	21.88	37.490
35	2023.81	1	SLU	-64026.40	-775.15	316.45	-2571250.00	-160035.00	66941.00	2-3	22.50	40.159
36	2083.33	1	SLU	-59472.00	-720.88	294.29	-2571250.00	-158344.00	66183.00	2-3	22.50	43.235
37	2142.86	1	SIJJ	-54920.80	-622.75	254.23	-2571250.00	-156647.00	65421.60	2-3	22.50	46.817
38	2202.38	1	SLU	-50372.60	-496.87	202.84	-2571250.00	-154947.00	64658.50	2-3	22.50	51.045
39	2261.90	1	SLU	-45827,00	-359.09	146.59	-2571250.00	-153240.00	63864.90	2-3	22.50	56.108
4.0	2321.43	1	SIAJ	-41283.90	-225.05	91.87	-2571250.00	-151531.00	63067.70	2-3	22.50	62.282
41	2380.95	1	SLU	-36743.10	-110.26	45.01	-2571250.00	-149815.00	62266.70	2-3	22.50	69.979
42	2440.48	1	SIU	-32204.10	-30.12	12.30	-2571250.00	-148097.00	61464.10	2-3	22.50	79.842
43	2500.00	1	SILI	-27667.00	0.00	0.00	-2571250.00					92,936

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRod <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIA	6649.98	719.13	0.85	11.31	6688.75	1.00	32294.70	360962.00	32294.70	4.828
- 2	59.52	1	SIJ	4275,85	462.39	0.85	11.31	4300.78	1.00	32294.70	360932.00	32294.70	7.50
3	119.05	1	SLU	2237.15	241.93	0.85	11.31	2250.19	1,00	32294.70	360630.00	32294.70	14.35
4	178.57	1	SLU	508.77	55.02	0.85	11.31	511.74	1.00	32294.70	360330.00	32294.70	63.108
.5	238.09	1	SLU	-934,89	-101.10	0.85	11.31	940.34	1.00	32294.70	360030.00	32294.70	34.34
- 6	297,62	1	SLU	-2119.58	-229.21	0.85	11.31	2131.94	1,00	32294.70	359732.00	32294.70	15.148
7	357.14	1	SLU	-3370.02	-364.44	0.85	11.31	3389.67	1.00	32294.70	359434.00	32294.70	9.52
.8	416.67	1	SLU	-4641.46	-501.93	0.85	11.31	4668.52	1.00	32294.70	358755.00	32294.70	6.91
.9	476.19	1	SLU	-5597.59	-605.33	0.85	11.31	5630.23	1.00	32294.70	358076.00	32294.70	5.73
10	535.71	1	SIAI	-6278.06	-678.91	0.85	11.31	6314.66	1.00	32294.70	357400.00	32294.70	5.11
11	595.24	1	SIJ	-6720.27	-726.74	0.85	11.31	6759.45	1.00	32294.70	356725.00	32294.70	4.77
12	654.76	1	SLU	-6959.14	-752.57	0.85	11.31	6999.71	1.00	32294.70	356051.00	32294.70	4.51
13	714.29	1	SLU	-7026.89	-759.89	0.85	11.31	7067.86	1.00	32294.70	355378.00	32294.70	4.56
14	773.81	1	SLU	-6952,99	-751.90	0.85	11.31	6993.53	1.00	32294.70	354707.00	32294.70	4,61
15	833.33	1	SIJ	-6764.10	-731.48	0.85	11.31	6803.54	1.00	32294.70	354037.00	32294.70	4.74
16	892.86	1	SIJJ	-6484.11	-701.20	0.85	11.31	6521.92	1.00	32294.70	353368.00	32294.70	4.95
17	952.38	1	SLU	-6134.23	-663.36	0.85	11.31	6169.99	1.00	32294.70	352700.00	32294.70	5.23
18	1011.90	1	SIJ	-5733.05	-619.98	0.85	11.31	5766.48	1.00	32294.70	352033.00	32294.70	5:60
19	1071.43	1	SIAI	-5296.77	-572.80	0.85	11.31	5327.65	1,00	32294.70	351368.00	32294.70	6.06
20	1130.95	1	SIAJ	-4839,26	-523.32	0.85	11.31	4867.48	1.00	32294.70	350703.00	32294.70	6.63
21	1190,48	1	SLU	-4372.31	-472.82	0.85	11.31	4397,80	1.00	32294.70	350040.00	32294.70	7.34
22	1250.00	1	SIA	-3905.77	-422.37	0.85	11.31	3928.54	1.00	32294.70	349377.00	32294.70	8.22
23	1309.52	1	SILI	-3447.74	-372.84	0.85	11.31	3467.84	1.00	32294.70	348716.00	32294.70	9.31
24	1369,05	1	SIJ	-3004.78	-324.94	0.85	11.31	3022.30	1.00	32294.70	348055.00	32294.70	10.58
25	1428.57	1	SIU	-2582.08	-279.23	0.85	11.31	2597.13	1.00	32294.70	347396.00	32294.70	12.43
26	1488.10	1	SLU	-2183.61	-236.14	0.85	11,31	2196.34	1.00	32294.70	346737.00	32294.70	14,70
27	1547.62	1	SLU	-1812,33	-195.99	0.85	11.31	1822.90	1.00	32294.70	346079.00	32294.70	17.71
28	1607.14	1	SLU	-1470.33	-159.00	0.85	11.31	1478.90	1,00	32294.70	345422.00	32294.70	21.83
29	1666.67	1	SLU	-1158.97	-125.33	0.85	11.31	1165.73	1.00	32294.70	344765.00	32294.70	27.70
30	1726,19	1	SIJ	-879.03	-95.06	0.85	11.31	884.16	1.00	32294.70	344109.00	32294.70	36.52
31	1785.71	1	SLU	-630.84	-68.22	0.85	11.31	634.51	1,00	32294.70	343454.00	32294.70	50.89
32	1845,24	1	SLU	-414.34	-44.81	0.85	11.31	416.75	1.00	32294.70	342799.00	32294.70	77.49
33	1904.76	1	SIAJ	-229.26	-24.79	0.85	11.31	230.60	1.00	32294.70	342145.00	32294.70	>100
34	1964.29	1	SLU	-75.15	-8.13	0.85	11.31	75.59	1.00	32294.70	341492.00	32294.70	>100
35	2023.81	1	SIAI	48.53	5.25	0.85	11.31	48.81	1.00	32294.70	340839.00	32294.70	>100
36	2083.33	1	SIU	142.35	15.39	0.85	11.31	143.18	1.00	32294.70	340187.00	32294.70	>100
37	2142.86	1	SIJ	206.87	22.37	0.85	11.31	208.07	1.00	32294.70	339535.00	32294.70	>100
38	2202.38	1	SLU	242.57	26.23	0.85	11.31	243.99	1.00	32294.70	338883.00	32294.70	>100
39	2261.90	1	SLU	249.88	27.02	0.85	11,31	251.33	1.00	32294.70	338232.00	32294.70	>100
40	2321.43	1	SLU	229.10	24.78	0.85	11.31	230.44	1.00	32294.70	337582.00	32294.70	>100
41	2380.95	1	SLU	180.46	19.51	0.85	11.31	181.51	1.00	32294.70	336931.00	32294.70	>100
42	2440.48	1	SLU	104.07	11.25	0.85	11.31	104.68	1.00	32294.70	336281.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <cmq></cmq>	σ _□ <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-151490.00	-16840.90	41252,40	28.27	50.27	38.21	535.13
4.5	59.52	2	SLE R	-151645.00	-17751.80	43483.50	31.42	47,12	40.23	561.96
46	119.05	2	SLE R	-150277.00	-18293.10	44809.60	31.42	47.12	41.48	578.20
47	178.57	2	SLE R	-148913.00	-18519.10	45363.10	31.42	47.12	42.02	585.10
48	238.09	2	SLE R	-147555.00	-18479.60	45266.30	31.42	47.12	41.94	583,81
49	297.62	2	SLE R	-146201.00	-18220.20	44630.90	31,42	47.12	41.35	575.64
50	357.14	2	SLE R	-144851.00	-17765.40	43516.80	31.42	47,12	40.29	561.42
51	416.67	2	SLE R	-141353.00	-17089.20	41860.60	31.42	47.12	38.74	540.25
52	476.19	2	SLE R	-137861.00	-16227.00	39748.50	31.42	47.12	36.77	513.55
53	535.71	2	SLE B	-134378.00	-15228.10	37301.70	28.27	50.27	34.53	483.10
54	595.24	2	SLE R	-130901.00	-14135.60	34625.60	28.27	50.27	32.12	450.52

							Rela	zion	e di calc	colo
::	[634.70]	2	اد صاف	-127431.00	-12986.50	31610.00			29.67	
0.5	714,19	-	922.0		-11812.20			33,41	27.23	384.38
97	778.01	·	5	Tm08731.00	10658.80	360000000	10.8.0	.:964	-01.37	257183
:::	833		T.	T1 7085, 00	9457170	3527,007,00	10.80	39.55	dz. 78	323219
9	890,96	/	977 R		-8000 LOS			(5.9)	770.79	0.981,780
6/0	980.23	4	977 R		-7717.87			70.06	70,97	07/01/68
	1011.90	2				10487,80	_	78,04	17.31	247.75
	1071.43	2	9 <u>22</u> 0			13122,30	_	78,04	10,77	116.38
0.0	_		977 7			111/0190		78.04	14.33	206.200
-	1130.46 1250.66	<u> </u>	977 S	96490.60 -96081.10	-0092109			780.54 780.54	18.00 11.78	150,88 150,80
_	1908.50				-0464.04		_	381.74	70,00	155.00
	1069.00	-	875.0		-1907.71	4717.08		78,04	9,64	141.01
	1428.07	2			-1407.79		_	78,04	1,73	118.17
-	1/88.10	-	977 7	797.91.00	10:8.74	2:33.71		78.54	9.30	776.81
-	1.07 (1.02		977 7	76104.60	927.537	1777.04	_	78.01	7.18	106.06
7:1	1007.14	7	977 R	-72700.00	-449.54	1101.15	0.00	381.54	619	97100
7:5	10 (6, 67)	7	977 R	±0.97(4,7°, (9)	-00%.61	21.77.42	0.00	491.54	5.95	981,800
7.3	1728,19	2	922.0	-63989.LC	-09.25	149,11	0.00	78,04	0.44	12.53
74	1785.71	2	922.0	-6250E.CC	06.85	-160.70	0.00	78,04	18	77.58
7.5	18/5.24		977.5	.83430.10	167.00	277.00	0.00	78.54	9.07	9.1.08
7.5	1904.256		977 7	8850	207.97	508.30	0.00	78.04	1.8"	77,197
-	1994,09	/	977 R		0077.58			780.74	4.59	691,194
-	1023.81	2	ă Н		134.41	-174,11		78,04	4,32	541.27
79	1083.33	2	877.0		118.00			78,04	4.02	19.88
::0	_		977 7		1:8:30			78.04	A . F	9.52.67
	Z********		977 7	33084.70	1500.05			78.54	a.38	90147
-	0241.90	4	977 R		100.59		_	481.74	2.05	45.58
9,7		4	977 R		641.06			30.54	0.79	40.75
-	2080,90	2			30.34 9.11		_	78,04	2,41	36.03
==	2440,48 2800100		<u>४ म्य ७</u> इस्ता स	-23697,10 00354,30	6.00	-22,31 0,00	_	78.04 78.04	1.20	31.50 27.68
87	0.00	,	977 Q			412,51,46		_	30.***	20.00
33	59.50	2			-1 (0.510.30)		31.47	47.10	40.73	561,96
39	119.65	-	977 0		-1101911.10		_	47.10	41.48	F78100
340	178.27	-	१.स. ७		-18010.10			47,10	41.02	287.10
91	228,69	4			-18479.60				41.04	252.81
-1/	737.57	-	977 Q			14530190		_	41.3.:	57.5184
9.5	3.:7.14	7	977 Q	177891.00	1.0560010	10016180	31.77	77.12	40.03	0.61 (4.0)
94	416.67	Ŀ	67. O	-1410(52.00)	=1 M(30.00)	41900.60	31.47	47.10	1(9), 74	540005
9.5	4.76,19		e E						76.77	513.55
90			_	-104375.00					34,30	
97				-100001.00						400.52
::				TU 25 81 100						
		_		703989,00						-
100		-	_	-120513.00			_			
				-11/063.00						
101				-110820,00						
203	1000.00			-110181.00				72,10	18,97	
	10 7 .4a			108/94 .00 103805 .00						
	1000.95			-9990-190				781.74		
	1190.49						_	781.74		
	1270.00									-
				-80670.30						
	1369105	_								
-	14,081,60	_					0.00	78.04	a.73	
	1499, 10					0593,41	_			
	1547.60					17/74/04				
	1607,14					1101,17				
	1668.07						_			-
	1778.114	_				17.3.12	_			
	1785.71	-					_			
	1945.04 1904.06		977 O			-2777.75 101.75	_	39.54 39.54		
	1964,58					-508.70 -069.70		78.54		
	2003.cT		877 Q					78.01		
	2083100	_	977 Q							99.88
	0140.96					-401.30				-A.04
	0200.38		977 G			-30 at 05				
	1261,90	-	8 AZ Q			-163,99		_		
	1001,43		8 A C			-166.70	_	_		
	z3801.ee		sta o			81 .87	0.00	78004		
	2770.46	7	str p	75,899,000	3.11	31	0.00	78.04		
109	0500.00	٤	977 0	-221654 JB0	0.00			780.74		

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	φ _{eq}	Δ _{⊞⊞} <mm></mm>	A _s <cmq></cmq>	Ac eff <cmq></cmq>	σ _∃ <dan cmq=""></dan>	eam	Wk <mm></mm>
87	0.00	4	SLE Q	-151490.00	41252.40	-16840.90	46,00	136,36	0.50	20.00	183.38	12.57	574.18	213.01	0.06	0.02
88	59.52	4	SLE Q	-151645.00	43483.50	-17751.80	46.00	136.36	0.50	20.00	194.72	12.57	645.40	254.66	0.07	0.02
89	119.05	4	SLE Q	-150277.00	44809.60	-18293.10	46.00	136.36	0.50	20.00	203.41	12.57	700.01	287.35	0.08	0.03
90	178.57	4	SLE Q	-148913.00	45363.10	-18519.10	46.00	136.36	0.50	20.00	184.85	15.71	729,23	305.22	0.09	0.03
91	238.09	4	SLE Q	-147555.00	45266.30	-18479.60	46.00	136.36	0.50	20.00	186.00	15.71	738.30	309.35	0.09	0.03
92	297.62	4	SLE Q	-146201.00	44630.90	-18220.20	46.00	136.36	0.50	20.00	185.20	15,71	731.98	301.70	0.09	0.03
93	357.14	.4	SLE Q	-144851.00	43516.80	-17765.40	46.00	136.36	0.50	20.00	205.08	12.57	710.50	283.83	0.08	0.03
94	416.67	4	SLE Q	-141353.00	41860.60	-17089.20	46.00	136.36	0.50	20.00	201.88	12.57	690.40	264.27	0.08	0.03
95	476.19	4	SLE Q	-137861.00	39748.50	-16227.00	46.00	136,36	0.50	20.00	195.93	12.57	653.02	235.82	0.07	0.02
96	535.71	4	SLE Q	-134378.00	37301.70	-15228.10	46.00	136.36	0.50	20.00	187.57	12.57	600.49	202.01	0.06	0.02
97	595.24	4	SLE Q	-130901.00	34625.60	-14135.60	46.00	136.36	0.50	20.00	177.12	12.57	534.79	166.00	0.05	0.01
98	654,76	4	SLE Q	-127431.00	31810.90	-12986.50	46.00	136.36	0.50	20.00	164.91	12.57	458.09	130.37	0.04	0.01
99	714.29	4	SLE Q	-123969.00	28934.30	-11812.20	46.00	136.36	0.50	20.00	171.12	9.42	372,83	97.04	0.03	0.01
100	773.B1	4	SLE Q	-120513.00	26060.00	-10638.80	46.00	136.36	0.50	20.00	181.96	6.28	282.62	67.23	0.02	0.01
101	833.33	4	SLE Q	-117063.00	23240.40	-9487.70	46.00	136.36	0.50	20.00	214.73	3.14	192.79	41.49	0.01	0.00
130	0.00	3	SLE F	-151490.00	41252.40	-16840.90	46.00	136.36	0.50	20.00	183.38	12.57	574.18	213.01	0.06	0.02
131	59.52	3	SLE F	-151645.00	43483.50	-17751.80	46.00	136.36	0.50	20.00	194.72	12.57	645.40	254.66	0.07	0.02
132	119.05	3	SLE F	-150277.00	44809.60	-18293.10	46.00	136.36	0.50	20.00	203.41	12.57	700.01	287.35	0.08	0.03
133	178.57	. 3	SLE F	-148913.00	45363.10	-18519,10	46.00	136,36	0.50	20.00	184.85	15,71	729,23	305.22	0.09	0.03
134	238.09	3	SLE F	-147555.00	45266.30	-18479.60	46.00	136.36	0.50	20.00	186.00	15.71	738.30	309.35	0.09	0.03
135	297,62	3	SLE F	-146201.00	44630.90	-18220.20	46.00	136,36	0.50	20.00	185.20	15.71	731.98	301.70	0.09	0.03
136	357,14	3	SLE F	-144B51.00	43516.80	-17765.40	46.00	136,36	0.50	20.00	205.08	12.57	710.50	283.83	0.08	0.03
137	416.67	3	SLE F	-141353.00	41860.60	-17089.20	46,00	136.36	0.50	20.00	201.88	12,57	690.40	264.27	0.08	0.03
138	476.19	3	SLE F	-137861.00	39748.50	-16227.00	46.00	136.36	0.50	20.00	195.93	12.57	653.02	235.82	0.07	0.02
139	535.71	3	SLE F	-134378.00	37301.70	-15228.10	46.00	136,36	0.50	20.00	187.57	12.57	600.49	202.01	0.06	0.02
140	595.24	3	SLE F	-130901.00	34625.60	-14135.60	46.00	136.36	0.50	20.00	177.12	12.57	534.79	166.00	0.05	0.01
141	654.76	3	SLE F	-127431.00	31810.90	-12986.50	46.00	136.36	0.50	20.00	164.91	12.57	458.09	130.37	0.04	0.01
142	714.29	. 3	SLE F	-123969.00	28934.30	-11812.20	46.00	136.36	0.50	20.00	171.12	9.42	372,83	97.04	0.03	0.01
143	773.81	3	SLE F	-120513.00	26060.00	-10638.80	46.00	136.36	0.50	20.00	181.96	6.28	282.62	67.23	0.02	0.01
144	833.33	3	SLE F	-117063.00	23240.40	-9487.70	46.00	136,36	0.50	20.00	214.73	3,14	192,79	41.49	0.01	0.00

Verifiche principali

Caso	Tipo
5	SLU N cost - min. sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
48	C.Rare - Sf max (max traz.)
-61	C.Rare - Sc max (min. compr.)
89	C.Q.Per Wk Max
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
91	C.Q.Per Sf max (max traz.)
104	C.Q.Per Sc max (min. compr.)
132	C.Freq - Wk Max

Palo n. 8

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmc=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	128535.00	7051.77	657.85	64491.40	10929.70
	1	SLU	TAG	1	<u>4</u> 2	- 1	0.00	0.00
	. 1	SLU	ECC				0.00	0.00
	1	SLU	TOT	128535.00	7051.77	657.85	64491.40	10929.70
2	2	SLE R	RVN	95211.30	5223.53	487.30	47771.40	8096.04
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	95211.30	5223.53	487.30	47771.40	8096.04
3	3	SLE F	RVN	95211.30	5223.53	487.30	47771,40	8096.04
	. 3	SLE F	TAG		A		0.00	0.00
	3	SLE F	ECC				0.00	0.00

L		3	SLE	F	TOT	95211.30	5223.53	487,30	47771.40	8096.04
	4	4	SLE	Q	RVN	95211.30	5223.53	487.30	47771.40	8096.04
Γ		4	SLE	Q	TAG	_			0.00	0.00
		4	SLE	Q	ECC				0.00	0.00
		4	SLE	Q	TOT	95211.30	5223.53	487.30	47771.40	8096.04

Sollecitazioni nei pali

Caso	cc	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
- 1	1	SIAI	- 1	-128535.00	-7051.77	-657.85	-64491.40	-10929.70
2	. 2	SLE R	. 1	-95211.30	-5223.53	-487.30	-47771.40	-8096.04
3	3	SLE F	1	-95211.30	-5223.53	-487.30	-47771.40	-8096.04
4	4	SLE Q	1	-95211.30	-5223.53	-487.30	-47771.40	-8096.04

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm></cm>	cc	200	N	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-128535.00	64234.90	-10886.20	-128535.00	195406.00	-34614,80	2-3	190.00	3.046
2	59,52	1	SIU	-128850.00	67621.20	-11460.10	-128850.00	195522.00	-34638.10	2-3	190.00	2.895
3	119.05	1	SIU	-127800.00	69611.80	-11797.40	-127800.00	195134.00	-34560.20	2-3	190.00	2.807
4	178.57	1	SLU	-126755.00	70411.80	-11933.00	-126755.00	194747.00	-34482.70	2-3	190.00	2.769
5	238.09	1	SLU	-125713.00	70210.10	-11898.80	-125713.00	194361.00	-34405.40	2-3	190.00	2.772
- 6	297.62	1	SIU	-124675.00	69179.20	-11724.10	-124675.00	193976.00	-34328.50	2-3	190.00	2,808
7	357,14	1	SIJ	-123642.00	67412.30	-11424,70	-123642.00	193593.00	-34251.90	2-3	190.00	2,875
8	416.67	1	SLU	-120682.00	64812.50	-10984.10	-120682.00	192491.00	-34030.20	2-3	190.00	2,974
9	476,19	1	SIU	-117729.00	61513.30	-10424.90	-117729.00	191389.00	-33808.60	2+3	190.00	3.115
10	535.71	1	SIJ	-114782.00	57701.70	~9778.97	-114782.00	190289.00	-33587.70	2-3	190.00	3.302
11	595.24	1	SLU	-111841.00	53540.30	-9073.72	-111841.00	189187.00	-33365.60	2-3	190.00	3.538
12	654.76	1	SLU	-108906.00	49168.80	-8332.86	-108906.00	188084.00	-33142.90	2-3	190.00	3.830
13	714,29	1	SLU	-105977.00	44705.40	-7576.43	-105977.00	186983.00	-32920.90	2-3	190.00	4.187
14	773.81	1	SLU	-103054.00	40248.90	-6821.17	-103054.00	185874.00	-32711.50	2-3	190.00	4.623
15	833.33	1	SILI	-100136.00	35880.20	-6080.79	-100136.00	184760.00	-32504.90	2-3	190.00	5.155
16	892.86	1	SLU	-97223.60	31664.20	-5366.28	-97223.60	183650.00	-32299.10	2-3	190.00	5.806
17	952.38	1	SLU	-94316.50	27651.40	-4686.22	-94316.50	182538.00	-32093.00	2-3	190.00	6,608
18	1011.90	1	SLU	-91414.40	23880.00	-4047.05	-91414.40	181423.00	-31885.80	2-3	190.00	7.605
19	1071,43	1	SLU	-88517.10	20376.80	-3453.35	-88517.10	180309,00	-31678.90	2-3	190.00	8.858
20	1130.95	1	SLU	-85624.70	17159.30	-2908.07	-85624.70	179197.00	-31472.40	2-3	190.00	10.454
21	1190.48	1	SLU	-82736.80	14237,00	-2412.81	-82736.80	178083.00	-31265.20	2-3	190.00	12.521
22	1250.00	1	SLU	-79853.40	11612.30	-1968.00	-79853.40	176968.00	-31057.60	2+3	190.00	15,255
23	1309.52	1	SIJ	-76974.20	9282.20	-1573.10	-76974.20	175854.00	-30850.30	2-3	190.00	18.964
24	1369.05	1	SIM	-74099.20	7238.87	-1226.80	-74099.20	174740.00	-30643.10	2-3	190.00	24.163
25	1428,57	1	SIU	-71228,20	5470.89	-927.18	-71228.20	173624,00	-30434.60	2-3	190.00	31.76
26	1488,10	1	SLU	-68360,90	3963.95	-671,79	-2571250.00	172508.00	-30226.40	2-3	190.00	37.613
27	1547.62	1	SIM	-65497.40	2701.56	-457.85	-2571250.00	171392.00	-30018.40	2+3	190.00	39.257
28	1607.14	1	SIU	-62637.30	1665.66	-282.29	-2571250.00	170275.00	-29809.80	2-3	190.00	41.050
29	1666.67	1	SIJ	-59780.70	837.11	-141.87	-2571250.00	169158.00	-29600.60	2-3	190.00	43,011
30	1726.19	1	SIU	-56927.20	196.13	-33.24	-2571250.00	168040.00	-29391.70	2-3	190.00	45.167
31	1785.71	1	SLU	-54076.80	-277.42	47.02	-2571250.00	-166777.00	29587.00	2-3	10.00	47.548
32	1845,24	1	SLU	-51229.20	-603.72	102.31	-2571250.00	-165628.00	29374.90	2-3	10.00	50.191
33	1904.76	1	SLU	-48384.40	-802.85	136.06	-2571250.00	-164479.00	29163.10	2-3	10.00	53.142
34	1964.29	1	SLU	-45542.30	-894.65	151.62	-2571250.00	-163329.00	28950.90	2-3	10.00	56.459
35	2023.81	1	SIJ	-42702.50	-898.63	152.29	-2571250.00	-162175.00	28737.40	2-3	10.00	60.213
36	2083.33	1	SLU	-39865.10	-833.93	141.33	-2571250.00	-161021.00	28524.10	2-3	10.00	64.499
37	2142,86	1	SLU	-37029,80	-719.33	121.91	-2571250.00	-159868.00	28310.90	_	10.00	69.43
38	2202,38	-	SIU	-34196,40	-573.29	97.16	-2571250.00	-158709.00	28095.80	2-3	10.00	75.191
39	2261.90	1	SIJ	-31364.90	-413.96	70.16	-2571250.00	-157551.00	27880.90	2-3	10.00	81,978
40	2321.43	1	SIA	-28535.10	-259.26	43.94	-2571250.00	-156394.00	27666.40	+	10.00	90.108
41	2380.95	1	SIU	-25706.90	-126.95	21.51	-2571250.00	-155231.00	27449.80	2-3	10.00	>100
42	2440,48	1	SIU	-22880.00	-34.67	5.88	-2571250.00	-154068.00	27233.20	2-3	10.00	>100
43	2500,00	1	SLU	-20054.30	0.00	0.00	-2571250.00					>100

Stato limite ultimo - Verifiche a taglio

Caso	X <cm></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7051.77	657.85	0.85	11.31	7082.39	1.00	32294.70	350079.00	32294.70	4.560
2	59,52	1	SLU	4500.94	419.89	0.85	11.31	4520.49	1.00	32294.70	350124,00	32294.70	7.144
- 3	119.05	1	SIJ	2311.56	215.64	0.85	11.31	2321.59	1,00	32294.70	349974.00	32294.70	13.911
.4	178.57	1	SLU	456.44	42.58	0.85	11.31	458.42	1,00	32294.70	349824.00	32294.70	70.448
5	238,09	1	SIU	-1092,11	-101.88	0.85	11.31	1096.86	1.00	32294.70	349675.00	32294.70	29.443
- 6	297.62	1	SLU	-2361.92	-220.34	0.85	11.31	2372.17	1.00	32294.70	349527.00	32294.70	13.614
7	357.14	1	SIJJ	-3700.75	-345.24	0.85	11.31	3716.82	1.00	32294.70	349378.00	32294.70	8.689
8	416.67	1	SIU	-5060.59	-472.10	0.85	11.31	5082.56	1.00	32294.70	348955.00	32294.70	6.354
. 9	476.19	1	SIJ	-6081.44	-567.33	0.85	11.31	6107.85	1.00	32294.70	348531,00	32294.70	5.287
10	535.71	1	SIJ	-6806.07	-634.93	0.85	11.31	6835.62	1.00	32294.70	348109.00	32294.70	4.724

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176	COLUMB CO.	u	Local	ICAL PICA	

								116	1102	OHE UI	Calcolo		
11	595.24	1	SLU	-7274.77	-678.65	0.85	11.31	7306.36	1.00	32294.70	347688.00	32294.70	4.420
12	654.76	1	SLU	-7525.17	-702.01	0.85	11.31	7557.85	1.00	32294.70	347268.00	32294.70	4.273
13	714.29	1	SIU	-7591.98	-708.25	0.85	11.31	7624.94	1.00	32294.70	346848.00	32294.70	4.235
14	773.81	1	SIJJ	-7506.90	-700.31	0.85	11.31	7539.49	1.00	32294.70	346429.00	32294.70	4.283
15	833.33	1	SLU	-7298.63	-680.88	0.85	11.31	7330.32	1.00	32294.70	346032.00	32294.70	4.406
16	892.86	1	SLU	-6992.88	-652,36	0.85	11.31	7023.24	1.00	32294.70	345594.00	32294.70	4.598
17	952.38	1	SLU	-6612.42	-616.86	0.85	11.31	6641.13	1.00	32294.70	345178.00	32294.70	4.863
18	1011.90	1	SIU	-6177.28	-576.27	0.85	11.31	6204,10	1.00	32294.70	344762.00	32294.70	5.205
19	1071.43	1	SLU	-5704.82	-532.20	0.85	11.31	5729.59	1.00	32294.70	344347.00	32294.70	5.636
20	1130.95	1	SIJ	-5209.97	-486.03	0.85	11.31	5232.59	1.00	32294.70	343933.00	32294.70	6.172
21	1190.48	1	SLU	-4705.35	-438.96	0.85	11.31	4725.78	1.00	32294.70	343519.00	32294.70	6.834
22	1250.00	1	SLU	-4201.54	-391.96	0.85	11.31	4219.79	1.00	32294.70	343106.00	32294.70	7.653
23	1309,52	1	SIAJ	-3707.23	-345.84	0.85	11.31	3723.33	1.00	32294.70	342694,00	32294.70	8.674
24	1369.05	-1	SLU	-3229.44	-301.27	0.85	11.31	3243.46	1.00	32294.70	342282,00	32294.70	9.957
25	1428.57	1	SLU	-2773.71	-258.76	0.85	11.31	2785.75	1.00	32294.70	341871.00	32294.70	11.593
26	1488.10	1	SLU	-2344.29	-218.70	0.85	11.31	2354.47	1.00	32294.70	341460.00	32294.70	13.716
-27	1547.62	1	SIJ	-1944.34	-181.38	0.85	11.31	1952.79	1.00	32294.70	341050.00	32294.70	16.538
28	1607.14	1	SLU	-1576.08	-147.03	0.85	11.31	1582.92	1.00	32294.70	340640.00	32294.70	20.402
29	1666.67	1	SLU	-1240.94	-115.77	0.85	11.31	1246.33	1.00	32294.70	340231.00	32294.70	25.912
30	1726.19	1	SIU	-939.74	-87.67	0.85	11.31	943.82	1.00	32294.70	339822.00	32294.70	34,217
31	1785.71	1	SLU	-672.80	-62.76	0.85	11.31	675.72	1.00	32294.70	339414.00	32294.70	47.793
32	1845.24	1	SIJJ	-440.07	-41.05	0.85	11.31	441.99	1.00	32294.70	339006.00	32294.70	73.067
33	1904.76	1	SLU	-241.23	-22.50	0.85	11.31	242.28	1.00	32294.70	338599.00	32294.70	>100
34	1964.29	1	SIJ	-75.78	-7.07	0.85	11.31	76.11	1.00	32294.70	338192.00	32294.70	>100
35	2023.81	1	SIU	56.88	5.31	0.85	11,31	57,12	1.00	32294.70	337785.00	32294.70	>100
36	2083.33	1	SLU	157.36	14.68	0.85	11.31	158.04	1.00	32294.70	337378.00	32294.70	>100
37	2142.86	1	SLU	226.27	21.11	0.85	11.31	227.25	1.00	32294.70	336972.00	32294.70	>100
38	2202.38	1	SLU	264.14	24.64	0.85	11.31	265.29	1.00	32294.70	336566.00	32294.70	>100
39	2261.90	1	SIAI	271.43	25.32	0.85	11.31	272.61	1.00	32294.70	336161.00	32294.70	>100
40	2321,43	1	SIJ	248,47	23.18	0.85	11.31	249.55	1.00	32294.70	335755.00	32294.70	>100
41	2380.95	1	SLU	195.50	18.24	0.85	11.31	196.35	1,00	32294.70	335350.00	32294.70	>100
42	2440.48	1	SIU	112.66	10.51	0.85	11.31	113.15	1.00	32294.70	334945.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <dann></dann>	AfT <cmq></cmq>	AfC <mq></mq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-95211.30	-8063.85	47581.40	40.84	37.70	43,41	644.35
45	59,52	2	SLE R	-95757,60	-8488.95	50089.80	40.84	37.70	46.02	719.99
46	119.05	2	SLE R	-95170.20	-8738.84	51564.30	43.98	34.56	47.62	774.10
47	178.57	2	SLE R	-94585.90	-8839.27	52156.90	43.98	34.56	48.29	799.57
48	238.09	2	SLE R	-94004.40	-8813.95	52007.50	43.98	34.56	48,17	B00.37
49	297.62	2	SLE R	-93426.00	-8684.53	51243.80	43.98	34.56	47.41	780.65
50	357.14	2	SLE R	-92850.40	-B462.72	49935.00	43.98	34.56	46.06	742.92
51	416.67	2	SLE R	-90673.20	-8136.35	48009.20	40.84	37.70	44.18	700.67
52	476,19	2	SLE R	-88500.80	-7722.17	45565.40	40.84	37.70	41.76	641.80
53	535.71	2	SLE R	-86333.20	-7243.68	42742.00	37.70	40.84	38,94	571.50
54	595.24	2	SLE R	-84170.30	-6721.28	39659.50	37.70	40.84	35.85	494.55
55	654.76	2	SLE R	-82011.80	-6172.49	36421.30	37.70	40.84	32.62	449.66
56	714.29	2	SLE R	-79857.70	-5612.17	33115.10	37.70	40.84	29.35	406.21
57	773.81	2	SLE R	-77707.90	-5052.72	29814.00	37.70	40.84	26.15	363.44
58	833.33	2	SLE R	-75562.30	-4504.29	26577.90	31.42	47.12	23.09	322.50
59	892.86	2	SLE R	-73420.80	-3975.02	23455.00	31.42	47.12	20.26	284.40
60	952.38	2	SLE R	-71283.20	-3471.27	20482.60	28.27	50.27	17.72	249.92
61	1011,90	2	SLE R	-69149.40	-2997.81	17688.90	25.13	53.41	15.49	219.52
62	1071.43	2	SLE R	-67019.30	-2558.03	15093.90	18.85	59.69	13,58	193.27
63	1130.95	2	SLE R	-64892.80	-2154.13	12710.60	12.57	65.97	11.95	170.89
64	1190.48	2	SLE R	-62769.80	-1787.27	10545.90	0.00	78.54	10.58	151.87
65	1250.00	2	SLE R	-60650.10	-1457.77	8601.73	0.00	78.54	9.40	135.35
- 55	1309.52	2	SLE R	-58533.70	-1165.26	6875.70	0.00	78.54	8.33	120.45
67	1369.05	2	SLE R	-56420.50	-908.74	5362.12	0.00	78.54	7.37	107.07
68	1428.57	2	SLE R	-54310.20	-686.80	4052.51	0.00	78.54	6.52	95.14
69	1488,10	2	SLE B	-52202.90	-497.62	2936.26	0.00	78.54	5.77	84.61
70	1547.62	2	SLE R	-50098.40	-339.14	2001.15	0.00	78.54	5.11	75.37
71	1607.14	2	SLE R	-47996.60	-209,10	1233.82	0.00	78.54	4.54	67.33
72	1666.67	2	SLE R	-45897.30	-105.09	620.08	0.00	78.54	4.05	60.39
7.3	1726,19	2	SLE R	-43800.50	-24.62	145.28	0.00	78.54	3.64	54.44
74	1785,71	2	SLE R	-41706.10	34,83	-205.50	0.00	78,54	3,50	52,31
75	1845.24	2	SLE R	-39613.90	75.79	-447.20	0.00	78.54	3.45	51.47
76	1904.76	2	SLE R	-37523.80	100.79	-594.71	0.00	78.54	3,36	49.97
77	1964.29	2	SLE R	-35435.80	112.31	-662.71	0.00	78.54	3.22	47.91
78	2023.81	2	SLE R	-33349.60	112.81	-665.65	0.00	78.54	3.06	45.39
79	2083,33	2	SLE R	-31265.20	104.69	-617.72	0.00	78.54	2.86	42.51
80	2142,86	2	SLE R	-29182.50	90,30	-532.84	0.00	78.54	2,65	39,36
81	2202.38	2	SLE R	-27101.40	71.97	-424.66	0.00	78,54	2.42	36.00
82	2261.90	2	SLE R	-25021.70	51.97	-306.64	0.00	78.54	2.19	32.68
83	2321,43	2	SLE R	-22943.30	32,55	-192.05	0.00	78.54	1.96	29.34
84	2380.95	2	SLE R	-20866.20	15.94	-94.04	0.00	78.54	1.74	26.11

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85	2440.48	2	SLE	R	-18790.20	4.35	-25.68	0.00	78.54	1.54	23.09
86	2500.00	2	SLE	R	-16715.30	0.00	0.00	0.00	78.54	1.36	20.38
87	0.00	â	SLE	Q	-95211.30	-8063.85	47581.40	40.84	37.70	43.41	644.35
88	59.52	4	SLE	Q	-95757.60	-8488.95	50089.80	40.84	37.70	46.02	719.99
89	119.05	4	SLE	Q	-95170.20	-8738.84	51564.30	43.98	34.56	47.62	774.10
90	178.57	4	SLE	Q	-94585.90	-8839.27	52156.90	43.98	34.56	48.29	799.57
91	238.09	4	SLE	Q	-94004.40	-8813.95	52007.50	43.98	34,56	48.17	800.37
92	297.62	4	SLE	Q	-93426.00	-8684.53	51243.80	43.98	34.56	47.41	780.65
93	357.14	4	SLE	Q	-92850.40	-8462.72	49935.00	43.98	34.56	46.06	742.92
94	416,67	4	SLE	Q	-90673.20	-8136.35	48009.20	40.84	37.70	44.18	700.67
95	476.19	4	SLE	Q	-88500.80	-7722.17	45565.40	40.84	37.70	41.76	641.80
96	535.71	4	SLE	Q	-86333.20	-7243.6B	42742.00	37.70	40.84	38.94	571.50
97	595,24	4	SLE	Q	-84170.30	-6721.28	39659.50	37.70	40.84	35.85	494.55
98	654.76	4	SLE	Q	-82011.80	-6172,49	36421.30	37.70	40.84	32.62	449.66
99	714.29	4	SLE	Q	-79857.70	-5612.17	33115.10	37.70	40.84	29.35	406.21
100	773.81	4	SLE	Q	-77707.90	-5052.72	29814.00	37.70	40.84	26.15	363.44
101	833.33	4	SLE	Q	-75562.30	-4504.29	26577.90	31.42	47.12	23.09	322.50
102	892.86	4	SLE	Q	-73420.80	-3975.02	23455.00	31.42	47.12	20.26	284.40
103	952.38	4	SLE	Q	-71283.20	-3471.27	20482.60	28.27	50.27	17,72	249.92
104	1011.90	4	SLE	Q	-69149.40	-2997.81	17688.90	25.13	53.41	15.49	219,52
105	1071.43	4	SLE	Q	-67019.30	-2558.03	15093.90	18.85	59.69	13.58	193.27
106	1130.95	4	SLE	Q	-64892.80	-2154.13	12710.60	12.57	65.97	11.95	170.89
107	1190.48	4	SLE	Q	-62769.80	-1787.27	10545.90	0.00	7B.54	10.58	151.87
108	1250.00	4	SLE	Q	-60650.10	-1457.77	8601.73	0.00	78.54	9.40	135.35
109	1309,52	4	SLE	Q	-58533.70	-1165.26	6875.70	0.00	78,54	8.33	120.45
110	1369.05	4	SIE	Q	-56420.50	-908.74	5362.12	0.00	78.54	7,37	107.07
111	1428.57	- 6	SLE	Q	-54310.20	-686.80	4052.51	0.00	78.54	6.52	95.14
112	1488.10	4	SLE	Q	-52202.90	-497.62	2936.26	0.00	78.54	5.77	84.61
113	1547.62	4	SLE	Q	-50098.40	-339.14	2001.15	0.00	78.54	5.11	75.37
114	1607,14	4	SLE	Q	-47996.60	-209,10	1233.82	0.00	78.54	4.54	67.33
115	1666.67	4	SLE	Q	-45897.30	-105.09	620.08	0.00	78.54	4.05	60.39
116	1726,19	4	SIE	Ω	-43800.50	-24.62	145.28	0.00	78.54	3.64	54.44
117	1785.71	4	SLE	Q	-41706.10	34.83	-205.50	0.00	78.54	3.50	52.31
118	1845,24	4	SLE	0	-39613.90	75.79	-447.20	0.00	78.54	3.45	51.47
119	1904.76	- 4	SIE	Q	-37523.80	100.79	-594.71	0.00	78.54	3.36	49.97
120	1964.29	4	SLE	Q	-35435.80	112,31	-662.71	0.00	78.54	3.22	47.91
121	2023.81	4	SLE	Q	-33349.60	112.81	-665.65	0.00	78.54	3.06	45.39
122	2083.33	4	SIE	Q	-31265.20	104.69	-617.72	0.00	78.54	2.86	42.51
123	2142.86	4	SLE	Q	-29182.50	90.30	-532.84	0.00	78.54	2,65	39.36
124	2202.38	4	SLE	Q	-27101.40	71.97	-424.66	0.00	78.54	2,42	36.06
125	2261.90	4	SLE	Q	-25021.70	51.97	-306.64	0.00	78.54	2.19	32.68
126	2321.43	9	SLE	Q	-22943.30	32.55	-192.05	0.00	78.54	1.96	29.34
127	2380.95	4	SLE	Q	-20866.20	15.94	-94.04	0.00	78.54	1.74	26,11
128	2440.48	4	SLE	Q	-18790.20	4.35	-25.68	0.00	78.54	1.54	23.09
129	2500.00	4	SLE	Q	-16715.30	0.00	0.00	0.00	78.54	1,36	20.38

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	•eq	Δ _{HM}	A _B	Ac eff <cmq></cmq>	σ _S <dan cmq=""></dan>	e _{am.}	Wk <mm></mm>
8.7	0.00	4	SLE C	-95211.30	47581.40	-8063.85	46.00	136.36	0.50	20.00	206.15	18.85	1075.84	644.35	0.19	0.07
88	59.52	4	SIE C	-95757.60	50089.80	-8488.95	46.00	136.36	0.50	20.00	208.37	18.85	1096.75	719.99	0.21	0.07
89	119.05	4	SLE Ç	-95170.20	51564.30	-8738.84	46.00	136.36	0.50	20.00	209.96	18.85	1111.71	774.10	0.23	0.08
90	178.57	4	SLE Ç	-94585.90	52156.90	-8839.27	46.00	136.36	0.50	20.00	210.71	18.85	1118.85	799.57	0.23	0.08
91	238.09	4	SLE C	-94004.40	52007,50	-8813.95	46.00	136.36	0.50	20.00	210.85	18.85	1120.16	800.37	0.23	0.08
92	297.62	4	SLE C	-93426.00	51243.80	-B684.53	46.00	136.36	0.50	20.00	210.49	18.85	1116.71	780.65	0.23	0.08
93	357.14	4	SLE Q	-92850.40	49935.00	-8462.72	46.00	136.36	0.50	20.00	209.63	18.85	1108,63	742.92	0.22	0.08
94	416.67	4	SLE C	-90673.20	48009.20	-8136.35	46.00	136.36	0.50	20.00	208.93	18.85	1102.02	700.67	0.20	0.07
95	476.19	4	SLE C	-88500.80	45565.40	-7722.17	46.00	136.36	0.50	20,00	207.62	18.85	1089.68	641.80	0.19	0.07
96	535.71	4	SLE C	-86333.20	42742.00	-7243.68	46.00	135.36	0.50	20.00	205.67	18.85	1071.33	571.50	0.17	0.06
97	595.24	4	SLE C	-84170.30	39659.50	-6721.28	46.00	136.36	0.50	20.00	203.01	18.85	1046.21	494.55	0.14	0.05
98	654.76	4	SLE C	-82011.80	36421.30	-6172.49	46.00	136.36	0.50	20.00	199.50	18.85	1013.12	415.24	0.12	0.04
99	714.29	4	SLE C	-79857.70	33115.10	-5612.17	46.00	136.36	0.50	20.00	194.94	18.85	970.20	337.39	0.10	0.03
100	773.81	4	SLE C	-77707.90	29814.00	-5052.72	46.00	136.36	0.50	20,00	188.82	18.85	912.47	264,34	0.08	0.02
101	833.33	4	SLE C	-75562.30	26577.90	-4504.29	46.00	136.36	0.50	20.00	198.27	15.71	834.64	198.79	0.06	0.02
102	892.86	4	SLE Ç	-73420.80	23455.00	-3975.02	46.00	136.36	0.50	20.00	208.35	12.57	731.06	142.58	0.04	0.01
103	952.38	4	SLE C	-71283.20	20482.60	-3471.27	46.00	136.36	0.50	20.00	184.94	12.57	583.99	96.54	0.03	0.01
104	1011,90	4	SLE Q	-69149.40	17688.90	-2997.81	46.00	136,36	0.50	20,00	160.53	12.57	430.57	60.47	0.02	0.00
105	1071.43	4	SLE C	-67019.30	15093.90	-2558.03	46.00	136,36	0.50	20.00	180.29	6.28	277.39	33.22	0.01	0.00
130	0.00	3	SLE F	-95211.30	47581.40	-8063.85	46.00	136,36	0.50	20,00	206.15	18.85	1075.84	644.35	0.19	0.07
131	59.52	3	SLE F	-95757.60	50089.80	-B488.95	46.00	136.36	0.50	20.00	208.37	18.85	1096.75	719.99	0.21	0.07
132	119.05	3	SLE F	-95170.20	51564.30	-8738.84	46.00	136.36	0.50	20.00	209.96	18.85	1111.71	774.10	0.23	0.08
133	178,57	3	SLE F	-94585.90	52156.90	-BB39.27	46.00	136,36	0.50	20.00	210.71	18.85	1118.85	799.57	0.23	0.08
134	238.09	-3	SLE F	-94004.40	52007,50	-8813.95	46.00	136.36	0.50	20,00	210,85	18.85	1120.16	800.37	0.23	0.08
135	297.62	3	SLE F	-93426.00	51243.80	-8684.53	46.00	136.36	0.50	20.00	210.49	18.85	1116.71	780.65	0.23	0.08
136	357.14	3	SLE F	-92850.40	49935.00	-8462.72	46.00	136.36	0.50	20,00	209.63	18.85	1108,63	742.92	0.22	0.08
137	416.67	3	SLE F	-90673.20	48009.20	-8136.35	46.00	136.36	0.50	20,00	208.93	18,85	1102.02	700.67	0.20	0.07
138	476.19	3	SLE F	-88500.80	45565.40	-7722.17	46.00	136.36	0.50	20,00	207.62	18.85	1089.68	641.80	0.19	0.07

139	535.71	3	SLE I	-86333.	20 42742.00	-7243.68	46.00	136.36	0.50	20.00	205.67	18.85	1071.33	571.50	0.17	0.06
140	595.24	3	SLE 3	-84170.	30 39659.50	-6721.28	46.00	136.36	0.50	20.00	203.01	18.85	1046.21	494.55	0.14	0.05
141	654.76	3	SLE I	F-82011.	80 36421.30	-6172.49	46.00	136.36	0.50	20.00	199.50	18,85	1013.12	415.24	0.12	0.04
142	714,29	93	SIE I	F-79857.	70 33115.10	-5612.17	46.00	136.36	0.50	20,00	194.94	18.85	970.20	337,39	0.10	0.03
143	773.81	177	SLE	-77707.	90 29814.00	-5052.72	46.00	136.36	0.50	20.00	188.82	18,85	912.47	264.34	0.08	0.02
144	833.33	3	SLE !	-75562.	30 26577.90	-4504.29	46.00	136.36	0.50	20.00	198.27	15.71	834.64	198.79	0.06	0.02
145	892.86	3	SLE I	73420.	80 23455.00	-3975.02	46.00	136.36	0.50	20.00	208.35	12.57	731,06	142,58	0.04	0.01
146	952,38	613	SLE :	-71283.	20 20482.60	-3471.27	46.00	136,36	0.50	20,00	184.94	12.57	583.99	96.54	0.03	0.01
147	1011.90	_			40 17688.90									60.47	0.02	0.00
148	1071.43	101	SLE !	F-67019.	30 15093.90	-2558.03	46.00	136,36	0.50	20.00	180.29	6.28	277.39	33.22	0.01	0.00

Verifiche principali

Caso	Tipo
4	SLU N cost - min. sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
48	C.Rare - Sf max (max traz.)
65	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
91	C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
108	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 9

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <om>></om>	Cls	Fck <dan cmq=""></dan>	Fetk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 9 (-23)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	BVN	70710.80	7354.68	387.35	62440.60	2004.95
	1	SLU	TAG				0.00	0.00
	1	SIAI	ECC				0.00	0.00
	1	SLU	TOT	70710.80	7354.68	387.35	62440.60	2004.99
2	2	SLE R	RVN	52378,40	5447.91	286.93	46252.30	1485,15
	2	SLE R	TAG			5 3	0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	52378.40	5447.91	286.93	46252.30	1485.19
- 3	3	SLE F	RVN	52378.40	5447.91	286,93	46252.30	1485.15
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	52378.40	5447.91	286.93	46252.30	1485.19
4	4	SLE Q	RVN	52378.40	5447.91	286,93	46252.30	1485.15
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00
	6	SLE Q	TOT	52378.40	5447.91	286.93	46252.30	1485.15

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
- 1	1	SIAT	1	-70710.80	-7354.68	-387.35	-62440.60	-2004.95
2	2	SLE R	1	-52378.40	-5447.91	-286.93	-46252.30	-1485.15
3	3	SLE F	1	-52378.40	-5447,91	-286,93	-46252.30	-1485.15
4	4	SIE Q	1	-92378.40	-5447.91	-286.93	-46252.30	-1485.15

Da 0 a -25

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SIU	-70710.80	62183.00	-1996.68	-70710.80	176095.00	-4472.43	2-3	181.25	2.831
	59.52	1	SIAI	-71427.40	65791.50	-2112.55	-71427.40	176385.00	-4485.54	2-3	181.25	2.680
3	119.05	1	SLU	-71179.90	67997.60	-2183.39	-71179.90	176285.00	-4481.01	2-3	181.25	2,592
4	178,57	1	SIU	-70934.60	69005.00	-2215.74	-70934.60	176186.00	-4476.52	2-3	181.25	2.553

-	La Companio de Com	T- 100	CONTRACTOR IN	NAME OF TAXABLE PARTY.
RO	azione	10 0	COL	COLO
1/6	ICIZI OI R	3 UI	Gai	COIO

							Relaz	ione ai c	alcolo			
5	238.09	1	SLU	-70691.50	69001.70	-2215.63	-70691.50	176087.00	-4472.08	2-3	181.25	2,551
6	297.62	1	SIJ	-70450.60	68159.40	-2188.59	-70450.60	175990.00	-4467.6B	2-3	181.25	2.582
7	357.14	1	SIU	-70212.00	66570.00	-2137.55	-70212.00	175894.00	-4463.32	2-3	181.25	2.642
8	416.67	1	SIJJ	-68610.10	64131.80	-2059.26	-68610.10	175246.00	-4434.12	2-3	181.25	2.732
9	476.19	1	SLU	-67011.90	60977.10	-1957.96	-67011.90	174599.00	-4405.09	2-3	181.25	2.863
10	535.71	1	SIU	-65417.30	57293.50	-1839.68	-65417.30	173954.00	-4376.22	2-3	181.25	3.036
11	595,24	1	SIU	-63826.20	53244.20	-1709.66	-63826.20	173309.00	-4347.52	2-3	181.25	3.254
12	654.76	Ĭ	SIU	-62238.50	48969.80	-1572,41	-62238.50	172663.00	-4318.01	2-3	181,25	3,525
13	714.29	1	SLU	-60654.20	44589.40	-1431.76	-60654.20	172018.00	~4288.54	2-3	181.25	3.857
14	773.81	1	SIJ	-59073.10	40202.90	-1290.91	-59073,10	171373.00	-4259.23	2-3	181.25	4.262
15	833.33	1	SLU	-57495.20	35892.20	-1152.49	-57495.20	170730.00	-4230.08	2-3	181.25	4.756
16	892.86	1	SLU	-55920.40	31723.30	-1018.63	-55920.40	170088.00	-4201.09	2-3	181.25	5.360
17	952.38	1	SIAJ	-54348.60	27747.90	-890.98	-54348.60	169446.00	-4171,98	2-3	181.25	6.105
18	1011.90	1	SLU	-52779,60	24005.10	-770.80	-52779.60	168802.00	-4142.15	2-3	181.25	7.030
19	1071.43	1	SLU	-51213.60	20522.90	-658.99	-51213.60	168159.00	~4112.48	2-3	181.25	8.192
20	1130.95	1	SLU	-49650.20	17319.70	-556.13	-49650.20	167518.00	-4082.97	2-3	181,25	9.670
-21	1190,48	1	SIJ	-48089.50	14405.90	-462.57	-48089.50	166877.00	-4053.62	2-3	181.25	11.581
22	1250.00	1	SLU	-46531.40	11784.90	-378.41	-46531.40	166234.00	-4016.93	2-3	181.25	14.102
23	1309,52	1	SLU	-44975.90	9454.29	-303.57	-44975.90	165590.00	-3978.02	2-3	181.25	17.511
24	1369.05	1	SLU	-43422.70	7407.10	-237.84	-43422.70	164944.00	-3938.33	2-3	181,25	22.263
25	1428.57	1	SLU	-41871.80	5632.52	-180.86	-41871.80	164300.00	-3898.87	2-3	181.25	29.163
26	1488.10	1	SIJJ	-40323,20	4116.83	-132.19	-40323.20	163657.00	-3859.63	2-3	181.25	39.744
27	1547.62	1	SLU	-38776.80	2844.08	-91.32	-38776.80	163014.00	-3820.61	2-3	181.25	57.303
28	1607.14	1	SLU	-37232.40	1796.65	-57.69	-2571250.00	162323.00	-5506.68	2-3	181.88	69.059
29	1666.67	1	SIU	-35690,00	955.82	-30.69	-2571250.00	161680.00	-5464.62	2-3	181.88	72.044
30	1726.19	1	SLU	-34149.60	302.15	-9.70	-2571250.00	161035.00	-5422.01	2-3	181.88	75.294
31	1785.71	1	SLU	-32610.90	-184.18	5.91	-2571250.00	-160534.00	4953.45	2-3	1.88	78.846
32	1845.24	1	SLU	-31074.10	-523.10	16.80	-2571250.00	-159891.00	4983.14	2-3	1.88	82.746
33	1904.76	1	SIJ	-29538.80	-734.47	23.58	-2571250.00	-159250.00	5012.47	2-3	1.88	87.046
34	1964.29	1	SIJ	-28005.20	-837.91	26.91	-2571250.00	-158609.00	5041,43	2-3	1.88	91,813
35	2023.81	1	SLU	-26473.10	-852.78	27.38	-2571250.00	-157968.00	5070.03	2-3	1.88	97,127
36	2083.33	1	SLU	-24942.40	~798.08	25.63	-2571250.00	-157328.00	5098.29	2-3	1.88	>100
37	2142.86	1	SIU	-23413.00	-692.47	22.23	-2571250.00	-156685.00	5130.22	2-3	1.88	>100
38	2202.38	1	SLU	-21884.90	-554.28	17.80	-2571250.00	-156043.00	5162.08	2-3	1.88	>100
39	2261.90	1	SLU	-20358.00	-401.57	12.89	-2571250.00	-155401.00	5193.57	2-3	1.88	>100
40	2321.43	1	SW	-18832,10	-252.17	8.10	-2571250.00	-154759.00	5224.69	2-3	1.88	>100
41	2380.95	1	SLU	-17307.30	-123.74	3.97	-2571250.00	-154118.00	5255.44	2-3	1.88	>100
42	2440.48	1	SILI	-15783.40	-33.85	1.09	-2571250.00	-153476.00	5285.86	2-3	1.88	>100
43	2500.00	1	SIJ	-14260.30	0.00	0.00	-2571250.00	93		8		>100

Stato limite ultimo - Verifiche a taglio

Caso	X <cm></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIJ	7354.68	387.35	0.85	11.31	7364.87	1.00	32294.70	341797,00	32294.70	4.385
2	59.52	1	SIU	4820.90	253.90	0.85	11.31	4827.58	1.00	32294.70	341899.00	32294.70	6.690
- 3	119.05	1	SLU	2642.18	139.16	0.85	11,31	2645.84	1.00	32294.70	341864.00	32294.70	12,200
4	178.57	1	SLU	792.31	41.73	0.85	11.31	793.41	1.00	32294.70	341829.00	32294.70	40.704
- 5	238.09	1	SLU	-755.53	-39.79	0.85	11.31	756.58	1,00	32294.70	341794.00	32294.70	42.685
.6	297.62	1	SLU	-2028.35	-106.83	0.85	11.31	2031.16	1.00	32294.70	341759.00	32294.70	15.900
7	357.14	1	SIJ	-3375.81	-177.79	0.85	11.31	3380.49	1.00	32294.70	341725.00	32294.70	9.553
8	416.67	1	SLU	-4749.98	-250.17	0.85	11.31	4756.56	1,00	32294.70	341496.00	32294.70	6.790
.9	476,19	1	SLU	-5788.20	-304.85	0.85	11.31	5796.22	1.00	32294.70	341267.00	32294.70	5.572
10	535.71	1	SIU	-6532,37	-344.04	0.85	11.31	6541.43	1.00	32294.70	34103B.00	32294.70	4.937
11	595.24	1	SLU	-7022.07	-369.83	0.85	11.31	7031.80	1.00	32294.70	340811.00	32294.70	4.593
12	654.76	1	SLU	-7294.26	-384.17	0.85	11.31	7304.37	1.00	32294.70	340583.00	32294.70	4.423
13	714.29	1	SIU	-7383.14	-388.85	0.85	11.31	7393.37	1.00	32294.70	340356.00	32294.70	4.368
14	773.81	1	SIU	-7319.96	-385.52	0.85	11.31	7330.10	1.00	32294.70	340130.00	32294.70	4.404
15	833.33	1	SLU	-7133.07	-375.68	0.85	11.31	7142.95	1.00	32294.70	339904.00	32294.70	4.523
16	892.86	1	SLU	-6847.88	-360.66	0.85	11,31	6857.37	1.00	32294.70	339678.00	32294.70	4,709
17	952.38	1	SLU	-6486.96	-341.65	0.85	11.31	6495.96	1.00	32294.70	339453.00	32294.70	4.972
18	1011.90	1	SLU	-6070.18	-319.70	0.85	11.31	6078.59	1.00	32294.70	339228.00	32294.70	5.313
19	1071.43	1	SLU	-5614.78	-295.71	0.85	11.31	5622.56	1.00	32294.70	339004.00	32294.70	5.74
20	1130.95	1	SIJ	-5135.62	-270.48	0.85	11.31	5142.74	1.00	32294.70	338780.00	32294.70	6.280
21	1190.48	1	SLU	-4645.31	-244.66	0.85	11.31	4651.74	1.00	32294.70	338556.00	32294,70	6.942
22	1250.00	1	SLU	-4154.40	-218.80	0.85	11.31	4160.16	1.00	32294.70	338333.00	32294.70	7.763
23	1309.52	1	SLU	-3671.63	-193.37	0.85	11.31	3676.72	1.00	32294.70	338110.00	32294.70	8.784
24	1369.05	1	SIJ	-3204.04	-168.75	0.85	11.31	3208.48	1.00	32294.70	337888.00	32294.70	10.069
25	1428.57	1	SEU	-2757.23	-145.22	0.85	11.31	2761.05	1.00	32294.70	337666.00	32294.70	11.69
26	1488.10	1	SLU	-2335,53	-123.01	0.85	11.31	2338.77	1.00	32294.70	337444.00	32294.70	13.808
27	1547.62	1	SLU	-1942.16	-102.29	0.85	11.31	1944.85	1.00	32294.70	337222.00	32294.70	16.605
28	1607.14	1	SLU	-1579.40	-83.18	0.85	11.31	1581.59	1.00	32294.70	337001.00	32294.70	20.419
29	1666.67	1	SLU	-1248.79	-65.77	0.85	11.31	1250.52	1.00	32294.70	336780.00	32294.70	25.825
30	1726.19	1	SIA	-951.20	-50.10	0.85	11.31	952.52	1.00	32294.70	336560.00	32294.70	33.905
31	1785.71	1	SLU	-687.04	-36.18	0.85	11.31	687.99	1,00	32294.70	336339.00	32294.70	46.941
32	1845.24	1	SIU	-456,31	-24.03	0.85	11.31	456.94	1.00	32294.70	336119.00	32294.70	70.676
33	1904.76	1	SLU	-258.75	-13.63	0.85	11.31	259.11	1.00	32294.70	335899,00	32294.70	>100
34	1964.29	1	SLU	-93.93	-4.95	0.85	11.31	94.06	1.00	32294.70	335680.00	32294.70	>100

35	2023.81	1	SLU	38.70	2.04	0.85	11.31	38.75	1.00	32294.70	335460.00	32294.70	>100
36	2083,33	1	SLU	139.72	7.36	0.85	11.31	139.91	1.00	32294.70	335241.00	32294.70	>100
37	2142.86	1	SIU	209.71	11.04	0.85	11,31	210.00	1.00	32294.70	335022.00	32294.70	>100
38	2202.38	1	SIAJ	249.16	13.12	0.85	11.31	249.51	1.00	32294.70	334803.00	32294.70	>100
39	2261.90	1	SLU	258.51	13.62	0.85	11.31	258.87	1.00	32294.70	334584.00	32294.70	>100
40	2321.43	1	SLU	238.10	12.54	0.85	11.31	238.43	1.00	32294.70	334366.00	32294.70	>100
41	2380.95	1	SLU	188.13	9.91	0.85	11.31	188.39	1.00	32294.70	334147.00	32294.70	>100
42	2440.48	1	SLU	108.75	5.73	0.85	11.31	108.90	1.00	32294.70	333929.00	32294.70	>100

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <dann></dann>	AfT <cmq></cmq>	AfC <mq></mq>	σ ₀ <dan cmq=""></dan>	σ _f <dan cmq<="" th=""></dan>
44	0.00	2	SLE R	-52378,40	-1479.02	46061.50	47.12	31.42	44,80	1037.8
45	59,52	2	SLE B	-53222,40	-1564.85	48734,50	47.12	31,42	47.55	1125.4
46	119.05	2			-1617.33	50368.60	47,12	31.42	49,26	1185.5
47	178.57	2	SLE R		-1641.29	51114.80	47.12	31.42	50.03	1212.9
48	238.09	-	SLE R		-1641.21	51112.30	47.12	31.42	50.03	
50	297.62	2	SLE R	-53259.40 -53272.90	-1621.17 -1583.37	50488.50	47.12	31.42	49,38 48,15	1189.5
51	416.67	_	SLE R		-	47505.00	-	31.42	46.33	1094.2
52	476.19	2	SLE R			45168.20	_	_	43.96	1023.0
53	535.71	2	SLE R	-49767.00	-1362.73	42439.60	47.12	31.42	41.18	937.6
54	595.24	2	SLE R	-48603.80	-1266.42	39440.20	47.12	31.42	38.10	842.7
55	654.76	2	SLE R	-47443.30	-1164.75	36273.90	47.12	31.42	34.85	742.2
56	714,29	2	SLE R			33029,20	43.98		31,50	639.7
57	773.81	2	SLE R	-	-956.23	29779.90	43.98		28.14	538.3
58	833.33	_	SLE R		-853.70 -754.54	26586.80	_	-	24.84	440.7
60	952.38	2	SLE R	-42825.80 -41677.30	-659.99	-	40.84	-	21.64 18.61	349.10 265.9
61	1011.90	2	SLE R	-40531.00	-570.96			40.84	15.80	215.1
62	1071.43	2	SLE R	-39387.00	-488.14			43.98	13.26	182.0
63	1130.95	_	SLE R		-411.95			47.12	11.04	152.8
64	1190.48	2	SLE R	-37105.10	-342.65	10671.10	28.27	50.27	9.18	128.2
65	1250.00	2	SLE R	-35967.20	-280.30	8729.56	21.99	56.55	7.68	108.1
66	1309.52	2	SLE R	-34831.20	-224.87	7003.18	15.71	62.83	6.51	92.2
67	1369.05	2	SLE R	-33697.10	-176.18	and the same of the same of	0.00	-	5.58	79.5
68	1428.57	2	SLE R	-32564.80	-133.97	4172.24	0.00		4,81	68.9
70	1488.10	2	SLE R		-97.92	3049.51			4.13	59.7
71	1547.62	-	SLE R	-30305.30 -29178.10	-67.65 -42.73			78.54	3.55	51.7
72	1666.67	2	SLE R	-28052.40	-22.73		0.00		2,65	39.1
73	1726.19	2	SLE R		-7.19		_	78.54	2.30	34.4
74	1785.71	2	SLE R	-25805.50	4.38		0.00	-	2.17	32,4
75	1845,24	2	SLE R	-24684.10	12.44	-387.48	0.00	78.54	2,21	32.83
76	1904.76	2	SLE R	-23564.10	17.47	-544.05	0.00	78.54	2.20	32.5
77	1964.29	2	SLE R	-22445.30	19.93	-620.68	0.00	78.54	2.15	31.7
78	2023.81	2	SLE R	-21327.80	20.28		_	78.54	2,06	30.4
79	2083.33	2	SLE R	-20211.40	18.98		_	78.54	1.95	28.8
80	2142,86	2	SLE R		16,47		0.00	_	1.82	26.8
81	2202.38	2	SLE R	-17981.70 -16868.40	13.18 9.55		0.00		1.67	24.8
83	2321.43	2	SLE R	-15755.90	6.00		0.00		1.38	20.5
_		_		-14644.30						
_		_		-13533.50		-25.07				
86	2500.00	2	SLE R	-12423.50	0.00	0.00	0.00	78.54	1.01	15.1
87	0.00	4	SLE Q	-52378.40	-1479.02	46061.50	47.12	31.42	44.80	1037.8
88		_		-53222.40					47.55	
89		_		-53229.20					49.26	
90		_		-53237.60					50.03	
91				-53247.70 -53259.40					50.03 49.38	
93				-53272.90					48.15	
94				-52101.50					46.33	
95				-50932.90						
96				-49767.00					41.18	
97	595.24	4	SLE Q	-48603.80	-1266.42	39440.20	47.12	31.42	38,10	842.7
98				-47443.30					34.85	742.2
99				-46285.20						
100				-45129.70						
101				-43976.50						
102				-42825.80						
THE RESERVE TO SHAPE THE PERSON NAMED IN	952,38			-41677.30 -40531.00						265.9 215.1
_	1071.43	_		-39387.00						
_	1130.95			-38245.00					11.04	
	1190.48	_		-37105.10					9.18	
_	1250.00	_		-35967.20						

					110	Hazioi	ic ui caic	OIO
109 1309,52	4 SLE	Q-34831.20	-224.87	7003.18	15.71	62.83	6.51	92.21
110 1369.05	4 SLE	Q-33697.10	-176.18	5486.74	0.00	78.54	5.58	79.56
111 1428.57	4 SLE	Q -32564.80	-133.97	4172.24	0.00	78.54	4.81	68.96
112 1488.10	4 SLE	Q -31434.20	-97.92	3049.51	0.00	78.54	4,13	59.71
113 1547.62	4 SLE	Q -30305.30	-67.65	2106.73	0.00	78.54	3.55	51.72
114 1607.14	4 SLE	Q -29178.10	-42.73	1330.85	0.00	78.54	3.06	44.91
115 1666,67	4 SLE	Q -28052.40	-22.73	708.01	0.00	78.54	2.65	39.17
116 1726.19	4 SLE	Q -26928,20	-7.19	223.81	0.00	78.54	2.30	34,40
117 1785.71	4 SLE	Q -25805.50	4.38	-136.43	0.00	78.54	2.17	32.42
118 1845.24	4 SLE	Q -24684.10	12.44	-387.48	0.00	78.54	2.21	32.82
119 1904.76	4 SLE	Q -23564.10	17,47	-544.05	0.00	78.54	2.20	32.56
120 1964.29	4 SLE	Q -22445.30	19.93	-620.68	0.00	78.54	2.15	31.74
121 2023.81	4 SLE	Q -21327.80	20.28	-631.69	0.00	78.54	2.06	30.45
122 2083,33	4 SLE	Q -20211.40	18.98	-591,17	0.00	78.54	1.95	28.80
123 2142.86	4 SLE	Q-19096.00	16.47	-512.94	0.00	78.54	1.82	26.89
124 2202.38	4 SLE	Q -17981.70	13.18	-410.57	0.00	78.54	1.67	24.81
125 2261,90	4 SLE	Q-16868.40	9,55	-297.46	0.00	78.54	1.53	22.66
126 2321.43	4 SLE	Q -15755.90	5.00	-186.79	0.00	78.54	1.38	20.53
127 2380.95	4 SLE	Q-14644.30	2,94	-91.66	0.00	78.54	1.24	18.50
128 2440.48	4 SLE	Q -13533.50	0.81	-25.07	0.00	78.54	1.31	16.68
129 2500.00	4 SLE	Q -12423.50	0.00	0.00	0.00	78.54	1.01	15,15

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	o ed	Δ _{HM}	λ _s <cmq></cmq>	Ac eff <cmq></cmq>	σ _S <dan cmq=""></dan>	eam	Wk <mm></mm>
87	0.00	4	SLE Q	-52378,40	46061.50	-1479.02	46.00	136,36	0.50	20.00	203.54	21.99	1226.47	1037.87	0.30	0.10
88	59.52	4	SLE Q	-53222.40	48734.50	-1564.85	46.00	136.36	0.50	20.00	204.22	21.99	1233.92	1125.43	0.33	0.11
89	119.05	4	SLE Q	-53229.20	50368.60	-1617.33	46.00	136.36	0.50	20.00	204.74	21.99	1239.66	1185.51	0.35	0.1
90	178,57	4	SLE Q	-53237.60	51114.80	-1641.29	46.00	136.36	0.50	20.00	204.97	21.99	1242.12	1212.93	0.35	0.13
91	238.09	4	SLE Q	-53247.70	51112.30	-1641.21	46.00	136.36	0.50	20.00	204.96	21.99	1242.08	1212.71	0.35	0.1
92	297.62	4	SLE Q	-53259.40	50488.50	-1621.17	46,00	136,36	0.50	20.00	204.77	21.99	1239.97	1189.54	0.35	0.1
93	357.14	4	SLE Q	-53272.90	49311.10	-1583.37	46.00	136.36	0.50	20.00	204,40	21.99	1235.84	1146.01	0.33	0.1
94	415.67	4	SLE Q	-52101.50	47505.00	-1525.38	46.00	136,36	0.50	20.00	204.15	21.99	1233.16	1094.26	0.32	0.1
95	476,19	4	SLE Q	-50932.90	45168.20	-1450.34	46.00	136,36	0.50	20,00	203.69	21.99	1228.06	1023.07	0.30	0.1
96	535.71	4	SLE Q	-49767.00	42439.60	-1362.73	46.00	136.36	0.50	20.00	203.00	21.99	1220.50	937.67	0.27	0.0
97	595.24	4	SLE Q	-48603.80	39440.20	-1266.42	46.00	136.36	0.50	20.00	202.07	21,99	1210.25	842.71	0.25	0.0
98	654.76	4	SLE Q	-47443.30	36273,90	-1164,75	46.00	136.36	0.50	20.00	200.85	21.99	1195.90	742.24	0.22	0.0
99	714.29	4	SLE Q	-46285.20	33029,20	-1060.56	46.00	136.36	0.50	20.00	199.30	21,99	1179.79	639,78	0,19	0.0
100	773.81	4	SLE Q	-45129.70	29779.90	-956.23	46.00	136.36	0.50	20.00	197.31	21.99	1157.91	538.38	0.16	0.0
101	833.33	4	SLE Q	-43976.50	26586.80	-853.70	46.00	136.36	0.50	20,00	194.74	21.99	1129.65	440.73	0.13	0.0
102	892.86	4	SLE Q	-42825.80	23498.70	-754.54	46.00	136.36	0.50	20,00	191.40	21,99	1092.96	349,18	0.10	0.0
103	952.38	4	SLE Q	-41677.30	20554.00	-659.99	46.00	136.36	0.50	20.00	202.76	18.85	1043.85	265.91	0.08	0.0
104	1011.90	4	SLE Q	-40531.00	17781.50	-570.96	46.00	136.36	0.50	20.00	216.38	15.71	976.89	192.91	0.06	0.0
105	1071,43	4	SLE Q	-39387.00	15202.10	-488.14	46.00	136.36	0.50	20.00	204.68	15.71	884,96	131.87	0.04	0.0
105	1130.95	4	SLE Q	-38245.00	12829,40	-411.95	46.00	136.36	0.50	20.00	187.37	15.71	749.04	83.79	0.02	0.0
107	1190.48	4	SLE Q	-37105.10	10671.10	-342.65	46.00	136,36	0.50	20.00	177.67	12.57	538.29	48.46	0.01	0.0
108	1250.00	4	SLE Q	-35967.20	8729.56	-280.30	46.00	136.36	0.50	20.00	160.19	9.42	321.33	24.13	0.01	0.0
130	0.00	3	SLE F	-52378.40	46061.50	-1479.02	46.00	136.36	0.50	20.00	203.54	21.99	1226.47	1037.87	0.30	0.1
131	59,52	3	SLE F	-53222.40	48734.50	-1564.85	46.00	136,36	0.50	20.00	204.22	21.99	1233.92	1125.43	0.33	0.1
132	119.05	3	SLE F	-53229.20	50368.60	-1617.33	46.00	136.36	0.50	20.00	204.74	21.99	1239.66	1185,51	0.35	0.1
133	178.57	3	SLE F	-53237.60	51114.80	-1641.29	46.00	136.36	0.50	20.00	204.97	21.99	1242.12	1212.93	0.35	0.1
134	238.09	3	SLE F	-53247.70	51112.30	-1641.21	46.00	136.36	0.50	20.00	204.96	21.99	1242.08	1212.71	0.35	0.1
135	297.62	3	SLE F	-53259.40	50488.50	-1621.17	46.00	136.36	0.50	20.00	204.77	21.99	1239.97	1189.54	0.35	0.1
136	357,14	3	SLE F	-53272.90	49311.10	-1583.37	46.00	136,36	0.50	20.00	204.40	21.99	1235.84	1146.01	0.33	0.1
137	416.67	3	SLE F	-52101.50	47505.00	-1525.38	46.00	136.36	0.50	20.00	204.15	21,99	1233.16	1094.26	0.32	0.1
138	476,19	3	SLE F	-50932,90	45168.20	-1450.34	46.00	136.36	0.50	20.00	203,69	21,99	1228.06	1023.07	0.30	0.1
139	535.71	3	SLE F	-49767.00	42439.60	-1362.73	46.00	136.36	0.50	20.00	203.00	21,99	1220.50	937.67	0.27	0.0
140	595,24	3	SLE F	-48603.80	39440.20	-1266.42	46.00	136.36	0.50	20,00	202.07	21.99	1210.25	842.71	0.25	0.0
141	654.76	3	SLE F	-47443.30	36273.90	-1164.75	46.00	135.36	0.50	20.00	200.85	21.99	1196.90	742.24	0.22	0.0
142	714.29	.3	SLE F	-46285.20	33029.20	-1060.56	46.00	136.36	0.50	20.00	199.30	21.99	1179.79	639,78	0.19	0.0
143	773.81	3	SLE F	-45129.70	29779.90	-956.23	46.00	136.36	0.50	20.00	197.31	21.99	1157.91	538.38	0.16	0.0
144	833.33	3	SLE F	-43976.50	26586.80	-853.70	46.00	136.36	0.50	20.00	194,74	21,99	1129.65	440.73	0.13	0.0
145	892.86	3	SLE F	-42825.80	23498.70	-754.54	46,00	136.36	0.50	20,00	191.40	21.99	1092.96	349.18	0.10	0.0
146	952.38	3	SLE F	-41677.30	20554.00	-659,99	46.00	136.36	0.50	20.00	202.76	18.85	1043.85	265.91	0.08	0.0
147	1011.90	3	SLE F	-40531.00	17781.50	-570.96	46.00	136.36	0.50	20.00	216.38	15.71	976.89	192.91	0.06	0.0
148	1071.43	3	SLE F	-39387.00	15202.10	-488.14	46.00	136.36	0.50	20.00	204.68	15.71	884,96	131.87	0.04	0.0
149	1130.95	3	SLE F	-38245.00	12829.40	-411,95	46.00	136.36	0.50	20,00	187.37	15.71	749.04	83,79	0.02	0.0
150	1190.48	3	SLE F	-37105.10	10671.10	-342.65	46.00	136.36	0.50	20.00	177.67	12.57	538.29	48.46	0.01	0.0
151	1250.00	3	SLE F	-35967.20	8729.56	-280.30	46.00	136.36	0.50	20.00	160.19	9.42	321.33	24.13	0.01	0.0

Verifiche principali

Caso	Tipo
. 5	SLU N cost - min. sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
68	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max trax.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max

Palo n. 10

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf (Om)	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	8450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP.	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 10 (-17)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SIJ	RVN	49182,60	7463.04	0.38	59871.20	47.77
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC			Ĩ	0.00	0.00
	1	SLU	TOT	49182,60	7463.04	0.38	59871.20	47.77
2	2	SLE R	BVN	36431.60	5528.18	0.28	44349.10	35,38
	2	SLE R	TAG	2 3		8	0.00	0.00
	2	SLE R	ECC				0.00	0.00
	. 2	SLE R	TOT	36431.60	5528.18	0.28	44349.10	35,38
- 3	3	SLE F	RVN	36431,60	5528.18	0.28	44349.10	35.38
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	36431.60	5528.18	0.28	44349.10	35.38
4	4	SLE Q	RVN	36431.60	5528,18	0,28	44349.10	35,38
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00
	4	SLE Q	TOT	36431.60	5528.18	0.28	44349.10	35.38

Sollecitazioni nei pali

Caso	8	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-49182.60	-7463.04	-0.38	-59871.20	-47.77
2	2	SLE R	1	-36431,60	-5528.18	-0.28	-44349.10	-35.38
3	3	SLE F	1.	-36431.60	-5528.18	-0.28	-44349.10	-35.38
4	4	SLE Q	1	-36431.60	-5528.18	-0.28	-44349.10	-35.38

Da 0 a -25

Caso	X <cm>></cm>	œ	TCC	N	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-49182,60	59618.00	-47.57	-49182.60	167390.00	-593.26	2-3	180.00	2.808
- 2	59.52	1	SLU	-50048.90	63300.60	-50.51	-50048.90	167747.00	-611.63	2-3	180.00	2.650
.3	119.05	1	SIU	-50100.00	65603.90	-52.34	-50100.00	167768.00	-612.72	2-3	180.00	2.557
4	178.57	1	SIU	-50152,60	66726.90	-53.24	-50152.60	167790.00	-613.84	2-3	180.00	2.515
- 5	238.09	1	SLU	-50206.80	66853.10	-53.34	-50206.B0	167812.00	-614.99	2-3	180.00	2.510
- 6	297.62	1	SLU	-50262.60	66150.70	-52.78	-50262.60	167835.00	-616.18	2-3	180.00	2,537
.7	357.14	1	SLU	-50320.00	64708.60	-51.63	-50320.00	167859.00	-617.40	2-3	180.00	2,594
- 8	416.67	1	SLU	-49223.70	62423.80	-49,81	-49223.70	167407.00	-594.13	2-3	180.00	2.682
. 9	476.19	2	SLU	-48130.00	59425.60	-47.41	-48130.00	166955.00	-571.02	2-3	180.00	2.809
10	535.71	1	SIJ	-47038.80	55898.20	-44.60	-47038.80	166505.00	-548.08	2-3	180.00	2.979
11	595.24	1	SLU	-45950.30	52001.90	-41.49	-45950.30	166055.00	-525.29	2-3	180.00	3.193
12	654.76	1	SLU	-44864,10	47875.10	-38,20	-44864.10	165606.00	-502,06	2-3	180.00	3.459
13	714.29	1	SIJ	-43780.40	43635.20	-34.81	-43780.40	165156.00	-477.66	2-3	180.00	3.785
14	773.81	1	SLU	-42699.00	39380.80	-31.42	-42699.00	164707.00	-453.43	2-3	180.00	4.182
15	833.33	1	SLU	-41619.90	35192.80	-28.08	-41619.90	164259.00	-429.36	2-3	180.00	4.667
16	892.86	1	SIU	-40543.10	31136.90	-24.84	-40543.10	163811.00	-405.45	2-3	180.00	5.261
17	952,38	1	SIU	-39468.40	27264.20	-21,75	-39468.40	163365.00	-381,70	2-3	180,00	5.992
.18	1011.90	1	SLU	-38395.80	23613.80	-18.84	-38395.80	162919.00	-358.11	2-3	180,00	6.899
19	1071.43	1	SLU	-37325.30	20213.90	-16,13	-37325.30	162474.00	-334.67	2-3	180.00	8.038
2.0	1130.95	1	SIAI	-36256.80	17083.20	-13.63	-36256.80	162029.00	-311.38	2-3	180.00	9.485
21	1190.48	1	SLU	-35190.30	14232.40	-11.36	+35190.30	161584.00	-286,80	2-3	180.00	11.353
22	1250.00	1	SIU	-34125.60	11665.40	-9.31	-34125.60	161139.00	-261.82	2-3	180,00	13.813
23	1309.52	1	SLU	-33062.80	9380.40	-7.48	-33062.80	160695.00	-236.99	2-3	180.00	17.131
24	1369.05	1	SIJ	-32001.70	7371.01	-5.88	-32001.70	160251.00	-212.33	2-3	180.00	21.741

-	 Colors & Access of Access 	1.4	Control of the second
Pa	azione	di co	COLO
170	CALCHE	UII CO	ICA JICA

25	1428.57	1	SLU	-30942,40	5627.09	-4.49	-30942.40	159808.00	-187,81	2-3	180.00	28.400
26	1488.10	1	SLU	-29884.70	4135.56	-3,30	-29884.70	159366.00	-163.44	2-3	180.00	38.536
27	1547.62	1	SIJ	-28828.60	2881.11	-2.30	-28828.60	158924.00	-139.22	2-3	180.00	55.161
28	1607.14	1	SIJJ	-27774.10	1846.79	-1.47	-27774.10	158483.00	-115.15	2-3	180.00	85.815
29	1666.67	1	SLU	-26721.00	1014.50	-0.81	-2571250.00	158042.00	-91.21	2-3	180.00	96.226
30	1726.19	1	SLU	-25669.40	365.42	-0.29	-2571250.00	157600.00	-65.47	2-3	180.00	>100
31	1785.71	1	SLU	-24619.20	-119.67	0.10	-2571250.00	-157158.00	-39.75	2-3	0.00	>100
32	1845.24	1	SIJ	-23570.20	-460.16	0.37	-2571250.00	-156717.00	-14,20	2-3:	0.00	>100
33	1904.76	1	SLU	-22522.60	-675.34	0.54	-2571250.00	-156276.00	11.22	2-3	0.00	>100
34	1964.29	1	SIJ	-21476.10	-784.36	0.63	-2571250.00	-155836.00	36.49	2-3	0.00	>100
35	2023.81	1	SLU	-20430.80	-806.05	0.64	-2571250.00	-155396.00	61.62	2-3	0.00	>100
36	2083.33	1	SLU	-19386.60	-758.95	0.61	-2571250.00	-154956.00	86.60	2-3	0.00	>100
37	2142.86	1	SLU	-18343.50	-661.28	0.53	-2571250.00	-154517.00	111.44	2-3	0.00	>100
38	2202.38	1	SLU	-17301.30	-530.94	0.42	-2571250,00	-154078.00	136.19	2-3	0.00	>100
39	2261.90	1	SLU	-16260.10	-385.56	0.31	-2571250.00	-153638.00	162.94	2-3	0.00	>100
40	2321.43	1	SLU	-15219.70	-242.56	0.19	-2571250.00	-153198.00	189.54	2-3	0.00	>100
41	2380.95	1	SIJ	-14180.10	-119.21	0.10	-2571250.00	-15275B.00	216.00	2-3	0.00	>100
42	2440.48	1	SLU	-13141.30	-32.65	0.03	-2571250.00	-152318.00	242.32	2-3	0.00	>100
43	2500.00	1	SLU	-12103.20	0.00	0.00	-2571250.00					>100

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	œ	1020	- Verif: Ty <dan></dan>	Tz <dan></dan>	bw ⊲m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7463.05	0.38	0.85	11.31	7463.05	1.00	32294.70	338713.00	32294.70	4.327
.2	59.52	1	SLU	4970.43	0.25	0.85	11.31	4970.43	1,00	32294.70	338837.00	32294.70	6.497
3	119.05	1	SLU	2824.52	0.14	0.85	11.31	2824,52	1.00	32294.70	338844.00	32294.70	11.434
4	178.57	1	SLU	1000.05	0.05	0.85	11.31	1000.05	1.00	32294.70	338852.00	32294.70	32.293
5	238.09	1	SLU	-528.91	-0.03	0.85	11.31	528,91	1.00	32294.70	338860.00	32294.70	61.059
6	297.62	1	SLU	-1788.54	-0.09	0.85	11.31	1788.54	1.00	32294.70	338868.00	32294.70	18.056
.7	357.14	1	SLU	-3125.56	-0.16	0.85	11.31	3125.56	1.00	32294.70	338876.00	32294.70	10,332
.8	416.67	1	SIJ	-4492.64	-0.23	0.85	11.31	4492.64	1,00	32294.70	338719.00	32294.70	7.188
9	476.19	1	SLU	-5529.74	-0.28	0.85	11.31	5529.74	1,00	32294.70	338562.00	32294.70	5.840
10	535.71	1	SEU	-6277.70	-0.32	0.85	11.31	6277.70	1.00	32294.70	338406.00	32294.70	5.144
11	595,24	1	SIU	-6775,14	-0.34	0.85	11.31	6775,14	1.00	32294.70	338250.00	32294.70	4.767
12	654.76	1	SIJ	-7058,19	-0.36	0.85	11.31	7058,19	1.00	32294.70	338094.00	32294.70	4.575
13	714.29	1	SIJJ	-7160.27	-0.36	0.85	11.31	7160.27	1,00	32294.70	337939.00	32294.70	4.510
14	773.81	1	SLU	-7112.01	-0.36	0.85	11.31	7112.01	1.00	32294.70	337784.00	32294,70	4.541
15	833.33	1	SIJI	-6941.16	-0.35	0.85	11.31	6941.16	1.00	32294.70	337630.00	32294.70	4.653
1.6	892.86	1	SIAI	-6672,66	-0.34	0.85	11.31	6672.66	1.00	32294.70	337475.00	32294.70	4.840
17	952.38	1	SIU	-6328.68	-0.32	0.85	11.31	6328.68	1.00	32294.70	337322.00	32294,70	5.103
18	1011,90	1	SLU	-5928.72	-0.30	0.85	11.31	5928,72	1,00	32294.70	337168.00	32294.70	5.44
19	1071.43	1	SIA	-5489.77	-0.28	0.85	11.31	5489.77	1.00	32294.70	337015.00	32294.70	5.883
20	1130.95	1	SIU	-5026.45	-0.25	0.85	11.31	5026.45	1.00	32294.70	336862.00	32294.70	6.425
21	1190.48	1	SIJ	-4551,22	-0.23	0.85	11.31	4551.22	1,00	32294.70	336709.00	32294.70	7.096
22	1250.00	1	SIU	-4074.50	-0.21	0.85	11.31	4074.50	1,00	32294.70	336556.00	32294.70	7.928
23	1309.52	1	SLU	-3604.93	-0.18	0.85	11.31	3604.93	1.00	32294.70	336404.00	32294.70	8.958
24	1369.05	1	SLU	-3149.50	-0.16	0.85	11.31	3149,50	1.00	32294.70	336252.00	32294,70	10.254
25	1428,57	1	SLU	-2713.78	-0.14	0.85	11.31	2713.78	1.00	32294.70	336100.00	32294.70	11.900
26	1488.10	1	SLU	-2302.08	-0.12	0.85	11.31	2302.08	1.00	32294.70	335949.00	32294.70	14.028
27	1547.62	-1	SIJ	-1917.64	-0.10	0.85	11.31	1917.64	1.00	32294.70	335797.00	32294.70	16.841
28	1607.14	1	SLU	-1562.76	-0.08	0.85	11.31	1562.76	1.00	32294.70	335646.00	32294.70	20.665
29	1666,67	1	SLU	-1239.01	-0.06	0.85	11.31	1239.01	1.00	32294.70	335496.00	32294.70	26.065
30	1726,19	1	SIAJ	-947,30	-0.05	0.85	11.31	947.30	1.00	32294.70	335345.00	32294.70	34.092
31	1785.71	1	SLU	-688.07	-0.03	0.85	11.31	688.07	1.00	32294.70	335195.00	32294.70	46.935
32	1845.24	1	SIAI	-461.38	-0.02	0.85	11.31	461.38	1.00	32294.70	335044.00	32294.70	69.997
33	1904.76	1.	SIA	-267.00	-0.01	0.85	11.31	267.00	1.00	32294.70	334894.00	32294.70	>100
34	1964.29	1	SIU	-104.55	-0.01	0.85	11.31	104.55	1,00	32294.70	334744.00	32294.70	>100
35	2023.81	1	SLU	26.48	0.00	0.85	11.31	26.48	1.00	32294.70	334595.00	32294.70	>100
36	2083.33	1	SLU	126.66	0.01	0.85	11,31	126,66	1.00	32294,70	334445.00	32294.70	>100
37	2142.86	1	SLU	196.50	0.01	0.85	11.31	196.50	1.00	32294.70	334296.00	32294,70	>100
38	2202.38	1	SLU	236.51	0.01	0.85	11.31	236.51	1.00	32294.70	334146.00	32294.70	>100
39	2261.90	1	SLU	247.09	0.01	0.85	11.31	247.09	1.00	32294.70	333997.00	32294.70	>100
40	2321.43	1	SIJ	228.56	0.01	0.85	11.31	228.56	1.00	32294.70	333848.00	32294.70	>100
41	2380.95	1	SLU	181.12	0.01	0.85	11.31	181.12	1.00	32294.70	333699.00	32294.70	>100
42	2440.48	1	SIJJ	104.92	0.01	0,85	11.31	104.92	1.00	32294.70	333550.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <mq></mq>	AfC <cmq></cmq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-36431.60	-35.23	44161.50	47.12	31.42	43.79	1169.54
45	59.52	2	SLE R	-37386.50	-37.41	46889.30	47.12	31.42	46.57	1258.91
4.6	119.05	2	SLE R	-37614.40	-38.77	48595.50	47.12	31.42	48.32	1319.76
47	178.57	2	SLE R	-37843.50	-39.44	49427.30	47.12	31.42	49.17	1347.87
48	238.09	2	SLE R	-38073.80	-39.51	49520.80	47.12	31.42	49.25	1348.30
49	297.62	2	SLE R	-38305.40	-39.10	49000.50	47.12	31.42	48.70	1325.73
50	357.14	2	SLE R	-38538.10	-38.24	47932.30	47.12	31.42	47.59	1282,67
51	416.67	2	SLE R	-37741.10	-36.89	46239.90	47.12	31.42	45.88	1229.93

									ione di d	calcolo
===	478,19	2		-36348.30						
:1	935.71 335.24		822 C	+36153,40 3384,40		41408,10 38319,90			40.95 38.00	1070.35 9/8.24
	6.27 J/26		977 7	47.078.40		A.27 8 8 . CC			37.287	869.44
7.6	774,09	-/	977 R	-26 (66, 10	-25.09	32900.40	47,77	31.47	311.64	6.31.99
F12	7774.91	/	977 R			09170.90	47.7%	31.47	09.08	6 AB . 10
19	803.33 802.33	-		-32217.10 -31435.10	-20,80 -18,40	16088.80 10084.30			13.18 12.08	994,77 498,66
00	9.001.00	-	977 5	40655.00		20195.70			19.08	363.75
οT	10001290		977 7.	23878,40		17730,790			16147	779,44
60	1077.43			-(19)(99,4))		14970,30			19.65	204,65
6.7	1130.95 1130.48	-	977 K	-00004.00 -17350.10		12/54,00 10342,00	97.70 94.58		11.08 9.18	1.639.64 2289.37
50	1230.00	-		-14777.70			32,42		7.42	203,17
0.0	1309.52		977.7	26008.70			".:." 3		6.000	841.47
	1369105	:	57	Za037.10	1.00			500,63	7.395	70.006
	14280.50 14880.10	_	977 K 977 K	-04468.90 -03700.00	-0.00 -0.44			78.54 78.54	4.15 9.51	58,14 50,40
	1347.00		875 P	-02936.30	-1.44	2134,13		78,34	2.97	42,90
	1607.14			-12171.90	-1,09	1067.90		78,74	2,51	26,54
97	1668.67		977 7.	N1408190	0.560	297.148	0.00	fp/	"." s	31
	1778.14		977 T.	20076.50	0.77	0.701.68		(:::/	1.80	117.07
	1795.01 1845.04	-		-19865.70 -19125.80	0.07	-889,68 -340,86		78.34	1.66	25.71
	1004.70	-		-18088.90	0.40	-300,10		72,34	75	25,31
_	1361.29		977.7	17609.00	0.45	81 .00		/m:/	1.73	"54.55
	2013.cT		977 7	16850.00	0.46	.:97.07		/::.:/	1.88	77.04
2.9	00001.22 0140.36		977 R 977 R	-1: 086: 00 -1:3940: 90	0.45	-860.19 -269.92		78.54 78.54	1.60	20.15 20.15
E.1	1202.35	-	8 M P	-14388.30	9,31	-093,10		78.74	39	20,00
22	1261,90	-		-10832.90		-285.00		78,74	27	_S.E7
::::	z311 .45		977 7	13080.00	0.14	1.79.58		fa/	1,118	17.21
8.1			977 T. 977 K	-115.76.40	0.07	-04.19	_	78.54	1,05	15000
3 (.		_		-10805.60	0.00	0.00		78.54	0.386	19.50
17	0.00		912 Q	-36431.00		44181.00			40.79	1169,04
11	39,01	-	8 A O			46889,30			46.57	1238.91
:: "	119006		977 Q 977 Q	376171.40		48.5950.50 497.570.50			48.50 49.17	1319.75 1347.65
91	2381.09			-29073, 90		49500.90			49.05	1949.30
90	297.60	_		-20005.40		490000.50	47,70	31.47	481.70	1325.02
93				-38338.10						
94				-37741.10					47.88	1229,93
40		_		36948.30 36158.40					431.80 401.95	Time (14.4) Time (14.4)
977				-25360.40					28100	
2:1				-34x70.30						0.9,99
99		4	8 A C	-30788.10	-25.79	32022,40	47,12	31,42	31.84	
100			94 S	-30000.70 					28.39	638,16 337,277
102		-		277,850,20		23084.50				
7.02	980.00			-20055.00	-16.11	00185.70	49, 99	34 . 50	19.08	
	1011.90			-09876,40						
	1071,43 1130,90			-19099,40 -18024,60						204,60 133,64
	1130.46			×4.50.10		10.250.00				175,04
	Thabled	7	9 5	26,177,790	8.00	8641.04	31 173	72.TT	1210	1.03.17
	1908.50			-01006.70					1.00	94,47
	1968.05 1428.07			-05207.10 -14488.90				59.79 78.74	4.15	39,14
	1488.10			-12702.00				78,74		30,41
110	Total Conz	7	977 0	27938.50	1,290			(0)	71.97	
_	1607.14			Z ¹¹¹ (11.50)				(0)	71.57	36.51
	1006.65	_		-01408.70 -0046.60				78.54 78.54		95.09 27.09
				-13885.70			_	78.74		
		- /	9 5	131 (9), 50	0.29			(m)	1.73	75.77
	1904.256			18388, 90				/m /		
	1994,09 0020,91			-17/08:00 -1/050:00	0.46			78.54 78.54	1.73	25.55 24.74
	1083.33	-		-16098.00				78.74		
	1142,80	4	y Y	-19040.80	0.39		_	78,74		22,10
	Z*********			17.588.50				/m:/		
	2000 1960 2002 142	-		13880.90 -19090.00				78.37 78.34		
	01800.95	_		-12007.90	0.05			78.54	1.05	15.35

128 2440.48	4	SLE (-11576.40	0.02	-24.19	0.00	78.54	0.95	14.28
129 2500.00	4	SLE (-10825.60	0.00	0.00	0.00	78.54	0.88	13,20

Stato	limita	A	eserciain.	_	Verifiche		fessurazione	
Statu	TTHE CO.	- 44	GRETCISTO	_	ARTITIONS	е.	ressurazione	

Stato	limite	a.	eserci	1000	The second second	fessura	THE RESERVE OF THE PERSON NAMED IN						1.			
Caso	X <cm></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K2	Φeq	Δ _{SIII}	A _S	A _{c eff}	σ _∃ <dan cmq=""></dan>	€ _{SEI}	Wk <mm></mm>
87	0.00	4	SLE Q	-36431.60	44161.50	-35.23	46,00	136,36	0.50	20.00	207.94	21.99	1274.80	1169.54	0.34	0.12
88	59,52	4	SLE Q	-37386.50	46889.30	-37.41	46.00	136.36	0.50	20.00	208.30	21.99	1278,83	1258.91	0.37	0.13
89	119.05	4	SLE Q	-37614.40	48595.50	-38.77	46,00	136.36	0.50	20.00	208.61	21.99	1282.18	1319.75	0.38	0.14
90	178.57	4	SLE Q	-37843.50	49427.30	-39,44	46,00	136.36	0.50	20.00	208.72	21.99	1283.38	1347.87	0.39	0.14
91	238.09	4	SLE Q	-38073.80	49520.80	-39.51	46.00	136.36	0.50	20.00	208.68	21.99	1282.93	1348.30	0.39	0.14
92	297,62	4	SLE Q	-38305.40	49000.50	-39.10	46.00	136.36	0.50	20.00	208.51	21.99	1281.08	1325.73	0.39	0.14
93	357.14	4	SLE Q	-38538.10	47932.30	-38.24	46.00	136.36	0.50	20.00	208.22	21.99	1277.86	1282.67	0.37	0.13
94	416.67	4	SLE Q	-37741.10	46239.90	-36.89	46.00	136.36	0.50	20.00	208.05	21.99	1276.08	1229.93	0.36	0,13
95	476.19	4	SLE Q	-36946.30	44019.00	-35.12	46.00	136.36	0.50	20.00	207.75	21.99	1272.69	1157.43	0.34	0.12
96	535.71	4	SLE Q	-36153,40	41406.10	-33.04	46,00	136.36	0.50	20.00	207.29	21.99	1267.66	1070.36	0.31	0.11
97	595.24	4	SLE Q	-35362.40	38519.90	-30.73	46.00	136.36	0.50	20.00	206.67	21.99	1260.86	973.24	0.28	0.10
98	654.76	4	SLE Q	-34573.30	35463.00	-28.29	46.00	136.36	0.50	20.00	205.87	21.99	1252.04	869,99	0.25	0.09
. 99	714,29	4	SLE Q	-33786.10	32322.40	-25.79	46,00	136,36	0.50	20.00	204.84	21.99	1240,79	763.99	0.22	0.08
100	773.81	4	SLE Q	-33000.70	29170.90	-23.27	46.00	136.36	0.50	20.00	203,55	21.99	1226.52	658.10	0.19	0.07
101	833,33	4	SLE Q	-32217,10	26068.80	-20.80	46.00	136.36	0.50	20.00	201.90	21.99	1208,39	554.77	0.16	0.06
102	892.86	4	SLE Q	-31435.20	23064.30	-18.40	46,00	136.36	0.50	20.00	199,80	21.99	1185.34	456.06	0.13	0.05
103	952.38	4	SLE Q	-30655.00	20195.70	-16.11	46.00	136.36	0.50	20.00	197,11	21.99	1155.79	363.75	0.11	0.04
104	1011.90	4	SLE Q	-29876.40	17491.70	-13.96	46.00	136.36	0.50	20.00	210.53	18.85	1117.08	279.44	0.08	0.03
105	1071.43	4	SLE Q	-29099.40	14973.30	-11.95	46.00	136.36	0.50	20.00	204,83	18.85	1063.42	204,65	0.06	0.02
106	1130.95	4	SLE Q	-28324.00	12654.20	-10.10	46.00	136.36	0.50	20.00	196.72	18.85	986.91	140.94	0.04	0.01
107	1190.48	4	SLE Q	-27550.10	10542.50	-8.41	46.00	136.36	0.50	20.00	203.60	15.71	876.48	89.69	0.03	0.01
108	1250.00	4	SLE Q	-26777.70	8641.04	-6.89	46.00	136.36	0.50	20.00	202.80	12.57	696.15	51.58	0.02	0.01
109	1309.52	4	SLE Q	-26006.70	6948.44	-5.54	46,00	136,36	0.50	20.00	184,83	9.42	437.44	25.73	0.01	0.00
110	1369.05	4	SLE Q	-25237.10	5460.01	-4.36	46.00	136.36	0.50	20.00	217.24	3.14	196.72	9.46	0.00	0.00
130	0.00	3	SLE F	-36431.60	44161.50	-35.23	46.00	136.36	0.50	20.00	207.94	21.99	1274.80	1169.54	0.34	0.12
131	59.52	3	SLE F	-37386.50	46889.30	-37,41	45,00	136.36	0.50	20.00	208.30	21.99	1278.83	1258.91	0.37	0.13
132	119.05	3	SLE F	-37614.40	48595.50	-38.77	46.00	136.36	0.50	20.00	208.61	21.99	1282.18	1319.75	0.38	0.14
133	178.57	3	SLE F	-37843.50	49427.30	-39.44	46,00	136.36	0.50	20.00	208.72	21.99	1283.38	1347.87	0.39	0.14
134	238.09	3	SLE F	-38073.80	49520.80	-39.51	46.00	136.36	0.50	20.00	208.68	21.99	1282.93	1348.30	0.39	0.14
135	297,62	3	SLE F	-38305.40	49000.50	-39.10	46,00	136.36	0.50	20.00	208.51	21.99	1281.08	1325.73	0.39	0.14
136	357.14	3	SLE F	-38538.10	47932.30	-38.24	46.00	136.36	0.50	20.00	208.22	21,99	1277.86	1282.67	0.37	0.13
137	416.67	3	SLE F	-37741,10	46239,90	-36.89	46,00	136,36	0.50	20.00	208,05	21,99	1276.08	1229,93	0.36	0,13
138	476.19	3	SLE F	-36946.30	44019.00	-35.12	46.00	136.36	0.50	20.00	207.75	21.99	1272.69	1157.43	0.34	0.12
139	535.71	3	SLE F	-36153.40	41406.10	-33.04	46.00	136.36	0.50	20.00	207.29	21.99	1267.66	1070.36	0.31	0.11
140	595.24	3	SLE F	-35362.40	38519.90	-30.73	46+00	136,36	0.50	20.00	206.67	21.99	1260.86	973.24	0.28	0.10
141	654.76	3	SLE F	-34573.30	35463.00	-28.29	46,00	136.36	0.50	20.00	205.87	21.99	1252.04	869.99	0.25	0.09
142	714.29	3	SLE F	-33786.10	32322.40	-25.79	46.00	136.36	0.50	20.00	204.84	21.99	1240.79	763.99	0.22	0.08
143	773.81	3	SLE F	-33000.70	29170.90	-23.27	46.00	136.36	0.50	20.00	203.55	21.99	1226.52	658,10	0.19	-
144	833.33	3	SLE F	-32217.10	26068.80	-20.80	46.00	136.36	0.50	20.00	201,90	21.99	1208.39	554.77	0.16	0.06
145	892.86	3	SLE F	-31435.20	23064.30	-18.40	46.00	136.36	0.50	20.00	199.80	21.99	1185.34	456.06	0.13	0.05
146	952.38	.3	SLE F	-30655.00	20195.70	-16.11	46,00	136.36	0.50	20.00	197.11	21.99	1155.79	363.75	0.11	0.04
147	1011.90	3	SLE F	-29876.40	17491.70	-13.96	46.00	136.36	0.50	20.00	210.53	18.85	1117.08	279.44	0.08	0.03
148	1071,43	3	SLE F	-29099,40	14973.30	-11.95	46.00	136.36	0.50	20.00	204,83	18.85	1063.42	204,65	0.06	0.02
149	1130.95	3	SLE F	-28324,00	12654,20	-10.10	46.00	136.36	0,50	20.00	196.72	18.85	986.91	140.94	0.04	0.01
150	1190.48	3	SIE F	-27550.10	10542,50	-8.41	46.00	136.36	0.50	20.00	203.60	15.71	876.48	89.69	0.03	0.01
151	1250.00	3	SLE F	-26777.70	8641.04	-6.89	46.00	136.36	0.50	20.00	202.80	12.57	696.15	51.58	0.02	0.01
152	1309.52	3	SLE F	-26006.70	6948.44	-5.54	46.00	136.36	0,50	20.00	184.83	9.42	437.44	25.73	0.01	0.00
153	1369.05	3	SLE F	-25237.10	5460.01	-4.36	45,00	136,36	0.50	20.00	217,24	3.14	196.72	9.46	0.00	0.00

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.s., SLU Taglio - min. sic. acciaio
. 5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
69	C.Rare - Sc max (min. compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
112	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 11

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	and the second s		Fck <dan cmq=""></dan>	Fetk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	5450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

1		N	Mx	Му	Mz
ı	AZ	<dan></dan>	<danm></danm>	<danm></danm>	<danm></danm>

PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 11 (-22)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	70857.90	7356.74	-383.97	62478.10	-1927.12
	1	SLU	TAG				0.00	0.00
	1	SIA	ECC				0.00	0.00
	1	SLU	TOT	70857.90	7356.74	-383.97	62478.10	-1927.12
- 2	2	SIE R	RVN	52487.40	5449.44	-284.42	46280.10	-1427.50
	. 2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	52487,40	5449.44	-284.42	46280.10	-1427.50
3	3	SLE F	RVN	52487.40	5449.44	-284.42	46280.10	-1427.50
	3	SLE F	TAG	3			0.00	0.00
	3	SLE F	ECC			4 4	0.00	0.00
	3	SLE F	TOT	52487.40	5449.44	-284.42	46280.10	-1427.50
4	4	SIE Q	RVN	52487.40	5449.44	-284.42	46280.10	-1427.50
-	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC		-		0.00	0.00
	4	SLE Q	TOT	52487.40	5449.44	-284.42	46280.10	-1427.50

Sollecitazioni nei pali

Caso	cc	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-70857.90	-7356.74	383.97	-62478.10	1927.12
2	2	SLE R	1	-52487.40	-5449,44	284,42	-46280.10	1427.50
- 3	3	SLE F	. 1	-52487.40	-5449.44	284.42	-462B0.10	1427.50
4	4	SLE Q	1	-52487.40	-5449.44	284.42	-46280.10	1427.50

Da 0 a -25

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <dann></dann>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SIJJ	-70857.90	62220.40	1919.17	-70857.90	175969.00	5357.94	2-3	178.12	2.828
- 2	59,52	1	SILI	-71573.50	65829.90	2030.50	-71573.50	176252.00	5373.94	2-3	178.12	2.677
- 3	119.05	1	SIU	-71324.00	68036.30	2098.56	-71324.00	176153.00	5368.36	2-3	178.12	2.589
4	178,57	1	SIJ	-71076.60	69043.40	2129.62	-71076.60	176055.00	5362.83	2-3	178.12	2.550
- 5	238.09	1	SLU	-70831.50	69039.30	2129.50	-70831.50	175958.00	5357.35	2-3	178.12	2.549
- 6	297.62	1	SIJ	-70588.60	68196.00	2103.49	-70588.60	175862.00	5351.92	2-3	178.12	2.579
7	357.14	1	SIU	-70348.00	66605.20	2054,42	-70348.00	175767.00	5346.54	2-3	178.12	2.639
8	416.67	1	SLU	-68742.60	64165.20	1979.16	-68742.60	175131.00	5310.72	2-3	178.12	2.729
.9	476.19	1	SLU	-67141.00	61008.40	1881.79	-67141.00	174497.00	5275.05	2+3	178.12	2.860
10	535.71	1	SIJJ	-65542.90	57322.60	1768,10	-65542.90	173864.00	5239.54	2-3	178,12	3.033
11	595.24	1	SIJ	-63948.40	53271.00	1643.13	-63948.40	173232.00	5204.17	2-3	178,12	3.252
12	654.76	1	SLU	-62357.30	48994.10	1511.21	-62357.30	172600.00	5168.38	2-3	178,12	3.523
13	714.29	1	SLU	-60769.50	44611.30	1376.02	-60769.50	171968.00	5132.45	2-3	178.12	3.855
14	773.81	1	SIU	-59185.00	40222.40	1240.65	-59185.00	171337.00	5096.67	2-3	178,12	4.260
15	833.33	1	SLU	-57603.70	35909.40	1107.62	-57603.70	170707.00	5061.04	2-3	178.12	4.754
16	892.86	1	SLU	-56025.50	31738.30	978.96	-56025.50	170078.00	5025.56	2-3	178.12	5.359
17	952.38	1	SIJJ	-54450.30	27760.90	856.28	-54450.30	169450.00	4990.21	2-3	178.12	6.104
18	1011.90	1	SLU	-52877.90	24016.20	740.77	-52877.90	168822.00	4954.67	2-3	178.12	7.029
19	1071.43	1	SLU	-51308.50	20532.20	633.31	-51308.50	168194.00	4918.70	2-3	178.12	8.191
20	1130.95	1	SLU	-49741.80	17327.50	534.46	-49741.BO	167567.00	4882.86	2-3	178.12	9.670
21	1190.48	1	SLU	-48177.70	14412.30	444.54	-48177.70	166940.00	4847.16	2-3	178.12	11.583
22	1250.00	1	SLU	-46616.20	11789.90	363.66	-46616.20	166314.00	4811.60	2-3	178.12	14.106
23	1309.52	1	SLU	-45057.30	9458.22	291.74	-45057.30	165689.00	4776.17	2-3	178.12	17.517
24	1369.05	1	SIJ	-43500.70	7410.05	228.56	-43500.70	165060.00	4759.26	2-3	178,12	22.274
25	1428.57	1	SLU	-41946.50	5634.64	173.80	-41946.50	164415.00	4787.25	2-3	178,12	29.178
26	1488.10	1	SLU	-40394.50	4118.26	127.03	-40394.50	163771.00	4815,00	2-3	178.12	39.765
27	1547.62	1	SIU	-38844.70	2844.93	87.75	-38844.70	163127.00	4842.37	2-3	178,12	57.337
28	1607.14	1	SLU	-37297.00	1797.04	55.43	-2571250.00	162484.00	4869.38	2-3	178.12	68.940
29	1666.67	1	SIU	-35751.30	955.85	29.48	-2571250.00	161842.00	4896.04	2-3	178.12	71.920
30	1726,19	1	SLU	-34207,50	301.91	9,31	-2571250.00	161200.00	4922.36	2-3	178.12	75.166
31	1785.71	1	SIU	-32665.60	-184.61	-5.69	-2571250.00	-160464.00	-3662.97	2+3	358.75	78.714
32	1845.24	1	SLU	-31125.30	-523.65	-16.15	-2571250.00	-159819.00	-3622.90	2-3	358.75	82.609
33	1904.76	1	SLU	-29586,80	-735.07	-22.67	-2571250.00	-159175.00	-3583.04	2-3	358.75	86.909
34	1964.29	1	SIJ	-28049.80	-838.52	-25.86	-2571250.00	-158532.00	-3543.39	2-3	358.75	91.667
35	2023.81	1	SLU	-26514.40	-853.36	-26.32	-2571250.00	-157888.00	-3502.98	2-3	358.75	96.976
36	2083.33	1	SIJ	-24980.40	-798.60	-24,63	-2571250.00	-157194.00	-5168.72	2-3	358.12	>100
37	2142.86	1	SIU	-23447.70	-692.90	-21.37	-2571250.00	-156549.00	-5125.58	2-3	358.12	>100
38	2202,38	1	SLU	-21916.20	-554.61	-17.11	-2571250.00	-155904.00	-5082.63	2-3	358,12	>100
39	2261.90	1	SLU	-20386.00	-401.81	-12.39	-2571250.00	-155260.00	-5039.86	2-3	358.12	>100

40	2321.43	1	SLU	-18856,80	-252.31	-7.78	-2571250.00	-154616.00	-4997.30	2-3	358.12	>100
41	2380.95	1	SLU	-17328.70	-123.81	-3.82	-2571250.00	-153971.00	-4954.09	2-3	358.12	>100
42	2440.48	1	SIU	-15801.50	-33.87	-1.04	-2571250.00	-153324.00	-4910.00	2-3	358.12	>100
43	2500.00	1	SIJ	-14275.10	0.00	0.00	-2571250.00	ē 8				>100

Stato	limite	ultimo	- Verifiche	a	taglio

Caso	X <cm>></cm>	oc	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7356.74	-383.97	0.85	11.31	7366.75	1.00	32294.70	341818.00	32294.70	4.384
2	59.52	1	SLU	4821.81	-251.67	0.85	11.31	4828.38	1.00	32294.70	341920.00	32294.70	6.689
3	119.05	1	SLU	2642.12	-137.90	0.85	11.31	2645.72	1.00	32294.70	341884.00	32294.70	12.200
4	178.57	1	SLU	791,44	-41.31	0.85	11.31	792.52	1.00	32294.70	341849.00	32294.70	40.749
5	238.09	1	SLU	-757.07	39.51	0.85	11.31	758.10	1,00	32294.70	341814.00	32294.70	42.500
- 6	297.62	1	SLU	-2030.42	105.97	0.85	11.31	2033.18	1.00	32294.70	341779.00	32294.70	15.884
7	357,14	- 5	SIJ	-3378.43	176.33	0.85	11.31	3383.02	1.00	32294.70	341745.00	32294.70	9.546
8	416.67	1	SLU	-4753.13	248.08	0.85	11.31	4759.60	1,00	32294.70	341515.00	32294.70	6.785
9	476,19	1	SIAI	-5791.73	302.29	0.85	11,31	5799.62	1.00	32294.70	341285,00	32294.70	5.568
1.0	535.71	1	SIU	-6536.15	341.14	0.85	11.31	6545.05	1.00	32294.70	341056.00	32294.70	4,934
11	595.24	1	SLU	-7025.98	366.71	0.85	11.31	7035.55	1.00	32294.70	340828.00	32294.70	4.590
12	654.76	1	SLU	-7298.21	380.92	0.85	11.31	7308.15	1.00	32294.70	340600.00	32294.70	4.419
13	714.29	1	SIJ	-7387.05	385.55	0.85	11.31	7397.10	1.00	32294.70	340373.00	32294.70	4.366
14	773.81	1	SIA	-7323,76	382.25	0.85	11.31	7333.73	1.00	32294.70	340146.00	32294.70	4.404
15	833.33	1	SLU	-7136.72	372.49	0.85	11.31	7146.43	1,00	32294.70	339919.00	32294.70	4.519
16	892,86	1	SLU	-6851.33	357.59	0.85	11.31	6860.66	1,00	32294.70	339693.00	32294.70	4.70
17	952.38	1	SLU	-6490.19	338.75	0.85	11.31	6499.03	1.00	32294.70	339467.00	32294.70	4.969
1.8	1011.90	1	SIAI	-6073.16	316.98	0.85	11.31	6081.43	1,00	32294.70	339242.00	32294.70	5.310
19	1071.43	1	SIU	-5617.51	293.20	0.85	11.31	5625.15	1.00	32294.70	339017.00	32294.70	5.741
20	1130.95	1	SLU	-5138.08	268.17	0.85	11.31	5145.08	1.00	32294.70	338793,00	32294.70	6.27
21	1190.48	1	SLU	-4647,51	242.57	0.85	11.31	4653.83	1.00	32294.70	338569.00	32294.70	6.939
22	1250.00	1	SILI	-4156.35	216.93	0.85	11.31	4162.01	1.00	32294.70	338345.00	32294.70	7.759
23	1309.52	1	SIJ	-3673.33	191.72	0.85	11.31	3678.33	1.00	32294.70	338122.00	32294.70	8.78
24	1369.05	1	SLU	-3205.50	167.31	0.85	11.31	3209.86	1.00	32294.70	337899.00	32294.70	10.06
25	1428.57	1	SLU	-2758.47	143.97	0.85	11.31	2762.23	1.00	32294.70	337676.00	32294.70	11.692
26	1488.10	1	SLU	-2336.56	121.95	0.85	11.31	2339.74	1.00	32294.70	337454.00	32294.70	13.803
27	1547.62	1	SIJ	-1943.00	101.41	0.85	11.31	1945,64	1.00	32294.70	337232.00	32294.70	16.599
28	1607.14	1	SIJJ	-1580.07	82.47	0.85	11.31	1582.22	1.00	32294.70	337010.00	32294.70	20.411
29	1666.67	1	SLU	-1249.29	65.20	0.85	11.31	1250.99	1.00	32294.70	336789,00	32294.70	25.815
30	1726.19	1	SIJ	-951,57	49.67	0.85	11.31	952.86	1.00	32294.70	336568.00	32294.70	33.892
31	1785.71	1	SIAI	-687.28	35.87	0.85	11.31	688,22	1,00	32294.70	336347.00	32294.70	46.923
32	1845,24	1	SIU	-456,44	23.82	0.85	11.31	457.06	1.00	32294.70	336126.00	32294.70	70.65
33	1904.76	1	SLU	-258.80	13.51	0.85	11.31	259,15	1.00	32294.70	335906,00	32294.70	>100
34	1964.29	1	SIU	-93.91	4.90	0.85	11.31	94.04	1.00	32294.70	335686.00	32294.70	>100
35	2023.81	1	SIAI	38.78	-2.02	0.85	11.31	38.83	1.00	32294.70	335466.00	32294.70	>100
36	2083.33	1	SIJ	139.84	-7.30	0.85	11.31	140.03	1.00	32294.70	335246.00	32294.70	>100
37	2142.86	1	SIU	209.85	-10.95	0.85	11.31	210.14	1.00	32294.70	335027.00	32294.70	>100
38	2202.38	1	SLU	249.32	-13.01	0.85	11,31	249.66	1.00	32294.70	334807.00	32294.70	>100
39	2261.90	1	SLU	258.67	-13.50	0.85	11.31	259.02	1.00	32294.70	334588.00	32294.70	>100
4.0	2321.43	1	SLU	238.24	-12.43	0.85	11.31	238.56	1,00	32294.70	334369.00	32294.70	>100
41	2380.95	1	SLU	188.24	-9.82	0.85	11.31	188.49	1.00	32294.70	334150.00	32294.70	>100
42	2440.48	1	SIU	108.81	-5.68	0.85	11.31	108.95	1.00	32294.70	333931.00	32294,70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	oc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <amq></amq>	AfC <cmq></cmq>	σ _□ <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-52487.40	1421.61	46089.20	43.98	34.56	44.82	1034.29
45	59.52	2	SLE R	-53330.60	1504.08	48762.90	47,12	31.42	47.57	1121.63
4.6	119.05	2	SLE R	-53335.90	1554.49	50397.20	47.12	31.42	49.28	1181.56
47	178.57	2	SLE R	-53342.80	1577.50	51143.20	47.12	31.42	50.06	1208.92
48	238.09	2	SLE R	-53351.40	1577.41	51140.20	47,12	31,42	50+05	1208.70
49	297.62	2	SLE R	-53361.60	1558.14	50515.50	47.12	31.42	49.40	1185.59
50	357.14	2	SLE R	-53373.60	1521.79	49337.20	47.12	31.42	48.17	1142.16
51	416.67	2	SLE R	-52199.60	1466.04	47529.70	47,12	31.42	46.35	1090.55
52	476.19	2	SLE R	-51028.50	1393.92	45191.40	43.98	34.56	43.98	1019.54
53	535.71	2	SLE R	-49860.10	1309.70	42461.20	43.98	34.56	41.19	934.36
54	595.24	2	SLE R	-48694.30	1217.13	39460.00	43.98	34.56	38,12	839.65
55	654.76	2	SLE R	-47531.20	1119.41	36291.90	43.98	34.56	34.86	739.44
56	714.29	2	SLE R	-46370.70	1019.28	33045.40	43.98	34.56	31.51	637.26
57	773.81	2	SLE R	-45212.60	919.00	29794.40	43.98	34.56	28,15	536.14
58	833.33	2	SLE R	-44056.90	820.46	26599.60	43.98	34.56	24.84	438.76
59	892.86	2	SLE R	-42903.60	725.16	23509.90	40.84	37.70	21.65	347.50
60	952.38	2	SLE R	-41752.60	634.28	20563.60	37.70	40.84	18.62	264.50
61	1011.90	2	SLE R	-40603.90	548.72	17789.80	37.70	40.84	15.80	216.02
62	1071.43	2	SLE R	-39457.30	469.12	15209.10	34.56	43.98	13,26	182.73
63	1130.95	2	SLE R	-38312.80	395.90	12835.20	31.42	47.12	11.04	153.42
64	1190.48	2	SLE R	-37170.40	329.29	10675.70	28.27	50.27	9,18	128.66
65	1250.00	2	SLE R	-36030.00	269,38	8733.29	21.99	56.55	7.69	108.50
66	1309.52	2	SLE R	-34891.50	216.10	7006.09	12.57	65.97	6.51	92.49

							R	elazi	one di ca	alcolo
67	1369.05	2	SLE R	-33754.90	169.30	5488.93	0.00	78.54	5.58	79.8
68	1428.57	2	SLE R	-32620.10	128.74	4173.81	0.00	78.54	4.81	69.1
69	1488.10	2	SLE R	-31487.10	94.09	3050.56	0.00	78.54	4.14	59.8
70	1547.62	2	SLE R	-30355.70	65.00	2107.36	0.00	78.54	3.56	51.8
71	1607.14	2	SLE R	-29226.00	41.06	1331.14	0.00	78.54	3,06	45.0
72	1666.67	2	SLE R	-28097.80	21.84	708.04	0.00	78.54	2.65	39.2
73	1726,19	2	SLE R	-26971.20	6.90	223.63	0.00	78.54	2.31	34.4
74	1785.71	2	SLE R	-25846.00	-4.22	-136.75	0.00	78.54	2,17	32.4
7.5	1845.24	2	SLE R	-24722.10	-11.96	-387.89	0.00	78.54	2,21	32.8
76	1904.76	2	SLE R	-23599.60	-16.79	-544.50	0.00	78.54	2.20	32.5
7.7	1964.29	2	SLE R	-22478.40	-19.16	-621.13	0.00	78.54	2,15	31.7
78	2023.81	2	SLE R	-21358.40	-19.50	-632.12	0.00	78.54	2.06	30.4
79	2083.33	2	SLE R	-20239.50	-18.25	-591.55	0.00	78.54	1.95	28.8
80	2142,86	2	SLE R	-19121.70	-15.83	-513.26	0.00	78.54	1.82	26.9
81	2202.38	2	SLE R	-18004.90	-12.67	-410.82	0.00	78.54	1.68	24.8
82	2261.90	2	SLE R	-16889.10	-9.18	-297.63	0.00	78.54	1.53	22.6
83	2321,43	2	SLE R	-15774.20	-5.76	-186.90	0.00	78.54	1,38	20.5
84	2380.95	2	SLE R	-14660.20	-2.83	-91.71	0.00	78.54	1.24	18.5
85	2440.48	2	SLE R	-13546.90	-0.77	-25.09	0.00	78.54	1.11	16.6
86	2500.00	2	SLE R	-12434.40	0.00	0.00	0.00	78.54	1.01	15.1
87	0.00	4	SLE Q	-52487.40	1421.61	46089.20	43,98	34.56	44,82	1034.2
88	59.52	4	SLE Q	-53330.60	1504.08	48762.90	47.12	31.42	47.57	1121.6
89	119.05	4	SLE Q	-53335.90	1554.49	50397.20	47.12	31.42	49.28	1181.5
90	178.57	4	SLE Q	-53342.80	1577.50	51143.20	47.12	31.42	50.06	1208.9
91	238.09	4	SLE Q	-53351.40	1577.41	51140.20	47,12	31,42	50.05	1208.7
.92	297.62	4	SLE Q	-53361.60	1558.14	50515.50	47.12	31,42	49.40	1185.5
93	357.14	- 4	SLE Q	-53373.60	1521.79	49337.20	47.12	31.42	48.17	1142.1
94	416.67	4	SLE Q	-52199.60	1466.04	47529.70	47.12	31.42	46.35	1090.5
95	476.19	4	SLE Q	-51028.50	1393.92	45191.40	43.98	34.56	43.98	1019.5
96	535.71	4	SLE Q	-49860.10	1309.70	42461.20	43,98	34.56	41.19	934.3
97	595.24	4	SLE Q	-48694.30	1217.13	39460.00	43.98	34.56	38.12	839.6
98	654.76	4	SLE Q	-47531.20	1119.41	36291.90	43,98	34.56	34.86	739.4
99	714.29	4	SLE Q	-46370.70	1019.28	33045.40	43.98	34.56	31.51	637.2
1.00	773.81	4	SLE Q	-45212.60	919.00	29794.40	43.98	34.56	28.15	536.1
101	833.33	4	SLE Q	-44056.90	820,46	26599.60	43.98	34.56	24.84	438.7
102	892,86	4	SLE Q	-42903.60	725.16	23509.90	40.84	37,70	21,65	347.5
103	952.38	4	SLE Q	-41752.60	634.28	20563.60	37.70	40.84	18.62	264.5
104	1011.90	4	SIE Q	-40603.90	548.72	17789.80	37,70	40.84	15.80	216.0
105	1071.43	4	SLE Q	-39457.30	469.12	15209.10	34.56	43.98	13.26	182.7
106	1130,95	4	SLE Q	-38312.80	395.90	12835.20	31.42	47.12	11,04	153.4
107	1190.48	4	SLE Q	-37170.40	329.29	10675.70	28.27	50.27	9.18	128.6
108	1250.00	4	SLE Q	-36030.00	269.38	8733.29	21.99	56.55	7.69	108.5
109	1309.52	4	SLE Q	-34891.50	216.10	7006.09	12,57	65.97	6,51	92.4
110	1369.05	4	SLE Q	-33754.90	169.30	5488.93	0.00	78.54	5.58	79.8
111	1428.57	_		-32620.10		4173.81	0.00	78.54	4,81	69.1
112	1488.10	_		-31487.10				78.54		59.8
113	1547.62			-30355.70		2107.36	0.00	78.54	3.56	51.8
	1607.14	_		-29226.00		1331,14	0.00	78.54		45.0
115	1666.67	_		-28097.80			_	78.54	2,65	39.2
	1726.19	_	_	-26971.20				78.54	2.31	34.4
	1785.71	_		-25846.00		-136.75		78.54	2,17	32.4
118	1845.24			-24722.10			0.00	78.54	2.21	32.8
	1904.76	_		-23599.60		-	THE RESIDENCE AND ADDRESS OF THE PERSON NAMED IN	78.54		32.5
	1964.29	_		-22478.40				78.54		31.7
121	2023.81	_		-21358.40				78.54	2.06	30.4
	2083.33			-20239.50				78.54	1,95	28.8
123	2142.86			-19121.70		-513.26	_	78.54	1,82	26.9
124	2202.38			-18004.90			_	78.54	1.68	24.8
125	2261.90			-16889.10			0.00	78.54	1.53	22.6
126	2321.43	4	SLE Q	-15774.20	-5.76	-186.90	0.00	78.54	1.38	20.5
	2380.95	_	SLE Q	-14660.20	-2.83	-91.71	0.00	78.54	1,24	18.5
128	2440.48	4	SLE Q	-13546.90	-0.77	-25.09	0.00	78.54	1.11	16.6
THE RESERVE	2500.00	1.0	CTP O	-12434.40	0.00	0.00	0.00	78.54	1.03	15.3

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c ∢mm>	s <mm></mm>	K 2	•eq	Δ _{SM}	A _s <cmq></cmq>	Ac eff <cmq></cmq>	σ _S <dan cmq=""></dan>	eam	Wk <mm></mm>
87	0.00	4	SLE Q	-52487.40	46089.20	1421.61	46.00	136.36	0.50	20.00	203,51	21.99	1226.11	1034.29	0.30	0.10
88	59,52	4	SLE Q	-53330.60	48762.90	1504.08	46.00	136.36	0.50	20.00	204,19	21.99	1233.59	1121,63	0.33	0.11
89	119.05	4	SLE Q	-53335.90	50397.20	1554.49	46.00	136.36	0.50	20.00	204.71	21.99	1239.35	1181.56	0.34	0.12
-90	178.57	4	SLE Q	-53342.80	51143.20	1577.50	45.00	136.36	0.50	20.00	204.94	21.99	1241.82	1208.92	0.35	0.12
91	238,09	4	SLE Q	-53351.40	51140.20	1577.41	46,00	136.36	0.50	20.00	204.93	21.99	1241.78	1208.70	0.35	0.12
92	297.62	4	SLE Q	-53361.60	50515.50	1558.14	46.00	136.36	0.50	20.00	204.74	21.99	1239.67	1185,59	0.35	0.12
93	357.14	4	SLE Q	-53373.60	49337.20	1521.79	46.00	136.36	0.50	20.00	204.37	21.99	1235.53	1142.16	0.33	0.12
94	416.67	4	SLE Q	-52199.60	47529.70	1466.04	46.00	136.36	0.50	20.00	204,12	21.99	1232.84	1090.55	0.32	0.11
95	476.19	4	SIE Q	-51028.50	45191.40	1393.92	46,00	136.36	0.50	20.00	203.66	21.99	1227.73	1019.54	0.30	0,10
96	535.71	4	SLE Q	-49860.10	42461.20	1309.70	46,00	136.36	0.50	20.00	202.97	21.99	1220.14	934.36	0.27	0.09

							R	elazio	ne o	di ca	lcolo					
97	595.24	4	SLE C	-48694.30	39460.00	1217.13	A 70 CO. C.					21.99	1209.87	839.65	0.24	0.08
98	654.76	4	SLE Q	-47531.20	36291.90	1119.41	46.00	136.36	0.50	20.00	200.81	21.99	1196.48	739.44	0.22	0.07
99	714.29	4	SLE C	-46370.70	33045.40	1019.28	46.00	136.36	0.50	20.00	217.13	18.85	1179.32	637.26	0.19	0.07
100	773.81	4	SIE C	-45212.60	29794.40	919.00	46.00	136.36	0.50	20.00	214.80	18.85	1157.38	536.14	0.16	0.06
101	833.33	4	SLE C	-44056.90	26599.60	820.46	46.00	136.36	0.50	20.00	211.80	18.85	1129.0B	438.76	0.13	0.05
102	892.86	4	SLE C	-42903.60	23509.90	725.16	46.00	136.36	0.50	20.00	207.90	18.85	1092.32	347.50	0.10	0.04
103	952.38	4	SLE C	-41752.60	20563.60	634.28	46.00	136.36	0.50	20.00	202.67	18.85	1043.07	264.50	0.08	0.03
104	1011.90	4	SLE C	-40603.90	17789,80	548.72	46.00	136.36	0.50	20.00	195,55	18.85	975.93	191.77	0.06	0.02
105	1071.43	4	SLE Ç	-39457.30	15209.10	469.12	45.00	136.36	0.50	20.00	185.77	18.85	883.77	130.97	0.04	0.01
106	1130.95	4	SLE C	-38312.80	12835.20	395.90	46.00	136.36	0.50	20.00	210.93	12.57	747.26	83.11	0.02	0.01
107	1190.48	4	SLE Ç	-37170.40	10675.70	329.29	46.00	136,36	0.50	20.00	177.36	12.57	536.33	47.97	0.01	0.00
108	1250.00	4	SLE C	-36030.00	8733.29	269.38	46.00	136.36	0.50	20.00	193.75	6.28	319.65	23.77	0.01	0.00
130	0.00	3	SLE F	-52487.40	46089.20	1421.61	46.00	136.36	0.50	20.00	203,51	21.99	1226.11	1034.29	0.30	0.10
131	59.52	3	SLE F	-53330.60	48762.90	1504.08	46.00	136.36	0.50	20,00	204,19	21,99	1233.59	1121.63	0.33	0.11
132	119.05	3	SLE F	-53335.90	50397.20	1554.49	46.00	136.36	0.50	20.00	204.71	21.99	1239.35	1181.56	0.34	0.12
133	178.57	3	SLE F	-53342.80	51143.20	1577.50	46.00	136.36	0.50	20.00	204.94	21.99	1241.82	1208.92	0.35	0.12
134	238.09	3	SLE F	-53351.40	51140,20	1577.41	46.00	136.36	0.50	20,00	204.93	21.99	1241.78	1208.70	0.35	0.12
135	297.62	3	SLE F	-53361.60	50515.50	1558.14	46.00	136.36	0.50	20.00	204.74	21.99	1239.67	1185.59	0.35	0,12
136	357.14	3	SLE F	-53373.60	49337.20	1521.79	46,00	136.36	0.50	20.00	204.37	21.99	1235.53	1142,16	0.33	0.12
137	416.67	3	SLE F	-52199.60	47529.70	1466.04	46.00	136.36	0.50	20.00	204.12	21.99	1232.84	1090.55	0.32	0.11
138	476.19	3	SLE F	-51028.50	45191.40	1393.92	46.00	136.36	0.50	20.00	203.66	21.99	1227.73	1019.54	0.30	0.10
139	535.71	3	SLE F	-49860,10	42461.20	1309.70	46.00	136.36	0.50	20.00	202.97	21.99	1220.14	934.36	0.27	0.09
140	595.24	.3	SLE F	-48694.30	39460.00	1217.13	46.00	136.36	0.50	20.00	202.03	21.99	1209.87	839,65	0.24	0.08
141	654.76	3	SLE F	-47531.20	36291.90	1119.41	46.00	136.36	0.50	20.00	200.81	21.99	1196.4B	739.44	0.22	0.07
142	714.29	3	SLE F	-46370.70	33045,40	1019.28	46.00	136.36	0.50	20.00	217.13	18.85	1179.32	637.26	0.19	0.07
143	773.81	3	SLE F	-45212.60	29794.40	919.00	46,00	136.36	0.50	20,00	214.80	18.85	1157.38	536.14	0.16	0.06
144	833,33	3	SLE F	-44056.90	26599.60	820.46	46.00	136.36	0.50	20.00	211.80	18.85	1129.08	438.76	0.13	0.05
145	892.86	3	SLE F	-42903.60	23509.90	725.16	46.00	136.36	0.50	20.00	207.90	18.85	1092.32	347.50	0.10	0.04
146	952.38	3	SLE F	-41752.60	20563.60	634.28	-	136.36	0.50	20.00	202.67	18.85	1043.07	264.50	0.08	0.03
147	1011,90	3	-	-40603.90	17789,80	548.72	46.00	136.36	0.50	20.00	195,55	18.85	975.93	191.77	0.06	0.02
148	1071.43	3		-39457.30	15209.10	469.12		136.36	0.50	20.00	185.77	18.85	883.77	130.97	-	0.01
149	1130.95	_	SLE F	-38312.80	12835.20	395.90			0.50	20.00	210.93		747.26	83.11	_	0.01
150	1190.48	3	SLE F	-37170.40	10675.70	329.29		136.36	0.50	20.00	177.36	12.57	536.33	47.97	-	0.00
151	1250.00	3	SLE F	-36030.00	8733.29	269.38	46.00	136.36	0.50	20.00	193.75	6.28	319.65	23,77	0.01	0.00

Verifiche principali

Caso	Tipo
.5	SLU N cost - min, sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
.68	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
111	C.Q.Per Sc max (min. compr.)
133	C.Freq - Nk Max

Palo n. 12

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <om></om>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	8450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 12 (-4)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	9426.53	7683.84	135.90	55210.30	270.25
	1	SLU	TAG				0.00	0.00
	1	SIA	ECC				0.00	0.00
	1	SLU	TOT	9426.53	7683.84	135,90	55210.30	270,25
-2	2	SLE R	RVN	6982.62	5691.73	100.67	40896.50	200.19
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	6982.62	5691.73	100.67	40896.50	200.19
3	. 3	SLE F	RVN	6982.62	5691.73	100.67	40896.50	200.19
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	6982.62	5691.73	100.67	40896.50	200.19
4	4	SLE Q	RVN	6982.62	5691.73	100.67	40896.50	200.19

L	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00
Е	4	SLE Q	TOT	6982.62	5691.73	100.67	40896.50	200.19

Sollecitazioni nei pali

Caso	cc	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SIJJ	1	-9426.53	-7683.84	-135.90	-55210.30	-270.25
2	2	SLE R	1	-6982.62	-5691.73	-100.67	-40896.50	-200.19
3	. 3	SLE F	1	-6982.62	-5691.73	-100.67	-40896.50	-200.19
4	4	SLE Q	- 1	-6982.62	-5691.73	-100.67	-40896.50	-200.19

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	oc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-9426.53	54964.30	-269.05	-9426.53	150746.00	335.48	2-3	180.00	2,74
.2	59.52	1	SIJ	-10569.10	58801.60	-287.83	-10569.10	151231.00	306.90	2-3	180.00	2.57
- 3	119.05	1	SIAI	-11171.70	61298.50	-300.05	-11171.70	151485.00	291.90	2-3	180.00	2.47
4	178.57	1	SIJ	-11774.50	62645.40	+306.65	-11774.50	151740.00	276.77	2-3	180.00	2,42
- 5	238.09	1	SIJJ	-12377.80	63018.50	-30B.47	-12377.80	151995.00	261.59	2-3	180.00	2.41
- 6	297.62	1	SLU	-12981.40	62579.30	-306.32	-12981.40	152251.00	246.36	2-3	180.00	2.43
7	357.14	1	SIAI	-13585.50	61411.70	-300.61	-13585.50	152506.00	231,08	2-3	180.00	2,48
8	416.67	1	SIJ	-13422.70	59410.40	-290.81	-13422.70	152437.00	235.20	2-3	180.00	2.56
9	476.19	1	SLU	-13260.70	56698.60	-277.54	-13260.70	152369.00	239.30	2-3	180.00	2.68
10	535.71	1	SIU	+13099.30	53454.80	-261.66	-13099.30	152301.00	243.38	2-3	180.00	2.84
11	595.24	1	SIAI	-12938.70	49834.80	-243.94	-12938.70	152233.00	247.44	2-3	180.00	3.05
12	654.76	1	SLU	-12778,80	45973.10	-225.04	-12778.80	152165.00	251,48	2-3	180.00	3.31
13	714.29	1	SLU	-12619.50	41984.50	-205.51	-12619.50	152097.00	255.50	2-3	180.00	3,62
14	773.81	-1	SLU	-12461.00	37965.30	-185.84	-12461.00	152030.00	259,49	2-3	180.00	4.00
15	833.33	1	SIJ	-12303.10	33995.20	-166.41	-12303.10	151964.00	263.47	2-3	180.00	4.47
1.6	892.86	1	SIAI	-12145.80	30138.60	-147.53	-12145.80	151897.00	267,43	2-3	180.00	5.04
17	952,38	1	SLU	-11989.20	26446.70	-129.46	-11989.20	151831.00	271.37	2-3	180.00	5.74
18	1011.90	1	SLU	-11833,30	22958.50	-112,38	-11833.30	151765.00	275,29	2-3	180.00	6.61
19	1071.43	1	SLU	-11678.00	19702.30	-96.44	-11678.00	151699.00	279.19	2-3	180.00	7.69
20	1130.95	1	SILI	-11523.30	16697.60	-81.73	-11523.30	151633.00	283.08	2-3	180.00	9.08
21	1190.48	1	SIJ	-11369.20	13955.90	-68,31	-11369.20	151568.00	286,94	2-3	180.00	10.86
22	1250.00	1	SLU	-11215.80	11482.00	-56,20	-11215.80	151503.00	290.79	2-3	180.00	13.19
23	1309.52	1	SLU	-11062.90	9275.10	-45.40	-11062.90	151439.00	294.62	2-3	180.00	16.32
24	1369,05	1	SIU	-10910.60	7330.07	-35.88	-10910,60	151374.00	298,41	2-3	180.00	20.65
25	1428.57	1	SIJ	-10759.00	5637.89	-27.60	-10759.00	151311.00	302,19	2-3	180,00	26.83
26	1488.10	1	SIU	-10607.90	4186.68	-20.49	-10607.90	151247.00	305.94	2-3	180,00	36,12
.27	1547.62	1	SLU	-10457.30	2962.34	-14,50	-10457.30	151184.00	309,68	2-3	180.00	51.03
28	1607.14	1	SLU	-10307.40	1949.06	-9.54	-10307.40	151121.00	313,40	2-3	180.00	77.53
29	1656.67	1	SIAI	-10158.00	1129.90	~5.53	-10158.00	151058.00	317.10	2-3	180.00	>100
30	1726.19	1	SIAJ	-10009,10	487.12	-2.38	-2571250.00	150995.00	320.80	2-3	180,00	>100
31	1785,71	1	SLU	-9860,74	2.54	-0.01	-2571250.00	150933.00	324,47	2-3	180.00	>100
32	1845.24	1	SLU	-9712.94	-342.19	1.68	-2571250.00	-150871.00	328.12	2-3	0.00	>100
33	1904.76	1	SIAI	-9565.65	-565.45	2.77	-9565.65	-150807.00	331.88	2-3	0.00	>100
34	1964.29	1	SIJ	-9418.88	-685.46	3,36	-9418.88	-150742.00	335.67	2-3	0.00	>100
35	2023.81	1	SIU	-9272.61	-720.20	3.53	-9272.61	-150680.00	339.31	2-3	0.00	-
36	2083.33	1	SLU	-9126.84	-687,39	3,36	-9126.84	-150619.00	342.93	2-3	0.00	>100
37	2142.86	1	SLU	-8981.56	-604.47	2.96	-8981.56	-150557.00	346.53	2-3	0.00	>100
38	2202.38	1	SLU	-8836.76	-488.56	2.39	-2571250.00	-150496.00	350.13	2-3	0.00	>100
39	2261.90	1	-	-8692.44	-356.58	1.75	-2571250.00	-150435.00	353.70	2-3	0.00	>100
40	2321.43	1	SIJ	-8548.58	-225.22	1.10	-2571250.00	-150374.00	357.27	2-3	0.00	>100
41	2380.95	1	SLU	-8405.18	-111.03	0.54	-2571250.00	-150313.00	360.82	2-3	0.00	>100
42	2440.48	1	SLU	-8262.23	-30.49	0.15	-2571250.00	-150253.00	364.36	2-3	0.00	>100
43	2500.00	1	SLU	-8119.73	0.00	0.00	-2571250.00	3				>100

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
- 1	0.00	1	SIJ	7683.84	135.90	0.85	11.31	7685.04	1.00	32294.70	333018.00	32294.70	4.202
- 2	59.52	1	SLU	5264.69	93.12	0.85	11.31	5265.51	1.00	32294.70	333182.00	32294.70	6.133
3	119.05	316	SEU	3177.03	56.19	0.85	11.31	3177.53	1.00	32294.70	333268.00	32294.70	10.164
-4	178.57	1	SIJ	1397.33	24.71	0.85	11.31	1397.55	1.00	32294.70	333355.00	32294.70	23.108
5	238.09	1	SLU	-98.71	-1.75	0.85	11.31	98.72	1.00	32294.70	333441,00	32294.70	>100
.6	297.62	1	SLU	-1335.70	-23.62	0.85	11.31	1335.90	1.00	32294.70	333528.00	32294.70	24.174
7	357.14	1	SLU	-2655.44	-46.97	0.85	11.31	2655.86	1.00	32294.70	333614.00	32294.70	12,160
.8	416.67	1	SIAI	-4011.71	-70.95	0.85	11.31	4012.34	1,00	32294.70	333591.00	32294.70	8.049
. 9	476,19	1	SLU	-5048.71	-89.30	0.85	11.31	5049.50	1,00	32294.70	333568.00	32294.70	6.396
10	535.71	1	SIU	-5805.34	-102.68	0.85	11.31	5806.24	1.00	32294.70	333544.00	32294.70	5.562
11	595.24	1	SLU	-6318.49	-111.75	0.85	11.31	6319.48	1.00	32294.70	333521,00	32294.70	5.110
12	654.76	1	SLU	-6622.75	-117.14	0.85	11.31	6623.78	1.00	32294.70	333498.00	32294.70	4.876

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13	714.29	1	SLU	-6750.17	-119.39	0.85	11.31	6751.23	1.00	32294.70	333476.00	32294.70	4,784
14	773.81	1	SLU	-6730.19	-119.03	0.85	11.31	6731.25	1.00	32294.70	333453.00	32294.70	4.798
15	833.33	1	SIJ	-6589.54	-116.55	0.85	11.31	6590.58	1.00	32294.70	333430.00	32294.70	4.900
16	892.86	1	SIJ	-6352.28	-112.35	0.85	11.31	6353.28	1.00	32294.70	333408.00	32294.70	5.083
17	952.38	1	SLU	-6039.84	-106.83	0.85	11.31	6040.78	1.00	32294.70	333385.00	32294.70	5.346
18	1011.90	1	SLU	-5671.11	-100,30	0.85	11.31	5672.00	1.00	32294.70	333363.00	32294.70	5.694
19	1071.43	1	SLU	-5262.60	+93.08	0.85	11.31	5263.42	1.00	32294.70	333341.00	32294.70	6,136
20	1130.95	1	SIJ	-4828,54	-85.40	0.85	11.31	4829.30	1.00	32294.70	333319.00	32294.70	6.687
21	1190.48	1	SLU	-4381.08	-77.49	0.85	11.31	4381.76	1.00	32294.70	333297.00	32294.70	7.370
22	1250.00	1	SIJ	-3930.42	-69.52	0.85	11.31	3931.04	1.00	32294.70	333275.00	32294.70	8.215
23	1309.52	1	SLU	-3485.05	-61.64	0.85	11.31	3485.59	1,00	32294.70	333253.00	32294.70	9.265
24	1369.05	1	SLU	-3051.87	-53.98	0.85	11.31	3052.34	1.00	32294.70	333231.00	32294.70	10.580
25	1428,57	1	SIJJ	-2636.39	-46.63	0.85	11.31	2636.80	1.00	32294.70	333209.00	32294.70	12.248
26	1488.10	1	SLU	-2242.93	-39.67	0.85	11.31	2243.28	1.00	32294.70	333188,00	32294.70	14.396
27	1547.62	1	SLU	-1874.73	-33.16	0.85	11.31	1875.02	1.00	32294.70	333166.00	32294.70	17.224
28	1607.14	1	SIJ	-1534.15	-27.13	0.85	11.31	1534.39	1.00	32294.70	333145.00	32294.70	21.047
29	1666.67	1	SIJ	-1222.82	-21.63	0.85	11.31	1223.01	1.00	32294.70	333123.00	32294.70	26.406
30	1726.19	1	SLU	-941.72	-16.66	0.85	11.31	941.86	1.00	32294.70	333102.00	32294.70	34.288
31	1785.71	1	SLU	-691.37	-12.23	0.85	11,31	691.48	1.00	32294.70	333081.00	32294.70	46,704
33	1845,24	1	SIU	-471.92	-8.35	0.85	11.31	471.99	1.00	32294.70	333059.00	32294.70	68.422
33	1904.76	1	SLU	-283.23	-5.01	0.85	11.31	283.27	1.00	32294.70	333038.00	32294.70	>100
34	1964.29	1	SIJ	-124.97	-2.21	0.85	11.31	124.99	1.00	32294.70	333017.00	32294.70	>100
35	2023.81	1	SIJ	3.29	0.06	0.85	11.31	3.29	1.00	32294.70	332996.00	32294.70	>100
36	2083.33	1	SLU	102.04	1.80	0.85	11.31	102.06	1.00	32294.70	332975.00	32294.70	>100
37	2142.86	1	SLU	171.76	3.04	0.85	11.31	171.79	1.00	32294.70	332955.00	32294.70	>100
38	2202.38	1	SLU	212.90	3.77	0.85	11.31	212.93	1.00	32294.70	332934.00	32294.70	>100
39	2261.90	1	SLU	225.83	3.99	0.85	11.31	225.87	1.00	32294.70	332913.00	32294.70	>100
40	2321.43	1	SEU	210.84	3.73	0.85	11.31	210.88	1.00	32294.70	332893.00	32294.70	>100
41	2380.95	1	SIA	168.15	2.97	0.85	11.31	168.17	1.00	32294.70	332872.00	32294.70	>100
42	2440.48	1	SIJ	97.85	1.73	0.85	11.31	97.86	1.00	32294.70	332852.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	oc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <mq></mq>	AfC <cmq></cmq>	σ ₀ <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-6982.62	-199.29	40714.30	50.27	28.27	41.26	1446.08
45	59.52	2	SLE R	-8142.20	-213.21	43556.70	50.27	28.27	44.14	1537.43
46	119.05	2	SLE R	-8778.63	-222.26	45406.30	50.27	28.27	46.01	1598.53
47	178.57	2	SLE R	-9415.33	-227.15	46404.00	50,27	28.27	47.01	1627.33
48	238.09	2	SLE R	-10052.30	-228.50	46680.40	50.27	28.27	47.28	1628.7
49	297.62	2	SLE R	-10689.60	-226.91	46355.00	50.27	28.27	46,94	1607.2
50	357,14	2	SLE R	-11327.30	-222.67	45490.20	50,27	28.27	46+05	1565.3
51	416.67	2	SLE R	-11221.90	-215.42	44007.70	50.27	28,27	44.55	1510.5
52	476,19	2	SLE R	-11117.10	-205.58	41998.90	50.27	28.27	42.51	1435.83
53	535,71	2	SLE R	-11013.00	-193.82	39596.10	50,27	28.27	40.06	1346.1
54	595.24	2	SLE R	-10909.40	-180.70	36914.60	50.27	28.27	37,34	1245.89
55	654.76	2	SLE R	-10806.40	-166,69	34054.20	50.27	28.27	34.43	1138.8
56	714.29	2	SLE R	-10704.00	-152.23	31099.60	50.27	28.27	31.42	1028.25
57	773.81	2	SLE R	-10602.10	-137.66	28122.40	50.27	28.27	28.39	916.83
58	833.33	2	SLE R	-10500.90	-123,26	25181,60	50.27	28.27	25.40	806.8
59	892.86	2	SLE R	-10400.20	-109.28	22324.90	50.27	28.27	22.48	700.1
50	952.38	2	SLE R	-10300.00	-95.89	19590.20	50.27	28.27	19.69	598.0
61	1011.90	2	SLE R	-10200.40	-83.25	17006.30	50.27	28.27	17.04	501.9
62	1071.43	2	SLE R	-10101.40	-71.44	14594.30	50.27	28.27	14.57	412.4
63	1130.95	2	SLE R	-10002.80	-60.54	12368.60	47.12	31.42	12,28	330.2
64	1190.48	2	SLE R	-9904.88	-50.60	10337.70	47.12	31.42	10.17	255.8
65	1250.00	2	SLE R	-9807.43	-41.63	8505.15	47.12	31.42	8.26	189.6
.66	1309.52	2	SLE R	~9710.52	-33.63	6870.45	43.98	34.56	6.55	131.8
67	1369.05	2	SLE R	-9614.12	-26.58	5429.68	40.84	37.70	5,02	83.3
68	1428.57	2	SLE R	-9518.24	-20.44	4176.21	37.70	40.84	3.71	50.6
69	1488.10	2	SLE R	-9422.87	-15.18	3101.25	31.42	47.12	2.67	37.0
70	1547.62	2	SLE R	-9328.01	-10.74	2194.32	21.99	56.55	1.94	27.4
71	1607.14	2	SLE B	-9233.64	-7.07	1443.75	0.00	78.54	1.50	21.4
72	1666.67	2	SLE R	-9139.78	-4.10	836.96	0.00	78.54	1.18	17.00
73	1726.19	2	SLE R	-9046.40	-1.77	360.83	0.00	78.54	0.92	13.5
74	1785.71	2	SLE R	-8953.50	+0.01	1.88	0.00	78.54	0.73	10.9
75	1845,24	-2	SLE R	-8861.09	1.24	-253.4B	0.00	78.54	0.85	12.5
7.6	1904.76	2	SLE R	-8769,15	2.05	-418.85	0.00	78,54	0.93	13.6
77	1964.29	2	SLE R	-8677.69	2.49	-507.75	0.00	78.54	0.97	14.1
78	2023.81	2	SLE R	-8586.68	2.61	-533.48	0.00	78.54	0.97	14.2
79	2083.33	2	SLE R	-8496.14	2.49	-509.18	0.00	78.54	0.95	13.9
80	2142.86	2	SLE R	-8406.06	2.19	-447.75	0.00	78.54	0.92	13.40
81	2202,38	2	SLE R	-8316.42	1.77	-361.90	0.00	78.54	0.86	12.6
82	2261,90	2	SLE R	-8227.23	1.29	-264.13	0.00	78.54	0.81	11.8
83	2321.43	2	SLE R	-8138.49	0.82	-166.83	0.00	78.54	0.75	11.1
84	2380.95	2	SLE R	-8050.18	0.40	-82.25	0.00	78.54	0.70	10.3
85	2440.48	2	SLE R	-7962.30	0.11	-22.59	0.00	78.54	0.66	9.8
86	2500.00	2	SLE R	-7874.85	0.00	0.00	0.00	78.54	0.64	9.60

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87	0.00	4	SLE	Q	-6982.62	-199,29	40714.30	50.27	28.27	41,26	1446.08
88	59.52	4	SLE	Q	-8142.20	-213.21	43556.70	50.27	28.27	44.14	1537.41
89	119.05	4	SLE	Q	-8778.63	-222.26	45406.30	50.27	28.27	46.01	1598.53
90	178.57	4	SLE	Q	-9415.33	-227.15	46404.00	50.27	28.27	47,01	1627.31
91	238.09	4	SLE	Q	-10052.30	-228.50	46680.40	50.27	28.27	47.28	1628.71
92	297.62	4	SLE	Q	-10689.60	-226.91	46355.00	50.27	28.27	46.94	1607.27
93	357.14	4	SLE	Q	-11327.30	-222.67	45490.20	50.27	28.27	46,05	1565.36
94	416.67	4	SLE	Q	-11221.90	-215.42	44007.70	50.27	28.27	44,55	1510.59
95	476.19	4	SLE	Q	-11117.10	-205.58	41998.90	50.27	28.27	42.51	1435.85
96	535.71	4	SLE	Q	-11013.00	-193.82	39596.10	50.27	28,27	40.06	1346.15
97	595.24	4	SLE	Q	-10909.40	-180.70	36914.60	50.27	28.27	37.34	1245.89
.98	654.76	4	SLE	Q	-10806.40	-166.69	34054.20	50.27	28.27	34.43	1138.84
99	714.29	4	SLE	Q	-10704.00	-152.23	31099.60	50.27	28.27	31.42	1028.25
100	773,81	4	SLE	Q	-10602.10	-137,66	28122.40	50.27	28.27	28,39	916.83
101	833.33	4	SLE	Q	-10500.90	-123.26	25181.60	50.27	28.27	25.40	806.84
102	892.86	4	SLE	Q	-10400.20	-109.28	22324.90	50.27	28.27	22.48	700.11
103	952,38	4	SLE	Q	-10300.00	-95.89	19590.20	50,27	28,27	19,69	598.09
104	1011.90	4	SLE	Q	-10200.40	-83.25	17006.30	50.27	28,27	17.04	501.92
105	1071.43	4	SLE	Q	-10101.40	-71.44	14594.30	50.27	28.27	14.57	412.44
106	1130.95	4	SLE	Q	-10002.80	-60.54	12368,60	47.12	31,42	12.28	330.28
107	1190.48	4	SLE	0	-9904.88	-50.60	10337.70	47.12	31.42	10.17	255.89
108	1250.00	4	SLE	Q	-9807.43	-41.63	8505.15	47.12	31.42	8,26	189.67
109	1309.52	4	SLE	Q	-9710.52	-33.63	6870.45	43.98	34.56	6.55	131.88
110	1369.05	4	SLE	Q	-9614.12	-26.58	5429.68	40.84	37.70	5.02	83.30
111	1428.57	4	SLE	Q	-9518.24	-20,44	4176.21	37.70	40.84	3.71	50.63
112	1488.10	4	SLE	Q	-9422.87	-15.18	3101.25	31.42	47.12	2,67	37.01
113	1547.62	- 6	SLE	Q	-9328.01	-10.74	2194.32	21.99	56.55	1.94	27.44
114	1607.14	4	SLE	Q	-9233.64	-7.07	1443.75	0.00	78.54	1.50	21.40
115	1666.67	4	SLE	Q	-9139.78	-4.10	836.96	0.00	78.54	1.18	17.02
116	1726.19	4	SLE	Q	-9046.40	-1.77	360.83	0.00	78.54	0.92	13.50
117	1785.71	4	SLE	Q	-8953.50	-0.01	1.88	0.00	78.54	0.73	10.93
118	1845,24	4	SLE	Q	-8861.09	1.24	-253.48	0.00	78.54	0.85	12.59
119	1904.76	4	SLE	Q	-8769.15	2.05	-418.85	0.00	78.54	0.93	13.64
120	1964.29	4	SLE	Q	-8677.59	2.49	-507.75	0.00	78.54	0,97	14.1
121	2023.81	4	SIE	0	-8586.68	2.61	-533.48	0.00	78.54	0.97	14.22
122	2083,33	4	SLE	0	-8496.14	2.49	-509.18	0.00	78.54	0,95	13.94
123	2142.86	4	SLE	Q	-8406.06	2.19	-447.75	0.00	78,54	0.92	13.40
124	2202.38	4	SLE	Q	-8316.42	1.77	-361.90	0.00	78.54	0.86	12.68
125	2261,90	4	SLE	Q	-8227.23	1.29	-264.13	0.00	78.54	0.81	11.89
126	2321.43	4	SLE	Q	-8138.49	0.82	-166.83	0.00	78.54	0.75	11.10
127	2380.95	4	SLE	Q	-8050.18	0.40	-82.25	0.00	78.54	0.70	10.39
128	2440.48	4	SLE	Q	-7962.30	0.11	-22.59	0.00	78.54	0.66	9.87
129	2500.00	_	SLE	Q		0.00	0.00		78.54	0.64	9.60

Stato limite	d'esercizio	- Verifiche a	fessurazione
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Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c ⊲mm>	s <mm></mm>	K 2	Фец	Δ _{SIII} <mm></mm>	A _{II} <cmq></cmq>	A _{c eff} <cmq></cmq>	σ _s <dan cmq=""></dan>	e _{ss}	Wk <mm></mm>
87	0.00	4	SLE (-6982.62	40714.30	-199.29	46.00	136.36	0.50	20.00	200.07	25.13	1358.00	1446.08	0.42	0.14
88	59,52	4	SLE (-8142.20	43556.70	-213.21	46.00	136.36	0.50	20.00	199,93	25.13	1356.29	1537.41	0.45	0.15
89	119.05	4	SLE (-8778.63	45406.30	-222.26	46,00	136.36	0.50	20.00	199.87	25.13	1355.58	1598.53	0.47	0.16
90	178.57	4	SIE (-9415.33	46404.00	+227.15	46.00	136.36	0.50	20.00	199.79	25.13	1354.51	1627.31	0.47	0.16
91	238.09	4	SLE (-10052.30	46680.40	-228.50	46.00	136.36	0.50	20.00	199.68	25.13	1353.11	1628.71	0.47	0.16
92	297.62	4	SLE (-10689.60	46355.00	-226.91	46.00	136.36	0.50	20.00	199.54	25.13	1351.39	1607.27	0.47	0.16
93	357.14	4	SLE (-11327.30	45490,20	-222.67	46.00	136.36	0.50	20,00	199,37	25.13	1349.29	1565.36	0.45	0.15
94	416.67	4	SLE (-11221.90	44007.70	-215.42	46.00	136.36	0.50	20.00	199.32	25.13	1348.61	1510.59	0.44	0.15
95	476,19	4	SLE (-11117.10	41998.90	-205.58	46.00	136,36	0.50	20.00	199.23	25.13	1347.50	1435.85	0.42	0.14
96	535.71	4	SLE (-11013.00	39596.10	-193.82	46,00	136.36	0.50	20.00	199.11	25.13	1345.95	1346.15	0.39	0,13
97	595.24	4	SLE (-10909.40	36914.60	-180.70	46.00	136.36	0.50	20.00	214.22	21.99	1343.93	1245.89	0.36	0.13
98	654.76	4	SLE (-10806.40	34054.20	-166.69	46.00	136.36	0.50	20.00	213.99	21.99	1341.39	1138.84	0.33	0.12
99	714.29	4	SLE (-10704.00	31099.60	-152.23	46.00	136.36	0.50	20.00	213.71	21.99	1338.22	1028.25	0.30	0.11
100	773.81	4	SLE (-10602.10	28122.40	-137.66	46,00	136.36	0.50	20.00	213.35	21.99	1334.30	916.83	0.27	0.10
101	833.33	4	SLE (-10500.90	25181.60	-123.26	46.00	136.36	0.50	20.00	212.91	21.99	1329,45	806.84	0.23	0.09
102	892.86	4	SLE (-10400.20	22324.90	-109.28	46,00	136.36	0.50	20.00	212,36	21.99	1323.41	700.11	0.20	0.07
103	952.38	4	SLE (-10300.00	19590.20	-95.89	46.00	136.36	0.50	20.00	211.67	21.99	1315.83	598.09	0.17	0.06
104	1011.90	4	SLE (-10200.40	17006.30	-83.25	46.00	136.36	0.50	20.00	210.79	21.99	1306.18	501.92	0.15	0.05
105	1071.43	4	SLE (-10101.40	14594.30	-71.44	46.00	136.36	0.50	20.00	209.66	21,99	1293.70	412,44	0.12	0.04
106	1130.95	4	SLE C	-10002.80	12368,60	-60.54	45.00	136.36	0.50	20.00	208.16	21,99	1277.19	330.28	0.10	0.03
107	1190.48	4	SLE (-9904.88	10337.70	-50.60	46.00	136.36	0.50	20.00	206.11	21.99	1254.68	255.89	0.07	0.03
108	1250.00	4	SLE (-9807.43	8505.15	-41.63	46.00	136.36	0.50	20.00	203.21	21.99	1222.82	189.62	0.06	0.02
109	1309.52	4	SLE (-9710.52	6870.45	-33.63	46.00	136.36	0.50	20.00	198.95	21.99	1175.93	131.88	0.04	0.01
110	1369.05	4	SLE (9514.12	5429.68	-26.58	46.00	136.36	0.50	20.00	209.08	18.85	1103.48	83.30	0.02	0.01
111	1428.57	4	SLE (-9518.24	4176,21	-20.44	46.00	136.36	0.50	20.00	195.51	18.85	975.58	45,20	0.01	0.00
112	1488.10	4	SLE (-9422.87	3101.25	-15.18	46.00	136.36	0.50	20.00	184,05	15.71	722.94	19,36	0.01	0.00
113	1547.62	4	SLE (-9328.01	2194.32	-10.74	46.00	136.36	0.50	20.00	182.39	6.28	283.96	5.40	0.00	0.00
130	0.00	3	SLE !	-6982.62	40714.30	-199.29	46.00	136.36	0.50	20.00	200.07	25.13	1358.00	1446.08	0.42	0.14
131	59.52	3	SLE I	-8142.20	43556.70	-213.21	46,00	136.36	0.50	20.00	199,93	25.13	1356.29	1537.41	0.45	0,15
132	119.05	3	SLE F	-8778.63	45406.30	-222.26	46,00	136.36	0.50	20.00	199.87	25.13	1355.58	1598.53	0.47	0.16

							R	elazio	ne o	di ca	Icolo					
133	178.57	3	SLE F	-9415.33	46404.00	-227.15	1 3 Land Control		CO COUNTY OF			25.13	1354.51	1627.31	0.47	0.16
134	238.09	3	SLE F	-10052.30	46680.40	-228.50	46.00	136.36	0.50	20.00	199.68	25.13	1353.11	1628.71	0.47	0.16
135	297.62	3	SLE F	-10689,60	46355.00	-226.91	46.00	136.36	0.50	20.00	199,54	25.13	1351.39	1607.27	0.47	0.16
136	357.14	3	SLE F	-11327.30	45490.20	-222.67	46.00	136.36	0.50	20.00	199.37	25.13	1349.29	1565.36	0.46	0.15
137	416.67	3	SLE F	-11221.90	44007.70	-215.42	46.00	136.36	0.50	20.00	199,32	25.13	1348.61	1510.59	0.44	0.15
138	476.19	3	SLE F	-11117.10	41998.90	-205.58	46.00	136.36	0.50	20.00	199.23	25.13	1347.50	1435.85	0.42	0.14
139	535.71	3	SLE F	-11013.00	39596.10	-193.B2	46.00	136.36	0.50	20.00	199.11	25.13	1345.95	1346.15	0.39	0.13
140	595.24	3	SLE F	-10909.40	36914.60	-180,70	46.00	136.36	0.50	20.00	214,22	21.99	1343.93	1245.89	0.36	0.13
141	654.76	3	SLE F	-10806.40	34054.20	-166.69	45.00	136.36	0.50	20.00	213.99	21.99	1341.39	1138.84	0.33	0.12
142	714.29	3	SLE F	-10704.00	31099.60	-152.23	46.00	136.36	0.50	20.00	213.71	21.99	1338.22	1028.25	0.30	0.11
143	773.81	3	SLE F	-10602.10	28122.40	-137.66	46.00	136,36	0.50	20.00	213.35	21,99	1334.30	916.83	0.27	0.10
144	833.33	3	SLE F	-10500.90	25181.60	-123.26	46.00	136.36	0.50	20.00	212.91	21.99	1329.45	806.84	0.23	0.09
145	892.86	3	SLE F	-10400.20	22324.90	-109.28	46.00	136.36	0.50	20.00	212.36	21.99	1323,41	700.11	0.20	0.07
146	952,38	3	SLE F	-10300.00	19590,20	-95.89	46.00	136.36	0.50	20,00	211,67	21.99	1315.83	598,09	0.17	0.06
147	1011.90	3	SLE F	-10200.40	17006.30	-83.25	46.00	136.36	0.50	20.00	210.79	21.99	1306.18	501.92	0.15	0.05
148	1071.43	3	SLE F	-10101.40	14594.30	-71.44	46.00	136.36	0.50	20.00	209,66	21.99	1293.70	412.44	0.12	0.04
149	1130,95	3	SLE F	-10002.80	12368.60	-60.54	46,00	136.36	0.50	20.00	208.16	21.99	1277.19	330.28	0.10	0.03
150	1190.48	3	SLE F	-9904.88	10337.70	-50.60	46.00	136.36	0.50	20.00	206.11	21.99	1254.68	255.89	0.07	0.03
151	1250.00	3	SLE F	-9807.43	8505.15	-41.63	46,00	136.36	0.50	20.00	203,21	21.99	1222.82	189.62	0.06	0.02
152	1309.52	3	SLE F	-9710.52	6870.45	-33.63	46.00	136.36	0.50	20.00	198.95	21.99	1175.93	131.88	0.04	0.01
153	1369.05	3	SLE F	-9614.12	5429.68	-26.58	46.00	136.36	0.50	20.00	209,08	18.85	1103.48	83.30	0.02	0.01
154	1428.57	3	SLE F	-9518.24	4176.21	-20.44	46.00	136.36	0.50	20.00	195.51	18.85	975.58	45.20	0.01	0.00
155	1488,10	.3	SLE F	-9422.87	3101,25	-15.18	46.00	136.36	0.50	20.00	184.05	15.71	722.94	19.36	0.01	0.00
156	1547.62	3	SLE F	-9328.01	2194.32	-10.74	46.00	136.36	0.50	20.00	182.39	6.28	283.96	5.40	0.00	0.00

Verifiche principali

Caso	Tipo
- 1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
- 5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
71	C.Rare - Sc max (min. compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
114	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 13

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 13 (-3)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
- 1	1	SIJ	RVN	9469.03	7682.76	-135.61	55220.30	-169.49
	1	SLU	TAG	3 3		ž 5	0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SIAI	TOT	9469.03	7682.76	-135.61	55220.30	-169,49
-2	2	SLE R	RVN	7014.10	5690.93	-100.45	40903.90	-125.55
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC	3		1	0.00	0.00
	. 2	SLE R	TOT	7014.10	5690.93	-100.45	40903.90	-125.55
3	3	SLE F	RVN	7014.10	5690.93	-100.45	40903.90	-125.55
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	7014.10	5690.93	-100.45	40903.90	-125.55
4	4	SLE Q	RVN	7014.10	5690.93	-100.45	40903.90	-125.55
	4	SIE Q	TAG	9		. 8	0.00	0.00
	4	SLE Q	ECC	9			0.00	0.00
	4	SLE Q	TOT	7014.10	5690.93	-100.45	40903.90	-125.55

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-9469.03	-7682.76	135.61	+55220.30	169.49
- 2	2	SLE R	- 1	-7014.10	-5690.93	100.45	-40903.90	125.55
3	3	SLE F	- 1	-7014.10	-5690.93	100.45	~40903.90	125.55

72

Da 0 a -25

4 1 5 2 6 2 7 3 8 6 8 9 8 10 5 11 5 8 10 15 8 10 15 8 10 15 8 10 15 8 10 15 15 8 10 15 15 8 10 15 15 15 15 15 15 15 15 15 15 15 15 15	0.00 59.52 119.05 178.57 238.09 297.62 357.14 416.67 476.19 535.71 595.24 654.76 714.29 773.81 833.33 892.86	bet het test test test het het het test tes	SLU SLU SLU SLU SLU SLU SLU SLU SLU SLU	-9469.03 -10611.30 -11213.30 -11815.60 -12418.20 -13021.30 -13624.70 -13461.00 -13297.90 -13135.60 -12974.00	54974.30 58810.90 61307.20 62653.40 63025.80 62585.90 61417.60 59415.50 56703.10 53458.70	168,73 180,51 188,17 192,30 193,44 192,09 188,51 182,36 174,04 164,08	-9469.03 -10611.30 -11213.30 -11815.60 -12418.20 -13021.30 -13624.70 -13461.00	150764.00 151248.00 151502.00 151757.00 152012.00 152268.00 152523.00 152454.00	334.42 305.86 290.86 275.74 260.57 245.35 230.09	2-3 2-3 2-3 2-3 2-3 2-3 2-3	180.00 180.00 180.00 180.00 180.00 180.00	2.747 2.577 2.477 2.427 2.417 2.437 2.437
3 1 4 1 5 2 6 2 6 1 6 8 1 7 9 1 6 8 1 7 9 1 6 1 8 1 6 1 7 9 1 6 1 8 1 7 9 1 6 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7	119.05 178.57 238.09 297.62 357.14 416.67 476.19 535.71 595.24 654.76 714.29 773.81 833.33 892.86	bet has but the bet bet bet bet the the test test	SLU SLU SLU SLU SLU SLU SLU SLU SLU	-11213.30 -11815.60 -12418.20 -13021.30 -13624.70 -13461.00 -13297.90 -13135.60 -12976.00	61307.20 62653.40 63025.80 62585.90 61417.60 59415.50 53458.70	188.17 192.30 193.44 192.09 188.51 182.36 174.04	-11213.30 -11815.60 -12418.20 -13021.30 -13624.70 -13461.00	151502.00 151757.00 152012.00 152268.00 152523.00	290.86 275.74 260.57 245.35 230.09	2-3 2-3 2-3 2-3	180.00 180.00 180.00 180.00	2.47 2.42 2.41 2.43
4 1 5 2 6 6 6 7 5 6 6 6 7 6 7 6 7 6 7 6 7 6 7 6	178.57 238.09 297.62 357.14 416.67 476.19 535.71 595.24 654.76 714.29 773.81 833.33 892.86	per lies lies and lies lies lies has lies per per lies	SLU SLU SLU SLU SLU SLU SLU SLU	-11815.60 -12418.20 -13021.30 -13624.70 -13461.00 -13297.90 -13135.60 -12974.00	62653.40 63025.80 62585.90 61417.60 59415.50 56703.10 53458.70	192.30 193.44 192.09 188.51 182.36	-11815.60 -12418.20 -13021.30 -13624.70 -13461.00	151757.00 152012.00 152268.00 152523.00	275.74 260.57 245.35 230.09	2-3 2-3 2-3	180.00 180.00 180.00	2.42 2.41 2.43
5 2 6 2 7 3 8 6 8 9 6 10 5 11 5 8 10 15 8 10 15 8 10 15 8 10 15 8 10 15 16 8 17 9 10 10 10 10 10 10 10 10 10 10 10 10 10	238.09 297.62 357.14 416.67 476.19 535.71 595.24 654.76 714.29 773.81 833.33 892.86	***	SLU SLU SLU SLU SLU SLU SLU	-12418.20 -13021.30 -13624.70 -13461.00 -13297.90 -13135.60 -12974.00	63025.80 62585.90 61417.60 59415.50 56703.10 53458.70	193.44 192.09 188.51 182.36 174.04	-12418.20 -13021.30 -13624.70 -13461.00	152012.00 152268.00 152523.00	260.57 245.35 230.09	2-3	180.00 180.00	2.41
6 2 7 3 8 2 9 6 10 5 11 5 12 6 16 8 17 6 18 10 10 11 11 11 11 11 11 11 11 11 11 11	297.62 357.14 416.67 476.19 535.71 595.24 654.76 714.29 773.81 833.33 892.86	the ties that the ties that the	SLU SLU SLU SLU SLU SLU SLU	-13021,30 -13624,70 -13461,00 -13297,90 -13135,60 -12974,00	62585.90 61417.60 59415.50 56703.10 53458.70	192.09 188.51 182.36 174.04	-13021.30 -13624.70 -13461.00	152268.00 152523.00	245.35 230.09	2-3	180.00	2.43
7 3 8 4 9 4 10 5 11 5 8 16 8 17 8 16 18 10 12 12 12 12 12 12 12 12 12 12 12 12 12	357.14 416.67 476.19 535.71 595.24 654.76 714.29 773.81 833.33 892.86	1 1 1	SLU SLU SLU SLU SLU	-13624.70 -13461.00 -13297.90 -13135.60 -12974.00	61417.60 59415.50 56703.10 53458.70	188.51 182.36 174.04	-13624.70 -13461.00	152523.00	230.09	-		
8 4 9 4 10 5 11 5 8 16 8 17 5 18 10 19 10 20 11 22 12 23 13 24 13 25 14 26 14	416.67 476.19 535.71 595.24 654.76 714.29 773.81 833.33	1 1 1	SLU SLU SLU SLU SLU	-13461.00 -13297.90 -13135.60 -12974.00	59415.50 56703.10 53458.70	182.36 174.04	-13461.00			2-3	180.00	2.48
9 4 10 5 11 5 12 6 16 8 17 6 18 10 19 10 20 11 22 12 22 12 23 13 24 13 25 14 26 14 15 16 16 16 16 16 16 16 16 16 16 16 16 16	476.19 535.71 595.24 654.76 714.29 773,81 833.33	100	SLU SLU SLU	-13297.90 -13135.60 -12974.00	56703.10 53458.70	174.04		152454.00				
10 5 11 5 12 6 13 7 14 15 8 16 8 17 8 16 19 10 20 11 22 12 23 13 24 13 25 14 26 14 15 16 16 16 16 16 16 16 16 16 16 16 16 16	535.71 595.24 654.76 714.29 773.81 833.33 892.86	1 1 1	SLU SLU	-13135.60 -12974.00	53458.70		-13297.90		234,24	2-3	180.00	2.56
11 5 6 14 17 18 10 19 10 11 12 12 12 12 12 12 12 12 12 12 12 12	595.24 654.76 714.29 773.81 833.33	1	SLU SLU	-12974.00		164.08	the state of the state of the state of	152385.00	238.36	2+3	180.00	2.68
12 6 13 7 14 7 15 8 16 8 17 9 18 10 20 11 22 12 23 13 24 13 25 14 26 14	654.76 714.29 773.81 833.33 892.86	1	SLU			+0.4105	-13135.60	152316.00	242.46	2-3	180.00	2.84
13 7 14 7 15 8 16 8 17 3 18 10 20 11 22 12 23 13 24 13 26 14	714.29 773.81 833.33 892.86	1	_	10015 10	49838.10	152.97	-12974.00	152248.00	246.55	2-3	180.00	3.05
14 17 15 8 16 8 17 9 18 16 19 16 20 11 12 12 12 12 12 12 12 12 12 12 12 12	773,81 833,33 892.86	1	CTIT	-12813.10	45975.90	141.11	-12813.10	152179.00	250.61	2-3	180.00	3.31
15 8 16 8 17 9 18 10 19 10 20 11 21 11 22 12 23 13 24 13 25 14 26 16	833,33 892.86	-	+2-1,0,1	-12652.80	41986.80	128.87	-12652.80	152112.00	254.66	2-3	180.00	3,62
16 8 17 9 18 10 19 10 20 11 21 11 22 12 23 13 24 13 25 14 26 14	892.86		SIU	-12493,30	37967.20	116.53	-12493.30	152044.00	258.68	2-3	180.00	4.00
17 5 18 10 19 10 20 11 21 11 22 12 23 13 24 13 25 14 26 14		1.	SLU	-12334,40	33996.70	104.34	-12334.40	151977.00	262.68	2-3	180.00	4,47
18 10 19 10 20 11 21 11 22 12 23 13 24 13 25 14 26 14	057 39	1	SIU	-12176.20	30139.80	92.51	-12176.20	151910.00	266.67	2=3	180.00	5.04
19 10 20 11 21 11 22 12 23 13 24 13 25 14 26 14	246140	1	SIU	-12018.60	26447.60	81.17	-12018.60	151843.00	270.63	2-3	180.00	5.74
20 11 21 11 22 12 23 13 24 13 25 14 26 14	011,90	1	SIJ	-11861,70	22959.10	70.47	-11861.70	151777.00	274.58	2-3	180.00	6.61
21 11 22 12 23 13 24 13 25 14 26 14	071,43	1	SLU	-11705.40	19702.70	60.47	-11705.40	151711.00	278.50	2-3	180.00	7.70
22 12 23 13 24 13 25 14 26 14	130,95	_	SLU	-11549,70	16697,80	51.25	-11549.70	151645,00	282,42	2-3	180.00	9.08
23 13 24 13 25 14 26 14	190.48	-	SLU	-11394.70	13955.90	42.83	-11394.70	151579.00	286.30	2-3	180.00	10.86
24 13 25 14 26 14	250.00	1	SLU	-11240.30	11481.80	35,24	-11240.30	151514.00	290.18	2-3	180.00	13.19
25 14 26 14	309.52	1	SLU	-11086.40	9274.89	28.47	-11086.40	151449.00	294.03	2-3	180.00	16.32
26 14	369.05	1	SIU	-10933.20	7329.79	22.50	-10933.20	151384.00	297.86	2-3	180.00	20.65
	428.57	1	SLU	-10780.50	5637.55	17.30	-10780.50	151320.00	301.65	2-3	180.00	26,84
27 15	488,10		SIAI	-10628.50	4186.32	12.85	-10628.50	151256.00	305,43	2-3	180.00	36.13
_	547.62	_	SLU	-10477.00	2961.95	9.09	-10477.00	151192.00	309.19	2-3	180.00	51.04
_	607.14	_	SLU	-10326.00	1948.67	5.98	-10326.00	151128.00	312.94	2+3	180.00	77.55
_	666.67	1	SEU	-10175.70	1129.52	3.47	-10175.70	151065.00	316.66	2-3	180.00	>100
-	726.19	1	SIU	-10025.80	486.75	1.49	-2571250.00	151002.00	320.38	2-3	180.00	>100
	785.71	1	SIJ	-9876.52	2,20	0.01	-2571250.00	150939.00	324.08	2+3	180.00	>100
	845.24	1	SLU	-9727.75	-342.50	-1.05	-2571250.00	-150877.00	327.76	2-3	0.00	>100
_	904.76	_	SLU	~9579.50	-565.73	-1.74	-9579.50	-150813.00	331.51	2-3	0.00	>100
	964.29	1	SIA	-9431.77	-685.70	-2.10	-9431.77	-150748.00	335.35	2-3	0.00	>100
_	023.81	1	SIM	-9284.54	-720.40	-2.21	-9284.54	-150685.00	339.01	2-3	0.00	>100
-	083.33	-	SLU	-9137.81	-687.56	-2.11	-9137.81	-150623.00	342.66	2-3	0.00	>100
	142,86	_	SLU	-8991.57	-604,59	-1.86	-8991.57	-150561.00	346.29	2-3	0.00	>100
	202,38	_	SLU	-8845.81	-488.65	-1.50	-2571250.00	-150500.00	349.90	2-3	0.00	>100
_	261.90	_	SLU	-8700.53	-356.64	-1.09	-2571250.00	-150438.00	353.50	2-3	0.00	>100
_	321.43		SLU	-8555.71	-225.25	-0.69	-2571250.00	-150377.00	357.10	2-3	0.00	>100
-	380.95 440.48	1	SIJJ	-8411.36	-111.05	-0.34	-2571250.00	-150316.00	360.67	2-3	0.00	>100
42 24		1	SLU	-8267.44 -8123.98	-30.50	0.00	-2571250.00 -2571250.00	-150255.00	364.23	2-3	0.00	>100

Caso	X <cm></cm>	8	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7682,76	-135.61	0.85	11.31	7683.96	1.00	32294.70	333024,00	32294.70	4,203
- 2	59.52	1	SLU	5263.55	-92.91	0.85	11.31	5264.37	1.00	32294.70	333188.00	32294.70	6.135
- 3	119.05	1	SLU	3175.86	-56.06	0.85	11.31	3176.35	1.00	32294.70	333274.00	32294.70	10.167
4	178.57	1	SIJ	1396.14	-24.64	0.85	11.31	1396.36	1.00	32294.70	333361.00	32294.70	23.128
5	238.09	1	SLU	-99.90	1.76	0.85	11.31	99.92	1,00	32294.70	333447.00	32294.70	>100
.6	297,62	1	SLU	-1336.88	23.60	0.85	11.31	1337.08	1.00	32294.70	333533.00	32294.70	24.153
7	357.14	1	SIU	-2656,59	46.89	0.85	11.31	2657.00	1.00	32294.70	333620.00	32294.70	12.155
.8	416.67	1	SLU	-4012.80	70.83	0.85	11.31	4013.43	1.00	32294.70	333596.00	32294.70	8.047
. 9	476.19	1	SIU	-5049.74	89.14	0.85	11.31	5050.53	1.00	32294.70	333573.00	32294.70	6.394
10	535.71	1	SIU	-5806.30	102.49	0.85	11.31	5807.20	1.00	32294.70	333550.00	32294.70	5.561
11	595,24	1	SIU	-6319.38	111.55	0.85	11.31	6320.36	1.00	32294.70	333526.00	32294.70	5.110
12	654.76	1	SLU	-6623.56	116.92	0.85	11.31	6624.59	1.00	32294.70	333503.00	32294.70	4.875
13	714.29	1	SLU	-6750.91	119.16	0.85	11.31	6751.96	1.00	32294.70	333480.00	32294.70	4.783
14	773.81	1	SIJ	-6730.85	118.81	0.85	11.31	6731.90	1.00	32294.70	333458.00	32294.70	4.797
15	833.33	1	SLU	-6590.12	116.33	0.85	11.31	6591.15	1,00	32294.70	333435.00	32294.70	4.900
15	892.86	1	SLU	-6352.79	112.14	0.85	11.31	6353.78	1.00	32294.70	333412.00	32294.70	5.083
17	952,38	1	SLU	-6040.27	106.62	0.85	11.31	6041.21	1.00	32294.70	333390,00	32294.70	5.346
18	1011.90	1	SLU	-5671.48	100.11	0.85	11.31	5672.37	1.00	32294.70	333367.00	32294.70	5,693
19	1071.43	1	SIU	-5262.91	92.90	0.85	11.31	5263.73	1.00	32294.70	333345.00	32294.70	6.135
20	1130.95	1	SIU	-4828.80	85.24	0.85	11.31	4829.55	1.00	32294.70	333322.00	32294.70	6.687
21	1190.48	1	SLU	-4381.28	77.34	0.85	11.31	4381.97	1.00	32294.70	333300.00	32294.70	7.370
22	1250.00	1	SIU	-3930.58	69.38	0.85	11.31	3931.20	1.00	32294.70	333278.00	32294.70	8.215

23	1309.52	1	SLU	-3485.17	61.52	0.85	11.31	3485.71	1.00	32294.70	333256.00	32294.70	9.265
24	1369.05	1	SLU	-3051.95	53.87	0.85	11.31	3052.43	1.00	32294.70	333234.00	32294.70	10.580
25	1428.57	1	SIU	-2636.45	46.54	0.85	11.31	2636.86	1.00	32294.70	333212.00	32294.70	12.247
26	1488.10	1	SIJ	-2242.96	39.59	0.85	11.31	2243.31	1.00	32294.70	333190.00	32294.70	14.396
27	1547.62	1	SLU	-1874,73	33.09	0.85	11.31	1875.03	1.00	32294.70	333169.00	32294.70	17.224
28	1607.14	116	SLU	-1534.14	27.08	0.85	11.31	1534.38	1.00	32294.70	333147.00	32294.70	21.047
29	1666.67	1	SIU	-1222.79	21.58	0.85	11.31	1222.98	1.00	32294.70	333126.00	32294.70	26.407
30	1726.19	1	SLU	-941.67	16.62	0.85	11.31	941.82	1.00	32294.70	333104.00	32294.70	34,290
31	1785.71	14	SLU	-691.32	12.20	0.85	11.31	691.43	1.00	32294.70	333083.00	32294.70	46.707
32	1845.24	1	SIJ	-471.86	8.33	0.85	11.31	471.94	1.00	32294.70	333061.00	32294.70	68.430
33	1904.76	1	SLU	-283.17	5.00	0.85	11.31	283.21	1,00	32294.70	333040.00	32294.70	>100
34	1964.29	1	SLU	-124.90	2.20	0.85	11.31	124.92	1.00	32294.70	333019,00	32294.70	>100
35	2023,81	1	SIJ	3,36	-0.06	0.85	11.31	3,36	1.00	32294.70	332998.00	32294.70	>100
36	2083,33	1	SLU	102.10	-1.80	0.85	11.31	102.12	1.00	32294.70	332977,00	32294.70	>100
37	2142.86	1	SLU	171.82	-3.03	0.85	11.31	171.85	1.00	32294.70	332956.00	32294.70	>100
38	2202.38	1	SILI	212.95	-3.76	0.85	11.31	212.99	1.00	32294.70	332935.00	32294.70	>100
39	2261,90	1	SLU	225,88	-3.99	0.85	11.31	225.91	1.00	32294.70	332914.00	32294.70	>100
40	2321.43	1	SLU	210.88	-3.72	0.85	11.31	210.91	1.00	32294.70	332894.00	32294.70	>100
41	2380.95	1	SLU	168.17	-2.97	0.85	11.31	168.20	1.00	32294.70	332873.00	32294.70	>100
42	2440.48	1	SLU	97.86	-1.73	0.85	11.31	97.88	1.00	32294.70	332852.00	32294.70	>100

so X		œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <mq></mq>	AfC <cmq></cmq>	σ ₀ <dan cmq=""></dan>	σ _f
200	.00	2	SLE R	-7014.10	124.99	40721.70	50.27	28.27	41.27	1445,41
45 59.	-	2	_	-8173.46	133.71	43563.70	50,27	28.27	44.14	
46 119.	_	2	SLE R	-8809.45	139.38	45412.70	50,27	28.27	46.01	1597.79
47 17B.	-	2	SLE R	-9445.72	142.44	46409.90	50.27	28.27	47.02	1626.55
48 238.	-	2	SLE R	-10082.30	143.29	46685.80	50.27	28.27	47.29	1627.93
49 297.	_	2	SLE R	-10719.20	142.29	46359.90	50.27	28.27	46.95	1606.48
50 357.	14	2	SLE R	-11356.40	139.63	45494.50	50.27	28.27	46.06	1564.57
51 416.	67	2	SLE R	-11250.30	135.08	44011.50	50.27	28.27	44,55	1509.81
52 476.	19	2	SLE R	-11144.80	128.92	42002.30	50.27	28.27	42.51	1435.09
53 535.	71	2	SLE R	-11039.90	121.54	39599.00	50.27	28.27	40.07	1345.41
54 595.	24	- 2	SLE R	-10935.50	113.31	36917.10	50.27	28.27	37.34	1245.18
55 654.	76	2	SLE R	-10831.80	104.53	34056.30	50.27	28.27	34.43	1138,16
56 714.	29	2	SLE R	-10728.70	95.46	31101,40	50,27	28.27	31.42	1027.63
57 773.	81	2	SLE R	-10626.10	86.32	28123.80	50,27	28.27	28,39	916.23
58 833.	33	2	SLE R	-10524.10	77.29	25182.70	50.27	28.27	25.40	806.2
59 892.	86	2	SLE R	-10422.70	68.52	22325.80	50.27	28.27	22.48	699.58
60 952.	38	2	SLE R	-10321.80	60.13	19590.80	50.27	28.27	19.69	597.60
61 1011.	90	2	SLE R	-10221.40	52.20	17006.70	50.27	28.27	17.04	501.46
62 1071.	43	2	SLE R	-10121.70	44.79	14594.60	50.27	28.27	14.57	412.03
63 1130.	95	2	SLE R	-10022.40	37.96	12368.80	47.12	31.42	12.28	329.90
64 1190.	48	- 2	SLE R	-9923.74	31.73	10337.70	47.12	31.42	10.17	255.5
65 1250.	.00	2	SLE R	-9825.58	26.10	8505.07	47.12	31.42	8.26	189.3
66 1309.	52	2	SLE R	-9727.94	21.09	6870.29	43.98	34.56	6.54	131.6
67 1369.	.05	2	SLE R	-9630.82	16.66	5429.47	40.84	37.70	5.02	83.0
68 1428,	57	2	SLE R	-9534.22	12.82	4175.97	37.70	40.84	3.71	50.6
69 1488,	10	2	SLE R	-9438.14	9.52	3100.98	31.42	47.12	2.66	37.0
70 1547.	62	2	SLE R	-9342.56	6.73	2194.04	21.99	56.55	1.95	27.4
71 1607.	14	2	SLE R	-9247.48	4.43	1443.46	0.00	78.54	1.50	21.43
72 1666.	67	2	SLE R	-9152.89	2.57	836.68	0.00	78.54	1.18	17.0
73 1726.	19	2	SLE R	-9058.80	1.11	360.56	0.00	78.54	0.92	13.5
74 1785.	71	-2	SLE R	-8965.19	0.01	1.63	0.00	78.54	0.73	10.9
75 1845.	24	2	SLE R	-8872.06	-0.78	-253,71	0.00	78.54	0.85	12.6
76 1904.	76	2	SLE B	-8779.41	-1.29	-419.06	0.00	78.54	0.93	13.6
77 1964.	29	2	SLE R	-8687.23	-1.56	-507.92	0.00	78.54	0.97	14.10
78 2023.	81	2	SLE R	-8595,52	-1.64	-533.63	0.00	78.54	0.97	14.2
79 2083.	33	2	SLE R	-8504.27	-1.56	-509.30	0.00	78.54	0.95	13.9
80 2142.	86	2	SLE R	-8413.47	-1,37	-447.85	0.00	78.54	0.92	13.4
B1 2202.	38	2	SLE B	-8323,13	-1,11	-361.96	0.00	78.54	0.86	12.6
B2 2261.	90	2	SLE R	-8233.23	-0.81	-264.18	0.00	78.54	0.81	11.8
	43	2	SLE R	-8143.77	-0.51	-166.85	0.00	78.54	0.75	11,1
84 2380.	_	_	-			-				
_	_	_	-	-7966.16			-	-		_
				-7878.00			0+00			
				-7014.10						
88 59,	_			-8173.46						
89 119.	_			-8809.45					46,01	
				~9445.72					47.02	
91 238.	_	-	-	-10082.30		Service and the service and th	_		47.29	
92 297.	_			-10719.20					46.95	
	-									
	_								44.55	
	_									
94 416.	6	7	7 4	7 4 SLE Q 9 4 SLE Q	7 4 SLE Q -11250.30 9 4 SLE Q -11144.80	77 4 SLE Q -11250.30 135.08 9 4 SLE Q -11144.80 128.92	7 4 SLE Q -11250.30 135.08 44011.50 9 4 SLE Q -11144.80 128.92 42002.30	7 4 SLE Q -11250.30 135.08 44011.50 50.27 9 4 SLE Q -11144.80 128.92 42002.30 50.27	7 4 SLE Q -11250.30 135.08 44011.50 50.27 28.27 9 4 SLE Q -11144.80 128.92 42002.30 50.27 28.27	77 4 SLE Q -11250.30 135.08 44011.50 50.27 28.27 44.55 9 4 SLE Q -11144.80 128.92 42002.30 50.27 28.27 42.51

								(elazi)	me ai c	alcolo
97	595.24	4	SLE Q	-10935.50	113.31	36917.10	50,27	28.27	37.34	1245.18
98	654.76	4	SLE Q	-10831.80	104.53	34056.30	50.27	28.27	34.43	1138.16
99	714.29	4	SLE Q	-10728.70	95.46	31101.40	50.27	28.27	31.42	1027.61
100	773.81	4	SLE Q	-10626.10	86.32	28123.80	50.27	28.27	28.39	916.23
101	833.33	4	SLE Q	-10524.10	77.29	25182,70	50.27	28.27	25.40	806.27
102	892.86	4	SLE Q	-10422.70	68.52	22325.80	50.27	28.27	22.48	699.58
103	952.38	4	SLE Q	-10321.80	60.13	19590.80	50.27	28.27	19.69	597.60
104	1011.90	4	SLE Q	-10221.40	52.20	17006.70	50.27	28.27	17.04	501.46
105	1071.43	4	SLE Q	-10121.70	44.79	14594.60	50.27	28.27	14.57	412.02
106	1130.95	4	SLE Q	-10022.40	37.96	12368.80	47.12	31.42	12.28	329,90
107	1190.48	4	SLE Q	-9923.74	31.73	10337.70	47.12	31.42	10.17	255.55
108	1250.00	4	SLE Q	-9825.58	26.10	8505.07	47+12	31.42	8.26	189.32
109	1309,52	4	SLE Q	-9727.94	21.09	6870.29	43.98	34.56	6.54	131.62
110	1369.05	4	SLE Q	-9630.82	16.66	5429.47	40.84	37.70	5.02	83.09
111	1428.57	4	SLE Q	-9534.22	12.82	4175.97	37.70	40.84	3.71	50.62
112	1488.10	4	SLE Q	~9438.14	9.52	3100.98	31.42	47.12	2.66	37.02
113	1547.62	-4	SLE Q	-9342.56	6.73	2194.04	21,99	56.55	1.95	27.45
114	1607.14	4	SLE Q	-9247.48	4.43	1443.46	0.00	78.54	1.50	21.42
115	1666.67	4	SLE Q	-9152.89	2.57	836,68	0.00	78.54	1.18	17.04
116	1726.19	4	SLE Q	-9058.80	1.11	360.56	0.00	78.54	0.92	13.58
117	1785.71	4	SLE Q	-8965.19	0.01	1,63	0.00	78.54	0.73	10.94
118	1845.24	4	SLE Q	-8872.06	-0.78	-253.71	0.00	78.54	0.85	12.60
119	1904.76	4	SLE Q	-8779.41	-1.29	-419.06	0.00	78.54	0.93	13.65
120	1964.29	4	SLE Q	-8687.23	-1.56	-507.92	0.00	78.54	0.97	14.16
121	2023.81	4	SLE Q	-8595.52	-1,64	-533.63	0.00	78.54	0.97	14.23
122	2083.33	4	SLE Q	-8504.27	-1.56	-509.30	0.00	78.54	0.95	13.95
123	2142.86	- 6	SLE Q	-8413.47	-1.37	-447.85	0.00	78.54	0.92	13.40
124	2202.38	4	SLE Q	-8323.13	-1.11	-361.96	0.00	78.54	0.86	12.69
125	2261.90	4	SLE Q	-8233.23	-0.81	-264.18	0.00	78.54	0.81	11.89
126	2321,43	4	SLE Q	-8143.77	-0.51	-166.85	0.00	78.54	0.75	11.10
127	2380.95	4	SLE Q	-8054.75	-0.25	-82.26	0.00	78.54	0.70	10.40
128	2440.48	4	SLE Q	-7966.16	-0.07	-22.59	0.00	78.54	0.66	9.87
129	2500.00	4	SLE Q	-7878.00	0.00	0.00	0.00	78.54	0.64	9.61

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	•eq	Δ _{BM}	A _s <cmq></cmq>	Ac eff <cmq></cmq>	σ _B <dan cmq=""></dan>	z am	Wk <mm∂< th=""></mm∂<>
87	0.00	4	SLE Q	-7014.10	40721,70	124.99	46.00	136,36	0.50	20.00	200.06	25.13	1357.91	1445,41	0.42	0.14
88	59.52	4	SLE Q	-8173.46	43563.70	133.71	46.00	136.36	0.50	20.00	199.92	25.13	1356.21	1536.70	0.45	0.13
89	119.05	4	SLE Q	-8809.45	45412.70	139.38	46.00	136.36	0.50	20.00	199.87	25.13	1355.50	1597.79	0.47	0.10
90	178.57	4	SLE Q	-9445.72	46409.90	142.44	46.00	136.36	0.50	20.00	199.78	25.13	1354.43	1626.55	0,47	0.10
91	238.09	4	SLE C	-10082.30	46685.80	143.29	46,00	136,36	0.50	20.00	199.67	25.13	1353.03	1627.93	0.47	0.1
92	297.62	4	SLE Q	-10719.20	46359.90	142.29	46.00	136.36	0.50	20.00	199,53	25.13	1351.31	1606.48	0.47	0.1
93	357.14	4	SLE Q	-11356.40	45494.50	139.63	46.00	136.36	0.50	20.00	199.37	25,13	1349,22	1564.57	0.46	0.1
94	416,67	4	SLE Q	-11250.30	44011.50	135.08	46.00	136.36	0.50	20.00	199.31	25.13	1348.53	1509.81	0.44	0.1
95	476,19	4	SLE Q	-11144.80	42002.30	128.92	46.00	136.36	0.50	20.00	199.22	25.13	1347.42	1435.09	0.42	0.1
96	535.71	4	SLE Q	-11039.90	39599.00	121.54	46,00	136.36	0.50	20.00	199.10	25.13	1345.87	1345.41	0.39	0.1
97	595.24	4	SLE Q	-10935.50	36917.10	113.31	46.00	136.36	0.50	20.00	198.94	25.13	1343.85	1245.18	0.36	0.1
98	654.76	4	SLE Q	-10831.80	34056.30	104.53	46.00	136.36	0.50	20.00	198.74	25,13	1341.30	1138.16	0.33	0.1
99	714,29	4	SLE Q	-10728.70	31101.40	95,46	46.00	136.36	0,50	20.00	198,48	25.13	1338.12	1027.61	0.30	0.1
100	773.81	4	SIE Q	-10626.10	28123,80	86.32	46.00	136.36	0.50	20.00	198.17	25.13	1334.19	916.23	0.27	0.0
101	833.33	4	SLE Q	-10524.10	25182.70	77.29	46.00	136.36	0.50	20.00	212.90	21.99	1329.33	806.27	0.23	0.0
102	892.86	4	SLE Q	-10422.70	22325.80	68.52	46.00	136.36	0.50	20.00	212.35	21.99	1323.28	699.58	0.20	0.0
103	952.38	4	SLE Q	-10321.80	19590.80	60.13	45.00	136,36	0.50	20.00	211.66	21.99	1315.68	597.60	0,17	0.0
104	1011.90	4	SLE Q	-10221.40	17006.70	52.20	46.00	136.36	0.50	20.00	210.78	21.99	1306.02	501.46	0.15	0.0
105	1071.43	4	SLE Q	-10121.70	14594.60	44.79	46.00	136.36	0.50	20.00	209.64	21.99	1293.51	412.02	0.12	0.0
106	1130.95	4	SLE Q	-10022.40	12368.80	37.96	46.00	136.36	0.50	20.00	208,13	21.99	1276.95	329.90	0.10	0.0
107	1190.48	4	SLE Q	-9923.74	10337.70	31.73	46.00	136.36	0.50	20.00	206.08	21.99	1254.39	255.55	0.07	0.0
108	1250.00	4	SLE C	-9825,58	8505.07	26.10	46.00	136.36	0.50	20.00	203.18	21.99	1222.45	189.32	0.06	0.0
109	1309.52	4	SLE Q	-9727.94	6870.29	21.09	46.00	136.36	0.50	20.00	198,90	21.99	1175.42	131.62	0.04	0.0
110	1369.05	4	SLE Q	-9630.82	5429.47	16.66	46.00	136.36	0.50	20.00	209.01	18.85	1102.77	83.09	0.02	0.0
111	1428.57	4	SLE Q	-9534.22	4175.97	12.82	46.00	136.36	0.50	20.00	195.39	18.85	974,44	45.04	0.01	0.0
112	1488.10	4	SLE Q	-9438.14	3100.98	9.52	46.00	136.36	0.50	20.00	183.76	15.71	720.67	19.27	0.01	0.0
113	1547.62	4	SLE Q	-9342.56	2194.04	6.73	46.00	136.36	0.50	20.00	181.78	6.28	282.06	5.36	0.00	0.0
130	0.00	3	SLE F	-7014.10	40721.70	124.99	46.00	136.36	0.50	20.00	200.06	25.13	1357.91	1445.41	0.42	0.1
131	59.52	3	SLE F	-8173.46	43563.70	133.71	46.00	136.36	0.50	20.00	199.92	25.13	1356.21	1536.70	0.45	0.1
132	119.05	3	SLE F	-8809.45	45412,70	139.38	46,00	136.36	0.50	20.00	199,87	25,13	1355.50	1597.79	0.47	0.1
133	178.57	3	SLE F	-9445.72	46409.90	142.44	46.00	136.36	0.50	20.00	199.78	25.13	1354.43	1626.55	0.47	0.1
134	238.09	3	SLE F	-10082.30	46685.80	143.29	46,00	136.36	0.50	20.00	199.67	25.13	1353.03	1627.93	0.47	0.1
135	297.62	3	SLE F	-10719.20	46359,90	142.29	46.00	136.36	0.50	20.00	199.53	25.13	1351.31	1606.48	0.47	0.1
136	357.14	3	SLE F	-11356.40	45494.50	139.63	46,00	136.36	0.50	20.00	199.37	25.13	1349.22	1564.57	0.46	0.1
137	416.67	3	SLE F	-11250.30	44011.50	135.0B	46.00	136.36	0,50	20.00	199,31	25.13	1348.53	1509.81	0.44	0.1
138	476.19	-3	SLE F	-11144.80	42002.30	128.92	46,00	136,36	0.50	20.00	199,22	25.13	1347.42	1435.09	0.42	0.1
139	535.71	3	SLE F	-11039.90	39599.00	121.54	46.00	136.36	0.50	20.00	199.10	25.13	1345.87	1345.41	0.39	0.1
140	595.24	3	SLE F	-10935.50	36917.10	113.31	46.00	136.36	0.50	20.00	198.94	25.13	1343.85	1245.18	0.36	0.1
141	654.76	3	SLE F	-10831.80	34056.30	104.53	46.00	136.36	0.50	20.00	198.74	25.13	1341.30	1138.16	0.33	0.1
142	714.29	3	SLE F	-10728.70	31101.40	95.46	46,00	136.36	0.50	20.00	198.48	25.13	1338.12	1027.61	0.30	0.10

143	773.81	3	SLE E	-10626.10	28123.80	86.32	46.00	136.36	0.50	20.00	198,17	25.13	1334.19	916.23	0.27	0.09
144	833,33	3	SLE 3	-10524.10	25182.70	77.29	46.00	136.36	0.50	20.00	212.90	21.99	1329.33	806.27	0.23	0.08
145	892.86	3	SLE F	-10422.70	22325.80	68.52	46.00	136.36	0,50	20.00	212.35	21.99	1323.28	699.58	0.20	0.07
146	952.38	3	SIE F	-10321.80	19590.80	60.13	46.00	136.36	0.50	20.00	211.66	21.99	1315.68	597.60	0.17	0.06
147	1011.90	3	SLE F	-10221.40	17006.70	52.20	46,00	136,36	0.50	20.00	210.78	21.99	1306.02	501.46	0.15	0.05
148	1071.43	3	SLE F	-10121.70	14594.60	44.79	46.00	136.36	0.50	20.00	209.64	21.99	1293.51	412.02	0.12	0.04
149	1130.95	3	SLE E	-10022.40	12368.80	37.96	46.00	136.36	0.50	20.00	208.13	21.99	1276.95	329.90	0.10	0.03
150	1190.48	3	SLE E	-9923.74	10337.70	31.73	46,00	136.36	0.50	20.00	206.08	21.99	1254.39	255.55	0.07	0.03
151	1250.00	3	SLE F	-9825.58	8505.07	26.10	46.00	136.36	0.50	20.00	203.18	21.99	1222.45	189.32	0.06	0.02
152	1309.52	3	SLE F	-9727.94	6870.29	21.09	46.00	136.36	0.50	20.00	198,90	21.99	1175.42	131.62	0.04	0.01
153	1369.05	3	SLE F	-9630.82	5429.47	16.66	46.00	136.36	0.50	20.00	209.01	18.85	1102.77	83.09	0.02	0.01
154	1428.57	3	SLE E	-9534.22	4175.97	12.82	46,00	136.36	0.50	20.00	195.39	18.85	974.44	45.04	0.01	0.00
155	1488.10	3	SLE F	-9438.14	3100.98	9.52	46.00	136.36	0.50	20.00	183.76	15.71	720.67	19,27	0.01	0,00
156	1547.62	3	SLE F	-9342.56	2194.04	6.73	46.00	136.36	0.50	20.00	181.78	6.28	282.06	5.36	0.00	0.00

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
71	C.Rare - Sc max (min. compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
114	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 14

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle rezzioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 14 (-7)

Caso	8	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
:1	-1	SLU	RVN	22330.90	7611.12	-392.01	56884.80	-1333.02
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SLU	TOT	22330.90	7611.12	-392.01	56884.80	-1333.02
2	2	SLE R	RVN	16541.40	5637.87	-290.38	42136.90	-987.42
	2	SLE R	TAG				0.00	0.00
	.2	SLE R	ECC				0.00	0.00
	-2	SLE R	TOT	16541.40	5637.87	-290.38	42136.90	-987.42
3	3	SLE F	RVN	16541.40	5637.87	-290.38	42136.90	-987.42
	3	SLE F	TAG			3	0.00	0.00
	3	SLE F	ECC				0.00	0.00
	.3	SLE F	TOT	16541.40	5637.87	-290.38	42136.90	-987.42
4	.4	SLE Q	RVN	16541.40	5637.87	-290.38	42136.90	-987.42
	4	SLE Q	TAG				0.00	0.00
	4	SIE Q	ECC				0.00	0.00
	4	SLE Q	TOT	16541.40	5637.87	-290.38	42136.90	-987.42

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	. 1	SLU	. 1	-22330.90	-7611.12	392.01	-56884.80	1333.02
2	2	SLE R	1	-16541.40	-5637.87	290.38	-42136.90	987.42
3	3	SLE F	1	-16541.40	-5637.87	290.38	-42136.90	987.42
4	4	SLE Q	- 1	-16541.40	-5637.87	290.38	-42136.90	987.42

Da 0 a -25

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
-1	0.00	1	SLU	-22330.90	56636.00	1327.19	-22330.90	156229.00	3434.76	2-3	178.75	2.758
2	59,52	1	SIU	-23383,80	60425.40	1415,98	-23383.BO	156672.00	3411.68	2-3	178.75	2.593

							Rela	zione di d	calcolo			
- 3	119.05	1	SLU	-23807.40	62859.20	1473.02	-23807.40	■ 전하시 집합이라면 하시네요 보다.		2-3	178.75	2.495
4	178.57	1	SLU	-24231.70	64131.00	1502.82	-24231.70	157028.00	3392.97	2-3	178.75	2.448
.5	238.09	1	SIU	-24656.70	64419.90	1509.59	-24656.70	157207.00	3383.56	2-3	178.75	2.440
- 6	297.62	1	SIJ	-25082.50	63889.70	1497.17	-25082.50	157386.00	3374.10	2-3	178.75	2.463
7	357.14	1	SLU	-25509.10	62626.30	1467.56	-25509.10	157565.00	3364.60	2-3	178.75	2.516
8	416.67	1	SLU	-25043.30	60525.00	1418.32	-25043.30	157369.00	3374.97	2-3	178.75	2.600
. 9	476.19	1	SIU	-24578.90	57711.20	1352.38	-24578.90	157174.00	3385.28	2-3	178.75	2.723
10	535.71	1	SIU	-24115.70	54365.60	1273.98	-24115.70	156980.00	3395.53	2-3	178.75	2.887
11	595.24	3	SLU	-23653.90	50645.90	1186.82	-23653.90	156785.00	3405.73	2-3	178.75	3.096
12	654.76	-1	SIJ	-23193.30	46688.00	1094.07	-23193.30	156592.00	3415.86	2-3	178.75	3.354
13	714.29	1	SLU	-22734.00	42607.80	998.45	-22734.00	156399.00	3425.94	2-3	178.75	3.671
14	773.81	1	SLU	-22275.90	38502.40	902.25	-22275.90	156206.00	3435.97	2-3	178.75	4.057
15	833,33	1	SLU	-21819.00	34452.10	807.34	-21819.00	156014.00	3445.94	2-3	178.75	4.528
16	892.86	-1	SLU	-21363.30	30521.90	715.24	-21363.30	155822.00	3455.85	2-3	178,75	5.105
17	952.38	1	SLU	-20908.70	26763.00	627.15	-20908.70	155631.00	3465.72	2-3	178.75	5.815
18	1011.90	1	SILI	-20455.20	23214.40	544.00	-20455.20	155440.00	3475.53	2-3	178.75	6.696
19	1071,43	7.	SIJ	-20002.80	19904.50	466,43	-20002.B0	155250.00	3485.29	2-3	178.75	7.800
20	1130.95	1	SLU	-19551.50	16852.50	394.92	-19551.50	155060.00	3495.00	2-3	178.75	9.201
21	1190.48	1	SLU	-19101.30	14069.60	329.70	-19101.30	154870.00	3504.66	2-3	178,75	11.007
22	1250.00	1	SLU	-18652.10	11560.40	270.90	-18652.10	154681.00	3514.27	2-3	178.75	13.380
23	1309.52	1	SLU	-18203.80	9323.75	218.49	-18203.BO	154493.00	3523.83	2-3	178.75	16.570
24	1369.05	1	SIU	-17756.60	7354.00	172,33	-17756.60	154305.00	3533.34	2-3	178.75	20.982
25	1428.57	1	SIU	-17310.30	5641.77	132.21	-17310.30	154117.00	3542.80	2-3	178.75	27.317
26	1488.10	1	SLU	-16864.90	4174.77	97.83	-16864.90	153930.00	3552.21	2-3	178.75	36.871
27	1547.62	1	SIA	-16420,50	2938.44	68,86	-16420.50	153742.00	3561.63	2-3	178.75	52.321
28	1607.14	1	SIJ	-15976.90	1916.57	44.91	-15976.90	153555.00	3571.59	2-3	178.75	80.119
29	1666.67	1	SLU	-15534.10	1091.80	25,58	-15534.10	153368.00	3582.07	2-3	178.75	>100
30	1726.19	1	SLU	-15092.30	445.99	10.45	-2571250.00	153181.00	3592.50	2-3	178.75	>100
31	1785.71	1	SIU	-14651,20	-39.41	-0.92	-2571250.00	-152887.00	-3182.88	2-3	358.75	>100
32	1845.24	1	SIJ	-14210.90	-383.15	-8,98	-2571250.00	-152701.00	-3170,74	2-3	358,75	>100
33	1904.76	1	SLU	-13771.30	-603.94	-14.15	-2571250.00	-152515.00	-3158.62	2-3	358.75	>100
34	1964.29	1	SLU	-13332.50	~720.33	-16,88	-2571250.00	-152329.00	-3146.55	2-3	358.75	>100
35	2023.81	1	SIJ	-12894.50	-750.64	-17.59	-2571250.00	-152143.00	-3134.51	2-3	358.75	>100
36	2083.33	1	SIU	-12457.10	+712.89	-16.71	-2571250.00	-151958.00	-3122.50	2-3	358.75	>100
37	2142.86	1	SLU	-12020.30	-624.79	-14.64	-2571250.00	-151773.00	-3110.53	2-3	358.75	>100
38	2202.J8	1	SLU	-11584,30	-503.77	-11.81	-2571250.00	-151589.00	-3098.59	2-3	358.75	>100
39	2261.90	1	SLU	-11148.80	-367.01	-B.60	-2571250.00	-151404.00	-3086,68	2-3	358.75	>100
40	2321.43	1	SILI	-10714.00	+231.47	~5.42	-2571250.00	-151220.00	-3074.83	2-3	358.75	>100
41	2380.95	1	SIA	-10279.70	-113.99	-2.67	-2571250.00	-151037.00	-3063.05	2-3	358.75	>100
42	2440.48	1	SLU	-9845.93	-31.27	-0.73	-2571250.00	-150852.00	-3051.14	2-3	358.75	>100
43	2500.00	1	SLU	-9412.73	0.00	0.00	-2571250.00					>100

Caso	X <cm></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw om>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7611.12	-392.01	0.85	11,31	7621.21	1.00	32294.70	334867.00	32294.70	4.237
2	59,52	1	SLU	5165,83	-266.07	0.85	11.31	5172.68	1.00	32294.70	33501B.00	32294.70	6.243
3	119.05	1	SLU	3057.38	-157.47	0.85	11.31	3061.43	1.00	32294.70	335078.00	32294.70	10.549
4	178.57	1	SLU	1261.63	-64.98	0.85	11.31	1263.30	1.00	32294.70	335139,00	32294.70	25.564
- 5	238.09	1	SIJJ	-246.29	12.69	0.85	11.31	246.61	1,00	32294.70	335200.00	32294.70	>100
-6	297.62	1	SLU	-1491.52	76.82	0.85	11.31	1493.50	1,00	32294.70	335261.00	32294.70	21.623
7	357,14	1	SLU	-2817.71	145.13	0.85	11.31	2821.44	1.00	32294.70	335322.00	32294.70	11.446
- 8	416.67	1	SIA	-4178.21	215.20	0.85	11.31	4183.75	1.00	32294.70	335255.00	32294.70	7.719
9	476.19	1	SLU	-5215.65	268.63	0.85	11.31	5222.57	1.00	32294.70	335189.00	32294.70	6.184
10	535.71	1	SLU	-5969.60	307.46	0.85	11.31	5977.52	1.00	32294.70	335122.00	32294.70	5.403
11	595,24	1	SIU	-6477.57	333.63	0.85	11.31	6486.16	1.00	32294.70	335056.00	32294.70	4.979
12	654.76	1	SIJ	-6774.67	348.93	0.85	11.31	6783.65	1.00	32294.70	334990.00	32294.70	4.763
13	714.29	1	SLU	-6893.46	355.05	0.85	11.31	6902.60	1.00	32294.70	334925.00	32294.70	4.679
14	773.81	1	SLU	-6863.77	353.52	0.85	11,31	6872.87	1.00	32294.70	334859.00	32294.70	4,699
15	833.33	1	SIJJ	-6712.71	345.74	0.85	11.31	6721.61	1.00	32294.70	334793.00	32294.70	4,805
15	892.86	1	SLU	-6464.64	332.96	0.85	11.31	6473.21	1.00	32294.70	334728.00	32294.70	4.989
17	952.38	1	SLU	-6141.26	316.31	0.85	11.31	6149.40	1.00	32294.70	334663.00	32294.70	5.252
18	1011.90	1	SIJ	-5761.68	296.75	0.85	11.31	5769.31	1,00	32294.70	334598.00	32294.70	5.598
19	1071.43	1	SLU	-5342.57	275.17	0.85	11.31	5349.65	1,00	32294.70	334533.00	32294,70	6.037
20	1130.95	1	SLU	-4898.31	252,29	0.85	11.31	4904.80	1.00	32294.70	334469.00	32294.70	6.584
21	1190.48	1	SIA	-4441,14	228.74	0.85	11.31	4447.03	1.00	32294.70	334404.00	32294.70	7.262
22	1250.00	1	SLU	-3981.37	205.06	0.85	11.31	3986.65	1.00	32294.70	334340.00	32294.70	8.101
23	1309.52	1	SEU	-3527.53	181.69	0.85	11.31	3532.20	1.00	32294.70	334276.00	32294.70	9.143
24	1369,05	1	SIJJ	-3086.54	158.97	0.85	11.31	3090.63	1.00	32294.70	334212.00	32294.70	10.449
25	1428.57	1	SIJ	-2663.96	137.21	0.85	11.31	2667.49	1.00	32294.70	334148.00	32294.70	12,107
26	1488.10	1	SLU	-2264.09	116.61	0.85	11.31	2267.09	1.00	32294.70	334084.00	32294.70	14.245
27	1547.62	1	SLU	-1890.18	97.35	0.85	11.31	1892.68	1.00	32294.70	334020.00	32294.70	17.063
28	1607.14	1	SIAI	-1544.57	79.55	0.85	11.31	1546.61	1.00	32294.70	333957.00	32294.70	20.883
29	1666.67	1	SLU	-1228.85	63.29	0.85	11.31	1230.48	1,00	32294.70	333893.00	32294.70	26.246
30	1726.19	1	SIU	-944.00	48.62	0.85	11.31	945.25	1.00	32294.70	333830.00	32294.70	34.165
31	1785.71	1	SLU	-690.51	35.56	0.85	11.31	691.42	1.00	32294.70	333767,00	32294.70	46.708
32	1845.24	1	SIU	-468.49	24.13	0.85	11.31	469,11	1.00	32294.70	333704.00	32294.70	68.843

33	1904.76	1	SLU	-277.77	14.31	0.85	11.31	278.14	1.00	32294.70	333641,00	32294.70	>100
34	1964.29	1	SLU	-118.02	6.08	0.85	11.31	118.17	1.00	32294.70	333578.00	32294.70	>100
35	2023.81	1	SIU	11.25	-0.58	0.85	11.31	11.26	1.00	32294.70	333515.00	32294.70	>100
36	2083.33	1	SIU	110.52							333452.00		
37	2142.86	1	SLU	180,31	-9.29	0.85	11.31	180.55	1.00	32294.70	333390,00	32294.70	>100
38	2202.38	1	SLU	221.08	-11,39	0.85	11.31	221.37	1.00	32294.70	333327.00	32294.70	>100
39	2261.90	1	SLU	233.21							333265.00		
40	2321,43	1	SLU	217.00	-11.18	0.85	11.31	217,29	1.00	32294.70	333203.00	32294.70	>100
41	2380.95	3	SLU	172.65							333141.00		
42	2440.48	1	SIJJ	100.31	-5.17	0.85	11.31	100.44	1.00	32294.70	333078.00	32294.70	>100

Caso	X <cm></cm>	oc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <amq></amq>	AfC <cmq></cmq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-16541.40	983.10	41952.60	50.27	28.27	42,33	1356.02
45	59.52	2	SLE R	-17634.60	1048.88	44759.50	50.27	28.27	45.16	1446.94
46	119.05	2	SLE R	-18138.40	1091.12	46562.40	50.27	28.27	46.99	1508.11
47	178.57	2	SLE R	-18642.80	1113.20	47504.50	50.27	28,27	47.93	1536.70
. 48	238.09	2	SLE R	-19147.80	1118.21	47718.40	50,27	28.27	48,14	1537.73
49	297.62	2	SLE R	-19653.40	1109.01	47325.70	50.27	28.27	47.72	1515.80
50	357,14	2	SLE R	-20159.60	1087.08	46389.90	50.27	28.27	46,75	1473.34
51	416.67	2	SLE R	-19829.80	1050.61	44833.30	50.27	28.27	45.17	1419.07
52	476,19	2	SLE R	-19501.00	1001.76	42749.00	50.27	28.27	43.06	1344.89
53	535.71	2	SIE R	-19173.30	943.69	40270.80	50,27	28.27	40.53	1255.74
54	595,24	2	SLE R	-18846.60	879,12	37515.50	50.27	28.27	37,73	1156.18
-55	654.76	2	SLE R	-18520.90	810.42	34583.70	50.27	28.27	34.74	1050.00
56	714.29	_	SLE R	-18196.20	739.60	31561.30	50.27	28.27	31,66	940.47
57	773.81	2	SLE R	-17872.50	668.33	28520.30	50.27	28.27	28.55	830.35
58	833.33	2	SLE R	-17549.70	598.03	25520.10	50.27	28.27	25,48	721.92
59		2	SLE R	-17227.90	529.81	22608.80	50.27	28.27	22.49	617.05
60	952.38	2	SLE R	-16907.00	464.56	19824.50	47.12	31,42	19,63	517.25
61	1011,90	2	SLE R	-16587.00	402.96	17195.90	47,12	31.42	16.92	423.73
62	1071.43	2	SLE R	-16267.90 -15949.70	345.51 292.53	12483.30	47.12	31.42	14.37	337.43 259.14
64	1190.48	2	SLE R	-15632.30	244.22	10422.00	43.98	34.56	9.86	189.60
65	1250.00	2	SLE B	-15315.80	200.67	8563.26	40.84	37.70	7,91	129.67
66	1309.52	2	SLE R	-15000.10	161.84	6906.48	37.70	40.84	6.18	84.23
67	1369.05	2	SLE R	-14685.20	127.65	5447.41	34.56	43.98	4,73	65.27
68	1428.57	2	SLE R	-14371.10	97.93	4179.09	28.27	50.27	3.59	50.28
69		2	SLE R	-14057.70	72.47	3092.42	18.85	59.69	2,79	39.50
70	1547.62	2	SLE R	-13745.10	51.01	2176.62	0.00	78.54	2.24	32.07
71	1607.14	2	SLE R	-13433.30	33.27	1419.69	_	78.54	1.83	26.37
72	1666.67	2	SLE R	-13122.10	18.95	808.74	-	78.54	1.49	21.69
73	1726.19	2	SLE R	-12811.70	7.74	330.37	0.00	78.54	1.21	17.95
74	1785.71	2	SLE R	-12502.00	-0.68	-29.20	0.00	78.54	1,03	15.45
75	1845.24	2	SLE R	-12192.90	-6.65	-283.82	0.00	78.54	1,14	16.86
76	1904.76	2	SLE R	-11884.50	-10.48	~447.36	0.00	78.54	1.20	17.63
7.7	1964.29	2	SLE R	-11576.70	-12.50	~533.58	0.00	78.54	1.22	17.86
78	2023.81	2	SLE R	-11269.50	-13.03	-556.03	0.00	78.54	1.20	17.64
79	2083,33	2	SLE R	-10963.00	-12.37	-528.07	0.00	78.54	1.16	17.07
80	2142.86	2	SIE R	-10657.00	-10.85	-462.81	0.00	78.54	1.11	16.24
81	2202.38	2	SLE R	-10351.60	-8.74	-373.16	0.00	78.54	1.03	15.24
82	2261.90	2	SLE R	-10046.80	-6.37	-271.86	0.00	78.54	0.96	14.16
83	2321.43	2	SLE R	-9742.47	-4.02	-171.46	0.00	78.54	0.88	13.08
		_		-9438.69		-84.44				
	2440.48	_		-9135.41		-23,17				
_		_		-8832.63			_	78.54		
87				-16541.40						
88		_		-17634.60				-	45.16 46.99	
90		_		-18138.40 -18642.80					47.93	
91				-19147.80						
92				-19653.40					47.72	
93				-20159.60						
94				-19829.80						
95				-19501.00					43.06	
96				-19173.30					40,53	
97				-18846,60						
98				-18520.90					34.74	
99		_		-18196.20					31,66	
100				-17872.50					28.55	
		_	_	-17549.70					25.48	
	892,86	_	_	-17227.90		22608.80			22,49	
_	952.38	-		-16907.00					19.63	
104	1011.90			-16587.00		17195.90		_	16.92	
_	1071,43			-16267.90		14744.10	47.12	31.42	14.37	337.43
400	1120 05			-15949.70		12483.30	43 00	24 55	12.02	259.14

107	1190.48	4	SLE Q	-15632.30	244.22	10422.00	43.98	34.56	9.86	189.60
108	1250.00	4	SLE Q	-15315.80	200.67	8563.26	40.84	37.70	7.91	129.67
109	1309.52	4	SLE Q	-15000.10	161.84	6906.48	37.70	40.84	6.18	84.23
110	1369.05	4	SLE Q	-14685.20	127.65	5447.41	34.56	43.98	4.73	65.27
111	1428.57	4	SLE Q	-14371.10	97.93	4179.09	28.27	50.27	3.59	50.28
112	1488.10	4	SLE Q	-14057.70	72.47	3092.42	18.85	59.69	2.79	39.50
113	1547.62	4	SLE Q	-13745.10	51.01	2176.62	0.00	78.54	2.24	32.07
114	1607.14	4	SLE Q	-13433.30	33.27	1419.69	0.00	78.54	1.83	26.37
115	1666.67	4	SLE Q	-13122,10	18.95	808.74	0.00	78.54	1.49	21.69
116	1726.19	4	SLE Q	-12811.70	7.74	330.37	0.00	78.54	1.21	17.95
117	1785.71	4	SLE Q	-12502.00	-0.68	-29.20	0.00	78.54	1.03	15.45
118	1845.24	4	SLE Q	-12192.90	-6.65	-283.82	0.00	78.54	1+14	16.86
119	1904.76	4	SLE Q	-11884.50	-10.48	-447.36	0.00	78.54	1.20	17.63
120	1964.29	4	SLE Q	-11576.70	-12.50	-533.58	0.00	78.54	1,22	17.86
121	2023.81	4	SLE Q	-11269.50	-13.03	-556.03	0.00	78.54	1.20	17.64
122	2083.33	4	SLE Q	-10963.00	-12.37	~528.07	0.00	78.54	1.16	17.07
123	2142.86	4	SLE Q	-10657.00	-10.85	-462.81	0.00	78.54	1,11	16.24
124	2202.38	4	SLE Q	-10351.60	-8.74	-373.16	0.00	78.54	1.03	15.24
125	2261.90	4	SLE Q	-10046.80	-6.37	-271.86	0.00	78.54	0.96	14.16
126	2321.43	4	SLE Q	-9742.47	-4.02	-171.46	0.00	78.54	0.88	13.08
127	2380.95	4	SLE Q	-9438.69	-1.98	-84.44	0.00	78.54	0.81	12.10
128	2440.48	4	SLE Q	-9135.41	-0.54	-23.17	0.00	78.54	0.75	11.30
129	2500.00	4	SLE Q	-8832.63	0.00	0.00	0.00	78.54	0.72	10.77

Stato limite d'esercizio - Verifiche a fessurazione

Statu	TIME	-	eserc.	izio - Ver	Ifiche a	ressuraz	TOTIE			_					_	_
Caso	X <cm>></cm>	oc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	Φeq	Δ _{±m} <mm></mm>	A ₃ <cmq></cmq>	Ac eff <cmq></cmq>	σ _s <dan cmq=""></dan>	e _{sm}	Wk <mm2< th=""></mm2<>
87	0.00	4	SIE Q	-16541.40	41952.60	983.10	46,00	136.36	0.50	20,00	198.03	25.13	1332.43	1356.02	0.39	0.1
88	59,52	4	SLE Q	-17634.60	44759.50	1048.88	46.00	136.36	0.50	20.00	198.03	25.13	1332.47	1446.94	0.42	0,1
89	119.05	4	SLE Q	-18138.40	46562.40	1091.12	46.00	136.36	0.50	20.00	198.08	25.13	1333.00	1508.11	0.44	0.1
90	17B.57	9	SLE Q	-18642.80	47504.50	1113.20	46.00	136.36	0.50	20.00	198,05	25.13	1332.65	1536.70	0.45	0.1
91	238.09	4	SLE Q	-19147.80	47718.40	1118.21	46.00	136.36	0.50	20.00	197.96	25.13	1331.58	1537.73	0.45	0.1
92	297.62	4	SLE Q	-19653.40	47325.70	1109.01	46.00	136.36	0.50	20.00	197.83	25.13	1329.88	1515.80	0.44	0.1
93	357.14	4	SLE Q	-20159.60	46389.90	1087.08	46.00	136.36	0.50	20,00	197.64	25.13	1327.51	1473.34	0.43	0.1
94	416.67	4	SLE Q	-19829.80	44833.30	1050.61	46.00	136.36	0.50	20.00	197.56	25.13	1326.56	1419.07	0.41	0.1
95	475.19	4	SLE Q	-19501.00	42749.00	1001.76	46.00	136.36	0.50	20.00	197,43	25.13	1324.84	1344.85	0.39	0.1
96	535.71	4	SLE Q	-19173.30	40270.80	943.69	46.00	136.36	0.50	20.00	197,23	25.13	1322.35	1255,74	0.37	0.1
97	595.24	4	SLE Q	-18846.60	37515.50	879.12	46.00	136.36	0.50	20,00	196,97	25.13	1319.04	1156,18	0.34	0.1
98	654.76	4	SLE Q	-18520.90	34583.70	810.42	46.00	136.36	0.50	20.00	196.63	25.13	1314.80	1050.00	0.31	0.1
99	714.29	4	SLE Q	-18196.20	31561.30	739.60	46.00	136.36	0.50	20.00	196.21	25.13	1309.48	940.47	0.27	0.0
100	773.81	4	SLE Q	-17872.50	28520.30	668.33	46.00	136.36	0.50	20.00	195.68	25.13	1302.85	830.35	0.24	0.0
101	833.33	4	SLE C	-17549.70	25520.10	598.03	46.00	136.36	0.50	20.00	209,74	21.99	1294.56	721.92	0.21	0.0
102	892.86	4	SLE Q	-17227.90	22608.80	529.81	46,00	136,36	_	20.00	208.79	21.99	1284.16	617.05	0.18	0.0
103	952.38	4	SLE Q	-16907.00	19824.50	464.56	46.00	136.36	0.50	20.00	207.59	21.99	1270.96	517,25	0.15	0.0
104	1011.90	4	SLE Q	-16587.00	17195.90	402.96	46.00	136.36	0.50	20.00	206,04	21.99	1253.94	423.73	0.12	0.0
105	1071.43	4	SLE Q	-16267.90	14744.10	345.51	46.00	136.36	0.50	20.00	204,01	21.99	1231.64	337.43	0.10	0.0
106	1130.95	4	SLE Q	-15949.70	12483.30	292.53	46.00	136.36	0.50	20,00	201,29	21.99	1201.69	259,14	0.08	0.0
107	1190.48	4	SLE Q	-15632.30	10422.00	244.22	46.00	136.36	0.50	20.00	215.10	18.85	1160.20	189.60	0.06	0.0
108	1250.00	4	SLE Q	-15315.80	8563.26	200.67	46.00	136.36	0.50	20.00	208.72	18.85	1100.07	129,67	0.04	0.0
109	1309,52	4	SLE Q	-15000.10	6906.4B	161,84	46+00	136.36	0.50	20.00	198.71	18.85	1005.73	80.52	0.02	0.0
110	1369.05	4	SIE Q	-14685.20	5447.41	127.65	46.00	136.36	0.50	20.00	200,40	15.71	851.35	43,58	0.01	0.0
111	1428.57	4	SLE Q	-14371.10	4179.09	97.93	46.00	136.36	0.50	20.00	179.94	12.57	552.54	19.39	0.01	0.0
112	1488.10	4	SLE C	-14057.70	3092.42	72.47	46.00	136.36	0.50	20.00	160.11	6.28	213.97	5.76	0.00	0.0
130	0.00	3	SLE F	-16541.40	41952.60	983.10	46,00	136.36	0.50	20,00	198.03	25.13	1332.43	1356,02	0.39	0.1
131	59,52	3	SLE F	-17634.60	44759.50	1048.88	46.00	136.36	0.50	20.00	198.03	25.13	1332.47	1446.94	0.42	0.1
132	119.05	3	SLE F	-18138.40	46562.40	1091,12	46.00	136,36	0.50	20.00	198.08	25.13	1333.00	1508.11	0.44	0.1
133	178.57	3	SLE F	-18642.80	47504.50	1113.20	46,00	136.36	_	20.00	198.05	25.13	1332.65	1536,70	0.45	0.1
134	238.09	3	SLE F	-19147.80	47718.40	1118,21	46.00	136.36	0.50	20.00	197.96	25.13	1331.58	1537.73	0.45	0.1
135	297.62	3	SLE F	-19653.40	47325.70	1109.01	46.00	136.36	0.50	20.00	197.83	25.13	1329.88	1515.80	0.44	0.1
136	357,14	3	SLE F	-20159.60	46389.90	1087.08	46.00	136.36	0.50	20.00	197.64	25.13	1327.51	1473.34	0.43	0.1
137	416.67	3	SLE F	-19829.80	44833.30	1050.61	46,00	136.36	0.50	20.00	197.56	25.13	1326.56	1419.07	0.41	0.1
138	476,19	3	SLE F	-19501.00	42749.00	1001.76	46.00	136.36		20.00	197,43	25.13	1324.84	1344.85	0.39	0.1
139	535.71	3	SLE F	-19173.30	40270.80	943.69	46,00	136.36	0.50	20,00	197.23	25.13	1322.35	1255.74	0.37	0.1
140	595,24	3	SLE F	-18846.60	37515.50	879.12	46.00	136.36		20.00	196.97	25.13	1319.04	1156.18	0.34	0.1
141	654.76	3	SLE F	-18520.90	34583.70	810.42	46.00	136.36	0.50	20.00	196.63	25.13	1314.80	1050.00	0.31	0.1
142	714.29	3	SLE F	-18196.20	31561.30	739.60	46.00	136.36		20.00	196.21	25.13	1309.4B	940.47	0.27	0.0
143	773.81	3	SLE F	-17872.50	28520,30	668.33	46.00	136.36	-	20.00	195,68	25.13	1302.85	830,35	0.24	0.0
144	833.33	3	SLE F	-17549.70	25520.10	598.03	46.00	136.36	0.50	20.00	209,74	21.99	1294.56	721.92	0.21	0.0
				-17227.90											_	_
_		_		-16907.00			_		_			_		517.25	_	+-
				-16587.00												_
	THE RESERVE OF THE PERSON NAMED IN	_	_	-16267.90	The second name of the second	The second second second	_								_	_
				-15949.70											-	
		_		-15632.30					_					189.60		
_		_		-15315.80					_					129.67	_	-
_	1309.52			-15000.10											-	-
153	1369.05	3	SLE F	-14685.20	5447.41	127.65	46,00	136,36	0.50	20.00	200,40	15,71	851.35	43.58	0.01	10.0

154 1428.	57 3 SL	E F -14371.10	4179.09	97.93 46.	00 136.36	0.50 20.0	0 179,94	12.57	552.54	19,39 0.01	0.00
155 1488.	10 3 SL	E F -14057.70	3092.42	72.47 46.	00 136.36	0.50 20.0	0 160.11	6.28	213.97	5.76 0.00	0.00

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
71	C.Rare - Sc max (min. compr.)
- 91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
114	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 15

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 15 (-15)

Caso	8	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
- 1	1	SLU	RVN	46827,10	7464.87	-621.44	59215.90	-4662.64
	1	SIU	TAG				0.00	0.00
	. 1	SLU	ECC				0.00	0.00
	1	SLU	TOT	46827.10	7464.87	-621.44	59215.90	-4662.64
2	2	SLE R	RVN	34686.80	5529.53	-460.33	43863.60	-3453.80
	2	SLE R	TAG				0.00	0.00
	2.	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	34686.80	5529.53	-460.33	43863.60	-3453.80
3	3	SLE F	RVN	34686.80	5529.53	-460.33	43863.60	-3453.80
	. 3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	34686.80	5529.53	-460.33	43863.60	-3453.BC
-4	4	SLE Q	RVN	34686.80	5529.53	-460.33	43863.60	-3453.80
	4	SIE Q	TAG				0.00	0.00
	.4	SLE Q	ECC				0.00	0.00
	4	SLE Q	TOT	34686.80	5529.53	-460.33	43863.60	-3453.80

Sollecitazioni nei pali

Caso	8	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SIJI	1	-46827.10	-7464.87	621.44	-59215.90	4662.64
- 2	2	SLE R	- 1	-34686.80	-5529.53	460.33	-43863.60	3453.80
- 3	-3	SLE F	1	-34686.80	-5529.53	460.33	-43863.60	3453.80
4	4	SLE Q	. 1	-34686.80	-5529.53	460.33	-43863.60	3453,80

Da 0 a -25

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SLU	-46827.10	58964.10	4642.81	-46827.10	165961.00	12911.50	2-3	175.62	2.814
2	59,52	1	SLU	-47709.80	62653.80	4933.33	-47709.80	166315.00	12935.00	2-3	175.62	2.654
- 3	119.05	1	SLU	-47793.50	64972.00	5115.87	-47793.50	166348.00	12937.20	2-3	175.62	2.560
4	178,57	1	SIU	-47878.80	66116.10	5205,95	-47878.80	166382.00	12939.50	2-3	175.62	2.516
- 5	238.09	1	SIJ	-47965.50	66268.50	5217.95	-47965.50	166417.00	12941.80	2-3	175.62	2.511
- 6	297.62	1	SIJ	-48053.80	65596.10	5165.01	-48053.80	166452.00	12944.20	2-3	175.62	2.537
- 7	357.14	1	SLU	-48143.50	64187.20	5054.07	-48143.50	166488.00	12946.60	2-3	175.62	2.594
. 8	416.67	1	SLU	-47102.50	61938.80	4877.04	-47102.50	166071.00	12918.80	2-3	175.62	2.681
9	476.19	1	SLU	-46064.00	58979.10	4643.99	-46064.00	165655.00	12891.10	2-3	175.62	2,809
10	535.71	1	SLU	-45028.00	55491.30	4369.36	-45028.00	165240.00	12863.40	2-3	175.62	2.978
11	595.24	1	SIJJ	-43994.40	51634.70	4065.70	-43994.40	164826.00	12835.80	2-3	175.62	3.192
12	654.76	1	SIAJ	-42963.10	47547.00	3743.83	-42963.10	164412.00	12808.20	2-3	175.62	3.458
13	714.29	1	SLU	-41934,20	43345.10	3412.98	-41934.20	163999.00	12780.60	2-3	175.62	3.783
14	773.81	1	SIU	-40907.50	39126.90	3080.84	-40907.50	163587.00	12753.20	2-3	175.62	4,181

Relazione di calcolo 1 SLU -39883.00 34973.20 2753.78 163175.00 12726.30 -38860,60 12699.50 175.62 892,86 SIU 30949.20 2436.92 -38860.60 5,259 162763.00 175.62 -37840.30 27105.90 2134.33 -37840.30 5.989 1011,90 -36822,10 23482.40 1848.99 -36822.10 161943.00 12645.90 2-3 375.62 6+896 -35805.80 20106.70 1583.19 -35805.80 8.033 1071.43 161533.00 12619.20 175.62 16997.60 -34791.40 161121.00 11,344 14165.90 12438.10 13,799 1250.00 914.60 160291.00 175.62 9344.84 1369.05 30752.10 7347.56 578,54 -30752.10 159462.00 12301.40 175.62 21,700 1428.5 29746.50 442.02 159048.00 28.328 5613.70 -29746.50 226,96 54.871 2882.38 158047.00 145.90 175.00 1853.00 157634.00 85,129 1666.67 -25739.70 1024.27 80.65 -2571250.00 157221.00 13670.80 175.00 99.894 SIU 13600.20 1726,19 24741.50 29,73 156809.00 175.00 >100 106,24 -35.14 1845.24 -446.30 1904.76 -52.11 -60.76 2023.81 19769.70 +794.74-62,58 -2571250.00 -154539.00 -13475.20 355.00 >100 13452,40 >100 -41.34 -13406.30 -381,45 -30.04 -2571250.00 >100 40 2321,43 -14824.40 -240.07 -18.90 -2571250.00 -152574.00 -11649.90 355.63 >100 41 2380.95 -13838.00 -118.02-9,29 -2571250.00 -152155.00 -11629.10 355.60 440.48 -151737.00

0.00 -2571250.00

>100

0.00

					che a t			Was dec		100 - 4	am - d	15-4-	
Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	/m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIJ	7464.87	-621.44	0.85	11.31	7490.69	1.00	32294.70	338376.00	32294.70	4,311
- 2	59.52	1	SLU	4987.45	-415.20	0.85	11.31	5004,70	1.00	32294.70	338502.00	32294.70	6.453
3	119.05	1	SIJJ	2854.09	-237.60	0.85	11.31	2863.96	1.00	32294.70	338514.00	32294.70	11.276
4	178.57	1	SLU	1039.77	-86.56	0.85	11.31	1043.37	1.00	32294.70	338526.00	32294.70	30.952
.5	238.09	1	SIJ	-481.18	40.06	0.85	11.31	482.84	1.00	32294.70	338539.00	32294.70	66.885
.6	297.62	1	SILI	-1734.68	144-41	0.85	11.31	1740.68	1,00	32294.70	338551.00	32294.70	18.553
7	357.14	1	SIU	-3065.92	255.23	0.85	11.31	3076.53	1.00	32294.70	338564,00	32294.70	10.497
- 8	416.67	1	SLU	-4427.83	368.61	0.85	11.31	4443.15	1.00	32294.70	338415.00	32294.70	7.268
9	476.19	1	SLU	-5461.88	454.69	0.85	11.31	5480.77	1.00	32294.70	338266.00	32294.70	5.892
10	535.71	1	SILI	-6208.58	516.86	0.85	11.31	6230.05	1.00	32294.70	338118.00	32294.70	5.184
11	595.24	1	SIJ	-6706.25	558.29	0.85	11.31	6729.45	1.00	32294.70	337970.00	32294.70	4.799
12	654.76	1	SIU	-6990.74	581.97	0.85	11.31	7014.93	1.00	32294.70	337822.00	32294.70	4.604
13	714.29	1	SLU	-7095.25	590.67	0.85	11,31	7119.79	1.00	32294.70	337675.00	32294.70	4,536
14	773.81	1	SLU	-7050.17	586.92	0.85	11.31	7074,55	1.00	32294.70	337528.00	32294.70	4.565
15	833.33	1	SLU	-6883.06	573.00	0.85	11.31	6906.87	1,00	32294.70	337381.00	32294.70	4.676
1.6	892,86	1	SLU	-6618.70	551.00	0.85	11.31	6641.60	1.00	32294.70	337234.00	32294.70	4.862
17	952.38	1	SIJJ	-6279.11	522.73	0.85	11.31	6300.83	1.00	32294.70	337088.00	32294.70	5.125
18	1011.90	1	SLU	-5883.68	489.81	0.85	11.31	5904.03	1,00	32294.70	336942.00	32294.70	5.470
19	1071.43	1	SLU	-5449.28	453.64	0.85	11.31	5468.13	1.00	32294.70	336797.00	32294.70	5.906
20	1130.95	1	SIU	-4990.47	415.45	0.85	11.31	5007.73	1.00	32294.70	336652.00	32294.70	5.449
21	1190.48	1	SLU	-4519.61	376.25	0.85	11.31	4535.24	1.00	32294.70	336507.00	32294.70	7.121
22	1250.00	1	SIAI	-4047.09	336.91	0.85	11.31	4061.09	1.00	32294.70	336362.00	32294.70	7.952
23	1309.52	1	SIJJ	-3581.49	298.15	0.85	11.31	3593.88	1.00	32294.70	336217.00	32294.70	8.986
24	1369.05	1	SLU	-3129.78	260.55	0.85	11.31	3140.61	1.00	32294.70	336073.00	32294.70	10.283
25	1428.57	1	SLU	-2697.51	224.56	0.85	11.31	2706.84	1.00	32294.70	335929.00	32294.70	11.931
26	1488.10	1	SLU	-2288.98	190.55	0.85	11,31	2296.90	1.00	32294.70	335785.00	32294.70	14.060
27	1547.62	1	SIU	-1907.41	158.79	0.85	11.31	1914.01	1.00	32294.70	335642.00	32294.70	16.873
28	1607.14	1	SLU	-1555.11	129.46	0.85	11.31	1560.49	1.00	32294.70	335498.00	32294.70	20.695
29	1666.67	1	SLU	-1233.64	102.70	0.85	11.31	1237.90	1.00	32294.70	335355.00	32294.70	26.088
30	1726.19	1	SIJ	-943.92	78.58	0.85	11.31	947.18	1.00	32294.70	335212.00	32294.70	34.096
31	1785.71	1	SLU	-686.40	57.14	0.85	11.31	688.78	1.00	32294.70	335069.00	32294,70	46.887
32	1845.24	1	SLU	-461.15	38.39	0.85	11.31	462.75	1.00	32294.70	334927.00	32294.70	69.789
33	1904.76	1	SIJ	-267.96	22.31	0.85	11.31	268.89	1.00	32294.70	334784.00	32294.70	>100
34	1964.29	1	SLU	-106.44	8.86	0.85	11.31	106.81	1.00	32294.70	334642.00	32294.70	>100
35	2023.81	1	SEU	23.92	-1.99	0.85	11.31	24.00	1.00	32294.70	334500.00	32294.70	>100
36	2083.33	1	SLU	123.64	-10.29	0.85	11.31	124.07	1.00	32294.70	334358.00	32294.70	>100
37	2142.86	1	SLU	193.27	-16.09	0.85	11.31	193.94	1.00	32294.70	334216.00	32294.70	>100
38	2202,38	1	SLU	233,28	-19.42	0.85	11.31	234.09	1.00	32294.70	334074.00	32294.70	>100
39	2261,90	1	SLU	244.08	-20.32	0.85	11,31	244.93	1.00	32294.70	333933.00	32294.70	>100
40	2321.43	1	SIAI	225.98	-18.81	0.85	11.31	226.76	1.00	32294.70	333792.00	32294.70	>100
41	2380,95	1	SLU	179.20	-14.92	0.85	11.31	179.82	1.00	32294.70	333650.00	32294.70	>100
42	2440.48	1	SIU	103.85	-8.65	0.85	11.31	104.21	1.00	32294.70	333509.00	32294.70	>100

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1 SLU -11867.20

							R	elazı	one di c	alcolo
Caso	x	oc	TCC	N	Mz	My	Aft	AfC	σ _C	σĒ
0.00	<cm></cm>		3350	<dan></dan>	<danm></danm>	<danm></danm>	<cmq></cmq>	<cmq></cmq>	<dan cmq=""></dan>	<dan cmq2<="" td=""></dan>
44	0.00	2	SLE R	-34686.80	3439.12	43677.10	50.27	28.27	43,33	1176.0
45	59.52	2	SLE R	-35653.80	3654.32	46410.20	50.27	28.27	46,10	1265.5
46	119.05	2	SLE R	-35905.90 -36159.20	3789.53	48127.40	50.27	28.27	47.85	1326.6
47	178.57	2	SLE R	-36159.20 -36413.60	3856.26	48974.90 49087.80	50.27	28.27	48,71	1355.0
49	238.09	2	SLE R	-36669.20	3865.15	48589.70	50.27	28.27	48.82 48.29	1355.8
50	357.14	2		-36925,90	3743.76	47546.10	50.27	28.27	47,20	1291.2
51	416.67	2	SLE R	-36169.90	3612.62	45880.60	50.27	28.27	45.52	1238.8
52	476.19	2	SLE R	-35415.90	3439.99	43688.30	50.27	28.27	43.30	1166.7
53	535.71	2	SLE R	-34663.80	3236.56	41104.60	50.27	28.27	40.67	1080.1
54	595.24	2	SLE R	-33913.60	3011.63	38247.90	50,27	28.27	37,76	983.3
55	654.76	2	SLE R	-33165.20	2773.21	35220.00	47.12	31.42	34,66	880.4
56	714.29	2	SLE R	-32418.50	2528.13	32107.50	47.12	31.42	31.47	774.6
57	773.81	2	SLE R	-31673.60	2282.10	28982.90	43.98	34.56	28.25	668.8
58	833.33	2	SLE R	-30930.40	2039.84	25906.10	43.98	34.56	25.08	565.5
59	892.86	2	SLE R	-30188.90	1805.13	22925.30	43.98	34.56	22.00	466.6
60	952,38	2	SLE R	-29449.00	1580,97	20078.50	43.98	34.56	19,04	374.0
61	1011,90	2	SLE R	-28710.60	1369.63	17394.40	43.98		16.25	289.0
62	1071.43	2	SLE R	-27973.80	1172.74	14893.90	40.84		13.66	213.3
63	1130.95	2	SLE R	-27238.50	991.40	12590.90	37,70	40.84	11.29	154.1
64	1190,48	2	SLE R	-26504.70	826.24	10493.30	37.70	40.84	9,19	126.7
65	1250.00	2	SLE R	-25772.20	677.48	8604.10	31.42	47.12	7.41	103.1
66	1309.52	2	SLE R	-25041.20	545.04	6922.10	25.13	53.41	5.98	84.0
68	1369.05	2	SLE R	-24311.50 -23583.10	428.55	5442.63 4158.29	6.28	59.69 72.26	4.89	69.2 58.1
69	1488.10	2	SLE R	-23583.10	240.91	3059.52	0.00	72.26	4.07 3.44	49.4
70	1547.62	2	SLE R	-22130.10	168.12	2135.10	0.00		2,90	42.0
71	1607.14	2	SLE R	-21405.40	108.08	1372.59	0.00	78.54	2,45	35.7
72	1666.67	2	SLE R	-20681.80	59.74	758.72	0.00	-	2.07	30.5
73	1726.19	2	SLE R		22.02	279.66	-	78.54	1,77	26.3
74	1785.71	2	SLE R	-19237.90	-6.20	-78.70	0.00	78.54	1.60	24.0
75	1845.24	2	SLE R	-18517.60	-26.03	-330.59	0.00	78.54	1.68	24.9
.76	1904.76	2	SLE R	-17798.20	-38.60	-490.22	0.00	78.54	1,70	25.1
77	1964.29	2	SLE R	-17079.80	-45.01	-571.63	0.00	78.54	1.68	24.8
78	2023,81	2	SLE R	-16362,30	-46.35	-588.70	0.00	78.54	1.63	24.0
79	2083.33	2	SLE R	-15645.70	-43.70	-555.04	0.00	78.54	1,56	22.9
80	2142.86	2	SLE R	-14929.90	-38.11	-484.05	0.00	_	1.46	21.6
81	2202.38	2	SLE R	-14215.00	-30.62	-388.90	0.00	-	1,36	20.0
82	2261.90	2	SLE R	-13500.80	-22.25	-282.56	0.00		1,24	18.4
83	2321.43	2	SLE R	-	-14.00	-177.83		78.54	1.13	16.8
85		-	SLE R	-12074.50 -11362.30			_	_	0.94	15.3
86		_		-10650.80				78.54	0.87	12.9
87	0.00			-34686.80					43.33	1176.0
88	59.52	_		-35653.80					46.10	1265.5
89	119.05			-35905.90					47.85	1326.6
90	178.57	4	SLE Q	-36159.20	3856.26	48974.90	50.27	28.27	48.71	1355.0
91	238.09	4	SLE Q	-36413.60	3865.15	49087.80	50.27	28.27	48.82	1355.8
92	297.62			-36669.20					48.29	1333.7
93	357,14			-36925.90					47,20	1291.2
94		_	_	-36169.90			_	_	45.52	1238.8
9.5	476.19	_		-35415.90					43.30	
96	535.71			-34663.80					40.67	1080.1
97	595.24			-33913.60					37.76	983.3
98		_		-33165.20					34.66	
99	714.29			-32418.50 -31673.60					31.47 28.25	774.6
100				-31673.60					25.0B	
102	892.86			-30188.90					22,00	466.6
103		-		-29449.00					19.04	374.0
_	1011.90			-28710.60					16.25	289.0
	1071.43			-27973.80					13.66	213.3
-	1130.95			-27238.50		12590.90			11.29	154.1
	1190.48	4	SLE Q	-26504.70					9.19	126.7
108	1250,00	4	SLE Q	-25772.20	677.48	8604.10		-	7,41	103.1
109	1309.52	4	SLE Q	-25041.20		6922.10	25.13	53.41	5.98	84.0
110	1369.05			-24311.50	428.55	5442.63			4.89	69.2
111	1428.57		SLE Q			4158.29	6,28	72.26	4,07	58.1
	1488.10			-22856.00		3059.52	_	78.54	3,44	49.4
	1547.62	•	SLE Q		168.12			78.54	2.90	42.0
	1607.14	_		-21405.40				78.54	2,45	35.7
_	1666.67	_		-20681.80				78.54	2,07	30.5
	1726.19	4	SIE Q	-19959.30	22.02	279.66		78.54	1.77	26.3
_	1785.71	100	CO. 10.	-19237.90	-6.20	-78.70	49	78.54	1.60	24.0

								CIGALO	ic ai cai	0010
118	1845.24	4	SLE Q	-18517.60	-26.03	-330.59	0.00	78.54	1.68	24.90
119	1904.76	4	SLE Q	-17798.20	-38.60	~490.22	0.00	78.54	1.70	25.14
1.20	1964.29	4	SLE Q	-17079.80	-45.01	-571.63	0.00	78.54	1.68	24.84
121	2023.81	4	SLE Q	-16362.30	-46.35	-588.70	0.00	78.54	1.63	24.0B
122	2083.33	4	SLE Q	-15645.70	-43.70	-555.04	0.00	78.54	1.56	22.97
123	2142.86	4	SLE Q	-14929.90	-38.11	-484.05	0.00	78.54	1.46	21.60
124	2202.38	4	SLE Q	-14215.00	-30.62	-388.90	0.00	78.54	1.36	20.06
125	2261,90	4	SLE Q	-13500.80	-22.25	-282.56	0.00	78.54	1.24	18.44
126	2321.43	4	SLE Q	-12787.30	-14.00	-177.83	0.00	78.54	1.13	16.84
127	2380.95	4	SLE Q	-12074.50	-6.88	-87.42	0.00	78.54	1.03	15.34
128	2440.48	4	SLE Q	-11362.30	-1.89	-23.95	0.00	78.54	0.94	14.02
129	2500.00	4	SLE Q	-10650.80	0.00	0.00	0.00	78.54	0.87	12.99

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	cc	manual)	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c omm>	s <mm></mm>	K 2	Φeq	Δ _{sm} <mm></mm>	A _S <cmq></cmq>	A _{c eff} <cmq></cmq>	σ ₁₁ <dan cmq=""></dan>	e _{sm}	Wk <mm< th=""></mm<>
87	0.00	4	SLE Q	-34686.80	43677.10	3439.12	46.00	136.36	0.50	20.00	194.12	25.13	1283.22	1176.01	0.34	0.1
88	59.52	4	SLE Q	-35653.80	46410,20	3654.32	46.00	136.36	0.50	20100	194.40	25.13	1286.83	1265.57	0.37	0.1
89	119.05	4	SLE Q	-35905.90	48127.40	3789.53	46.00	136.36	0.50	20,00	194.65	25.13	1289.88	1326,61	0.39	0.1
90	178.57	4	SLE Q	-36159.20	48974.90	3856.26	46.00	136.36	0.50	20.00	194.73	25.13	1290.94	1355.03	0.39	0.1
91	238.09	4	SLE Q	-36413.60	49087.80	3865.15	46.00	136.36	0.50	20.00	194.69	25.13	1290,47	1355.87	0.39	0.1
92	297.62	4	SLE Q	-36669.20	48589.70	3825.93	46.00	136.36	0.50	20.00	194,55	25.13	1288.70	1333.78	0.39	0.1
93	357.14	4	SLE Q	-36925.90	47546.10	3743.76	46.00	136.36	0.50	20.00	194.31	25.13	1285.66	1291.24	0.38	0.1
94	416.67	4	SLE Q	-36169.90	45880.60	3612.62	45.00	136.36	0.50	20.00	194.18	25.13	1284.03	1238.88	0.36	0.1
95	476.19	4	SLE Q	-35415.90	43688.30	3439.99	46.00	136.36	0.50	20.00	193.93	25.13	1280.91	1166,79	0.34	0.1
96	535.71	4	SLE Q	-34663.80	41104.60	3236.56	46.00	136.36	0.50	20.00	193.56	25.13	1276.28	1080.12	0.31	0.1
.97	595.24	4	SLE Q	-33913.60	38247.90	3011.63	46.00	136.36	0.50	20.00	193.06	25.13	1270.03	983.36	0.29	0.0
98	654.76	4	SLE Q	-33165.20	35220.00	2773.21	46,00	136.36	0.50	20.00	206.77	21.99	1261.94	880,41	0.26	0.0
99	714.29	4	SLE Q	-32418.50	32107.50	2528.13	46.00	136.36	0.50	20.00	205.83	21.99	1251.66	774.64	0.23	0.0
100	773.81	4	SLE Q	-31673.60	28982.90	2282.10	46.00	136.36	0.50	20.00	204.65	21.99	1238.68	668.88	0.19	0.0
101	833.33	4	SLE Q	-30930.40	25906.10	2039.84	46.00	136.36	0.50	20.00	203,16	21.99	1222.26	565.55	0.16	0.0
102	892,86	4	SLE Q	-30188.90	22925.30	1805.13	46.00	136.36	0.50	20.00	219.45	18.85	1201.15	466.68	0.14	0.0
103	952.38	4	SLE Q	-29449.00	20078.50	1580.97	46.00	136.36	0.50	20.00	216.51	18.85	1173.53	374.01	0.11	0.0
104	1011.90	4	SLE Q	-28710.60	17394.40	1369.63	46.00	136.36	0.50	20,00	212.60	18.85	1136.62	289.09	0.08	0.0
105	1071.43	4	SLE O	-27973.80	14893.90	1172.74	46.00	136.36	0.50	20,00	207.24	18.85	1086.15	213.39	0.06	0.0
106	1130,95	4	SLE O	-27238.50	12590.90	991.40	46,00	136.36	0.50	20.00	199.74	18.85	1015.38	148.38	0.04	0.0
107	1190.48	4	SLE O	-26504.70	10493.30	B26.24	46.00	136,36	0.50	20.00	188.82	18.85	912.49	95.48	0.03	0.0
108	1250.00	4	SLE Q	-25772,20	8604.10	677.48	46.00	136.36	0.50	20.00	211.74	12.57	752.37	55.63	0.02	0.0
109	1309.52	4	SLE O	-25041.20	6922.10	545.04	46,00	136,36	0.50	20.00	170.93	12.57	495.93	28,28	0.01	0.0
110	1369.05	4	SLE O	-24311.50	5442.63	428,55	46,00	136,36	0.50	20.00	168,60	6.28	240.65	11.02	0.00	0.0
130	0.00	3	SLE F	-34686.80	43677.10	3439.12	46.00	136,36	0.50	20.00	194.12	25.13	1283,22	1176.01	0.34	0.1
131	59.52	3	SLE F	-35653.80	46410.20	3654.32	46.00	136.36	0.50	20.00	194,40	25.13	1286.83	1265.57	0.37	0.1
132	119.05	3	-	-35905.90	48127.40	3789.53	46,00	136.36	0.50	20.00	194.65	25.13	1289.88	1326.61	0.39	0.1
133	178.57	3	_	-36159.20	48974.90	3856.26	46.00	136.36	0.50	20.00	194.73	25.13	1290.94	1355.03	0.39	0.1
134	238.09	3	-	-36413.60	49087.80	3865.15	46.00	136.36	0.50	20,00	194.69	25.13	1290.47	1355.87	0.39	0.3
135	297.62	3	SLE F	-36669,20	48589.70	3825.93	46.00	136,36	0.50	20.00	194.55	25.13	1288.70	1333.78	0.39	0.1
136	357.14	3	SLE F	-36925.90	47546.10	3743.76	46.00	136.36	0.50	20.00	194.31	25.13	1285.66	1291.24	0.38	0.1
137	416.67	3	SLE F	-36169.90	45880,60	3612.62	46.00	136.36	0.50	20.00	194.18	25.13	1284.03	1238.88	0.36	0.1
138	476,19	3	SLE F	-35415.90	43688.30	3439.99	-	136,36	0.50	20.00	193.93	25.13	1280.91	1166,79	0.34	0.1
139	535.71	3	_	-34663.80	41104.60	3236.56	46.00	136,36	0.50	20.00	193.56	25.13	1276.28	1080.12	0.31	0.1
140	595.24	3	SIE F	-33913.60	38247,90	3011.63	46.00	136,36	0.50	20.00	193.06	25.13	1270.03	983.36	0.29	0.0
141	654.76	3	SLE F	-33165,20	35220.00	2773.21	46.00	136.36	0.50	20,00	206,77	21.99	1261.94	880.41	0.26	0.0
142	714,29	3	SLE F	-32418.50	32107.50	2528.13	46,00	136,36	0.50	20,00	205,83	21.99	1251.66	774.64	0.23	0.0
143	773.81	3	SLE F	-31673.60	28982.90	2282.10	46,00	136.36	0.50	20.00	204.65	21.99	1238.68	668.88	0.19	0.0
144	833.33	3	SLE F	-30930.40	25906.10	2039.84	46.00	136.36	0.50	20.00	203,16	21.99	1222.26	565.55	0.16	0.0
145	892.86	3		-30188.90	22925.30	1805.13	46.00	136.36	0.50	20.00	219.45	18.85	1201.15	466.68	0.14	0.0
146	952.38	3	_	-29449.00	20078.50	1580.97	46.00	136.36	0.50	20.00	216.51	18.85	1173.53	374.01	0.11	0.0
147	1011.90	3	_	-28710.60	17394.40	1369.63	46.00	136.36	0.50	20.00	212,60	18.85	1136.62	289.09	0.08	0.0
148	1071.43	3	SLE F	-27973.80	14893.90	1172.74	46.00	136.36	0.50	20.00	207.24	18.85	1086.15	213.39	0.06	0.0
149	1130.95	3	SLE F	-27238.50	12590.90	991.40	46.00	136.36	0.50	20.00	199.74	18.85	1015.38	148.38	0.04	0.0
150	1190.48	3	SLE F	-26504.70	10493.30	826.24	46.00	136.36	0.50	20.00	188.82	18.85	912.49	95.48	0.03	0.0
151	1250.00	3	SLE F	-25772.20	8604.10	677.48	46.00	136.36	0.50	20.00	211.74	12.57	752.37	55.63	0.02	0.0
152	1309,52	3	SLE F	-25041.20	6922.10	545.04	46,00	136.36	0.50	20.00	170.93	12.57	495.93	28.28	0.02	0.0
126	7003675	3	SLE F	-24311.50	5442.63	428.55	46.00	136.36	0.50	20.00	168.60	6.2B	240.65	11.02	0.00	0.0

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
. 5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.),C.Rare - Sf max (max traz.),C.Rare - Sf min (max compr.)
69	C.Rare - Sc max (min. compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
112	C.Q.Per, - Sc max (min. compr.)
134	C.Freq - Wk Max

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf (B)	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307,10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 16 (-29)

Caso	8	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	81184.60	7266.56	-802.52	60509.70	-10373.50
	1	SIJ	TNG	-		5 1	0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SLU	TOT	81184.60	7266.56	-802.52	60509.70	-10373.50
- 2	2	SLE R	RVN	60136.70	5382.63	-594.46	44822.00	-7684.04
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	60136.70	5382.63	-594.46	44822.00	-7684.04
3	3	SLE P	RVN	60136.70	5382.63	-594.46	44822.00	-7684.04
	3	SLE F	TAG				0.00	0.00
	. 3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	60136.70	5382.63	-594.46	44822.00	-7684.04
-4	4	SLE Q	RVN	60136.70	5382.63	-594.46	44822.00	-7684.04
	4	SLE Q	TAG				0.00	0.00
	4	SIR Q	ECC				0.00	0.00
	4	SIE Q	TOT	60136.70	5382.63	-594.46	44822.00	-7684.04

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-81184.60	-7266.56	802.52	-60509,70	10373.50
.2	2	SLE R	1	-60136.70	-5382,63	594.46	-44822.00	7684.04
- 3	3	SLE F	1	-60136.70	-5382.63	594.46	-44822.00	7684.04
4	. 4	SLE Q	- 1	-60136.70	-5382,63	594,46	-44822.00	7684.04

Da 0 a -25

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SIJ	-81184.60	60259.00	10330.50	-81184.60	177580.00	31570.30	2-3	170.00	2.950
2	59.52	1	SLU	-81828,40	63795.60	10936.80	-81828,40	177834.00	31616.90	2-3	170.00	2.791
- 3	119.05	1	SLU	-B1435.60	65967.00	11309.00	-81435.60	177679.00	31588.50	2-3	170.00	2.696
4	178.57	1	SIU	-81045.30	66971.30	11481.20	-81045.30	177525.00	31560.20	2-3	170.00	2.654
- 5	238.09	1	SLU	-80657.60	66991.10	11484.60	-80657.60	177372.00	31532.20	2-3	170.00	2,651
.6	297.62	1	SLU	-80272.40	66193.60	11347.90	-80272.40	177220.00	31504.30	2-3	170.00	2.680
7	357.14	1	SLU	-79889.70	64668.00	11086.30	-79889.70	177068.00	31476.60	2-3	170.00	2.741
.8	416.67	1	SIJ	-78041.90	62314.60	10682.90	-78041.90	176338.00	31342.80	2-3	170.00	2.833
9	476.19	1	SIAI	-76198.30	59262,20	10159.60	-76198.30	175610.00	31209.40	2-3	176.00	2.966
10	535.71	1	SLU	-74358.70	55693.30	9547.76	-74358.70	174883.00	31076.30	2-3	170.00	3.143
11	595,24	1	SLU	-72523,10	51766.90	8874.62	-72523,10	174155.00	30942.80	2-3	170.00	3.368
12	654.76	1	SLU	-70691.40	47619.60	8163.63	-70691.40	173426.00	30809.00	2-3	170.00	3.646
13	714.29	1	SLU	-68863.60	43367.60	7434.70	-68863.60	172698.00	30675.40	2+3	170.00	3.986
14	773.81	1	SLU	-67039.40	39108.00	6704.47	-67039.40	171972.00	30542.10	2-3	170.00	4.402
15	833.33	1	SLU	-65218.80	34920.90	5986.65	-65218.80	171247.00	30409.10	2-3	170.00	4.909
16	892.86	11	SEU	-63401.70	30870.50	5292.26	-63401.70	170520.00	30275.70	2-3	170.00	5.529
17	952,38	1	SIJ	-61588.00	27007.20	4629.96	-61588.00	169793.00	30141.90	2-3	170.00	6.293
18	1011,90	1	SIJ	-59777.60	23369.10	4006.27	-59777.60	169068.00	30008.40	2-3	170.00	7.242
19	1071.43	1	SLU	-57970.40	19983.70	3425.90	-57970.40	168343.00	29875,10	2-3	170.00	B.433
20	1130.95	1	SLU	-56166.30	16869.00	2891.93	-56166.30	167619.00	29742.00	2-3	170.00	9.947
21	1190.48	1	SLU	-54365.20	14035.20	2406.12	-54365.20	166894.00	29608.40	2-3	170.00	11.903
22	1250.00	1	SLU	-52567.10	11485.60	1969.03	-52567.10	166168.00	29474,50	2-3	170.00	14.482
23	1309.52	1	SIU	-50771.70	9218.11	1580.30	-50771.70	165443.00	29340.80	2-3	170.00	17.966
24	1369.05	-1	SLU	-48979.10	7225.94	1238.78	-48979.10	164719.00	29207.40	2-3	170.00	22.818
25	1428.57	1	SIU	-47189.10	5498.69	942.66	-47189.10	163996.00	29074.10	2-3	170.00	29.854
26	1488.10	1	SIJ	-45401.70	4023.06	689.69	-45401.70	163272.00	28940.30	2+3	170,00	40.624
27	1547.62	1	SIJ	-43616.70	2783.59	477.20	-43616.70	162546.00	28806.10	2-3	170.00	58.452
28	1607.14	1	SLU	-41834.00	1763.21	302.27	-2571250.00	161822.00	28672.10	2-3	170.00	61.463
29	1666.67	1	SLU	-40053.60	943.73	161.79	-2571250.00	161098.00	28538.30	2-3	170.00	64.195

	 Control of the Control of the Control 	1.4	APPROXITE (100 miles	
Pa	lazione	a	00	COL	\sim
11	azione:	111	Local		

30	1726.19	1	SLU	-38275.30	306.30	52.51	-2571250.00	160375.00	28404.60	2-3	170,00	67.178
31	1785.71	1	SLU	-36499.00	-168.34	-28.86	-2571250.00	-159940.00	-27992.70	2-3	350.00	70.447
32	1845.24	1	SIU	-34724,80	-499.55	-85.64	-2571250.00	-159206.00	-27928.40	2+3	350.00	74.046
33	1904.76	1	SLU	-32952.40	-706.60	-121.14	-2571250.00	-158471.00	-27866.80	2-3	350.00	78.029
34	1964.29	1	SLU	-31101.70	-808.60	-138.62	-2571250.00	-157735.00	-27806.20	2-3	350.00	82,460
35	2023.81	1	SLU	-29412.70	-824.34	-141.32	-2571250.00	-156999.00	-27745.10	2+3	350.00	87.419
36	2083.33	1	SLU	-27645.30	-772.28	-132,40	-2571250.00	-156264.00	-27683.60	2-3	350.00	93.008
37	2142,86	1	SLU	-25879.40	-670.58	-114.96	-2571250.00	-155530.00	-27621.60	2-3	350.00	99.355
38	2202.38	1	SLU	-24114.90	-537.04	~92.07	-2571250.00	-154794.00	-27560.50	2-3	350.00	>100
39	2261.90	1	SIJ	-22351.70	-389.24	-66.73	-2571250.00	-154052.00	-27458.60	2-3	350,00	>100
40	2321.43	1	SLU	-20589.60	-244.51	~41.92	-2571250.00	-153306.00	-27321.00	2-3	350.00	>100
41	2380.95	1	SLU	-18828.70	-120.01	-20.57	-2571250.00	-152561.00	-27183.50	2-3	350.00	>1.00
42	2440.48	1	SIAJ	-17068.80	-32.84	-5.63	-2571250.00	-151815.00	-27046,20	2-3	350.00	>100
43	2500.00	1	SLU	-15309,80	0.00	0.00	-2571250.00					>100

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7266.56	-802.52	0.85	11.31	7310.74	1.00	32294.70	343297.00	32294.70	4.417
- 2	59.52	1	SLU	4777.25	-527.60	0.85	11.31	4806.29	1.00	32294.70	343389.00	32294.70	6.719
3	119.05	1	SIAI	2636.30	-291.15	0.85	11.31	2652.33	1.00	32294.70	343333.00	32294.70	12.176
4	178.57	1	SIJ	818.06	-90.35	0.85	11.31	823.03	1.00	32294.70	343277,00	32294.70	39.239
- 5	238.09	1	SLU	-703.74	77.72	0.85	11.31	708.02	1,00	32294.70	343221.00	32294.70	45.613
6	297.62	1	SLU	-1955.57	215.97	0.85	11.31	1967.46	1.00	32294.70	343166.00	32294.70	16,414
7	357.14	1	SLU	-3281.44	362.40	0.85	11.31	3301.39	1.00	32294.70	343111.00	32294.70	9.782
- 8	416.67	1	SLU	-4634.22	511.81	0.85	11.31	4662.40	1.00	32294.70	342847.00	32294.70	6.927
9	476.19	1	SIU	-5657.06	624.77	0.85	11.31	5691.45	1.00	32294.70	342583.00	32294.70	5.674
10	535.71	1	SLU	-6391.02	705.83	0.85	11.31	6429.88	1.00	32294.70	342319,00	32294.70	5.023
11	595.24	1	SLU	-6874.95	759.27	0.85	11.31	6916.75	1.00	32294.70	342056.00	32294.70	4,669
12	654.76	1	SILI	-7145.11	789.11	0.85	11.31	7188.55	1.00	32294.70	341794.00	32294.70	4.493
13	714,29	1	SLU	-7235.06	799.04	0.85	11.31	7279.05	1.00	32294.70	341532.00	32294.70	4.437
14	773.81	1	SLU	-7175.49	792.46	0.85	11.31	7219.11	1.00	32294.70	341271.00	32294.70	4.473
15	833.33	1	SIU	-6994.21	772.44	0.85	11.31	7036.74	1.00	32294.70	341010.00	32294.70	4.589
16	892.86	1	SLU	-6716,20	741.74	0.85	11.31	6757.03	1.00	32294.70	340750.00	32294.70	4,779
17	952,38	1	SIJ	-6363.61	702.80	0.85	11.31	6402.30	1.00	32294.70	340490.00	32294.70	5.044
18	1011.90	1	SIJJ	-5955.94	657.78	0.85	11.31	5992.15	1.00	32294.70	340231.00	32294.70	5.389
19	1071.43	1	SIU	-5510.16	608.54	0.85	11.31	5543.66	1.00	32294.70	339972.00	32294.70	5.826
2.0	1130.95	1	SIJ	-5040.86	556.71	0.85	11.31	5071.51	1.00	32294.70	339713.00	32294.70	6.368
21	1190.48	1	SIAI	-4560.43	503.65	0.85	11.31	4588.16	1,00	32294.70	339455.00	32294.70	7.039
.22	1250.00	1	SIAJ	-4079,26	450.51	0.85	11.31	4104.06	1.00	32294.70	339198.00	32294.70	7.869
23	1309.52	1	SLU	-3605.92	398.24	0.85	11.31	3627,85	1.00	32294.70	338941.00	32294.70	8.902
24	1369.05	1	SIAI	-3147.36	347.60	0.85	11.31	3166.49	1.00	32294.70	338684.00	32294.70	10.199
25	1428,57	1	SILI	-2709.08	299.19	0.85	11.31	2725.55	1.00	32294.70	338427,00	32294.70	11.849
26	1488.10	1	SIJ	-2295,35	253.50	0.85	11.31	2309.30	1.00	32294.70	338171,00	32294.70	13.985
27	1547.62	1	SIU	-1909.33	210.87	0.85	11.31	1920.94	1.00	32294.70	337916.00	32294.70	16.812
28	1607,14	1	SLU	-1553.30	171.55	0.85	11,31	1562.75	1.00	32294.70	337660.00	32294.70	20.665
29	1666.67	1	SLU	-1228.76	135.70	0.85	11.31	1236.23	1.00	32294.70	337405.00	32294.70	26,124
30	1726.19	1	SLU	-936.58	103.44	0.85	11.31	942.28	1,00	32294.70	337151.00	32294.70	34.273
31	1785.71	1	SLU	-677.17	74.79	0.85	11.31	681.29	1.00	32294.70	336896.00	32294.70	47.403
32	1845.24	1	SIJJ	-450.54	49.76	0.85	11.31	453.28	1.00	32294.70	336642.00	32294.70	71.246
33	1904.76	1	SLU	-256.45	28.32	0.85	11.31	258.01	1,00	32294.70	336388.00	32294.70	>100
34	1964.29	1	SLU	-94.47	10.43	0.85	11.31	95.04	1.00	32294.70	336135.00	32294.70	>100
35	2023.81	1	SIJ	35,94	-3.97	0.85	11.31	36.15	1.00	32294.70	335881.00	32294.70	>100
36	2083.33	1	SLU	135.33	-14.95	0.85	11.31	136.15	1.00	32294.70	335628.00	32294.70	>100
37	2142.86	1	SLU	204.26	-22.56	0.85	11.31	205.51	1.00	32294.70	335375.00	32294.70	>100
38	2202.38	1	SLU	243.24	-26.86	0.85	11.31	244.72	1.00	32294.70	335122.00	32294.70	>100
39	2261.90	1	SIJ	252.68	-27.91	0.85	11.31	254.22	1.00	32294.70	334870.00	32294.70	>100
40	2321.43	1	SLU	232.90	-25.72	0.85	11.31	234.31	1.00	32294.70	334617.00	32294.70	>100
41	2380.95	1	SLU	184.12	-20.33	0.85	11,31	185.24	1.00	32294.70	334365.00	32294.70	>100
42	2440.48	1	SIJ	106.47	-11.76	0.85	11.31	107.11	1.00	32294.70	334113.00	32294.70	>100

Caso 44	X <cm>></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <mq></mq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>	
	0.00	2	SLE R	-60136.70	7652.20	44636.30	47.12	31,42	42,87	915.33	
45	59.52	2	SLE R	-60926.80	8101.31	47256.00	47.12	31.42	45.57	1001.60	
46	119.05	2	SLE R	-60826.00	8377.05	48864.50	47.12	31,42	47.27	1061.89	
47	178.57	2	SLE R	-60727.00	8504.58	49608.30	47.12	31,42	48.06	1090.50	
48	238.09	2	SLE R	-60630.00	8507.10	49623.00	47.12	31.42	48.08	1092.23	
49	297.62	2	SLE R	-60534.80	8405.83	49032.30	47.12	31.42	47.47	1071.60	
50	357.14	2	SLE B	-60441.60	8212.09	47902.20	47.12	31.42	46.29	1031.14	
51	416.67	2	SLE R	-59088.00	7913.24	46159.00	47.12	31.42	44,54	983.44	
52	476.19	2	SLE R	-57737.60	7525.62	43897.90	47.12	31.42	42,26	916.82	
53	535.71	2	SLE R	-56390.30	7072.41	41254.30	47.12	31.42	39.57	836.46	
54	595.24	2	SLE R	-55046.00	6573.80	38345.80	43.98	34.56	36.59	746.97	
55	654.76	2	SLE B	-53704.70	6047.14	35273.80	43.98	34.56	33.44	652.38	
56	714,29	2	SLE R	-52366.20	5507.18	32124.10	40.84	37.70	30,20	556.27	

72	5 8		1 6				R	elazi	one di c			
57		_	_	-51030.60			_	_	26,95			
- 58	833.33	-	SLE R			25867.30	-	_	23.76	371.61		
59	892.86	$\overline{}$	SLE R		3920.19	22867.00	-	_	20.69	288.31		
60	952.38	2	SLE R	-47039.80 -45714.70	2967.61	20005.30	37.70	40.84	17.81	244.79		
62	1071.43	_	SLE B	-	2537.70	14802.70	34.56	_	12.82	178.72		
-	1130.95	-	SLE R		2142.17	12495.60		50.27	10.81	151.78		
64	1190.48	2	SLE R	-41753.80	1782.31	10396.40	21.99	56.55	9.15	129.32		
-65	1250.00	2	SLE R	-40438.00	1458.54	8507.86	15.71	62.83	7.81	111.04		
66	1309.52	2	SLE R	-39124.50	1170.59	6828.23	3.14	75.40	6.74	96.29		
67	1369.05	2	SLE B		917.61	5352.55	0.00	_	5.86	84.11		
_	1428.57	2	SLE B		698.27	4073.10	-	78.54	5.08	73.43		
	1488.10	2	_		510.88	2980.05	0.00	_	4,41	64.07		
_	1547.62	2	-		353.48 223.91	2061.92	-	78.54	3,83	55.96 49.01		
-	1666.67	_	SLE R		119.84	699.06		78.54	2.91	43.11		
_	1726.19	2			38.90	226.89	_	78.54	2,56	38.17		
_	1785.71	2	SLE B	-28685.60	-21.38	-124.70	-	78.54	2,40	35.87		
75	1845.24	2	SLE R	-27388.40	-63.44	-370.03	0.00	78.54	2,42	36.04		
76	1904.76	2	SLE R		-89.73	-523.41	0.00	78.54	2.39	35.55		
77	1964.29	2	-		-102.68	-598.96	0.00	-	2,33	34.51		
_	2023,81	2	_		-104.68	~610.62	_	78.54	2,23	33.02		
79	2083,33	2	SLE R	-22213.60 -20923.00	-98.07 -85.16	-572.06 -496.72	0.00	78.54	2,10	31.17 29.06		
81		2	SLE R		-68.20	-397.81	0.00	_	1.96	26.78		
82	2261.90	_	SLE B	-18345.20	-49.43	-288.33	0.00	_	1.64	24.43		
_	2321.43	_	SLE R		-31.05	-181.12	-	78.54	1,48	22.09		
84		2	SLE B		-15.24	-88.90	0.00	-	1.33	19.86		
85	2440.48	2	SLE R	-14485.70	-4.17	-24.32	0.00	78.54	1.19	17.84		
86	2500.00	2	SLE R	-13200.80	0.00	0.00	0.00	78,54	1.07	16.09		
87	0.00	_	SLE Q		7652.20		47,12	_	42.87	915.33		
88	59,52	4			8101.31	47256.00	47.12	31.42	45,57	1001.60		
89	119.05	_	SLE O		8377.05	48864.50	47.12	31.42	47.27 48.06	1061.89		
91	238.09	4	-		8507.10	49623.00	47.12	31.42	48.08	1092.23		
92	297.62	4	-		8405.83	49032.30	47.12	31.42	47.47	1071.60		
93	357.14	4	SLE Q	-60441.60	8212.09	47902.20	47.12	31.42	46,29	1031.14		
94	416,67	4	SLE Q	-59088.00	7913.24	46159.00	47.12	31.42	44.54	983.44		
95	476.19	_	SLE Q		7525.62	43897.90	47.12	31,42	42.26	916.82		
96	535.71	4			7072.41	41254.30	47,12	31.42	39.57	836.46		
97	595.24	-	SLE Q			38345.80			36.59	746.97		
98		_		-53704.70 -52366.20					33.44			
100	-	_		-51030.60								
101				-49697.70					23.76			
102		_		-48367.40					20.69			
1.03	952,38			-47039.80					17.81	244.79		
104	1011,90			-45714.70					15,17	209,91		
	1071.43			-44392.00					12,82	178.72		
$\overline{}$	1130.95			-43071.70					10.81	151.78		
	1190.48			-41753.80					9,15	129.32		
_	1250.00			-40438.00 -39124.50					7,81 6,74	111.04 96.29		
	1369.05			-37813.00		-	-	-	-	84.11		
_	1428.57			-36503.60								
	1488.10			-35196.10				78.54	4.41	64.07		
	1547.62	4	SLE Q	-33890.50	353.48		_	-	3,83	55.96		
$\overline{}$	1607.14			-32586,70		1306.08	_		3,33	49.01		
	1666.67			-31284.70				78.54	2.91	43.11		
	1726.19	_	-	-29984.30		226.89	The second second second second	78.54	2.56	38.17		
	1785.71 1845.24			-28685.60					-			
	1904.76			-27388.40 -26092.60				78.54	2.42	36.04 35.55		
-	1964.29	_	_	-24798.30				78.54	2,33	34.51		
	2023.81			-23505.30				78.54	2.23	33.02		
- Acres	2083.33			-22213.60		The second linear second linear second	-	78.54		-		
123	2142.86	4	SLE Q	-20923.00	-85.16			78.54	1.96	29.06		
_	2202.38			-19633.60				78.54				
_	2261.90			-18345.20				78.54	1,64	24.43		
	2321.43			-17057.80				78.54	1,48			
_	2380.95			-15771.30 -14485.70				78.54 78.54		19.86 17.84		
	2500.00		SLE Q					78.54	1.19	16.09		
463	E100.00	-	oratio hi	40500.00	0.00	0.00	0.00	10.04	4.97	10:03		

Stato	limite	d'e	eserci	zio - Ver	ifiche a	fessuraz	ione									
Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c damp	s <nm></nm>	K 2	$\Phi_{\theta q}$	Δ _{SIB}	A _S <cmq></cmq>	Ac eff <mq></mq>	σ _a <dan cmq=""></dan>	€ _{SIR}	Wk <mm></mm>

							R	elazio	ne o	di ca	Icolo					
87	0.00	4	SLE C	-60136.70	44636.30	7652.20	46,00	136.36	0.50	20.00	202.09	21.99	1210.52	915,33	0.27	0.09
88	59.52	4	SLE Q	-60926.80	47256.00	8101.31	46.00	136.36	0.50	20.00	203.00	21.99	1220.54	1001.60	0.29	0.10
89	119.05	4	SLE Ç	-60826.00	48864.50	8377.05	46.00	136.36	0.50	20.00	203.69	21.99	1228.04	1061.89	0.31	0.11
90	178.57	4	SIE C	-60727.00	49608.30	8504.58	46.00	136.36	0.50	20.00	204.00	21.99	1231.46	1090.50	0.32	0.11
91	238.09	4	SLE C	-60630.00	49623.00	8507.10	46.00	136.36	0.50	20.00	204.03	21.99	1231.84	1092.23	0.32	0.11
92	297.62	4	SLE Ç	-60534.80	49032.30	8405.83	46.00	136.36	0.50	20.00	203.84	21.99	1229.73	1071.60	0.31	0.13
93	357.14	4	SLE C	-60441.60	47902.20	8212.09	46.00	136.36	0.50	20.00	203,43	21.99	1225.20	1031.14	0.30	0.10
94	416.67	4	SLE C	-59088.00	46159.00	7913.24	46.00	136.36	0.50	20.00	203,15	21.99	1222.11	983.44	0.29	0.10
9.5	476.19	4	SLE Ç	-57737.60	43897.90	7525.62	46.00	136.36	0.50	20.00	202.60	21.99	1216.09	916.82	0.27	0.09
96	535.71	4	SLE C	-56390.30	41254.30	7072.41	46.00	136.36	0.50	20.00	201.78	21.99	1207.06	836.46	0.24	0.08
97	595.24	4	SLE Q	-55046.00	38345.80	6573.80	46.00	136,36	0.50	20.00	200.65	21,99	1194.69	746.97	0.22	0.03
. 98	654.76	4	SLE C	-53704.70	35273.80	6047.14	46.00	136.36	0.50	20.00	199,17	21.99	1178.37	652.38	0.19	0.0
. 99	714.29	4	SLE C	-52366.20	32124.10	5507.18	46,00	136.36	0.50	20.00	197.24	21.99	1157.20	556.27	0.16	0.0
100	773.81	4	SLE C	-51030.60	28968.90	4966.27	46.00	136.36	0.50	20,00	194,75	21.99	1129,81	461,75	0.13	0.04
101	833.33	4	SLE Q	-49697.70	25867.30	4434.55	46.00	136.36	0.50	20.00	191.52	21.99	1094.23	371.61	0.11	0.04
102	892.86	4	SLE Ç	-48367.40	22867,00	3920.19	46.00	136.36	0.50	20.00	203.16	18.85	1047.69	288.31	0.08	0.03
103	952,38	4	SLE C	-47039.80	20005+30	3429.60	46.00	136.36	0.50	20,00	217.59	15.71	986,38	214,09	0.06	0.02
104	1011.90	4	SLE C	-45714.70	17310.40	2967.61	46.00	136.36	0.50	20.00	206.76	15.71	901.30	150.84	0.04	0.02
105	1071.43	4	SLE Q	-44392.00	14802.70	2537.70	46.00	136.36	0.50	20.00	191.28	15.71	779.77	99.79	0.03	0.03
106	1130.95	4	SLE C	-43071.70	12495.60	2142.17	46.00	136.36	0.50	20.00	186.98	12.57	596.76	60.98	0.02	0.03
107	1190.48	4	SLE Ç	-41753.80	10396.40	1782.31	46.00	136.36	0.50	20.00	176.11	9.42	396.38	33.18	0.01	0.00
108	1250.00	4	SLE C	-40438.00	8507.86	1458.54	46.00	136.36	0.50	20.00	221.17	3.14	202.90	14.10	0.00	0.00
130	0.00	.3	SLE F	-60136.70	44636.30	7652.20	46.00	136.36	0.50	20.00	202.09	21.99	1210.52	915.33	0.27	0.09
131	59.52	3	SLE F	-60926.80	47256.00	8101.31	46.00	136.36	0.50	20.00	203.00	21.99	1220.54	1001,60	0.29	0.10
132	119.05	3	SLE F	-60826.00	48864.50	8377.05	46.00	136.36	0.50	20.00	203.69	21.99	1228.04	1061.89	0.31	0.1
133	178.57	3	SLE F	-60727.00	49608.30	8504.58	46,00	136.36	0.50	20,00	204.00	21.99	1231.46	1090.50	0.32	0.13
134	238.09	3	SLE F	-60630.00	49623.00	8507.10	46.00	136.36	0.50	20.00	204.03	21.99	1231.84	1092.23	0.32	0.1
135	297.62	3	SLE F	-60534.80	49032.30	8405.83	46.00	136.36	0.50	20.00	203.84	21.99	1229.73	1071.60	0.31	0.13
136	357.14	3	SLE F	-60441.60	47902,20	8212.09	46.00	136.36	0.50	20.00	203.43	21.99	1225.20	1031.14	0.30	0.10
137	416.67	3	SLE F	-59088.00	46159,00	7913.24	46.00	136.36	0.50	20.00	203.15	21.99	1222.11	983.44	0.29	0.10
138	476.19	3	SLE F	-57737.60	43897.90	7525.62	46.00	136.36	0.50	20.00	202,60	21.99	1216.09	916.82	0.27	0.09
139	535.71	3	SLE F	-56390.30	41254.30	7072.41	46.00	136.36	0.50	20.00	201.78	21.99	1207.06	836,46	0.24	0.08
140	595.24	3	SLE F	-55046.00	38345.80	6573.80	46,00	136.36	0.50	20.00	200.65	21.99	1194.69	746.97	0.22	0.0
141	654.76	3	SLE F	-53704.70	35273.80	6047.14	46.00	136.36	0.50	20.00	199,17	21.99	1178.37	652.38	0.19	0.00
142	714.29	3	SIE E	-52366.20	32124.10	5507.18	45.00	136.36	0.50	20,00	197.24	21.99	1157.20	556.27	0.16	0.0
143	773,81	-3	SLE F	-51030.60	28968,90	4966.27	46.00	136.36	0.50	20.00	194,75	21.99	1129,81	461,75	0.13	0.0
144	833.33	3	SLE F	-49697.70	25867.30	4434.55	46.00	136.36	0.50	20.00	191.52	21.99	1094.23	371.61	0.11	0.04
145	892.86	3	SLE F	-48367.40	22867.00	3920.19	46.00	136.36	0.50	20.00	203.16	18.85	1047.69	288.31	0.08	0.0
146	952.38	3	SLE F	-47039.80	20005.30	3429.60	46.00	136.36	0.50	20,00	217.59	15.71	986.38	214.09	0.06	0.0
147	1011.90	3	SLE F	-45714.70	17310.40	2967.61	46.00	136.36	0.50	20.00	206.76	15.71	901.30	150.84	0.04	0.03
148	1071.43	3	SLE F	-44392.00	14802.70	2537.70	46.00	136.36	0.50	20.00	191.28	15.71	779.77	99.79	0.03	0.03
149	1130.95	3	SLE F	-43071.70	12495.60	2142.17	46.00	136.36	0.50	20.00	186.98	12.57	596.76	60.98	0.02	0.03
150	1190.48	3	SLE F	-41753.80	10396.40	1782.31	46.00	136.36	0.50	20.00	176,11	9.42	396.38	33.18	0.01	0.00

terrecase bermebers	Verifiche	princi	pali
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Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
67	C.Rare - Sc max (min. compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
110	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 17

Caratteristiche del palo e dei materiali utilizzati

aract	errs.	creue o	er baro e	der macer	rarr nerrr	ZZALL			
R <cm>></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20,59	174.02	13.73	B450C	4300.00	3913.04

151 1250.00 3 SLE F -40438.00 8507.86 1458.54 46.00 136.36 0.50 20.00 221.17 3.14 202.90

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVB	0.00			

Azioni ed effetti - Plinto/Palo n. 17 (-44)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	122467.00	7018.75	-918.56	59119.70	-17875.50
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC	1	3		0.00	0.00
	1	SLU	TOT	122467.00	7018.75	-918.56	59119.70	-17875.50

2	2	SLE F	RVN	90716.20	5199.08	-680,41	43792.40	-13241.10
	2	SLE F	TAG				0.00	0.00
	2	SLE F	ECC				0.00	0.00
	2	SIE I	TOT	90716.20	5199.08	-680.41	43792.40	-13241.10
3	3	SLE I	RVN	90716.20	5199.08	-680.41	43792.40	-13241.10
	3	SLE I	TAG				0.00	0.00
	. 3	SLE I	ECC		7 7		0.00	0.00
	3	SLE I	TOT	90716.20	5199.08	-680.41	43792.40	-13241.10
- 4	4	SLE (RVN	90716.20	5199.08	-680.41	43792.40	-13241.10
	4	SLE (TAG				0.00	0.00
	4	SIE (ECC				0.00	0.00
	4	SLE (TOT	90716.20	5199.08	-680.41	43792.40	-13241.10

Sollecitazioni nei pali

Caso	8	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	. 1	-122467,00	-7018.75	918.56	-59119.70	17875.50
2	2	SLE R	1	-90716.20	-5199.08	680.41	-43792.40	13241.10
.3	3	SLE F	1	-90716.20	-5199.08	680.41	-43792.40	13241.10
4	4	SLE Q	. 1	-90716.20	-5199.08	580.41	-43792.40	13241.10

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm></cm>	oc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
-1	0.00	1	SLU	-122467.00	58878.80	17802.70	-122467.00	187601.00	57009,40	2-3	163.12	3.188
- 2	59.52	1	SLU	-122824.00	62188.80	18803.50	-122824.00	187729.00	57051.80	2-3	163.12	3,020
- 3	119.05	1	SLU	-121858.00	64187,50	19407.80	-121858,00	187382,00	56936,60	2-3	163.12	2,920
4	178.57	1	SLU	-120897.00	65066.20	19673.50	-120897.00	187034.00	56821.10	2-3	163.12	2.876
- 5	238.09	1	SILI	-119939.00	65001.00	19653.80	-119939.00	186688.00	56706.10	2+3	163.12	2.873
- 6	297.62	1	SIJ	-118985.00	64153.10	19397.40	-118985.00	186344.00	56591.50	2-3	163.12	2.906
7	357.14	1	SLU	-118035.00	62609.10	18930.60	-118035.00	186000.00	56477.50	2-3	163.12	2.972
8	416.67	1	SEU	-115217.00	60275.00	18224.80	-115217.00	184981.00	56139.30	2-3	163.12	3.070
9	476.19	1	SLU	-112406.00	57275.30	17317.80	-112406.00	183964.00	55801.60	2-3	163.12	3,213
10	535.71	1	SIJ	-109601.00	53785.40	16262.60	-109601.00	182943.00	55461.40	2-3	163.12	3.402
11	595.24	1	SIJJ	-106802.00	49958.10	15105.40	-106802.00	181914.00	55134.40	2-3	163.12	3,642
12	654.76	1	SLU	-104009.00	45924.50	13885.80	-104009,00	180886.00	54810.00	2-3	163.12	3.939
13	714.29	1	SLU	-101221.00	41796.20	12637.50	-101221.00	179855.00	54484.30	2-3	163.12	4.304
14	773.81	1	SIM	-98438.30	37666.10	11388.80	-9843B.30	178824.00	54158.40	2-3	163.12	4.748
15	833.33	1	SIAJ	-95661.10	33610.80	10162.60	-95661.10	177794.00	53833.00	2-3	163.12	5,290
16	892,86	1	SLU	-92889,10	29691.70	8977.63	-92889,10	176765.00	53507,70	2-3	163.12	5,954
17	952.38	1	SIA	-90122.10	25956.90	7848.37	-90122.10	175733.00	53180.50	2-3	163.12	6.771
18	1011.90	1	SILI	-87359.90	22442.60	6785.79	-87359,90	174703.00	52854.10	2-3	163.12	7.785
19	1071,43	1	SIJ	-84602.40	19174.80	5797.73	-84602.40	173673.00	52527.80	2-3	163.12	9.058
20	1130.95	1	SIU	-81849.40	16170.50	4889.33	-81849.40	172641.00	52200.40	2-3	163.12	10.676
21	1190.48	1	SLU	-79100.80	13438.90	4063.41	-79100.80	171609.00	51872.40	2-3	163.12	12.769
22	1250.00	1	SLU	-76356,40	10983.10	3320.86	-76356,40	170578.00	51544.90	2-3	163.12	15.530
23	1309.52	1	SLU	-73616,20	8800.52	2660.94	-73616.20	169548.00	51217.80	2-3	163.12	19.264
24	1369.05	1	SLU	-70879.90	6884.44	2081.59	-70879.90	168515.00	50888.50	2-3	163.12	24.475
25	1428.57	1	SIJJ	-68147.40	5224.54	1579.70	-68147.40	167483.00	50559.60	2-3	163.12	32.053
26	1488.10	1	SLU	-65418.50	3807.77	1151.32	-2571250.00	166451.00	50231.00	2-3	163.12	39.305
27	1547.62	1	SLU	-62693.20	2619.02	791.89	-2571250.00	165418.00	49901.80	2-3	163.12	41.013
28	1607.14	1	SIAJ	-59971.20	1641.67	496.38	-2571250.00	164384.00	49571.50	2-3	163.12	42.875
29	1666.67	1	SLU	-57252.50	858.04	259.44	-2571250.00	163351.00	49241.40	2-3	163.12	44.911
30	1726.19	1	SLU	-54536.80	249.81	75.53	-2571250.00	162318.00	48911.80	2-3	163.12	47.147
31	1785.71	1	SIU	-51824.00	-201.66	-60.97	-2571250,00	-161603.00	-47507.70	2-3	343.75	49.615
32	1845.24	1	SIJ	-49114.10	-515,12	-155.75	-2571250.00	-160539.00	-47177.20	2-3	343.75	52.353
33	1904.76	1	SLU	-46406.70	-709.25	-214.45	-2571250.00	-159476.00	-46847.20	2-3	343.75	55,407
34	1964.29	1	SLU	-43701.90	-802.49	-242.64	-2571250.00	-158409.00	-46514.80	2-3	343.75	58.836
35	2023.81	1	SIJ	-40999,30	-813.01	-245.82	-2571250.00	-157342.00	-46181.80	2-3	343.75	62.714
36	2083.33	1	SLU	-38299.00	-758.65	-229.39	-2571250.00	-156274.00	-45843.90	2-3	343.75	67,136
37	2142.86	1	SLU	-35600.80	-656.93	-198.63	-2571250.00	-155203.00	~45493.10	2-3	343.75	72.225
38	2202.38	1	SIJJ	-32904.40	-525.05	-158.75	-2571250.00	-154129.00	~45139.80	2-3	343.75	78.143
39	2261.90	1	SLU	-30209.80	-379.96	-114.89	-2571250.00	-152571.00	-46429.60	2-3	343.12	85,113
40	2321.43	1	SLU	-27516.90	-238,38	-72.08	-2571250.00	-151498.00	-46073.00	2-3	343.12	93,443
41	2380.95	1	SIAJ	-24825.40	-116,89	-35.34	-2571250.00	-150422.00	-45713.20	2-3	343.12	>100
42	2440.48	1	SLU	-22135.20	-31.96	-9.66	-2571250.00	-149346.00	-45353.70	2-3	343.12	>100
43	2500.00	1	SEU	-19446.20	0.00	0.00	-2571250.00					>100

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <mq></mq>	Vsdu <dan></dan>	atg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7018.75	-918.56	0.85	11.31	7078.60	1.00	32294.70	349210.00	32294.70	4,562
2	59.52	1	SLU	4561.75	-597.01	0.85	11.31	4600.65	1.00	32294.70	349261.00	32294.70	7.020
- 3	119.05	1	SLU	2450.34	-320.68	0.85	11.31	2471.23	1.00	32294.70	349123.00	32294.70	13.068

	 Company of the company 	12.10	Park Property
RA	lazione	di co	COLO
176	ICIZIONE	UI GO	COIO

								T.E	Hazi	one ai	Calcolo		
4	178.57	1	SLU	658.83	-86.22	0.85	11.31	664.45	1.00	32294.70	348985.00	32294.70	48.604
.5	238.09	1	SIA	-838.99	109.80	0.85	11.31	846.14	1.00	32294.70	348848.00	32294.70	38.167
6	297.62	1	SIU	-2069.52	270.84	0.85	11.31	2087.17	1.00	32294.70	348711.00	32294.70	15.473
7	357.14	1	SIJ	-3370.48	441.10	0.85	11.31	3399.22	1.00	32294.70	348575.00	32294.70	9.501
8	416.67	1	SLU	-4695.44	614.50	0.85	11.31	4735.48	1.00	32294.70	348172.00	32294.70	6.820
9	476.19	1	SLU	~5694.39	745.24	0.85	11.31	5742.94	1.00	32294.70	347769.00	32294.70	5.623
10	535.71	1	SLU	-6408.13	838.64	0.85	11.31	6462.77	1.00	32294.70	347367.00	32294.70	4.997
11	595.24	ĭ	SIU	-6875,19	899.77	0.85	11.31	6933.82	1.00	32294.70	346966.00	32294.70	4.658
12	654.76	1	SLU	-7131.56	933.32	0.85	11.31	7192.37	1.00	32294.70	346566.00	32294.70	4.490
13	714.29	1	SIJ	-7210.47	943.65	0.85	11.31	7271.95	1.00	32294.70	346167.00	32294.70	4.441
14	773.81	1	SLU	+7142.32	934.73	0.85	11.31	7203.22	1.00	32294.70	345768.00	32294.70	4.483
15	833.33	1	SLU	-6954.63	910.17	0.85	11.31	7013.94	1.00	32294.70	345371.00	32294.70	4.604
1.6	892.86	1	SIAJ	-6672.10	873.19	0.85	11.31	6729.00	1.00	32294.70	344973.00	32294,70	4,799
17	952.38	1	SLU	-6316.64	826.67	0.85	11.31	6370.50	1.00	32294.70	344577.00	32294.70	5.069
18	1011.90	1	SIU	-5907.49	773.13	0.85	11.31	5957.87	1.00	32294.70	344181.00	32294.70	5.421
19	1071.43	1	SILI	-5461.40	714.75	0.85	11,31	5507.97	1.00	32294.70	343786.00	32294.70	5,863
-20	1130,95	1	SIU	-4992.76	653.41	0.85	11.31	5035.34	1.00	32294.70	343392.00	32294.70	6.414
21	1190.48	1	SLU	-4513.77	590.73	0.85	11.31	4552.27	1.00	32294.70	342998.00	32294.70	7.094
22	1250.00	1	SLU	-4034.67	528.02	0.85	11,31	4069.07	1.00	32294.70	342605,00	32294.70	7.937
23	1309.52	1	SIJ	-3563.86	466.41	0.85	11.31	3594,25	1.00	32294.70	342213.00	32294.70	8.985
24	1369.05	1	SLU	-3108.18	406.77	0.85	11.31	3134.68	1.00	32294.70	341821.00	32294.70	10.302
25	1428.57	1	SLU	-2673.01	349.82	0.85	11.31	2695.81	1.00	32294.70	341429.00	32294.70	11.980
26	1488,10	.1	SIU	-2262.53	296.10	0.85	11.31	2281.82	1.00	32294.70	341039.00	32294.70	14.153
27	1547.62	1	SLU	-1879.81	246.01	0.85	11.31	1895.84	1.00	32294.70	340648.00	32294.70	17.035
28	1607.14	1	SIA	+1527.07	199.85	0.85	11,31	1540.09	1.00	32294.70	34025B.00	32294.70	20.969
29	1666.67	1	SLU	-1205.73	157.80	0.85	11.31	1216.01	1.00	32294.70	339869.00	32294.70	26.558
30	1726.19	1	SLU	-916.65	119.96	0.85	11.31	924.46	1.00	32294.70	339480.00	32294.70	34.934
31	1785.71	1	SLU	-660.17		_	11.31	665.80	1.00	32294.70	339091.00	32294.70	48,505
32	1845.24	1	SIU	-436.29	57.10	0.85	11.31	440.01	1.00	32294.70	338703.00	32294.70	73.396
33		1	SIJ	-244.73	32,03	_		246,82	_	32294.70	338315,00	32294.70	_
34	1964.29	1	SLU	-85,06	11.13	0.85	11.31	85.79	1.00	32294.70	337928.00	32294.70	>100
35	2023,81	1	SIU	43.27	~5.66	0.85	11.31	43.64	_	32294.70	337541,00	32294.70	>100
36		1	SIJ	140.84	-18.43	_		142.04	_	32294.70	337154.00	32294.70	>100
37	2142.86	1	SLU	208,21	-27.25	0.85	_	209.99	1.00	32294.70	336768.00	32294.70	>100
38	2202.38	1	SLU	245.88	-32.18	0.85	11.31	247.98	1.00	32294.70	336381.00	32294.70	>100
39	2261,90	1	SLU	254.27	-33.28	0.85	11.31	256.43	1.00	32294.70	335995,00	32294.70	>100
40	2321.43	1	SLU	233.69	-30.58	0.85	11.31	235.69	1.00	32294.70	335610.00	32294,70	>100
41	2380.95	1	SILI	184.39	-24.13	0.85	11.31	185.96	1.00	32294.70	335224.00	32294.70	>100
42	2440.48	1	SIJ	106.47	-13.93	0.85	11.31	107.38	1.00	32294.70	334839.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <cmq></cmq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-90716.20	13187,20	43613.90	37.70	40.84	41.37	600.82
45	59.52	2	SLE R	-91293.80	13928.50	46065.80	40.84	37.70	44.04	676.44
46	119.05	2	SLE R	-90768.80	14376.20	47546.30	43.98	34.56	45.72	731,47
47	178.57	2	SLE R	-90246.60	14573.00	48197.10	43.98	34.56	46.48	758.88
48	238.09	2	SLE R	-89727.20	14558.40	48148.90	43.98	34.56	46.47	762.39
49	297.62	2	SLE R	-89210.70	14368.50	47520.80	43.98	34,56	45.81	745.95
50	357.14	2	SLE R	-88697.00	14022.60	46377.10	43.98	34.56	44.58	711.92
51	416.67	2	SLE R	-86625.30	13499.90	44648.20	40.84	37.70	42.82	673.39
52	476.19	2	SLE R	-84558.30	12828.00	42426.20	40.84	37.70	40.52	618.48
53	535.71	2	SLE R	-82495.80	12046.40	39841.10	37.70	40.84	37.82	552.22
54	595.24	2	SLE R	-80437.80	11189,20	37006.00	37.70	40.84	34.85	479.20
55	654.76	2	SLE R	-78384.00	10285.80	34018.20	37.70	40.84	31.74	432.88
56	714.29	2	SLE R	-76334.50	9361.15	30960.10	37.70	40.84	28.58	391.44
57	773.81	2	SLE R	-74289.00	8436.13	27900.80	37.70	40.84	25.47	350.54
58	833.33	2	SLE R	-72247.60	7527.86	24896.90	31.42	47.12	22.50	311.28
59	892.86	2	SLE R	-70210.00	6650.10	21993.90	31.42	47.12	19.74	274.64
60	952.38	2	SLE R	-68176.20	5813.61	19227.30	28.27	50.27	17.25	241.40
61	1011.90	2	SLE R	-66146.00	5026.51	16624.20	25.13	53.41	15.07	212.03
62	1071.43	2	SLE B	-64119,40	4294.62	14203.60	18.85	59.69	13.20	186.62
63	1130.95	2	SLE R	-62096.20	3621.73	11978.10	12.57	65.97	11.61	164.94
64	1190.48	2	SLE R	-60076.40	3009,94	9954.76	0.00	78.54	10.27	146.53
65	1250.00	2	SLE R	-58059.80	2459.90	8135.62	0.00	78.54	9.12	130.61
66	1309.52	2	SLE R	-56046.30	1971.07	6518.90	0.00	78.54	8.08	116.26
.67	1369.05	2	SLE R	-54035.80	1541.92	5099.58	0.00	78.54	7,15	103.38
68	1428.57	2	SLE R	-52028.20	1170.15	3870.03	0.00	78.54	6,32	91.89
69	1488.10	2	SLE R	-50023.40	852.83	2820.57	0.00	78.54	5.59	81.73
70	1547.62	2	SLE R	-48021.20	586.59	1940.02	0.00	78.54	4.95	72.81
71	1607.14	2	SLE R	-46021.70	367.69	1216.05	0.00	78.54	4.40	65.05
72	1666.67	2	SLE R	-44024.60	192.18	635,58	0.00	78.54	3.92	58.35
73	1726,19	2	SLE R	-42029.90	55.95	185.05	0.00	78.54	3.52	52.61
74	1785.71	2	SLE R	-40037.40	-45.17	-149.38	0.00	78,54	3.34	49.91
75	1845.24	2	SLE R	-38047.10	-115.37	-381.57	0.00	78.54	3,30	49.18
76	1904.76	2	SLE R	-36058.80	-158.85	-525.37	0.00	78.54	3.21	47.81
77	1964.29	2	SLE R	-34072.50	-179.73	-594.43	0.00	78.54	3.09	45.89

Re	lazione	di	ca	Icolo
176	10210116	· ui	ua	ICCIO

							Re	lazio	ne di ca	ICOIO
78	2023.81	2	SLE R	-32088.00	-182.09	-602.23	 	E. 1903 C. 1915 C. 1915		43.53
79	2083.33	2	SLE R	-30105.20	-169.91	-561.96	0.00	78.54	2.75	40.82
80	2142.86	2	SLE R	-28124.00	-147.13	-486.61	0.00	78.54	2.55	37.85
81	2202.38	2	SLE R	-26144.30	-117.60	-388.93	0.00	78.54	2,34	34.72
82	2261.90	2	SLE B	-24166.00	-85.10	-281.45	0.00	78.54	2,12	31.52
83	2321.43	2	SLE R	-22189.10	~53.39	-176.58	0.00	78.54	1.90	28.35
84	2380.95	2	SLE R	-20213.30	-26.1B	-86.59	0.00	78.54	1.69	25.28
85	2440.48	2	SLE R	-18238.60	-7.16	-23.67	0.00	78.54	1.50	22,41
86	2500.00	2	SLE R	-16264.90	0.00	0.00	0.00	78.54	1.32	19.83
87	0.00	4	SLE Q	-90716.20	13187.20	43613.90	37.70	40.84	41.37	600.82
88	59.52	4	_		13928.50	46065.80	40.84	37.70	44.04	676.44
89	119.05	4	SLE Q	-90768.80	14376.20	47546.30	43.98	34.56	45.72	731.47
90	178,57	-	SLE Q		14573.00	48197.10	43.98	34.56	46.48	758.88
91	238.09	_	SLE Q				_	-	46.47	762.39
92	297.62	-	SLE Q				43.98		45.81	745.95
93	357.14	_	SLE Q					_	44.58	711.92
94	416.67	_	SLE Q				40.84		42,82	673.39
95	476.19	_	SLE Q				-	-	40.52	618.48
96	535.71	_	SLE Q	-			-	_	37,82	552.22
97	595,24	_	SLE Q				37.70		34.85	479.20
98	654.76	-	SLE Q				37.70	_	31.74	432.86
99	714.29	-	SLE Q			30960.10		-	28.58	391.44
100	773.81	-	SLE Q		_	27900.80	-	-	25.47	350.54
101	833.33	_	SLE Q			24896.90	_		22.50	311.28
102	892.86	_	SLE Q			21993.90		-	19.74	274.64
103	952.38	_	SLE Q		5813.61		28.27	-	17.25	241.40
	1011.90	_	SLE Q				25.13		15.07	212.03
105	1071.43	_	SLE Q		4294.62		18.85		13.20	186.62
106	1130.95	_	SLE Q				12,57		11.61	164.94
_	1190.48	-	SLE Q		3009.94	9954,76	0.00	-	10,27	146.53
_	1250.00	-	SLE Q		2459.90			78.54	9.12	130.61
	1309.52	_	SLE Q		1971.07	6518.90	-	78.54	8.08	116.26
$\overline{}$	1369.05	_	SLE Q		1541.92	5099.58		78.54	7,15	103.38
111	1428.57	_	SLE O		1170.15	3870.03	0.00		6.32	91.89
112	1488.10	-	SIE Q		852.83	2820.57	0.00	_	5.59	81.73
_	1547.62	-	SLE Q	-	586.59	1940.02	0.00	-	4.95	72.B1
$\overline{}$	1607.14	_	SLE Q		367.69	1216.05	-	78.54	4.40	65.05
-	1666.67	-	SIE Q		192.18	635.58	0.00		3.92	58.35
_	1726.19	_	SLE Q		55.95	185.05		78.54	3,52	52.61
	1785.71	_	SLE Q		-45.17	-149.38		78.54	3.34	49.91
_	1845.24	_	SLE Q		-115.37	-381.57	0.00	_	3.30	49.18
	1904.76	-	SLE Q		-158.85	-525.37		78.54	3.21	47.81
_	1964.29	_	SLE Q				-	78.54		45.89
-	2023.81	_		-32088.00		-602.23		-		43.53
$\overline{}$	2083,33			-30105.20				78.54		40.82
	2142.86	_		-28124.00				78.54		37.85
_	2202.38			-26144.30				78.54		34.72
	2261.90			-24166.00				78.54		31.52
	2321.43			-22189.10		THE RESERVE AND ADDRESS OF THE PARTY.		78.54		28.35
	2380.95	_	SLE Q					78.54		25.28
$\overline{}$	2440.48	_	_	-18238.60			_	78.54		22.41
	2500.00	_	SLE Q	-			_	78.54		19.83

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm></cm>	oc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	•eq	Δ _{EM}	A _S	Ac eff <mq></mq>	σ _S <dan cmq=""></dan>	esm	Wk <mm></mm>
87	0.00	4	SLE Q	-90716.20	43613.90	13187.20	46.00	136.36	0.50	20.00	203.64	18.85	1052.17	600.82	0.17	0.06
88	59.52	4	SLE Q	-91293.80	46065,80	13928.50	46.00	136.36	0.50	20,00	206.05	18.85	1074.92	676.44	0.20	0.07
89	119.05	4	SLE Q	-90768.80	47546.30	14376.20	46.00	136.36	0.50	20.00	207.77	18.85	1091.09	731.47	0.21	0.08
90	178.57	4	SLE Q	-90246.60	48197.10	14573.00	46.00	136.36	0.50	20.00	208.61	18.85	1099.00	758.88	0.22	0.08
91	238,09	4	SLE Q	-89727.20	48148.90	14558.40	46.00	136.36	0.50	20.00	208.81	18.85	1100.91	762.39	0.22	0.08
92	297.62	4	SLE Q	-89210.70	47520.80	14368.50	46.00	136.36	0.50	20,00	208.50	18.85	1097.97	745.95	0.22	0.08
93	357.14	4	SLE Q	-88697.00	46377.10	14022.60	46,00	136,36	0.50	20,00	207.69	18.85	1090.33	711.92	0.21	0.07
94	416.67	4	SLE Q	-86625.30	44648,20	13499.90	46.00	136.36	0.50	20.00	207.04	18,85	1084.25	673.39	0.20	0.07
95	476.19	4	SLE Q	-84558.30	42426.20	12828.00	46.00	136.36	0.50	20.00	205.78	18.85	1072.37	618.48	0.18	0.06
96	535,71	4	SLE Q	-82495.80	39841.10	12046.40	46.00	136.36	0.50	20.00	203.87	18,85	1054.39	552,22	0.16	0.06
. 97	595,24	4	SLE Q	-80437.80	37006.00	11189.20	46.00	136,36	0.50	20,00	201.23	18.85	1029.49	479,20	0.14	0.05
98	654.76	4	SLE Q	-78384.00	34018.20	10285.80	46.00	136,36	0.50	20.00	197.71	18.85	996.33	403.57	0.12	0.04
99	714.29	4	SLE Q	-76334.50	30960.10	9361.15	46.00	136,36	0.50	20.00	193.11	18.85	952.97	329.03	0.10	0.03
100	773.81	4	SLE Q	-74289.00	27900.80	B436.13	46.00	136.36	0.50	20.00	187.16	18.85	896.86	258.77	0.08	0.02
101	833.33	4	SLE Q	-72247.60	24896.90	7527.86	46.00	136.36	0.50	20.00	196.93	15.71	824.15	195.41	0.06	0.02
102	892,86	4	SLE Q	-70210.00	21993.90	6650.10	46.00	136,36	0.50	20.00	205.94	12,57	715.92	140.82	0.04	0.01
103	952,38	4	SLE Q	-68176.20	19227.30	5813.61	46.00	136.36	0.50	20,00	182,74	12.57	570.11	95,96	0.03	0.01
104	1011.90	4	SLE Q	-66146.00	16624.20	5026.51	46.00	136.36	0.50	20.00	158.17	12.57	415.76	60.66	0.02	0.00
105	1071.43	4	SLE Q	-64119.40	14203.60	4294.62	46.00	136.36	0.50	20,00	176.82	6.28	266.48	33,90	0.01	0.00
130	0.00	3	SLE F	-90716.20	43613.90	13187.20	46.00	136,36	0.50	20.00	203.64	18.85	1052.17	600.82	0.17	0.06
131	59.52	3	SLE F	-91293.80	46065.80	13928.50	46.00	136.36	0.50	20,00	206.05	18.85	1074.92	676.44	0.20	0.07

132	119.05	3	SLE F	-90768.80	47546.30	14376.20	46.00	136.36	0.50	20.00	207,77	18.85	1091.09	731.47	0.21	0.08
133	178.57	3	SLE F	-90246.60	48197.10	14573.00	46.00	136.36	0.50	20.00	208.61	18.85	1099.00	758.88	0.22	0.08
134	238.09	3	SLE F	-89727.20	48148.90	14558.40	46.00	136.36	0.50	20.00	208.81	18.85	1100.91	762.39	0.22	0.08
135	297.62	3	SLE F	-89210.70	47520.80	14368.50	46.00	136.36	0.50	20.00	208.50	18.85	1097.97	745.95	0.22	0.08
136	357.14	3	SLE F	-88697.00	46377.10	14022.60	46.00	136.36	0.50	20.00	207.69	18.85	1090.33	711.92	0.21	0.07
137	416.67	3	SLE F	-86625.30	44648.20	13499.90	46.00	136.36	0.50	20.00	207.04	18.85	1084.25	673.39	0.20	0.07
138	476.19	3	SLE F	-84558.30	42426.20	12828.00	46.00	136.36	0.50	20.00	205.78	18.85	1072.37	618,48	0.18	0.06
139	535.71	3	SLE F	-82495.80	39841.10	12046.40	46.00	136,36	0.50	20.00	203.87	18.85	1054.39	552.22	0.16	0.06
140	595.24	3	SLE F	-80437.80	37006.00	11189.20	45.00	136.36	0.50	20.00	201.23	18.85	1029.49	479.20	0.14	0.05
141	654.76	3	SLE F	-78384.00	34018.20	10285.80	46.00	136,36	0.50	20.00	197.71	18.85	996.33	403.57	0.12	0.04
142	714.29	3	SLE F	-76334.50	30960.10	9361.15	46.00	136.36	0.50	20.00	193.11	18.85	952.97	329,03	0.10	0.03
143	773,81	3	SLE F	-74289.00	27900.80	8436.13	46.00	136.36	0.50	20.00	187.16	18.85	896.86	258.77	0.08	0.02
144	833,33	3	SLE F	-72247.60	24896.90	7527.86	46.00	136,36	0.50	20.00	196.93	15.71	824.15	195.41	0.06	0.02
145	892,86	3	SLE F	-70210.00	21993.90	6650.10	46.00	136.36	0.50	20.00	205,94	12.57	715.92	140.82	0.04	0.01
146	952.38	3	SLE F	-68176.20	19227.30	5813.61	46.00	136.36	0.50	20.00	182.74	12.57	570.11	95.96	0.03	0.01
147	1011.90	3	SLE F	-66146.00	16624.20	5026.51	46.00	136.36	0.50	20.00	158.17	12,57	415.76	60.66	0.02	0.00
148	1071,43	3	SLE F	-64119.40	14203.60	4294.62	46.00	136.36	0.50	20,00	176.82	6,28	266.48	33,90	0.01	0.00

Verifiche principali

Caso	Tipo
- 5	SLU N cost - min. sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
48	C.Rare - Sf max (max traz.)
65	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
91	C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
108	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 18

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307,10	20.59	174.02	13.73	8450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP.	0.00	0.00	0.00	-
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 18 (-78)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	166477.00	6757.23	-965.38	54140.50	-25200.60
	1	SLU	TAG				0.00	0.00
	. 1	SLU	ECC		4 0		0.00	0.00
	1	SLU	TOT	166477.00	6757.23	-965.38	54140.50	-25200.60
2	. 2	SLE R	RVN	123316.00	5005.36	-715.09	40104.10	-18667.10
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC		0 0		0.00	0.00
	2	SLE R	TOT	123316.00	5005.36	-715.09	40104.10	-18667.10
. 3	3	SLE F	RVN	123316.00	5005.36	-715.09	40104.10	-18667.10
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	123316.00	5005.36	-715.09	40104.10	-18667.10
- 4	-4	SLE Q	RVN	123316.00	5005.36	-715.09	40104.10	-18667.10
	4	SLE Q	TAG		1		0.00	0.00
	4	SLE Q	ECC	2	<u>4</u> 2		0.00	0.00
	4	SLE Q	TOT	123316.00	5005.36	-715.09	40104.10	-18667.10

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	. 1	SLU	- 1	-166477.00	-6757.23	965.38	-54140.50	25200.60
- 2	2	SLE R	1	-123316.00	-5005.36	715.09	-40104.10	18667.10
3	3	SLE F	- 1	-123316.00	-5005.36	715.09	-40104.10	18667.10
- 4	4	SLE Q	- 1	-123316.00	-5005.36	715.09	-40104.10	18667.10

Caso	X <cm>></cm>	œ	1300	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-166477.00	53920.20	25098.00	-166477.00	192226.00	89633.60	2-3	155.00	3.566
2	59.52	1	SLU	-166528.00	56942.30	26504.70	-166528,00	192242.00	89641.30	2-3	155.00	3.377
3	119.05	1	SIU	-164952.00	58764.90	27353.10	-164952.00	191736.00	89403.50	2-3	155.00	3.264
4	178.57	1	SLU	-163382.00	59563.00	27724.60	-163382.00	191232.00	89166.40	2-3	155.00	3.212
5	238.09	1	SIU	-161816.00	59498.00	27694.30	-161816.00	190726.00	88928.70	2-3	155.00	3.207
- 6	297.62	1	SLU	-160255.00	58717.30	27330.90	-160255.00	190222.00	88691.50	2+3	155.00	3.243
7	357,14	1	SLU	-158700.00	57299.90	26671.20	-158700.00	189719.00	88454.90	2-3	155.00	3.312
8	416.67	1	SLU	-154849.00	55160.20	25675.20	-154849.00	188474.00	87869.10	2+3	155.00	3.418
9	476.19	1	SLU	-151007.00	52412.00	24396.00	-151007.00	187227,00	87282,20	2-3	155.00	3.573
10	535.71	1	SLU	-147172.00	49215.90	22908.30	-147172.00	185978.00	86694.50	2-3	155.00	3.780
11	595.24	1	SILI	-143346.00	45711.40	21277.10	-143346,00	184731.00	86107.50	2-3	155.00	4.042
12	654.76	1	SIJ	-139527.00	42018.80	19558.30	-139527.00	183481.00	85518.50	2-3	155.00	4.368
13	714.29	1	SLU	-135716.00	38239.70	17799.30	-135716.00	182231.00	84929,70	2-3	155.00	4.767
14	773.81	1	SIU	-131912.00	34459.50	16039.70	-131912.00	180981.00	84341.00	2-3	155.00	5.253
15	833.33	1	SLU	-128115.00	30748.00	14312.20	-128115.00	179729.00	83750.60	2-3	155.00	5.846
16	892,86	1	SLU	-124325.00	27161.40	12642.70	-124325.00	178477.00	83160.80	2-3	155.00	6.572
17	952.38	1	SIU	-120542.00	23743.70	11051.90	-120542.00	177224.00	82570.10	2-3	155.00	7.465
18	1011.90	1	SLU	-116765.00	20527.90	9555.05	-116765.00	175970.00	81978.80	2-3	155.00	8.574
19	1071.43	1	SLU	-112994.00	17537.80	8163.27	-112994.00	174717.00	81387.90	2-3	155.00	9.964
20	1130.95	1	SIJ	-109230.00	14789.00	6883.76	-109230.00	173462.00	80795+60	2-3	155.00	11.731
21	1190.48	1	SIA	-105471.00	12289.80	5720.49	-105471.00	172177.00	80237.00	2+3	155.00	14.013
- 22	1250.00	1	SLU	-101718.00	10043.00	4674.68	-101718.00	170831.00	79732.20	2-3	155.00	17.018
23	1309.52	1	SLU	-97970.20	8046.34	3745.30	-97970.20	169494.00	79102.90	2-3	155.00	21.075
24	1369.05	1	SIJ	-94227.80	6293,55	2929.43	-94227.80	168156.00	78473.10	2-3	155.00	26.731
-25	1428.57	1	SIJ	-90490.50	4775.19	2222.69	-2571250.00	166814.00	77841,00	2-3	155.00	28.415
26	1488.10	1	SLU	-86758.10	3479.32	1619.51	-2571250.00	165470.00	77208.30	2-3	155.00	29.637
27	1547.62	1	SLU	-83030.30	2392.10	1113.44	-2571250.00	164124.00	76574.60	2-3	155.00	30.968
28	1607.14	1	SIJ	-79307.00	1498.29	697.40	-2571250.00	162773.00	75938.50	2+3	155.00	32.422
29	1666.67	1	SLU	-75587.90	781.73	363.87	-2571250.00	161423.00	75302.90	2-3	155.00	34.017
30	1726.19	1	SLU	-71872.90	225.65	105.03	-2571250.00	160066.00	74663.70	2-3	155.00	35.779
31	1785.71	1	SIJ	-68161.70	-187.02	-87.05	-2571250.00	-158674.00	-73896.60	2-3	335.00	37.723
32	1845.24	1	SLU	-64454.20	-473.45	-220.37	-2571250.00	-157343.00	-73269.10	2-3	335.00	39.893
33	1904.76	1	SIJJ	-60750.10	-650,71	-302,88	-2571250,00	-156010.00	-72640,80	2-3	335.00	42.325
34	1964,29	1	SLU	-57049.30	-735.69	-342.44	-2571250.00	-154676.00	-72012.60	2-3	335.00	45.071
35	2023.81	1	SLU	-53351.60	-745.01	-346.78	-2571250.00	-153339.00	-71382,60	2-3	335.00	48.194
36	2083.33	1	SLU	-49656.70	-695.01	-323.50	-2571250.00	-152002.00	-70752.40	2-3	335.00	51.783
37	2142.86	1	SIJ	-45964.50	-601.71	-280.08	-2571250.00	-150663.00	-70121.90	2-3	335.00	55,940
38	2202,38	1	SIJ	-42274.70	-480.85	-223.82	-2571250.00	-149321.00	-69490,10	2-3	335.00	60.822
39	2261.90	1	SLU	-38587.20	-347.94	-161.95	-2571250.00	-147979.00	-68858.00	2-3	335.00	66.635
40	2321,43	1	SLU	-34901.80	-218.28	-101.60	-2571250.00	-146635.00	-68225.40	2+3	335.00	73.671
41	2380.95	1	SIJ	-31218.30	-107.02	-49.82	-2571250.00	-145277.00	-67606,00	2-3	335.00	82.364
42	2440.48	1	SIAI	-27536.40	-29.26	-13.62	-2571250.00	-143831.00	-67091.40	2-3	335.00	93.376
43	2500.00	1	SLU	-23856.00	0.00	0.00	-2571250.00					>100

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIU	6757.23	-965.38	0.85	11.31	6825.85	1.00	32294.70	355514.00	32294.70	4,731
2	59.52	1	SIJ	4388.15	-626.92	0.85	11.31	4432.71	1.00	32294.70	355521,00	32294.70	7.286
- 3	119.05	1	SLU	2352.40	-336.08	0.85	11.31	2376.28	1.00	32294.70	355296.00	32294.70	13.590
4	178,57	1	SLU	625.21	-89.32	0.85	11.31	631.56	1.00	32294.70	355071.00	32294.70	51.135
- 5	238.09	1	SIJJ	-818.74	116.97	0.85	11.31	827.05	1.00	32294.70	354847,00	32294.70	39.048
- 6	297.62	1	SIJ	-2004.90	286.43	0.85	11.31	2025.26	1.00	32294.70	354623.00	32294.70	15.946
7	357.14	1	SLU	-3258.78	465.57	0.85	11,31	3291.87	1.00	32294.70	354400.00	32294.70	9.810
.8	416.67	1	SIU	-4535.64	647.99	0.85	11.31	4581.69	1.00	32294.70	353849.00	32294.70	7.049
9	476.19	1	SLU	-5498.13	785.49	0.85	11.31	5553.95	1.00	32294.70	353298.00	32294.70	5.815
10	535.71	1	SLU	-6185.61	883.71	0.85	11.31	6248.42	1.00	32294.70	352749.00	32294.70	5.168
11	595.24	1	SIJ	-6635.25	947.95	0.85	11.31	6702.62	1,00	32294.70	352201.00	32294.70	4.818
12	654.76	1	SLU	-6881.74	983.16	0.85	11.31	6951.62	1,00	32294.70	351654.00	32294.70	4.64
13	714.29	1	SLU	-6957.16	993.94	0.85	11.31	7027.80	1.00	32294.70	351108.00	32294.70	4.593
14	773.81	1	SIU	-6890.81	984.46	0.85	11.31	6960.78	1.00	32294.70	350563.00	32294.70	4.640
15	833.33	1	SLU	-6709.25	958.52	0.85	11.31	6777.38	1.00	32294.70	350019.00	32294.70	4,765
16	892.86	1	SIU	-6436.28	919.52	0.85	11.31	6501.64	1.00	32294.70	349476.00	32294.70	4,96
17	952.38	1	SIU	-6093.03	870.49	0.85	11.31	6154.90	1.00	32294.70	348934.00	32294.70	5.24
18	1011,90	1	SLU	-5698.07	814.06	0.85	11.31	5755.92	1.00	32294.70	348393.00	32294.70	5.611
19	1071.43	1	SLU	-5267.53	752.55	0.85	11.31	5321.01	1.00	32294.70	347853.00	32294.70	6.069
20	1130.95	1	SLU	-4815.29	687.94	0.85	11.31	4864.18	1.00	32294.70	347314.00	32294.70	6.639
21	1190.48	1	SIU	-4353.12	621.91	0.85	11.31	4397.32	1.00	32294.70	346776.00	32294.70	7.344
22	1250.00	1	SLU	-3890.87	555.87	0.85	11.31	3930.38	1,00	32294.70	346238.00	32294.70	8.21
23	1309.52	1	SLU	-3436.67	490.98	0.85	11.31	3471.56	1.00	32294.70	345701.00	32294.70	9.30
24	1369.05	1	SLU	-2997.08	428.18	0.85	11.31	3027.51	1.00	32294.70	345165.00	32294.70	10.66
25	1428.57	1	SLU	-2577.31	368.21	0.85	11.31	2603.48	1.00	32294.70	344630.00	32294.70	12,409
26	1488,10	1	SILI	-2181.37	311.64	0.85	11.31	2203.52	1.00	32294.70	344095.00	32294.70	14,656
27	1547,62	1	SIU	-1812.23	258.91	0.85	11.31	1830.63	1.00	32294.70	343561.00	32294,70	17.641

28	1607.14	1	SLU	-1472.01	210.30	0.85	11.31	1486.96	1.00	32294.70	343028.00	32294.70	21,719
29	1666.67	1	SIJ	-1162.11	166.03	0.85	11.31	1173.91	1.00	32294.70	342495.00	32294.70	27.510
30	1726.19	1	SIJ	-883.32	126.20	0.85	11.31	892.29	1.00	32294.70	341963.00	32294.70	36.193
31	1785,71	1	SIJJ	-635,99	90.86	0.85	11.31	642.45	1.00	32294.70	341432.00	32294.70	50.268
32	1845.24	1	SLU	-420.11	60.02	0.85	11.31	424.37	1.00	32294.70	340900.00	32294.70	76.100
33	1904.76	1	SLU	-235.41	33.63	0.85	11.31	237.80	1.00	32294.70	340370.00	32294.70	>100
34	1964.29	1	SLU	-81.46	11.64	0.85	11.31	82,29	1.00	32294.70	339840.00	32294.70	>100
35	2023.81	1	SLU	42.25	-6.04	0.85	11.31	42.68	1.00	32294.70	339310,00	32294.70	>100
36	2083.33	44	SLU	136.30	-19.47	0.85	11.31	137.68	1.00	32294.70	338781.00	32294.70	>100
37	2142.86	1	SIJ	201.21	-28.75	0.85	11.31	203.25	1.00	32294.70	338252.00	32294.70	>100
38	2202.38	1	SLU	237.47	-33.93	0.85	11.31	239.88	1,00	32294.70	337723.00	32294.70	>100
39	2261.90	1	SLU	245.50	-35.07	0.85	11.31	247.99	1.00	32294.70	337195.00	32294.70	>100
40	2321.43	1	SIAJ	225.59	-32.23	0.85	11.31	227.88	1.00	32294.70	336667.00	32294.70	>100
41	2380.95	-1	SLU	177.97	-25.43	0.85	11.31	179.78	1.00	32294.70	336140.00	32294.70	>100 .
42	2440.48	1	SLU	102.75	-14.68	0.85	11.31	103.80	1.00	32294.70	335612.00	32294.70	>100

		400		e d'esercia			_			
Caso	X <cm></cm>	cc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC	o _c	of
4.4	11000	-	0111 5	-123316.00		39940.90	-	And in column 2 is not a local division of	<dan cmq=""></dan>	THE RESERVE THE PERSON NAMED IN COLUMN 1
44	59.52	2	SLE R	-123316.00	18591.10	42179.50	34.56	43.98	37.85 40.18	524.0 554.6
46	119.05	2	SLE R	-122690.00	20261.50	43529.60	34.56	43.98	41.67	573.7
47	178.57	2	SLE R	-121717.00	20536.70	44120.80	34.56	43.98	42,35	582.3
48	238.09	2	SLE R	-120747.00	20514.30	44072.60	34.56	43.98	42.35	582.0
49	297.62	2	SLE R	-119781.00	20245.10	43494.30	34.56	43.98	41.76	574.1
50	357.14	2	SLE R	-118819.00		42444.30	34.56	43,98		559.6
51	416.67	2						43,98	40.67	
52	476.19	2	SLE R	-115982.00 -113151.00	19018.70	40859.40 38823.70	34.56	43.98	39.08	538,2 510,6
53	-	-	-			100000000000000000000000000000000000000		43.98	34.61	
54	535.71	2	SLE R	-110326.00	16969.10 15760.80	36456.20	34.56			478.6 443.9
55	654.76	2	SLE R	-107507.00				43.98	32.01	
-		2		-104694.00		31125.00		-		408.1
56	714.29	2	SLE R	-101887.00	13184.70	28325.70	28.27	50.27	26.67	372.4
57	773.81	2	SLE R		11881.30	Manager a Co	28.27	50.27	24.11	337.9
58	833,33	2	SLE R	-96287.60	10601.60	22776.30	21.99	56,55	21.72	305.6
59	892.86	2	SLE R	-93495.90	9364.98	20119.60	21.99	56.55	19.53	275.9
60	952,38	2	SLE R	-90709.20	8186.57	17587.90	15.71	62.83	17.57	249.1
61	1011.90	2	SLE R	-87927.40	7077.B1	15205.90	9,42	69,11	15.83	225.2
62	1071,43	2	SLE R	-85150,40	6046.87	12991.00	0,00	78,54	14.29	203.9
63	1130.95	2	SLE R	-82377.90	5099.08	10954.80	0.00	78.54	12.90	184.8
64	1190.48	2	SLE R	-79609.80	4237.40	9103.55	0.00	78.54	11.63	167.2
65	1250,00	2	SLE R	-76846.00	3462.73	7439.27	0.00	78.54	10.46	151.0
66	1309.52	2	SLE R	-74086.30	2774.30	5960.25	0.00	78.54	9.40	136.2
67	1369.05	2	SLE R	-71330.60	2169,95	4661.89	0.00	78.54	8.44	122.9
68	1428.57	2	SLE R	-68578.70	1646.44	3537.18	0.00	78.54	7,58	110.8
69	1488,10	2	SLE R	-65830.40	1199.63	2577.27	0.00	78,54	6.81	100.1
70	1547.62	2	SLE R	-63085.80	824.77	1771.92	0.00	78.54	6.13	90.5
71	1607,14	2	SLE R	-60344.50	516.60	1109.85	0.00	78.54	5.53	82.1
72	1666.67	2	SLE R	-57606.40	269.53	579.06	0.00	78.54	5.01	74.7
73	1726,19	2	SLE R	-54871.40	77.80	167.15	0.00	78.54	4.55	68.1
74	1785.71	2	SLE R	-52139.40	-64.48	-138,53	0.00	78.54	4,32	64.6
75	1845,24	2	SLE R	-49410.20	-163.24	-350.70	0.00	78.54	4.21	62.9
76	1904.76	2	SLE R	~46683.60	-224.36	-482.00	0.00	78.54	4.07	60.6
77	1964.29	2	SLE R	-43959.50	-253.66	-544.95	0.00	78.54	3.88	57.8
78	2023.81	2	SLE R	-41237.80	~256.B7	-551.86	0.00	78.54	3.66	54.5
79	2083,33	2	SLE R	-38518.30	-239.63	-514.82	0.00	78.54	3.42	50.9
80	2142.86	2	SLE R	-35800.80	-207.46	-445.71	0.00	78.54	3.16	47.1
81	2202.38	2	SLE R	-33085.30	-165.79	-356.19	0.00	78.54	2.89	43.1
82	2261.90	2	SLE R	-30371.50	-119.97	-257.73	0.00	78.54	2,61	39.0
83	2321.43	2	SLE R	-27659.40	-75.26	-161.69	0.00	78.54	2.34	34.9
84	2380.95	2	SLE R	-24948.80	-36.90	-79.28	0.00	78.54		31.0
85	2440.48	2	SLE R	-22239.50	-10.09	-21.67	0.00	78.54	1.82	27.2
86	2500.00	2	SLE B	-19531.40	0.00		0.00			23.8
.87	0.00	4	SLE Q	-123316.00			34.56	43.98	37.85	524.0
88	59.52			-123667.00						554.6
89	119.05	_		-122690.00						573.7
90	178.57			-121717.00						582.3
91	238.09			-120747.00						582.0
92	297.62			-119781.00						574.1
93	357.14	_		-118819.00						559.6
94	416.67	_		-115982.00						538.2
95	476.19	_		-113151.00						510.6
96	535.71	_	-	-110326.00			-			478.6
97	595.24			-107507.00						443.9
98	654.76			-104694.00					29.33	408.1
99	714.29	_		-101887.00					26.67	372.4
100	773.81		SLE Q							337.9
101	833.33	_	SLE Q						21.72	305.6

								Lei	azioi	le ui caic	OIO
102	892,86	4	SLE	o	-93495.90	9364.98	20119.60	21.99	56.55	19.53	275.96
103	952.38	4	SLE	Q	-90709.20	8186.57	17587.90	15.71	62.83	17.57	249.15
104	1011.90	4	SLE	Q	-87927.40	7077.81	15205.90	9.42	69.11	15.83	225.24
105	1071,43	4	SLE	Q	-85150.40	6046.87	12991.00	0.00	78.54	14.29	203.99
106	1130,95	4	SLE	Q	-82377.90	5099.0B	10954.80	0.00	78.54	12.90	184.87
107	1190.48	4	SLE	Q	-79609.80	4237.40	9103.55	0.00	78.54	11.63	167.23
108	1250.00	4	SLE	Q	-76846.00	3462.73	7439.27	0.00	78.54	10.46	151.03
109	1309.52	4	SLE	Q	-74086.30	2774.30	5960.25	0.00	78,54	9.40	136.27
110	1369.05	4	SLE	Q	+71330.60	2169.95	4661.89	0.00	78.54	8.44	122.90
111	1428.57	4	SLE	Q	-68578.70	1646.44	3537.18	0.00	78.54	7.58	110.88
112	1488.10	4	SLE	Q	-65830.40	1199.63	2577.27	0.00	78.54	6.81	100.13
113	1547.62	4	SLE	Q	-63085.80	B24.77	1771.92	0.00	78,54	6.13	90.5
114	1607.14	4	SLE	Q	-60344.50	516.60	1109.85	0.00	78.54	5.53	82.13
115	1666,67	4	SLE	Q	-57606.40	269.53	579.06	0.00	78.54	5.01	74.70
116	1726.19	4	SLE	Q	-54871.40	77.80	167.15	0.00	78.54	4.55	68.1
117	1785.71	4	SLE	Q	-52139.40	-64.48	-138.53	0.00	78.54	4.32	64.63
118	1845.24	4	SLE	Q	-49410.20	-163.24	-350,70	0.00	78.54	4.21	62.97
119	1904.76	4	SLE	Q	-46683.60	-224.36	-482.00	0.00	78.54	4.07	60.6
120	1964.29	4	SLE	Q	-43959.50	-253.66	-544.95	0.00	78.54	3.88	57.83
121	2023.81	4	SLE	Q	-41237.80	-256.B7	-551.86	0.00	78,54	3,66	54.56
122	2083.33	4	SLE	Q	-38518.30	-239.63	-514.82	0.00	78.54	3.42	50.96
123	2142.86	4	SLE	Q	-35800.80	-207.46	-445.71	0.00	78.54	3.16	47.13
124	2202,38	4	SLE	Q	-33085.30	+165.79	-356.19	0.00	78,54	2.89	43.10
125	2261.90	4	SLE	Q	-30371.50	-119.97	-257.73	0.00	78.54	2.61	39.0
126	2321,43	4	SLE	Q	-27659.40	-75.26	-161.69	0.00	78.54	2,34	34,98
127	2380.95	4	SLE	Q	-24948.80	-36.90	-79.28	0.00	78.54	2.07	31.03
128	2440.48	- 6	SLE	Q	-22239,50	-10.09	-21.67	0.00	78.54	1.82	27.28
129	2500.00	4	SLE	Q	-19531.40	0.00	0.00	0.00	78.54	1,59	23.81

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <nm></nm>	K 2	Φeq	Δ _{sim}	A _S	Ac eff <cmq></cmq>	σ _B <dan cmg=""></dan>	eam	Wk <mm></mm>
87	0.00	4	SLE Q	-123316.00	39940.90	18591.10	46.00	136,36	0.50	20.00	197.57	15.71	829.15	328.18	0.10	0.03
88	59.52	4	SLE Q	-123667.00	42179.50	19633.10	46.00	136,36	0.50	20,00	203,68	15.71	877.11	383,98	0.11	0.04
89	119.05	4	SLE Q	-122690.00	43529.60	20261.50	46.00	136.36	0.50	20.00	207.89	15.71	910.17	426.93	0.12	0.04
.90	178.57	4	SLE Q	-121717.00	44120.80	20536.70	46.00	136.36	0.50	20.00	210.02	15.71	926.92	450.04	0.13	0.05
91	238.09	4	SLE Q	-120747.00	44072.60	20514,30	46.00	136.36	0.50	20.00	210.68	15,71	932,13	455.17	0.13	0.05
92	297.62	4	SLE Q	-119781.00	43494.30	20245.10	46.00	136,36	0.50	20.00	210,19	15.71	928.23	445.03	0,13	0.05
93	357.14	4	SLE Q	-118819.00	42444.30	19756.40	46.00	136.36	0.50	20.00	208.58	15.71	915.58	421.55	0.12	0.04
94	416.67	4	SLE Q	-115982.00	40859.40	19018.70	46.00	136.36	0.50	20,00	207.16	15.71	904.46	395.51	0.12	0.04
95	476.19	4	SLE Q	-113151.00	38823.70	18071,10	46.00	136.36	0.50	20,00	204.34	15.71	882.31	357.52	0.10	0.04
96	535.71	4	SLE Q	-110326.00	36456.20	16969,10	46.00	136.36	0.50	20,00	200.02	15.71	848.36	311.89	0.09	0.03
97	595,24	4	SLE Q	-107507.00	33860.30	15760.80	46.00	136.36	0.50	20.00	193.99	15,71	801.02	262.60	0.08	0.03
98	654.76	4	SLE Q	-104694.00	31125,00	14487.60	46.00	136.36	0.50	20.00	185.88	15.71	737.30	213,10	0.06	0.02
- 99	714.29	4	SLE Q	-101887.00	28325.70	13184.70	46.00	136.36	0.50	20.00	174.06	15.71	644.54	166.17	0.05	0.01
100	773.B1	4	SLE Q	-99084.40	25525.60	11881.30	46.00	136,36	0.50	20,00	206,69	9.42	540.49	123.81	0.04	0.01
101	833.33	4	SLE Q	-96287.60	22776.30	10601.60	46.00	136.36	0.50	20.00	183.02	9.42	428.94	87.20	0.03	0.01
102	892.86	4	SLE Q	-93495.90	20119.60	9364.98	46.00	136.36	0.50	20.00	158.51	9.42	313.42	56.70	0.02	0.00
103	952.38	4	SLE Q	-90709.20	17587.90	8186.57	46.00	136,36	0.50	20.00	218.57	3.14	198.81	32.02	0.01	0.00
130	0.00	3	SLE F	-123316.00	39940.90	18591.10	46.00	136.36	0.50	20.00	197.57	15.71	829.15	328.18	0.10	0.03
131	59.52	3	SLE F	-123667.00	42179.50	19633.10	46.00	136.36	0.50	20.00	203.68	15.71	877.11	383.98	0.11	0.04
132	119.05	3	SLE F	-122690.00	43529.60	20261.50	46.00	136.36	0.50	20.00	207.89	15.71	910.17	426.93	0.12	0.04
133	178.57	3	SLE F	-121717.00	44120.80	20536.70	46.00	136.36	0.50	20.00	210.02	15.71	926.92	450.04	0.13	0.05
134	238.09	3	SLE F	-120747.00	44072.60	20514.30	46.00	136,36	0.50	20.00	210.68	15,71	932.13	455.17	0.13	0.05
135	297.62	3	SLE F	-119781.00	43494.30	20245.10	46.00	136,36	0.50	20.00	210.19	15.71	928.23	445.03	0.13	0.05
136	357.14	3	SLE F	-118819.00	42444.30	19756.40	46.00	136.36	0.50	20.00	208.58	15.71	915.58	421.55	0.12	0.04
137	416.67	3	SLE F	-115982.00	40859.40	19018.70	46.00	136.36	0.50	20.00	207.16	15.71	904.46	395.51	0.12	0.04
138	476.19	3	SLE F	-113151.00	38823.70	18071.10	46.00	136.36	0.50	20.00	204.34	15.71	882.31	357.52	0.10	0.04
139	535.71	3	SLE F	-110326.00	36456.20	16969.10	46.00	135.36	0.50	20.00	200,02	15.71	848.36	311.89	0.09	0.03
140	595.24	. 3	SLE F	-107507.00	33860.30	15760.80	46.00	136.36	0.50	20.00	193,99	15.71	801.02	262.60	0.08	0.03
141	654.76	3	SLE F	-104694.00	31125.00	14487.60	46.00	136.36	0.50	20.00	185,88	15.71	737.30	213.10	0.06	0.02
142	714,29	3	SLE F	-101887.00	28325.70	13184.70	46.00	136.36	0.50	20.00	174.06	15,71	644.54	166.17	0.05	0.01
143	773.81	3	SLE F	-99084,40	25525.60	11881.30	46.00	136.36	0.50	20,00	206.69	9,42	540.49	123,81	0.04	0.01
144	833.33	3	SLE F	-96287.60	22776.30	10601.60	46.00	136.36	0.50	20.00	183.02	9.42	428.94	87.20	0.03	0.01
145	892.86	3	SLE F	-93495.90	20119.60	9364.98	46.00	136.36	0.50	20.00	158.51	9.42	313.42	56.70	0.02	0.00
146	952.38	3	SLE F	-90709.20	17587.90	8186.57	46.00	136,36	0.50	20.00	218.57	3,14	198.B1	32.02	0.01	0.00

Verifiche principali

Caso	Tipo
5	SLU N cost - min. sic.
1.3	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
48	C.Rare - Sf max (max traz.)
63	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
91	C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
106	C.Q.Per Sc max (min. compr.)

Palo n. 19

Caratteristiche del palo e dei materiali utilizzati

r di	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	5450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 19 (-126)

Caso	8	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	212368.00	6475.78	-930.75	44827.10	-30893.40
	1	SIJ	TAG		2 2		0.00	0.00
	. 1	SLU	ECC				0.00	0.00
	1	SLU	TOT	212368.00	6475.78	-930.75	44827.10	-30893.40
- 2	2	SLE R	RVN	157310.00	4796.87	-689.44	33205.30	-22884.00
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC		6 (1		0.00	0.00
	- 2	SLE R	TOT	157310.00	4796.87	-689.44	33205.30	-22884.00
3	3	SLE F	RVN	157310.00	4796.87	-689.44	33205.30	-22884.00
	. 3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	157310.00	4796.87	-689.44	33205.30	-22884.00
.4	4	SLE Q	RVN	157310.00	4796.87	-689,44	33205.30	-22884.00
	4	SLE Q	TAG		~ *		0.00	0.00
	4	SLE Q	ECC		9 9		0.00	0.00
	4	SIE Q	TOT	157310.00	4796.87	-689.44	33205.30	-22884.00

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-212368.00	-6475.78	930.75	-44827.10	30893.40
2	2	SLE R	1	-157310.00	-4796.87	689.44	-33205.30	22884.00
- 3	3	SLE F	1	-157310.00	-4796.87	6B9.44	-33205.30	22884.00
4	. 4	SLE Q	. 1	-157310.00	-4796.87	689.44	-33205.30	22884.00

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SIU	-212368.00	44640.60	30764.90	-21236B.00	188055.00	129102.00	2-3	145.62	4.20
2	59.52	1	SLU	-212100.00	47287.50	32589.00	-212100.00	187981.00	129054.00	2-3	145,62	3.970
3	119.05	1	SLU	-209888.00	48918.80	33713.30	-209888.00	187375.00	128658.00	2-3	145.62	3.826
-4	178.57	1	SIU	-207682.00	49681.70	34239.10	-207682.00	186769.00	128262.00	2-3	145.62	3.75
- 5	238.09	1	SIU	~205483.00	49712.00	34259.90	-205483.00	186172.00	127829.00	2-3	145.62	3,741
.6	297.62	1	SLU	-203290,00	49133.90	33861.50	-203290.00	184203.00	129295.00	2-3	145.00	3.773
7	357.14	1	SLU	-201103.00	48013.60	33089.40	-201103.00	183619.00	128828.00	2-3	145.00	3.84
- 8	416.67	1	SIJ	-196175.00	46276.50	31892.30	-196175.00	182299.00	127770.00	2-3	145.00	3.963
- 9	476.19	1	SLU	-191257.00	4401B.50	30336.10	-191257.00	180977.00	126711.00	2-3	145.00	4.13
10	535.71	1	SLU	-186349.00	41375.10	28514.40	-186349.00	179652.00	125647.00	2-3	145.00	4.363
11	595.24	1	SIJ	-181452.00	38464.60	26508.60	-181452.00	178326.00	124581.00	2-3	145.00	4.65
12	654.76	1	SLU	-176564.00	35388.80	24388.80	-176564.00	176988.00	123517.00	2-3	145.00	5.02
13	714.29	1	SLU	-171686,00	32234.00	22214.70	-171686.00	175632.00	122462.00	2-3	145.00	5.46
14	773.81	1	SIJ	-166816.00	29072.60	20035.90	-166816,00	174274.00	121404.00	2-3	145.00	6.01
15	833,33	1	SLU	-161956.00	25964.10	17893.60	-161956.00	172914.00	120343.00	2-3	145.00	6.68
16	892.86	1	SEU	+157105.00	22956.40	15820.80	-157105.00	171551.00	119279.00	2-3	145.00	7.49
17	952.38	1	SLU	-152261.00	20087.00	13843.30	-152261,00	170162.00	118232.00	2-3	145.00	8.49
18	1011,90	1	SLU	-147426.00	17384.40	11980.80	-147426.00	168657,00	117264.00	2-3	145.00	9.72
19	1071.43	1	SLU	-142599.00	14869.00	10247.30	-142599.00	167148.00	116294.00	2-3	145.00	11.27
20	1130.95	1	SLU	-137780.00	12554.50	8652.13	-137780.00	165633.00	115323.00	2-3	145.00	13,23
21	1190.48	1	SIAI	-132968.00	10448.20	7200.57	-132968.00	164114.00	114351.00	2-3	145.00	15.76
22	1250.00	1	SLU	-128163.00	8552.92	5894.40	-128163.00	162590.00	113377.00	2-3	145.00	19,082
23	1309.52	1	SIU	-123365.00	6867.03	4732.54	-2571250,00	161061.00	112402.00	2-3	145.00	20.843
24	1369.05	1	SLU	-118574.00	5385.58	3711.57	-2571250,00	159527.00	111425.00	2-3	145.00	21,68
25	1428.57	1	SLU	-113789.00	4100.88	2826.19	-2571250.00	157989.00	110447.00	2-3	145.00	22.59

	Lanca de la Contraction de Contraction	11.40	ATTOCATED IN		part 15
Pa	lazione	di	00	00	0
176	Idaliulie	u	La	COL	

26	1488.10	1	SLU	-109010.00	3003.08	2069.63	-2571250.00	156445.00	109468.00	2-3	145.00	23.587
27	1547.62	1	SLU	-104237.00	2080.74	1433.98	-2571250.00	154899.00	108487.00	2-3	145.00	24.667
28	1607.14	1	SILI	⇒99469.10	1321.20	910.53	-2571250,00	153346.00	107505.00	2-3	145.00	25.850
29	1666.67	1	SIA	-94707.00	710.97	489.98	-2571250.00	151790.00	106521.00	2-3	145.00	27,149
30	1726.19	1	SLU	-89949.90	236.05	162.68	-2571250.00	151367.00	103855.00	2-3	145.62	28.585
31	1785.71	1	SLU	-85197.60	-117.84	-81.21	-2571250.00	-149203.00	-103960.00	2-3	325.00	30.180
32	1845,24	1	SIU	-80449.90	-365.08	-251.60	-2571250.00	-147764.00	-102796.00	2-3	325.00	31.961
33	1904.76	ĭ	SLU	-75706.60	-519.98	-358.36	-2571250.00	-146324.00	-101625.00	2-3	325.00	33.963
34	1964.29	1	SLU	-70967.20	-596.73	~411.25	-2571250.00	-144793.00	-100523.00	2-3	325.00	36.231
35	2023.81	1	SLU	-66231.70	-609.28	-419.90	-2571250.00	-143195.00	-99463.00	2-3	325.00	38,822
36	2083.33	1	SLU	-61499.80	-571.37	-393.77	-2571250.00	-141592.00	-98400.80	2-3	325.00	41.809
37	2142.86	1	SLU	-56771.10	-496.45	-342.14	-2571250+00	-139984.00	-97335.50	2-3	325.00	45.291
38	2202.38	1	SIAJ	-52045.50	-397.79	-274.14	-2571250.00	-138369.00	-96267.50	2-3	325.00	49.404
39	2261,90	1	SLU	-47322,70	-288.42	-198.77	-2571250.00	-136728.00	-95211.30	2-3	325.00	54.334
40	2321.43	1	SLU	-42602.40	-181.23	-124.90	-2571250.00	-135077.00	-94154.70	2-3	325.00	60.355
41	2380.95	1	SLU	-37884.40	-88.98	-61.32	-2571250,00	-133422.00	-93096.00	2-3	325.00	67.871
42	2440,48	1	SLU	-33168.50	-24.35	-16.7B	-2571250.00	-131760.00	-92035.50	2-3	325.00	77,521
43	2500.00	1	SLU	-28454.30	0.00	0.00	-2571250.00					90.364

Caso	X <cm>></cm>	cc		- Verifi Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
- 1	0.00	1	SLU	6475.78	-930.75	0.85	11.31	6542.33	1,00	32294.70	362088.00	32294.70	4.936
2	59.52	1	SLU	4268.64	-613.52	0.85	11.31	4312.50	1.00	32294.70	362049,00	32294.70	7.489
- 3	119.05	1	SLU	2370.00	-340.63	0.85	11.31	2394.35	1.00	32294.70	361732.00	32294.70	13.488
- 4	178.57	1	SLU	757.19	-108.83	0.85	11.31	764.97	1,00	32294.70	361416.00	32294.70	42.217
- 5	238.09	1	SIU	-593.02	85.23	0.85	11.31	599.11	1.00	32294.70	361101.00	32294.70	53.904
- 6	297.62	1	SLU	-1704.03	244.92	0.85	11.31	1721.54	1.00	32294.70	360787,00	32294.70	18.759
- 7	357.14	1	SLU	-2881.26	414.12	0.85	11.31	2910.87	1.00	32294.70	360474.00	32294.70	11.095
8	416.67	1	SIA	-4082.91	586.83	0.85	11.31	4124.86	1.00	32294.70	359768.00	32294.70	7.829
. 9	476.19	1	SLU	-4992.07	717.50	0.85	11.31	5043.37	1.00	32294.70	359064.00	32294.70	6.403
10	535.71	1	SLU	-5645.14	811.36	0.85	11.31	5703.15	1.00	32294.70	358361,00	32294.70	5.663
11	595.24	1	SIU	-6076.47	873.36	0.85	11.31	6138.91	1.00	32294.70	357659.00	32294.70	5.261
12	654.76	1	SLU	-6318.22	908.10	0.85	11.31	6383.15	1.00	32294.70	356959.00	32294.70	5.059
13	714.29	1	SIJ	-6400.09	919.87	0.85	11.31	6465.85	1.00	32294.70	356260,00	32294.70	4.995
14	773.81	1	SIJJ	-6349.27	912.57	0.85	11.31	6414.52	1.00	32294.70	355563.00	32294.70	5.035
15	833,33	1	SLU	-6190.43	889.74	0.85	11.31	6254.04	1.00	32294.70	354867.00	32294.70	5.164
16	892.86	1	SIJ	-5945.66	854.56	0.85	11,31	6006.76	1.00	32294.70	354172.00	32294.70	5.376
17	952.38	1	SIAI	-5634.64	809.85	0.85	11.31	5692.54	1,00	32294.70	353478.00	32294.70	5.573
18	1011.90	1	SIU	-5274.64	758.11	0.85	11.31	5328.84	1.00	32294.70	352785.00	32294.70	5.060
19	1071,43	1	SLU	-4880.69	701.49	0.85	11.31	4930.85	1.00	32294.70	352094,00	32294.70	6.550
20	1130.95	1	SLU	-4465.75	641.85	0.85	11.31	4511.64	1.00	32294.70	351404.00	32294.70	7.158
21	1190.48	1	SIAI	-4040.B1	580.78	0.85	11,31	4082.33	1.00	32294.70	350714.00	32294.70	7.911
22	1250.00	1	SIJ	-3615.08	519.59	0.85	11.31	3652.22	1.00	32294.70	350026.00	32294.70	8.842
23	1309.52	1	SW	-3196.16	459.38	0.85	11.31	3229.01	1.00	32294.70	349339.00	32294.70	10.001
24	1369.05	1	SLU	-2790.24	401.04	0.85	11,31	2818.91	1.00	32294.70	348653.00	32294.70	11,457
25	1428.57	1	SLU	-2402,20	345.26	0.85	11.31	2426.88	1.00	32294.70	347967.00	32294.70	13.307
26	1488.10	1	SIAI	-2035.81	292.60	0.85	11.31	2056.73	1,00	32294.70	347283.00	32294.70	15.702
27	1547.62	1	SLU	-1693.92	243.46	0.85	11.31	1711.33	1.00	32294.70	346599,00	32294.70	18.871
28	1607,14	1	SIJ	+1378.54	198.13	0.85	11.31	1392.70	1,00	32294.70	345916.00	32294.70	23.189
29	1666.67	1	SLU	-1090.99	156.81	0.85	11.31	1102.20	1,00	32294.70	345234.00	32294.70	29.300
30	1726.19	1	SLU	-832,09	119.59	0.85	11.31	840.64	1.00	32294.70	344552.00	32294.70	38.417
31	1785.71	1	SIU	-602,17	86.55	0.85	11.31	608.36	1.00	32294.70	343872.00	32294.70	53.085
32	1845,24	1	SLU	-401.27	57.67	0.85	11.31	405.40	1.00	32294.70	343192,00	32294.70	79.562
33	1904.76	1	SIAI	-229.18	32.94	0.85	11.31	231.53	1.00	32294.70	342512.00	32294.70	>100
34	1964.29	1	SIU	-85.51	12.29	0.85	11.31	86.39	1.00	32294.70	341833.00	32294.70	>100
35	2023.81	1	SIJJ	30.19	-4.34	0.85	11.31	30.50	1.00	32294.70	341155.00	32294.70	>100
36	2083,33	1	SLU	118.43	-17.02	0.85	11.31	119,65	1.00	32294.70	340477.00	32294.70	>100
37	2142.86	1	SLU	179.70	-25.83	0.85	11,31	181.54	1.00	32294.70	339800.00	32294.70	>100
38	2202.38	1	SIJ	214.43	-30.82	0.85	11.31	216.63	1.00	32294.70	339123.00	32294.70	>100
39	2261.90	1	SLU	222.99	-32.05	0.85	11.31	225.28	1.00	32294.70	338447.00	32294.70	>100
40	2321.43	1	SLU	205.68	-29.56	0.85	11.31	207.79	1.00	32294.70	337770.00	32294.70	>100
41	2380.95	1	SIJ	162,68	-23.38	0.85	11.31	164.35	1.00	32294.70	337095.00	32294.70	>100
42	2440.48	1	SIJJ	94.10	-13.53	0.85	11.31	95.07	1.00	32294.70	336419.00	32294.70	>100

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44	0.00	2	SLE R	-157310.00	22788.80	33067.10	25.13	53.41	35.00	492.81
45	59.52	2	SLE R	-157425.00	24140.00	35027.80	25.13	53.41	36.78	516.61
46	119.05	2	SLE B	-155976.00	24972.B0	36236.20	25.13	53.41	37.90	531,16
47	178.57	2	SLE R	-154532.00	25362.30	36801.30	28.27	50.27	38.42	537.91
48	238.09	2	SLE R	-153093.00	25377.70	36823.70	28.27	50.27	38.43	537,70
49	297.62	2	SLE R	-151659.00	25082.60	36395.50	28.27	50.27	37.98	531.56
50	357.14	2	SLE R	-150229.00	24510.70	35565.60	28.27	50.27	37.15	520.18
51	416.67	2	SLE B	-146594.00	23623.90	34278.90	25.13	53.41	35,83	502.07
52	476.19	2	SLE R	-142966.00	22471.20	32606.30	25.13	53.41	34,15	479.12

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87	0.00	4	SLE Q	-157310.00	33067.10	22788.80	46.00	136.36	0.50	20.00	172.80	9,42	380.76	129,33	0.04	0.01
88	59.52	4	SLE Q	-157425.00	35027.80	24140.00	46.00	136.36	0.50	20.00	164.16	12.57	453.42	162.03	0.05	0.01
89	119.05	4	SLE Q	-155976.00	36236,20	24972.80	46.00	136.36	0.50	20.00	173.34	12.57	511.05	188.59	0.05	0.02
90	178.57	4	SLE Q	-154532.00	36801.30	25362.30	46.00	136.36	0.50	20.00	178.71	12.57	544.79	204.31	0.06	0.02
.91	238.09	4	SLE Q	-153093.00	36823.70	25377.70	46.00	136.36	0.50	20.00	180.89	12.57	558.49	209.70	0.06	0.02
92	297.62	4	SLE Q	-151659.00	36395.50	25082.60	46.00	136,36	0.50	20.00	180.38	12.57	555.34	206.06	0.06	0.02
93	357.14	4	SLE Q	-150229.00	35565.60	24510.70	46.00	136.36	0.50	20.00	177.42	12.57	536.70	194,47	0.06	0.02
94	416.67	4	SLE Q	-146594.00	34278.90	23623.90	46.00	136.36	0.50	20.00	174.74	12.57	519.87	181.50	0.05	0.02
95	476.19	4	SLE Q	-142966.00	32606.30	22471.20	46.00	136.36	0.50	20.00	169.38	12.57	486.21	161,50	0.05	0.01
96	535.71	4	SLE Q	-139346.00	30648.20	21121.80	46.00	136.36	0.50	20.00	161.75	12.57	438.26	137.18	0.04	0.01
97	595.24	4	SLE Q	-135734.00	28492.30	19636.00	46.00	136.36	0.50	20.00	172.44	9.42	379.06	110.96	0.03	0.01
98	654.76	4	SLE Q	-132129.00	26213.90	18065.80	46.00	136.36	0.50	20.00	191.24	6.28	311.76	84.81	0.02	0.01
99	714.29	4	SLE Q	-128531.00	23877.10	16455.30	46.00	136.36	0.50	20.00	168.28	6,28	239.64	60.15	0.02	0.01
130	0.00	3	SLE F	-157310.00	33067.10	22788.80	46.00	136.36	0.50	20.00	172.80	9,42	380.76	129,33	0.04	0.01
131	59.52	3	SLE F	-157425.00	35027.80	24140.00	46.00	136,36	0.50	20.00	164.16	12.57	453.42	162.03	0.05	0.01
132	119.05	3	SLE F	-155976.00	36236.20	24972.80	46.00	136.36	0.50	20,00	173.34	12.57	511.05	188.59	0.05	0.02
133	178.57	3	SLE F	-154532.00	36801.30	25362.30	46.00	136.36	0.50	20.00	178.71	12.57	544.79	204.31	0.06	0.02
134	238.09	3	SLE F	-153093.00	36823.70	25377.70	46.00	136.36	0.50	20.00	180.89	12.57	558.49	209.70	0.06	0.02
135	297.62	3	SLE F	-151659.00	36395.50	25082.60	46.00	136.36	0.50	20.00	180.38	12.57	555.34	206.06	0.06	0.02
136	357.14	. 3	SLE F	-150229.00	35565.60	24510.70	46.00	136.36	0.50	20,00	177.42	12.57	536,70	194,47	0.06	0.02
137	416.67	3	SLE F	-146594.00	34278.90	23623.90	46.00	136.36	0.50	20.00	174.74	12.57	519.87	181.50	0.05	0.02
138	476.19	3	SLE F	-142966.00	32606.30	22471.20	46.00	136,36	0.50	20.00	169.38	12.57	486.21	161.50	0.05	0.01
139	535.71	3	SLE F	-139346.00	30648,20	21121.80	46.00	136,36	0.50	20.00	161.75	12.57	438.26	137,18	0.04	0.01
140	595.24	3	SLE F	-135734.00	28492.30	19636.00	46.00	136.36	0.50	20.00	172.44	9.42	379.06	110.96	0.03	0.01
141	654.76	3	SLE F	-132129.00	26213.90	18065.80	46.00	136.36	0.50	20.00	191.24	6.28	311.76	84.81	0.02	0.01
142	714,29	3	SLE F	-128531.00	23877.10	16455.30	46.00	136.36	0.50	20.00	168.28	6,28	239.64	60.15	0.02	0.01

Verifiche principali

Caso	Tipo
- 1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
- 5	SLU N cost - min. sic.
47	C.Rare - Sf min (max compr.)
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.)
61	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sf min (max compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
104	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 20

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti.

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVB	0.00			

Azioni ed effetti - Plinto/Palo n. 20 (-142)

Caso	00	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
- 1	1	SLU	RVN	253743.00	6222.70	-820.92	33060.30	-32330.90
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SLU	TOT	253743.00	6222.70	-820.92	33060.30	-32330.90
2	2	SLE R	RVN	187958.00	4609.41	-608.09	24489.10	-23948.80
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	187958.00	4609.41	-608.09	24489.10	-23948.80
3	3	SLE F	RVN	187958.00	4609.41	-608.09	24489.10	-23948.80
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC	ŝ	i = j		0.00	0.00
	3	SLE F	TOT	187958.00	4609.41	-608.09	24489.10	-23948.80
4	4	SLE Q	RVN	187958.00	4609.41	-608.09	24489.10	-23948.80
- 1	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SIJ	1	-253743.00	-6222.70	820.92	-33060.30	32330.90
- 2	2	SLE R	1	-187958.00	-4609.41	608.09	-24489.10	23948.80
- 3	3	SLE F	1	-187958.00	-4609.41	608.09	-24489.10	23948.80
4	4	SLE Q	1	-187958.00	-4609.41	608.09	-24489.10	23948.80

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SLU	-253743.00	32914.80	32188.60	-253743.00	172789.00	168767.00	2-3	135.62	5.246
2	59.52	1	SLU	-253187.00	35149.70	34374.30	-253187.00	172666.00	168641.00	2-3	135.62	4.909
.3	119.05	1	SLU	-250401.00	36591.80	35784.50	-250401.00	172053.00	168010.00	2-3	135.62	4.699
4	178.57	1	SLU	-247622.00	37354.00	36529.90	-247622.00	171439.00	167378.00	2-3	135.62	4.580
- 5	238.09	1	SIJJ	-244852.00	37540.80	36712.60	-244852.00	170824.00	166745.00	2-3	135.62	4.54
- 6	297.62	1	SLU	-242088.00	37248.10	36426.40	-242088.00	170211.00	166113.00	2-3	135.62	4.563
7	357.14	1	SLU	-239333.00	36525.90	35720.10	-239333.00	169599.00	165483.00	2-3	135.62	4.63
.8	416.67	1	SIAI	-233433.00	35312.40	34533.40	-233433.00	168281.00	164123.00	2-3	135.62	4.75
- 9	476.19	1	SLU	-227546.00	33681.00	32938.00	-227546.00	166963.00	162763.00	2-3	135.62	4.95
10	535.71	1	SLU	-221670.00	31737.30	31037.20	-221670.00	165640.00	161395.00	2-3	135.62	5.21
11	595.24	1	SLU	-215807.00	29573.50	28921.10	-215807.00	164250.00	160057.00	2-3	135.62	5.54
12	654.76	1	SIAI	-209955.00	27269.10	26667.50	-209955.00	162748.00	158769.00	2-3	135.62	5.96
13	714.29	1	SIJ	-204115.00	24891.90	24342.80	-204115.00	161239.00	157477.00	2-3	135.62	6.47
14	773.81	1	SLU	-198285.00	22498.90	22002.50	-198285.00	159727.00	156183.00	2-3	135.62	7.09
15	833,33	1	SIU	-192466.00	20136.90	19692.70	-192466.00	158203.00	154884.00	2+3	135.62	7.86
16	892.86	1	SIJJ	-186658.00	17844.20	17450.50	-186658.00	156677.00	153584.00	2-3	135.62	8,79
17	952.38	1	SLU	-180859.00	15650.60	15305.40	-180859.00	155143.00	152281.00	2-3	135.62	9.93
18	1011.90	1	SLU	-175070.00	13579.20	13279.70	-175070.00	155278.00	149288.00	2-3	136.25	11.34
19	1071.43	1	SLU	-169291,00	11646,60	11389.70	-169291,00	153742,00	147949.00	2-3	136.25	13,09
20	1130.95	1	SLU	-163520.00	9864.18	9646.57	-163520.00	152200.00	146607.00	2-3	136.25	15.31
21	1190.48	1	SILI	-157759.00	8238.48	8056.73	-2571250.00	150652,00	145263.00	2-3	136.25	16.29
22	1250.00	1	SLU	-152005.00	6772.27	6622.87	-2571250.00	149125.00	143865.00	2-3	136.25	16.91
23	1309.52	1	SLU	-146260.00	5464.99	5344.43	-2571250.00	147655.00	142324.00	2-3	136.25	17.58
24	1369.05	1	SLU	-140523.00	4313.41	4218.25	-2571250.00	146183.00	140780.00	2-3	136.25	18.29
25	1428.57	1	SLU	-134794.00	3312.08	3239.02	-2571250.00	144705.00	139226.00	2-3	136.25	19.07
26	1488.10	1	SIJ	-129071.00	2453.89	2399.75	-2571250.00	143224.00	137666.00	2-3	136,25	19.92
27	1547.62	1	SLU	-123356.00	1730.36	1692.19	-2571250.00	140210.00	137560.00	2-3	135.62	20.84
28	1607.14	1	SLU	-117647.00	1132.07	1107.10	-2571250,00	138727.00	135980.00	2-3	135.62	21.85
29	1666.67	1	SLU	-111944.00	648.91	634.60	-2571250.00	137241.00	134396.00	2-3	135.62	22.96
30	1726.19	1	SIAI	-106248.00	270.31	264.35	-2571250.00	135750.00	132801.00	2-3	135.62	24.20
31	1785.71	1	SIAJ	-100557.00	-14.56	-14.23	-2571250.00	-134145.00	-131466.00	2-3	315.62	25.57
32	1845.24	1	SLU	-94871.30	-216,60	-211.83	-2571250,00	-132472.00	-130050.00	2-3	315.62	27,10
33	1904.76	1	SLU	-89190.90	-346.76	-339.11	-2571250.00	-132260.00	-127155.00	2-3	316.25	28.82
34	1964.29	1	SLU	-83515.30	-415.85	-406.67	-2571250.00	-130572.00	-125737.00	2-3	316.25	30.78
35	2023.81	1	SIJ	-77844.10	-434.55	-424.96	-2571250.00	-128872.00	-124318.00	2-3	316.25	33.03
36	2083.33	1	SLU	-72177.20	-413.39	-404.27	-2571250.00	-127214.00	-122809.00	2-3	316.25	35.62
37	2142.86	1	SLU	-66514.10	-362.72	-354.72	-2571250.00	-125609.00	-121175.00	2-3	316.25	38.65
38	2202.38	1	SLU	-60854.60	-292.70	-286.25	-2571250.00	-123999.00	-119533.00	2-3	316.25	42.25
39	2261.90	1	SLU	-55198.30	-213.37	-208.67	-2571250.00	-122385.00	-117887.00	2-3	316.25	46.58
40	2321.43	1	SLU	-49545.10	-134.64	-131.67	-2571250.00	-120764.00	-116229.00	2-3	316.25	51,89
41	2380.95	1	SIJ	-43894.40	-66.33	-64.87	-2571250.00	-119153.00	-114534.00	2-3	316.25	58.57
42	2440.48	1	SLU	-38246.20	-18.20	-17.80	-2571250.00	-116232.00	-114077.00	2-3	315.62	67.22
43	2500.00	-	SIAI	-32599,90	0.00	0.00	-2571250.00					78.87

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	6222.70	-820.92	0.85	11.31	6276.62	1.00	32294.70	368014,00	32294.70	5.145
2	59,52	1	SIAJ	4237.53	-559.03	0.85	11.31	4274.25	1.00	32294.70	367934.00	32294.70	7.556
3	119.05	916	SLU	2525.33	-333.15	0.85	11.31	2547.21	1.00	32294.70	367535.00	32294.70	12.678
4	178.57	1	SEU	1066.59	-140.71	0.85	11.31	1075.83	1.00	32294.70	367137.00	32294.70	30.018
.5	238.09	1	SIJJ	-158.79	20.95	0.85	11.31	160.17	1.00	32294.70	366740.00	32294.70	>100
- 6	297.62	-1	SLU	-1171,15	154.50	0.85	11.31	1181,30	1.00	32294.70	366345.00	32294.70	27,338
7	357.14	1	SLU	-2249.99	296.83	0.85	11.31	2269.49	1.00	32294.70	365950.00	32294.70	14.230
- 8	416,67	1	SLU	-3357.42	442.92	0.85	11.31	3386.51	1.00	32294.70	365105.00	32294.70	9.536
9	476.19	1	SIAI	-4202.67	554.43	0.85	11.31	4239.08	1.00	32294.70	364262.00	32294.70	7.618
10	535.71	1	SLU	-4817.80	635.58	0.85	11.31	4859.54	1,00	32294.70	363420.00	32294.70	6.546
11	595.24	1	SIU	-5233.20	690.38	0.85	11.31	5278.54	1.00	32294.70	362580.00	32294.70	6.118
12	654.76	1	SLU	-5477,33	722.59	0.85	11.31	5524.79	1.00	32294.70	361742,00	32294.70	5.845
13	714.29	1	SIU	-5576.58	735.68	0.85	11.31	5624.90	1.00	32294.70	360905.00	32294.70	5.741

	Berthall Committee Committee Committee	1.0	0.00	CO. CO. C.	100
20	azione	CII /	20	COL	0
176	MAINIE.	1111	-01		

								111	HUZ	OHO UI	Calcolo		
14	773.81	1	SLU	-5555.14	732.86	0.85	11.31	5603.27	1.00	32294.70	360070.00	32294.70	5.764
15	833.33	1	SLU	-5435.00	717.01	0.85	11.31	5482.09	1.00	32294.70	359237.00	32294.70	5.891
16	892.86	1	SIU	-5235.93	690.75	0.85	11.31	5281.29	1.00	32294.70	358405.00	32294.70	6.115
17	952.38	1	SIJJ	-4975.52	656.39	0.85	11.31	5018.63	1.00	32294.70	357574.00	32294.70	6.435
18	1011.90	1	SLU	-4669.29	615.99	0.85	11.31	4709.75	1.00	32294.70	356745.00	32294.70	6.857
19	1071.43	1	SLU	-4330.78	571.33	0.85	11.31	4368.31	1.00	32294.70	355917.00	32294.70	7.393
20	1130.95	1	SLU	-3971.67	523.96	0.85	11.31	4006.08	1.00	32294.70	355091.00	32294.70	8.061
21	1190.48	ĭ	SIU	-3601.89	475.18	0.85	11.31	3633.10	1.00	32294.70	354265.00	32294.70	8.889
22	1250.00	2	SLU	-3229.83	426.09	0.85	11.31	3257.81	1.00	32294.70	353441.00	32294.70	9.913
23	1309.52	1	SIJ	-2862.41	377.62	0.85	11.31	2887.21	1.00	32294.70	352618.00	32294.70	11.185
24	1369.05	1	SLU	-2505.28	330.51	0.85	11.31	2526.99	1,00	32294.70	351797.00	32294.70	12.780
25	1428.57	1	SLU	-2162.95	285.35	0.85	11.31	2181.69	1.00	32294.70	350976.00	32294.70	14.803
26	1488,10	1	SIAJ	-1838.93	242.60	0.85	11.31	1854.86	1.00	32294.70	350156.00	32294.70	17,411
27	1547.62	1	SLU	-1535.86	202.62	0.85	11.31	1549.17	1.00	32294.70	349337,00	32294.70	20.846
28	1607.14	1	SLU	+1255.66	165.65	0.85	11.31	1266.54	1.00	32294.70	348520.00	32294.70	25.498
29	1666.67	1	SILI	-999.63	131.88	0.85	11.31	1008.30	1.00	32294.70	347703.00	32294.70	32.029
30	1726.19	1	SIJ	-768.59	101.39	0.85	11.31	775.25	1.00	32294.70	346887.00	32294.70	41.657
31	1785.71	1	SLU	-562.92	74.26	0.85	11.31	567.79	1.00	32294.70	346072.00	32294.70	56.877
32	1845.24	1	SLU	-382.73	50.49	0.85	11,31	386.05	1.00	32294.70	345257,00	32294.70	83.655
33	1904.76	1	SIU	-227.90	30.07	0.85	11.31	229.87	1.00	32294.70	344444.00	32294.70	>100
34	1964.29	1	SLU	-98.14	12.95	0.85	11.31	98.99	1.00	32294.70	343631.00	32294.70	>100
35	2023.81	1	SIJJ	6.91	-0.91	0.85	11.31	6.97	1.00	32294.70	342818.00	32294.70	>100
36	2083.33	1	SIJI	87.65	-11.56	0.85	11.31	88.41	1.00	32294.70	342007.00	32294.70	>100
37	2142.86	1	SLU	144.50	-19.06	0.85	11,31	145.75	1,00	32294.70	341196.00	32294.70	>100
.38	2202,38	1	SIU	177.83	-23.46	0.85	11,31	179.37	1.00	32294.70	340385.00	32294.70	>100
39	2261.90	1	SIJ	187.94	-24.79	0.85	11.31	189.57	1.00	32294.70	339575.00	32294.70	>100
40	2321.43	1	SLU	175.08	-23.10	0.85	11.31	176.60	1.00	32294.70	338765.00	32294.70	>100
41	2380.95	1	SLU	139.41	-18.39	0.85	11.31	140.62	1.00	32294.70	337955.00	32294.70	>100
42	2440.48	1	SIJ	81.04	-10.69	0.85	11.31	81.74	1.00	32294.70	337146.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <cmq></cmq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-187958.00	23843.40	24381.30	6.28	72,26	32.80	469.82
45	59.52	2	SLE R	-187859.00	25462.40	26036.80	12.57	65.97	34.09	487.41
46	119.05	2	SLE R	-185985.00	26507.00	27105.00	15.71	62.83	34.83	497.32
47	178.57	2	SLE R	-184117.00	27059,20	27669.60	15.71	62.83	35,18	501,93
48	238.09	2	SLE R	-182255.00	27194.50	27808.00	18,85	59.69	35.19	501.73
49	297.62	2	SLE R	-180399.00	26982.50	27591.20	18.85	59.69	34.88	497.40
50	357.14	2	SLE R	-178548.00	26459.30	27056.20	18.85	59.69	34.31	489.35
51	416.67	2	SLE R	-174193.00	25580.30	26157.30	15.71	62.83	33.27	474.63
52	476.19	2	SLE R	-169847.00	24398.50	24948.90	15.71	62.83	31.97	456.40
53	535.71	2	SLE R	-165510.00	22990.50	23509.10	12.57	65.97	30.49	435.70
54	595,24	2	SLE R	-161182.00	21423.00	21906.30	12.57	65.97	28,90	413.49
55	654.76	2	SLE R	-156863.00	19753.70	20199.30	6.28	72.26	27.26	390.55
56	714.29	2	SLE R	-152552.00	18031,70	18438.50	0.00	78.54	25.61	367.48
57	773.81	2	SLE R	-148250.00	16298.20	16665.80	0.00	78.54	23.99	344.69
58	833.33	2	SLE R	-143955.00	14587.20	14916.20	0.00	78.54	22.39	322.25
59	892,86	2	SLE R	-139668.00	12926.30	13217.90	0.00	78.54	20.82	300.31
60	952.38	2	SLE R	-135389.00	11337.30	11593.10	0.00	78,54	19.31	279.11
61	1011.90	2	SLE R	-131117.00	9836.78	10058.70	0.00	78.54	17.86	258.81
62	1071.43	2	SLE R	-126852.00	8436.82	8627.14	0.00	78.54	16.49	239.53
63	1130.95	2	SLE R	-122593.00	7145.61	7306.80	0.00	78.54	15.20	221.35
64	1190.48	2	SLE R	-118341.00	5967.95	6102.58	0.00	78.54	13.99	204.32
65	1250.00	2	SLE R	-114096.00	4905.B3	5016.49	0.00	78.54	12.87	188.46
66	1309.52	2	SLE R	-109857.00	3958.84	4048.14	0.00	78.54	11.83	173.76
67	1369.05	2	SLE R	-105623.00	3124.63	3195.12	0.00	78.54	10.87	160.21
68	1428.57	2	SLE R	-101396.00	2399.27	2453.40	0.00	78.54	10.00	147.76
69	1488.10	2	SLE R	-97173.40	1777.59	1817.69	0.00	78.54	9.20	136.36
70	1547.62	2	SLE R	-92956.40	1253.47	1281.75	0.00	78.54	8.47	125.94
71	1607.14	2	SLE R	-88744.30	820.07	838.57	0.00	78.54	7.81	116.45
72	1666.67	2	SLE B	-84537.00	470.07	480.67	0.00	78.54	7.22	107.80
73	1726.19	2	SLE R	-80334.20	195.81	200.23	0.00	78.54	6.67	99,92
74	1785.71	2	SLE R	-76135.70	-10.54	-10.78	0.00	78.54	6.20	92.93
75	1845.24	2	SLE R	-71941.30	+156.91	-160.45	0.00	78.54	5.96	89.29
76	1904.76	2	SLE R	-67750.80	-251.19	-256.86	0.00	78.54	5.69	85.12
.77	1964,29	2	SLE R	-63563.90	-301.24	-308,03	0.00	78.54	5.39	80.52
78	2023.81	2	SLE R	-59380.40	-314.79	-321.89	0.00	78.54	5.06	75.56
79	2083,33	2	SLE R	-55200.10	-299.46	-306.22	0.00	78.54	4.71	70.31
80	2142.86	2	SLE R	-51022.80	-262.75	-268.68	0.00	78.54	4.34	64.85
81	2202.38	2	SLE R	-46848.10	-212.03	-216.82	0.00	78.54	3.96	59.25
82	2261.90	2	SLE R	-42676.10	-154.57	-158,05	0.00	78.54	3.58	53.58
83	2321.43	2	SLE R	-38506.20	-97.53	-99,73	0.00	78.54	3.20	47.93
84	2380.95	2	SLE R	-34338.50	-48.05	-49.13	0.00	78.54	2.83	42.35
85	2440.48	2	SLE R	-30172.60	-13.19	-13.48	0.00	78,54	2.46	36.92
86	2500,00	2	SLE R	-26008.30	0.00	0.00	0.00	78.54	2.11	31.71
87	0.00	4	SLE Q	-187958.00	23843.40	24381.30	6.28	72.26	32.80	469.82

								1101	420	ie ui caic	OIO
88	59,52	4	SLE	Q	-187859,00	25462.40	26036.80	12.57	65.97	34.09	487.41
89	119.05	4	SLE	Q	-185985.00	26507.00	27105.00	15.71	62.83	34.83	497.32
90	178.57	4	SLE	Q	-184117.00	27059.20	27669.60	15.71	62.83	35.18	501.93
91	238.09	4	SLE	Q	-182255.00	27194.50	27808.00	18.85	59,69	35.19	501.73
92	297.62	4	SLE	Q	-180399.00	26982.50	27591.20	18.85	59.69	34.88	497.40
93	357.14	4	SLE	Q	-178548.00	26459.30	27056.20	18.85	59.69	34.31	489.35
94	416.67	4	SLE	Q	-174193.00	25580.30	26157.30	15.71	62.83	33.27	474.63
95	476.19	4	SLE	Q	-169847.00	24398.50	24948.90	15.71	62.83	31.97	456.40
96	535.71	4	SLE	Q	-165510.00	22990.50	23509.10	12.57	65.97	30.49	435.70
97	595.24	4	SLE	Q	-161182.00	21423.00	21906.30	12.57	65.97	28.90	413.49
-98	654.76	4	SLE	Q	-156863.00	19753.70	20199.30	6.28	72.26	27.26	390.55
99	714.29	4	SLE	Q	-152552.00	18031.70	18438.50	0.00	78.54	25,61	367.48
100	773,81	4	SLE	Q	-148250.00	16298.20	16665.80	0.00	78.54	23.99	344.69
101	833,33	4	SLE	Q	-143955.00	14587.20	14916.20	0.00	78.54	22.39	322.25
102	892.86	4	SLE	Q	-139668.00	12926.30	13217.90	0.00	78.54	20.82	300.31
103	952.38	4	SLE	Q	-135389.00	11337.30	11593.10	0.00	78.54	19.31	279.11
104	1011,90	4	SLE	Q	-131117.00	9836.78	10058,70	0.00	78.54	17.86	258.81
105	1071.43	4	SLE	Q	-126852.00	8436.82	8627.14	0.00	78.54	16.49	239.53
106	1130.95	4	SLE	Q	-122593.00	7145.61	7306.80	0.00	78.54	15,20	221.35
107	1190.48	4	SLE	Q	-118341.00	5967.95	6102.58	0.00	78,54	13.99	204,32
108	1250.00	4	SLE	Q	-114096.00	4905.B3	5016.49	0.00	78.54	12.87	188.46
109	1309.52	4	SLE	Q	-109857.00	3958.84	4048.14	0.00	78.54	11.83	173.76
110	1369.05	4	SLE	Q	-105623.00	3124.63	3195.12	0.00	78,54	10.87	160.21
111	1428.57	4	SLE	Q	-101396.00	2399.27	2453.40	0.00	78.54	10.00	147.70
112	1488.10	4	SLE	Q	-97173.40	1777.59	1817.69	0.00	78.54	9.20	136.36
113	1547.62	4	SLE	Q	-92956.40	1253.47	1281.75	0.00	78.54	8.47	125.94
114	1607.14	- 4	SLE	Q	-88744.30	820.07	838.57	0.00	78.54	7.81	116.45
115	1666.67	4	SLE	Q	-84537.00	470.07	480.67	0.00	78.54	7,22	107.80
116	1726.19	4	SLE	Q	-80334.20	195.81	200.23	0.00	78.54	6.67	99.92
117	1785.71	4	SLE	Q	-76135.70	-10.54	-10.78	0.00	78.54	6.20	92.93
118	1845.24	4	SLE	Q	-71941.30	-156.91	-160.45	0.00	78,54	5,96	89.29
119	1904.76	4	SLE	Q	-67750.80	-251.19	-256.86	0.00	78,54	5.69	85.12
120	1964.29	4	SLE	Q	-63563.90	-301.24	-308.03	0.00	78.54	5.39	80.52
121	2023.81	4	SLE	Q	-59380.40	-314.79	-321.89	0.00	78.54	5.06	75.50
122	2083.33	- 4	SIE	Q	-55200.10	-299.46	-306.22	0.00	78.54	4.71	70.33
123	2142,86	-	-	Q	-51022.80	-262,75	-268,68	0.00	78,54	4.34	64.85
124	2202.38	4	_	Q		-212.03	-216.82	0.00	78.54	3.96	59.25
125	2261.90	4	_	Q		-154.57	-158.05		78.54	3.58	53.58
126	2321.43	4	-	Q		-97.53	-99.73	0.00	78.54	3,20	47.93
127	2380.95	4	-	Q		-48.05	-49.13	0.00	78.54	2.83	42.35
_	2440.48	4		Q		-13.19	-13.48	_	78.54	2.46	36.92
_	2500.00	4	_	Q		0.00	0.00		78.54	2.11	31.71

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K ₂	Φeq	Δ _{Sm}	A ₃ <cmq></cmq>	Ac eff <emq></emq>	σ _S <dan cmq=""></dan>	€ sm	Wk <mm></mm>
90	178.57	4	SLE Q	-184117.00	27669.60	27059.20	46.00	136.36	0.50	20.00	211.44	3.14	187.61	57.42	0.02	0.01
91	238.09	4	SLE Q	-182255.00	27808.00	27194.50	46.00	136.36	0.50	20.00	156.65	6.28	203.11	62.53	0.02	0.00
92	297.62	4	SLE Q	-180399.00	27591.20	26982.50	46.00	136,36	0.50	20.00	157,45	6.28	205.61	62.81	0.02	0.00
93	357.14	4	SLE Q	-178548.00	27056,20	26459.30	45.00	136.36	0.50	20.00	216.80	3.14	196.03	58.71	0.02	0.01
94	416.67	4	SLE Q	-174193.00	26157.30	25580.30	46.00	136.36	0.50	20.00	210.93	3.14	186.81	54.05	0.02	0.01
133	178.57	3	SLE F	-184117.00	27669.60	27059.20	46.00	136.36	0.50	20.00	211.44	3.14	187.61	57.42	0.02	0.01
134	238.09	3	SLE F	-182255.00	27808.00	27194.50	46.00	136.36	0.50	20.00	156.65	6.28	203.11	62.53	0.02	0.00
135	297.62	3	SLE F	-180399.00	27591.20	26982.50	46.00	136,36	0.50	20.00	157,45	6.28	205.61	62.81	0.02	0.00
136	357.14	3	SLE F	-178548.00	27056.20	26459.30	46.00	136,36	0.50	20.00	216.80	3.14	196.03	58.71	0.02	0.01
137	416.67	3	SLE F	-174193.00	26157.30	25580.30	46.00	136.36	0.50	20.00	210.93	3.14	186.81	54.05	0.02	0.01

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
- 5	SLU N cost - min. sic.
47	C.Rare - Sf min (max compr.)
48	C.Rare - Sc min (max compr.)
49	C.Rare - Sf max (max traz.)
57	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sf min (max compr.)
91	C.Q.Per Sc min (max compr.)
92	C.Q.Per Sf max (max traz.)
93	C.Q.Per Wk Max
100	C.Q.Per Sc max (min. compr.)
136	C.Freq - Wk Max

Palo n. 21

Caratteristiche del palo e dei materiali utilizzati

R	Cf	01-	Fck	Fetk	Fod	Fetd	m.	Fyk	Fyd
<cm></cm>	<cm></cm>	CTS	<dan cmg=""></dan>	<dan cmg=""></dan>	<dan cmq=""></dan>	<dan cmq=""></dan>	тр	<dan cmg=""></dan>	<dan cmq=""></dan>

1	60.00 6.	00 030/37	307.10	20.59	174.02	13.73 B450C	4300.00	3913.0

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti.

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 21 (-154)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SIAI	RVN	287981.00	6007.07	-640.81	20770.30	-28669.60
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SLU	TOT	287981.00	6007.07	-640.81	20770.30	-28669.60
2	2	SLE R	BVN	213319.00	4449.68	-474.67	15385.40	-21236.70
	2	SLE R	TAG	į.			0.00	0.00
	2	SLE R	ECC		0. 0		0.00	0.00
	2	SLE R	TOT	213319.00	4449.68	-474.67	15385.40	-21236.70
3	. 3	SLE F	RVN	213319.00	4449.68	-474.67	15385.40	-21236.70
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	213319.00	4449.58	-474.67	15385.40	-21236,70
4	4	SLE Q	RVN	213319.00	4449.68	-474.67	15385.40	-21236.70
	4	SLE Q	TAG				0.00	0.00
	4	SIE Q	ECC				0.00	0.00
	4	SLE Q	TOT	213319.00	4449.68	-474.67	15385.40	-21236.70

Sollecitazioni nei pali

Caso CC 1		TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-287981.00	-6007.07	640.81	-20770.30	28669.60
- 2	2	SLE R	-1	-213319,00	-4449.68	474.67	-15385.40	21236,70
3	3	SLE F	1	-213319,00	-4449.68	474.67	-15385.40	21236.70
- 4	4	SLE Q	1	-213319.00	-4449.68	474.67	-15385.40	21236.70

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-287981.00	20667.70	28527.90	-287981.00	149329.00	203596.00	2+3	126.25	7.16
2	59.52	1	SIA	-287187.00	22470.30	31016.10	-287187.00	149192.00	203408.00	2+3	126.25	6.586
3	119.05	1	SIU	-283926.00	23713.00	32731.40	-283926+00	148633.00	202626.00	2-3	126.25	6.21
4	178.57	1	SIJ	-280674.00	24473.00	33780.50	-280674.00	148079.00	201839.00	2-3	126.25	6.00
5	238.09	1	SLU	-277430.00	24822.20	34262.50	-277430.00	147524.00	201050.00	2-3	126.25	5.894
6.	297.62	1	SLU	-274195.00	24826.60	34268.60	-274195.00	146969.00	200261.00	2-3	126.25	5.870
.7	357.14	1	SIU	-270969.00	24519.40	33844.50	-270969.00	146321.00	199499.00	2-3	126.25	5.920
- 8	416.67	1	SLU	-264265.00	23852.30	32923.70	-264265.00	144989.00	197830.00	2-3	126.25	6.033
9	476.19	1	SLU	-257575.00	22875,20	31575.00	-257575.00	143705.00	196070.00	2-3	126.25	6.23
10	535.71	1	SIJ	-250899.00	21662.20	29900.70	-250899.00	142415.00	194301.00	2-3	126.25	6,525
11	595.24	1	SLU	-244237.00	20278.40	27990.60	-244237.00	141116.00	192521.00	2-3	126.25	6.90
12	654.76	1	SLU	-237587.00	18780.00	25922.30	-237587.00	139814.00	190735.00	2-3	126.25	7.388
13	714.29	1	SIAJ	-230951.00	17215.30	23762.60	-230951.00	138505.00	188941.00	2-3	126.25	7.984
14	773.81	1	SLU	-224326.00	15625.20	21567,70	-224326.00	137189.00	187136.00	2-3	126.25	8.71
15	833.33	1	SLU	-217714.00	14043.60	19384.50	-217714.00	135869.00	185325.00	2-3	126.25	9.600
1.6	892.86	1	SLU	-211113.00	12498.10	17251.40	-211113.00	134543.00	183507.00	2-3	126.25	10.683
17	952,38	1	SIU	-204524.00	11011.00	15198.70	-204524.00	133210.00	181678.00	2-3	126,25	12,00
18	1011.90	1	SLU	-197946.00	9599.42	13250.20	-2571250.00	131873.00	179844.00	2-3	126.25	12,99
19	1071.43	1	SLU	-191378.00	8276.07	11423.60	-2571250.00	130530.00	178002.00	2-3	126.25	13.43
20	1130.95	1	SIJ	-184821.00	7049.93	9731.14	-2571250.00	129181.00	176151.00	2-3	126.25	13.912
21	1190.48	1	SLU	-178273.00	5926.66	8180.66	-2571250.00	127827.00	174295.00	2-3	126.25	14.423
22	1250.00	1	SLU	-171735.00	4909.10	6776.10	-2571250.00	126469.00	172431.00	2-3	126.25	14.972
23	1309.52	1	SLU	-165207.00	3997.73	5518.13	-2571250,00	125104.00	170559.00	2-3	126.25	15,564
24	1369.05	1	SIA	-158687.00	3191.10	4404.73	-2571250.00	123735.00	168681.00	2-3	126.25	16.203
25	1428,57	1	SIU	-152176.00	2486.15	3431.67	-2571250.00	122361.00	166796.00	2-3	126.25	16.89
26	1488.10	1	SIU	-145672.00	1878.54	2592.99	-2571250.00	120982.00	164904.00	2-3	126.25	17,653
27	1547.62	1	SIU	-139177.00	1362.98	1881.35	-2571250.00	119599.00	163007.00	2-3	126.25	18.47
28	1607.14	1	SLU	-132689.00	933.40	1288.39	-2571250.00	118211.00	161102.00	2-3	126.25	19.378
29	1666.67	1	SLU	-126208.00	583.19	804.99	-2571250.00	116818.00	159192.00	2-3	126.25	20.373
30	1726.19	1	SLU	-119734.00	305.39	421.54	-2571250.00	115422.00	157276.00	2-3	126.25	21.475
31	1785.71	1	SLU	-113267.00	92.80	128.09	-2571250.00	114020.00	155353.00	2-3	126.25	22.701
32	1845.24	1	SLU	-106805.00	-61.91	-85.46	-2571250.00	-112400.00	-153273.00	2-3	306.25	24.074

33	1904.76	1	SLU	-100349.00	-166.10	-229.27	-2571250.00	-110927.00	-151253.00	2-3	306.25	25,623
34	1964.29	1	SIA	-93899.00	-227.09	-313.46	-2571250.00	-109449.00	-149227.00	2-3	306.25	27.383
35	2023.81	1	SILI	-87453.60	-252.15	-348.05	-2571250,00	-107965.00	-147191.00	2-3	306.25	29.401
36	2083.33	1	SLU	-81012.90	-248.45	-342.94	-2571250.00	-106474.00	-145146.00	2-3	306.25	31,739
37	2142.86	1	SLU	-74576.60	-223.06	-307.90	-2571250.00	-104980.00	-143095.00	2-3	306.25	34.478
38	2202.38	1	SLU	-68144.30	-182.95	-252.52	-2571250.00	-103479.00	-141035.00	2-3	306.25	37.732
39	2261.90	1	SLU	-61715.60	-134.98	-186.32	-2571250.00	-101974.00	-138969.00	2-3	306.25	41,663
40	2321,43	1	SLU	-55290.20	-85.98	-118.67	-2571250.00	-100465.00	-136897.00	2-3	306.25	46.505
41	2380.95	3	SLU	-48867.80	-42.67	-58.90	-2571250.00	-98949.80	-134816.00	2-3	306.25	52.616
42	2440.48	1	SIJ	-42448.00	-11.78	-16.26	-2571250.00	-97431.30	-132730.00	2-3	306.25	60.574
43	2500.00	1	SLU	-36030.50	0.00	0.00	-2571250.00					71.363

Caso	X <cm>></cm>	œ	0.00	- Verifi Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	atg0	VRsd <dan></dan>	VRod <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	6007.07	-640.81	0.85	11.31	6041.15	1.00	32294.70	372918.00	32294.70	5,340
2	59.52	1	SIA	4297.61	-458.45	0.85	11.31	4321.99	1.00	32294.70	372805.00	32294.70	7.47
- 3	119.05	1	SIJ	2815.86	-300.38	0.85	11.31	2831.84	1.00	32294.70	372337.00	32294.70	11.40
- 4	178.57	1	SLU	1546.46	-164.97	0.85	11.31	1555.24	1.00	32294.70	371872.00	32294.70	20.765
5	238.09	1	SLU	473.42	-50.50	0.85	11.31	476.10	1.00	32294.70	371407.00	32294.70	67.83
- 6	297.62	1	SIU	-419.66	44.77	0.85	11.31	422.04	1.00	32294.70	370944.00	32294.70	76.52
7	357.14	1	SLU	-1381.23	147.34	0.85	11.31	1389.07	1.00	32294.70	370481,00	32294.70	23.24
8	416.67	1	SLU	-2378.24	253.70	0.85	11.31	2391.73	1,00	32294.70	369521.00	32294.70	13.50
9	476,19	1	SLU	-3150.92	336.13	0.85	11.31	3168.80	1.00	32294.70	368563.00	32294.70	10.193
10	535.71	1	SLU	-3725.82	397.45	0.85	11.31	3746.96	1.00	32294.70	367607.00	32294.70	8.61
11	595.24	1	SLU	-4128.22	440.38	0.85	11.31	4151.64	1,00	32294.70	366652.00	32294.70	7.77
12	654.76	1	SIU	-4381.93	467.44	0.85	11.31	4406.79	1.00	32294.70	365700.00	32294.70	7.32
13	714,29	1	SLU	-4509.12	481.01	0.85	11.31	4534.70	1.00	32294.70	364749,00	32294.70	7.123
14	773.81	1	SLU	-4530.19	483.26	0.85	11.31	4555.89	1.00	32294.70	363800.00	32294.70	7.08
15	833.33	1	SIU	-4463.76	476.17	0.85	11,31	4489.09	1.00	32294.70	362853.00	32294.70	7.19
16	892.86	1	SIJ	-4326.66	461.55	0.85	11.31	4351.21	1.00	32294.70	361908.00	32294.70	7.42
17	952.38	1	SLU	-4133.91	440.99	0.85	11.31	4157.37	1.00	32294.70	360964.00	32294.70	7.76
18	1011.90	1	SLU	-3898.84	415.91	0.85	11.31	3920.96	1.00	32294.70	360022.00	32294.70	8.23
19	1071.43	1	SLU	-3633.10	387.56	0.85	11.31	3653.71	1.00	32294.70	359081.00	32294.70	8.83
20	1130.95	1	SIJ	-3346.81	357.02	0.85	11.31	3365.80	1.00	32294.70	358142.00	32294.70	9.59
21	1190.48	1	SIJJ	-3048.65	325.22	0.85	11.31	3065.95	1.00	32294.70	357204.00	32294.70	10.53
22	1250.00	1	SLU	-2745.94	292.92	0.85	11.31	2761.52	1.00	32294.70	356267.00	32294.70	11.69
23	1309.52	1	SIJ	-2444.80	260.80	0.85	11.31	2458.67	1.00	32294.70	355332.00	32294.70	13.13
24	1369.05	1	SIAI	-2150.25	229.38	0.85	11.31	2162.45	1,00	32294.70	354398.00	32294.70	14.93
25	1428,57	1	SIAJ	-1866,36	199.09	0.85	11.31	1876.95	1.00	32294.70	353466.00	32294.70	17.20
26	1488,10	1	SLU	-1596.32	170.29	0.85	11.31	1605.38	1.00	32294.70	352534,00	32294.70	20.11
27	1547.62	1	SLU	-1342.57	143.22	0.85	11.31	1350.19	1.00	32294.70	351604.00	32294.70	23.91
28	1607.14	1	SIAI	-1106.94	118.08	0.85	11.31	1113.23	1.00	32294.70	350674.00	32294.70	29.01
29	1666.67	1	SIJ	-890.71	95.02	0.85	11.31	895.76	1.00	32294.70	349746.00	32294.70	36.05
30	1726.19	1	SIU	-694.72	74.11	0.85	11.31	698.66	1.00	32294.70	348819.00	32294.70	46.22
31	1785.71	1	SLU	-519.44	55.41	0.85	11,31	522,39	1.00	32294.70	347892.00	32294.70	61.82
32	1845,24	1	SLU	-365,10	38.95	0.85	11.31	367.18	1.00	32294.70	346967.00	32294.70	87,95
33	1904.76	1	SLU	-231.70	24.72	0.85	11.31	233.01	1,00	32294.70	346042.00	32294.70	>100
34	1964.29	1	SLU	-119.09	12.70	0.85	11.31	119.76	1.00	32294.70	345118.00	32294.70	>100
35	2023.81	-1	SIJ	-27.03	2.88	0.85	11.31	27.19	1.00	32294.70	344195.00	32294.70	>100
36	2083.33	1	SLU	44.75	-4.77	0.85	11.31	45.00	1.00	32294.70	343272.00	32294.70	>100
37	2142.86	1	SLU	96.55	-10.30	0.85	11.31	97.09	1.00	32294.70	342350.00	32294.70	>100
38	2202,38	1	SIU	128.64	-13.72	0.85	11.31	129.37	1.00	32294.70	341429.00	32294.70	>100
39	2261.90	1	SLU	141.27	-15.07	0.85	11.31	142.07	1.00	32294.70	340508.00	32294.70	>100
40	2321.43	1	SIA	134.62	-14.36	0.85	11.31	135.38	1.00	32294.70	339588.00	32294.70	>100
41	2380.95	1	SIAI	108.81	-11.61	0.85	11.31	109.42	1.00	32294.70	338668.00	32294.70	>100
42	2440.48	1	SIU	63.93	-6.82	0.85	11.31	64.29	1.00	32294.70	337748.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <amq></amq>	σ ₀ <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE F	-213319.00	21131.80	15309.40	0.00	78,54	30.85	442.36
45	59.52	2	SLE P	-213044.00	22974.90	16644.70	0.00	78.54	32.00	457.92
46	119.05	- 2	SLE F	-210819.00	24245.50	17565.20	0.00	78,54	32.63	466.17
47	178,57	2	SLE F	-208600.00	25022.60	18128.20	0.00	78.54	32.95	470.17
48	238.09	2	SLE P	-206387.00	25379.60	18386.80	0.00	78.54	33.00	470.55
49	297.62	-2	SLE F	-204181.00	25384.10	18390.10	0.00	78,54	32.82	467.90
50	357.14	2	SLE P	-201982.00	25070.00	18162.50	0.00	78.54	32.44	462.50
51	416.67	2	SLE F	-197031.00	24387.90	17668.40	0.00	78.54	31.60	450.59
52	476.19	2	SLE F	-192091.00	23388.90	16944.60	0.00	78.54	30.56	435.94
53	535,71	2	SLE F	-187161.00	22148.70	16046.10	0.00	78.54	29.37	419,24
54	595,24	2	SLE F	-182241.00	20733.70	15021.00	0.00	78.54	28.07	401.03
55	654.76	2	SLE F	-177331.00	19201.70	13911.10	0.00	78.54	26.69	381.83
56	714.29	2	SLE F	-172431.00	17601.90	12752.10	0.00	78.54	25.27	362.06
5.7	773.81	2	SLE P	-167539.00	15976.10	11574.20	0.00	78.54	23.83	342.07
58	833,33	-2	SLE F	-162657.00	14358.90	10402.60	0.00	78.54	22,40	322.17
59	892,86	2	SLE F	-157784.00	12778.80	9257.87	0.00	78.54	20.99	302.60

								Rel	azio	ne di cal	colo
- 60	952.38	2	SLE	Ŕ	-152919,00	11258.30	8156.32	0.00	78.54	19.63	283.55
61	1011.90	2	SLE !	R	-148062.00	9814.99	7110.68	0.00	78.54	18.31	265.18
62	1071.43	2	SLE	R	-143213.00	8461.92	6130.42	0.00	78.54	17.05	247.60
63	1130.95	2	SLE	R	-138371.00	7208.25	5222.17	0.00	78.54	15.85	230.88
64	1190,48	2	SLE	R	-133538.00	6059.75	4390.12	0.00	78.54	14,73	215.08
65	1250.00	2	SLE !	R	-128711.00	5019.34	3636,37	0.00	78.54	13.67	200.22
.66	1309.52	2	SLE 1	Ŕ	-123891.00	4087.51	2961.28	0.00	78.54	12,68	186.31
67	1369.05	2		R	-119078.00	3262.76	2363.78	0.00	78,54	11.76	173.33
-68	1428.57	2	_	R	-114271.00	2541.98	1841.59	0.00	78.54	10.91	161.25
69	1488.10	2	_	R	-109471.00	1920.73	1391.52	0.00	_	10.13	150.04
70		2	-	R	-104676.00	1393.59	1009.62		78.54	9.40	139.65
71	1607.14	2	_	R	-99886.80	954.36	691.41	-	78,54	8.73	130.02
72	1666.67	2	-	R	-95103.00	596.29	432,00	0.00	78.54	8.11	121.10
$\overline{}$	1726,19	-	-	R	-90324.30	312.25	226.22	-	78,54	7.54	112.82
74		2	-	R	-85550.50	94.88	68.74	0.00	78.54	7.01	105.12
_	1845,24	2	-	R	-80781.30	-63.30	-45.86		78.54	6,61	99.04
_		2	-	R	-76016.40	-169.83	-123.04	0.00	78.54	6.29	94,16
77	1964.29	2	_	R	-71255.50	-232.19	-168.22	-	78.54	5.94	88.90
78	2023.81	2	_	R	-66498.50	-257.82	-186.78	_	78.54	5.57	83.32
79	2083.33	2	_	R	-61743.10	-254.03	-184.04		78.54	5.18	77.49
80	2142.86	_	-	R	-56995.00	-228.07	-165.23	0.00	78.54	4.78	71.47
81	2202.38	2	-	R	-52247.90	-187.06	-135.52	_	78.54	4.37	65.33
82	2261.90	2	_	R	-47503.60	-138.01	-99.99		78,54	3.95	59.12
83		2	-	R	-42761.90	-87.91	-63.69	_	78.54	3.53	52.90
84	2380.95	2	-	R	-38022.50	-43.63	-31.61	-	78.54	3,12	46.74
	2440.48	_	-	R	-33285.10 -28549.50	-12.05	-8.73	-	78.54	2,71	40.69
86	2500.00	2	-	R	-213319.00		0.00	0.00		2.32	442.36
88	59.52	_	_	0	-213319.00	21131.80	16644.70		78.54	32,00	442.36
89	119.05	_	-	Q	-210819.00	24245.50	17565.20	-	78.54	32,63	466.17
90	178.57	_	_	Q	-208600.00	25022.60	18128.20	-	78.54	32.95	470.17
91	238.09	_		Q	-206387.00	25379.60	18386.80	0.00	78.54	33.00	470.55
92	297.62	_	-	O.	-204181.00	25384.10	18390.10		78.54	32.82	467.90
93	357.14	_	-	Q	-201982.00	25070.00	18162.50	-	78.54	32,44	462.50
94	416.67	_	-	Ö	-197031.00	24387.90	17668.40	0.00	78.54	31.60	450.59
95	476.19	-	-	Ó	-192091.00	23388.90	16944.60	-	78.54	30.56	435.94
96	535.71	_	-	Q	-187161.00	22148.70	16046.10		78.54	29,37	419.24
97	595,24	-	-	Ö	-182241.00	20733.70	15021.00	0.00	78.54	28.07	401.03
98	654.76	4	-	ò	-177331.00	19201.70	13911.10	0.00	78.54	26,69	381.83
99	714.29	4	-	Q	-172431.00	17601.90	12752.10	0.00	78.54	25.27	362.06
100	773.81	4	SLE	Q	-167539.00	15976.10	11574.20	0.00	78.54	23,83	342.07
101	833.33	4	SLE	Q	-162657.00	14358.90	10402.60	0.00	78.54	22,40	322,17
102	892,86	4	SLE	Q	-157784.00	12778.80	9257.87	0.00	78.54	20.99	302.60
103	952.38	4	SLE	Q	-152919.00	11258.30	8156.32	0.00	78.54	19.63	283.55
	1011.90				-148062.00		7110.68	0.00	78,54	18.31	265.18
105	1071.43	4	SLE	Q	-143213.00	8461.92	6130.42	0.00	78.54	17.05	247.60
-	1130.95	_	SLE	Q	-138371.00	7208.25	5222.17	0.00	78.54	15.85	230.88
_	1190.48	_			-133538.00				78.54	14,73	215.08
-	1250.00				-128711.00			_	78,54	13.67	
$\overline{}$	1309.52		SLE				2961.28		78.54	12.68	186.31
_	1369.05				-119078.00		2363.78		78.54		173.33
	1428.57				-114271.00		1841.59	_	78.54	10.91	161.25
					-109471.00		1391.52	-	78.54	10.13	150.04
	1547.62		SLE			1393.59	1009.62		78.54	9.40	139.65
	1607.14								78.54		
	1666.67		SLE						78.54		121.10
	1726.19		SLE						78.54		112.82
	1845.24								78.54		99.04
	1904.76		SLE				-123.04		78.54	6.29	94.16
-	1964.29		SLE			-			78.54		88.90
	2023.81		SLE				-186.78		78.54		83.32
_	2083.33		SLE				-184.04	_	78.54		77.49
$\overline{}$	2142.86		SLE				-165.23		78.54	4.78	71.47
	2202.38		SLE				-135.52	_	78.54		65.33
The second second	2261.90		SLE				-99.99	ASSESSMENT OF THE PARTY OF THE	78.54		59.12
	2321.43		SLE		-42761.90		-63.69		78.54	3,53	52.90
$\overline{}$	2380.95		SLE				-31.61		78.54		46.74
_	2440.48		SLE				-8.73		78.54	2.71	40.69
		_	_	-						-	

Verifiche principali

129 2500.00 4 SLE Q -28549.50

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
6	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
49	C.Rare - Sc max (min. compr.)

0.00

0.00 0.00 78.54

34.81

91	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr	.)
92	C.Q.Per Sc max (min. compr.)	
94	C.Q.Per Sf max (max traz.)	Т

Palo n. 22

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fetk <dan cmq=""></dan>	Fed. <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 22 (-162)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	312560.00	5856.31	-408.23	10688.80	-19675.30
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SLU	TOT	312560.00	5856.31	-408.23	10688.80	-19675.30
2	2	SLE R	RVN	231526.00	4338.00	-302.39	7917.60	-14574.30
	. 2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC				0.00	0,00
	2	SLE R	TOT	231526.00	4338.00	-302.39	7917.60	-14574.30
.3	.3	SLE F	RVN	231526.00	4338.00	-302.39	7917.60	-14574.30
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC		0 7		0.00	0.00
	3	SLE F	TOT	231526.00	4338.00	-302.39	7917.60	-14574.30
- 4	4	SLE Q	RVN	231526.00	4338.00	-302.39	7917.60	-14574.30
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00
	4	SLE Q	TOT	231526.00	4338.00	-302.39	7917.60	-14574.30

Sollecitazioni nei pali

Caso	8	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	. 1	SLU	. 1	-312560.00	-5856.31	408.23	-10688.80	19675.30
- 2	2	SLE R	1	-231526.00	-4338.00	302.39	-7917.60	14574.30
3	3	SLE F	1	-231526.00	-4338.00	302.39	-7917.60	14574.30
- 4	4	SIE Q	1	-231526.00	-4338.00	302.39	-7917.60	14574.30

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SIJ	-312560.00	10620.80	19550.20	-2571250.00	124920.00	227607.00	2-3	118.75	8.220
2	59,52	1	SIJ	-311596.00	12086.30	22247.70	-2571250.00	124781.00	227353.00	2-3	118.75	8.25
- 3	119.05	1	SLU	-307993.00	13180.20	24261.30	-2571250,00	124259.00	226406.00	2-3	118.75	B.348
4	178.57	1	SLU	-304401.00	13950.80	25679.80	-2571250.00	123739.00	225461.00	2-3	118.75	B.44
.5	238.09	1	SLU	-300818.00	14443.30	26586.40	-300818.00	123216.00	224513,00	2-3	118.75	8.46
- 6	297.62	1	SLU	-297244.00	14699.70	27058,40	-297244.00	122692.00	223564,00	2-3	118.75	8.283
7	357.14	1	SLU	-293680.00	14739.40	27131.40	-293680.00	122170.00	222617.00	2-3	118.75	8.22
8	416.67	1	SIJ	-286399.00	14524.60	26736.10	-286399.00	121093.00	220665.00	2-3	118.75	8.27
. 9	476.19	1	SLU	-279133.00	14086.40	25929.40	-279133.00	120012.00	218706.00	2-3	118.75	8.45
10	535.71	1	SLU	-271882.00	13473.20	24800.70	-271882.00	118925.00	216739.00	2-3	118.75	8.75
.11	595,24	1	SIJ	-264646.00	12728.10	23429.10	-264646.00	117832.00	214760.00	2-3	118.75	9.18
12	654.76	1	SLU	-257424.00	11888.60	21883.90	-257424.00	116735.00	212773.00	2-3	118.75	9.74
13	714.29	1	SEU	-250216.00	10987.30	20224.90	-2571250.00	115633.00	210777.00	2-3	118.75	10.27
14	773.81	1	SLU	-243021.00	10052.10	18503.30	-2571250.00	114526.00	208773.00	2-3	118.75	10.58
15	833.33	1	SIJ	-235839.00	9106.23	16762.20	-2571250.00	113415.00	206758,00	2-3	118.75	10.903
16	892,86	1	SLU	-228670.00	8169.22	15037.40	-2571250.00	112300.00	204735.00	2-3	118.75	11.24
17	952.38	-1	SLU	-221513.00	7256.84	13358.00	-2571250.00	111182.00	202706.00	2-3	118.75	11.608
18	1011.90	1	SIAI	-214368.00	6381.63	11746.90	-2571250.00	110059.00	200666.00	2+3	118.75	11.99
19	1071.43	1	SLU	-207235.00	5553.25	10222.10	-2571250.00	108931.00	198617.00	2-3	118.75	12.40
20	1130.95	1	SIU	-200113.00	4778.81	8796.57	-2571250,00	107802.00	196563.00	2-3	118.75	12.84
21	1190.48	1	SLU	-193001.00	4063.21	7479.33	-2571250.00	106668.00	194500,00	2-3	118.75	13,32
22	1250.00	1	SIA	-185900.00	3409.44	6275.91	-2571250.00	105553.00	192393.00	2-3	118.75	13.83

-	 Control of the control of the control	COLUMN TRACTOR	BASIC STREET, SPINS
Pa	lazione	di co	COLO
170	Id ZI UI IC	UI Co	ICOIO

							The state of the s					
23	1309,52	1	SLU	-178808.00	2818.89	5188.86	-2571250.00	104337.00	190177.00	2-3	118.75	14.380
24	1369.05	1	SLU	-171727.00	2291.58	4218.21	-2571250.00	103114.00	187947.00	2-3	118.75	14.973
25	1428.57	1	SIU	-164654.00	1826.41	3361.96	-2571250,00	101883.00	185702.00	2-3	118.75	15.616
26	1488.10	1	SIJ	-157590.00	1421.37	2616.38	-2571250.00	100646.00	183444.00	2-3	118.75	16,316
27	1547.62	1	SLU	-150535.00	1073.73	1976.46	-2571250.00	99402.70	181176.00	2-3	118.75	17.081
28	1607.14	116	SLU	-143488.00	780.18	1436.11	-2571250.00	98154.00	178896.00	2-3	118.75	17.920
29	1666.67	1	SIU	-136449.00	536.99	988.46	-2571250.00	96897.30	176600.00	2-3	118.75	18.844
30	1726.19	1	SIU	-129416.00	340.13	626.09	-2571250.00	95634.80	174293.00	2-3	118.75	19.868
31	1785.71	4	SLU	-122391.00	185.34	341.16	-2571250.00	94363.70	171977.00	2-3	118.75	21.008
32	1845.24	1	SIJ	-115373.00	68.24	125.61	-2571250.00	93068.90	169628.00	2-3	118.75	22.287
33	1904.76	1	SLU	-108360.00	-15.63	-28.77	-2571250.00	-91885.80	-167506.00	2-3	298.75	23.729
34	1964.29	1	SLU	-101353,00	-70.76	-130.25	-2571250+00	-90642.00	-165150.00	2-3	298.75	25.369
35	2023,81	1	SIAJ	-94352.30	-101.62	-187.05	-2571250.00	-89315.70	-162725.00	2-3	298.75	27.252
36	2083,33	1	SLU	-87356.10	-112.66	-207,38	-2571250.00	-87981.60	-160286.00	2-3	298.75	29,434
37	2142.86	1	SIU	-80364.70	-108.29	-199.33	-2571250.00	-86640.40	-157835.00	2-3	298.75	31.995
38	2202.38	1	SILI	-73377.50	-92.87	-170.95	-2571250,00	-85292.20	-155370.00	2-3	298.75	35.041
39	2261,90	1	SIU	-66394.30	-70.72	-130.1B	-2571250.00	-83936.50	-152893.00	2-3	298.75	38.727
40	2321.43	1	SLU	-59414.70	-46.12	-84.89	-2571250.00	-82571.80	-150401.00	2-3	298.75	43.276
41	2380.95	1	SLU	-52438.20	-23.31	-42.91	-2571250.00	-81200.30	-147897.00	2-3	298.75	49.034
42	2440.48	1	SIU	-45464.60	-6.53	-12.02	-2571250.00	-79821.90	-145382,00	2-3	298.75	56.555
43	2500.00	1	SLU	-38493.40	0.00	0.00	-2571250.00					66.797

Stato limite ultimo - Verifiche a taglio

Caso	X <cm></cm>	oc	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	atg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	5856.31	-408.23	0.85	11.31	5870.52	1.00	32294.70	376439.00	32294.70	5.501
- 2	59.52	1	SLU	4463.64	-311.15	0.85	11.31	4474.47	1.00	32294.70	376301.00	32294.70	7.218
- 3	119.05	1	SLU	3245.58	-226.24	0.85	11.31	3253.45	1.00	32294.70	375785.00	32294.70	9.926
4	178.57	1	SLU	2191.76	-152.78	0.85	11.31	2197.08	1.00	32294.70	375270.00	32294.70	14.699
- 5	238.09	1	SILI	1291.07	~90.00	0.85	11.31	1294.20	1.00	32294.70	374757.00	32294.70	24.953
- 6	297.62	1	SIJ	531.87	-37.08	0.85	11.31	533.16	1.00	32294.70	374245.00	32294.70	60.572
7	357.14	1	SLU	-299.84	20.90	0.85	11.31	300.57	1.00	32294.70	373735.00	32294.70	>100
8	416.67	1	SEU	-1176.46	82.01	0.85	11.31	1179.32	1.00	32294.70	372692.00	32294.70	27.384
. 9	476.19	1	SLU	-1872.46	130.53	0.85	11.31	1877.01	1.00	32294.70	371651.00	32294.70	17.205
10	535.71	1	SLU	-2407.89	167.85	0.85	11.31	2413.73	1.00	32294.70	370612.00	32294.70	13.380
11	595.24	2	SLU	-2802.05	195.33	0.85	11.31	2808.85	1.00	32294.70	369576.00	32294.70	11.498
12	654.76	1	SLU	-3073.27	214.23	0.85	11.31	3080.73	1.00	32294.70	368541.00	32294.70	10.483
13	714.29	1	SLU	-3238,79	225.77	0.85	11,31	3246.65	1.00	32294.70	367509.00	32294.70	9.947
14	773.81	1	SIM	-3314.61	231.06	0.85	11.31	3322.66	1,00	32294.70	366478.00	32294.70	9.720
15	833,33	1	SIU	-3315.44	231.11	0.85	11.31	3323.49	1.00	32294.70	365450.00	32294.70	9.717
16	892,86	1	SLU	-3254.68	226.88	0.85	11.31	3262.58	1.00	32294.70	364423.00	32294.70	9.899
17	952.38	1	SIA	-3144.39	219.19	0.85	11.31	3152.02	1.00	32294.70	363398.00	32294.70	10.246
18	1011.90	1	SILI	-2995.35	208.80	0.85	11,31	3002.61	1.00	32294.70	362374.00	32294.70	10.755
19	1071,43	1	SIU	-2817.08	196.37	0.85	11.31	2823.91	1.00	32294.70	361352.00	32294.70	11.436
20	1130.95	1	SLU	-2617.91	182.49	0.85	11.31	2624.26	1.00	32294.70	360332.00	32294.70	12.306
21	1190.48	1	SLU	-2405.05	167.65	0.85	11,31	2410.89	1.00	32294.70	359313.00	32294.70	13.395
22	1250.00	1	SLU	-2184.66	152.29	0.85	11.31	2189.97	1.00	32294.70	358296.00	32294.70	14,747
23	1309.52	1	SLU	-1961.96	136.76	0.85	11.31	1966.72	1,00	32294.70	357280.00	32294.70	16.421
24	1369.05	1	SLU	-1741.27	121.38	0.85	11.31	1745.50	1.00	32294.70	356266.00	32294.70	18.502
2.5	1428.57	1	SIJ	-1526,16	106.39	0.85	11.31	1529.86	1.00	32294.70	355253.00	32294.70	21.110
26	1488.10	1	SLU	-1319.48	91.98	0.85	11.31	1322.68	1,00	32294.70	354241.00	32294.70	24.416
27	1547.62	1	SLU	-1123.49	78.32	0.85	11.31	1126.21	1.00	32294.70	353231.00	32294.70	28.675
28	1607.14	1	SIAJ	-939.91	65.52	0.85	11.31	942.19	1.00	32294.70	352221.00	32294.70	34,276
29	1666.67	1	SLU	-770.03	53.68	0.85	11.31	771.90	1.00	32294.70	351213.00	32294.70	41.838
30	1726.19	1	SLU	-614.75	42.85	0.85	11.31	616.25	1.00	32294.70	350206.00	32294.70	52.40€
31	1785.71	1	SIU	-474.68	33.09	0.85	11.31	475.83	1.00	32294.70	349199.00	32294.70	67.870
32	1845,24	1	SIU	-350.16	24.41	0.85	11.31	351.01	1.00	32294.70	348194,00	32294.70	92.004
33	1904.76	1	SLU	-241.37	16.83	0.85	11.31	241.96	1.00	32294.70	347190.00	32294.70	>100
34	1964.29	1	SLU	-148.33	10.34	0.85	11,31	148.69	1.00	32294.70	346186.00	32294.70	>100
35	2023.81	1	SIJ	-70.96	4.95	0.85	11.31	71.13	1.00	32294.70	345183.00	32294.70	>100
36	2083.33	1	SLU	-9.15	0.64	0.85	11.31	9.17	1.00	32294.70	344181.00	32294.70	>100
37	2142.86	1	SLU	37.27	-2.60	0.85	11.31	37.37	1.00	32294.70	343179.00	32294.70	>100
38	2202.38	1	SIJJ	68.46	-4.77	0.85	11.31	68.63	1.00	32294.70	342179.00	32294.70	>100
39	2261,90	1	SLU	84.57	-5.90	0.85	11,31	B4.77	1.00	32294.70	341178.00	32294,70	>100
40	2321.43	1	SLU	85,71	-5.97	0.85	11.31	85.91	1.00	32294.70	340179.00	32294.70	>100
41	2380,95	1	SLU	71.96	-5.02	0.85	11.31	72.14	1.00	32294.70	339179.00	32294.70	>100
42	2440.48	1	SLU	43.38	-3.02	0.85	11.31	43.49	1.00	32294.70	338180.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	150 TO 15	AfC <cmq></cmq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE I	-231526.00	14481.60	7867.25	0.00	78.54	27.28	398.30
45	59.52	2	SLE I	-231125.00	16479.80	8952.79	0.00	78.54	28.41	413.82
46	119.05	2	SLE I	-228647.00	17971.30	9763.09	0.00	78.54	29.08	422.74
47	178.57	2	SLE F	3-226176.00	19022.10	10333.90	0.00	78.54	29.49	428.15
48	238.09	-2	SLE. B	-223712.00	19693.60	10698.70	0.00	78.54	29.69	430.52
49	297.62	2	SLE E	3-221255.00	20043.20	10888.70	0.00	78.54	29.69	430.33

	l	l -1		1	l				ne di cal	
II	237,14	2		-118800.00				78,54	29,00	
17	418.57 7.78.119		912 J	-010427.00 208080.00		10703.00 1048/180		78.54 78.54	28,92	418.87
*::	.:35.271		977 -	201704.00		9900213		78.54		3 -41.31
4	595,04	-	977 B	-197059.00	176:4140	9400019	0.00	78, 54	26, 18	10.914.6
7.7	1.54.76	/			16016130	890 737		78, 54	05.08	78,71,99
25	714,19	-	9 <u>- 2</u> - 2		14081.40	\$138.77		78.54	23,90	347.65
17	773.81 838.55	2	825 C	-18_387.00	13700.10 13716.30	7443.98		78,54	22.73	330.05
7.0			::	176088.00	0018230 00182	87/4.0185 80/610.07		78.54 78.54	30 . 56 30 . 29	314.18 337.78
60	980.00	-		-10.55000.00	9894.80	5777.44		78.54	19,03	091.06
6.1	1011.90	7		-100006.00	8/01.44	4757274	0.00	as. 54	78.11	756-106
52	1071,43	2	9 <u>1</u> 2	-134958.00	7571.04	4110.52	0.00	78,54	17,62	249.39
-	1100,00	2		-140000.00		3039188		78,54	15,97	234.72
-	1130.46			1777777,00		3009179		78154	14.03	
-	T0::00:00 1908::50	_	977 S		7845.80 0845.40	0028107 0028107		78154 78154	7.0.3	006036 194110
_	19.8.65			-128762.00		1697.47		78.54	10.00	131,04
	1428.07		922.0		2490.04	1302190		78,54	11,49	1761.94
	1488,10		y H	-118299.00	1938.08	1002187	0.00	78,54	10,73	109.78
76	1.07 (1.62		977 7		1464.05	790138	0.00	78154	10.03	149.61
	1607.14		977 7		1060178	697.30		78,54	9.53	140.08
	1726.19	4	977 R 977 R		4600.19 4600.77	297177 251195		785, 54 785, 54	8.77 8.70	101107 100189
$\overline{}$	1785.71	2				137.29		78,54	7,03	114.37
-	18/5.24		977 B	87.07.00	98.105	50.55		78.54	7,17	105.37
-	1904-256		977 7	81,950,000	21.31	T 158		78.54	6.57	100109
7/7	1994,09	/	977 R		-96.48	-57.4°	0.00	49, 54	6.20	94.188
	0023,91	-	977 R		-1799 Little	-1: h = 11; i		78, 54	5.90	88.25
	1083,33	2			-103.61	-20,45		78,54	5,40	E1.23
$\overline{}$	2142,85 2000,00		972 7 977 7	+61281,40	-147.68 125.63	-80.21 68.79		78.54 78.54	5,67	70.89
-	200 Lac		977 -	(03/8 4 / 40	40.73	571.39		78.54	1.76	07.3
	0321.43	7	977 B		-60° 1883	+34116		78, 54	3.79	F6476
94	01880 J 95	/	977 R	-40(6667,190)	-21.78	-17.007	0.00	78, 54	3.32	49.84
11	2440,48	-	875.0			-4.84		78.54	2,50	43.38
E 5		-	8 <u></u>		0.00	0.00		78.54	2,47	37.03
= 17	0.00	-	977 Q 977 Q	×31,349,00		70 67 436 8 460 4 79		78154 78154	37.28	890.30 415.80
33	09.02 118.05			-0×8647.000		9763.09		78.54	09.08	400.74
90	1/80.57	_		-020 T (6),000				78.54	09.49	409115
91				-120711.00				78,54	29,00	
90		_		-121250.00				78,54		
4.1		_		21.880a.00				781.54		1771.11
9.5		_		-000060.00				78.54		/1618/
96		-		-00×704.00				785, 54 785, 54		40%.34 394.33
97		-		-197359.00				78,54		
95				-102020.00				78,54		
	2000	7	977 Q	186,701,00	17961170	81.8.77		78154	33.93	
1.00		-		181,887,00				781.54		8500,395
101				-1 0 082 00 -1 0 063 00				735. 54 700 KA		014.16
100				-170789.00 -163503.00				78,54 78,54		099.46 281.08
	1011,90	_		-160225.00				78.54		250.08
_	107 .45			Tu/ 95c : 00		7113.50		78154		-04 (0.09)
	11/301/00	7	957 0	1/3899,00	8515138	3503188		78154		da4175
	1190.49	_		-144447.00		rytyw i 7g		78, 54	14,98	
	1250.00	-		-199000.00 -100000.00		0505.50		78.54 20.54		006.296 154 - 2
	1000.01 1060.00			-100985.00 -108737.00				78,54 78,54		
				10350 5.00				78.54		
	1/88/10			T18099.00		1050187		78154		1 5 5 7 78
11.7	1547.60			-100009.00		0.98106	0.700	78, 54	10.05	
	1007.14	-		-107886.00				78, 54		
	1668.07			-102688.00				78.54		
			822 0 875 0	-97495,20 97809,40		101.05		78.54 28.54		
	1785.01 1845.04		5 77 0 577 0			757559 50555		78,54 78,54		103.047
	1904.76		977 G			-11.58		78.54	6.67	100.08
	1964,19							78.54		
	1023.81	4	? К	-71608.60		-73.27		78,54	5,90	
-	2083100		977 0			63145		78154	5.43	
	217 duba 02000.09		977 Q 977 Q		-10%L68	500.00 =200.00		78154 20154		09.44 69.44
	02000.09 0200.090	_	877 O		-1006240 -96240	+681.78 +521.78		785, 54 785, 54		59.44 67.41
	. / · · 7 · ·			, su; च , घ 1,		/ 18		111. 14		

126	2321.43	4	SLE (-45817.10	-62.8B	-34,16	0.00	78.54	3.76	56.36
127	2380.95	4	SLE (2	-40667.30	-31.78	-17.27	0.00	78.54	3.32	49.84
1.28	2440.48	4	SLE (a	-35519.60	-8.90	-4.84	0.00	78.54	2.89	43.38
129	2500.00	4	SIE (-30373.90	0.00	0.00	0.00	78.54	2.47	37.03

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
7	SLU N cost - min. sic.
48	C.Rare - Sf min (max compr.)
4.9	C.Rare - Sc min (max compr.)
.86	C.Rare - Sc max (min. compr.), C.Rare - Sf max (max traz.)
91	C.Q.Per Sf min (max compr.)
92	C.Q.Per Sc min (max compr.)
129	C.Q.Per Sc max (min. compr.), C.Q.Per Sf max (max traz.

Palo n. 23

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	ê ₽	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00		1110000	

Azioni ed effetti - Plinto/Palo n. 23 (-166)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
- 1	1	SLU	RVN	325273.00	5774.99	-137.89	4780.05	-6966.63
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC		8 8		0.00	0.00
	1	SLU	TOT	325273.00	5774.99	-137.89	4780.05	-6966,63
2	2	SLE R	RVN	240943.00	4277.77	-102.14	3540.78	-5160.46
	. 2	SLE R	TAG	_			0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	240943.00	4277.77	-102.14	3540.78	-5160.46
3	3	SLE F	RVN	240943.00	4277.77	-102.14	3540.78	-5160.46
	3	SLE F	TAG		8 - 8		0.00	0.00
	3	SLE F	ECC	Ta .	6 - 0		0.00	0.00
	-3	SLE F	TOT	240943.00	4277.77	-102.14	3540.78	-5160.46
4	4	SLE Q	RVN	240943.00	4277.77	-102.14	3540.78	-5160.46
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC		0 0		0.00	0.00
	4	SLE Q	TOT	240943.DO	4277.77	-102.14	3540.78	-5160.46

Sollecitazioni nei pali

Caso	8	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	. 1	-325273,00	-5774.99	137,89	-4780.05	6966.63
- 2	2	SLE R	1	-240943.00	-4277.77	102.14	-3540.78	5160.46
3	3	SLE F	1	-240943.00	-4277.77	102.14	-3540.78	5160.46
4	4	SLE Q	1	-240943.00	-4277.77	102.14	-3540.78	5160.46

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-325273.00	4718.47	6876.88	-2571250,00	148613.00	217313.00	2-3	124.38	7.905
- 2	59.52	1	SIU	-324221.00	6481.42	9446.27	-2571250.00	148441.00	217070.00	2-3	124.38	7.931
- 3	119.05	1	SIU	-320442.00	7906.39	11523.10	-2571250.00	147821.00	216196.00	2-3	124.3B	8.024
4	178.57	1	SLU	-316674.00	9032.49	13164.30	-2571250.00	147185.00	215322.00	2-3	124.38	8.120
5	238.09	1	SIU	-312915.00	9896.97	14424.20	-2571250.00	146544.00	214450.00	2-3	124.38	8,217
- 5	297.62	1	SLU	-309166.00	10535.00	15354.10	-2571250.00	145902.00	213578.00	2-3	124.3B	8.317
7	357.14	- 1	SLU	-305427.00	10960.10	15973.60	-2571250.00	145259.00	212704.00	2-3	124.38	8.419
8	416.67	1	SIJJ	-297848.00	11128.70	16219.40	-2571250.00	143949.00	210926.00	2-3	124.38	8.633
	476.19	1	SIAI	-290284.00	11065.70	16127.60	-2571250.00	145043.00	207487.00	2-3	125.00	8.858
10	535.71	1	SLU	-282736.00	10814.20	15761.00	-2571250.00	143725.00	205677.00	2-3	125.00	9.094
11	595.24	1	SIU	-275203.00	10413.10	15176.50	-2571250,00	140244.00	205149.00	2-3	124.38	9.343

12	654.76	1	SLU	-267685.00	9896.94	14424.20	-2571250.00	one di ca 139033.00		2-3	124.38	9.606
13	714.29	1	SLU	-2601B1.00	9296.07	13548.40	-2571250.00	137816.00	201149.00	2-3	124.38	9,883
14	773.81	1	SIJ	-252691.00	8636.94	12587.80	-2571250,00	136595.00	199129.00	2-3	124.38	10.175
15	833.33	1	SIJ	-245214.00	7942.30	11575.40	-2571250.00	135195.00	197142.00	2-3	124.38	10,486
16	892.86	1	SLU	-237751.00	7231.43	10539.40	-2571250.00	133751.00	195135.00	2-3	124.38	10,815
17	952.38	1	SLU	-230301.00	6520.49	9503.21	-2571250.00	132309.00	193102.00	2-3	124.38	11.165
18	1011.90	1	SIJJ	-222863.00	5822.73	8486.26	-2571250.00	130857.00	191055.00	2-3	124.38	11.537
19	1071.43	1	SLU	-215437.00	5148.79	7504.05	-2571250.00	129397.00	188998.00	2-3	124.38	11,935
20	1130.95	4	SLU	-208022.00	4507.04	6568.74	-2571250.00	127931.00	186933.00	2-3	124.38	12.361
21	1190.48	1	SIJJ	-200618.00	3903.76	5689.49	-2571250.00	126457.00	184856.00	2-3	124.38	12.817
22	1250.00	1	SLU	-193226.00	3343.44	4872.86	-2571250.00	124973.00	182767.00	2-3	124.38	13.307
23	1309.52	1	SLU	-185844.00	2829.03	4123.14	-2571250+00	123482.00	180670.00	2-3	124.38	13.836
24	1369.05	1	SIAJ	-178471.00	2362.15	3442.68	-2571250.00	121985.00	178563.00	2-3	124.38	14.407
25	1428.57	1	SLU	-171108.00	1943.26	2832.19	-2571250.00	120480.00	176446.00	2-3	124.38	15.027
26	1488.10	1	SLU	-163755.00	1571.93	2290.99	-2571250.00	118967.00	174318.00	2-3	124.38	15.702
27	1547.62	1	SILI	-156410.00	1246.92	1817.31	-2571250,00	119396.00	170811.00	2-3	125.00	16.439
-28	1607.14	1	SIJ	-149074.00	966.38	1408.43	-2571250.00	117862.00	168672.00	2-3	125.00	17,248
29	1666.67	1	SLU	-141745.00	727.95	1060.94	-2571250.00	116321.00	166523.00	2-3	125.00	18.140
30	1726.19	1	SLU	-134424.00	528.91	770.85	-2571250.00	114774.00	164365.00	2-3	125.00	19,128
31	1785,71	1	SLU	-127111.00	366.22	533.75	-2571250.00	113221.00	162199.00	2-3	125.00	20.228
32	1845,24	1	SLU	-119804.00	236.66	344.92	-2571250.00	111663.00	160026.00	2-3	125.00	21.462
33	1904.76	1	SIJJ	-112504.00	136,85	199,45	-2571250.00	110097.00	157843.00	2-3	125.00	22,855
34	1964.29	1	SIU	-105209.00	63.31	92.27	-2571250.00	108672.00	155468.00	2-3	125.00	24.439
35	2023.81	1	SLU	-97920.50	12.52	18,24	-2571250.00	105567.00	154155.00	2-3	124.38	26.259
36	2083.33	1	SIU	-90637.00	-19.08	-27.81	-2571250,00	-103642.00	-151818.00	2-3	304.38	28.369
37	2142,86	1	SIJ	-83358.50	-35,04	-51.07	-2571250.00	-101991.00	-149495.00	2-3	304.38	30.846
38	2202.38	1	SLU	-76084.40	-38.90	-56.70	-2571250.00	-102007.00	-145977,00	2-3	305.00	33.795
39	2261.90	1	SLU	-68814.30	-34.21	-49.86	-2571250.00	-100328.00	-143640.00	2-3	305.00	37.365
40	2321.43	1	SIJ	-61548.00	-24.48	-35.67	-2571250.00	-98642.60	-141296.00	2-3	305.00	41.776
41	2380.95	1	SLU	-54285.00	-13,20	-19.24	-2571250,00	-96949.40	-138943.00	2-3	305,00	47,366
42	2440.48	1	SLU	-47024.80	-3.88	-5.66	-2571250.00	-95247.00	-136581.00	2-3	305.00	54.678
43	2500.00	- 1	SIU	-39767,20	0.00	0.00	-2571250,00					64.657

Caso	X <cm>></cm>	cc	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	-1	SLU	5774.99	-137.89	0.85	11.31	5776.64	1.00	32294.70	378260.00	32294.70	5.59
.2	59.52	1	SLU	4712.07	-112.51	0.85	11.31	4713.41	1.00	32294.70	378109.00	32294.70	6.85
3	119.05	1	SIM	3767.63	-89.96	0.85	11.31	3768.70	1,00	32294.70	377568.00	32294.70	8.56
4	178,57	1	SIN	2936.67	-70.12	0.85	11.31	2937.50	1.00	32294.70	377028.00	32294.70	10.99
.5	238.09	1	SLU	2213.30	-52.85	0.85	11.31	2213.94	1.00	32294.70	376490.00	32294.70	14.58
- 6	297.62	1	SIU	1590.97	-37.99	0.85	11.31	1591.43	1.00	32294.70	375953.00	32294.70	20.29
7	357.14	1	SILI	890.63	-21.27	0.85	11.31	890.89	1.00	32294.70	375417.00	32294.70	36.25
8	416.67	1	SIJ	134.26	-3.21	0.85	11.31	134.30	1.00	32294.70	374332.00	32294.70	>100
9	476.19	1	SIU	-487.15	11.63	0.85	11.31	487.29	1.00	32294.70	373248.00	32294.70	66.27
10	535.71	1	SLU	-986.76	23.56	0.85	11,31	987.04	1.00	32294.70	372167.00	32294.70	32,71
11	595,24	1	SLU	-1377.54	32.89	0.85	11.31	1377.93	1.00	32294.70	371088.00	32294.70	23.43
12	654.76	1	SLU	-1672.06	39.92	0.85	11.31	1672.54	1.00	32294.70	370011.00	32294.70	19.30
13	714.29	1	SLU	-1882.35	44.94	0.85	11.31	1882.89	1.00	32294.70	368936.00	32294.70	17.15
14	773.81	-1	SIJJ	-2019.77	48.23	0.85	11.31	2020.35	1.00	32294.70	367863.00	32294.70	15.98
15	833.33	1	SLU	-2094.93	50.02	0.85	11.31	2095.52	1,00	32294.70	366792.00	32294.70	15.41
16	892.86	1	SLU	-2117.62	50.56	0.85	11.31	2118.23	1.00	32294.70	365723.00	32294.70	15.24
17	952,38	1	SIU	-2096,83	50.07	0.85	11.31	2097.43	1.00	32294.70	364656.00	32294.70	15.39
18	1011.90	1	SLU	-2040.68	48.72	0.85	11.31	2041.26	1.00	32294.70	363591.00	32294.70	15.B2
19	1071.43	1	SLU	-1956.46	46.71	0.85	11.31	1957.02	1.00	32294.70	362527.00	32294.70	16.50
20	1130.95	1	SIU	-1850.65	44.19	0.85	11.31	1851.17	1.00	32294.70	361465.00	32294.70	17.44
21	1190.48	1	SIU	-1728.95	41.28	0.85	11.31	1729.44	1.00	32294.70	360405.00	32294.70	18.67
22	1250.00	1	SLU	-1596.32	38.11	0.85	11.31	1596.77	1.00	32294.70	359346.00	32294.70	20.22
23	1309.52	1	SLU	-1457.03	34.79	0.85	11,31	1457,45	1.00	32294.70	358288.00	32294.70	22,15
24	1369.05	1	SIU	-1314.74	31.39	0.85	11.31	1315.11	1.00	32294.70	357232.00	32294.70	24.55
25	1428.57	1	SLU	-1172.48	27.99	0.85	11.31	1172.82	1.00	32294.70	356178.00	32294.70	27.53
26	1488.10	1	SLU	-1032.81	24.66	0.85	11.31	1033.10	1.00	32294.70	355124.00	32294.70	31.26
27	1547.62	1	SIJ	-897.77	21.44	0.85	11.31	898.03	1.00	32294.70	354072.00	32294.70	35.96
28	1607.14	1	SLU	-769.04	18.36	0.85	11.31	769.26	1,00	32294.70	353021.00	32294,70	41.98
29	1666.67	1	SLU	-647.90	15.47	0.85	11.31	648.09	1.00	32294.70	351972.00	32294.70	49.83
30	1726.19	1	SIJ	-535.36	12.78	0.85	11.31	535.51	1.00	32294.70	350923.00	32294.70	60.30
31	1785.71	1	SLU	-432.13	10.32	0.85	11.31	432.26	1.00	32294.70	349875.00	32294.70	74.71
32	1845.24	1	SIU	-338.76	8.09	0.85	11.31	338.85	1.00	32294.70	348829.00	32294.70	95.30
33	1904.76	1	SIU	-255.57	6.10	0.85	11.31	255.64	1.00	32294.70	347783.00	32294.70	>100
34	1964,29	1	SIU	-182.79	4.36	0.85	11.31	182.84	1.00	32294.70	34673B.00	32294.70	>100
35	2023.81	1	SLU	-120.53	2.88	0.85	11.31	120.57	1.00	32294.70	345694.00	32294.70	>100
36	2083,33	1	SLU	-68.83	1.64	0.85	11.31	68.85	1.00	32294.70	344651.00	32294.70	>100
37	2142.86	1	SIAI	-27.67	0.66	0.85	11.31	27.68	1,00	32294.70	34360B.00	32294.70	>100
38	2202.38	1	SLU	2,97	-0.07	0.85	11.31	2.97	1,00	32294.70	342566.00	32294.70	>100
39	2261.90	1	SIU	23,15	-0.55	0.85	11.31	23.16	1.00	32294.70	341525.00	32294.70	>100
40	2321.43	1	SLU	32,91	-0.79	0.85	11.31	32.92	1.00	32294.70	340484,00	32294.70	>100
41	2380.95	1	SIAI	32,30	-0.77	0.85	11.31	32,30	1.00	32294.70	339444.00	32294.70	>100

Veri	fiche st	ato	limit	e d'eserci	zio					
Caso	x	cc	TCC	N	Mz	My	AfT	AfC	σ _C	o _f
	<cm>></cm>	-		<dan></dan>	<danm></danm>	<danm></danm>	<cmq></cmq>	<cmq></cmq>	<dan cmq=""></dan>	
44		2	SLE R		5093.98	3495,16	0.00	78.54	22.78	337.04
45		2	SLE R	-240477.00	6997.24	4801.05	0.00	78.54	23.94	352.64
46	_	_	SLE R		8535.62	5856.59		78.54	24,69	362.53
47	178.57	2	SLE R	-235267.00	9751.33	6690.73	0.00	78.54	25.24	369.69
48		-	SLE R		10684.60	7331.09	0.00	78.54	25.62	374.45
49	-	2	SLE R		11373.40	7803.69	0.00	78.54	25.84	377.15
50	357,14	-	SLE R	-227506.00	11832.30	8118.58	0.00	78.54	25.92	377.91
51	416.67	2	SLE R		12014.40	8243.51 8196.81	0.00	78.54	25.58	372.63
53		2	SLE R		11674.80	8010.52	-	78.54	25.08	365.24 356.13
54	-	2	SLE R		11241.80	7713.42	0.00	78.54	23.73	345.67
55		-	SLE R		10684.60	7331.07	0.00	78.54	22.93	334.16
56	714.29	-	SLE R		10035.90	6885.98	0.00	78.54	22.07	321.89
57	773.81	2	SLE R	-188550.00	9324.30	6397.73	_	78.54	21.18	309.10
58	and the second second	-	SLE R		8574.38	5883.18	0.00	78.54	20,26	296.00
59	-	-	SLE R		7806.94			78.54	19.33	282.76
60	_	-	SLE R		7039.42	4829.99		78.54	18.40	269.53
- 61	1011,90	2	SLE R		6286.12	4313.13	0.00	78.54	17.48	256.43
62	1071.43	2	SLE R		5558.56	3813.92	0.00	78.54	16,58	243.56
63	-	2	SLE R	-	4865.73	3338.55	0.00	78.54	15.70	231.00
64	_	2	SLE B		4214.44		_	78.54	14,84	218.80
65	1250.00	- 2	SLE R	-144630.00	3609.53	2476.62	0.00	78.54	14.02	207.00
66	1309.52	2	SLE R	-139178.00	3054.18	2095.58	0.00	78.54	13.23	195.64
67	1369.05	2	SLE R	-133733.00	2550.14	1749.74	0.00	78.54	12.47	184.72
-68	1428.57	2	SLE B	-128296.00	2097.92	1439.45	0.00	78.54	11.74	174.25
69	1488.10	2	SLE R	-122865.00	1697.03	1164.39	0.00	78,54	11.05	164.22
70	1547.62	2	SLE B	-117441.00	1346,15	923.64	0.00	78.54	10.39	154.62
71	1607.14	2	SLE R	-112023.00	1043.28	715.83	0.00	78.54	9.76	145.45
72	1666,67	2	SLE R	-106612.00	785.88	539.22	0.00	78.54	9,16	136.66
73	1726.19	2	SLE R	-101206.00	571.00	391.78	0.00	78.54	8.58	128.25
74	1785.71	2	SLE B	-95805.30	395.37	271.27	0.00	78.54	8.04	120.17
75	1845.24	2	SLE R	-90409.90	255.50	175.31	0.00	78.54	7.51	112,40
76	1904.76	2	SLE R	-85019.40	147.74	101.37	0.00	78.54	7.00	104.92
77	1964.29	2	SLE R	-79633.50	68.35	46.90	0.00	78.54	6.52	97.67
78	2023.81	2	SLE R	-74251.80	13.51	9.27	0.00	78.54	6.04	90.65
7.9	2083.33	2	SLE R	-68874.10	-20.60	-14.13	0.00	78.54	5,61	84.15
80	2142.86	2	SLE R	-63500.10	-37.83	-25.95	0.00	78.54	5.19	77.74
81	2202.38	2	SLE R	-58129,50	-42.00	-28.82	0.00	78.54	4.75	71.23
82	2261.90	2	SLE R		-36.93	-25.34	0.00	78.54	4,31	64.64
83	-	_	SLE R				0.00		3,87	58.01
	2380.95	_	_	+42035.20						
_	2440.48	-	_	-36675.30			0.00			
	2500.00	-		-31317.50			0.00			
87		-	_	-240943.00			_	-		
88				-240477.00						
89				-237868.00						
90	_			-235267.00				78.54		
91	_			-232673.00						374.45
92	Training the second			-230086.00				78.54		
93	-			-227506.00 -221907.00						
95		-		-216320.00						
96	-	_		-210744.00						
-97		_		-205179.00						
98		-	_	-199626.00		_	_	78.54		
99		-		-194083.00				78.54		
	773.81			-188550.00						
101				-183028.00						
_	892.86			-177515.00						
				-172012.00						
	1011.90			-166518.00				78.54		
	1071,43			-161034.00						
	1130.95			-155557.00						
	1190.48			-150090.00						
_	1250.00			-144630.00						
	1309.52			-139178.00						
	1369.05			-133733.00						
	1428.57			-128296.00						
	1488.10	_		-122865.00						
113	1547.62	_	-	-117441.00			-	78.54		
114	1607,14			-112023.00				78.54		

						relazione di calcolo							
116	1726.19	4	SLE	Q	-101206.00	571.00	391.78	0.00	78.54	8.58	128.25		
117	1785.71	4	SLE	Q	-95805.30	395.37	271.27	0.00	78.54	8.04	120.17		
118	1845.24	4	SLE	Q	~90409.90	255.50	175.31	0.00	78.54	7.51	112.40		
119	1904.76	4	SLE	Q	-85019.40	147.74	101.37	0.00	78.54	7,00	104.92		
120	1964.29	4	SLE	Q	-79633.50	68.35	46.90	0.00	78.54	6.52	97.67		
121	2023.81	4	SLE	0	-74251.80	13.51	9.27	0.00	78.54	6.04	90.65		
122	2083.33	4	SLE	Q	-68874.10	-20.60	-14.13	0.00	78.54	5.61	84.15		
123	2142,86	4	SLE	Q	-63500.10	-37.83	-25.95	0.00	78.54	5.19	77.74		
124	2202.38	4	SLE	Q	-58129.50	-42.00	-28.82	0.00	78.54	4.75	71.23		
125	2261.90	4	SLE	Q	-52762.00	-36.93	-25.34	0.00	78.54	4.31	64.64		
126	2321.43	4	SLE	Q	-47397.30	-26.42	-18.13	0.00	78.54	3,87	58.01		
127	2380.95	4	SLE	Q	-42035.20	-14.25	-9.78	0.00	78.54	3.43	51.37		
128	2440.48	4	SLE	Q	-36675.30	-4.19	-2.88	0.00	78.54	2.98	44.75		
129	2500.00	4	SLE	Q	-31317.50	0.00	0.00	0.00	78.54	2,55	38.18		

Verifiche principali

Caso	Tipo											
1	SLU N cost - min. sic., SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio											
50	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)											
86	C.Rare - Sc max (min. compr.), C.Rare - Sf max (max traz.)											
93	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)											
129	C.Q.Per Sc max (min. compr.), C.Q.Per Sf max (max traz.)											

Palo n. 24

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
50.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 24 (-167)

Caso	oc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	BVN	325212.00	5775.78	139.45	4784.90	7112.64
	. 1	SLU	TAG	_			0.00	0.00
	1	SIAI	ECC				0.00	0.00
	1	SLU	TOT	325212.00	5775.78	139.45	4784.90	7112.64
2	2	SLE R	RVN	240898.00	4278.35	103.30	3544.37	5268,62
	2	SLE R	TAG		8 - 8		0.00	0.00
	2	SLE R	ECC	8	a 5		0.00	0.00
	2	SLE R	TOT	240898.00	4278.35	103.30	3544.37	5268.62
- 3	3	SLE F	RVN	240898.00	4278.35	103.30	3544.37	5268.62
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC		0 0		0.00	0.00
	3	SLE F	TOT	240898.00	4278.35	103.30	3544.37	5268.62
4	4	SLE Q	RVN	240898.00	4278.35	103.30	3544.37	5268.62
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00
	4	SLE Q	TOT	240898.00	4278.35	103.30	3544.37	5268.62

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>	
- 1	1	SIA	1	-325212.00	-5775.78	-139,45	-4784.90	-7112.64	
2	2	SLE R	1	-240898.00	-4278.35	-103.30	-3544.37	-5268,62	
- 3	3	SLE F	1	-240898.00	-4278.35	-103,30	-3544.37	-5268.62	
4	4	SLE Q	1	-240898.00	-4278.35	-103,30	-3544.37	-5268.62	

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SIU	-325212.00	4723.98	+7022.09	-2571250.00	146611.00	-218744.00	2-3	236.25	7.906
- 2	59.52	1	SLU	-324159.00	6463.07	~9607.19	-2571250.00	146433.00	-218489.00	2-3	236.25	7.932
3	119.05	1	SLU	-320382.00	7867.81	-11695.30	-2571250.00	145794.00	-217576.00	2-3	236.25	8.026
4	178,57	1	SIU	-316614.00	8976.95	-13344.00	-2571250.00	145150.00	-216656.00	2-3	236.25	8.121

-	 ************************************	COLUMN TRACTOR	Participation of the
Pa	lazione	al co	ICOLO
1/6	Id ZI UI IC	ui ca	UUUU

			Relazione di calcolo												
5	238.09	1	SLU	-312856.00	9827,38	-14608.20	-2571250.00	144507.00	-215739.00	2-3	236.25	8.219			
- 6	297.62	1	SLU	-309108.00	10453.90	-15539.50	-2571250.00	143863.00	-214820.00	2-3	236.25	8.318			
7	357.14	1	SIU	-305370.00	10870.00	-16158.00	-2571250.00	143217.00	-213899.00	2-3	236.25	8.420			
8	416.67	1	SIU	-297792.00	11032.70	-16399.90	-2571250.00	141901.00	-212023.00	2-3	236.25	8,634			
9	476.19	1	SLU	-290230.00	10966.50	-16301.50	-2571250.00	140578.00	-210138.00	2-3	236.25	8.859			
10	535.71	1	SLU	-282683.00	10714.30	-15926.50	-2571250.00	139244.00	-208241.00	2-3	236.25	9.096			
11	595,24	1	SIU	-275151.00	10314.30	-15332.00	-2571250.00	137903.00	-206335.00	2-3	236.25	9.345			
12	654.76	ĭ	SIU	-267635.00	9800.89	-14568.80	-2571250.00	136556.00	-204421.00	2-3	236.25	9.607			
13	714.29	3	SLU	-260132.00	9203.99	-13681.50	-2571250.00	135201.00	-202498.00	2-3	236.25	9.884			
14	773.81	1	SIJ	-252644.00	8549.77	-12709.00	-2571250.00	133837.00	-200563.00	2-3	236.25	10.177			
15	833.33	1	SLU	-245169.00	7860.72	-11684.80	-2571250.00	132467.00	-198621.00	2-3	236.25	10.488			
1.6	892.86	1	SLU	-237707.00	7155.89	-10637.10	-2571250.00	131091.00	-196672.00	2-3	236.25	10.817			
1.7	952.38	1	SIU	-230258.00	6451.25	-9589.62	-2571250.00	129707.00	-194713.00	2-3	236.25	11.167			
18	1011.90	1	SLU	-222821.00	5759.87	-8561,90	-2571250.00	128315.00	-192745.00	2-3	236.25	11.540			
19	1071.43	1	SLU	-215397.00	5092.28	-7569.55	-2571250.00	126919.00	-190770.00	2-3	236.25	11.937			
20	1130.95	1	SIU	-207983.00	4456.72	-6624.81	-2571250.00	125561.00	-188729.00	2-3	236.25	12.363			
-21	1190,48	1	SIJ	-200581,00	3859.39	-5736.89	-2571250.00	124297.00	-186541.00	2-3	236.25	12.819			
22	1250,00	1	SLU	-193190.00	3304.71	-4912.37	-2571250.00	123031.00	-184341.00	2-3	236.25	13.309			
23	1309.52	1	SLU	-185809.00	2795.58	-4155.56	-2571250.00	121761.00	-182129.00	2-3	236.25	13.838			
24	1369.05	1	SLU	-178438.00	2333.57	-3468.79	-2571250.00	120487.00	-179905.00	2-3	236.25	14,410			
25	1428.57	1	SLU	-171077.00	1919.14	-2852.76	-2571250.00	119212.00	-177665.00	2-3	236.25	15.030			
26	1488.10	1	SIJJ	-163725.00	1551.84	-2306.77	-2571250.00	117891.00	-175423.00	2-3	236.25	15.705			
27	1547.62	1	SIJJ	-156381.00	1230.42	-1829.00	-2571250.00	116524.00	-173182.00	2-3	236.25	16.442			
28	1607.14	1	SLU	-149046.00	953.05	-1416.69	-2571250.00	114944.00	-170985.00	2-3	236.25	17.251			
29	1666.67	1	SIU	-141719.00	717.39	-1066.38	-2571250.00	113353.00	-168774.00	2-3	236.25	18.143			
30	1726.19	1	SLU	-134400.00	520.71	-774.03	-2571250.00	111752.00	-166551.00	2-3	236.25	19.131			
31	1785.71	1	SLU	-127088.00	360.03	-535.18	-2571250.00	110142.00	-164318.00	2-3	236.25	20.232			
32	1845.24	1	SEU	-119782.00	232.13	-345.05	-2571250.00	108524.00	-162075.00	2-3	236.25	21.466			
33	1904.76	1	SIJ	-112483.00	133.66	-198.68	-2571250.00	106895.00	-159821.00	2-3	236.25	22.859			
34	1964.29	1	SLU	-105190.00	61.18	-90.94	-2571250.00	105254.00	-157557.00	2-3	236.25	24.444			
35	2023.81	1	SLU	-97903,10	11.19	-16.63	-2571250.00	103604.00	-155283.00	2-3	236.25	26.263			
36	2083,33	1	SLU	-90621.10	-19.82	29.47	-2571250,00	-102482.00	152802.00	2-3	56.25	28.374			
37	2142.86	1	SIJJ	-83343.90	-35.38	52,60	-2571250.00	-101096.00	150336.00	2-3	56.25	30.851			
38	2202.38	1	SLU	-76071.20	-39.00	57.98	-2571250.00	-99644.60	147876.00	2-3	56.25	33.B00			
39	2261.90	1	SLU	-68802,60	-34.19	50.82	-2571250.00	-97969.20	145470.00	2-3	56.25	37.371			
40	2321.43	1	SLU	-61537.60	-24,41	36.29	-2571250.00	-96282.00	143051.00	2-3	56.25	41,783			
41	2380.95	1	SLU	-54276.00	-13.15	19.55	-2571250.00	-94583.40	140622.00	2-3	56.25	47.374			
42	2440.48	1	SILI	-47017.30	-3.86	5.74	-2571250.00	-92870.00	138179.00	2-3	56.25	54,687			
43	2500.00	1	SIJ	-39761.00	0.00	0.00	-2571250.00	6	B 8		1 1	64.668			

Stato limite ultimo - Verifiche a taglio

Caso	X <cm></cm>	oc	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIJ	5775.78	139.45	0.85	11,31	5777.46	1,00	32294.70	378251,00	32294.70	5.590
2	59.52	1	SIU	4709.91	113.72	0.85	11.31	4711.29	1.00	32294.70	378100.00	32294.70	6.855
3	119.05	1	SLU	3763.03	90.86	0.85	11.31	3764.13	1.00	32294.70	377559.00	32294,70	8.580
4	178.57	1	SLU	2930.09	70.75	0.85	11.31	2930.94	1.00	32294.70	377020.00	32294.70	11.019
5	238.09	1	SLU	2205.14	53.24	0.85	11.31	2205.78	1.00	32294.70	376481.00	32294.70	14,641
.6	297.62	1	SLU	1581.59	38.19	0.85	11.31	1582.05	1.00	32294.70	375945.00	32294.70	20.413
7	357.14	1	SIJ	880.07	21.25	0.85	11.31	880.33	1.00	32294.70	375409.00	32294.70	36.685
8	416.67	1	SIJ	122.63	2.96	0.85	11.31	122.66	1.00	32294.70	374324.00	32294.70	>100
.9	476,19	1	SIAJ	-499.45	-12.06	0.85	11.31	499.60	1,00	32294.70	373240.00	32294,70	64.642
1.0	535.71	1	SIAJ	-999,39	-24.13	0.85	11.31	999.68	1.00	32294.70	372159.00	32294.70	32.305
11	595.24	1	SLU	-1390.20	-33.57	0.85	11.31	1390.61	1,00	32294.70	371081.00	32294.70	23.224
12	654.76	1	SLU	-1684.52	-40.67	0.85	11.31	1685.01	1.00	32294.70	370004.00	32294.70	19.166
13	714.29	1	SIJJ	-1894.42	-45.74	0.85	11.31	1894.97	1.00	32294.70	368929.00	32294,70	17.042
14	773.81	1	SIJ	~2031.29	-49.04	0.85	11,31	2031.88	1.00	32294.70	367857.00	32294.70	15.894
15	833.33	1	SLU	-2105.79	-50.84	0.85	11.31	2106.40	1.00	32294.70	366786.00	32294,70	15.332
16	892.86	1	SLU	-2127.74	-51.37	0.85	11.31	2128.36	1.00	32294.70	365717.00	32294.70	15.174
17	952.38	1	SILI	-2106.16	-50.85	0.85	11.31	2106.77	1.00	32294.70	364650.00	32294.70	15.329
18	1011.90	1	SLU	-2049.18	-49.48	0.85	11.31	2049.77	1.00	32294.70	363585.00	32294.70	15.755
19	1071.43	1	SLU	-1964.12	-47.42	0.85	11.31	1964.69	1.00	32294.70	362521.00	32294.70	16.438
20	1130.95	1	SIJ	-1857.48	-44.85	0.85	11.31	1858.02	1.00	32294.70	361460.00	32294.70	17.381
21	1190.48	1	SLU	-1734.97	-41.89	0.85	11.31	1735.47	1.00	32294.70	360399.00	32294.70	18,609
22	1250.00	1	SLU	-1601.56	-38.67	0.85	11.31	1602.02	1.00	32294.70	359341.00	32294,70	20.159
23	1309.52	1	SIA	-1461.53	-35.29	0.85	11.31	1461.96	1,00	32294.70	358283.00	32294.70	22,090
24	1369.05	1	SLU	-1318.54	-31.84	0.85	11.31	1318.92	1.00	32294.70	357227.00	32294.70	24.486
25	1428.57	1	SLU	-1175.64	-28.39	0.85	11.31	1175.98	1.00	32294.70	356173.00	32294.70	27.462
26	1488.10	1	SLU	-1035,36	-25.00	0.85	11.31	1035,66	1.00	32294,70	355120.00	32294.70	31.183
27	1547.62	1	SLU	-899.7B	-21,73	0.85	11.31	900.05	1,00	32294.70	354068.00	32294,70	35.881
28	1607.14	1	SLU	-770.56	-18.61	0.85	11.31	770.79	1.00	32294.70	353017.00	32294,70	41.898
29	1666,67	1	SLU	-648.99	-15.67	0.85	11.31	649.18	1.00	32294.70	351968.00	32294.70	49.747
30	1726.19	1	SIAI	-536.07	-12.94	0.85	11.31	536.22	1.00	32294.70	350919.00	32294.70	60.226
31	1785.71	1	SLU	-432.52	-10.44	0.85	11.31	432.64	1.00	32294.70	349872.00	32294.70	74.645
32	1845.24	1	SIU	-338,86	-8.18	0.85	11.31	338.96	1.00	32294.70	348826.00	32294.70	95.276
33	1904.76	1	SLU	-255.45	-6.17	0.85	11,31	255.52	1,00	32294.70	347780.00	32294,70	>100
34	1964.29	1	SIA	-182.49	-4.41	0.85	11.31	182.54	1.00	32294.70	346736.00	32294.70	>100

35	2023.81	1	SLU	-120.09	-2.90	0.85	11.31	120.13	1.00	32294.70	345692.00	32294,70	>100
36	2083,33	1	SLU	-68.30	-1.65	0.85	11.31	68.32	1.00	32294.70	344649.00	32294.70	>100
37	2142.86	1	SIU	-27.10	-0.65	0.85	11.31	27.10	1,00	32294.70	343606.00	32294.70	>100
38	2202.38	1	SIU	3.55	0.09	0.85	11.31	3.55	1.00	32294.70	342564.00	32294.70	>100
39	2261.90	1	SLU	23.70	0.57	0.85	11,31	23.70	1.00	32294.70	341523.00	32294.70	>100
40	2321.43	1	SLU	33.38	0.81	0.85	11.31	33.39	1.00	32294.70	340483.00	32294.70	>100
41	2380.95	1	SIU	32.65	0.79	0.85	11.31	32.66	1.00	32294.70	339443.00	32294.70	>100
42	2440.48	1	SLU	21.52	0.52	0.85	11.31	21.52	1.00	32294.70	338403.00	32294.70	>100

Caso	X <cm>></cm>	œ	TCC	e d'eserci: N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <amq></amq>	o₁ <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-240898.00	-5201.55	3499.25	0.00	78.54	22.82	337.81
45	59,52	2	SLE B	-240431.00	-7116,44	4787.46	0.00	78.54	23.98	353.48
46	119.05	2	SLE R	-237823.00	-8663.19	5828.01	0.00	78.54	24,73	363.42
47	178.57	2	-		-9884.46	6649.59	0.00	_	25.28	370.60
48	238.09	2	_		-10820.90	7279.54	0.00		25.65	375.38
49	297.62	2	SLE R		-11510.70	7743.65	0.00	78.54	25.87	378.07
50	357.14	2	SLE R		-11968.90	8051.86	0.00	-	25.95	378.81
51	416.67	2	SLE R	-221866.00 -216279.00	-12148,00	8172.38 8123.35	0.00	78.54	25.61	373.50 366.08
53	535.71	2	SLE R		-11797.40	7936.49	0.00	78.54	24.48	356.92
54	595.24	2	_		-11357.00	7640.24	0.00	78.54	23.75	346.41
55	654.76	2	_		-10791.70	7259.92	0.00	78.54	22.95	334.84
56	714.29	2	SLE R		-10134.50	6817.77	0.00	-	22.09	322.51
57	773.81	2	_		-9414.10	6333.17	0.00		21.19	309.66
58	833.33	2	SLE R	-182994.00	-8655.38	5822.75	0.00	78.54	20.27	296.50
59	892.86	2	SLE R	-177483.00	-7879.30	5300.66	0.00	78.54	19.34	283.20
60	952.38	2	SLE R	-171981.00	-7103.42	4778.70	0.00	78.54	18.41	269.91
61	1011.90	2	SLE R	-166488.00	-6342.15	4266.57	0.00	78.54	17.49	256.76
62	1071.43	2	SLE R	_	-5607.08	3772.06	0.00	78,54	16.58	243.84
63	1130.95	2	SLE R		-4907.26	3301.27	0.00	78.54	15,70	231,23
64		2			-4249,54	2858.81	0.00	-	14.85	218.99
65	1250.00	2	SLE R		-3638.79	2447.93	0.00	78,54	14.02	207.16
- 56	1309.52	2	SLE R	-139152.00	-3078.19	2070.80	0.00		13.23	195.76
67	1369.05 1428.57	2	SLE R	-133709.00	-2569.47 -2113.15	1728.57	0.00	78.54 78.54	12.47	184.81
69	-	2	-			1149.51	0.00	-	11.05	164.26
70	1547.62	2	SLE R		-1354.81	911.42	0.00	78.54	10.39	154.65
71	1607.14	2	_	-112003.00	-1049.40	705.97	0.00		9.76	145.46
72	1666.67	2	SLE R		-789.91	531.40	0.00	78.54	9.16	136.66
73	1726.19	2	SLE R	-101188.00	-573.36	385.71	0.00	78.54	8.58	128.23
74	1785.71	2	SLE R	-95788.30	-396.43	266.69	0.00	78.54	8.03	120.15
75	1845,24	2	SLE R	-90394.00	-255,59	171.95	0.00	78.54	7,51	112,38
76	1904.76	2	SLE R	-85004.50	-147.17	99.01	0.00	78.54	7.00	104.89
77	1964.29	2	SLE R	-79619.60	-67,36	45.32	0.00	78.54	6.51	97.65
78	2023,81	2	SLE R	-74238,90	-12.32	8.29	0.00	78.54	6.04	90.62
79	2083.33	2	SLE R		21.83	-14.68	0.00	78.54	5.61	84.14
80	2142,86	2	SLE R	-63489.30	38.96	-26.21	0.00	78.54	5,18	77.74
81	2202.38	2	_	-58119.70	42.95	-28.89	0.00	-	4.75	71.22
82	2321,43	2	SLE R	-52753.30 -47389.60	37.64 26.88	-25.32 -18.08	0.00	78.54	4.31	54.64 58.01
	2000 00				2 2 2 2 2	4 1			4.00	55.00
		_		-42028.60 -36669.70		-2.86				
	2500.00	_	CONTRACTOR OF THE PARTY OF	-31312.90		-	0.00	ALC: UNKNOWN STREET		
87				-240898.00						
88				-240431.00						
89	119.05			-237823.00						
-90	178.57			-235222.00				78.54	25.28	370.60
91	238.09			-232629.00				78.54		375.38
92				-230043.00						378.07
93				-227464.00						
	416.67	4	SLE Q	-221866.00	-12148.00	8172.38	0.00	78.54	25.61	373,50
95	_			-216279,00						366.08
96				-210705.00						
97	654.76	4	STE N	-205141.00 -199589.00	-10791 70	7250 02	0.00	70.54	23.75	346.41 334.84
	714.29			-194047.00						
	773.81			-188515.00						
101				-182994.00				78.54		296.50
_	892.86			-177483.00						283.20
	952.38			-171981.00						
_	1011.90			-166488.00				78.54		
_	1071.43			-161004.00						
_	1130.95	_		-155529.00						
107	1190.48			-150062.00				78.54	14.85	218.99
108	1250.00			-144603.00				78.54	14.02	207.16

								1,101	02011	C GI CGIC	OIO
109	1309.52	4	SLE	Q	-139152.00	-3078.19	2070.80	0.00	78.54	13.23	195.76
110	1369.05	4	SLE	Q	-133709.00	-2569.47	1728.57	0.00	78.54	12.47	184.81
111	1428.57	4	SLE	Q	-128272.00	-2113.15	1421.59	0.00	78.54	11.74	174.31
112	1488.10	4	SLE	Q	-122843.00	-1708.72	1149.51	0.00	78.54	11.05	164.26
113	1547.62	4	SLE	Q	-117420.00	-1354.81	911.42	0.00	78.54	10.39	154.65
114	1607.14	4	SLE	Q	-112003.00	-1049.40	705.97	0.00	78.54	9.76	145.46
115	1666.67	4	SLE	Q	-106593.00	-789.91	531.40	0.00	78.54	9.16	136.66
116	1726.19	4	SLE	Q	-101188.00	-573.36	385.71	0.00	78,54	8.58	128.23
117	1785.71	4	SLE	Q	-95788.30	-396.43	266.69	0.00	78.54	8.03	120.15
118	1845.24	4	SLE	Q	-90394.00	-255.59	171.95	0.00	78.54	7.51	112.38
119	1904.76	4	SLE	Q	-85004.50	-147.17	99.01	0.00	78.54	7.00	104.89
120	1964.29	4	SLE	Q	-79619.60	-67.36	45.32	0.00	78.54	6.51	97.65
121	2023,81	4	SLE	Q	-74238.90	-12,32	8,29	0.00	78.54	6.04	90.62
122	2083,33	4	SLE	Q	-68862.30	21.83	-14,68	0.00	78.54	5.61	84.14
123	2142.86	4	SLE	Q	-63489.30	38.96	-26.21	0.00	78.54	5.18	77.74
124	2202.38	4	SLE	Q	-58119.70	42.95	-28.89	0.00	78.54	4.75	71.22
125	2261,90	4	SLE	Q	-52753.30	37.64	-25.32	0.00	78.54	4.31	64.64
126	2321.43	4	SLE	Q	-47389.60	26.88	-18.08	0.00	78.54	3.87	58.01
127	2380.95	4	SLE	Q	-42028.60	14.48	-9.74	0.00	78.54	3.43	51.37
128	2440.48	4	SLE	Q	-36669.70	4.25	-2.86	0.00	78.54	2.98	44.75
129	2500.00	4	SLE	0	-31312.90	0.00	0.00	0.00	78.54	2,55	38.18

Verifiche principali

Caso	Tipo
1	SLU N cost - min. sic., SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
50	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
86	C.Rare - Sc max (min. compr.), C.Rare - Sf max (max traz.)
93	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
129	C.Q.Per Sc max (min. compr.), C.Q.Per Sf max (max traz.)

Palo n. 25

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Тр		P <dan cmq=""></dan>	Fyd <dan cmq2<="" th=""></dan>
60.00	6.00	C30/37	307,10	20.59	174.02	13.73	B450C	4300.00	3913.04	

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP.	0.00	0.00	0.00	-
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 25 (-163)

Caso	8	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	312389.00	5857.57	408.31	10679.60	19788.80
	-1	SLU	TAG				0.00	0.00
	.1	SLU	ECC	2	/s		0.00	0.00
	1	SLU	TOT	312389.00	5857.57	408.31	10679.60	19788.80
2	. 2	SLE R	RVN	231400.00	4338.94	302.46	7910.80	14658.40
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC		0 0		0.00	0.00
	2	SLE R	TOT	231400.00	4338.94	302.46	7910.80	14658.40
3	3	SLE F	RVN	231400.00	4338.94	302.46	7910.80	14658.40
	3	SLE F	TAG				0.00	0.00
	. 3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	231400.00	4338.94	302.46	7910.80	14658.40
4	-4	SIE Q	RVN	231400.00	4338.94	302.46	7910.80	14658.40
	4	SLE Q	TAG		Y Y		0.00	0.00
	4	SLE Q	ECC		Q 2	- 9	0.00	0.00
	. 4	SLE Q	TOT	231400.00	4338,94	302.46	7910.80	14658,40

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <dann></dann>
1	. 1	SLU	. 1	-312389.00	-5857.57	-408.31	-10679.60	-19788.80
.2	2	SLE R	1	-231400.00	-4338.94	-302.46	-7910.80	-14658.40
- 3	3	SLE F	1	-231400.00	-4338.94	-302.46	-7910.80	-14658.40
.4	4	SLE Q	- 1	-231400.00	-4338.94	-302.46	-7910.80	-14658.40

Caso	X <cm>></cm>	œ	1.00	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SLU	-312389.00	10611.90	-19663.30	-2571250.00	124958.00	-227696.00	2-3	241.25	8.23
2	59.52	1	SLU	-311426.00	12069.90	-22364.90	-2571250.00	124825.00	-227454.00	2-3	241,25	8,25
3	119.05	1	SLU	-307826.00	13157.60	-24380.40	-2571250.00	124326.00	-226549.00	2-3	241.25	8.35
4	178.57	1	SLU	-304236.00	13923.10	-25799.00	-2571250.00	123829.00	-225646.00	2-3	241.25	8.45
5	238.09	1	SIU	-300656.00	14411.60	-26704.10	-300656.00	123330.00	-224741.00	2-3	241.25	8.44
-6	297.62	1	SLU	-297084.00	14664.90	-27173.40	-297084.00	122830.00	-223836.00	2-3	241.25	8,26
7	357,14	1	SLU	-293523.00	14702.30	-27242.70	-293523.00	122332.00	-222932.00	2-3	241.25	8.21
8	416.67	1	SLU	-286245.00	14486.20	-26842.30	-286245.00	121306.00	-221073.00	2-3	241.25	8,26
9	476.19	1	SLU	-278984.00	14047,60	-26029.50	-278984.00	120276.00	-219208.00	2-3	241.25	8.45
10	535.71	1	SLU	-271737.00	13434.80	-24894.10	-271737.00	119233.00	-217248.00	2-3	241.25	8.76
11	595.24	1	SLU	-264505.00	12690.70	-23515.30	-264505.00	118093.00	-215209.00	2-3	241.25	9.18
12	654.76	1	SLU	-257286.00	11852.70	-21962.60	-257286.00	116956.00	-213150.00	2-3	241.25	9.74
13	714.29	1	SLU	-250082.00	10953.40	-20296.10	-2571250.00	115814.00	-211081.00	2-3	241.25	10.28
14	773.81	1	SLU	-242891.00	10020.30	-18567.10	-2571250.00	114666.00	-209001.00	2-3	241.25	10.58
15	833.33	1	SLU	-235714.00	9076.73	-16818.80	-2571250.00	113510.00	-206906.00	2-3	241.25	10.90
15	892,86	1	SIU	-228548.00	8142.16	-15087,10	-2571250.00	112350.00	-204801.00	2-3	241.25	11.25
17	952.38	3	SIJ	-221395.00	7232.26	-13401.10	-2571250.00	111186.00	-202687.00	2-3	241.25	11.61
18	1011.90	1	SLU	-214254.00	6359.53	-11783.90	-2571250.00	110015.00	-200560.00	2-3	241.25	12.00
19	1071.43	1	SLU	-207125.00	5533.56	-10253.40	-2571250.00	108839.00	-198421.00	2-3	241.25	12.41
20	1130.95	1	SIJ	-200006.00	4761.44	-8822.73	-2571250.00	107658.00	-196274.00	2-3	241.25	12.85
21	1190.48	1	SIU	-192899.00	4048.03	-7500.83	-2571250.00	106473.00	-194117.00	2-3	241.25	13.32
22	1250.00	1	SLU	-185801.00	3396.33	-6293.25	-2571250.00	105281.00	-191947.00	2-3	241.25	13,83
23	1309.52	1	SIA	-178714.00	2807.69	-5202.52	-2571250.00	104085.00	-189768.00	2-3	241.25	14.38
24	1369.05	1	SIJ	-171636.00	2282.12	-4228.67	-2571250.00	102885.00	-187581.00	2-3	241,25	14.98
-25	1428.57	1	SLU	-164567.00	1818.53	-3369.66	-2571250.00	101679.00	-185383.00	2-3	241.25	15.62
26	1488.10	1	SLU	-157508.00	1414.91	-2621.76	-2571250.00	100468.00	-183175.00	2-3	241.25	16.32
27	1547,62	1	SLU	-150456.00	1068.51	-1979.91	-2571250.00	99254.10	-180959.00	2-3	241.25	17.09
28	1607.14	1	SLU	-143413.00	776.05	-1437.99	-2571250.00	98035.30	-178735.00	2-3	241.25	17.92
29	1666.67	1	SLU	-136377.00	533.80	-989.10	-2571250.00	96811.20	-176501.00	2-3	241.25	18.85
30	1726.19	1	SLU	-129349.00	337.73	-625.79	-2571250.00	95583.60	-174259.00	2-3	241.25	19.87
31	1785.71	1	SIU	-122328.00	183.59	-340.19	-2571250.00	94352.30	-172011.00	2-3	241.25	21.01
32	1845.24	1	SLU	-115313.00	67.03	-124.20	-2571250.00	93115.70	-169753.00	2-3	241.25	22,29
33	1904.76	1	SLU	-108304.00	-16.42	30.43	-2571250,00	-91762.00	167241.00	2-3	61.25	23.74
34	1964,29	1	SIU	-101302.00	-71.23	131.98	-2571250.00	-90461.40	164864.00	2-3	61.25	25,38
35	2023,81	1	SLU	-94304.40	-101.86	188.73	-2571250.00	-89155.30	162478.00	2-3	61.25	27.26
36	2083.33	1	SLU	-87312.10	-112.74	208.90	-2571250.00	-87843.70	160082.00	2-3	61.25	29.44
37	2142.86	1	SIA	-80324.50	-108.27	200.62	-2571250.00	-86525.90	157675.00	2-3	61.25	32.01
38	2202,38	1	SIJ	-73341,20	-92.81	171.97	-2571250.00	-85203.60	155260.00	2-3	61,25	35.05
39	2261.90	1	SLU	-66361.90	-70.64	130.90	-2571250.00	-83876.60	152837.00	2-3	61.25	38.74
40	2321.43	1	SLU	-59386.10	-46.05	85.34	-2571250.00	-B2543.00	150403.00	2+3	61.25	43.29
41	2380.95	1	SIJ	-52413,40	-23.27	43.12	-2571250.00	-81205.10	147962.00	2-3	61.25	49.05
42	2440.48	1	SIAI	-45443.60	~6.52	12.08	-2571250.00	-79862.90	145514.00	2-3	61.25	56.5B
43	2500.00	1	SLU	-38476.30	0.00	0.00	-2571250.00					66.82

Caso	X <cm>></cm>	cc	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
- 1	0.00	1	SIU	5857.57	408.31	0.85	11.31	5871.78	1.00	32294.70	376415.00	32294.70	5.500
2	59.52	1	SIJ	4462.53	311.07	0.85	11.31	4473.36	1.00	32294.70	376277,00	32294.70	7,219
- 3	119.05	1	SLU	3242.50	226.03	0.85	11.31	3250.37	1.00	32294.70	375761.00	32294.70	9.936
4	178,57	1	SIU	2187.07	152.46	0.85	11.31	2192.38	1.00	32294.70	375247.00	32294.70	14.730
- 5	238.09	1	SIJ	1285,09	89.58	0.85	11.31	1288.21	1.00	32294.70	374734.00	32294.70	25.070
- 6	297.62	1	SIU	524.89	36.59	0.85	11.31	526.16	1.00	32294.70	374222.00	32294.70	61.378
7	357.14	1	SLU	-307.81	-21.46	0.85	11,31	308.55	1.00	32294.70	373712.00	32294.70	>100
.8	416.67	1	SIA	-1185,34	-82.63	0.85	11.31	1188.21	1.00	32294.70	372670.00	32294.70	27,179
9	476.19	1	SLU	-1881,92	-131.18	0.85	11.31	1886.49	1.00	32294.70	371630.00	32294.70	17.119
10	535.71	1	SLU	-2417.65	-168.53	0.85	11.31	2423.52	1.00	32294.70	370592.00	32294.70	13.326
11	595.24	1	SIJ	-2811.88	-196.01	0.85	11.31	2818.70	1.00	32294.70	369556.00	32294.70	11.457
12	654.76	1	SLU	-3082.98	-214.91	0.85	11.31	3090.46	1.00	32294.70	368522.00	32294.70	10.450
13	714.29	1	SLU	-3248.22	-226.43	0.85	11.31	3256.10	1.00	32294.70	367490.00	32294.70	9.918
14	773.81	1	SIU	-3323.64	-231.68	0.85	11.31	3331.71	1.00	32294.70	366460.00	32294.70	9.693
15	833.33	1	SLU	-3323,98	-231.71	0.85	11.31	3332.04	1.00	32294.70	365432.00	32294.70	9.692
16	892.86	1	SLU	-3262.65	-227.43	0.85	11.31	3270.57	1.00	32294.70	364405.00	32294.70	9.874
17	952.38	1	SIU	-3151.75	-219.70	0.85	11:31	3159.40	1.00	32294.70	363381.00	32294.70	10.222
18	1011,90	1	SIU	-3002.07	-209.27	0.85	11.31	3009.35	1.00	32294.70	362358.00	32294.70	10.731
19	1071.43	1	SIU	-2823.15	-196.79	0.85	11.31	2830.00	1.00	32294.70	361337.00	32294.70	11.412
20	1130.95	1	SLU	-2623.34	-182.87	0.85	11.31	2629.70	1.00	32294.70	360317.00	32294.70	12,281
21	1190.48	1	SLU	-2409.85	-167.98	0.85	11.31	2415.69	1.00	32294.70	359299.00	32294.70	13.369
22	1250.00	1	SLU	-2188.85	-152.58	0.85	11.31	2194.16	1,00	32294.70	358282.00	32294.70	14.719
23	1309.52	1	SLU	-1965.56	-137.01	0.85	11.31	1970.33	1.00	32294.70	357267.00	32294.70	16.390
24	1369.05	1	SLU	-1744.33	-121.59	0.85	11.31	174B.56	1.00	32294.70	356253,00	32294.70	18.469
25	1428.57	1	SLU	-1528.70	-106.56	0.85	11.31	1532.41	1,00	32294.70	355241.00	32294.70	21.075
26	1488,10	1	SIU	-1321.55	-92.12	0.85	11.31	1324.76	1.00	32294.70	354229.00	32294.70	24.378
27	1547.62	1	SIA	-1125.13	-78.43	0.85	11.31	1127.86	1.00	32294.70	353219.00	32294.70	28.634

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28	1607.14	1	SLU	-941.16	-65.61	0.85	11.31	943.45	1.00	32294.70	352210.00	32294.70	34.231
29	1666.67	1	SIA	-770.94	-53.74	0.85	11.31	772.81	1.00	32294.70	351203.00	32294.70	41.789
30	1726.19	1	SIU	-615.36	-42.90	0.85	11.31	616.85	1.00	32294.70	350196.00	32294.70	52.354
31	1785,71	1	SIJJ	-475.02	-33.11	0.85	11.31	476.18	1.00	32294.70	349190.00	32294.70	67.821
32	1845.24	1	SLU	-350,28	-24.42	0.85	11.31	351.13	1.00	32294.70	348185.00	32294.70	91.973
33	1904.76	1	SLU	-241.31	-16.82	0.85	11.31	241.89	1.00	32294.70	347182.00	32294.70	>100
34	1964.29	1	SLU	-148.12	-10.32	0.85	11.31	148.47	1.00	32294.70	346178.00	32294.70	>100
35	2023.81	1	SLU	-70.64	-4.92	0.85	11.31	70.81	1.00	32294.70	345176,00	32294.70	>100
36	2083.33	3	SLU	-8.75	-0.61	0.85	11.31	8.77	1.00	32294.70	344175.00	32294.70	>100
37	2142.86	1	SIJJ	37.71	2.63	0.85	11.31	37.80	1.00	32294.70	343174.00	32294.70	>100
38	2202.38	1	SLU	68,91	4.80	0.85	11.31	69.08	1,00	32294.70	342173.00	32294.70	>100
39	2261.90	1	SLU	84.99	5.92	0.85	11.31	85.19	1.00	32294.70	341174.00	32294.70	>100
40	2321.43	1	SIAJ	86.07	6.00	0.85	11.31	86.28	1.00	32294.70	340175.00	32294.70	>100
41	2380.95	-1	SLU	72.23	5.04	0.85	11.31	72.41	1.00	32294.70	339176,00	32294.70	>100
42	2440.48	1	SLU	43.54	3.03	0.85	11.31	43.64	1.00	32294.70	338177.00	32294.70	>100

erii	iche sta	ato	Timit	e d'eserci:	210					
Caso	X <cm></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <mq></mq>	AfC <mq></mq>	σ _c <dan cmq=""></dan>	σ _f <dan cmo<="" th=""></dan>
44	0.00	2	SLE R	-231400.00	-14565.40	7860.63	0.00	78.54	27.30	397.8
45	59.52	2	SLE R	-230999.00	-16566.60	8940,64	0.00	78.54	28.43	413.2
46	119.05	2	SLE R	-228523.00	-18059.60	9746.36	0.00	78.54	29.10	422.0
47	178.57	2	SLE R	-226054.00	-19110.30	10313.40	0.00	78.54	29.51	427.4
48	238.09	2	SLE R	-223591.00	-19780.80	10675.30	0.00	78.54	29.71	429.7
49	297,62	2	SLE R	-221136.00	-20128.40	10862.90	0.00	78,54	29.71	429.5
50	357.14	2	SLE R	-218688.00	-20179.70	10890.60	0.00	78.54	29.54	426.9
51	416.67	2	SLE R	-213313.00	-19883.20	10730.50	0.00	78.54	28.93	418.0
52	476.19	2	SLE R	-207949.00	-19281,10	10405.60	0.00	78,54	28.14	406.
53	535.71	2	SLE R	-202596.00	-18440.00	9951.69	0.00	78.54	27.22	393.
54	595.24	2	SLE R	-197254.00	-17418.70	9400.51	0.00	78.54	26.19	378.
55	654.76	2	SLE R	-191923.00	-16268.60	8779.81	0.00	78.54	25.08	363.
56	714.29	2	SLE R	-186602,00	-15034.10	8113.60	0.00	78.54	23.93	346.
57	773.81	2	SLE R	-181291.00	-13753.40	7422.41	0.00	78.54	22.75	330.
58	833,33	2	SLE R	-175990.00	-12458.40	6723.51	0.00	78.54	21.57	313.
59	892.86	2	SLE R	-170698.00	-11175.60	6031.23	0.00	78.54	20.39	296.
60	952.38	2	SLE R	-165416.00	-9926.71	5357.23	0.00	78.54	19.23	280.
61	1011.90	2	SLE R	-160142.00	-8728.83	4710.76	0,00	78,54	18.11	264.
.62	1071.43	2	SLE R	-154877.00	-7595.14	4098,93	0.00	78.54	17.02	249.
63	1130.95	2	SLE R	-149620.00	~6535.35	3526.99	0.00	78.54	15.97	234.
64	1190.48	2	SLE R	-144371.00	-5556.17	2998.54	0.00	78.54	14.97	220.
65	1250.00	2	SLE R	-139130.00	-4661.66	2515,80	0.00	78,54	14.03	206.
66	1309.52	2	SLE R	-133896.00	-3853.72	2079.77	0.00	78,54	13.13	193.
67	1369.05	2	SLE R	-128670.00	-3132.35	1690.46	0.00	78.54	12.28	181.
68	1428.57	2	SLE R	-123450.00	-2496.05	1347.06	0.00	78.54	11.49	170.
69	1488,10	2	SLE R	-118238.00	-1942.05	1048.08	0.00	78.54	10.74	159.
.70	1547.62	2	SLE R	-113031.00	-1466.60	791.49	0.00	78.54	10.04	149.
71	1607,14	2	SLE R	-107830.00	-1065.17	574.85	0.00	78.54	9.39	139.
72	1666.67	2	SLE R	-102636.00	-732.67	395.40	0.00	78.54	8.77	130.
73	1726,19	2	SLE R	-97446.50	-463.55	250,17	0.00	78.54	8.19	122.
74	1785.71	2	SLE R	-92262.50	-251,99	136,00	0.00	78,54	7.65	114.
75	1845.24	2	SLE R		-92.00	49.65	0.00	78.54	7.13	106.
76	1904.76	2	SLE R	-81909.00	22.54	-12.17	0.00	78.54	6.67	100.
77	1964.29	2	SLE R	-76739.00	97.77	-52.76	0.00	78.54	6.29	94.
78	2023.81	2	SLE R	-71573.20	139.80	-75.45	0.00	78.54	5.90	88.
79	2083.33	2	SLE R	-66411.10	154.74	-83.51	0.00	78.54	5.49	82.
80	2142.86	2	SLE R	-61252.70	148.61	-80.20	-	78.54	5.07	75.
81	2202.38	2	SLE R	~56097.50	127.38	-68.75	_	78.54	4.63	69.
82	2261.90	2	SLE R	-50945.30	96.96	-52,33	0.00	78.54	4.20	62.
83	2321.43	2	SLE R	~45795.90	63.21	-34.11	0.00	78.54	3.76	
84	2380.95	2	SLE R	-40648.90	31.94	-17.24	0.00	78.54	3.32	49.
	2440.48	_		-35504.10				78.54		
86	2500.00	2	SLE R	-30361.20				78.54		
87	0.00	-		-231400.00				78,54		
88	59.52			-230999,00				78.54		
89	119.05	_		-228523.00				78.54		
90	178.57	4	SLE Q	-226054.00	-19110.30	10313.40	0.00	78,54		427.
91	238.09			-223591.00				78.54		429.
92				-221136.00			and being a body	78.54		429.
93	357.14	_		-218688.00				78.54		-
94		_		-213313.00				78.54		
95	476.19	_		-207949.00				78.54		
96	535.71	_		-202596.00				78.54		393.
97	595.24	-	The second second	-197254.00	THE RESERVE AND ADDRESS OF THE PARTY OF THE		_	78,54		
98		_		-191923.00				78.54		363.
99	714.29	_		-186602.00			_	78.54		
100	773.81	_		-181291.00			_	78.54		-
101	833.33	_	SLE Q					78,54	21.57	313.

							Rela	Relazione di calcolo				
102	892,86	4	SLE	Q	-170698,00	-11175.60	6031.23	0.00	78.54	20.39	296.90	
103	952.38	4	SLE	Q	-165416.00	-9926.71	5357.23	0.00	78.54	19.23	280.54	
104	1011.90	4	SLE	Q	-160142.00	-8728.83	4710.76	0.00	78,54	18.11	264.59	
105	1071,43	4	SLE	Q	-154877.00	-7595.14	4098.93	0.00	78.54	17.02	249.16	
106	1130.95	4	SLE	Q	-149620.00	-6535.35	3526,99	0.00	78.54	15.97	234.34	
107	1190.48	4	SLE	Q	-144371.00	~5556.17	2998.54	0.00	78.54	14.97	220.16	
108	1250.00	4	SLE	Q	-139130.00	-4661.66	2515.80	0.00	78.54	14.03	206.66	
109	1309.52	4	SLE	Q	-133896.00	-3853.72	2079.77	0.00	78.54	13.13	193.86	
110	1369.05	4	SLE	Q	-128670.00	-3132.35	1690.46	0.00	78.54	12.28	181.76	
111	1428.57	4	SLE	Q	-123450.00	-2496.05	1347.06	0.00	78.54	11.49	170.34	
112	1488.10	4	SLE	Q	-118238.00	-1942.05	1048.08	0.00	78.54	10.74	159.59	
113	1547.62	4	SLE	Q	-113031.00	-1466.60	791.49	0.00	78.54	10.04	149.46	
114	1607.14	4	SLE	Q	-107830.00	-1065.17	574.85	0.00	78,54	9.39	139.93	
115	1666.67	4	SLE	Q	-102636.00	-732.67	395.40	0.00	78.54	8.77	130.96	
116	1726.19	4	SLE	Q	-97446.50	-463.55	250.17	0.00	78.54	8.19	122.49	
117	1785.71	4	SLE	Q	-92262.50	-251.99	136.00	0.00	78.54	7.65	114.49	
118	1845.24	4	SLE	Q	-87083.40	-92.00	49.65	0.00	78.54	7.13	106,91	
119	1904.76	4	SLE	Q	-81909.00	22.54	-12,17	0.00	78.54	6.67	100.05	
120	1964.29	4	SLE	Q	-76739.00	97.77	-52,76	0.00	78.54	6.29	94.35	
121	2023.81	4	SLE	Q	-71573.20	139,80	-75.45	0.00	78.54	5.90	88,38	
122	2083.33	4	SLE	Q	-66411.10	154.74	-83.51	0.00	78.54	5.49	82,21	
123	2142.86	4	SLE	Q	-61252.70	148.61	-B0,20	0.00	78.54	5.07	75.87	
124	2202,38	4	SLE	Q	-56097.50	127.38	-68.75	0.00	78,54	4.63	69.42	
125	2261,90	4	SLE	Q	-50945.30	96.96	-52.33	0.00	78.54	4.20	62.89	
126	2321,43	4	SLE	Q	-45795.90	63.21	-34,11	0.00	78,54	3.76	56.34	
127	2380.95	4	SLE	Q	-40648.90	31,94	-17.24	0.00	78,54	3.32	49.82	
128	2440.48	4	SLE	Q	-35504.10	8.95	-4,83	0.00	78,54	2.89	43.36	
129	2500.00	4	SLE	Q	-30361.20	0.00	0.00	0.00	78.54	2.47	37.02	

Verifiche	princi	pali
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Caso	Tipo									
-1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio									
7	SLU N cost - min, sic.									
48	C.Rare - Sf min (max compr.)									
49	C.Rare - Sc min (max compr.)									
86	C.Rare - Sc max (min. compr.), C.Rare - Sf max (max traz.)									
91	C.Q.Per Sf min (max compr.)									
92	C.Q.Per Sc min (max compr.)									
129	C.Q.Per Sc max (min. compr.), C.Q.Per Sf max (max traz.									

Palo n. 26

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf (m)	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmc=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>	
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04	

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti.

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	-
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 26 (-155)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>	
1	1	SLU	RVN	287771.00	6009.55	641.18	20713.80	28716.10	
	1	SLU	TAG				0.00	0.00	
	1	SLU	ECC				0.00	0.00	
	1	SLU	TOT	287771.00	6009.55	641.18	20713.80	28716.10	
.2	2	SLE R	RVN	213163.00	4451.52	474.95	15343.50	21271.20	
	2	SLE R	TAG				0.00	0.00	
	2	SLE R	ECC	8			0.00	0.00	
	. 2	SLE R	TOT	213163.00	4451.52	474.95	15343.50	21271.20	
77	3	SLE F	RVN	213163.00	4451.52	474.95	15343.50	21271.20	
	. 3	SLE F	TAG				0.00	0.00	
	3	SLE F	ECC				0.00	0.00	
	3	SIE F	TOT	213163.00	4451.52	474.95	15343.50	21271.20	
4	4	SLE Q	RVN	213163.00	4451,52	474.95	15343.50	21271.20	
	4	SIE Q	TAG				0.00	0.00	
	4	SLE Q	ECC				0.00	0.00	
	4	SLE Q	TOT	213163.00	4451.52	474.95	15343.50	21271.20	

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Sollecitazioni nei pali

Caso	cc	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>	
1	. 1	SLU	. 1	-287771.00	-6009.55	-641.18	-20713.80	-28716.10	
2	2	SLE R	1	-213163.00	-4451.52	-474.95	-15343.50	-21271.20	
3	3	SLE F	1	-213163.00	-4451,52	-474.95	-15343.50	-21271.20	
4	4	SLE Q	1	-213163.00	-4451.52	-474.95	-15343.50	-21271.20	

Da 0 a -25

Stato lin	nite ultimo	- Verifiche	a flessione	pressoflessione
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Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SIJ	-287771.00	20611.40	-28574.10	-287771.00	148994.00	-203222.00	2-3	233.75	7.152
2	59.52	1	SLU	-286978.00	22409.60	-31067.10	-286978.00	148851.00	-203025.00	2-3	233.75	6.572
3	119.05	1	SIU	-283720.00	23649.40	-32785.80	-283720.00	148260.00	-202216.00	2-3	233.75	6.203
.4	178.57	1	SLU	-280471.00	24407.80	-33837.20	-280471.00	147671.00	-201407.00	2-3	233.75	5.986
.5	238.09	1	SLU	-277230.00	24756.30	-34320.40	-277230.00	147078.00	-200595.00	2-3	233.75	5.878
- 6	297.62	1	SIU	-273998.00	24761.00	-34326.90	-273998.00	146487.00	-199784.00	2-3	233.75	5.853
7	357.14	-1	SLU	-270775.00	24454.80	-33902.40	-270775.00	145897.00	-198975.00	2-3	233.75	5.902
8	416.67	1	SLU	-264076.00	23789.70	-32980.30	-264076.00	144661.00	-197279.00	2-3	233.75	6.01
.9	476.19	1	SLU	-257391.00	22815.30	-31629.50	-257391.00	143421.00	-195578.00	2-3	233.75	6.211
10	535.71	1	SLU	-250720.00	21605.60	-29952.50	-250720.00	142178.00	-193872.00	2-3	233.75	6.510
11	595.24	1	SLU	-244062.00	20225.50	-28039.20	-244062.00	140927.00	-192157.00	2-3	233.75	6.893
12	654.76	1	SLU	-237418.00	18731.10	-25967.50	-237418.00	139674.00	-190437.00	2-3	233.75	7.376
13	714.29	1	SLU	-230786.00	17170.60	-23804.10	-230786.00	138416.00	-188711.00	2-3	233.75	7.974
14	773.81	1	SLU	-224167.00	15584.70	-21605.50	-224167.00	137152.00	-186977.00	2-3	233.75	8.704
15	833.33	1	SIU	-217559.00	14007.30	-19418.70	-217559.00	135886.00	-185239.00	2-3	233.75	9.595
16	892,86	1	SIJ	-210963.00	12465.90	-17281.80	-210963.00	134615.00	-183495.00	2-3	233.75	10.680
17	952.38	1	SLU	-204379.00	10982.70	-15225.60	-204379.00	133341,00	-181747.00	2-3	233.75	12.00
18	1011.90	1	SIAI	-197806.00	9574,77	-13273.80	-2571250.00	132061.00	-179989.00	2-3	233.75	12.999
19	1071.43	1	SIA	-191243.00	8254.88	-11444.00	-2571250.00	130777.00	-178227.00	2-3	233.75	13,44
20	1130,95	1	SLU	-184690.00	7031.93	~9748.56	-2571250.00	129477.00	-176465.00	2-3	233.75	13.922
21	1190.48	1	SLU	-178148.00	5911.57	-8195.38	-2571250.00	127999.00	-174733.00	2-3	233.75	14.433
22	1250.00	1	SIJ	-171614.00	4896.64	-6788.35	-2571250.00	126614.00	-172835.00	2-3	233.75	14.983
23	1309.52	1	SIJ	-165090.00	3987.64	-5528.17	-2571250.00	125222.00	-170930.00	2-3	233.75	15.575
24	1369.05	1	SLU	-158575.00	3183.08	-4412.80	-2571250.00	123825.00	-169016.00	2-3	233.75	16.21
25	1428.57	1	SLU	-152069.00	2479.94	-3438.01	-2571250.00	122420.00	-167091.00	2-3	233.75	16.908
26	1488.10	1	SLU	-145571.00	1873.90	-2597.84	-2571250.00	121007.00	-165157.00	2-3	233.75	17.663
27	1547.62	1	SLU	-139080.00	1359.66	-1884.93	-2571250.00	119589.00	-163214.00	2-3	233.75	18.488
28	1607.14	1	SLU	-132597.00	931.17	-1290.91	-2571250.00	118170.00	-161255.00	2-3	233,75	19.392
29	1666.67	1	SIJ	-126121.00	581.85	-806.64	-2571250.00	116760.00	-159258.00	2-3	233.75	20.38
30	1726.19	1	SLU	-119652.00	304.75	-422.49	-2571250.00	115311.00	-157263.00	2-3	233.75	21.489
31	1785,71	1	SIU	-113189.00	92.69	-128.50	-2571250.00	113851.00	-155262.00	2-3	233.75	22.716
32	1845.24	1	SLU	-106732.00	-61.64	85.45	-2571250.00	-112599.00	153403.00	2-3	53.75	24.091
33	1904.76	1	SLU	-100281.00	-165.57	229.54	-2571250.00	-111110.00	151502.00	2-3	53.75	25.640
34	1964.29	1	SLU	-93835.30	-226.43	313.90	-2571250.00	-109538.00	149543.00	2-3	53.75	27.402
35	2023.81	1	SIJ	-87394.70	-251.44	348.57	-2571250.00	-108029.00	147477.00	2-3	53.75	29.421
36	2083.33	1	SIJ	-80958.70	-247.76	343.48	-2571250.00	-106514.00	145402.00	2-3	53.75	31.760
37	2142.86	1	SLU	-74527.10	-222.45	308.39	-2571250.00	-104990.00	143314.00	2-3	53.75	34.50
38	2202.38	1	SLU	-68099.60	-182.45	252.93	-2571250.00	-103458.00	141216.00	2-3	53.75	37.75
39	2261.90	1	SIJ	-61675.60	-134.62	186.62	-2571250.00	-101919.00	139108.00	2-3	53.75	41.690
40	2321.43	1	SIAI	-55255.00	-85.74	118.87	-2571250.00	-100374.00	136990.00	2-3	53.75	46.534
41	2380.95	1	SLU	-48837.30	-42.56	59.00	-2571250.00	-98820.20	134859.00	2+3	53.75	52.649
42	2440.48	1	SLU	-42422.30	-11.75	16.29	-2571250.00	-97260.10	132720.00	2-3	53.75	60.611
43	2500.00	1	SLU	-36009.50	0.00	0.00	-2571250.00				-	71.405

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIA	6009.55	641.18	0.85	11.31	6043.66	1.00	32294.70	372888.00	32294.70	5.344
2	59.52	1	SLU	4299.62	458.74	0.85	11.31	4324.02	1.00	32294.70	372775.00	32294.70	7.469
3	119.05	1	SIU	2817.44	300.60	0.85	11.31	2833.44	1.00	32294.70	37230B.00	32294.70	11.398
4	178.57	1	SIU	1547.68	165.13	0.85	11.31	1556.46	1.00	32294.70	371843.00	32294.70	20.749
5	238.09	1	SLU	474.31	50.61	0.85	11,31	477.00	1.00	32294.70	371378,00	32294.70	67,703
.6	297.62	1	SIA	-419.04	-44.71	0.85	11.31	421.41	1.00	32294.70	370915.00	32294.70	76.634
7	357.14	1	SLU	-1380,92	-147.34	0.85	11.31	1388.76	1.00	32294.70	370454.00	32294,70	23,254
- 8	416.67	1	SLU	-2378.26	-253.75	0.85	11.31	2391.76	1.00	32294.70	369494.00	32294.70	13.502
9	476.19	1	SIJJ	-3151.21	-336.21	0.85	11.31	3169.09	1.00	32294.70	368537.00	32294.70	10.191
10	535.71	1	SLU	-3726.32	-397.57	0.85	11.31	3747.47	1.00	32294.70	367581.00	32294.70	8.618
11	595,24	1	SLU	-4128.89	-440.53	0.85	11.31	4152.33	1.00	32294.70	366627.00	32294.70	7.778
12	654.76	1	SIJ	-4382.73	-467.61	0.85	11.31	4407.60	1.00	32294.70	365676,00	32294.70	7.327
13	714.29	1	SLU	-4510.00	-481.19	0.85	11.31	4535.60	1.00	32294.70	364726.00	32294.70	7.120
14	773.81	1	SIU	-4531.13	-483.44	0.85	11.31	4556.84	1.00	32294.70	363778.00	32294.70	7.087
15	833.33	1	SIU	-4464.73	-476.36	0.85	11.31	4490.07	1.00	32294.70	362831.00	32294.70	7.192
16	892,86	1	SLU	-4327.63	-461.73	0.85	11.31	4352.19	1.00	32294.70	361886,00	32294.70	7.420

			Trelazione di calcolo										
17	952.38	1	SLU	-4134.87	-441.16	0.85	11.31	4158.34	1.00	32294.70	360943.00	32294.70	7,766
18	1011.90	1	SLU	-3899.77	-416.08	0.85	11.31	3921.90	1.00	32294.70	360002.00	32294.70	8.234
19	1071.43	1	SIU	-3633.99	-387.72	0.85	11.31	3654.61	1.00	32294.70	359062.00	32294.70	8.837
-20	1130.95	1	SIJJ	-3347.65	-357.17	0.85	11.31	3366.65	1.00	32294.70	358123.00	32294.70	9.593
21	1190,48	1	SLU	-3049.43	-325.35	0.85	11.31	3066.74	1.00	32294.70	357186.00	32294.70	10.531
22	1250.00	1	SIU	-2746.65	-293.05	0.85	11.31	2762.24	1.00	32294.70	356250.00	32294.70	11.691
23	1309.52	1	SLU	-2445,45	-260.91	0.85	11.31	2459.33	1.00	32294.70	355316.00	32294.70	13.132
24	1369.05	1	SLU	-2150.84	-229.48	0.85	11.31	2163.05	1.00	32294.70	354382.00	32294.70	14.930
25	1428.57	1	SLU	-1866.89	-199.19	0.85	11.31	1877.48	1.00	32294.70	353450.00	32294.70	17.201
26	1488.10	1	SIJ	-1596.78	-170.37	0.85	11.31	1605.84	1.00	32294.70	352520.00	32294.70	20.111
27	1547.62	1	SLU	-1342.97	-143.29	0.85	11.31	1350.59	1.00	32294.70	351590.00	32294.70	23.912
28	1607.14	1	SLU	-1107.28	-118.14	0.85	11.31	1113.57	1.00	32294.70	350661.00	32294.70	29.001
29	1666.67	1	SIAJ	-891.00	-95.06	0.85	11.31	896.05	1.00	32294.70	349734.00	32294.70	36.041
30	1726,19	-1	SLU	-694.95	-74.15	0.85	11.31	698.89	1.00	32294.70	348807,00	32294.70	46.208
31	1785.71	1	SLU	-519.63	-55.44	0.85	11.31	522.58	1.00	32294.70	347881.00	32294.70	61.799
32	1845,24	1	SILI	-365.25	-38.97	0.85	11.31	367.32	1.00	32294.70	346956.00	32294.70	87.919
33	1904.76	1	SIJ	-231,81	-24.73	0.85	11.31	233.12	1.00	32294.70	346032.00	32294.70	>100
34	1964.29	1	SLU	-119.17	-12.71	0.85	11.31	119.84	1.00	32294.70	345109.00	32294.70	>100
35	2023.81	1	SLU	-27.08	-2.89	0.85	11.31	27.24	1.00	32294.70	344186,00	32294.70	>100
36	2083.33	1	SIU	44.72	4.77	0.85	11.31	44.97	1.00	32294.70	343265.00	32294.70	>100
37	2142.86	1	SLU	96.54	10.30	0.85	11.31	97.09	1.00	32294.70	342343.00	32294.70	>100
38	2202.38	1	SIJJ	128.65	13.73	0.85	11.31	129.38	1.00	32294.70	341423.00	32294.70	>100
39	2261.90	-1	SIJJ	141,28	15.07	0.85	11.31	142.08	1.00	32294.70	340502.00	32294.70	>100
40	2321.43	1	SLU	134.63	14.36	0.85	11.31	135.40	1.00	32294.70	339583.00	32294.70	>100
41	2380.95	1	SIU	108.82	11.61	0.85	11,31	109.44	1.00	32294.70	338664.00	32294.70	>100
42	2440.48	1	SIU	63.94	6.82	0.85	11.31	64.30	1.00	32294.70	337745.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <mq></mq>	σ _□ <dan cmq=""></dan>	of <dan cmq≥<="" th=""></dan>
44	0.00	2	SLE R	-213163.00	-21166.00	15267.70	0.00	78.54	30.83	443.63
45	59.52	2	SLE B	-212890.00	-23012,70	16599.70	0.00	78.54	31.99	459.30
46	119.05	2	SLE R	-210666.00	-24285.80	17518.10	0.00	78.54	32.62	467.64
47	178.57	2	SLE R	-208450.00	-25064.60	18079.80	0.00	78.54	32.94	471.70
48	238.09	2	SLE B	-206239.00	-25422,50	18338.00	0.00	78.54	32.99	472.13
49	297.62	2	SLE B	-204035.00	-25427.30	18341.50	0.00	78+54	32.81	469.4
50	357.14	2	SLE R	-201838.00	-25112.90	18114.70	0.00	78,54	32,43	464.00
51	416.67	2	SLE R	-196891.00	-24429,80	17622.00	0.00	78.54	31.59	452.10
52	476.19	2	SLE B	-191954.00	-23429.20	16900.20	0.00	78.54	30.56	437.39
53	535.71	2	SLE R	-187028.00	-22187.00	16004.20	0.00	78.54	29.36	420.63
54	595.24	2	SLE R	-182112.00	-20769.80	14981.90	0.00	78,54	28.06	402.33
55	654.76	2	SLE B	-177206.00	-19235.20	13874.90	0.00	78,54	26.68	383.0
5€	714.29	2	SLE R	-172309,00	-17632.70	12719.00	0.00	78.54	25.26	363.13
57	773.81	2	SLE F	-167421.00	-16004.10	11544,20	0.00	78.54	23.82	343.04
58	833.33	2	SLE R	-162542.00	-14384.20	10375.70	0.00	78.54	22.39	323,03
59	892.86	2	SLE R	-157672.00	-12801.30	9233.99	0.00	78.54	20.99	303.35
60	952.38	2	SLE R	-152811.00	-11278.20	8135.32	0.00	78.54	19.62	284.20
61	1011.90	2	SLE R	-147958.00	-9832,42	7092.42	0.00	78.54	18.30	265.7
62	1071.43	2	SLE B	-143112.00	-8477.01	6114,72	0.00	78.54	17.04	248.00
63	1130.95	2	SLE R	-138275.00	-7221,16	5208.84	0.00	78,54	15.85	231.2
64	1190.48	2	SIE R	-133444.00	-6070.65	4378.94	0.00	78,54	14.72	215.3
65	1250.00	- 2	SLE R	-128621.00	-5028.41	3627.14	0.00	78.54	13.66	200.4
66	1309.52	2	SLE R	-123805.00	-4094.94	2953:80	0.00	78.54	12.68	186.49
67	1369.05	2	SLE P	-118995.00	-3268.74	2357,84	0.00	78,54	11.76	173.40
68	1428.57	2	SLE R	-114192.00	-2546.68	1836.99	0.00	78.54	10.91	161.33
69	1488.10	2	SLE R	-109395.00	-1924.33	1388.07	0.00	78.54	10.12	150.08
7.0	1547.62	2	SLE P	-104604.00	-1396.25	1007.15	0.00	78.54	9.39	139.60
71	1607.14	2	SLE R	-99818.40	-956.23	689.75	0.00	78.54	8.72	130.00
72	1666.67	2	SLE R	-95038.20	-597.51	431.00	0.00	78.54	8.11	121.00
73	1726,19	2	SLE R	-90263.00	-312.95	225.74	0.00	78.54	7.54	112.7
74	1785.71	2	SLE R	-85492.80	-95.18	68.66	0.00	78.54	7.01	105.00
75	1845,24	2	SLE B	-80727.00	63.30	-45.66	0.00	78.54	6.60	98.9
7.6	1904.76	2	SLE R	-75965.70	170.03	-122.65	0.00	78,54	6.28	94.09
77	1964.29	2	SLE R	-71208.40	232.52	-167.72	0.00	78.54	5.94	88.83
78	2023.81	2	SLE P	-66454.90	258.20	-186.25	0.00	78.54	5.57	83.23
79	2083.33	2	SLE R	-61705.00	254.43	-183.53	0.00	78.54	5.18	77.4
80	2142.86	2	SLE B	-56958.30	228.43	-164.78	0.00	78.54	4.78	71.4
81	2202.38	2	SLE B	-52214.80	187.36	-135.15	0.00	78.54	4.36	65.28
82	2261.90	2	SLE R		138.24	-99.72	0.00	78.54	3.95	59.0
83	2321.43	2	SLE B	-42735.80	88.05	-63.51	0.00	78.54	3.53	52.80
84	2380.95	2	SLE R	-37999.90	43.70	-31.52	0.00	78,54	3.12	46.7
85	2440.48	2	SLE R	-33266.00	12,07	-8.70	0.00	78.54	2.71	40.66
86	2500.00	2	SLE B	-28533.90	0.00	0.00	0.00	78,54	2.32	34.79
87	0.00	4	SLE Q	-213163.00	-21166.00	15267.70	0.00	78.54	30.83	443.6
88	59.52	4	SLE Q	-212890.00	-23012.70	16599,70	0.00	78.54	31.99	459.30
89	119.05	4	SLE C	-210666.00	-24285.80	17518.10	0.00	78,54	32.62	467.64
90	178.57	4	SLE C		-25064.60	18079.80	0.00	78,54	32.94	471.70

							Rela	zion	e di calco	olo
91	238.09	4	SLE Q	-206239,00	-25422.50	18338.00	0.00	78.54	32.99	472.11
92	297.62	4	SLE Q	-204035.00	-25427.30	18341.50	0.00	78.54	32.B1	469.47
93	357.14	4	SLE Q	-201838.00	-25112.90	18114.70	0.00	78,54	32.43	464.06
-94	416.67	4	SIE Q	-196891.00	-24429.80	17622.00	0.00	78.54	31.59	452.10
95	476.19	4	SLE C	-191954.00	-23429.20	16900.20	0.00	78.54	30.56	437.39
96	535.71	4	SLE Q	-187028.00	-22187.00	16004.20	0.00	78.54	29.36	420.61
97	595,24	4	SLE Q	-182112.00	-20769.80	14981.90	0.00	78.54	28.06	402.31
98	654.76	4	SLE Q	-177206.00	-19235,20	13874.90	0.00	78.54	26.68	383.01
99	714.29	4	SLE C	-172309.00	-17632.70	12719.00	0.00	78.54	25.26	363.13
100	773.81	4	SLE Q	-167421.00	-16004.10	11544.20	0.00	78.54	23.82	343.04
101	833.33	4	SLE Q	-162542.00	-14384.20	10375,70	0.00	78.54	22.39	323.03
102	892,86	4	SLE Q	-157672.00	-12801.30	9233.99	0.00	78+54	20.99	303.35
103	952.38	4	SLE Q	-152811.00	-11278.20	8135.32	0.00	78.54	19.62	284.20
104	1011.90	4	SLE Q	-147958.00	-9832.42	7092.42	0.00	78.54	18.30	265.74
105	1071.43	4	SLE Q	-143112.00	-8477.01	6114.72	0.00	78.54	17.04	248.06
106	1130.95	4	SLE Q	-138275.00	-7221.16	5208.84	0.00	78.54	15.85	231.27
107	1190,48	4	SLE Q	-133444.00	-6070.65	4378.94	0.00	78.54	14.72	215,39
108	1250.00	4	SLE Q	-128621.00	-5028.41	3627,14	0.00	78.54	13.66	200.47
109	1309.52	4	SLE Q	-123805.00	-4094.94	2953.80	0.00	78.54	12.68	186.49
110	1369.05	4	SLE Q	-118995.00	-3268.74	2357.84	0.00	78.54	11.76	173,46
111	1428.57	4	SLE Ç	-114192.00	-2546.68	1836.99	0.00	78.54	10.91	161.33
112	1488.10	4	SLE C	-109395.00	-1924.33	1388.07	0.00	78.54	10.12	150.08
113	1547.62	-4	SLE Q	-104604.00	-1396.25	1007.15	0.00	78.54	9.39	139.66
114	1607.14	4	SLE Q	-99818.40	-956.23	689.75	0.00	78.54	8.72	130.00
115	1666.67	4	SLE Q	-95038.20	-597.51	431.00	0.00	78,54	8.11	121.06
116	1726.19	4	SLE C	-90263.00	-312,95	225.74	0.00	78,54	7.54	112.77
117	1785.71	- 4	SLE Q	-85492.80	-95.18	68.66	0.00	78.54	7.01	105.06
118	1845.24	4	SLE Q	-80727.00	63.30	-45.66	0.00	78.54	6.60	98.97
119	1904.76	4	SLE Q	-75965.70	170.03	-122.65	0.00	78.54	6.28	94.09
120	1964.29	4	SLE Q	-71208.40	232,52	-167,72	0.00	78.54	5.94	88.82
121	2023.81	4	SLE Q	-66454.90	258,20	-186,25	0.00	78.54	5.57	83.25
122	2083.33	4	SLE Q	-61705.00	254.43	-183,53	0.00	78,54	5.18	77.43
123	2142.86	4	SLE Q	-56958.30	228.43	-164.78	0.00	78.54	4.78	71.41
124	2202.38	4	SLE Q	-52214.80	187.36	-135,15	0.00	78+54	4.36	65.28
125	2261.90	4	SIE Q	-47474.00	138,24	-99,72	0.00	78.54	3.95	59.07
126	2321.43	4	SLE Q	-42735,80	88.05	-63.51	0.00	78,54	3,53	52.86
127	2380.95	4	SLE Q	-37999.90	43.70	-31.52	0.00	78.54	3.12	46.71
128	2440.48	4	SIE Q	-33266.00	12.07	-8.70	0.00	78.54	2.71	40.66
_		_								

Verifiche principali

Caso	Tipo										
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio										
- 6	SLU N cost - min. sic.										
48	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)										
4.9	C.Rare - Sc max (min. compr.)										
51	C.Rare - Sf max (max traz.)										
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)										
.92	C.Q.Per Sc max (min. compr.)										
94	C.Q.Per Sf max (max traz.)										

Palo n. 27

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <om></om>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>	
60.00	6.00	C30/37	307.10	20,59	174.02	13.73	8450C	4300.00	3913.04	

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 27 (-143)

Caso	8	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <dann></dann>	My <danm></danm>	
1	1	SIA	RVN	253546.00	6224.89	820.64	32975.90	32425.90	
	1	SIA	TAG				0.00	0.00	
	1	SLU	ECC				0.00	0.00	
	1	SLU	TOT	253546.00	6224.89	820.64	32975.90	32425.90	
- 2	2	SLE R	RVN	187812.00	4611.03	607.88	24426.60	24019.20	
	. 2	SLE R	TAG				0.00	0.00	
	2	SLE R	ECC		·		0.00	0.00	
	2	SLE R	TOT	187812.00	4611.03	607.88	24426.60	24019.20	

14		4.1					2		
3	3	SIE	F	RVN	187812.00	4611.03	607.88	24426.60	24019.20
	3	SLE	F	TAG		J		0.00	0.00
	3	SLE	F	ECC				0.00	0.00
	3	SLE	F	TOT	187812.00	4611.03	607.88	24426.60	24019.20
4	-4	SLE	Q	RVN	187812.00	4611.03	607.88	24426.60	24019.20
	4	SLE	Q	TAG				0.00	0.00
	4	SLE	Q	ECC	1	(V		0.00	0.00
	.4	SLE	Q	TOT	187812.00	4611.03	607.88	24425.50	24019.20

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	. 1	-253546.00	-6224.89	-B20.64	-32975.90	-32425.90
- 2	2	SLE R	1	-187812.00	-4611.03	-607,88	-24426.60	-24019.20
- 3	3	SLE F	- 1	-187812.00	-4611.03	-607,88	-24426.60	-24019.20
.4	4	SLE Q	1	-187812.00	-4611.03	-607.88	-24426.60	-24019.20

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	oc	TCC	M	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SLU	-253546.00	32830.80	-32283.20	-253546.00	172466.00	-169357.00	2-3	224.38	5.250
2	59,52	1	SLU	-252992.00	35060.50	-34475.70	-252992.00	172335.00	-169241.00	2-3	224.38	4.912
- 3	119.05	1	SLU	-250208.00	36499.30	-35890.50	-250208.00	171676.00	-168660.00	2-3	224.38	4.701
-4	178.57	1	SLU	-247432.00	37259.90	-36638.40	-247432.00	171017.00	-168079.00	2-3	224.38	4.589
.5	238.09	1	SLU	-244664.00	37446.60	-36822.00	-244664.00	170387.00	-167429.00	2-3	224.38	4.549
- 6	297.62	1	SLU	-241904.00	37154.90	-36535.10	-241904.00	169763.00	-166769.00	2-3	224.38	4.56
7	357,14	1	SLU	-239151.00	36434.70	-35826.90	-239151.00	169140.00	-166111.00	2-3	224.38	4.639
- 8	416,67	1	SLU	-233256.00	35224.40	-34636.90	-233256.00	167798.00	-164687.00	2-3	224.38	4.759
.9	476.19	1	SILI	-227373.00	33597.20	-33036.90	-227373.00	166453.00	-163260.00	2-3	224.38	4.948
10	535.71	1	SLU	-221503.00	31658.50	-31130.50	-221503.00	165103.00	-161826.00	2-3	224.38	5.207
11	595.24	1	SLU	-215644.00	29500.20	-29008.10	-215644.00	162111.00	-162183.00	2-3	225.00	5.543
12	654.76	1	SLU	-209797.00	27201.60	-26747.90	-209797.00	160727.00	-160747.00	2-3	225.00	5.959
13	714.29	1	SLU	-203961.00	24830.40	-24416.20	-203961.00	159338.00	-159303.00	2-3	225.00	6.470
14	773.81	1	SIJ	-198136.00	22443.30	-22069.00	-198136.00	157947.00	-157857.00	2-3	225.00	7.095
15	833.33	1	SIJJ	-192321.00	20087.30	-19752.20	-192321.00	156549.00	-156402.00	2-3	225.00	7.85
16	892.86	1	SLU	-186517.00	17800.30	-17503.40	-186517.00	155149.00	-154945.00	2-3	225.00	8.783
1.7	952.38	1	SIJ	-180723.00	15612.20	-15351.80	-180723.00	153744.00	-1534B3.00	2-3	225.00	9.922
18	1011.90	1	SIAI	-174939.00	13545.90	-13320.00	-174939.00	152335.00	-152015.00	2-3	225.00	11.328
19	1071,43	1	SIU	-169164.00	11618.10	-11424.30	-169164.00	150924,00	-150544.00	2-3	225.00	13.083
20	1130,95	1	SLU	-163398.00	9840.08	-9675.95	-163398.00	149508.00	-149066.00	2-3	225.00	15.298
21	1190.48	1	SIU	-157641.00	8218.40	-8081.32	-2571250.00	148090.00	-147586.00	2-3	225,00	16.311
22	1250.00	1	SIAI	-151892.00	6755.81	-6643.13	-2571250.00	146667.00	-146099.00	2-3	225.00	16.928
23	1309.52	1	SIJ	-146152.00	5451.76	-5360.83	-2571250.00	145241.00	-144609.00	2-3	225.00	17.593
24	1369.05	1	SIU	-140419.00	4303.01	-4231.23	-2571250.00	143812.00	-143114.00	2-3	225.00	18.311
25	1428.57	1	SLU	-134694.00	3304.14	-3249.03	-2571250.00	142380.00	-141615.00	2-3	225.00	19.090
26	1488.10	1	SLU	-128976.00	2448.05	-2407,22	-2571250.00	140945.00	-140113.00	2-3	225.00	19.936
2.7	1547.62	1	SIU	-123265.00	1726,29	-1697.50	-2571250.00	139341.00	-138693.00	2-3	225.00	20.860
28	1607.14	1	SLU	-117560.00	1129.46	-1110.62	-2571250.00	137710.00	-137284.00	2-3	225.00	21.872
29	1666.67	1	SIJ	-111862.00	647.48	-636.67	-2571250.00	136066.00	-135872.00	2-3	225.00	22.986
30	1726.19	1	SLU	-106170.00	269.79	-265.29	-2571250.00	134417.00	-134458.00	2-3	225.00	24.218
31	1785,71	1	SLU	-100484.00	-14.39	14.15	-2571250.00	-132875.00	132701.00	2-3	45.00	25,589
32	1845.24	1	SLU	-94802.70	-215.96	212.36	-2571250.00	-131383.00	131089.00	2-3	45.00	27.122
33	1904.76	1	SLU	-89126.80	-345.81	340.04	-2571250.00	-129888.00	129473.00	2-3	45.00	28.849
34	1964.29	1	SLU	-83455.60	-414.74	407.82	-2571250.00	-128382.00	127855.00	2-3	45.00	30.810
35	2023.81	1	SIU	-77789.00	-433.42	426.19	-2571250.00	-126844.00	126243.00	2-3	45.00	33.054
36	2083.33	1	SIU	-72126.50	-412.32	405.45	-2571250.00	-125304.00	124628.00	2-3	45.00	35.649
37	2142.86	1	SLU	-66467,80	-361.79	355.75	-2571250.00	-123759.00	123005.00	2-3	45.00	38.684
38	2202.38	1	SLU	-60812.70	-291.95	287.08	-2571250.00	-122212.00	121380.00	2-3	45.00	42.281
39	2261.90	1	SIJ	-55160.90	-212.83	209.28	-2571250.00	-120660.00	119747.00	2-3	45.00	46.614
40	2321,43	1	SLU	-49512.10	-134.30	132.06	-2571250.00	-119020.00	118162.00	2-3	45.00	51.932
41	2380.95	1	SLU	-43865.90	-66,16	65.06	-2571250.00	-117253.00	116641.00	2-3	45.00	58.616
42	2440.48	1	SIJJ	-38222.00	-18.16	17.86	-2571250.00	-115475.00	115118.00	2-3	45.00	67.271
43	2500.00	1	SLU	-32580.20	0.00	0.00	-2571250.00					78.921

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SIA	6224.89	820.64	0.85	11.31	6278.75	1.00	32294.70	367986.00	32294.70	5.144
2	59.52	1	SIU	4239,23	558.87	0.85	11.31	4275.91	1.00	32294.70	367906.00	32294.70	7.553
- 3	119.05	1	SIJ	2526.60	333.09	0.85	11.31	2548.47	1.00	32294.70	367508.00	32294.70	12.672
4	178.57	1	SIU	1067.49	140.73	0.85	11.31	1076.73	1.00	32294.70	367110.00	32294.70	29.993
5	238.09	1	SLU	-158.20	-20.86	0.85	11,31	159.57	1.00	32294.70	366714.00	32294.70	>100
.6	297.62	1	SIU	-1170.83	-154.35	0.85	11.31	1180.96	1.00	32294.70	366318.00	32294.70	27.346
7	357.14	1	SIJ	-2249.97	-296.62	0.85	11.31	2269.43	1.00	32294.70	365924.00	32294.70	14,230

-	Berlin Control Control Control	1.1	Particular Company
Pa	azione	di co	COLO
176	COLUMB CO.	UII GO	K A JIC

Relazione di calcolo													
- 8	416.67	1	SLU	-3357.71	-442.66	0.85	11.31	3386.76	1.00	32294.70	365080.00	32294.70	9.536
9	476.19	1	SIJ	-4203.21	-554.12	0.85	11.31	4239.58	1.00	32294.70	364237.00	32294.70	7.617
1.0	535.71	1	SIU	-4818.54	-635.24	0.85	11.31	4860.23	1.00	32294.70	363396.00	32294.70	6.645
11	595.24	1	SIU	-5234.08	-690.02	0.85	11.31	5279.37	1.00	32294.70	362557.00	32294.70	6.117
12	654.76	1	SLU	-5478.32	-722.22	0.85	11.31	5525.72	1.00	32294.70	361719,00	32294.70	5.844
13	714.29	1	SLU	~5577.63	-735.32	0.85	11.31	5625.89	1.00	32294.70	360883.00	32294.70	5.740
14	773.81	1	SLU	-5556.23	-732.49	0.85	11.31	5604.31	1.00	32294.70	360049.00	32294.70	5.762
15	833.33	1	SIU	-5436.10	-716.66	0.85	11.31	5483.14	1.00	32294.70	359216.00	32294.70	5.B90
1.6	892.86	1	SLU	~5237.01	-690.41	0.85	11.31	5282.33	1.00	32294.70	358385.00	32294.70	6.114
17	952.38	-1	SLU	-4976.57	-656.08	0.85	11.31	5019.63	1.00	32294.70	357555.00	32294.70	6.434
18	1011.90	1	SLU	-4670.30	-615.70	0.85	11.31	4710.71	1,00	32294.70	356726.00	32294.70	6.856
19	1071.43	1	SLU	-4331.74	-571.07	0.85	11.31	4369.22	1.00	32294.70	355899,00	32294.70	7.391
20	1130.95	1	SIJ	-3972.56	-523.71	0.85	11.31	4006.93	1.00	32294.70	355073.00	32294.70	8.060
21	1190.48	-1	SLU	-3602.71	-474.96	0.85	11.31	3633.89	1.00	32294.70	354248,00	32294.70	8.887
22	1250.00	1	SLU	-3230.58	-425.90	0.85	11.31	3258.53	1.00	32294.70	353425.00	32294.70	9.911
23	1309.52	1	SLU	-2863.08	-377.45	0.85	11.31	2887.86	1.00	32294.70	352603.00	32294.70	11.183
-24	1369.05	1	SIJ	-2505,88	-330.36	0.85	11.31	2527.56	1.00	32294.70	351782,00	32294.70	12.777
25	1428.57	1	SLU	-2163.48	-285.22	0.85	11.31	2182.20	1.00	32294.70	350962.00	32294.70	14.799
26	1488,10	1	SLU	-1839.39	-242.49	0.85	11.31	1855.30	1.00	32294.70	350143,00	32294.70	17.407
27	1547.62	1	SLU	-1536.25	-202.53	0.85	11.31	1549.55	1.00	32294.70	349324.00	32294.70	20,841
28	1607.14	1	SLU	-1255,99	-165.58	0.85	11.31	1266.86	1.00	32294.70	348507.00	32294.70	25,492
29	1666.67	1	SIU	-999.91	-131.82	0.85	11.31	1008.56	1.00	32294.70	347691.00	32294.70	32.021
30	1726.19	1	SIU	-768.81	-101.35	0.85	11.31	775.46	1.00	32294.70	346876.00	32294.70	41.646
31	1785.71	1	SLU	-563.09	-74.23	0.85	11,31	567.96	1.00	32294.70	346061.00	32294.70	56,861
32	1845.24	1	SIU	-382,86	-50.47	0.85	11,31	386.17	1.00	32294.70	345248.00	32294.70	83.628
.33	1904.76	1	SIU	-227.99	-30.06	0.85	11.31	229.96	1.00	32294.70	344435.00	32294.70	>100
34	1964.29	1	SLU	-98,20	-12.95	0.85	11.31	99.05	1.00	32294.70	343622.00	32294.70	>100
35	2023.81	1	SEU	6.87	0.91	0.85	11.31	6.93	1.00	32294.70	342811.00	32294.70	>100
36	-	1	SIU	87.64	11.55	_		88.40	1.00	32294.70	341999.00	32294.70	>100
37	2142,86	1	SIJ	144.51	19.05	0.85	11.31	145.76	1.00	32294.70	341189,00	32294.70	>100
38		1	SLU	177.85	23.45	0.85	_	179.38	1,00	32294.70	340379.00		>100
39	2261,90	_1	SLU	187.96	24.78	0.85	11.31	189.59	1.00	32294.70	339569,00	32294.70	>100
40	2321.43	1	SIJ	175.10	23.08	0.85	11,31	176.62	1.00	32294.70	338760.00	32294.70	>100
41	2380.95	1	SLU	139.44	18.38	0.85	11.31	140.64	1.00	32294.70	337951.00	32294.70	>100
42	2440.48	1	SLU	81.05	10.69	0.85	11.31	81.76	1.00	32294.70	337143.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <cmq></cmq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-187812.00	-23913.50	24319.10	9.42	69.11	32.79	469.02
45	59.52	2	SLE R	-187715,00	-25537.60	25970.70	12,57	65,97	34.07	486.57
46	119.05	2	SLE R	-185843.00	-26585.60	27036.50	15.71	62.83	34.82	496.47
47	178.57	2	SLE R	-183977,00	-27139.60	27599.90	15.71	62.83	35.17	501.06
48	238.09	2	SLE R	-182117.00	-27275,50	27738,20	15.71	62.83	35.17	500.87
49	297,62	2	SLE R	-180262.00	-27063.10	27522.10	15.71	62.83	34.87	496.55
50	357.14	2	SLE R	-178413.00	-26538.50	26988.60	15.71	62.83	34.30	488.51
51	416.67	2	SLE R	-174061.00	-25656.90	26092.20	15.71	62.83	33.26	473.82
52	476.19	2	SLE R	-169719.00	-24471.70	24886.80	15.71	62.83	31.96	455.63
53	535,71	2	SLE B	-165386.00	-23059,60	23450.70	15.71	62.83	30.48	434.97
54	595.24	2	SLE R	-161061.00	-21487.50	21852,00	9.42	69.11	28.89	412.80
55	654.76	2	SLE R	-156746.00	-19813.20	20149.30	9.42	69,11	27.25	389.90
56	714.29	2	SLE R	-152438.00	-18086.10	18392.90	0.00	78.54	25.60	366.88
57	773.81	2	SLE R	-148139.00	-16347.40	16624.70	0.00	78.54	23.98	344.14
58	833.33	2	SLE R	-143848.00	-14631.30	14879.50	0.00	78,54	22.37	321.74
59	892.86	2	SLE R	-139564.00	-12965.50	13185.40	0.00	78.54	20.81	299.86
60	952.38	2	SLE R	-135288.00	-11371.70	11564,60	0.00	78.54	19.30	278.70
61	1011.90	2	SLE R	-131019.00	-9866.65	10034.00	0.00	78,54	17.85	258.44
62	1071.43	2	SLE R	-126758.00	-8462.48	8606.03	0.00	78.54	16.48	239.20
63	1130.95	2	SLE R	-122503.00	-7167.37	7288.95	0.00	78.54	15.19	221.06
64	1190.48	2	SLE R	-118254.00	-5986.16	6087.71	0.00	78.54	13.98	204.06
65	1250.00	2	SLE R	-114012.00	-4920.83	5004,31	0.00	78.54	12.86	188.23
66		2	SLE B	-109776.00	-3970.98	4038.34	0.00	78.54	11.82	173.56
67	1369.05	2	SLE R	-105546.00	-3134.25	3187.41	0.00	78,54	10.87	160.04
-68	1428.57	2	SLE R	-101322.00	-2406.69	2447.51	0.00	78,54	9,99	147.61
59	1488.10	2	SLE R	-97102.80	-1783.12	1813.37	0.00	78.54	9.19	136.23
70	1547.62	2	SLE R	-92889.10	-1257.40	1278.73	0.00	78.54	8.47	125.83
71	1607.14	2	SLE R	-88680.30	-822,68	836.64	0.00	78.54	7.81	116.35
72	1666.67	2	SLE R	-84476.30	-471.61	479.61	0.00	78.54	7.21	107.72
73	1726.19	2	SLE R	-80276.80	-196.51	199.84	0.00	78.54		99.84
74	1785.71	2	SLE R	-76081.70	10.48	-10.66	0.00	78.54	6.19	92.87
75	1845.24	2	SLE R	-71890.60	157.30	-159.97	0.00	78.54	5.96	89.23
76	1904.76	2	SLE R	-67703.30	251.88	-256,15	0.00	78.54	5,69	85.07
77	1964.29	2	SLE R	-63519.70	302.09		0.00	78,54		80.48
78	2023.81	2	SLE R	-59339.50	315.69	-321.05	0.00	78.54	5.05	75.52
79		2	SLE R	-55162.50	300.33	-305.43	0.00	78.54	4.70	70.27
80	2142.86	2	SLE R	-50988.50	263.52	-267.99	0.00	78,54		64.81
81	2202.38	2	_	-46817.10	212.66		0.00	78,54		59.21

Relazione	di	calcolo	î
1 CIGATORIC	u	Calcolo	

							Rela	izion	e di calci	Olo
82	2261.90	2	SLE R	-42648.30	155.02	-157.65	0.00	78.54	3.58	53.55
83	2321.43	2	SLE R	-38481.80	97.82	-99.48	0.00	78.54	3.20	47.90
84	2380.95	2	SLE R	-34317.40	48.19	-49.01	0.00	78,54	2.82	42.32
85	2440.48	2	SLE R	-30154.70	13.23	-13.45	0.00	78.54	2.46	36.90
86	2500,00	2	SLE R	-25993.70	0.00	0.00	0.00	78.54	2.11	31.69
87	0.00	4	SLE Q	-187812.00	-23913.50	24319.10	9.42	69.11	32.79	469.02
88	59,52	4	SLE Q	-187715.00	-25537.60	25970.70	12.57	65,97	34.07	486.57
89	119.05	4	SLE Q	-185843.00	-26585,60	27036.50	15.71	62,83	34.82	496.47
90	178.57	4	SLE Q	-183977.00	-27139.60	27599.90	15.71	62.83	35.17	501.06
91	238.09	4	SLE Q	-182117.00	-27275.50	27738.20	15.71	62.83	35.17	500.87
92	297.62	4	SLE Q	-180262.00	-27063.10	27522,10	15.71	62.83	34.87	496.55
93	357.14	4	SLE Q	-178413.00	-26538.50	26988.60	15.71	62.83	34.30	488.51
94	416.67	4	SLE Q	-174061.00	-25656.90	26092.20	15.71	62.83	33.26	473.82
95	476.19	4	SLE Q	-169719.00	-24471.70	24886.80	15.71	62,83	31.96	455.63
96	535.71	4	SLE Q	-165386.00	-23059.60	23450.70	15.71	62.83	30.48	434.97
97	595.24	4	SLE Q	-161061.00	-21487.50	21852.00	9.42	69.11	28.89	412.80
98	654.76	4	SLE Q	-156746.00	-19813,20	20149.30	9,42	69,11	27.25	389,90
99	714.29	4	SLE Q	-152438.00	-18086.10	18392.90	0.00	78.54	25.60	366.88
100	773.81	4	SLE Q	-148139,00	-16347.40	16624.70	0.00	78.54	23.98	344.14
101	833.33	4	SLE Q	-143848.00	-14631.30	14879.50	0.00	78.54	22.37	321.74
102	892.86	4	SLE Q	-139564.00	-12965.50	13185.40	0.00	78.54	20.81	299.86
103	952.38	-4	SLE Q	-135288.00	-11371.70	11564.60	0.00	78.54	19.30	278.70
104	1011.90	4	SLE Q	-131019.00	-9866.65	10034.00	0.00	78,54	17.85	258.44
105	1071.43	4	SLE Q	-126758.00	-8462.48	8606.03	0.00	78.54	16.48	239.20
106	1130.95	4	SLE Q	-122503.00	-7167.37	7288.95	0.00	78,54	15.19	221.06
107	1190.48	4	SLE Q	-118254.00	~5986.16	6087.71	0.00	7B ₊ 54	13.98	204.06
108	1250.00	- 4	SLE Q	-114012.00	~4920.83	5004.31	0.00	78,54	12.86	188.23
109	1309.52	4	SLE Q	-109776.00	-3970.98	4038.34	0.00	78.54	11.82	173.56
110	1369.05	4	SLE Q	-105546.00	-3134.25	3187.41	0.00	78.54	10.87	160.04
111	1428.57	4	SLE Q	-101322.00	-2406,69	2447.51	0.00	78.54	9.99	147,61
112	1488.10	4	SLE Q	-97102.80	-1783,12	1813,37	0.00	78.54	9.19	136.23
113	1547.62	4	SLE Q	-92889.10	-1257.40	1278.73	0.00	78.54	8.47	125.83
114	1607.14	4	SLE Q	-88680.30	-822.68	836.64	0.00	78.54	7.81	116.35
115	1666.67	4	SLE Q	-84476.30	-471.61	479.61	0.00	78+54	7.21	107.72
116	1726.19	4	SIE Q	-80276.80	-196.51	199.84	0.00	78.54	6.67	99.84
117	1785,71	4	-	-76081.70	10,48	-10.66	0,00	78,54	6.19	92.87
	1845.24	-	SLE Q	-71890.60	157.30	-159.97	0.00		5.96	89.23
119	1904.76	4	-	-67703.30	251.88	-256,15	0.00	78,54	5.69	85.07
120	1964,29	-	SLE Q	-63519.70	302.09	-307,21	0.00	78,54	5.38	80.48
121	2023.81	4	-	-59339,50	315.69	-321.05	0.00	78,54	5.05	75.52
122	2083.33	-	SLE Q	-55162.50	300.33	-305.43	0.00	78.54	4.70	70.27
123	2142.86	4	-	-50988.50	263.52	-267.99	0.00	78.54	4.34	64.81
- Interest	2202,38	-	SLE Q	-46817.10	212,66	-216,26		78.54	3.96	59.21
125	-	_	SLE Q	-42648.30	155.02	-157.65	0.00	-	3,58	53.55
	2321.43	_	SLE Q	-38481.80	97.82	-99,48	0.00		3.20	47.90
127		4	- K	-34317.40	48,19	-49.01	0.00	78.54	2.82	42132
-	2440.48	_	SLE Q	-30154.70	13.23	-13.45	-	78.54	2.46	36.90
129	2500.00	4	SLE Q	-25993.70	0.00	0,00	0.00	78,54	2,11	31,69

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	Фед	Δ _{BM}	A _B <cmq></cmq>	Ac eff <mq></mq>	σ _S <dan cmq=""></dan>	€ _{SM}	Wk <mm></mm>
90	178.57	4	SLE Q	-183977.00	27599.90	-27139.60	46.00	136.36	0.50	20.00	212.54	3,14	189.34	58.47	0.02	0.01
91	238.09	4	SLE Q	-182117.00	27738,20	-27275.50	46.00	136.36	0.50	20.00	222,45	3.14	204.91	63.59	0.02	0.01
92	297.62	4	SLE Q	-180262.00	27522.10	-27063.10	46.00	136.36	0.50	20.00	224.06	3.14	207.44	63.87	0.02	0.01
93	357.14	4	SLE Q	-178413.00	26988.60	-26538.50	46.00	136.36	0.50	20.00	217.93	3.14	197.81	59.75	0.02	0.01
94	416.67	4	SLE Q	-174061.00	26092.20	-25656.90	46.00	136,36	0.50	20.00	212.04	3.14	188.56	55.05	0.02	0.01
95	476.19	4	SLE Q	-169719.00	24886,80	-24471.70	46.00	136,36	0.50	20.00	198.30	3.14	166.98	46.30	0.01	0.00
133	178.57	3	SLE F	-183977.00	27599.90	-27139.60	46.00	136.36	0.50	20.00	212.54	3.14	189.34	58.47	0.02	0.01
134	238.09	3	SLE F	-182117.00	27738.20	-27275.50	46.00	136.36	0.50	20.00	222.45	3.14	204.91	63.59	0.02	0.01
135	297,62	3	SLE F	-180262.00	27522.10	-27063.10	46.00	136.36	0.50	20.00	224.06	3.14	207.44	63.87	0.02	0.01
136	357.14	3	SLE F	-178413.00	26988.60	-26538.50	46.00	136,36	0.50	20.00	217.93	3,14	197.81	59.75	0.02	0.01
137	416.67	3	SLE F	-174061.00	26092.20	-25656.90	46.00	136,36	0.50	20.00	212.04	3.14	188.56	55.05	0.02	0.01
138	476.19	3	SLE F	-169719.00	24886.80	-24471.70	46.00	136.36	0.50	20.00	198.30	3.14	166.98	46.30	0.01	0.00

Verifiche principali

Caso	Tipo										
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio										
. 5	SLU N cost - min. sic.										
47	C.Rare - Sf min (max compr.)										
48	C.Rare - Sc min (max compr.)										
49	C.Rare - Sf max (max traz.)										
57	C.Rare - Sc max (min. compr.)										
90	C.Q.Per Sf min (max compr.)										
91	C.Q.Per Sc min (max compr.)										
92	C.Q.Per Sf max (max traz.), C.Q.Per Wk Max										
100	C.Q.Per Sc max (min. compr.)										

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Palo n. 28

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Cf <om></om>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 28 (-127)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
-1	1	SLU	RVN	212189.00	6476.40	929.59	44873.60	30881.60
	1	SIJJ	TAG	-	() ()		0.00	0.00
	1	SLU	ECC				0.00	0.00
	1	SLU	TOT	212189.00	6476.40	929.59	44873.60	30881.60
- 2	2	SLE R	RVN	157177.00	4797.33	688.59	33239.70	22875.20
	2	SLE R	TAG				0.00	0.00
	2	SLE R	ECC	3			0.00	0.00
	2	SLE R	TOT	157177.00	4797.33	688.59	33239.70	22875.20
3	3	SLE F	RVN	157177.00	4797.33	688.59	33239,70	22875.20
	. 3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	157177.00	4797.33	688.59	33239.70	22875.20
-4	-4	SLE Q	RVN	157177.00	4797.33	688.59	33239,70	22875.20
.31	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC	100	9 9	- 8	0.00	0.00
	4	SIE Q	TOT	157177.00	4797.33	688.59	33239.70	22875.20

Sollecitazioni nei pali

Caso	cc	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-212189.00	-6476.40	-929.59	-44873.60	-30881.60
2	2	SLE R	1	-157177.00	-4797.33	-688,59	-33239.70	-22875.20
- 3	3	SLE F	1	-157177.00	-4797.33	-688,59	-33239.70	-22875.20
4	. 4	SLE Q	1	-157177.00	-4797.33	-688,59	-33239.70	-22875.20

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SIU	-212189.00	44686.90	-30753.10	-212189.00	186851.00	-130640.00	2-3	215.00	4,203
2	59.52	1	SLU	-211922.00	47335.00	-32575.50	-211922.00	186776.00	-130590.00	2-3	215.00	3.966
3	119.05	1	SLU	-209712.00	48966.70	-33698.50	-209712.00	186147.00	-130173.00	2-3	215.00	3.821
-4	178.57	1	SIU	-207509.00	49729.40	-34223.30	-207509.00	185516.00	-129755.00	2-3	215.00	3.750
- 5	238.09	1	SIU	~205312.00	49758.80	-34243.50	~205312.00	184887.00	-129338.00	2-3	215.00	3.735
.6	297.62	1	SLU	-203122,00	49179.40	-33844.BO	-203122.00	184261.00	-128924.00	2-3	215.00	3.767
7	357.14	1	SLU	-200938.00	48057.30	-33072.60	-200938.00	183633.00	-128507.00	2-3	215.00	3.842
.8	416.67	1	SIU	-196013.00	46318.20	-31875.70	-196013.00	182211.00	-127567.00	2-3	215.00	3.956
9	476.19	1	SLU	-191100.00	44057.60	-30320.00	-191100.00	180790.00	-126627.00	2-3	215.00	4.127
1.0	535.71	1	SLU	-186196.00	41411.40	-28499.00	-186196.00	179362.00	-125584.00	2-3	215.00	4.357
11	595.24	1	SIJ	-181303.00	38498.00	-26494.00	-181303.00	177933.00	-124741.00	2-3	215.00	4.650
12	654.76	1	SLU	-176419.00	35419.20	-24375.20	-176419.00	177837,00	-121795.00	2-3	214.38	5,013
13	714.29	1	SLU	-171545,00	32261.40	-22202.00	-171545,00	176397.00	-120855.00	2-3	214.38	5.460
14	773.81	1	SLU	-166680.00	29097.10	-20024.30	-166680.00	174953.00	-119913.00	2-3	214.38	6.005
15	833.33	1	SLU	-161824.00	25985.70	-17883.10	-161824.00	173506.00	-118970.00	2-3	214.38	6.669
16	892.86	1	SEU	+156976.00	22975.20	-15811.30	-156976.00	172096.00	-118025.00	2-3	214.38	7.481
17	952.38	1	SLU	-152137.00	20103.30	-13834,90	-152137.00	170602.00	-117080.00	2-3	214.38	8.479
18	1011,90	1	SIJ	-147307.00	17398.30	-11973.40	-147307.00	169146.00	-116134.00	2-3	214.38	9.715
19	1071.43	1	SLU	-142484.00	14880.80	-10240.80	-142484.00	167686.00	-115187.00	2-3	214.38	11.262
20	1130.95	1	SLU	-137668.00	12564.20	-8646.58	-137668.00	166223.00	-114239.00	2-3	214.38	13.224
21	1190.48	1	SIAI	-132860.00	10456.20	-7195.85	-132860.00	164757.00	-113290.00	2-3	214.38	15.753
22	1250.00	1	SLU	-128060.00	8559.30	-5890.43	-128060.00	163289.00	-112340.00	2-3	214.38	19.076
23	1309.52	1	SIU	-123266.00	6872.00	-4729.25	-2571250.00	161816.00	-111389.00	2-3	214.38	20.859
24	1369.05	1	SLU	-118478.00	5389.33	-3708.89	-2571250.00	160390.00	-110283.00	2-3	214.38	21.702
25	1428.57	1	SLU	-113698.00	4103.58	-2824.05	-2571250.00	158964.00	-109157.00	2-3	214.38	22.615

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26	1488.10	1	SLU	-108923.00	3004.91	-2067.95	-2571250.00	157536.00	-108029.00	2-3	214.38	23.606
27	1547.62	1	SLU	-104154.00	2081.85	-1432.71	-2571250.00	154909.00	-108553.00	2-3	215.00	24.687
28	1607.14	1	SILI	-99390.30	1321.72	-909.60	-2571250.00	153481.00	-107408.00	2-3	215.00	25.870
29	1666.67	1	SLU	-94632.20	711.04	-489.33	-2571250.00	152050.00	-106257.00	2-3	215.00	27.171
30	1726.19	1	SLU	-89879.20	235.78	-162.26	-2571250.00	150617.00	-105103.00	2-3	215.00	28.608
31	1785.71	1	SLU	-85131.00	-118.35	81.45	-2571250.00	-149783.00	102830.00	2-3	34.38	30.203
32	1845,24	1	SIJ	-80387.40	-365.74	251.70	-2571250.00	-148217.00	101818.00	2-3	34.38	31.986
33	1904.76	Ĭ	SLU	-7564B.10	-520.72	358.35	-2571250.00	-146649.00	100804.00	2-3	34.38	33.990
34	1964.29	1	SLU	-70912.80	-597.48	411.18	-2571250.00	-145076.00	99788.40	2-3	34.38	36.259
35	2023.81	1	SIJJ	-66181.40	-609.99	419.79	-2571250.00	-143500.00	98770.50	2-3	34.38	38.852
36	2083.33	1	SLU	-61453.50	-572.00	393.65	-2571250.00	-141921.00	97751.00	2-3	34.38	41.841
37	2142.86	1	SLU	-56728.90	-496.99	342.02	-2571250.00	-140337.00	96729.40	2-3	34.38	45,325
38	2202.38	1	SIAJ	-52007.30	-398.21	274.04	-2571250.00	-138751.00	95706.40	2-3	34.38	49,440
39	2261,90	1	SLU	-47288.50	-288.72	198.69	-2571250.00	-137160.00	94681.40	2-3	34.38	54.374
40	2321.43	1	SIU	-42572.30	-181.41	124.85	-2571250.00	-135621.00	93496.40	2-3	34.38	60.397
41	2380.95	1	SILI	-37858.40	-89.06	61.29	-2571250.00	-134088.00	92276.00	2-3	34.38	67.918
42	2440,48	1	SIJ	-33146.40	-24,37	16.77	-2571250.00	-132553.00	91053.30	2-3	34.38	77.572
43	2500.00	1	SLU	-28436.30	0.00	0.00	-2571250.00		0 9			90,421

Caso	X <cm></cm>	cc		Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	6476.40	929.59	0.85	11.31	6542.77	1,00	32294.70	362062.00	32294.70	4.936
- 2	59.52	1	SLU	4268.41	612.67	0.85	11.31	4312.16	1.00	32294.70	362024.00	32294.70	7,489
- 3	119.05	1	SLU	2369.07	340.05	0.85	11.31	2393.35	1.00	32294.70	361707.00	32294.70	13.493
- 4	178.57	1	SLU	755.69	108.47	0.85	11.31	763.43	1.00	32294.70	361392.00	32294.70	42.302
- 5	238.09	1	SLU	-594.98	-85.40	0.85	11.31	601.08	1.00	32294.70	361077.00	32294.70	53.728
- 6	297.62	1	SLU	-1706.35	-244.92	0.85	11.31	1723.84	1.00	32294.70	360763.00	32294.70	18.734
7	357.14	1	SLU	-2883.94	-413.95	0.85	11.31	2913.50	1.00	32294.70	360450.00	32294.70	11.085
8	416,67	1	SLU	-4085.92	-586.47	0.85	11.31	4127.80	1.00	32294.70	359745.00	32294.70	7.824
- 9	476.19	1	SLU	-4995.31	-717.00	0.85	11.31	5046.50	1.00	32294.70	359041.00	32294.70	6.399
10	535.71	1	SLU	-5648.49	-810.76	0.85	11.31	5706.38	1.00	32294.70	358339.00	32294.70	5.659
11	595.24	1	SLU	-6079.86	-872.67	0.85	11.31	6142.17	1.00	32294.70	357638.00	32294.70	5.258
12	654.76	1	SLU	-6321,58	-907.37	0.85	11.31	6386.36	1.00	32294.70	356938.00	32294.70	5.057
13	714.29	1	SIJ	-6403.36	-919.11	0.85	11.31	6468.98	1.00	32294.70	356240.00	32294.70	4,992
14	773.81	1	SIJJ	~6352.41	-911.79	0.85	11.31	6417.51	1.00	32294.70	355543.00	32294.70	5.032
15	833,33	1	SLU	-6193.40	-888.97	0.85	11.31	6256.87	1.00	32294.70	354848.00	32294.70	5.161
16	892.86	1	SIAI	-5948.44	-893.81	0.85	11.31	6009.41	1.00	32294.70	354153.00	32294.70	5.374
17	952.38	1	SIAI	-5637.21	-809.14	0.85	11.31	5694.98	1,00	32294.70	353460.00	32294.70	5.671
18	1011.90	1	SIAJ	-5276.99	-757.43	0.85	11.31	5331.07	1.00	32294.70	352768.00	32294.70	6.058
19	1071.43	1	SLU	-4882.82	-700.86	0.85	11.31	4932,87	1.00	32294.70	352077.00	32294.70	6.547
20	1130.95	1	SLU	-4467.66	-641.27	0.85	11.31	4513.45	1.00	32294.70	351388.00	32294.70	7.155
21	1190.48	1	SIAI	-4042.50	-580.24	0.85	11.31	4083.93	1.00	32294.70	350699,00	32294.70	7.908
22	1250.00	1	SIJ	-3616.55	-519.10	0.85	11.31	3653.62	1.00	32294.70	350011,00	32294.70	8.839
23	1309.52	1	SIU	-3197.44	-458.94	0.85	11.31	3230.21	1.00	32294.70	349325.00	32294.70	9.998
24	1369.05	1	SLU	-2791.32	-400.65	0.85	11,31	2819.93	1.00	32294.70	348639.00	32294.70	11.452
25	1428.57	1	SLU	-2403.10	-344.93	0.85	11.31	2427.73	1.00	32294.70	347954.00	32294.70	13.303
26	1488,10	1	SLU	-2036.55	-292.32	0.85	11.31	2057.42	1.00	32294.70	347270.00	32294.70	15.697
27	1547.62	1	SLU	-1694.51	-243.22	0.85	11.31	1711.88	1.00	32294.70	346587.00	32294.70	18.865
28	1607,14	1	SIJ	-1378.99	-197.93	0.85	11.31	1393.12	1.00	32294.70	345905.00	32294.70	23.182
29	1666.67	1	SLU	-1091.32	-156.64	0.85	11.31	1102.51	1,00	32294.70	345223.00	32294.70	29.292
30	1726.19	1	SLU	-832,31	-119.47	0.85	11.31	840.84	1.00	32294.70	344542.00	32294.70	38.408
-31	1785.71	1	SIA	-602,30	-86,45	0.85	11.31	608.48	1.00	32294.70	343862.00	32294.70	53.075
32	1845.24	1	SLU	-401.33	-57.60	0.85	11.31	405.44	1.00	32294.70	343183.00	32294.70	79.654
33	1904.76	1	SIAI	-229.17	-32.89	0.85	11.31	231.51	1.00	32294.70	342504.00	32294.70	>100
34	1964.29	1	SLU	-85.45	-12.26	0.85	11.31	86.32	1.00	32294.70	341826.00	32294.70	>100
35	2023.81	1	SIU	30.29	4.35	0.85	11.31	30.61	1.00	32294.70	341148.00	32294.70	>100
36	2083.33	1	SLU	118.56	17.02	0.85	11.31	119.78	1.00	32294.70	340471.00	32294.70	>100
37	2142.86	1	SLU	179.84	25.81	0.85	11,31	181.69	1.00	32294.70	339794.00	32294.70	>100
38	2202.38	1	SIAI	214.58	30.80	0.85	11.31	216.78	1.00	32294.70	339118.00	32294.70	>100
39	2261.90	1	SLU	223.14	32.03	0.85	11.31	225.42	1.00	32294.70	338442.00	32294.70	>100
40	2321.43	1	SLU	205.80	29.54	0.85	11.31	207.91	1.00	32294.70	337766.00	32294.70	>100
41	2380.95	1	SIJ	162.77	23.36	0.85	11.31	164.44	1.00	32294.70	337091.00	32294.70	>100
42	2440.48	1	SLU	94.15	13.51	0.85	11.31	95.12	1.00	32294.70	336416.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	8	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <mq></mq>	σ _c <dan cmq=""></dan>	of <dan cmq=""></dan>
44	0.00	2	SLE R	-157177.00	-22780.10	33101.40	21.99	56.55	35.01	491.95
45	59.52	2	SLE B	-157293.00	-24130.00	35063.00	25.13	53.41	36.80	515.70
46	119.05	2	SLE F	-155846.00	-24961.80	36271.70	28.27	50.27	37.91	530.20
47	178.57	2	SLE R	-154404.00	-25350.60	36836.60	28.27	50.27	38.44	536.92
48	238.09	2	SLE B	-152967.00	-25365.60	36858.40	28.27	50.27	38.44	536,69
49	297.62	2	SLE R	-151534.00	-25070.20	36429.20	28.27	50.27	38.00	530.57
50	357.14	2	SLE B	-150107.00	-24498.20	35598.00	28.27	50.27	37.16	519.20
51	416.67	2	SLE B	-146474.00	-23611.60	34309.70	28.27	50.27	35.84	501.13
52	476.19	2	SLE R	-142850.00	-22459,30	32635.20	28.27	50.27	34.16	478.22

							Rela	zion	e di cald	colo
1 :3	705.71	2	د صولا	-100233.00	-21110.30	30,079,10			32,24	402.04
Ī4	395,14	-	922.0						30 7	410.98
:::	6.51.276		977 7	13000×100	18055.0	35236.70	JT 133	.:8.00	da . 06	3,932,13
2.0	11/2/1		T. 5.	1087.00.00	184490	da 63 7 180	10.8.0	.:964	35.37	200.87
77	7771.91	1	is S	-1248000.00	-14992190	01553.40	75.71	00.00	22.98	229,000
7.3	9771.22	/	977 R	-121057.00	-110146 180	19040.00	70.57	15.97	W C.	213.01
1.9	802.80	2					3.14	75,40	25,27	188.60
50	002.38	2	877.0		-10148.10	14891,30	0.00	78,04	18,60	107.88
61	10001290		977 7	11 0997 .00	8069177	12687.70	0.00	780.54	17.08	247.73
	1077,145		977 7	106994.00	(55.008)	110001.80	0.00	780.54	1::6"	777.538
6.7	1000.95	_	977 B	-103444.00	-6404169	92001.00	6.00	381.54	14.75	005.04
	1190.49	/					0.00	480.54	70.98	197173
-	1290.00	-	875.0		-4300.28	5340,21	_	78,04	11.81	171.45
-	1009,00	2	875.0		-3000.15	0000.37	_	78,04	20,74	106.50
-	1369105		977 7	89094.00	3747130	2.4800000	_	78.54	9.11	1401.85
-	14,08190		977 7	 	50 W 189			78.54	::.88	TA0175
\rightarrow	1499, 10	_	977 R		-1531.80	0025.86	_	781.74	9.109	119.00
\vdash	1547.60	4			-1060.07	1542.71		481.54	7.37	109,10
	1607,14	-	875 0		-070.78	979,00		78,04	5,73	100.05
-	1668.57	2			-302.47	026,69		78,04	5,16	91.92
-	1778.14	Щ	877 J	68,09,70	120.19			78.04	* . 6.:	07.185
-	1785.71		977 7		00.33	87.87		78.01	5.31	79.84
\vdash	1045.04	_	977 R		190.44 065.45	-0.700, 90°	_	381.54 381.54	7.11A	79 J.95
\vdash	1904.76	/	977 R			-395.30 -442.58			4.9%	79.67
-	1964,19	2			304.58			78,04	4.60	33190
-	2003.01 2092.00		877 T		310.98 33. 59			78.04	4.71	6.00 (4)
-	2083.33 0140.96	\vdash	977 S		2 # 159 0:9195			780.54 780.54	7.79	61 - 61 51 - 50
\rightarrow	0200.29	-	877 S				_	381.54	2.20	51.550 51.65
\longrightarrow	1261,90	2	8 A 3		147.18			78,04	3,12	46.72
	1021,43		8 TE 19			-104.38		78,04	2,79	42.80
::1	2380. ve		977 7				_	78.01	7.7.7	30.98
-	2//0.46		977 7		10.43			78.01	7.16	A" - 31
-	0.00.00		977 3		0.00		_	781.74	1.39	07.85
377	0.00	-	977 0				_	26.22	1(F.101	491.45
==	39,00	_	875 S				202	33.41	35,80	217.70
E 9	9.60	4						30.27	37.02	030.20
-11	1.787.43	-	977 0						30.77	0.00.90
-71		-	977 0			30008.10	_	30.27	30.77	536.89
90	297.60	-	977 0					_	39.00	530.57
9,7	357.14	_		-15010%.00			_		70.75	519,00
94		-		-146474.00				_	30.84	
90				-142850.00					34.16	
40				133034.00					37.77	
49		-		13.864.00			_	_	30.77	
93		-		-132000 .000			_		28.40	
99		_		-128475.000			_		75-197	
200	773,81	4	912 O	-124838.00	-14832.80	21000,40	10.74	62,83	23,03	339.12
				-121257.00				65,97	21.03	
								25,40	400,007	
	3.50.00			T1711A.00					1 : . 6.3	
	1011.90			-110551.00				781.74	77.00	
				-10/334.00			_			
-	1100.90			-100444.00		9306,83	0.00	78,04	14,23	
=				-00808.40				78,04		
$\overline{}$	Thebloc	-				657 0002		78.54	11.81	
$\overline{}$	1309.52	-	977 Q		3503115	5030130	0.00	78.54	10.74	156.150
	19/8,65		977 3		-07/47/000	2997,10	0.00	781.74	9.77	
- 11	14280.50							781.74	9.00	1.900.45
$\overline{}$	1488,10		8 М							
	1347.01	÷	ř K	-78731.70	-10 GL J 27	1042,11	0.00	78,04	7.07	100.12
	1607.14					973.05	0.00	78.04	6.73	
$\overline{}$	1668.67	_			2,677,777	576.89	0.00	78.04	6.16	97.190
-	1726.19		977 0				_	780.74	5.05	
\longrightarrow	1795.71	-						780.74		
	1845,14					-170,91		78,04	0.13	
	1904.70	-	875 S			-383,71		78,04	4,00	73167
	1964.29							78.04	4.63	
	0023.91		977 0			-45°, ita	_	30.54	4.41	
\vdash	0000.22	-	977 0					30.54	4.**	
	1142,86		875 G					78,04	3,79	
	1202.38		8 A C			-194.97		78,04	3,46	
-	N., 61, 1940	_	977 0					78.04	A.1.3	
-	z3''' .4.:	-	977 Q					78.04	2.73	
1.009	00000.95		977 0				_	480.54		
$\overline{}$	0440.49	-	977 0	-24 GRE 100	17.4%	-10.05		39.54	2.11	37.34

				100				
129 2500.00	4 SLE O	-22924,20	0.00	0.00	0.00 78.	54	1.86	27.9

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	Φeq	Δ _{SIII} <mm></mm>	A _{ff}	Ac eff <cmq></cmq>	σ ₅ <dan cmq=""></dan>	esm	Wk <mm></mm>
87	0.00	4	SLE Q	-157177.00	33101.40	-22780.10	46.00	136,36	0.50	20.00	173.19	9,42	382,58	130.96	0.04	0.01
88	59.52	4	SLE Q	-157293.00	35063.00	-24130.00	46.00	136.36	0.50	20.00	188.62	9.42	455.31	163.83	0.05	0.03
89	119.05	4	SLE Q	-155846.00	36271.70	-24961.80	46.00	136.36	0.50	20.00	173.64	12.57	512.94	190.51	0.06	0.02
90	178.57	4	SLE Q	-154404.00	36836.60	-25350.60	46.00	136.36	0.50	20.00	179.00	12.57	546.66	206.29	0.06	0.02
91	238.09	4	SLE Q	-152967.00	36858.4D	-25365.60	46.00	136.36	0.50	20.00	181,18	12.57	560.33	211.68	0.06	0.0;
92	297.62	4	SLE Q	-151534.00	36429.20	-25070.20	46.00	136.36	0.50	20.00	180.67	12.57	557.16	208.00	0.06	0.02
93	357.14	4	SLE Q	-150107.00	35598.00	-24498.20	46.00	136.36	0.50	20.00	177.70	12.57	538.48	196.33	0.06	0.03
94	416.67	4	SLE Q	-146474.00	34309.70	-23611.60	46.00	136.36	0.50	20.00	175.02	12.57	521.63	183.26	0.05	0.0
95	476.19	4	SLE Q	-142850.00	32635.20	-22459.30	46.00	136,36	0.50	20.00	195.54	9.42	487.94	163.13	0.05	0.03
96	535.71	4	SLE Q	-139233.00	30675.10	-21110.30	46.00	136.36	0.50	20.00	185.36	9.42	439.94	138.66	0.04	0.0
97	595.24	4	SLE 0	-135624.00	28517.10	-19625.20	46.00	136,36	0.50	20.00	172.77	9,42	380.62	112.28	0.03	0.0
98	654.76	4	SLE Q	-132022.00	26236.40	-18055.70	46.00	136.36	0.50	20.00	158.46	9.42	313.20	85.96	0.03	0.0
99	714.29	4	SLE Q	-128427.00	23897.30	-16445.90	46.00	136.36	0.50	20.00	168.69	6,28	240.94	61.15	0.02	0.0
130	0.00	3	SLE F	-157177.00	33101.40	-22780.10	46.00	136,36	0.50	20.00	173.19	9,42	382.58	130.96	0.04	0.0
131	59.52	3	SLE F	-157293.00	35063.00	-24130.00	46,00	136.36	0.50	20.00	188.62	9.42	455.31	163.83	0.05	0.0
132	119.05	3	SLE F	-155846.00	36271.70	-24961.80	46.00	136.36	0.50	20.00	173.64	12.57	512.94	190.51	0.06	0.0
133	178.57	3	SLE F	-154404.00	36836.60	-25350.60	46.00	136,36	0.50	20.00	179.00	12.57	546.66	206.29	0.06	0.0
134	238.09	3	SLE F	-152967.00	36858.40	-25365.60	46.00	136.36	0.50	20.00	181,18	12.57	560.33	211.68	0.06	0.0
135	297.62	3	SLE F	~151534.00	36429.20	-25070.20	46.00	136.36	0.50	20.00	180.67	12.57	557.16	208.00	0.06	0.0
136	357.14	. 3	SLE F	-150107.00	35598.00	-24498.20	46.00	136.36	0.50	20.00	177.70	12.57	538.48	196.33	0.06	0.0
137	416.67	3	SLE F	-146474.00	34309.70	-23611.60	46.00	136,36	0.50	20.00	175.02	12.57	521.63	183,26	0.05	0.0
138	476.19	3	SLE F	-142850.00	32635.20	-22459.30	46.00	136.36	0.50		_	9,42	487.94	163.13	0.05	0.0
	535.71	-	SLE F	-139233.00					-			9.42	439.94	138.66	_	
140	595.24	3	SLE F	-135624.00	28517.10		-	136.36	-	-	-	9.42	380.62	112.28	0.03	0.0
141	654.76	3	SLE F	-132022.00	26236.40	-18055.70	46.00	136.36	0.50	20.00	158.46	9.42	313.20	85.96		-
142	714,29	$\overline{}$		-128427.00		_					168.69	6.28	240.94	61.15	-	_

Verifiche principali

Caso	Tipo
- 1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
- 5	SLU N cost - min. sic.
47	C.Rare - Sf min (max compr.)
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.)
61	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sf min (max compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
104	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 29

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20,59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti.

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVB	0.00			

Azioni ed effetti - Plinto/Palo n. 29 (-81)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <dann></dann>
-1	1	SLU	RVN	166267.00	6757.66	963.45	54146.30	25252,60
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC		8 3		0.00	0.00
	1	SLU	TOT	166267.00	6757.66	963.45	54146.30	25252.60
2	2	SLE R	RVN	123161.00	5005.68	713.67	40108.40	18705.60
	2	SLE R	TAG				0.00	0.00
	.2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	123161.00	5005.68	713.67	40108.40	18705.60
3	3	SLE F	RVN	123161.00	5005.68	713.67	40108.40	18705.60
	3	SLE F	TAG				0.00	0.00
	3	SLE F	ECC		ā 5	5	0.00	0.00
	3	SLE F	TOT	123161.00	5005.68	713.67	40108.40	18705.60
4	-6	SLE Q	RVN	123161.00	5005.68	713.67	40108.40	18705.60
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00

Sollecitazioni nei pali

Caso	cc	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
- 4	1	SIJ	1	-166267.00	-6757.66	-963.45	-54146.30	-25252.60
2	2	SLE R	1	-123161.00	-5005.68	-713,67	-4010B.40	-18705.60
- 3	3	SLE F	1	-123161.00	-5005.68	-713.67	-40108.40	-18705.60
4	4	SLE Q	1	-123161.00	-5005.68	-713.67	-40108.40	-18705.60

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	oc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SLU	-166267.00	53926.00	-25149.80	-166267.00	192445.00	-89846.80	2-3	205.00	3.569
2	59.52	1	SLU	-166320.00	56947.00	-26558.70	-166320.00	192462.00	-89854.90	2-3	205.00	3.380
.3	119.05	1	SIJ	-164747.00	5876B.50	-27408.20	-164747.00	191946.00	-89612.80	2-3	205.00	3.267
4	178.57	1	SLU	-163179.00	59565.70	-27780.00	-163179.00	191432.00	-89371.40	2-3	205.00	3.214
- 5	238.09	1	SIJJ	-161616.00	59499.80	-27749.30	-161616.00	190917.00	-89129.60	2-3	205.00	3.20
- 6	297.62	1	SIJJ	-160059.00	58718.30	-27384.80	-160059.00	190402.00	-88887.70	2-3	205.00	3.24
7	357.14	1	SLU	-158506.00	57300.20	-26723.40	-158506.00	189889.00	-88646.60	2-3	205.00	3.31
.8	416.67	1	SIU	-154660.00	55160.00	-25725.30	-154660.00	188616.00	-88049.00	2-3	205.00	3.42
- 9	476.19	1	SLU	-150823.00	52411.30	-24443.40	-150823.00	187340.00	-87449,30	2-3	205.00	3.57
10	535.71	1	SLU	-146993.00	49214.80	-22952.60	-146993.00	186063.00	-86848.90	2-3	205.00	3.78
11	595.24	1	SLU	-143172.00	45710.10	-21318.10	-143172.00	184785.00	-86248.30	2-3	205.00	4.04
12	654.76	1	SIJ	-139358.00	42017.20	-19595.80	-139358.00	183503.00	-85645.10	2-3	205.00	4.36
13	714.29	1	SIJ	-135551.00	38238.00	-17833.30	-135551.00	182222.00	-85042.70	2-3	205.00	4.76
14	773.81	1	SLU	-131752.00	34457.70	-16070.20	-131752.00	180936.00	-84437.60	2-3	205.00	5.25
15	833,33	1	SLU	-127960.00	30746.20	-14339.30	-127960.00	179651.00	-83832,50	2+3	205.00	5.84
16	892.86	1	SIJ	-124175.00	27159.60	-12666.60	-124175.00	178364.00	-83215.00	2-3	205.00	6.56
17	952.38	1	SLU	-120397.00	23741.80	-11072.60	-120397.00	177076.00	-82582.30	2-3	205.00	7.45
18	1011.90	1	SLU	-116625.00	20526.20	-9572.91	-116625.00	175779.00	-81960.30	2-3	205.00	8,56
19	1071.43	1	SLU	-112859.00	17536.20	-8178.45	-112859.00	174469.00	-81343,10	2-3	205.00	9.94
20	1130.95	1	SLU	-109099.00	14787.40	-6896.48	-109099.00	173159.00	-80725.90	2-3	205.00	11.70
21	1190.48	1	SILI	-105345.00	12288.30	-5730.99	-105345.00	171849.00	-80108.40	2-3	205.00	13.98
22	1250.00	1	SIJ	-101597.00	10041.70	-4683.19	-101597.00	170535.00	-79488.80	2-3	205.00	16.98
23	1309.52	1	SLU	-97854.00	8045.11	-3752.05	-97854.00	169224.00	-78870.90	2-3	205.00	21,03
24	1369.05	1	SLU	-94116.50	6292.44	-2934.64	-94116.50	167905.00	-78248.70	2-3	205.00	26.68
25	1428.57	1	SLU	-90384.00	4774.20	-2226.57	-2571250.00	166586.00	-77627.20	2-3	205.00	28.44
26	1488.10	1	SLU	-86656.30	3478.45	-1622.26	-2571250.00	165269.00	-77006.00	2-3	205.00	29.67
27	1547.62	1	SLU	-82933.30	2391.33	-1115.26	-2571250.00	163946.00	-76382.20	2-3	205.00	31.00
28	1607.14	1	SLU	-79214.70	1497.63	-698.46	-2571250.00	162623.00	-75758.70	2+3	205.00	32.45
29	1666.67	1	SLU	-75500.40	781.17	-364.32	-2571250.00	161300.00	-75134.60	2-3	205.00	34.05
30	1726,19	1	SIM	-71790.20	225.18	-105.02	-2571250.00	159973.00	-74508.90	2-3	205.00	35.81
31	1785.71	1	SIU	-68083.80	-187.42	87.41	-2571250.00	-158680.00	74011.40	2-3	25.00	37.76
32	1845,24	1	SLU	-64381.00	-473.77	220.96	-2571250.00	-157320.00	73371.40	2-3	25.00	39.93
33	1904.76	1	SLU	-60681.70	-650.97	303.60	-2571250.00	-155957.00	72730.10	2-3	25.00	42.37
34	1964.29	1	SIA	-56985.60	-735.89	343.20	-2571250.00	-154594.00	72088.50	2-3	25.00	45.12
35	2023.81	1	SIU	-53292.60	-745.17	347.53	-2571250.00	-153224.00	71444,10	2-3	25.00	48.24
36	2083.33	1	SIU	-49602.50	-695.13	324.19	-2571250.00	-151854.00	70799.90	2-3	25.00	51.83
37	2142.86	1	SLU	-45915.00	-601.79	280.66	-2571250.00	-150479.00	70153.60	2-3	25.00	56.00
38	2202.38	1	SLU	-42230.00	-480.91	224,28	-2571250.00	-149102.00	69506.40	2-3	25.00	60.488
39	2261.90	1	SLU	-38547.30	-347.97	162.29	-2571250.00	-147724.00	68858.50	2-3	25.00	66.70
40	2321.43	1	SLU	-34865.60	-218.29	101.81	-2571250.00	-146340.00	68208.60	2-3	25.00	73.74
41	2380.95	1	SIJ	-31187.80	-107.03	49.92	-2571250.00	-144955.00	67558.50	2-3	25.00	82.44
42	2440.48	1	SLU	-27510.70	-29.26	13.65	-2571250.00	-143566.00	66906.60	2-3	25.00	93.46
43	2500.00	1	SIA	-23835,00	0.00	0.00	-2571250,00					>100

Stato limite ultimo - Verifiche a taglio

Caso	X <cm>></cm>	cc	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	6757.66	963,45	0.85	11.31	6826.00	1.00	32294.70	355484,00	32294.70	4.731
2	59.52	1	SIAJ	4387.84	625.58	0.85	11.31	4432.21	1.00	32294.70	355492.00	32294.70	7.286
.3	119.05	1	SLU	2351.48	335.25	0.85	11.31	2375.26	1.00	32294.70	355266.00	32294.70	13.596
4	178.57	1	SEU	623.78	88.93	0.85	11.31	630.09	1.00	32294.70	355042.00	32294.70	51.254
.5	238.09	1	SIJJ	-820.56	-116.99	0.85	11.31	828.86	1.00	32294.70	35481B.00	32294.70	38.963
- 6	297.62	1	SIJ	-2007.04	-286.15	0.85	11.31	2027,33	1.00	32294.70	354595+00	32294.70	15.930
7	357.14	1	SLU	-3261.23	-464.96	0.85	11.31	3294.20	1.00	32294.70	354372.00	32294.70	9.803
- 8	416,67	1	SLU	-4538.37	-647.04	0.85	11.31	4584.26	1.00	32294.70	353822.00	32294.70	7.045
.9	476.19	1	SIAI	-5501.04	-784.29	0.85	11.31	5556.67	1,00	32294.70	353272.00	32294.70	5.812
10	535.71	1	SLU	-6188.62	-882.32	0.85	11.31	6251.20	1,00	32294.70	352723.00	32294.70	5.166
11	595.24	1	SIU	-6638,28	-946.43	0.85	11.31	6705.41	1.00	32294.70	352176.00	32294.70	4.816
12	654.76	1	SLU	-6884.74	-981.57	0.85	11.31	6954.36	1.00	32294.70	351630,00	32294.70	4.544
13	714.29	1	SIU	-6960.08	-992.31	0.85	11.31	7030.46	1.00	32294.70	351084.00	32294.70	4.594

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								111	1102	OILC OI	Calcolo		
14	773.81	1	SLU	-6893.61	-982.83	0.85	11.31	6963.32	1.00	32294.70	350540.00	32294.70	4.638
15	833,33	1	SLU	-6711.90	-956.92	0.85	11.31	6779.77	1.00	32294.70	349997.00	32294.70	4.763
16	892.86	1	SIU	-6438.75	-917.98	0.85	11.31	6503.86	1.00	32294.70	349455.00	32294.70	4.965
17	952.38	1	SIJJ	-6095.31	-869.02	0.85	11.31	6156.95	1.00	32294.70	348914.00	32294.70	5.245
18	1011.90	1	SLU	-5700.15	-812.68	0.85	11.31	5757.79	1.00	32294.70	348373.00	32294.70	5.609
19	1071.43	1	SLU	~5269.41	-751.27	0.85	11.31	5322.70	1.00	32294.70	347834.00	32294.70	6.067
20	1130.95	1	SLU	-4816.97	-686.76	0.85	11.31	4865.68	1.00	32294.70	347295.00	32294.70	6.637
21	1190.48	1	SLU	-4354.60	-620.84	0.85	11.31	4398.64	1.00	32294.70	346758.00	32294.70	7.342
22	1250.00	4	SLU	-3892.17	-554.91	0.85	11.31	3931.53	1.00	32294.70	346221.00	32294.70	8.214
23	1309.52	1	SIJ	-3437.79	-490.13	0.85	11.31	3472.55	1,00	32294.70	345685.00	32294.70	9.300
24	1369.05	1	SLU	-2998.03	-427.43	0.85	11.31	3028.35	1.00	32294.70	345149.00	32294.70	10.664
25	1428.57	1	SLU	-2578.10	-367.56	0.85	11.31	2604.17	1.00	32294.70	344615.00	32294.70	12.401
26	1488,10	1	SIAJ	-2182.01	-311.09	0.85	11.31	2204.08	1.00	32294.70	344081.00	32294.70	14,652
27	1547.62	1	SLU	-1812.74	-258.44	0.85	11.31	1831.07	1.00	32294.70	343547,00	32294.70	17.637
28	1607.14	1	SLU	-1472.41	-209.92	0.85	11.31	1487.30	1.00	32294.70	343015.00	32294.70	21.714
29	1666.67	1	SILI	-1162.39	-165.72	0.85	11.31	1174.15	1.00	32294.70	342483.00	32294.70	27.505
30	1726.19	1	SIJ	-883.51	-125.96	0.85	11.31	892.45	1.00	32294.70	341951,00	32294.70	36.187
31	1785.71	1	SLU	-636.10	-90.69	0.85	11.31	642.53	1.00	32294.70	341420.00	32294.70	50.262
32	1845.24	1	SLU	-420.15	-59.90	0.85	11.31	424.39	1.00	32294.70	340890,00	32294.70	76.096
33	1904.76	1	SIU	-235,39	-33.56	0.85	11.31	237.77	1.00	32294.70	340360.00	32294.70	>100
34	1964.29	1	SLU	-81.40	-11.61	0.85	11.31	82.22	1.00	32294.70	339831.00	32294.70	>100
35	2023.81	1	SIU	42.35	6.04	0.85	11.31	42.78	1.00	32294.70	339302.00	32294.70	>100
36	2083.33	1	SIJJ	136.42	19.45	0.85	11.31	137.80	1.00	32294.70	338773.00	32294.70	>100
37	2142.86	1	SLU	201.34	28.71	0.85	11.31	203.38	1.00	32294.70	338245.00	32294.70	>100
3.8	2202,38	1	SLU	237.61	33.88	0.85	11,31	240.01	1.00	32294.70	337717.00	32294.70	>100
39	2261.90	1	SIU	245.63	35.02	0.85	11.31	248.11	1.00	32294.70	337190.00	32294.70	>100
40	2321.43	1	SLU	225.70	32.18	0.85	11.31	227.99	1.00	32294.70	336662.00	32294.70	>100
41	2380.95	1	SLU	178.05	25.39	0.85	11.31	179.85	1.00	32294.70	336135.00	32294.70	>100
42	2440.48	1	SLU	102,80	14.66	0.85	11.31	103.84	1.00	32294.70	335609.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	œ	TCC	e d'eserci: N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <mq></mq>	σ _c <dan cmq=""></dan>	σ _f <dan cmg=""></dan>
44	0.00	2	SLE R	-123161.00	-18629.50	39945,20	31.42	47.12	37.87	527.45
45	59.52	2	SLE R	-123513.00	-19673.10	42182.90	37.70	40.84	40.20	558.37
46	119.05	2	SLE R	-122538.00	-20302.40	43532.20	37.70	40.84	41.69	577.72
47	178.57	2	SLE R	-121567.00	-20577.80	44122.70	37.70	40.84	42.38	586.50
48	238.09	2	SLE R	-120599.00	-20555.00	44073.90	37.70	40.84	42.37	586.17
49	297.62	2	SLE R	-119636.00	-20285.00	43495.00	37.70	40.84	41.78	578.23
50	357.14	2	SLE R	-118676.00	-19795.10	42444.60	37.70	40.84	40.69	563.56
51	416.67	2	SLE R	-115842.00	-19055.80	40859,20	37.70	40.84	39.10	541.97
52	476.19	2	SLE R	-113015.00	-18106.20	38823.20	37.70	40,84	37.03	514.07
53	535.71	2	SLE R	-110194.00	-17001.90	36455,40	31.42	47.12	34.63	481.76
54	595,24	2	SLE R	-107378.00	-15791,20	33859.30	31,42	47.12	32.02	446.73
55	654.76	2	SLE R	-104569.00	-14515,40	31123.80	31,42	47.12	29.34	410.53
56	714.29	2	SLE R	-101769.00	-13209.80	28324.40	31.42	47.12	26.68	374.49
57	773.81	2	SLE R	-98966.10	-11903.90	25524.20	25.13	53.41	24.11	339.73
58	833.33	2	SLE R	-96172.90	-10621.70	22774.90	25.13	53.41	21.72	307.11
59	892.86	2	SLE R	-93384.80	-9382.64	20118.20	18.85	59.69	19.53	277.16
60	952.38	2	SLE R	-90601.80	-8201,95	17586.50	18.85	59.69	17.57	250.13
-61	1011.90	2	SLE R	-87823.60	-7091.04	15204.60	12.57	65.97	15.82	226.04
62	1071.43	2	SLE R	-85050.10	~6058.11	12989.80	0.00	78.54	14.28	204.64
63	1130.95	2	SLE R	-82281.10	~5108.51	10953.60	0.00	78.54	12.90	185.40
64	1190.48	2	SLE R	-79516.60	-4245.18	9102.47	0.00	78,54	11.62	167.65
65	1250.00	2	SLE R	-76756.40	-3469.03	7438,27	0.00	78.54	10.46	151.36
66	1309.52	2	SLE R	-74000.20	-2779.30	5959.34	0.00	78.54	9.39	136.51
67	1369.05	2	SLE R	-71248.10	-2173.81	4661.07	0.00	78.54	8.43	123.07
68	1428.57	2	SLE R	-68499.70	-1649.31	3536.45	0.00	78.54	7.57	110.99
69	1488.10	2	SLE R	-65755.00	-1201.68	2576.63	0.00	78.54	6.81	100.19
70	1547.62	2	SLE R	-63013.90	-826,12	1771.36	0.00	78.54	6,13	90.59
71	1607.14	2	SLE R	-60276.10	-517.38	1109.36	0.00	78.54	5.53	82.11
72	1666,67	2	SLE B	-57541.60	-269.87	578.64	0.00	78.54	5.01	74.65
73	1726.19	2	SLE R	-54810.20	-77.79	166.80	0.00	78,54	4.55	68.12
74	1785.71	2	SLE R	-52081.70	64.75	-138.83	0.00	78.54	4.31	64.57
75	1845.24	2	SLE R	-49356.00	163.67	-350.94	0.00	78.54	4.21	62.88
7.6	1904.76	2	SLE R	-46632.90	224.88	-482,20	0.00	78,54	4.06	60.57
77	1964,29	2	SLE R	-43912.30	254,22	-545,11	0.00	78.54	3.88	57,74
78	2023.81	2	SLE R	-41194.10	257.43	-551.98	0.00	78.54	3.66	54.48
79	2083.33	2	SLE R	-38478.10	240.14	-514.91	0.00	78.54	3.42	50.88
80	2142.86	2	SLE R	-35764.20	207.90	-445.77	0.00	78.54	3.16	47.04
81	2202.38	2	SLE R	-33052.20	166.14	-356,23	0.00	78,54	2.89	43.04
82	2261.90	2	SLE R	-30341.90	120.21	-257.76	0.00	78.54	2.61	38.98
83	2321.43	2	-	-27633.30	75.41	-161,70	0.00	-	2.34	34.94
84	2380.95	2	SLE R	-24926.20	36.98	-79.28	0.00	78.54	2.07	31.00
85	2440.48	2	SLE R	-22220.40	10.11	+21.67	_	78.54	1.82	27.26
86		2		-19515.80	0.00	0.00	0.00		1.59	23.79
87	0.00	-	SLE Q	-123161.00	-18629.50		31.42	47.12	37.87	527.45

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88	59.52	4	SLE Q	-123513.00	-19673.10	42182.90	37.70	40.84	40.20	558.37
89	119.05	4	SLE Q	-122538.00	-20302.40	43532.20	37.70	40.84	41.69	577.72
90	178.57	4	SLE Q	-121567.00	-20577.80	44122.70	37.70	40.84	42.38	586.50
91	238.09	4	SLE Q	-120599.00	-20555.00	44073.90	37.70	40.84	42.37	586.17
92	297.62	4	SLE Q	-119636.00	-20285.00	43495.00	37.70	40.84	41.78	578.23
93	357.14	4	SLE Q	-118676.00	-19795.10	42444.60	37.70	40.84	40.69	563.56
94	416.67	4	SLE Q	-115842.00	-19055.80	40859,20	37.70	40.84	39.10	541.97
95	476.19	4	SLE Q	-113015.00	-18106.20	38823,20	37.70	40.84	37.03	514.07
96	535.71	4	SLE Q	-110194.00	-17001.90	36455.40	31.42	47.12	34.63	481.76
97	595.24	4	SLE Q	-107378.00	-15791.20	33859.30	31.42	47.12	32.02	446.73
98	654.76	4	SLE Q	-104569.00	-14515.40	31123.80	31.42	47.12	29.34	410.53
99	714.29	4	SLE Q	-101765.00	-13209,80	28324.40	31.42	47+12	26.68	374.49
100	773,81	4	SIE Q	-98966.10	-11903.90	25524.20	25,13	53,41	24.11	339.73
101	833,33	4	SLE Q	-96172.90	-10621.70	22774.90	25.13	53,41	21.72	307,11
102	892.86	4	SLE Q	-93384.80	-9382.64	20118.20	18.85	59.69	19.53	277.16
103	952.38	4	SLE Q	-90601.80	-8201.95	17586.50	18.85	59.69	17.57	250.13
104	1011,90	-4	SLE Q	-87823.60	-7091,04	15204.60	12,57	65,97	15.82	226.04
105	1071.43	4	SLE Q	-85050.10	-6058.11	12989.80	0.00	78.54	14.28	204.64
106	1130.95	- 6	SLE Q	-82281.10	-5108.51	10953,60	0.00	78.54	12.90	185.40
107	1190.48	4	SLE Q	-79516.60	-4245,18	9102.47	0.00	78.54	11.62	167.65
108	1250.00	4	SLE Q	-76756.40	-3469.03	7438,27	0.00	78.54	10.46	151.36
109	1309.52	4	SLE Q	-74000.20	-2779,30	5959.34	0.00	78.54	9.39	136,51
110	1369.05	4	SLE Q	-71248.10	-2173.81	4661.07	0.00	78,54	8.43	123.07
111	1428.57	4	SLE Q	-68499.70	-1649.31	3536.45	0.00	78.54	7.57	110.99
112	1488,10	4	SLE Q	-65755.00	-1201.68	2576.63	0.00	78,54	6.81	100.19
113	1547.62	4	SLE Q	-63013.90	-826.12	1771.36	0.00	7B ₊ 54	6.13	90.59
114	1607.14	- 4	SLE Q	-60276.10	-517.38	1109.36	0.00	78,54	5.53	82.11
115	1666.67	4	SLE Q	-57541.60	-269.87	578.64	0.00	78.54	5.01	74.65
116	1726.19	4	SLE Q	-54810.20	-77.79	166.80	0.00	78.54	4.55	68.12
117	1785.71	4	SLE Q	-52081.70	64.75	-138,83	0.00	78.54	4.31	64,57
118	1845.24	4	SLE Q	-49356.00	163,67	-350.94	0.00	78.54	4.21	62.88
119	1904.76	4	SLE Q	-46632.90	224.88	-482.20	0.00	78.54	4.06	60.57
120	1964.29	- 4	SLE Q	-43912.30	254.22	-545.11	0.00	78.54	3.88	57.74
121	2023.81	4	SLE Q	-41194.10	257.43	-551.98	0.00	78+54	3.66	54.48
122	2083.33	4	SIE Q	-38478.10	240.14	-514.91	0.00	78.54	3.42	50.88
123	2142,86	4	SLE Q	-35764.20	207,90	-445,77	0,00	78,54	3,16	47.04
124	2202.38	4	SLE Q	-33052.20	166.14	-356,23	0.00	78.54	2.89	43.04
125	2261.90	4	SLE Q	-30341.90	120.21	-257.76	0.00	78.54	2.61	38.98
126	2321.43	4	SLE Q	-27633.30	75.41	-161,70	0.00	78,54	2.34	34.94
127	2380,95	4	SLE Q	-24926.20	36.98	-79.28	0.00	78.54	2.07	31.00
128	2440.48	4	SIE Q	-22220.40	10.11	-21.67	0.00	78.54	1.82	27.26
129	2500.00	4	SLE Q	-19515,80	0.00	0.00	0.00	78.54	1.59	23,79

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	Φeq	Δ _{BBB}	A _S <cmq></cmq>	Ac eff <mq></mq>	σ _S <dan cmq=""></dan>	€ _{SM}	Wk <mm></mm>
87	0.00	4	SLE Q	-123161.00	39945.20	-18629.50	46.00	136.36	0.50	20.00	180.17	18.85	831.00	326,29	0.10	0.03
88	59.52	4	SLE Q	-123513.00	42182.90	-19673.10	46.00	136.36	0.50	20.00	185.24	18.85	878.77	381.88	0.11	0.04
89	119.05	4	SLE Q	-122538.00	43532.20	-20302.40	46.00	136.36	0.50	20.00	188.73	18.85	911,68	424.67	0.12	0.04
90	178.57	4	SLE Q	-121567.00	44122.70	-20577.80	46.00	136,36	0.50	20.00	190.50	18.85	928.35	447.67	0.13	0.04
91	238.09	4	SLE Q	-120599.00	44073.90	+20555.00	46.00	136,36	0.50	20.00	191.05	18.85	933.53	452.76	0.13	0.04
92	297.62	4	SLE Q	-119636.00	43495.00	-20285.00	46.00	136.36	0.50	20.00	190.64	18.85	929.62	442.65	0.13	0.04
93	357.14	4	SLE Q	-118676.00	42444.60	-19795.10	46.00	136.36	0.50	20.00	189.30	18.85	917.00	419.23	0.12	0.04
94	416.67	4	SLE Q	-115842.00	40859,20	-19055.80	46.00	136,36	0.50	20.00	188.12	18.85	905.91	393.30	0.11	0.04
95	476.19	4	SLE Q	-113015.00	38823.20	-18106.20	46.00	136.36	0.50	20.00	185.78	18,85	883.82	355.44	0.10	0.03
96	535,71	4	SLE Q	-110194.00	36455.40	-17001.90	46.00	136.36	0.50	20.00	182,19	18.85	849.98	309.98	0.09	0.03
97	595.24	4	SLE Q	-107378.00	33859.30	-15791.20	46.00	136,36	0.50	20.00	219.77	12.57	802.78	260.87	0.08	0.03
98	654.76	4	SLE Q	-104569.00	31123,80	-14515.40	46.00	136,36	0.50	20.00	209.69	12,57	739.46	211.56	0.06	0.02
99	714.29	4	SLE Q	-101765.00	28324.40	-13209.80	46.00	136.36	0.50	20.00	194.95	12.57	646.88	164.80	0.05	0.02
100	773.81	4	SLE Q	-98966.10	25524.20	-11903.90	46.00	136.36	0.50	20.00	178.38	12.57	542.74	122.60	0.04	0.01
101	833.33	4	SLE Q	-96172.90	22774.90	-10621.70	46.00	136.36	0.50	20.00	160.61	12.57	431.06	86.14	0.03	0.01
102	892.86	4	SLE Q	-93384.80	20118.20	-9382.64	46.00	136,36	0.50	20.00	192.39	6.28	315.37	55.77	0.02	0.01
103	952.38	4	SLE Q	-90601.80	17586.50	-8201.95	46.00	136,36	0.50	20.00	155.81	6.28	200.47	31.21	0.01	0.00
130	0.00	3	SLE F	-123161.00	39945,20	-18629.50	46.00	136.36	0.50	20.00	180.17	18.85	831.00	326.29	0.10	0.03
131	59.52	3	SLE F	-123513.00	42182.90	-19673.10	46.00	136.36	0.50	20.00	185.24	18.85	878.77	381.88	0.11	0.04
132	119.05	3	SLE F	-122538.00	43532.20	-20302.40	46.00	136,36	0.50	20.00	188.73	18,85	911.68	424.67	0.12	0.04
133	178,57	3	SLE F	-121567.00	44122,70	-20577.80	46.00	136,36	0.50	20.00	190.50	18.85	928.35	447.67	0.13	0.04
134	238.09	3	SLE F	-120599.00	44073.90	-20555.00	46.00	136.36	0.50	20.00	191.05	18,85	933.53	452.76	0.13	0.04
135	297.62	3	SLE F	-119636.00	43495.00	-20285.00	46.00	136,36	0.50	20.00	190.64	18.85	929,62	442.65	0.13	0.04
136	357.14	3	SLE F	-118676.00	42444.60	-19795.10	46.00	136.36	0.50	20.00	189.30	18.85	917.00	419.23	0.12	0.04
137	416.57	3	SLE F	-115842.00	40859.20	-19055.80	46.00	136.36	0.50	20.00	188.12	18.85	905.91	393.30	0.11	0.04
138	475,19	3	SLE F	-113015.00	38823,20	-18106.20	46.00	136.36	0.50	20.00	185.78	18,85	883.82	355.44	0.10	0.03
139	535.71	.3	SLE F	-110194.00	36455.40	-17001.90	46.00	136,36	0.50	20.00	182,19	18.85	849,98	309.98	0.09	0.03
140	595.24	3	SLE F	-107378.00	33859.30	-15791.20	46.00	136.36	0.50	20.00	219.77	12.57	802.78	260.87	0.08	0.03
141	654.76	3	SLE F	-104569.00	31123.80	-14515.40	46.00	136.36	0.50	20.00	209.69	12.57	739.46	211.56	0.06	0.02
142	714.29	3	SLE F	-101765.00	28324.40	-13209.80	46.00	136,36	0.50	20.00	194.95	12.57	646.88	164.80	0.05	0.02
143	773.81	3	SLE F	-98966.10	25524.20	-11903.90	46.00	136,36	0.50	20.00	178.38	12.57	542.74	122.60	0.04	0.01

144 833.33	3 SLE F	-96172.90 22	2774.90	-10621.70	46.00	136.36	0.50	20.00	160.61	12.57	431.06	86.14	0.03	0.01
145 892.86	3 SLE F	-93384.80 20	0118.20	-9382.64	46.00	136.36	0.50	20.00	192.39	6.28	315.37	55.77	0.02	0.01
146 952.38	3 SLE F	-90601.80 17	7586.50	-8201.95	46.00	136,36	0.50	20.00	155.81	6.28	200.47	31.21	0.01	0.00

Verifiche principali

Caso	Tipo
- 5	SLU N cost - min. sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
48	C.Rare - Sf max (max traz.)
63	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
91	C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
106	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 30

Caratteristiche del palo e dei materiali utilizzati

R <cm></cm>	Ct S	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20,59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 30 (-45)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	122242.00	7017.10	919.22	59193.90	17945.20
	1	SLU	TAG				0.00	0.00
	1	SLU	ECC		9		0.00	0.00
	1	SLU	TOT	122242.00	7017,10	919,22	59193.90	17945.20
2	2	SLE R	RVN	90549.90	5197.85	680.90	43847.30	13292.70
	. 2	SLE R	TAG	_			0.00	0.00
	2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	90549.90	5197.85	680.90	43847.30	13292.70
3	3	SLE F	RVN	90549.90	5197.85	680.90	43847.30	13292.70
	3	SLE F	TAG		3		0.00	0.00
	. 3	SLE F	ECC	-	6 5		0.00	0.00
	-3	SLE F	TOT	90549.90	5197.85	680.90	43847.30	13292.70
4	4	SLE Q	RVN	90549.90	5197.85	680.90	43847.30	13292.70
- 4	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC	7	e :		0.00	0.00
	4	SLE Q	TOT	90549.90	5197.85	680.90	43847.30	13292.70

Sollecitazioni nei pali

Caso	8	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
-1	1	SLU	. 1	-122242.00	-7017,10	-919,22	-59193.90	-17945.20
- 2	2	SLE R	1	-90549.90	-5197.85	-680.90	-43847.30	-13292.70
.3	3	SLE F	1	-90549.90	-5197.85	-680.90	-43847.30	-13292.70
4	4	SLE Q	1	-90549.90	-5197.85	-680.90	-43847.30	-13292.70

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1	0.00	1	SIU	-122242.00	58952.90	-17872.10	-122242.00	187689.00	-56570.80	2-3	196.88	3.182
2	59.52	1	SIAJ	-122601.00	62260.80	-18874.90	-122601.00	187814.00	-56610.50	2-3	196.88	3,015
-3	119.05	1	SIU	-121638.00	64256.70	-19480.00	-121638.00	187478.00	-56504.00	2-3	196.88	2.916
4	178.57	1	SLU	-120680.00	65131.90	-19745.30	-120680.00	187144.00	-56397.90	2-3	196.88	2.872
5	238.09	1	SLU	-119725.00	65062.90	-19724.40	-119725.00	186811.00	-56292.30	2-3	196.88	2.870
- 6	297.62	1	SLU	-118774.00	64211.10	-19466.20	-118774.00	186477.00	-56186.40	2-3	196.88	2.903
7	357.14	1	SLU	-117827.00	62662.80	-18996.80	-117827.00	186145.00	-56081.00	2-3	196.88	2.969
8	416.67	1	SIJJ	-115015.00	60324.30	-18287.80	-115015.00	185159.00	-55767.90	2-3	196.88	3.068
	476.19	1	SLU	-112209.00	57320.00	-17377.10	-112209.00	184160.00	-55477.50	2-3	196.88	3.211
1.0	535.71	1	SLU	-109409.00	53825.60	-16317.70	-109409.00	183119.00	-55251.20	2-3	196.88	3.401
11	595,24	1	SIU	-106616.00	49993.90	-15156.10	-106616.00	182074.00	-55028.20	2-3	196.88	3.641

							Relazio	ne di cal	colo			
12	654.76	1	SW	-103827.00	45956.10	-13932.00		181030.00	· Control of the cont	2-3	196.88	3.939
13	714.29	1	SLU	-101045.00	41823.60	-12679.20	-101045.00	179989.00	-54580.40	2+3	196.88	4.304
14	773.81	1	SIU	-98267.40	37689.80	-11426.00	-98267.40	178944.00	-54358.80	2-3	196.88	4.749
15	833.33	1	SIJJ	-95495.50	33630.90	-10195.50	-95495.50	177898.00	-54138.00	2-3	196.88	5,291
16	892.86	1	SLU	-92728.70	29708.60	-9006.42	-92728.70	176855.00	-53916.50	2-3	196.88	5.956
17	952.38	1	SLU	-89966.80	25970.80	-7873.28	-89966.80	175811.00	-53695.40	2-3	196.88	6.774
18	1011.90	1	SIJJ	-87209.80	22453.90	-6807.09	-87209.80	175279.00	-51537,20	2-3	196.25	7.787
19	1071.43	1	SLU	-84457.50	19183.70	-5815.71	-84457.50	174232.00	-51322.90	2-3	196.25	9,061
20	1130.95	1	SLU	-81709.60	16177.30	~4904.28	-81709,60	173185.00	-51080.50	2-3	196.25	10.681
21	1190.48	1	SIJJ	-78966.20	13443.90	~4075.64	-78966.20	172132.00	-50757.20	2-3	196.25	12.775
22	1250.00	1	SLU	-76227.00	10986.50	-3330.65	-76227.00	171080.00	-50433.90	2-3	196.25	15.536
23	1309.52	1	SLU	-73491,90	8802.62	-2668.59	-73491.90	170028.00	-50111.20	2-3	196.25	19.271
24	1369.05	1	SIAJ	-70760.70	6885.45	-2087.39	-70760.70	168974.00	-49786.60	2-3	196.25	24.483
25	1428.57	1	SLU	-68033,40	5224.67	-1583.90	-68033,40	167918.00	-49461.10	2-3	196.25	32,064
26	1488.10	1	SLU	-65309.60	3807.21	-1154.19	-2571250.00	166864.00	-49136.00	2-3	196.25	39.370
27	1547.62	1	SILI	-62589.40	2617.94	-793.65	-2571250.00	165808.00	-48810.30	2-3	196.25	41.081
-28	1607.14	1	SLU	-59872.60	1640,21	-497.24	-2571250.00	164749.00	-48482.40	2-3	196.25	42,945
29	1666.67	1	SLU	-57158.90	856.33	-259.61	-2571250.00	163691.00	-48155.00	2-3	196.25	44.984
30	1726.19	1	SLU	-54448.30	247.98	-75.18	-2571250.00	162633.00	-47827.80	2-3	196.25	47.224
31	1785,71	1	SIA	-51740.70	-203,53	61.70	-2571250.00	-161252.00	48570.30	2-3	16.88	49,695
32	1845,24	1	SLU	-49035.80	-516.95	156.72	-2571250.00	-160218.00	48239.40	2-3	16.88	52.436
33	1904.76	1	SIJJ	-46333.50	-710.96	215.53	-2571250.00	-159185.00	47908.70	2-3	16.88	55.494
34	1964.29	1	SIJJ	-43633.70	-804.04	243.75	-2571250.00	-158152.00	47578.10	2-3	16.88	58,928
35	2023.81	1	SLU	-40936.30	-814.36	246.88	-2571250.00	-157117.00	47245.60	2-3	16.88	62.811
36	2083.33	1	SLU	-38241.10	-759.78	230.33	-2571250.00	-156082.00	46913.30	2-3	16.88	67.238
37	2142.86	1	SLU	-35547.90	-657.83	199.43	-2571250.00	-155006.00	46647.40	2-3	16.88	72.332
38	2202.38	1	SLU	-32856.60	-525.73	159.38	-2571250.00	-153910.00	46411.70	2-3	16.88	78.257
39	2261.90	1	SLU	-30167.10	-380.42	115.33	-2571250.00	-152811.00	46178.00	2-3	16.88	85.234
40	2321.43	1	SIA	-27479.20	-238.66	72.35	-2571250.00	-151712.00	45943.30	2-3	16.88	93.571
41	2380.95	1	SLU	-24792.80	-117.02	35.48	-2571250.00	-150613.00	45707,50	2-3	16.88	>100
42	2440.48	1	SLU	-22107.70	-31.99	9.70	-2571250.00	-149508.00	45476.50	2-3	16.88	>100
43	2500.00	- 1	SIU	-19423.70	0.00	0.00	-2571250.00	l.				>100

Caso	X <cm>></cm>	cc	1000	- Verifi Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7017.10	919,22	0.85	11.31	7077.05	1.00	32294.70	349178.00	32294.70	4.56
.2	59.52	1	SLU	4558.30	597.12	0.85	11.31	4597.25	1,00	32294.70	349229.00	32294.70	7.02
3	119.05	1	SIAI	2445.42	320.34	0.85	11.31	2466.31	1,00	32294.70	349091.00	32294.70	13.09
4	178,57	1	SIA	652.75	85.51	0.85	11.31	658.32	1.00	32294.70	348954.00	32294.70	49.05
.5	238.09	1	SLU	-845.99	-110.82	0.85	11.31	853.21	1.00	32294.70	348817,00	32294.70	37.85
- 6	297.62	1	SLU	-2077.20	-272.11	0.85	11.31	2094.94	1.00	32294.70	348681.00	32294.70	15.41
7	357.14	1	SLU	-3378.76	-442.61	0.85	11.31	3407.63	1.00	32294.70	348546.00	32294.70	9.47
8	416.67	1	SIJ	-4704.23	-616.24	0.85	11.31	4744.42	1.00	32294.70	348143.00	32294.70	6.80
9	476.19	1	SIU	-5703.44	-747.13	0.85	11.31	5752.17	1.00	32294.70	347741.00	32294.70	5.61
10	535.71	1	SLU	-6417.24	-840.64	0.85	11,31	6472.06	1.00	32294.70	347340.00	32294.70	4.99
11	595,24	1	SLU	-6884.17	-901.81	0.85	11.31	6942.99	1.00	32294.70	346940.00	32294.70	4,65
12	654.76	1	SLU	-7140.27	-935.36	0.85	11.31	7201.28	1,00	32294.70	346540.00	32294.70	4.48
13	714.29	3	SLU	-7218.80	-945.64	0.85	11.31	7280.48	1.00	32294.70	346142,00	32294.70	4.43
14	773.81	-1	SIJJ	-7150.19	-936.65	0.85	11.31	7211.27	1,00	32294.70	345744.00	32294.70	4.47
15	833.33	1	SLU	-6961.98	-912.00	0.85	11.31	7021.46	1,00	32294.70	345347.00	32294.70	4.59
16	892,86	1	SLU	-6678.88	-874.91	0.85	11.31	6735.95	1.00	32294.70	344951.00	32294.70	4.79
17	952,38	1	SIU	-6322,83	-828.27	0.85	11.31	6376.85	1.00	32294.70	344555.00	32294.70	5.06
18	1011.90	1	SLU	-5913.08	-774.60	0.85	11.31	5963.60	1.00	32294.70	344160.00	32294.70	5.41
19	1071.43	1	SIAI	-5466.40	-716.08	0.85	11.31	5513.10	1.00	32294.70	343766.00	32294.70	5.85
20	1130.95	1	SIU	-4997.18	-654.62	0.85	11.31	5039.87	1.00	32294.70	343372.00	32294.70	6,40
21	1190.48	1	SIJJ	-4517.63	-591.80	0.85	11.31	4556.22	1.00	32294.70	342979,00	32294.70	7.08
22	1250.00	1	SLU	-4037.99	-528.97	0.85	11.31	4072.48	1.00	32294.70	342587.00	32294.70	7.93
23	1309.52	1	SLU	-3566.68	-467.23	0.85	11,31	3597,15	1.00	32294.70	342195.00	32294.70	8,97
24	1369.05	1	SLU	-3110.52	-407.47	0.85	11.31	3137.10	1.00	32294.70	341804.00	32294.70	10.29
25	1428.57	1	SLU	-2674.93	-350.41	0.85	11.31	2697.78	1.00	32294.70	341413.00	32294.70	11.97
26	1488.10	1	SLU	-2264.05	-296.58	0.85	11.31	2283.39	1.00	32294.70	341023.00	32294.70	14.14
27	1547.62	1	SIJJ	-1880.98	-246.40	0.85	11.31	1897.05	1.00	32294.70	340633.00	32294.70	17.02
28	1607.14	1	SLU	-1527.91	-200.15	0.85	11.31	1540.97	1,00	32294.70	340244.00	32294,70	20.95
29	1666.67	1	SLU	-1206.30	-158.02	0.85	11.31	1216.61	1.00	32294.70	339855.00	32294.70	26.54
30	1726.19	1	SLU	-916.97	-120.12	0.85	11.31	924.81	1.00	32294.70	339467.00	32294.70	34.92
31	1785.71	1	SLU	-660.29	-86.50	0.85	11.31	665.93	1.00	32294.70	339079,00	32294.70	48.49
32	1845.24	1	SLU	-436.23	-57.15	0.85	11.31	439.96	1.00	32294.70	338692.00	32294.70	73.40
33	1904.76	1	SIJ	-244.54	-32.03	0.85	11.31	246.63	1.00	32294.70	338305,00	32294.70	>100
34	1964,29	1	SIU	-84.76	-11,10	0.85	11.31	85.48	1.00	32294.70	337918.00	32294.70	>100
35	2023.81	1	SLU	43.65	5.72	0.85	11.31	44.02	1.00	32294.70	337532.00	32294.70	>100
36	2083,33	1	SLU	141.27	18.51	0.85	11.31	142.48	1.00	32294.70	337146.00	32294.70	>100
37	2142.86	1	SLU	208.66	27.33	0.85	11.31	210.44	1.00	32294.70	336760.00	32294.70	>100
38	2202.38	1	SLU	246.31	32.27	0.85	11.31	248.42	1,00	32294.70	336374.00	32294.70	>100
39	2261,90	1	SIU	254.67	33.36	0.85	11.31	256.84	1.00	32294.70	335989.00	32294.70	>100
40	2321,43	1	SLU	234.03	30.66	0.85	11.31	236.03	1.00	32294.70	335604,00	32294.70	>100
41	2380.95	1	SLU	184.64	24.19	0.85	11.31	186.22	1.00	32294.70	335219.00	32294.70	>100

erifiche	stato	limite	d	esercizio	

	x	-		e d'eserc	Mz	My	AfT	AfC	σ _{i2}	o _f
Caso	<cm></cm>	cc	TCC	<dan></dan>	<danm></danm>	<danm></danm>	<amq></amq>	<mq></mq>		<dan cmq=""></dan>
44	0.00	2	SLE R	-90549.90	-13238.60	43668.80	40.84	37.70	41.46	607.54
45	59.52	2	SLE R	-91128.60	-13981.40	46119.10	40.84	37.70	44,12	683.53
46	119.05	2	SLE R	-90605.90	-14429.60	47597.50	40.84	37.70	45,80	738.78
47	178.57	2	SLE R	-90086.00	-14626.20	48245.90	40.84	37.70	46.56	766.23
48	238.09	2	SLE R	-89568.90	-14610.70	48194.80	40.84	37,70	46.54	769.64
49	297.62	2	SLE R	-89054.70	-14419.40	47563.80	40.84	37.70	45.88	752.98
50	357.14	2	SLE R	-88543.20	-14071.70	46416.90	40.84	37.70	44.65	718.64
51	416.67	2	SLE R	-86475.50	-13546.50	44684.70	40.84	37.70	42.89	679.75
52	476,19	2	SLE R	-84412.40	-12871.90	42459.30	40.84	37.70	40.58	624.40
53	535.71	2	SLE R	-82353.80	-12087.20	39870.80	40.84	37.70	37.87	557.62
54	595.24	2	SLE R	-80299.60	-11226.70	37032.50	40.84	37.70	34,90	484.04
55	654.76	2	SLE R	-78249.80	-10320.00	34041.50	40.84	37.70	31.78	431.12
56	714.29	2	SLE R	-76204.10	-9392.01	30980.50	37.70	40.84	28.61	389.93
57	773.81	2	SLE R	-74162.50	-8463.70	27918.40	34.56	43.98	25.50	349.25
58	833.33	2	SLE R	-72124.90	-7552.23	24911.80	34.56	43.98	22.52	310.19
59	892.86	2	SLE R	-70091.20	-6671.42	22006.40	31.42	47.12	19.76	273.72
60	952.38	2	SLE R	-68061.20	-5832.06		28.27	50.27	17.27	
61	1011.90	2	SLE R		-5042.29	19237.60	25.13	53.41	15.08	240.62
-		-		-66034.90						
62	1071.43	2	SIE R	-64012.10	-4307.93	14210.20	21.99	56.55	13.20	186.02
63	1130.95	2	SLE R	-61992.70	-3632.80	11983.20	15.71	62.83	11.61	164.42
64	1190.48	2	SLE R	-59976.70	-3018.99	9958.44	3.14	75.40	10.27	146.06
65	1250.00	2		-57963.90	-2467.15	8138.14	0.00	78.54	9.11	130.20
66	1309,52	2	SLE R	-55954.20	-1976.74	6520.46	0.00	78.54	8.07	115.92
67	1369.05	2	SLE R	-53947.50	-1546.21	5100.34	0.00	78.54	7.14	103.08
- 68	1428.57	2	SLE R	-51943.70	-1173.26	3870.13	0.00	78.54	6.31	91.64
69	1488.10	2	SLE R	-49942.70	-854.96	2820.16	0.00	78,54	5,58	81.52
7.0	1547.62	2	SLE R	-47944.40	-587.89	1939.21	0.00	78.54	4.95	72.64
71	1607.14	2	SLE R	-45948.60	-368.33	1214.97	0.00	78.54	4.39	64.91
72	1666.67	2	SLE R	-43955.30	-192.30	634.32	0.00	78,54	3.92	58.23
73	1726.19	2	SLE R	-41964.40	-55.69	183.69	0.00	78.54	3.51	52.51
74	1785.71	2	SLE R	-39975.70	45.70	-150.76	0.00	78.54	3.33	49.85
75	1845.24	2	SLE R	-37989.10	116.09	-382.92	0.00	78.54	3.29	49.13
76	1904.76	2	SLE R	-36004.60	159.66	-526,64	0.00	78,54	3.21	47,77
77	1964.29	2	SLE R	-34022.00	180.56	-595.58	0.00	78.54	3.09	45.86
78	2023.81	2	SLE R	-32041.30	182.87	-603.23	0.00	78.54	2.93	43.50
79	2083.33	2	SLE R	-30062.20	170.62	-562.80	0.00	78.54	2,75	40.79
80	2142.86	2	SLE R	-28084.80	147.72	-487.28	0.00	78.54	2.55	37.83
81	2202.38	2	SLE R	-26108.90	118.06	-389.43	0.00	78.54	2,33	34.70
82	2261.90	2	SLE R	-24134.40	85,43	-281.80	0.00	78,54	2.11	31,50
83	2321.43	2	SLE R	-22161,20	53.59	-176.79	0.00	78.54	1,90	28.32
84	2380.95	2	SLE R	-20189.10	26.28	+86.68	0.00	_	1.69	25.25
-	2440.48	-	-	-18218.20						22.39
-	2500.00	_		-16248.20			0.00			
		_					-	_		19.81
87	0.00				-13238.60					
88					-13981.40					683.53
89	119.05	_			-14429.60					
90	178.57	_			-14626.20				46.56	
91	238.09				-14610.70				46.54	769.64
92	297.62				-14419.40					
93		_			-14071.70	THE RESERVE AND ADDRESS OF THE PARTY.	-		44.65	
94					-13546.50					
95					-12871.90					
96	Commence of the Control of the Contr				-12087.20					557.62
-97	595.24				-11226.70					484.04
98		_			-10320.00					431.12
99					-9392.01					389.93
100	773.81				-8463.70	27918,40	34.56	43,98	25,50	
101	833.33	4	SLE Q	-72124.90	-7552.23	24911.80	34.56	43.98	22.52	310.19
102	892.86	4	SLE Q	-70091.20	-6671,42	22006.40	31.42	47.12	19.76	273.72
103	952.38			-68061.20					17.27	240.62
104	1011.90			-66034.90		16632.50	25.13	53.41	15.08	211.35
105	1071,43				-4307.93	The second secon			13,20	186.02
	1130.95	_			-3632.80				11.61	164.42
	1190.48				-3018.99					
	1250.00			-57963.90		8138.14			9.11	130.20
-	1309.52			-55954.20						115.92
_	1369.05	_	_	-53947.50					7.14	103.08
	1428.57			-51943.70				78.54		91.64
-	1488.10			-49942.70			_	78.54	-	81.52
-	1547.62		SLE Q					78.54	4.95	72.64
_	1607.14			-45948.60			_	78.54		64.91
_							_	_		58.23
113	1666.67	1 9	SLE Q	-43955.30	-192.30	634.32	0.00	78.54	3.92	58.2

116	1726.19	4	SLE	Q	-41964.40	-55.69	183.69	0.00	78.54	3.51	52.51
117	1785.71	4	SLE	Q	-39975.70	45.70	-150.76	0.00	78.54	3.33	49.85
118	1845.24	4	SLE	Q	-37989.10	116.09	-382.92	0.00	78.54	3.29	49.13
119	1904.76	4	SLE	Q	-36004.60	159.66	-526.64	0.00	78.54	3.21	47.77
120	1964.29	4	SLE	Q	-34022.00	180.56	-595.58	0.00	78.54	3.09	45.86
121	2023.81	4	SLE	Q	-32041.30	182.87	-603.23	0.00	78.54	2.93	43.50
122	2083.33	4	SLE	Q	-30062.20	170.62	-562.80	0.00	78.54	2.75	40.79
123	2142,86	4	SLE	Q	-28084.80	147.72	-487.28	0.00	78.54	2,55	37.83
124	2202.38	4	SLE	Ö	-26108.90	118.05	-389.43	0.00	78.54	2.33	34.70
125	2261.90	4	SLE	Q	-24134.40	85.43	-281.80	0.00	78.54	2.11	31.50
126	2321.43	4	SLE (Q	-22161.20	53.59	-176.79	0.00	78.54	1.90	28.32
127	2380.95	4	SLE	Q	-20189,10	26.28	-86.68	0.00	78,54	1.69	25.25
128	2440.48	4	SLE	Q	-18218.20	7.18	-23.70	0.00	78.54	1.49	22,39
129	2500.00	4	SLE	Ó	-16248.20	0.00	0.00	0.00	78.54	1.32	19.81

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	C <mm></mm>	s <mm></mm>	K 2	Фец	Δ _{SIM} <mm></mm>	A _H <cmq></cmq>	A _{c eff}	σ _g <dan cmq=""></dan>	esm	Wk <mm></mm>
87	0.00	4	SLE Q	-90549.90	43668.80	-13238.60	46.00	136,36	0.50	20.00	203.81	18.85	1053.77	607.54	0.18	0.06
88	59.52	4	SLE Q	-91128.60	46119.10	-13981.40	46,00	136.36	0.50	20.00	189.89	21.99	1076.32	683,53	0.20	0.06
89	119.05	4	SLE Q	-90605.90	47597.50	-14429.60	46.00	136.36	0.50	20.00	191.34	21.99	1092.35	738.78	0.22	0.07
90	178.57	4	SLE Q	-90086.00	48245.90	-14626.20	46.00	136,36	0.50	20.00	192.06	21.99	1100.18	766.23	0.22	0.07
91	238.09	4	SLE Q	-89568.90	48194,80	-14610.70	46.00	136.36	0.50	20.00	192.23	21.99	1102.05	769.64	0.22	0.07
92	297.62	4	SLE Q	-89054.70	47563.80	-14419.40	46.00	136.36	0.50	20.00	191.96	21.99	1099.09	752.98	0.22	0.07
93	357,14	4	SLE Q	-88543.20	46416.90	-14071.70	46.00	136.36	0.50	20.00	191.27	21,99	1091.48	718.64	0.21	0.07
94	416.67	4	SLE Q	-86475.50	44684.70	-13546.50	46.00	136.36	0.50	20.00	190.71	21.99	1085.41	679.75	0.20	0.06
95	476.19	4	SLE Q	-84412.40	42459.30	-12871.90	46.00	136,36	0.50	20.00	189.64	21.99	1073.57	624.40	0.18	0.08
96	535.71	4	SIE Q	-82353.80	39870.80	-12087.20	46.00	136,36	0.50	20.00	204.01	18.85	1055.67	557.62	0.16	0.06
97	595.24	4	SLE Q	-80299.60	37032.50	-11226.70	46.00	136.36	0.50	20.00	201.38	18.85	1030.89	484.04	0,14	0.05
98	654.76	4	SLE Q	-78249.80	34041.50	-10320.00	46.00	136.36	0.50	20.00	219.05	15.71	997.87	407.83	0.12	0.04
99	714.29	4	SLE Q	-76204.10	30980.50	-9392.01	46.00	136.36	0.50	20.00	213,56	15.71	954.70	332,70	0.10	0.04
100	773.81	4	SLE Q	-74162.50	27918.40	-8463.70	46.00	136.36	0.50	20.00	206.44	15.71	898.81	261.85	0.08	0.03
101	833.33	4	SLE Q	-72124.90	24911.80	-7552.23	46.00	136.36	0.50	20.00	197.23	15.71	826.49	197.93	0.06	0.02
102	892.86	4	SLE Q	-70091.20	22006.40	-6671.42	46.00	136,36	0.50	20.00	183.57	15.71	719.20	142.83	0.04	0.03
103	952.38	4	SLE Q	-68061.20	19237.60	-5832.06	46.00	136.36	0.50	20.00	183.27	12.57	573.46	97.53	0.03	0.01
104	1011.90	4	SLE Q	-66034.90	16632,50	-5042.29	46.00	136.36	0.50	20.00	180.87	9,42	418.78	61.87	0.02	0.01
105	1071.43	4	SLE Q	-64012.10	14210,20	-4307.93	46.00	136,36	0.50	20.00	177.63	6,28	269.00	34.83	0.01	0.00
130	0.00	3	SLE F	-90549.90	43668.80	-13238.60	46.00	136,36	0.50	20.00	203.81	18.85	1053,77	607.54	0.18	0.00
131	59.52	3	SLE F	-91128.60	46119.10	-13981.40	46.00	136.36	0.50	20.00	189.89	21.99	1076.32	683.53	0.20	0.00
132	119.05	3	SLE F	-90605.90	47597.50	-14429.60	46.00	136,36	0.50	20.00	191.34	21.99	1092.35	738.78	0.22	0.0
133	178.57	3	SLE F	-90086.00	48245.90	-14626.20	46.00	136,36	0.50	20.00	192.06	21.99	1100,18	766.23	0.22	0.0
134	238.09	3	SLE F	-89568.90	48194.80	-14610.70	46.00	136.36	0.50	20.00	192.23	21,99	1102.05	769.64	0.22	0.07
135	297.62	3	SLE F	-89054.70	47563.80	-14419.40	46.00	136.36	0.50	20.00	191.96	21.99	1099.09	752.98	0.22	0.07
136	357.14	3	SLE F	-88543.20	46416.90	-14071.70	46.00	136.36	0.50	20.00	191.27	21,99	1091.48	718.64	0.21	0.07
137	416.67	3	SLE F	-86475.50	44684.70	-13546.50	46.00	136.36	0.50	20.00	190.71	21.99	1085.41	679.75	0.20	0.00
138	476.19	3	SLE F	-84412.40	42459.30	-12871.90	46.00	136.36	0.50	20.00	189.64	21.99	1073.57	524.40	0.18	0.06
139	535.71	.3	SLE F	-82353.80	39870.80	-12087.20	46.00	136.36	0.50	20.00	204.01	18.85	1055.67	557.62	0.16	0.06
140	595.24	3	SLE F	-80299.60	37032.50	-11226.70	46.00	136.36	0.50	20.00	201.38	18.85	1030.89	484.04	0.14	0.09
141	654.76	3	SLE F	-78249.80	34041.50	-10320.00	46.00	136,36	0.50	20.00	219.05	15.71	997.87	407.83	0.12	0.04
142	714.29	3	SLE F	-76204.10	30980.50	-9392,01	46.00	136.36	0.50	20.00	213.56	15.71	954.70	332.70	0.10	0.04
143	773.81	3	SIE F	-74162.50	27918.40	-8463.70	46.00	136,36	0.50	20.00	206.44	15.71	898.81	261.85	0.08	0.03
144	833.33	3	SLE F	-72124.90	24911.80	-7552.23	46.00	136.36	0.50	20.00	197.23	15.71	826.49	197.93	0.06	0.02
145	892.86	3	SLE P	-70091.20	22006.40	-6671.42	46.00	136.36	0.50	20.00	183.57	15,71	719,20	142.83	0.04	0.00
146	952.38	3	SLE F	-68061.20	19237.60	-5832.06	46.00	136,36	0.50	20.00	183.27	12.57	573.46	97.53	0.03	0.01
147	1011.90	3	SLE F	-66034.90	16632.50	-5042.29	46.00	136.36	0.50	20.00	180.87	9.42	418.78	61.87	0.02	0.01
148	1071.43	3	SLE F	-64012.10	14210.20	-4307.93	46.00	136.36	0.50	20.00	177.63	6.28	269.00	34.83	0.01	0.00

Verifiche principali

Caso	Tipo
5	SLU N cost - min. sic.
13	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
47	C.Rare - Sc min (max compr.), C.Rare - Sf min (max compr.)
48	C.Rare - Sf max (max traz.)
65	C.Rare - Sc max (min. compr.)
90	C.Q.Per Sc min (max compr.), C.Q.Per Sf min (max compr.)
91	C.Q.Per Sf max (max traz.), C.Q.Per Wk Max
108	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 31

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq2<="" th=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	8450C	4300.00	3913.04

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 31 (-28)

Caso	cc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	80635,20	7265.62	800.64	60527.60	10374.60
	-1	SLU	TAG			3 3	0.00	0.00
	. 1	SIU	ECC				0.00	0.00
	1	SLU	TOT	80635.20	7265.62	800.64	60527.60	10374.60
2	. 2	SLE R	RVN	59729.80	5381.94	593.07	44835.20	7684.90
	2	SLE R	TAG				0.00	0.00
	49	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	59729.80	5381.94	593.07	44835.20	7684.90
3	3	SLE F	RVN	59729.80	5381.94	593.07	44835.20	7684.90
	3	SLE F	TAG			<u>.</u>	0.00	0.00
	. 3	SLE F	ECC				0.00	0.00
	3	SLE F	TOT	59729.80	5381.94	593.07	44835.20	7684.90
- 4	-4	SLE Q	RVN	59729.80	5381.94	593.07	44835.20	7684.90
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC			5 3	0.00	0.00
	4	SLE Q	TOT	59729.80	5381.94	593.07	44835.20	7684.90

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mix <danm></danm>	My <danm></danm>	
1	1	SLU	- 1	-80635.20	-7265.62	-800.64	-60527.60	-10374.60	
2	2	SLE R	1	-59729.80	-5381.94	-593.07	-44835.20	-7684.90	
- 3	3	SLE F	1	-59729.80	-5381.94	-593.07	-44835.20	-7684.90	
4	.4	SLE Q	1	-59729.80	-5381.94	-593.07	-44835.20	-7684.90	

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflession

Caso	Y		TCC	N	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SIJ	-80635.20	60276.80	-10331.60	-80635.20	177270.00	-31113.90	2-3	190.00	2.943
2	59,52	1	SLU	-81282.80	63812.70	-10937.70	-81282.80	177521.00	-31160.50	2-3	190.00	2.784
- 3	119.05	1	SLU	-80897.60	65983.30	-11309.70	-80897.60	177372.00	-31132,80	2-3	190.00	2.690
4	178.57	1	SIU	-80515.00	66986.50	-11481.70	-80515.00	177224.00	-31105.20	2-3	190.00	2.647
5	238.09	1	SLU	-80134.80	67005.30	-11484.90	-80134.80	177077.00	-31077.90	2-3	190.00	2.645
- 6	297.62	1	SLU	-79757.20	66206.80	-11348.10	-79757.20	176931.00	-31050.70	2-3	190.00	2.674
7	357.14	1	SIJ	-79382.10	64680.10	-11086.40	-79382.10	176786.00	-31023.60	2-3	190.00	2.735
B	416.67	1	SLU	-77547.20	62325.60	-10682.80	-77547.20	176076.00	-30891.50	2-3	190.00	2.827
:9	476,19	1	SIU	-75716.40	59272.10	-10159,40	-75716.40	175367.00	-30759.70	2-3	190.00	2,961
10	535.71	1	SLU	-73889.70	55702.10	-9547.52	-73889,70	174659.00	-30627.90	2-3	190.00	3.138
11	595.24	1	SLU	-72067.00	51774.60	-8874.33	-72067.00	173950.00	-30495.50	2-3	190.00	3.362
12	654.76	1	SLU	-70248.10	47626.30	-8163.30	-7024B.10	173242.00	-30363.40	2-3	190.00	3.640
13	714.29	1	SIU	-68433.00	43373.40	-7434.33	-68433.00	172536.00	-30231.60	2-3	190.00	3.980
14	773.81	1	SIU	-66621,50	39113.00	-6704.09	-66621,50	171830.00	-30100.10	2-3	190.00	4,396
15	833.33	1	SLU	-64813.60	34925.00	-5986.26	-64813.60	171126.00	-29968.80	2-3	190.00	4,903
16	892.86	1	SIU	-63009.30	30873.90	-5291.88	-63009.30	170421.00	-29837.00	2-3	190.00	5.523
17	952.38	1	SIJJ	-61208.20	27009.90	-4629.58	-61208.20	169716.00	-29705.10	2-3	190.00	6.287
18	1011.90	1	SILI	-59410.50	23371.30	-4005.91	-59410.50	169013.00	-29573.50	2-3	190.00	7.236
19	1071.43	1	SLU	-57616.00	19985.30	-3425.55	-57616.00	168310.00	-29442.10	2-3	190.00	8.427
20	1130.95	-1	SLU	-55824,50	16870.20	-2891.61	-55824,50	167608.00	-29310.90	2-3	190.00	9,941
21	1190.48	1	SIU	-54036.00	14036.00	-2405.82	-54036.00	166907.00	-29179.90	2-3	190.00	11.898
22	1250.00	1	SIU	-52250.50	11486.10	-1968.75	-52250.50	166205.00	-29048.10	2-3	190.00	14.478
23	1309.52	1	SIU	-50467.70	9218.33	-1580.05	-50467.70	165504.00	-28916.50	2-3	190.00	17.964
24	1369.05	1	SIJ	-48687,70	7225.94	-1238.55	-48687.70	164803.00	-28785.10	2-3	190.00	22.820
25	1428.57	11	SEU	-46910.20	5498.51	-942.46	-46910.20	164103.00	-28653.80	2-3	190.00	29.861
26	1488.10	1	SIU	-45135.30	4022.76	-689,51	-45135,30	163404.00	-28522.80	2-3	190.00	40.643
27	1547.62	1	SIJ	-43362.80	2783.19	-477.05	-43362.80	162705.00	-28391,60	2-3	190.00	58.490
28	1607.14	1	SLU	-41592.60	1762.74	-302.14	-2571250.00	162005.00	-28259.90	2-3	190.00	61.820
29	1666.67	1	SIU	-39824.70	943.24	-161.67	-2571250.00	161306.00	-28128.30	2-3	190.00	64.564
30	1726.19	1	SLU	-38058.90	305.79	-52.41	-2571250.00	160584.00	-28048.80	2+3	190.00	67.560
31	1785.71	1	SLU	-36295.10	-168.84	28.94	-2571250.00	-159568.00	28255,10	2-3	10.00	70.843
32	1845.24	1	SIJJ	-34533.30	-500.02	85.71	-2571250.00	-158847.00	28121.40	2-3	10.00	74.457
33	1904.76	1	SLU	-32773,30	-707.04	121.19	-2571250.00	-158127.00	27987.80	2-3	10.00	78.456
34	1964.29	1	SIJ	-31015.10	-808.99	138.66	-2571250.00	-157408.00	27854.40	2-3	10.00	82.903
35	2023.81	1	SIU	-29258.50	-824.67	141.35	-2571250,00	-156690.00	27721.20	2-3	10.00	87.880

36	2083.33	1	SLU	-27503,60	-772.56	132.42	-2571250.00	-155970.00	27587.50	2-3	10.00	93.488
37	2142.86	1	SLU	-25750.10	-670.79	114.98	-2571250.00	-155248.00	27453.10	2-3	10.00	99.854
38	2202.38	1	SIU	-23997.90	-537.21	92.08	-2571250,00	-154528.00	27318.90	2-3	10.00	>100
39	2261,90	1	SIJ	-22247.10	-389.35	66.74	-2571250.00	-153807.00	27184.70	2-3	10.00	>100
40	2321.43	1	SLU	-20497.50	-244.57	41.92	-2571250.00	-153087.00	27050.60	2-3	10.00	>100
41	2380.95	1	SLU	-18748.90	-120.05	20.58	-2571250.00	-152366.00	26916.60	2-3	10.00	>100
42	2440.48	1	SIU	-17001.40	-32.85	5.63	-2571250.00	-151644.00	26781.40	2-3	10.00	>100
43	2500.00	1	SLU	-15254.80	0.00	0.00	-2571250.00					>100

Caso	X <cm>></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	atg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7265.62	800.64	0.85	11.31	7309.60	1,00	32294.70	343218.00	32294.70	4.418
- 2	59.52	1	SLU	4776.01	526.29	0.85	11.31	4804.92	1.00	32294.70	343311.00	32294.70	6.721
- 3	119.05	1	SIJ	2634.82	290.35	0.85	11.31	2650.77	1.00	32294.70	343256,00	32294.70	12.183
4	178.57	1	SLU	816.40	89.96	0.85	11.31	821.34	1.00	32294.70	343201.00	32294.70	39.319
5	238.09	1	SIA	-705.53	-77.75	0.85	11,31	709.80	1.00	32294.70	343147.00	32294.70	45,498
- 6	297.62	1	SIJJ	-1957,45	-215.70	0.85	11.31	1969.30	1.00	32294.70	343092.00	32294.70	16.399
7	357.14	1	SLU	-3283.39	-361.81	0.85	11.31	3303.26	1.00	32294.70	343039.00	32294.70	9.777
. 8	416.67	1	SLU	-4636.22	-510.89	0.85	11.31	4664.28	1.00	32294.70	342776.00	32294.70	6.924
. 9	476.19	1	SIJJ	-5659.05	-623.60	0.85	11.31	5693.30	1.00	32294.70	342514.00	32294.70	5.672
10	535.71	1	SIJ	-6392.97	-704.48	0.85	11.31	6431.67	1.00	32294.70	342252.00	32294.70	5.021
-11	595.24	1	SLU	-6876.83	-757.80	0.85	11.31	6918.46	1,00	32294.70	341991.00	32294.70	4.668
12	654.76	1	SLU	-7146.90	-787.56	0.85	11.31	7190.17	1.00	32294.70	341730.00	32294.70	4,492
13	714.29	1	SLU	-7236.75	-797.46	0.85	11.31	7280.55	1.00	32294.70	341470.00	32294.70	4.436
14	773.81	1	SLU	-7177.06	-790.88	0.85	11.31	7220.50	1.00	32294.70	341211.00	32294.70	4.473
15	833.33	1	SLU	-6995.66	-770.89	0.85	11.31	7038.01	1.00	32294.70	340952.00	32294.70	4.589
16	892,86	1	SLU	-6717,51	-740.24	0.85	11.31	6758.18	1.00	32294.70	340693,00	32294.70	4,779
17	952.38	1	SLU	-6364.79	-701.37	0.85	11.31	6403.32	1.00	32294.70	340436.00	32294.70	5.043
18	1011.90	1	SLU	-5957.00	-656.43	0.85	11.31	5993.06	1.00	32294.70	34017B.00	32294.70	5,389
19	1071.43	1	SLU	-5511.09	-607.30	0.85	11.31	5544.45	1.00	32294.70	339921.00	32294.70	5.825
20	1130.95	1	SLU	-5041.67	-555.57	0.85	11.31	5072.19	1.00	32294.70	339664.00	32294.70	6.36
21	1190.48	1	SLU	-4561.13	-502.62	0.85	11.31	4588.74	1.00	32294.70	339408.00	32294.70	7.038
22	1250.00	1	SLU	-4079,85	-449.58	0.85	11.31	4104,55	1.00	32294.70	339152.00	32294.70	7.868
23	1309.52	1	SIU	-3606.41	-397.41	0.85	11.31	3628.24	1.00	32294.70	338897.00	32294.70	8.900
24	1369.05	1	SIJJ	-3147.76	-346.87	0.85	11.31	3166.81	1.00	32294.70	338642.00	32294.70	10.198
25	1428.57	1	SLU	-2709.40	-298.56	0.85	11.31	2725.80	1.00	32294.70	338387.00	32294.70	11.848
26	1488.10	1	SLU	-2295.59	-252.96	0.85	11,31	2309.48	1.00	32294.70	338133.00	32294.70	13.983
27	1547.62	1	SIM	-1909.51	-210.42	0.85	11.31	1921.07	1,00	32294.70	337879.00	32294.70	16.811
.28	1607.14	1	SIAJ	-1553.42	-171.18	0.85	11.31	1562.82	1.00	32294.70	337626.00	32294.70	20.664
29	1666.67	1	SLU	-1228.82	-135.41	0.85	11.31	1236.26	1.00	32294.70	337373.00	32294.70	26.123
30	1726.19	1	SIA	-936.60	-103.21	0.85	11.31	942.27	1.00	32294.70	337120.00	32294.70	34.273
31	1785.71	1	SILI	-677.15	-74.62	0.85	11.31	681.25	1.00	32294.70	336867,00	32294.70	47.405
32	1845,24	1	SIJ	-450.50	-49.64	0.85	11.31	453.22	1.00	32294.70	336615.00	32294.70	71.256
33	1904.76	1	SIJJ	-256.38	-28.25	0.85	11.31	257.94	1.00	32294.70	336363.00	32294.70	>100
34	1964.29	1	SLU	-94.38	-10.40	0.85	11,31	94.95	1.00	32294.70	336111.00	32294.70	>100
35	2023.81	1	SLU	36.03	3.97	0.85	11.31	36.25	1.00	32294.70	335859.00	32294.70	>100
36	2083.33	1	SLU	135,43	14.92	0.85	11.31	136.25	1.00	32294.70	335608.00	32294.70	>100
37	2142.86	1	SLU	204.37	22.52	0.85	11.31	205.60	1.00	32294.70	335356.00	32294.70	>100
38	2202.38	1	SIJ	243.34	26.81	0.85	11.31	244.81	1,00	32294.70	335106.00	32294.70	>100
39	2261.90	1	SLU	252.77	27.85	0.85	11.31	254.30	1,00	32294.70	334855.00	32294.70	>100
40	2321.43	1	SLU	232.97	25.67	0.85	11,31	234.38	1.00	32294.70	334604,00	32294.70	>100
41	2380.95	1	SIU	184.17	20.29	0.85	11.31	185.29	1.00	32294.70	334354.00	32294.70	>100
42	2440.48	1	SLU	106.50	11.74	0.85	11.31	107.14	1.00	32294.70	334103.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm>></cm>	cc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <mq></mq>	o _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-59729.80	-7653.06	44649.50	43.98	34.56	42.91	916.46
45	59.52	2	SLE B	-60522.70	-8102.00	47268.70	43.98	34.56	45.61	1002,42
46	119.05	2	SLE R	-60427.50	-8377.59	48876.50	43.98	34.56	47.31	1062,45
47	178.57	2	SLE B	-60334.20	-8504.97	49619.70	43.98	34.56	48.09	1090.89
48	238.09	-2	SLE R	-60242.70	-8507.36	49633.60	43.98	34.56	48.11	1092.52
49	297.62	2	SLE R	-60153.20	-8405.97	49042.10	43.98	34.56	47.50	1071.86
50	357,14	2	SLE R	-60065.50	-8212.13	47911,20	43.98	34.56	46.32	1031,42
51	416.67	2	SLE R	-58721.50	-7913.19	46167.10	43.98	34.56	44.58	983.74
52	476.19	2	SLE R	-57380.70	-7525.50	43905.20	43.98	34.56	42.29	917.21
53	535.71	2	SLE R	-56042.90	-7072.24	41260.80	43.98	34.56	39.60	836.97
54	595.24	2	SLE R	-54708.10	-6573.58	38351.50	43.98	34.56	36.62	747.61
55	654.76	2	SLE R	-53376.30	-6046.89	35278.70	43.98	34.56	33.47	653.16
56	714.29	2	SLE R	-52047.30	-5506.91	32128.40	43,98	34,56	30,23	557.16
57	773.81	2	SLE R	-50721.10	-4965.99	28972.60	43.98	34.56	26.98	462.73
58	833.33	2	SLE R	-49397.60	-4434.27	25870.40	40.84	37.70	23.79	372.62
59	892.86	2	SLE R	-48076.80	-3919.91	22869.50	37.70	40.84	20.72	289.30
6.0	952.38	2	SLE R	-46758.50	-3429.32	20007.30	37.70	40.84	17.83	246.22
61	1011.90	2	SLE B	-45442.80	-2967.34	17312.00	37.70	40.84	15.18	211.01
- 62	1071.43	2	SLE R	-44129.50	-2537.45	14804.00	31.42	47.12	12,82	179.51

66 1309.0 8 2 51E R - 41509.9 0 1-782.0 9 10397.00 55.13 53.41 9.14 129.65 6 1269.07 2 11E R - 40509.5 9 1-782.0 9 10397.00 55.13 53.41 9.14 129.65 6 1309.5 2 2 51E R - 37897.10 - 1917.44 5352.5 5 0.00 78.54 5.84 84.0 6 1428.37 5 2 51E R - 36997.00 - 698.1 4028.37 0.00 78.54 5.84 84.0 6 6 1428.37 5 2 51E R - 36997.00 - 698.12 4072.97 0.00 78.54 5.80 5.07 73.3 19.6 1438.30 12 51E R - 30397.00 - 698.2 4072.97 0.00 78.54 4.39 63.9 10 1547.6 2 51E R - 33702.40 - 353.37 2051.6 0.00 78.54 4.39 63.9 171 1607.14 2 51E R - 33407.90 -5223.81 1305.74 0.00 78.54 4.39 63.9 171 1607.14 2 51E R - 33407.90 -223.81 1305.74 0.00 78.54 2.39 48.20 171 1607.14 2 51E R - 33407.90 -223.81 1305.74 0.00 78.54 2.39 48.20 173 1726.10 2 51E R - 33407.90 -223.81 1305.74 0.00 78.54 2.39 48.20 173 1726.10 2 51E R - 32407.90 -3882 226.51 0.00 78.54 2.39 43.30 36.60 75 1845.2 2 51E R - 72746.50 63.49 -370.39 0.00 78.54 2.39 43.30 36.60 75 1845.2 2 51E R - 72746.50 63.49 -370.39 0.00 78.54 2.39 35.60 75 1845.2 2 51E R - 72746.50 63.49 -370.39 0.00 78.54 2.33 35.60 75 1845.2 2 51E R - 72746.50 63.49 -370.39 0.00 78.54 2.33 35.60 75 1945.2 2 51E R - 72746.50 63.49 -370.39 0.00 78.54 2.33 35.60 75 1945.2 2 51E R - 72746.50 63.49 -370.39 0.00 78.54 2.33 35.60 75 1945.2 2 51E R - 72746.50 63.09 -370.2 2 51E R - 72746.50 63.00 89.77 -523.73 0.00 78.54 2.33 35.60 75 1945.2 2 51E R - 72746.50 63.09 -370.2 2 51E R - 72746.50 63.00 89.77 -523.73 0.00 78.54 2.32 34.2 2 51E R - 72746.50 63.00 89.77 -523.73 0.00 78.54 2.32 34.2 3 51E R - 72745.50 63.00 89.77 -523.73 0.00 78.54 2.32 34.2 3 51E R - 72745.50 63.00 89.77 -523.73 0.00 78.54 2.32 34.2 3 51E R - 72745.50 63.00 89.77 -523.73 0.00 78.54 1.00 8.2 3 51E R - 72745.50 63.00 89.77 -523.73 0.00 78.54 1.00 8.2 3 51E R - 72745.50 63.00 89.77 -523.73 0.00 78.54 1.00 8.2 3 51E R - 72745.50 50 89.77 -7244 8.2 50.00 78.54 1.00 8.2 3 51E R - 72745.50 50 89.77 -7244 8.2 50.00 78.54 1.00 8.2 3 51E R - 72745.50 68.2 3 51					1	S		£	 		ne ui ca	
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105 1071,43	103	952.38	4	SLE	Q	-46758.50	-3429.32	20007.30	37.70	40.84	17.83	246.22
106 1130.95	1.04	1011.90	4	SLE	Q	-45442.80	-2967.34	17312.00	37.70	40.84	15.18	211.01
106 1130.95	105	1071.43	4	SLE	0	-44129.50	-2537.45	14804.00	31.42	47.12	12.82	179.51
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129 2500.00 4 SLE Q -13160.10 0.00 0.00 0.00 78.54 1.07 16.05			_	_						-		
	129	2500.00	4	SLE	Q	-13160.10	0.00	0.00	0.00	78.54	1.07	16.05

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	Φ_{eq}	Δ _{SID} <mm></mm>	A _S <cmq></cmq>	A _{C REF}	σ _S <dan cmq=""></dan>	eam	Wk <mm></mm>
87	0.00	4	SLE Q	-59729.80	44649.50	-7653.06	46.00	136.36	0.50	20.00	202.24	21.99	1212.19	915.46	0.27	0.09
88	59.52	4	SLE Q	-60522.70	47268,70	-8102.00	46.00	136.36	0.50	20,00	203.14	21,99	1222.06	1002.42	0.29	0.10
89	119.05	4	SLE Q	-60427.50	48876.50	-8377.59	46.00	136.36	0.50	20.00	203.81	21.99	1229.45	1062.45	0.31	0.11
90	178,57	4	SLE Q	-60334,20	49619.70	-8504.97	46.00	136.36	0.50	20,00	204.12	21.99	1232.81	1090,89	0.32	0.11
91	238.09	4	SLE Q	-60242.70	49633.60	-8507.36	46.00	136.36	0.50	20.00	204.15	21.99	1233.17	1092.52	0.32	0.11
92	297.62	4	SLE Q	-60153.20	49042.10	-8405.97	46.00	136.36	0.50	20.00	203.96	21.99	1231.07	1071.86	0.31	0.11

							Re	lazio	ne d	i cal	colo					
93	357.14	4	SLE Q	-60065.50	47911.20	-8212.13						21.99	1226.56	1031.42	0.30	0.10
94	416.67	4	SLE Q	-58721.50	46167.10	-7913.19	_	136.36	0.50	20.00	203.27	21.99	1223.49	983.74	-	_
95	476.19	4	SLE Q	-57380.70	43905.20	-7525.50	46.00	136.36	0.50	20.00	202.73	21,99	1217.53	917.21	0.27	0.09
-96	535.71	4	SLE Q	-56042.90	41260.80	-7072.24	46.00	136.36	0.50	20,00	220.24	18.85	1208.59	836.97	0.24	0.09
97	595.24	4	SLE Q	-54708.10	38351.50	-6573.58	46.00	136.36	0.50	20.00	218.94	18.85	1196.35	747.61	0.22	0.08
98	654.76	4	SLE Q	-53376.30	35278.70	-6046.89	46.00	136.36	0.50	20.00	217.22	18.85	1180.20	653.16	0.19	0.07
99	714.29	4	SLE Q	-52047.30	32128.40	-5506.91	46.00	136.36	0.50	20.00	215.00	18.85	1159.25	557.16	0.16	0.06
100	773.81	4	SLE Q	-50721.10	28972.60	-4965.99	46.00	136,36	0.50	20.00	212.12	18.85	1132.15	462.73	0.13	0.05
101	833.33	4	SLE Q	-49397.60	25870.40	~4434.27	46.00	136,36	0.50	20.00	208.39	18.85	1096.96	372.62	0.11	0.04
102	892.86	4	SLE Q	-48076.80	22869.50	-3919.91	46.00	136.36	0.50	20.00	203.50	18.85	1050.91	289.30	0.08	0.03
103	952,38	4	SLE Q	-46758.50	20007.30	-3429.32	46.00	136.36	0.50	20.00	197.07	18.85	990.23	214.99	0.06	0.02
104	1011.90	4	SLE Q	-45442.80	17312.00	-2967.34	46.00	136.36	0.50	20.00	188.17	18.85	906.36	151.57	0.04	0.01
105	1071.43	4	SLE Q	-44129.50	14804.00	-2537.45	46.00	136,36	0.50	20.00	217.13	12.57	786.19	100.32	0.03	0.01
106	1130.95	4	SLE Q	-42818.60	12496.50	-2141.93	46.00	136,36	0.50	20.00	188.28	12.57	604.95	61.31	0.02	0.01
107	1190.48	4	SLE Q	-41509.90	10397.00	-1782.09	46.00	136.36	0.50	20.00	177.68	9.42	403.74	33.34	0.01	0.00
108	1250.00	4	SLE Q	-40203.50	8508.22	-1458.34	46.00	136.36	0.50	20.00	158.53	6.28	209.00	14.17	0.00	0.00
130	0.00	3	SLE F	-59729.80	44649,50	-7653.06	46.00	136.36	0.50	20,00	202.24	21,99	1212.19	916.46	0.27	0.09
131	59,52	3	SLE F	-60522.70	47268.70	-8102.00	46.00	136.36	0.50	20.00	203.14	21.99	1222.06	1002.42	0.29	0.10
132	119.05	3	SLE F	-60427.50	48876.50	-8377.59	46.00	136.36	0.50	20.00	203.81	21.99	1229.45	1062.45	0.31	0.11
133	178.57	3	SLE F	-60334,20	49619.70	-85G4.97	46.00	136,36	0.50	20.00	204.12	21.99	1232.81	1090.89	0.32	0.11
134	238.09	3	SLE F	-60242.70	49633.60	-8507.36	46.00	136,36	0.50	20.00	204.15	21.99	1233.17	1092.52	0.32	0.11
135	297.62	3	SLE F	-60153.20	49042.10	-8405.97	46.00	136,36	0.50	20.00	203.96	21.99	1231.07	1071.86	0.31	0.11
136	357,14	.3	SLE F	-60065.50	47911,20	-8212.13	46.00	136.36	0.50	20.00	203.55	21,99	1226.56	1031.42	0.30	0.10
137	416.67	3	SLE F	-58721.50	46167.10	-7913.19	46.00	136.36	0.50	20.00	203.27	21.99	1223.49	983.74	0.29	0,10
138	476.19	3	SLE F	-57380.70	43905.20	-7525.50	46.00	136.36	0.50	20.00	202.73	21,99	1217,53	917.21	0.27	0.09
139	535.71	3	SLE F	-56042.90	41260.80	-7072.24	46.00	136.36	0.50	20.00	220.24	18.85	1208.59	836.97	0.24	0.09
140	595,24	3	SLE F	-54708.10	38351.50	-6573.58	46.00	136.36	0.50	20.00	218.94	18.85	1196.35	747.61	0.22	0.08
141	654.76	3	SLE F	-53376.30	35278.70	-6046.89	46.00	136.36	0.50	20.00	217.22	18.85	1180.20	653.16	0.19	0.07
142	714.29	3	SLE F	-52047.30	32128.40	-5506.91	46.00	136.36	0.50	20.00	215.00	18.85	1159.25	557.16	0.16	0.06
143	773.81	3	SLE F	-50721.10	28972,60	-4965.99	46.00	136.36	0.50	20,00	212.12	18,85	1132.15	462,73	0.13	0.05
144	833,33	3	SLE F	-49397.60	25870.40	-4434.27	46.00	136,36	0.50	20.00	208.39	18.85	1096.96	372,62	0.11	0.04
145	892.86	3	SLE F	-48076.80	22869.50	-3919.91	46.00	136,36	0.50	20,00	203.50	18,85	1050.91	289.30	0.08	0.03
146	952.38	3	SLE F	-46758.50	20007.30	-3429.32	46.00	136.36	0.50	20.00	197.07	18.85	990.23	214.99	0.06	0.02
147	1011.90	3	SLE F	-45442.80	17312.00	-2967.34	46.00	136,36	0.50	20.00	188.17	18.85	906.36	151.57	0.04	0.01
148	1071.43	3	SLE F	-44129.50	14804.00	-2537.45	46.00	136,36	0.50	20.00	217.13	12,57	786.19	100.32	0.03	0.01
149	1130.95	3	SLE F	-42818.60	12496.50	-2141.93	46.00	136.36	0.50	20,00	188,28	12,57	604.95	61,31	0.02	0.01
150	1190.48	3	SLE F	-41509.90	10397.00	-1782.09	46.00	136.36	0.50	20.00	177.68	9.42	403.74	33.34	0.01	0.00
151	1250.00	3	SLE F	-40203.50	8508.22	-1458.34	46.00	136.36	0.50	20.00	158.53	6.28	209.00	14.17	0.00	0.00

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
67	C.Rare - Sc max (min. compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
110	C.Q.Per Sc max (min. compr.)
	C.Freq - Wk Max

Palo n. 32

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307.10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 32 (-16)

Caso	oc	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	46634.90	7464.38	623.03	59187.90	4732.68
	.1	SIU	TAG				0.00	0.00
	1	SIJI	ECC				0.00	0.00
	1	SLU	TOT	46634.90	7464.38	623.03	59187.90	4732,68
2	2	SLE R	RVN	34544.40	5529.17	461.50	43842.90	3505.69
	2	SLE R	TAG			8 8	0.00	0.00
	2	SLE R	ECC			\$ B	0.00	0.00
	2	SLE R	TOT	34544.40	5529.17	461.50	43842.90	3505.69
-3	3	SLE F	RVN	34544.40	5529.17	461.50	43842.90	3505.69

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1	_1	3	SLE	F	TAG				0.00	0.00
		3	SLE	F	ECC				0.00	0.00
		3	SLE	F	TOT	34544.40	5529.17	461.50	43842.90	3505.69
Г	4	4	SLE	Q	RVN	34544.40	5529.17	461.50	43842.90	3505.69
		4	SLE	Q	TAG				0.00	0.00
		4	SLE	Q	ECC				0.00	0.00
Г		4	SLE	Q	TOT	34544.40	5529.17	461.50	43842.90	3505.69

Sollecitazioni nei pali

Caso	œ	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	1	-46634,90	-7464.38	-623.03	-59187.90	-4732.68
2	2	SLE R	1	-34544.40	-5529,17	-461.50	-43842.90	-3505.69
- 3	3	SLE F	1	-34544.40	-5529.17	-461.50	-43842.90	-3505,69
4	4	SLE Q	1	-34544.40	-5529.17	-461.50	-43842.90	-3505.69

Da 0 a -25

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1	0.00	1	SIA	-46634.90	58936.20	-4712.55	-46634.90	165723.00	-14208,90	2-3	185.00	2,813
- 2	59.52	1	SLU	-47518.90	62625.50	-5007.55	-47518.90	166086.00	-14235.80	2=3	185.00	2.653
- 3	119.05	1	SLU	-47605.30	64943.70	-5192.91	-47605.30	166122.00	-14238.40	2-3	185.00	2.559
- 4	178.57	1	SLU	-47693.20	66088.30	-5284.43	-47693.20	166158.00	-14241.10	2-3	185.00	2.515
- 5	238.09	1	SIJ	~47782.60	66241,40	-5296.67	-47782,60	166194.00	-14243.80	2-3	185.00	2,510
.6	297.62	1	SLU	-47873.50	65570.00	-5242.99	-47873.50	166232.00	-14246.60	2-3	185.00	2.536
- 7	357.14	1	SIU	-47965.90	64162.20	-5130.42	-47965.90	166270.00	-14249.40	2-3	185,00	2.593
8	416.67	1	SIJ	-46929.40	61915.20	-4950.75	-46929.40	165844.00	-14217.80	2-3	185.00	2.680
9	476.19	1	SLU	-45895.40	58957.10	-4714.22	-45895,40	165419.00	-14186.30	2-3	185.00	2.807
1.0	535.71	1	SLU	-44863.90	55470.90	-4435,46	-44863.90	164995.00	-14154.90	2-3	185.00	2.976
11	595.24	1	SLU	-43834.80	51616.10	-4127.23	-43834.80	164572.00	-14123.50	2-3	185.00	3.190
12	654.76	1	SLU	-42808.00	47530.20	-3800.52	-42808.00	164150.00	-14092.10	2-3	185.00	3.455
13	714.29	1	SIAI	-41783.50	43330.00	-3464.67	-41783.50	163727.00	-14061.50	2-3	185.00	3,780
14	773.81	1	SLU	-40761.30	39113.50	-3127.52	-40761,30	163304.00	-14030.90	2-3	185.00	4.177
15	833.33	1	SLU	-39741.20	34961.40	-2795.52	-39741.20	162883.00	-14000.30	2-3	185.00	4.661
16	892.86	1	SEU	-38723.30	30938.90	-2473.88	-38723.30	162462.00	-13969.80	2-3	185.00	5.254
17	952.38	1	SLU	-37707.50	27097.10	-2166.69	-37707.50	162041.00	-13939.20	2+3	185,00	5.983
18	1011,90	1	SIJ	-36693.60	23474.90	-1877.06	-36693.60	161622.00	-13908.70	2-3	185.00	6.888
19	1071.43	1	SIJ	-35681.80	20100.50	-1607.24	-35681.80	161203.00	-13878.30	2-3	185.00	8.024
20	1130.95	1	SLU	-34671.80	16992.50	-1358.72	-34671.80	160785.00	-13847.80	2-3	185.00	9.467
21	1190.48	1	SLU	-33663.80	14161.80	-1132.38	-33663.80	160368.00	-13817.40	2-3	185.00	11.330
22	1250.00	1	SIAI	-32657.50	11612.30	+928,52	-32657.50	159949.00	-13787.80	2-3	185.00	13.781
23	1309.52	1	SIAJ	-31653.00	9342.34	-747.01	-31653.00	159531.00	-13758.20	2-3	185.00	17.085
24	1369.05	1	SLU	-30650,10	7345.72	-587.37	-30650,10	159113.00	-13730.80	2-3	185.00	21,672
25	1428.57	1	SIU	-29649.00	5612.42	-448.77	-29649.00	158693.00	-13707.00	2-3	185.00	28.290
26	1488,10	1	SIA	-28649.40	4129.55	-330.20	-28649.40	158274.00	-13683.30	2-3	185.00	38.348
27	1547,62	1	SIJ	-27651.30	2881.96	-230.44	-27651,30	157855.00	-13659.40	2-3	185.00	54.803
28	1607.14	1	SIU	-26654.70	1852.87	-148.16	-26654.70	157438.00	-13639.60	2-3	185.00	85.016
29	1666.67	1	SLU	-25659.60	1024.38	-81.91	-2571250.00	157020.00	-13611.70	2-3	185.00	>100
30	1726.19	1	SIJ	-24665.80	377.83	-30.21	-2571250.00	156603.00	-13587.90	2-3	185,00	>100
31	1785.71	1	SLU	-23673.40	-105.84	8,46	-2571250.00	-156368.00	13524.80	2-3	5.00	>1.00
32	1845,24	1	SLU	-22682.20	-445.84	35,65	-2571250.00	-155958.00	13454.90	2-3	5.00	>100
-33	1904.76	-1	SIJ	-21692.30	-661.31	52.88	-2571250.00	-155549.00	13385.30	2-3	5.00	>100
34	1964.29	1	SLU	-20703.50	-771.23	61.67	-2571250.00	-155139.00	13313.60	2-3	5.00	>100
35	2023.81	1	SLU	-19715.80	-794.30	63.51	-2571250.00	-154730.00	13241.80	2-3	5.00	>100
36	2083.33	1	SIJJ	-18729.20	-748.91	59.88	-2571250.00	-154322.00	13170.20	2-3	5.00	>100
37	2142.86	1	SLU	-17743.50	-653.15	52.23	-2571250,00	-153914.00	13098.90	2-3	5.00	>100
38	2202.38	1	SLU	-16758.90	-524.77	41.96	-2571250.00	-153502.00	13027.20	2-3	5.00	>100
39	2261.90	1	SIU	-15775.10	-381.27	30.49	-2571250.00	-153094.00	12956.10	2-3	5.00	>100
40	2321.43	1	SIU	-14792.20	~239.97	19.19	-2571250.00	-152686.00	12885.20	2-3	5.00	>100
41	2380.95	1	SLU	-13810.10	-117.97	9.43	-2571250,00	-152263.00	12852.40	2-3	5.00	>100
42	2440.48	1	SIU	-12828.70	-32.32	2,58	-2571250.00	-151840.00	12821.60	2-3	5.00	>100
43	2500.00	1	SIJ	-11848.00	0.00	0.00	-2571250.00					>100

Stato limite ultimo - Verifiche a taglio

Caso	X <cm></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
:1	0.00	1	SIJ	7464.38	623.03	0.85	11.31	7490.34	1.00	32294.70	338348.00	32294.70	4.312
- 2	59.52	1	SLU	4987.57	416.30	0.85	11.31	5004.91	1,00	32294.70	338475.00	32294.70	6.453
3	119.05	1	SIU	2854.72	238.27	0.85	11.31	2864.64	1.00	32294.70	338487.00	32294.70	11.274
- 4	178.57	1	SLU	1040.82	86.87	0.85	11.31	1044.44	1.00	32294.70	338500.00	32294.70	30.921
.5	238.09	1	SIU	-479.79	-40.05	0.85	11.31	481.46	1.00	32294.70	338512.00	32294.70	67.07€
6	297.62	1	SLU	-1733.03	-144.65	0.85	11.31	1739.06	1.00	32294.70	338525.00	32294.70	18.570
7	357.14	1	SIU	-3064.02	-255.74	0.85	11.31	3074.67	1.00	32294.70	338539.00	32294.70	10.504
8	416.67	1	SIJ	-4425.68	-369.40	0.85	11.31	4441.07	1.00	32294.70	338390.00	32294.70	7.272

								RE	Hazi	one ai	caicoio		
9	476.19	1	SLU	-5459.57	-455.69	0.85	11.31	5478.56	1.00	32294.70	338242.00	32294.70	5.895
1.0	535.71	1	SIJ	-6206.18	-518.01	0.85	11.31	6227.76	1.00	32294.70	338094.00	32294.70	5.186
11	595.24	1	SIU	-6703.82	-559.55	0.85	11.31	6727.13	1.00	32294.70	337947.00	32294.70	4.801
12	654.76	1	SIJJ	-6988.34	-583.29	0.85	11.31	7012.64	1.00	32294.70	337800.00	32294.70	4.605
13	714.29	1	SLU	-7092.90	-592.02	0.85	11.31	7117.57	1.00	32294.70	337653.00	32294.70	4.537
14	773.81	1	SLU	-7047.91	-588.27	0.85	11.31	7072.42	1.00	32294.70	337507.00	32294.70	4.566
15	833.33	1	SLU	-6880.93	-574.33	0.85	11.31	6904.85	1.00	32294.70	337361.00	32294.70	4.677
1.5	892,86	ĭ	SIU	-6616.70	-552.27	0.85	11.31	6639.71	1.00	32294.70	337215.00	32294.70	4.864
17	952.38	1	SLU	-6277.26	-523.94	0.85	11.31	6299.09	1.00	32294.70	337069.00	32294.70	5.127
18	1011.90	1	SIJ	-5881.98	-490.95	0.85	11.31	5902.43	1,00	32294.70	336924.00	32294.70	5.471
19	1071.43	1	SLU	-5447.75	-454.71	0.85	11.31	5466.69	1,00	32294.70	336779.00	32294.70	5,908
20	1130.95	1	SLU	-4989.09	-416.42	0.85	11.31	5006.44	1.00	32294.70	336634.00	32294.70	6.451
21	1190.48	1	SIAJ	-4518.39	-377.14	0.85	11.31	4534.10	1.00	32294.70	336490.00	32294.70	7.123
22	1250.00	-1	SLU	-4046.02	-337.71	0.85	11.31	4060.09	1.00	32294.70	336346,00	32294.70	7.954
23	1309.52	1	SLU	-3580.57	-298.86	0.85	11.31	3593.02	1.00	32294.70	336202.00	32294.70	8.988
24	1369.05	1	SILI	-3129.00	-261.17	0.85	11.31	3139.88	1.00	32294.70	33605B.00	32294.70	10.285
25	1428.57	1	SIU	-2696.86	-225.10	0.85	11.31	2706.24	1.00	32294.70	335915.00	32294.70	11.933
26	1488.10	1	SIU	-2288.45	-191.01	0.85	11.31	2296.40	1.00	32294.70	335772.00	32294.70	14.063
27	1547.62	1	SLU	-1906.98	-159.17	0.85	11.31	1913.61	1.00	32294.70	335629,00	32294.70	16.876
28	1607.14	1	SLU	-1554.78	-129.77	0.85	11.31	1560.19	1.00	32294.70	335486.00	32294.70	20,699
29	1666.67	1	SLU	+1233.39	-102.95	0.85	11.31	1237.68	1.00	32294.70	335344.00	32294.70	26.093
30	1726.19	1	SIU	-943.76	-78.77	0.85	11.31	947.04	1.00	32294.70	335201.00	32294.70	34.101
31	1785.71	1	SIJJ	-686.31	-57.28	0.85	11.31	688.69	1.00	32294.70	335059.00	32294.70	46.893
32	1845.24	1	SLU	-461.12	-38.49	0.85	11.31	462.72	1.00	32294.70	334917.00	32294.70	69.793
.33	1904.76	1	SIU	-267.97	-22.37	0.85	11,31	268.90	1.00	32294.70	334775.00	32294.70	>100
34	1964.29	1	SLU	-106.48	-8.89	0.85	11.31	106.86	1.00	32294.70	334634.00	32294.70	>100
35	2023.81	1	SLU	23.84	1.99	0.85	11.31	23.92	1.00	32294.70	334492.00	32294.70	>100
36	2083.33	1	SLU	123.55	10.31	0.85	11.31	123.98	1.00	32294.70	334351.00	32294.70	>100
37	2142.86	1	SIU	193.16	16.12	0.85	11.31	193.84	1.00	32294.70	334210.00	32294.70	>100
38	2202,38	1	SIJ	233.17	19.46	0.85	11.31	233.99	1.00	32294.70	334069,00	32294.70	>100
39	2261.90	1	SLU	243.98	20.36	0.85	11.31	244.83	1,00	32294.70	333928.00	32294.70	>100
40	2321.43	1	SIU	225.89	18.85	0.85	11.31	226.68	1,00	32294.70	333787.00	32294.70	>100
41	2380.95	1	SLU	179.13	14.95	0.85	11.31	179.75	1.00	32294.70	333646.00	32294.70	>100
42	2440.48	1	SLU	103.81	8.67	0.85	11.31	104.18	1.00	32294.70	333506.00	32294.70	>100

Verifiche stato limite d'esercizio

Caso	X <cm></cm>	cc	TCC	N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <mg></mg>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
44	0.00	2	SLE R	-34544.40	-3490.78	43656.40	47.12		43.31	1182.42
45	59.52	2	SLE R	-35512.40	-3709.29	46389.30	47.12	31.42	46.08	1272.34
4.6	119,05	2	SLE R	-35766.50	-3846.60	48106.50	47.12	31.42	47.83	1333.61
47	178.57	2	SLE R	-36021.80	-3914.39	48954.30	47.12	31.42	48.70	1362.14
48	238.09	2	SLE R	-36278.10	-3923.46	49067.70	47.12	31.42	48.80	1362.98
49	297.62	2	SLE R	-36535.70	-3883.69	48570.30	47.12	31.42	48,28	1340.79
50	357,14	2	SLE R	-36794.30	-3800.31	47527,60	47.12	31.42	47.19	1298.09
51	416.67	2	SLE R	-36041.70	-3667.22	45863.10	47.12	31.42	45.51	1245.50
52	476,19	2	SLE R	-35291.10	-3492.01	43671.90	47.12	31.42	43.29	1173.10
53	535.71	2	SLE R	-34542.30	-3285.53	41089.50	47.12	31.42	40.66	1086.06
54	595,24	2	SLE R	-33795.40	-3057.21	38234.10	47.12	31.42	37.75	988.89
55	654.76	2	SLE R	-33050.30	-2815,20	35207.50	47.12	31.42	34.65	885.50
56	714.29	2	SIE R	-32306.90	-2566.43	32096.30	47.12	31,42	31.46	779.27
57	773.81	2	SLE R	-31565.30	-2316.68	28973.00	47.12	31.42	28.25	673.05
58	833.33	2	SLE R	-30825.40	-2070.76	25897.40	47.12	31.42	25.08	569.25
59	892.86	2	SLE R	-30087.20	-1832,50	22917.70	47.12	31.42	22.00	469.93
60	952.38	2	SLE B	-29350.60	-1604.95	20071.90	43.98	34.56	19.04	376.82
61	1011.90	2	SLE R	-28615.50	-1390.41	17388.80	40.84	37.70	16.25	291.47
62	1071.43	2	SLE B	-27882.00	-1190.55	14889.20	40.84	37.70	13.66	215.35
63	1130.95	2	SLE R	-27149.90	-1006.46	12587.00	40.84	37.70	11.29	153.32
64	1190.48	2	SLE R	-26419.40	-838,80	10490.20	34.56	43.98	9.19	126.06
65	1250.00	2	SLE R	-25690.20	-687.79	8601.68	34.56	43.98	7.40	102.67
66	1309.52	2	SLE R	-24962.40	-553.34	6920.25	28.27	50.27	5.97	83.66
67	1369.05	2	SLE B	-24236.00	-435.08	5441.27	21,99	56.55	4.88	68.98
-68	1428.57	2	SLE R	-23510.80	-332.42	4157.35	6.28	72.26	4.07	57.91
69	1488.10	2	SLE R	-22786.90	-244.59	3058.92	0.00	78.54	3.44	49.26
70	1547.62	2	SLE R	-22064.30	-170.70	2134.78	0.00	78.54	2.90	41.89
71	1607.14	2	SLE R	-21342.80	-109.75	1372.50	0.00	78.54	2,45	35.66
72	1666.67	2	SLE R	-20622.50	-60,67	758.80	0.00	78,54	2.07	30,47
73	1726,19	2	SLE R	-19903.30	-22.38	279.87	0.00	78.54	1.76	26.23
74	1785.71	2	SLE R	-19185.10	6,27	-78.40	0.00	78.54	1,60	23.94
75	1845.24	2	SLE R	-18468.00	26.41	-330.25	0.00	78.54	1.67	24.85
76	1904.76	2	SLE R	-17751.80	39.17	-489.86	0.00	78.54	1,70	25.10
77	1964,29	2	SLE R	-17036.60	45.68	-571.28	0.00	78.54	1,68	24.81
78	2023.81	2	SLE R	-16322.40	47.05		0.00	78.54	1.63	24.06
79	2083.33	2	SLE R	-15609.00	44.36	-554.75	0.00	78,54	1.56	22.95
80	2142.86	2	SLE B	-14896.40	38.69	-483.81	0.00	78.54	1.46	21.58
81	2202.38	2	SLE R		31.08			78.54	1,35	20.04
82	2261.90	2	SLE R	-13473.70	22.58		0.00	78.54	1.24	18.42

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83	2321.43	2	SLE	R	-12763.40	14.21	-177.75	0.00	78.54	1,13	16.82
84	2380.95	2	SLE	R	-12053.80	6.99	-87.38	0.00	78.54	1.02	15.31
85	2440.48	2	SLE	R	-11344.80	1.91	-23.94	0.00	78.54	0.93	14.00
86	2500.00	2	SLE	R	-10636.50	0.00	0.00	0.00	78.54	0.86	12.97
87	0.00	4	SLE	Q	-34544.40	-3490.78	43656.40	47.12	31.42	43.31	1182.42
88	59.52	4	SLE	Q	-35512.40	-3709.29	46389.30	47.12	31.42	46.08	1272.34
89	119.05	4	SLE	Q	-35766.50	-3846,60	48106.50	47.12	31.42	47.83	1333.61
90	178.57	4	SLE	Q	-36021.80	-3914.39	48954.30	47.12	31.42	48.70	1362.14
91	238.09	4	SLE	Q	-36278.10	-3923.46	49067.70	47.12	31.42	48.80	1362.98
92	297.62	4	SLE	Q	-36535.70	-3883.69	48570.30	47.12	31.42	48.28	1340.79
93	357.14	4	SLE	Q	-36794.30	-3800.31	47527.60	47.12	31.42	47.19	1298.09
94	416.67	4	SLE	Q	-36041.70	-3667.22	45863.10	47.12	31.42	45.51	1245.50
95	476.19	4	SLE	Q	-35291.10	-3492.01	43671.90	47,12	31,42	43.29	1173.10
96	535.71	4	SLE	Q	-34542.30	-3285.53	41089.50	47.12	31.42	40.66	1086.06
97	595.24	4	SLE	Q	-33795.40	-3057.21	38234.10	47.12	31.42	37.75	988.89
.98	654.76	4	SLE	Q	-33050.30	-2815.20	35207.50	47.12	31.42	34,65	885.50
99	714.29	4	SLE	Q	-32306.90	-2566.43	32096.30	47.12	31.42	31.46	779.27
100	773.81	_	SLE	0		-2316.68	28973.00	47.12	31.42	28.25	673.05
101	833.33	_	SLE	Q		-2070.76	_	47.12	31,42	25.08	569.25
102	892.86	4	SLE	0		-1832.50	22917.70	_	31.42	22.00	469.93
103	952.38	4	SLE	0		-1604.95	20071.90	43.98	34.56	19.04	376.82
104		_	SLE	Q	-28615.50	-1390.41	17388.80		37.70	16.25	291.47
105	1071.43	-	SLE	_		-1190.55		-	-	13.66	215.35
_	1130.95	$\overline{}$	_	_	-27149.90	-1006.46		_	_	11.29	153.32
107	1190.48	4	-	Q		-838.80	10490.20	34.56	43.98	9.19	126.06
108	1250.00	_	SLE	0		-687.79	8601.68		43.98	7.40	102.67
_	1309.52	_	SLE	_		-553.34	6920.25	_	50.27	5.97	83.66
_	1369.05	4	SLE	0		-435.08	5441.27	_	56.55	4.88	68.98
-	1428.57	_	-	_	-23510.80	-332.42	4157.35		72.26	4.07	57.91
112	-	4	-	Q		-244.59	3058.92	-	78.54	3.44	49.26
_	1547.62	_	SLE	Q		-170.70	2134.78		78.54	2,90	41.89
	1607.14	4	-	0		-109.75	1372.50	_	78.54	2.45	35.66
115	1666.67	4	SLE	0		-60.67	758.80	_	78.54	2.07	30.47
_	1726.19	4	SLE	0	-19903.30	-22.38	279.87	0.00	78.54	1,76	26.23
_	1785.71	4	SLE	Q		6.27	-78.40	_	78.54	1.60	23.94
-	1845,24	4	-	0		26,41	-330.25	-	78.54	1.67	24.85
119	1904.76	4	SLE	Q	-17751.80	39.17	-489.86	0.00	78.54	1,70	25.10
120	1964.29	4	_	_		45.68	-571.28	0.00	78.54	1.68	24.81
121		_	SLE	Q	-16322.40	47.05	-588.37	_	78.54	1,63	24.06
122	2083.33	4	-	Q	-15609.00	44.36	-554.75		78.54	1.56	22.95
123	2142.86	4	-	Q		38.69	-483.81	0.00	-	1.46	21.58
124	2202.38	4	SLE	Q		31.08	-388.72	0.00	78.54	1.35	20.04
125	2261,90	_	SLE	Q		22.58	-282.43	_	78.54	1.24	18,42
-	2321.43	_	SLE	Q		14.21	-177.75		78.54	1.13	16.82
127		_	SLE	Q	-12053.80	6,99	-87.38	_	78.54	1,02	15.31
128	2440.48	_	SLE	Q		1.91	-23.94	_	78.54	0.93	14.00
_	2500.00	_	SLE	_		0.00	0.00	_	78.54	0.86	12.97

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	Φeq	Δ _{mm}	A ₂	Ac eff <cmq></cmq>	σ _S <dan cmq=""></dan>	e _{am}	Wk <mm></mm>
87	0.00	4	SLE Q	-34544.40	43656.40	-3490.78	46.00	136.36	0.50	20.00	208.75	21.99	1283.77	1182.42	0.34	0.12
88	59.52	4	SLE Q	-35512.40	46389.30	-3709.29	46.00	136.36	0.50	20.00	209.08	21.99	1287.34	1272.34	0.37	0.13
89	119.05	4	SLE Q	-35766.50	48106,50	-3846.60	46.00	136,36	0.50	20.00	209.35	21.99	1290.37	1333.61	0.39	0.14
90	178.57	4	SLE Q	-36021.80	48954.30	-3914.39	46.00	136.36	0.50	20.00	209.45	21.99	1291.42	1362.14	0.40	0.14
91	238.09	4	SLE Q	-36278.10	49067.70	-3923.46	46.00	136.36	0.50	20.00	209.41	21,99	1290.94	1362.98	0.40	0.14
.92	297.62	4	SLE Q	-36535.70	48570.30	~3883.69	46.00	136.36	0.50	20.00	209.25	21.99	1289.18	1340.79	0.39	0.14
93	357.14	4	SLE Q	-36794.30	47527.60	-3800.31	46.00	136,36	0.50	20.00	208.97	21.99	1286.15	1298.09	0.38	0.13
94	416.67	4	SLE Q	-36041.70	45863.10	-3667.22	46.00	135.36	0.50	20.00	208.82	21.99	1284.52	1245.50	0.36	0.13
95	476.19	4	SLE Q	-35291.10	43671.90	-3492.01	46.00	136.36	0.50	20.00	208.54	21.99	1281.41	1173,10	0.34	0.12
96	535.71	4	SLE Q	-34542.30	41089.50	-3285.53	46.00	136.36	0.50	20.00	208.12	21.99	1276,80	1086.06	0.32	0.11
97	595,24	4	SLE Q	-33795.40	38234.10	-3057.21	46.00	136.36	0.50	20.00	207.55	21,99	1270.58	988.89	0.29	0.10
98	654.76	4	SLE C	-33050.30	35207.50	-2815,20	46.00	136.36	0.50	20,00	206.82	21.99	1262.53	885.50	0.26	0.09
99	714.29	4	SLE Q	-32306.90	32096.30	-2566.43	46.00	136.36	0.50	20.00	205.89	21.99	1252.31	779.27	0.23	0.08
100	773.81	4	SLE Q	-31565.30	28973.00	-2316.68	46.00	136.36	0.50	20.00	204.72	21.99	1239.40	673.05	0.20	0.07
101	833.33	4	SLE Q	-30825.40	25897.40	-2070.76	46.00	136.36	0.50	20.00	203.23	21,99	1223.06	569,25	0.17	0.06
102	892,86	4	SLE Q	-30087.20	22917,70	-1832.50	46.00	136.36	0.50	20,00	201.32	21.99	1202.06	469,93	0.14	0.05
103	952.38	4	SLE Q	-29350.60	20071.90	-1604.95	46.00	136.36	0.50	20.00	198.82	21,99	1174.58	376.82	0.11	0.04
104	1011.90	4	SLE Q	-28615.50	17388.80	-1390.41	46.00	136.36	0.50	20.00	195.48	21.99	1137.87	291.47	0.08	0.03
105	1071.43	4	SLE Q	-27882.00	14889.20	-1190.55	46.00	136.36	0.50	20.00	190.92	21.99	1087.68	215.35	0.06	0.02
106	1130.95	4	SLE Q	-27149.90	12587.00	-1006.46	46.00	136.36	0.50	20.00	199.94	18.85	1017.31	149.93	0.04	0.01
107	1190,48	4	SLE Q	-26419.40	10490.20	-838.80	46.00	136,36	0.50	20.00	208.50	15.71	915.00	96.65	0.03	0.01
108	1250.00	4	SLE Q	-25690.20	B601.6B	-687,79	46.00	136.36	0.50	20,00	188.28	15.71	756.19	56.45	0.02	0.01
109	1309.52	4	SLE Q	-24962.40	6920.25	-553.34	46.00	136.36	0.50	20.00	198.13	9.42	500.15	28.83	0.01	0.00
110	1369.05	4	SLE Q	-24236.00	5441.27	-435.08	46.00	136.36	0.50	20,00	169.67	6,28	244.00	11.39	0.00	0.00
130	0.00	3	SLE F	-34544.40	43656.40	-3490.78	46.00	136,36	0.50	20.00	208.75	21,99	1283.77	1182,42	0.34	0.12
131	59.52	3	SLE F	-35512.40	46389.30	-3709.29	46.00	136.36	0.50	20,00	209.08	21.99	1287.34	1272.34	0.37	0.13

-	Maria Carlo Maria Carlo Car	A 12 (1985)		CONTRACTOR
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132	119.05	3	SLE F	-35766.50	48106.50	-3846.60	46.00	136.36	0.50	20.00	209.35	21,99	1290.37	1333.61	0.39	0.14
133	178.57	3	SLE F	-36021.80	48954.30	-3914.39	46.00	136.36	0.50	20.00	209.45	21.99	1291.42	1362.14	0.40	0.14
134	238.09	3	SLE F	-36278.10	49067.70	-3923.46	46.00	136.36	0.50	20.00	209.41	21,99	1290.94	1362.98	0.40	0.14
135	297.62	3	SLE F	-36535.70	48570.30	-3883.69	46.00	136.36	0.50	20.00	209.25	21.99	1289.18	1340.79	0.39	0.14
136	357.14	3	SLE F	-36794.30	47527.60	-3800.31	46.00	136.36	0.50	20,00	208.97	21,99	1286.15	1298.09	0.38	0.13
137	416.67	3	SLE F	-36041.70	45863.10	-3667.22	46.00	136.36	0.50	20.00	208.82	21,99	1284.52	1245.50	0.36	0.13
138	476.19	3	SLE F	-35291.10	43671.90	-3492.01	46.00	136.36	0.50	20.00	20B.54	21.99	1281.41	1173,10	0.34	0.12
139	535.71	3	SLE F	-34542.30	41089.50	-3285.53	46.00	136,36	0.50	20.00	208,12	21.99	1276.B0	1086.06	0.32	0.11
140	595.24	3	SLE F	-33795.40	38234.10	-3057.21	46.00	136,36	0.50	20.00	207.55	21.99	1270.58	988.89	0.29	0.10
141	654.76	3	SLE F	-33050.30	35207.50	-2815.20	46.00	136.36	0.50	20.00	206.82	21.99	1262.53	885.50	0.26	0.09
142	714.29	3	SLE F	-32306.90	32096.30	~2566.43	46.00	136.36	0.50	20.00	205.89	21.99	1252.31	779.27	0.23	0.08
143	773.81	3	SLE F	-31565.30	28973.00	-2316.68	46.00	136.36	0.50	20.00	204.72	21,99	1239.40	673.05	0.20	0.07
144	833,33	3	SLE F	-30825.40	25897.40	-2070.76	46.00	136,36	0.50	20.00	203.23	21,99	1223.06	569.25	0.17	0.06
145	892,86	3	SLE F	-30087,20	22917.70	-1832,50	46.00	136.36	0.50	20.00	201.32	21,99	1202.06	469.93	0,14	0.05
146	952.38	3	SLE F	-29350.60	20071.90	-1604.95	46.00	136.36	0.50	20.00	198.82	21.99	1174.58	376.82	0.11	0.04
147	1011.90	3	SLE F	-28615.50	17388.80	-1390.41	46.00	136.36	0.50	20.00	195.48	21.99	1137.87	291.47	0.08	0.03
148	1071.43	3	SLE F	-27882.00	14889,20	-1190.55	46.00	136.36	0.50	20,00	190.92	21,99	1087.68	215.35	0.06	0.02
149	1130.95	3	SLE F	-27149.90	12587.00	-1006.46	46.00	136.36	0.50	20.00	199.94	18.85	1017.31	149.93	0.04	0.01
150	1190,48	3	SLE F	-26419.40	10490,20	-838.80	46.00	136.36	0.50	20.00	208.50	15.71	915.00	96.65	0.03	0.01
151	1250.00	3	SLE F	-25690.20	8601.68	-687.79	46.00	136,36	0.50	20.00	188.28	15.71	756.19	56.45	0.02	0.01
152	1309.52	3	SLE F	-24962.40	6920.25	-553.34	46.00	136,36	0.50	20.00	198.13	9.42	500.15	28.83	0.01	0.00
153	1369.05	3	SLE F	-24236.00	5441.27	-435.08	46.00	136,36	0.50	20.00	169.67	5.28	244.00	11.39	0.00	0.00

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
69	C.Rare - Sc max (min. compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
112	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Palo n. 33

Caratteristiche del palo e dei materiali utilizzati

R <cm>></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
60.00	6.00	C30/37	307,10	20.59	174.02	13.73	B450C	4300.00	3913.04

Le sollecitazioni nei pali vengono calcolate oltre che per l'effetto delle reazioni vincolari anche considerando i seguenti effetti

Azioni ed effetti comuni

Az	N <dan></dan>	Mx <danm></danm>	My <danm></danm>	Mz <danm></danm>
PP	0.00	0.00	0.00	
SVR	0.00			

Azioni ed effetti - Plinto/Palo n. 33 (-8)

Caso	œ	TCC	Az	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	RVN	22207.30	7608.59	392.10	56863.60	1420.21
	1	SLU	TAG				0.00	0.00
	1	SIJ	ECC			3	0.00	0.00
	1	SLU	TOT	22207.30	7608.59	392.10	56863.60	1420.21
2	2	SLE R	RVN	16449.90	5636.00	290.44	42121.10	1052.01
	2	SLE R	TAG				0.00	0.00
	.2	SLE R	ECC				0.00	0.00
	2	SLE R	TOT	16449.90	5636.00	290.44	42121.10	1052,01
3	3	SLE F	RVN	16449.90	5636.00	290.44	42121.10	1052.01
	3	SLE F	TAG			3 3	0.00	0.00
	3	SLE F	ECC				0.00	0.00
	3	SLE P	TOT	16449.90	5636.00	290.44	42121.10	1052.01
4	. 4	SLE Q	RVN	16449.90	5636.00	290.44	42121.10	1052.01
	4	SLE Q	TAG				0.00	0.00
	4	SLE Q	ECC				0.00	0.00
	4	SLE Q	TOT	16449,90	5636.00	290.44	42121.10	1052.01

Sollecitazioni nei pali

Caso	00	TCC	Palo	N <dan></dan>	Tx <dan></dan>	Ty <dan></dan>	Mx <danm></danm>	My <danm></danm>
1	1	SLU	. 1	-22207.30	-7608.59	-392.10	-56863.60	-1420.21
2	. 2	SLE R	1	-16449.90	-5636.00	-290.44	-42121.10	-1052.01
- 3	3	SLE F	1	-16449.90	-5636.00	-290.44	-42121.10	-1052.01
4	4	SLE Q	- 1	-16449.90	-5636.00	-290.44	-42121.10	-1052.01

142

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
-1	0.00	1	SLU	-22207.30	56614.80	-1414.00	-22207.30	156076.00	-3387.27	2-3	181,25	2.757
2	59.52	1	SLU	-23261.10	60402.80	-1508.61	-23261,10	156519,00	-3415.44	2-3	181.25	2,591
3	119.05	1	SIU	-23686.30	62835.70	-1569.37	-23686,30	156698.00	-3426.84	2-3	181.25	2.494
4	178.57	1	SLU	-24112.30	64107.10	-1601.13	-24112.30	156878.00	-3438.27	2-3	181.25	2.447
.5	238.09	1	SLU	-24539,10	64395.80	-1608.34	-24539,10	157057.00	-3449,73	2-3	181.25	2.439
- 6	297.62	1	SLU	-24966.60	63865.90	-1595.10	-24966.60	157237.00	-3461.23	2-3	181.25	2,462
7	357.14	1	SLU	-25394,90	62603.00	-1563.56	-25394.90	157417.00	-3472,77	2-3	181.25	2,514
8	416.67	1	SLU	-24932.00	60502.40	-1511.10	-24932.00	157222.00	-3460.30	2-3	181.25	2.598
9	476.19	1	SLU	-24470.40	57689.70	-1440.85	-24470.40	157028.00	-3447.89	2-3	181,25	2.722
10	535.71	1	SIJ	-24010.20	54345.40	-1357.32	-24010.20	156835.00	-3435.53	2-3	181.25	2,886
-11	595.24	1	SLU	-23551.30	50627.10	-1264.45	-23551.30	156641.00	-3423.22	2-3	181.25	3.094
12	654.76	1	SLU	-23093.60	46670.60	-1165.64	-23093.60	156449.00	-3410.96	2-3	181.25	3.352
13	714.29	1	SLU	-22637.10	42591.90	-1063.77	-22637.10	156257.00	-3398.75	2-3	181.25	3,668
14	773.81	1	SIU	-22181.90	38488,10	-961.27	-22181.90	156065.00	-3386.59	2-3	181.25	4.055
15	833.33	2	SIJI	-21727.80	34439.30	-860.15	-21727.80	155874.00	-3374.47	2-3	181.25	4.526
16	892.86	1	SLU	+21275.00	30510.60	-762.03	-21275.00	155683.00	-3362.41	2-3	181.25	5,102
17	952.38	1	SLU	-20823.20	26753.10	-668.18	-20823.20	155493.00	-3350.3B	2-3	181.25	5,812
1.8	1011.90	1	SIU	-20372.60	23205.80	-579.58	-20372.60	155303.00	-3338.41	2-3	181.25	6,692
19	1071.43	1	SIU	-19923.10	19897.10	-496.95	-19923.10	155114.00	-3326.48	2-3	181.25	7.795
20	1130.95	1	SLU	-19474,60	16846.30	-420,75	-19474.60	154925,00	-3314.60	2-3	181.25	9,196
21	1190.48	1	SIU	-19027.20	14064.40	-351.27	-19027.20	154737.00	-3302.76	2-3	181.25	11.001
22	1250.00	1	SIU	-18580.80	11556.10	-288.62	-18580.80	154549.00	-3290.97	2-3	181.25	13.373
-23	1309.52	1	SIU	-18135.40	9320.29	-232.78	-18135.40	154361.00	-3279.16	2-3	181.25	16.560
24	1369.05	1	SLU	-17691.00	7351.28	-183.60	-17691.00	154173.00	-3267.17	2-3	181.25	20.971
25	1428,57	1	SLU	-17247,50	5639.69	-140.86	-17247,50	153986.00	-3254.83	2-3	181.25	27.302
26	1488.10	1	SIU	-16805,00	4173.23	-104.23	-16805.00	153799.00	-3242.52	2-3	181.25	36,850
27	1547.62	1	SLU	-16363.30	2937.36	-73.36	-16363.30	153612.00	-3230.26	2-3	181.25	52,291
-28	1607.14	1	SLU	-15922.60	1915.87	-47.85	-15922.60	153425.00	-3218.05	2-3	181.25	80.074
29	1666.67	1	SIJ	-15482.60	1091.41	-27.26	-15482.60	153239.00	-3205.86	2-3	181.25	>100
30	1726.19	1	SLU	-15043.60	445.84	-11.14	-2571250.00	153053.00	-3193.72	2-3	181.25	>100
31	1785,71	1	SLU	-14605.30	-39.39	0.98	-2571250.00	-152975.00	3603.97	2-3	1,25	>100
32	1845.24	1	SIJ	-14167.80	-383.01	9,57	-2571250.00	-152790.00	3614.24	2-3	1.25	>100
33	1904.76	1	SLU	-13731.00	-603.71	15.08	-2571250.00	-152605.00	3624.45	2-3	1.25	>100
34	1964.29	1	SEU	-13295.00	-720.06	17.98	-2571250.00	-152421.00	3634.63	2-3	1.25	>100
35	2023.81	1	SIU	-12859.80	-750.36	18.74	-2571250.00	-152237.00	3644.77	2-3	1.25	>100
36	2083.33	1	SIJ	-12425.20	-712,62	17.80	-2571250.00	-152053.00	3654.86	2-3	1.25	>100
37	2142.86	1	SLU	-11991.20	-624.55	15.60	-2571250.00	-151869.00	3664.90	2-3	1.25	>100
38	2202.38	1	SLU	-11557.90	-503.58	12.58	-2571250.00	-151686.00	3674.91	2-3	1.25	>100
39	2261.90	1	SIJ	-11125.30	-366.87	9.16	-2571250.00	-151503.00	3684.88	2-3	1.25	>100
40	2321.43	1	SIM	-10693.20	-231.39	5.78	-2571250.00	-151320.00	3694.80	2-3	1.25	>100
41	2380.95	1	SLU	-10261.70	-113.95	2.85	-2571250.00	-151138.00	3704.69	2-3	1.25	>100
42	2440.48	1	SLU	-9830,76	-31.26	0.78	-2571250.00	-150955.00	3714.54	2-3	1.25	>100
43	2500.00	1	SLU	-9400.35	0.00	0.00	-2571250.00					>100

Caso	X <cm></cm>	œ	TCC	Ty <dan></dan>	Tz <dan></dan>	bw <m></m>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	1	SLU	7608.59	392.10	0.85	11.31	7618.69	1.00	32294.70	334849.00	32294.70	4,239
2	59.52	1	SLU	5164.12	266.13	0.85	11.31	5170.97	1.00	32294.70	335000.00	32294.70	6.245
3	119,05	1	SIJ	3056.38	157.51	0.85	11.31	3060.44	1.00	32294.70	335061,00	32294.70	10.552
4	178,57	1	SIU	1261.23	65.00	0.85	11.31	1262.90	1.00	32294.70	335122.00	32294.70	25.572
- 5	238.09	1	SLU	-246.18	-12.69	0.85	11,31	246.51	1.00	32294.70	335183.00	32294.70	>100
6	297.62	1	SIU	-1491,00	-76.84	0.85	11.31	1492.98	1.00	32294.70	335244.00	32294.70	21,631
7	357.14	1	SLU	-2816.74	-145.16	0.85	11.31	2820.48	1.00	32294.70	335306.00	32294.70	11.450
- 8	416.67	1	SLU	-4176.79	-215.25	0.85	11.31	4182.33	1.00	32294.70	335239.00	32294.70	7.722
9	476,19	1	SIJ	-5213.88	-268.69	0.85	11.31	5220.80	1.00	32294.70	335173.00	32294.70	6.186
10	535.71	1	SLU	-5967.58	-307.53	0.85	11.31	5975.50	1,00	32294.70	335107.00	32294.70	5.405
11	595.24	1	SLU	-6475,38	-333.70	0.85	11.31	6483.97	1.00	32294.70	335042.00	32294.70	4.983
12	654.76	1	SIU	-6772,39	-349.01	0.85	11.31	6781.37	1.00	32294.70	334976.00	32294.70	4.762
13	714.29	1	SLU	-6891.13	-355.13	0.85	11.31	6900.28	1.00	32294.70	334911.00	32294.70	4.680
14	773.81	1	SIU	-6861.46	-353.60	0.85	11.31	6870.56	1.00	32294.70	334845.00	32294.70	4.700
15	833.33	1	SIU	-6710.45	-345.82	0.85	11.31	6719.35	1.00	32294.70	334780.00	32294.70	4.806
16	892.86	1	SLU	-6462.46	-333.04	0.85	11.31	6471.04	1.00	32294.70	334716.00	32294.70	4,991
17	952.38	1	SLU	-6139.19	-316.38	0.85	11.31	6147.34	1.00	32294.70	334651.00	32294.70	5.253
18	1011.90	1	SLU	-5759.74	-296.82	0.85	11.31	5767.38	1.00	32294.70	334586.00	32294.70	5.600
19	1071.43	1	SIL	-5340.77	-275.23	0.85	11.31	5347.86	1.00	32294.70	334522.00	32294.70	6.039
20	1130.95	1	SLU	-4896.66	-252.34	0.85	11.31	4903.16	1,00	32294.70	33445B.00	32294.70	6.587
21	1190.48	1	SLU	-4439.65	-228.79	0.85	11.31	4445.54	1.00	32294.70	334394.00	32294.70	7.265
22	1250.00	1	SLU	-3980.04	-205.11	0.85	11.31	3985.32	1.00	32294.70	334330.00	32294.70	8.103
23	1309.52	1	SLU	-3526.34	-181.73	0.85	11.31	3531.02	1.00	32294.70	334266.00	32294.70	9.140
24	1369.05	1	SIJ	-3085.51	-159.01	0.85	11.31	3089.60	1.00	32294.70	334202.00	32294.70	10.453
25	1428.57	3	SIU	-2663.07	-137.24	0.85	11.31	2666.60	1.00	32294.70	334139.00	32294.70	12.111

26	1488.10	1	SIU	-2263.33	-116.64	0.85	11.31	2266.34	1.00	32294.70	334075.00	32294.70	14.250
27	1547.62	1	SIJ	-1889.54	-97.38	0.85	11.31	1892.05	1.00	32294.70	334012.00	32294.70	17.069
28	1607.14	1	SIU	-1544.05	-79.57	0.85	11.31	1546.10	1.00	32294.70	333949.00	32294.70	20.888
-29	1666.67	1	SIU	-1228.43	-63.31	0.85	11.31	1230.07	1.00	32294.70	333886.00	32294.70	26.255
30	1726.19	1	SLU	-943.68	-48.63	0.85	11.31	944.93	1.00	32294.70	333823.00	32294.70	34.177
31	1785.71	1	SLU	-690.28	-35.57	0.85	11.31	691.19	1.00	32294.70	333760.00	32294.70	46.723
32	1845,24	1	SLU	-468.33	-24.14	0.85	11.31	468.95	1.00	32294.70	333697.00	32294.70	68.865
33	1904.76	ĭ	SIU	-277.68	-14.31	0.85	11.31	278.05	1.00	32294.70	333635.00	32294.70	>100
34	1964.29	1	SLU	-117.98	-6.08	0.85	11.31	118.14	1.00	32294.70	333572.00	32294.70	>100
35	2023.81	1	SIJ	11.24	0.58	0.85	11.31	11.26	1,00	32294.70	333510.00	32294.70	>100
36	2083.33	1	SLU	110.48	5.69	0.85	11.31	110.63	1,00	32294.70	333448.00	32294.70	>100
37	2142,86	1	SLU	180.25	9.29	0.85	11.31	180.49	1.00	32294.70	333386.00	32294.70	>100
38	2202.38	1	SIAJ	221.00	11.39	0.85	11.31	221.30	1.00	32294.70	333324.00	32294.70	>100
39	2261.90	1	SLU	233.13	12.01	0.85	11.31	233.44	1.00	32294.70	333262,00	32294.70	>100
40	2321.43	1	SIU	216.93	11.18	0.85	11.31	217.22	1.00	32294.70	333200.00	32294.70	>100
41	2380.95	1	SIJ	172.60	8.89	0.85	11.31	172.83	1.00	32294.70	333138.00	32294.70	>100
42	2440,48	1	SIJ	100.28	5.17	0.85	11.31	100.41	1.00	32294.70	333076,00	32294.70	>100

Caso	X <cm>></cm>	œ		e d'eserc: N <dan></dan>	Mz <danm></danm>	My <danm></danm>	AfT <cmq></cmq>	AfC <mq></mq>	σ _c <dan cmq=""></dan>	σ _f <dan cmq=""></dan>
:44	0.00	2	SLE R	-16449.90	-1047.41	41936.90	50.27	28.27	42,31	1359.62
45	59.52	2	SLE R	-17543.60	-1117.49	44742.80	50.27	28.27	45,15	1450.68
46	119.05	2	SLE R	-18048.70	-1162.50	46545.00	50.27	28.27	46.97	1511.94
4.7	178.57	2	SLE R	-18554.40	-1186.02	47486.80	50.27	28.27	47.92	1540.56
48	238.09	2	SLE R	-19060.70	-1191.36	47700.60	50.27	28.27	48.12	1541.58
4.9	297.62	2	SLE R	-19567.50	-1181.56	47308.10	50.27	28.27	47,71	1519.55
50	357.14	2	SLE R	-20075.00	-1158.19	46372.60	50.27	28.27	46.74	1477.05
51	416.67	2	SLE R	-19747.30	-1119.33	44816.60	50.27	28.27	45,16	1422.66
52	476.19	2	SLE R	-19420.70	-1067.30	42733.10	50.27	28.27	43.04	1348.28
53	535,71	2	SLE R	-19095.10	-1005.42	40255.90	50.27	28.27	40.52	1258.99
54	595.24	2	SLE R	-18770.50	-936,63	37501.50	50.27	28,27	37.72	1159.22
55	654.76	2	SLE R	-18447.00	-863.44	34570.90	50.27	28.27	34.73	1052.83
56	714.29	2	SLE R	-18124.40	-787.98	31549.60	50.27	28.27	31.65	943.0
57	773.81	- 2	SLE R	-17802.80	-712.05	28509.70	47.12	31.42	28.54	832.74
58	833.33	2	SLE R	-17482.20	-637.15	25510.60	47.12	31.42	25.47	724.05
59	892.86	2	SLE R	-17162.50	-564.47	22600.40	47.12	31.42	22,49	619.0
60	952,38	2	SLE R	-16843.70	-494.95	19817,10	47.12	31.42	19.62	519.00
61	1011.90	2	SLE R	-16525.80	-429.32	17189.50	47.12	31.42	16.91	425.2
62	1071.43	2	SLE R	-16208.80	-368.11	14738.60	47.12	31.42	14.37	338.7
63	1130,95	2	SLE R	-15892.70	-311.67	12478.70	47.12	31.42	12.02	260.36
64	1190.48	2	SLE R	-15577.50	-260.20	10418.10	43.98	34.56	9.86	190.5
65	1250.00	2	SLE R	-15263.00	-213.79	8560.09	40.84	37.70	7.91	130,4
66	1309.52	2	SLE R	-14949.40	-172.43	6903.92	40.84	37.70	6.19	83.9
67	1369.05	2	SLE R	-14636.60	-136.00	5445.39	34.56	43.98	4.73	65.0
68	1428.57	2	SLE R	-14324.60	-104.34	4177.55	28.27	50.27	3,59	50.1
69	1488.10	2	SLE R	-14013.30	-77.21	3091.28	18.85	59.69	2,79	39.3
70	1547.62	2	SLE R	-13702.80	-54.34	2175.82	0.00	78.54	2.24	31.9
71	1607,14	2	SLE R	-13393.00	-35,44	1419.16	0.00	78.54	1.82	26.29
72	1666.67	2	SLE R	-13084.00	-20.19	808.45	0.00	78.54	1,48	21.6
73	1726.19	2	SLE R	-12775.60	-8,25	330.25	0.00	78.54	1.21	17.8
74	1785.71	2	SLE R	-12468.00	0.73	-29.18	0.00	78.54	1.03	15.4
75	1845.24	2	SLE R	-12161.00	7.09	-283.71	0.00	78.54	1,14	16.83
7.6	1904.76	2	SLE R	-11854.60	11.17	-447.19	0.00	78.54	1.20	17.60
77	1964.29	2	SLE R	-11548.90	13.32	-533.38	0.00	78.54	1,21	17.8
78	2023.81	2	SLE R	-11243.80	13.88	-555.82	0.00	78.54	1.20	17.6
79	2083.33	2	SLE B	-10939.30	13.18	-527.87	0.00	78.54	1,16	17.03
80	2142.86	2	SLE R	-10635.40	11.55	-462,63	0.00	78.54	1.10	16.23
81	2202.38	2	SLE R	-10332.10	9.32	-373.02	0.00	78.54	1.03	15.23
82	2261,90	2	SLE R	-10029.30	6.79	-271.76	0.00	78.54	0.96	14.1
83	2321.43	2	SLE R	-9727.10	4.28	-171.40	0.00	78.54	0.88	13.0
84	2380.95	2	SLE B	-9425.39	2.11	-84,41	0.00	78.54	0.81	12.0
8.5	2440.48	2	SLE R	-9124.17						
86	2500.00	2	SLE R	-8823.46	0.00	0.00	0.00	78.54	0.72	10.7
87	0.00	4	SLE Q	-16449.90	-1047.41	41936.90	50.27	28.27	42.31	1359.63
88	59.52			-17543.60						
89	119.05	4	SLE Q	-18048.70	-1162.50	46545.00	50.27	28.27	46,97	1511.9
90	178.57	4	SLE Q	-18554.40	-1186.02	47486.80	50,27	28.27	47.92	1540.5
91	238.09	4	SLE Q	-19060.70	-1191.36	47700.60	50.27	28.27	48.12	
92				-19567.50						
.93				-20075.00					46.74	
94				-19747.30					45.16	1422.6
95				-19420.70						
96		_	_	-19095.10						
97		_	_	-18770.50						
98		_		-18447.00						-
-	and the same of the same of	_	_	-18124.40	A STATE OF THE PARTY OF THE PAR			-		

								MALO	ic di can	3010
100	773.81	4	SLE Q	-17802.80	-712.05	28509.70	47.12	31.42	28.54	832.74
101	833.33	4	SLE Q	-17482.20	-637.15	25510.60	47.12	31.42	25.47	724.09
102	892.86	4	SLE Q	-17162.50	+564.47	22600.40	47.12	31.42	22.49	619.01
103	952.38	4	SLE Q	-16843.70	-494.95	19817.10	47.12	31.42	19.62	519.00
104	1011.90	4	SLE Q		-429.32	17189.50	47.12	31.42	16.91	425.27
105	1071.43	4	SLE Q	-16208.80	-368.11	14738.60	47.12	31.42	14.37	338.77
106	1130.95	4	SLE Q		-311.67	12478.70	47.12	31.42	12.02	260.30
107	1190.48	4	SLE Q	-15577.50	-260.20	10418.10	43.98	34.56	9.86	190.58
108	1250.00	4	SLE Q	-15263.00	-213.79	8560.09	40.84	37.70	7.91	130.46
109	1309.52	4	SLE Q	-14949.40	-172.43	6903.92	40.84	37.70	6,19	83.97
110	1369.05	4	SLE Q	-14636.60	-136.00	5445.39	34.56	43.98	4.73	65.09
111	1428.57	4	SLE Q	-14324.60	-104.34	4177.55	28.27	50.27	3.59	50.14
112	1488,10	4	SLE Q	-14013.30	-77.21	3091.28	18.85	59.69	2.79	39.38
113	1547.62	4	SLE Q	-13702.80	-54.34	2175.82	0.00	78.54	2.24	31.97
114	1607.14	4	SLE Q	-13393.00	-35.44	1419.16	0.00	78.54	1.82	26.28
115	1666.67	4	SLE Q	-13084.00	-20.19	808.45	0.00	78.54	1.48	21.62
116	1726.19	-4	SLE Q	-12775.60	-8,25	330.25	0.00	78.54	1.21	17.89
117	1785.71	4	SLE Q	-12468.00	0.73	-29.18	0.00	78.54	1.03	15.41
118	1845.24	4	SLE Q	-12161.00	7.09	-283.71	0.00	78.54	1.14	16.82
119	1904.76	4	SLE Q	-11854,60	11.17	-447.19	0.00	78.54	1.20	17.60
120	1964.29	4	SLE Q	-11548.90	13.32	-533.38	0.00	78.54	1,21	17.83
121	2023.81	4	SLE Q	-11243.80	13.88	-555.82	0.00	78.54	1.20	17.62
122	2083.33	4	SLE Q	-10939.30	13.18	-527.87	0.00	7B.54	1.16	17.05
123	2142.86	4	SLE Q	-10635.40	11.55	-462.63	0.00	78.54	1.10	16.22
124	2202,38	4	SLE Q	-10332,10	9.32	-373.02	0.00	78,54	1.03	15.22
125	2261.90	4	SLE Q	-10029.30	6.79	-271.76	0.00	78.54	0.96	14.14
126	2321.43	4	SLE Q	-9727.10	4,28	-171.40	0.00	78.54	0.88	13.07
127	2380.95	4	SLE Q	-9425.39	2.11	-84.41	0.00	78.54	0.81	12.09
128	2440.48	4	SLE Q	-9124.17	0.58	-23.16	0.00	78.54	0.75	11,29
129	2500.00	4	SLE Q	-8823.46	0.00	0.00	0.00	78.54	0.72	10.76

Stato limite d'esercizio - Verifiche a fessurazione

Caso	X <cm>></cm>	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	c <mm></mm>	s <mm></mm>	K 2	Φeq	Δ _{sm} <mm></mm>	A _B <cmq></cmq>	Ac eff <cmq></cmq>	σ _{ii} <dan cmq=""></dan>	€ stm	Wk <mm></mm>
87	0.00	4	SLE Q	-16449.90	41936.90	-1047,41	46.00	136.36	0.50	20.00	213.20	21.99	1332.71	1359.62	0.40	0.14
88	59.52	4	SLE Q	-17543.60	44742.80	-1117.49	46.00	136.36	0.50	20.00	213.21	21,99	1332.72	1450.68	0.42	0.15
89	119.05	4	SLE Q	-18048.70	46545.00	-1162.50	46.00	136.36	0.50	20.00	213.25	21.99	1333.25	1511.94	0.44	0.16
90	178.57	4	SLE Q	-18554.40	47486.80	-1186.02	46.00	136.36	0.50	20,00	213,22	21,99	1332.89	1540.56	0.45	0.16
91	238.09	4	SLE Q	-19060.70	47700.60	-1191.36	46.00	136.36	0.50	20.00	213.12	21.99	1331.82	1541.58	0.45	0.16
92	297.62	4	SLE Q	-19567.50	47308.10	-1181.56	46.00	136.36	0.50	20.00	212.97	21.99	1330.11	1519.59	0.44	0.16
93	357,14	4	SLE Q	-20075.00	46372.60	-1158.19	46.00	136.36	0.50	20.00	212.75	21,99	1327.75	1477.05	0.43	0.16
94	416.67	4	SLE Q	-19747.30	44816.60	-1119.33	46.00	136.36	0.50	20.00	212.67	21.99	1326.80	1422.66	0.41	0.15
95	476.19	4	SLE Q	-19420.70	42733.10	-1067.30	46.00	136.36	0.50	20.00	212.51	21.99	1325.08	1348.28	0.39	0.14
96	535,71	19	SLE Q	-19095.10	40255.90	-1005.42	46.00	136.36	0.50	20.00	212.28	21.99	1322,60	1258.99	0.37	0.13
97	595.24	4	SLE Q	-18770.50	37501.50	-936.63	46.00	136.36	0.50	20.00	211.99	21.99	1319.30	1159.22	0.34	0.12
98	654.76	4	SLE Q	-18447.00	34570.90	-863.44	46.00	136,36	0.50	20,00	211.60	21,99	1315.09	1052.83	0.31	0.11
99	714.29	4	SLE Q	-18124.40	31549.60	-787.98	46.00	136.36	0.50	20,00	211.12	21,99	1309.79	943.09	0.27	0.10
100	773.81	4	SLE Q	-17802.80	28509.70	-712.05	46.00	136.36	0.50	20.00	210.52	21.99	1303.18	832.74	0.24	0.09
101	833,33	4	SLE Q	-17482.20	25510.60	-637.15	46.00	136,36	0.50	20.00	209.77	21,99	1294.93	724.09	0.21	0.08
102	892.86	4	SLE Q	-17162.50	22600.40	-564.47	46.00	136.36	0.50	20.00	208.83	21.99	1284.57	619.01	0.18	0.06
103	952.38	4	SLE Q	-16843.70	19817,10	-494.95	46.00	136.36	0.50	20,00	207.63	21,99	1271.43	519.00	0.15	0.05
104	1011.90	4	SLE Q	-16525.80	17189.50	-429.32	46.00	136.36	0.50	20.00	206.09	21.99	1254.49	425.27	0.12	0.04
105	1071.43	4	SLE Q	-16208.80	14738.60	-368.11	46.00	136.36	0.50	20.00	204.07	21.99	1232.30	338.77	0.10	0.03
106	1130.95	4	SLE Q	-15892.70			46.00	136.36	0.50	20.00	201.36	21.99	1202.51	260,30	0.08	0.03
107	1190.48	4	SLE Q	-15577.50	10418.10	-260.20	46.00	136.36	0.50	20.00	197.61	21.99	1161.24	190,58	0.06	0.02
108	1250.00	4	SLE Q	-15263.00	8560.09	-213.79	46.00	136.36	0.50	20.00	192.16	21.99	1101.37	130.46	0.04	0.01
109	1309.52	4	SLE Q	-14949.40	6903.92	-172,43	46.00	136.36	0.50	20.00	198.91	18.85	1007.58	81,11	0.02	0.01
110	1369.05	4	SLE Q	-14636.60	5445.39	-136.00	46.00	136.36	0.50	20.00	200.73	15.71	853.99	43.99	0.01	0.00
111	1428.57	4	SLE O	-14324.60	4177.55		_	-	_	20.00	180.59		556.63	19.64	0.01	0.00
112	1488.10	4	SLE O	-14013.30	3091.28		_	136.36	_	20.00	230.07	3,14	216.88	5,90	0.00	0.00
130	0.00	3	SLE F	-16449.90	41936.90		46.00	-	0.50	20,00	213.20	21.99	1332.71	1359,62	0.40	1
131	59.52	3	SLE F	-17543.60			_		_	20.00	213.21	21,99	1332.72	1450.68	0.42	_
132	119.05	3	SLE F				_	136,36	0.50	20,00	213.25	21.99	1333.25	1511.94	0.44	_
133	178.57	3	SLE F	-18554.40			46.00	-	_	20.00	213.22	21,99	1332.89	1540.56	0.45	-
134	238.09	3	SLE F	-19060.70		-	-		-	20.00	213.12	21,99	1331.82	1541.58	0.45	0.16
135	297.62	3	SLE P				46.00		0.50	20.00	212.97	21,99	1330.11	1519.59	0.44	0.16
136	357.14	3	SLE F	-	46372.60	-			_	20,00	212,75	21.99	1327.75	1477.05	0.43	+
137	416.67	3	SLE F	-19747.30	44816.60		46.00	_	0.50	20.00	212.67	21,99	1326.80	1422.66	0.41	0.15
138	476.19	3	SLE F	-	_		-	-	_	_	212,51	21,99	1325.08	1348.28	0.39	_
139	535.71	3	SLE F				_	136.36	_	-	212.28		1322.60	1258.99		0.13
140	595.24	3	SLE F				_	_	0.50	_	_		1319.30	1159.22		-
141	654.76	3	SLE F	-18447.00	34570.90		-	_	_	20,00	211.60	21,99	1315.09	1052.83	0.31	0.11
142	714.29	-	-	-	-	_	_	_	_	-		21.99	1309.79	943.09	_	0.10
143	773.81	3	SLE F	-17802.80	28509.70		46.00			20.00	210.52	21.99	1303.18	832.74	0.24	_
144	833.33	3	SLE F	_	25510.60		_		-	20.00	209.77	21,99	1294.93	724.09	0.21	_
145	892.86	3	SLE F	-17162.50	22600.40		46.00	-		20,00	208.83	21,99	1284.57	619.01	0.18	-
146	952.38	3	SLE F				-		_		207.63	21.99	1271.43	519.00	0.15	-

147	1011.90	3	SLE	P	-16525.80	17189.50	-429.32	46.00	136.36	0.50	20.00	206.09	21,99	1254.49	425.27	0.12	0.04
148	1071.43	3	SLE	F	-16208.80	14738.60	-368.11	46.00	136.36	0.50	20.00	204.07	21.99	1232.30	338.77	0.10	0.03
149	1130.95	3	SLE	F	-15892.70	12478.70	-311.67	46.00	136.36	0.50	20.00	201.36	21.99	1202.51	260.30	0.08	0.03
150	1190.48	3	SLE	F	-15577.50	10418.10	-260.20	46.00	136.36	0.50	20,00	197.61	21,99	1161.24	190.58	0.06	0.02
151	1250.00	177	SLE	F	-15263.00	8560.09	-213.79	46.00	136.36	0.50	20.00	192.16	21,99	1101.37	130.46	0.04	0.01
152	1309.52	3	SLE	1	-14949.40	6903.92	-172.43	46.00	136.36	0.50	20.00	198.91	18.85	1007.58	81.11	0.02	0.01
153	1369.05	3	SLE	P	-14636.60	5445.39	-136,00	46.00	136.36	0.50	20.00	200.73	15.71	853.99	43.99	0.01	0.00
154	1428.57	173	SLE	112	-14324.60	4177.55	-104.34	46.00	136,36	0.50	20.00	180.59	12.57	556.63	19.64	0.01	0.00
155	1488.10	3	SLE	F	-14013.30	3091.28	-77.21	46.00	136.36	0.50	20.00	230.07	3.14	216.88	5,90	0.00	0.00

Verifiche principali

Caso	Tipo
1	SLU Taglio - min. sic. c.a., SLU Taglio - min. sic. acciaio
5	SLU N cost - min. sic.
48	C.Rare - Sc min (max compr.), C.Rare - Sf max (max traz.), C.Rare - Sf min (max compr.)
71	C.Rare - Sc max (min. compr.)
91	C.Q.Per Sc min (max compr.), C.Q.Per Sf max (max traz.), C.Q.Per Sf min (max compr.), C.Q.Per Wk Max
114	C.Q.Per Sc max (min. compr.)
134	C.Freq - Wk Max

Verifiche sezioni aste

```
Simbologia
Δ<sub>SM</sub> = Distanza media tra le fessure
Φ<sub>eG</sub> = Diametro equivalente delle barre
α = Angolo asse neutro a rottura
\epsilon_{\mathrm{SM}} = Deformazione unitaria media dell'armatura (*1000)
σ<sub>B</sub> = Tensione nell'acciaio nella sezione fessurata
Ac eff = Area di calcestruzzo efficace
As = Area complessiva dei ferri nell'area di calcestruzzo efficace
Asw = Area armatura trasversale
B = Base
CC = Numero della combinazione delle condizioni di carico elementari
Caso = Caso di verifica
Cf = Copriferro
Cls = Tipo di calcestruzzo
Fcd = Resistenza di calcolo a compressione del calcestruzzo
Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo
Fctd = Resistenza di calcolo a trazione del calcestruzzo
Fctk = Resistenza caratteristica a trazione del calcestruzzo
Fyd = Resistenza di calcolo dell'acciaio
Fyk = Tensione caratteristica di snervamento dell'acciaio
H = Altezza
K2 = Coefficiente per distribuzione deformazioni
M'ydy = Momento resistente massimo in campo sostanzialmente elastico intorno all'asse Y
M'ydz = Momento resistente massimo in campo sostanzialmente elastico intorno all'asse Z
MRdy = Momento resistente allo stato limite ultimo intorno all'asse Y
MRdz = Momento resistente allo stato limite ultimo intorno all'asse Z
My = Momento flettente intorno all'asse Y
Mz = Momento flettente intorno all'asse Z
N = Sforzo normale
Nu = Sforzo normale ultimo
Rott. - Tipo di rottura
1-2 = Rott. acciaio: ey=eyd, ec<ecu
2-3 = Rott. cls: εγ<εγd, ε<sub>C</sub>=ε<sub>Cu</sub>
3-4 = Rott. cls: &co<&c<&cu
Sez. - Numero della sezione
Sic. = Sicurezza
TCC = Tipo di combinazione di carico
SIN = State limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
Tipo = Tipo di verifica effettuata
```

SEZIONE N.10

Tp = Tipo di acciaio Ty = Taglio in dir. Y Tz = Taglio in dir. Z

VRcd = Taglio ultimo lato calcestruzzo VRsd = Taglio ultimo lato armatura Vrdu = Taglio ultimo resistente

c = Ricoprimento dell'armatura

s - Distanza massima tra le barre

Wk = Ampiezza caratteristica delle fessure bw = Larghezza membratura resistente al taglio

Sezione: Rettangolare - Dati geometrici della sezione

Vsdu = Taglio agente nella direzione del momento ultimo

ctg0 = Cotangente dell'angolo di inclinazione dei puntoni di calcestruzzo

Base <m></m>	=	2,58
Altezza <m></m>	=	2.60

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Tipo	B <cm>></cm>	H <cm>></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq2<="" th=""></dan>
10	R:	258.00	260,00	3.00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.07

Stato limite ultimo - Verifiche a flessione/pressoflessione

Scaco	-	THE C	M HT-	ano - Aeriti	LCINE &	TTGSST	Otie/ bressor	T69970	. Die		
Caso	oc	TCC	N <dan></dan>	My <dann></dann>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
-1		SLV	0.00	1152480.00	0.00	0.00	1179210.00	19.52	1-2	179.79	1.023

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	(III)	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	0.00	2.58	40.21	0.00	2.50	913262.00	2428570.00	913262.00	

Verifiche principali

Caso	000	223	Ti	po	
- 1	SLU	N	cost.	- min.	sic.

SEZIONE N.2

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	=	1,20
Altezza <m></m>	=	1.50

Caratteristiche delle sezioni e dei materiali utilizzati

Sez. Tipo	B <cm></cm>	H <cm>></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan emg=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
2 R	120.00	150.00	3.00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.0

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1		SLU	0.00	118798.00	0.00	0.00	176901.00	0.00	1-2	180,00	1,489

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	om>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctge	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	0.00	1.20	40.21	0.00	2.50	520445.00	643708.00	520445.00	

Verifiche principali

Caso		Tipo							
1	SLU	N	cost -	min.	sic.				

SEZIONE N.3

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	-	2.58
Altezza <m></m>	-	1.50

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Tipo	B <cm>></cm>	H <cm>></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
3	B	258.00	150,00	3.00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.04

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	oc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1		SLU	0.00	777000.00	0.00	0.00	822417.00	-4.17	1-2	179.75	1.058

Stato limite ultimo - Verifiche a taglio

					Vsdu <dan></dan>			VRcd <dan></dan>	Vrdu <dan></dan>	Sic
- 1	0.00	0.00	2.58	20.11	0.00	2.50	262187.00	1394430.00	262187.00	

Verifiche principali

Caso			Tip	90	
1	SLU	N	cost -	min.	sic.

SEZIONE N. 4

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	=	1,20
Altezza <m></m>	=	1.50

Caratteristiche delle sezioni e dei materiali utilizzati

Sez. Tip	o B	H <cm></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fcd <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
4 R	120.0	0 150.0	3.00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.04

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1		SLU	0.00	284471.00	0.00	0.00	304398.00	-0.28	1-2	179.63	1.070

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	E WG	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg8	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic
1	0.00	0.00	1,20	20.11	0.00	2.50	261556.00	647021.00	261556.00	

Verifiche principali

Caso		1000	Tip	po	
-1	SLU	N	cost -	- mina	sic.

SEZIONE N.5

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	=	1.14
Altezza <m></m>	=	2,60

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Tipo	B <cm>></cm>	H <cm></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fct.k <dan cmq=""></dan>	Fcd <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
- 5	R.	114,00	260,00	3.00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.04

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	cc	TCC	N <dan></dan>	My <dann></dann>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danu></danu>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1		SLU	0.00	1531750.00	0.00	0.00	1573580.00	-0.00	1+2	180.00	1.027

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	pw Aq	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRod <dan></dan>	Vrdu <dan></dan>	Sic.
- 1	0.00	0.00	1.14	40.21	0.00	2.50	909893.00	1069120.00	909893.00	

Verifiche principali

Caso		Tipo									
1	SLU	N.	cost -	min.	sic.						

SEZIONE N.6

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	-	1.00
Altezza <m></m>	-	2.60

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Tipo	B <cm>></cm>	H <cm>></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fod <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
- 6	R	100.00	260,00	3.00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.04

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1		SLU	0.00	995994.00	0.00	0.00	1024820.00	0.00	1-2	180.00	1.029

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	om>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
- 1	0.00	0.00	1.00	40.21	0.00	2.50	909893.00	937828.00	909893.00	

Verifiche principali

Caso			Ti	po	
1	Stat	M	cost.	- min.	sic.

SEZIONE N.7

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	=	1.14 3.50
Altezza <m></m>	=	3.50

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Tipo	B <cm></cm>	H <cm></cm>	Cf <cm>></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fcd <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
7							25.17	235.17	16.78	B450C	4500.00	3913.04

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	oc	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
- 1		SIJJ	0.00	1531750.00	0.00	0.00	1615800.00	0.00	1-2	180,00	1.055

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	om>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
- 1	0.00	0.00	1,14	40.21	0.00	2.50	1228530.00	1443530.00	1228530.00	

Verifiche principali

Caso	Tipo							
1	SLU	N	cost -	- min.	sic.			

SEZIONE N.8

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	=	0.67
Altezza <m></m>	=	3.50

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Tipo	B (m)	H <cm>></cm>	Cf <am></am>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fcd <dan cmq=""></dan>	Fctd <dan cmq=""></dan>	Tp	Fyk <dan cmq=""></dan>	Fyd <dan cmq2<="" th=""></dan>
8							25,17	235.17	16.78	B450C	4500.00	3913.04

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
:1		SLU	0.00	2133810.00	0.00	0.00	2166050.00	-22.97	1-2	180.39	1.015

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	bw on>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
							240244.00	849455.00	240244.00	

Verifiche principali

Caso		Tipo							
- 1	SLU	N	cost	- min.	sic.				

SEZIONE N.9

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	-	1.00
Alterza <m></m>	-	3,50

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Tipo	B <cm></cm>	H <cm></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk <dan cmq=""></dan>	Fed <dan cmq=""></dan>	Fetd <dan cmq=""></dan>	Тр	Fyk <dan cmq=""></dan>	Fyd <dan cmq=""></dan>
.9	B	100,00	350.00	3,00	C40/50	415.00	25.17	235.17	16.78	B450C	4500.00	3913.04

Stato limite ultimo - Verifiche a flessione/pressoflessione

				Mo Verri						-	
Caso	cc	TCC	<dan></dan>	My <danm></danm>	<danm></danm>	<dan></dan>	<danm></danm>	<danm></danm>	Rott.	<grad></grad>	Sic.
1		SIJ	0.00	1963830.00	0.00	0.00	2008400.00	3.22	1+2	179.13	1.023

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	pw Aq	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRod <dan></dan>	Vrdu <dan></dan>	Sic.
- 1	0.00	0.00	1.00	20.11	0.00	2.50	616800.00	1271620.00	616800.00	

Verifiche principali

Caso		_	Tip	0	
-4	SLU	N	cost -	min.	sic.

SEZIONE.1 BIS

Sezione: Rettangolare - Dati geometrici della sezione

Base <m></m>	=	3.19
Altezza <m></m>	=	1,50

Caratteristiche delle sezioni e dei materiali utilizzati

Caraceara			2011		T MALCETTAL	- ALTERNAT		V.			
Sez. Tipo	B <cm></cm>	H <cm></cm>	Cf <cm></cm>	Cls	Fck <dan cmq=""></dan>	Fctk	Fed <dan cmc=""></dan>	Fctd <dan cmg=""></dan>	Tp	Fyk <dan cmg=""></dan>	Fyd <dan cmg=""></dan>

- 1		Management of the contract of the	When the said from the common to the	A CONTRACTOR OF THE PARTY OF				Secretary and the second secretary of the	
п	9.19	240 00 450 00	9 00 000 EM	49 C 00	Ph. C. 19 19 1	A 7 2 1 1 17 1	16.78 B450C	AE 0.0 - 0.0	2012 0

Stato limite ultimo - Verifiche a flessione/pressoflessione

Caso	œ	TCC	N <dan></dan>	My <danm></danm>	Mz <danm></danm>	Nu <dan></dan>	MRdy <danm></danm>	MRdz <danm></danm>	Rott.	α <grad></grad>	Sic.
1		SLV	0.00	296794.00	0.00	0.00	388399.00	12.35	1-2	179.74	1.309

Stato limite ultimo - Verifiche a taglio

Caso	Ty <dan></dan>	Tz <dan></dan>	om>	Asw <cmq></cmq>	Vsdu <dan></dan>	ctg0	VRsd <dan></dan>	VRcd <dan></dan>	Vrdu <dan></dan>	Sic.
1	0.00	0.00	3.19	20.11	0.00	2,50	262800.00	1728160.00	262800.00	

Verifiche principali

Caso		Tipo									
1	SLU	N	cost	-	min.	sic.					

Computo armature, cls e acciaio nelle sezioni

Sezione	g10 <dan></dan>	g16 <dan></dan>	ø20 <dan></dan>	ø26 <dan></dan>	ø30 <dan></dan>	Peso <dan></dan>	Vol.	ρ <dan mc=""></dan>
Sezione 10 (SEZIONE ATTACCO POST. DEL PALO POSTERIORE: 258X260) - Soll. man.		138.48	44.39	145.87		328.75	6.71	49.01
Sezione 2 (Sezione attacco testa pali ext concentr. 120x150) - Soll. man.	144	73.14	49.32		199	122.46	1.80	68.04
Sezione 3 (Sezione attacco pali int. radiale 258x150) - Soll. man.		102.18			233.05	335.23	3.87	86.62
Sezione 4 (Sezione attacco pali int. concentr. 120x150) - Soll. man.		73.14	29.59		55.49	158.22	1.80	87.90
Sezione 5 (Sezione attacco al nucleo radiale 114x260) - Soll, man.	144	106.60	122	83.36	177.56	367.52	2.96	123.99
Sezione 6 (Sezione attacco al nucleo concentrica 100x260) - Soll. man.		103.66		75.02	88.78	267.46	2,60	102.87
Sezione 7 (Sezione attacco al nucleo concentrica H=350 114x350) - Soll. man.		135.01		50.01	144.27	329.29	3.99	82.53
Sezione 8 (Sezione attacco al nucleo radiale H=350: 67x350) - Soll. man.	9.60	65.74		50.01	210.86	336.21	2.35	143.37
Sezione 9 (Sezione attacco al nucleo, concentrica H=350: 100x350) - Soll. man.	122	132.06	- 22	75.02	166.47	373.55	3.50	106.73
Sezione 1 (Sezione d'attacco pali ext radiale 319x150) - Soll. man.		115.02	24.66	83.36		223.04	4.79	46.61
Peso totale ferri	9.60	1045.03	147.97	562.65	1076.47	2841.73	34,36	82.70

Computo armature, cls e acciaio nei plinti/pali

Plinto/Palo	ø12 <dan></dan>	ø20 <dan></dan>	Peso <dan></dan>	Vol.	p <dan mc=""></dan>
Palo 1	391.99	1584.50	1976.49	28.27	69.90
Palo 2	391.99	1584.50	1976.49	28.27	69.90
Palo 3	391.99	1584.50	1976.49	28.27	69.90
Palo 4	391.99	1584.50	1976.49	28.27	69.90
Palo 5	391.99	1584.50	1976.49	28.27	59.90
Palo 6	391.99	1584.50	1976.49	28.27	69.90
Palo 7	391.99	1584.50	1976.49	28.27	69,90
Palo 8	391.99	1584.50	1976.49	28.27	69.90
Palo 9	391.99	1584.50	1976.49	28.27	69.90
Palo 10	391.99	1584.50	1976.49	28.27	69.90
Palo 11	391.99	1584.50	1976.49	28.27	69.90
Palo 12	391,99	1584.50	1976.49	28.27	69.90
Palo 13	391.99	1584.50	1976.49	28,27	69.90
Palo 14	391.99	1584.50	1976.49	28.27	69.90
Palo 15	391.99	1584.50	1976.49	28.27	69,90
Palo 16	391.99	1584.50	1976.49	28.27	69.90
Palo 17	391.99	1584.50	1976.49	28.27	69.90
Palo 18	391.99	1584.50	1976.49	28,27	69.90
Palo 19	391.99	1584.50	1976.49	28.27	69.90
Palo 20	391.99	1584.50	1976.49	28.27	69.90
Palo 21	391.99	1584.50	1976.49	28.27	59.90
Palo 22	391.99	1584.50	1976.49	28.27	69.90
Palo 23	391.99	1584.50	1976.49	28.27	69.90
Palo 24	391.99	1584.50	1976.49	28.27	69,90
Palo 25	391.99	1584,50	1976,49	28,27	69.90
Palo 26	391.99	1584.50	1976.49	28,27	69.90
Palo 27	391.99	1584.50	1976.49	28.27	69.90
Palo 28	391.99	1584.50	1976.49	28.27	69.90
Palo 29	391.99	1584.50	1976.49	28.27	69.90
Palo 30	391.99	1584.50	1976.49	28.27	69.90
Palo 31	391.99	1584.50	1976.49	28,27	69.90
Palo 32	391.99	1584.50	1976.49	28.27	69.90
Palo 33	391.99	1584.50	1976.49	28.27	69.90
Peso totale ferr	1 12935,60	52288.60	65224.20	933.05	69,90

Computo armature, cls e acciaio nelle solette/platee

					<mc></mc>	ρ <dan mc=""></dan>	
Armatura soletta a quota 0.00	807.65	1315.55	16705.90	18829.10	917.77	20.52	

Criteri di analisi geotecnica e progetto delle fondazioni

Fondazioni profonde

Generali	
Generali	
Calcolo capacità portante per carichi verticali	Secondo formule statiche
Considera capacità portante	Entrambe
Condizioni di calcolo per terreni coesivi	Sia drenate che non drenate
Calcolo della profondità critica	No.
Effettua calcolo elasto-plastico per cedimenti	Si
Effettua calcolo elasto-plastico per spostamenti orizzontali	Si
Rapporto di elasticità trazione/compressione pari a	1.00
Fattori di correlazione	1.70
Considera fattori di correlazione anche per carichi orizzontali	No
Considera peso del palo	No
Divisore del raggio del palo per lunghezza conci	1.00
Max numero conci palo	50.00
Attrito laterale limite da prove in sito	
Correlato con prove CPT	No
Correlato con prove SPT	No.
Fattore di riduzione attrito laterale per pali trivellati	No.
Pressione limite alla base da prove in sito	
Correlata con prove CP7	No.
Correlata con prove SPT	No
Fattore di riduzione pressione limite alla base per pali trivellati	No
Spostamenti orizzontali	
	a elastica in funzione della stratigrafia
WASHING THE PROPERTY OF THE PR	
Attrito laterale limite	
Calcolo dell'attrito laterale limite	
-Condizioni non drenate	
contribution of the contri	
-Calcolo di a	
-Calcolo di α -Pari a	
-Calcolo di o -Pari a -A.G.I. (1984)	
-Calcolo di o -Pari a -A.G.I. (1984) -A.P.I. (1984)	
-Calcolo di o -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999)	
-Calcolo di a -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982)	
-Calcolo di a -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984)	
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986)	
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989)	
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali	
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniezioni ripetute	
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Clson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniexioni ripetute -Unica iniezione	
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniezioni ripetute -Unica iniezione -Condizioni drenate	
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniexioni ripetute -Unica iniexione -Condizioni drenate -Calcolo di β	
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniezioni ripetute -Unica iniezione -Condizioni drenate -Calcolo di β -Pari a	0.00
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniezioni ripetute -Unica iniezione -Condizioni drenate -Calcolo di β -Pari a -Reese e O'Neill (1989)	0.
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniezioni ripetute -Unica iniezione -Condizioni drenate -Calcolo di β -Pari a -Reese e O'Neill (1989)	0.
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Vigglani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniexioni ripetute -Unica iniezione -Condizioni drenate -Calcolo di β -Pari a -Reese e O'Neill (1989) -Calcolato -Calcolo di k	0.
Calcolo di a Pari a A.G.I. (1984) A.P.I. (1984) Vigglani (1999) Olson e Dennis (1982) Stas e Kulhavy (1984) Skempton (1986) Reese e O'Neill (1989) Metodo di Bustamente e Doix (1985) per micropali Iniexioni ripetute Unica iniezione Condizioni drenate Calcolo di ß Pari a Reese e O'Neill (1989) Calcolato Calcolo di k Pari a	
Calcolo di o Pari a A.G.I. (1984) A.P.I. (1984) Viggiani (1999) Olson e Dennis (1982) Stas e Kulhavy (1984) Skempton (1986) Reese e O'Neill (1989) Metodo di Bustamente e Doix (1985) per micropali Iniezioni ripetute Unica iniezione Condizioni drenate Calcolo di ß Pari a Reese e O'Neill (1989) Calcolato Calcolo di k Pari a Calcolo di k	0.
Calcolo di o Pari a A.G.I. (1984) A.P.I. (1984) Vigglani (1999) Olson e Dennis (1982) Stas e Kulhavy (1984) Skempton (1986) Reese e O'Neill (1989) Metodo di Bustamente e Doix (1985) per micropali Iniezioni ripetute Unica iniezione Condizioni drenate Calcolo di ß Pari a Reese e O'Neill (1989) Calcolato Calcolo di k Pari a Fal rapporto con ko pari a Feleming (1985)	
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Calcolo di G Pari a A.G.I. (1984) A.P.I. (1984) Viggiani (1999) Olson e Dennis (1982) Stas e Kulhavy (1984) Skempton (1986) Reese e O'Neill (1989) Metodo di Bustamente e Doix (1985) per micropali Iniezioni ripetute Unica iniezione Condizioni drenate Calcolo di ß Pari a Reese e O'Neill (1989) Calcolato Calcolo di k Pari a Dal rapporto con ko pari a Fleming (1985) Calcolo di δ Pari a <grad></grad>	0.
Calcolo di G Pari a A.G.I. (1984) A.P.I. (1984) Viggiani (1999) Olson e Dennis (1982) Stas e Kulhavy (1984) Skempton (1986) Reese e O'Neill (1989) Metodo di Bustamente e Doix (1985) per micropali Iniezioni ripetute Unica iniezione Condizioni drenate Calcolo di ß Pari a Reese e O'Neill (1989) Calcolato Calcolo di k Pari a Dal rapporto con ko pari a Fleming (1985) Calcolo di δ Pari a <grad> Dal rapporto con φ' pari a</grad>	0:
Calcolo di G Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniezioni ripetute -Unica iniezione -Condizioni drenate -Calcolo di B -Pari a -Reese e O'Neill (1989) -Calcolo di k -Pari a -Dal rapporto con ko pari a -Fleming (1985) -Calcolo di δ -Pari a <grad> -Calcolo di α -Calcolo di α -Calcolo di δ -Pari a <grad> -Calcolo di α -Calc</grad></grad>	0.
Calcolo di α Pari a A.G.I. (1984) A.P.I. (1984) Viggiani (1999) Olson e Dennis (1982) Stas e Kulhavy (1984) Skempton (1986) Reesse e O'Neill (1989) Metodo di Bustamente e Doix (1985) per micropali Iniezioni ripetute Unica iniezione Condizioni drenate Calcolo di β Pari a Reesse e O'Neill (1989) Calcolato Calcolo di k Pari a Fleming (1985) Calcolo di δ Pari a sgrad> Dal rapporto con φ' pari a Calcolo di a' dal rapporto con c' Calcolo dell'attrito laterale limite per trazione	0.
Calcolo di α Pari a A.G.I. (1984) A.P.I. (1984) Viggiani (1999) Olson e Dennis (1982) Stas e Kulhavy (1984) Skempton (1986) Reesse e O'Neill (1989) Metodo di Bustamente e Doix (1985) per micropali Iniezioni ripetute Unica iniezione Condizioni drenate Calcolo di β Pari a Reesse e O'Neill (1989) Calcolato Calcolo di k Pari a Fleming (1985) Calcolo di δ Pari a sgrad> Dal rapporto con ψ' pari a Calcolo di a' dal rapporto con c' Calcolo dell'attrito laterale limite per trazione Considera i risultati del calcolo per l'attrito laterale limite percompres	0. 0. 1. sione con un fattore di riduzione pari a 0.
Calcolo di a Pari a A.G.I. (1984) A.P.I. (1984) Viggiani (1999) Olson e Dennis (1982) Stas e Kulhavy (1984) Skempton (1986) Reese e O'Neill (1989) Metodo di Bustamente e Doix (1985) per micropali Iniezioni ripetute Unica iniezione Condizioni drenate Calcolo di ß Pari a Reese e O'Neill (1989) Calcolato Calcolo di k Pari a Dal rapporto con kö pari a Fleming (1985) Calcolo di ö Pari a <grad> Dal rapporto con o' pari a Calcolo di a' dal rapporto con e' Calcolo di i' attrito laterale limite per trazione Considera i risultati del calcolo per l'attrito laterale limite percompres Sowa (1970)</grad>	0.
-Calcolo di α -Pari a -A.G.I. (1984) -A.P.I. (1984) -Viggiani (1999) -Olson e Dennis (1982) -Stas e Kulhavy (1984) -Skempton (1986) -Reese e O'Neill (1989) -Metodo di Bustamente e Doix (1985) per micropali -Iniezioni ripetute -Unica iniezione -Condizioni drenate -Calcolo di β -Pari a	0. 0. 1. sione con un fattore di riduzione pari a 0.

relazione di Calcolo	1
Pressione limite alla base	
C. long of the comparation of limit of a Harrist the property	31
-terraghi (1943)	×
-Meyerhof (1963)	\top
Talken (1970)	\top
Mexico (1975)	\top
-Parcy, at the (19c1)	
Particle of the (19ck)	\top
-Staggle Lienkiewicz (1968)	\top
-welazione generale, coefficienti il capacita portante	\top
To condition' crenate	
य _ु	\top
-3 _{1,1}	
-Thispordia por improdusamble	\top
-14 ₀	Т
-Fathane in office cas partisement access of second case to	Mo
Cedimenti	+-
Rispost, a nation of amily -Calcalitate to a famiginary can be a total	+-
-Coefficiente di influenza	4,00
-Barria <ah ar="" indicensa<="" refrance="" td=""><td>+1.0%</td></ah>	+1.0%
Pisposta e astida a la base	+-
Calcolata da Talifginezza de lo Aliato	+ ,
-Burning also be the ingreezed be to visitation.	+ ^
-ear . Available	+-
Spostamenti orizzontali	
Ripper, e retion	\top
-vesic (1961)	+-
-groups (1964)	\top
G17.x (1 ± 8)	\top
Crear (1978)	\top
-Farris Kmit/r dz	\top
-Datined to known rec	\top
-Coefficiente effetto tridimensionale	2,00
wesistenza limite	
Cathoriata da' pararétri ditas.'di	
Coefficience e fetto inidimensionale rexiste valven autrito	3.00
-CoeffChien cleffotto inidimonsiona chesistenza por posiciono	4,00
-Familia Kimit/mide	

Geotecnica

Elenco unità geotecniche

1 ARGILLE BRECCIATE DI COLORE NOCCIOLA:

Constituy violet Constive

Pesi:

- = Persy specific, v. .es. Tempore, no u.e. lest γ = 1947.00 a. M/ma. Pess specific to the literage value of v_{SSE} = 1000.00 deK/m.

- Promost multiplication of the Principle of the Principle

- Ormittem sticket litestatick: Pracopi yoyrado so haz chec XR = 1000
- Coeff. di apinta a riposo: $\kappa_{\rm Q} = 0.06$

Parametri elastici:

- Parametri elastic: = Modulo v accinct norm. Let $T = 901500.00 \; \mathrm{com}/\mathrm{rg}$ Modulo e as, acclarge v a et $T = 210300.00 \; \mathrm{deK/rg}$ = Esponente del parametro tensionale: $\lambda_j = 0.00$

- Coeff. di Piisson: v = 0.35 Mod.lo edomo rico: T_{er.} = 500000.00 chN/mo
- Modulo elastico non direnato: $E_{\rm p}$ = 346200.00 daM/mg

2 ARGILLE BRECCIATE GRIGIO-AZZURRE:

Constituy kioner Constvo

- Relay appoint "Low Loss Tempore, notice, last y = 1987,000 to Maint Peach specific to the Cherrent Aerickology, p. = 1980,000 deN75.

Pararela viax. Laic

- Angolo di attrito efficace: \$^* 22.23 grai Section efficace: \$^* 400.00 deM/ng
- These forces on the average TWOSDIGC be Windows

Caratter sticks litestaticks

- Grado di sovraconsolidazione: OCR = 1.00
- Coeff. di spinta a riposo: KO = 0.66

Parametri elastici:

- Modulo elastico normale: E = 533200.00 daN/mg
- Modulo elastico tangenziale: G = 359900.00 daN/mg
- Esponente del parametro tensionale: kj = 0.00
- Coeff. di Poisson: v = 0.35
- Modulo edometrico: Eed 855800.00 daN/mq
- Modulo elastico non drenato: E_{II} = 592400.00 daN/mq

Elenco colonne stratigrafiche

Colonna stratigrafica numero 1

Posizione: X=0.00 <m> Y=0.00 <m> Z=1.00 <m> Falda non presente

Simbologia

φ' = Angolo di attrito efficace

y = Peso specifico del terreno naturale

Ysat - Peso specifico del terreno saturo

κ₀ = Coeff. di spinta a riposo

Class. = Classificazione

Coes. = Coesivo Crit. = Criterio di progetto

 D_r = Densità relativa

Ip = Indice di plasticità

OCR - Grado di sovraconsolidazione

St. = Strato

Unità geotecnica - Unità geotecnica

c_D = Coesione non drenata

c' = Coesione efficace

z = Profondità della superficie superiore dello strato

St.	z (m)	Unità geotecnica	Class.	Y <dan mc=""></dan>	Ysat <dan mc=""></dan>	Dr	ıp	φ' <grad></grad>	c' <dan mq=""></dan>	cu <dan mq=""></dan>	OCR	x 0	Crit.
-1	0.00	1 ARGILLE BRECCIATE DI COLORE NOCCIOLA	Coes.	1947.00	2030.00			19.18	3190.00	6110.00	1.00	0.66	- 1
- 2	4.50	2 ARGILLE BRECCIATE GRIGIO-AZZURRE	Coes.	1997.00	2130.00			22.23	4710.00	13090.00	1.00	0.66	- 1

Simbologia

v = Coeff. di Poisson

Crit. = Criterio di progetto

E = Modulo elastico normale

E_{ed} = Modulo edometrico

E_U = Modulo elastico non drenato

G = Modulo elastico tangenziale

St. = Strato

k- = Esponente del parametro tensionale

z = Profondità della superficie superiore dello strato

St.	z <m></m>	E <dan mq=""></dan>	G <dan mq=""></dan>	kj	v	E _{ed} <dan mq=""></dan>	E ₁ <dan mq=""></dan>	Crit.
1	0.00	311500.00	210300.00	0.00	0.35	500000.00	346200.00	1
- 2	4.50	533200.00	359900.00	0.00	0.35	855800.00	592400.00	1

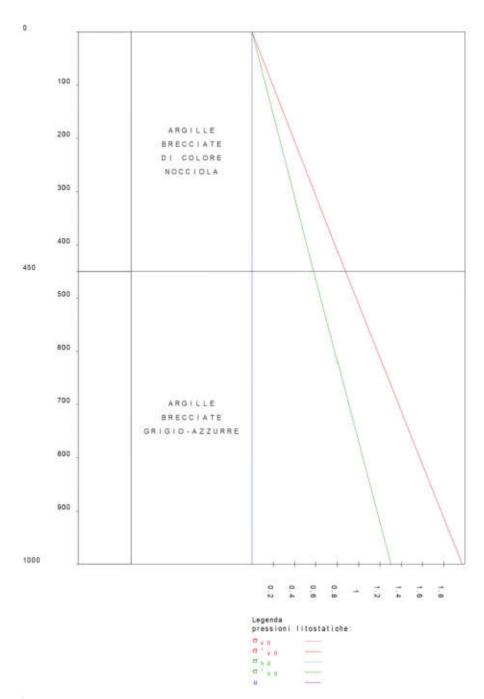


Figura numero 1: Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA

```
Coefficienti parziali per le azioni, per verifiche in condizioni statiche:
Permanenti strutturali, sicurezza a favore ya = 1.00;
Permanenti strutturali, sicurezza a sfavore yA = 1.30;
Permanenti non strutturali, sicurezza a favore ya = 0.00;
Permanenti non strutturali, sicurezza a sfavore ya = 1.50;
Variabili, sicurezza a favore VA = 0.00;
Variabili, sicurezza a sfavore YA = 1.50.
I coefficienti parziali per le azioni sono posti pari all'unità per le verifiche in condizioni sismiche.
Tali coefficienti sono comunque desumibili dalla tabella delle combinazioni delle CCE (Parametri di calcolo).
Coefficienti parziali per i parametri geoteonici: Tangente dell'angolo di attrito \gamma_{M} = 1.00;
Coesione efficace VM = 1.00;
Coesione non drenata \gamma_{\text{M}} = 1.00;
Coefficienti parziali per la resistenza delle fondazioni superficiali:
Capacità portante \gamma_R = 2.30;
Scorrimento yR = 1.10;
Coefficienti parziali per la resistenza delle fondazioni profonde:
```

Le verifiche degli elementi di fondazione sono state effettuate utilizzando l'approccio 2.

```
Per pali infissi:
Resistenza alla base yR,b = 1.15;
Resistenza laterale in compressione yR,s = 1.15;
Resistenza laterale in trazione yR,t = 1.25;
Per pali trivellati:
Resistenza alla base yR,b = 1.35;
Resistenza alla base yR,b = 1.35;
Resistenza laterale in compressione yR,s = 1.15;
Resistenza laterale in trazione yR,t = 1.25;
Per pali ad elica continua:
Resistenza alla base yR,b = 1.30;
Resistenza laterale in compressione yR,s = 1.15;
Resistenza laterale in trazione yR,t = 1.25;
Fattore di correlazione per la determinazione della resistenza caratteristica desumibile dai criteri di progetto.
```

Fondazioni profonde

Simbologia

```
σh = Pressione limite per carichi orizzontali
\tau_S = Attrito laterale limite per compressione
CC = Numero della combinazione delle condizioni di carico elementari
Caso = Caso di verifica
Ced = Cedimento calcolato
D = Profondită della testa del palo
Dp = Diametro pali
Lp = Lunghezza pali
M - Momento flettente
N = Sforzo normale
QP<sub>lim</sub> = Resistenza di progetto alla base del palo
QSlim = Resistenza laterale di progetto per compressione
Sic.O = Sicurezza a rottura orizzontale
Sic.V = Sicurezza a rottura verticale
Sps = Spostamento
T = Taglio in testa
Wp = Peso del palo
Zp = Profondità del tratto di integrazione
k<sub>h</sub> = Risposta elastica per carichi orizzontali
k<sub>p</sub> = Risposta elastica alla base del palo
kg = Risposta elastica laterale per compressione
qp = Pressione limite alla base del palo
```

Verifiche capacità portante e cedimenti

```
Palo n. 1
```

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _≘ <dan cmq=""></dan>	k ₈ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

```
QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>
```

Verifiche in condizioni non drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _∃ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

```
QS<sub>lim</sub>=472754.00 <daN>
qp=13.92 <daN/cmq>
QP<sub>lim</sub>=157422.00 <daN>
kp=1.17 <daN/cmc>
```

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-128741.00	0.91	6,53	7086.36	65401.70	0.74	>1
- 3	2	-95363.70	0.67		5249.16	48445.70	0.55	
- 35	. 3	-95363.70	0.67		5249,16	48445.70	0.55	
7	4	-95363.70	0.67		5249.16	48445.70	0.55	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
2	-1	-128741.00	0.91	2.41	7086.36	65401.70	0.74	>1
4	2	-95363.70	0.67		5249.16	48445.70	0.55	
- 6	3	-95363.70	0.67		5249.16	48445.70	0.55	
8	- 4	-95363.70	0.67		5249.16	48445.70	0.55	

Palo n. 2

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	t _s <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _□ <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

 $QS_{lim}=472754.00 < daN> \\ q_p=13.92 < daN/cmq> \\ QP_{lim}=157422.00 < daN> \\ k_p=1.17 < daN/cmc>$

Verifiche in condizioni drenate

Caso	000	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 1	1	-204703.00	1.45	4.11	6687.11	60353.10	0.69	>1
:3	.2	-151632.00	1.07		4953.41	44706.00	0.51	
- 5	3	-151632.00	1.07		4953.41	44706.00	0.51	
7	.4	-151632.00	1.07		4953.41	44706.00	0.51	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
2	1	-204703.00	1.45	1.52	6687.11	60353.10	0.69	>1
4	2	-151632.00	1.07		4953.41	44706.00	0.51	8-
.6	3	-151632.00	1.07		4953.41	44706.00	0.51	
. 8	4	-151632.00	1.07		4953,41	44706.00	0.51	

Palo n. 3

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _∃ <dan cmq=""></dan>	k _B <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89

26.00 1.76 0.15 40.00 0.89

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _β <dan cmq=""></dan>	kg <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

 $\begin{array}{l} {\rm QSlim} = 472754.00 < {\rm daN}> \\ {\rm q_p} = 13.92 < {\rm daN/cmq}> \\ {\rm QPlim} = 157422.00 < {\rm daN}> \\ {\rm k_p} = 1.17 < {\rm daN/cmd}> \end{array}$

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <am></am>	Sic.O
- 1	1	-274379.00	1,94	3.07	6293,40	44922.90	0.57	>1
- 3	2	-203244.00	1.44		4661.78	33276.20	0.42	
- 5	. 3	-203244.00	1.44		4661.78	33276.20	0.42	
:7	4	-203244.00	1.44		4661.78	33276.20	0.42	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
- 2	1	-274379.00	1,94	1.13	6293.40	44922.90	0.57	>1
4	. 2	-203244.00	1.44		4661.78	33276,20	0.42	
- 6	3	-203244.00	1.44		4661.78	33276.20	0.42	
. 8	4	-203244.00	1.44	9-40	4661.78	33276.20	0.42	

Palo n. 4

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ ₀ <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _∃ <dan cmq=""></dan>	k _B <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
1	1	-315710.00	2.23	2.66	6046.37	23929.60	0.42	>1
3	2	-233859.00	1.65		4478.79	17725+60	0.31	
- 5	3	-233859.00	1.65		4478.79	17725.60	0.31	-
7	4	-233859.00	1,65		4478.79	17725.60	0.31	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 2	1	-315710.00	2.23	<1	6046.37	23929.60	0.42	>1
4	2	-233859,00	1.65		4478.79	17725.60	0.31	
- 6	3	-233859.00	1.65		4478.79	17725,60	0.31	
.8	4	-233859.00	1.65		4478,79	17725.60	0.31	

Palo n. 5

Tipo palo-Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _E <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ ₂ <dan cmq=""></dan>	k ₀ σ _h <dan cmc=""> <dan cmc<="" th=""><th colspan="2">k_{ii} <dan cmc=""></dan></th></dan></dan>		k _{ii} <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

 $\begin{array}{l} {\rm QS_{lim}=472754.00~<daN>} \\ {\rm q_p=13.92~<daN/cmq>} \\ {\rm QP_{lim}=157422.00~<daN>} \\ {\rm k_p=1.17~<daN/cmc>} \end{array}$

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-315619.00	2,23	2.67	6042.40	23993.40	0.42	>1
- 3	2	-233792.00	1,65		4475.85	17772.90	0.31	
5	3	-233792.00	1.65		4475.85	17772.90	0.31	
7	4	-233792.00	1.65		4475.85	17772.90	0.31	

Verifiche in condizioni non drenate

Caso	cc	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	<cm></cm>	Sic.0
- 2	1	-315619.00	2,23	<1.	6042.40	23993.40	0.42	>1
4	. 2	-233792.00	1.65		4475.85	17772.90	0.31	
-6	3	-233792.00	1.65		4475.85	17772.90	0.31	
.8	4	-233792.00	1.65		4475.85	17772.90	0.31	

Pale n. 6

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Mp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h /cmc> <dan cmq=""> <dz< th=""></dz<></dan>	
1.00	0.37	0.09	4.75	0.52
4,50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Zp <m></m>	τ _β <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	8	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
1	1	-274241.00	1.94	3.07	6295.05	44648.90	0.57	>1
3	2	-203142.00	1,44		4663.00	33073,30	0.42	
- 5	3	-203142.00	1.44		4663.00	33073.30	0.42	
- 7	4	-203142.00	1,44		4663,00	33073.30	0.42	

Verifiche in condizioni non drenate

Caso	00	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
- 2	1	-274241.00	1.94	1.13	6295.05	44648.90	0.57	>1
4	2	-203142.00	1.44		4663.00	33073.30	0.42	
6	. 3	-203142.00	1.44		4663.00	33073.30	0.42	
.8	4	-203142.00	1.44		4663.00	33073.30	0.42	

Palo n. 7

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna atratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _≘ <dan cmq=""></dan>	k _B <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	t _S <dan cmq=""></dan>	k _{ii} <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0,52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	8	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
1	1	-204511.00	1.45	4,11	6688.75	60395.30	0.59	>1
3	2	-151490.00	1.07	(40.00)	4954.63	44737.20	0.51	
.5	3	-151490.00	1.07		4954.63	44737.20	0.51	
.7	4	-151490.00	1.07		4954.63	44737,20	0.51	

Caso	8	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
- 2	1	-204511.00	1.45	1.52	6688.75	60395,30	0.69	>1
4	2	-151490.00	1.07		4954.63	44737.20	0.51	
- 5	3	-151490.00	1.07		4954.63	44737.20	0.51	

. 8	4	-151490.00	1.07	 4954.63	44737.20	0.51	

Palo n. 8

Tipo palo=Trivellato Rotazione testa libera

Coefficiente di efficienza=1.00 Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m> Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA

Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _{ii} <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QS_{lim}=1054060.00 <daN> qp=61.31 <daN/cmq> QP1:m=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp ∢m>	τ _≘ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmg> QP1im=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 1	1	-128535.00	0.91	6.55	7082,39	65411.00	0.74	>1
- 3	2	-95211.30	0.67		5246.21	48452.60	0.55	
- 5	. 3	-95211.30	0.67		5246.21	48452.60	0.55	
- 37	.4	-95211.30	0.67		5246,21	48452,60	0.55	

Verifiche in condizioni non drenate

Caso	cc	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
- 2	1	-128535.00	0.91	2.41	7082.39	65411.00	0.74	>1
4	. 2	-95211.30	0.67		5246.21	48452.60	0.55	
-6	3	-95211.30	0.67		5246.21	48452.60	0.55	
8	4	-95211.30	0.67		5246.21	48452.60	0.55	

Palo n. 9

Tipo palo=Trivellato Rotazione testa libera Coefficiente di efficienza=1.00 Dp=1.200000 <n> Lp=25.000000 <n> Wp=70685.80 <daN> D=1.00 <n> Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _S <dan cmc=""></dan>	on <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QP_{lim}=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	t _∃ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	

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26.00	0.52	0.15	10.47	0.89
er or er or or	0.100	10.4 4.07		0.00

 $\begin{array}{l} {\rm QS_{lim}=472754.00~<daN>} \\ {\rm q_p=13.92~<daN/cmq>} \\ {\rm QP_{lim}=157422.00~<daN>} \\ {\rm k_p=1.17~<daN/cmc>} \end{array}$

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-70710.80	0.50	11,90	7364.87	62472,80	0.73	>1
- 3	. 2	-52378.40	0.37		5455.46	46276.10	0.54	
.5	3	-52378.40	0.37		5455.46	46276.10	0.54	
7	4	-52378.40	0.37		5455.46	46276.10	0.54	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
2	1	-70710.80	0.50	4.39	7364.87	62472.80	0.73	>1
4	2	-52378.40	0.37		5455.46	46276.10	0.54	
- 6	3	-52378.40	0.37		5455.46	46276.10	0.54	
- 8	4	-52378,40	0.37		5455.46	46276.10	0.54	

Palo n. 10

Tipo palo-Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200600 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drepate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmq>

Verifiche in condizioni non drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <am></am>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-49182.60	0.35	17.11	7463.04	59871.30	0.72	>1
- 3	2	-36431.60	0.26		5528.18	44349.10	0.53	77
- 5	3	-36431.60	0.26		5528.18	44349.10	0.53	
7	4	-36431.60	0.26		5528.18	44349.10	0.53	

Verifiche in condizioni non drenate

Caso	cc	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
2	-1	-49182.60	0.35	6.31	7463.04	59871.30	0.72	>1
4	2	-36431.60	0.26		5528.18	44349.10	0.53	
- 6	3	-36431.60	0.26		5528.18	44349.10	0.53	
. 8	4	-36431.60	0.26		5528.18	44349.10	0.53	

Palo n. 11

Tipo palo-Trivellato Rotazione testa libera Coefficiente di efficienza-1.00

Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m> Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _∃ <dan cmq=""></dan>	k _B <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _b <dan cmc=""></dan>	
1,00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

 $QS_{lim}=472754.00 < daN>$ qp=13.92 < daN/cmq> $<math>QP_{lim}=157422.00 < daN>$ kp=1.17 < daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
1	1	-70857.90	0.50	11.87	7366.75	62507.80	0.73	>1
.3	2	-52487.40	0.37		5456.85	46302.10	0.54	
. 5	3	-52487.40	0.37		5456.85	46302,10	0.54	
7	4	-52487.40	0.37		5456.85	46302.10	0.54	

Verifiche in condizioni non drenate

Caso	8	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
- 2	1	-70857,90	0.50	4,38	7366.75	62507.80	0.73	>1
4	2	-52487.40	0.37		5456.85	46302.10	0.54	
- 6	3	-52487.40	0.37		5456.85	46302.10	0.54	
8	4	-52487.40	0.37		5456.85	46302.10	0.54	

Palo n. 12

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _∃ <dan cmq=""></dan>	k _B <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	kh <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4,50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _g <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

QS_{lim}=472754.00 <daN> q_p=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> k_p=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	cc	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
- 1	-2	-9426.53	0.07	89.25	7685.04	55211.00	0.70	>1
3	2	-6982.62	0.05		5692.63	40897.00	0.52	
5	3	-6982.62	0.05		5692.63	40897.00	0.52	
7	6	-6982.62	0.05		5692.63	40897.00	0.52	

Verifiche in condizioni non drenate

Caso	oc	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 2	. 1	-9426.53	0.07	32.93	7685.04	55211.00	0.70	>1
- 4	2	-6982.62	0.05		5692.63	40897.00	0.52	
- 6	3	-6982.62	0.05		5692.63	40897.00	0.52	
- 8	4	-6982,62	0.05		5692.63	40897.00	0.52	

Palo n. 13

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m> Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp ⟨m⟩	τ _S <dan cmq=""></dan>	k ₈ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	kh <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1,76	0.15	40.00	0.89

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QFlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	t _≘ <dan cmq=""></dan>	k _B <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

OSlim=472754.00 <daN>
qp=13.92 <daN/cmq>
QPlim=157422.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <am></am>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
1	1	-9469.03	0.07	88.85	7683.96	55220.60	0.70	>1
- 3	2	-7014.10	0.05		5691.82	40904.10	0.52	
- 5	3	-7014.10	0.05		5691.82	40904.10	0.52	
7	. 4	-7014.10	0.05		5691.82	40904.10	0.52	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 2	1	-9469.03	0.07	32.78	7683.96	55220.60	0.70	>1
4	2	-7014.10	0.05		5691.82	40904.10	0.52	
- 6	3	-7014.10	0.05		5691.82	40904.10	0.52	
8	4	-7014.10	0.05		5691.82	40904.10	0.52	

Palo n. 14

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp	t _B <dan cmq=""></dan>	k _s	σ _n	k _h
<m></m>		<dan cmc=""></dan>	<dan cmq=""></dan>	<dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52

	4.50	0.69	0.15	11.44	0.89
ĺ	26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	t _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10,47	0.89

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-22330,90	0.16	37.67	7621.21	56900.50	0.71	>1
- 3	. 2	-16541,40	0.12		5645.34	42148.50	0.52	
.5	3	-16541.40	0.12		5645.34	42148.50	0.52	
7	4	-16541.40	0.12		5645.34	42148,50	0.52	

Verifiche in condizioni non drenate

Caso	œ		Ced <cm></cm>		<dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
2	. 1	-22330.90	0.16	13.90	7621.21	56900.50	0.71	>1
- 4	2	-16541.40	0.12		5645.34	42148.50	0.52	
- 6	3	-16541.40	0.12		5645.34	42148.50	0.52	
- 8	4	-16541.40	0.12		5645.34	42148.50	0.52	

Palo n. 15

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Np=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _s <dan cmq=""></dan>	k ₈ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _b <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k ₈ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4,89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> kp=1.17 <daN/cmc>

Caso	8	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <as></as>	Sic.O
1	1	-46827.10	0.33	17.97	7490.69	59399.20	0.72	>1
3	2	-34686.80	0.25		5548.66	43999.40	0.53	-
- 5	3	-34686.80	0.25		5548.66	43999.40	0.53	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <am></am>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.0
- 2	1	-46827.10	0.33	6.63	7490.69	59399.20	0.72	>1
4	2	-34686.80	0.25	75.	5548.66	43999,40	0.53	to to
6	3	-34686.80	0.25		5548.66	43999.40	0.53	
8	4	~34686.80	0.25		5548.66	43999.40	0.53	

Palo n. 16

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1,00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _≘ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QS_{lim}=472754.00 <daN> q_p=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> k_p=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ		Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-81184.60	0.57	10.36	7310.74	61392.50	0.72	>1
3	. 2	-60136.70	0.43		5415.36	45475.90	0.54	
5	3	-60136.70	0.43		5415.36	45475.90	0.54	
7	4	-60136.70	0.43		5415.36	45475.90	0.54	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
2	. 1	-81184.60	0.57	3.82	7310.74	61392.50	0.72	>1
4	.2	-60136.70	0.43		5415.36	45475.90	0.54	
:6	3	-60136.70	0.43		5415.36	45475.90	0.54	
8	4	-60136.70	0.43		5415.36	45475.90	0.54	

Palo n. 17

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _b <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN>

kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _∃ <dan cmq=""></dan>	k _⊞ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Cod <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
1	.1	-122467.00	0.87	6.87	7078.60	61763.00	0.72	>1
3	2	-90716.20	0.64		5243.41	45750.40	0.53	
- 5	3	-90716.20	0.64		5243.41	45750,40	0.53	4-
7	4	-90716.20	0.64		5243.41	45750.40	0.53	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
:2	1	-122467.00	0.87	2.53	7078,60	61763.00	0.72	>1
4	2	-90716.20	0.64		5243.41	45750.40	0.53	
- 6	3	-90716.20	0.64		5243.41	45750.40	0.53	
8	4	-90716.20	0.64		5243.41	45750.40	0.53	

Palo n. 18

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _∃ <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QS_{lim}=1054060.00 <daN> qp=61.31 <daN/cmq> QP_{lim}=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _≘ <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	cc	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 1	-1	-166477.00	1,18	5.05	6825.85	59718,20	0.69	>1
3	2	-123316.00	0.87		5056.18	44235.70	0.51	
5	3	-123316.00	0.87		5056.18	44235.70	0.51	
7	4	-123316.00	0.87		5056.18	44235,70	0.51	

Caso				Sic.V		M <danm></danm>		
- 2	1	-166477.00	1.18	1.86	6825.85	59718.20	0.69	>1

1	4	2	-123316.00	0.87		5056,18	44235.70	0.51	
	- 6	3	-123316.00	0.87		5056.18	44235.70	0.51	
Ī	.8	4	+123316.00	0.87	(40.00)	5056,18	44235.70	0.51	

Palo n. 19

Tipo palo=Trivellato

Rotazione testa libera Coefficiente di efficienza=1.00 Dp=1.200000 <m> lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m> Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA Verifiche in condizioni drenate

Zp <m></m>	τ _≘ <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QS1±m=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN>

 $k_p=1.17 < daN/cmc>$

Verifiche in condizioni non drenate

Zp ⟨m⟩	τ _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10,47	0.89	

QS_{11m}=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> $k_p=1.17 < daN/cmc>$

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
_ 1	1	-212368.00	1.50	3.96	6542.33	54441.50	0.64	>1
- 3	2	-157310.00	1.11		4846,17	40327.00	0.48	
- 5	3	-157310.00	1.11		4846.17	40327.00	0.48	
7	4	-157310.00	1.11		4846.17	40327,00	0.48	

Verifiche in condizioni non drenate

Caso	cc	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	sic.o
.2	1	-212368.00	1.50	1.46	6542.33	54441.50	0.64	>1
- 4	2	-157310.00	1.11		4846.17	40327.00	0.48	
- 6	3	-157310.00	1.11		4846,17	40327.00	0.48	
- 8	4	-157310.00	1.11		4846.17	40327.00	0.48	

Palo n. 20

Tipo palo=Trivellato Rotazione testa libera

Coefficiente di efficienza=1.00

Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>

Colonna stratigrafica numero I COLONNA STRATIGRAFICA

Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _n <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QS_{lim}=1054060.00 <daN> qp=61.31 <daN/cmq>

QP_{11m}=693364.00 <daN>

kp=1.17 <daN/cmc>

	Zp	tg <dan cmq=""></dan>	k _S	σ'n	k _b
ı	<m></m>	<dan cmq=""></dan>	<dan cmc=""></dan>	<dan cmg=""></dan>	<dan cmc=""></dan>

1	1.00	0.37	0.09	4.89	0.52
1	4.50	0.52	0.15	10.47	0.89
	26.00	0.52	0.15	10.47	0.89

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
1	-1	-253743.00	1.79	3,32	6276.62	46241.50	0.58	>1
- 3	2	-187958.00	1,33		4649.35	34252.90	0.43	
- 5	3	-187958.00	1.33		4649.35	34252.90	0.43	
7	4	-187958.00	1.33		4649.35	34252.90	0.43	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
- 2	1	-253743.00	1.79	1,22	6276.62	46241,50	0.58	>1
4	2	-187958.00	1.33		4649.35	34252.90	0.43	
6	. 3	-187958.00	1.33		4649.35	34252.90	0.43	
8	4	-187958.00	1.33		4649.35	34252.90	0.43	

Palo n. 21

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _⊞ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	kh <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _{ii} <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	8	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
1	1	-287981.00	2.04	2.92	6041,15	35402,70	0.50	>1
3	2	-213319.00	1.51	~~	4474.93	26224.20	0.37	
5	3	-213319.00	1,51		4474.93	26224.20	0.37	
7	4	-213319.00	1,51		4474.93	26224,20	0.37	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 2	1	-287981.00	2.04	1.08	6041.15	35402.70	0.50	>1
4	2	-213319.00	1,51		4474.93	26224,20	0.37	
- 6	3	-213319.00	1,51		4474.93	26224,20	0.37	
- 8	4	-213319.00	1,51		4474.93	26224.20	0.37	

Palo n. 22

Tipo palo-Trivellato

Rotazione testa libera Coefficiente di efficienza=1.00 Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m> Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA

Zp <m></m>	τ _≘ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QFlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Verifiche in condizioni drenate

Zp <m></m>	t _g <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	8	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
1	1	-312560.00	2,21	2.69	5870,52	22391.20	0.40	>1
3	2	-231526.00	1.64		4348.53	16586.10	0.30	
- 5	3	-231526.00	1.64		4348.53	16586,10	0.30	
7.	4	-231526.00	1.64		4348.53	16586.10	0.30	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
- 2	1	-312560.00	2,21	<1	5870.52	22391,20	0.40	>1
- 4	2	-231526.00	1,64		4348.53	16586,10	0.30	
- 6	3	-231526.00	1.64		4348.53	16586.10	0.30	
.8	4	-231526.00	1.64		4348.53	16586.10	0.30	

Palo n. 23

Tipo palo=Trivellato
Rotazione testa libera
Ccefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m> Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _s <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	kh <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	t _∈ <dan cmq=""></dan>	k _{ii} <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QS_{lim}=472754.00 <daN> q_p=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-325273.00	2,30	2.59	5776.64	8448.83	0.30	>1
3	2	-240943.00	1,70		4278.99	6258.39	0.22	77
5.	. 3	-240943.00	1.70		4278.99	6258,39	0.22	
- 7	-6	-240943.00	1.70		4278.99	6258.39	0.22	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.0
2	1	-325273.00	2.30	<1	5776.64	8448.83	0.30	>1
- 4	2	-240943.00	1.70	or so	4278.99	6258.39	0.22	
- 6	3	-240943.00	1.70		4278.99	6258.39	0.22	
- 8	4	-240943.00	1.70		4278.99	6258.39	0.22	

Palo n. 24

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _β <dan cmq=""></dan>	k ₈ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _∃ <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-325212.00	2,30	2.59	5777.46	8572.34	0.30	>1
3	2	-240898.00	1.70		4279.60	6349.88	0.23	
5	3	-24089B.00	1.70		4279.60	6349.88	0.23	
7	4	-240898.00	1.70		4279.60	6349.88	0.23	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
- 2	1	-325212.00	2.30	<1	5777,46	8572.34	0.30	>1
4	2	-24089B.00	1.70		4279.60	6349.88	0.23	
- 5	3	-240898.00	1.70		4279.60	6349.88	0.23	
.8	4	-240898.00	1.70		4279.60	6349.88	0.23	

Palo n. 25

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QS_{lim}=1054060.00 <daN> qp=61.31 <daN/cmq> QP_{lim}=693364.00 <daN> kp=1.17 <daN/cmq>

Verifiche in condizioni non drenate

Zp <m></m>	τ _{ii} <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc2<="" th=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
-1	1	-312389.00	2,21	2.69	5871.78	22486.70	0.40	>1
3	2	-231400.00	1,64		4349,47	16656,80	0.30	
5	.3	-231400.00	1.64		4349.47	16656.80	0.30	
7	4	-231400.00	1,64		4349,47	16656.80	0.30	

Verifiche in condizioni non drenate

Caso	cc	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 2	1	-312389.00	2,21	<1	5871.78	22486,70	0.40	>1
4	2	-231400.00	1,64		4349.47	16656.80	0.30	
6	3	-231400.00	1.64		4349,47	16656.80	0.30	
- 8	4	-231400.00	1.64		4349.47	16656.80	0.30	

Palo n. 26

Tipo palo-Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp-1.200000 <m> Lp-25.000000 <m> Wp-70685.80 <dan> D-1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _R <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	kh <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4,50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmq> QP_{lim}=157422.00 <daN> kp=1.17 <daN/cmc>

Caso CC	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
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1	1	-287771.00	2.03	2,92	6043.66	35407.20	0.50	>1
3	. 2	-213163.00	1.51		4476.78	26227.60	0.37	
5	3	-213163.00	1.51		4476.78	26227,60	0.37	
7	4	-213163.00	1,51		4476.78	26227.60	0.37	

Verifiche in condizioni non drenate

Caso	cc	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
- 2	.1	-287771.00	2.03	1.08	6043.66	35407.20	0.50	>1
- 4	2	-213163.00	1.51	(40.00)	4476.78	26227.60	0.37	
- 6	3	-213163.00	1,51		4476,78	26227.60	0.37	
8	4	-213163.00	1,51		4476.78	26227.60	0.37	

Palo n. 27

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero i COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	t _B <dan cmq=""></dan>	k ₈ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _≘ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _n <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

 QS_{lim} =472754.00 <daN> q_p =13.92 <daN/cmq> QP_{lim} =157422.00 <daN> k_p =1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	00	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-253546.00	1.79	3.32	6278.75	46247.70	0.58	>1
13	2	-187812.00	1,33		4650.92	34257.60	0.43	
.5	3	-187812.00	1,33		4650.92	34257,60	0.43	
7	4	-187812.00	1.33	m m .	4650.92	34257.60	0.43	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
2	1	-253546.00	1.79	1,22	6278.75	46247.70	0.58	>1
4	. 2	-187812.00	1,33	m m	4650.92	34257.60	0.43	
6	3	-187812.00	1.33	~~	4650.92	34257.60	0.43	
:8	4	-187812.00	1,33	100.000	4650.92	34257.60	0.43	

Palo n. 28

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Ip=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _s <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.0
1	1	-212189.00	1,50	3.96	6542.77	54473.00	0.65	>1
- 3	2	-157177.00	1.11		4846.50	40350.40	0.48	
.5	3	-157177.00	1.11		4846.50	40350.40	0.48	
7	4	-157177.00	1,11		4846.50	40350.40	0.48	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
2	. 1	-212189.00	1,50	1.46	6542.77	54473.00	0.65	>1
4	2	-157177.00	1.11		4846.50	40350.40	0.48	
- 6	3	-157177.00	1.11		4846.50	40350.40	0.48	
- 8	4	-157177.00	1.11		4846.50	40350.40	0.48	

Palo n. 29

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp om>	t ₈ <dan cmq=""></dan>	k ₈ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _∃ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <am></am>	Sic.0
1	1	-166267.00	1.18	5.06	6826.00	59745.40	0.69	>1
- 3	2	-123161.00	0,87		5056,29	44255,90	0.51	
- 5	3	-123161.00	0.87		5056,29	44255.90	0.51	
7	4	-123161.00	0.87		5056.29	44255.90	0.51	

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 2	1	-166267.00	1,18	1,87	6826.00	59745,40	0.69	>1
4	2	-123161.00	0.87		5056,29	44255.90	0.51	
- 6	. 3	-123161.00	0.87		5056.29	44255.90	0.51	
- 8	4	-123161.00	0.87		5056.29	44255.90	0.51	

Palo n. 30

Tipo palo-Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp-1.200000 <m> Lp-25.000000 <m> Wp-70685.80 <daN> D-1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _⊞ <dan cmq=""></dan>	k ₈ <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0,89	
26.00	1.76	0,15	40.00	0.89	

QS_{lim}=1054060.00 <daN> qp=61.31 <daN/cmq> QP_{lim}=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	τ _S <dan cmq=""></dan>	k _{ii} <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _b <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QFlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	8	N <dan></dan>	Ced <cm>></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
1	1	-122242.00	0.86	6,88	7077.05	61854.20	0.72	>1
- 3	. 2	-90549.90	0.64		5242.26	45818.00	0.53	
5	3	-90549.90	0.64		5242,26	45818.00	0.53	
7	4	-90549.90	0.64		5242.26	45818.00	0.53	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
- 2	1	-122242.00	0.86	2.54	7077.05	61854.20	0.72	>1
- 4	.2	-90549.90	0.64	54 Art	5242.26	4581B.00	0.53	
.6	3	-90549.90	0.64		5242.26	45818.00	0.53	
- 8	.4	-90549.90	0.64		5242.26	45818.00	0.53	

Palo n. 31

Tipo palo=Trivellato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA
Verifiche in condizioni drenate

Zp <m></m>	τ _s <dan cmq=""></dan>	k _S <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.75	0.52	
4.50	0.69	0.15	11.44	0.89	
26.00	1.76	0.15	40.00	0.89	

QSlim=1054060.00 <daN>
qp=61.31 <daN/cmq>
QPlim=693364.00 <daN>
kp=1.17 <daN/cmc>

Zp ∢m>	τ _s <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmg=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
1	1	-80635.20	0.57	10.43	7309.60	61410.20	0.72	>1
- 3	2	-59729.80	0.42		5414.52	45489.10	0.54	
- 5	3	-59729.80	0.42		5414.52	45489.10	0.54	
7	4	-59729.80	0.42	## T	5414.52	45489.10	0.54	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced. <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
2	1	-80635.20	0.57	3.85	7309.60	61410.20	0.72	>1
4	. 2	-59729.80	0.42		5414.52	45489.10	0.54	
6	3	-59729.80	0.42		5414.52	45489.10	0.54	
- 8	4	-59729.80	0.42		5414.52	45489.10	0.54	

Palo n. 32

Tipo palo=Trivellato Tipo palo=Triveliato
Rotazione testa libera
Coefficiente di efficienza=1.00
Dp=1.200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m>
Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA

Zp <m></m>	τ _≘ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QSlim=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	t _S <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.89	0.52
4.50	0.52	0.15	10.47	0.89
26.00	0.52	0.15	10.47	0.89

QS_{lim}=472754.00 <daN> qp=13.92 <daN/cmq> QP1im=157422.00 <daN> kp=1.17 <daN/cmc>

Varifishe is conditioni drenate

Caso	8	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
1	1	-46634.90	0.33	18.04	7490.34	59376.80	0.72	>1
. 3	2	-34544.40	0.24		5548.40	43982.80	0.53	
- 5	3	-34544.40	0.24		5548.40	43982.80	0.53	
7	4	-34544.40	0.24		5548.40	43982.80	0.53	

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cs></cs>	Sic.0
.2	1	-46634.90	0.33	6.66	7490.34	59376,80	0.72	>1
4	2	-34544,40	0.24		5548.40	43982,80	0.53	77
6	.3	-34544.40	0.24		5548.40	43982,80	0.53	
- 8	4	-34544.40	0.24		5548.40	43982.80	0.53	

Palo n. 33

Tipo palo=Trivellato Rotazione testa libera Coefficiente di efficienza=1.00 Dp=1,200000 <m> Lp=25.000000 <m> Wp=70685.80 <daN> D=1.00 <m> Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA Verifiche in condizioni drenate

Zp <m></m>	τ _≘ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>
1.00	0.37	0.09	4.75	0.52
4.50	0.69	0.15	11.44	0.89
26.00	1.76	0.15	40.00	0.89

QS_{11m}=1054060.00 <daN> qp=61.31 <daN/cmq> QPlim=693364.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni non drenate

Zp <m></m>	t ₈ <dan cmq=""></dan>	k _s <dan cmc=""></dan>	σ _h <dan cmq=""></dan>	k _h <dan cmc=""></dan>	
1.00	0.37	0.09	4.89	0.52	
4.50	0.52	0.15	10.47	0.89	
26.00	0.52	0.15	10.47	0.89	

QSlim=472754.00 <daN> qp=13.92 <daN/cmq> QPlim=157422.00 <daN> kp=1.17 <daN/cmc>

Verifiche in condizioni drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm>></cm>	Sic.O
1	1	-22207.30	0.16	37.88	7618.69	56881.30	0.71	>1
3	. 2	-16449.90	0.12		5643.47	42134.30	0.52	
5	3	-16449.90	0.12		5643.47	42134.30	0.52	
7	4	-16449.90	0.12		5643.47	42134.30	0.52	

Verifiche in condizioni non drenate

Caso	œ	N <dan></dan>	Ced <cm></cm>	Sic.V	T <dan></dan>	M <danm></danm>	Sps <cm></cm>	Sic.O
2	. 1	-22207.30	0.16	13.98	7618.69	56881,30	0.71	>1
4	2	-16449.90	0.12		5643.47	42134.30	0.52	
.6	3	-16449.90	0.12		5643.47	42134.30	0.52	
8	4	-16449.90	0.12		5643.47	42134.30	0.52	

Sintesi

Tipo di normativa: stati limite D.M. 18 Tipo di calcolo: statico

Dati generali della struttura

- Sito di costruzione: sconosciuto
- Edificio esistente: No
- Tipo di opera: Grande opera
- Vita nominale V_N: 100.00
- Classe d'uso: Classe III
- Coefficiente d'uso CU: 1.50 Periodo di riferimento VR: 150.00

Condizioni di carico elementari

Simbologia

CCE = Numero della condizione di carico elementare

Comm. - Commenta

Dir. = Direzione del vento

Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y

Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

Mx = Moltiplicatore della massa in dir. X My = Moltiplicatore della massa in dir. Y

Mz = Moltiplicatore della massa in dir. Z Sic. = Contributo alla sicurezza

S = a sfavore

Tipo = Tipologia di pressione vento

M = Massimizzata

E = Esterna

I = Interna

Tipo CCE = Tipo di CCE per calcolo agli stati limite Var. = Tipo di variabilità B = di base s = Coeff. di riduzione (T.A. o S.L. D.M. 96)

CCE	Comm.	Tipo CCE	Sic.	Var.		Dir. <grad></grad>	Tipo	Mx	му	Mz	Јрк	Лру	Jpz
13		1	S	~~	1.00		25	1.00	1.00	0.00	0.00	0.00	1.00

Materiali

Elenco dei criteri di progetto e delle loro principali caratteristiche meccaniche utilizzate: Sezioni generiche: 3 Solo normativa generica Solette/Platee: 3

Tipo di calcestruzzo: C40/50

Rck calcestruzzo (Rck calcestruzzo): 500.00 <daN/cmg>

Resistenza caratteristica cilindrica a compressione del calcestruzzo (Fck): 415.00 <daN/cmq>

Resistenza caratterística a trazione del calcestruzzo (Fctk): 25.17 <daN/cmq>

acc: 0.85

Yc: 1.50

Resistenza di calcolo a compressione del calcestruzzo (Fcd): 235.17 <daN/cmg> Resistenza di calcolo a trazione del calcestruzzo (Fctd): 16.78 <daN/cmq>

Acciaio

Tipo di acciaio: B450C

Tensione caratteristica di snervamento dell'acciaio (Fyk): 4500.00 <daN/cmq>

Vs: 1.15

Resistenza di calcolo dell'acciaio (Fyd): 3913.04 <daN/cmq>

Plinti/Pali: 3

Calcestruzzo

Tipo di calcestruzzo: C30/37

Rck calcestruzzo (Rck calcestruzzo): 370.00 <daN/cmq>

Resistenza caratteristica cilindrica a compressione del calcestruzzo (Fck): 307.10 <daN/cmq>

Resistenza caratteristica a trazione del calcestruzzo (Fctk): 20.59 <daN/cmq>

acc: 0.85

Yc: 1.50

Resistenza di calcolo a compressione del calcestruzzo (Fcd): 174.02 <daN/cmq> Resistenza di calcolo a trazione del calcestruzzo (Fctd): 13.73 <daN/cmg>

Acciato

Tipo di acciaio: B450C

Tensione caratteristica di snervamento dell'acciaio (Fyk): 4500.00 <daN/cmq>

ys: 1.15

Resistenza di calcolo dell'acciaio (Fyd): 3913.04 <daN/cmq>

Prove in sito

Elenco colonne stratigrafiche

Simbologia

φ' = Angolo di attrito efficace

y = Peso specifico del terreno naturale

y_{sat} = Peso specifico del terreno saturo

Class. - Classificazione

Coes, - Coesivo

E = Modulo elastico normale

E_{ed} = Modulo edometrico

G = Modulo elastico tangenziale

Spess. = Spessore

St. = Strato

Unità geotecnica - Unità geotecnica

cu = Coesione non drenata

c' = Coesione efficace

z = Profondità della superficie superiore dello strato

Colonna stratigrafica numero 1 COLONNA STRATIGRAFICA

St.	z <m></m>	Spess.	Unità geotecnica	Class.	Y <dan mc=""></dan>	Ysat <dan mc=""></dan>	φ' <grad></grad>	c' <dan mq=""></dan>	c _{ii} <dan mq=""></dan>	E <dan mq=""></dan>	G <dan mq=""></dan>	E _{ed} <dan mq=""></dan>
1	0.00	4.50	1 ARGILLE BRECCIATE DI COLORE NOCCIOLA	Coes.	THE CONTRACTOR	Toronto construction	San San San	(Antonio Control of	rouse refress	311500.00	Charles and a second	Percenta aeroles
2	4.50	==	2 ARGILLE BRECCIATE GRIGIO- AZZURRE	Coes.	1997.00	2130.00	22.23	4710.00	13090.00	533200.00	359900.00	855800.00

Le verifiche degli elementi di fondazione sono state effettuate utilizzando l'approccio 2 - Combinazione 1.

Coefficienti parziali per le azioni, per verifiche in condizioni statiche: Permanenti strutturali, sicurezza a favore $\gamma_A=1.00$;

Permanenti strutturali, sicurezza a sfavore yA = 1.30;

Permanenti non strutturali, sicurezza a favore $\gamma_A = 0.00$;

```
Permanenti non strutturali, sicurezza a sfavore yA = 1.50;
Variabili, sicurezza a favore ya = 0.00;
Variabili, sicurezza a sfavore ya - 1.50.
I coefficienti parziali per le azioni sono posti pari all'unità per le verifiche in condizioni sismiche.
Tali coefficienti sono comunque desumibili dalla tabella delle combinazioni delle CCE (Parametri di calcolo).
Coefficienti parziali per i parametri geotecnici:
Tangente dell'angolo di attrito ym = 1.00;
Coesione efficace ym = 1.00;
Coesione non drenata ym = 1.00;
Coefficienti parziali per la resistenza delle fondazioni superficiali:
Capacità portante yR = 2.30;
Scorrimento va = 1.10;
Coefficienti parziali per la resistenza delle fondazioni profonde:
Per pall infissi:
Resistenza alla base yR,b = 1.15;
Resistenza laterale in compressione yg,s = 1.15;
Resistenza laterale in trazione yR,t = 1.25;
Per pali trivellati:
Resistenza alla base y_R, b = 1.35;
Resistenza laterale in compressione yg,s = 1.15;
Resistenza laterale in trazione \gamma_R, t = 1.25;
Per pali ad elica continua:
Resistenza alla base y_R, b = 1.30;
Resistenza laterale in compressione yg,s = 1.15;
Resistenza laterale in trazione \gamma_R, t = 1.25;
Fattore di correlazione per la determinazione della resistenza caratteristica desumibile dai criteri di progetto.
```

Minimo coefficiente di sicurezza

Simbologia

```
CC = Numero della combinazione delle condizioni di carico elementari
Elem. = Elemento
Sic. = Sicurezza
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
TV = Tipo di verifica
PRFL = Flessione e pressoflessione
TAG = Taglio o altre rotture fragili
NOD - Nodi in c.a. e collegamenti in acciaio
STAB - Stabilità
CP = Capacità portante
RNP = Resistenza nel piano
RFP = Resistenza fuori piano
CIN = Cinematismi
CON - Connessioni
```

Tabella elementi e minimo coefficiente di sicurezza

Elem.	cc	TCC	TV	Sic.
Platea a quota 0	1	SLU	PRFL	0.030
Platea a quota 0	1	SLU	TAG	0.074
Plinto/Palo n. 12	2	SLE R	PRFL	2.112
Plinto/Palo n. 12	1	SLU	TAG	4.202
Sezione SEZIONE N.8		SIU	PRFL	1.015
Sezione SEZIONE N.10		SLV	TAG	>100.0

Minimo coefficiente di sicurezza:0.030